



3D Thermal and Electrochemical Model for Spirally Wound Large Format Lithium-ion Batteries

218th ECS Meeting, Las Vegas, NV

Oct 14, 2010

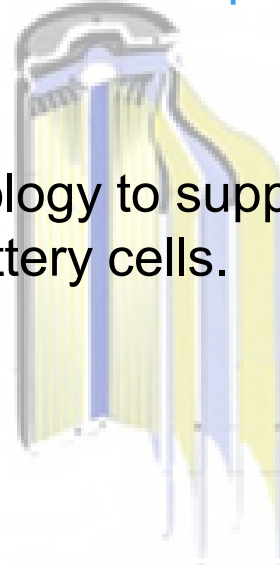
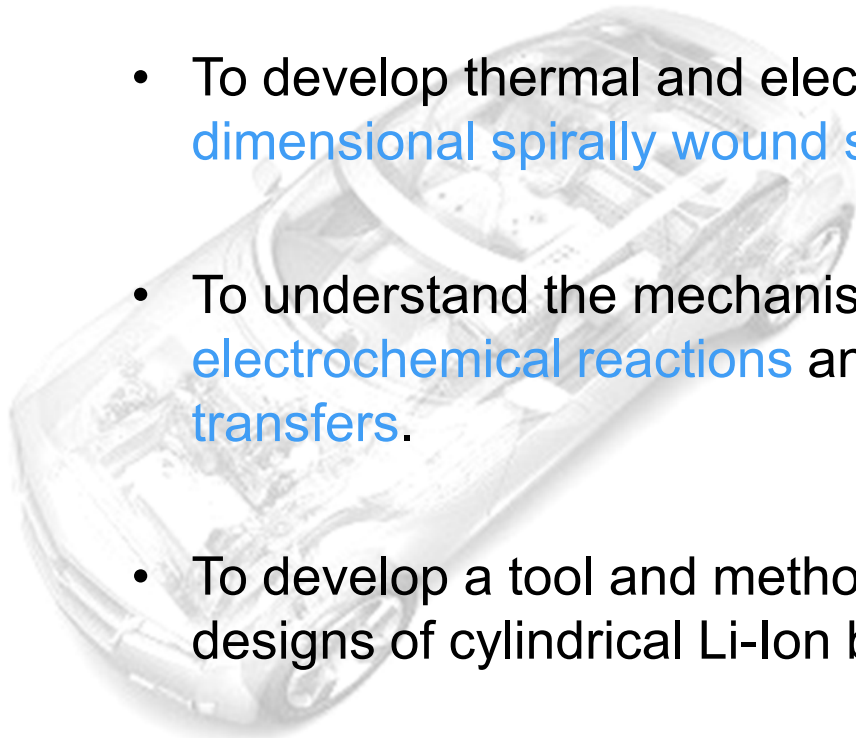
Kyu-Jin Lee*, Gi-Heon Kim, Kandler Smith

NREL/PR-5400-49795

Objectives of this Study

Behaviors of spirally wound large format Li-Ion batteries are affected by macroscopic designs of cells.

- To develop thermal and electrochemical models resolving **3 dimensional spirally wound structures** of cylindrical cells.
- To understand the mechanisms and interactions between **local electrochemical reactions** and **macroscopic heat and electron transfers**.
- To develop a tool and methodology to support macroscopic designs of cylindrical Li-Ion battery cells.

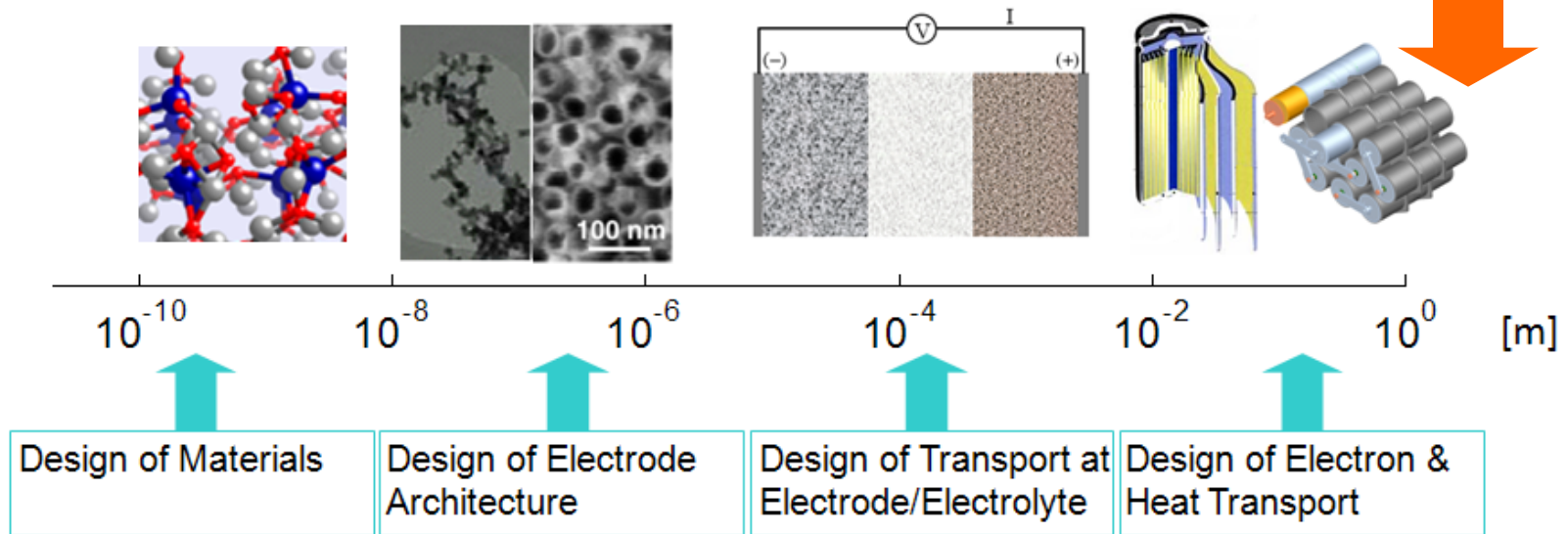


Multi-Scale Physics in Li-Ion Battery

Requirements & Resolutions

“Requirements” are usually defined in a macro-scale domain and terms

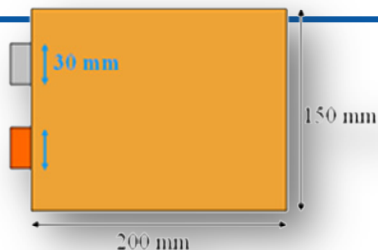
*Performance
Life
Cost
Safety*



- Wide range of length and time scale physics
- Design improvements required at different scales
- Need for better understanding of interaction among varied scale physics

Multi-Physics Interaction

- Previous study

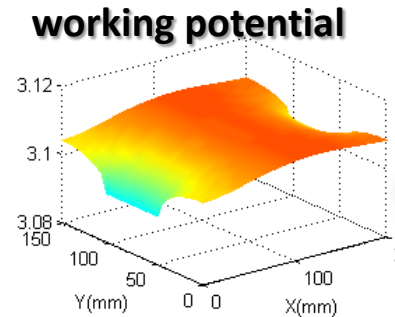
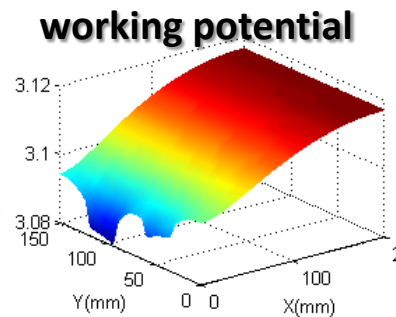


Comparison of two 40 Ah flat cell designs

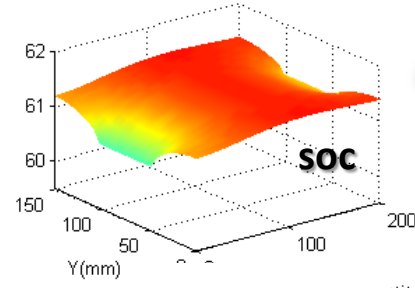
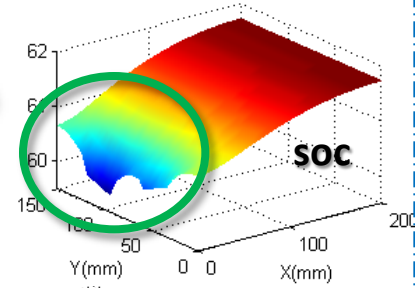
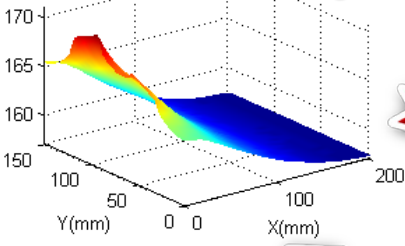


- Larger over-potential promotes faster discharge reaction
- Converging current causes higher potential drop along the collectors

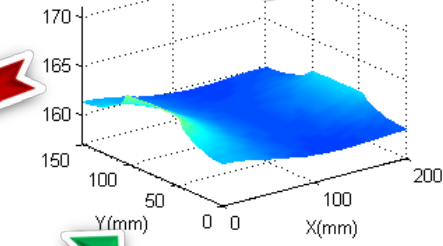
This cell is cycled more uniformly, can therefore use less active material (\$) and has longer life.



