

RECLAMATION

Managing Water in the West

Flow Characterization Study

Instream Flow Assessment Big Timber Creek, Idaho



U.S. Department of the Interior
Bureau of Reclamation
Technical Service Center
Denver, Colorado

June 2004

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Prepared for:

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Denver, Colorado**

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SUMMARY

The Bureau of Reclamation conducted flow characterization and habitat studies on Big Timber Creek, located in the Lemhi River sub-basin in Idaho, to identify stream flow needs to support relevant life history stages of summer steelhead (*Oncorhynchus mykiss*), spring chinook salmon (*O. tshawytscha*), and bull trout (*Salvelinus confluentus*). The study area encompassed the mainstem Big Timber Creek from its confluence with the Lemhi River upstream to Basin Creek. Seven study sites were selected to represent mesohabitat types within each stream reach distinguished by unique hydrology, channel morphology, slope, or land use characteristics. Big Timber flows were measured at one study site located upstream from major diversions using a stage recorder during the 2003 irrigation season. Unimpaired flows ranged from 16 cfs in late September to 295 cfs on May 31. Reclamation characterized flow needs for various life stages of the selected species in Big Timber Creek using the Physical Habitat Simulation (PHABSIM) model at each study site. Attempts to conduct field surveys at low, medium, and high flows at most sites were confounded by diversions downstream from the unimpaired site. In most cases, only medium and low flows were measured. However, these conditions typically occur during the summer irrigation season with the diversions. Habitat modeling results reflected differences in stream channel hydraulics among study sites. Cross-sectional profile and wetted area comparisons of study sites showed a narrower, more confined stream channel and less wetted surface area per any given flow in lower reaches of Big Timber Creek than upstream reaches. Thus, less flow was needed for suitable fish habitat in the lower reaches than the upper reaches given present stream channel morphology. For example, at the most downstream study site, flow required for adult salmonid passage was 13 cfs. This compared with the most upstream site where passage flow was 17 cfs. Study results can be used to determine a target flow or flows to improve passage, spawning, and rearing conditions for salmon, steelhead, and bull trout.

1.0 INTRODUCTION

The Bureau of Reclamation (Reclamation, BOR) participates with many other Federal, State, local, Tribal, and private parties in Endangered Species Act (ESA)-listed anadromous fish protection and restoration activities in selected parts of the Upper Salmon River Basin. Reclamation participation is related to avoid jeopardy to the survival of ESA- listed anadromous fish due to operation of dams in the Columbia River basin as explained in the Biological Opinion on Operation of the Federal Columbia River Power System (BiOp) issued by the National Marine Fisheries Service (NMFS) (currently National Oceanic Atmospheric Administration (NOAA) Fisheries) in December, 2000. Reclamation was assigned 16 Columbia River sub-basins through the BiOp-- four of those assigned sub-basins are in the Salmon and Clearwater River basins in Idaho. In the Upper Salmon River Basin, assigned sub-basins are the Lemhi River sub-basin and the “Upper Salmon River sub-basin”, which is defined through the BiOp as the Salmon River basin upstream from the confluence of the Pahsimeroi and Salmon Rivers, but excludes the Pahsimeroi River basin.

Action 149 of the BiOp states Reclamation obligations related to stream flow issues: “BOR shall initiate programs in three priority sub-basins (identified in the Basinwide Recovery Strategy) per year over 5 years, in coordination with NMFS, Fish and Wildlife Service (FWS), the states and others, to address all flow, passage, and screening problems in each sub-basin over ten years.”

Further, “The Federal Agencies have identified priority sub-basins where addressing flow, passage, and screening problems could produce short term benefits. This action initiates immediate work in three such sub-basins per year, beginning in the first year with the Lemhi, Upper John Day, and Methow sub-basins. Sub-basins to be addressed in subsequent years will be determined in the annual and 5-year implementation plans. NMFS will consider the level of risk to individual ESU’s and spawning aggregations in the establishment of priorities for subsequent years. At the end of 5 years, work will be underway in at least 15 sub-basins. The objective of this action is to restore flows needed to avoid jeopardy to listed species, screen all diversions, and resolve all passage obstructions within 10 years of initiating work in each sub-basin. BOR is the lead agency for these initiatives and will facilitate their implementation. In addition, recognizing the critical importance of starting this work quickly, BPA will expand on measures under the Northwest Power Planning Council (NWPPC) program to complement BOR’s action. To support this work, NMFS will supply BOR with passage and screening criteria and one or more methodologies for determining instream flows that will satisfy ESA requirement.”

Priority streams have been identified in the Lemhi River sub-basin based on inventory and assessment needs. The objective of this study was to conduct habitat studies on the highest priority stream, Big Timber Creek, to identify stream flow needs to support relevant life history stages of summer steelhead (*Oncorhynchus mykiss*), spring chinook salmon (*O. tshawytscha*), and bull trout (*Salvelinus confluentus*). Information obtained from this study may be used by the public, State, and Federal agencies to direct management actions addressing stream flow needs of ESA-listed anadromous and

resident native fish. Study results can be used to help determine target flow objectives to improve passage, spawning, and rearing conditions for salmon, steelhead, and bull trout.

1.1 Background

Rivers and streams in the Lemhi River sub-basin historically provided significant spawning and rearing habitat for anadromous spring/summer chinook salmon, sockeye salmon, and steelhead trout. However, anadromous fish populations have plummeted in the last 100 years and led in the 1990s to listing of these salmon and steelhead stocks as threatened under the ESA. Wild salmon and steelhead continue to migrate into the area and depend on spawning and rearing habitat in the basin. Bull trout also inhabit many of these rivers and streams. However, human development has modified the original flow and habitat conditions thereby affecting migration and/or access to suitable spawning and rearing habitat for all of these fish.

Many Federal, State, Tribal, local, and private parties work together to protect and restore ESA-listed anadromous and native fish species in the basin. One part of this work involves providing enough stream flow for these fish. Although sufficient stream flows are essential for fish to thrive, flows in the basin are also used for agricultural, domestic, commercial, municipal, industrial, recreational and other purposes. There is considerable information available that can be used to identify the amount of stream flow needed and used by people, however, there is little information about how much stream flow is needed to support various life history stages of ESA-listed fish. A reliable identification of stream flow needs for these fish will provide a basis that the public and Federal, State Tribal, and local parties can use to determine how to make the available water supply meet both the needs of ESA-listed fish and the needs of the people who live in these areas.

Some river reaches are more vulnerable than others to limitations in available stream flow. Fishery biologists with the Idaho Department of Fish and Game (IDFG), Bureau of Land Management (BLM), U.S. Forest Service, and Shoshone-Bannock Tribes compiled professional biological recommendations and known anadromous and resident fish population densities and chinook redd counts. They used this information to prioritize 11 sub-basins and to develop a list of 30 river reaches in the basin for immediate inventory and assessment for mitigation efforts (IDFG draft report, 5/10/02). The geographic area covered in their report included the entire Upper Salmon River Basin upstream from the confluence of the Middle Fork and main stem of the Salmon River.

1.2 Species of Interest

Snake River summer-run steelhead are Federally listed as threatened under the ESA within the NOAA Fisheries designated ESU. In the Lemhi River sub-basin, summer steelhead are part of the Snake River Basin steelhead Evolutionary Significant Unit (ESU) which is listed as threatened (Federal Register Vol. 64, No. 57, March 25 1999). Critical habitat for this ESU was designated February 16, 2000 (Federal Register, Vol. 65, No. 32, February 16, 2000), and includes all accessible portions of the project area. This critical habitat designation has been withdrawn and is currently being reviewed by NOAA Fisheries,

pursuant to a consent decree on April 30, 2002 (NMFS 2002).

Spring/summer chinook salmon are Federally listed as threatened under the ESA and by the State of Idaho. Chinook salmon are part of the federally threatened Snake River Chinook “Spring/Summer Run” ESU (Federal Register Vol. 57, April 22, 1992) in the Lemhi River sub-basin. Designated critical habitat for this ESU occurs in the Lemhi hydrologic unit (Federal Register Vol. 64, No. 205, October 25, 1999).

Bull trout are listed as threatened under the Federal ESA and as a species of concern by the State of Idaho. Bull trout are part of the Columbia River Basin bull trout distinct population segment (DPS) which is listed as threatened (Federal Register, Vol. 63, No. 111, June 10 1998). In 2002, FWS proposed critical habitat for bull trout in the Columbia River basin (Federal Register, Vol. 67, No. 230, November 29, 2002). In 2003, FWS reopened the comment period for the proposal to designate critical habitat for Columbia River DPS bull trout (Federal Register Vol. 68, No. 28, February 11, 2003). Final designation of critical habitat has been delayed due to a funding shortfall (Letter from R. Mark Wilson, FWS Montana Field Supervisor, June 17, 2003).

2.0 STUDY REGION

The following definitions apply to the following discussion:

Study area – The study area is defined as the stream reach impacted by flow alteration. Typically, only a small portion of a single stream makes up the study area.

Hydrologic segment – The portion of the study area that has a homogeneous flow regime. A study area may have one or more hydrologic segments (+/- 10% of the mean monthly flow (Q)).

Sub-segment (Reach) – A physical aspect of the channel within a hydrologic segment that affects the microhabitat versus flow relationship (e.g., channel morphology, slope, or land use).

Study site – A mesohabitat unit within a hydrologic segment or sub-segment.

The study area encompassed the mainstem Big Timber Creek from its confluence with the Lemhi River upstream to Basin Creek. Field reconnaissance, topographic maps, and interviews with IDFG indicated that Big Timber Creek could be divided into two hydrologic stream segments, defined as follows:

- Confluence with Lemhi River upstream to confluence with Little Timber Creek;
- Confluence with Little Timber Creek upstream to confluence with Basin Creek.

A hydrologic segment may be subdivided based on slope, channel morphology, or valley orientation (Bovee et al. 1998). Using U.S. Geological Survey (USGS) topographic maps, longitudinal gradient was plotted for Big Timber Creek within the study area (Figure 1). Within the two hydrologic segments, seven sub-segments, or reaches, were identified, distinguished primarily by differences in stream channel morphology and locations of major diversions. These were distributed sequentially proceeding upstream. Each sub-segment, or reach, is described below. Study sites selected to represent mesohabitat types within each sub-segment are identified on Figures 2 and 3.

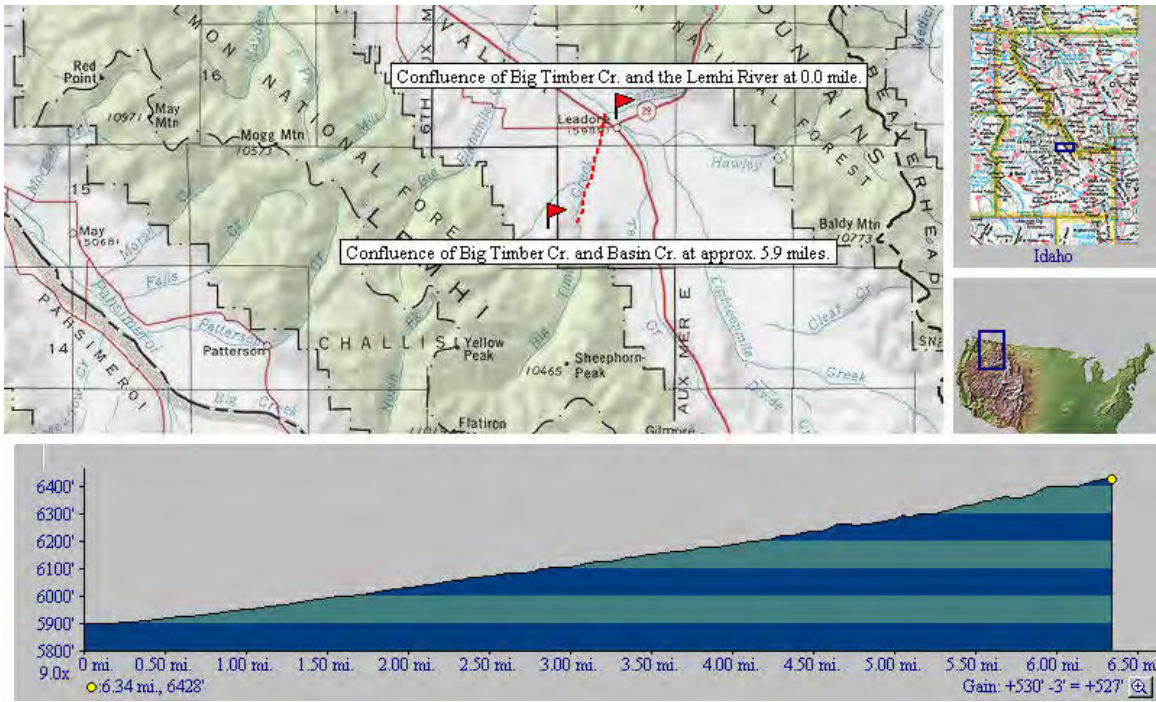


Figure 1. Big Timber Creek study area for flow characterization study.

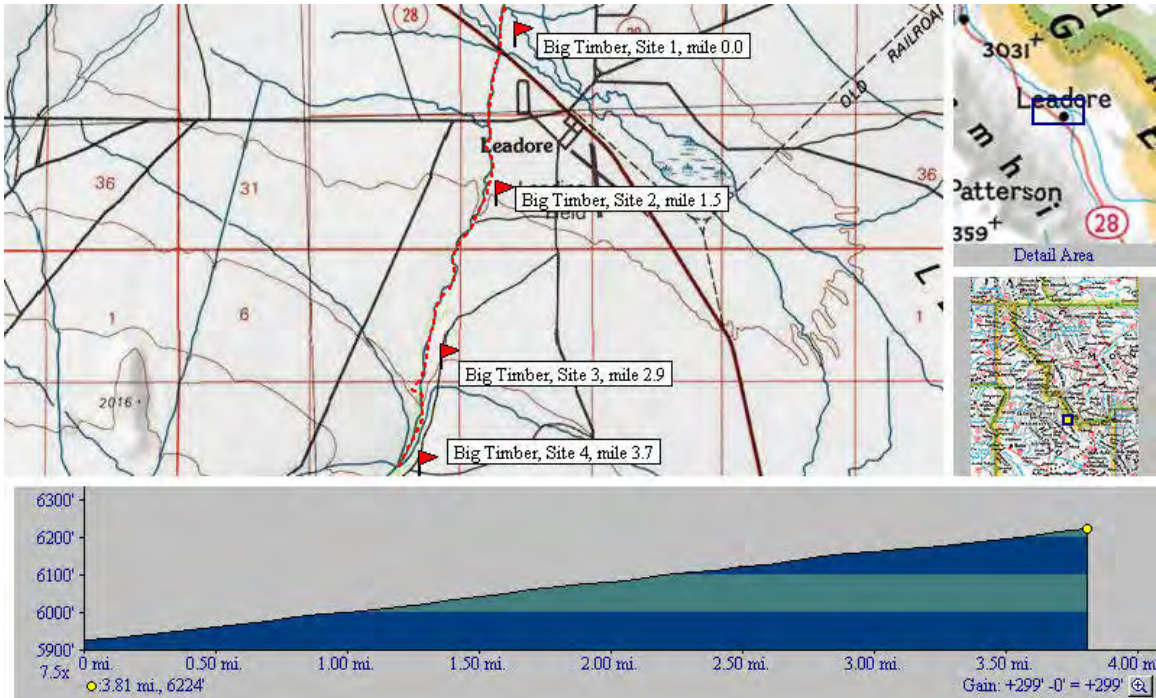


Figure 2. Big Timber Creek locations of study sites 1-4.

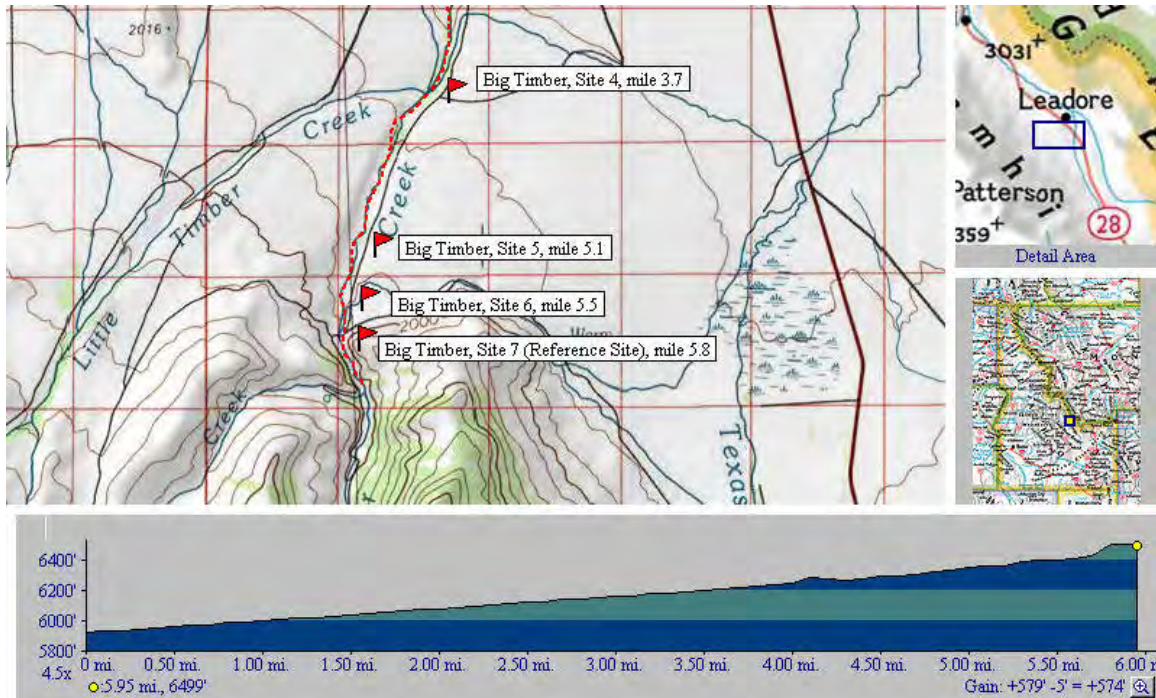


Figure 3. Big Timber Creek locations of study sites 4-7.

Reach 1: This reach extended from the confluence with the Lemhi River upstream to the first major diversion (N44.67760186 W113.3700417) that dewateres the stream channel during the irrigation season. The study site for this reach was located downstream from the dewatered channel where the stream was recharged by groundwater seeps on private property. The stream channel was narrower and shallower than the other reaches.

Reach 2: This reach extended from the diversion site at the upstream boundary for reach 1 upstream to another major diversion (N44.66095604 W113.3763557). The study site for this reach was represented by low gradient riffles and runs.

Reach 3: This reach was located between two major diversions that defined the upstream and downstream boundaries of reaches 2 and 4, respectively. The study site for this reach was located just downstream from a bridge crossing and represented by riffles and runs.

Reach 4: This reach extended from a relatively new major diversion (N44.660844 W113.377399) located upstream from the bridge crossing upstream to the confluence with Little Timber Creek (N44.64249705 W113.3831149). The study site for this reach represented a mixture of riffle, run, and pool habitat types.

Reach 5: This reach was located between the confluence with Little Timber Creek and the next major upstream diversion (N44.620541 W113.396212). This reach was characterized by beaver dams mixed with riffle, run, and pool habitats. Abundant riparian vegetation was dominated by willows. The study site represented riffles, runs, and pools within this reach.

Reach 6: This reach was located between the upstream diversion boundary for reach 5 upstream to the Cary Act Diversion (N44.61482736 W113.3967245) and Pipe Diversion (N44.613771 W113.397011). This reach had similar habitat characteristics as reach 5, including blown-out beaver dams and excellent riparian vegetation. The study site in this reach represented a mixture of riffles, runs, and pools.

Reach 7: This reach was located between the Pipe Diversion upstream to Basin Creek (N44.608750 W113.393787). The study site represented natural flow conditions (reference site) immediately upstream from the major diversions on Big Timber Creek. Habitat types included plunge pools, riffles, and runs.

3.0 LIMITING FACTORS ANALYSIS

The main components in this analysis were existing hydrology and fish population data. Existing USGS natural streamflow estimates and measured streamflows during 2003 were used to determine recent historic hydrology. Existing fish population data were used as an index of fish populations in the study streams. Additionally, any existing water quality data, including water temperature, were evaluated to determine if water quality was limiting. Water temperature was monitored continuously at one location in Big Timber Creek by Reclamation between July and September, 2003 using Onset TidBit data loggers to assess whether summer water temperatures limited the fishery.

Federal ESA listed species addressed in this section include the anadromous Snake River spring/summer Chinook salmon ESU; Snake River steelhead ESU; and resident Columbia River Basin bull trout DPS.

3.1 Steelhead

The Lemhi River sub-basin summer steelhead are classified as A-run steelhead (early migrators and spawners). Specific data on spawning populations of steelhead within Lemhi River sub-basin are very limited. These fish arise from stocks that were introduced by IDFG but are now considered natural populations. Periodicity for steelhead in the Lemhi River Drainage is summarized in Table 1.

Table 1. Periodicity chart for steelhead in Lemhi River Drainage (EA Engineering 1991a).

| Life Stage | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Adult | | | | | | ■ | | | | | | |
| Spawning | | | | | | ■ | | | | | | |
| Incubation | | | | | | | | ■ | | | | |
| Fry | | | | | | | | | | ■ | | |
| Juvenile | | | | | | | | | | | | ■ |
| Outmigrate | | | | | | ■ | | | | | | |

Steelhead migrate inland towards spawning areas, overwinter in larger rivers, resume migration to natal streams in early spring, and then spawn (Nickelson et al.1992).

Steelhead are widely distributed throughout the sub-basin, and juveniles are present year-round. The lower 27 miles of the mainstem Lemhi River from the mouth to Agency Creek serves mainly as a migration corridor. The 11-mile reach between Agency and Hayden Creeks provides rearing and limited spawning habitat. Tributary streams also provide spawning habitat. The IDFG collected resident rainbow/redband trout in Big Timber Creek below Rocky Creek confluence in 2003 (Murphy and Horsmon 2004). Mean density was 5.04 fish per 100 m² (1,076 ft²). Steelhead were not collected.

Irrigation, grazing, and road construction have affected habitat conditions throughout the Lemhi sub-basin (NPPC 2001). Limiting factors on the mainstem river can be grouped based on three distinct river segments, each having its own limiting factors. The lower 27-mile mainstem reach is degraded because of the lack of riparian vegetation and lack of pools for rearing and adult holding. The next segment, an 11-mile reach between Agency and Hayden Creeks, provides habitat, but riparian degradation has led to elevated water temperatures and unstable banks. The third mainstem segment, 28 miles from Hayden Creek to Leadore, has fluctuating summer temperatures, unstabilized banks, and few high quality pools. Salmonid habitat threats in the tributary streams include bank erosion leading to sedimentation, elevated temperatures, and degraded riparian habitat. Irrigation withdrawals have resulted in dewatered lower reaches in most tributaries. Water does not flow into the Lemhi River from many of the tributaries except during spring runoff, substantially reducing downstream migrations of fish and creating migration barriers. Many irrigation diversions on lower reaches of tributaries are not screened to protect migrating fish.

3.2 Spring/Summer Chinook Salmon

The two “races” of spring/summer chinook salmon in the Salmon River are classified by the season of adult passage at Bonneville Dam on the Columbia River during upstream migration. Spring/summer chinook enter the Columbia River March through July. Chinook that pass from March 1 to May 31 are considered “spring chinook” and those that pass from June 1 to July 31 are considered “summer chinook.” Spawning occurs in August through October. Eggs hatch in April and May, and the fry emerge approximately 1 month later. Juveniles rear for 1 year before out-migrating to the ocean (Simpson and Wallace 1982). Periodicity for Chinook salmon in the Lemhi River Drainage is summarized in Table 2.

The Lemhi River is believed to have supported substantial, relatively productive historic runs of this ESU. The “spring” race of chinook salmon spawn in the Lemhi River upstream of Hayden Creek. Over 95 percent of the salmon spawning and rearing in this sub-basin takes place in the upper 28 miles of the mainstem between Hayden Creek and Leadore. Most Snake River Spring/Summer Run Chinook salmon enter the sub-basin from May through September. Spawning occurs in late summer and early fall. All spawning is natural, as hatchery releases from Hayden Creek were suspended in 1982.

Table 2. Periodicity chart for Chinook salmon in Lemhi River Drainage (EA Engineering 1991a).

| Life Stage | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Adult | | | | | | | | | | ■ | | |
| Spawning | | | | | | | | | | ■ | | |
| Incubation | | | | | | | | | | | | ■ |
| Fry | | | | | | | ■ | | | | | |
| Juvenile | | | | | | | | | | | | ■ |
| Outmigrate | | | | | | ■ | | | | | | |

Juveniles reside in rearing areas for approximately 12 months before migrating downstream the following April and May (Bugert et al 1990; Cannamela 1992). The IDFG did not find Chinook salmon in Big Timber Creek during 2003 fish surveys (Murphy and Horsmon 2004).

Threats to chinook salmon are the same as those discussed for steelhead in the Lemhi sub-basin.

3.3 Bull Trout

Bull trout in the Lemhi sub-basin are considered fluvial stock, as they migrate between streams and larger rivers. Bull trout typically spawn in September and October but may begin their spawning migration as early as April. Spawning occurs in clean gravels, with areas of groundwater upwelling preferred. Fry emerge from early April through May. Small juveniles tend to remain in the gravels and cobbles. After reaching 4 inches in length, they move to backwater and sidewater channels, eddies, or pools (Goetz 1989). Periodicity for bull trout in the Lemhi River Drainage is summarized in Table 3.

Table 3. Periodicity chart for bull trout in Lemhi River Drainage (EA Engineering 1991a).

| Life Stage | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Adult | | | | | | | | | | ■ | | |
| Spawning | | | | | | | | | | ■ | | |
| Incubation | | | | | | | | | | | | ■ |
| Fry | | | | | | | | | | ■ | | |
| Juvenile | | | | | | | | | | | | ■ |

Within the project area, bull trout are widely distributed. They are present year-round. Bull trout are found in Big Eightmile, Big Timber, Eighteen Mile, Geertson, Hauley, Hayden, Kenny, Bohannon, Kirtley, Little Eight Mile, Mill, Pattee, and Texas Creeks; their tributaries; and in the Lemhi River (NPPC 2001). The IDFG collected juvenile and adult bull trout from mainstem Big Timber Creek upstream from Basin Creek confluence in 2003 (Murphy and Horsmon 2004). They were the most abundant species found in the Big Timber Creek watershed, with densities as high as 19.18 fish per 100 m² (1,076 ft²), indicating excellent water quality and high quality habitat.

Threats to bull trout and their habitat are the same as listed for steelhead in the Lemhi Subbasin. Of particular concern to fluvial bull trout is dewatering of lower tributary reaches and un-screened diversion structures that inhibit downstream migration into mainstem waters.

3.4 Hydrology

Natural streamflow estimates characterize seasonal flow variability in each stream segment . Large fluctuations in flow during the year are products of variable weather and the free-flowing condition of Big Timber Creek upstream from the major diversions Table 4 shows monthly flow exceedances and mean annual flows in Big Timber Creek for Study Site 4 downstream from the confluence with Little Timber Creek and Study Site 7 that represented natural flow conditions immediately upstream from the major diversions. An exceedance flow is defined as the flow that is equaled or exceeded a certain percentage of time. Flows were calculated for 20, 50, and 80 percent exceedance. These values were based on regional regression equations developed by USGS in Boise for the Forest Service (Hortness and Berenbrock 2001). Table 5 summarizes flows measured by USGS using a stage recorder during the 2003 irrigation season at Study Site 7. Figures 4 and 5 are graphical representations of tabular flows for Big Timber Creek discharge (cfs) in summer, 2003 using continuous gaging data and exceedance estimates. Flows ranged from 16 cfs in late September to 295 cfs on May 31. Flows will continue to be monitored at the stream gage on Big Timber Creek during 2004 and will eventually be accessible from the following website:

http://id.water.usgs.gov/projects/salmon_streamflow.

The hydrology of much of Big Timber Creek has changed dramatically since the mid-1840s because of diversions that resulted in a lack of connectivity to the floodplain. During irrigation season most of the water is diverted off-channel through diversion headgates and either used for flood or sprinkler irrigation. Big Timber Creek is entirely or significantly diverted for irrigation purposes between late April and the end of October (IDEQ 1999). As a result, most available water in Big Timber Creek only reaches the Lemhi River during spring runoff.

Table 4. Monthly exceedance flows on Big Timber Creek using USGS regional regression equations.

| Month | Flow value (cfs) | | |
|----------------|------------------|--------------|--------------|
| | | Study Site 4 | Study Site 7 |
| October | Q.80 = | 8.8 | 6.41 |
| | Q.50 = | 14.9 | 10.9 |
| | Q.20 = | 22.5 | 16.6 |
| November | Q.80 = | 11.2 | 8.1 |
| | Q.50 = | 13.9 | 10.1 |
| | Q.20 = | 20.2 | 14.9 |
| December | Q.80 = | 9.46 | 6.87 |
| | Q.50 = | 11.9 | 8.69 |
| | Q.20 = | 17.2 | 12.6 |
| January | Q.80 = | 8.94 | 6.47 |
| | Q.50 = | 10.8 | 7.89 |
| | Q.20 = | 15.5 | 11.4 |
| February | Q.80 = | 8.83 | 6.36 |
| | Q.50 = | 11.2 | 8.12 |
| | Q.20 = | 15.7 | 11.6 |
| March | Q.80 = | 9.14 | 6.58 |
| | Q.50 = | 13.1 | 9.52 |
| | Q.20 = | 18.5 | 13.6 |
| April | Q.80 = | 15.4 | 11.3 |
| | Q.50 = | 25 | 18.9 |
| | Q.20 = | 49.6 | 38.8 |
| May | Q.80 = | 58.7 | 49 |
| | Q.50 = | 116 | 97.3 |
| | Q.20 = | 217 | 184 |
| June | Q.80 = | 139 | 110 |
| | Q.50 = | 223 | 178 |
| | Q.20 = | 353 | 284 |
| July | Q.80 = | 31.9 | 24.2 |
| | Q.50 = | 59.9 | 45.2 |
| | Q.20 = | 101 | 76.3 |
| August | Q.80 = | 18.5 | 14.1 |
| | Q.50 = | 27.5 | 20.9 |
| | Q.20 = | 45 | 34.4 |
| September | Q.80 = | 15 | 11.3 |
| | Q.50 = | 21.3 | 15.9 |
| | Q.20 = | 32 | 24.1 |
| Average annual | Qaverage = | 36.9 | 27.8 |

Table 5. Water resource records for Big Timber Creek upstream from diversion structures, 2003.

U.S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY - WATER RESOURCES

STATION NUMBER 13303500 BIG TIMBER CREEK ABV DIVERSIONS NR LEADORE ID SOURCE AGENCY USGS STATE 16 COUNTY 059
 LATITUDE 443700 LONGITUDE 1132400 NAD27 DRAINAGE AREA 57.00 CONTRIBUTING DRAINAGE AREA 57* DATUM 6420. NGVD29

Date Processed: 2004-01-05 09:38 By dfgreen

Discharge, cubic feet per second

WATER YEAR OCTOBER 2002 TO SEPTEMBER 2003

DAILY MEAN VALUES

| DAY | OCT | NOV | DEC | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP |
|-------|-----|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|
| 1 | --- | --- | --- | --- | --- | --- | --- | --- | 257 | 43 | 21 | 17 |
| 2 | --- | --- | --- | --- | --- | --- | --- | --- | 208 | 42 | 20 | 17 |
| 3 | --- | --- | --- | --- | --- | --- | --- | --- | 168 | 41 | 22 | 17 |
| 4 | --- | --- | --- | --- | --- | --- | --- | --- | 153 | 40 | 22 | 17 |
| 5 | --- | --- | --- | --- | --- | --- | --- | --- | 136 | 39 | 21 | 17 |
| 6 | --- | --- | --- | --- | --- | --- | --- | --- | 119 | 37 | 20 | 17 |
| 7 | --- | --- | --- | --- | --- | --- | --- | --- | 113 | 36 | 20 | 19 |
| 8 | --- | --- | --- | --- | --- | --- | --- | --- | 108 | 35 | 19 | 17 |
| 9 | --- | --- | --- | --- | --- | --- | --- | --- | 109 | 34 | 19 | 17 |
| 10 | --- | --- | --- | --- | --- | --- | --- | --- | 109 | 33 | 19 | 18 |
| 11 | --- | --- | --- | --- | --- | --- | --- | --- | 103 | 32 | 18 | 18 |
| 12 | --- | --- | --- | --- | --- | --- | --- | --- | 97 | 31 | 18 | 17 |
| 13 | --- | --- | --- | --- | --- | --- | --- | --- | 89 | 30 | 18 | 17 |
| 14 | --- | --- | --- | --- | --- | --- | --- | --- | 82 | 30 | 18 | 17 |
| 15 | --- | --- | --- | --- | --- | --- | --- | --- | 77 | 29 | 18 | 17 |
| 16 | --- | --- | --- | --- | --- | --- | --- | --- | 74 | 28 | 18 | 17 |
| 17 | --- | --- | --- | --- | --- | --- | --- | --- | 73 | 27 | 18 | 17 |
| 18 | --- | --- | --- | --- | --- | --- | --- | --- | 70 | 26 | 18 | 17 |
| 19 | --- | --- | --- | --- | --- | --- | --- | --- | 68 | 26 | 18 | 17 |
| 20 | --- | --- | --- | --- | --- | --- | --- | --- | 68 | 25 | 17 | 17 |
| 21 | --- | --- | --- | --- | --- | --- | --- | --- | 65 | 25 | 18 | 17 |
| 22 | --- | --- | --- | --- | --- | --- | --- | 36 | 58 | 24 | 18 | 16 |
| 23 | --- | --- | --- | --- | --- | --- | --- | 49 | 54 | 24 | 20 | 16 |
| 24 | --- | --- | --- | --- | --- | --- | --- | 70 | 54 | 24 | 18 | 16 |
| 25 | --- | --- | --- | --- | --- | --- | --- | 102 | 51 | 25 | 18 | 16 |
| 26 | --- | --- | --- | --- | --- | --- | --- | 135 | 47 | 25 | 17 | 16 |
| 27 | --- | --- | --- | --- | --- | --- | --- | 153 | 44 | 24 | 18 | 16 |
| 28 | --- | --- | --- | --- | --- | --- | --- | 176 | 44 | 23 | 18 | 16 |
| 29 | --- | --- | --- | --- | --- | --- | --- | 226 | 43 | 22 | 18 | 16 |
| 30 | --- | --- | --- | --- | --- | --- | --- | 258 | 43 | 22 | 18 | 16 |
| 31 | --- | --- | --- | --- | --- | --- | --- | 295 | --- | 21 | 17 | --- |
| TOTAL | --- | --- | --- | --- | --- | --- | --- | --- | 2784 | 923 | 580 | 505 |
| MEAN | --- | --- | --- | --- | --- | --- | --- | --- | 92.8 | 29.8 | 18.7 | 16.8 |
| MAX | --- | --- | --- | --- | --- | --- | --- | --- | 257 | 43 | 22 | 19 |
| MIN | --- | --- | --- | --- | --- | --- | --- | --- | 43 | 21 | 17 | 16 |
| MED | --- | --- | --- | --- | --- | --- | --- | --- | 76 | 28 | 18 | 17 |
| AC-FT | --- | --- | --- | --- | --- | --- | --- | --- | 5520 | 1830 | 1150 | 1000 |
| CFSM | --- | --- | --- | --- | --- | --- | --- | --- | 1.63 | 0.52 | 0.33 | 0.30 |

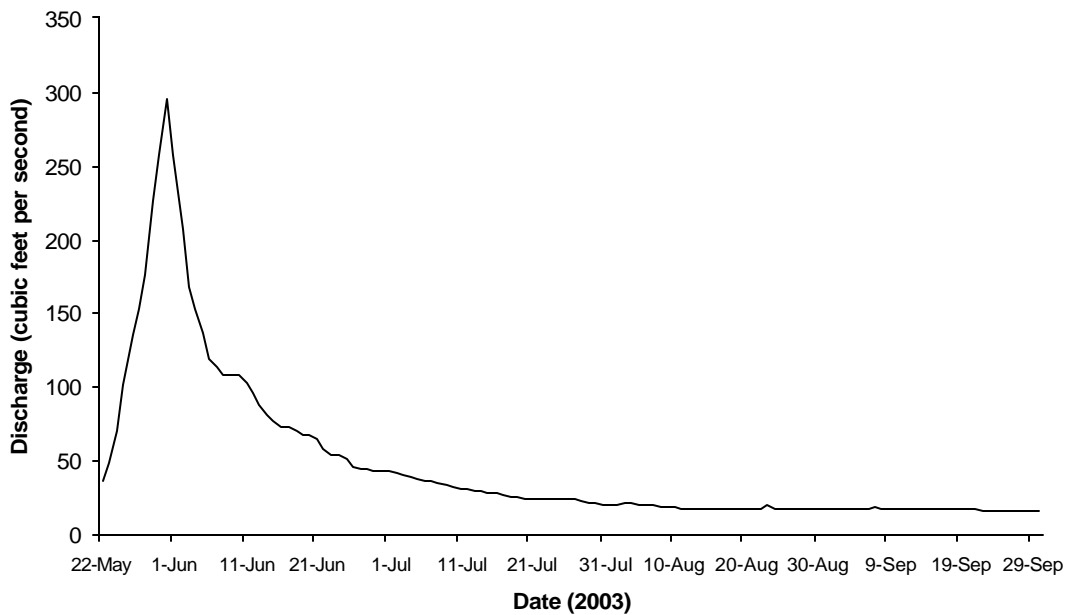


Figure 4. Graphical representation of data in Table 5 for unimpaired discharge (cfs) measured in Big Timber Creek upstream from diversions (2003).

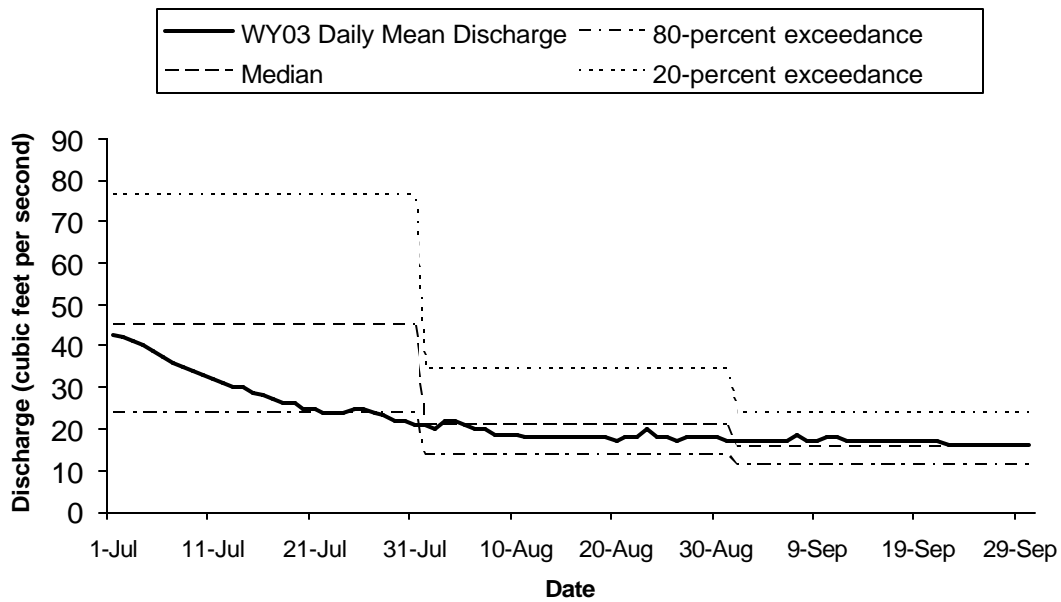


Figure 5. Graphical representation of Tables 4 and 5 for Big Timber Creek discharge (cfs) in summer, 2003 using continuous gaging data and exceedance estimates.

3.5 Water Quality

Water bodies are designated in Idaho to protect water quality for existing or designated uses. Big Timber Creek from its source to Little Timber Creek is designated by *Idaho Administrative Code 58.01.02 - Water Quality Standards* as:

- a. Cold water: water quality appropriate for the protection and maintenance of a viable aquatic life community for cold water species (4-5-00); and
- b. Salmonid spawning: waters which provide or could provide a habitat for active self-propagating populations of salmonid fishes (7-1-93).

Although Big Timber Creek is not listed on Idaho's 1998 303(d) list, the potential exists for elevated summer temperatures. Stream temperature is driven by the interaction of many variables, including shade, geographic location, vegetation, climate, topography, and flow. Based on *Idaho Administrative Code 58.01.02 - Water Quality Standards, SURFACE WATER QUALITY CRITERIA FOR AQUATIC LIFE USE DESIGNATIONS*, Idaho waters designated for cold water aquatic life are not to vary from the following characteristic: water temperatures of 22°C (72°F) or less with a maximum daily average of no greater than 19°C (66°F). (8-24-94). Hourly temperatures measured July 17, 2003 to September 18, 2003 for Big Timber Creek in the vicinity of Reach 4 are plotted in Figure 6. The maximum temperature reading was 21.1°C (70°F) on July 21. Average temperature was 14.0°C (57°F), which met this standard. Abundant riparian vegetation along Big Timber Creek likely shaded the stream and kept water temperatures from reaching extremely high levels during summer, 2003.

Water temperature - Big Timber Creek

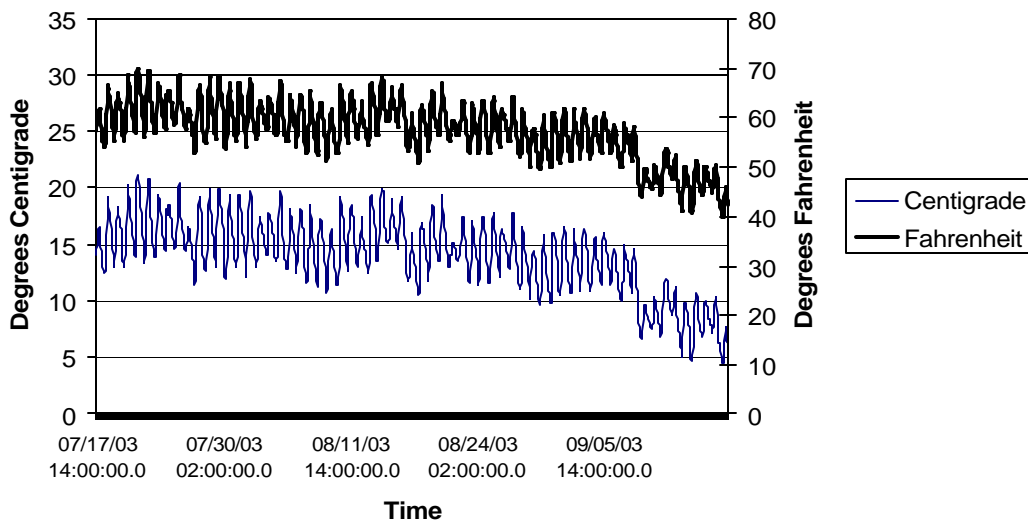


Figure 6. Water temperatures in Big Timber Creek during summer of 2003 measured by Reclamation near Reach 4.

Flow levels are affected by weather, snowpack, rainfall, and water withdrawal. Diverted water can reduce water quality. Shallower, slower water tends to warm faster than deeper, faster water. Warmer water holds less dissolved oxygen than cooler water. The combination of warm water with less dissolved oxygen, especially water temperatures above 20°C (68°F) and dissolved oxygen below 5 milligrams per liter, can stress salmonids (Bjornn and Reiser 1991). The temperature at which 50% mortalities (LC-50) occur in juvenile Chinook salmon is 25°C (77°F), when acclimated to 15°C (59°F) (Armour 1991). The upper lethal limit is 24°C (75°F) for steelhead (Bell 1991). In general, problem eutrophication is a partial result of irrigation return flow (non-point source) and possibly cattle feedlots (point source). However, agricultural runoff presents a low level of potential impact to water quality.

Water withdrawals have degraded the aquatic resources in the Lemhi River sub-basin by reducing flow in the river channels. Water use for irrigation is heavy, with water appropriations exceeding natural flows at times, most notably in the summer. Water appropriation varies by season, with less proportion of consumptive use in winter and most in summer. Artificially low streamflow limits the movement of fish, reduces the amount of physical habitat available for fish to live in, and reduces quality of habitat.

3.6 Summary

Based on this analysis, the primary limiting factors for fisheries in Big Timber Creek appear to be summer temperature and flow. Self-sustaining fish populations exist for the species of interest with no reported fish die-offs, and there is an available water supply throughout the year upstream from the major diversions. However, warm summer water temperatures are affected partly by water withdrawals, which also affect stream flows. Although high summer water temperature may limit the fisheries in late July and early August, fish populations continue to exist within available physical habitat throughout the year.

4.0 METHODS

The approach for characterizing flow needs in Big Timber Creek involved planning and execution of a Physical Habitat Simulation (PHABSIM) study in the stream segments identified above. The Technical Service Center (TSC) of Reclamation in Denver, Colorado was responsible for (1) collecting and compiling existing hydrology and biological data for salmon, steelhead, and bull trout using these streams; (2) conducting the study; and (3) providing Reclamation's Snake River Area Office in Boise, Idaho with a final report and associated data. These tasks are briefly outlined below.

4.1 Microhabitat Analysis

PHABSIM predicts changes in the relationships between in-stream flows and fish habitat for individual species and life stages and is best used for decision-making when alternative discharges are being evaluated (Bovee et al. 1998). It is useful for comparing the relative effects of various in-stream flow release schedules. Stream flow and habitat

data are used in a group of models called PHABSIM. Hydraulic models are used to calculate water surface elevations and depths and to simulate velocities for specific flows. Depth, velocity, substrate material, and cover data are used to determine available habitat. The model outputs proportions of suitable and unsuitable reaches of the stream and shows how often a specified quantity of suitable habitat is available. This methodology is scientifically tested and is generally an accepted technique for determining flows needed for fish. The habitat requirements of a number of species are not known; therefore, application can be limited unless emphasis is placed on developing habitat suitability criteria (HSC) for species of interest. The output of the model must be measured against biological knowledge.

Studies utilizing PHABSIM require extensive data collection and analyses. The steps in a PHABSIM study are briefly outlined below.

4.1.1 Mesohabitat Classification and Inventory

Specific procedures at each study site included:

- Locate study segments for study site selection.
- Map habitat features for stream segment. Habitat mapping, or mesohabitat typing, started at the upper segment boundary and proceeded downstream. The “cumulative-lengths approach” described by Bovee (1997) was used for habitat mapping. Habitat types were defined based on the purpose of hydraulic modeling to capture hydraulic changes (e.g., backwater and slopes).
- Thus, Reclamation used the following mesohabitat classification scheme:
 - low gradient riffles (slope),
 - moderate gradient riffles (slope),
 - high gradient riffles (slope),
 - runs (slope), and
 - pools (backwater).

Linear distance of each major habitat type was recorded and the total of each habitat type and total length mapped were recorded at the end of each segment. The mapped data were used to determine percentages of each habitat type.

- Study sites were selected based on habitat mapping.

4.1.2 Collection of hydraulic data

PHABSIM requires hydraulic and habitat suitability data to determine the instream flow requirements for the species and/or life history stage of interest. Several hydraulic sub-models can be used with PHABSIM including STGQ, WSP, and MANSQ. Field data collection was designed to accommodate any of these models. PHABSIM data

collection included several steps: study segment location, habitat mapping, transect (cross section) placement and data collection.

- Transects were placed in all habitat types that represented over 5 percent of the total available habitat. Transects were placed in homogeneous habitat types with the number of transects dependent upon the physical and hydraulic features of each habitat type. The number of transects necessary to capture the depth, velocity, cover and substrate distribution and variability is in large part a function of the specific river being worked on, the mesohabitat type being sampled, and the HSCs.
- Additional non-habitat simulation transects were placed at hydraulic controls (HC) by professional judgment to aid in hydraulic calibrations. The shallowest path across riffles or shallow runs within the study site was used to address passage issues for juvenile and adult salmonids.
- At each set of transects in each habitat type the following data were collected: establishment of horizontal reference points, distance between transects, field notes referencing general habitat and stream conditions in the transect areas, and reference photos of habitat and of each transect within each habitat type.

Field data were collected according to Bovee (1997) using standard surveying equipment above the water surface and using depth measured from a wading rod for wet areas. Reclamation personnel coordinated field survey procedures with the USGS flow study conducted in the upper Salmon River for quality control. We attempted to conduct the surveys at low medium, and high discharges. Vertical elevations were established throughout each habitat type by using differential leveling with a total station instrument (Bovee 1997). A benchmark was established (with rebar) and assigned the arbitrary elevation of 100.00 feet. All differential leveling was referenced to this benchmark. Water surface elevations (WSL) were measured to the nearest 0.01 ft near the water's edge along each transect at all discharges. Channel cross sections were measured (vertical and horizontal) to the nearest 0.1 ft between headpins at each transect during low discharge. Discharge measurements at each transect were taken at the three discharges.

4.1.3 Depth, Velocity, Substrate, and Cover

Depths, mean velocities, substrates, and cover were measured at various points along each transect. Stationing across transects was oriented with 0.0 on the left bank looking upstream for modeling purposes. Depths were measured using a top setting wading rod. Streambed elevations and water depths were measured to the nearest 0.1 ft. Mean column water was measured to the nearest 0.1 ft/sec using a Marsh McBirney Flo-Mate 2000 velocity meter attached to the wading rod. Substrate and cover for PHABSIM were visually assessed using a system developed by EA Engineering (1991b) (Table 6). A temporary staff gage was installed at each site so that fluctuations in WSL could be monitored during data collection.

Table 6. Big Timber Creek instream substrate and cover coding system.¹

| Code | SUBSTRATE | diameter (in) | diameter (mm) |
|-------|---------------------|------------------------------|---------------|
| 1 | Detritus | organic matter | |
| 2 | Silt | <0.0024 | 0-0.062 |
| 3 | Sand | 0.0024 - 0.125 | 0.062-3.2 |
| 4 | Small Gravel | 0.125 – 1.0 | 3.2-25 |
| 5 | Coarse Gravel | 1-3 | 25-76 |
| 6 | Cobble | 3-10 | 76-256 |
| 7 | Boulder | >10 | >256 |
| 8 | Bedrock | | |
| 9 | Aquatic Veg | | |
| COVER | | | |
| 1 | Woody debris | | |
| 2 | Undercut | undercut bank | |
| 3 | Cobble/Boulder | (>3") | |
| 4 | Aquatic vegetation | | |
| 5 | Large gravel | (2-3") | |
| 6 | Canopy | canopy or overhead structure | |
| 7 | Emergent vegetation | | |
| 8 | No cover | | |

¹ Source: EA Engineering (1991b)

Velocity calibration sets were collected at three different time periods between June and September, 2003 in an attempt to cover a range of flows.

Additional transect-specific data (i.e., flow and water surface elevations) were also collected during each of the velocity surveys at each site. These stage-discharge measurements provided the data necessary for model calibration and extended the range for hydraulic simulations. The applicability of the range of flows simulated to actual flows in the stream is dependent on the flows measured.

4.1.4 Habitat Suitability Criteria (HSC)

Species HSCs are required for PHABSIM analysis. Habitat suitability criteria, or curves, are interpreted using a suitability index (SI) on a scale of 0 to 1, with 0 being unsuitable and 1 being most utilized or preferred. Habitat suitability criteria that accurately reflect the habitat requirements of the species of interest are essential to developing meaningful and defensible instream flow recommendations. The recommended approach is to develop site specific criteria for each species and life stage of interest. An alternative involves using existing curves and literature to develop suitability criteria for the species of interest. No site-specific HSCs are available in the Lemhi River sub-basin and time and budgetary constraints precluded developing HSCs specific to Big Timber Creek. While such information may become available in the future through a separate study, the TSC worked with other interested parties and agencies in the interim to evaluate existing criteria curves appropriate for the Lemhi River sub-basin and decided to use HSCs that were developed for the upper Salmon River and Clearwater Basins by EA Engineering (1991b) for the Bureau of Indian

Affairs, and which represented the general habitat requirements of each particular fish species and lifestage for the Lemhi River sub-basin streams.

4.1.5 Hydraulic Model Selection and Calibration

Reclamation used the USGS Windows version of PHABSIM (USGS 2001) and coordinated hydraulic modeling procedures with the USGS flow study conducted in the upper Salmon River for quality control. PHABSIM has several submodels available for hydraulic simulations. These include STGQ, WSP, and MANSQ (USGS 2001), with STGQ being the most rigorous in terms of data requirements. Each hydraulic model requires multiple flow measurements to extend the predictive range. Depending on model performance, the predictive range may be restrictive, or wide ranging (i.e., 0.1 to 10 times the measured discharges) (USGS 2001). Since water is diverted between April 1 and September 30 of each year for irrigation, the range of flows for the hydraulic simulations covered flows that typically occur during these months.

Field sampling was designed to collect data in formats suitable for application in any of the hydraulic models identified above. The following approach was used:

- Enter field data into appropriate format for water surface simulations
- Calibrate STGQ, MANSQ, or WSP (depending on site specific conditions) to measured WSL
- Document calibration procedure
- Simulate a range of flows to predict water surface elevations
- Simulate depths and velocities for range of flows that occur during the irrigation season
- Evaluate simulation range based on velocity adjustment factors (VAF's) and other calibration sub-models
- Document acceptable range of simulations
- Conduct velocity simulation production run for applicable range of flows that may occur during the irrigation season.

4.1.6 Habitat Modeling

Table 7 shows various life stages and variables used to describe microhabitat.

Table 7. Life stages for species of interest and microhabitat variables used to describe habitat.

| Life Stage | Depth | Velocity | Substrate | Cover |
|------------------|-------|----------|-----------|-------|
| Adult passage | X | | | |
| Adult holding | X | X | X | |
| Adult spawning | X | X | X | |
| Juvenile rearing | X | X | X | X |

Since velocity HSCs for juvenile and adult bull trout were developed for nose velocities at 0.2 feet off the stream bottom (EA Engineering 1991b), the nose velocity option in the habitat model was used for these life stages of bull trout.

The following example describes how habitat weighting factors (WF) were determined. Study Site 3 had five cross sections: one deep run, three shallow runs, and one moderate gradient riffle. Within this site, based on the habitat mapping percentages (Appendix B), the three shallow runs represented 340 ft (34%), the moderate gradient riffle 540 ft (54%), and the deep run represented 120 ft (12%) of a 1,000 ft idealized reach. The shallow run distance of 340 ft was divided equally by three (113', 113', 114') to represent the three shallow runs at Study Site 3. Both the deep run and moderate gradient riffle distances remained the same. Weighting factors of 0.00-1.0 were calculated for each cross section to accurately represent the entire stream reach (Table 8).

Table 8. Example of setting cross section weighting factors for habitat modeling.

| Cross section | Habitat type | Distance from previous cross section (ft) | Weighting factor |
|---------------|--------------|---|------------------|
| 1 | Riffle | 0 | 1.0 |
| 2 | Shallow run | 540 | 1.0 |
| 3 | Shallow run | 114 | 1.0 |
| 4 | Shallow run | 113 | 0.48 |
| 5 | Deep run | 233 | 0.0 |
| Total | | 1,000 | |

An assigned WF of 1.0 moved upstream, and an assigned WF of 0.0 moved downstream, or backwards from the cross section. Weighting factors greater than 0.0 up to 1.0 moved the habitat upstream in proportion to the value assigned. For instance, the X-sec 1 WF of 1.0 applied continually upstream to X-sec 2, the entire 540 ft. The same applied to X-sec 2 and 3. The final cross section was handled differently. Essentially, it was combined into one unit, and assigned two WFs to complete the study site. The distances of X-sec 4 and 5 were combined (113+120) for a total distance of 233 ft. The formula below was used for attaining a WF:

$$233(x) = 113$$

$$X = 113/233 = 0.48$$

where X represented the unknown WF, 233 ft was the combined distance (X-sec 4 & 5), and 113 ft was the distance of X-sec 4.

The WF of 0.48 applied the habitat weighting 48% upstream to represent the final run. A weighting factor of 0.0 applied the habitat weighting of the remaining area, or 52% downstream from cross section 5. Figure 7 illustrates this procedure.

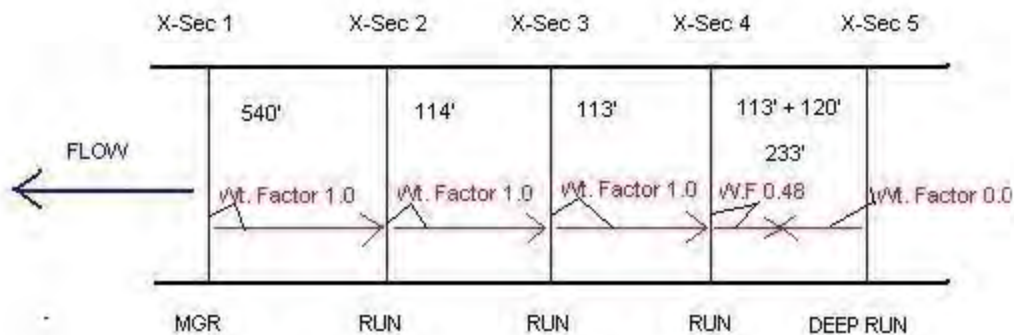


Figure 7. Example of weighting factor assignments at a PHABSIM study site.

