

DEFECT ASSESSMENT METHODS
PRCI Project No. PR-218-05404

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DEFECTS THAT COULD AFFECT PIPELINE INTEGRITY

- Corrosion-caused metal loss
- Longitudinally-oriented cracks
- Circumferentially-oriented corrosion
- Circumferentially-oriented cracks
- Dents
- Dents with reduced wall & damage



METHODS USED TO EVALUATE FLAWS IN PIPELINES

Corrosion-Caused Metal Loss

ASME B31G	Modified B31G
RSTRENG	KAPA
PCORR	COR-LAS™
PAFFC	API RP 579
DNV RP F-101	

Cracks (axial)

SURFFLAW	KAPA
COR-LAS™	PAFFC
API RP 579	BS 7910

Cracks and Blunt Flaws (circumferential)

API STD. 1104, Appendix A
CSA Z662, Appendix K
API RP 579
BS 7910



METHODS USED TO EVALUATE FLAWS IN PIPELINES

Plane Dents

API Publication 1156

B31.8

API 579

PRCI PR-218-9405 Fatigue Rating Shallow Unrestrained Dents

PRCI PR-218-9822 Guidelines for the Assessment of Dents on Welds

Dents with Gouges

API 579

Dent-Gouge Fracture Model (EPRG)

Patch to Ductile Flaw Growth Model (PRCI-Battelle)

Empirical Q-factor Model (PRCI)



STATUS OF MODELS FOR EVALUATING CORROSION-CAUSE METAL LOSS

- Mature technology
- Most of the models are based on Maxey's Surface Flaw Equation
- Comparisons show that the models give similar predictions and all have been validated against PRCI's Database of Corroded Pipe Tests
 - Any of the models can be used with confidence, but ASME B31G tends to give excessively conservative predictions
- Further research is being carried out to better address multiple defect interaction and varying axial stress
- Little or no need to pursue this in the future



STATUS OF MODELS FOR EVALUATING AXIAL CRACKS

- Log-secant equation (a.k.a. NG-18 surface flaw equation) is empirically based
 - Can be used without the need for special software and utilizes Charpy energy (upper shelf) to represent material toughness.
- PAFFC and CorLas™ are based on J-integral and tearing modulus theory.
 - Can use Charpy energy correlations for toughness.
 - Are implement in software packages.
- API RP 579 Level II and BS 7910 methodologies are based on the FAD methodology.
 - Can be used without special software and can accommodate toughness based on Charpy energy.



STATUS OF MODELS FOR EVALUATING AXIAL CRACKS CONTINUED

- These models have been validated against PRCI full-scale test results and other data.
- Comparisons show that the models give similar predictions.
 - Log-sec equation tends to give excessively conservative predictions for flaws with depth/thickness ratios less than 0.3.
- Further research is being carried out to develop a “new” model for axial cracks.
- The weak link in fracture mechanics based models are fracture toughness correlations.
- The existing methods work well, so further effort beyond the on-going work on a new model is probably not necessary.



STATUS OF MODELS FOR EVALUATING ROCK DENTS AND PLAIN DENTS

- API 579 has dent radius criteria
 - requires radius $> 15 \times$ remaining wall
- B31.8
 - Maximum strain $< 6\%$ (4% in ductile welds) calculated from curvature
- Calculation based on caliper or in the ditch readings
 - Kiefner methodology – trace & compare
- Need to better understand the effect of length and membrane strain on fatigue life



STATUS OF MODELS FOR EVALUATING DENTS WITH METAL LOSS OR CRACKS

- ASME B31.8 –
 - Evaluate dent and metal loss independently
 - Grind out cracks
 - Not ideal, needs validation
- Dent & Gouge Fracture Model
 - Conservative
 - Requires high toughness
 - Curvature limited to $>5t$
 - Length not included
- API 579 Level 2
 - Uses Q factor
 - Limits cyclic stresses
- Q Factor – not recommended
- R&D overlaps mechanical damage (dents with gouges)



STATUS OF MODELS FOR EVALUATING DENTS WITH GOUGES

- The current dent-gouge fracture model results in better predictions if the depth of cracking from re-rounding of the dent is added to the gouge depth in the model.
- Patch to ductile flaw growth model has not been codified or fully validated.
- The empirical Q-factor model is not recommended.

STATUS OF MODELS FOR EVALUATING DENTS WITH GOUGES CONTINUED

- This area is the focus of much current research:
 - Dent and Gouge Fracture Model (FAD) approach is being extended by AF&A with KAI (improved burst test prediction) and Advantica (time dependent model)
 - Patch to the Ductile Flaw Growth Model will be extended by Battelle (time dependent model)

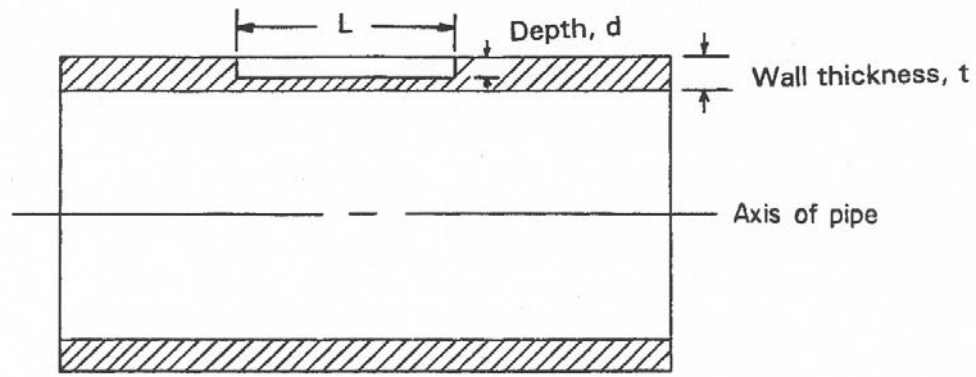


STATUS OF MODELS FOR EVALUATING DENTS AND DENTS WITH GOUGES CONT.