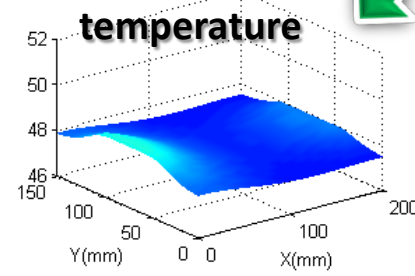
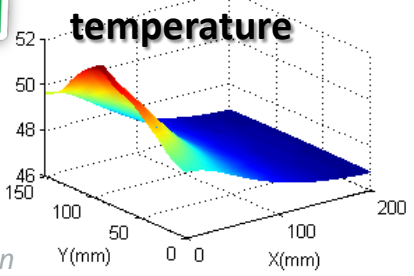
transfer current generation



transfer current generation



- High temperature promotes faster electrochemical reaction
- Higher localized reaction causes more heat generation



2 min
5C discharge

Porous Electrode Model

Charge Transfer Kinetics at Reaction Sites

$$j^{Li} = a_s i_o \left\{ \exp \left[\frac{\alpha_a F}{RT} \eta \right] - \exp \left[- \frac{\alpha_c F}{RT} \eta \right] \right\}$$

$$i_o = k(c_e)^{\alpha_a} (c_{s,max} - c_{s,e})^{\alpha_a} (c_{s,e})^{\alpha_c} \quad \eta = (\phi_s - \phi_e) - U$$

Species Conservation

$$\frac{\partial c_s}{\partial t} = \frac{D_s}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial c_s}{\partial r} \right)$$

$$\frac{d(\varepsilon_e c_e)}{dt} = \nabla \cdot (D_e^{eff} \nabla c_e) + \frac{1-t_+^o}{F} j^{Li} - \frac{\mathbf{i}_e \cdot \nabla t_+^o}{F}$$

Charge Conservation

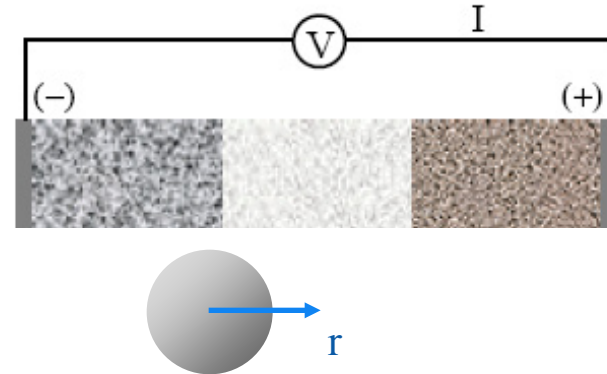
$$\nabla \cdot (\sigma^{eff} \nabla \phi_s) - j^{Li} = 0$$

$$\nabla \cdot (\kappa^{eff} \nabla \phi_e) + \nabla \cdot (\kappa_D^{eff} \nabla \ln c_e) + j^{Li} = 0$$

Energy Conservation

$$\rho c_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) + q'''$$

$$q''' = j^{Li} \left(\phi_s - \phi_e - U + T \frac{\partial U}{\partial T} \right) + \sigma^{eff} \nabla \phi_s \cdot \nabla \phi_s + \kappa^{eff} \nabla \phi_e \cdot \nabla \phi_e + \kappa_D^{eff} \nabla \ln c_e \cdot \nabla \phi_e$$



- Pioneered by Newman group (*Doyle, Fuller, and Newman 1993*)
- Captures *lithium diffusion dynamics and charge transfer kinetics*
- Predicts *current/voltage response* of a battery
- Provides design guide for thermodynamics, kinetics, and transport across electrodes

- Difficult to resolve *heat and electron current transport* in large cell systems

Porous Electrode Model

Charge Transfer Kinetics at Reaction Sites

$$j^{Li} = a_s i_o \left\{ \exp \left[\frac{\alpha_a F}{RT} \eta \right] - \exp \left[- \frac{\alpha_c F}{RT} \eta \right] \right\}$$

$$i_o = k(c_e)^{\alpha_a} (c_{s,max} - c_{s,e})^{\alpha_a} (c_{s,e})^{\alpha_c} \quad \eta = (\phi_s - \phi_e) - U$$

Species Conservation

$$\frac{\partial c_s}{\partial t} = \frac{D_s}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial c_s}{\partial r} \right)$$

$$\frac{d(\varepsilon_e c_e)}{dt} = \nabla \cdot (D_e^{eff} \nabla c_e) + \frac{1-t_+^o}{F} j^{Li} - \frac{\mathbf{i}_e \cdot \nabla t_+^o}{F}$$

Charge Conservation

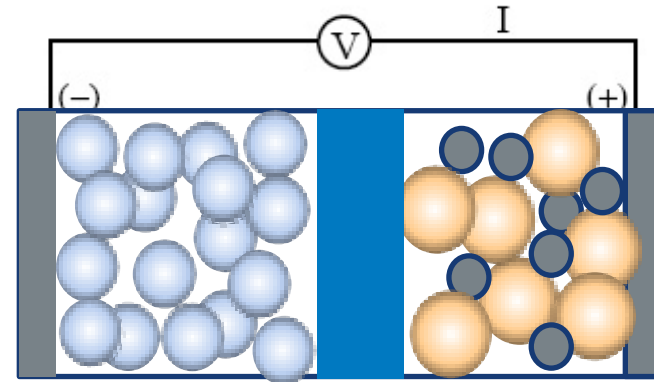
$$\nabla \cdot (\sigma^{eff} \nabla \phi_s) - j^{Li} = 0$$

$$\nabla \cdot (\kappa^{eff} \nabla \phi_e) + \nabla \cdot (\kappa_D^{eff} \nabla \ln c_e) + j^{Li} = 0$$

Energy Conservation

$$\rho c_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) + q'''$$

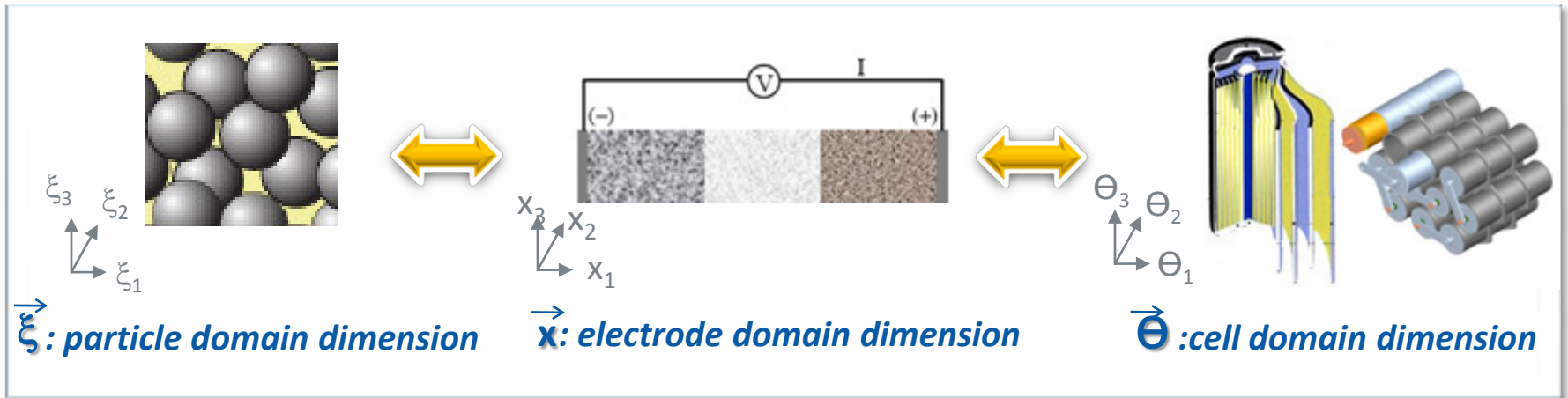
$$q''' = j^{Li} \left(\phi_s - \phi_e - U + T \frac{\partial U}{\partial T} \right) + \sigma^{eff} \nabla \phi_s \cdot \nabla \phi_s + \kappa^{eff} \nabla \phi_e \cdot \nabla \phi_e + \kappa_D^{eff} \nabla \ln c_e \cdot \nabla \phi_e$$



