



# Design of Electric Drive Vehicle Batteries for Long Life and Low Cost

Robustness to Geographic and Consumer-Usage Variation



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NREL/PR-540-48933



# **Motivation**



### The fuel-displacement potential of EVs and PHEVs is elusive

- Cost reduction needed for significant market penetration to be achieved
- Batteries are the most expensive component of the vehicle
- Consumers expect >10 years vehicle life
  - Periodic battery replacement (e.g., every 5 years) not warranted

### Battery life and cost are intimately related

- Batteries are substantially oversized to meet power and energy performance requirements at the end-of-life
- HEVs: only 10% to 25% of energy is used
  - Toyota Prius HEV: 1.2 kWh total energy, typically < 300 Wh is used</li>
- PHEVs: only 50% of energy is used
  - Chevy Volt PHEV: ~16 kWh total energy, only 8 kWh is used

### Need to understand worst-case conditions for battery aging

- Worst-case duty cycles and environments drive the need to oversize batteries
- Systems solutions and controls can be added to overcome some of these conditions
- Life-predictive models are preferable to rules-of-thumb



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### NREL Battery Optimization & Trade-off Analysis





- Explore strategies to extend life and/or reduce cost
  - Battery sizing, thermal preconditioning and standby cooling, 2<sup>nd</sup> use, battery ownership, vehicle-to-grid...
- Missing : Life model capable of analyzing arbitrary real-world scenarios

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## **Typical Structure of Li-ion Batteries**





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Aging mechanisms in Li-ion batteries

Aging models based on accelerated testing

Robust design for long life, low cost



# Outline



# Aging mechanisms in Li-ion batteries

 Aging models based on accelerated testing

# Robust design for long life, low cost

Images: Vetter et al., "Ageing mechanisms in lithiumion batteries," *J. Power Sources*, 147 (2005) 269-281



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# **Performance Fade**



- System-level observations
  - Capacity loss
  - Impedance rise/power fade
  - Potential change
- ◆ Calendar life goal: 10 to 15 years → Effects during storage
  - Self discharge, impedance rise
- ♦ Cycle life goal: 3,000 to 5,000 deep cycles → Effects during use
  - Mechanical degradation, Li metal plating
- Where do changes occur?
  - 1. Electrode/electrolyte interface, affecting both electrode & electrolyte
  - 2. Active materials
  - 3. Composite electrode

<u>Anode:</u> graphitic carbons  $Li_{x}C_{6}$ 

<u>Cathode</u>: metal oxides  $Li_yCoO_2$ ,  $Li_y(Ni,Co,Mn,Al)O_2$ ,  $Li_yMnO_4$ ,



**Anode Aging** 



### 1. Solid/Electrolyte Interphase (SEI) Layer

- Passive protective layer, product of organic electrolyte decomposition
  SEI formation = f(a<sub>s</sub>, formation conditions)
- Mostly formed during first cycle of battery, but continues to grow at slow rate
- May penetrate into electrode & separator pores  $\rightarrow a_s \& D_e^{eff}$
- High temperature effects
  - Exothermic side reactions cause self heating
  - Film breaks down and dissolves, later precipitates
  - More-stable inorganic SEI formed, blocking Li insertion
- Low temperature effects (during charging)
  - Slow diffusion causes Li saturation at Li<sub>x</sub>C<sub>6</sub> surface
  - Slow kinetics causes increased overpotential



**Anode Aging** 



### **2. Changes of Active Material**

- Volume changes during insertion/de-insertion (~10%)
- Solvent intercalation, electrolyte reduction, gas evolution inside Li<sub>x</sub>C<sub>6</sub>

 $\rightarrow$  Stress  $\rightarrow$  Cracks

- **3. Changes of Composite Electrode**
- SEI & volume changes cause:
  - contact loss between Li<sub>x</sub>C<sub>6</sub>, conductive binder, and current collector
  - reduced electrode porosity



# **Anode Aging**





Image: Vetter et al., "Ageing mechanisms in lithium-ion batteries," J. Power Sources, 147 (2005) 269-281

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# **Cathode Aging**



### Li(Ni,Co,Al)O<sub>2</sub> Materials

- LiCoO<sub>2</sub> common cathode material
- LiNiO<sub>2</sub> structure unstable unless doped with Co or Al
- Li(Ni,Co,Al)O<sub>2</sub> volume changes are small → good cycle life
- Discharged state stable at high temperatures
- LiCoO<sub>2</sub> charged beyond 4.2 volts, Co dissolves and migrates to anode



