



**OAK RIDGE
NATIONAL
LABORATORY**



**An Extension of the Validation
of SCALE (SAS2H)
Isotopic Predictions
for PWR Spent Fuel**

**M. D. DeHart
O. W. Hermann**

MANAGED AND OPERATED BY
LOCKHEED MARTIN ENERGY RESEARCH CORPORATION
FOR THE UNITED STATES
DEPARTMENT OF ENERGY

This report has been reproduced directly from the best available copy.

Available to DOE and DOE contractors from the Office of Scientific and Technical Information, P.O. Box 62, Oak Ridge, TN 37831; prices available from (615) 576-8401, FTS 626-8401.

Available to the public from the National Technical Information Service, U.S. Department of Commerce, 5285 Port Royal Rd., Springfield, VA 22161.

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

Computational Physics and Engineering Division

**AN EXTENSION OF THE VALIDATION OF SCALE (SAS2H)
ISOTOPIC PREDICTIONS FOR PWR SPENT FUEL**

M. D. DeHart and O. W. Hermann

Date Published: September 1996

Prepared for
Sandia National Laboratories
under subcontract AD-4072 with Oak Ridge National Laboratory

Prepared by the
OAK RIDGE NATIONAL LABORATORY
managed by
LOCKHEED MARTIN ENERGY RESEARCH CORP.
for the
U.S. DEPARTMENT OF ENERGY
under contract DE-AC05-96OR22464

CONTENTS

	<u>Page</u>
LIST OF FIGURES	iv
LIST OF TABLES	v
ABSTRACT	vii
ACKNOWLEDGMENTS	ix
1 INTRODUCTION	1
2 DEVELOPMENT OF FUEL ASSEMBLY MODELS FOR DEPLETION ANALYSES ..	4
2.1 TRINO VERCELLES PWR SPENT FUEL DEPLETION MODELS	4
2.2 TURKEY POINT UNIT 3 SPENT FUEL DEPLETION MODELS	14
3 PREDICTED AND MEASURED ISOTOPIC COMPOSITIONS	20
3.1 TRINO VERCELLES PWR ISOTOPIC RESULTS	20
3.2 TURKEY POINT UNIT 3 PWR ISOTOPIC RESULTS	23
3.3 SUMMARY OF COMBINED ISOTOPIC RESULTS	23
4 STATISTICAL COMBINATION OF MEASURED-TO-COMPUTED ISOTOPIC RATIOS	36
5 SUMMARY	40
6 REFERENCES	43
APPENDIX A. DESCRIPTION OF THE SCALE SAS2H DEPLETION APPROACH	47
APPENDIX B. INPUT LISTINGS FOR TRINO VERCELLES SAS2H DEPLETION CALCULATION	53
APPENDIX C. SAMPLE INPUT FOR A TURKEY POINT UNIT 3 SAS2H DEPLETION CALCULATION	81
APPENDIX D. MEASURED AND COMPUTED ISOTOPIC CONCENTRATIONS FOR TRINO VERCELLES FUEL SAMPLES	91
APPENDIX E. MEASURED AND COMPUTED ISOTOPIC CONCENTRATIONS FOR TURKEY POINT UNIT 3 FUEL SAMPLES	101
APPENDIX F. EFFECT OF INCORRECT ABSORBER SPECIFICATION FOR TRINO VERCELLES CALCULATIONS	105

LIST OF FIGURES

<u>Figure</u>	<u>Page</u>
1 Core, assembly, and sample fuel pin configurations for Trino Vercelles	6
2 One-dimensional assembly approximation for Trino Vercelles assemblies	12
3 15 × 15 assembly configuration for Turkey Point Unit 3 PWR	19
4 Percentage difference between measured and calculated results (27BURNUPLIB)	30
5 Percentage difference between measured and calculated results (44GROUPNDF5)	31
6 Combined results for earlier and current validation analyses (27BURNUPLIB)	34
7 Combined results for earlier and current validation analyses (44GROUPNDF5)	35
A.1 Flow path invoked in SAS2H depletion and decay sequences	49

LIST OF TABLES

<u>Table</u>	<u>Page</u>
1 Basic parameters of the measured spent fuel	5
2 Design data for Trino Vercelles square fuel assemblies	8
3 Design data for Trino Vercelles cruciform fuel and control rod assemblies	9
4 Initial composition of Trino Vercelles fuel assemblies	9
5 Summary of general operations of cycles 1 and 2	10
6 Effective dimensions determined for 1-D SAS2H assembly model	12
7 Axially dependent effective fuel and water temperature and water densities	13
8 Fuel burnup and operating power histories for Trino Vercelles PWR pellet samples	15
9 Turkey Point Unit 3 PWR assembly and operating data	16
10 Initial composition of Turkey Point fuel assemblies	16
11 Turkey Point Unit 3 operating history of assemblies D01 and D04	18
12 Turkey Point pellet sample data	18
13 Average measured irradiation composition of Trino Vercelles PWR fuel	21
14 Percentage difference between measured and computed nuclide compositions for Trino Vercelles PWR samples and averages (27BURNUPLIB library)	24
15 Percentage difference between measured and computed nuclide compositions for Trino Vercelles PWR samples and averages (44GROUPNDF5 library)	25
16 Measured irradiation composition of Turkey Point Unit 3 PWR fuel	26
17 Percentage difference between measured and computed nuclide compositions for Turkey Point Unit 3 PWR samples and averages (27BURNUPLIB library)	27
18 Percentage difference between measured and computed nuclide compositions for Turkey Point Unit 3 PWR samples and averages (44GROUPNDF5 library)	28

LIST OF TABLES (continued)

<u>Table</u>	<u>Page</u>
19 Summary of percentage differences between measured and computed compositions in this study as averages and spreads	29
20 Combination of the current and previous validation summaries, listing percentage differences between measured and computed compositions	32
21 Best-estimate and conservative correction factors for 27BURNUPLIB results	38
22 Best-estimate and conservative correction factors for 44GROUPNDF5 results	39
A.1 List of fuel nuclides automatically included by SAS2 for neutronics processing	50
F.1 Results of corrected depletion calculations for Assembly 509-069, Rod E11, Level 2 . . .	107
F.2 Differences between reported and corrected calculated isotopic concentrations	108

ABSTRACT

Isotopic characterization of spent fuel via depletion and decay calculations is necessary for determination of source terms for subsequent system analyses involving heat transfer, radiation shielding, isotopic migration, etc. Unlike fresh fuel assumptions typically employed in the criticality safety analysis of spent fuel configurations, burnup credit applications also rely on depletion and decay calculations to predict the isotopic composition of spent fuel. These isotopics are used in subsequent criticality calculations to assess the reduced worth of spent fuel. To validate the codes and data used in depletion approaches, experimental measurements are compared with numerical predictions for relevant spent fuel samples. Such comparisons have been performed in earlier work at the Oak Ridge National Laboratory (ORNL). This report describes additional independent measurements and corresponding calculations, which supplement the results of the earlier work. The current work includes measured isotopic data from 19 spent fuel samples obtained from the Italian Trino Vercelles pressurized-water reactor (PWR) and the U.S. Turkey Point Unit 3 PWR.

In addition, an approach to determine biases and uncertainties between calculated and measured isotopic concentrations is discussed, together with a method to statistically combine these terms to obtain a conservative estimate of spent fuel isotopic concentrations. Results are presented based on the combination of measured-to-calculated ratios for earlier work and the current analyses.

The results described herein represent an extension to a new reactor design not included in the earlier work, and spent fuel samples with enrichment as high as 3.9 wt % ^{235}U . Results for the current work are found to be, for the most part, consistent with the findings of the earlier work. This consistency was observed for results obtained from each of two different cross-section libraries and suggests that the estimated biases determined for each of the isotopes in the earlier work are reasonably good estimates, as the additional measurement/calculated ratios resulting from the current work tend to confirm these estimates.

ACKNOWLEDGMENTS

The authors wish to express their appreciation to several individuals who contributed their ideas and efforts in the analyses described herein. Particular thanks go to F. J. Davis of Sandia National Laboratories, who provided technical oversight for most of the duration of the work, C. V. Parks of Oak Ridge National Laboratory, who provided both programmatic and technical guidance in the preparation of this report and also reviewed and commented on the original draft; also, technical review and comments were provided by B. D. Murphy of Oak Ridge National Laboratory, Meraj Rahimi of E. R. Johnson and Associates, and K. D. Seager and M. C. Brady of Sandia National Laboratories. Final clearance and release of the report were facilitated by D. E. Hampton of Sandia National Laboratories. Last, but not least, the authors also wish to acknowledge L. F. Norris for her continuing efforts in the text editing, formatting, and release of this report.

This work was sponsored as part of the Cask System Development Program within the U.S. Department of Energy's Office of Civilian Radioactive Waste Management. This report and all calculational work described herein were performed by the Oak Ridge National Laboratory for Sandia National Laboratories in accordance with the technical and quality assurance requirements specified in Sandia National Laboratories subcontract AD-4072 and the Sandia Burnup Credit Quality Assurance Program and implementing procedures.

1. INTRODUCTION

The isotopic composition of spent fuel discharged from a commercial light-water-reactor (LWR) is a key factor in the design, licensing, and operation of radioactive waste transportation systems, interim storage facilities, and a final repository site. An accurate estimate of the time-dependent radionuclide inventory in spent fuel is necessary to evaluate many spent fuel issues, including (1) neutron multiplication for criticality safety concerns, (2) neutron and gamma-ray source terms for shielding analyses, (3) decay-heat source terms for temperature distribution and heat-transfer concerns, and (4) radiological and chemical toxicity terms for environmental impact considerations. One of the functions of the SCALE (Standardized Computer Analyses for Licensing Evaluation) code system¹ is the capability to predict the isotopic composition of discharged LWR fuel. Recent applications of nuclide depletion and production estimates for LWR fuel include criticality analyses for the evaluation of spent fuel shipment or storage packages.²⁻⁶ The ANSI/ANS 8.1 criticality safety standard⁷ recommends the validation of the analytical methods used in these spent fuel criticality analyses. This report describes efforts to validate the capability of Version 4.2 of the SCALE system to predict isotopic concentrations as part of a larger effort to validate SCALE for the criticality analysis of spent fuel configurations. Nevertheless, the results presented here should be applicable to other aspects of spent fuel analysis, as mentioned above.

A study of the use of SCALE-4 depletion analysis methods for pressurized-water-reactor (PWR) spent fuel was recently conducted^{8,9} by Oak Ridge National Laboratory (ORNL). The earlier work was based on a comparison of predicted (calculated) with measured isotopic concentrations for 19 spent fuel samples from 10 fuel assemblies representing three different PWRs. The current report will present results of further SCALE-4.2 depletion analyses^{10,11} for 19 additional PWR spent fuel samples, obtained from 5 fuel assemblies of 2 additional PWRs not included in the earlier study. The report will focus on the development of assembly-specific depletion models for each of the unique assemblies studied in these analyses and a comparison of isotopic concentrations predicted using these models to measured concentrations for each fuel sample. This report will also include a statistical combination³ of the current results with those reported in refs. 8 and 9 to obtain an improved estimate of error associated with isotopic predictions.

The 19 fuel samples analyzed in this work were modeled based on the operational data available for samples obtained from the Trino Vercelles PWR (Italy) and the Turkey Point Unit 3 PWR (U.S.). Trino Vercelles was selected because of the relatively high (3.9 wt %) enrichment of one fuel sample and because of its significantly different core design; Turkey Point was selected simply because of detailed data that were readily available. Comparisons were made for selected isotopes measured via radiochemical analysis of each fuel sample. The isotopic measurements for Trino Vercelles spent fuel were conducted by the Ispra (Italy) and Karlsruhe (Germany) facilities of the European Joint Research Centre and provided data for 14 fuel samples.¹²⁻¹⁴ Burnup analyses for the five Turkey Point Unit 3 spent fuel samples were performed by Battelle Columbus Laboratory (BCL) with direction provided by the Hanford Engineering Development Laboratory (HEDL).^{15,16} Data collected under these programs did not fall under the quality assurance standards in place for this document, and are therefore not considered explicitly qualified. However, these data are felt to be implicitly qualified because (1) the nature of procedures for handling, processing, and storage of nuclear materials is inherently consistent with quality assurance principles, and (2) the data reported have received several levels of technical review in multiple publications.¹²⁻¹⁶

The parameters of the problems analyzed in this study cover a fairly wide range. The fuel burnups are in the range of 11.53 to 31.56 gigawatt days/metric ton U (GWd/MTU). The initial fuel enrichments vary from 2.56 to 3.90 wt % ²³⁵U. The two PWR designs are significantly different; as a result there are significant variations in assembly-specific powers (7.15 to 33.12 MW/MTU), effective fuel temperatures (915 to 1015 K), moderator densities (0.73 to 0.80 g/cm³), and other pertinent operating conditions.

For consistency with earlier work,^{8,9} the results reported here were produced using the SAS2H¹⁰ control module in Version 4.2 of the SCALE code system. SAS2H is a multicode sequence that determines the isotopic composition of spent fuel using the ORIGEN-S code¹¹ for depletion and decay calculations and a one-dimensional (1-D) neutronics model of a LWR fuel assembly to prepare burnup-dependent cross sections for ORIGEN-S. The details of SAS2H depletion calculations are provided in Appendix A. All calculations were performed on an IBM RS/6000-580 workstation under AIX Version 3 Release 2.

The nature of the neutron cross-section data used in fuel depletion analyses by the SCALE system is a significant aspect of a validation effort. Two different cross-section libraries were applied in these analyses: the hybrid SCALE 27-group burnup library² and the more recent 44-group library. The 27-group cross-section library has actinide and light-element data derived from Version IV of the Evaluated Nuclear Data Files (ENDF) and fission-product data processed from ENDF/B-V files.¹⁷ The 44-group library¹⁸ applied in these analyses was derived from ENDF/B-V data, with the exception of three nuclides. The cross sections for ¹⁶O, ¹⁵⁴Eu, and ¹⁵⁵Eu in this library were obtained from ENDF/B-VI files. The ENDF/B-VI files provided data with a significant change to resonance region cross sections for ¹⁵⁴Eu and ¹⁵⁵Eu (ref. 19) which result in improved predictions for ¹⁵⁵Eu and ¹⁵⁵Gd (ref. 9). The ¹⁶O change involved improvements in the scattering kernel and is insignificant in the analyses described in this report.