- Pioneered by Newman group (Doyle, Fuller, and Newman 1993)
- Captures *lithium diffusion dynamics and charge transfer kinetics*
- Predicts *current/voltage response* of a battery
- Provides design guide for thermodynamics, kinetics, and transport across electrodes

- Difficult to resolve **heat** and **electron current** transport in large cell systems

Multi-Scale Multi-Dimension (MSMD) Model



- Introducing separate computational domains for corresponding length scale physics
- Geometry decoupling between the domains
- Using independent coordinate systems for each domain
- Two-way coupling of solution variables using multi-scale model schemes
- Selectively resolve higher spatial resolution for smaller characteristic length scale physics
- Achieve high computational efficiency
- Provide flexible & expandable modularized framework

Large Cell Design Issues

Prismatic cell



- *Stacking electrodes coated on metal current collectors*
- *Less efficient manufacturing processes for mass production*

Cylindrical cell



- *Rolling electrodes coated on metal current collectors*
- *Well established manufacturing process for small batteries*
- *More difficulties for large cell design (cf. **tap design**, heat management, etc)*

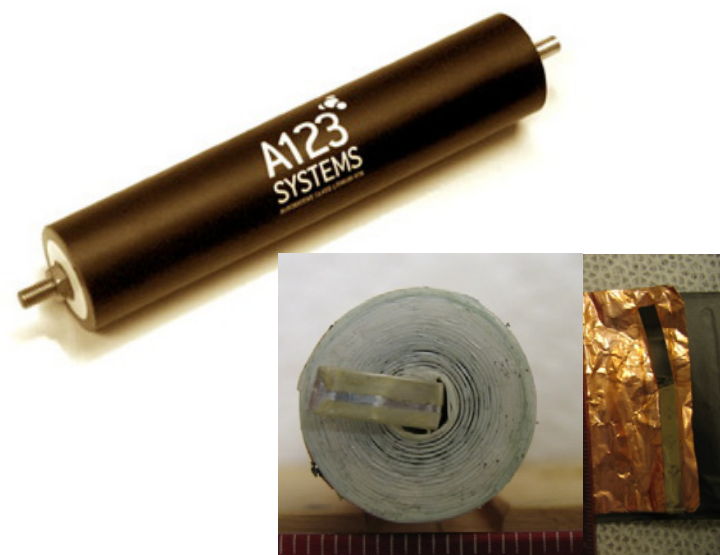
Large Cell Design Issues

Prismatic cell



- *Stacking electrodes coated on metal current collectors*
- *Less efficient manufacturing processes for mass production*

Cylindrical cell

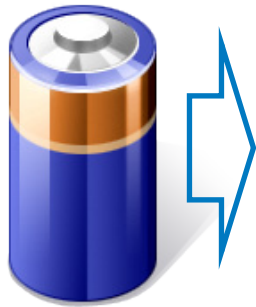


- *Rolling electrodes coated on metal current collectors*
- *Well established manufacturing process for small batteries*
- *More difficulties for large cell design (cf. **tap design**, heat management, etc)*

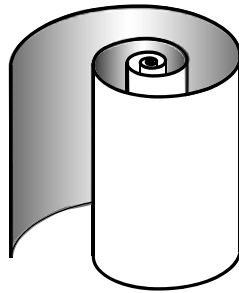
Previous Development of Wound Cell Model

Applicable to continuous tab design

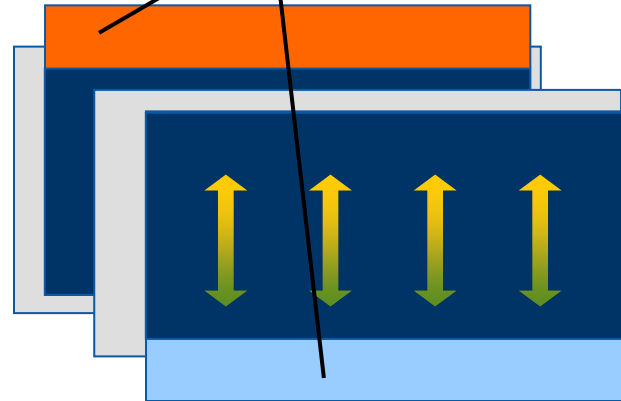
Extended Foil



Cylindrical cell



Unwinding jellyrolls



continuous tab design



Axisymmetric assumption

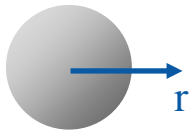
Sub-model choice for spirally wound continuous tab cells

- Previous study

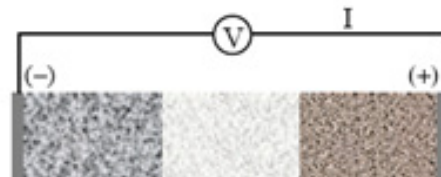
: particle domain sub-model

: electrode domain sub-model

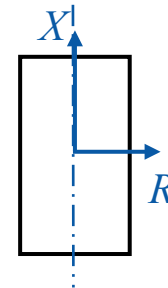
: cell domain sub-model



1D spherical particle representation model



1D porous electrode model

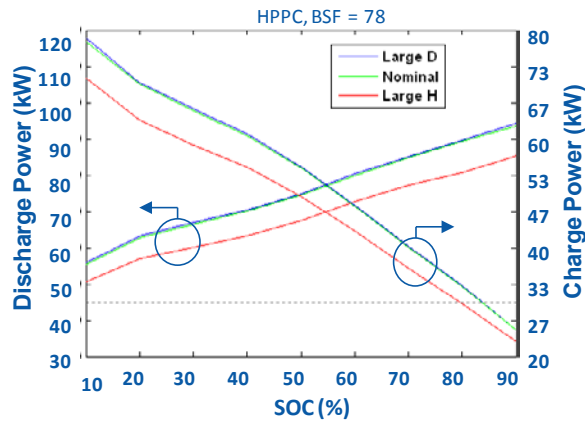


2D axisymmetric cell model

Tab-less Wound Cell Design Evaluation

Effects of “Aspect Ratio” of a Cylindrical Cell - Previous study

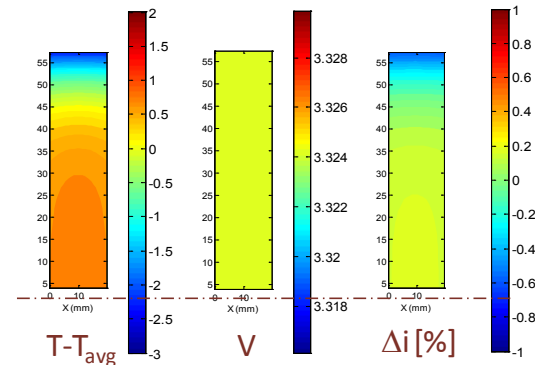
10s pulse power capability comparison



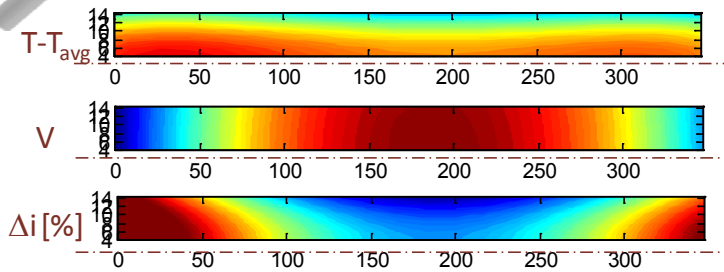
- Large H design has almost 10% less power capability.

