PNNL-13359 WTP-RPT-004, Rev. 0 (Formerly BNFL-RPT-040)



Rheological Studies on Pretreated Feed and Melter Feed from C-104 and AZ-102

P. R. Bredt L. K. Jagoda D. E. Rinehart

January 2001



Prepared for the U.S. Department of Energy under Contract DE-AC06-76RL01830

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor Battelle Memorial Institute, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof, or Battelle Memorial Institute. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

PACIFIC NORTHWEST NATIONAL LABORATORY operated by BATTELLE for the UNITED STATES DEPARTMENT OF ENERGY under Contract DE-AC06-76RL01830

Printed in the United States of America

Available to DOE and DOE contractors from the Office of Scientific and Technical Information, P.O. Box 62, Oak Ridge, TN 37831-0062; ph: (865) 576-8401 fax: (865) 576-5728 email: reports@adonis.osti.gov

Available to the public from the National Technical Information Service, U.S. Department of Commerce, 5285 Port Royal Rd., Springfield, VA 22161 ph: (800) 553-6847 fax: (703) 605-6900 email: orders@ntis.fedworld.gov online ordering: http://www.ntis.gov/ordering.htm

 $\widetilde{\mathbb{C}}$ This document was printed on recycled paper.

PNNL-13359 WTP-RPT-004, Rev. 0 (Formerly BNFL-RPT-040)

Rheological Studies on Pretreated Feed and Melter Feed from C-104 and AZ-102

P. R. Bredt L. K. Jagoda D. E. Rinehart

January 2001

Prepared for CH2M Hill Hanford Group under Project Number 41503

Pacific Northwest National Laboratory Richland, Washington 99352

Summary

Rheological and physical properties testing was conducted on actual AZ-102 and C-104 melter feed samples prior to the addition of glass formers and secondary waste products. Analyses were repeated on the C-104 samples following the addition of simulated Sr/TRU secondary waste. Analyses were repeated again following addition of glass formers to both AZ-102 and C-104 samples. Samples from both feeds were tested at the target solids concentrations of 5, 15, and 25 wt\%^1 . This data on actual waste is required to validate and qualify results obtained with simulants.

The AZ-102 feed was received for this task after washing and leaching. The AZ-102 feed contained 9.54 wt% solids. At this solids concentration, no standing liquid was observed in the AZ-102 feed. The C-104 feed was also received following washing and leaching. The AZ-102 feed contained 20 wt% solids and contained roughly 15 vol% standing liquid.

The initial AZ-102 and C-104 feeds displayed very different rheological properties. The initial 5 and 15 wt% C-104 feeds displayed near Newtonian behavior, and the 25 feed has a small yield stress of ~5 Pa giving it a slight Bingham Plastic component. The viscosity of the feeds at 33 s⁻¹ were 9.8, 15, and 160 cP for the 5, 15, and 25 wt% feeds respectively with very little if any thixotropic behavior. By comparison, the AZ-102 feed showed much higher initial viscosities of 12, 530, 900, and 4600 cP for the 5, 15, 20, and 25 wt% feeds. In addition, the AZ-102 feeds displayed significant irreversible shear thinning. Surprisingly, no significant temperature effects were seen for the C-104 or AZ-102 samples measured at 25 and 50°C.

Very little change in rheological properties was observed following secondary waste product and glass former addition to the C-104 feed while the yield and viscosity the AZ-102 feed dropped following glass former and secondary waste addition. Since the addition of dry glass formers to the AZ-102 feed should have increased the total solids load, it would have been expected to see an increase the rheological properties. The observed decrease is most likely the result of the irreversible shear thinning of the AZ-102 samples as the testing progressed.

A mixing and aging study was conducted on the 15 wt% AZ-102 and 25 wt% C-104 feeds following glass former and secondary waste product additions. The additions were made and the slurries were stirred at a rate that delivered the same energy per volume as expected in the River Protection Project Waste Treatment Plant flow sheet. Slurries were stirred at this rate for one week. The rheology of the mixed slurries were examined at 1 hr, 1 day and 1 week. The yield and viscosity of the AZ-102 slurry decreased over the one week mixing period consistent with the previous observations of irreversible shear thinning in this slurry. By contrast the yield and viscosity of the C-104 slurry increased over the one week. Over this same period, the viscosity of the C-104 slurry increased from 910 cP to 1700 cP at 33s⁻¹.

Following the mixing study, the 15 wt% AZ-102 and 25 wt% C-104 slurries were allowed to settle for one week. The AZ-102 sample contained standing liquid, which was removed, while the C-104 sample contained no standing liquid. The rheology of the settled solids were then examined. The yield and viscosity of the AZ-102 settled solids were higher than similar testing after one week of mixing. This increase was expected and attributed to increased solids loading

¹ In this report, wt% solids are based on residual mass after 24 hours at 105°C.

resulting from removal of the standing liquid. The viscosity of the C-104 settled material was similar to the results after one week of mixing, but the yield increased to approximately 80 Pa.

The results of the mixing and aging studies suggest that while the AZ-102 initial feed and final melter feed material may be very difficult to mix and transport, irreversible shear thinning significantly reduces the yield and viscosity. Therefore, exposing this material to some initial shearing may be an option for reducing these critical transport properties. By contrast, the yield and viscosity of the initial C-104 material did not display significant irreversible shear thinning. The yield and viscosity of the C-104 melter feed increased with mixing and the yield increased further with aging. These results suggest the final C-104 melter feed could be very difficult to mix and transport on a 25 wt% basis.