Image: Vetter et al., "Ageing mechanisms in lithium-ion batteries," *J. Power Sources*, 147 (2005) 269-281

- Surface effects
  - SEI film formation accelerated when charged > 4.2 V, high temperatures
  - Electrolyte oxidation and LiPF<sub>6</sub> decomposition
  - Li(Ni,Co,Al)O<sub>2</sub> source  $O_2 \rightarrow$  rock-salt structure with low  $\sigma$ , D<sub>s</sub>
  - Gas evolution



# **Cathode Aging**





Source: Vetter et al., "Ageing mechanisms in lithium-ion batteries," *J. Power Sources*, 147 (2005) 269-281



Source: Wohlfahrt-Mehrens et al., "Aging mechanisms of lithium cathode materials," *J. Power Sources*, 127 (2004) 58-64

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**Summary of Aging** 



# Aging influenced by:

- Both <u>high</u> and low SOC
- High temperatures
- Low temperatures during charging
- Surface chemistry (anode and cathode)
- Phase transitions/structural changes (cathode)



# Outline





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# **How Can We Predict Battery Life?**



### Accelerated storage tests

- Relatively well understood
- Mechanism: SEI growth, Li loss
- Model:
  - t<sup>1</sup>/<sub>2</sub> time dependency
  - Arrhenius T dependency

### Accelerated cycling tests

- Poorly understood
- Mechanism: Mechanical stress & fracture (may be coupled with SEI fracture+regrowth)
- Model:
  - Typical t or N dependency
  - Often correlated log(# cycles) with ΔDOD





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### Accelerated Tests May Not Predict Correct Real-Time Result

• Cycle-life study for geosynchronous satellite battery shows possible change in degradation mechanisms depending upon how frequently the battery is cycled



Important for a life-predictive model to accurately capture both cycling conditions. Prediction based on accelerated cycling results would over-estimate life!

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# **How Can We Predict Battery Life?**



#### Accelerated storage tests

- Relatively well understood
- Mechanism: SEI growth, Li loss
- Model: (e.g., DOE TLVT)
  - t<sup>1</sup>/<sub>2</sub> time dependency
  - Arrhenius T dependency

### Accelerated cycling tests

- Poorly understood
- Mechanism: Mechanical stress & fracture (may be coupled with SEI fracture + regrowth)
- Model: (e.g., VARTA)
  - Typical t or N dependency
  - Often correlated log(# cycles) with  $\Delta DOD$

#### Real-world cycling & storage

- Poorly understood
- NREL model extends previous work by enabling extrapolation beyond tested conditions







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# Life Modeling Approach

NCA datasets fit with empirical, yet physically justifiable formulas

2.6

\*K. Smith, T. Markel, A. Pesaran, "PHEV Battery Trade-off Study and Standby Thermal Control," 26<sup>th</sup> International Battery Seminar & Exhibit, Fort Lauderdale, FL, March, 2009.



# Predictive model that considers effects of real-world storage and cycling scenarios

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## Fitting of NCA/Graphite Baseline Life Model to Lab Data



- 1. Resistance growth during storage
  - Broussely (Saft), 2007:
    - T = 20°C, 40°C, 60°C
    - SOC = 50%, 100%
- 2. Resistance growth during cycling
  - ◆ Hall (Boeing), 2005-2006:
    - DoD = 20%, 40%, 60%, 80%
    - End-of-charge voltage = 3.9, 4.0, 4.1 V
    - Cycles/day = 1, 4
- 3. Capacity fade during storage
  - Smart (NASA-JPL), 2009
    - T = 0°C, 10°C, 23°C, 40°C, 55°C
  - Broussely (Saft), 2001
    - V = 3.6V, 4.1V
- 4. Capacity fade during cycling
  - Hall/Boeing, 2005-2006: (same as # 2 above)

- 30 different tests
- >\$1M in test equipment
- 1-4 years duration

### → <u>Expensive!!</u>

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### Model Comparison with Vehicle Battery Laboratory Data