If there was a hydraulic control (HC) cross section anywhere in the site it would not affect the habitat weighting. As for the distances (from previous cross section), the cross section immediately upstream from the HC would have a distance of '0 ft'; canceling out the HC in the model. For example, the distances and WF for the cross sections at Study Site 1 are listed in Table 9.

Table 9. Example of setting cross section weighting factors for habitat modeling with hydraulic controls.

| Cross section | Habitat type | Distance from previous cross section (ft) | Weighting factor (WF) |
|---------------|------------------------|---|-----------------------|
| 1 | Run | 0 | 1.0 |
| 2 | Hydraulic Control (HC) | 55 | 1.0 |
| 3 | Pool | 0 | 1.0 |
| 4 | Pool | 170 | 1.0 |
| 5 | HC | 170 | 1.0 |
| 6 | Pool | 0 | 1.0 |
| 7 | Riffle | 170 | 0.87 |
| 8 | Run | 435 | 0.0 |
| Total | | 1,000 | |

Weighted usable area (WUA) within each representative stream reach was calculated for each discharge of interest for each species. Weighted usable area is an index of habitat availability or quantity for the selected species/life stage at each simulated flow. The WUA for each species was computed by multiplying the depth, velocity, substrate, and cover HSC values for a life stage at predicted hydraulic conditions, and cell surface area in the HABTAE submodel of PHABSIM. The output from the HABTAE simulation was habitat area, expressed as WUA (ft²/1,000 ft of stream). Weighted Usable Area was predicted for a range of discharges at the six study sites. For presentation purposes, WUAs were normalized as a percentage of maximum habitat. It

should be noted that there is a level of uncertainty associated with the WUAs. Sources of uncertainty include errors in HSCs, hydraulic simulations, or selection of options to simulate microhabitat (e.g., geometric versus multiplicative means). Recognition that there is uncertainty in these sources is important in the interpretation and use of PHABSIM model results (Bovee et al. 1998).

Habitat for juveniles of each species was modeled separately using substrate and cover because of the known association of this life stage with cover. Since all substrates and cover were considered most suitable (SI=1.0) for juveniles, habitat modeled for substrate included the discrete cover component because cells containing cover were already accounted for by the continuous substrate variable.

4.2 Passage

Suggested passage criteria for adult Chinook salmon, steelhead trout, and bull trout follow guidelines adopted by Oregon Department of Fish and Wildlife and taken from Thompson (1972) and Scott et al. (1981) (Table 10). To determine the recommended flow for passage, shallow bars most critical to passage of adult fish were located, and a linear transect was measured which followed the shallowest course from bank to bank. For each transect, a flow was computed for conditions which met the minimum depth criteria in Table 10 where at least 25% of the total transect width and a continuous portion equaling at least 10% of its total width, equal to or greater than the minimum depth, was maintained (Thompson 1972). Both width criteria must be met to insure passage.

Table 10. Suggested Big Timber River salmonid passage criteria (Thompson 1972; Scott et al. 1981).

| Species | Minimum Depth (ft) | Maximum Water Velocity (ft/sec) |
|-----------------|--------------------|---------------------------------|
| Steelhead Trout | 0.6 | 8.0 |
| Chinook Salmon | 0.8 | 8.0 |
| Bull Trout | 0.4 | 4.0 |

4.3 Flow Recommendations using PHABSIM

The NOAA Fisheries draft protocol estimates idealized annual flow schedules for Pacific and interior northwest streams (Arthaud et al. 2002). The protocol identifies objectives for deriving minimum flow conditions necessary to protect sensitive salmonid life stages that can be quantified using PHABSIM methodologies. Results from this study can be used to help determine target flow objectives to improve passage, spawning, and rearing conditions for salmon, steelhead, and bull trout. Table 11 provides suggested critical life stage assignments for each month in the Lemhi River Drainage which could be used to determine target flows from the PHABSIM analysis.

Table 11. Suggested critical life-stage assignments for applying flow recommendations in the Lemhi River Drainage.

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Steelhead | | | | | | | | | | | |
| J | J | A | P/S | S | S | J | J | J | J | J | J |
| Chinook salmon | | | | | | | | | | | |
| J | J | J | J | A | A | P/S | P/S | S | S | J | J |
| Bull trout | | | | | | | | | | | |
| J | J | A | A | A | A | A | A | P/S | S | J | J |

J=juvenile; A=adult; S=spawning; P=passage

5.0 RESULTS AND DISCUSSION

Measured discharges and dates of field surveys are summarized in Table 12. Attempts to measure low, medium, and high flows at most sites were confounded by diversions downstream from Study Site 7. In most cases, only medium and low flows were measured. However, these conditions typically occur during the summer irrigation season with diversions. At Study Site 1, only low flow from groundwater seepage was present each time it was visited during the summer. Reclamation was able to measure one additional higher flow in late March, 2004 to improve model calibration and habitat simulations.

Written descriptions and photos of each selected study site are provided in Appendix A. Habitat mapping proportions are presented in Appendix B. Cross sectional profiles and measured WSLs are illustrated in Appendix C. Hydraulic model calibration results are summarized in Appendix D. Habitat suitability criteria (HSCs) are presented in Appendix E.

Complete habitat modeling output results (i.e., WUA vs discharge) are summarized in Appendix F for each stream reach. Graphical representations of final normalized WUA versus discharge relationships are presented in Figures 8 to 28 for each site. Juvenile habitat using the cover component independent of substrate did not model well because of the binary HSC criteria (i.e., present (SI=1.0) or absent (SI=0.0)). If a method could be developed to provide some quality ranking of cover types, the modeling could be improved. Separate cover habitat modeling results are included in Appendix F tables for juveniles. Appendix G contains site-specific IFG4 files for input into the PHABSIM program.

Passage flow results for contiguous widths at depths greater than the passage criteria (Table 10) are illustrated in Figures 29-35.

Summary results, including flows required for optimal WUAs and to flows needed to meet the 0.6 feet deep passage criteria are presented in Tables 13 to 19. Summary results reflected differences in stream channel hydraulics among study sites.

Table 12. Discharges measured from highest to lowest at Big Timber Creek study sites during field surveys in 2003.

| Stream Site | Discharge (cfs) | Survey Dates |
|--------------------------|-----------------|----------------|
| Study Site 1 | 2.0 | June 24 |
| | 1.2 | July 15 |
| | 1.3 | September 18 |
| | 6.5 | March 31, 2004 |
| Study Site 2 | 8.2 | September 18 |
| | 6.0 | June 29 |
| | 4.9 | July 17 |
| Study Site 3 | 15.8 | June 25 |
| | 8.9 | September 18 |
| Study Site 4 | 8.0 | July 15 |
| | 11.0 | June 29 |
| | 9.0 | September 17 |
| Study Site 5 | 8.0 | July 17 |
| | 28.0 | June 28 |
| | 25.0 | July 16 |
| Study Site 6 | 15.0 | September 17 |
| | 29.0 | July 16 |
| | 16.0 | June 27 |
| Study Site 7 (Reference) | 13.0 | September 16 |
| | 47.0 (gage) | June 26 |
| | 27.0 (gage) | July 17 |
| | 17.0 (gage) | September 15 |

Examination of cross-sectional profiles of study site transects (Appendix C) showed a narrower stream channel in the lower reaches (e.g., Study Site 1) of Big Timber Creek than the upstream reaches (e.g., Study Site 7). At any given flow, more wetted area occurred at Study Site 7 than Study Site 1. For example, at 10 cfs, 13,106 ft² of wetted area per 1,000 ft of stream occurred at Study Site 1. This compared with 21,993 ft² of wetted area per 1,000 ft of stream at Study Site 7 (Appendix F). Thus, with a smaller channel, less flow was needed to optimize habitat in the lower reaches than the upper reaches (Tables 13 to 19). For example, at Study Site 1, 5 cfs provided optimal habitat for juvenile bull trout, 9 cfs for adult bull trout, 10 cfs for spawning, and 13 cfs was required for passage of adults. These flows were less than Study Site 7 where 20 cfs provided optimal habitat for adult and juvenile bull trout, 60 cfs for spawning, and 17 cfs was required for passage.

Weighted Usable Area (WUA) estimates from a previous unpublished study conducted by EA Engineering on Big Timber Creek (Dudley Reiser, personal communication, July 21, 2003) were compared to our results at Study Site 7 (Appendix F). The objective of the EA Engineering study was to determine flows for fish recovery based on undisturbed stream segments and unimpaired flows for the Bureau of Indian Affairs adjudication process. This differed from our study objectives to determine target flows to improve passage, spawning, and rearing conditions for salmon, steelhead, and bull

trout in stream segments impacted by irrigation diversions. Thus, the value of this comparison was a relative check on our ability to replicate the habitat modeling results from a previous study and was only appropriate at Study Site 7 because this was the only stream segment located upstream from the major diversions where the stream channel hydraulics were similar between studies. Appendix F includes graphical comparisons of the habitat modeling results between this study and the less intensive EA Engineering study in the vicinity of Study Site 7. Although study results show similarities for the spawning life stage, reasons for differences between WUA estimates for other life stages are unknown since the EA Engineering study was never published. The results of this study are not easily transferrable to other drainages unless hydrology, hydraulics, and limiting factors (e.g., temperature, passage) are similar among streams.

6.1 Guidelines for Using Study Results

The results presented in this report summarize the hydrology, habitat, and temperature characteristics of Big Timber Creek during summer, 2003. PHABSIM analysis of the data collected and compiled for this study resulted in a series of graphs that illustrate relations between a dimensionless value called weighted usable area (WUA) and discharge (Figures 8-28). The highest point on each curve represents the discharge at which habitat is optimized for adult, spawning, or juvenile life stages for the fish species analyzed in this study (salmon, steelhead, and bull trout). These optimized values, summarized in Tables 13-19, rarely coincide among life stages for any one species. Furthermore, adult, spawning, and juvenile life stages for salmon, steelhead, and bull trout occur at different times of the year (Table 11). These results imply that the optimum amount of water needed for adult, spawning, and juvenile life stages is not constant, but varies during the year. It is suggested to consider these implications during development of flow targets. Also, WUAs do not address water availability in any way and even the unregulated flow may commonly exceed or be less than the discharge at which the maximum WUA is available. The amount of WUA available, in terms of lost or gained, can be determined by comparing to a reference or unregulated streamflow condition. Typically, the maximum, percentiles, or inflections are chosen from these curves at the level of protection desired or at points above which greater amounts of flow only provide minor gains in usable habitat. In streams with more than one species of interest, the results should be reviewed to insure the recommended flows are beneficial to all species and harmful to none.

The mechanisms by which the various components are integrated and the relative importance they are assigned within the water management decision process is a matter of professional judgment and beyond the scope of this study. However, it would seem reasonable that providing connectivity to the Lemhi River by providing enough water for adult fish passage would be foremost in management priorities. Water depths are an additional consideration for the adult life stage (Figures 29-35). Choice of target flows should not be reduced below the optimum flow to the point that stream depth is reduced below the level needed for fish passage (Tables 13-19), depending on available water supply.

Discharge estimates providing optimal WUA for juvenile salmonid lifestages are usually less than summer base flows, suggesting a disconnect between the models used and actual juvenile salmonid needs. Reasons for this may include: inability to accurately measure and/or quantify habitat parameters such as, flow velocity, cover, and substrate, at a scale that is meaningful for small fishes; inability to accurately quantify side channels, bank indentations, riparian wetlands, or other lateral habitats that are important for rearing juvenile salmonids; and inability to adequately incorporate temperature, or other water quality parameters, into the model. Thus, until juvenile habitat modeling can be improved, the existing juvenile WUA results should be used with caution in developing flow recommendations.

The selection of a target flow should be based on a hierarchical system of highest priority life stage and species present for the month or period of concern, using the assumption that the priority life stage and species would require higher streamflows than other life stages and species. Table 11 provides some general guidelines. For small tributary streams of the Lemhi River sub-basin, suggested priority life stage ranking would be (from high to low): passage > spawning > adult > juvenile. Once the priority life stage and species are ranked, then each study site should be examined to determine streamflow and passage conditions for the time period of concern.

Once an adequate number of sites have been characterized using PHABSIM, it may be feasible to develop habitat-discharge relations for streams with similar basin characteristics within specific geographic locations. This could possibly provide a regional planning tool that could eliminate intensive site-specific studies.

The natural hydrograph also needs to be considered when developing flow targets. In drought years, summer flows that provide maximum possible habitat may not be attainable because of the hydrologic limits on the stream. Also, PHABSIM does not estimate flow or habitat needs of downstream migrants or spring runoff conditions necessary for maintenance of channel morphology or riparian zone functions. Arthaud and others (2002) have shown that downstream migrant survival can significantly increase with discharge. Thus, high spring flows that mimic the natural hydrograph should be a consideration in managing streamflows outside PHABSIM analysis.

Finally, it should be noted that PHABSIM was designed as a tool to provide science-based linkage between biology and river hydraulics with results to be used in negotiations or mediated settlements (Arthaud et al. 2002).

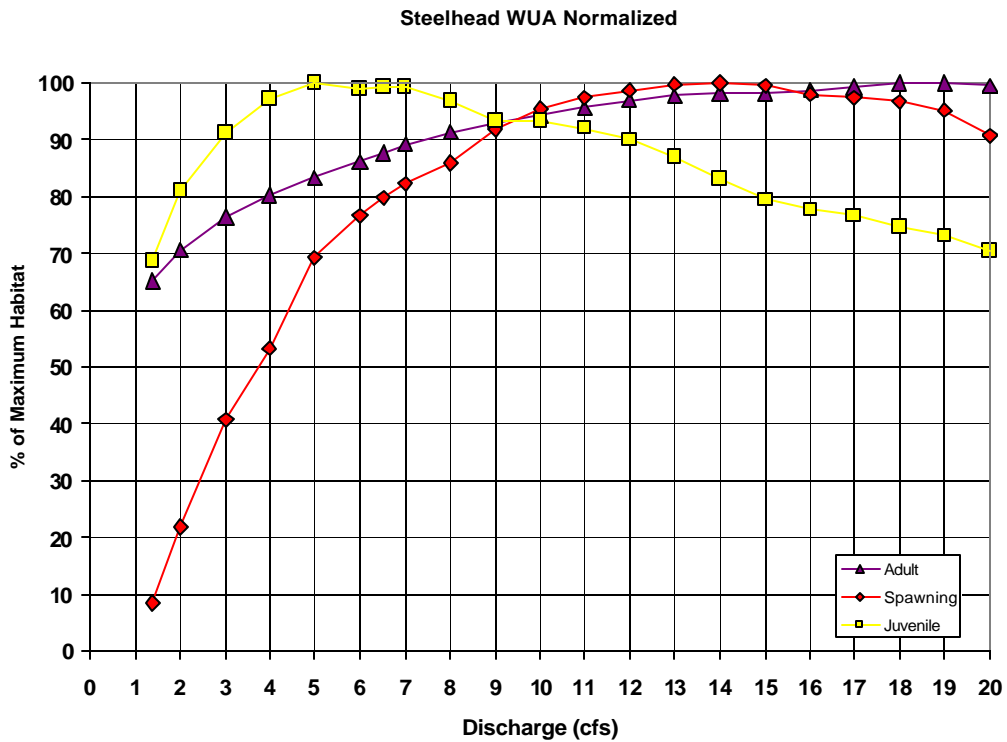


Figure 8. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for steelhead in Big Timber Creek, Study Site 1.

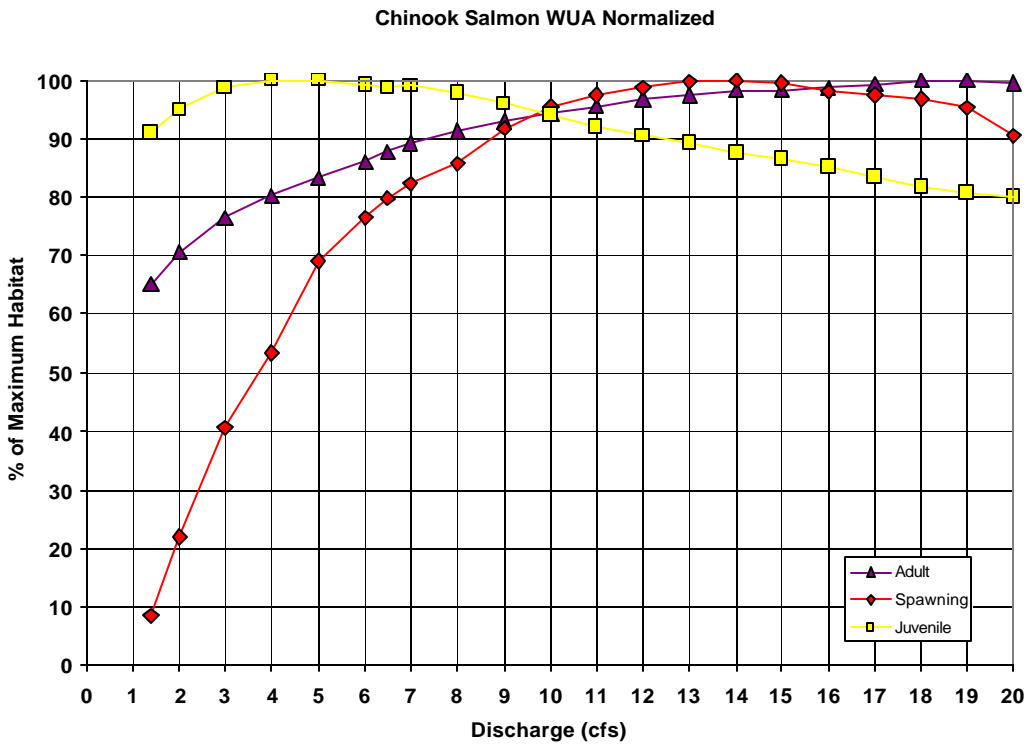


Figure 9. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for Chinook salmon in Big Timber Creek, Study Site 1.

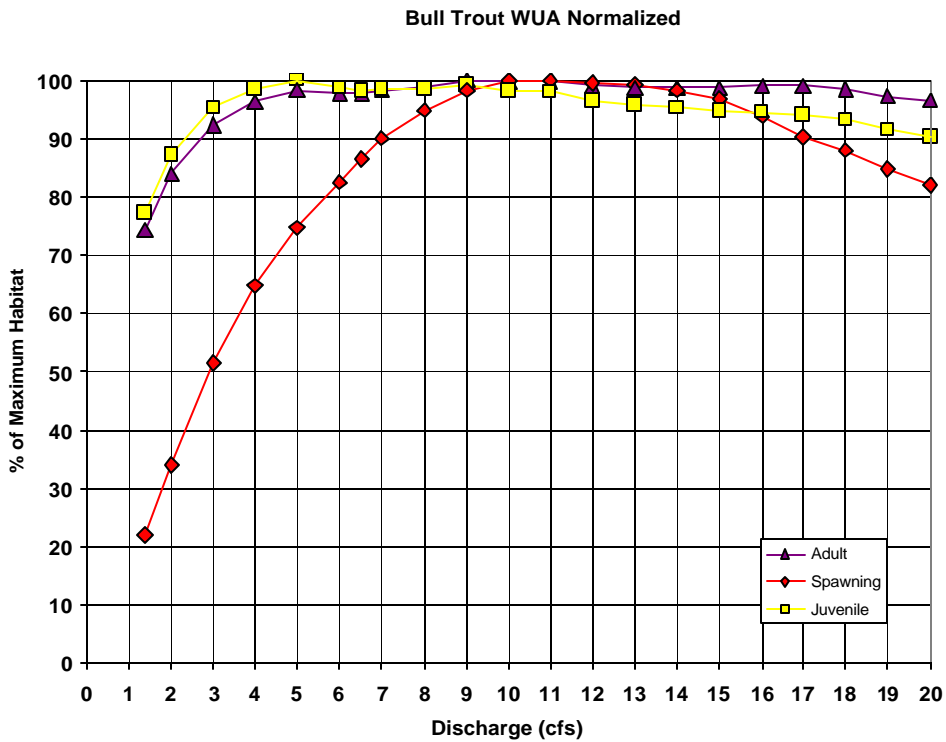


Figure 10. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for bull trout in Big Timber Creek, Study Site 1.

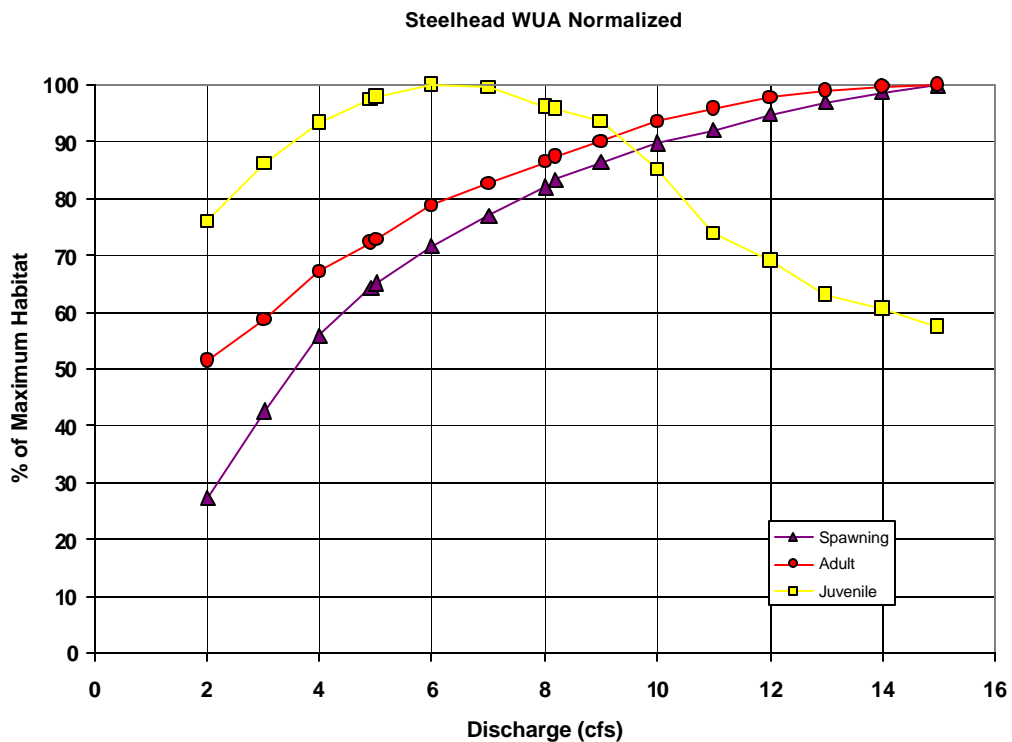


Figure 11. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for steelhead in Big Timber Creek, Study Site 2.

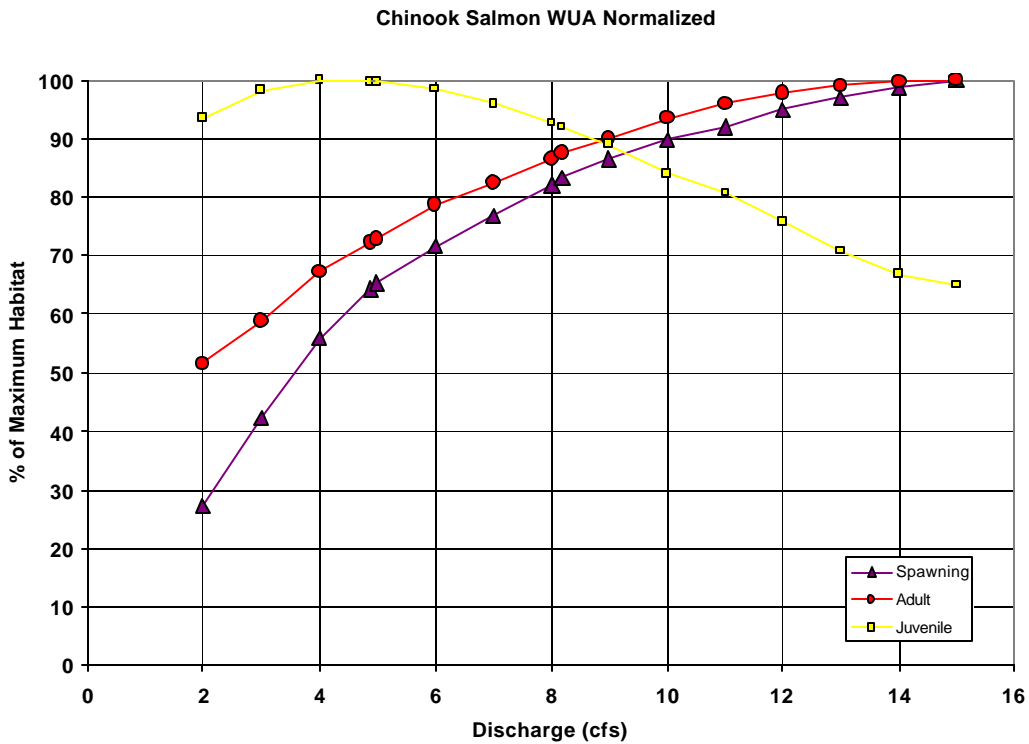


Figure 12. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for Chinook salmon in Big Timber Creek, Study Site 2.

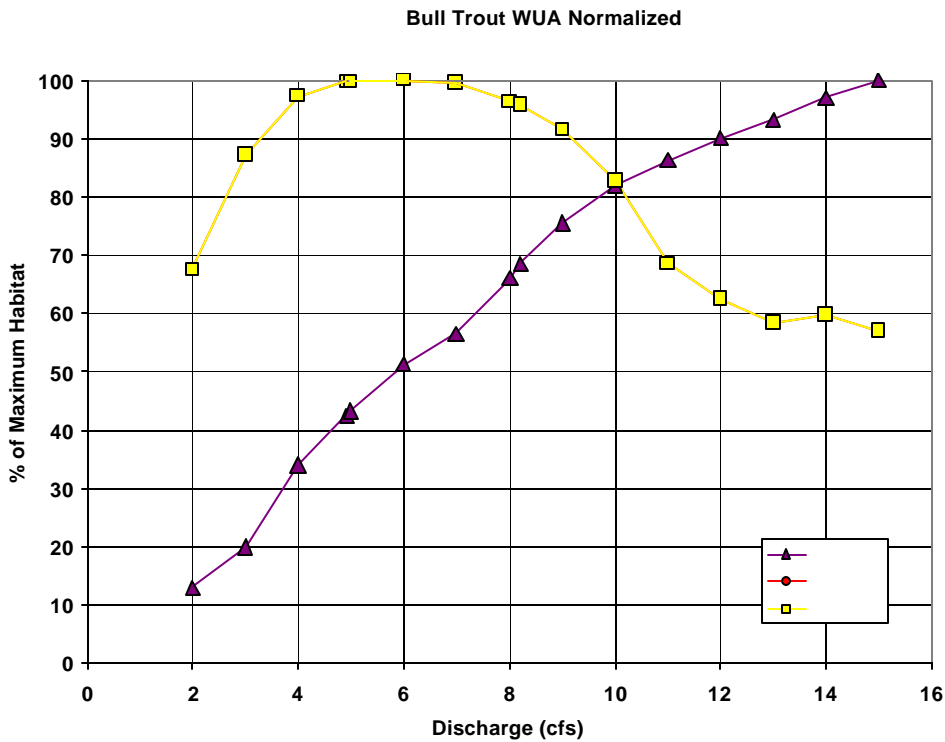


Figure 13. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for bull trout in Big Timber Creek, Study Site 2 (adults same as juveniles).

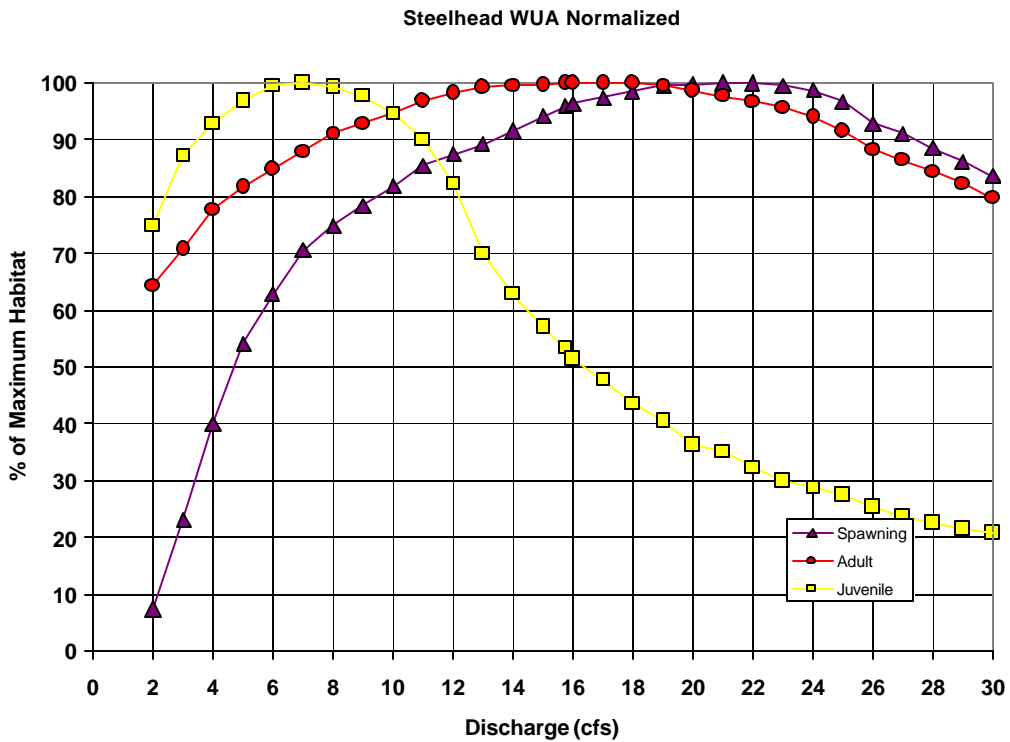


Figure 14. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for steelhead in Big Timber Creek, Study Site 3.

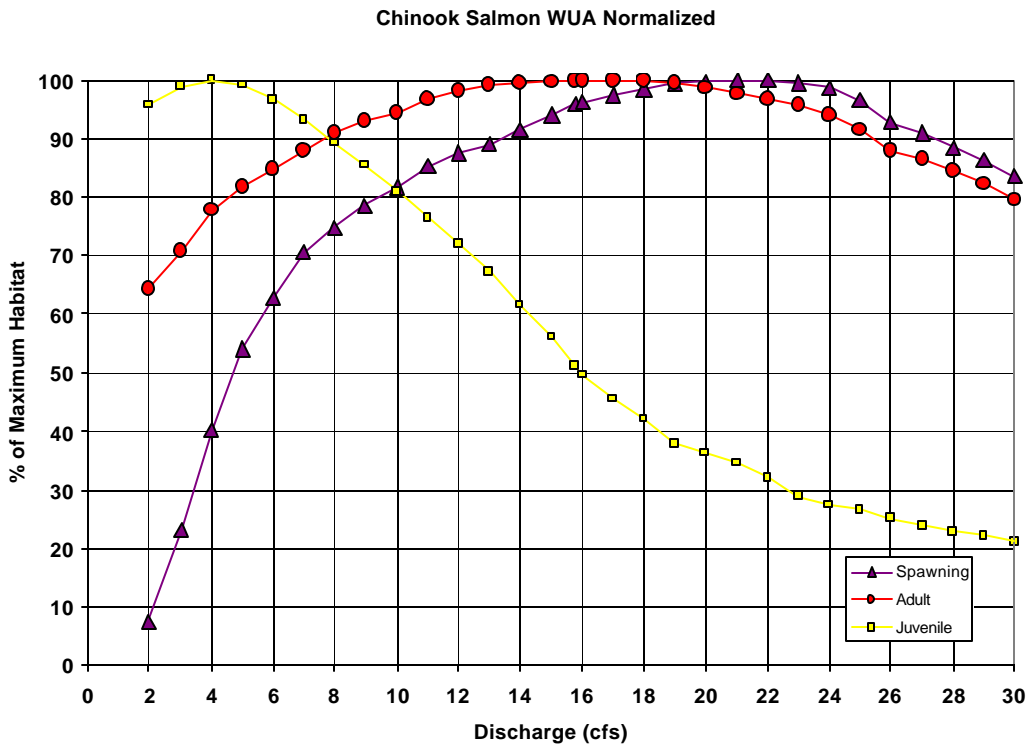


Figure 15. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for Chinook salmon in Big Timber Creek, Study Site 3.

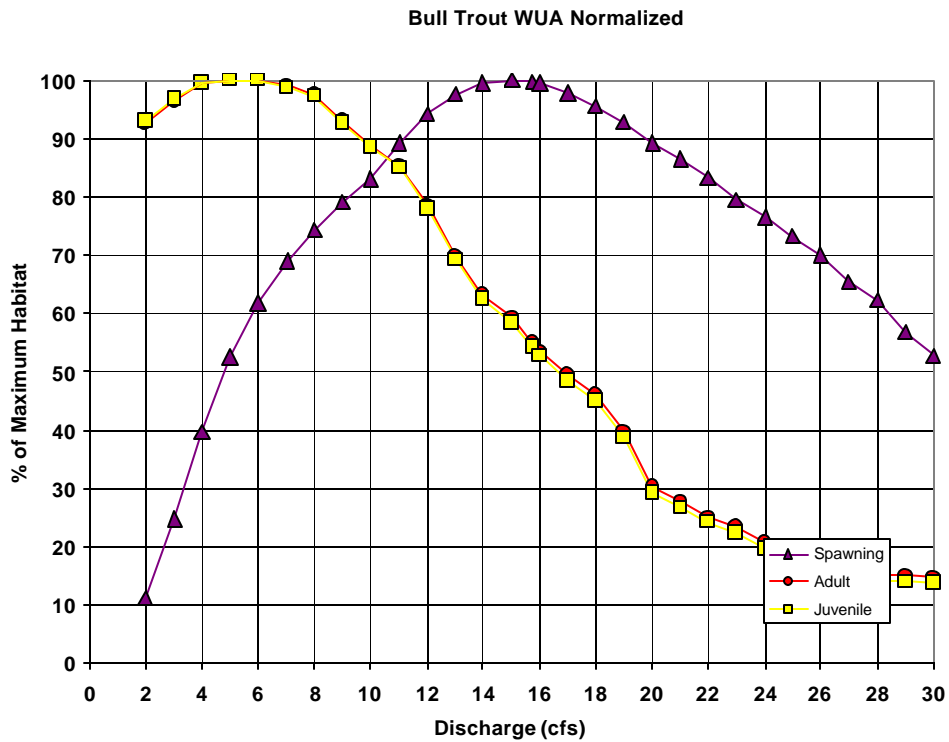


Figure 16. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for bull trout in Big Timber Creek, Study Site 3.

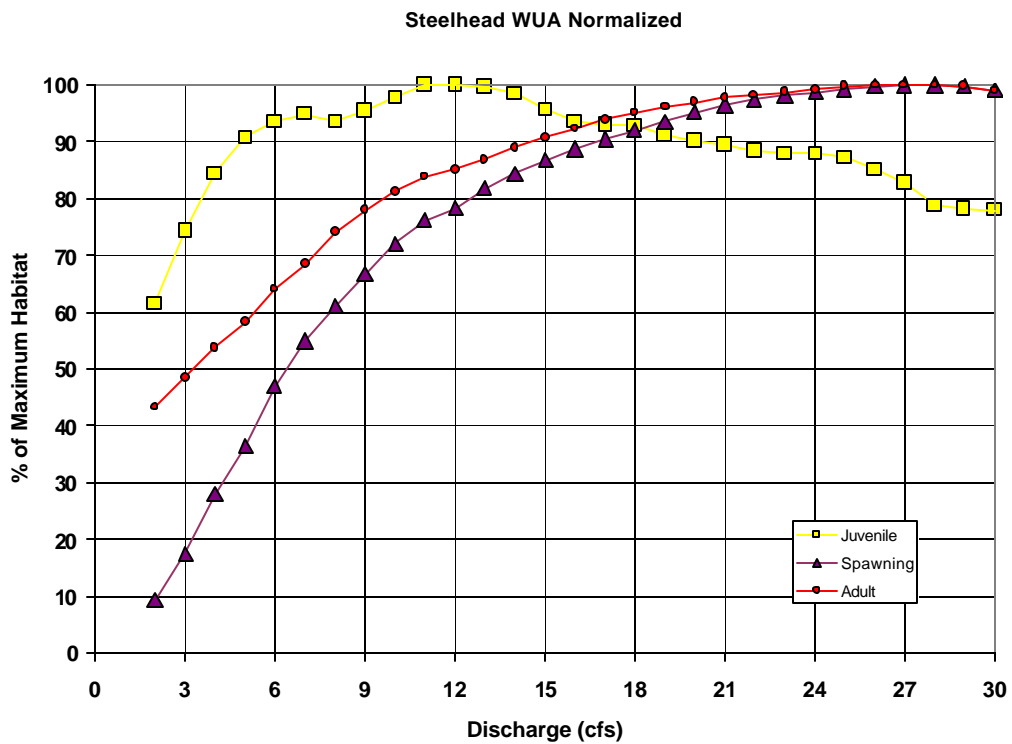


Figure 17. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for steelhead in Big Timber Creek, Study Site 4.

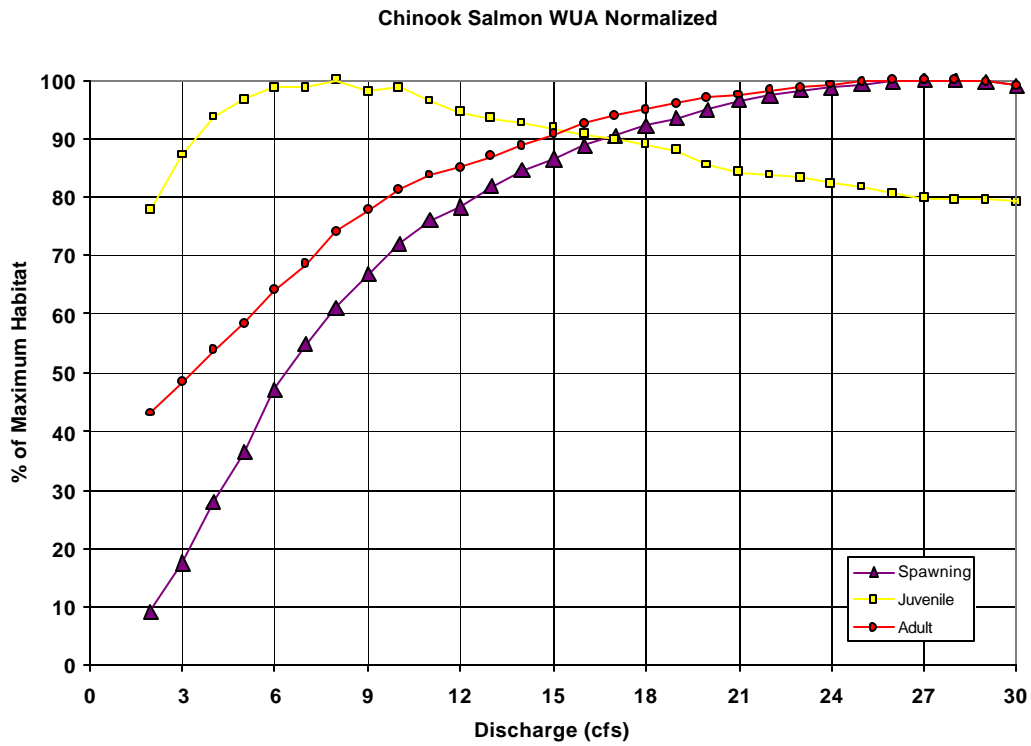


Figure 18. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for Chinook salmon in Big Timber Creek, Study Site 4.

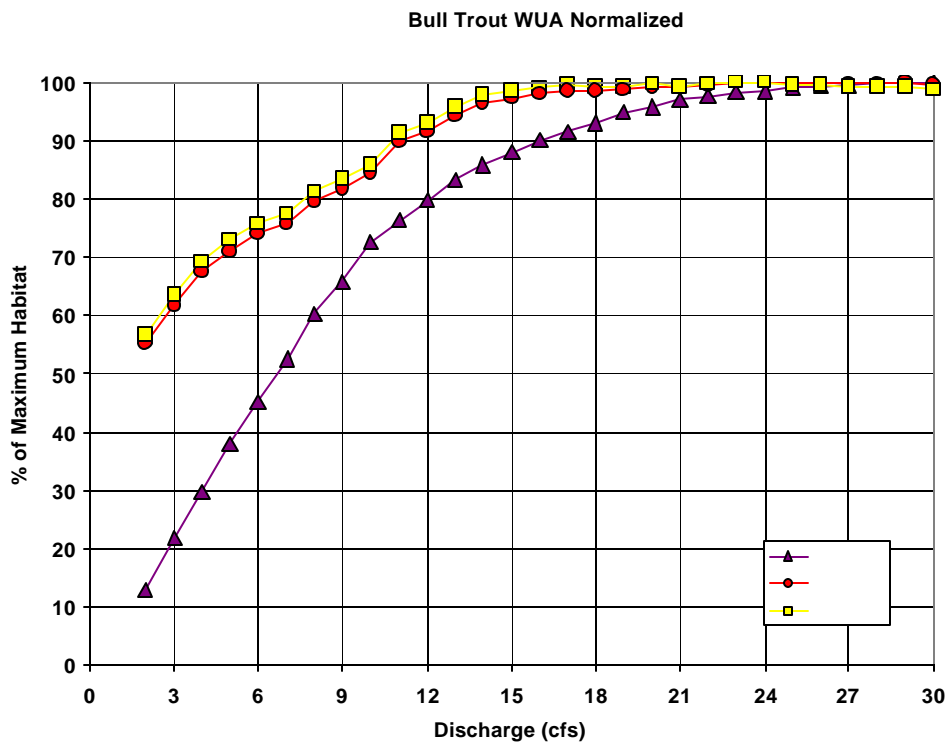


Figure 19. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for bull trout in Big Timber Creek, Study Site 4.

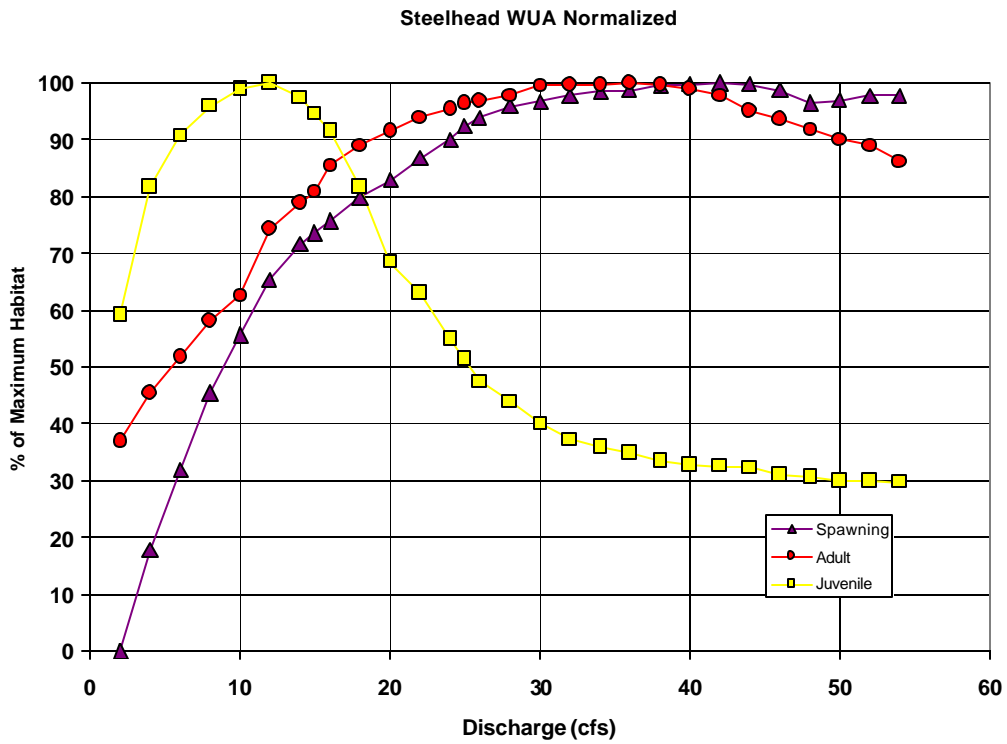


Figure 20. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for steelhead in Big Timber Creek, Study Site 5.

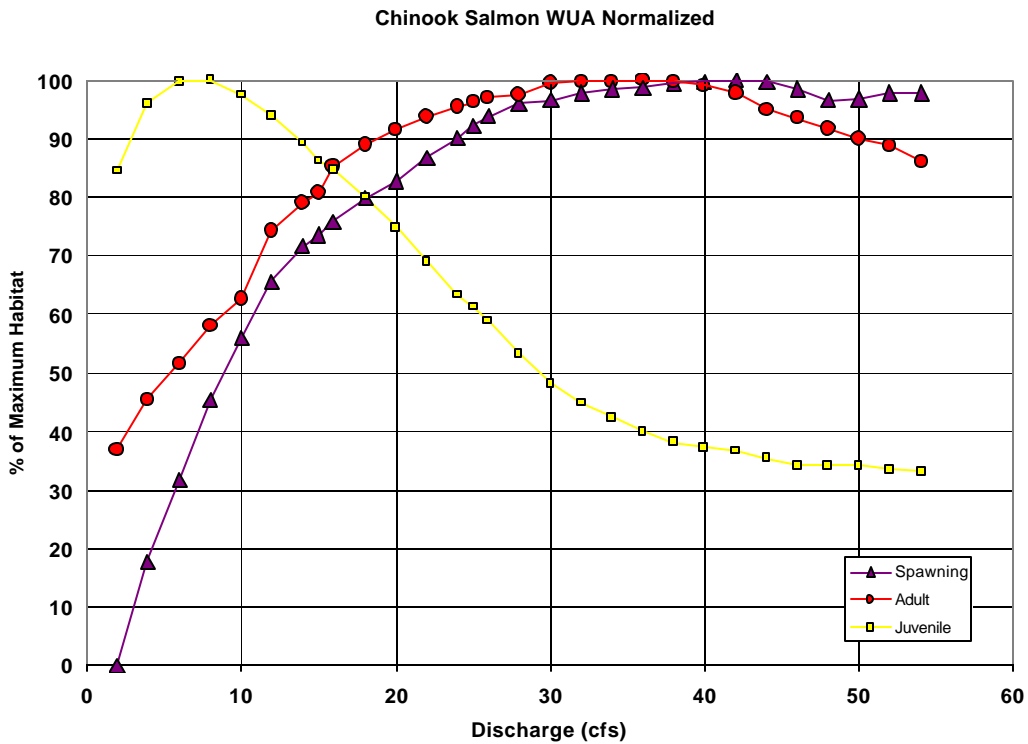


Figure 21. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for Chinook salmon in Big Timber Creek, Study Site 5.

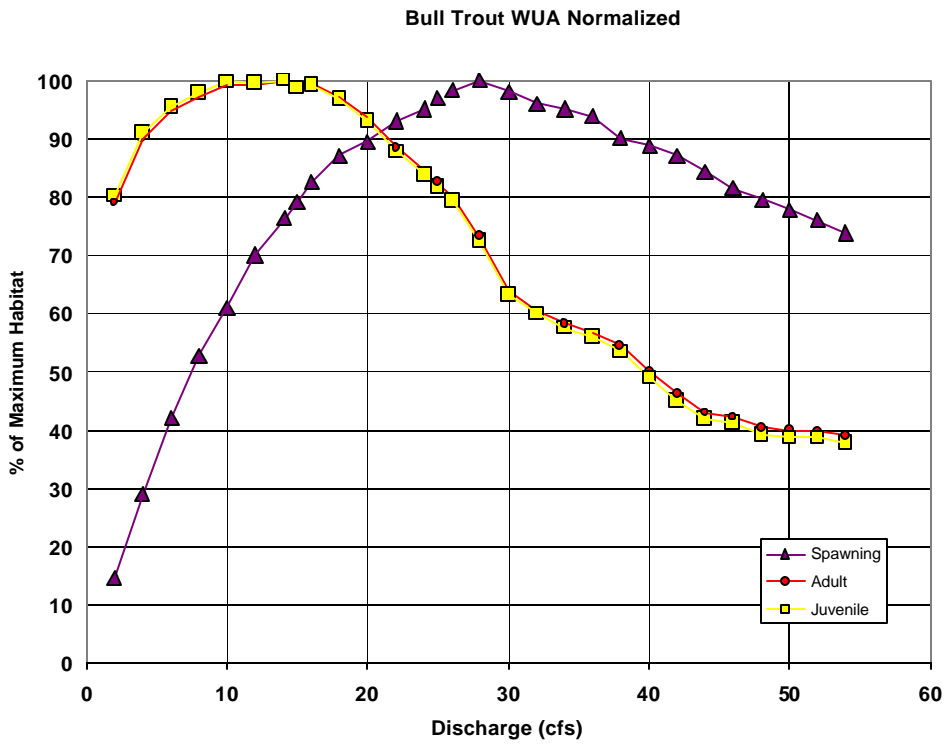


Figure 22. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for bull trout in Big Timber Creek, Study Site 5.

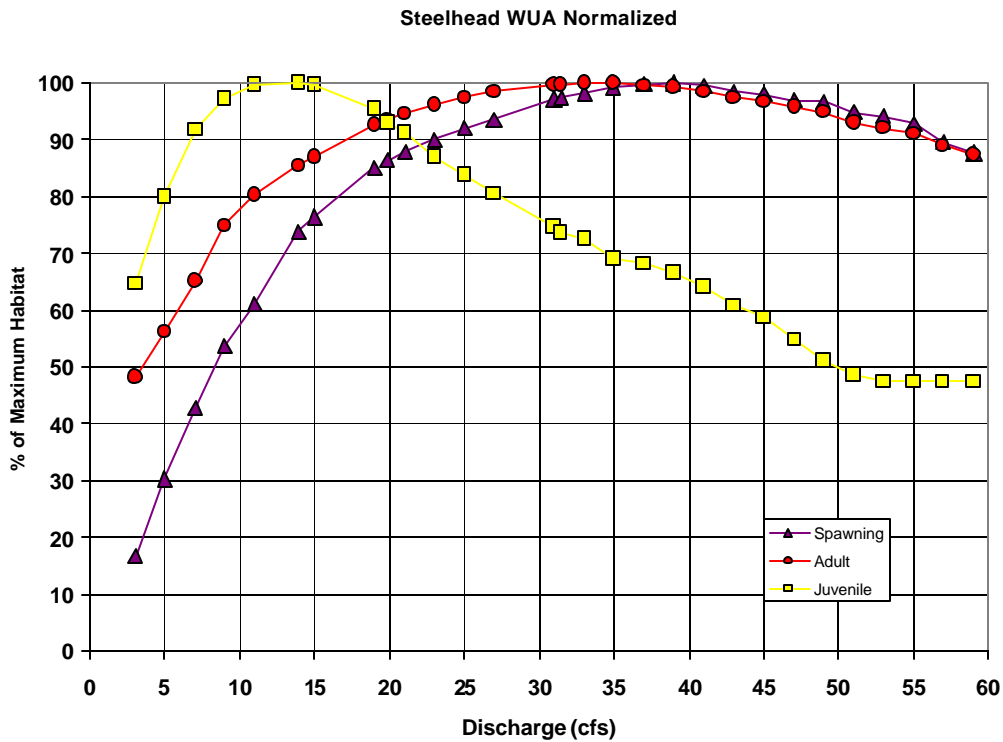


Figure 23. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for steelhead in Big Timber Creek, Study Site 6.

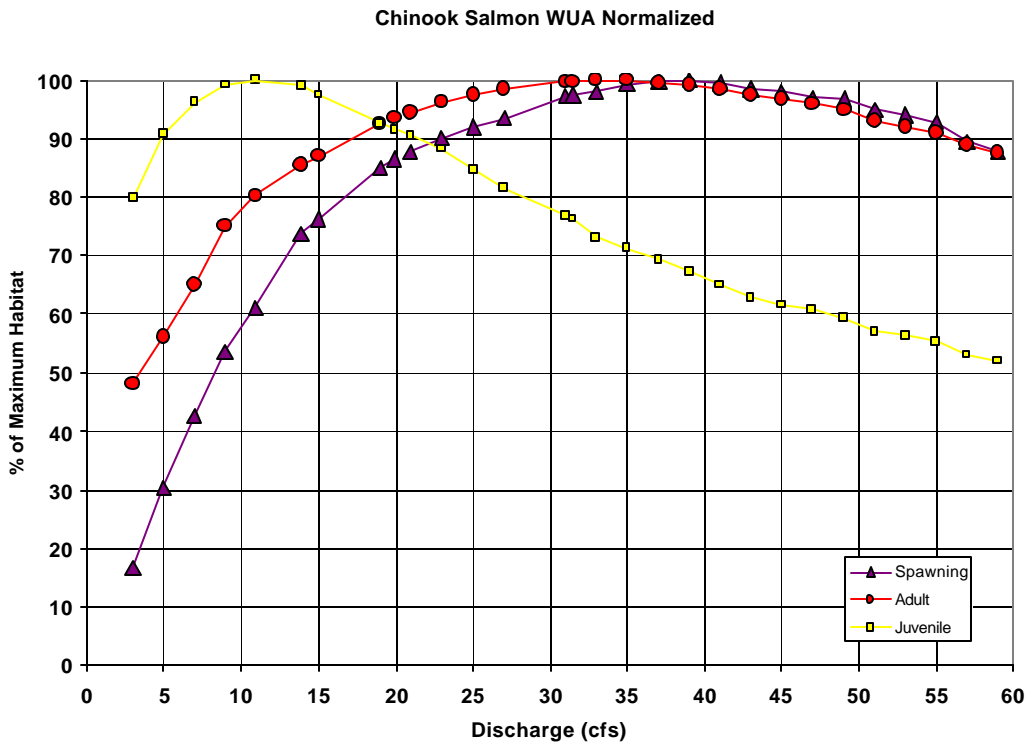


Figure 24. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for Chinook salmon in Big Timber Creek, Study Site 6.

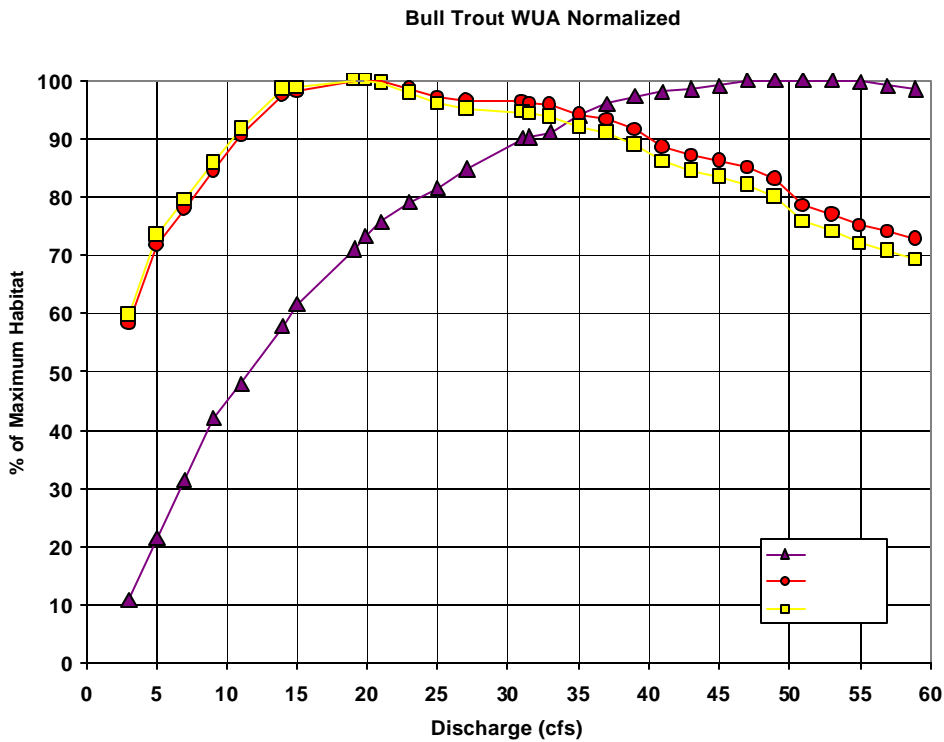


Figure 25. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for bull trout in Big Timber Creek, Study Site 6.