The reactor configurations and SAS2H models used to represent each fuel sample are described in the following section. In the subsequent sections, comparisons of the predicted and measured nuclide compositions are presented and are combined statistically with the results of the earlier analyses^{8,9} to obtain best-estimate and conservatively bounding estimates of nuclide concentrations in spent fuel based on SAS2H isotopic predictions.

2. DEVELOPMENT OF FUEL ASSEMBLY MODELS FOR DEPLETION ANALYSES

The 19 spent fuel cases selected as a basis for SCALE-4 depletion analysis in this validation study were obtained from radiochemical assay data for spent fuel samples from the Trino Vercelles and Turkey Point Unit 3 PWRs. The initial ^{235}U enrichment, accumulated burnup, axial location, and cooling time are basic parameters in characterizing the analyzed samples of spent fuel. Table 1 shows these parameters for 14 samples obtained from 3 Trino Vercelles assemblies and 5 samples from 2 Turkey Point assemblies. The parameters in this table, in conjunction with the similar data described in ref. 9, are representative of a large percentage of the current PWR spent fuel inventory. The following subsections provide, for each reactor type, the fuel assembly design data, pertinent control rod data, and operating conditions assembled from various sources^{12-16,20-22} in order to perform the depletion calculations for this study.

2.1 TRINO VERCELLES PWR SPENT FUEL DEPLETION MODELS

The Trino Vercelles Nuclear Power Plant is a 825-MW PWR located in Italy and operated by the Ente Nazionale per l'Energia Elettrica (ENEL). The steam generation plant and fuel were designed by Westinghouse Electric Corp. The reactor is based on one of the earlier Westinghouse designs and is unlike most PWR designs in the United States. However, its design is similar to that of the U.S. Yankee Rowe PWR. Use of this uncommon design in this validation will serve to demonstrate the relative insensitivity of isotopic depletion methods to PWR reactor core design.

Radiochemical assay data obtained from the analysis of three fuel assemblies were used in this study. Two of the assemblies, numbered 509-104 and 509-032, were irradiated in the core during the first cycle only. The remaining assembly, identified as 509-069, was irradiated during both the first and second fuel cycles.

The Trino reactor core contains assemblies with two different configurations, square and cruciform. All square assemblies contain fuel and are based on a 15×15 lattice of fuel pins with 16 of the outer pins excluded to accommodate cruciform positions, as illustrated in Fig. 1. This figure shows the details of the assembly and core layouts for the Trino core. As indicated in the figure,

Table 1. Basic parameters of the measured spent fuel

No.	Unit name	Test assembly (pin No.)	Initial enrichment (wt % ²³⁵ U)	Axial level No.	Axial location ^a (cm)	Burnup (GWd/MTU)	Cooling time (d)				
1	Trino Vercelles	509-104(M11)	3.897	7	79.2	12.042	10 ^b				
2	Trino Vercelles	509-032(E11)	3.13	4	158.5	15.377	10 ^b				
3				7	79.2	15.898					
4				9	26.4	11.529					
5	Trino Vercelles	509-069 (E11)	3.13	1	237.7	12.859	10 ^b				
6				2	211.3	20.602					
7				4	158.5	23.718					
8				7	79.2	24.304					
9				509-069 (E5)	4	158.5		23.867			
10				7	79.2	24.548					
11				509-069 (L11)	4	158.5		23.928			
12				7	79.2	24.362					
13				4	158.5	24.330					
14				7	79.2	24.313					
15				Turkey Point Unit 3	D01 (G9)	2.556		NA	167.6	30.720	927
16					D01 (G10)			NA	167.0	30.510	
17					D01 (H9)			NA	167.0	31.560	
18				Turkey Point Unit 3	D04 (G9)	2.556		NA	167.6	31.260	927
19	D04 (G10)	NA	167.0		31.310						

^aHeight of sample above bottom of fuel.

^bIsotopic values were adjusted to discharge time.

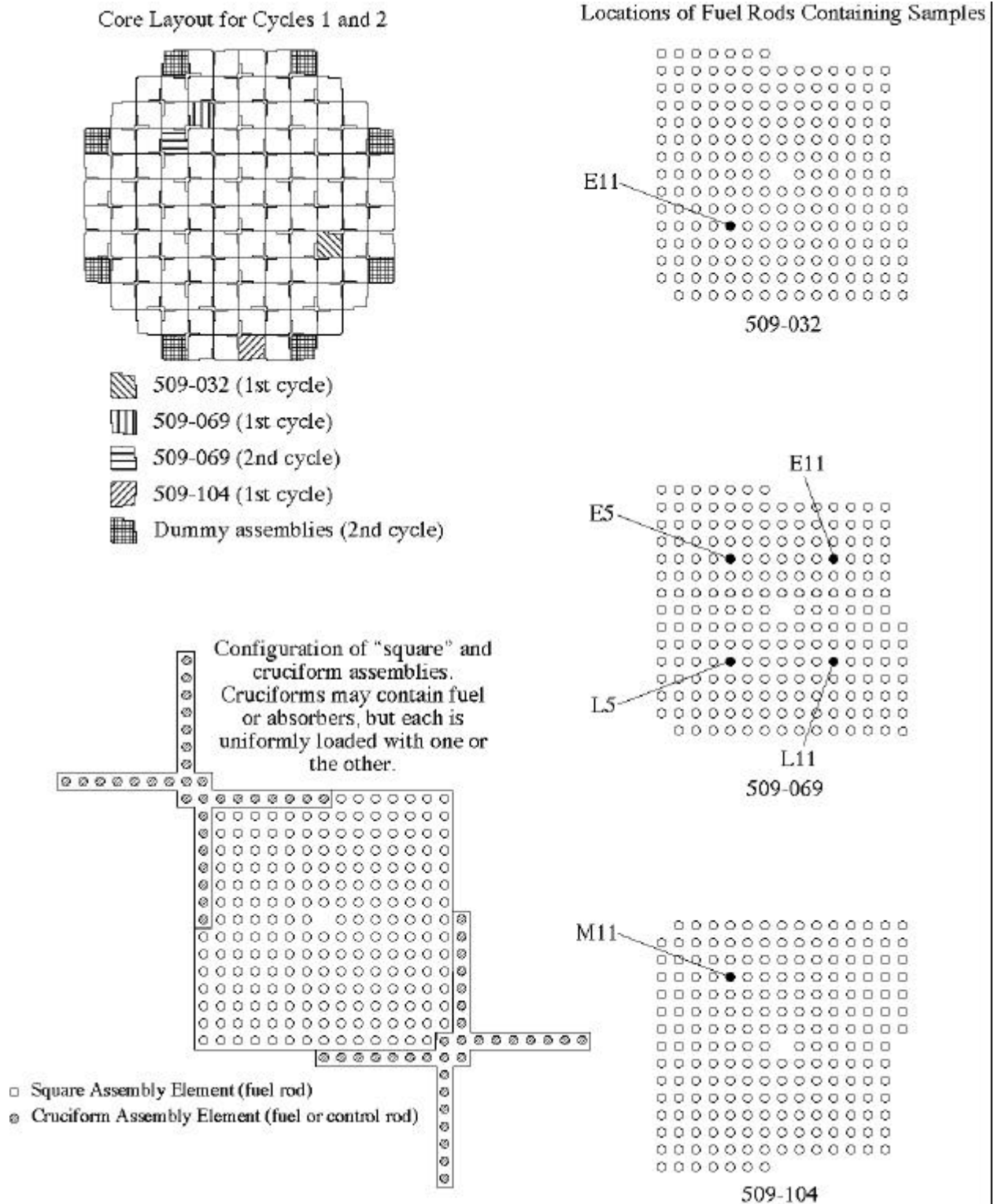


Fig. 1. Core, assembly, and sample fuel pin configurations for Trino Vercelles.

square assemblies are surrounded by a stainless steel channel tube. The center position in each assembly is used for instrumentation and was assumed vacant for depletion calculations. Cruciform assemblies can contain either fuel rods or Ag-In-Cd absorber rods. Cruciforms containing absorber rods are partially inserted from the top during operation; the remaining volume below the absorber cruciform contains coolant. Design data for square fuel assemblies¹² and cruciform fuel and absorber rods¹²⁻¹⁴ are given in Tables 2 and 3, respectively.

Spent fuel samples from the Trino Vercelles PWR were obtained from three square fuel assemblies. Initial enrichments varied between the three assemblies; initial isotopic compositions based on these specifications are given in Table 4. Initial ²³⁵U enrichment was given in ref. 12; initial ²³⁴U, ²³⁶U, ²³⁸U concentrations were estimated using empirical relationships.²¹

During cycle 1, two downtime intervals occurred prior to the end of the cycle. For this reason, cycle 1 was represented as three distinct subcycle periods. Cycle 2 was completed with no downtime, hence it was represented as a single operating period.

Operational parameters for cycles 1 and 2 and for subcycle periods I, II, and III of cycle 1 are given in Table 5. Burnups given in the table for each period or cycle were used to determine the relative specific power for each assembly during depletion steps. The exact specific power used for each individual sample in a given assembly was determined from the final burnup of the sample (given in Table 1). Note that assembly-specific burnups were supplied for assembly 509-069 only. These data were not given for the other two assemblies; relative burnup per depletion step for these assemblies was assumed based on total core burnup data.

As was indicated in Table 1, isotopic measurements were based on a 10-day cooling time. However, this 10-day cooling time was an assumption made in this work. Measurements were actually performed several years after shutdown, but isotopic concentrations reported in ref. 12 were adjusted back to “time zero.” It was not clear whether the adjusted time represented actual shutdown time or discharge time, which is usually several days after shutdown. Typically, such adjustments are made to put a number of measurements on a common basis; these adjustments are calculated, and are generally performed to estimate isotopic composition at discharge time. Assuming this was the intent of original experimentalists, a 10-day cooling time was taken to represent the time between shutdown

and discharge. Thus SAS2H calculations reported here include a 10-day post-irradiation decay period. Note that a longer post-irradiation discharge time (20 to 50 days) would not significantly

Table 2. Design data for Trino Vercelles square fuel assemblies

Parameter	Data
Square fuel assembly data	
Designer	Westinghouse
Lattice	15 × 15 ^a
Square assemblies/core, cycle 1 (cycle 2)	120(112)
Number of fuel rods	208
Number of inner holes	1
Assembly fuel, kg UO ₂	353.81
Water pressure, kg/cm ²	140
Average coolant temperature, °C, cycle 1 (cycle 2)	279 (269)
Inlet/outlet temperature increase, °C	30.0
Assembly tube outer side, cm	20.1
Channel tube thickness, cm	0.06
Channel tube material	SS-304
Fuel rod data	
Type fuel pellet	UO ₂
Stack density with no gap, g/cm ³	10.079 ^b
Rod pitch, cm (in.)	1.303 (0.513)
Rod OD, cm (in.)	0.9786 (0.3853)
Rod ID, cm (in.)	0.9020 (0.3551)
Active fuel length, cm (in.)	264.1 (104.0)
Clad material	SS-304
Clad temperature, K	570 ^c

^aThe lattice is a 15 × 15 array with 16 pins excluded in the outer rows or columns to accommodate space for cruciform assemblies (Table 3).

^bComputed from the fuel mass and volume listed in this table.

^cClad temperature was not available in literature. Temperature data for a similar design (Yankee Rowe PWR²⁰) was used.

Table 3. Design data for Trino Vercelles cruciform fuel and control rod assemblies

Parameter	Data
Number of cruciform assemblies/core	52
Cruciform fuel assembly data	
Number of assemblies/core	24
Fuel weight/assembly, kg UO ₂	44
Cruciform control rod data	
Number of control assemblies/core	28
Neutron absorber composition, wt %	
Ag	85
In	15
Cd	5
Absorber density, g/cm ³ (lbs/in. ³)	10.159 (0.341) ^a
Number of absorber rods/control rod	32
Absorber rod OD, cm (in.)	1.001 (0.394)
Absorber rod clad thickness, cm	0.0432
Maximum control group insertion (Period I), %	30

^aAbsorber density was not given. Applied the density data for the same Ag-In-Cd ratios that are listed in FSAR for Sequoyah Nuclear Plant Units 1 and 2.

Table 4. Initial composition of Trino Vercelles fuel assemblies

Uranium isotope	Assembly ID		
	509-104	509-32	509-069
wt % ²³⁵ U	3.897	3.13	3.13
wt % ²³⁴ U	0.035	0.028	0.028
wt % ²³⁶ U	0.018	0.014	0.014
wt % ²³⁸ U	96.050	96.828	96.828

Table 5. Summary of general operations of cycles 1 and 2

Parameter	Cycle/period data			
	1	1	1	2
Cycle	I	II	III	All of cycle
Starting date	10/23/64	8/31/65	7/11/66	5/20/70
Uptime, d	226	263	292	416
Downtime, d	86	51	1117	0
Coolant average temperature, °C	282	278	278	269
Control rod insertion, %	30	4 ^d	4 ^d	0 ^a
Average boron, ppm (wt)	1175	850	325	650 ^b
509-069 burnup, GWd/MTU	2.726	4.927	6.327	7.720
Core burnup, ^c GWd/MTU	2.260	4.085	5.245	NA

^aNot given, assumed to be insignificant.

^bNot given, assumed average of cycle 1 range: 1,300 to 0 ppm.

^cApplied to the cycle 1 burnup for assemblies 509-032 and 509-104.

^dNot modeled, assumed to be negligible.

affect isotopic compositions. However, a shorter decay period would affect isotopes whose inventory comes in part from the decay of short-lived parents. The nuclide most significantly affected by this decay period is ²³⁹Pu, which increases in inventory by roughly 1% during the first ten days post-irradiation due to the beta decay of ²³⁹U and ²³⁹Np (e.g., ²³⁹U(T_{1/2} = 23.5 m) → ²³⁹Np(T_{1/2} = 2.350 d) → ²³⁹Pu].