Table of Contents

1.0	Introduction	1.1
2.0	Experimental Approach	2.1
2.1	Simulated Secondary Waste Products	2.1
2.1.1 Cs Eluant Simulant		2.1
2.	.1.2 Sr/TRU Precipitate Simulant	2.3
2.2	Evaporation and Settling Study	2.5
2.3	Shear Stress Versus Shear Rate Analysis (Rheology)	2.8
2.4	Mixing and Aging Study	2.9
3.0	Experimental Results	3.1
3.1	Density and Settling Study	3.1
3.2	Rheology	3.21
3.	.2.1 Rheology of Evaporated Feed Samples	3.21
3.	.2.2 Rheology of Melter Feed with Secondary Waste Products	3.24
3.2.3 Rheology of Melter Feed with Glass Formers		3.27
3.3	AZ-102 Mixing and Aging Study	3.30
3.4	C-104 Mixing and Aging Study	3.33
4.0	Conclusions	4.1
5.0	References	5.1
Appendix A: Test Plans		A.1
Appen	dix B: Rheograms	B.1
Appen	dix C: Test Instruction	C.1

Figures

Figure 3.1. Volume Percent Settled Solids Versus Time for AZ-102 Evaporated Feed	
Using a Linear Scale	3.5
Figure 3.2. Volume Percent Settled Solids Versus Time for AZ-102 Evaporated Feed	
Using a Semi-Log Scale	3.6
Figure 3.3. Settling Rates for AZ-102 Evaporated Feed	3.8
Figure 3.4. Volume Percent Settled Solids Versus Time for AZ-102 Evaporated Feed	
With Glass Formers Using a Linear Scale	3.9
Figure 3.5 Volume Percent Settled Solids Versus Time for AZ-102 Evaporated Feed	
With Glass Formers Using a Semi-Log Scale	3.10
Figure 3.6. Settling Rates for AZ-102 Evaporated Feed with Glass Formers	3.11
Figure 3.7. Volume Percent Settled Solids Versus Time for C-104 Evaporated Feed	
Using a Linear Scale	3.12
Figure 3.8. Volume Percent Settled Solids Versus Time for C-104 Evaporated Feed	
Using a Semi-Log Scale	3.13
Figure 3.9. Settling Rates for C-104 Evaporated Feed	3.14
Figure 3.10. Volume Percent Settled Solids Versus Time for C-104 Evaporated Feed	
With Secondary Waste Using a Linear Scale	3.15
Figure 3.11. Volume Percent Settled Solids Versus Time for C-104 Evaporated Feed	
With Secondary Waste Using a Semi-Log Scale	3.16
Figure 3.12. Settling Rates for C-104 Evaporated Feed With Secondary Waste Products	3.17
Figure 3.13. Volume Percent Settled Solids Versus Time for C-104 Evaporated Feed	
With Secondary Waste and Glass Formers Using a Linear Scale	3.18
Figure 3.14. Volume Percent Settled Solids Versus Time for C-104 Evaporated Feed	
With Secondary Waste and Glass Formers Using a Semi-Log Scale	3.19
Figure 3.15. Settling Rates for C-104 Evaporated Feed With Secondary Waste Products	
and Glass Formers	3.20
Figure 3.16. Rheograms for C-104 Initial Evaporated Feeds at 25°C	3.22
Figure 3.17. Rheograms for AZ-102 Initial Feeds at 25°C	3.26
Figure 3.18. Comparison of C-104 25 wt% Feed Initial Alone, With Secondary Waste	
and With Glass Formers and Secondary Waste at 25°C	3.28
Figure 3.19. Comparison of AZ-102 15 wt% Feed Alone and With Glass Former at 25°C.	3.29
Figure 3.20. Rheograms for AZ-102 15 wt% Mixing Study, Measurement Performed at	
25°C	3.31
Figure 3.21. Rheograms for AZ-102 15 wt% Aging Study Measurements Performed at	
25°C	3.32
Figure 3.22. Rheograms for C-104 15 wt% Mixing Study Measurement Performed at	
25°C	3.34
Figure 3.23. Rheograms for C-104 25 wt% Aging Study Measurement Performed at	
25°C	3.35

Tables

Table 2.1. Co	mponents in Evaporated Cs Eluant Simulant	2.2
Table 2.2. De	ensity Measurements for Simulant Solution	2.3
Table 2.3 Con	npositional Data on AN-107 Filtrate Simulant	2.4
Table 2.4. Sr/	TRU Precipitate Simulant ICP Results for Dried Solids from Subsamples	
SI	M-05 and SM-06. Results Are in µg/g of Dried Solids.	2.5
Table 2.5. Ma	ass of Samples and Secondary Waste Products For C-104 Tests	2.7
Table 2.6. Ma	ass of Samples and Glass Formers in Grams Added to AZ-102 Samples.	
Sa	ample 15 wt%-2 Was Used for Mixing and Aging Study	2.7
Table 2.7. Ma	ass of Samples and Glass Formers Added to C-104 Samples	2.8
Table 3.1. De	nsity of AN-107 and AW-101 Samples at 25°C and 50°C With and	
W	/ithout Addition of Glass Formers in g/ml	3.2
Table 3.2. Vo	Plume Percent Settles Solids for the AZ-102 Samples	3.3
Table 3.3. Vis	scosity Data for Evaporated Feeds	3.23
Table 3.4. Vis	scosity Data (cP) for C-104 with Secondary Waste	3.25
Table 3.5. Vis	scosity Data for Evaporated Feeds with Secondary Waste and Glass	
Fo	ormers	3.27
Table 3.6. Vis	scosity Data for AZ-102 Mixing and Aging Study Measured at 25°C	3.30
Table 3.7. Vis	scosity Data for C-104 Mixing and Aging Study Measured at 25°C	3.33