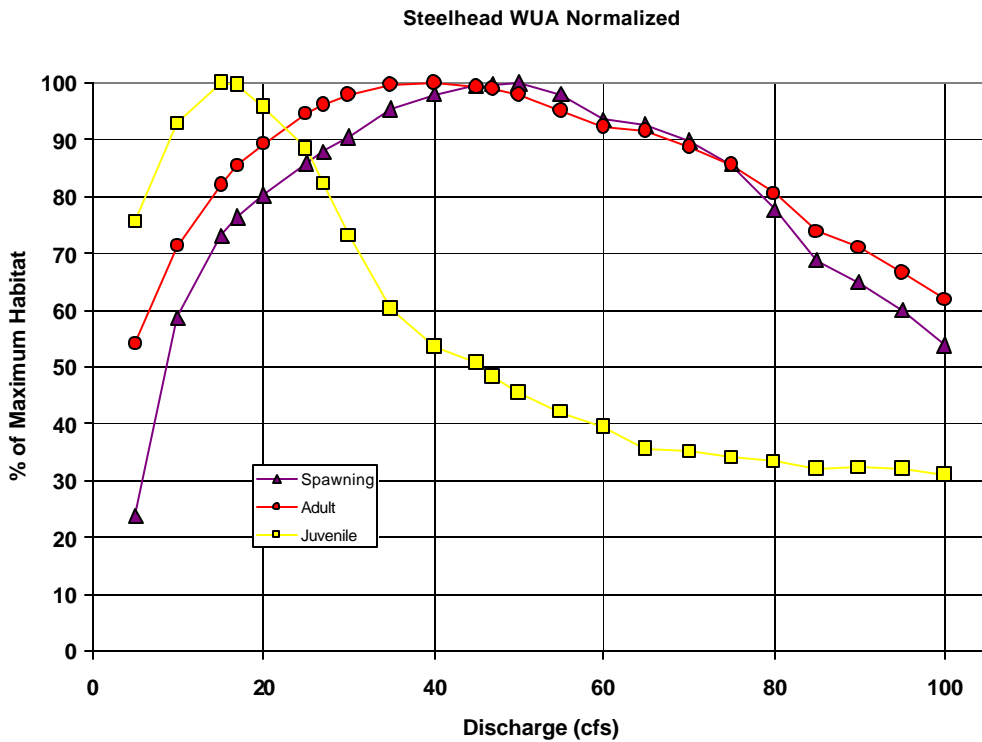


Figure 26. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for steelhead in Big Timber Creek, Reference Site.

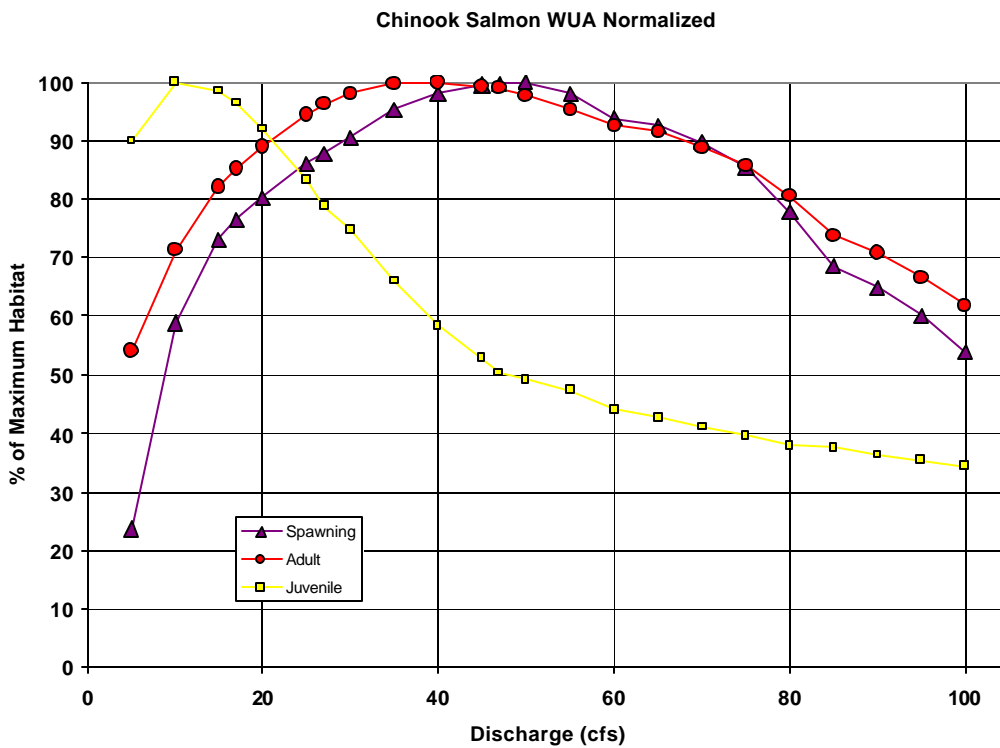


Figure 27. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for Chinook salmon in Big Timber Creek, Reference Site.

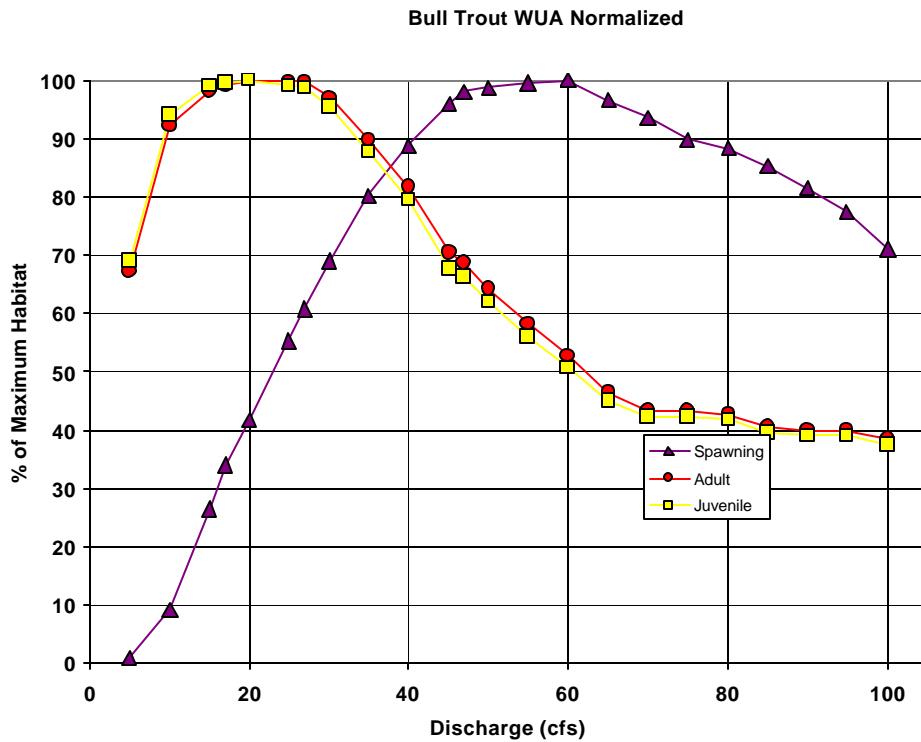


Figure 28. Normalized (% of maximum habitat) weighted usable area (WUA) versus discharge relationships for bull trout in Big Timber Creek, Reference Site.

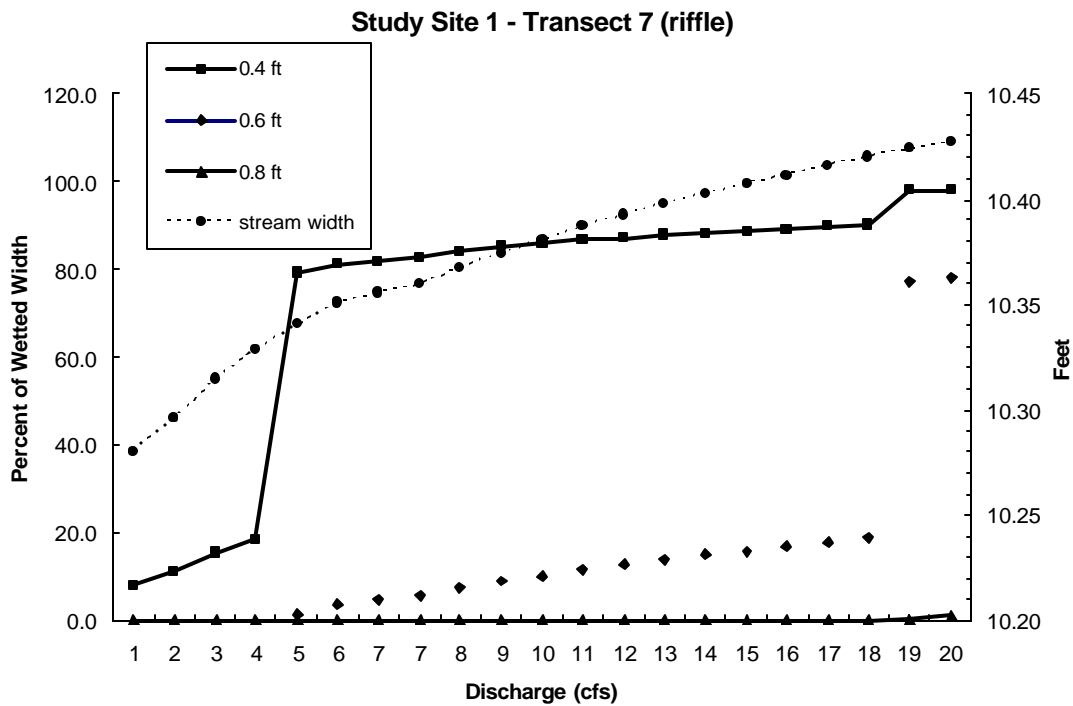


Figure 29. Contiguous widths at depths greater than passage criteria at a riffle transect (56 feet longitudinal distance) on Big Timber Creek, Study Site 1.

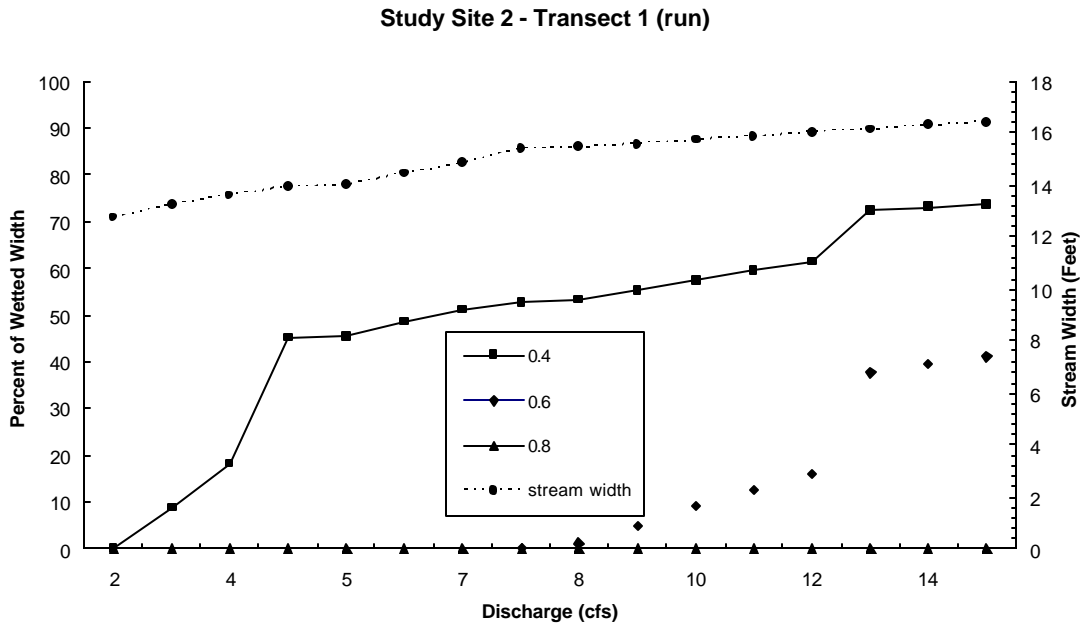


Figure 30. Contiguous widths at depths greater than passage criteria at a run transect (17 feet longitudinal distance) on Big Timber Creek, Study Site 2.

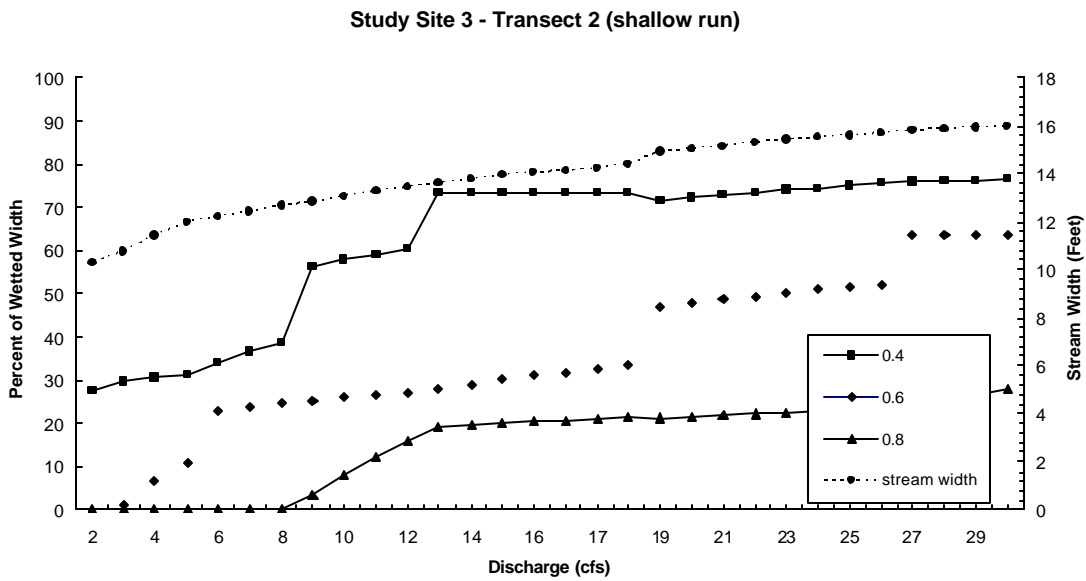


Figure 31. Contiguous widths at depths greater than passage criteria at a run transect (75 feet longitudinal distance) on Big Timber Creek, Study Site 3.

Study Site 4 - Transect 1

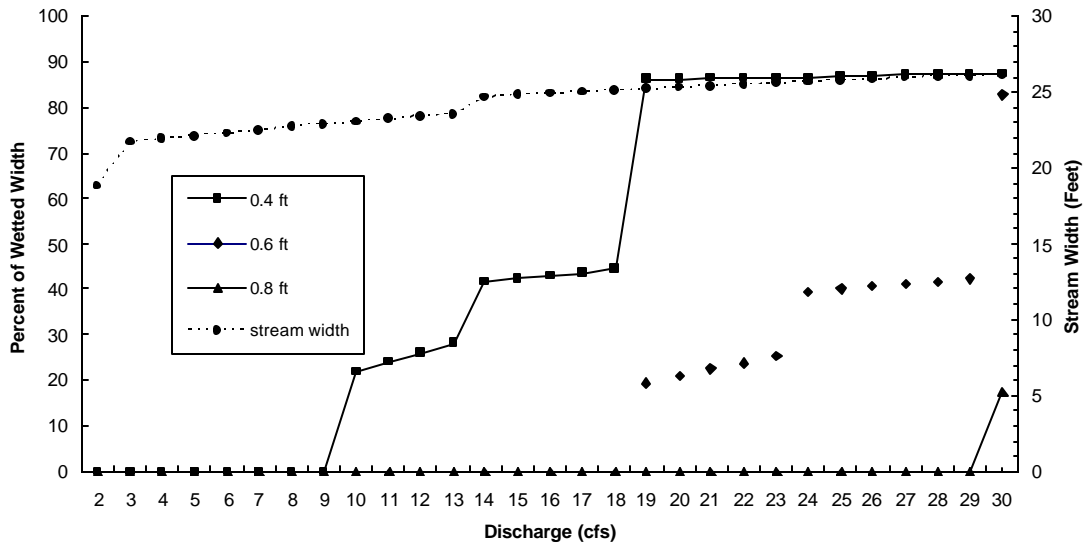


Figure 32. Contiguous widths at depths greater than passage criteria at a riffle transect (17 feet longitudinal distance) on Big Timber Creek, Study Site 4.

Study Site 5 - Transect 5 (riffle)

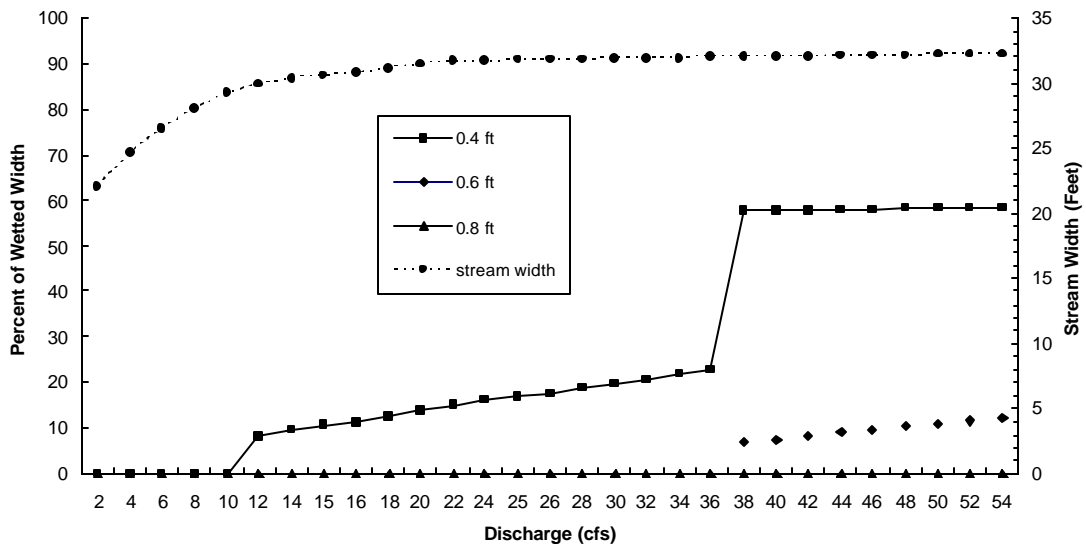


Figure 33. Contiguous widths at depths greater than passage criteria at a riffle transect (30 feet longitudinal distance) on Big Timber Creek, Study Site 5.

Study Site 6 - Transect 7

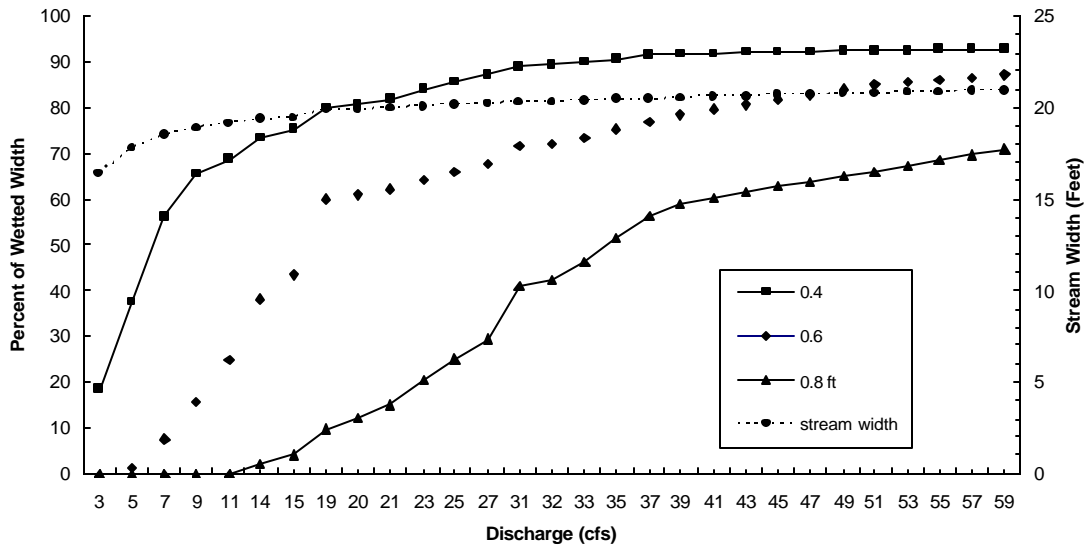


Figure 34. Contiguous widths at depths greater than passage criteria at a shallow run transect (23 feet longitudinal distance) on Big Timber Creek, Study Site 6.

Study Site 7 - Transect 3

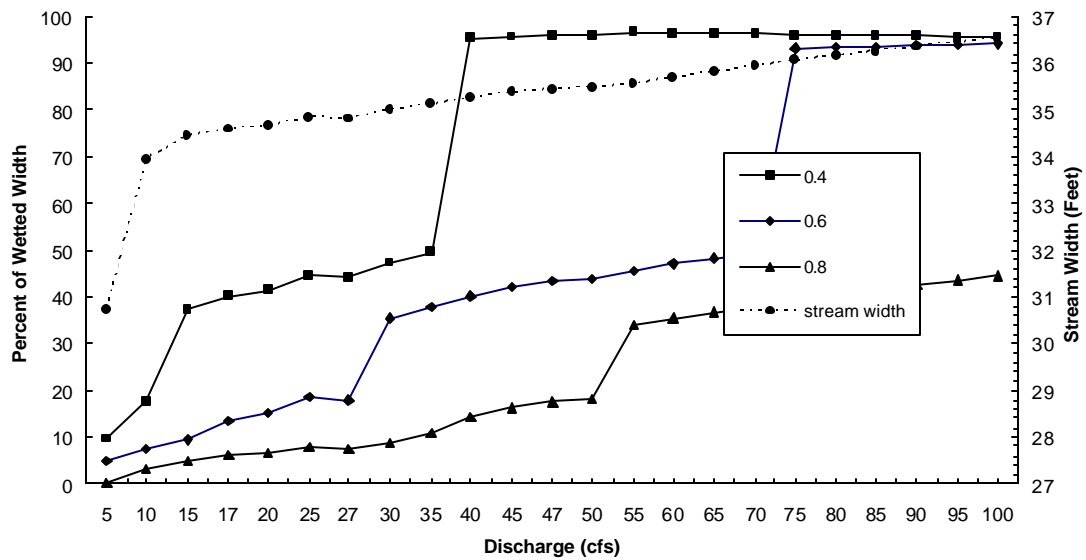


Figure 35. Contiguous widths at depths greater than passage criteria at a riffle transect (22 feet longitudinal distance) on Big Timber Creek, Study Site 7.

Table 13. Habitat modeling summary at Study Site 1 on Big Timber Creek.

| Life Stage | Discharge (cfs) required for optimum weighted usable area (WUA) | | | Discharge (cfs) required for adult salmonid passage using 0.6 foot depth criterion ¹ | |
|------------|---|----------------|------------|---|----------------------------------|
| | Steelhead | Chinook salmon | Bull trout | >25% of total channel width | >10% of contiguous channel width |
| Spawning | 14 | 14 | 10 | NA ² | NA |
| Adult | 18 | 18 | 9 | 13 | 10 |
| Juvenile | 5 | 4 | 5 | NA | NA |

¹ Passage criteria taken from Thompson (1972) and Scott et al. (1981); both width criteria must be met to insure passage.

² NA – Not applicable

Table 14. Habitat modeling summary at Study Site 2 on Big Timber Creek.

| Life Stage | Discharge (cfs) required for optimum weighted usable area (WUA) | | | Discharge (cfs) required for adult salmonid passage using 0.6 foot depth criterion ¹ | |
|------------|---|----------------|------------|---|----------------------------------|
| | Steelhead | Chinook salmon | Bull trout | >25% of total channel width | >10% of contiguous channel width |
| Spawning | >15 | >15 | >15 | NA ² | NA |
| Adult | >15 | >15 | 6 | 13 | 11 |
| Juvenile | 6 | 4 | 6 | NA | NA |

¹ Passage criteria taken from Thompson (1972) and Scott et al. (1981); both width criteria must be met to insure passage.

² NA – Not applicable

Table 15. Habitat modeling summary at Study Site 3 on Big Timber Creek.

| Life Stage | Discharge (cfs) required for optimum weighted usable area (WUA) | | | Discharge (cfs) required for adult salmonid passage using 0.6 foot depth criterion ¹ | |
|------------|---|----------------|------------|---|----------------------------------|
| | Steelhead | Chinook salmon | Bull trout | >25% of total channel width | >10% of contiguous channel width |
| Spawning | 21 | 21 | 15 | NA ² | NA |
| Adult | 16 | 16 | 6 | 9 | 5 |
| Juvenile | 7 | 4 | 6 | NA | NA |

¹ Passage criteria taken from Thompson (1972) and Scott et al. (1981); both width criteria must be met to insure passage.

² NA – Not applicable

Table 16. Habitat modeling summary at Study Site 4 on Big Timber Creek.

| Life Stage | Discharge (cfs) required for optimum weighted usable area (WUA) | | | Discharge (cfs) required for adult salmonid passage using 0.6 foot depth criterion ¹ | |
|------------|---|----------------|------------|---|----------------------------------|
| | Steelhead | Chinook salmon | Bull trout | >25% of total channel width | >10% of contiguous channel width |
| Spawning | 28 | 28 | 29 | NA ² | NA |
| Adult | 27 | 27 | 24 | 19 | 19 |
| Juvenile | 11 | 8 | 23 | NA | NA |

¹ Passage criteria taken from Thompson (1972) and Scott et al. (1981); both width criteria must be met to insure passage.

² NA – Not applicable

Table 17. Habitat modeling summary at Study Site 5 on Big Timber Creek.

| Life Stage | Discharge (cfs) required for optimum weighted usable area (WUA) | | | Discharge (cfs) required for adult salmonid passage using 0.6 foot depth criterion ¹ | |
|------------|---|----------------|------------|---|----------------------------------|
| | Steelhead | Chinook salmon | Bull trout | >25% of total channel width | >10% of contiguous channel width |
| Spawning | 42 | 42 | 28 | NA ² | NA |
| Adult | 36 | 36 | 14 | >54 | 48 |
| Juvenile | 12 | 8 | 14 | NA | NA |

¹ Passage criteria taken from Thompson (1972) and Scott et al. (1981); both width criteria must be met to insure passage.

² NA – Not applicable

Table 18. Habitat modeling summary at Study Site 6 on Big Timber Creek.

| Life Stage | Discharge (cfs) required for optimum weighted usable area (WUA) | | | Discharge (cfs) required for adult salmonid passage using 0.6 foot depth criterion ¹ | |
|------------|---|----------------|------------|---|----------------------------------|
| | Steelhead | Chinook salmon | Bull trout | >25% of total channel width | >10% of contiguous channel width |
| Spawning | 39 | 39 | 49 | NA ² | NA |
| Adult | 35 | 35 | 20 | 11 | 9 |
| Juvenile | 14 | 11 | 19 | NA | NA |

¹ Passage criteria taken from Thompson (1972) and Scott et al. (1981); both width criteria must be met to insure passage.

² NA – Not applicable

Table 19. Habitat modeling summary at Study Site 7 (Reference Site) on Big Timber Creek.

| Life Stage | Discharge (cfs) required for optimum weighted usable area (WUA) | | | Discharge (cfs) required for adult salmonid passage using 0.6 foot depth criterion ¹ | |
|------------|---|----------------|------------|---|----------------------------------|
| | Steelhead | Chinook salmon | Bull trout | >25% of total channel width | >10% of contiguous channel width |
| Spawning | 50 | 50 | 60 | NA ² | NA |
| Adult | 40 | 40 | 20 | 15 | 17 |
| Juvenile | 15 | 10 | 20 | NA | NA |

¹ Passage criteria taken from Thompson (1972) and Scott et al. (1981); both width criteria must be met to insure passage.

² NA – Not applicable

6.0 ACKNOWLEDGEMENTS

We thank the numerous representatives from various organizations who contributed to the success of this project. Al Simpson of Reclamation and Greg Lowell of IDFG provided valuable assistance in obtaining landowner permission on private land. Joe Spinazola of Reclamation contributed to the planning and funding of the study. Jim Henriksen of USGS provided quality control of the PHABSIM modeling. Terry Maret, John Hortness, Joseph Bunt, and Alvin Sablan assisted with obtaining valuable hydrology data. Patrick Murphy of IDFG provided recently collected fishery data for Big Timber Creek. Dudley Reiser of R2 Resource Consultants provided useful information on previous PHABSIM work completed for BIA. Representatives on the Interagency Technical Workgroup organized by Reclamation also provided guidance, including Cynthia Robertson (IDFG), Jim Morrow and Donald Anderson (NOAA Fisheries), Jana Brimmer (FWS), and Jude Trapani (BLM).

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Appendix A – Reach and Study Site Descriptions and Photos

Reach 1: This reach extended from the confluence with the Lemhi River upstream to the first major diversion (N44.67760186 W113.3700417) that dewateres the stream channel during the irrigation season. The study site for this reach was located downstream from the dewatered channel where the stream was fed only by groundwater seeps on private property. The stream channel was narrower in this reach than the other reaches.

Study Site 1 - Most downstream study site (N44.69674 W113.37238)

Transect 1 – run (most downstream transect)

Transect 2 – hydraulic control

Transect 3 – pool

Transect 4 – pool

Transect 5 – hydraulic control

Transect 6 – pool

Transect 7 – riffle/passage

Transect 8 – run (most upstream transect)



Reach 2: This reach extended from the upstream diversion boundary for reach 1 upstream to another major diversion (N44.66095604 W113) on and BLM property. The study site for this reach was represented by low gradient riffles and runs.

Study Site 2 (N44.670527 W113.371053)

- Transect 1 – low gradient run/passage (most downstream transect)
- Transect 2 – run
- Transect 3 – run
- Transect 4 – low gradient riffle (most upstream transect)



Reach 3: This reach was located between two major diversions that defined the upstream and downstream boundaries of reaches 2 and 4, respectively. The study site for this reach was located on BLM property just downstream from a bridge crossing.

Study Site 3 (N44.66358 W113.37464)

- Transect 1 – riffle (most downstream transect)
- Transect 2 – run/passage
- Transect 3 – narrow run
- Transect 4 – riffle
- Transect 5 – deep run (most upstream transect)



Reach 4: This reach extended from a relatively new major diversion (N44.660844 W113.377399) located upstream from the bridge crossing upstream to the confluence with Little Timber Creek (N44.64249705 W113.3831149). The study site for this reach was located on private property and represented a mixture of riffle, run, and pool habitat types.

Study Site 4 (N44.653344 W113.381240)

Transect 1 – hydraulic control/passage (most downstream transect)

Transect 2 – run/shallow pool

Transect 3 – run

Transect 4 – run

Transect 5 – high gradient riffle

Transect 6 – moderate gradient riffle

Transect 7 – hydraulic control

Transect 8 – pool (most upstream transect)



Reach 5: This reach was located between the confluence with Little Timber Creek and the next major upstream diversion (N44.620541 W113). This reach was characterized by beaver dams mixed with riffle, run, and pool habitats. Riparian vegetation was dominated by willows. The study site represented the riffles, runs, and pools within this reach.

Study Site 5 (N44.624548 W113.394656)

Transect 1 – hydraulic control/ riffle (most downstream transect)

Transect 2 – run/shallow pool

Transect 3 – pool

Transect 4 – high gradient riffle

Transect 5 – moderate gradient riffle/passage (most upstream transect)



Reach 6: This reach was located between the upstream diversion boundary for reach 5 upstream to the Cary Act Diversion (N44.61482736 W113.3967245) and Pipe Diversion (N44.613771 W113.397011). This reach had similar habitat characteristics as reach 5, including blown-out beaver dams and excellent riparian vegetation. The study site in this reach represented a mixture of riffles, runs, and pools.

Study Site 6 (N44.620337 W113.396056)

Transect 1 – hydraulic control (most downstream transect)

Transect 2 – run/shallow pool

Transect 3 – moderate gradient riffle

Transect 4 – hydraulic control

Transect 5 – pool

Transect 6 – high gradient riffle

Transect 7 – run/passage (most upstream transect)



Reach 7: The reach was located between the Pipe Diversion upstream to Basin Creek (N44.608750 W113.393787) and represented Big Timber Creek undisturbed by diversion structures. The study site represented natural flow conditions immediately upstream from the major diversions on Big Timber Creek.

Study Site 7 (Reference) (N44.610365 W113.398288) (undisturbed) – most upstream study site

Transect 1 – run (most downstream transect)

Transect 2 – high gradient riffle

Transect 3 – hydraulic control/passage

Transect 4 – pool

Transect 5 – plunge/chute (most upstream transect)



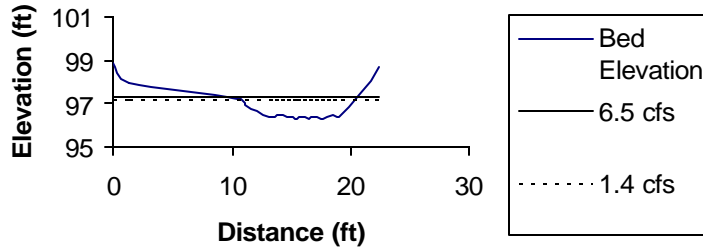
Appendix B – Habitat Mapping Proportions

| | DISTANCE MAPPED | PROPORTIONS |
|------------------------|-----------------|-------------|
| Study site 1 | (FEET) | (%) |
| LOW GRADIENT RIFFLE | 479 | 38 |
| POOL | 638 | 51 |
| RUN | 133 | 11 |
| TOTAL | 1250 | 100 |
| Study sites 2 and 3 | | |
| MOD GRADIENT RIFFLE | 961 | 54 |
| DEEP RUN | 209 | 12 |
| RUN | 607 | 34 |
| TOTAL | 1777 | 100 |
| Study site 4 | | |
| HIGH GRADIENT RIFFLE | 308 | 13 |
| MOD GRADIENT RIFFLE | 698 | 31 |
| POOL | 167 | 7 |
| RUN | 1106 | 49 |
| TOTAL | 2279 | 100 |
| Study site 5 | | |
| HIGH GRADIENT RIFFLE | 419 | 21 |
| MOD GRADIENT RIFFLE | 798 | 40 |
| POOL | 206 | 10 |
| RUN | 580 | 29 |
| TOTAL | 2003 | 100 |
| Study site 6 | | |
| HIGH GRADIENT RIFFLE | 463 | 7 |
| MOD GRADIENT RIFFLE | 2477 | 37 |
| POOL | 639 | 10 |
| RUN | 3065 | 46 |
| TOTAL | 6644 | 100 |
| Study site 7 REFERENCE | | |
| HIGH GRADIENT RIFFLE | 1211 | 56 |
| POOL | 1657 | 7 |
| RUN | 671 | 31 |
| PLUNGE | 129 | 6 |
| TOTAL | 2176 | 100 |

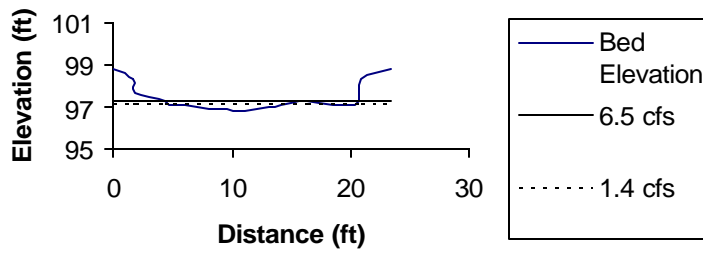
Appendix C – Cross-sectional Profiles and Measured Water Surface Elevations

Site 1

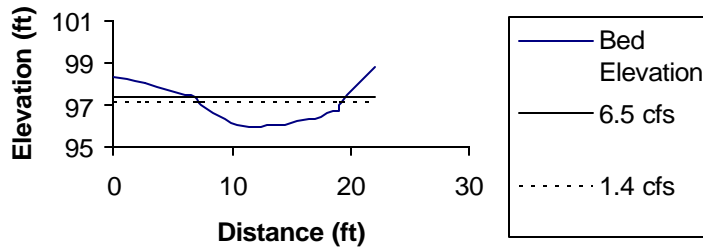
Transect 1



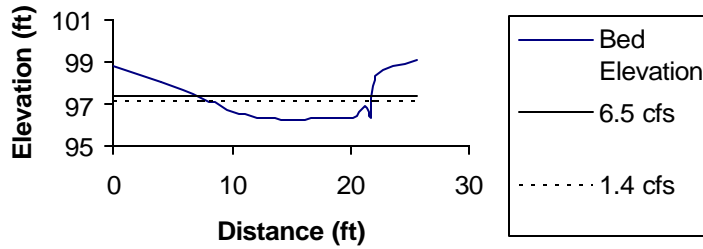
Transect 2



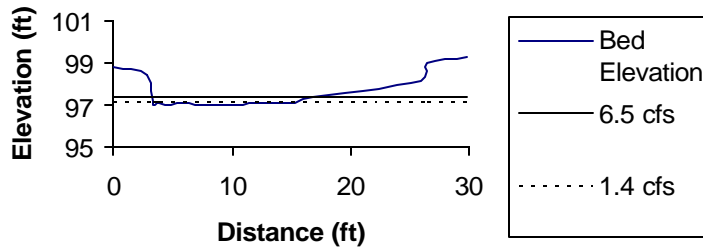
Transect 3



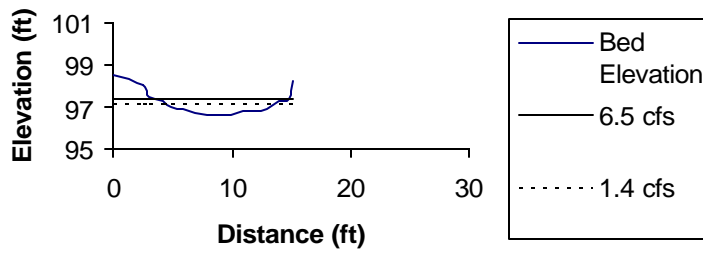
Transect 4



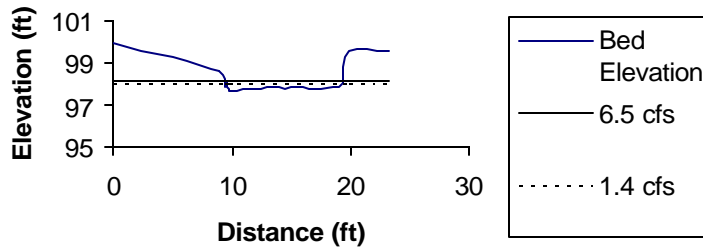
Transect 5



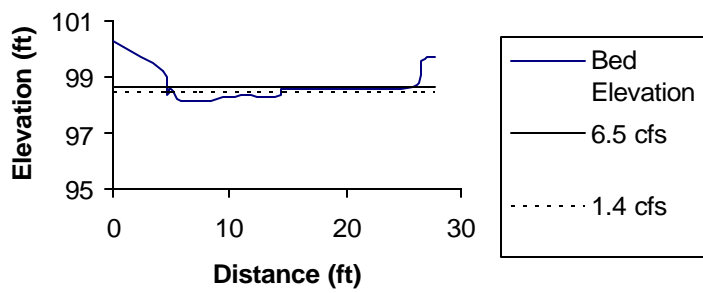
Transect 6



Transect 7

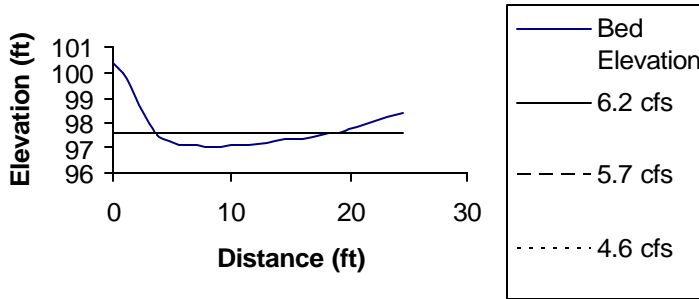


Transect 8

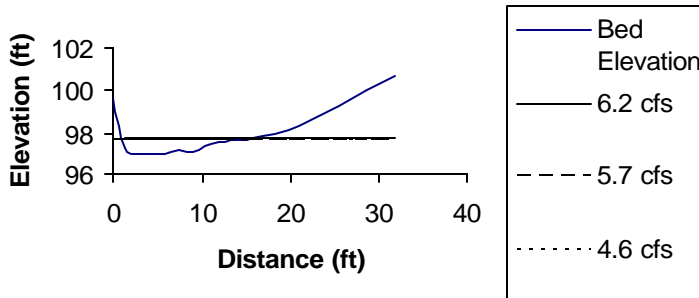


Site 2

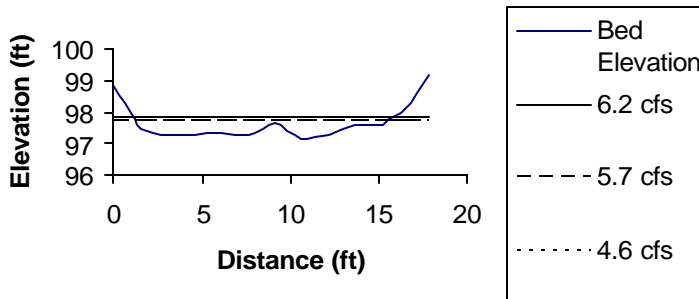
Transect 1



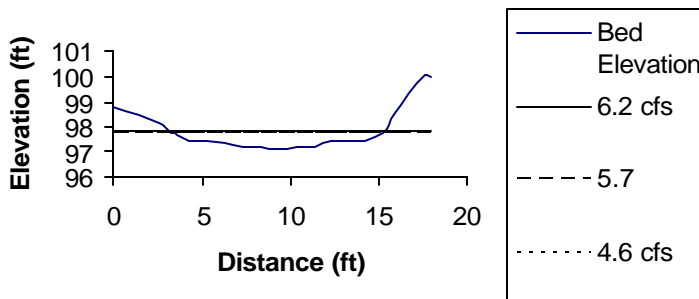
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Transect 3

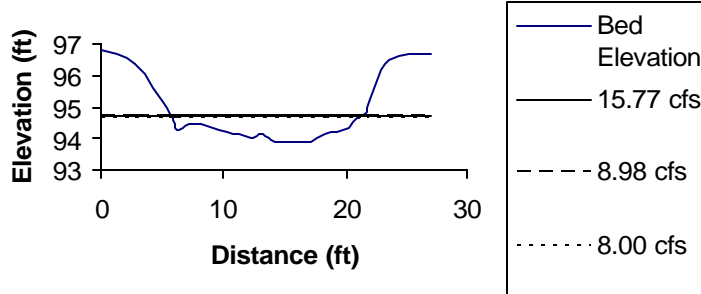


Transect 4

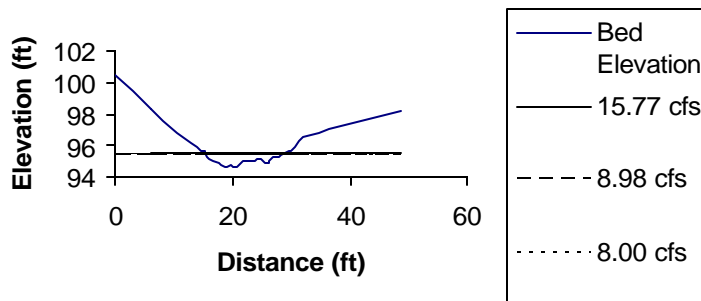


Site 3

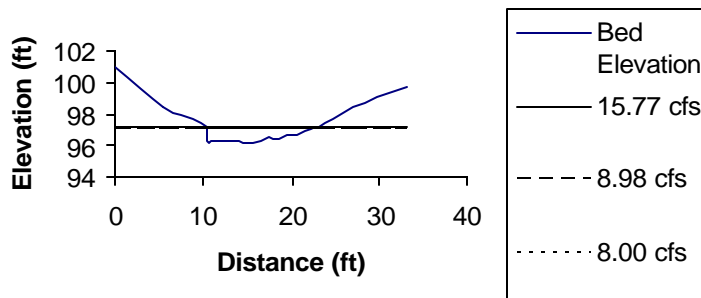
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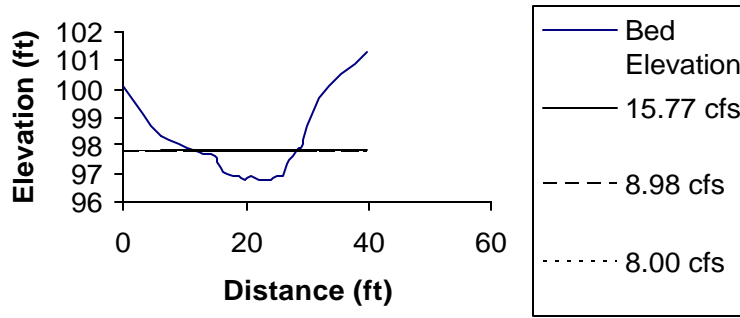
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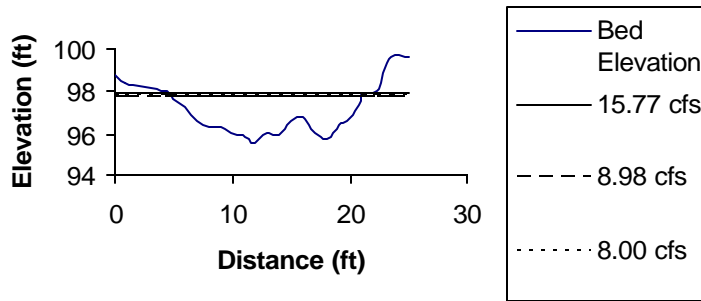
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Transect 4

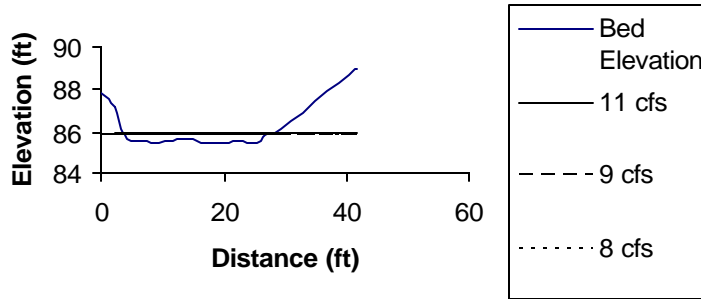


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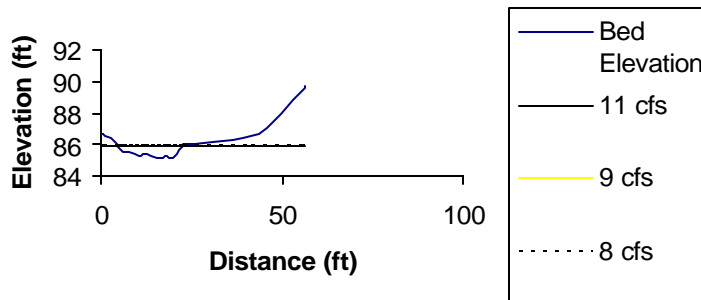


Site 4

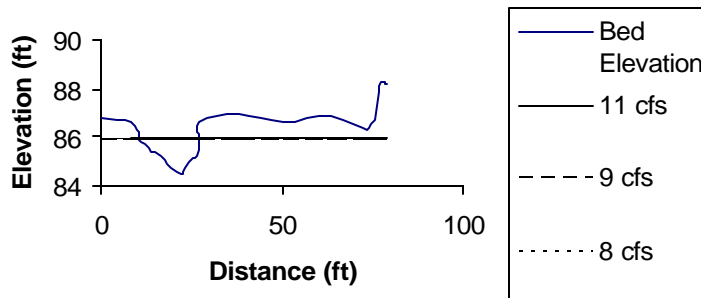
Transect 1



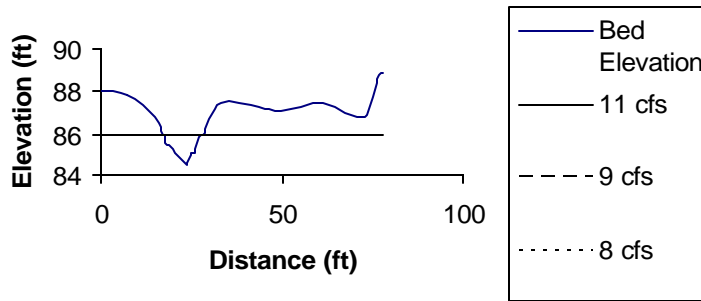
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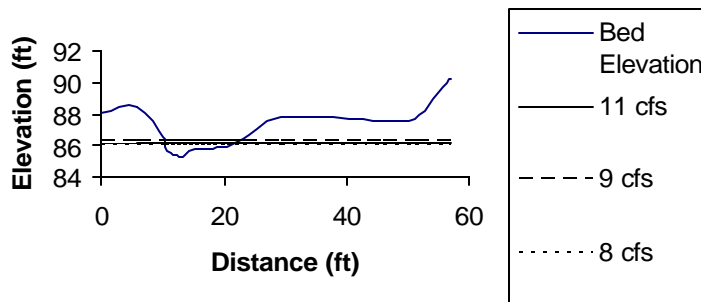
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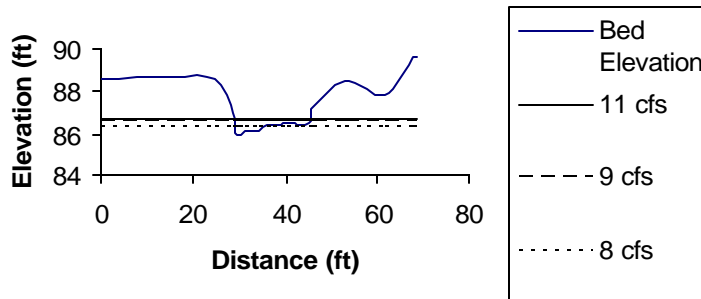
Transect 4



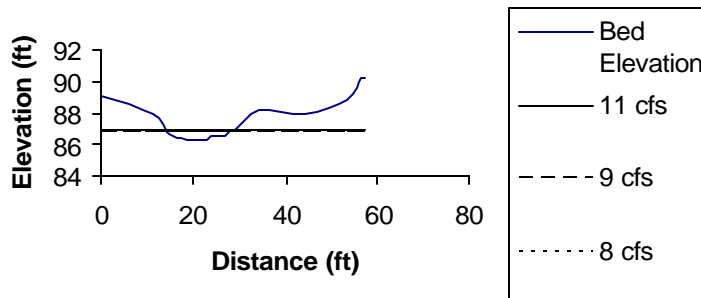
Transect 5



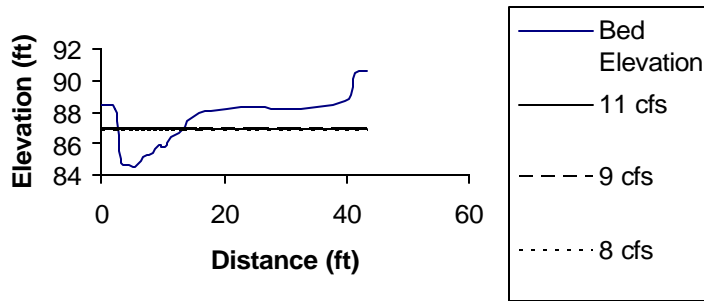
Transect 6



Transect 7

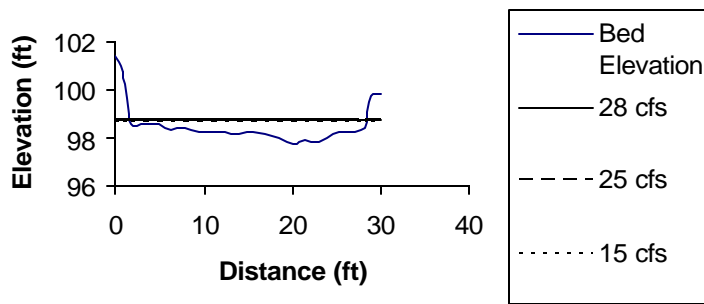


Transect 8

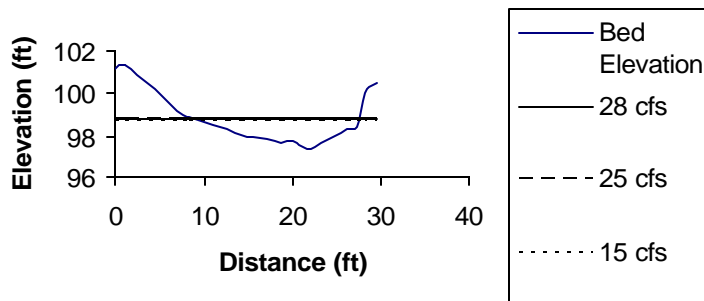


Site 5

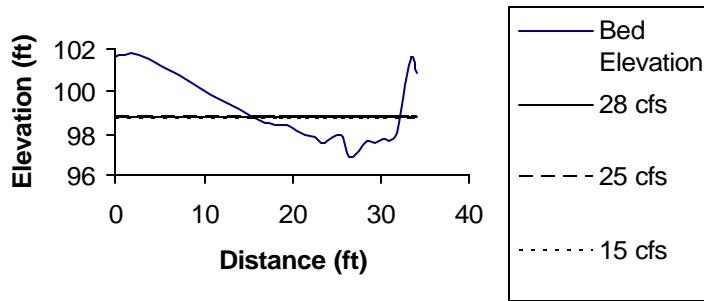
Transect 1



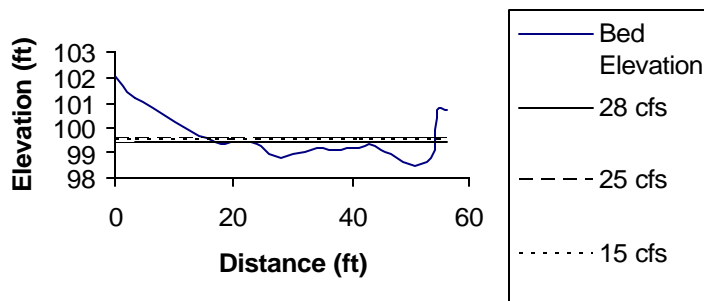
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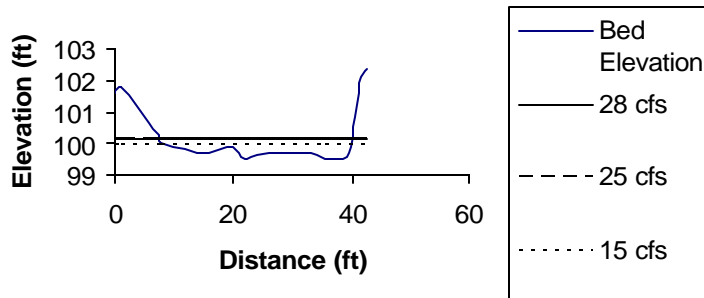
Transect 3



Transect 4

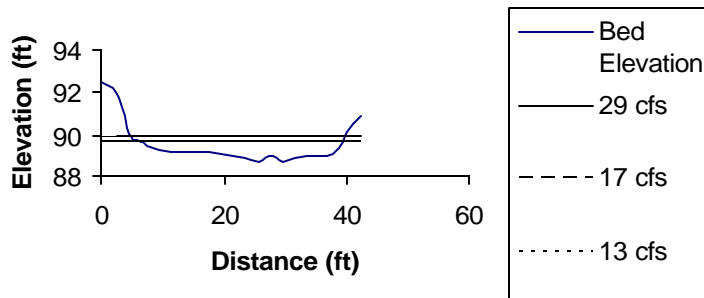


Transect 5

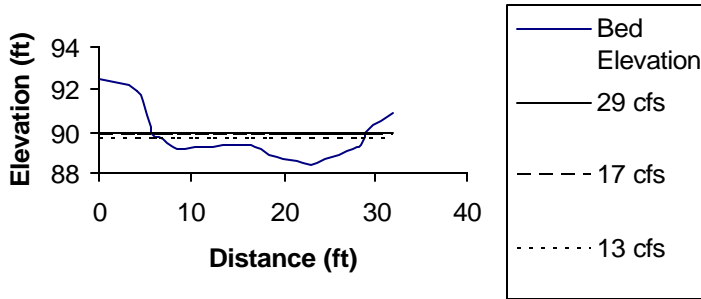


Site 6

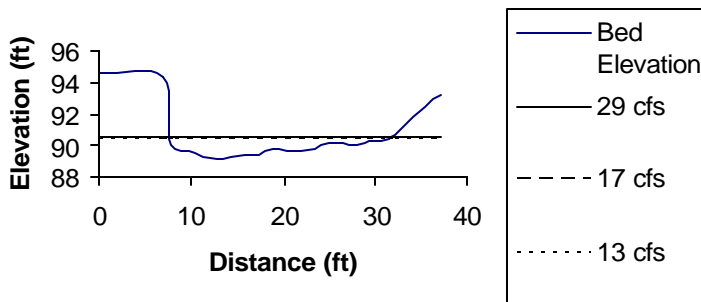
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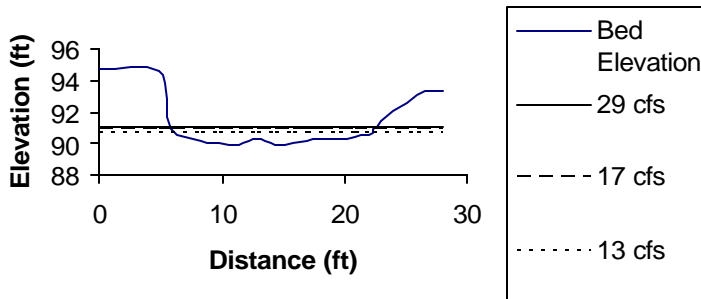
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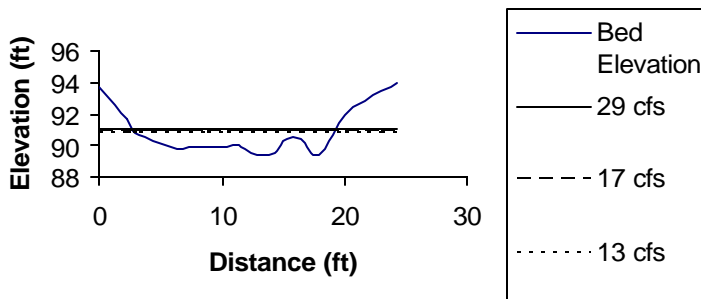
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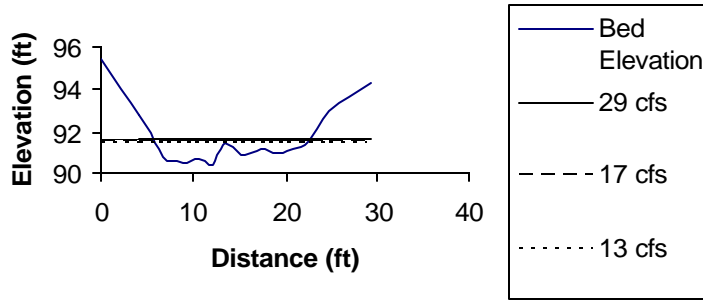
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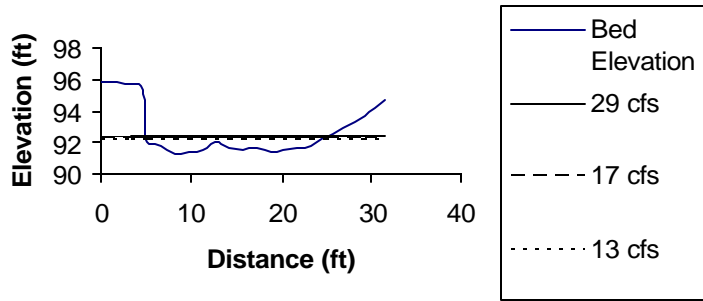
Transect 5