The SAS2H Pass A pin-cell calculation was based on the nominal fuel pin dimensions and pitch as specified in Table 2. However, the Trino Vercelles assembly lattice is more complex than those of PWR configurations analyzed in earlier work; channel tubes and external cruciform assemblies are not present in conventional PWR designs. Although cruciforms loaded with fuel result in a near-uniform assembly lattice, cruciforms loaded with Ag-In-Cd absorber rods result in an asymmetric assembly configuration. In addition, axial symmetry is defeated by the partial insertion of control rods during operation. This problem is aggravated by the fact that control assemblies may be moved vertically during irradiation. Hence, one must make assumptions and approximations in the development of a 1-D SAS2H Pass B model to approximate the assembly layout.

Because of the 1-D nature of SAS2H models, assembly lattices are generally approximated by a 1-D radial model. Thus it is necessary to determine effective radii that can account for the presence

of significant material in a manner that conserves masses. Figure 1 illustrates the locations of each of the rods from which spent fuel samples were obtained within each assembly: E11 in assembly 509-032, E5, E11, L5, and L11 in 509-069, and M11 in 509-104. Each of these fuel rods is located roughly halfway between the center and the edge of the assembly, and thus will be well approximated by the average behavior of a circular ring of fuel/moderator mixture surrounding the vacant position at the center of the assembly. The form of the 1-D representation is shown in Fig. 2, centered around the vacant center of the assembly. This figure is drawn to scale, and shows the relative size of each different zone in the 1-D approximation. Table 6 lists the contents and effective radii of each zone.

A complication encountered in this procedure was introduced by the fact that although detailed information was provided for most core parameters, these data did not include the exact location of control rod and fuel rod cruciforms in the core. All that is known is the total number of each type of cruciform. Some assemblies might effectively contain 224 fuel pins (208 square assembly pins + 16 cruciform fuel pins), while others could contain as few as 208 fuel pins and 16 control rod pins. Thus it was decided to base each assembly model on the average number of cruciform fuel rods and cruciform absorber rods per assembly in the core. With 32 fuel pins/cruciform assembly and 24 cruciform assemblies mixed with 120 square assemblies, there are 6.4 cruciform pins per square assembly. Since SAS2H requires an integral number of fuel pins per assembly, the average assembly was assumed to contain 214 (208 + 6) fuel pins.

The effective area of absorber material per assembly was calculated knowing the size and number of absorber rods present and dividing by the number of assemblies in the core. However, since the control rods were only inserted by 30% during Period I of Cycle 1, the effective area of the control rods was reduced to 30% of the total area. Because of the 1-D nature of SAS2H, absorber material placed in the model simulates a fully inserted rod (since axial uniformity is implicit in a 1-D radial model); however, weighting the area of the control rod area by the fraction of insertion helps to compensate for this approximation. For Periods II and III of Cycle 1, control rods were inserted 4% of full length, and were completely withdrawn during Cycle 2. It was assumed that the 4% insertion was negligible during Periods II and III. Thus it was assumed that no absorber material was present during these exposure periods, and the effective area of absorber was replaced with moderator for these periods.

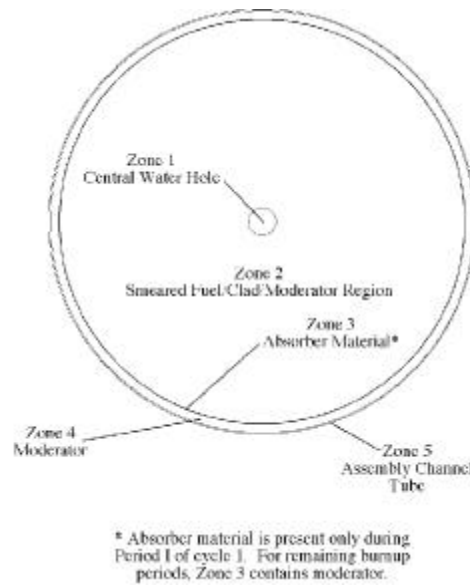


Fig. 2. One-dimensional assembly approximation for Trino Vercelles assemblies.

Table 6. Effective dimensions determined for 1-D SAS2H assembly model

Radial zone	Composition	Area (cm ²)	Cumulative area (cm ²)	Effective radius (cm)
1	Borated moderator	1.698	1.698	0.735
2	Homogenized fuel, clad, and borated moderator	363.332	365.030	10.779
3	<i>Period I, Cycle 1:</i> homogenized Ag-In-Cd absorber and clad	2.034	367.064	10.809
	<i>Remaining Periods and Cycles:</i> borated moderator			
4	Borated moderator	32.136	399.200	11.273
5	Stainless steel	4.810	404.010	11.340

Zone 4 of the radial model accounts for all moderator around and below each control rod. The final radius represents the total thickness of stainless steel in the assembly and cruciform assembly channel tubes. Calculations were performed using a reflective boundary condition beyond the outermost zone.

As was shown in Table 1, spent fuel samples were obtained from a variety of axial locations within the cores. The 14 different Trino Vercelles fuel samples included in this study were taken from the fuel pins identified in Table 1 and located as shown in Fig. 1. From each fuel rod, up to four samples were studied, each at different axial heights. In characterizing the rod axially in the original radiochemical assay work, the length of the rod was subdivided into ten equal-height levels where levels 1 and 10 are located at the top and the bottom of the rod, respectively. The sample pellet locations were identified by level number and were taken from the midpoint of the corresponding level number. The exact axial location of a pellet is not important neutronically since axial uniformity is assumed in depletion calculations; however, efforts were taken to match pellet locations to the expected local temperatures and moderator density corresponding to that height. Axially dependent material temperatures and moderator densities are given in Table 7 for each axial location. Water temperatures were computed using data given in Tables 2 and 5 along with the axially varying temperature formulation used in the previous validation study.⁹ The water densities were derived from correlations¹ based on cycle operating pressure data and the calculated water temperature. The effective fuel temperatures were computed from resonance-effective temperatures given in operating data for the similar-design Yankee Rowe PWR.²⁰

Table 7. Axially dependent effective fuel and water temperature and water densities

Level No.	Effective fuel temperature, K		Effective water temperature, K		Water density, g/cm ³	
	Cycle 1	Cycles 1 and 2	Cycle 1	Cycles 1 and 2	Cycle 1	Cycle 2
1	915	915	567	563	0.7365	0.7555
2	968	968	565	561	0.7407	0.7595
4	1015	1015	557	553	0.7554	0.7730
7	1001	1001	543	540	0.7795	0.7953
9	927	927	537	534	0.7885	0.8032

Power histories for each sample are listed in Table 8. The burnup given in this table is the burnup at discharge and was determined experimentally from the measured ^{148}Nd concentration. Although burnup estimates were also experimentally determined by other methods, burnup data based on ^{148}Nd measurements were applied in this study for consistency with burnup estimates performed in earlier validation calculations.⁹ The specific powers for each depletion period were calculated using the burnup for each sample and the relative power in each period inferred from the period burnups given in Table 5.

SAS2H input cases for each of the 14 Trino Vercelles fuel samples are given in Appendix B. These input cases are for calculations using the SCALE 27-group burnup library, known within SCALE as “27BURNULIB.” Calculations were also performed using the SCALE “44GROUPNDF5” cross-section library, using identical input with the exception of the cross-section library specification, and the material specification for Zircaloy (which must be specified explicitly by nuclide for the 44-group library in SCALE-4.2). Light-element masses were computed based on the assembly's Zircaloy content. (Note: Input specifications for the cadmium component of the Trino Vercelles absorber rods were found to contain an error after completion of these calculations. The error is corrected in the Appendix B listings. The effect of this error was subsequently determined to be negligible. The nature and effect of this error are discussed in Appendix F.)

2.2 TURKEY POINT UNIT 3 SPENT FUEL DEPLETION MODELS

The Turkey Point Unit 3 PWR, operated by Florida Power and Light Co., was designed by Westinghouse Electric Corp. The fuel assembly design is based on a 15×15 square lattice, with 21 positions containing control rod and instrumentation guide tubes. Design and operating parameters^{15,16,21,22} providing the key relevant characteristics of the reactor, fuel, and fuel assembly configurations are given in Table 9.

Radiochemical assay data obtained from the analysis of two fuel assemblies, identified as D01 and D04, were used as a basis for models developed in this study. The initial fuel isotopic compositions for each of the two assemblies is given in Table 10. Initial ^{235}U and ^{238}U enrichments were given in available references; initial ^{234}U and ^{236}U concentrations were estimated using

Table 8. Fuel burnup and operating power histories for Trino Vercelles PWR pellet samples

Assembly ID	509-104	509-032	509-032	509-032	509-069	509-069	509-069	509-069	509-069
Fuel rod location	M11	E11	E11	E11	E11	L11	E11	E11	E11
Axial level no.	7	4	7	9	1	4	2	4	4
Burnup, ^a GWd/MTU	12.042	15.377	15.898	11.529	12.859 ^b	20.602	20.602	23.718	23.718
Powers, ^c MW/MTU:									
Cycle 1, Period I	10.390	13.268	13.717	9.947	7.148	11.452	11.452	13.184	13.184
Cycle 1, Period II	16.138	20.607	21.309	15.451	11.101	17.786	17.786	20.476	20.476
Cycle 1, Period III	18.663	23.831	24.639	17.868	12.840	20.571	20.571	23.683	23.683
Cycle 2	—	—	—	—	10.997	17.619	17.619	20.283	20.283
Assembly ID	509-069	509-069	509-069	509-069	509-069	509-069	509-069	509-069	509-069
Fuel rod location	E11	E5	E5	L11	L11	L5	L5	L5	L5
Axial level no.	7	4	7	4	7	4	4	7	7
Burnup, ^a GWd/MTU	24.304	23.867	24.548	23.928	24.362	24.330	24.330	24.313 ^b	24.313 ^b
Powers, ^c W/MTU:									
Cycle 1, Period I	13.509	13.266	13.645	13.300	13.542	13.524	13.524	13.514	13.514
Cycle 1, Period II	20.982	20.605	21.193	20.657	21.032	21.004	21.004	20.990	20.990
Cycle 1, Period III	24.268	23.832	24.512	23.893	24.326	24.294	24.294	24.277	24.277
Cycle 2	20.785	20.411	20.993	20.463	20.834	20.807	20.807	20.792	20.792

^aBurnup based on measured ¹⁴⁸Nd concentration, unless otherwise specified.

^bBurnup based on measured ¹³⁷Cs concentration because there was no analysis of ¹⁴⁸Nd for the sample.

^cPowers determined from the above burnups and the specified uptimes and burnup distributions in Table 5.

Table 9. Turkey Point Unit 3 PWR assembly and operating data^a

Parameter	Data
Assembly general data	
Designer	Westinghouse
Lattice	15 × 15
Number of fuel rods	204
Number of guide tubes	20
Number of instrument tubes	1
Average 3-cycle water pressure, psia	2083
Water temperature at sample axial location, K (°F)	570 (567)
Water density at sample axial location, g/cm ³	0.731
Soluble boron, cycle average, ppm (wt)	450
Assembly mass, kg UO ₂	456.9
Fuel rod data	
Type fuel pellet	UO ₂
Stack density with gap, g/cm ³ (% TD)	10.235 (93.38)
Rod pitch, cm (in.)	1.4300 (0.563)
Rod OD, cm (in.)	1.0719 (0.422)
Rod ID, cm (in.)	0.9484 (0.3734)
Pellet OD, cm (in.)	0.9296 (0.366)
Active fuel length, cm (in.)	365.76 (144)
Effective fuel temperature, K	922
Clad material	Zircaloy-4
Clad temperature, K	595
Guide tube data	
Inner radius, cm (ID as in.)	0.6502(0.512)
Outer radius, cm (OD as in.)	0.6934(0.546)
Tube material	Zircaloy-4

^aSources: refs. 15, 16, 21, and 22.

Table 10. Initial composition of Turkey Point fuel assemblies

Uranium isotope	Assembly ID	
	D01	D04
wt % ²³⁵ U	2.556	2.556
wt % ²³⁴ U	0.023	0.023
wt % ²³⁶ U	0.012	0.012
wt % ²³⁸ U	97.409	97.409

empirical relationships.²¹ Both assemblies were present in the reactor during fuel cycles 2 through 4; cycle lengths and downtimes are shown in Table 11. In the spent fuel assays, a single sample was taken from each of five different rods; all samples were taken from a location of either 167.0 or 167.6 cm above the bottom of the fuel, as shown in Table 1. The assembly, rod identification, and burnup for each sample are supplied in Table 12. Figure 3 shows the configuration of the 15×15 assembly design and illustrates the position of each of the fuel sample pin locations within the assembly. As with the Trino Vercelles measurements and those reported in ref. 9, burnups for the Turkey Point fuel samples were determined based on measured ^{148}Nd concentrations. No data were available indicating the operating power for the assemblies or core on a cycle-by-cycle basis. However, other fuel assemblies for which power histories were available during cycles 2 through 4 varied by less than 8% from the average power.¹⁵ Thus it was assumed that the reactor was operated at a constant power over all three cycles; average specific power was then computed for each sample based on the total length of the three cycles and the final burnup of the sample. These average powers are also given in Table 12.

The 1-D assembly model for the Turkey Point assemblies was developed assuming a water-filled guide tube surrounded by a cell-equivalent volume of water, surrounded in turn by the equivalent material corresponding to a homogenized fuel-pin cell. Since the full assembly consisted of 21 guide tubes intermixed with fuel cells, the 1-D approximation was based on a single guide tube cell surrounded by the volume equivalent of 9.714 fuel cells. This value was obtained as the ratio of fuel pins to water holes (204/21). This proportion results in the same water cell to fuel cell ratio as existed in the actual assembly.

SAS2H input cases for each of the five Turkey Point fuel samples are given in Appendix C. These input cases are for calculations using the SCALE 27-group burnup library, known within SCALE as “27BURNULIB.” Calculations were also performed using the SCALE “44GROUPNDF5” cross-section library, using identical input with the exception of the cross-section library specification and the material specification for Zircaloy.