- Further FEM & full scale testing research is being carried out to validate a range of models for fabricated gouges and dents.
 - Most existing test data on gouge and dent defects may not simulate the behavior of real gouges and dents.
 - Are a starting point for dents with gouge damage, but there is still a need for more realistic mechanical damage.
- Consideration should be given to developing a *realistic* mechanical damage test method to validate new and existing models.

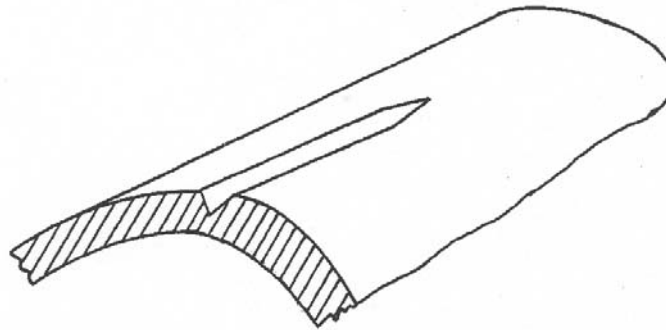
Questions?



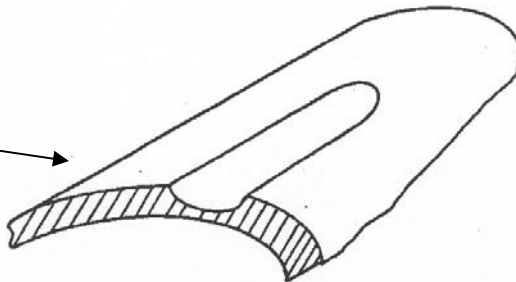


SURFACE FLAW

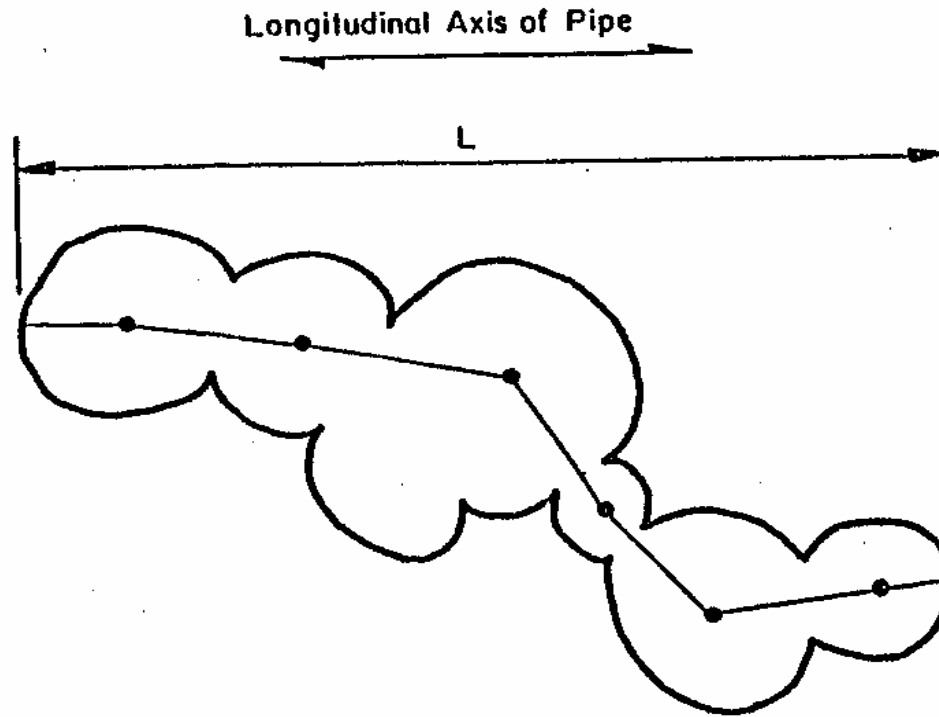
Sharp
Flaw



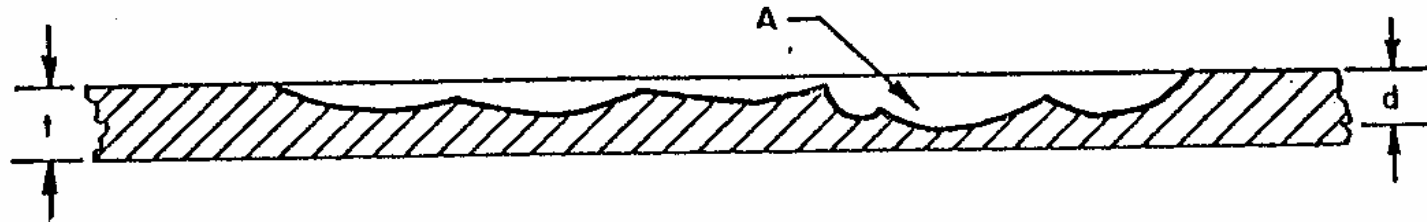
Blunt
Flaw



**Kie
& Associates**
incorporated



Length and depth determination



Maxey's Surface Flaw Equation

$$S = S_o \left[\frac{1 - A/A_o}{1 - (A/A_o)(1/M)} \right]$$

$A = Ld$ (for a rectangular defect)

$$A_o = Lt$$

$$M = \sqrt{1 + \frac{0.8L^2}{Dt}}$$

API RP 579 Level II Assessment Failure Assessment Diagram Approach

Failure Assessment Diagram (FAD)