Transect 6

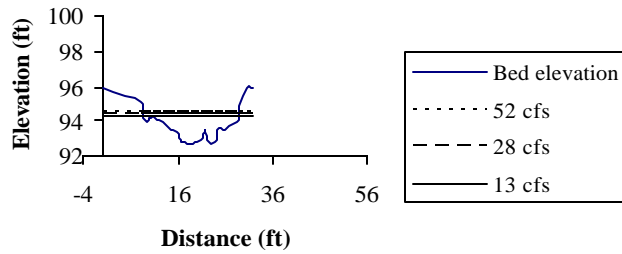


Transect 7

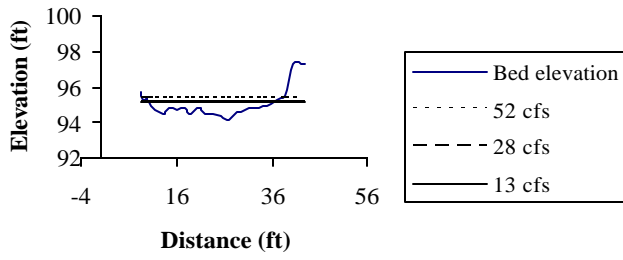


Reference Site

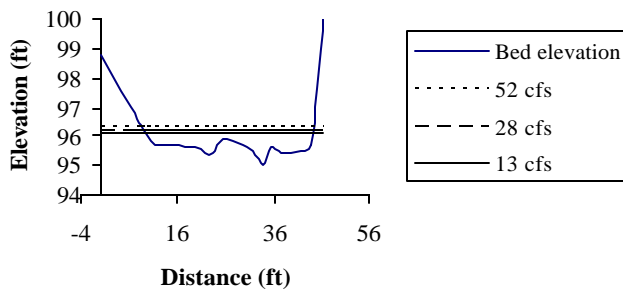
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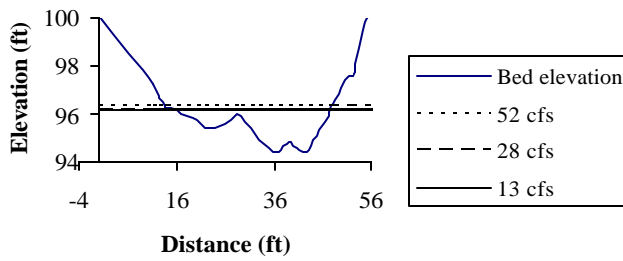
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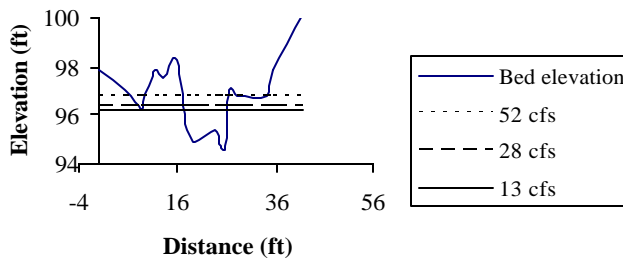
Transect 3



Transect 4



Transect 5



Appendix D – Hydraulic Calibration Results

Table D-1 Water surface elevation calibration results (ft) for Big Timber Cr. Site 1 using the WSP (transects 2-6) and STGQ (transects 1,7,8) models.

| Transect | Distance from next downstream transect (ft) | Water surface elevations (ft) | | | | | |
|----------|---|-------------------------------|-----------|------------|----------|-----------|------------|
| | | 1.4 cfs | | | 6.5 cfs | | |
| | | Measured | Simulated | Difference | Measured | Simulated | Difference |
| 1 | 0 | 97.13 | 97.13 | 0.000 | 97.35 | 97.35 | 0.000 |
| 2 | 12 | 97.14 | 97.14 | 0.000 | 97.36 | 97.36 | 0.000 |
| 3 | 25 | 97.15 | 97.145 | -0.005 | 97.42 | 97.419 | -0.001 |
| 4 | 43 | 97.16 | 97.147 | -0.013 | 97.44 | 97.431 | -0.009 |
| 5 | 21 | 97.17 | 97.17 | 0.000 | 97.45 | 97.45 | 0.000 |
| 6 | 9 | 97.18 | 97.177 | -0.003 | 97.46 | 97.459 | -0.001 |
| 7 | 69 | 97.98 | 97.98 | 0.000 | 98.15 | 98.15 | 0.000 |
| 8 | 43 | 98.45 | 98.45 | 0.000 | 98.70 | 98.70 | 0.000 |

Table D-2 Water surface elevation calibration results (ft) for Big Timber Cr. Site 2 using the STGQ model.

| Transect | Distance from next downstream transect (ft) | Water surface elevations (ft) | | | | | | | | |
|----------|---|-------------------------------|-----------|------------|----------|-----------|------------|----------|-----------|------------|
| | | 4.9 cfs | | | 6.0 cfs | | | 8.2 cfs | | |
| | | Measured | Simulated | Difference | Measured | Simulated | Difference | Measured | Simulated | Difference |
| 1 | 0 | 97.51 | 97.51 | 0.00 | 97.56 | 97.55 | -0.01 | 97.60 | 97.61 | 0.01 |
| 2 | 17 | 97.58 | 97.56 | -0.02 | 97.59 | 97.61 | 0.02 | 97.70 | 97.70 | 0.00 |
| 3 | 27 | 97.74 | 97.74 | 0.00 | 97.78 | 97.77 | -0.01 | 97.80 | 97.81 | 0.01 |
| 4 | 9 | 97.80 | 97.80 | 0.00 | 97.81 | 97.82 | 0.01 | 97.85 | 97.85 | 0.00 |

Table D-3 Water surface elevation calibration results (ft) for Big Timber Cr. Site 3 using the STGQ model.

| Transect | Distance from next downstream transect (ft) | Water surface elevations (ft) | | | | | | | | |
|----------|---|-------------------------------|-----------|------------|----------|-----------|------------|----------|-----------|------------|
| | | 8.0 cfs | | | 9.0 cfs | | | 15.8 cfs | | |
| | | Measured | Simulated | Difference | Measured | Simulated | Difference | Measured | Simulated | Difference |
| 1 | 0 | 94.70 | 94.70 | 0.00 | 94.72 | 94.71 | -0.01 | 94.74 | 94.74 | 0.00 |
| 2 | 75 | 95.41 | 95.39 | -0.02 | 95.40 | 95.42 | 0.02 | 95.55 | 95.55 | 0.00 |
| 3 | 75 | 97.13 | 97.13 | 0.01 | 97.16 | 97.14 | -0.02 | 97.19 | 97.20 | 0.01 |
| 4 | 40 | 97.71 | 97.72 | 0.01 | 97.75 | 97.73 | -0.01 | 97.82 | 97.82 | 0.00 |
| 5 | 8 | 97.81 | 97.81 | 0.00 | 97.83 | 97.83 | 0.00 | 97.93 | 97.93 | 0.00 |

Table D-4 Water surface elevation calibration results (ft) for Big Timber Cr. Site 4 using the WSP (transects 1-5, 7- 8) and STGQ (transect 6) models.

| Transect | Distance from next downstream transect (ft) | 8.0 cfs | | | 9.0 cfs | | | 11.0 cfs | | |
|----------|---|-------------------------------|-----------|------------|----------|-----------|------------|----------|-----------|------------|
| | | Measured | Simulated | Difference | Measured | Simulated | Difference | Measured | Simulated | Difference |
| | | Water surface elevations (ft) | | | | | | | | |
| 1 | 0 | 85.78 | 85.78 | 0.00 | 85.79 | 85.79 | 0.00 | 85.85 | 85.85 | 0.00 |
| 2 | 17 | 85.82 | 85.83 | 0.01 | 85.84 | 85.84 | 0.00 | 85.90 | 85.90 | 0.00 |
| 3 | 31 | 85.84 | 85.85 | 0.01 | 85.84 | 85.87 | 0.03 | 85.91 | 85.94 | 0.03 |
| 4 | 34 | 85.88 | 85.87 | -0.01 | 85.90 | 85.89 | -0.01 | 85.96 | 85.96 | 0.00 |
| 5 | 50 | 86.00 | 86.01 | 0.01 | 86.06 | 86.04 | -0.02 | 86.09 | 86.10 | 0.01 |
| 6 | 26 | 86.69 | 86.68 | -0.01 | 86.70 | 86.71 | 0.01 | 86.76 | 86.76 | 0.00 |
| 7 | 12 | 86.88 | 86.88 | 0.00 | 86.90 | 86.90 | 0.00 | 86.96 | 86.96 | 0.00 |
| 8 | 21 | 86.89 | 86.91 | 0.02 | 86.90 | 86.94 | 0.04 | 86.98 | 87.00 | 0.02 |

Table D-5 Water surface elevation calibration results (ft) for Big Timber Cr. Site 5 using the WSP (transects 1, 2, 3) and STGQ (transects 4-5) models.

| Transect | Distance from next downstream transect (ft) | 15.0 cfs | | | 25.0 cfs | | | 28.0 cfs | | |
|----------|---|-------------------------------|-----------|------------|----------|-----------|------------|----------|-----------|------------|
| | | Measured | Simulated | Difference | Measured | Simulated | Difference | Measured | Simulated | Difference |
| | | Water surface elevations (ft) | | | | | | | | |
| 1 | 0 | 98.68 | 98.68 | 0.00 | 98.72 | 98.72 | 0.00 | 98.73 | 98.73 | 0.00 |
| 2 | 19 | 98.77 | 98.72 | -0.05 | 98.84 | 98.81 | -0.03 | 98.86 | 98.84 | -0.02 |
| 3 | 13 | 98.74 | 98.74 | 0.00 | 98.84 | 98.85 | 0.01 | 98.86 | 98.88 | 0.02 |
| 4 | 16 | 99.40 | 99.40 | 0.00 | 99.49 | 99.49 | 0.00 | 99.51 | 99.51 | 0.00 |
| 5 | 30 | 99.95 | 99.95 | 0.00 | 100.03 | 100.03 | 0.00 | 100.05 | 100.05 | 0.00 |

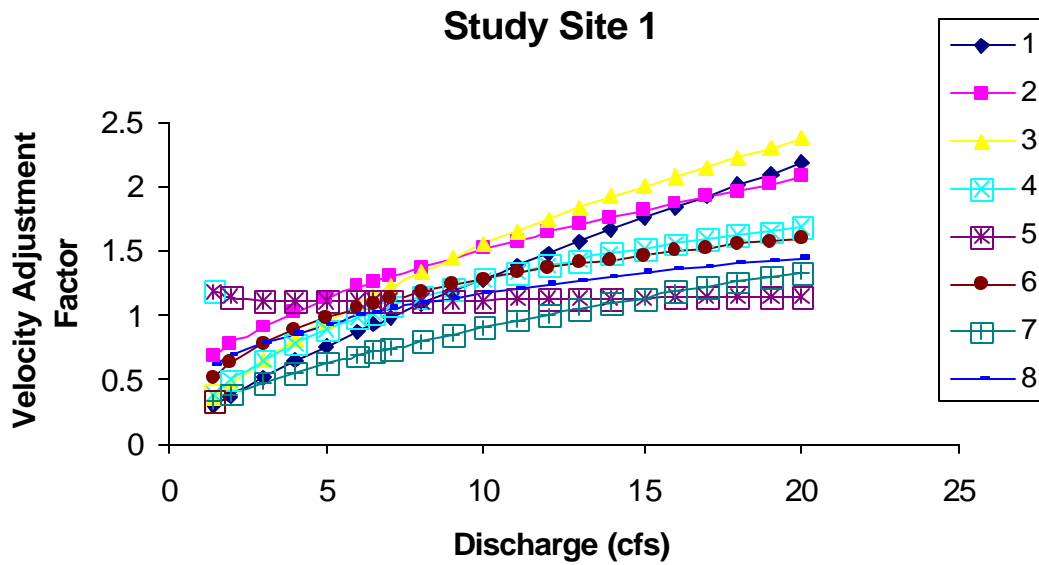
Table D-6 Water surface elevation calibration results (ft) for Big Timber Cr. Site 6 using the WSP (transects 4,5) and STGQ (transects 1,2,3,6,7) models.

| Transect | Distance from next downstream transect (ft) | 13.9 cfs | | | 19.9 cfs | | | 31.5 cfs | | |
|----------|---|-------------------------------|-----------|------------|----------|-----------|------------|----------|-----------|------------|
| | | Measured | Simulated | Difference | Measured | Simulated | Difference | Measured | Simulated | Difference |
| | | Water surface elevations (ft) | | | | | | | | |
| 1 | 0 | 89.59 | 89.59 | 0.00 | 89.72 | 89.72 | 0.00 | 89.92 | 89.92 | 0.00 |
| 2 | 38 | 89.66 | 89.67 | 0.01 | 89.82 | 89.80 | -0.02 | 89.97 | 89.98 | 0.01 |
| 3 | 40 | 90.44 | 90.42 | -0.02 | 90.46 | 90.49 | 0.03 | 90.59 | 90.59 | 0.00 |
| 4 | 27 | 90.85 | 90.85 | 0.00 | 90.96 | 90.96 | 0.00 | 91.14 | 91.14 | 0.00 |
| 5 | 21 | 90.90 | 90.87 | -0.03 | 91.03 | 91.00 | -0.03 | 91.15 | 91.19 | 0.04 |
| 6 | 12 | 91.36 | 91.36 | 0.00 | 91.46 | 91.47 | 0.01 | 91.63 | 91.63 | 0.00 |
| 7 | 23 | 92.12 | 92.12 | 0.00 | 92.22 | 92.21 | -0.01 | 92.34 | 92.34 | 0.00 |

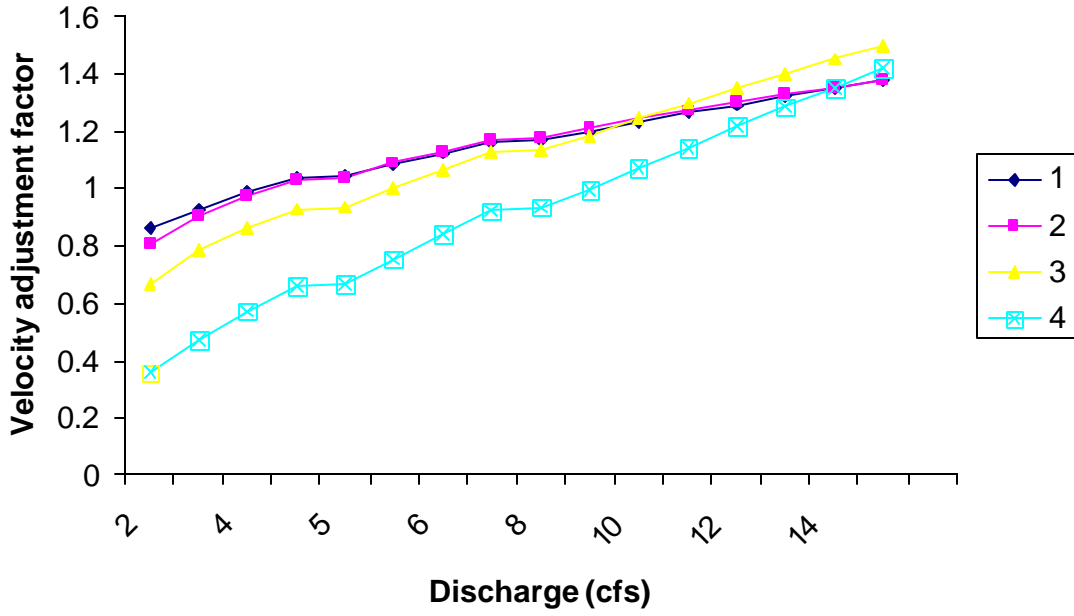
Table D-7 Water surface elevation calibration results (ft) for Big Timber Cr. Reference Site using the WSP (transects 3, 4) and STGQ (transects 1, 2, 5) models.

| Transect | Distance from next downstream transect (ft) | Water surface elevations (ft) | | | | | | | | |
|----------|---|-------------------------------|-----------|------------|----------|-----------|------------|----------|-----------|------------|
| | | 17.0 cfs | | | 27.0 cfs | | | 47.0 cfs | | |
| | | Measured | Simulated | Difference | Measured | Simulated | Difference | Measured | Simulated | Difference |
| 1 | 0 | 94.21 | 94.21 | 0.00 | 94.35 | 94.36 | 0.01 | 94.56 | 94.56 | 0.00 |
| 2 | 58 | 95.17 | 95.17 | 0.00 | 95.27 | 95.27 | 0.00 | 95.41 | 95.41 | 0.00 |
| 3 | 36 | 96.09 | 96.09 | 0.00 | 96.16 | 96.16 | 0.00 | 96.36 | 96.36 | 0.00 |
| 4 | 8 | 96.14 | 96.10 | -0.04 | 96.17 | 96.18 | 0.01 | 96.38 | 96.39 | 0.01 |
| 5 | 24 | 96.36 | 96.35 | -0.01 | 96.55 | 96.56 | 0.01 | 96.86 | 96.85 | -0.01 |

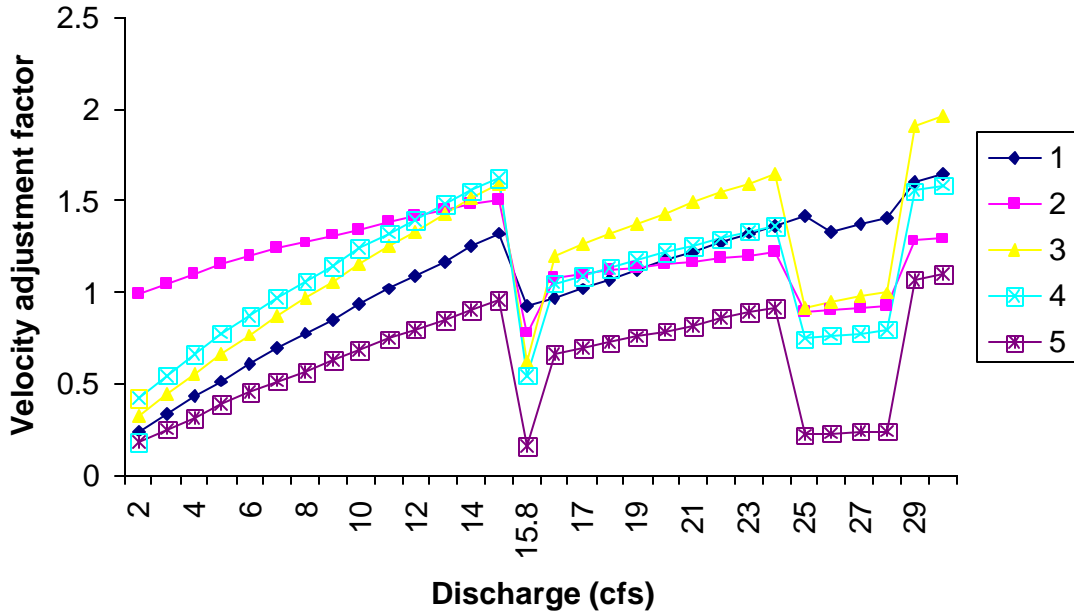
Velocity adjustment factors for each transect (indicated in legends):



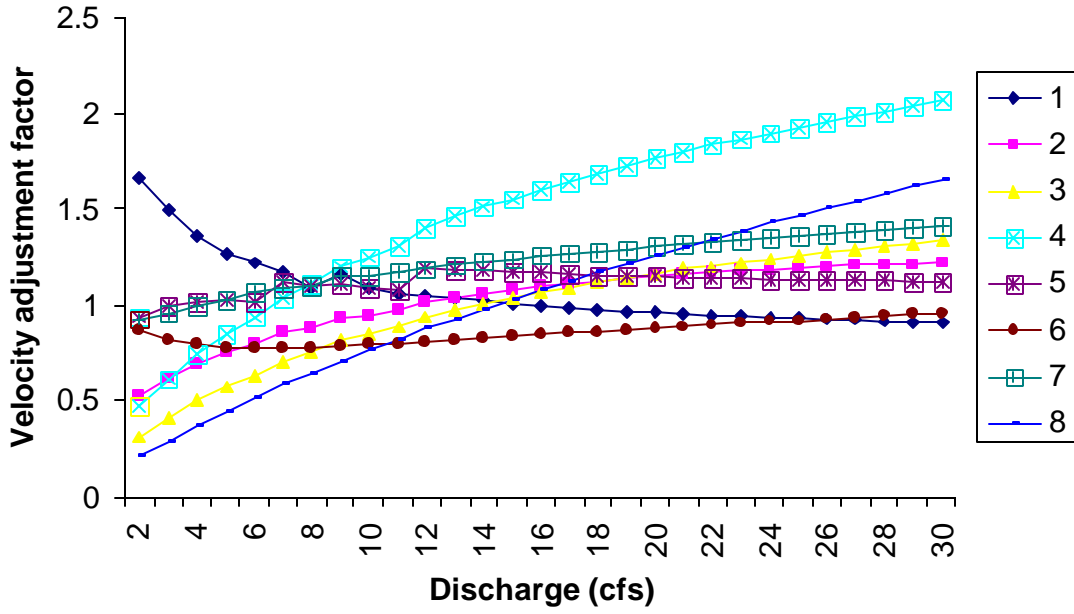
Study Site 2



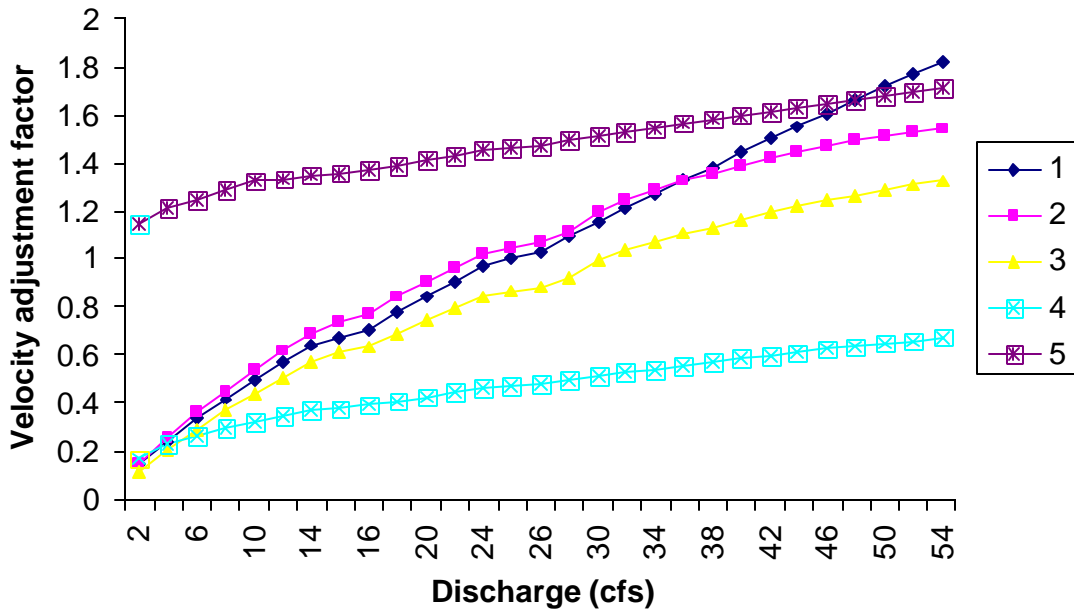
Study Site 3



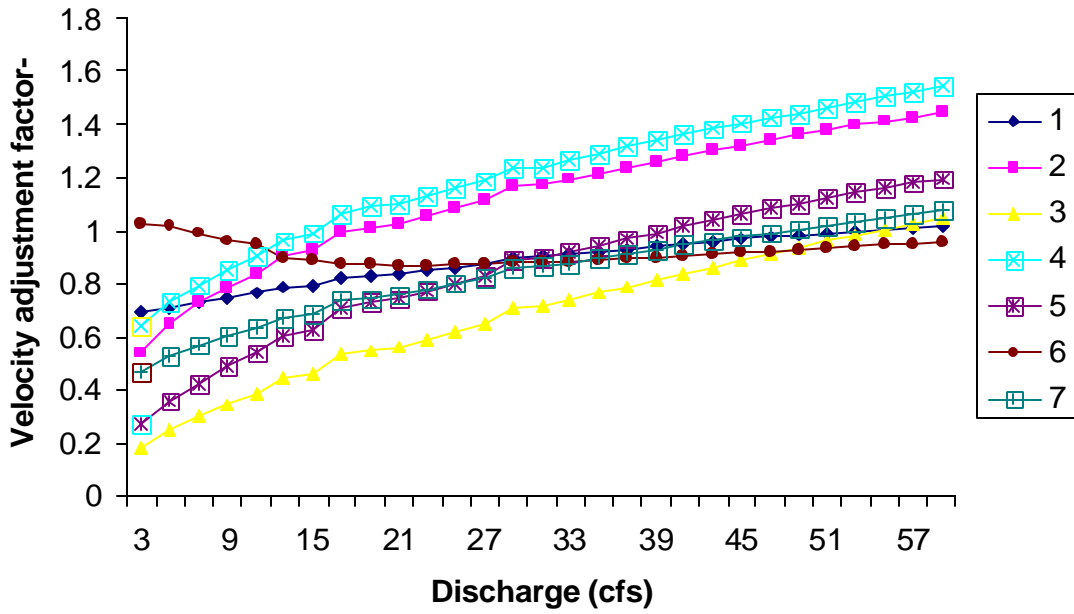
Study Site 4



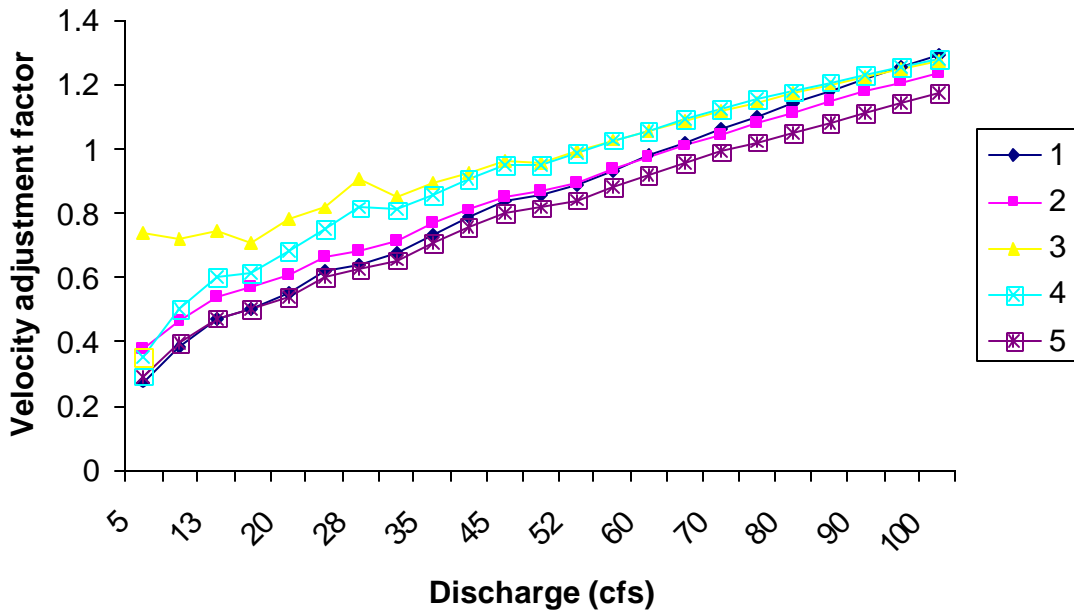
Study Site 5



Study Site 6



Reference Site (Study Site 7)



Appendix E - Habitat Suitability Criteria

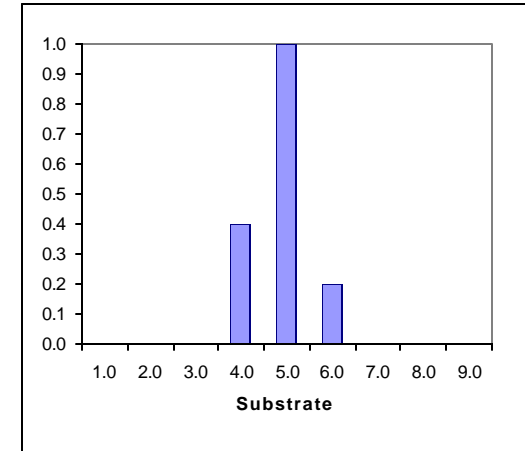
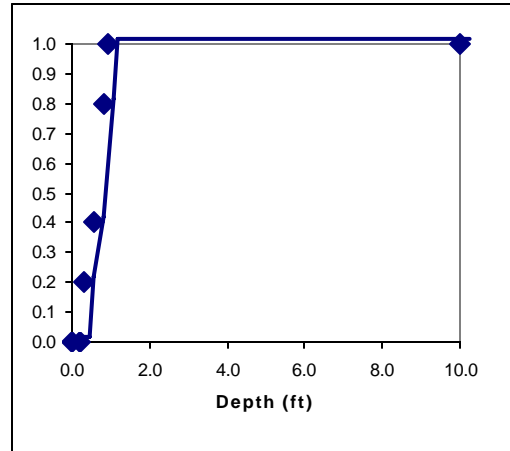
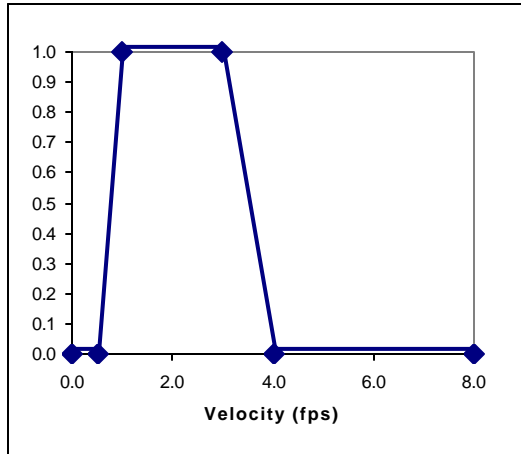
Fish Curves

| | | | | | | | | | | | | | |
|---|-------|--------|------|--------|------|-----------------------|----------|--------|------|--------|------|--------|------|
| H | 10000 | 8 | 8 | 11 | 0 | CHINOOK SALMON* | SPAWNING | | | | | | |
| V | 10000 | 0.00 | 0.00 | 0.50 | 0.00 | 1.00 | 1.00 | 3.00 | 1.00 | 4.00 | 0.00 | 8.00 | 0.00 |
| V | 10000 | 10.00 | 0.00 | 100.00 | 0.00 | | | | | | | | |
| D | 10000 | 0.00 | 0.00 | 0.20 | 0.00 | 0.30 | 0.20 | 0.58 | 0.40 | 0.80 | 0.80 | 0.95 | 1.00 |
| D | 10000 | 10.00 | 1.00 | 100.00 | 1.00 | | | | | | | | |
| S | 10000 | 1.00 | 0.00 | 2.00 | 0.00 | 3.00 | 0.00 | 4.00 | 0.40 | 5.00 | 1.00 | 6.00 | 0.20 |
| S | 10000 | 7.00 | 0.00 | 8.00 | 0.00 | 9.00 | 0.00 | 10.00 | 0.00 | 100.00 | 0.00 | | |
| H | 10100 | 6 | 6 | 4 | 0 | CHINOOK SALMON* | ADULT | | | | | | |
| V | 10100 | 0.00 | 1.00 | 2.00 | 1.00 | 4.00 | 0.00 | 8.00 | 0.00 | 10.00 | 0.00 | 100.00 | 0.00 |
| D | 10100 | 0.00 | 0.00 | 0.20 | 0.00 | 1.00 | 0.30 | 4.00 | 1.00 | 10.00 | 1.00 | 100.00 | 1.00 |
| S | 10100 | 1.00 | 1.00 | 9.00 | 1.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |
| H | 10200 | 25 | 13 | 4 | 0 | CHINOOK SALMON* | JUVENILE | | | | | | |
| V | 10200 | 0.00 | 0.88 | 0.10 | 0.95 | 0.20 | 0.99 | 0.30 | 1.00 | 0.40 | 0.99 | 0.50 | 0.95 |
| V | 10200 | 0.60 | 0.89 | 0.70 | 0.81 | 0.80 | 0.72 | 1.00 | 0.52 | 1.10 | 0.43 | 1.20 | 0.34 |
| V | 10200 | 1.30 | 0.26 | 1.40 | 0.20 | 1.50 | 0.15 | 1.60 | 0.11 | 1.70 | 0.07 | 1.80 | 0.05 |
| V | 10200 | 1.90 | 0.03 | 2.00 | 0.02 | 2.10 | 0.01 | 2.20 | 0.01 | 2.30 | 0.00 | 8.00 | 0.00 |
| V | 10200 | 100.00 | 0.00 | | | | | | | | | | |
| D | 10200 | 0.00 | 0.00 | 0.20 | 0.02 | 0.40 | 0.07 | 0.60 | 0.16 | 0.80 | 0.26 | 1.00 | 0.37 |
| D | 10200 | 1.20 | 0.48 | 1.40 | 0.59 | 1.60 | 0.68 | 1.80 | 0.76 | 2.00 | 1.00 | 10.00 | 1.00 |
| D | 10200 | 100.00 | 1.00 | | | | | | | | | | |
| S | 10200 | 1.00 | 1.00 | 9.00 | 1.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |
| H | 10300 | 7 | 8 | 11 | 0 | STEELHEAD* | SPAWNING | | | | | | |
| V | 10300 | 0.00 | 0.00 | 0.50 | 0.00 | 1.00 | 1.00 | 3.00 | 1.00 | 4.00 | 0.00 | 8.00 | 0.00 |
| V | 10300 | 100.00 | 0.00 | | | | | | | | | | |
| D | 10300 | 0.00 | 0.00 | 0.20 | 0.00 | 0.30 | 0.20 | 0.58 | 0.40 | 0.80 | 0.80 | 0.95 | 1.00 |
| D | 10300 | 10.00 | 1.00 | 100.00 | 1.00 | | | | | | | | |
| S | 10300 | 1.00 | 0.00 | 2.00 | 0.00 | 3.00 | 0.00 | 4.00 | 0.40 | 5.00 | 1.00 | 6.00 | 0.20 |
| S | 10300 | 7.00 | 0.00 | 8.00 | 0.00 | 9.00 | 0.00 | 10.00 | 0.00 | 100.00 | 0.00 | | |
| H | 10400 | 5 | 6 | 4 | 0 | STEELHEAD* | ADULT | | | | | | |
| V | 10400 | 0.00 | 1.00 | 2.00 | 1.00 | 4.00 | 0.00 | 8.00 | 0.00 | 100.00 | 0.00 | | |
| D | 10400 | 0.00 | 0.00 | 0.20 | 0.00 | 1.00 | 0.30 | 4.00 | 1.00 | 10.00 | 1.00 | 100.00 | 1.00 |
| S | 10400 | 1.00 | 1.00 | 9.00 | 1.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |
| H | 10500 | 9 | 7 | 4 | 0 | STEELHEAD* | JUVENILE | | | | | | |
| V | 10500 | 0.00 | 0.00 | 0.20 | 0.15 | 0.30 | 0.90 | 0.50 | 0.97 | 0.70 | 1.00 | 1.20 | 1.00 |
| V | 10500 | 2.00 | 0.00 | 8.00 | 0.00 | 100.00 | 0.00 | | | | | | |
| D | 10500 | 0.00 | 0.00 | 0.30 | 0.20 | 0.60 | 0.65 | 1.00 | 0.96 | 1.20 | 1.00 | 10.00 | 1.00 |
| D | 10500 | 100.00 | 1.00 | | | | | | | | | | |
| S | 10500 | 1.00 | 1.00 | 9.00 | 1.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |
| H | 10600 | 24 | 9 | 11 | 0 | BULL TROUT* | SPAWNING | | | | | | |
| V | 10600 | 0.00 | 0.00 | 0.20 | 0.00 | 0.32 | 0.03 | 0.42 | 0.06 | 0.48 | 0.11 | 0.60 | 0.18 |
| V | 10600 | 0.70 | 0.30 | 0.77 | 0.50 | 0.87 | 0.57 | 0.92 | 0.78 | 1.00 | 0.90 | 1.10 | 1.00 |
| V | 10600 | 1.90 | 1.00 | 2.05 | 0.96 | 2.14 | 0.90 | 2.25 | 0.72 | 2.40 | 0.48 | 2.52 | 0.32 |
| V | 10600 | 2.72 | 0.20 | 2.95 | 0.15 | 3.12 | 0.05 | 3.50 | 0.00 | 8.00 | 0.00 | 100.00 | 0.00 |
| D | 10600 | 0.00 | 0.00 | 0.20 | 0.00 | 0.25 | 0.04 | 0.31 | 0.11 | 0.45 | 0.30 | 0.50 | 0.56 |
| D | 10600 | 0.60 | 1.00 | 10.00 | 1.00 | 100.00 | 1.00 | | | | | | |
| S | 10600 | 1.00 | 0.00 | 2.00 | 0.00 | 3.00 | 0.00 | 4.00 | 1.00 | 5.00 | 1.00 | 6.00 | 0.00 |
| S | 10600 | 7.00 | 0.00 | 8.00 | 0.00 | 9.00 | 0.00 | 10.00 | 0.00 | 100.00 | 0.00 | | |
| H | 10700 | 5 | 5 | 4 | 0 | BULL TROUT* | ADULT | | | | | | |
| V | 10700 | 0.00 | 1.00 | 0.40 | 1.00 | 1.50 | 0.00 | 8.00 | 0.00 | 100.00 | 0.00 | | |
| D | 10700 | 0.00 | 0.00 | 0.30 | 0.00 | 2.00 | 1.00 | 10.00 | 1.00 | 100.00 | 1.00 | | |
| S | 10700 | 1.00 | 1.00 | 9.00 | 1.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |
| H | 10800 | 5 | 5 | 4 | 0 | BULL TROUT* | JUVENILE | | | | | | |
| V | 10800 | 0.00 | 1.00 | 0.40 | 1.00 | 1.50 | 0.00 | 8.00 | 0.00 | 100.00 | 0.00 | | |
| D | 10800 | 0.00 | 0.00 | 0.30 | 0.00 | 1.00 | 1.00 | 10.00 | 1.00 | 100.00 | 1.00 | | |
| S | 10800 | 1.00 | 1.00 | 9.00 | 1.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |
| H | 10900 | 25 | 13 | 10 | 0 | CHINOOK SALMON-COVER* | JUVENILE | | | | | | |
| V | 10900 | 0.00 | 0.88 | 0.10 | 0.95 | 0.20 | 0.99 | 0.30 | 1.00 | 0.40 | 0.99 | 0.50 | 0.95 |
| V | 10900 | 0.60 | 0.89 | 0.70 | 0.81 | 0.80 | 0.72 | 1.00 | 0.52 | 1.10 | 0.43 | 1.20 | 0.34 |
| V | 10900 | 1.30 | 0.26 | 1.40 | 0.20 | 1.50 | 0.15 | 1.60 | 0.11 | 1.70 | 0.07 | 1.80 | 0.05 |
| V | 10900 | 1.90 | 0.03 | 2.00 | 0.02 | 2.10 | 0.01 | 2.20 | 0.01 | 2.30 | 0.00 | 8.00 | 0.00 |
| V | 10900 | 100.00 | 0.00 | | | | | | | | | | |
| D | 10900 | 0.00 | 0.00 | 0.20 | 0.00 | 0.40 | 0.10 | 0.60 | 0.20 | 0.80 | 0.30 | 1.00 | 0.40 |
| D | 10900 | 1.20 | 0.50 | 1.40 | 0.60 | 1.60 | 0.70 | 1.80 | 0.80 | 2.00 | 1.00 | 10.00 | 1.00 |
| D | 10900 | 100.00 | 1.00 | | | | | | | | | | |
| S | 10900 | 1.00 | 1.00 | 2.00 | 1.00 | 3.00 | 1.00 | 4.00 | 1.00 | 5.00 | 1.00 | 6.00 | 1.00 |
| S | 10900 | 7.00 | 1.00 | 8.00 | 0.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |
| H | 11000 | 9 | 7 | 10 | 0 | STEELHEAD-COVER* | JUVENILE | | | | | | |

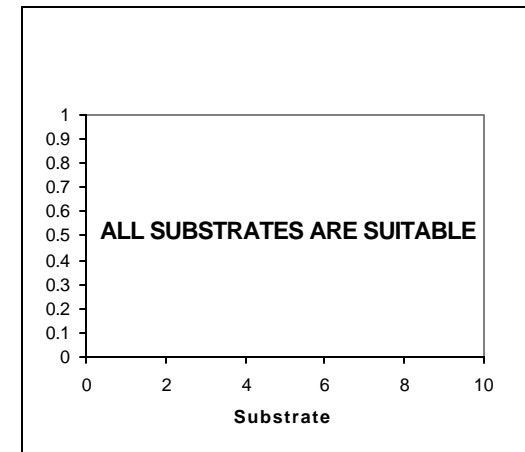
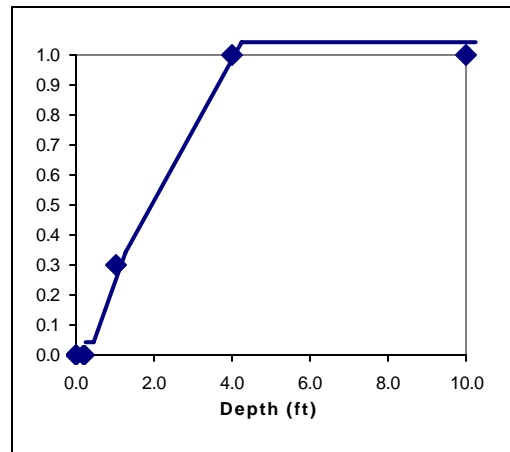
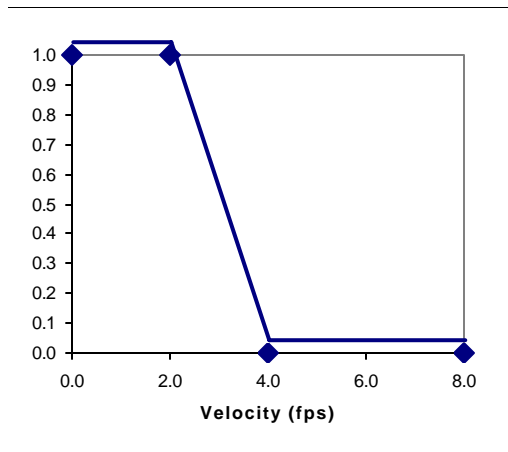
| | | | | | | | | | | | | | |
|---|-------|--------|------|------|------|-------------------|------|--------|------|----------|------|-------|------|
| V | 11000 | 0.00 | 0.00 | 0.20 | 0.20 | 0.30 | 0.90 | 0.50 | 1.00 | 0.70 | 1.00 | 1.20 | 1.00 |
| V | 11000 | 2.00 | 0.00 | 8.00 | 0.00 | 10.00 | 0.00 | | | | | | |
| D | 11000 | 0.00 | 0.00 | 0.30 | 0.20 | 0.60 | 0.65 | 1.00 | 0.96 | 1.20 | 1.00 | 10.00 | 1.00 |
| D | 11000 | 100.00 | 1.00 | | | | | | | | | | |
| S | 11000 | 1.00 | 1.00 | 2.00 | 1.00 | 3.00 | 1.00 | 4.00 | 1.00 | 5.00 | 1.00 | 6.00 | 1.00 |
| S | 11000 | 7.00 | 1.00 | 8.00 | 0.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |
| H | 11100 | 5 | 5 | 10 | 0 | BULL TROUT-COVER* | | | | | | | |
| | | | | | | | | | | JUVENILE | | | |
| V | 11100 | 0.00 | 1.00 | 0.40 | 1.00 | 1.50 | 0.00 | 8.00 | 0.00 | 100.00 | 0.00 | | |
| D | 11100 | 0.00 | 0.00 | 0.30 | 0.00 | 1.00 | 1.00 | 10.00 | 1.00 | 100.00 | 1.00 | | |
| S | 11100 | 1.00 | 1.00 | 2.00 | 1.00 | 3.00 | 1.00 | 4.00 | 1.00 | 5.00 | 1.00 | 6.00 | 1.00 |
| S | 11100 | 7.00 | 1.00 | 8.00 | 0.00 | 10.00 | 0.00 | 100.00 | 0.00 | | | | |

Habitat Suitability Criteria (HSC)

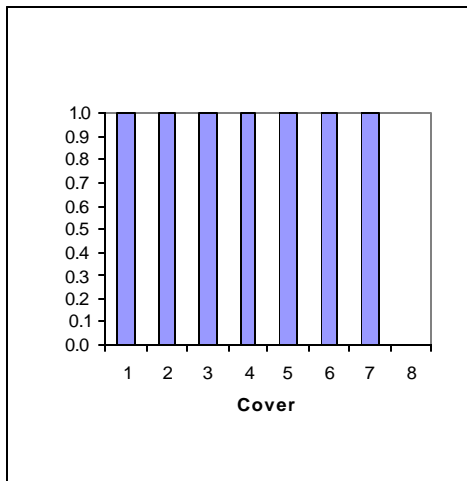
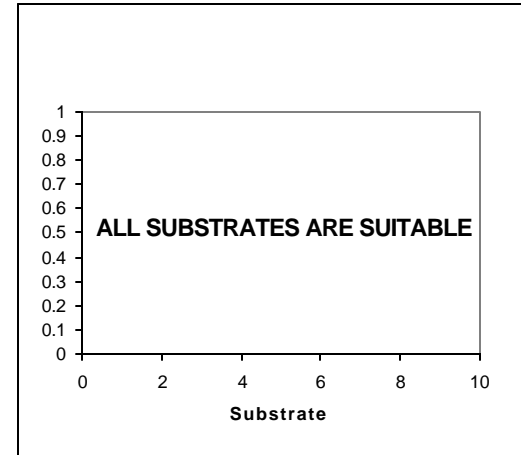
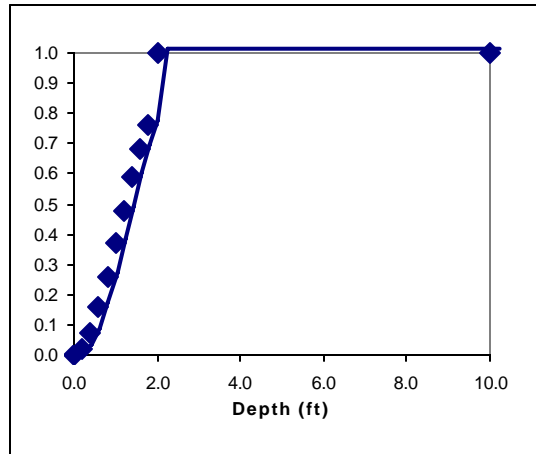
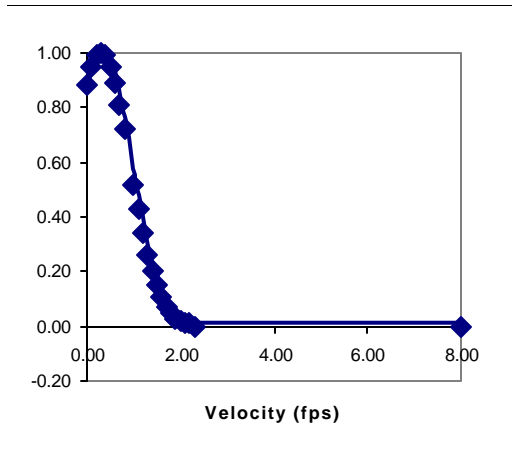
Chinook Salmon – spawning



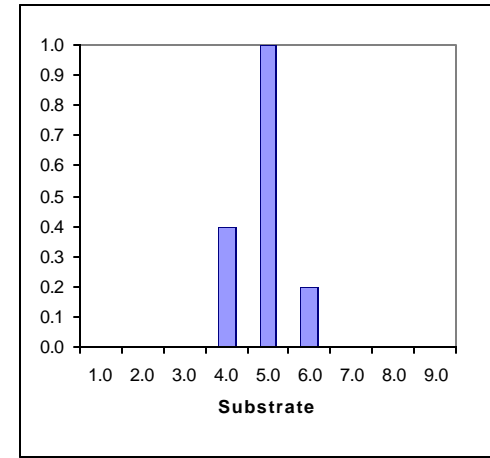
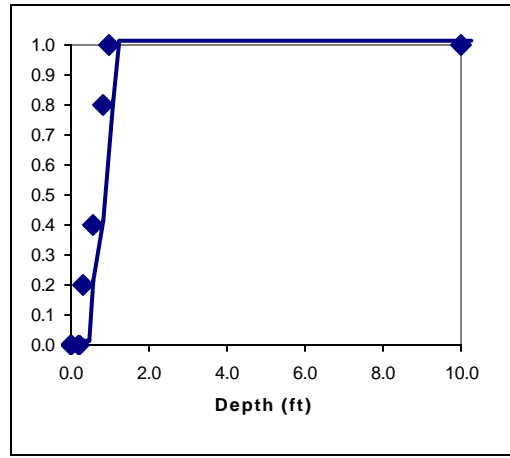
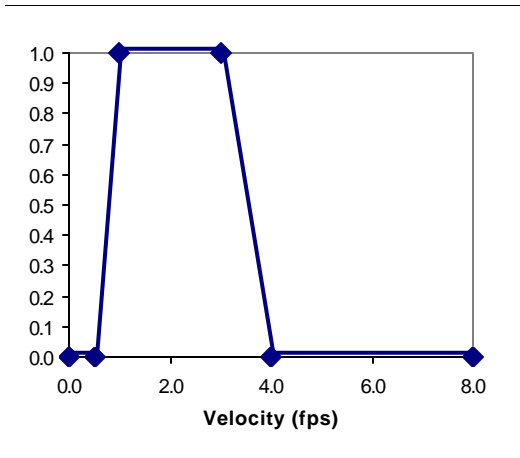
Chinook Salmon – adult holding



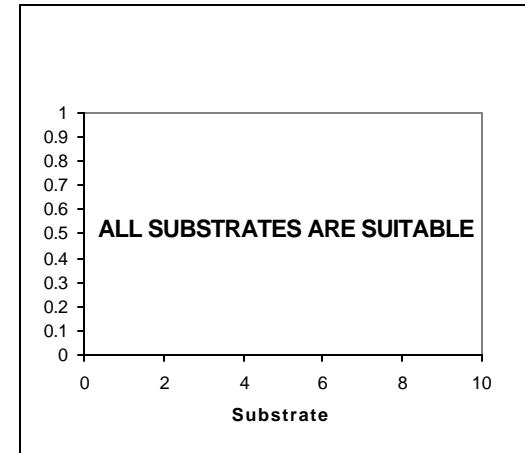
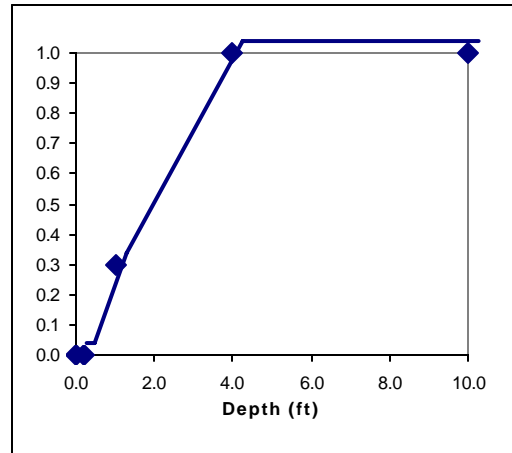
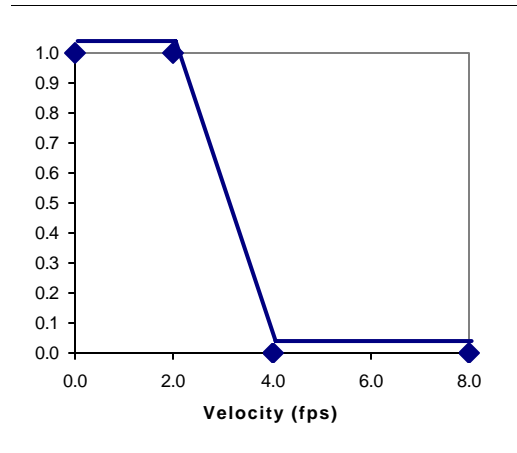
Chinook Salmon - juvenile



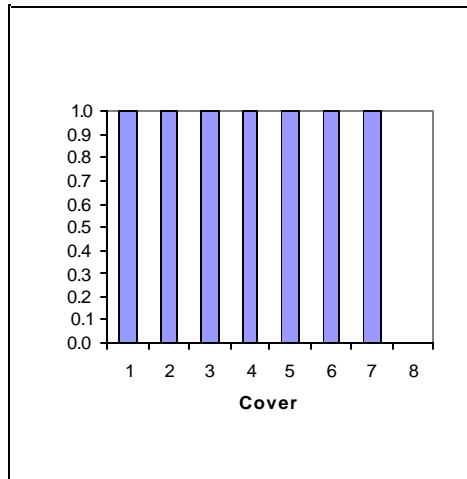
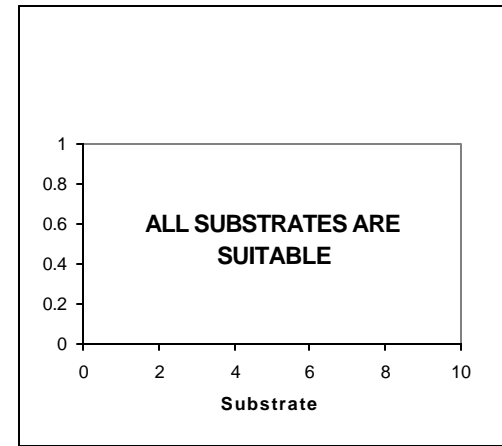
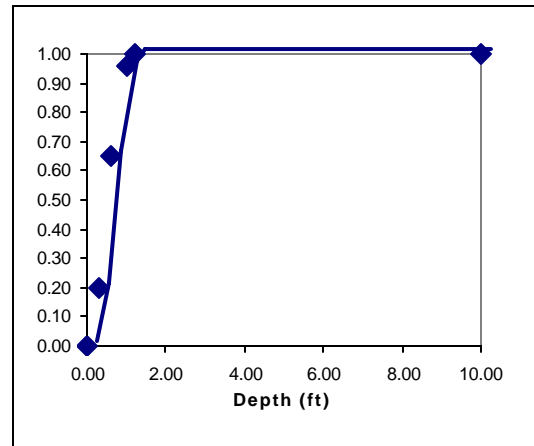
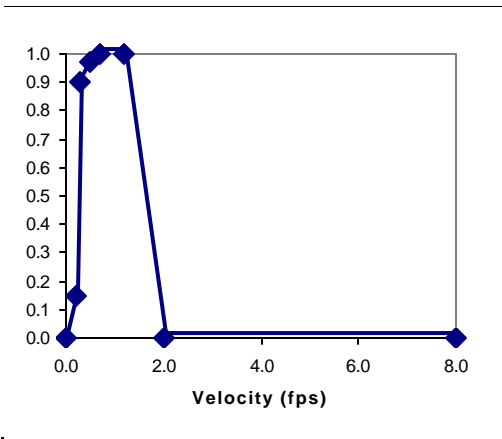
Steelhead – spawning