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#### Aging mechanisms in ...for the vehicle systems Li-ion batteries integrator Capacity Temperature Relative 68.0 Effects Aging models based on 0.8 accelerated testing 0.75 Time (years) PHEV 20, Opportunity Charge Ծ **Duty-cycle** 30 40 50 Maximum Daily ASOC (% Robust design for long Effects <del>ک</del> 25 ື້ອ 20 life, low cost 60 40 Aaximum Daily ASOC (%

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# **Impact of Geographic Region**



- ◆ Example: PHEV20 battery, 1 cycle/day, △DoD=0.54, various climates
  - NREL Typical Meteorological Year data used to simulate ambient conditions for each city



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# Impact of Thermal Management in Phoenix



- Cooling strategies investigated:
  - 1. No cooling
  - 2. Air cooling
    - h = 15 W/m<sup>2</sup>K
    - T<sub>inf</sub> = 30°C (passenger cabin air)
  - 3. Liquid cooling
    - h = 80 W/m<sup>2</sup>K
    - T<sub>inf</sub> = 20°C (refrigerated ethylene glycol)
  - 4. Air cooling, with low impedance cell
    - h = 15 W/m<sup>2</sup>K
    - T<sub>inf</sub> = 30°C (passenger cabin air)
    - Use of a high power/low impedance cell reduces heat generation rates by 50%



#### Other assumptions used to generate temperature profiles for the various cases:

- CD and CS heat generation rates chosen to represent average driving (between US06 and city driving measurements taken in the NREL lab)
- Two trips per day
  - 8:00-8:30 a.m. morning commute
  - 5:00-5:30 p.m. evening commute
- 34 mph average speed



### **Impact of Thermal Management in Phoenix**



- Battery life differs depending on how the battery is cooled
  - Example below: PHEV20, 1 cycle/day at  $\Delta DoD=0.54$



Liquid cooling is very effective at reducing peak temperatures as well as lowering the average daily temperature during the summer. It is uncertain whether the extra expense is warranted.

Use of a low impedance cell reduces heat generation rates while driving, but does not lower temperature due to ambient exposure. This higher power cell costs more upfront, but does appear to have longer life.

#### Liquid cooling

Air cooling, low impedance cell Air cooling

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### **\$\$ Value of Thermal Management in** Phoenix



- Slower degradation saves battery cost by allowing smaller battery to meet end-of-life performance requirements
  - All values below are compared to a baseline battery pack designed for 1 cycle/day at 30°C.



No thermal management increases baseline battery cost by 5% to 10%.

Slower fade rate of low impedance cell does not justify the upfront cost of extra power in this design.

Effective thermal management decreases baseline pack costs by 5%.

• PHEV40 shows most benefit from liquid-cooled system that lowers daily average temperatures during the summer.



**Impact of Duty-Cycle** 



#### Two scenarios with similar petroleum displacement 1. PHEV 20, opportunity charge 227 GPS-measured speed traces 2. PHEV 40, nightly charge **Vehicle Simulation** Resistance Growth (%) • PHEVxx PHEV 20, Opportunity Charge 200 • Charging frequency PHEV40, Nightly Charge Battery 150 *duty-cycle* 100 **Battery Life Simulation** • 15 years, 30°C 0 10 20 30 40 50 60 70 80 Maximum Daily ∆SOC (%) Battery wear outcome 25 Capacity Fade (%) 20 Frequent deep 15 cycling can lead to 10 early failure. 10 30 70 0 20 50 60 80 40 Maximum Daily ∆SOC (%)

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# Conclusions



- Battery degradation is complex
  - Stressors: Chemical, electrochemical, thermal, and mechanical
  - Physics-based models do not yet capture all relevant mechanisms
- Aging tests are expensive and time consuming
  - Accelerated tests do not always reveal real-time fade rates!
  - Models useful for proper interpretation and extrapolation
    - Present: Semi-empirical, requires large test matrix
    - Future: Physics-based, requires fewer tests + useful as battery design tool
- Robust design tools require accurate battery life prediction under multiple scenarios
  - Knowledge must be efficiently passed from electrochemists to vehicle systems engineers
- Significant cost savings may be achieved through streamlined battery life verification methods and robust design





- Funding provided by DOE Office of Vehicle Technologies
  - Dave Howell, Energy Storage Program Manager
- Battery aging data and discussion
  - Jeffrey Belt, Idaho National Laboratory
  - Loïc Gaillac and Naum Pinsky, Southern California Edison
  - John C. Hall, Boeing
  - Marshall Smart, NASA-Jet Propulsion Laboratory