9 min 5C discharge

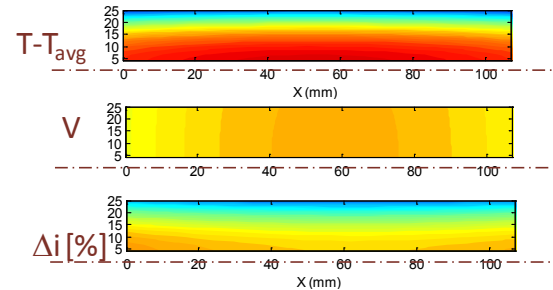
Large D D[mm]: 115 H[mm]: 20



Large H D[mm]: 14 H[mm]: 350

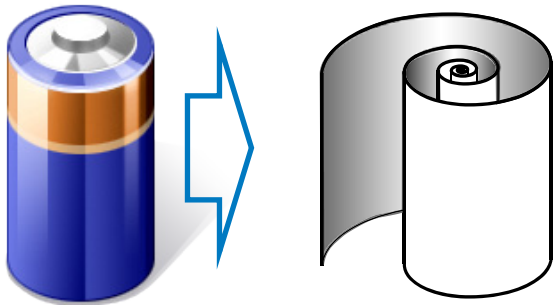


Nominal D[mm]: 50 H[mm]: 107



Present Study

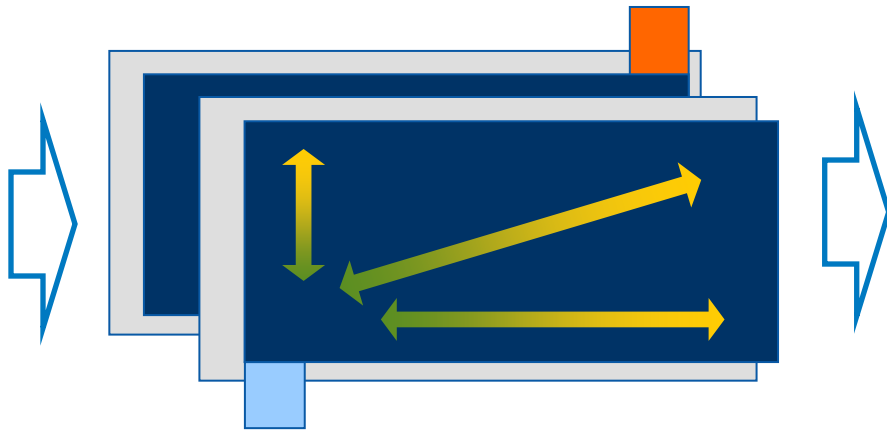
Tab configuration: number & size



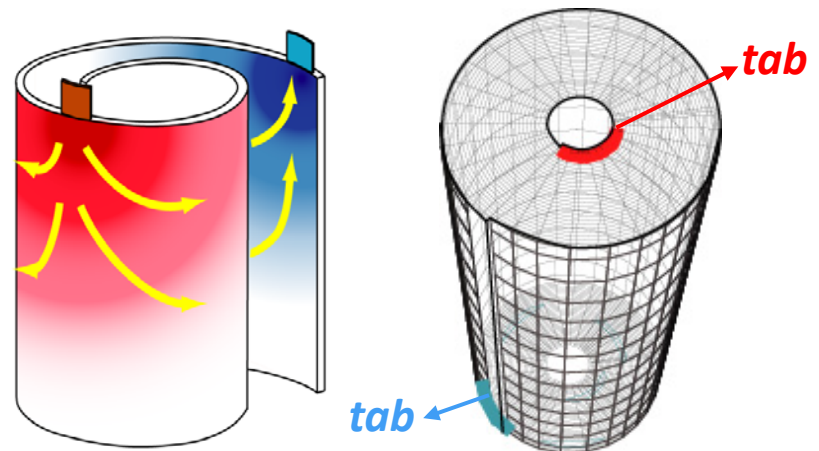
Cylindrical cell

Unwinding jellyrolls

- 2D axisymmetric model is not applicable to a wound cell with a finite number of current tabs where lateral electric current is not negligible in current collector foils.
- Geometries and materials of electric current paths in spirally wound layer structure should be properly resolved.



Current flows along the winding direction

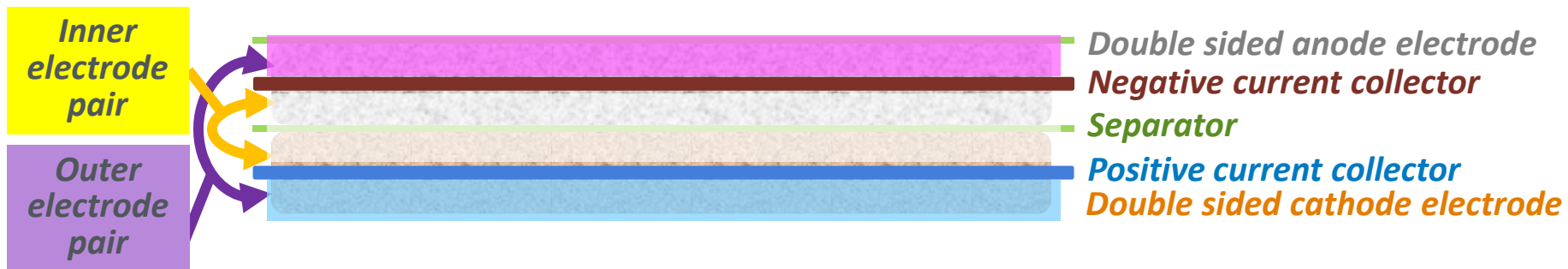


3 dimensional spiral wound geometry

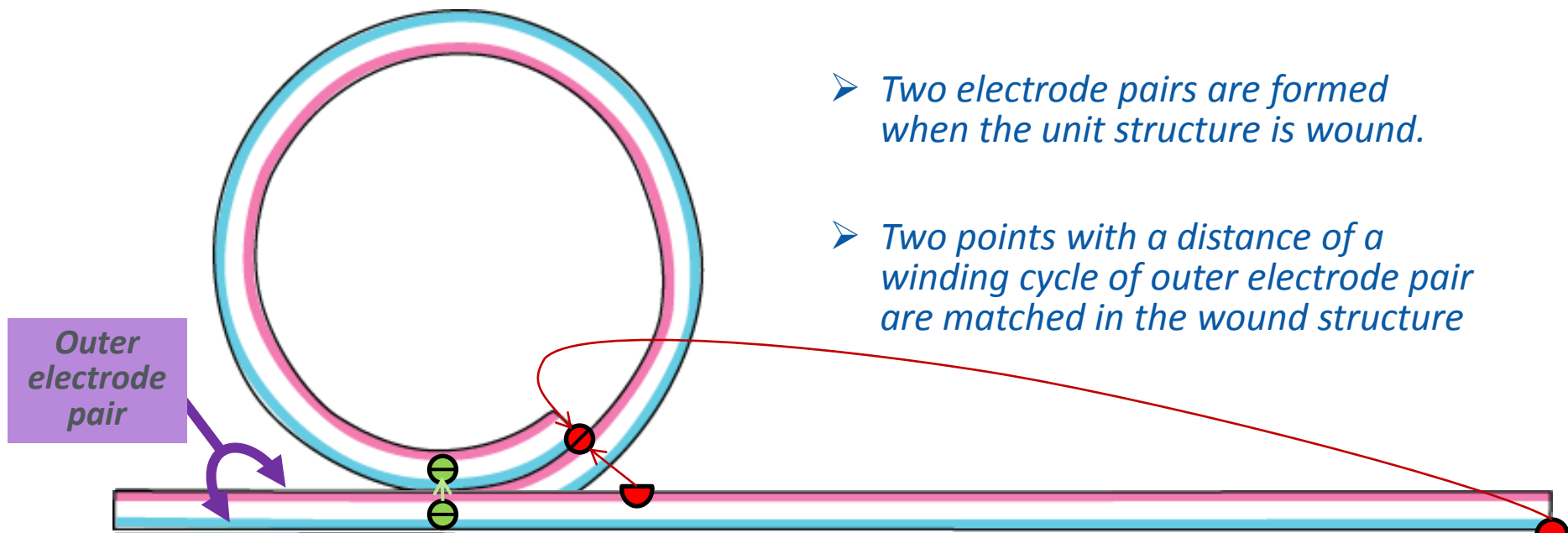
New Development of Cell Domain Model

Spirally Wound Cell Model:

Unit structure: Double Paired Electrodes on Single-Paired Current Collectors

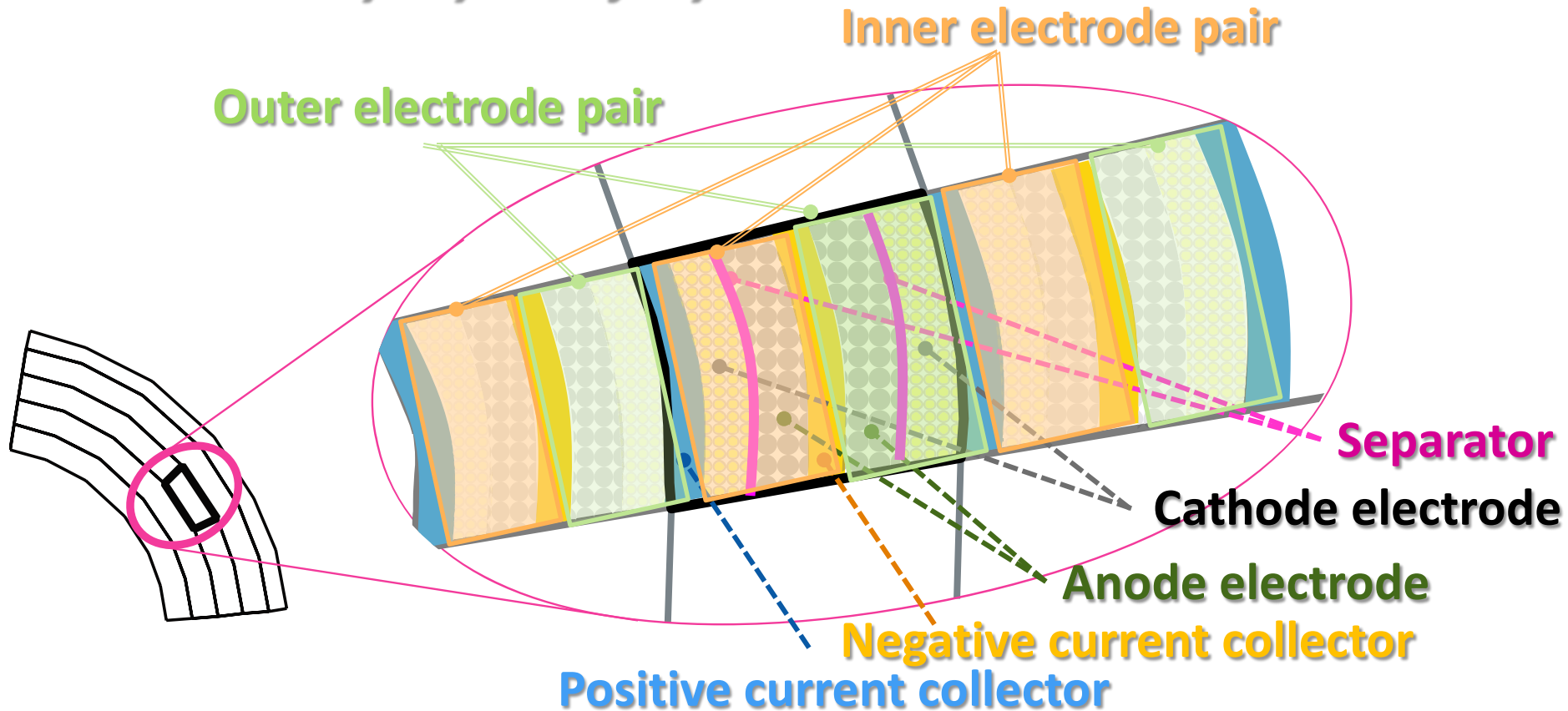


Winding: Alternating Radial Placement of Double Paired-Electrodes



Spiral cell structures

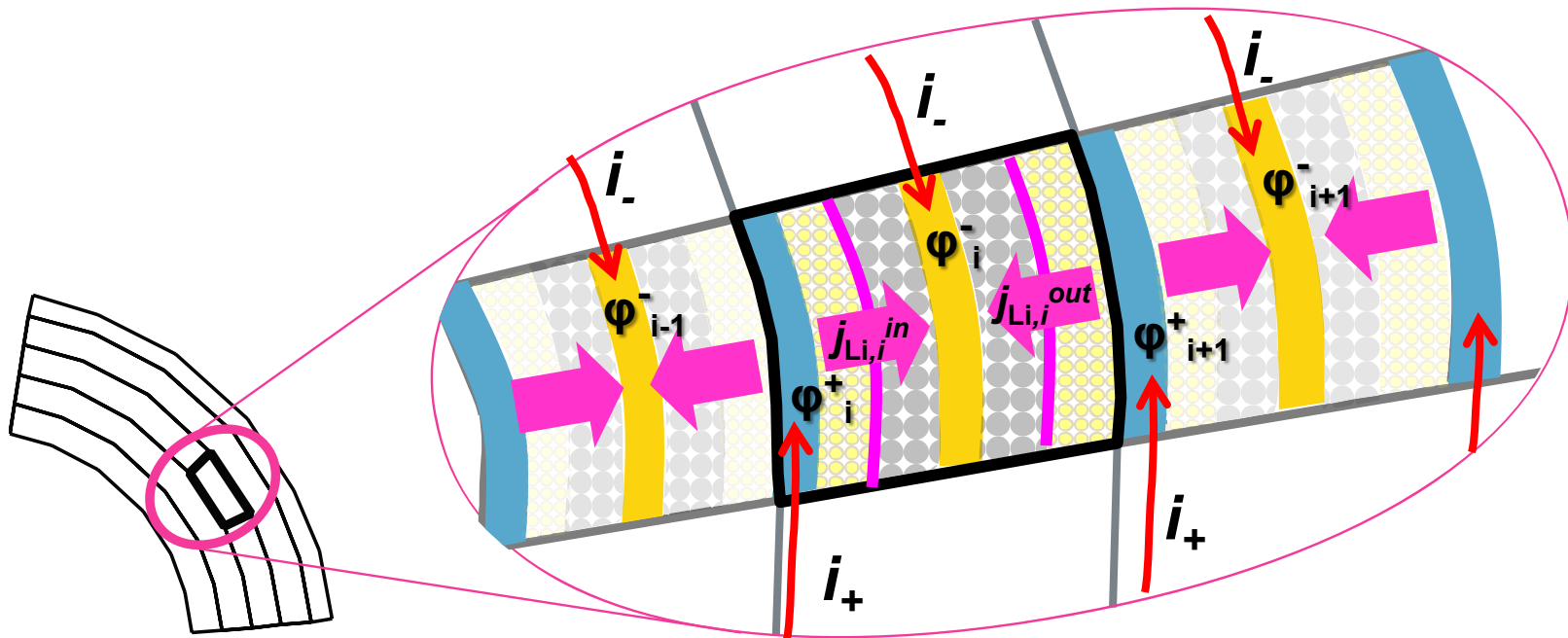
Alternatively layered jelly roll



A current collector has two electrode pairs in both sides.

Spiral cell structures

Non-uniform electrical potential along current collectors
Non-uniform charge transfer reaction

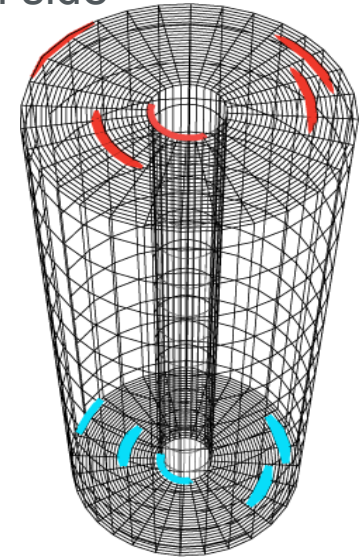
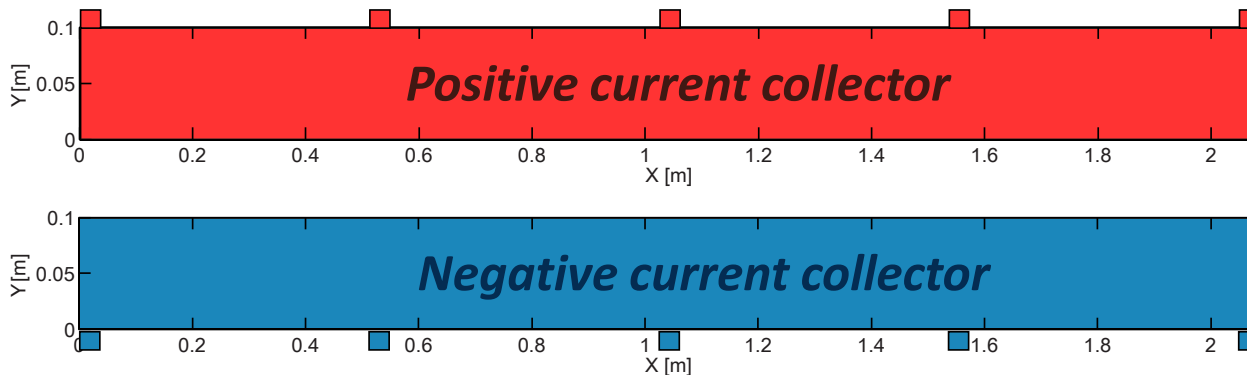


We cannot expect uniform potential along the current collectors due to inevitable electric current in winding direction.

Modeling case

- ✓ Diameter 40mm, inner diameter 8mm, height 100 mm form factor
- ✓ Positive tabs on the top side, negative tabs on the bottom side
- ✓ 10 Ah capacity

Tab locations for 5 tab case



Tab configuration of each electrode pairs

5C constant current discharge

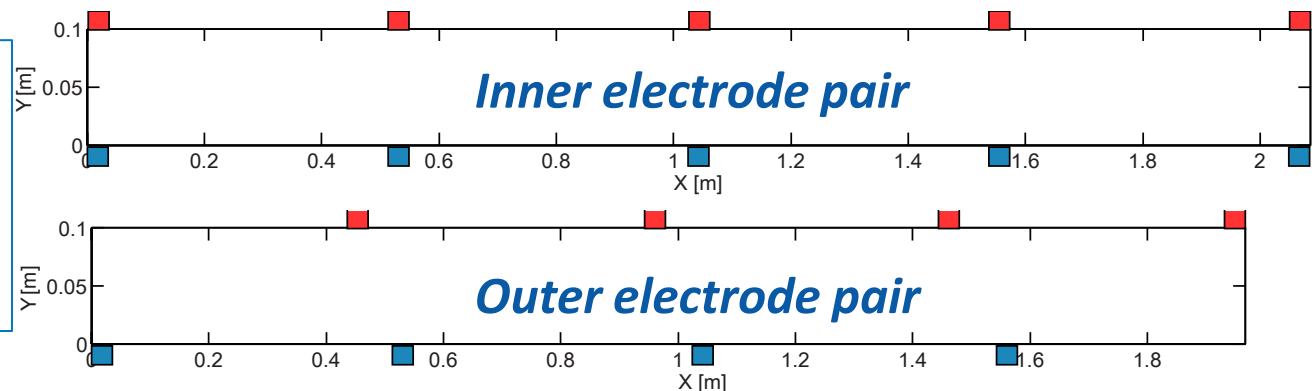
$\text{soc}_{ini} = 90\%$

Natural convection :