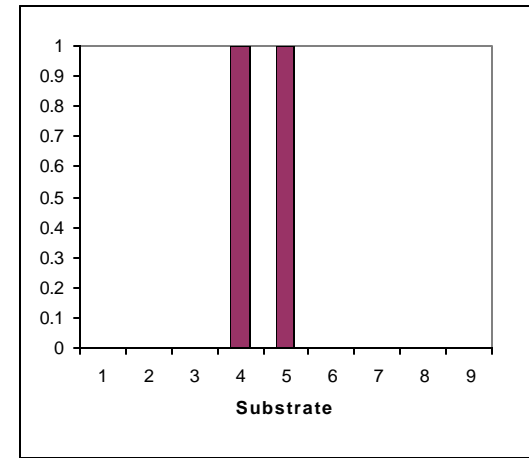
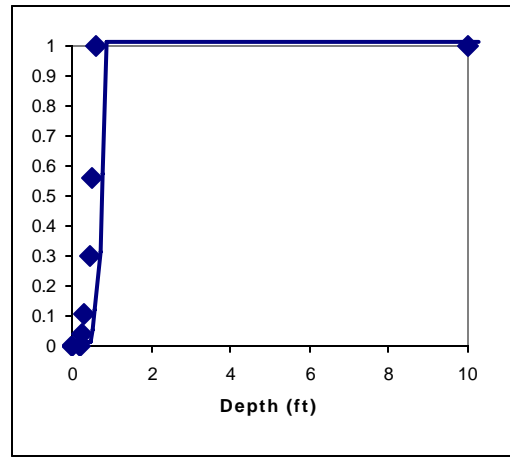
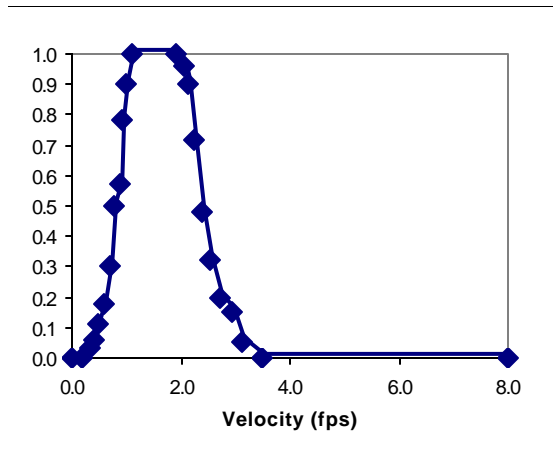
Steelhead – adult holding



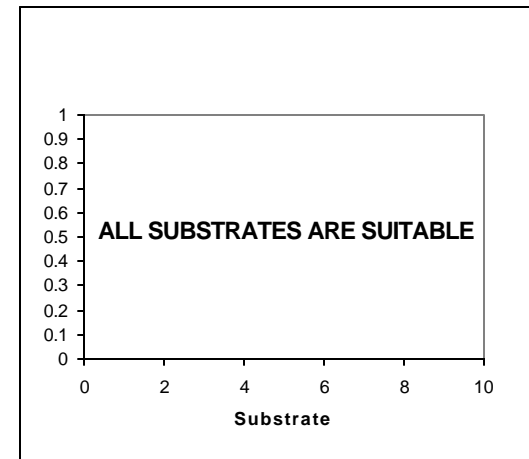
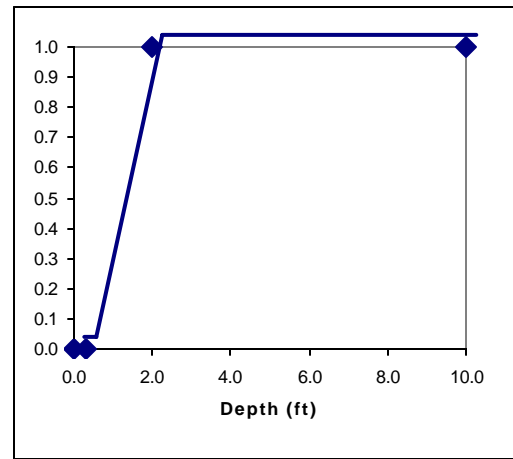
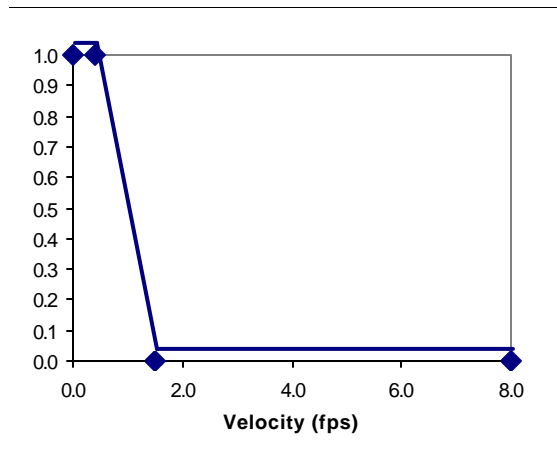
Steelhead - juvenile



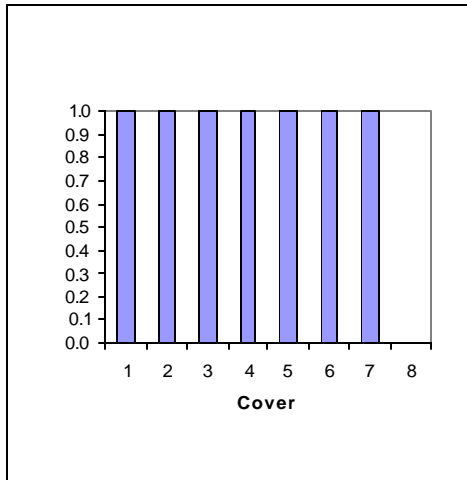
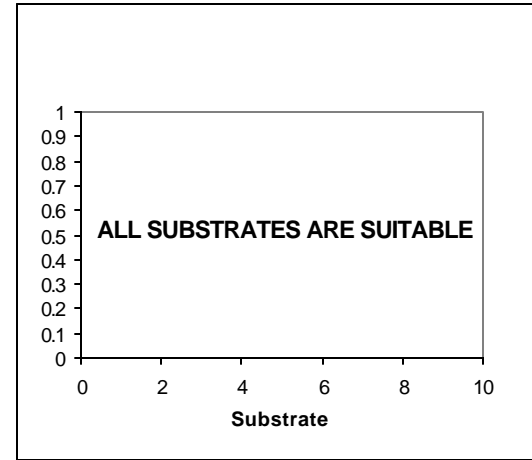
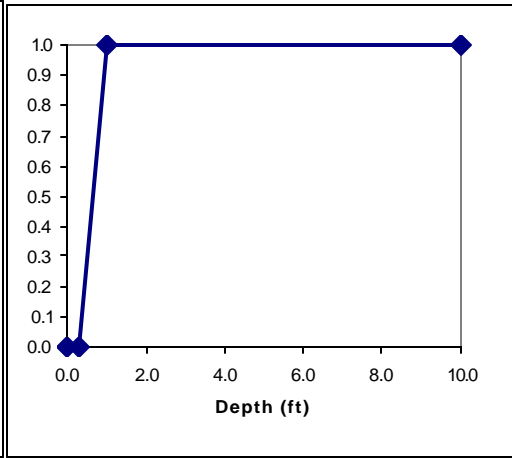
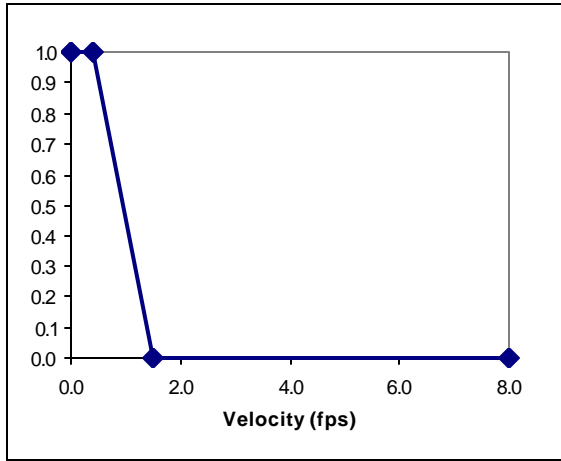
Bull trout - spawning



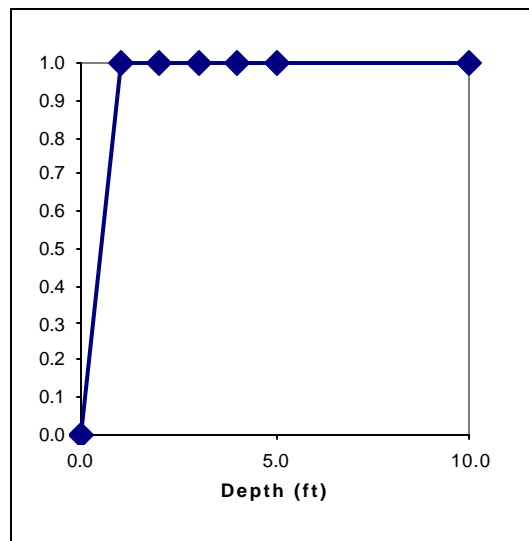
Bull trout – adult



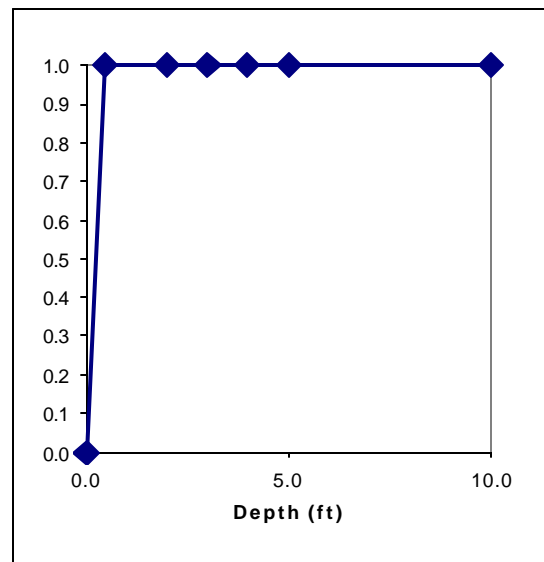
Bull trout – juvenile



Upstream anadromous passage



Upstream resident passage



Appendix F – Weighted usable area (WUA) versus discharge relationships

Reach 1 (Study Site 1):

Table F-1. Weighted usable area (WUA) versus discharge relationships for steelhead at Big Timber Creek, Study Site 1.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 1.4 | 11253 | 375 | 4725 | 5488 | 1985 | 8.4 | 65.1 | 68.7 | 58.0 |
| 2 | 11370 | 970 | 5114 | 6474 | 2381 | 21.8 | 70.5 | 81.0 | 69.5 |
| 3 | 11528 | 1812 | 5548 | 7304 | 2742 | 40.8 | 76.5 | 91.4 | 80.1 |
| 4 | 11657 | 2370 | 5825 | 7762 | 2994 | 53.3 | 80.3 | 97.1 | 87.4 |
| 5 | 11768 | 3076 | 6052 | 7991 | 3131 | 69.2 | 83.4 | 100.0 | 91.4 |
| 6 | 12040 | 3407 | 6252 | 7916 | 3214 | 76.6 | 86.2 | 99.1 | 93.8 |
| 6.5 | 12109 | 3550 | 6365 | 7924 | 3248 | 79.8 | 87.7 | 99.2 | 94.8 |
| 7 | 12639 | 3656 | 6470 | 7927 | 3279 | 82.2 | 89.2 | 99.2 | 95.7 |
| 8 | 12895 | 3818 | 6626 | 7738 | 3336 | 85.9 | 91.3 | 96.8 | 97.4 |
| 9 | 13003 | 4078 | 6750 | 7459 | 3380 | 91.7 | 93.0 | 93.3 | 98.7 |
| 10 | 13106 | 4243 | 6846 | 7453 | 3418 | 95.4 | 94.3 | 93.3 | 99.8 |
| 11 | 13202 | 4334 | 6932 | 7348 | 3425 | 97.5 | 95.5 | 92.0 | 100.0 |
| 12 | 13296 | 4388 | 7030 | 7187 | 3407 | 98.7 | 96.9 | 89.9 | 99.5 |
| 13 | 13387 | 4430 | 7082 | 6949 | 3289 | 99.6 | 97.6 | 87.0 | 96.0 |
| 14 | 13473 | 4446 | 7131 | 6645 | 3182 | 100.0 | 98.3 | 83.2 | 92.9 |
| 15 | 13558 | 4418 | 7134 | 6343 | 3188 | 99.4 | 98.3 | 79.4 | 93.1 |
| 16 | 13640 | 4356 | 7165 | 6203 | 3181 | 98.0 | 98.7 | 77.6 | 92.9 |
| 17 | 13720 | 4335 | 7205 | 6126 | 3166 | 97.5 | 99.3 | 76.7 | 92.4 |
| 18 | 13798 | 4299 | 7256 | 5972 | 3111 | 96.7 | 100.0 | 74.7 | 90.8 |
| 19 | 13875 | 4231 | 7256 | 5832 | 3107 | 95.2 | 100.0 | 73.0 | 90.7 |
| 20 | 13950 | 4030 | 7227 | 5639 | 3096 | 90.6 | 99.6 | 70.6 | 90.4 |

Table F-2. Weighted usable area (WUA) versus discharge relationships for Chinook salmon at Big Timber Creek, Study Site 1.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 1.4 | 11253 | 375 | 4725 | 5308 | 1985 | 8.4 | 65.1 | 91.1 | 58.0 |
| 2 | 11370 | 970 | 5114 | 5539 | 2381 | 21.8 | 70.5 | 95.0 | 69.5 |
| 3 | 11528 | 1812 | 5548 | 5751 | 2742 | 40.8 | 76.5 | 98.7 | 80.1 |
| 4 | 11657 | 2370 | 5825 | 5828 | 2994 | 53.3 | 80.3 | 100.0 | 87.4 |
| 5 | 11768 | 3076 | 6052 | 5825 | 3131 | 69.2 | 83.4 | 100.0 | 91.4 |
| 6 | 12040 | 3407 | 6252 | 5785 | 3214 | 76.6 | 86.2 | 99.3 | 93.8 |
| 6.5 | 12109 | 3550 | 6365 | 5757 | 3248 | 79.8 | 87.7 | 98.8 | 94.8 |
| 7 | 12639 | 3656 | 6470 | 5765 | 3279 | 82.2 | 89.2 | 98.9 | 95.7 |
| 8 | 12895 | 3818 | 6626 | 5691 | 3336 | 85.9 | 91.3 | 97.7 | 97.4 |
| 9 | 13003 | 4078 | 6750 | 5590 | 3380 | 91.7 | 93.0 | 95.9 | 98.7 |
| 10 | 13106 | 4243 | 6846 | 5476 | 3418 | 95.4 | 94.3 | 94.0 | 99.8 |
| 11 | 13202 | 4334 | 6932 | 5359 | 3425 | 97.5 | 95.5 | 92.0 | 100.0 |
| 12 | 13296 | 4388 | 7030 | 5275 | 3407 | 98.7 | 96.9 | 90.5 | 99.5 |
| 13 | 13387 | 4430 | 7082 | 5204 | 3289 | 99.6 | 97.6 | 89.3 | 96.0 |
| 14 | 13473 | 4446 | 7131 | 5101 | 3182 | 100.0 | 98.3 | 87.5 | 92.9 |
| 15 | 13558 | 4418 | 7134 | 5040 | 3188 | 99.4 | 98.3 | 86.5 | 93.1 |
| 16 | 13640 | 4356 | 7165 | 4975 | 3181 | 98.0 | 98.7 | 85.4 | 92.9 |
| 17 | 13720 | 4335 | 7205 | 4863 | 3166 | 97.5 | 99.3 | 83.4 | 92.4 |
| 18 | 13798 | 4299 | 7256 | 4761 | 3111 | 96.7 | 100.0 | 81.7 | 90.8 |
| 19 | 13875 | 4231 | 7256 | 4705 | 3107 | 95.2 | 100.0 | 80.7 | 90.7 |
| 20 | 13950 | 4030 | 7227 | 4670 | 3096 | 90.6 | 99.6 | 80.1 | 90.4 |

Table F-3. Weighted usable area (WUA) versus discharge relationships for bull trout at Big Timber Creek, Study Site 1.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 1.4 | 11253 | 1026 | 4208 | 5515 | 3229 | 21.9 | 74.2 | 77.4 | 76.3 |
| 2 | 11370 | 1595 | 4768 | 6225 | 3377 | 34.1 | 84.1 | 87.3 | 79.8 |
| 3 | 11528 | 2404 | 5236 | 6789 | 3513 | 51.4 | 92.3 | 95.2 | 83.0 |
| 4 | 11657 | 3028 | 5462 | 7029 | 3709 | 64.8 | 96.3 | 98.6 | 87.6 |
| 5 | 11768 | 3500 | 5576 | 7129 | 3804 | 74.8 | 98.3 | 100.0 | 89.9 |
| 6 | 12040 | 3861 | 5543 | 7034 | 3864 | 82.5 | 97.8 | 98.7 | 91.3 |
| 6.5 | 12109 | 4049 | 5538 | 7004 | 3914 | 86.6 | 97.7 | 98.2 | 92.5 |
| 7 | 12639 | 4213 | 5572 | 7027 | 3947 | 90.1 | 98.3 | 98.6 | 93.2 |
| 8 | 12895 | 4434 | 5601 | 7023 | 3987 | 94.8 | 98.8 | 98.5 | 94.2 |
| 9 | 13003 | 4593 | 5671 | 7077 | 4009 | 98.2 | 100.0 | 99.3 | 94.7 |
| 10 | 13106 | 4677 | 5652 | 7011 | 4070 | 100.0 | 99.7 | 98.4 | 96.2 |
| 11 | 13202 | 4676 | 5658 | 6982 | 4099 | 100.0 | 99.8 | 97.9 | 96.8 |
| 12 | 13296 | 4658 | 5616 | 6887 | 4163 | 99.6 | 99.0 | 96.6 | 98.3 |
| 13 | 13387 | 4644 | 5596 | 6821 | 4187 | 99.3 | 98.7 | 95.7 | 98.9 |
| 14 | 13473 | 4591 | 5594 | 6782 | 4216 | 98.2 | 98.6 | 95.1 | 99.6 |
| 15 | 13558 | 4530 | 5606 | 6763 | 4230 | 96.9 | 98.9 | 94.9 | 99.9 |
| 16 | 13640 | 4387 | 5618 | 6744 | 4233 | 93.8 | 99.1 | 94.6 | 100.0 |
| 17 | 13720 | 4224 | 5608 | 6698 | 4231 | 90.3 | 98.9 | 94.0 | 100.0 |
| 18 | 13798 | 4117 | 5591 | 6645 | 4221 | 88.0 | 98.6 | 93.2 | 99.7 |
| 19 | 13875 | 3963 | 5517 | 6519 | 4201 | 84.7 | 97.3 | 91.4 | 99.2 |
| 20 | 13950 | 3834 | 5475 | 6440 | 4161 | 82.0 | 96.6 | 90.3 | 98.3 |

Reach 2 (Study Site 2):

Table F-4. Weighted usable area (WUA) versus discharge relationships for steelhead at Big Timber Creek, Study Site 2.

| Discharge (cfs) | Total (ft ²)/1,000 ft | WUA (ft ²)/1,000 ft | | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|---------------------------------|-------|----------|----------------|----------------------------|-------|----------|----------------|
| | | Spawning | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 11891 | 1437 | 3310 | 6566 | 1577 | 27.1 | 51.6 | 75.8 | 85.2 |
| 3 | 12300 | 2257 | 3774 | 7468 | 1670 | 42.5 | 58.8 | 86.2 | 90.2 |
| 4 | 12629 | 2964 | 4315 | 8083 | 1773 | 55.8 | 67.3 | 93.3 | 95.8 |
| 5 | 13036 | 3419 | 4643 | 8451 | 1838 | 64.4 | 72.4 | 97.5 | 99.3 |
| 5.9 | 13082 | 3462 | 4671 | 8478 | 1842 | 65.2 | 72.8 | 97.9 | 99.5 |
| 6 | 13593 | 3797 | 5054 | 8664 | 1851 | 71.5 | 78.8 | 100.0 | 100.0 |
| 7 | 13812 | 4083 | 5292 | 8621 | 1778 | 76.9 | 82.5 | 99.5 | 96.0 |
| 8 | 14067 | 4358 | 5549 | 8331 | 1657 | 82.1 | 86.5 | 96.2 | 89.5 |
| 8.2 | 14094 | 4423 | 5606 | 8309 | 1627 | 83.3 | 87.4 | 95.9 | 87.9 |
| 9 | 14198 | 4594 | 5767 | 8103 | 1477 | 86.5 | 89.9 | 93.5 | 79.8 |
| 10 | 14319 | 4761 | 5994 | 7374 | 1064 | 89.7 | 93.5 | 85.1 | 57.5 |
| 11 | 14431 | 4891 | 6149 | 6407 | 591 | 92.1 | 95.9 | 74.0 | 31.9 |
| 12 | 14538 | 5038 | 6270 | 5985 | 518 | 94.9 | 97.8 | 69.1 | 28.0 |
| 13 | 14639 | 5152 | 6344 | 5469 | 457 | 97.0 | 98.9 | 63.1 | 24.7 |
| 14 | 14741 | 5240 | 6389 | 5237 | 464 | 98.7 | 99.6 | 60.5 | 25.1 |
| 15 | 14838 | 5309 | 6413 | 4970 | 471 | 100.0 | 100.0 | 57.4 | 25.4 |

Table F-5. Weighted usable area (WUA) versus discharge relationships for Chinook salmon at Big Timber Creek, Study Site 2.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 11891 | 1437 | 3310 | 3957 | 1047 | 27.1 | 51.6 | 93.4 | 100.0 |
| 3 | 12300 | 2257 | 3774 | 4168 | 1041 | 42.5 | 58.8 | 98.4 | 99.4 |
| 4 | 12629 | 2964 | 4315 | 4237 | 994 | 55.8 | 67.3 | 100.0 | 94.9 |
| 5 | 13036 | 3419 | 4643 | 4229 | 933 | 64.4 | 72.4 | 99.8 | 89.1 |
| 5.9 | 13082 | 3462 | 4671 | 4226 | 925 | 65.2 | 72.8 | 99.7 | 88.3 |
| 6 | 13593 | 3797 | 5054 | 4177 | 899 | 71.5 | 78.8 | 98.6 | 85.8 |
| 7 | 13812 | 4083 | 5292 | 4072 | 828 | 76.9 | 82.5 | 96.1 | 79.1 |
| 8 | 14067 | 4358 | 5549 | 3930 | 750 | 82.1 | 86.5 | 92.7 | 71.6 |
| 8.2 | 14094 | 4423 | 5606 | 3899 | 732 | 83.3 | 87.4 | 92.0 | 69.9 |
| 9 | 14198 | 4594 | 5767 | 3776 | 669 | 86.5 | 89.9 | 89.1 | 63.9 |
| 10 | 14319 | 4761 | 5994 | 3564 | 592 | 89.7 | 93.5 | 84.1 | 56.5 |
| 11 | 14431 | 4891 | 6149 | 3422 | 530 | 92.1 | 95.9 | 80.8 | 50.6 |
| 12 | 14538 | 5038 | 6270 | 3217 | 436 | 94.9 | 97.8 | 75.9 | 41.7 |
| 13 | 14639 | 5152 | 6344 | 3002 | 312 | 97.0 | 98.9 | 70.9 | 29.8 |
| 14 | 14741 | 5240 | 6389 | 2832 | 307 | 98.7 | 99.6 | 66.8 | 29.3 |
| 15 | 14838 | 5309 | 6413 | 2755 | 280 | 100.0 | 100.0 | 65.0 | 26.7 |

Table F-6. Weighted usable area (WUA) versus discharge relationships for bull trout at Big Timber Creek, Study Site 2.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 11891 | 170 | 2000 | 2689 | 1228 | 12.9 | 67.5 | 67.5 | 96.1 |
| 3 | 12300 | 263 | 2587 | 3478 | 1278 | 19.9 | 87.3 | 87.3 | 100.0 |
| 4 | 12629 | 447 | 2881 | 3873 | 1272 | 33.9 | 97.3 | 97.3 | 99.6 |
| 5 | 13036 | 561 | 2954 | 3971 | 1245 | 42.5 | 99.7 | 99.7 | 97.4 |
| 5.9 | 13082 | 571 | 2956 | 3973 | 1241 | 43.3 | 99.8 | 99.8 | 97.1 |
| 6 | 13593 | 677 | 2962 | 3982 | 1189 | 51.3 | 100.0 | 100.0 | 93.0 |
| 7 | 13812 | 744 | 2950 | 3965 | 1115 | 56.4 | 99.6 | 99.6 | 87.3 |
| 8 | 14067 | 870 | 2848 | 3828 | 1009 | 66.0 | 96.1 | 96.1 | 79.0 |
| 8.2 | 14094 | 904 | 2835 | 3810 | 982 | 68.5 | 95.7 | 95.7 | 76.9 |
| 9 | 14198 | 997 | 2711 | 3644 | 792 | 75.6 | 91.5 | 91.5 | 62.0 |
| 10 | 14319 | 1083 | 2450 | 3294 | 549 | 82.1 | 82.7 | 82.7 | 43.0 |
| 11 | 14431 | 1138 | 2031 | 2730 | 239 | 86.3 | 68.6 | 68.6 | 18.7 |
| 12 | 14538 | 1188 | 1852 | 2490 | 181 | 90.1 | 62.5 | 62.5 | 14.2 |
| 13 | 14639 | 1231 | 1735 | 2332 | 182 | 93.4 | 58.6 | 58.6 | 14.2 |
| 14 | 14741 | 1278 | 1769 | 2378 | 244 | 96.9 | 59.7 | 59.7 | 19.1 |
| 15 | 14838 | 1319 | 1685 | 2265 | 258 | 100.0 | 56.9 | 56.9 | 20.2 |

Reach 3 (Study Site 3):

Table F-7. Weighted usable area (WUA) versus discharge relationships for steelhead at Big Timber Creek, Study Site 3.

| Discharge (cfs) | Total (ft ²)/1,000 ft | WUA (ft ²)/1,000 ft | | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|---------------------------------|-------|----------|----------------|----------------------------|-------|----------|----------------|
| | | Spawning | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 12326 | 544 | 4295 | 6889 | 2969 | 7.4 | 64.4 | 74.9 | 76.1 |
| 3 | 12582 | 1715 | 4723 | 8026 | 3476 | 23.2 | 70.8 | 87.3 | 89.1 |
| 4 | 12890 | 2959 | 5188 | 8545 | 3654 | 40.0 | 77.7 | 92.9 | 93.7 |
| 5 | 13146 | 4005 | 5464 | 8926 | 3811 | 54.2 | 81.9 | 97.0 | 97.7 |
| 6 | 13287 | 4649 | 5659 | 9146 | 3900 | 62.9 | 84.8 | 99.4 | 100.0 |
| 7 | 13405 | 5221 | 5867 | 9198 | 3884 | 70.6 | 87.9 | 100.0 | 99.6 |
| 8 | 13538 | 5529 | 6070 | 9124 | 3804 | 74.8 | 91.0 | 99.2 | 97.5 |
| 9 | 13655 | 5809 | 6201 | 8989 | 3731 | 78.6 | 92.9 | 97.7 | 95.7 |
| 10 | 13772 | 6045 | 6308 | 8692 | 3593 | 81.8 | 94.5 | 94.5 | 92.1 |
| 11 | 13878 | 6310 | 6462 | 8281 | 3394 | 85.4 | 96.8 | 90.0 | 87.0 |
| 12 | 13977 | 6472 | 6556 | 7582 | 3048 | 87.5 | 98.2 | 82.4 | 78.1 |
| 13 | 14070 | 6588 | 6616 | 6432 | 2649 | 89.1 | 99.1 | 69.9 | 67.9 |
| 14 | 14159 | 6771 | 6647 | 5768 | 2566 | 91.6 | 99.6 | 62.7 | 65.8 |
| 15 | 14243 | 6953 | 6657 | 5263 | 2449 | 94.1 | 99.7 | 57.2 | 62.8 |
| 15.8 | 14304 | 7090 | 6669 | 4902 | 2415 | 95.9 | 99.9 | 53.3 | 61.9 |
| 16 | 14322 | 7121 | 6674 | 4736 | 2408 | 96.3 | 100.0 | 51.5 | 61.7 |
| 17 | 14398 | 7209 | 6666 | 4383 | 2360 | 97.5 | 99.9 | 47.7 | 60.5 |
| 18 | 14470 | 7284 | 6668 | 4004 | 2292 | 98.5 | 99.9 | 43.5 | 58.8 |
| 19 | 14691 | 7349 | 6639 | 3715 | 2159 | 99.4 | 99.5 | 40.4 | 55.4 |
| 20 | 14758 | 7381 | 6591 | 3349 | 2032 | 99.8 | 98.8 | 36.4 | 52.1 |
| 21 | 14822 | 7393 | 6528 | 3223 | 1938 | 100.0 | 97.8 | 35.0 | 49.7 |
| 22 | 14883 | 7389 | 6452 | 2962 | 1722 | 100.0 | 96.7 | 32.2 | 44.1 |
| 23 | 14943 | 7358 | 6383 | 2770 | 1580 | 99.5 | 95.6 | 30.1 | 40.5 |
| 24 | 14999 | 7293 | 6280 | 2631 | 1460 | 98.7 | 94.1 | 28.6 | 37.4 |
| 25 | 15062 | 7142 | 6113 | 2523 | 1386 | 96.6 | 91.6 | 27.4 | 35.5 |
| 26 | 15115 | 6853 | 5882 | 2340 | 1274 | 92.7 | 88.1 | 25.4 | 32.7 |
| 27 | 15166 | 6723 | 5773 | 2167 | 1243 | 90.9 | 86.5 | 23.6 | 31.9 |
| 28 | 15202 | 6536 | 5637 | 2080 | 1186 | 88.4 | 84.5 | 22.6 | 30.4 |
| 29 | 15238 | 6373 | 5490 | 1977 | 1089 | 86.2 | 82.3 | 21.5 | 27.9 |
| 30 | 15272 | 6180 | 5316 | 1922 | 1076 | 83.6 | 79.6 | 20.9 | 27.6 |

Table F-8. Weighted usable area (WUA) versus discharge relationships for Chinook salmon at Big Timber Creek, Study Site 3.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 12326 | 544 | 4295 | 5195 | 2150 | 7.4 | 64.4 | 95.8 | 91.5 |
| 3 | 12582 | 1715 | 4723 | 5364 | 2286 | 23.2 | 70.8 | 98.9 | 97.3 |
| 4 | 12890 | 2959 | 5188 | 5424 | 2350 | 40.0 | 77.7 | 100.0 | 100.0 |
| 5 | 13146 | 4005 | 5464 | 5382 | 2305 | 54.2 | 81.9 | 99.2 | 98.1 |
| 6 | 13287 | 4649 | 5659 | 5243 | 2222 | 62.9 | 84.8 | 96.7 | 94.5 |
| 7 | 13405 | 5221 | 5867 | 5056 | 2177 | 70.6 | 87.9 | 93.2 | 92.6 |
| 8 | 13538 | 5529 | 6070 | 4845 | 2152 | 74.8 | 91.0 | 89.3 | 91.6 |
| 9 | 13655 | 5809 | 6201 | 4634 | 2067 | 78.6 | 92.9 | 85.4 | 88.0 |
| 10 | 13772 | 6045 | 6308 | 4396 | 1954 | 81.8 | 94.5 | 81.0 | 83.2 |
| 11 | 13878 | 6310 | 6462 | 4155 | 1841 | 85.4 | 96.8 | 76.6 | 78.3 |
| 12 | 13977 | 6472 | 6556 | 3906 | 1713 | 87.5 | 98.2 | 72.0 | 72.9 |
| 13 | 14070 | 6588 | 6616 | 3655 | 1590 | 89.1 | 99.1 | 67.4 | 67.7 |
| 14 | 14159 | 6771 | 6647 | 3347 | 1409 | 91.6 | 99.6 | 61.7 | 59.9 |
| 15 | 14243 | 6953 | 6657 | 3048 | 1220 | 94.1 | 99.7 | 56.2 | 51.9 |
| 15.8 | 14304 | 7090 | 6669 | 2770 | 1116 | 95.9 | 99.9 | 51.1 | 47.5 |
| 16 | 14322 | 7121 | 6674 | 2697 | 1088 | 96.3 | 100.0 | 49.7 | 46.3 |
| 17 | 14398 | 7209 | 6666 | 2472 | 1014 | 97.5 | 99.9 | 45.6 | 43.1 |
| 18 | 14470 | 7284 | 6668 | 2293 | 964 | 98.5 | 99.9 | 42.3 | 41.0 |
| 19 | 14691 | 7349 | 6639 | 2059 | 915 | 99.4 | 99.5 | 38.0 | 38.9 |
| 20 | 14758 | 7381 | 6591 | 1973 | 862 | 99.8 | 98.8 | 36.4 | 36.7 |
| 21 | 14822 | 7393 | 6528 | 1877 | 817 | 100.0 | 97.8 | 34.6 | 34.8 |
| 22 | 14883 | 7389 | 6452 | 1741 | 762 | 100.0 | 96.7 | 32.1 | 32.4 |
| 23 | 14943 | 7358 | 6383 | 1572 | 715 | 99.5 | 95.6 | 29.0 | 30.4 |
| 24 | 14999 | 7293 | 6280 | 1487 | 695 | 98.7 | 94.1 | 27.4 | 29.6 |
| 25 | 15062 | 7142 | 6113 | 1442 | 672 | 96.6 | 91.6 | 26.6 | 28.6 |
| 26 | 15115 | 6853 | 5882 | 1360 | 613 | 92.7 | 88.1 | 25.1 | 26.1 |
| 27 | 15166 | 6723 | 5773 | 1292 | 578 | 90.9 | 86.5 | 23.8 | 24.6 |
| 28 | 15202 | 6536 | 5637 | 1242 | 573 | 88.4 | 84.5 | 22.9 | 24.4 |
| 29 | 15238 | 6373 | 5490 | 1209 | 555 | 86.2 | 82.3 | 22.3 | 23.6 |
| 30 | 15272 | 6180 | 5316 | 1152 | 514 | 83.6 | 79.6 | 21.2 | 21.9 |

Table F-9. Weighted usable area (WUA) versus discharge relationships for bull trout at Big Timber Creek, Study Site 3.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 12326 | 497 | 4142 | 5525 | 2544 | 11.3 | 92.8 | 92.9 | 94.8 |
| 3 | 12582 | 1090 | 4313 | 5750 | 2625 | 24.8 | 96.6 | 96.7 | 97.8 |
| 4 | 12890 | 1750 | 4442 | 5920 | 2681 | 39.8 | 99.5 | 99.6 | 99.9 |
| 5 | 13146 | 2309 | 4459 | 5940 | 2685 | 52.5 | 99.9 | 99.9 | 100.0 |
| 6 | 13287 | 2710 | 4464 | 5944 | 2637 | 61.6 | 100.0 | 100.0 | 98.2 |
| 7 | 13405 | 3033 | 4417 | 5877 | 2559 | 69.0 | 98.9 | 98.9 | 95.3 |
| 8 | 13538 | 3264 | 4352 | 5787 | 2526 | 74.2 | 97.5 | 97.4 | 94.1 |
| 9 | 13655 | 3472 | 4150 | 5515 | 2418 | 79.0 | 93.0 | 92.8 | 90.1 |
| 10 | 13772 | 3645 | 3958 | 5254 | 2230 | 82.9 | 88.7 | 88.4 | 83.1 |
| 11 | 13878 | 3928 | 3809 | 5052 | 2117 | 89.3 | 85.3 | 85.0 | 78.8 |
| 12 | 13977 | 4147 | 3504 | 4640 | 1827 | 94.3 | 78.5 | 78.1 | 68.1 |
| 13 | 14070 | 4283 | 3116 | 4116 | 1487 | 97.4 | 69.8 | 69.2 | 55.4 |
| 14 | 14159 | 4377 | 2819 | 3716 | 1273 | 99.5 | 63.1 | 62.5 | 47.4 |
| 15 | 14243 | 4397 | 2641 | 3475 | 1162 | 100.0 | 59.2 | 58.5 | 43.3 |
| 15.8 | 14304 | 4383 | 2452 | 3221 | 995 | 99.7 | 54.9 | 54.2 | 37.1 |
| 16 | 14322 | 4376 | 2390 | 3138 | 980 | 99.5 | 53.5 | 52.8 | 36.5 |
| 17 | 14398 | 4298 | 2206 | 2889 | 854 | 97.7 | 49.4 | 48.6 | 31.8 |
| 18 | 14470 | 4197 | 2051 | 2680 | 807 | 95.4 | 45.9 | 45.1 | 30.1 |
| 19 | 14691 | 4079 | 1775 | 2310 | 748 | 92.7 | 39.8 | 38.9 | 27.9 |
| 20 | 14758 | 3925 | 1347 | 1738 | 589 | 89.3 | 30.2 | 29.2 | 21.9 |
| 21 | 14822 | 3805 | 1238 | 1593 | 545 | 86.5 | 27.7 | 26.8 | 20.3 |
| 22 | 14883 | 3665 | 1121 | 1436 | 431 | 83.3 | 25.1 | 24.2 | 16.1 |
| 23 | 14943 | 3497 | 1045 | 1333 | 384 | 79.5 | 23.4 | 22.4 | 14.3 |
| 24 | 14999 | 3368 | 923 | 1168 | 304 | 76.6 | 20.7 | 19.7 | 11.3 |
| 25 | 15062 | 3217 | 806 | 1011 | 307 | 73.2 | 18.1 | 17.0 | 11.4 |
| 26 | 15115 | 3074 | 783 | 979 | 306 | 69.9 | 17.5 | 16.5 | 11.4 |
| 27 | 15166 | 2881 | 746 | 928 | 304 | 65.5 | 16.7 | 15.6 | 11.3 |
| 28 | 15202 | 2737 | 684 | 847 | 300 | 62.2 | 15.3 | 14.2 | 11.2 |
| 29 | 15238 | 2500 | 674 | 833 | 296 | 56.8 | 15.1 | 14.0 | 11.0 |
| 30 | 15272 | 2322 | 663 | 817 | 291 | 52.8 | 14.8 | 13.7 | 10.8 |

Reach 4 (Study Site 4):

Table F-10. Weighted usable area (WUA) versus discharge relationships for steelhead at Big Timber Creek, Study Site 4.

| Discharge (cfs) | Total (ft ²)/1,000 ft | WUA (ft ²)/1,000 ft | | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|---------------------------------|-------|----------|----------------|----------------------------|-------|----------|----------------|
| | | Spawning | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 11551 | 628 | 3633 | 5662 | 707 | 9.1 | 43.2 | 61.4 | 59.3 |
| 3 | 12888 | 1208 | 4074 | 6851 | 822 | 17.5 | 48.5 | 74.3 | 68.9 |
| 4 | 13889 | 1928 | 4522 | 7785 | 896 | 28.0 | 53.8 | 84.5 | 75.1 |
| 5 | 14144 | 2517 | 4898 | 8371 | 986 | 36.5 | 58.3 | 90.8 | 82.7 |
| 6 | 14295 | 3243 | 5380 | 8615 | 1054 | 47.0 | 64.0 | 93.5 | 88.4 |
| 7 | 14403 | 3775 | 5759 | 8750 | 1104 | 54.7 | 68.5 | 94.9 | 92.6 |
| 8 | 14542 | 4205 | 6235 | 8629 | 1122 | 61.0 | 74.2 | 93.6 | 94.1 |
| 9 | 14633 | 4604 | 6542 | 8787 | 1134 | 66.8 | 77.8 | 95.3 | 95.2 |
| 10 | 14754 | 4965 | 6841 | 9014 | 1160 | 72.0 | 81.4 | 97.8 | 97.4 |
| 11 | 14853 | 5249 | 7048 | 9213 | 1188 | 76.1 | 83.8 | 100.0 | 99.7 |
| 12 | 14899 | 5400 | 7148 | 9217 | 1192 | 78.3 | 85.0 | 100.0 | 100.0 |
| 13 | 14974 | 5643 | 7310 | 9205 | 1189 | 81.9 | 87.0 | 99.9 | 99.8 |
| 14 | 15144 | 5825 | 7469 | 9079 | 1141 | 84.5 | 88.9 | 98.5 | 95.8 |
| 15 | 15229 | 5969 | 7637 | 8819 | 1154 | 86.6 | 90.9 | 95.7 | 96.8 |
| 16 | 15314 | 6113 | 7767 | 8633 | 1162 | 88.7 | 92.4 | 93.7 | 97.5 |
| 17 | 15501 | 6242 | 7898 | 8579 | 1164 | 90.5 | 94.0 | 93.1 | 97.7 |
| 18 | 15686 | 6355 | 7995 | 8550 | 1151 | 92.2 | 95.1 | 92.8 | 96.6 |
| 19 | 15862 | 6452 | 8075 | 8392 | 1097 | 93.6 | 96.1 | 91.1 | 92.1 |
| 20 | 16036 | 6551 | 8145 | 8328 | 1101 | 95.0 | 96.9 | 90.3 | 92.4 |
| 21 | 16205 | 6652 | 8203 | 8253 | 1098 | 96.5 | 97.6 | 89.5 | 92.1 |
| 22 | 16372 | 6717 | 8253 | 8145 | 1060 | 97.4 | 98.2 | 88.4 | 88.9 |
| 23 | 16532 | 6768 | 8304 | 8114 | 1065 | 98.2 | 98.8 | 88.0 | 89.4 |
| 24 | 16698 | 6813 | 8343 | 8104 | 1070 | 98.8 | 99.3 | 87.9 | 89.8 |
| 25 | 16849 | 6845 | 8383 | 8033 | 1075 | 99.3 | 99.7 | 87.2 | 90.2 |
| 26 | 17008 | 6873 | 8400 | 7855 | 1079 | 99.7 | 99.9 | 85.2 | 90.5 |
| 27 | 17164 | 6890 | 8405 | 7630 | 1081 | 99.9 | 100.0 | 82.8 | 90.7 |
| 28 | 17325 | 6895 | 8402 | 7267 | 1084 | 100.0 | 100.0 | 78.8 | 90.9 |
| 29 | 17478 | 6884 | 8383 | 7208 | 1086 | 99.8 | 99.7 | 78.2 | 91.1 |
| 30 | 17625 | 6825 | 8322 | 7173 | 1088 | 99.0 | 99.0 | 77.8 | 91.3 |

Table F-11. Weighted usable area (WUA) versus discharge relationships for Chinook salmon at Big Timber Creek, Study Site 4.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 11551 | 628 | 3633 | 4265 | 761 | 9.1 | 43.2 | 77.9 | 91.5 |
| 3 | 12888 | 1208 | 4074 | 4774 | 796 | 17.5 | 48.5 | 87.2 | 95.8 |
| 4 | 13889 | 1928 | 4522 | 5137 | 815 | 28.0 | 53.8 | 93.8 | 98.0 |
| 5 | 14144 | 2517 | 4898 | 5303 | 824 | 36.5 | 58.3 | 96.9 | 99.1 |
| 6 | 14295 | 3243 | 5380 | 5407 | 826 | 47.0 | 64.0 | 98.8 | 99.4 |
| 7 | 14403 | 3775 | 5759 | 5402 | 819 | 54.7 | 68.5 | 98.7 | 98.5 |
| 8 | 14542 | 4205 | 6235 | 5475 | 816 | 61.0 | 74.2 | 100.0 | 98.2 |
| 9 | 14633 | 4604 | 6542 | 5371 | 803 | 66.8 | 77.8 | 98.1 | 96.7 |
| 10 | 14754 | 4965 | 6841 | 5400 | 830 | 72.0 | 81.4 | 98.6 | 99.8 |
| 11 | 14853 | 5249 | 7048 | 5288 | 831 | 76.1 | 83.8 | 96.6 | 100.0 |
| 12 | 14899 | 5400 | 7148 | 5173 | 815 | 78.3 | 85.0 | 94.5 | 98.1 |
| 13 | 14974 | 5643 | 7310 | 5120 | 811 | 81.9 | 87.0 | 93.5 | 97.6 |
| 14 | 15144 | 5825 | 7469 | 5073 | 808 | 84.5 | 88.9 | 92.7 | 97.2 |
| 15 | 15229 | 5969 | 7637 | 5021 | 801 | 86.6 | 90.9 | 91.7 | 96.4 |
| 16 | 15314 | 6113 | 7767 | 4965 | 799 | 88.7 | 92.4 | 90.7 | 96.1 |
| 17 | 15501 | 6242 | 7898 | 4914 | 778 | 90.5 | 94.0 | 89.8 | 93.6 |
| 18 | 15686 | 6355 | 7995 | 4878 | 762 | 92.2 | 95.1 | 89.1 | 91.7 |
| 19 | 15862 | 6452 | 8075 | 4816 | 758 | 93.6 | 96.1 | 88.0 | 91.2 |
| 20 | 16036 | 6551 | 8145 | 4685 | 751 | 95.0 | 96.9 | 85.6 | 90.3 |
| 21 | 16205 | 6652 | 8203 | 4610 | 747 | 96.5 | 97.6 | 84.2 | 89.8 |
| 22 | 16372 | 6717 | 8253 | 4586 | 744 | 97.4 | 98.2 | 83.8 | 89.5 |
| 23 | 16532 | 6768 | 8304 | 4554 | 742 | 98.2 | 98.8 | 83.2 | 89.3 |
| 24 | 16698 | 6813 | 8343 | 4512 | 733 | 98.8 | 99.3 | 82.4 | 88.2 |
| 25 | 16849 | 6845 | 8383 | 4477 | 740 | 99.3 | 99.7 | 81.8 | 89.0 |
| 26 | 17008 | 6873 | 8400 | 4405 | 721 | 99.7 | 99.9 | 80.5 | 86.7 |
| 27 | 17164 | 6890 | 8405 | 4375 | 722 | 99.9 | 100.0 | 79.9 | 86.9 |
| 28 | 17325 | 6895 | 8402 | 4362 | 723 | 100.0 | 100.0 | 79.7 | 87.0 |
| 29 | 17478 | 6884 | 8383 | 4350 | 722 | 99.8 | 99.7 | 79.4 | 86.9 |
| 30 | 17625 | 6825 | 8322 | 4336 | 721 | 99.0 | 99.0 | 79.2 | 86.7 |

Table F-12. Weighted usable area (WUA) versus discharge relationships for bull trout at Big Timber Creek, Study Site 4.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 11551 | 525 | 3053 | 3956 | 948 | 13.1 | 55.2 | 56.8 | 79.9 |
| 3 | 12888 | 872 | 3415 | 4420 | 1002 | 21.8 | 61.8 | 63.5 | 84.5 |
| 4 | 13889 | 1188 | 3732 | 4825 | 1035 | 29.7 | 67.5 | 69.3 | 87.2 |
| 5 | 14144 | 1522 | 3933 | 5076 | 1059 | 38.0 | 71.1 | 72.9 | 89.2 |
| 6 | 14295 | 1811 | 4099 | 5278 | 1075 | 45.2 | 74.1 | 75.9 | 90.6 |
| 7 | 14403 | 2105 | 4192 | 5387 | 1094 | 52.6 | 75.8 | 77.4 | 92.2 |
| 8 | 14542 | 2417 | 4401 | 5645 | 1113 | 60.4 | 79.6 | 81.1 | 93.8 |
| 9 | 14633 | 2635 | 4525 | 5802 | 1116 | 65.8 | 81.8 | 83.4 | 94.1 |
| 10 | 14754 | 2903 | 4670 | 5975 | 1129 | 72.5 | 84.4 | 85.9 | 95.1 |
| 11 | 14853 | 3056 | 4965 | 6351 | 1133 | 76.3 | 89.8 | 91.3 | 95.5 |
| 12 | 14899 | 3194 | 5066 | 6480 | 1124 | 79.7 | 91.6 | 93.1 | 94.8 |
| 13 | 14974 | 3333 | 5207 | 6654 | 1124 | 83.2 | 94.2 | 95.6 | 94.7 |
| 14 | 15144 | 3433 | 5332 | 6808 | 1122 | 85.7 | 96.4 | 97.8 | 94.6 |
| 15 | 15229 | 3524 | 5380 | 6860 | 1119 | 88.0 | 97.3 | 98.6 | 94.3 |
| 16 | 15314 | 3600 | 5414 | 6892 | 1166 | 89.9 | 97.9 | 99.0 | 98.2 |
| 17 | 15501 | 3669 | 5444 | 6919 | 1179 | 91.6 | 98.4 | 99.4 | 99.4 |
| 18 | 15686 | 3726 | 5450 | 6913 | 1185 | 93.0 | 98.5 | 99.4 | 99.9 |
| 19 | 15862 | 3791 | 5456 | 6910 | 1187 | 94.7 | 98.7 | 99.3 | 100.0 |
| 20 | 16036 | 3838 | 5494 | 6948 | 1185 | 95.8 | 99.3 | 99.9 | 99.9 |
| 21 | 16205 | 3880 | 5469 | 6905 | 1182 | 96.9 | 98.9 | 99.2 | 99.6 |
| 22 | 16372 | 3908 | 5509 | 6947 | 1174 | 97.6 | 99.6 | 99.8 | 99.0 |
| 23 | 16532 | 3931 | 5524 | 6958 | 1162 | 98.2 | 99.9 | 100.0 | 97.9 |
| 24 | 16698 | 3948 | 5530 | 6958 | 1141 | 98.6 | 100.0 | 100.0 | 96.2 |
| 25 | 16849 | 3962 | 5511 | 6925 | 1108 | 98.9 | 99.6 | 99.5 | 93.4 |
| 26 | 17008 | 3976 | 5523 | 6928 | 1104 | 99.3 | 99.9 | 99.6 | 93.0 |
| 27 | 17164 | 3988 | 5522 | 6914 | 1098 | 99.6 | 99.9 | 99.4 | 92.5 |
| 28 | 17325 | 3997 | 5522 | 6902 | 1091 | 99.8 | 99.9 | 99.2 | 92.0 |
| 29 | 17478 | 4003 | 5529 | 6900 | 1103 | 100.0 | 100.0 | 99.2 | 92.9 |
| 30 | 17625 | 4005 | 5509 | 6865 | 1094 | 100.0 | 99.6 | 98.7 | 92.2 |

Reach 5 (Study Site 5):

Table F-13. Weighted usable area (WUA) versus discharge relationships for steelhead at Big Timber Creek, Study Site 5.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 19398 | 0 | 3938 | 7989 | 409 | 0.0 | 36.8 | 59.3 | 48.5 |
| 4 | 21895 | 946 | 4866 | 11021 | 463 | 17.7 | 45.5 | 81.8 | 54.9 |
| 6 | 23157 | 1692 | 5526 | 12226 | 499 | 31.7 | 51.7 | 90.7 | 59.2 |
| 8 | 24144 | 2428 | 6213 | 12922 | 530 | 45.5 | 58.1 | 95.9 | 62.9 |
| 10 | 25019 | 2977 | 6697 | 13334 | 560 | 55.8 | 62.6 | 99.0 | 66.4 |
| 12 | 25578 | 3494 | 7948 | 13473 | 584 | 65.5 | 74.3 | 100.0 | 69.3 |
| 14 | 26020 | 3821 | 8455 | 13126 | 602 | 71.6 | 79.1 | 97.4 | 71.5 |
| 15 | 26752 | 3930 | 8635 | 12733 | 606 | 73.6 | 80.7 | 94.5 | 71.9 |
| 16 | 26875 | 4043 | 9122 | 12342 | 642 | 75.7 | 85.3 | 91.6 | 76.1 |
| 18 | 27107 | 4259 | 9522 | 11022 | 676 | 79.8 | 89.0 | 81.8 | 80.2 |
| 20 | 27326 | 4420 | 9787 | 9213 | 699 | 82.8 | 91.5 | 68.4 | 83.0 |
| 22 | 27462 | 4631 | 10037 | 8488 | 716 | 86.7 | 93.8 | 63.0 | 84.9 |
| 24 | 27545 | 4805 | 10211 | 7403 | 727 | 90.0 | 95.5 | 54.9 | 86.3 |
| 25 | 27586 | 4928 | 10307 | 6948 | 729 | 92.3 | 96.4 | 51.6 | 86.5 |
| 26 | 27627 | 5010 | 10366 | 6379 | 735 | 93.9 | 96.9 | 47.3 | 87.3 |
| 28 | 27706 | 5125 | 10438 | 5912 | 746 | 96.0 | 97.6 | 43.9 | 88.5 |
| 30 | 27737 | 5155 | 10634 | 5383 | 743 | 96.6 | 99.4 | 40.0 | 88.2 |
| 32 | 27809 | 5214 | 10674 | 5004 | 721 | 97.7 | 99.8 | 37.1 | 85.5 |
| 34 | 27881 | 5259 | 10673 | 4842 | 609 | 98.5 | 99.8 | 35.9 | 72.3 |
| 36 | 27953 | 5272 | 10695 | 4689 | 634 | 98.8 | 100.0 | 34.8 | 75.3 |
| 38 | 28024 | 5311 | 10667 | 4533 | 658 | 99.5 | 99.7 | 33.6 | 78.1 |
| 40 | 28103 | 5330 | 10583 | 4419 | 681 | 99.9 | 99.0 | 32.8 | 80.8 |
| 42 | 28183 | 5338 | 10442 | 4398 | 696 | 100.0 | 97.6 | 32.6 | 82.6 |
| 44 | 28262 | 5323 | 10163 | 4356 | 713 | 99.7 | 95.0 | 32.3 | 84.6 |
| 46 | 28341 | 5264 | 10006 | 4183 | 739 | 98.6 | 93.6 | 31.1 | 87.7 |
| 48 | 28420 | 5146 | 9823 | 4153 | 768 | 96.4 | 91.9 | 30.8 | 91.2 |
| 50 | 28497 | 5169 | 9629 | 4038 | 795 | 96.8 | 90.0 | 30.0 | 94.3 |
| 52 | 28548 | 5214 | 9505 | 4026 | 819 | 97.7 | 88.9 | 29.9 | 97.2 |
| 54 | 28598 | 5214 | 9206 | 3994 | 843 | 97.7 | 86.1 | 29.6 | 100.0 |

Table F-14. Weighted usable area (WUA) versus discharge relationships for Chinook salmon at Big Timber Creek, Study Site 5.

| Discharge (cfs) | Total (ft ²)/ 1,000 ft | WUA (ft ²)/1,000 ft | | | | Percent of optimal habitat | | | |
|--------------------|--|---------------------------------|-------|----------|-------------------|----------------------------|-------|----------|-------------------|
| | | Spawning | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 19398 | 0 | 3938 | 6126 | 373 | 0.0 | 36.8 | 84.5 | 57.7 |
| 4 | 21895 | 946 | 4866 | 6960 | 460 | 17.7 | 45.5 | 96.0 | 71.2 |
| 6 | 23157 | 1692 | 5526 | 7238 | 480 | 31.7 | 51.7 | 99.9 | 74.3 |
| 8 | 24144 | 2428 | 6213 | 7248 | 487 | 45.5 | 58.1 | 100.0 | 75.4 |
| 10 | 25019 | 2977 | 6697 | 7065 | 490 | 55.8 | 62.6 | 97.5 | 75.8 |
| 12 | 25578 | 3494 | 7948 | 6817 | 490 | 65.5 | 74.3 | 94.1 | 75.8 |
| 14 | 26020 | 3821 | 8455 | 6475 | 487 | 71.6 | 79.1 | 89.3 | 75.4 |
| 15 | 26752 | 3930 | 8635 | 6258 | 482 | 73.6 | 80.7 | 86.3 | 74.7 |
| 16 | 26875 | 4043 | 9122 | 6144 | 480 | 75.7 | 85.3 | 84.8 | 74.4 |
| 18 | 27107 | 4259 | 9522 | 5794 | 477 | 79.8 | 89.0 | 79.9 | 73.8 |
| 20 | 27326 | 4420 | 9787 | 5431 | 473 | 82.8 | 91.5 | 74.9 | 73.2 |
| 22 | 27462 | 4631 | 10037 | 5010 | 470 | 86.7 | 93.8 | 69.1 | 72.7 |
| 24 | 27545 | 4805 | 10211 | 4593 | 467 | 90.0 | 95.5 | 63.4 | 72.3 |
| 25 | 27586 | 4928 | 10307 | 4441 | 468 | 92.3 | 96.4 | 61.3 | 72.5 |
| 26 | 27627 | 5010 | 10366 | 4261 | 470 | 93.9 | 96.9 | 58.8 | 72.7 |
| 28 | 27706 | 5125 | 10438 | 3866 | 470 | 96.0 | 97.6 | 53.3 | 72.7 |
| 30 | 27737 | 5155 | 10634 | 3483 | 459 | 96.6 | 99.4 | 48.1 | 71.0 |
| 32 | 27809 | 5214 | 10674 | 3258 | 458 | 97.7 | 99.8 | 44.9 | 70.9 |
| 34 | 27881 | 5259 | 10673 | 3082 | 457 | 98.5 | 99.8 | 42.5 | 70.8 |
| 36 | 27953 | 5272 | 10695 | 2888 | 453 | 98.8 | 100.0 | 39.8 | 70.2 |
| 38 | 28024 | 5311 | 10667 | 2769 | 477 | 99.5 | 99.7 | 38.2 | 73.8 |
| 40 | 28103 | 5330 | 10583 | 2700 | 484 | 99.9 | 99.0 | 37.2 | 74.9 |
| 42 | 28183 | 5338 | 10442 | 2654 | 464 | 100.0 | 97.6 | 36.6 | 71.7 |
| 44 | 28262 | 5323 | 10163 | 2568 | 452 | 99.7 | 95.0 | 35.4 | 70.0 |
| 46 | 28341 | 5264 | 10006 | 2481 | 548 | 98.6 | 93.6 | 34.2 | 84.8 |
| 48 | 28420 | 5146 | 9823 | 2471 | 581 | 96.4 | 91.9 | 34.1 | 90.0 |
| 50 | 28497 | 5169 | 9629 | 2471 | 606 | 96.8 | 90.0 | 34.1 | 93.9 |
| 52 | 28548 | 5214 | 9505 | 2423 | 628 | 97.7 | 88.9 | 33.4 | 97.1 |
| 54 | 28598 | 5214 | 9206 | 2408 | 646 | 97.7 | 86.1 | 33.2 | 100.0 |