Table 11. Turkey Point Unit 3 operating history^a of assemblies D01 and D04

Cycle	Cycle start	Cycle end	Uptime, d	Downtime, d
2	12/16/74	10/26/75	314	58
3	12/23/75	11/15/76	327	62
4	1/16/77	11/24/77	312	927 ^b

^aFlorida Power and Light Co. data provided by E. R. Knuckles.

^bCooling time from shutdown to date of radiochemical analyses.

Table 12. Turkey Point pellet sample data

Assembly ID	Rod column	Rod row	Burnup, GWd/MTU	Power (avg.), MW/MTU
D01	G	9	30.720	32.235
D01	G	10	30.510	32.015
D01	H	9	31.560	33.116
D04	G	9	31.260	32.802
D04	G	10	31.310	32.854

3. PREDICTED AND MEASURED ISOTOPIC COMPOSITIONS

Comparisons of spent PWR fuel isotopic compositions predicted by SCALE-4 calculations to those measured by radiochemical assay analyses are provided in this section. Percentage differences between the computed and measured values for all isotopes selected for assay analysis are given for each sample. Also included in this section are the average percentage differences for each of the two reactor types, both for the set of analyses included in this study and for the combined results for this and earlier⁹ validation analyses. Comparisons are made based on results obtained using the two different SCALE cross-section libraries described in Sect. 1: the SCALE 27-group burnup library (27BURNULIB), and the SCALE 44-group library (44GROUPNDF5). Additional comparisons listing measurements, computed predictions, and percentage differences for each isotope of each sample are included in Appendix D for Trino Vercelles and Appendix E for Turkey Point Unit 3.

3.1 TRINO VERCELLES PWR ISOTOPIC RESULTS

Radiochemical nuclide analyses of the Trino Vercelles spent fuel samples were conducted by the Ispra and Karlsruhe facilities of the Joint Research Center. Thirty-nine samples from 14 different fuel rods were analyzed at one or both facilities; approximately half of the cases selected in this study were analyzed at both laboratories. Isotopic concentrations for all the major uranium and plutonium nuclides were measured by both laboratories for most samples. The average concentrations measured for the 14 samples selected for this study are listed in Table 13. This table also indicates the isotopes and samples for which only a single measurement was performed. The compositions were reported in several different types of units; each type of reported concentration is included in the table. However, all data were converted to units of milligrams per initial gram of uranium or curies per initial gram of uranium for consistency with the previous validation study. Measured (sample average) and computed nuclide concentrations are listed in these units in Appendix D for all Trino Vercelles samples.

Table 13. Average measured irradiation composition of Trino Vercelles PWR fuel

Assembly ID		509-104	509-032	509-032	509-032	509-069	509-069	509-069	509-069
Fuel rod ID		M11	E11	E11	E11	E11	E11	E11	E11
Sample height, level number		7	4	7	9	1	2	2	4
Burnup, ^b GWd/MTU		12.042	15.377 ^e	15.898 ^e	11.529 ^e	12.859 ^e	20.602	20.602	23.718
Nuclide	Units of reported analysis								
²³⁵ U	depletion as kg/MTU (initial)	1.2345 × 10 ⁻¹	1.402 × 10 ^{1e}	1.469 × 10 ^{1e}	1.113 × 10 ^{1e}	1.184 × 10 ^{1e}	1.694 × 10 ¹	1.694 × 10 ¹	1.882 × 10 ¹
²³⁶ U	atoms/atom ²³⁸ U (final)	2.900 × 10 ⁻³	2.990 × 10 ^{-3e}	2.890 × 10 ^{-3e}	2.630 × 10 ^{-3e}	2.580 × 10 ^{-3e}	3.515 × 10 ⁻³	3.515 × 10 ⁻³	3.835 × 10 ⁻³
²³⁸ U	depletion as kg/MTU (initial)	—	—	—	—	9.610 ^e	1.6495 × 10 ¹	1.6495 × 10 ¹	1.894 × 10 ¹
²³⁹ Pu ^d	kg/MTU (initial)	4.586	5.266 ^e	5.234 ^e	4.418 ^e	4.580 ^e	5.755	5.755	5.895
²⁴⁰ Pu	kg/MTU (initial)	7.165 × 10 ⁻¹	1.118 ^e	1.137 ^e	7.550 × 10 ^{1e}	8.400 × 10 ^{1e}	1.520	1.520	1.755
²⁴¹ Pu	kg/MTU (initial)	3.475 × 10 ⁻¹	6.140 × 10 ^{1e}	6.180 × 10 ^{1e}	3.690 × 10 ^{1e}	4.000 × 10 ^{1e}	8.850 × 10 ⁻¹	8.850 × 10 ⁻¹	1.030
²⁴² Pu	kg/MTU (initial)	—	—	—	—	4.600 × 10 ^{-2e}	1.720 × 10 ⁻¹	1.720 × 10 ⁻¹	2.435 × 10 ⁻¹
^{242m} Pu	atoms/atom ²³⁹ Pu	6.750 × 10 ⁻³	1.620 × 10 ^{-2e}	1.790 × 10 ^{-2e}	8.500 × 10 ^{-3e}	—	—	—	—
^{242m} Am	atoms/atom U (initial)	—	—	—	—	—	1.365 × 10 ⁻⁶	1.365 × 10 ⁻⁶	2.090 × 10 ^{-6f}
²⁴³ Am	atoms/atom U (initial)	—	—	—	—	—	2.345 × 10 ⁻⁵	2.345 × 10 ⁻⁵	4.440 × 10 ^{-5f}
²⁴² Cm	atoms/atom U (initial)	—	—	—	—	—	1.740 × 10 ⁻⁵	1.740 × 10 ⁻⁵	2.395 × 10 ⁻⁵
²⁴⁴ Cm	atoms/atom U (initial)	—	—	—	—	—	4.560 × 10 ⁻⁶	4.560 × 10 ⁻⁶	8.795 × 10 ⁻⁶
¹⁰⁶ Ru	dis-s ⁻¹ /g U (final)	5.291 × 10 ^{9e}	8.029 × 10 ^{9e}	8.584 × 10 ^{9e}	5.846 × 10 ^{9e}	—	—	—	—
¹³⁴ Cs	dis-s ⁻¹ /g U (final)	1.029 × 10 ^{9e}	1.765 × 10 ^{9e}	1.869 × 10 ^{9e}	1.021 × 10 ^{9e}	9.410 × 10 ^{8e}	2.312 × 10 ^{9e}	2.312 × 10 ^{9e}	2.914 × 10 ^{9e}
¹³⁷ Cs	dis-s ⁻¹ /g U (final)	1.469 × 10 ^{9e}	1.876 × 10 ^{9e}	1.902 × 10 ^{9e}	1.369 × 10 ^{9e}	1.486 × 10 ^{9e}	2.418 × 10 ^{9e}	2.418 × 10 ^{9e}	2.775 × 10 ^{9e}
¹⁴⁴ Ce	dis-s ⁻¹ /g U (final)	2.179 × 10 ^{10e}	2.716 × 10 ^{10e}	2.660 × 10 ^{10e}	2.098 × 10 ^{10e}	—	—	—	—
¹⁴⁸ Nd	atoms/atom ²³⁸ U (final)	—	—	—	—	—	3.900 × 10 ^{-4f}	3.900 × 10 ^{-4f}	4.500 × 10 ^{-4f}
¹⁵⁴ Eu	dis-s ⁻¹ /g U (final)	—	—	—	—	5.170 × 10 ^{7e}	1.398 × 10 ^{8e}	1.398 × 10 ^{8e}	1.779 × 10 ^{8e}

Table 13 (continued)

Assembly ID	509-069	509-069	509-069	509-069	509-069	509-069	509-069	509-069	509-069
Fuel rod ID	E11	E5	L11	L11	L11	L5	L5	L5	L5
Sample height, level number	7	4	4	4	7	4	4	7	7
Burnup, ^b GWd/MTU	24.304	23.867 ^e	24.548	23.928 ^e	24.362	24.330 ^e	24.330 ^e	24.313 ^c	24.313 ^c
Nuclide	Units of reported analysis								
²³⁵ U	1.8955 × 10 ¹	1.839 × 10 ^{1e}	1.909 × 10 ¹	1.848 × 10 ^{1f}	1.905 × 10 ¹	1.833 × 10 ^{1e}	1.833 × 10 ^{1e}	1.899 × 10 ^{1e}	1.899 × 10 ^{1e}
²³⁶ U	3.865 × 10 ⁻³	3.740 × 10 ^{-3e}	3.765 × 10 ⁻³	3.990 × 10 ^{-3f}	3.685 × 10 ⁻³	3.690 × 10 ^{-3e}	3.690 × 10 ^{-3e}	3.800 × 10 ^{-3e}	3.800 × 10 ^{-3e}
²³⁸ U	1.912 × 10 ¹	1.913 × 10 ^{1e}	1.9955 × 10 ¹	1.980 × 10 ^{1f}	2.010 × 10 ¹	1.960 × 10 ^{1e}	1.960 × 10 ^{1e}	2.109 × 10 ^{1e}	2.109 × 10 ^{1e}
²³⁹ Pu ^d	6.070	5.950 ^e	5.980	6.060 ^f	1.810	6.060 ^e	6.060 ^e	5.970 ^e	5.970 ^e
²⁴⁰ Pu	1.825	1.760 ^e	1.785	1.790 ^f	1.055	1.770 ^e	1.770 ^e	1.790 ^e	1.790 ^e
²⁴¹ Pu	1.060	1.050 ^e	1.055	1.050 ^f	2.590 × 10 ⁻¹	1.060 ^e	1.060 ^e	1.060 ^e	1.060 ^e
²⁴² Pu	2.575 × 10 ⁻¹	2.400 × 10 ^{-1e}	2.540 × 10 ⁻¹	2.470 × 10 ^{-1f}	2.155 × 10 ⁻⁶	2.440 × 10 ^{-1e}	2.440 × 10 ^{-1e}	2.500 × 10 ^{-1e}	2.500 × 10 ^{-1e}
^{242m} Am	2.220 × 10 ^{-6f}	—	2.400 × 10 ⁻⁶	1.930 × 10 ^{-6f}	4.160 × 10 ⁻⁵	—	—	—	—
²⁴³ Am	4.490 × 10 ^{-5f}	—	4.520 × 10 ⁻⁵	4.360 × 10 ^{-5f}	2.425 × 10 ⁻⁵	—	—	—	—
²⁴² Cm	2.620 × 10 ⁻⁵	2.280 × 10 ^{-5e}	2.470 × 10 ⁻⁵	2.750 × 10 ^{-5f}	9.495 × 10 ⁻⁶	2.480 × 10 ^{-5e}	2.480 × 10 ^{-5e}	2.440 × 10 ^{-5e}	2.440 × 10 ^{-5e}
²⁴⁴ Cm	9.660 × 10 ⁻⁶	8.740 × 10 ^{-6e}	9.190 × 10 ⁻⁶	8.930 × 10 ^{-6f}	—	9.290 × 10 ^{-6e}	9.290 × 10 ^{-6e}	8.570 × 10 ^{-6e}	8.570 × 10 ^{-6e}
¹⁰⁶ Ru	—	—	—	—	3.048 × 10 ^{9e}	—	—	—	—
¹³⁴ Cs	2.987 × 10 ^{9e}	2.939 × 10 ^{9e}	3.054 × 10 ^{9e}	—	2.881 × 10 ^{9e}	2.939 × 10 ^{9e}	2.939 × 10 ^{9e}	3.005 × 10 ^{9e}	3.005 × 10 ^{9e}
¹³⁷ Cs	2.818 × 10 ^{9e}	2.788 × 10 ^{9e}	2.909 × 10 ^{9e}	—	—	2.821 × 10 ^{9e}	2.821 × 10 ^{9e}	2.862 × 10 ^{9e}	2.862 × 10 ^{9e}
¹⁴⁴ Ce	—	—	—	—	4.620 × 10 ^{-4e}	—	—	—	—
¹⁴⁸ Nd	4.610 × 10 ^{-4f}	4.520 × 10 ^{-4e}	4.650 × 10 ^{-4f}	4.540 × 10 ^{-4f}	1.718 × 10 ^{8e}	4.590 × 10 ^{-4e}	4.590 × 10 ^{-4e}	4.590 × 10 ^{-4e}	4.590 × 10 ^{-4e}
¹⁵⁴ Eu	1.650 × 10 ^{8e}	1.765 × 10 ^{8e}	1.919 × 10 ^{8e}	—	—	1.768 × 10 ^{8e}	1.768 × 10 ^{8e}	1.849 × 10 ^{8e}	1.849 × 10 ^{8e}

^aAdjusted to the shutdown composition, except for ²³⁹Pu.

^bBurnup, based on measured ¹⁴⁸Nd concentration, unless otherwise specified.

^cBurnup, based on measured ¹³⁷Cs concentration.

^dCompositions of ²³⁹Pu include ²³⁹U and ²³⁹Np at shutdown. Source: Ref. 12.

^eMeasured at Ispra only.

^fMeasured at Karlsruhe only.

The percentage differences between measured and calculated concentrations for each isotope of each sample are given in Tables 14 and 15 for the results of calculations using the 27-group and the 44-group cross-section libraries, respectively. These tables also provide the average difference for all samples.

As was noted earlier, an error was identified in the specification of the absorber rod contents for all Trino Vercelles calculations, and has an effect on the values reported in Tables 14 and 15. However, the effect is very minor and may be neglected. The nature of the error and its effect are described in Appendix F.

3.2 TURKEY POINT UNIT 3 PWR ISOTOPIC RESULTS

Radiochemical isotopic analyses of five pellet samples from two spent fuel assemblies of the Turkey Point Unit 3 PWR were analyzed by BCL for the Climax Spent Fuel Test.¹⁵ The measured post-irradiation nuclide concentrations are listed in Table 16 as reported, in terms of atomic percentages or as ratios to ²³⁸U atomic content. Again, the concentration data were converted to units of milligrams of the nuclide per gram of initial uranium; measured and computed concentrations are given in these units in Appendix E for all Turkey Point samples. The percentage differences between measured and calculated concentrations for each isotope of each sample are given in Tables 17 and 18 for the results of calculations using the 27-group and the 44-group cross-section libraries, respectively. These tables also provide the average difference for all samples.