$h_{inf} = 5 \text{ W/m}^2\text{K}$

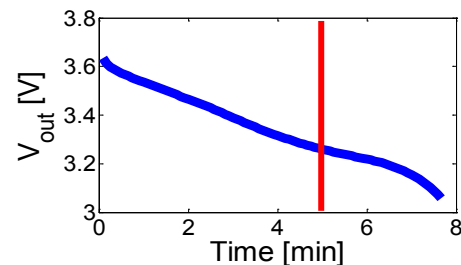
$T_{amb} = 25^\circ\text{C}$

$T_{ini} = 25^\circ\text{C}$

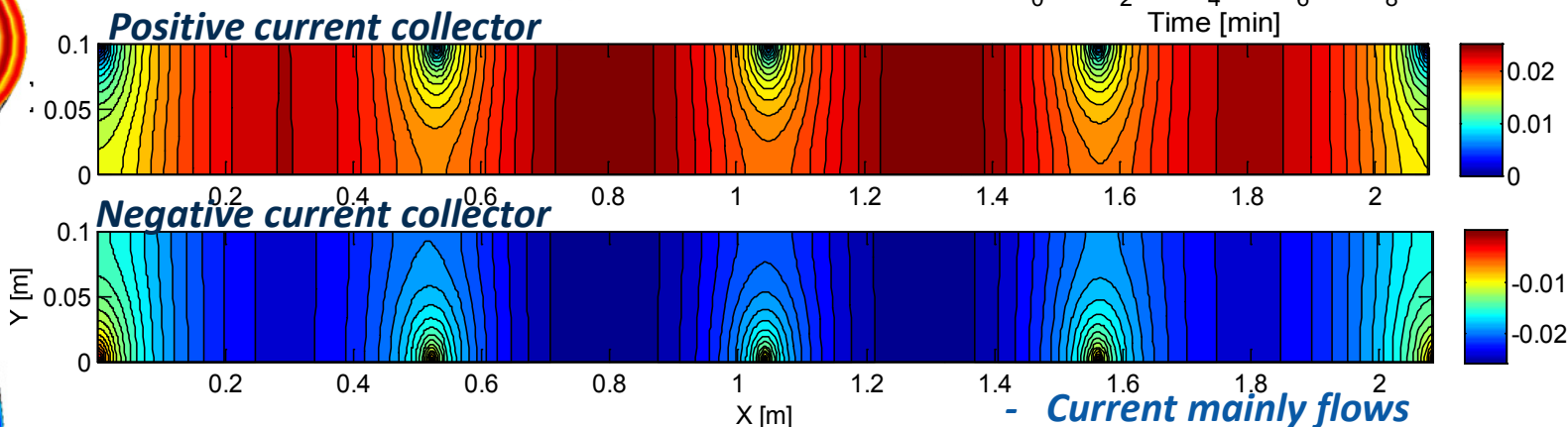
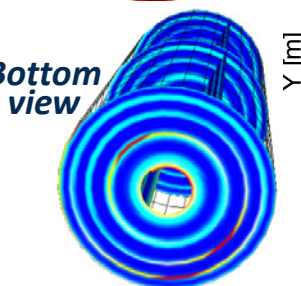
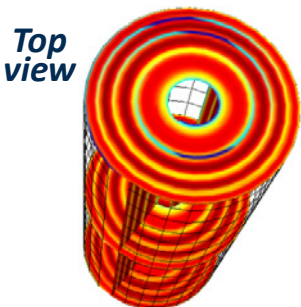


Modeling results

- 5 tabs in each current collector
- 5C discharge for 5 min

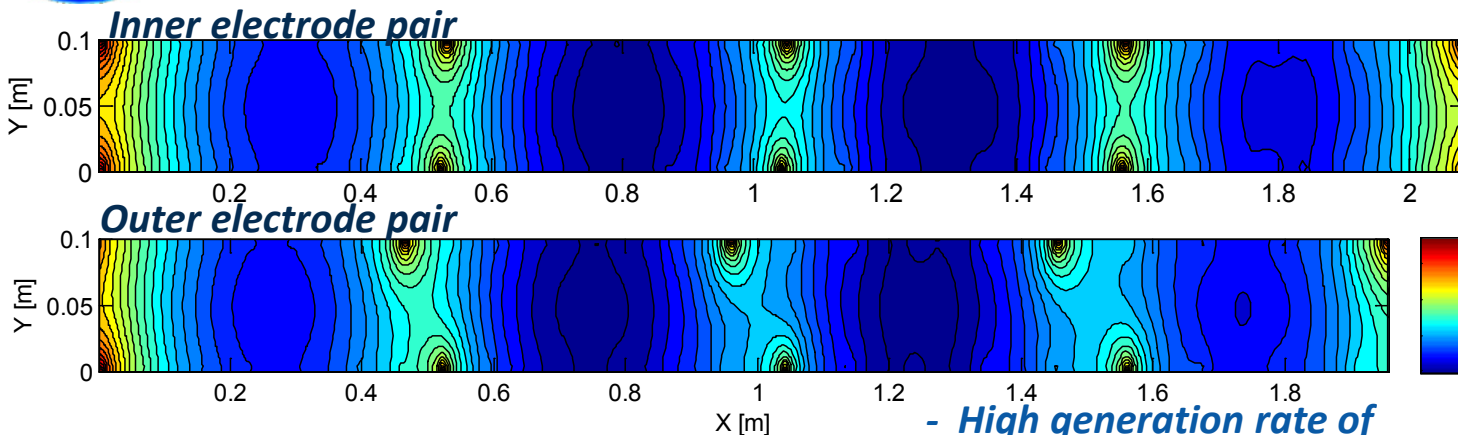


Electric potential

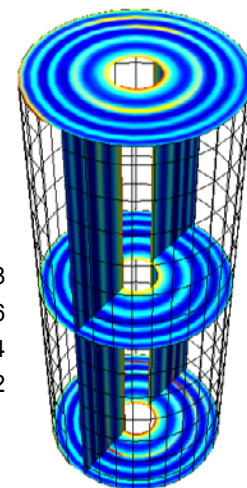


- Current mainly flows in the winding direction

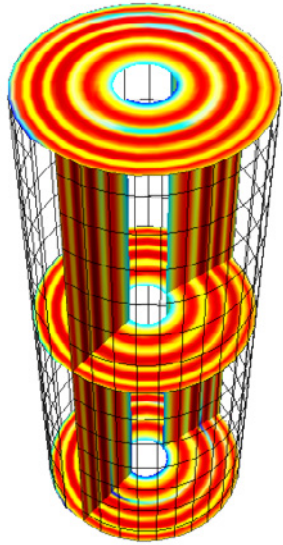
Electrochemical reaction rate



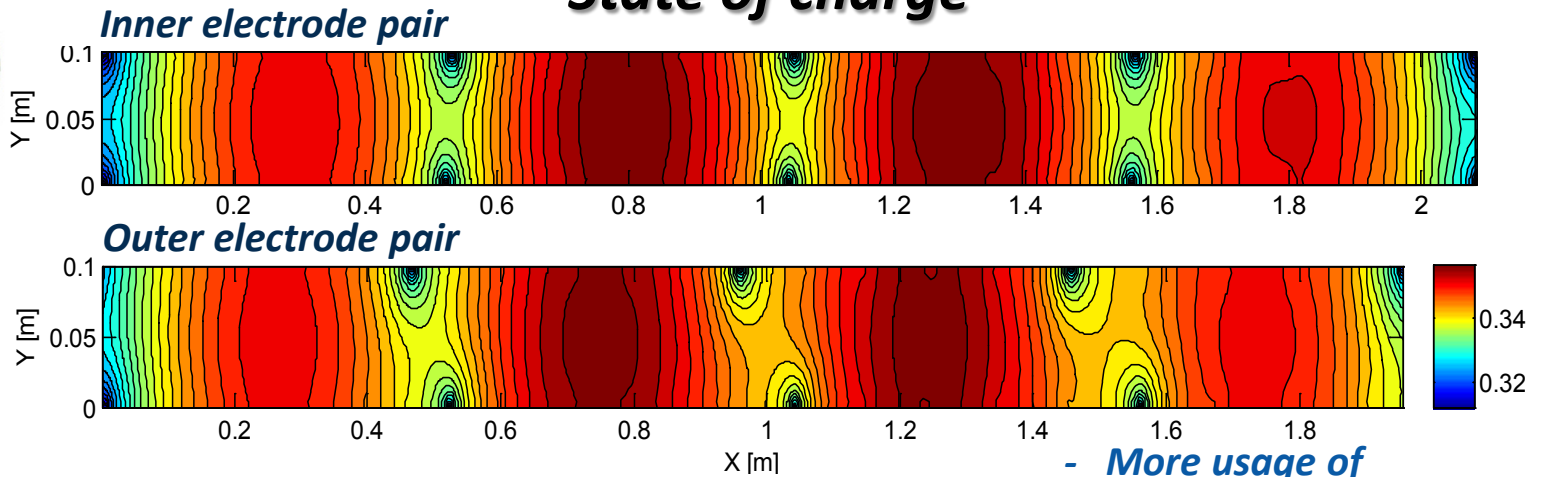
- High generation rate of transfer current near tabs