Table F-15. Weighted usable area (WUA) versus discharge relationships for bull trout at Big Timber Creek, Study Site 5.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 2 | 19398 | 503 | 3610 | 4790 | 494 | 14.7 | 79.1 | 80.3 | 71.0 |
| 4 | 21895 | 991 | 4104 | 5427 | 519 | 29.0 | 89.9 | 90.9 | 74.7 |
| 6 | 23157 | 1436 | 4323 | 5702 | 529 | 42.0 | 94.7 | 95.6 | 76.2 |
| 8 | 24144 | 1803 | 4431 | 5834 | 558 | 52.7 | 97.1 | 97.8 | 80.3 |
| 10 | 25019 | 2085 | 4528 | 5948 | 633 | 60.9 | 99.2 | 99.7 | 91.0 |
| 12 | 25578 | 2395 | 4530 | 5937 | 657 | 70.0 | 99.3 | 99.5 | 94.5 |
| 14 | 26020 | 2612 | 4563 | 5967 | 672 | 76.4 | 100.0 | 100.0 | 96.7 |
| 15 | 26752 | 2699 | 4507 | 5894 | 672 | 78.9 | 98.8 | 98.8 | 96.7 |
| 16 | 26875 | 2823 | 4534 | 5926 | 677 | 82.5 | 99.4 | 99.3 | 97.4 |
| 18 | 27107 | 2981 | 4428 | 5775 | 684 | 87.1 | 97.1 | 96.8 | 98.4 |
| 20 | 27326 | 3066 | 4264 | 5548 | 689 | 89.6 | 93.5 | 93.0 | 99.1 |
| 22 | 27462 | 3179 | 4035 | 5238 | 692 | 92.9 | 88.4 | 87.8 | 99.5 |
| 24 | 27545 | 3247 | 3848 | 4990 | 694 | 94.9 | 84.3 | 83.6 | 99.8 |
| 25 | 27586 | 3321 | 3764 | 4877 | 695 | 97.1 | 82.5 | 81.7 | 99.9 |
| 26 | 27627 | 3365 | 3656 | 4734 | 695 | 98.3 | 80.1 | 79.3 | 100.0 |
| 28 | 27706 | 3421 | 3342 | 4326 | 695 | 100.0 | 73.3 | 72.5 | 100.0 |
| 30 | 27737 | 3355 | 2914 | 3769 | 686 | 98.1 | 63.9 | 63.2 | 98.7 |
| 32 | 27809 | 3286 | 2765 | 3577 | 684 | 96.0 | 60.6 | 59.9 | 98.3 |
| 34 | 27881 | 3252 | 2653 | 3436 | 680 | 95.1 | 58.2 | 57.6 | 97.8 |
| 36 | 27953 | 3204 | 2583 | 3336 | 674 | 93.6 | 56.6 | 55.9 | 96.9 |
| 38 | 28024 | 3083 | 2483 | 3196 | 666 | 90.1 | 54.4 | 53.6 | 95.8 |
| 40 | 28103 | 3034 | 2285 | 2928 | 656 | 88.7 | 50.1 | 49.1 | 94.4 |
| 42 | 28183 | 2975 | 2107 | 2689 | 644 | 86.9 | 46.2 | 45.1 | 92.6 |
| 44 | 28262 | 2881 | 1965 | 2507 | 626 | 84.2 | 43.1 | 42.0 | 90.0 |
| 46 | 28341 | 2789 | 1933 | 2462 | 595 | 81.5 | 42.4 | 41.3 | 85.6 |
| 48 | 28420 | 2718 | 1844 | 2344 | 502 | 79.4 | 40.4 | 39.3 | 72.2 |
| 50 | 28497 | 2661 | 1821 | 2316 | 516 | 77.8 | 39.9 | 38.8 | 74.2 |
| 52 | 28548 | 2598 | 1816 | 2305 | 536 | 75.9 | 39.8 | 38.6 | 77.2 |
| 54 | 28598 | 2522 | 1777 | 2250 | 548 | 73.7 | 39.0 | 37.7 | 78.9 |

Reach 6 (Study Site 6):

Table F-16. Weighted usable area (WUA) versus discharge relationships for steelhead at Big Timber Creek, Study Site 6.

| Discharge (cfs) | Total (ft ²)/1,000 ft | WUA (ft ²)/1,000 ft | | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|---------------------------------|-------|----------|----------------|----------------------------|-------|----------|----------------|
| | | Spawning | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 3 | 17400 | 1222 | 5849 | 9188 | 1801 | 16.7 | 48.1 | 64.6 | 61.4 |
| 5 | 19218 | 2216 | 6836 | 11359 | 2142 | 30.3 | 56.2 | 79.9 | 73.0 |
| 7 | 19912 | 3122 | 7925 | 13038 | 2534 | 42.7 | 65.1 | 91.7 | 86.4 |
| 9 | 20346 | 3910 | 9124 | 13805 | 2705 | 53.5 | 75.0 | 97.1 | 92.2 |
| 11 | 20659 | 4466 | 9766 | 14198 | 2843 | 61.0 | 80.2 | 99.8 | 96.9 |
| 13.9 | 20945 | 5398 | 10411 | 14222 | 2910 | 73.8 | 85.5 | 100.0 | 99.2 |
| 15 | 21023 | 5592 | 10591 | 14197 | 2933 | 76.4 | 87.0 | 99.8 | 100.0 |
| 19 | 21358 | 6228 | 11254 | 13564 | 2887 | 85.1 | 92.5 | 95.4 | 98.4 |
| 19.9 | 21411 | 6324 | 11393 | 13248 | 2828 | 86.5 | 93.6 | 93.1 | 96.4 |
| 21 | 21456 | 6428 | 11515 | 12984 | 2750 | 87.9 | 94.6 | 91.3 | 93.8 |
| 23 | 21525 | 6593 | 11711 | 12380 | 2539 | 90.1 | 96.2 | 87.0 | 86.6 |
| 25 | 21589 | 6728 | 11852 | 11925 | 2481 | 92.0 | 97.4 | 83.9 | 84.6 |
| 27 | 21649 | 6848 | 11972 | 11452 | 2424 | 93.6 | 98.4 | 80.5 | 82.7 |
| 31 | 21760 | 7110 | 12139 | 10606 | 2138 | 97.2 | 99.7 | 74.6 | 72.9 |
| 31.5 | 21773 | 7129 | 12142 | 10488 | 2106 | 97.5 | 99.8 | 73.7 | 71.8 |
| 33 | 21812 | 7177 | 12165 | 10326 | 2060 | 98.1 | 99.9 | 72.6 | 70.2 |
| 35 | 21861 | 7255 | 12172 | 9818 | 1930 | 99.2 | 100.0 | 69.0 | 65.8 |
| 37 | 21909 | 7295 | 12125 | 9686 | 1910 | 99.7 | 99.6 | 68.1 | 65.1 |
| 39 | 21955 | 7315 | 12077 | 9479 | 1879 | 100.0 | 99.2 | 66.6 | 64.1 |
| 41 | 21998 | 7278 | 11986 | 9131 | 1828 | 99.5 | 98.5 | 64.2 | 62.3 |
| 43 | 22041 | 7196 | 11870 | 8626 | 1693 | 98.4 | 97.5 | 60.7 | 57.7 |
| 45 | 22082 | 7164 | 11775 | 8353 | 1646 | 97.9 | 96.7 | 58.7 | 56.1 |
| 47 | 22121 | 7090 | 11676 | 7790 | 1482 | 96.9 | 95.9 | 54.8 | 50.5 |
| 49 | 22160 | 7074 | 11566 | 7244 | 1411 | 96.7 | 95.0 | 50.9 | 48.1 |
| 51 | 22206 | 6946 | 11327 | 6919 | 1406 | 95.0 | 93.1 | 48.6 | 47.9 |
| 53 | 22252 | 6884 | 11214 | 6752 | 1316 | 94.1 | 92.1 | 47.5 | 44.9 |
| 55 | 22295 | 6783 | 11083 | 6756 | 1350 | 92.7 | 91.1 | 47.5 | 46.0 |
| 57 | 22337 | 6552 | 10829 | 6760 | 1388 | 89.6 | 89.0 | 47.5 | 47.3 |
| 59 | 22378 | 6415 | 10653 | 6750 | 1423 | 87.7 | 87.5 | 47.5 | 48.5 |

Table F-17. Weighted usable area (WUA) versus discharge relationships for Chinook salmon at Big Timber Creek, Study Site 6.

| Discharge (cfs) | Total (ft ²)/1,000 ft | WUA (ft ²)/1,000 ft | | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|---------------------------------|-------|----------|----------------|----------------------------|-------|----------|----------------|
| | | Spawning | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 3 | 17400 | 1222 | 5849 | 6808 | 1223 | 16.7 | 48.1 | 79.7 | 72.9 |
| 5 | 19218 | 2216 | 6836 | 7760 | 1275 | 30.3 | 56.2 | 90.8 | 76.0 |
| 7 | 19912 | 3122 | 7925 | 8228 | 1425 | 42.7 | 65.1 | 96.3 | 84.9 |
| 9 | 20346 | 3910 | 9124 | 8481 | 1644 | 53.5 | 75.0 | 99.2 | 98.0 |
| 11 | 20659 | 4466 | 9766 | 8545 | 1677 | 61.0 | 80.2 | 100.0 | 100.0 |
| 13.9 | 20945 | 5398 | 10411 | 8448 | 1649 | 73.8 | 85.5 | 98.9 | 98.3 |
| 15 | 21023 | 5592 | 10591 | 8336 | 1624 | 76.4 | 87.0 | 97.6 | 96.8 |
| 19 | 21358 | 6228 | 11254 | 7916 | 1615 | 85.1 | 92.5 | 92.6 | 96.3 |
| 19.9 | 21411 | 6324 | 11393 | 7828 | 1600 | 86.5 | 93.6 | 91.6 | 95.4 |
| 21 | 21456 | 6428 | 11515 | 7727 | 1575 | 87.9 | 94.6 | 90.4 | 93.9 |
| 23 | 21525 | 6593 | 11711 | 7534 | 1546 | 90.1 | 96.2 | 88.2 | 92.2 |
| 25 | 21589 | 6728 | 11852 | 7241 | 1502 | 92.0 | 97.4 | 84.7 | 89.6 |
| 27 | 21649 | 6848 | 11972 | 6969 | 1441 | 93.6 | 98.4 | 81.6 | 85.9 |
| 31 | 21760 | 7110 | 12139 | 6563 | 1378 | 97.2 | 99.7 | 76.8 | 82.1 |
| 31.5 | 21773 | 7129 | 12142 | 6510 | 1371 | 97.5 | 99.8 | 76.2 | 81.8 |
| 33 | 21812 | 7177 | 12165 | 6239 | 1347 | 98.1 | 99.9 | 73.0 | 80.3 |
| 35 | 21861 | 7255 | 12172 | 6096 | 1322 | 99.2 | 100.0 | 71.3 | 78.8 |
| 37 | 21909 | 7295 | 12125 | 5925 | 1279 | 99.7 | 99.6 | 69.3 | 76.3 |
| 39 | 21955 | 7315 | 12077 | 5756 | 1226 | 100.0 | 99.2 | 67.4 | 73.1 |
| 41 | 21998 | 7278 | 11986 | 5564 | 1174 | 99.5 | 98.5 | 65.1 | 70.0 |
| 43 | 22041 | 7196 | 11870 | 5372 | 1133 | 98.4 | 97.5 | 62.9 | 67.6 |
| 45 | 22082 | 7164 | 11775 | 5272 | 1115 | 97.9 | 96.7 | 61.7 | 66.5 |
| 47 | 22121 | 7090 | 11676 | 5205 | 1107 | 96.9 | 95.9 | 60.9 | 66.0 |
| 49 | 22160 | 7074 | 11566 | 5078 | 1081 | 96.7 | 95.0 | 59.4 | 64.5 |
| 51 | 22206 | 6946 | 11327 | 4874 | 1065 | 95.0 | 93.1 | 57.0 | 63.5 |
| 53 | 22252 | 6884 | 11214 | 4817 | 1071 | 94.1 | 92.1 | 56.4 | 63.9 |
| 55 | 22295 | 6783 | 11083 | 4729 | 1046 | 92.7 | 91.1 | 55.3 | 62.4 |
| 57 | 22337 | 6552 | 10829 | 4541 | 993 | 89.6 | 89.0 | 53.1 | 59.2 |
| 59 | 22378 | 6415 | 10653 | 4462 | 1010 | 87.7 | 87.5 | 52.2 | 60.2 |

Table F-18. Weighted usable area (WUA) versus discharge relationships for bull trout at Big Timber Creek, Study Site 6.

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 3 | 17400 | 135 | 5042 | 6775 | 1481 | 10.9 | 58.3 | 59.8 | 69.4 |
| 5 | 19218 | 264 | 6208 | 8321 | 1666 | 21.4 | 71.8 | 73.4 | 78.1 |
| 7 | 19912 | 389 | 6751 | 9020 | 1722 | 31.6 | 78.1 | 79.6 | 80.7 |
| 9 | 20346 | 518 | 7297 | 9728 | 1820 | 42.0 | 84.4 | 85.8 | 85.3 |
| 11 | 20659 | 591 | 7833 | 10411 | 1938 | 48.0 | 90.6 | 91.8 | 90.8 |
| 13.9 | 20945 | 713 | 8425 | 11153 | 2122 | 57.8 | 97.4 | 98.4 | 99.5 |
| 15 | 21023 | 757 | 8466 | 11186 | 2134 | 61.4 | 97.9 | 98.7 | 100.0 |
| 19 | 21358 | 875 | 8643 | 11335 | 2088 | 70.9 | 99.9 | 100.0 | 97.9 |
| 19.9 | 21411 | 902 | 8648 | 11323 | 2076 | 73.2 | 100.0 | 99.9 | 97.3 |
| 21 | 21456 | 933 | 8625 | 11268 | 2053 | 75.7 | 99.7 | 99.4 | 96.2 |
| 23 | 21525 | 974 | 8518 | 11087 | 1993 | 79.0 | 98.5 | 97.8 | 93.4 |
| 25 | 21589 | 1003 | 8397 | 10897 | 1941 | 81.4 | 97.1 | 96.1 | 91.0 |
| 27 | 21649 | 1044 | 8336 | 10785 | 1962 | 84.7 | 96.4 | 95.1 | 92.0 |
| 31 | 21760 | 1109 | 8316 | 10710 | 1908 | 90.0 | 96.2 | 94.5 | 89.4 |
| 31.5 | 21773 | 1113 | 8310 | 10694 | 1905 | 90.3 | 96.1 | 94.3 | 89.3 |
| 33 | 21812 | 1123 | 8273 | 10628 | 1888 | 91.1 | 95.7 | 93.8 | 88.5 |
| 35 | 21861 | 1159 | 8131 | 10419 | 1808 | 94.0 | 94.0 | 91.9 | 84.7 |
| 37 | 21909 | 1184 | 8063 | 10310 | 1808 | 96.1 | 93.2 | 91.0 | 84.7 |
| 39 | 21955 | 1198 | 7917 | 10102 | 1785 | 97.2 | 91.5 | 89.1 | 83.7 |
| 41 | 21998 | 1209 | 7667 | 9764 | 1700 | 98.1 | 88.6 | 86.1 | 79.7 |
| 43 | 22041 | 1215 | 7533 | 9570 | 1714 | 98.5 | 87.1 | 84.4 | 80.4 |
| 45 | 22082 | 1220 | 7464 | 9465 | 1700 | 99.0 | 86.3 | 83.5 | 79.7 |
| 47 | 22121 | 1231 | 7349 | 9303 | 1666 | 99.9 | 85.0 | 82.1 | 78.1 |
| 49 | 22160 | 1233 | 7177 | 9072 | 1598 | 100.0 | 83.0 | 80.0 | 74.9 |
| 51 | 22206 | 1233 | 6788 | 8585 | 1393 | 100.0 | 78.5 | 75.7 | 65.3 |
| 53 | 22252 | 1231 | 6656 | 8401 | 1353 | 99.9 | 77.0 | 74.1 | 63.4 |
| 55 | 22295 | 1228 | 6482 | 8166 | 1357 | 99.7 | 75.0 | 72.0 | 63.6 |
| 57 | 22337 | 1222 | 6387 | 8016 | 1358 | 99.1 | 73.9 | 70.7 | 63.6 |
| 59 | 22378 | 1213 | 6283 | 7856 | 1355 | 98.4 | 72.7 | 69.3 | 63.5 |

Reach 7 (Reference Site):

Table F-19. Weighted usable area (WUA) versus discharge relationships for steelhead at Big Timber Creek, Reference Site (Study Site 7).

| Discharge (cfs) | Total (ft ²)/1,000 ft | WUA (ft ²)/1,000 ft | | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|---------------------------------|-------|----------|----------------|----------------------------|-------|----------|----------------|
| | | Spawning | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 5 | 19737 | 2383 | 7138 | 12490 | 817 | 23.8 | 54.1 | 75.7 | 20.2 |
| 10 | 21993 | 5898 | 9412 | 15300 | 1382 | 58.8 | 71.4 | 92.7 | 34.2 |
| 15 | 23080 | 7335 | 10831 | 16498 | 1794 | 73.1 | 82.2 | 100.0 | 44.4 |
| 17 | 23364 | 7678 | 11254 | 16475 | 1959 | 76.5 | 85.4 | 99.9 | 48.5 |
| 20 | 23620 | 8058 | 11747 | 15806 | 2184 | 80.3 | 89.1 | 95.8 | 54.0 |
| 25 | 23937 | 8630 | 12462 | 14574 | 2747 | 86.0 | 94.5 | 88.3 | 68.0 |
| 27 | 24036 | 8819 | 12679 | 13567 | 2963 | 87.9 | 96.2 | 82.2 | 73.3 |
| 30 | 24246 | 9073 | 12922 | 12038 | 3189 | 90.4 | 98.0 | 73.0 | 78.9 |
| 35 | 24729 | 9561 | 13133 | 9941 | 3464 | 95.3 | 99.6 | 60.3 | 85.7 |
| 40 | 25145 | 9833 | 13182 | 8846 | 3662 | 98.0 | 100.0 | 53.6 | 90.6 |
| 45 | 25933 | 9974 | 13096 | 8372 | 3849 | 99.4 | 99.3 | 50.7 | 95.2 |
| 47 | 26013 | 10008 | 13040 | 7933 | 3914 | 99.7 | 98.9 | 48.1 | 96.8 |
| 50 | 26096 | 10033 | 12901 | 7482 | 3972 | 100.0 | 97.9 | 45.3 | 98.3 |
| 55 | 26236 | 9840 | 12555 | 6948 | 4026 | 98.1 | 95.2 | 42.1 | 99.6 |
| 60 | 26367 | 9396 | 12184 | 6517 | 4041 | 93.7 | 92.4 | 39.5 | 100.0 |
| 65 | 26489 | 9276 | 12071 | 5897 | 3794 | 92.5 | 91.6 | 35.7 | 93.9 |
| 70 | 26605 | 8997 | 11704 | 5781 | 3862 | 89.7 | 88.8 | 35.0 | 95.5 |
| 75 | 26709 | 8583 | 11299 | 5616 | 3900 | 85.5 | 85.7 | 34.0 | 96.5 |
| 80 | 26805 | 7802 | 10609 | 5488 | 3865 | 77.8 | 80.5 | 33.3 | 95.6 |
| 85 | 26896 | 6889 | 9740 | 5288 | 3932 | 68.7 | 73.9 | 32.0 | 97.3 |
| 90 | 26980 | 6514 | 9347 | 5319 | 3977 | 64.9 | 70.9 | 32.2 | 98.4 |
| 95 | 27053 | 6020 | 8783 | 5286 | 3968 | 60.0 | 66.6 | 32.0 | 98.2 |
| 100 | 27109 | 5406 | 8160 | 5138 | 3863 | 53.9 | 61.9 | 31.1 | 95.6 |

Table F-20. Weighted usable area (WUA) versus discharge relationships for Chinook salmon at Big Timber Creek, Reference Site (Study Site 7).

| Discharge (cfs) | Total (ft ²)/1,000 ft | WUA (ft ²)/1,000 ft | | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|---------------------------------|-------|----------|----------------|----------------------------|-------|----------|----------------|
| | | Spawning | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 5 | 19737 | 2383 | 7138 | 8272 | 482 | 23.8 | 54.1 | 90.1 | 21.5 |
| 10 | 21993 | 5898 | 9412 | 9184 | 700 | 58.8 | 71.4 | 100.0 | 31.1 |
| 15 | 23080 | 7335 | 10831 | 9045 | 1085 | 73.1 | 82.2 | 98.5 | 48.3 |
| 17 | 23364 | 7678 | 11254 | 8873 | 1227 | 76.5 | 85.4 | 96.6 | 54.6 |
| 20 | 23620 | 8058 | 11747 | 8462 | 1411 | 80.3 | 89.1 | 92.1 | 62.8 |
| 25 | 23937 | 8630 | 12462 | 7647 | 1658 | 86.0 | 94.5 | 83.3 | 73.8 |
| 27 | 24036 | 8819 | 12679 | 7247 | 1708 | 87.9 | 96.2 | 78.9 | 76.0 |
| 30 | 24246 | 9073 | 12922 | 6866 | 1758 | 90.4 | 98.0 | 74.8 | 78.2 |
| 35 | 24729 | 9561 | 13133 | 6059 | 1810 | 95.3 | 99.6 | 66.0 | 80.6 |
| 40 | 25145 | 9833 | 13182 | 5363 | 1854 | 98.0 | 100.0 | 58.4 | 82.5 |
| 45 | 25933 | 9974 | 13096 | 4846 | 1878 | 99.4 | 99.3 | 52.8 | 83.6 |
| 47 | 26013 | 10008 | 13040 | 4617 | 1875 | 99.7 | 98.9 | 50.3 | 83.5 |
| 50 | 26096 | 10033 | 12901 | 4521 | 1866 | 100.0 | 97.9 | 49.2 | 83.1 |
| 55 | 26236 | 9840 | 12555 | 4357 | 1930 | 98.1 | 95.2 | 47.4 | 85.9 |
| 60 | 26367 | 9396 | 12184 | 4061 | 2087 | 93.7 | 92.4 | 44.2 | 92.9 |
| 65 | 26489 | 9276 | 12071 | 3907 | 2214 | 92.5 | 91.6 | 42.5 | 98.6 |
| 70 | 26605 | 8997 | 11704 | 3785 | 2245 | 89.7 | 88.8 | 41.2 | 99.9 |
| 75 | 26709 | 8583 | 11299 | 3639 | 2247 | 85.5 | 85.7 | 39.6 | 100.0 |
| 80 | 26805 | 7802 | 10609 | 3486 | 2191 | 77.8 | 80.5 | 38.0 | 97.5 |
| 85 | 26896 | 6889 | 9740 | 3454 | 2220 | 68.7 | 73.9 | 37.6 | 98.8 |
| 90 | 26980 | 6514 | 9347 | 3352 | 2208 | 64.9 | 70.9 | 36.5 | 98.3 |
| 95 | 27053 | 6020 | 8783 | 3263 | 2153 | 60.0 | 66.6 | 35.5 | 95.8 |
| 100 | 27109 | 5406 | 8160 | 3166 | 2132 | 53.9 | 61.9 | 34.5 | 94.9 |

Table F-21. Weighted usable area (WUA) versus discharge relationships for bull trout at Big Timber Creek, Reference Site (Study Site 7).

| Discharge (cfs) | Total (ft ²)/1,000 ft | Spawning | WUA (ft ²)/1,000 ft | | | Percent of optimal habitat | | | |
|-----------------|-----------------------------------|----------|---------------------------------|----------|----------------|----------------------------|-------|----------|----------------|
| | | | Adult | Juvenile | Juvenile cover | Spawning | Adult | Juvenile | Juvenile cover |
| 5 | 19737 | 31 | 5936 | 7850 | 409 | 1.0 | 67.2 | 69.1 | 13.6 |
| 10 | 21993 | 289 | 8145 | 10666 | 782 | 9.2 | 92.3 | 93.9 | 26.0 |
| 15 | 23080 | 832 | 8677 | 11257 | 965 | 26.4 | 98.3 | 99.1 | 32.1 |
| 17 | 23364 | 1067 | 8748 | 11305 | 1072 | 33.9 | 99.1 | 99.5 | 35.7 |
| 20 | 23620 | 1317 | 8829 | 11361 | 1241 | 41.8 | 100.0 | 100.0 | 41.3 |
| 25 | 23937 | 1736 | 8812 | 11257 | 1652 | 55.1 | 99.8 | 99.1 | 55.0 |
| 27 | 24036 | 1917 | 8804 | 11227 | 1890 | 60.9 | 99.7 | 98.8 | 62.9 |
| 30 | 24246 | 2175 | 8560 | 10858 | 2074 | 69.0 | 97.0 | 95.6 | 69.1 |
| 35 | 24729 | 2531 | 7916 | 9969 | 2362 | 80.3 | 89.7 | 87.8 | 78.6 |
| 40 | 25145 | 2794 | 7213 | 9027 | 2488 | 88.7 | 81.7 | 79.5 | 82.8 |
| 45 | 25933 | 3027 | 6214 | 7704 | 2566 | 96.1 | 70.4 | 67.8 | 85.4 |
| 47 | 26013 | 3086 | 6066 | 7515 | 2589 | 98.0 | 68.7 | 66.1 | 86.2 |
| 50 | 26096 | 3107 | 5683 | 7033 | 2615 | 98.6 | 64.4 | 61.9 | 87.0 |
| 55 | 26236 | 3134 | 5148 | 6359 | 2718 | 99.5 | 58.3 | 56.0 | 90.5 |
| 60 | 26367 | 3150 | 4654 | 5774 | 2758 | 100.0 | 52.7 | 50.8 | 91.8 |
| 65 | 26489 | 3041 | 4095 | 5105 | 2773 | 96.5 | 46.4 | 44.9 | 92.3 |
| 70 | 26605 | 2947 | 3827 | 4801 | 2768 | 93.6 | 43.3 | 42.3 | 92.2 |
| 75 | 26709 | 2830 | 3816 | 4791 | 2887 | 89.9 | 43.2 | 42.2 | 96.1 |
| 80 | 26805 | 2780 | 3770 | 4744 | 3004 | 88.3 | 42.7 | 41.8 | 100.0 |
| 85 | 26896 | 2684 | 3581 | 4499 | 2809 | 85.2 | 40.6 | 39.6 | 93.5 |
| 90 | 26980 | 2569 | 3525 | 4440 | 2835 | 81.5 | 39.9 | 39.1 | 94.4 |
| 95 | 27053 | 2440 | 3533 | 4443 | 2824 | 77.5 | 40.0 | 39.1 | 94.0 |
| 100 | 27109 | 2236 | 3409 | 4270 | 2669 | 71.0 | 38.6 | 37.6 | 88.9 |

**Comparison with EA Engineering Habitat Modeling Results at Reference Site
(Study Site 7)**

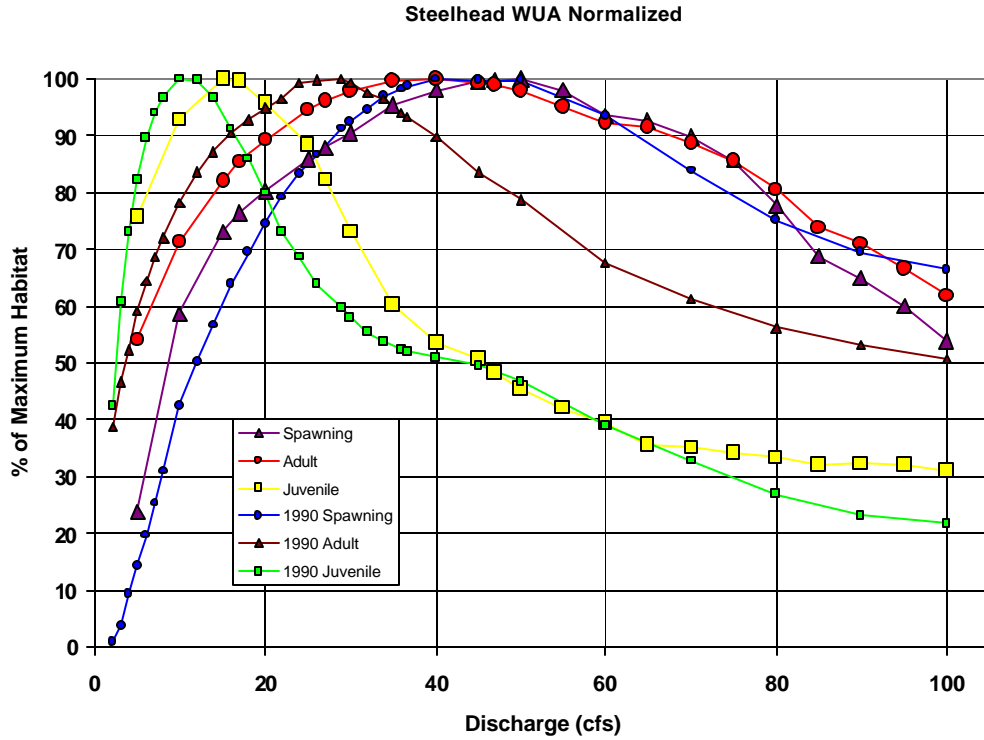


Figure F-1. Habitat versus flow relationships for steelhead in Big Timber Creek upstream from diversions comparing EA Engineering study and Reclamation's study (2003).

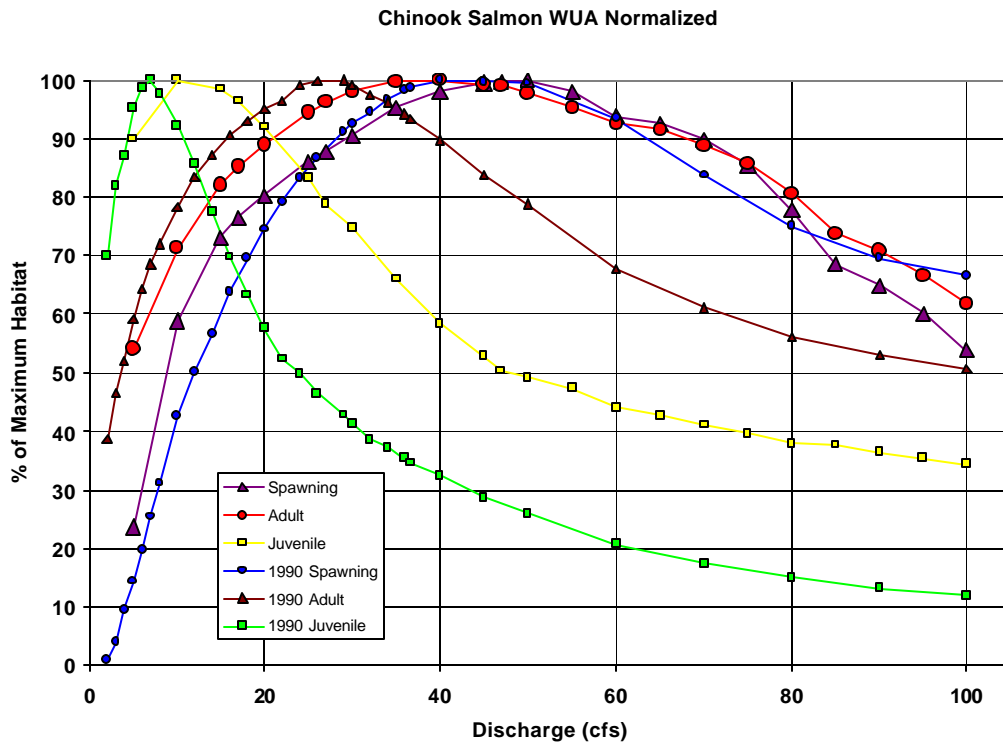


Figure F-2. Habitat versus flow relationships for Chinook salmon in Big Timber Creek upstream from diversions comparing EA Engineering study and Reclamation’s study (2003)

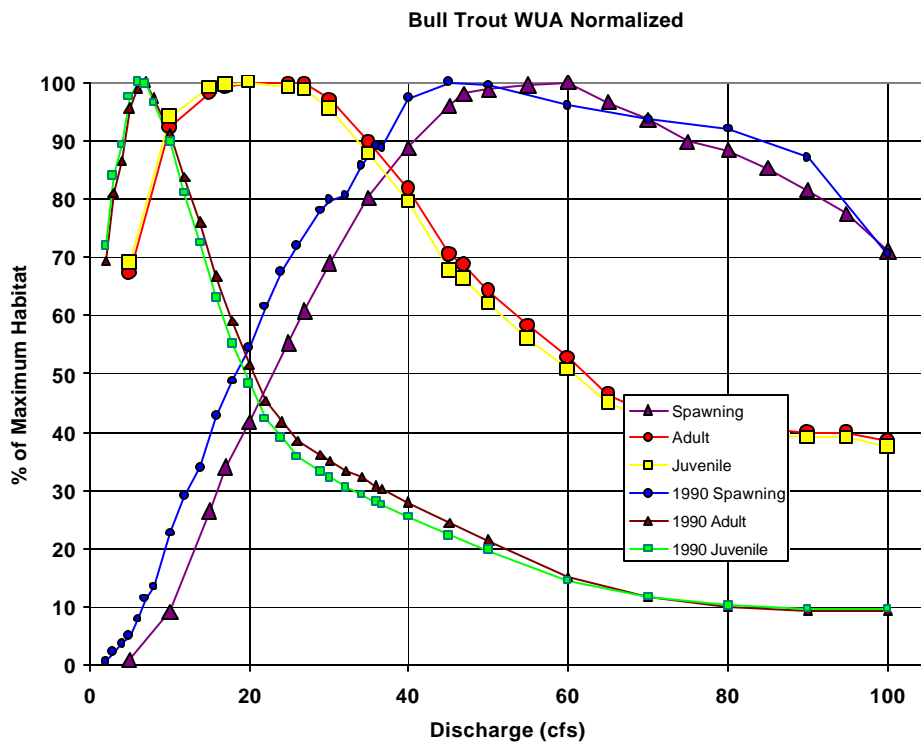


Figure F-3. Habitat versus flow relationships for bull trout in Big Timber Creek upstream from diversions comparing EA Engineering study and Reclamation’s study (2003)

Appendix G – IFG4 input files for PHABSIM

Big Timber Study Site 1 - substrate

Export from PHABSIM for Windows

```

IOC      0000000100010000100000
QARD    1.4
QARD    2.0
QARD    3.0
QARD    4.0
QARD    5.0
QARD    6.0
QARD    6.5
QARD    7.0
QARD    8.0
QARD    9.0
QARD   10.0
QARD   11.0
QARD   12.0
QARD   13.0
QARD   14.0
QARD   15.0
QARD   16.0
QARD   17.0
QARD   18.0
QARD   19.0
QARD   20.0
XSEC    1.0      0.0 1.0      96.15  0.00083
        1.0  0.0 98.9  1.3 98.0  9.6 97.3 10.4 97.0 11.0 96.8 12.0 96.3
        1.0 13.6 96.3 14.0 96.3 14.5 96.3 15.0 96.3 16.0 96.2 16.5 96.3
        1.0 17.0 96.2 17.5 96.3 18.0 96.3 18.5 96.3 19.0 96.3 22.4 98.7
NS      1.0      1.0      1.0      2.0      2.0      2.0      4.0
NS      1.0      4.0      5.0      4.0      4.0      6.0      4.0
NS      1.0      4.0      4.0      3.0      2.0      2.0      1.0
WSL    1.0      97.1      97.2      97.2      97.3      97.3      97.3
WSL    1.0      97.3      97.4      97.4      97.4      97.4      97.4
WSL    1.0      97.5      97.5      97.5      97.5      97.5      97.5
WSL    1.0      97.5      97.5      97.5
CAL1   1.0      97.13      1.40      0.99
VEL1   1.0      0.05 0.03 0.01 0.03 0.04 0.16 0.33 0.28 0.28
VEL1   1.0 0.37 0.29 0.10 0.01 0.01
CAL2   1.0      97.35      6.50      6.90
VEL2   1.0      0.02 0.01 0.01 0.77 1.29 1.29 1.03 1.05 1.04
VEL2   1.0 1.09 1.15 0.87 0.31 0.06
XSEC   2.0      55.0 1.0      96.70  0.00280
        2.0  0.0 98.8  1.6 98.4  1.8 97.7  3.5 97.3  4.6 97.1  5.1 97.0
        2.0  6.1 97.0  7.1 96.9  8.1 96.8  9.1 96.9 10.1 96.8 11.1 96.7
        2.0 12.1 96.7 13.1 96.8 14.1 96.9 15.1 97.0 16.1 97.2 17.1 97.3
        2.0 18.0 97.4 20.3 97.2 20.7 98.4 23.5 98.8
NS     2.0      1.0      1.0      2.0      2.0      2.0      4.0
NS     2.0      4.0      4.0      4.0      4.0      4.0      4.0
NS     2.0      4.0      4.0      3.0      2.0      2.0      2.0
NS     2.0      2.0      2.0      2.0      1.0
WSL    2.0      97.1      97.2      97.2      97.3      97.3      97.3
WSL    2.0      97.4      97.4      97.4      97.4      97.4      97.5
WSL    2.0      97.5      97.5      97.5      97.5      97.5      97.6
WSL    2.0      97.6      97.6      97.6
CAL1   2.0      97.14      1.40      0.72
VEL1   2.0      0.05 0.17 0.20 0.26 0.27 0.46
VEL1   2.0 0.44 0.40 0.24
CAL2   2.0      97.36      6.50      5.80
VEL2   2.0      0.01 0.36 0.47 0.73 0.93 0.82 1.05 1.11 1.22
VEL2   2.0 1.19 1.05 1.20 0.47 0.05 0.04 0.01 0.01
XSEC   3.0      0.0 1.0      96.70  0.00023
        3.0  0.0 98.4  2.6 98.1  6.9 97.4  7.4 97.0  8.0 96.9  8.4 96.8
        3.0  9.4 96.2 10.4 95.9 11.4 95.8 12.4 95.7 13.4 95.8 14.4 95.9
        3.0 15.4 96.0 16.4 96.1 17.4 96.4 18.4 96.5 19.4 97.0 19.7 97.4
        3.0 21.9 98.8
NS     3.0      1.0      1.0      3.0      2.0      2.0      2.0
NS     3.0      2.0      4.0      3.0      5.0      5.0      5.0
NS     3.0      5.0      3.0      2.0      2.0      1.0      1.0
NS     3.0      1.0

```


| | | | | | | | | | | | | | |
|------|-----|-------|-------|-------|---------|------|------|------|------|------|------|------|------|
| WSL | 3.0 | 97.1 | 97.2 | 97.3 | 97.3 | 97.4 | 97.4 | | | | | | |
| WSL | 3.0 | 97.4 | 97.4 | 97.5 | 97.5 | 97.5 | 97.6 | | | | | | |
| WSL | 3.0 | 97.6 | 97.6 | 97.7 | 97.7 | 97.7 | 97.7 | | | | | | |
| WSL | 3.0 | 97.8 | 97.8 | 97.8 | | | | | | | | | |
| CAL1 | 3.0 | 97.15 | 1.40 | 1.10 | | | | | | | | | |
| VEL1 | 3.0 | | | 0.11 | 0.03 | 0.02 | 0.05 | 0.10 | 0.15 | 0.20 | 0.11 | | |
| VEL1 | 3.0 | 0.14 | 0.14 | 0.10 | 0.01 | | | | | | | | |
| CAL2 | 3.0 | 97.42 | 6.50 | 6.10 | | | | | | | | | |
| VEL2 | 3.0 | | 0.05 | 0.07 | 0.18 | 0.36 | 0.58 | 0.59 | 0.62 | 0.62 | 0.67 | | |
| VEL2 | 3.0 | 0.04 | 0.15 | 0.02 | 0.02 | | | | | | | | |
| XSEC | 4.0 | 170.0 | 1.0 | 96.70 | 0.00048 | | | | | | | | |
| | 4.0 | 0.0 | 98.8 | 4.0 | 98.1 | 7.1 | 97.4 | 8.1 | 97.4 | 9.1 | 97.0 | 10.1 | 96.8 |
| | 4.0 | 11.1 | 96.6 | 12.1 | 96.4 | 13.1 | 96.3 | 14.1 | 96.2 | 15.1 | 96.2 | 16.1 | 96.1 |
| | 4.0 | 17.1 | 96.1 | 18.1 | 96.1 | 19.1 | 96.1 | 20.1 | 96.1 | 21.1 | 96.2 | 21.6 | 97.0 |
| | 4.0 | 22.6 | 97.0 | 25.7 | 99.1 | | | | | | | | |
| NS | 4.0 | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 | 1.0 | 3.0 | | | | | |
| NS | 4.0 | 3.0 | 4.0 | 3.0 | 3.0 | 3.0 | 3.0 | 4.0 | | | | | |
| NS | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 2.0 | 1.0 | | | | | |
| NS | 4.0 | 1.0 | 1.0 | 1.0 | | | | | | | | | |
| WSL | 4.0 | 97.1 | 97.2 | 97.3 | 97.3 | 97.4 | 97.4 | 97.4 | | | | | |
| WSL | 4.0 | 97.4 | 97.5 | 97.5 | 97.5 | 97.5 | 97.6 | 97.6 | | | | | |
| WSL | 4.0 | 97.6 | 97.7 | 97.7 | 97.7 | 97.7 | 97.8 | 97.8 | | | | | |
| WSL | 4.0 | 97.8 | 97.8 | 97.9 | | | | | | | | | |
| CAL1 | 4.0 | 97.16 | 1.40 | 1.10 | | | | | | | | | |
| VEL1 | 4.0 | | | 0.08 | 0.34 | 0.36 | 0.26 | 0.11 | 0.05 | 0.04 | 0.07 | | |
| VEL1 | 4.0 | 0.11 | 0.05 | 0.03 | 0.02 | 0.01 | | | | | | | |
| CAL2 | 4.0 | 97.44 | 6.50 | 6.20 | | | | | | | | | |
| VEL2 | 4.0 | | 0.01 | 0.01 | 0.75 | 0.70 | 1.00 | 0.50 | 0.87 | 0.84 | 0.80 | 0.60 | |
| VEL2 | 4.0 | 0.25 | 0.07 | 0.07 | 0.01 | 0.01 | 0.07 | 0.10 | | | | | |
| XSEC | 5.0 | 170.0 | 1.0 | 96.95 | 0.00111 | | | | | | | | |
| | 5.0 | 0.0 | 98.8 | 2.9 | 98.5 | 3.4 | 97.0 | 3.9 | 97.0 | 4.9 | 97.0 | 5.9 | 97.0 |
| | 5.0 | 6.9 | 97.0 | 7.9 | 97.0 | 8.9 | 97.0 | 9.9 | 97.0 | 10.9 | 97.0 | 11.9 | 97.2 |
| | 5.0 | 12.9 | 97.0 | 13.9 | 97.0 | 14.9 | 97.0 | 15.9 | 97.2 | 17.9 | 97.2 | 19.0 | 97.5 |
| | 5.0 | 25.9 | 98.2 | 26.4 | 99.0 | 29.8 | 99.3 | | | | | | |
| NS | 5.0 | 1.0 | 1.0 | 1.0 | 1.0 | 2.0 | 4.0 | 4.0 | | | | | |
| NS | 5.0 | 4.0 | 4.0 | 4.0 | 5.0 | 4.0 | 4.0 | 4.0 | | | | | |
| NS | 5.0 | 4.0 | 4.0 | 3.0 | 2.0 | 2.0 | 2.0 | 2.0 | | | | | |
| NS | 5.0 | 1.0 | 1.0 | 1.0 | | | | | | | | | |
| WSL | 5.0 | 97.2 | 97.2 | 97.3 | 97.3 | 97.4 | 97.4 | 97.4 | | | | | |
| WSL | 5.0 | 97.4 | 97.5 | 97.5 | 97.5 | 97.5 | 97.6 | 97.6 | | | | | |
| WSL | 5.0 | 97.6 | 97.7 | 97.7 | 97.7 | 97.7 | 97.8 | 97.8 | | | | | |
| WSL | 5.0 | 97.8 | 97.8 | 97.9 | | | | | | | | | |
| CAL1 | 5.0 | 97.17 | 1.40 | 0.64 | | | | | | | | | |
| VEL1 | 5.0 | | 0.01 | 0.31 | 0.56 | 0.11 | 0.55 | 0.52 | 0.07 | 0.55 | 0.33 | | |
| VEL1 | 5.0 | 0.25 | 0.34 | 0.31 | | | | | | | | | |
| CAL2 | 5.0 | 97.45 | 6.50 | 5.80 | | | | | | | | | |
| VEL2 | 5.0 | | 0.02 | 0.18 | 1.09 | 1.06 | 1.07 | 1.04 | 1.35 | 0.88 | 1.35 | 1.44 | |
| VEL2 | 5.0 | 1.24 | 0.92 | 1.07 | 0.04 | 0.07 | 0.01 | | | | | | |
| XSEC | 6.0 | 0.0 | 1.0 | 96.95 | 0.00986 | | | | | | | | |
| | 6.0 | 0.0 | 98.6 | 2.5 | 98.1 | 3.0 | 97.5 | 3.8 | 97.5 | 4.2 | 97.3 | 4.9 | 97.0 |
| | 6.0 | 5.9 | 96.8 | 6.9 | 96.7 | 7.9 | 96.6 | 8.9 | 96.6 | 9.9 | 96.6 | 10.9 | 96.7 |
| | 6.0 | 11.9 | 96.7 | 12.9 | 96.9 | 13.9 | 97.1 | 14.9 | 97.5 | 15.1 | 98.3 | | |
| NS | 6.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | | | | |
| NS | 6.0 | 3.0 | 4.0 | 4.0 | 4.0 | 5.0 | 4.0 | 4.0 | | | | | |
| NS | 6.0 | 4.0 | 4.0 | 2.0 | 1.0 | 1.0 | | | | | | | |
| WSL | 6.0 | 97.2 | 97.2 | 97.3 | 97.3 | 97.4 | 97.4 | 97.4 | | | | | |
| WSL | 6.0 | 97.5 | 97.5 | 97.5 | 97.6 | 97.6 | 97.6 | 97.6 | | | | | |
| WSL | 6.0 | 97.7 | 97.7 | 97.7 | 97.7 | 97.7 | 97.8 | 97.8 | | | | | |
| WSL | 6.0 | 97.8 | 97.8 | 97.9 | | | | | | | | | |
| CAL1 | 6.0 | 97.18 | 1.40 | 1.00 | | | | | | | | | |
| VEL1 | 6.0 | | | 0.13 | 0.18 | 0.19 | 0.24 | 0.30 | 0.20 | 0.30 | | | |
| VEL1 | 6.0 | 0.28 | 0.16 | 0.12 | | | | | | | | | |
| CAL2 | 6.0 | 97.46 | 6.50 | 6.30 | | | | | | | | | |
| VEL2 | 6.0 | | | 0.03 | 0.35 | 0.76 | 0.53 | 0.85 | 1.20 | 1.16 | 1.21 | | |
| VEL2 | 6.0 | 1.17 | 0.53 | 0.25 | 0.15 | | | | | | | | |
| XSEC | 7.0 | 170.0 | 0.9 | 97.50 | 0.01302 | | | | | | | | |
| | 7.0 | 0.01 | 100.0 | 8.9 | 98.7 | 9.0 | 97.8 | 9.7 | 97.6 | 10.4 | 97.7 | 11.4 | 97.5 |
| | 7.0 | 12.4 | 97.7 | 13.4 | 97.7 | 14.4 | 97.7 | 15.4 | 97.6 | 16.4 | 97.7 | 17.4 | 97.7 |
| | 7.0 | 18.4 | 97.9 | 19.2 | 97.8 | 19.8 | 99.6 | 23.3 | 99.6 | | | | |
| NS | 7.0 | 1.0 | 1.0 | 1.0 | 1.0 | 5.0 | 5.0 | 4.0 | | | | | |
| NS | 7.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 4.0 | 6.0 | | | | | |

| | | | | | | | | | | | | | |
|------|-----|----------|------|-------|---------|------|------|------|------|------|------|------|------|
| NS | 7.0 | 6.0 | 2.0 | 1.0 | 1.0 | | | | | | | | |
| WSL | 7.0 | 98.0 | 98.0 | 98.1 | 98.1 | 98.1 | 98.1 | 98.1 | 98.1 | 98.1 | 98.1 | | |
| WSL | 7.0 | 98.2 | 98.2 | 98.2 | 98.2 | 98.2 | 98.2 | 98.2 | 98.2 | 98.2 | 98.2 | | |
| WSL | 7.0 | 98.2 | 98.2 | 98.3 | 98.3 | 98.3 | 98.3 | 98.3 | 98.3 | 98.3 | 98.3 | | |
| WSL | 7.0 | 98.3 | 98.3 | 98.3 | 98.3 | | | | | | | | |
| CAL1 | 7.0 | 97.98 | 1.40 | 0.72 | | | | | | | | | |
| VEL1 | 7.0 | | 0.01 | 0.61 | 0.75 | 0.79 | 0.22 | 0.31 | 0.48 | 0.53 | 0.35 | 0.18 | |
| VEL1 | 7.0 | 0.78 | 0.09 | | | | | | | | | | |
| CAL2 | 7.0 | 98.15 | 6.50 | 6.80 | | | | | | | | | |
| VEL2 | 7.0 | | 0.01 | 1.62 | 2.13 | 2.30 | 1.07 | 1.47 | 1.14 | 1.03 | 2.87 | 2.16 | |
| VEL2 | 7.0 | 1.44 | 0.04 | | | | | | | | | | |
| XSEC | 8.0 | 435.0 | 0.0 | 98.00 | 0.01302 | | | | | | | | |
| | 8.0 | 0.0100.3 | 4.2 | 99.2 | 4.5 | 98.4 | 5.9 | 98.1 | 7.4 | 98.0 | 8.4 | 98.0 | |
| | 8.0 | 9.4 | 98.0 | 10.4 | 98.2 | 11.4 | 98.2 | 12.4 | 98.2 | 13.4 | 98.1 | 14.4 | 98.3 |
| | 8.0 | 15.4 | 98.4 | 16.4 | 98.4 | 17.7 | 98.7 | 25.9 | 98.7 | 26.5 | 99.6 | 27.7 | 99.7 |
| NS | 8.0 | 1.0 | 1.0 | 1.0 | 1.0 | 4.0 | 5.0 | 4.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| NS | 8.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| NS | 8.0 | 4.0 | 1.0 | 0.5 | 1.0 | 0.5 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| WSL | 8.0 | 98.4 | 98.5 | 98.6 | 98.6 | 98.6 | 98.6 | 98.6 | 98.6 | 98.6 | 98.6 | 98.6 | 98.7 |
| WSL | 8.0 | 98.7 | 98.7 | 98.7 | 98.7 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 |
| WSL | 8.0 | 98.8 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 |
| WSL | 8.0 | 98.9 | 99.0 | 99.0 | | | | | | | | | |
| CAL1 | 8.0 | 98.45 | 1.40 | 0.71 | | | | | | | | | |
| VEL1 | 8.0 | | 0.01 | 0.35 | 0.19 | 0.61 | 0.43 | 0.28 | 0.43 | 0.41 | 0.11 | | |
| VEL1 | 8.0 | | | | | | | | | | | | |
| CAL2 | 8.0 | 98.70 | 6.50 | 6.60 | | | | | | | | | |
| VEL2 | 8.0 | | 0.01 | 0.80 | 1.00 | 1.19 | 1.09 | 1.35 | 1.08 | 1.34 | 0.89 | 1.03 | |
| VEL2 | 8.0 | 0.76 | 0.80 | 0.01 | | | | | | | | | |
| ENDJ | | | | | | | | | | | | | |