3.3 SUMMARY OF COMBINED ISOTOPIC RESULTS

Average percentage differences between measured and computed isotopic concentrations combined from both Trino Vercelles and Turkey Point data are given in Table 19. This table also provides the number of samples used to calculate the average and the minimum and maximum differences for all cases. These results are also illustrated in Figs. 4 and 5 for 27-group and 44-group results, respectively. The results for all samples described herein were combined with those reported in ref. 9; Table 20 summarizes averages from the current study, the earlier study, and the combined average, for both cross-section libraries. Figures 6 and 7 illustrate the results for the combined samples for each isotope for 27-group and 44-group results, respectively.

Table 14. Percentage difference^a between measured and computed^b nuclide compositions for Trino Vercelles PWR samples and averages (27BURNULIB library)

Assembly (wt % ²³⁵ U) Burnup, GWd/MTU	509-069 (3.13)												Average		
	509-104 (3.897)	509-032 (3.13)		12.859	20.602	23.718	24.304	23.867	24.548	23.928	24.362	24.330		24.313	
²³⁵ U	1.2	3.4	5.1	1.4	-0.1	1.9	3.8	1.7	-0.2	1.8	0.2	2.2	-2.4	1.9	1.6
²³⁶ U	-10.4	-7.8	-2.4	-14.5	-5.4	-5.0	-5.5	-4.9	-2.8	-1.8	-8.7	-0.1	-0.4	-3.1	-5.2
²³⁸ U	0.1	<0.1	<0.1	<0.1	-0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	0.1	<0.1	0.2	<0.1
²³⁹ Pu	-3.7	-1.2	-1.3	-1.8	2.5	0.9	2.4	-2.1	1.7	-0.4	-0.1	-0.8	0.4	-0.5	-0.3
²⁴⁰ Pu	-7.0	-4.4	-3.1	-4.0	1.7	-3.6	-4.1	-6.2	-3.8	-3.2	-5.2	-5.3	-2.6	-4.4	-3.9
²⁴¹ Pu	-4.5	2.9	5.7	-0.2	7.7	3.2	6.3	4.5	5.1	6.4	5.5	5.3	6.7	4.6	4.2
²⁴² Pu	-19.2	-11.3	-12.3	-12.6	-3.4	-8.3	-8.5	-8.5	-5.8	-5.0	-7.9	-8.5	-3.0	-5.6	-8.6
^{242m} Am	-	-	-	-	-	60.4	23.4	15.3	-	7.8	35.0	19.1	-	-	26.8
²⁴³ Am	-	-	-	-	-	-4.2	-18.0	-13.4	-	-11.0	-14.0	-5.8	-	-	-11.1
²⁴² Cm	-	-	-	-	-	-21.4	-21.7	-25.8	-16.6	-19.5	-30.5	-19.4	-20.0	-20.2	-21.7
²⁴⁴ Cm	-	-	-	-	-	-27.5	-28.4	-29.2	-25.8	-22.0	-26.5	-27.1	-23.7	-20.0	-25.6
¹⁰⁶ Ru	-7.8	1.5	-1.0	-10.5	-	-	-	-	-	-	-	-	-	-	-4.5
¹³⁴ Cs	-23.3	-19.5	-19.9	-23.0	-23.3	-20.2	-16.8	-15.7	-37.7	-15.8	-	-16.9	-13.3	-15.9	-20.1
¹³⁷ Cs	1.1	1.4	3.5	3.5	0.7	0.3	1.1	2.0	1.2	-0.1	-	0.2	2.0	0.7	1.4
¹⁴⁴ Ce	-2.6	-3.9	1.5	-5.0	-	-	-	-	-	-	-	-	-	-	-2.5
¹⁴⁸ Nd	-	-	-	-	-	-1.6	-1.7	-1.6	-1.5	-1.4	-1.6	-1.5	-1.0	-	-1.5
¹⁵⁴ Eu	-	-	-	-	8.7	13.0	19.0	33.6	21.5	17.4	-	29.1	26.2	19.6	20.9

^a(Calculated/measured - 1) × 100%.

^bUsing SAS2H/ORIGEN-S analysis sequence and 27-group cross-section library of SCALE-4.

Table 15. Percentage difference^a between measured and computed^b nuclide compositions for Trino Vercelles PWR samples and averages (44GROUPNDF5 library)

Assembly (wt % ²³⁵ U) Burnup, GWd/MTU	509-069 (3.13)										Average			
	509-004 (3.897)	509-032 (3.13)		12.859	20.602	23.718	24.304	23.867	24.548	23.928		24.362	24.330	24.313
²³⁵ U	1.2	3.9	4.8	1.3	2.5	4.5	1.0	0.5	1.1	1.0	1.5	-1.7	1.2	1.7
²³⁶ U	-10.6	-8.1	-2.6	-14.6	-5.2	-5.7	-5.0	-3.0	-1.9	-8.9	-0.1	-0.6	-3.1	-5.4
²³⁸ U	0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	0.1	0.1	<0.1	0.2	<0.1
²³⁹ Pu	-4.1	-5.3	-1.2	-2.0	-3.6	-2.4	-1.7	-3.1	<0.1	-4.8	-0.4	-4.3	-0.1	-2.5
²⁴⁰ Pu	-6.4	1.7	-1.8	-3.5	2.3	1.6	-4.4	1.9	-1.3	0.5	-3.4	3.2	-2.5	-0.3
²⁴¹ Pu	-11.9	-1.4	-2.2	-8.1	-1.6	1.1	-2.5	<0.1	-0.8	0.3	-1.7	1.5	-2.4	-1.9
²⁴² Pu	-14.5	1.6	-7.4	-8.6	4.0	3.5	-2.9	6.6	0.8	4.2	-2.9	9.8	0.1	0.3
^{242m} Am	-	-	-	-	19.3	-9.0	-19.4	-	-24.6	-0.5	-16.7	-	-	-8.5
²⁴³ Am	-	-	-	-	7.3	-8.7	-10.3	-	-7.8	-4.2	-2.4	-	-	-4.3
²⁴² Cm	-	-	-	-	-28.0	-28.1	-35.5	-23.4	-30.0	-36.2	-29.9	-26.5	-30.7	-29.8
²⁴⁴ Cm	-	-	-	-	-9.6	-11.6	-19.4	-8.5	-11.3	-9.4	-17.1	-6.0	-9.0	-11.3
¹⁰⁶ Ru	-8.7	2.3	-2.1	-11.5	-	-	-	-	-	-	-	-	-	-5.0
¹³⁴ Cs	-26.0	-22.5	-22.7	-25.5	-23.2	-20.1	-18.7	-40.2	-18.8	-	-19.9	-16.7	-19.0	-23.0
¹³⁷ Cs	1.1	1.4	3.5	3.5	0.3	1.0	2.0	1.2	-0.1	-	0.2	2.0	0.7	1.3
¹⁴⁴ Ce	-2.5	-4.0	1.6	-4.9	-	-	-	-	-	-	-	-	-	-2.4
¹⁴⁸ Nd	-	-	-	-	-1.5	-1.6	-1.5	-1.4	-1.3	-1.5	-1.4	-1.0	-	-1.4
¹⁵⁴ Eu	-	-	-	-	-26.2	-23.8	-12.8	-22.3	-23.5	-	-15.8	-19.4	-22.0	-21.3
					-25.6									

^a(Calculated/measured - 1) × 100%.

^bUsing SAS2H/ORIGEN-S analysis sequence and a 44-group ENDF/B-V cross-section library with data for ¹⁵⁴Eu and ¹⁵⁵Eu taken from ENDF/B-VI.

Table 16. Measured irradiation composition^a of Turkey Point Unit 3 PWR fuel

Assembly ID	D01	D01	D01	D04	D04
Fuel rod ID	G9	G10	H9	G9	G10
Sample ID	15	4	7	9	7
Sample height, cm	167.6	167.0	167.0	167.6	167.0
Burnup, ^b GWd/MTU	30.720	30.510	31.560	31.260	31.310
Atom % burnup	3.200	3.179	3.288	3.256	3.262
²³⁴ U atom %	0.014	0.014	0.013	0.012	0.014
²³⁵ U atom %	0.619	0.599	0.590	0.582	0.598
²³⁶ U atom %	0.342	0.342	0.334	0.332	0.342
²³⁸ U atom %	99.025	99.045	99.063	99.074	99.046
²³⁸ Pu atom %	1.561	1.545	1.592	1.535	1.570
²³⁹ Pu atom %	55.107	54.757	54.806	54.654	54.574
²⁴⁰ Pu atom %	25.701	25.846	25.411	25.553	25.851
²⁴¹ Pu atom %	11.984	11.988	12.177	12.329	12.113
²⁴² Pu atom %	5.647	5.864	6.014	5.929	5.892
¹⁴⁸ Nd/ ²³⁸ U atom ratio ^c	5.66×10^{-4}	5.62×10^{-4}	5.82×10^{-4}	5.76×10^{-4}	5.77×10^{-4}
²³⁹ Pu/ ²³⁸ U atom ratio ^c	5.07×10^{-3}	5.07×10^{-3}	5.17×10^{-3}	5.18×10^{-3}	5.02×10^{-3}

^aRadiochemical analyses conducted after a cooling time of 927 days.

^bBased on measured ¹⁴⁸Nd concentration.

^cPer final ²³⁸U atom.

Table 17. Percentage difference ^a between measured and computed ^b nuclide compositions for Turkey Point Unit 3 PWR samples and averages (27BURNUPLIB library)

Assembly (wt % ²³⁵ U)	D01 (2.556)			D04 (2.556)		Average
	Burnup, GWd/MTU	30.720	30.510	31.560	31.260	
<u>Nuclide</u>						
²³⁴ U	4.4	4.8	10.9	20.8	3.4	8.9
²³⁵ U	-7.1	-2.9	-7.1	-4.2	-7.0	-5.6
²³⁶ U	3.0	2.8	6.5	6.8	3.7	4.6
²³⁸ U	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1
²³⁸ Pu	7.3	6.2	8.5	9.8	11.0	8.6
²³⁹ Pu	5.0	4.9	3.3	3.0	6.3	4.5
²⁴⁰ Pu	-5.2	-6.9	-4.7	-6.3	-4.5	-5.5
²⁴¹ Pu	9.4	8.1	7.4	4.7	10.0	7.9
²⁴² Pu	2.5	-3.4	-0.6	-1.6	2.3	-0.2
¹⁴⁸ Nd	1.6	1.6	1.6	1.6	1.6	1.6

^a(Calculated/measured – 1) × 100%.

^bUsing SAS2H/ORIGEN-S analysis sequence and 27-group cross-section library of SCALE-4.

Table 18. Percentage difference ^a between measured and computed ^b nuclide compositions for Turkey Point Unit 3 PWR samples and averages (44GROUPNDF5 library)

Assembly (wt % ²³⁵ U)	D01 (2.556)			D04 (2.556)		Average
	Burnup, GWd/MTU	30.720	30.510	31.560	31.260	
<u>Nuclide</u>						
²³⁴ U	1.8	2.2	8.1	17.7	0.8	6.1
²³⁵ U	-5.8	-1.5	-5.7	-2.8	-5.7	-4.3
²³⁶ U	3.0	2.7	6.5	6.7	3.6	4.5
²³⁸ U	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1
²³⁸ Pu	1.4	0.4	2.6	3.8	4.9	2.6
²³⁹ Pu	-0.6	-0.7	-2.3	-2.6	0.6	-1.1
²⁴⁰ Pu	0.5	-1.2	1.1	-0.6	1.3	0.2
²⁴¹ Pu	2.8	1.6	0.9	-1.6	3.3	1.4
²⁴² Pu	13.9	7.3	10.4	9.2	13.6	10.9
¹⁴⁸ Nd	1.7	1.6	1.6	1.7	1.7	1.7

^a(Calculated/measured – 1) × 100%.

^bUsing SAS2H/ORIGEN-S analysis sequence and 44-group cross-section library with data for ¹⁵⁴Eu and ¹⁵⁵Eu taken from ENDF/B-VI.

Table 19. Summary of percentage differences^a between measured and computed compositions in this study as averages and spreads

Nuclide	Number of cases	27BURNUPLIB data			44GROUPNDF5 data		
		Average	Max	Min	Average	Max	Min
²³⁴ U	5	8.9	20.8	3.4	6.1	17.7	0.8
²³⁵ U	19	-0.3	5.1	-7.1	0.1	4.8	-5.8
²³⁶ U	19	-2.6	6.8	-14.5	-2.8	6.7	-14.6
²³⁸ U	19	< 0.1	0.2	-0.1	< 0.1	0.2	-0.1
²³⁸ Pu	5	8.6	11.0	6.2	2.6	4.9	0.4
²³⁹ Pu	19	1.0	6.3	-3.7	-2.1	0.6	-5.3
²⁴⁰ Pu	19	-4.4	1.7	-7.0	-0.2	8.2	-6.4
²⁴¹ Pu	19	5.2	10.0	-4.5	-1.0	3.6	-11.9
²⁴² Pu	19	-6.3	2.5	-19.2	3.1	13.9	-14.5
^{242m} Am	6	26.8	60.4	7.8	-8.5	19.3	-24.6
²⁴³ Am	6	-11.1	-4.2	-18.0	-4.3	7.3	-10.3
²⁴² Cm	9	-21.7	-16.6	-30.5	-29.8	-23.4	-36.2
²⁴⁴ Cm	9	-25.6	-20.0	-29.2	-11.3	-6.0	-19.4
¹⁰⁶ Ru	4	-4.5	1.5	-10.5	-5.0	2.3	-11.5
¹³⁴ Cs	13	-20.1	-13.3	-37.7	-23.0	-16.7	-40.2
¹³⁷ Cs	13	1.4	3.5	-0.1	1.3	3.5	-0.1
¹⁴⁴ Ce	4	-2.5	1.5	-5.0	-2.4	1.6	-4.9
¹⁴⁸ Nd	13	-0.3	1.6	-1.7	-0.2	1.7	-1.6
¹⁵⁴ Eu	9	20.9	33.6	8.7	-21.3	-12.8	-26.2

^a(Calculated/measured – 1) × 100%.