Modeling results

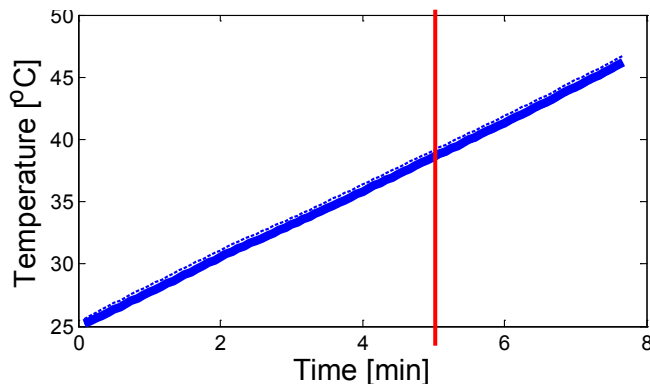
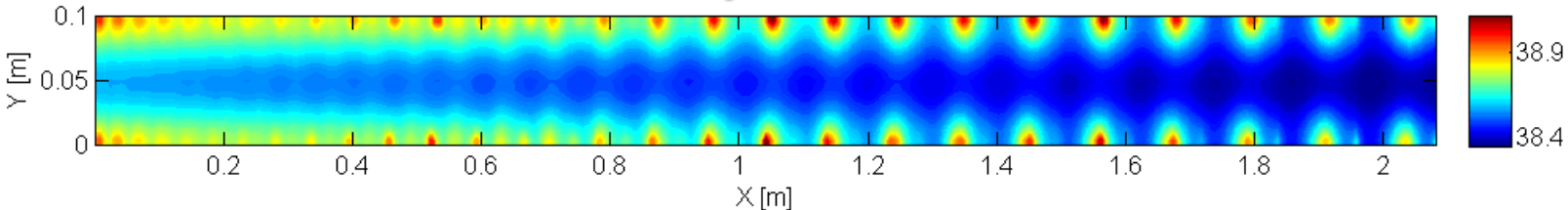


State of charge

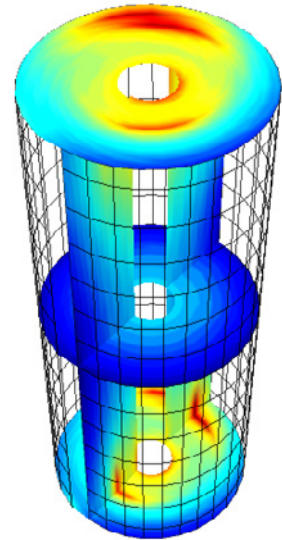


- More usage of electrode near tabs

Temperature



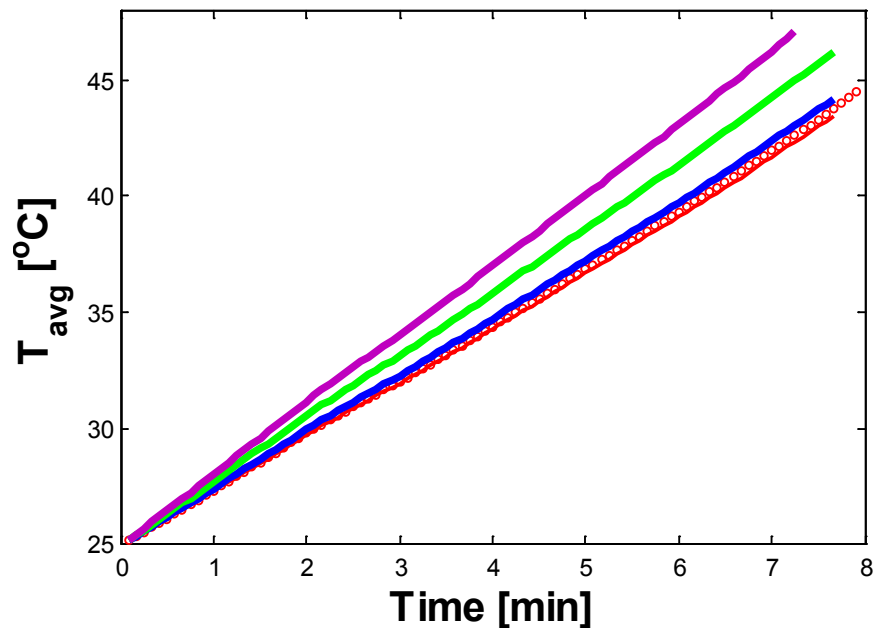
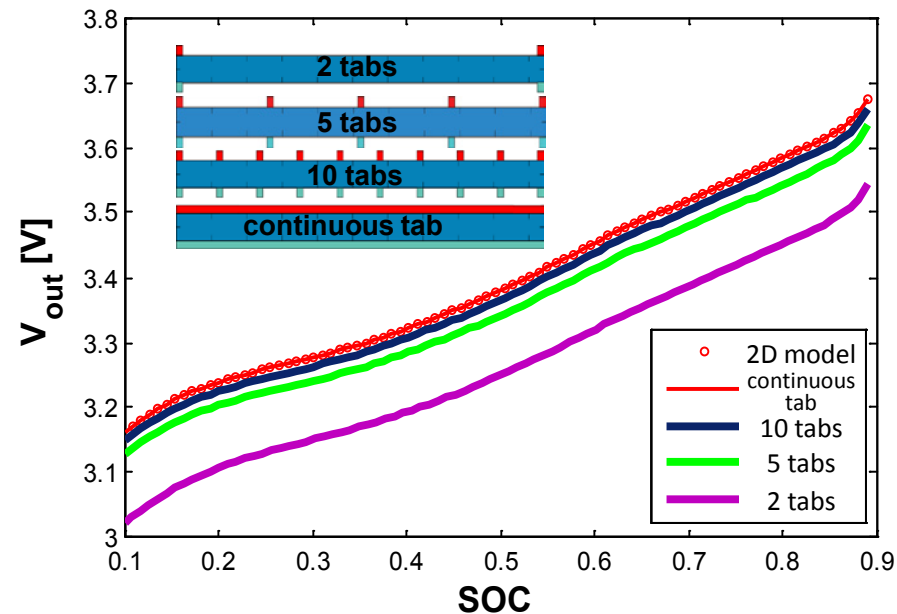
- High rate discharge with a moderate heat transfer condition
- Heat generation dominates temperature distribution in the system.
- Temperature difference in the system is relatively small yet.



Modeling results

Parametric study

- Different tab numbers (2,5,10 and continuous tab) on cell performance
- 10 Ah capacity, 5C discharge



$soc_{ini} = 90\%$
Natural convection :
 $h_{inf} = 5 \text{ W/m}^2\text{K}$
 $T_{amb} = 25^\circ\text{C}$
 $T_{ini} = 25^\circ\text{C}$

Cells with fewer tabs ...