Big Timber Study Site 2 - substrate

Export from PHABSIM for Windows

IOC 0000000100010000100000

| | | | | | | | | | | | | | |
|------|------|----------|----------|-------|---------|------|------|------|------|------|------|------|------|
| QARD | 2.0 | | | | | | | | | | | | |
| QARD | 3.0 | | | | | | | | | | | | |
| QARD | 4.0 | | | | | | | | | | | | |
| QARD | 4.9 | | | | | | | | | | | | |
| QARD | 5.0 | | | | | | | | | | | | |
| QARD | 6.0 | | | | | | | | | | | | |
| QARD | 7.0 | | | | | | | | | | | | |
| QARD | 8.0 | | | | | | | | | | | | |
| QARD | 8.2 | | | | | | | | | | | | |
| QARD | 9.0 | | | | | | | | | | | | |
| QARD | 10.0 | | | | | | | | | | | | |
| QARD | 11.0 | | | | | | | | | | | | |
| QARD | 12.0 | | | | | | | | | | | | |
| QARD | 13.0 | | | | | | | | | | | | |
| QARD | 14.0 | | | | | | | | | | | | |
| QARD | 15.0 | | | | | | | | | | | | |
| XSEC | 1.0 | 0.0 | 1.0 | 97.00 | 0.00588 | | | | | | | | |
| | 1.0 | 0.0100.4 | 0.9100.0 | 3.5 | 97.6 | 3.7 | 97.6 | 3.8 | 97.4 | 5.5 | 97.1 | | |
| | 1.0 | 7.0 | 97.1 | 8.5 | 97.0 | 10.0 | 97.1 | 11.5 | 97.1 | 13.0 | 97.2 | 14.5 | 97.3 |
| | 1.0 | 16.0 | 97.3 | 17.5 | 97.5 | 18.9 | 97.6 | 19.5 | 97.7 | 24.6 | 98.4 | | |
| NS | 1.0 | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 5.0 |
| NS | 1.0 | 6.0 | 6.0 | 6.0 | 7.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| NS | 1.0 | 6.0 | 5.0 | 2.0 | 2.0 | 2.0 | 3.0 | | | | | | |
| WSL | 1.0 | 97.4 | 97.5 | 97.5 | 97.5 | 0.0 | 97.5 | 97.5 | 97.5 | 97.5 | 97.5 | 97.6 | 97.6 |
| WSL | 1.0 | 97.6 | 97.6 | 97.6 | 0.0 | 97.6 | 97.6 | 97.6 | 97.6 | 97.6 | 97.6 | 97.7 | 97.7 |
| WSL | 1.0 | 97.7 | 97.7 | 97.7 | 97.7 | 97.8 | | | | | | | |
| CAL1 | 1.0 | 97.60 | 8.20 | 6.40 | | | | | | | | | |
| VEL1 | 1.0 | | 0.10 | 0.80 | 1.00 | 1.80 | 1.10 | 1.60 | 1.60 | 1.30 | 0.90 | | |
| VEL1 | 1.0 | 1.00 | 0.60 | 0.10 | | | | | | | | | |
| CAL2 | 1.0 | 97.56 | 6.00 | 5.20 | | | | | | | | | |
| VEL2 | 1.0 | | 0.10 | 0.30 | 0.90 | 1.60 | 0.90 | 0.90 | 1.50 | 1.00 | 0.80 | | |
| VEL2 | 1.0 | 1.00 | 0.40 | 0.10 | | | | | | | | | |
| CAL3 | 1.0 | 97.51 | 4.90 | 4.50 | | | | | | | | | |
| VEL3 | 1.0 | | 0.10 | 0.10 | 0.50 | 1.30 | 0.70 | 0.50 | 1.20 | 1.00 | 0.30 | | |
| VEL3 | 1.0 | 0.90 | 0.30 | 0.10 | | | | | | | | | |
| XSEC | 2.0 | 305.0 | 1.0 | 96.90 | 0.00370 | | | | | | | | |
| | 2.0 | 0.0 | 99.7 | 1.4 | 97.2 | 2.9 | 96.9 | 4.4 | 96.9 | 5.9 | 96.9 | 7.4 | 97.1 |

| | | | | | | | | | | | | | |
|------|-----|------|-------|------|------|-------|------|---------|------|------|------|------|-------|
| | 2.0 | 8.9 | 97.0 | 10.4 | 97.3 | 11.9 | 97.5 | 14.6 | 97.6 | 15.0 | 97.6 | 19.8 | 98.2 |
| | 2.0 | 31.8 | 100.7 | | | | | | | | | | |
| NS | 2.0 | | 1.0 | | 7.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 |
| NS | 2.0 | | 6.0 | | 6.0 | | 6.0 | | 2.0 | | 2.0 | | 3.0 |
| NS | 2.0 | | 3.0 | | | | | | | | | | |
| WSL | 2.0 | | 97.4 | | 97.5 | | 97.5 | | 0.0 | | 97.6 | | 97.7 |
| WSL | 2.0 | | 97.7 | | 97.7 | | 0.0 | | 97.8 | | 97.8 | | 97.9 |
| WSL | 2.0 | | 97.9 | | 97.9 | | 98.0 | | 98.0 | | | | |
| CAL1 | 2.0 | | 97.70 | | 8.20 | | 6.90 | | | | | | |
| VEL1 | 2.0 | | 0.70 | 1.50 | 1.30 | 1.70 | 0.20 | 0.80 | 0.70 | 0.30 | 0.10 | 0.10 | |
| VEL1 | 2.0 | | | | | | | | | | | | |
| CAL2 | 2.0 | | 97.59 | | 6.00 | | 5.30 | | | | | | |
| VEL2 | 2.0 | | 0.10 | 1.50 | 1.20 | 1.70 | 0.20 | 0.60 | 0.40 | 0.20 | 0.10 | | |
| VEL2 | 2.0 | | | | | | | | | | | | |
| CAL3 | 2.0 | | 97.58 | | 4.90 | | 4.40 | | | | | | |
| VEL3 | 2.0 | | 0.10 | 1.30 | 0.90 | 1.70 | 0.10 | 0.50 | 0.30 | 0.10 | 0.10 | | |
| VEL3 | 2.0 | | | | | | | | | | | | |
| XSEC | 3.0 | | 195.0 | 0.4 | | 97.10 | | 0.01111 | | | | | |
| | 3.0 | 0.0 | 98.9 | 1.2 | 97.8 | 1.6 | 97.5 | 3.1 | 97.3 | 4.6 | 97.3 | 6.1 | 97.4 |
| | 3.0 | 7.6 | 97.3 | 9.1 | 97.7 | 10.6 | 97.1 | 12.1 | 97.3 | 13.6 | 97.6 | 15.1 | 97.6 |
| | 3.0 | 15.6 | 97.8 | 16.5 | 98.1 | 17.9 | 99.2 | | | | | | |
| NS | 3.0 | | 1.0 | | 2.0 | 1.0 | 2.0 | 1.0 | 5.0 | | 5.0 | | 6.0 |
| NS | 3.0 | | 6.0 | | 7.0 | | 5.0 | 1.0 | 6.0 | | 7.0 | | 7.0 |
| NS | 3.0 | | 2.0 | | 1.0 | | 1.0 | | | | | | |
| WSL | 3.0 | | 97.6 | | 97.6 | | 97.7 | | 0.0 | | 97.8 | | 97.8 |
| WSL | 3.0 | | 97.8 | | 97.9 | | 0.0 | | 97.9 | | 98.0 | | 98.0 |
| WSL | 3.0 | | 98.0 | | 98.0 | | 98.1 | | 98.1 | | | | |
| CAL1 | 3.0 | | 97.80 | | 8.20 | | 7.10 | | | | | | |
| VEL1 | 3.0 | | 0.10 | 0.40 | 0.90 | 1.70 | 2.20 | 1.70 | 1.70 | 1.60 | 0.80 | 1.30 | 0.20 |
| VEL1 | 3.0 | 0.10 | | | | | | | | | | | |
| CAL2 | 3.0 | | 97.78 | | 6.00 | | 6.00 | | | | | | |
| VEL2 | 3.0 | | 0.10 | 0.10 | 0.60 | 1.50 | 1.90 | 1.70 | 1.60 | 1.60 | 0.20 | 1.20 | 0.10 |
| VEL2 | 3.0 | 0.10 | | | | | | | | | | | |
| CAL3 | 3.0 | | 97.74 | | 4.90 | | 4.90 | | | | | | |
| VEL3 | 3.0 | | 0.10 | 0.10 | 0.20 | 1.20 | 1.60 | 1.50 | 1.10 | 1.40 | 0.10 | 1.00 | 0.10 |
| VEL3 | 3.0 | 0.10 | | | | | | | | | | | |
| XSEC | 4.0 | | 500.0 | 0.0 | | 97.10 | | 0.01111 | | | | | |
| | 4.0 | 0.0 | 98.8 | 2.6 | 98.2 | 3.3 | 97.8 | 3.5 | 97.8 | 4.3 | 97.4 | 5.3 | 97.4 |
| | 4.0 | 6.3 | 97.3 | 7.3 | 97.2 | 8.3 | 97.2 | 9.3 | 97.1 | 10.3 | 97.2 | 11.3 | 97.2 |
| | 4.0 | 12.3 | 97.4 | 13.3 | 97.4 | 14.3 | 97.4 | 15.3 | 97.8 | 15.9 | 98.6 | 17.5 | 100.0 |
| | 4.0 | 18.0 | 100.0 | | | | | | | | | | |
| NS | 4.0 | | 1.0 | | 1.0 | | 1.0 | | 6.0 | | 6.0 | | 6.0 |
| NS | 4.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 |
| NS | 4.0 | | 6.0 | | 6.0 | | 7.0 | | 7.0 | | 1.0 | | 1.0 |
| NS | 4.0 | | 1.0 | | | | | | | | | | |
| WSL | 4.0 | | 97.6 | | 97.7 | | 97.8 | | 0.0 | | 97.8 | | 97.9 |
| WSL | 4.0 | | 97.9 | | 97.9 | | 0.0 | | 98.0 | | 98.0 | | 98.0 |
| WSL | 4.0 | | 98.1 | | 98.1 | | 98.1 | | 98.1 | | | | |
| CAL1 | 4.0 | | 97.85 | | 8.20 | | 8.20 | | | | | | |
| VEL1 | 4.0 | | | | 0.10 | 0.80 | 1.70 | 1.80 | 2.10 | 1.70 | 2.10 | 1.50 | 2.10 |
| VEL1 | 4.0 | 1.20 | 0.40 | 0.70 | 0.10 | | | | | | | | |
| CAL2 | 4.0 | | 97.81 | | 6.00 | | 7.10 | | | | | | |
| VEL2 | 4.0 | | | | 0.10 | 0.80 | 0.30 | 0.90 | 2.10 | 1.60 | 1.50 | 1.40 | 1.50 |
| VEL2 | 4.0 | 1.10 | 0.10 | 0.10 | 0.10 | | | | | | | | |
| CAL3 | 4.0 | | 97.80 | | 4.90 | | 5.40 | | | | | | |
| VEL3 | 4.0 | | | | 0.10 | 0.50 | 0.10 | 0.80 | 1.90 | 1.60 | 1.40 | 1.30 | 1.30 |
| VEL3 | 4.0 | 0.30 | 0.10 | 0.10 | 0.10 | | | | | | | | |
| ENDJ | | | | | | | | | | | | | |

Big Timber Study Site 3 - substrate

Export from PHABSIM for Windows

IOC 0000000100010000100000

QARD 2.0

QARD 3.0

QARD 4.0

QARD 5.0

QARD 6.0

QARD 7.0

QARD 8.0

QARD 9.0

| | | | | | | | | | | | | | |
|------|------|--------|-------|-------|---------|------|---------|------|------|------|------|------|------|
| QARD | 10.0 | | | | | | | | | | | | |
| QARD | 11.0 | | | | | | | | | | | | |
| QARD | 12.0 | | | | | | | | | | | | |
| QARD | 13.0 | | | | | | | | | | | | |
| QARD | 14.0 | | | | | | | | | | | | |
| QARD | 15.0 | | | | | | | | | | | | |
| QARD | 15.8 | | | | | | | | | | | | |
| QARD | 16.0 | | | | | | | | | | | | |
| QARD | 17.0 | | | | | | | | | | | | |
| QARD | 18.0 | | | | | | | | | | | | |
| QARD | 19.0 | | | | | | | | | | | | |
| QARD | 20.0 | | | | | | | | | | | | |
| QARD | 21.0 | | | | | | | | | | | | |
| QARD | 22.0 | | | | | | | | | | | | |
| QARD | 23.0 | | | | | | | | | | | | |
| QARD | 24.0 | | | | | | | | | | | | |
| QARD | 25.0 | | | | | | | | | | | | |
| QARD | 26.0 | | | | | | | | | | | | |
| QARD | 27.0 | | | | | | | | | | | | |
| QARD | 28.0 | | | | | | | | | | | | |
| QARD | 29.0 | | | | | | | | | | | | |
| QARD | 30.0 | | | | | | | | | | | | |
| XSEC | 1.0 | 0.0 | 1.0 | 93.90 | 0.01080 | | | | | | | | |
| | 1.0 | 0.0 | 96.8 | 2.7 | 96.4 | 5.5 | 94.9 | 5.9 | 94.7 | 6.2 | 94.3 | 7.2 | 94.5 |
| | 1.0 | 8.2 | 94.5 | 9.2 | 94.4 | 10.2 | 94.2 | 11.2 | 94.1 | 12.2 | 94.0 | 13.2 | 94.1 |
| | 1.0 | 14.2 | 93.9 | 15.2 | 93.9 | 16.2 | 93.9 | 17.2 | 93.9 | 18.2 | 94.1 | 19.2 | 94.2 |
| | 1.0 | 20.2 | 94.4 | 20.9 | 94.7 | 21.7 | 94.9 | 23.7 | 96.5 | 27.0 | 96.7 | | |
| NS | 1.0 | | 1.0 | | 1.0 | | 1.0 | | 2.0 | | 3.0 | | 4.0 |
| NS | 1.0 | 1.0 | 5.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 |
| NS | 1.0 | | 5.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 5.0 |
| NS | 1.0 | | 4.0 | | 2.0 | | 1.0 | | 1.0 | | 2.0 | | |
| WSL | 1.0 | | 94.6 | | 94.6 | | 94.7 | | 94.7 | | 94.7 | | 94.7 |
| WSL | 1.0 | | 94.7 | | 94.7 | | 94.7 | | 94.7 | | 94.7 | | 94.7 |
| WSL | 1.0 | | 94.7 | | 94.7 | | 94.7 | | 94.7 | | 94.7 | | 94.8 |
| WSL | 1.0 | | 94.8 | | 94.8 | | 94.8 | | 94.8 | | 94.8 | | 94.8 |
| WSL | 1.0 | | 94.8 | | 94.8 | | 94.8 | | 94.8 | | 94.8 | | 94.8 |
| CAL1 | 1.0 | | 94.74 | | 15.77 | | 16.00 | | | | | | |
| VEL1 | 1.0 | | | | 0.00 | 0.60 | 0.70 | 1.30 | 1.50 | 1.50 | 1.10 | 2.30 | 2.60 |
| VEL1 | 1.0 | 2.70 | 2.80 | 2.30 | 2.40 | 1.00 | 1.60 | 0.80 | 0.00 | | | | |
| CAL2 | 1.0 | | 94.72 | | 8.98 | | 11.30 | | | | | | |
| VEL2 | 1.0 | | | | 0.00 | 0.10 | 0.00 | 0.50 | 1.00 | 0.90 | 0.80 | 2.00 | 1.90 |
| VEL2 | 1.0 | 2.10 | 2.10 | 1.70 | 1.00 | 1.10 | 1.40 | 0.70 | 0.00 | | | | |
| CAL3 | 1.0 | | 94.70 | | 8.00 | | 10.70 | | | | | | |
| VEL3 | 1.0 | | | | 0.00 | 0.10 | 0.10 | 0.00 | 1.30 | 1.00 | 0.70 | 1.80 | 2.00 |
| VEL3 | 1.0 | 2.30 | 1.80 | 1.70 | 1.50 | 0.80 | 1.40 | 0.70 | 0.00 | | | | |
| XSEC | 2.0 | | 75.0 | 1.0 | 94.60 | | 0.02190 | | | | | | |
| | 2.0 | 0.0100 | 0.5 | 6.2 | 98.4 | 14.7 | 95.6 | 15.1 | 95.6 | 15.7 | 95.3 | 16.7 | 95.0 |
| | 2.0 | 17.7 | 94.9 | 18.7 | 94.6 | 19.7 | 94.7 | 20.7 | 94.6 | 21.7 | 95.0 | 22.7 | 95.0 |
| | 2.0 | 23.7 | 95.0 | 24.7 | 95.1 | 25.7 | 94.9 | 26.7 | 95.2 | 27.7 | 95.3 | 28.2 | 95.4 |
| | 2.0 | 29.6 | 95.6 | 30.2 | 95.7 | 33.2 | 96.8 | 48.8 | 98.3 | | | | |
| NS | 2.0 | | 1.0 | | 1.0 | | 6.0 | | 3.0 | | 3.0 | | 6.0 |
| NS | 2.0 | | 5.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 5.0 |
| NS | 2.0 | | 5.0 | | 5.0 | | 5.0 | | 5.0 | | 5.0 | | 5.0 |
| NS | 2.0 | | 3.0 | | 3.0 | | 3.0 | | 1.0 | | | | |
| WSL | 2.0 | | 95.1 | | 95.2 | | 95.3 | | 95.3 | | 95.3 | | 95.4 |
| WSL | 2.0 | | 95.4 | | 95.4 | | 95.4 | | 95.5 | | 95.5 | | 95.5 |
| WSL | 2.0 | | 95.5 | | 95.5 | | 95.6 | | 95.6 | | 95.6 | | 95.6 |
| WSL | 2.0 | | 95.6 | | 95.6 | | 95.6 | | 95.6 | | 95.7 | | 95.7 |
| WSL | 2.0 | | 95.7 | | 95.7 | | 95.7 | | 95.7 | | 95.7 | | 95.7 |
| CAL1 | 2.0 | | 95.55 | | 15.77 | | 14.50 | | | | | | |
| VEL1 | 2.0 | | | | 0.00 | 0.60 | 2.40 | 2.20 | 2.10 | 1.80 | 1.70 | 1.90 | 2.00 |
| VEL1 | 2.0 | 2.10 | 2.10 | 2.10 | 2.20 | 1.10 | 0.90 | 0.00 | | | | | |
| CAL2 | 2.0 | | 95.40 | | 8.98 | | 7.90 | | | | | | |
| VEL2 | 2.0 | | | | 0.00 | 0.30 | 1.40 | 1.80 | 1.90 | 1.50 | 1.20 | 1.30 | 1.60 |
| VEL2 | 2.0 | 1.30 | 1.30 | 1.50 | 1.60 | 0.40 | 0.00 | 0.00 | | | | | |
| CAL3 | 2.0 | | 95.41 | | 8.00 | | 7.20 | | | | | | |
| VEL3 | 2.0 | | | | 0.00 | 0.10 | 1.30 | 1.00 | 1.50 | 1.30 | 1.60 | 1.90 | 1.30 |
| VEL3 | 2.0 | 1.60 | 1.50 | 1.00 | 1.10 | 0.60 | 0.00 | 0.00 | | | | | |
| XSEC | 3.0 | | 75.0 | 1.0 | 96.10 | | 0.01580 | | | | | | |
| | 3.0 | 0.0101 | 1.0 | 5.5 | 98.5 | 8.8 | 97.7 | 10.3 | 97.2 | 10.5 | 96.2 | 11.5 | 96.3 |
| | 3.0 | 12.5 | 96.2 | 13.5 | 96.2 | 14.5 | 96.1 | 15.5 | 96.1 | 16.5 | 96.3 | 17.5 | 96.5 |

| | | | | | | | | | | | | | |
|------|-----|--------|-------|------|-------|-------|-------|---------|-------|------|------|------|------|
| | 3.0 | 18.5 | 96.4 | 19.5 | 96.7 | 20.5 | 96.8 | 21.5 | 97.0 | 22.7 | 97.2 | 23.0 | 97.3 |
| | 3.0 | 27.0 | 98.5 | 33.3 | 99.8 | | | | | | | | |
| NS | 3.0 | | 1.0 | | | | 3.0 | | 2.0 | | 3.0 | | 3.0 |
| NS | 3.0 | | 5.0 | | 5.0 | | 6.0 | | 6.0 | | 6.0 | | 4.0 |
| NS | 3.0 | | 4.0 | | 4.0 | | 4.0 | | 4.0 | | 2.0 | | 3.0 |
| NS | 3.0 | | 2.0 | | 1.0 | | | | | | | | |
| WSL | 3.0 | | 97.0 | | 97.0 | | 97.1 | | 97.1 | | 97.1 | | 97.1 |
| WSL | 3.0 | | 97.1 | | 97.1 | | 97.2 | | 97.2 | | 97.2 | | 97.2 |
| WSL | 3.0 | | 97.2 | | 97.2 | | 97.2 | | 97.2 | | 97.2 | | 97.2 |
| WSL | 3.0 | | 97.2 | | 97.2 | | 97.2 | | 97.2 | | 97.2 | | 97.2 |
| WSL | 3.0 | | 97.2 | | 97.2 | | 97.2 | | 97.2 | | 97.2 | | 97.2 |
| WSL | 3.0 | | 97.2 | | 97.3 | | 97.3 | | 97.3 | | 97.3 | | 97.3 |
| CAL1 | 3.0 | | 97.19 | | 15.77 | | 12.80 | | | | | | |
| VEL1 | 3.0 | | | | 0.00 | 0.30 | 0.90 | 1.20 | 1.60 | 1.70 | 1.80 | 1.50 | 1.60 |
| VEL1 | 3.0 | 1.80 | 1.80 | 1.50 | 0.80 | 0.00 | | | | | | | |
| CAL2 | 3.0 | | 97.16 | | | | 8.98 | | 8.90 | | | | |
| VEL2 | 3.0 | | | | 0.00 | 0.30 | 0.60 | 0.80 | 1.20 | 1.30 | 1.40 | 1.20 | 1.30 |
| VEL2 | 3.0 | 1.00 | 1.10 | 0.80 | 0.20 | 0.00 | | | | | | | |
| CAL3 | 3.0 | | 97.13 | | | | 8.00 | | 8.50 | | | | |
| VEL3 | 3.0 | | | | 0.00 | 0.10 | 0.50 | 0.80 | 1.20 | 1.30 | 1.30 | 1.20 | 1.30 |
| VEL3 | 3.0 | 1.30 | 0.90 | 1.10 | 0.30 | 0.00 | | | | | | | |
| XSEC | 4.0 | | 40.0 | 0.5 | | 96.80 | | 0.01380 | | | | | |
| | 4.0 | 0.0100 | 1.1 | 6.1 | 98.4 | 11.2 | 97.8 | 12.9 | 97.7 | 13.9 | 97.7 | 14.9 | 97.6 |
| | 4.0 | 15.9 | 97.2 | 16.9 | 97.0 | 17.9 | 96.9 | 18.9 | 96.9 | 19.9 | 96.8 | 20.9 | 96.9 |
| | 4.0 | 21.9 | 96.8 | 22.9 | 96.8 | 23.9 | 96.8 | 24.9 | 96.9 | 25.9 | 96.9 | 26.6 | 97.3 |
| | 4.0 | 28.4 | 97.9 | 28.8 | 97.9 | 31.9 | 99.7 | 39.5 | 101.3 | | | | |
| NS | 4.0 | | 1.0 | | 2.0 | | 3.0 | 1.0 | 5.0 | 1.0 | 5.0 | | 5.0 |
| NS | 4.0 | | 5.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 |
| NS | 4.0 | | 6.0 | | 4.0 | | 4.0 | | 4.0 | | 3.0 | 1.0 | 3.0 |
| NS | 4.0 | | 7.0 | | 7.0 | | 3.0 | | 3.0 | | | | |
| WSL | 4.0 | | 97.5 | | 97.6 | | 97.6 | | 97.6 | | 97.7 | | 97.7 |
| WSL | 4.0 | | 97.7 | | 97.7 | | 97.8 | | 97.8 | | 97.8 | | 97.8 |
| WSL | 4.0 | | 97.8 | | 97.8 | | 97.8 | | 97.8 | | 97.8 | | 97.8 |
| WSL | 4.0 | | 97.9 | | 97.9 | | 97.9 | | 97.9 | | 97.9 | | 97.9 |
| WSL | 4.0 | | 97.9 | | 97.9 | | 97.9 | | 97.9 | | 97.9 | | 97.9 |
| CAL1 | 4.0 | | 97.82 | | 15.77 | | 15.10 | | | | | | |
| VEL1 | 4.0 | | | | 0.00 | 0.30 | 1.00 | 2.60 | 2.40 | 2.30 | 2.30 | 2.00 | 1.60 |
| VEL1 | 4.0 | 1.20 | 0.90 | 0.70 | 0.50 | 0.40 | 0.00 | 0.00 | | | | | |
| CAL2 | 4.0 | | 97.75 | | | | 8.98 | | 9.90 | | | | |
| VEL2 | 4.0 | | | | | 0.00 | 0.10 | 0.80 | 2.40 | 2.20 | 1.90 | 1.00 | 0.80 |
| VEL2 | 4.0 | 1.00 | 0.90 | 0.60 | 0.40 | 0.30 | 0.00 | | | | | | |
| CAL3 | 4.0 | | 97.71 | | | | 8.00 | | 9.50 | | | | |
| VEL3 | 4.0 | | | | 0.00 | 0.00 | 1.00 | 2.50 | 2.00 | 1.60 | 1.60 | 1.50 | 1.30 |
| VEL3 | 4.0 | 0.90 | 0.30 | 0.50 | 0.30 | 0.10 | 0.00 | | | | | | |
| XSEC | 5.0 | | 8.0 | 0.0 | | 96.80 | | 0.01380 | | | | | |
| | 5.0 | 0.0 | 98.8 | 0.9 | 98.4 | 4.3 | 98.0 | 4.6 | 97.9 | 4.9 | 97.7 | 5.9 | 97.3 |
| | 5.0 | 6.9 | 96.6 | 7.9 | 96.3 | 8.9 | 96.3 | 9.9 | 96.1 | 10.9 | 95.9 | 11.9 | 95.5 |
| | 5.0 | 12.9 | 96.1 | 13.9 | 96.0 | 14.9 | 96.6 | 15.9 | 96.8 | 16.9 | 96.1 | 17.9 | 95.7 |
| | 5.0 | 18.9 | 96.4 | 19.9 | 96.7 | 20.9 | 97.6 | 21.1 | 97.9 | 22.3 | 98.0 | 23.6 | 99.6 |
| | 5.0 | 25.1 | 99.6 | | | | | | | | | | |
| NS | 5.0 | | 3.0 | | 3.0 | | 3.0 | | 4.0 | 0.5 | 3.0 | | 3.0 |
| NS | 5.0 | | 3.0 | | 5.0 | | 6.0 | | 6.0 | | 6.0 | | 7.0 |
| NS | 5.0 | | 7.0 | | 7.0 | | 7.0 | | 7.0 | 2.0 | 6.0 | | 6.0 |
| NS | 5.0 | | 7.0 | | 6.0 | | 1.0 | | 1.0 | | 1.0 | | 1.0 |
| NS | 5.0 | | 3.0 | | | | | | | | | | |
| WSL | 5.0 | | 97.6 | | 97.7 | | 97.7 | | 97.7 | | 97.8 | | 97.8 |
| WSL | 5.0 | | 97.8 | | 97.8 | | 97.8 | | 97.9 | | 97.9 | | 97.9 |
| WSL | 5.0 | | 97.9 | | 97.9 | | 97.9 | | 97.9 | | 97.9 | | 98.0 |
| WSL | 5.0 | | 98.0 | | 98.0 | | 98.0 | | 98.0 | | 98.0 | | 98.0 |
| WSL | 5.0 | | 98.0 | | 98.0 | | 98.0 | | 98.0 | | 98.0 | | 98.1 |
| CAL1 | 5.0 | | 97.93 | | 15.77 | | 20.00 | | | | | | |
| VEL1 | 5.0 | | | | 0.00 | 0.20 | 0.30 | 0.20 | 0.60 | 1.30 | 2.00 | 2.70 | 2.00 |
| VEL1 | 5.0 | 1.50 | 0.50 | 0.40 | 0.20 | 0.10 | 0.20 | 0.30 | 0.30 | 0.20 | 0.00 | | |
| VEL1 | 5.0 | | | | | | | | | | | | |
| CAL2 | 5.0 | | 97.83 | | | | 8.98 | | 9.60 | | | | |
| VEL2 | 5.0 | | | | 0.00 | 0.10 | 0.20 | 0.10 | 0.20 | 0.80 | 1.60 | 1.30 | 1.00 |
| VEL2 | 5.0 | 1.00 | 0.20 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.00 | 0.00 | | |
| VEL2 | 5.0 | | | | | | | | | | | | |
| CAL3 | 5.0 | | 97.81 | | | | 8.00 | | 13.90 | | | | |
| VEL3 | 5.0 | | | | 0.00 | 0.20 | 0.60 | 0.50 | 0.30 | 0.20 | 1.90 | 1.60 | 1.60 |
| VEL3 | 5.0 | 0.70 | 0.10 | 0.10 | 0.10 | 0.20 | 0.20 | 0.20 | 0.10 | 0.00 | 0.00 | 0.00 | |
| VEL3 | 5.0 | | | | | | | | | | | | |

ENDJ

Big Timber Study Site 4 - substrate

Export from PHABSIM for Windows

| | | | | | | | | | | | | | |
|------|------------------------|-------|------|-------|---------|-------|------|---------|------|------|------|------|------|
| IOC | 0000000100010000100000 | | | | | | | | | | | | |
| QARD | 2.0 | | | | | | | | | | | | |
| QARD | 3.0 | | | | | | | | | | | | |
| QARD | 4.0 | | | | | | | | | | | | |
| QARD | 5.0 | | | | | | | | | | | | |
| QARD | 6.0 | | | | | | | | | | | | |
| QARD | 7.0 | | | | | | | | | | | | |
| QARD | 8.0 | | | | | | | | | | | | |
| QARD | 9.0 | | | | | | | | | | | | |
| QARD | 10.0 | | | | | | | | | | | | |
| QARD | 11.0 | | | | | | | | | | | | |
| QARD | 12.0 | | | | | | | | | | | | |
| QARD | 13.0 | | | | | | | | | | | | |
| QARD | 14.0 | | | | | | | | | | | | |
| QARD | 15.0 | | | | | | | | | | | | |
| QARD | 16.0 | | | | | | | | | | | | |
| QARD | 17.0 | | | | | | | | | | | | |
| QARD | 18.0 | | | | | | | | | | | | |
| QARD | 19.0 | | | | | | | | | | | | |
| QARD | 20.0 | | | | | | | | | | | | |
| QARD | 21.0 | | | | | | | | | | | | |
| QARD | 22.0 | | | | | | | | | | | | |
| QARD | 23.0 | | | | | | | | | | | | |
| QARD | 24.0 | | | | | | | | | | | | |
| QARD | 25.0 | | | | | | | | | | | | |
| QARD | 26.0 | | | | | | | | | | | | |
| QARD | 27.0 | | | | | | | | | | | | |
| QARD | 28.0 | | | | | | | | | | | | |
| QARD | 29.0 | | | | | | | | | | | | |
| QARD | 30.0 | | | | | | | | | | | | |
| XSEC | 1.0 | 0.0 | 0.0 | 85.40 | 0.00294 | | | | | | | | |
| | 1.0 | 0.0 | 87.8 | 2.3 | 87.2 | 3.6 | 85.9 | 3.8 | 85.9 | 4.3 | 85.6 | 5.8 | 85.5 |
| | 1.0 | 7.3 | 85.5 | 8.8 | 85.4 | 10.3 | 85.5 | 11.8 | 85.5 | 13.3 | 85.6 | 14.8 | 85.6 |
| | 1.0 | 16.3 | 85.4 | 17.8 | 85.4 | 19.3 | 85.4 | 20.8 | 85.4 | 22.3 | 85.5 | 23.8 | 85.4 |
| | 1.0 | 25.3 | 85.4 | 26.3 | 85.7 | 27.4 | 85.9 | 28.2 | 85.9 | 41.1 | 89.0 | 41.5 | 89.0 |
| NS | 1.0 | 1.0 | 1.0 | | 1.0 | | 1.0 | | 3.0 | | 5.0 | | |
| NS | 1.0 | 5.0 | 4.0 | | 5.0 | | 5.0 | | 5.0 | | 6.0 | | |
| NS | 1.0 | 5.0 | 5.0 | | 6.0 | | 5.0 | | 6.0 | | 5.0 | | |
| NS | 1.0 | 5.0 | 2.0 | | 1.0 | | 2.0 | | 6.0 | | 6.0 | | |
| WSL | 1.0 | 85.6 | | 85.6 | | 85.6 | | 85.7 | | 85.7 | | 85.7 | |
| WSL | 1.0 | 85.8 | | 85.8 | | 85.8 | | 85.8 | | 85.9 | | 85.9 | |
| WSL | 1.0 | 85.9 | | 85.9 | | 86.0 | | 86.0 | | 86.0 | | 86.0 | |
| WSL | 1.0 | 86.0 | | 86.1 | | 86.1 | | 86.1 | | 86.1 | | 86.1 | |
| WSL | 1.0 | 86.1 | | 86.2 | | 86.2 | | 86.2 | | 86.2 | | | |
| CAL1 | 1.0 | 85.85 | | 11.00 | | 9.60 | | | | | | | |
| VEL1 | 1.0 | 0.10 | | 0.90 | 0.80 | | 1.00 | 0.90 | 1.30 | 1.30 | 1.10 | 1.50 | |
| VEL1 | 1.0 | 1.50 | 1.60 | 1.40 | 1.40 | 1.40 | 1.10 | 1.10 | 0.90 | 0.10 | | | |
| CAL2 | 1.0 | 85.79 | | 9.00 | | 7.30 | | | | | | | |
| VEL2 | 1.0 | 0.10 | | 0.80 | 0.60 | | 0.90 | 0.80 | 1.20 | 1.10 | 1.00 | 1.30 | |
| VEL2 | 1.0 | 1.40 | 1.40 | 1.20 | 1.30 | 1.10 | 0.50 | 1.00 | 0.60 | 0.10 | | | |
| CAL3 | 1.0 | 85.78 | | 8.00 | | 6.60 | | | | | | | |
| VEL3 | 1.0 | 0.10 | | 0.50 | 0.50 | | 0.80 | 0.80 | 1.10 | 0.90 | 1.00 | 0.60 | |
| VEL3 | 1.0 | 1.30 | 1.40 | 0.90 | 1.20 | 1.00 | 0.40 | 0.80 | 0.40 | 0.10 | | | |
| XSEC | 2.0 | 1.0 | | 1.0 | | 85.40 | | 0.00032 | | | | | |
| | 2.0 | 0.0 | 86.7 | 0.5 | 86.7 | 4.2 | 86.0 | 4.5 | 85.9 | 4.8 | 85.7 | 6.3 | 85.5 |
| | 2.0 | 7.8 | 85.5 | 9.3 | 85.4 | 10.8 | 85.3 | 12.3 | 85.4 | 13.8 | 85.2 | 15.3 | 85.1 |
| | 2.0 | 16.8 | 85.1 | 18.3 | 85.2 | 19.8 | 85.1 | 21.3 | 85.6 | 22.3 | 85.9 | 22.7 | 86.0 |
| | 2.0 | 41.0 | 86.5 | 55.4 | 89.5 | 56.2 | 89.8 | | | | | | |
| NS | 2.0 | 2.0 | | 2.0 | | 2.0 | | 2.0 | | 2.0 | | 5.0 | |
| NS | 2.0 | 5.0 | | 5.0 | | 4.0 | | 5.0 | | 5.0 | | 4.0 | |
| NS | 2.0 | 4.0 | | 5.0 | | 6.0 | | 2.0 | | 2.0 | | 3.0 | |
| NS | 2.0 | 3.0 | | 2.0 | | 2.0 | | | | | | | |
| WSL | 2.0 | 85.6 | | 85.7 | | 85.7 | | 85.7 | | 85.8 | | 85.8 | |
| WSL | 2.0 | 85.8 | | 85.8 | | 85.9 | | 85.9 | | 85.9 | | 85.9 | |
| WSL | 2.0 | 86.0 | | 86.0 | | 86.0 | | 86.0 | | 86.0 | | 86.1 | |
| WSL | 2.0 | 86.1 | | 86.1 | | 86.1 | | 86.1 | | 86.1 | | 86.2 | |

| | | | | | | | | | | | | | |
|------|-----|-------|-------|-------|---------|------|------|------|------|------|------|------|------|
| WSL | 2.0 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | | | | | | | |
| CAL1 | 2.0 | 85.90 | 11.00 | 10.10 | | | | | | | | | |
| VEL1 | 2.0 | | 0.10 | 0.60 | 0.70 | 0.70 | 1.00 | 1.00 | 1.30 | 1.20 | 1.30 | | |
| VEL1 | 2.0 | 1.20 | 1.20 | 1.90 | 0.60 | 0.10 | | | | | | | |
| CAL2 | 2.0 | 85.84 | 9.00 | 9.50 | | | | | | | | | |
| VEL2 | 2.0 | | 0.10 | 0.10 | 0.70 | 0.70 | 0.90 | 0.90 | 1.10 | 1.10 | 1.20 | | |
| VEL2 | 2.0 | 1.20 | 1.00 | 0.90 | 0.40 | 0.10 | | | | | | | |
| CAL3 | 2.0 | 85.82 | 8.00 | 7.50 | | | | | | | | | |
| VEL3 | 2.0 | | 0.10 | 0.10 | 0.60 | 0.50 | 0.80 | 0.80 | 1.10 | 1.00 | 1.10 | | |
| VEL3 | 2.0 | 1.10 | 1.00 | 0.80 | 0.40 | 0.10 | | | | | | | |
| XSEC | 3.0 | 154.0 | 1.0 | 85.40 | 0.00147 | | | | | | | | |
| | 3.0 | 0.0 | 86.8 | 8.0 | 86.7 | 10.3 | 86.0 | 10.4 | 85.9 | 12.0 | 85.7 | 13.5 | 85.4 |
| | 3.0 | 15.0 | 85.4 | 16.5 | 85.2 | 18.0 | 84.9 | 19.5 | 84.7 | 21.0 | 84.6 | 22.5 | 84.5 |
| | 3.0 | 23.0 | 84.7 | 25.0 | 85.1 | 26.3 | 85.2 | 26.7 | 85.9 | 27.1 | 86.7 | 38.1 | 87.0 |
| | 3.0 | 50.1 | 86.7 | 63.0 | 86.9 | 74.0 | 86.4 | 77.6 | 88.3 | 78.9 | 88.2 | | |
| NS | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 5.0 |
| NS | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 5.0 |
| NS | 3.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 |
| NS | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| WSL | 3.0 | 85.6 | 85.7 | 85.7 | 85.7 | 85.8 | 85.8 | 85.8 | 85.8 | 85.8 | 85.8 | 85.8 | 85.8 |
| WSL | 3.0 | 85.9 | 85.9 | 85.9 | 85.9 | 85.9 | 85.9 | 85.9 | 85.9 | 85.9 | 85.9 | 85.9 | 86.0 |
| WSL | 3.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 |
| WSL | 3.0 | 86.1 | 86.1 | 86.1 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 |
| WSL | 3.0 | 86.2 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 |
| CAL1 | 3.0 | 85.91 | 11.00 | 8.80 | | | | | | | | | |
| VEL1 | 3.0 | | 0.10 | 0.40 | 0.80 | 1.00 | 1.20 | 1.00 | 1.00 | 1.60 | 0.90 | | |
| VEL1 | 3.0 | 0.70 | 0.20 | 0.30 | 0.10 | | | | | | | | |
| CAL2 | 3.0 | 85.84 | 9.00 | 7.90 | | | | | | | | | |
| VEL2 | 3.0 | | 0.10 | 0.10 | 0.70 | 1.00 | 1.10 | 0.90 | 1.00 | 1.00 | 0.40 | | |
| VEL2 | 3.0 | 0.30 | 0.20 | 0.20 | 0.10 | | | | | | | | |
| CAL3 | 3.0 | 85.84 | 8.00 | 9.90 | | | | | | | | | |
| VEL3 | 3.0 | | 0.10 | 0.10 | 0.60 | 0.70 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.30 | |
| VEL3 | 3.0 | 0.10 | 0.10 | 0.10 | 0.10 | | | | | | | | |
| XSEC | 4.0 | 153.0 | 1.0 | 85.40 | 0.00260 | | | | | | | | |
| | 4.0 | 0.0 | 88.0 | 7.1 | 87.8 | 14.8 | 86.8 | 16.9 | 86.0 | 17.4 | 86.0 | 17.6 | 85.5 |
| | 4.0 | 18.6 | 85.4 | 19.6 | 85.2 | 20.6 | 85.0 | 21.6 | 84.8 | 22.6 | 84.7 | 23.6 | 84.5 |
| | 4.0 | 24.6 | 85.0 | 25.6 | 85.0 | 26.6 | 85.5 | 27.7 | 86.0 | 27.8 | 86.0 | 32.7 | 87.5 |
| | 4.0 | 43.2 | 87.3 | 49.4 | 87.1 | 61.1 | 87.5 | 72.3 | 86.8 | 77.1 | 88.8 | 78.2 | 88.9 |
| NS | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| NS | 4.0 | 4.0 | 4.0 | 5.0 | 5.0 | 5.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| NS | 4.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| NS | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 2.0 | 2.0 | 1.0 | 1.0 |
| WSL | 4.0 | 85.6 | 85.7 | 85.7 | 85.7 | 85.8 | 85.8 | 85.8 | 85.8 | 85.8 | 85.8 | 85.8 | 85.8 |
| WSL | 4.0 | 85.9 | 85.9 | 85.9 | 85.9 | 85.9 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 |
| WSL | 4.0 | 86.0 | 86.0 | 86.0 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 |
| WSL | 4.0 | 86.1 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 |
| WSL | 4.0 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 |
| CAL1 | 4.0 | 85.96 | 11.00 | 7.90 | | | | | | | | | |
| VEL1 | 4.0 | | 0.10 | 0.30 | 0.60 | 0.70 | 0.90 | 1.10 | 1.20 | 1.20 | 1.20 | 1.20 | 1.20 |
| VEL1 | 4.0 | 1.40 | 0.70 | 0.40 | 0.10 | | | | | | | | |
| CAL2 | 4.0 | 85.90 | 9.00 | 6.20 | | | | | | | | | |
| VEL2 | 4.0 | | 0.10 | 0.20 | 0.40 | 0.50 | 0.70 | 1.00 | 1.10 | 1.00 | 1.00 | 1.00 | 1.00 |
| VEL2 | 4.0 | 1.00 | 0.50 | 0.30 | 0.10 | | | | | | | | |
| CAL3 | 4.0 | 85.88 | 8.00 | 5.60 | | | | | | | | | |
| VEL3 | 4.0 | | 0.10 | 0.20 | 0.40 | 0.40 | 0.60 | 0.80 | 1.00 | 0.60 | 0.60 | 0.60 | 0.60 |
| VEL3 | 4.0 | 0.70 | 0.40 | 0.10 | 0.10 | | | | | | | | |
| XSEC | 5.0 | 153.0 | 1.0 | 85.40 | 0.02615 | | | | | | | | |
| | 5.0 | 0.0 | 88.1 | 5.8 | 88.5 | 10.0 | 86.6 | 10.4 | 86.1 | 10.5 | 85.9 | 11.3 | 85.5 |
| | 5.0 | 12.3 | 85.4 | 13.3 | 85.3 | 14.3 | 85.6 | 15.3 | 85.7 | 16.3 | 85.7 | 17.3 | 85.7 |
| | 5.0 | 18.3 | 85.8 | 19.3 | 85.9 | 20.3 | 85.9 | 21.6 | 86.1 | 23.1 | 86.4 | 29.2 | 87.9 |
| | 5.0 | 46.1 | 87.6 | 51.2 | 87.8 | 56.7 | 90.2 | 57.1 | 90.2 | | | | |
| NS | 5.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| NS | 5.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| NS | 5.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| NS | 5.0 | 5.0 | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| WSL | 5.0 | 85.8 | 85.8 | 85.9 | 85.9 | 85.9 | 85.9 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 |
| WSL | 5.0 | 86.0 | 86.0 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 | 86.1 |
| WSL | 5.0 | 86.1 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.2 | 86.3 |
| WSL | 5.0 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 | 86.4 | 86.4 | 86.4 | 86.4 |
| WSL | 5.0 | 86.4 | 86.4 | 86.4 | 86.4 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 |
| CAL1 | 5.0 | 86.09 | 11.00 | 10.50 | | | | | | | | | |

| | | | | | | | | | | | | | | |
|------|-----|------|-------|------|-------|-------|-------|---------|------|------|------|------|------|------|
| VEL1 | 5.0 | | | 0.10 | 0.10 | 3.70 | 3.70 | 4.30 | 1.80 | 1.60 | 3.20 | 3.90 | | |
| VEL1 | 5.0 | 3.40 | 2.50 | 0.10 | 0.10 | | | | | | | | | |
| CAL2 | 5.0 | | 86.06 | | | 9.00 | | 8.80 | | | | | | |
| VEL2 | 5.0 | | | 0.10 | 0.10 | 0.80 | 3.60 | 4.30 | 1.50 | 1.60 | 2.10 | 3.40 | | |
| VEL2 | 5.0 | 3.10 | 1.70 | 0.10 | 0.10 | | | | | | | | | |
| CAL3 | 5.0 | | 86.00 | | | 8.00 | | 8.80 | | | | | | |
| VEL3 | 5.0 | | | 0.10 | 0.10 | 0.40 | 3.60 | 3.50 | 1.40 | 1.60 | 0.10 | 1.20 | | |
| VEL3 | 5.0 | 3.10 | 1.50 | 0.10 | 0.10 | | | | | | | | | |
| XSEC | 6.0 | | 70.0 | 1.0 | | 85.90 | | 0.01583 | | | | | | |
| | 6.0 | 0.0 | 88.6 | 15.1 | 88.7 | 24.8 | 88.6 | 28.4 | 87.0 | 28.8 | 86.1 | 29.8 | 85.9 | |
| | 6.0 | 31.3 | 86.2 | 32.8 | 86.2 | 34.3 | 86.2 | 35.8 | 86.4 | 37.3 | 86.4 | 38.8 | 86.4 | |
| | 6.0 | 40.3 | 86.5 | 41.8 | 86.5 | 43.3 | 86.4 | 44.8 | 86.5 | 45.3 | 86.8 | 46.0 | 87.3 | |
| | 6.0 | 52.9 | 88.5 | 61.8 | 87.8 | 67.9 | 89.6 | 68.6 | 89.6 | | | | | |
| NS | 6.0 | | 1.0 | | 6.0 | | 6.0 | | 6.0 | | 1.0 | | 6.0 | |
| NS | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | |
| NS | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 7.0 | | 6.0 | | 5.0 | |
| NS | 6.0 | | 5.0 | | 5.0 | | 2.0 | | 1.0 | | | | | |
| WSL | 6.0 | | 86.4 | | 86.5 | | 86.5 | | 86.6 | | 86.6 | | 86.7 | |
| WSL | 6.0 | | 86.7 | | 86.7 | | 86.7 | | 86.8 | | 86.8 | | 86.8 | |
| WSL | 6.0 | | 86.8 | | 86.8 | | 86.9 | | 86.9 | | 86.9 | | 86.9 | |
| WSL | 6.0 | | 86.9 | | 86.9 | | 87.0 | | 87.0 | | 87.0 | | 87.0 | |
| WSL | 6.0 | | 87.0 | | 87.0 | | 87.0 | | 87.0 | | 87.1 | | | |
| CAL1 | 6.0 | | 86.76 | | 11.00 | | 11.80 | | | | | | | |
| VEL1 | 6.0 | | | | | 0.60 | 2.20 | 2.40 | 2.50 | 2.80 | 3.00 | 1.40 | 0.90 | |
| VEL1 | 6.0 | 0.20 | 1.10 | 0.90 | 1.10 | 0.10 | | | | | | | | |
| CAL2 | 6.0 | | 86.70 | | 9.00 | | 9.70 | | | | | | | |
| VEL2 | 6.0 | | | | | 0.20 | 1.40 | 2.30 | 2.30 | 2.70 | 1.70 | 1.10 | 0.90 | |
| VEL2 | 6.0 | 0.20 | 0.40 | 0.50 | 1.10 | 0.10 | | | | | | | | |
| CAL3 | 6.0 | | 86.69 | | 8.00 | | 7.80 | | | | | | | |
| VEL3 | 6.0 | | | | | 0.10 | 1.30 | 2.00 | 1.80 | 1.70 | 1.70 | 0.50 | 0.60 | |
| VEL3 | 6.0 | 0.20 | 0.20 | 0.50 | 0.50 | 0.10 | | | | | | | | |
| XSEC | 7.0 | | 370.0 | 1.0 | | 86.20 | | 0.00143 | | | | | | |
| | 7.0 | 0.0 | 89.1 | 11.3 | 88.0 | 14.2 | 86.9 | 14.4 | 87.0 | 14.6 | 86.8 | 15.6 | 86.5 | |
| | 7.0 | 17.1 | 86.4 | 18.6 | 86.2 | 20.1 | 86.3 | 21.6 | 86.3 | 23.1 | 86.2 | 24.6 | 86.6 | |
| | 7.0 | 26.1 | 86.5 | 27.1 | 86.8 | 28.1 | 87.0 | 29.1 | 87.0 | 34.1 | 88.3 | 44.1 | 88.0 | |
| | 7.0 | 53.0 | 88.9 | 56.1 | 90.3 | 57.2 | 90.3 | | | | | | | |
| NS | 7.0 | | 5.0 | | 5.0 | | 6.0 | | 2.0 | | 2.0 | | 3.0 | |
| NS | 7.0 | | 5.0 | | 4.0 | | 5.0 | | 5.0 | | 6.0 | | 6.0 | |
| NS | 7.0 | | 6.0 | | 6.0 | | 6.0 | | 5.0 | | 4.0 | | 3.0 | |
| NS | 7.0 | | 6.0 | | 1.0 | | 1.0 | | | | | | | |
| WSL | 7.0 | | 86.6 | | 86.7 | | 86.7 | | 86.8 | | 86.8 | | 86.8 | |
| WSL | 7.0 | | 86.9 | | 86.9 | | 86.9 | | 87.0 | | 87.0 | | 87.0 | |
| WSL | 7.0 | | 87.0 | | 87.0 | | 87.1 | | 87.1 | | 87.1 | | 87.1 | |
| WSL | 7.0 | | 87.1 | | 87.2 | | 87.2 | | 87.2 | | 87.2 | | 87.2 | |
| WSL | 7.0 | | 87.2 | | 87.2 | | 87.3 | | 87.3 | | 87.3 | | | |
| CAL1 | 7.0 | | 86.96 | | 11.00 | | 9.10 | | | | | | | |
| VEL1 | 7.0 | | | | 0.10 | 0.30 | 1.00 | 1.50 | 1.50 | 1.50 | 1.40 | 1.40 | 1.30 | |
| VEL1 | 7.0 | 1.20 | 0.80 | 0.10 | | | | | | | | | | |
| CAL2 | 7.0 | | 86.90 | | 9.00 | | 7.60 | | | | | | | |
| VEL2 | 7.0 | | | | 0.10 | 0.10 | 0.90 | 1.40 | 1.40 | 1.30 | 1.30 | 1.30 | 1.20 | |
| VEL2 | 7.0 | 1.00 | 0.60 | 0.10 | | | | | | | | | | |
| CAL3 | 7.0 | | 86.88 | | 8.00 | | 7.00 | | | | | | | |
| VEL3 | 7.0 | | | | 0.10 | 0.10 | 0.70 | 1.30 | 1.30 | 1.20 | 1.30 | 1.20 | 1.10 | |
| VEL3 | 7.0 | 0.80 | 0.10 | 0.10 | | | | | | | | | | |
| XSEC | 8.0 | | 1.0 | 0.0 | | 86.20 | | 0.00143 | | | | | | |
| | 8.0 | 0.0 | 88.5 | 2.3 | 88.2 | 3.3 | 84.8 | 4.5 | 84.6 | 5.5 | 84.5 | 6.5 | 84.9 | |
| | 8.0 | 7.5 | 85.2 | 8.5 | 85.4 | 9.5 | 85.9 | 10.5 | 85.8 | 11.5 | 86.4 | 12.5 | 86.7 | |
| | 8.0 | 13.2 | 87.0 | 13.4 | 87.0 | 16.0 | 88.0 | 25.0 | 88.4 | 30.0 | 88.3 | 39.7 | 88.8 | |
| | 8.0 | 41.3 | 90.5 | 43.3 | 90.6 | | | | | | | | | |
| NS | 8.0 | | 6.0 | | 1.0 | | 1.0 | | 3.0 | | 3.0 | | 5.0 | |
| NS | 8.0 | | 6.0 | | 6.0 | | 1.0 | | 3.0 | | 6.0 | | 5.0 | |
| NS | 8.0 | | 5.0 | | 5.0 | | 5.0 | | 4.0 | | 4.0 | | 1.0 | |
| NS | 8.0 | | 1.0 | | 1.0 | | | | | | | | | |
| WSL | 8.0 | | 86.6 | | 86.7 | | 86.7 | | 86.8 | | 86.8 | | 86.9 | |
| WSL | 8.0 | | 86.9 | | 86.9 | | 87.0 | | 87.0 | | 87.0 | | 87.1 | |
| WSL | 8.0 | | 87.1 | | 87.1 | | 87.1 | | 87.1 | | 87.2 | | 87.2 | |
| WSL | 8.0 | | 87.2 | | 87.2 | | 87.2 | | 87.3 | | 87.3 | | 87.3 | |
| WSL | 8.0 | | 87.3 | | 87.3 | | 87.3 | | 87.4 | | 87.4 | | | |
| CAL1 | 8.0 | | 86.98 | | 11.00 | | 11.00 | | | | | | | |
| VEL1 | 8.0 | | | | 1.10 | 1.70 | 1.30 | 1.00 | 0.50 | 0.10 | 0.10 | 0.30 | 0.40 | 0.20 |

| | | | | | | | | | | | | | |
|------|-----|-------|------|-------|------|---------|------|------|------|------|------|------|------|
| VEL1 | 8.0 | 0.10 | | | | | | | | | | | |
| CAL2 | 8.0 | 86.90 | | 9.00 | | 10.50 | | | | | | | |
| VEL2 | 8.0 | | 0.10 | 1.20 | 1.20 | 0.80 | 0.30 | 0.10 | 0.10 | 0.30 | 0.30 | 0.20 | |
| VEL2 | 8.0 | 0.10 | | | | | | | | | | | |
| CAL3 | 8.0 | 86.89 | | 8.00 | | 6.70 | | | | | | | |
| VEL3 | 8.0 | | 0.10 | 0.80 | 1.10 | 0.60 | 0.20 | 0.10 | 0.10 | 0.20 | 0.10 | 0.10 | |
| VEL3 | 8.0 | 0.10 | | | | | | | | | | | |
| XSEC | 9.0 | 100.0 | 0.0 | 86.20 | | 0.00143 | | | | | | | |
| | 9.0 | 0.0 | 88.5 | 2.3 | 88.2 | 3.3 | 84.8 | 4.5 | 84.6 | 5.5 | 84.5 | 6.5 | 84.9 |
| | 9.0 | 7.5 | 85.2 | 8.5 | 85.4 | 9.5 | 85.9 | 10.5 | 85.8 | 11.5 | 86.4 | 12.5 | 86.7 |
| | 9.0 | 13.2 | 87.0 | 13.4 | 87.0 | 16.0 | 88.0 | 25.0 | 88.4 | 30.0 | 88.3 | 39.7 | 88.8 |
| | 9.0 | 41.3 | 90.5 | 43.3 | 90.6 | | | | | | | | |
| NS | 9.0 | 6.0 | | 1.0 | | 1.0 | | 3.0 | | 3.0 | | 5.0 | |
| NS | 9.0 | 6.0 | | 6.0 | | 1.0 | | 3.0 | | 6.0 | | 5.0 | |
| NS | 9.0 | 5.0 | | 5.0 | | 5.0 | | 4.0 | | 4.0 | | 1.0 | |
| NS | 9.0 | 1.0 | | 1.0 | | | | | | | | | |
| WSL | 9.0 | 86.6 | | 86.7 | | 86.7 | | 86.8 | | 86.8 | | 86.9 | |
| WSL | 9.0 | 86.9 | | 86.9 | | 87.0 | | 87.0 | | 87.0 | | 87.1 | |
| WSL | 9.0 | 87.1 | | 87.1 | | 87.1 | | 87.1 | | 87.2 | | 87.2 | |
| WSL | 9.0 | 87.2 | | 87.2 | | 87.2 | | 87.3 | | 87.3 | | 87.3 | |
| WSL | 9.0 | 87.3 | | 87.3 | | 87.3 | | 87.4 | | 87.4 | | | |
| CAL1 | 9.0 | 86.98 | | 11.00 | | 11.00 | | | | | | | |
| VEL1 | 9.0 | | 1.10 | 1.70 | 1.30 | 1.00 | 0.50 | 0.10 | 0.10 | 0.30 | 0.40 | 0.20 | |
| VEL1 | 9.0 | 0.10 | | | | | | | | | | | |
| CAL2 | 9.0 | 86.90 | | 9.00 | | 10.50 | | | | | | | |
| VEL2 | 9.0 | | 0.10 | 1.20 | 1.20 | 0.80 | 0.30 | 0.10 | 0.10 | 0.30 | 0.30 | 0.20 | |
| VEL2 | 9.0 | 0.10 | | | | | | | | | | | |
| CAL3 | 9.0 | 86.89 | | 8.00 | | 6.70 | | | | | | | |
| VEL3 | 9.0 | | 0.10 | 0.80 | 1.10 | 0.60 | 0.20 | 0.10 | 0.10 | 0.20 | 0.10 | 0.10 | |
| VEL3 | 9.0 | 0.10 | | | | | | | | | | | |
| ENDJ | | | | | | | | | | | | | |