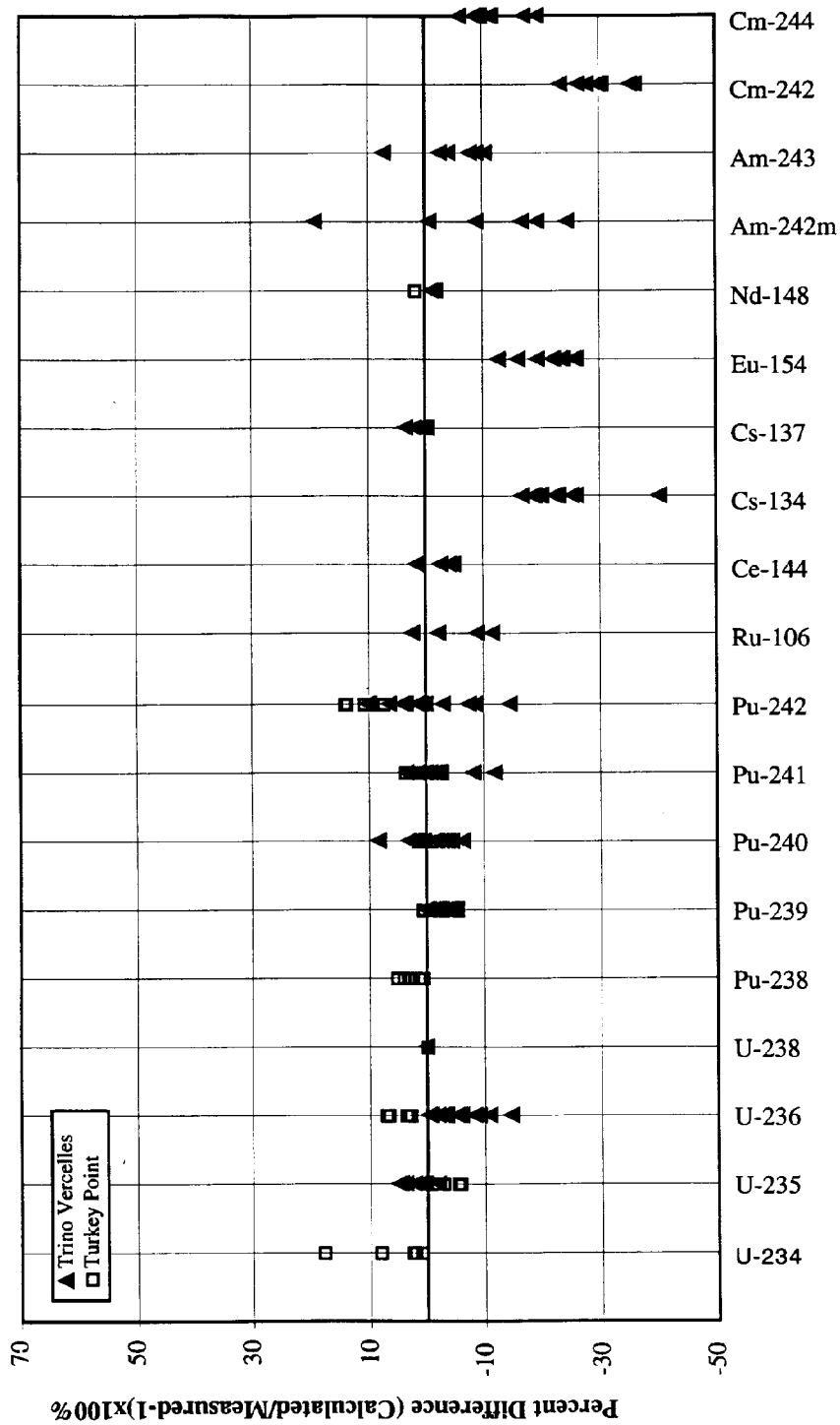


Fig. 4. Percentage difference between measured and calculated results (27BURNUPLIB).

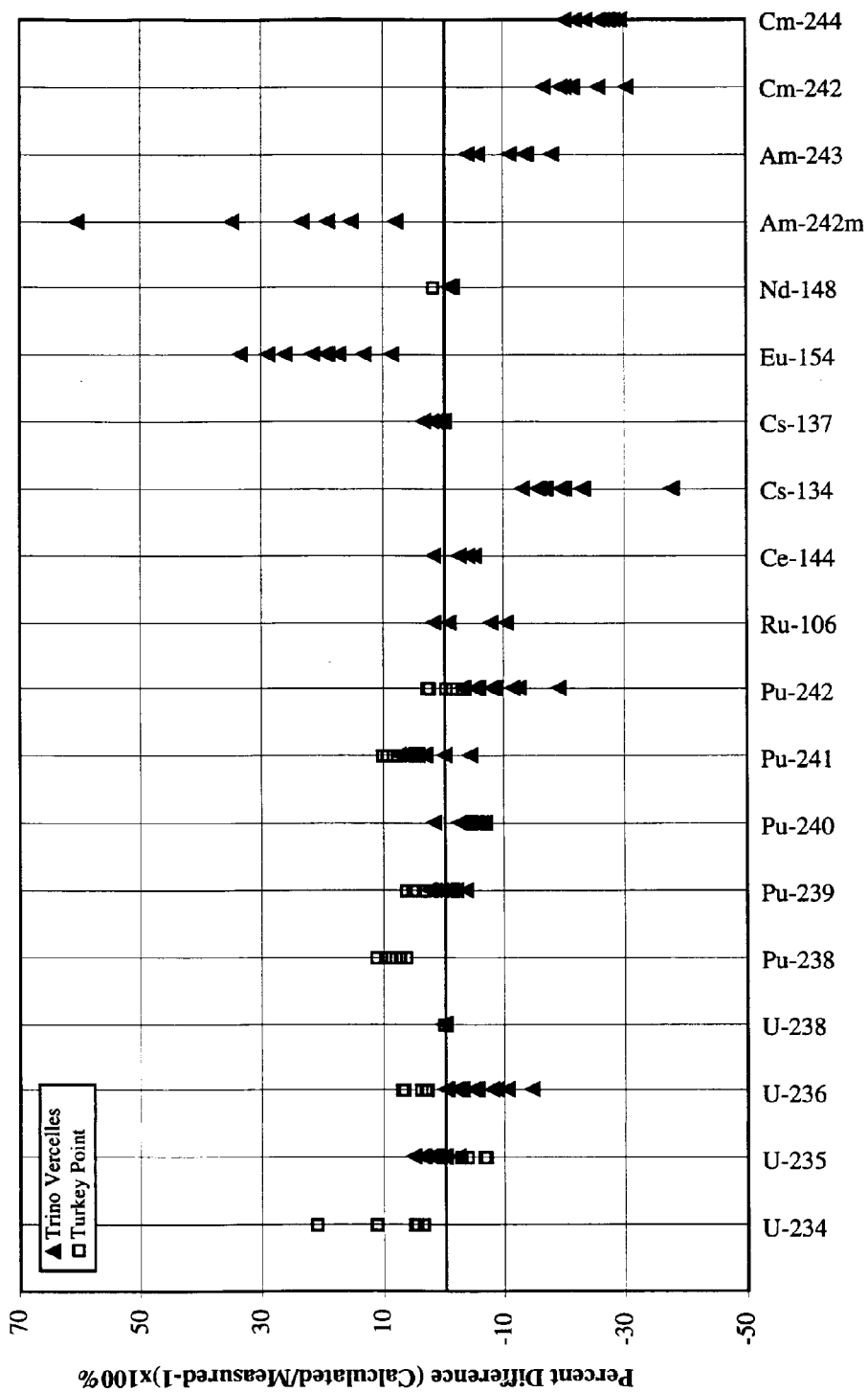


Fig. 5. Percentage difference between measured and calculated results (44GROUPNDF5).

Table 20. Combination of the current and previous validation summaries, listing percentage differences between measured and computed compositions

No.	Nuclide, isobar, or sum of nuclides	Total cases	Average percentage differences ^a					
			27BURNUPLIB data			44GROUPNDF5 data		
			Current ^b	Previous ^c	Combined	Current ^b	Previous ^c	Combined
1	²³⁴ U	14	8.9	4.7	6.2	6.1	1.8	3.3
2	²³⁵ U	38	-0.3	-2.9	-1.6	0.1	-1.9	-0.9
3	²³⁶ U	38	-2.6	0.7	-1.0	-2.8	0.6	-1.1
4	²³⁸ U	32	<0.1	-0.6	-0.3	<0.1	-0.6	-0.3
5	²³⁸ Pu	24	8.6	0.7	2.4	2.6	-4.6	-3.1
6	²³⁹ Pu	38	1.0	5.3	3.1	-2.1	-0.6	-1.3
7	²⁴⁰ Pu	38	-4.4	-5.8	-5.1	-0.2	-0.3	-0.2
8	²⁴¹ Pu	38	5.2	5.0	5.1	-1.0	-1.2	-1.1
9	²⁴² Pu	34	-6.3	-10.3	-8.1	3.1	-0.2	1.7
10	²³⁷ Np	13	–	19.2	19.2	–	6.4	6.4
11	²⁴¹ Am	9	–	-5.9	-5.9	–	-11.0	-11.0
12	^{242m} Am	6	26.8	–	26.8	-8.5	–	-8.5
13	²⁴³ Am	6	-11.1	–	-11.1	-4.3	–	-4.3
14	²⁴² Cm	15	-21.7	-18.7	-20.5	-29.8	-25.0	-27.9
15	²⁴³ Cm + ²⁴⁴ Cm	9	–	-15.8	-15.8	–	-2.3	-2.3
16	²⁴⁴ Cm	15	-25.6	-22.7	-24.4	-11.3	-7.1	-9.6
17	¹⁴ C	3	–	-14.2	-14.2	–	-13.8	-13.8
18	⁷⁹ Se	9	–	14.1	14.1	–	14.0	14.0
19	⁹⁰ Sr	9	–	6.1	6.1	–	6.0	6.0
20	⁹⁹ Tc	13	–	15.8	15.8	–	16.3	16.3
21	¹⁰⁶ Ru	4	-4.5	–	-4.5	-5.0	–	-5.0
22	¹²⁶ Sn	6	–	230.3	230.3	–	229.8	229.8
23	¹²⁹ I	3	–	-10.8	-10.8	–	-10.8	-10.8
24	¹³³ Cs	3	–	1.9	1.9	–	2.5	2.5
25	¹³⁴ Cs	16	-20.1	-8.1	-17.8	-23.0	-11.4	-20.8

Table 20 (continued)

No.	Nuclide, isobar, or sum of nuclides	Total cases	Average percentage differences ^a					
			27BURNUPLIB data			44GROUPNDF5 data		
			Current ^b	Previous ^c	Combined	Current ^b	Previous ^c	Combined
26	¹³⁵ Cs	9	–	10.9	10.9	–	5.7	5.7
27	¹³⁷ Cs	26	1.4	0.9	1.1	1.3	0.8	1.1
28	¹⁴⁴ Ce	4	-2.5	–	-2.5	-2.4	–	-2.4
29	¹⁴³ Nd	3	–	1.3	1.3	–	0.4	0.4
30	¹⁴⁴ Nd	3	–	0.1	0.1	–	0.5	0.5
31	¹⁴⁵ Nd	3	–	0.4	0.4	–	-0.3	-0.3
32	¹⁴⁶ Nd	3	–	0.4	0.4	–	1.1	1.1
33	¹⁴⁸ Nd	16	-0.3	0.3	-0.2	-0.2	0.4	-0.1
34	¹⁵⁰ Nd	3	–	3.2	3.2	–	3.4	3.4
35	¹⁴⁷ Pm... ¹⁴⁷ Sm	3	–	-4.5	-4.5	–	-2.8	-2.8
36	¹⁴⁸ Sm	3	–	-15.9	-15.9	–	-16.9	-16.9
37	¹⁴⁹ Sm	3	–	-30.3	-30.3	–	-35.9	-35.9
38	¹⁵⁰ Sm	3	–	-0.5	-0.5	–	-1.5	-1.5
39	¹⁵¹ Sm... ¹⁵¹ Eu	3	–	26.1	26.1	–	28.1	28.1
40	¹⁵² Sm	3	–	17.3	17.3	–	20.2	20.2
41	¹⁵³ Eu	3	–	-4.8	-4.8	–	5.0	5.0
42	¹⁵⁴ Eu	9	20.9	–	20.9	-21.3	–	-21.3
43	¹⁵⁴ Eu... ¹⁵⁴ Gd	3	–	30.8	30.8	–	-2.1	-2.1
44	¹⁵⁵ Eu... ¹⁵⁵ Gd	3	–	96.0	96.0	–	-24.4	-24.4

^a(Calculated/measured – 1) × 100%.

^bSummary of current study (as in Table 19).

^cSummary of previous study, in ref. 9.