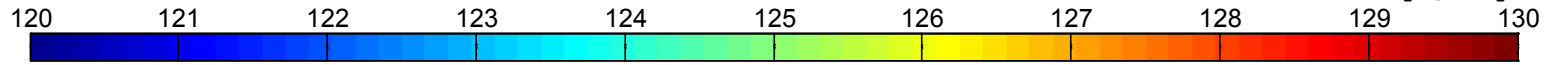
- **lower output voltage**
- **higher average temperature**

Electrochemical reaction rate comparison

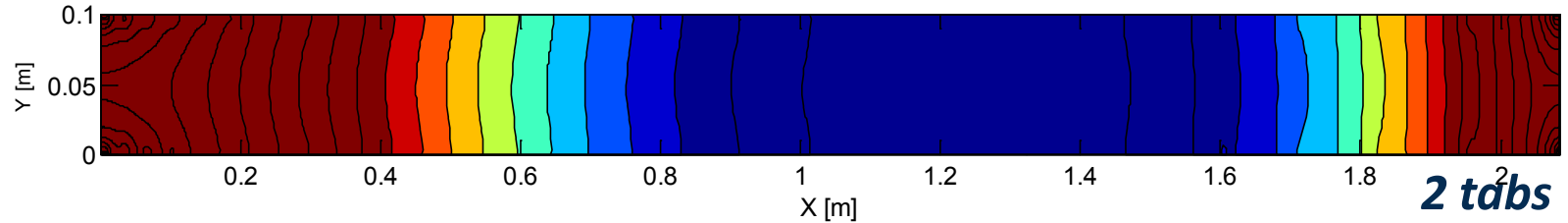
in the inner electrode pair at 5 min

i'' [A/m²]

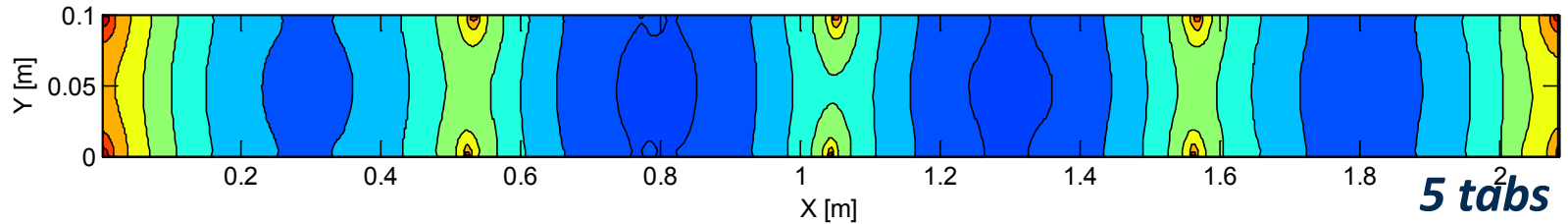
$\Delta i'' / i''_{avg}$



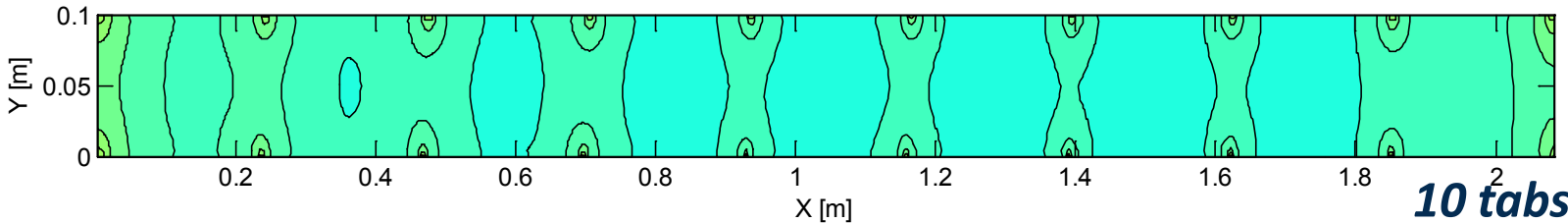
32.2%



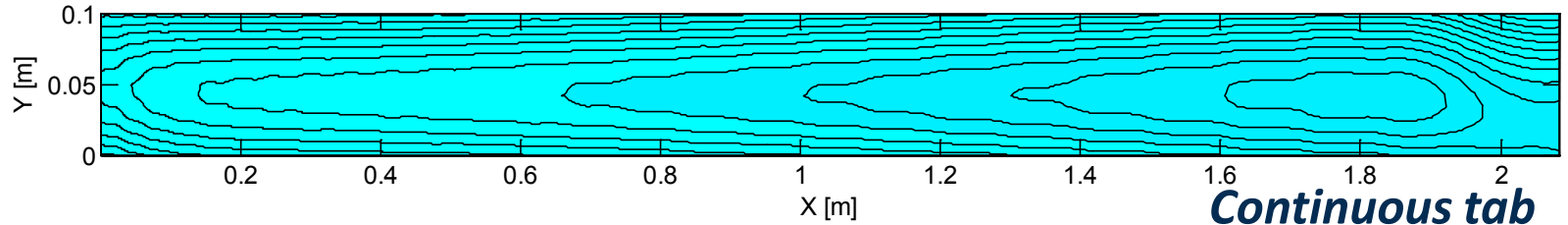
6.6%



2.2%

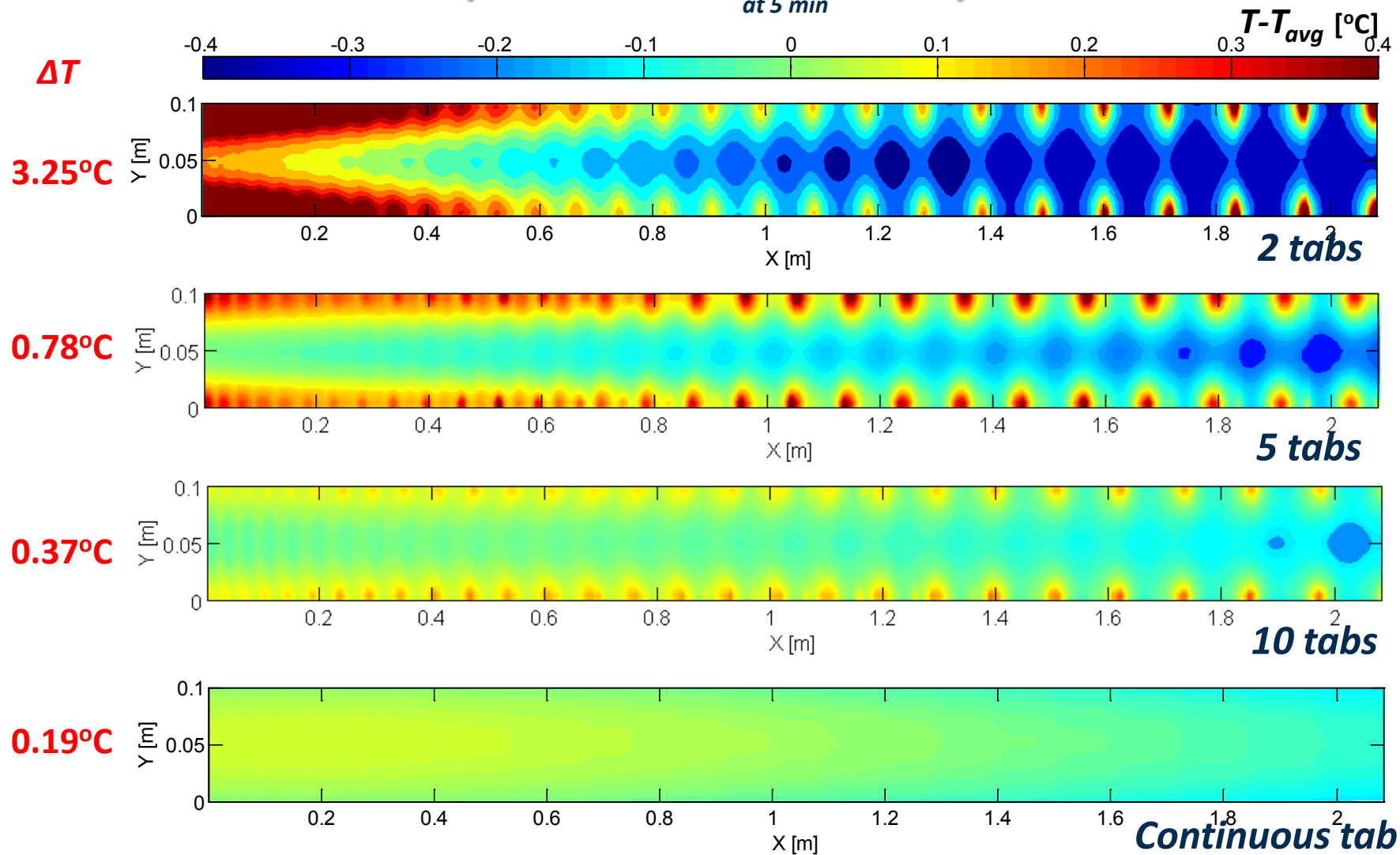


0.2%



Temperature deviation comparison

at 5 min



Conclusion

- **A Multi-Scale Multi-Dimension model** was used for evaluating large format automotive cell designs by integrating micro-scale electrochemical process and macro-scale heat and electrical current transports.
- Spatial non-uniformity of battery physics, which becomes significant in large batteries, cause unexpected performance in spiral wound lithium-ion batteries.
- **A macro-scale domain model based on spirally wound structures** of lithium-ion batteries was developed to understand effects of tab configurations and the double sides electrodes structure.
- Spiral wound cells with more tabs would be preferable to manage cell internal heat and electron current transport, and consequently to achieve uniform electrochemical kinetics over a system.
- The spiral wound cell model can provide **quantitative data** in terms of finding the optimum number of tabs to battery manufacturers.

Acknowledgments

US. Department of Energy, Vehicle Technology Program

Dave Howell, *Hybrid Electric Systems Team Lead*



National Renewable Energy Laboratory

Ahmad Pesaran, *Energy Storage Team Lead*