Big Timber Study Site 5 - substrate

Export from PHABSIM for Windows

IOC 0000000100010000100000

| | | | | | | | | | | | | | |
|------|------|------|-------|------|-------|-------|------|---------|------|------|------|------|------|
| QARD | 2.0 | | | | | | | | | | | | |
| QARD | 4.0 | | | | | | | | | | | | |
| QARD | 6.0 | | | | | | | | | | | | |
| QARD | 8.0 | | | | | | | | | | | | |
| QARD | 10.0 | | | | | | | | | | | | |
| QARD | 12.0 | | | | | | | | | | | | |
| QARD | 14.0 | | | | | | | | | | | | |
| QARD | 15.0 | | | | | | | | | | | | |
| QARD | 16.0 | | | | | | | | | | | | |
| QARD | 18.0 | | | | | | | | | | | | |
| QARD | 20.0 | | | | | | | | | | | | |
| QARD | 22.0 | | | | | | | | | | | | |
| QARD | 24.0 | | | | | | | | | | | | |
| QARD | 25.0 | | | | | | | | | | | | |
| QARD | 26.0 | | | | | | | | | | | | |
| QARD | 28.0 | | | | | | | | | | | | |
| QARD | 30.0 | | | | | | | | | | | | |
| QARD | 32.0 | | | | | | | | | | | | |
| QARD | 34.0 | | | | | | | | | | | | |
| QARD | 36.0 | | | | | | | | | | | | |
| QARD | 38.0 | | | | | | | | | | | | |
| QARD | 40.0 | | | | | | | | | | | | |
| QARD | 42.0 | | | | | | | | | | | | |
| QARD | 44.0 | | | | | | | | | | | | |
| QARD | 46.0 | | | | | | | | | | | | |
| QARD | 48.0 | | | | | | | | | | | | |
| QARD | 50.0 | | | | | | | | | | | | |
| QARD | 52.0 | | | | | | | | | | | | |
| QARD | 54.0 | | | | | | | | | | | | |
| XSEC | 1.0 | | 0.0 | 0.0 | | 97.70 | | 0.00368 | | | | | |
| | 1.0 | 0.0 | 101.4 | 0.9 | 100.8 | 1.9 | 98.6 | 3.4 | 98.6 | 4.9 | 98.6 | 6.4 | 98.4 |
| | 1.0 | 7.9 | 98.5 | 9.4 | 98.2 | 10.9 | 98.2 | 12.4 | 98.2 | 13.9 | 98.1 | 15.4 | 98.2 |
| | 1.0 | 16.9 | 98.1 | 18.4 | 98.0 | 19.9 | 97.7 | 21.4 | 97.9 | 22.9 | 97.8 | 24.4 | 98.1 |
| | 1.0 | 25.9 | 98.3 | 28.2 | 98.5 | 29.0 | 99.8 | 30.2 | 99.9 | | | | |
| NS | 1.0 | | 2.0 | | 2.0 | | 3.0 | | 4.0 | | 5.0 | | 5.0 |

| | | | | | | | | | | | | | |
|------|-----|----------|----------|-------|---------|------|-------|------|-------|------|-------|------|-------|
| NS | 1.0 | 5.0 | 5.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | | | |
| NS | 1.0 | 6.0 | 7.0 | 6.0 | 4.0 | 4.0 | 4.0 | 6.0 | | | | | |
| NS | 1.0 | 4.0 | 3.0 | 1.0 | 1.0 | | | | | | | | |
| WSL | 1.0 | 98.5 | 98.6 | 98.6 | 98.6 | 98.6 | 98.6 | 98.7 | | | | | |
| WSL | 1.0 | 98.7 | 98.7 | 98.7 | 98.7 | 98.7 | 98.7 | 98.7 | | | | | |
| WSL | 1.0 | 98.7 | 98.7 | 98.7 | 98.7 | 98.7 | 98.7 | 98.7 | | | | | |
| WSL | 1.0 | 98.7 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | | | | | |
| WSL | 1.0 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | | | | | |
| CAL1 | 1.0 | 98.73 | 28.00 | 25.10 | | | | | | | | | |
| VEL1 | 1.0 | | 0.80 | 1.40 | 0.20 | 1.00 | 1.80 | 1.50 | 1.60 | 2.30 | 2.50 | 2.30 | |
| VEL1 | 1.0 | 2.40 | 2.80 | 2.50 | 2.30 | 2.20 | 1.30 | 1.00 | 0.30 | | | | |
| CAL2 | 1.0 | 98.72 | 25.00 | 22.30 | | | | | | | | | |
| VEL2 | 1.0 | | 0.70 | 0.70 | 0.20 | 1.00 | 1.70 | 1.20 | 1.30 | 2.20 | 2.20 | 2.10 | |
| VEL2 | 1.0 | 1.10 | 2.10 | 2.20 | 2.20 | 1.70 | 1.30 | 0.90 | 0.20 | | | | |
| CAL3 | 1.0 | 98.68 | 15.00 | 15.30 | | | | | | | | | |
| VEL3 | 1.0 | | 0.60 | 0.10 | 0.10 | 0.70 | 0.10 | 0.60 | 0.90 | 1.50 | 1.80 | 1.70 | |
| VEL3 | 1.0 | 1.00 | 1.90 | 1.90 | 1.60 | 1.20 | 0.80 | 0.80 | 0.10 | | | | |
| XSEC | 2.0 | 1.0 | 1.0 | 97.70 | 0.00154 | | | | | | | | |
| | 2.0 | 0.0101.2 | 1.2101.3 | 7.6 | 99.0 | 8.4 | 98.9 | 9.6 | 98.7 | 11.1 | 98.5 | | |
| | 2.0 | 12.6 | 98.3 | 14.1 | 98.1 | 15.6 | 98.0 | 17.1 | 97.8 | 18.6 | 97.6 | 20.1 | 97.7 |
| | 2.0 | 21.6 | 97.3 | 23.1 | 97.6 | 24.6 | 98.0 | 26.1 | 98.3 | 27.1 | 98.4 | 28.0 | 100.0 |
| | 2.0 | 29.6 | 100.5 | | | | | | | | | | |
| NS | 2.0 | 1.0 | 2.0 | 2.0 | 7.0 | 4.0 | 5.0 | | | | | | |
| NS | 2.0 | 5.0 | 5.0 | 5.0 | 3.0 | 6.0 | 7.0 | | | | | | |
| NS | 2.0 | 4.0 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 1.0 | | | | | |
| NS | 2.0 | 1.0 | | | | | | | | | | | |
| WSL | 2.0 | 98.5 | 98.6 | 98.6 | 98.7 | 98.7 | 98.7 | | | | | | |
| WSL | 2.0 | 98.7 | 98.7 | 98.7 | 98.7 | 98.8 | 98.8 | | | | | | |
| WSL | 2.0 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | 98.8 | | | | | | |
| WSL | 2.0 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 | 98.9 | | | | | | |
| WSL | 2.0 | 99.0 | 99.0 | 99.0 | 99.0 | 99.0 | 99.0 | | | | | | |
| CAL1 | 2.0 | 98.86 | 28.00 | 23.40 | | | | | | | | | |
| VEL1 | 2.0 | | 0.10 | 0.80 | 1.30 | 1.40 | 1.90 | 2.00 | 2.10 | 1.40 | 2.90 | | |
| VEL1 | 2.0 | 2.20 | 1.10 | 0.70 | 0.30 | 0.10 | | | | | | | |
| CAL2 | 2.0 | 98.84 | 25.00 | 22.20 | | | | | | | | | |
| VEL2 | 2.0 | | 0.10 | 0.30 | 1.00 | 1.30 | 1.40 | 1.60 | 2.00 | 1.10 | 2.60 | | |
| VEL2 | 2.0 | 2.00 | 0.50 | 0.40 | 0.10 | 0.10 | | | | | | | |
| CAL3 | 2.0 | 98.77 | 15.00 | 14.40 | | | | | | | | | |
| VEL3 | 2.0 | | 0.10 | 0.10 | 0.50 | 0.70 | 0.90 | 1.30 | 1.50 | 0.80 | 1.90 | | |
| VEL3 | 2.0 | 1.70 | 0.40 | 0.10 | 0.10 | 0.10 | | | | | | | |
| XSEC | 3.0 | 290.0 | 1.0 | 97.70 | 0.03625 | | | | | | | | |
| | 3.0 | 0.0101.6 | 2.6101.7 | 15.1 | 98.9 | 15.4 | 98.8 | 16.4 | 98.6 | 18.4 | 98.4 | | |
| | 3.0 | 19.4 | 98.4 | 20.4 | 98.2 | 21.4 | 98.0 | 22.4 | 97.8 | 23.4 | 97.5 | 24.4 | 97.8 |
| | 3.0 | 25.4 | 98.0 | 26.4 | 96.8 | 27.4 | 97.1 | 28.4 | 97.6 | 29.4 | 97.5 | 30.4 | 97.7 |
| | 3.0 | 31.7 | 97.8 | 33.4 | 101.5 | 34.2 | 100.9 | | | | | | |
| NS | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | |
| NS | 3.0 | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 7.0 | |
| NS | 3.0 | 7.0 | 6.0 | 4.0 | 7.0 | 4.0 | 4.0 | | | | | | |
| NS | 3.0 | 1.0 | 1.0 | 1.0 | | | | | | | | | |
| WSL | 3.0 | 98.5 | 98.6 | 98.6 | 98.7 | 98.7 | 98.7 | | | | | | |
| WSL | 3.0 | 98.7 | 98.7 | 98.7 | 98.8 | 98.8 | 98.8 | | | | | | |
| WSL | 3.0 | 98.8 | 98.8 | 98.9 | 98.9 | 98.9 | 98.9 | | | | | | |
| WSL | 3.0 | 98.9 | 98.9 | 99.0 | 99.0 | 99.0 | 99.0 | | | | | | |
| WSL | 3.0 | 99.0 | 99.1 | 99.1 | 99.1 | 99.1 | 99.1 | | | | | | |
| CAL1 | 3.0 | 98.86 | 28.00 | 25.70 | | | | | | | | | |
| VEL1 | 3.0 | | 0.10 | 0.20 | 0.10 | 0.50 | 1.00 | 1.60 | 2.20 | 2.60 | 3.00 | | |
| VEL1 | 3.0 | 3.70 | 3.10 | 2.70 | 1.60 | 0.50 | 0.20 | 0.10 | | | | | |
| CAL2 | 3.0 | 98.84 | 25.00 | 25.40 | | | | | | | | | |
| VEL2 | 3.0 | | 0.10 | 0.10 | 0.10 | 0.10 | 0.50 | 1.30 | 1.80 | 2.40 | 2.60 | | |
| VEL2 | 3.0 | 2.80 | 2.80 | 2.10 | 1.50 | 0.20 | 0.20 | 0.10 | | | | | |
| CAL3 | 3.0 | 98.74 | 15.00 | 15.20 | | | | | | | | | |
| VEL3 | 3.0 | | 0.10 | 0.10 | 0.10 | 0.10 | 0.30 | 0.50 | 0.80 | 1.30 | 1.70 | | |
| VEL3 | 3.0 | 2.00 | 2.00 | 2.10 | 1.40 | 0.10 | 0.10 | 0.10 | | | | | |
| XSEC | 4.0 | 100.0 | 0.3 | 98.50 | 0.02167 | | | | | | | | |
| | 4.0 | 0.0102.1 | 3.4101.2 | 16.7 | 99.4 | 19.7 | 99.4 | 24.0 | 99.3 | 26.0 | 98.9 | | |
| | 4.0 | 28.0 | 98.8 | 30.0 | 98.9 | 32.0 | 99.0 | 34.0 | 99.2 | 36.0 | 99.1 | 38.0 | 99.1 |
| | 4.0 | 40.0 | 99.2 | 41.0 | 99.2 | 43.0 | 99.3 | 45.0 | 99.1 | 47.0 | 98.9 | 49.0 | 98.6 |
| | 4.0 | 51.0 | 98.5 | 53.0 | 98.6 | 54.2 | 99.1 | 54.7 | 100.7 | 56.3 | 100.7 | | |
| NS | 4.0 | 3.0 | 3.0 | 2.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | |
| NS | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 4.0 | 5.0 | | | |

| | | | | | | | | | | | |
|------|-----|----------|----------|----------|----------|----------|-------|-------|-------|-------|-------|
| NS | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 6.0 | 6.0 | | | | |
| NS | 4.0 | 5.0 | 5.0 | 2.0 | 1.0 | 1.0 | | | | | |
| WSL | 4.0 | 99.1 | 99.2 | 99.3 | 99.3 | 99.3 | 99.3 | 99.4 | | | |
| WSL | 4.0 | 99.4 | 99.4 | 99.4 | 99.4 | 99.4 | 99.4 | 99.5 | | | |
| WSL | 4.0 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5 | | | |
| WSL | 4.0 | 99.5 | 99.6 | 99.6 | 99.6 | 99.6 | 99.6 | 99.6 | | | |
| WSL | 4.0 | 99.6 | 99.6 | 99.6 | 99.6 | 99.6 | 99.6 | 99.6 | | | |
| CAL1 | 4.0 | 99.51 | 28.00 | 42.70 | | | | | | | |
| VEL1 | 4.0 | | 0.10 | 0.10 | 4.00 | 4.20 | 3.80 | 3.50 | 3.80 | 3.70 | 2.10 |
| VEL1 | 4.0 | 1.80 | 2.70 | 0.60 | 2.00 | 2.90 | 3.50 | 4.10 | 2.80 | 0.90 | |
| CAL2 | 4.0 | 99.49 | 25.00 | 46.60 | | | | | | | |
| VEL2 | 4.0 | | 0.10 | 0.10 | 3.20 | 2.60 | 2.60 | 3.40 | 3.60 | 2.10 | 2.10 |
| VEL2 | 4.0 | 0.80 | 2.10 | 0.10 | 1.90 | 2.80 | 3.20 | 3.50 | 2.50 | 0.40 | |
| CAL3 | 4.0 | 99.40 | 15.00 | 19.40 | | | | | | | |
| VEL3 | 4.0 | | 0.10 | 0.10 | 0.90 | 1.70 | 0.10 | 0.90 | 1.40 | 2.00 | 0.90 |
| VEL3 | 4.0 | 0.10 | 0.10 | 0.10 | 0.10 | 1.60 | 2.40 | 3.30 | 2.40 | 0.70 | |
| XSEC | 5.0 | 610.0 | 0.0 | 99.50 | 0.02167 | | | | | | |
| | 5.0 | 0.0101.6 | 1.0101.8 | 7.1100.4 | 7.4100.2 | 7.9100.0 | 9.9 | 99.9 | | | |
| | 5.0 | 11.9 | 99.8 | 13.9 | 99.7 | 15.9 | 99.7 | 17.9 | 99.8 | 19.9 | 99.9 |
| | 5.0 | 23.9 | 99.6 | 25.9 | 99.7 | 27.9 | 99.7 | 29.9 | 99.7 | 31.9 | 99.7 |
| | 5.0 | 35.5 | 99.5 | 37.5 | 99.5 | 39.3 | 99.7 | 41.4 | 102.1 | 42.5 | 102.4 |
| NS | 5.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | 8.0 | 1.0 | 8.0 | 1.0 | 8.0 |
| NS | 5.0 | 1.0 | 8.0 | 1.0 | 8.0 | 1.0 | 8.0 | 1.0 | 8.0 | 1.0 | 8.0 |
| NS | 5.0 | 1.0 | 8.0 | 1.0 | 8.0 | 1.0 | 8.0 | 1.0 | 8.0 | 1.0 | 8.0 |
| NS | 5.0 | 1.0 | 8.0 | 1.0 | 8.0 | 1.0 | 8.0 | 6.0 | 8.0 | | |
| WSL | 5.0 | 99.7 | 99.8 | 99.8 | 99.8 | 99.9 | 99.9 | 99.9 | 99.9 | 99.9 | |
| WSL | 5.0 | 99.9 | 99.9 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | |
| WSL | 5.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.1 | 100.1 | 100.1 | |
| WSL | 5.0 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 | |
| WSL | 5.0 | 100.1 | 100.2 | 100.2 | 100.2 | 100.2 | 100.2 | 100.2 | 100.2 | 100.2 | |
| CAL1 | 5.0 | 100.05 | 28.00 | 18.90 | | | | | | | |
| VEL1 | 5.0 | | 0.10 | 0.50 | 1.50 | 2.30 | 1.80 | 1.50 | 2.40 | 2.50 | 2.00 |
| VEL1 | 5.0 | 1.50 | 2.20 | 1.90 | 2.60 | 1.50 | 2.20 | 2.50 | 2.50 | 0.80 | |
| CAL2 | 5.0 | 100.03 | 25.00 | 19.10 | | | | | | | |
| VEL2 | 5.0 | | 0.10 | 0.40 | 1.10 | 2.00 | 1.30 | 1.20 | 2.20 | 1.90 | 2.00 |
| VEL2 | 5.0 | 1.30 | 2.20 | 1.70 | 1.80 | 1.40 | 2.00 | 2.40 | 2.20 | 0.70 | |
| CAL3 | 5.0 | 99.95 | 15.00 | 9.90 | | | | | | | |
| VEL3 | 5.0 | | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.80 | 1.00 | 1.00 | 1.60 |
| VEL3 | 5.0 | 1.10 | 1.70 | 1.10 | 1.30 | 0.70 | 1.50 | 2.30 | 1.30 | 0.40 | |
| ENDJ | | | | | | | | | | | |

Big_Timber Study Site 6 - substrate

Export from PHABSIM for Windows

IOC 0000000100010000100000

QARD 3.0
 QARD 5.0
 QARD 7.0
 QARD 9.0
 QARD 11.0
 QARD 13.0
 QARD 15.0
 QARD 17.0
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 QARD 49.0
 QARD 51.0
 QARD 53.0

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|------|------|-------|------|-------|---------|-------|------|------|------|------|------|------|------|
| QARD | 55.0 | | | | | | | | | | | | |
| QARD | 57.0 | | | | | | | | | | | | |
| QARD | 59.0 | | | | | | | | | | | | |
| XSEC | 1.0 | 0.0 | 0.0 | 88.70 | 0.00263 | | | | | | | | |
| | 1.0 | 0.0 | 92.5 | 2.5 | 91.9 | 5.0 | 89.9 | 6.9 | 89.6 | 7.5 | 89.4 | 9.5 | 89.2 |
| | 1.0 | 11.5 | 89.1 | 13.5 | 89.1 | 15.5 | 89.1 | 17.5 | 89.1 | 19.5 | 89.0 | 21.5 | 88.9 |
| | 1.0 | 23.5 | 88.8 | 25.5 | 88.7 | 27.5 | 88.9 | 29.5 | 88.7 | 31.5 | 88.8 | 33.5 | 88.9 |
| | 1.0 | 35.5 | 88.9 | 37.5 | 89.0 | 39.3 | 89.6 | 39.9 | 90.2 | 42.1 | 90.9 | | |
| NS | 1.0 | 1.0 | | 1.0 | | 1.0 | | 6.0 | | 6.0 | | 4.0 | |
| NS | 1.0 | 5.0 | | 5.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | |
| NS | 1.0 | 6.0 | | 6.0 | | 7.0 | | 6.0 | | 6.0 | | 6.0 | |
| NS | 1.0 | 6.0 | | 5.0 | | 4.0 | | 7.0 | | 1.0 | | | |
| WSL | 1.0 | 89.2 | | 89.3 | | 89.4 | | 89.4 | | 89.5 | | 89.6 | |
| WSL | 1.0 | 89.6 | | 89.6 | | 89.7 | | 89.8 | | 89.8 | | 89.8 | |
| WSL | 1.0 | 89.9 | | 89.9 | | 89.9 | | 90.0 | | 90.0 | | 90.0 | |
| WSL | 1.0 | 90.1 | | 90.1 | | 90.1 | | 90.2 | | 90.2 | | 90.2 | |
| WSL | 1.0 | 90.2 | | 90.3 | | 90.3 | | 90.3 | | 90.3 | | | |
| CAL1 | 1.0 | 89.92 | | 29.00 | | 34.60 | | | | | | | |
| VEL1 | 1.0 | | 0.10 | 0.10 | 0.60 | 0.60 | 0.70 | 0.80 | 0.70 | 1.00 | 1.20 | 1.10 | |
| VEL1 | 1.0 | 1.50 | 1.20 | 1.50 | 1.50 | 1.50 | 1.70 | 1.20 | 0.90 | 0.70 | | | |
| CAL2 | 1.0 | 89.65 | | 17.00 | | 22.10 | | | | | | | |
| VEL2 | 1.0 | | 0.10 | 0.30 | 0.50 | 0.60 | 0.70 | 0.60 | 0.60 | 1.00 | 1.00 | | |
| VEL2 | 1.0 | 1.30 | 0.80 | 1.20 | 1.40 | 1.30 | 1.30 | 0.90 | 0.70 | 0.30 | | | |
| CAL3 | 1.0 | 89.59 | | 13.00 | | 16.90 | | | | | | | |
| VEL3 | 1.0 | | 0.10 | 0.20 | 0.60 | 0.40 | 0.60 | 0.60 | 0.60 | 0.70 | 0.80 | | |
| VEL3 | 1.0 | 1.30 | 0.70 | 0.70 | 0.90 | 1.30 | 1.10 | 0.70 | 0.50 | 0.00 | | | |
| XSEC | 2.0 | 0.0 | 1.0 | 88.70 | 0.01500 | | | | | | | | |
| | 2.0 | 0.0 | 92.5 | 4.2 | 91.9 | 5.9 | 89.8 | 6.4 | 89.7 | 8.4 | 89.1 | 10.4 | 89.2 |
| | 2.0 | 12.4 | 89.2 | 14.4 | 89.3 | 16.4 | 89.3 | 18.4 | 88.8 | 19.9 | 88.7 | 21.4 | 88.6 |
| | 2.0 | 22.9 | 88.4 | 24.4 | 88.7 | 25.9 | 88.8 | 27.4 | 89.1 | 28.3 | 89.3 | 29.5 | 90.2 |
| | 2.0 | 31.9 | 90.9 | | | | | | | | | | |
| NS | 2.0 | 2.0 | | 2.0 | | 2.0 | | 2.0 | | 6.0 | | 6.0 | |
| NS | 2.0 | 4.0 | | 7.0 | | 7.0 | | 6.0 | | 6.0 | | 6.0 | |
| NS | 2.0 | 6.0 | | 6.0 | | 5.0 | | 5.0 | | 6.0 | | 1.0 | |
| NS | 2.0 | 1.0 | | | | | | | | | | | |
| WSL | 2.0 | 89.3 | | 89.4 | | 89.5 | | 89.6 | | 89.6 | | 89.6 | |
| WSL | 2.0 | 89.7 | | 89.8 | | 89.8 | | 89.9 | | 89.9 | | 89.9 | |
| WSL | 2.0 | 90.0 | | 90.0 | | 90.0 | | 90.1 | | 90.1 | | 90.1 | |
| WSL | 2.0 | 90.1 | | 90.2 | | 90.2 | | 90.2 | | 90.2 | | 90.3 | |
| WSL | 2.0 | 90.3 | | 90.3 | | 90.3 | | 90.3 | | 90.4 | | | |
| CAL1 | 2.0 | 89.97 | | 29.00 | | 23.90 | | | | | | | |
| VEL1 | 2.0 | | 0.10 | 0.10 | 0.30 | 0.60 | 0.80 | 0.80 | 1.60 | 1.00 | 1.60 | 2.20 | |
| VEL1 | 2.0 | 2.20 | 1.60 | 1.00 | 0.60 | 0.20 | | | | | | | |
| CAL2 | 2.0 | 89.82 | | 17.00 | | 16.20 | | | | | | | |
| VEL2 | 2.0 | | 0.10 | 0.10 | 0.20 | 0.30 | 0.50 | 0.10 | 1.10 | 0.50 | 1.50 | 1.90 | |
| VEL2 | 2.0 | 1.10 | 1.60 | 0.90 | 0.40 | 0.10 | | | | | | | |
| CAL3 | 2.0 | 89.66 | | 13.00 | | 8.70 | | | | | | | |
| VEL3 | 2.0 | | 0.10 | 0.20 | 0.20 | 0.40 | 0.10 | 0.10 | 0.40 | 1.30 | 1.70 | | |
| VEL3 | 2.0 | 1.10 | 1.20 | 0.70 | 0.30 | 0.10 | | | | | | | |
| XSEC | 3.0 | 245.0 | 1.0 | 89.10 | 0.01850 | | | | | | | | |
| | 3.0 | 0.0 | 94.6 | 7.0 | 94.4 | 7.5 | 90.4 | 8.3 | 89.8 | 9.8 | 89.6 | 11.3 | 89.3 |
| | 3.0 | 12.8 | 89.1 | 14.3 | 89.3 | 15.8 | 89.4 | 17.3 | 89.4 | 18.8 | 89.8 | 20.3 | 89.6 |
| | 3.0 | 21.8 | 89.6 | 23.3 | 89.7 | 24.8 | 90.1 | 26.3 | 90.1 | 27.8 | 90.0 | 29.3 | 90.2 |
| | 3.0 | 30.8 | 90.3 | 31.5 | 90.4 | 32.3 | 90.7 | 36.3 | 93.0 | 37.2 | 93.2 | | |
| NS | 3.0 | 1.0 | | 1.0 | | 7.0 | | 7.0 | | 7.0 | | 6.0 | |
| NS | 3.0 | 6.0 | | 7.0 | | 7.0 | | 7.0 | | 6.0 | | 6.0 | |
| NS | 3.0 | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | |
| NS | 3.0 | 1.0 | 2.0 | 1.0 | 2.0 | 2.0 | | 1.0 | | 1.0 | | | |
| WSL | 3.0 | 90.2 | | 90.3 | | 90.3 | | 90.4 | | 90.4 | | 90.4 | |
| WSL | 3.0 | 90.5 | | 90.5 | | 90.5 | | 90.5 | | 90.5 | | 90.6 | |
| WSL | 3.0 | 90.6 | | 90.6 | | 90.6 | | 90.6 | | 90.6 | | 90.6 | |
| WSL | 3.0 | 90.7 | | 90.7 | | 90.7 | | 90.7 | | 90.7 | | 90.7 | |
| WSL | 3.0 | 90.7 | | 90.7 | | 90.7 | | 90.7 | | 90.7 | | | |
| CAL1 | 3.0 | 90.59 | | 29.00 | | 38.60 | | | | | | | |
| VEL1 | 3.0 | | 0.10 | 0.40 | 1.70 | 2.50 | 3.20 | 0.90 | 1.10 | 4.20 | 3.00 | 2.20 | |
| VEL1 | 3.0 | 0.70 | 3.80 | 2.50 | 1.40 | 2.20 | 2.10 | 0.20 | 0.10 | | | | |
| CAL2 | 3.0 | 90.46 | | 17.00 | | 23.10 | | | | | | | |
| VEL2 | 3.0 | | 0.10 | 0.40 | 1.40 | 1.90 | 2.10 | 0.30 | 0.30 | 3.20 | 1.10 | 0.80 | |
| VEL2 | 3.0 | 0.60 | 2.70 | 1.70 | 1.10 | 1.40 | 1.80 | 0.40 | 0.10 | | | | |
| CAL3 | 3.0 | 90.44 | | 13.00 | | 13.60 | | | | | | | |
| VEL3 | 3.0 | | 0.10 | 0.10 | 1.30 | 1.60 | 1.90 | 0.10 | 0.10 | 0.50 | 0.20 | 0.40 | |

| | | | | | | | | | | | | | | | | | | | |
|------|-----|------|-------|------|-------|-------|-------|---------|------|------|------|------|------|--|--|--|--|--|--|
| VEL3 | 3.0 | 0.10 | 2.00 | 1.30 | 0.20 | 1.20 | 0.90 | 0.10 | 0.10 | | | | | | | | | | |
| XSEC | 4.0 | | 310.0 | 1.0 | | 89.90 | | 0.00001 | | | | | | | | | | | |
| | 4.0 | 0.0 | 94.7 | 4.8 | 94.6 | 5.8 | 91.0 | 8.3 | 90.1 | 9.8 | 90.0 | 11.3 | 89.9 | | | | | | |
| | 4.0 | 12.8 | 90.2 | 14.3 | 89.9 | 15.8 | 90.0 | 16.8 | 90.1 | 17.8 | 90.2 | 19.4 | 90.3 | | | | | | |
| | 4.0 | 20.8 | 90.4 | 22.3 | 90.7 | 22.4 | 91.0 | 26.0 | 93.1 | 28.1 | 93.4 | | | | | | | | |
| NS | 4.0 | | 7.0 | | 7.0 | | 7.0 | | 7.0 | | 7.0 | | 6.0 | | | | | | |
| NS | 4.0 | | 7.0 | | 7.0 | | 7.0 | | 6.0 | | 6.0 | | 6.0 | | | | | | |
| NS | 4.0 | | 5.0 | | 5.0 | | 5.0 | | 7.0 | | 7.0 | | | | | | | | |
| WSL | 4.0 | | 90.5 | | 90.6 | | 90.7 | | 90.7 | | 90.8 | | 90.8 | | | | | | |
| WSL | 4.0 | | 90.9 | | 91.0 | | 91.0 | | 91.0 | | 91.1 | | 91.1 | | | | | | |
| WSL | 4.0 | | 91.1 | | 91.1 | | 91.2 | | 91.2 | | 91.2 | | 91.3 | | | | | | |
| WSL | 4.0 | | 91.3 | | 91.3 | | 91.3 | | 91.3 | | 91.4 | | 91.4 | | | | | | |
| WSL | 4.0 | | 91.4 | | 91.4 | | 91.4 | | 91.5 | | 91.5 | | | | | | | | |
| CAL1 | 4.0 | | 91.14 | | 29.00 | | 25.00 | | | | | | | | | | | | |
| VEL1 | 4.0 | | | 0.10 | 1.90 | 0.90 | 2.20 | 2.90 | 2.30 | 2.10 | 1.00 | 1.30 | 1.20 | | | | | | |
| VEL1 | 4.0 | 0.90 | 0.70 | 0.10 | | | | | | | | | | | | | | | |
| CAL2 | 4.0 | | 90.96 | | 17.00 | | 16.80 | | | | | | | | | | | | |
| VEL2 | 4.0 | | | 0.10 | 1.90 | 0.80 | 1.60 | 1.90 | 1.50 | 1.40 | 0.80 | 0.70 | 1.10 | | | | | | |
| VEL2 | 4.0 | 0.70 | 0.50 | 0.10 | | | | | | | | | | | | | | | |
| CAL3 | 4.0 | | 90.85 | | 13.00 | | 11.50 | | | | | | | | | | | | |
| VEL3 | 4.0 | | | | 1.50 | 0.70 | 1.30 | 1.40 | 1.40 | 1.00 | 0.80 | 0.40 | 1.10 | | | | | | |
| VEL3 | 4.0 | 0.50 | 0.50 | | | | | | | | | | | | | | | | |
| XSEC | 5.0 | | 0.0 | 1.0 | | 89.90 | | 0.03300 | | | | | | | | | | | |
| | 5.0 | 0.0 | 93.7 | 2.2 | 91.8 | 2.8 | 91.0 | 3.3 | 90.7 | 4.3 | 90.2 | 5.3 | 90.0 | | | | | | |
| | 5.0 | 6.3 | 89.8 | 7.3 | 89.9 | 8.8 | 89.9 | 10.3 | 89.9 | 11.3 | 90.0 | 12.3 | 89.5 | | | | | | |
| | 5.0 | 13.3 | 89.4 | 14.3 | 89.5 | 15.3 | 90.4 | 16.3 | 90.4 | 17.3 | 89.4 | 18.3 | 89.7 | | | | | | |
| | 5.0 | 20.0 | 92.0 | 23.1 | 93.5 | 24.4 | 94.0 | | | | | | | | | | | | |
| NS | 5.0 | | 6.0 | | 6.0 | | 2.0 | | 3.0 | | 4.0 | | 6.0 | | | | | | |
| NS | 5.0 | | 6.0 | | 6.0 | | 7.0 | | 7.0 | | 7.0 | | 7.0 | | | | | | |
| NS | 5.0 | | 7.0 | | 6.0 | | 7.0 | | 7.0 | | 6.0 | | 7.0 | | | | | | |
| NS | 5.0 | | 7.0 | | 7.0 | | 1.0 | | | | | | | | | | | | |
| WSL | 5.0 | | 90.6 | | 90.7 | | 90.8 | | 90.8 | | 90.9 | | 90.9 | | | | | | |
| WSL | 5.0 | | 91.0 | | 91.0 | | 91.0 | | 91.1 | | 91.1 | | 91.1 | | | | | | |
| WSL | 5.0 | | 91.2 | | 91.2 | | 91.2 | | 91.2 | | 91.3 | | 91.3 | | | | | | |
| WSL | 5.0 | | 91.3 | | 91.3 | | 91.3 | | 91.4 | | 91.4 | | 91.4 | | | | | | |
| WSL | 5.0 | | 91.4 | | 91.4 | | 91.4 | | 91.5 | | 91.5 | | | | | | | | |
| CAL1 | 5.0 | | 91.15 | | 29.00 | | 31.40 | | | | | | | | | | | | |
| VEL1 | 5.0 | | | 0.10 | 0.20 | 0.10 | 1.70 | 2.40 | 0.30 | 0.40 | 2.30 | 3.20 | 4.00 | | | | | | |
| VEL1 | 5.0 | 3.80 | 3.00 | 1.60 | 0.40 | 0.10 | 0.20 | | | | | | | | | | | | |
| CAL2 | 5.0 | | 91.04 | | 17.00 | | 18.80 | | | | | | | | | | | | |
| VEL2 | 5.0 | | | 0.10 | 0.10 | 0.10 | 1.30 | 2.00 | 0.20 | 0.10 | 0.70 | 1.60 | 2.30 | | | | | | |
| VEL2 | 5.0 | 2.50 | 2.40 | 1.10 | 0.20 | 0.10 | 0.10 | | | | | | | | | | | | |
| CAL3 | 5.0 | | 90.90 | | 13.00 | | 10.20 | | | | | | | | | | | | |
| VEL3 | 5.0 | | | 0.10 | 0.10 | 0.10 | 0.50 | 1.20 | 0.10 | 0.10 | 0.20 | 0.50 | 0.20 | | | | | | |
| VEL3 | 5.0 | 1.90 | 2.30 | 0.90 | 0.10 | 0.10 | 0.10 | | | | | | | | | | | | |
| XSEC | 6.0 | | 70.0 | 0.3 | | 90.40 | | 0.34780 | | | | | | | | | | | |
| | 6.0 | 0.0 | 95.4 | 4.2 | 92.8 | 6.2 | 91.1 | 7.2 | 90.6 | 8.2 | 90.6 | 9.2 | 90.5 | | | | | | |
| | 6.0 | 10.2 | 90.7 | 11.2 | 90.6 | 12.2 | 90.4 | 13.2 | 91.3 | 14.2 | 91.2 | 15.2 | 90.8 | | | | | | |
| | 6.0 | 16.2 | 90.9 | 17.2 | 91.1 | 18.2 | 91.0 | 19.2 | 90.9 | 20.2 | 91.0 | 21.7 | 91.2 | | | | | | |
| | 6.0 | 22.4 | 91.5 | 24.7 | 93.0 | 29.5 | 94.3 | | | | | | | | | | | | |
| NS | 6.0 | | 2.0 | | 1.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | | | | | |
| NS | 6.0 | | 7.0 | | 6.0 | | 7.0 | | 7.0 | | 7.0 | | 7.0 | | | | | | |
| NS | 6.0 | | 6.0 | | 7.0 | | 7.0 | | 7.0 | | 6.0 | | 7.0 | | | | | | |
| NS | 6.0 | | 6.0 | | 1.0 | | 1.0 | | | | | | | | | | | | |
| WSL | 6.0 | | 91.0 | | 91.1 | | 91.2 | | 91.3 | | 91.3 | | 91.4 | | | | | | |
| WSL | 6.0 | | 91.4 | | 91.4 | | 91.5 | | 91.5 | | 91.6 | | 91.6 | | | | | | |
| WSL | 6.0 | | 91.6 | | 91.6 | | 91.7 | | 91.7 | | 91.7 | | 91.7 | | | | | | |
| WSL | 6.0 | | 91.8 | | 91.8 | | 91.8 | | 91.8 | | 91.8 | | 91.9 | | | | | | |
| WSL | 6.0 | | 91.9 | | 91.9 | | 91.9 | | 91.9 | | 91.9 | | | | | | | | |
| CAL1 | 6.0 | | 91.63 | | 29.00 | | 28.10 | | | | | | | | | | | | |
| VEL1 | 6.0 | | | 1.20 | 1.20 | 1.10 | 1.90 | 5.70 | 1.20 | 1.90 | 5.30 | 3.70 | 2.60 | | | | | | |
| VEL1 | 6.0 | 2.80 | 4.20 | 4.20 | 3.40 | 2.50 | 3.20 | 0.10 | | | | | | | | | | | |
| CAL2 | 6.0 | | 91.46 | | 17.00 | | 17.70 | | | | | | | | | | | | |
| VEL2 | 6.0 | | | 0.30 | 0.40 | 0.80 | 1.80 | 3.10 | 0.40 | 1.80 | 4.20 | 2.60 | 2.30 | | | | | | |
| VEL2 | 6.0 | 2.40 | 0.80 | 0.90 | 1.60 | 2.50 | 2.00 | 0.10 | | | | | | | | | | | |
| CAL3 | 6.0 | | 91.36 | | 13.00 | | 12.10 | | | | | | | | | | | | |
| VEL3 | 6.0 | | | 0.10 | 0.10 | 0.10 | 1.50 | 2.30 | 0.20 | 1.30 | 2.30 | 2.40 | 1.40 | | | | | | |
| VEL3 | 6.0 | 1.00 | 0.20 | 0.10 | 0.80 | 0.60 | 0.10 | 0.10 | | | | | | | | | | | |
| XSEC | 7.0 | | 375.0 | 0.0 | | 91.30 | | 0.34780 | | | | | | | | | | | |
| | 7.0 | 0.0 | 95.9 | 3.3 | 95.8 | 4.6 | 95.4 | 4.9 | 92.2 | 5.2 | 91.9 | 6.7 | 91.7 | | | | | | |
| | 7.0 | 8.2 | 91.3 | 9.7 | 91.4 | 11.2 | 91.5 | 12.7 | 92.0 | 14.2 | 91.6 | 15.7 | 91.5 | | | | | | |

| | | | | | | | | | | | | | |
|------|-----|------|-------|------|-------|------|-------|------|------|------|------|------|------|
| | 7.0 | 17.2 | 91.6 | 18.7 | 91.4 | 20.2 | 91.5 | 21.7 | 91.6 | 23.2 | 91.8 | 24.6 | 92.2 |
| | 7.0 | 24.8 | 92.2 | 29.2 | 93.7 | 31.7 | 94.7 | | | | | | |
| NS | 7.0 | | 1.0 | | 1.0 | | 2.0 | | 7.0 | | 7.0 | | 7.0 |
| NS | 7.0 | | 6.0 | | 6.0 | | 6.0 | | 7.0 | | 6.0 | | 6.0 |
| NS | 7.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 |
| NS | 7.0 | | 6.0 | | 2.0 | | 1.0 | | | | | | |
| WSL | 7.0 | | 91.8 | | 91.9 | | 92.0 | | 92.0 | | 92.1 | | 92.1 |
| WSL | 7.0 | | 92.2 | | 92.2 | | 92.2 | | 92.3 | | 92.3 | | 92.3 |
| WSL | 7.0 | | 92.3 | | 92.4 | | 92.4 | | 92.4 | | 92.4 | | 92.4 |
| WSL | 7.0 | | 92.4 | | 92.5 | | 92.5 | | 92.5 | | 92.5 | | 92.5 |
| WSL | 7.0 | | 92.5 | | 92.6 | | 92.6 | | 92.6 | | 92.6 | | 92.6 |
| CAL1 | 7.0 | | 92.34 | | 29.00 | | 31.30 | | | | | | |
| VEL1 | 7.0 | | | | 0.10 | 2.10 | 3.10 | 2.90 | 4.30 | 3.70 | 3.00 | 3.00 | 3.10 |
| VEL1 | 7.0 | 2.50 | 2.20 | 1.90 | 0.50 | 0.40 | 0.10 | | | | | | |
| CAL2 | 7.0 | | 92.22 | | 17.00 | | 19.70 | | | | | | |
| VEL2 | 7.0 | | | | 0.10 | 0.50 | 1.90 | 2.50 | 2.20 | 3.40 | 2.70 | 2.00 | 1.80 |
| VEL2 | 7.0 | 1.70 | 1.60 | 1.60 | 0.10 | 0.30 | 0.10 | | | | | | |
| CAL3 | 7.0 | | 92.12 | | 13.00 | | 15.50 | | | | | | |
| VEL3 | 7.0 | | | | | 0.10 | 0.70 | 2.40 | 0.90 | 3.10 | 2.20 | 1.40 | 1.50 |
| VEL3 | 7.0 | 1.30 | 1.10 | 1.40 | 0.10 | 0.10 | 0.10 | | | | | | |
| ENDJ | | | | | | | | | | | | | |

Big_Timber Study Site 7 - substrate

Export from PHABSIM for Windows

IOC 0000000100010000100000

| | | | | | | | | | | | | | | |
|------|-------|------|-------|------|-------|-------|---------|------|------|------|------|------|------|------|
| QARD | 5.0 | | | | | | | | | | | | | |
| QARD | 10.0 | | | | | | | | | | | | | |
| QARD | 15.0 | | | | | | | | | | | | | |
| QARD | 17.0 | | | | | | | | | | | | | |
| QARD | 20.0 | | | | | | | | | | | | | |
| QARD | 25.0 | | | | | | | | | | | | | |
| QARD | 27.0 | | | | | | | | | | | | | |
| QARD | 30.0 | | | | | | | | | | | | | |
| QARD | 35.0 | | | | | | | | | | | | | |
| QARD | 40.0 | | | | | | | | | | | | | |
| QARD | 45.0 | | | | | | | | | | | | | |
| QARD | 47.0 | | | | | | | | | | | | | |
| QARD | 50.0 | | | | | | | | | | | | | |
| QARD | 55.0 | | | | | | | | | | | | | |
| QARD | 60.0 | | | | | | | | | | | | | |
| QARD | 65.0 | | | | | | | | | | | | | |
| QARD | 70.0 | | | | | | | | | | | | | |
| QARD | 75.0 | | | | | | | | | | | | | |
| QARD | 80.0 | | | | | | | | | | | | | |
| QARD | 85.0 | | | | | | | | | | | | | |
| QARD | 90.0 | | | | | | | | | | | | | |
| QARD | 95.0 | | | | | | | | | | | | | |
| QARD | 100.0 | | | | | | | | | | | | | |
| XSEC | 1.0 | | 0.0 | 1.0 | | 92.70 | 0.01550 | | | | | | | |
| | 1.0 | 0.0 | 96.0 | 8.3 | 95.1 | 8.4 | 94.5 | 8.6 | 94.1 | 9.6 | 93.9 | 10.6 | 94.2 | |
| | 1.0 | 11.6 | 94.0 | 12.6 | 93.9 | 13.6 | 93.7 | 14.6 | 93.5 | 15.6 | 93.3 | 16.6 | 92.8 | |
| | 1.0 | 17.6 | 92.8 | 18.6 | 92.7 | 19.6 | 92.8 | 20.6 | 92.9 | 21.6 | 93.5 | 22.6 | 92.8 | |
| | 1.0 | 23.6 | 92.8 | 24.6 | 93.6 | 25.6 | 93.5 | 26.6 | 93.7 | 27.6 | 93.8 | 28.6 | 94.0 | |
| | 1.0 | 28.8 | 94.9 | 30.3 | 95.9 | 31.8 | 96.0 | | | | | | | |
| NS | 1.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | | 6.0 | |
| NS | 1.0 | | 6.0 | | 6.0 | | 8.0 | | 8.0 | | 8.0 | | 8.0 | |
| NS | 1.0 | | 8.0 | | 8.0 | | 8.0 | | 8.0 | | 8.0 | | 8.0 | |
| NS | 1.0 | | 8.0 | | 8.0 | | 8.0 | | 6.0 | | 6.0 | | 6.0 | |
| NS | 1.0 | | 6.0 | | 6.0 | | 6.0 | | | | | | | |
| WSL | 1.0 | | 93.9 | | 94.1 | | 94.2 | | 94.2 | | 94.3 | | 94.3 | |
| WSL | 1.0 | | 94.4 | | 94.4 | | 94.4 | | 94.5 | | 94.5 | | 94.6 | |
| WSL | 1.0 | | 94.6 | | 94.6 | | 94.7 | | 94.7 | | 94.7 | | 94.7 | |
| WSL | 1.0 | | 94.8 | | 94.8 | | 94.8 | | 94.8 | | 94.9 | | | |
| CAL1 | 1.0 | | 94.56 | | 47.00 | | 54.20 | | | | | | | |
| VEL1 | 1.0 | | | | 0.10 | 0.60 | 0.60 | 0.80 | 0.90 | 1.40 | 1.80 | 2.50 | 3.10 | |
| VEL1 | 1.0 | 3.30 | 3.00 | 2.70 | 3.00 | 4.00 | 2.40 | 2.50 | 2.90 | 1.40 | 1.70 | 0.80 | 0.10 | |
| VEL1 | 1.0 | | | | | | | | | | | | | |
| CAL2 | 1.0 | | 94.35 | | 27.00 | | 31.20 | | | | | | | |
| VEL2 | 1.0 | | | | 0.10 | 0.10 | 0.30 | 0.40 | 0.50 | 0.70 | 0.60 | 1.10 | 1.30 | 1.70 |
| VEL2 | 1.0 | 1.80 | 2.30 | 2.50 | 3.00 | 2.90 | 2.10 | 1.60 | 1.50 | 0.90 | 0.70 | 0.10 | 0.10 | |
| VEL2 | 1.0 | | | | | | | | | | | | | |

| | | | | | | | | | | | | | |
|------|-----|--------|-------|-------|---------|------|-------|------|-------|------|------|------|------|
| CAL3 | 1.0 | 94.21 | 17.00 | 18.10 | | | | | | | | | |
| VEL3 | 1.0 | | | | | 0.10 | 0.30 | 0.60 | 0.80 | 0.90 | 1.00 | | |
| VEL3 | 1.0 | 1.30 | 1.50 | 0.80 | 1.90 | 2.00 | 1.50 | 1.30 | 1.00 | 0.70 | 0.10 | 0.10 | |
| VEL3 | 1.0 | | | | | | | | | | | | |
| XSEC | 2.0 | 310.0 | 1.0 | 94.10 | 0.26500 | | | | | | | | |
| | 2.0 | 0.0 | 97.2 | 8.3 | 95.8 | 9.0 | 95.3 | 9.9 | 95.4 | 10.0 | 95.2 | 11.5 | 94.7 |
| | 2.0 | 13.0 | 94.4 | 14.5 | 94.8 | 16.0 | 94.7 | 17.5 | 94.8 | 19.0 | 94.5 | 20.5 | 94.9 |
| | 2.0 | 22.0 | 94.4 | 23.5 | 94.5 | 25.0 | 94.3 | 26.5 | 94.1 | 28.0 | 94.4 | 29.5 | 94.6 |
| | 2.0 | 31.0 | 94.8 | 32.5 | 94.8 | 34.0 | 95.0 | 35.5 | 95.1 | 37.8 | 95.4 | 38.5 | 95.6 |
| | 2.0 | 40.3 | 97.3 | 42.6 | 97.3 | | | | | | | | |
| NS | 2.0 | 6.0 | 6.0 | 1.5 | 6.0 | 1.0 | 6.0 | 1.0 | 6.0 | 1.0 | 6.0 | | |
| NS | 2.0 | 6.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | |
| NS | 2.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | |
| NS | 2.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 3.0 | 1.0 | | |
| NS | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | |
| WSL | 2.0 | 94.9 | 95.1 | 95.1 | 95.1 | 95.1 | 95.2 | 95.2 | 95.2 | 95.2 | 95.3 | | |
| WSL | 2.0 | 95.3 | 95.3 | 95.3 | 95.3 | 95.3 | 95.4 | 95.4 | 95.4 | 95.4 | 95.4 | | |
| WSL | 2.0 | 95.4 | 95.5 | 95.5 | 95.5 | 95.5 | 95.5 | 95.5 | 95.5 | 95.5 | 95.5 | | |
| WSL | 2.0 | 95.6 | 95.6 | 95.6 | 95.6 | 95.6 | 95.6 | 95.6 | 95.6 | 95.6 | 95.6 | | |
| CAL1 | 2.0 | 95.41 | 47.00 | 53.30 | | | | | | | | | |
| VEL1 | 2.0 | | 0.10 | 0.60 | 0.60 | 3.20 | 1.40 | 2.40 | 4.00 | 4.20 | 3.70 | | |
| VEL1 | 2.0 | 2.50 | 3.30 | 3.10 | 3.30 | 2.40 | 3.00 | 2.30 | 2.20 | 1.80 | 1.00 | 0.10 | |
| VEL1 | 2.0 | | | | | | | | | | | | |
| CAL2 | 2.0 | 95.27 | 27.00 | 33.00 | | | | | | | | | |
| VEL2 | 2.0 | | 0.10 | 0.10 | 0.10 | 2.60 | 0.80 | 2.20 | 3.10 | 2.80 | 3.50 | | |
| VEL2 | 2.0 | 2.50 | 2.20 | 2.20 | 2.90 | 1.60 | 2.60 | 1.70 | 1.30 | 1.70 | 0.80 | 0.10 | |
| VEL2 | 2.0 | | | | | | | | | | | | |
| CAL3 | 2.0 | 95.17 | 17.00 | 20.30 | | | | | | | | | |
| VEL3 | 2.0 | | 0.10 | 0.60 | 0.30 | 1.70 | 1.70 | 2.20 | 2.10 | | | | |
| VEL3 | 2.0 | 1.30 | 1.60 | 1.90 | 2.00 | 1.40 | 1.40 | 1.00 | 1.10 | 0.10 | | | |
| VEL3 | 2.0 | | | | | | | | | | | | |
| XSEC | 3.0 | 560.0 | 1.0 | 95.00 | 0.00250 | | | | | | | | |
| | 3.0 | 0.0 | 98.8 | 7.7 | 96.6 | 8.5 | 96.4 | 9.5 | 96.0 | 11.5 | 95.7 | 13.5 | 95.7 |
| | 3.0 | 15.5 | 95.7 | 17.5 | 95.6 | 19.5 | 95.6 | 21.5 | 95.4 | 23.5 | 95.4 | 25.5 | 95.9 |
| | 3.0 | 27.5 | 95.8 | 29.5 | 95.7 | 31.5 | 95.5 | 33.5 | 95.0 | 35.5 | 95.6 | 37.5 | 95.4 |
| | 3.0 | 39.5 | 95.4 | 41.5 | 95.5 | 43.6 | 95.7 | 46.6 | 100.2 | | | | |
| NS | 3.0 | 8.0 | 6.0 | 6.0 | 6.0 | 6.0 | 8.0 | 6.0 | 6.0 | 6.0 | 1.0 | | |
| NS | 3.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | |
| NS | 3.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | |
| NS | 3.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 2.0 | | | | | | |
| WSL | 3.0 | 95.8 | 95.9 | 96.0 | 96.0 | 96.1 | 96.1 | 96.1 | 96.1 | 96.1 | 96.2 | | |
| WSL | 3.0 | 96.2 | 96.2 | 96.3 | 96.3 | 96.3 | 96.3 | 96.3 | 96.3 | 96.3 | 96.4 | | |
| WSL | 3.0 | 96.4 | 96.4 | 96.4 | 96.4 | 96.4 | 96.5 | 96.5 | 96.5 | 96.5 | 96.5 | | |
| WSL | 3.0 | 96.5 | 96.5 | 96.6 | 96.6 | 96.6 | 96.6 | 96.6 | 96.6 | 96.6 | 96.6 | | |
| CAL1 | 3.0 | 96.36 | 47.00 | 48.40 | | | | | | | | | |
| VEL1 | 3.0 | | 0.10 | 0.30 | 2.50 | 3.00 | 3.50 | 3.30 | 2.80 | 2.10 | 1.50 | 1.20 | |
| VEL1 | 3.0 | 1.60 | 1.70 | 1.60 | 1.50 | 1.30 | 1.20 | 1.20 | 0.90 | 1.60 | | | |
| CAL2 | 3.0 | 96.16 | 27.00 | 27.90 | | | | | | | | | |
| VEL2 | 3.0 | | 0.10 | 0.20 | 1.40 | 2.30 | 3.20 | 2.90 | 2.40 | 1.80 | 1.30 | 1.10 | |
| VEL2 | 3.0 | 1.00 | 1.20 | 0.80 | 1.00 | 1.10 | 1.10 | 1.10 | 1.00 | 1.10 | | | |
| CAL3 | 3.0 | 96.09 | 17.00 | 21.00 | | | | | | | | | |
| VEL3 | 3.0 | | 0.10 | 1.00 | 1.70 | 2.10 | 2.10 | 2.30 | 1.70 | 1.30 | 0.80 | | |
| VEL3 | 3.0 | 0.60 | 0.50 | 0.50 | 0.60 | 1.10 | 1.00 | 1.00 | 1.00 | 0.70 | | | |
| XSEC | 4.0 | 1.0 | 0.5 | 95.00 | 0.01250 | | | | | | | | |
| | 4.0 | 0.0100 | 11.1 | 97.3 | 12.3 | 96.7 | 13.5 | 96.4 | 13.9 | 96.3 | 15.9 | 96.2 | |
| | 4.0 | 17.9 | 95.9 | 19.9 | 95.7 | 21.9 | 95.4 | 23.9 | 95.4 | 25.9 | 95.6 | 27.9 | 95.9 |
| | 4.0 | 28.9 | 95.9 | 30.9 | 95.4 | 32.9 | 94.9 | 34.9 | 94.6 | 36.9 | 94.4 | 38.9 | 94.8 |
| | 4.0 | 40.9 | 94.5 | 42.9 | 94.5 | 44.9 | 95.3 | 46.9 | 95.9 | 47.7 | 96.4 | 48.7 | 96.6 |
| | 4.0 | 51.4 | 97.6 | 52.2 | 97.6 | 55.2 | 100.0 | 56.6 | 100.1 | | | | |
| NS | 4.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 1.0 | 8.0 | | |
| NS | 4.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | |
| NS | 4.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | |
| NS | 4.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | | |
| NS | 4.0 | 5.0 | 7.0 | 2.0 | 1.0 | | | | | | | | |
| WSL | 4.0 | 95.8 | 96.0 | 96.1 | 96.1 | 96.1 | 96.1 | 96.1 | 96.1 | 96.1 | 96.2 | | |
| WSL | 4.0 | 96.2 | 96.2 | 96.3 | 96.3 | 96.3 | 96.3 | 96.3 | 96.4 | 96.4 | 96.4 | | |
| WSL | 4.0 | 96.4 | 96.4 | 96.4 | 96.5 | 96.5 | 96.5 | 96.5 | 96.5 | 96.5 | 96.6 | | |
| WSL | 4.0 | 96.6 | 96.6 | 96.6 | 96.6 | 96.6 | 96.7 | 96.7 | 96.7 | 96.7 | 96.7 | | |
| CAL1 | 4.0 | 96.38 | 47.00 | 46.10 | | | | | | | | | |
| VEL1 | 4.0 | | 0.10 | 0.10 | 1.40 | 3.30 | 3.70 | 3.60 | 3.10 | 2.00 | 1.80 | | |

| | | | | | | | | | | | | | |
|------|-----|-------|-------|-------|-------|-------|---------|------|------|------|------|------|------|
| VEL1 | 4.0 | 1.30 | 0.10 | 0.30 | 0.70 | 2.70 | 0.80 | 0.20 | 0.90 | 0.30 | 0.70 | 0.10 | |
| VEL1 | 4.0 | | | | | | | | | | | | |
| CAL2 | 4.0 | 96.17 | | 27.00 | | 27.00 | | | | | | | |
| VEL2 | 4.0 | | | 0.10 | 0.10 | 1.10 | 2.40 | 3.70 | 3.10 | 2.50 | 1.90 | 1.30 | |
| VEL2 | 4.0 | 1.00 | 0.10 | 0.10 | 0.60 | 1.90 | 0.20 | 0.20 | 0.50 | 0.10 | 0.10 | | |
| VEL2 | 4.0 | | | | | | | | | | | | |
| CAL3 | 4.0 | 96.14 | | 17.00 | | 19.10 | | | | | | | |
| VEL3 | 4.0 | | | | | 0.10 | 1.60 | 2.30 | 2.50 | 2.30 | 1.50 | 1.00 | |
| VEL3 | 4.0 | 0.70 | 0.10 | 0.10 | 0.20 | 1.10 | 0.10 | 0.10 | 0.40 | 0.10 | | | |
| VEL3 | 4.0 | | | | | | | | | | | | |
| XSEC | 5.0 | 130.0 | 0.0 | | 94.60 | | 0.01250 | | | | | | |
| | 5.0 | 0.0 | 97.9 | 5.3 | 97.1 | 8.5 | 96.3 | 8.8 | 96.6 | 11.5 | 97.9 | 12.9 | 97.6 |
| | 5.0 | 15.9 | 98.3 | 17.7 | 95.4 | 19.4 | 94.9 | 23.4 | 95.4 | 24.2 | 94.9 | 24.5 | 94.8 |
| | 5.0 | 25.7 | 94.6 | 26.3 | 97.1 | 27.9 | 96.8 | 28.3 | 96.8 | 34.3 | 96.8 | 35.2 | 97.9 |
| | 5.0 | 41.3 | 100.2 | | | | | | | | | | |
| NS | 5.0 | | 6.0 | | 6.0 | 1.0 | 6.0 | 1.0 | 8.0 | | 8.0 | | 8.0 |
| NS | 5.0 | | 8.0 | | 8.0 | | 8.0 | | 8.0 | | 8.0 | | 8.0 |
| NS | 5.0 | | 8.0 | | 8.0 | 1.0 | 8.0 | 1.0 | 6.0 | 1.0 | 6.0 | 1.0 | 6.0 |
| NS | 5.0 | | 8.0 | | | | | | | | | | |
| WSL | 5.0 | 95.9 | | 96.1 | | 96.3 | | 96.4 | | 96.4 | | 96.5 | |
| WSL | 5.0 | 96.6 | | 96.6 | | 96.7 | | 96.8 | | 96.8 | | 96.9 | |
| WSL | 5.0 | 96.9 | | 96.9 | | 97.0 | | 97.0 | | 97.1 | | 97.1 | |
| WSL | 5.0 | 97.2 | | 97.2 | | 97.2 | | 97.3 | | 97.3 | | | |
| CAL1 | 5.0 | 96.86 | | 47.00 | | 43.30 | | | | | | | |
| VEL1 | 5.0 | | | | | | | 2.80 | 6.20 | 0.10 | 6.20 | 5.60 | |
| VEL1 | 5.0 | 4.50 | | | | | | | | | | | |
| CAL2 | 5.0 | 96.55 | | 27.00 | | 37.60 | | | | | | | |
| VEL2 | 5.0 | | | | | | | 0.10 | 4.30 | 0.10 | 5.90 | 5.00 | |
| VEL2 | 5.0 | 0.90 | | | | | | | | | | | |
| CAL3 | 5.0 | 96.36 | | 17.00 | | 11.30 | | | | | | | |
| VEL3 | 5.0 | | | | | | | 0.10 | 0.80 | 0.10 | 1.60 | 2.40 | |
| VEL3 | 5.0 | 0.60 | | | | | | | | | | | |
| ENDJ | | | | | | | | | | | | | |