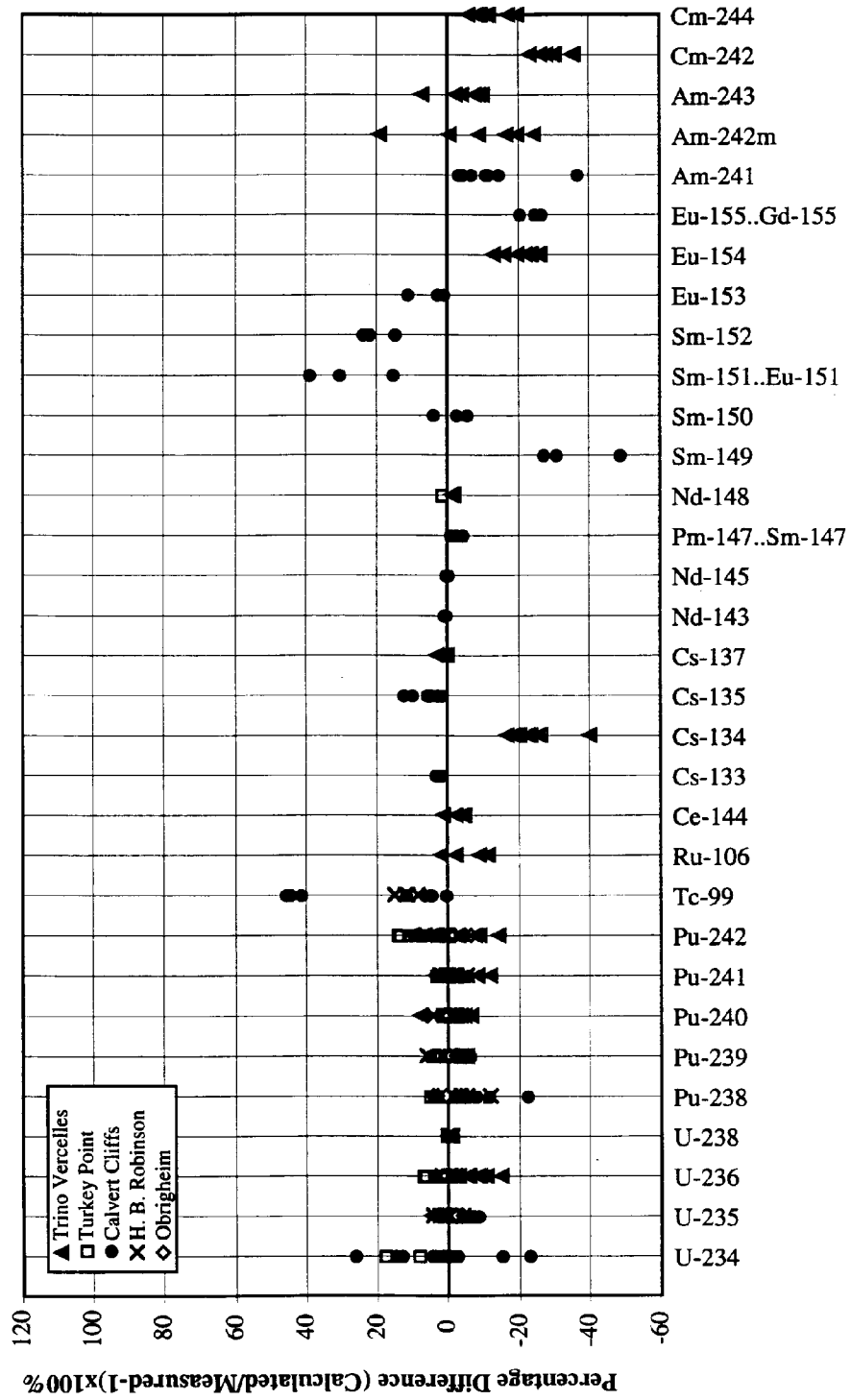


Fig. 6. Combined results for earlier and current validation analyses (27BURNUPLIB).

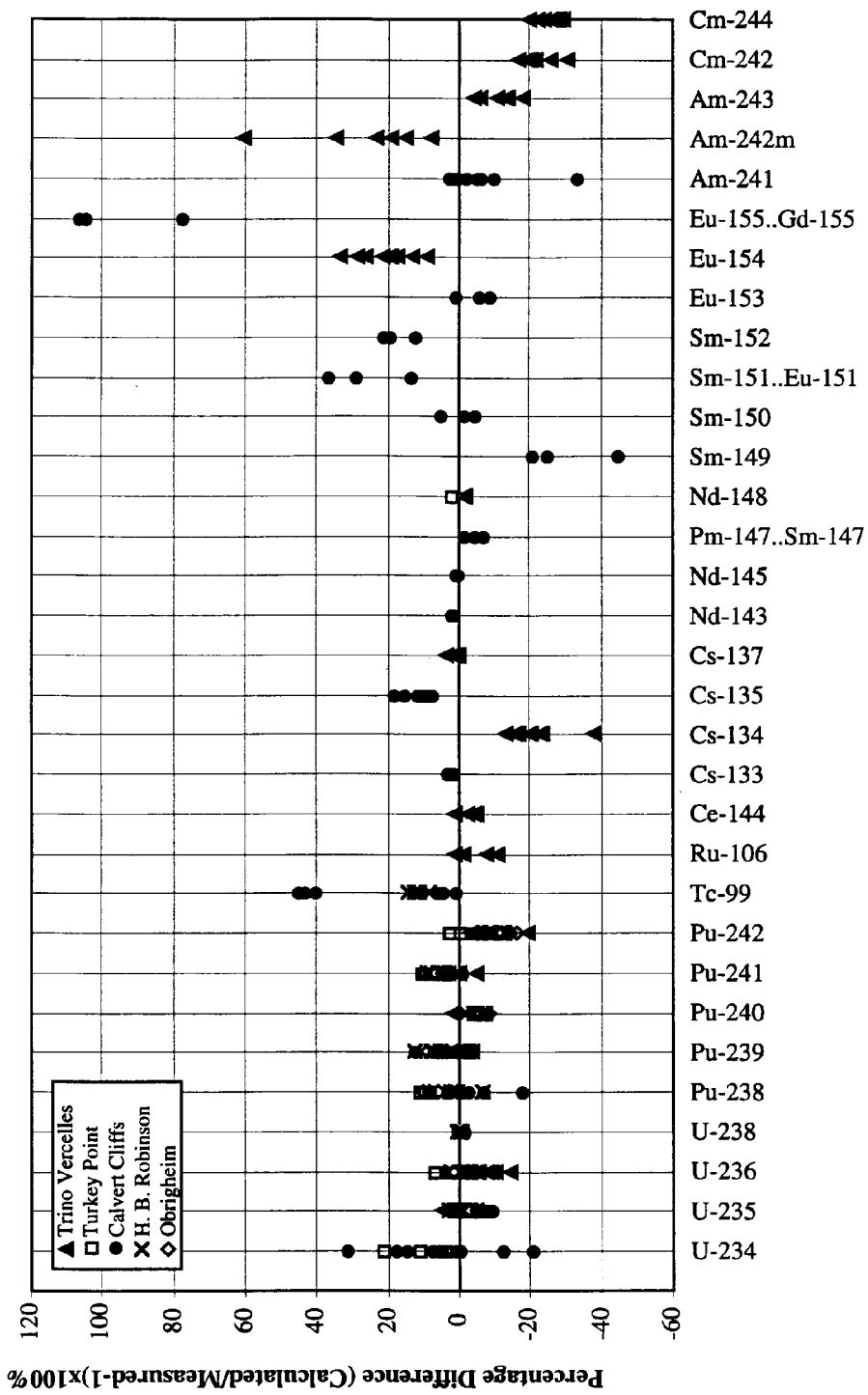


Fig. 7. Combined results for earlier and current validation analyses (44GROUPNDF5).

4. STATISTICAL COMBINATION OF MEASURED-TO-COMPUTED ISOTOPIC RATIOS

Differences between calculated and measured isotopic concentrations for any given fuel sample result from biases and uncertainties in both the calculational method and in the original experimental measurement. Isotopic uncertainty is a consequence of the variation of physical parameters in a random fashion relative to modeled parameters, combined with the random error associated with experimental measurements. Isotopic bias, on the other hand, is the offset between the measured nuclide concentration for a given nuclide and the corresponding calculational prediction of the concentration of that nuclide after accounting for uncertainties. Isotopic bias can result from both the method used in experimental measurements and from the assumptions, data, and method used in computational prediction of nuclide densities.

Reference 3 describes a statistical approach in which the bias and uncertainty terms associated with the prediction of the concentration of a given isotope are estimated from a set of measured-to-calculated ratios. Although the details of this statistical approach are provided in ref. 3, the key aspects are summarized here to provide a basic understanding of the computed parameters provided later in this section.

In this statistical approach, calculational bias is represented by the term \bar{x} , which is defined as the average measured (M) to calculated (C) ratio for a number of comparisons (n) made for a given isotope [i.e., $\bar{x} = (1/n) \sum_1 M_i/C_i$]. Thus, based on a sufficient number of measured-to-calculated ratios, the “expected” isotopic concentration, e , that would be experimentally measured for an additional fuel sample may be estimated from a calculated concentration for that sample, C, by the relationship $e = C \cdot \bar{x}$. This is a best-estimate approach for predicting actual spent fuel contents; however, this does not account for the effect of the uncertainty associated with \bar{x} . The upper and lower bounds on e , e^\pm , are defined as $e^\pm = C \cdot (\bar{x} \pm T \cdot s)$, where s is the standard deviation associated with \bar{x} , and T is a tolerance factor selected for a desired confidence level; the definition and significance of these terms are provided in ref. 3. The term $(\bar{x} \pm T \cdot s)$ is a bounding correction factor for C and is often referred to simply as f .

In a criticality calculation, conservatism would require selecting an upper bound for estimates of productive ($\nu\sigma_f/\sigma_a > 1$) isotopes (also called fissile isotopes) and a lower bound for nonproductive

($v\sigma_f/\sigma_a < 1$), or absorber, nuclides. Thus there are two definitions of f , depending on whether it is calculated for a fissile or absorber nuclide: $f_{\text{fissile}} = \bar{x} + T \cdot s$, and $f_{\text{absorber}} = \bar{x} - T \cdot s$.

Additional conservatism can be included in this approach by prohibiting compensating effects. (Compensating effects can occur when the correction of one nuclide results in a positive increase in system reactivity, while the correction of another nuclide results in a negative offsetting change in reactivity. Hence the negative contribution compensates for the positive effect.) It is mathematically possible that the most conservative correction factor for a given isotope will result in a value of ϵ that is less conservative (in a relative sense) than the calculated concentration. In other words, for a fissile material, if $f_{\text{fissile}} < 1$, then ϵ will be less than C , and C represents the more conservative value (because C would result in increased neutron production). Conversely, for absorber isotopes, $f_{\text{absorber}} > 1$ means that ϵ will be greater than C , and again C represents the more conservative value (in this case, C would result in less neutron absorption). Thus to disallow compensating effects, a modified correction factor, f' , is defined as $f'_{\text{fissile}} = \max[(\bar{x} + T \cdot s), 1]$ for fissile isotopes, and $f'_{\text{absorber}} = \min[(\bar{x} - T \cdot s), 1]$ for absorber isotopes. The modified correction factor, f' , has been developed specifically for the needs of burnup credit applications.³

Based on the measured and computed nuclides provided in Appendices D and E for Trino Vercelles and Turkey Point Unit 3 fuel samples, respectively, and those provided in ref. 9 for 19 other fuel samples, Table 21 provides the values of n (number of independent fuel samples), \bar{x} , s , T , f , and f' for each of the isotopes for which both calculated and measured values are available; calculated values were obtained using the SCALE 27-group cross-section library. Table 22 lists the same parameters with calculated values obtained using the more recently developed SCALE 44-group cross-section library. Note that in both tables T is a tabulated value determined as a function of n for a 95%/95% confidence level. The value of n ranges from as few as 3 samples to as many as 38 spent fuel samples. The value of f calculated based on the earlier subset of measurements (for a more limited set of nuclides) is given in the final column of each table. Note that because no additional measurements were included for most fission products in the current work, f remains unchanged for these nuclides. However, for nuclides for which additional measurements were available, f is seen to improve, for the most part. (Improvement is determined as a revised f value that is closer to 1.0 than the earlier value.)

Table 21. Best-estimate and conservative correction factors for 27BURNUPBLIB results

Isotope	n	\bar{x}	s	$T_{95/95}$	f	f'	f' (earlier work) ^c
¹⁴ C	3 ^b	1.1726	0.109	7.656	0.338	0.338	
⁷⁹ Se	9 ^b	0.8842	0.087	3.031	0.621	0.621	
⁹⁰ Sr	9 ^b	0.9422	0.011	3.031	0.909	0.909	
⁹⁹ Tc	13 ^b	0.8767	0.106	2.671	0.594	0.594	0.594
¹⁰⁶ Ru	4 ^c	1.0494	0.062	5.144	0.730	0.730	
¹²⁶ Sn	6 ^b	0.3085	0.046	3.708	0.138	0.138	
¹²⁹ I	3 ^b	1.1230	0.055	7.656	0.702	0.702	
¹³³ Cs	3 ^b	0.9814	0.007	7.656	0.928	0.928	0.928
¹³⁴ Cs	16	1.2285	0.128	2.524	0.905	0.905	
¹³⁵ Cs	9 ^b	0.9022	0.027	3.031	0.820	0.820	0.820
¹³⁷ Cs	26	0.9892	0.014	2.275	0.957	0.957	
¹⁴⁴ Ce	4 ^c	1.0264	0.029	5.144	0.877	0.877	
¹⁴³ Nd	3 ^b	0.9909	0.008	7.656	0.930	0.930	0.930
¹⁴⁴ Nd	3 ^b	1.0034	0.006	7.656	0.957	0.957	
¹⁴⁵ Nd	3 ^b	0.9961	0.002	7.656	0.981	0.981	0.981
¹⁴⁶ Nd	3 ^b	0.9993	0.006	7.656	0.953	0.953	
¹⁴⁸ Nd	16	0.9997	0.018	2.524	0.954	0.954	
¹⁵⁰ Nd	3 ^b	0.9549	0.017	7.656	0.825	0.825	
¹⁴⁷ Pm... ¹⁴⁷ Sm	3 ^b	1.0346	0.047	7.656	0.675	0.675	0.675
¹⁴⁸ Sm	3 ^b	1.1755	0.031	7.656	0.938	0.938	
¹⁴⁹ Sm	3 ^b	1.3892	0.378	7.656	0.000 ^d	0.000 ^d	0.000
¹⁵⁰ Sm	3 ^b	0.9923	0.048	7.656	0.625	0.625	0.625
¹⁵² Sm	3 ^b	0.8361	0.008	7.656	0.775	0.775	0.775
¹⁵¹ Sm... ¹⁵¹ Eu	3 ^b	0.7703	0.036	7.656	0.495	0.495	0.495
¹⁵³ Eu	3 ^b	1.0369	0.057	7.656	0.601	0.601	0.601
¹⁵⁴ Eu	9 ^c	0.8301	0.053	3.031	0.669	0.669	
¹⁵⁴ Sm... ¹⁵⁴ Gd	3 ^b	0.7603	0.041	7.656	0.446	0.446	
¹⁵⁵ Eu... ¹⁵⁵ Gd	3 ^b	0.5272	0.069	7.656	0.000 ^d	0.000 ^d	0.000
²³⁴ U	14	0.9564	0.128	2.614	0.622	0.622	0.509
²³⁵ U ^a	38	1.0175	0.039	2.141	1.101	1.101	1.115
²³⁶ U	38	1.0119	0.048	2.141	0.909	0.909	0.955
²³⁸ U	32	1.0027	0.005	2.197	0.992	0.992	0.990
²³⁷ Np	13 ^b	0.8467	0.084	2.671	0.622	0.622	
²³⁸ Pu	24	0.9780	0.071	2.309	0.814	0.814	0.830
²³⁹ Pu ^a	38	0.9708	0.036	2.141	1.048	1.048	1.033
²⁴⁰ Pu	38	1.0536	0.021	2.141	1.009	1.000	1.013
²⁴¹ Pu ^a	38	0.9522	0.029	2.141	1.014	1.014	1.016
²⁴² Pu	34	1.0908	0.059	2.176	0.962	0.962	1.006
²⁴¹ Am	9 ^b	1.0800	0.164	3.031	0.583	0.583	0.583
^{242m} Am	6 ^c	0.8016	0.107	3.708	0.405	0.405	
²⁴³ Am	6 ^c	1.1279	0.066	3.708	0.883	0.883	
²⁴² Cm	15	1.2609	0.068	2.566	1.086	1.000	
²⁴³ Cm+ ²⁴⁴ Cm	9 ^b	1.1934	0.094	3.031	0.908	0.908	
²⁴⁴ Cm	15	1.3250	0.052	2.566	1.192	1.000	

^a Fissile isotope.^b Based on measurements reported in ref. 9 only; not measured in current work.^c Based on measurements reported herein; not included in ref. 9.^d Factors less than zero are set to zero, as negative concentrations are meaningless.^e From ref. 8.

Table 22. Best-estimate and conservative correction factors for 44GROUPNDF5 results

Isotope	n	\bar{x}	s	$T_{95/95}$	f	f'	f (earlier work) ^e
¹⁴ C	3 ^b	1.1677	0.108	7.656	0.341	0.341	
⁷⁹ Se	9 ^b	0.8850	0.087	3.031	0.621	0.621	
⁹⁰ Sr	9 ^b	0.9432	0.011	3.031	0.910	0.910	
⁹⁹ Tc	13 ^b	0.8732	0.106	2.671	0.590	0.590	0.590
¹⁰⁶ Ru	4 ^c	1.0563	0.070	5.144	0.696	0.696	
¹²⁶ Sn	6 ^b	0.3088	0.045	3.708	0.142	0.142	
¹²⁹ I	3 ^b	1.1224	0.055	7.656	0.701	0.701	
¹³³ Cs	3 ^b	0.9759	0.009	7.656	0.907	0.907	0.910
¹³⁴ Cs	16	1.2752	0.133	2.524	0.940	0.940	
¹³⁵ Cs	9 ^b	0.9471	0.029	3.031	0.859	0.859	0.859
¹³⁷ Cs	26	0.9894	0.014	2.275	0.958	0.958	
¹⁴⁴ Ce	4 ^c	1.0256	0.030	5.144	0.871	0.871	
¹⁴³ Nd	3 ^b	1.0000	0.005	7.656	0.962	0.962	0.962
¹⁴⁴ Nd	3 ^b	0.9993	0.007	7.656	0.946	0.946	
¹⁴⁵ Nd	3 ^b	1.0032	0.004	7.656	0.973	0.973	0.973
¹⁴⁶ Nd	3 ^b	0.9925	0.007	7.656	0.939	0.939	
¹⁴⁸ Nd	16	0.9992	0.018	2.524	0.954	0.954	
¹⁵⁰ Nd	3 ^b	0.9535	0.017	7.656	0.823	0.823	
¹⁴⁷ Pm... ¹⁴⁷ Sm	3 ^b	1.0170	0.042	7.656	0.695	0.695	
¹⁴⁸ Sm	3 ^b	1.1891	0.029	7.656	0.967	0.967	
¹⁴⁹ Sm	3 ^b	1.5095	0.406	7.656	0.000 ^d	0.000 ^d	0.000
¹⁵⁰ Sm	3 ^b	1.0018	0.050	7.656	0.619	0.619	0.619
¹⁵² Sm	3 ^b	0.8162	0.008	7.656	0.755	0.755	0.755
¹⁵¹ Sm... ¹⁵¹ Eu	3 ^b	0.7584	0.033	7.656	0.506	0.506	0.506
¹⁵³ Eu	3 ^b	0.9395	0.039	7.656	0.641	0.641	0.641
¹⁵⁴ Eu	9 ^c	1.2735	0.070	3.031	1.061	1.000	
¹⁵⁴ Sm... ¹⁵⁴ Gd	3 ^b	1.0144	0.035	7.656	0.746	0.746	
¹⁵⁵ Eu... ¹⁵⁵ Gd	3 ^b	1.3586	0.109	7.656	0.524	0.524	0.524
²³⁴ U	14	0.9829	0.133	2.614	0.635	0.635	0.519
²³⁵ U ^a	38	1.0104	0.035	2.141	1.085	1.085	1.104
²³⁶ U	38	1.0132	0.048	2.141	0.910	0.910	0.956
²³⁸ U	32	1.0026	0.005	2.197	0.992	0.992	0.991
²³⁷ Np	13 ^b	0.9484	0.094	2.671	0.697	0.697	
²³⁸ Pu	24	1.0338	0.077	2.309	0.856	0.856	0.871
²³⁹ Pu ^a	38	1.0142	0.029	2.141	1.076	1.076	1.092
²⁴⁰ Pu	38	1.0030	0.027	2.141	0.945	0.945	0.957
²⁴¹ Pu ^a	38	1.0119	0.035	2.141	1.087	1.087	1.080
²⁴² Pu	34	0.9875	0.064	2.176	0.848	0.848	0.911
²⁴¹ Am	9 ^b	1.1420	0.176	3.031	0.609	0.609	0.609
^{242m} Am	6 ^c	1.1181	0.177	3.708	0.462	0.462	
²⁴³ Am	6 ^c	1.0491	0.066	3.708	0.804	0.804	
²⁴² Cm	15	1.3916	0.087	2.566	1.168	1.000	
²⁴³ Cm+ ²⁴⁴ Cm	9 ^b	1.0266	0.063	3.031	0.836	0.836	
²⁴⁴ Cm	15	1.1090	0.053	2.566	0.973	0.973	

^aFissile isotope.^bBased on measurements reported in ref. 9 only; not measured in current work.^cBased on measurements reported herein; not included in ref. 9.^dFactors less than zero are set to zero, as negative concentrations are meaningless.^eFrom ref. 8.

5. SUMMARY

Knowledge of the isotopic composition of spent commercial LWR fuel is important in many aspects of transportation and storage of the fuel. Because it is not feasible to destructively assay every spent fuel element removed from a reactor, it is necessary to use computational methods to estimate spent fuel contents. The ultimate goal is to provide an adequate prediction of isotopic contents of PWR spent fuel assemblies based solely on calculational methods and to provide an estimate of the uncertainty in that prediction. Thus it is necessary to perform validation studies to assess the accuracy of a computational method relative to reality, where reality is gauged by experimental measurements.

The results presented in Sect. 3 of this report demonstrate the accuracy of the SAS2H sequence in SCALE-4.2 for prediction of isotopic concentrations. As illustrated in Table 20, in comparing the current and the earlier work, no major differences in the ability to predict specific nuclide concentrations are noted. In other words, those nuclides which were predicted within a few percent in the earlier work were predicted within a few percent in the current work, and isotopes for which errors were greater than a few percent in the earlier work were found to be in error by comparable amounts in the current work. This consistency was observed for results obtained from each of the two different cross-section libraries that have been used in the validation studies. This consistency suggests that the estimated biases determined for each of the isotopes in the earlier work are reasonably good estimates, as the additional measurement/calculated ratios resulting from the current work tend to confirm these estimates. The fact that the more recent results are taken from different reactor types and facilities and were based on measurements performed by different organizations than those of the earlier work indicates that the biases are largely independent of other factors or modeling.

In general, the prediction of nuclide inventories for uranium isotopes is within about 1%, with the exception of ^{234}U , which is generally predicted in the range of 2 to 6% (this relatively broad variation may result from the correlation used to estimate the initial loading of this isotope, since these data are not generally directly provided in available references). Predictions for plutonium isotopic concentrations vary by isotope. Plutonium-238 and -242 show the largest variation between measurements; hence these isotopes show the most significant variation between earlier and current

averages. This may be due in part to the small amount of each nuclide present in spent fuel relative to the other plutonium nuclides. Plutonium-239, -240, and -241 are predicted on the order of about 5% using the 27-group library, and within 1 to 2% based on calculations using the 44-group library. Much of the improvement in plutonium prediction for these nuclides using the 44-group library may result from the fact that the group structure for this cross-section library was specifically tailored to capture the 0.3-eV resonance in ^{239}Pu (which, due to low energy and lack of resonance data, cannot be properly modeled via the SCALE Nordheim Integral Treatment module NITAWL-II). This improved cross-section representation not only improves the prediction of ^{239}Pu depletion, but also the production of ^{240}Pu and ^{241}Pu , which are daughter products by absorption.

This study has provided calculation-to-measurement comparisons for a number of important actinides not included in earlier work. Specifically, data are available in the current work for $^{242\text{m}}\text{Am}$ and ^{243}Am , both daughter products of plutonium isotopes by beta decay, and additional measurements for ^{244}Cm are included. The majority of earlier measurements of ^{244}Cm also contained ^{243}Cm ; the current work contains nine new measurements of ^{244}Cm only. Unfortunately, little measurement data are available for fission-product nuclides so that the range of validation data for most fission products is unchanged in this work; however, additional data were included for ^{134}Cs , ^{137}Cs , and ^{148}Nd , and data for three new fission products, ^{106}Ru , ^{144}Ce , and ^{154}Eu , were introduced.

Section 4 of this report provided the means by which spent fuel nuclide concentrations calculated using SCALE-4.2/SAS2H and either of the two cross-section libraries (27BURNUPLIB or 44GROUPLIB) could be converted to a best-estimate prediction for actual spent fuel contents or a conservative representation of the spent fuel isotopic concentration. The latter is conservative in terms of a subsequent criticality analysis (i.e., use of conservative correction factors would result in an upper limit in the multiplication factor computed based on spent fuel contents). Use of best-estimate isotopics (i.e., isotopics corrected via multiplication by \bar{x}) should provide a more realistic estimate for the reactivity of a given spent fuel system; however, it must be recognized that (1) nuclides for which no measurement data exist cannot be validated and are of unknown error, and (2) omission of such nuclides would result in a conservative estimate in total neutron multiplication as these nuclides are neutron absorbers and act to reduce the reactivity worth of the system.

Much work remains in the arena of validation for spent fuel isotopic prediction methods. Although the primary actinides are considered to be well characterized by the up to 38 comparisons

performed, trending analysis as a function of burnup, initial enrichment, and cooling time have not been performed rigorously; such trending analysis may highlight functional dependencies in the data. In addition, large uncertainties are associated with the prediction of fission-product inventories. Calculation of fission-product concentrations have greater uncertainties due to larger uncertainties in fission-product cross-section data. Thus it is imperative that many more measurements of fission-product nuclides be performed for spent fuel samples in order to validate computational methods and data for estimating fission-product contents in spent fuel.

6. REFERENCES

1. *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4), Vols. I, II, and III (April 1995). Available from Radiation Shielding Information Center, Oak Ridge National Laboratory, as CCC-545.
2. T. L. Sanders and R. M. Westfall, "Feasibility and Incentives for Burnup Credit in Spent Fuel Transport Casks," *Nucl. Sci. Eng.* **104** 66 (1990).
3. M. D. DeHart, *Sensitivity and Parametric Evaluations of Significant Aspects of Burnup Credit for PWR Spent Fuel Packages*, ORNL/TM-12973, Lockheed Martin Energy Research Corp., Oak Ridge Natl. Lab., 1996.
4. M. C. Brady, T. L. Sanders, K. D. Seager, and W. H. Lake, "Burnup Credit Issues in Transportation and Storage," *Proc. Tenth International Symposium on the Packaging and Transportation of Radioactive Materials*, September 13-18, 1992, Yokohama City, Japan.
5. S. M. Bowman, M. D. DeHart, and C. V. Parks, "Validation of SCALE-4 for Burnup Credit Applications," *Nucl. Tech.* **110** 53 (April 1995).
6. M. D. DeHart and C. V. Parks, "Issues Related to Criticality Safety Analysis for Burnup Credit," *ICNC '95 Fifth International Conference on Nuclear Criticality Safety*, Albuquerque, N.M., September 17-21, 1995, Vol. 1, pp. 1B-26-36 (1995).
7. "American National Standard for Nuclear Criticality Safety in Operations with Fissionable Materials Outside Reactors," ANSI/ANS-8.1-1983, American Nuclear Society, 1983.
8. M. D. DeHart, O. W. Hermann, and C. V. Parks, "Validation of a Method for Prediction of Isotopic Concentrations in Burnup Credit Applications," *Fifth International Conference on Nuclear Criticality Safety*, Albuquerque, N.M., September 17-21, 1995, Vol. 1, pp. 5-26-34 (1995).
9. O. W. Hermann, S. M. Bowman, M. C. Brady, and C. V. Parks, *Validation of the SCALE System for PWR Spent Fuel Isotopic Composition Analyses*, ORNL/TM-12667, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., 1995.
10. O. W. Hermann and C. V. Parks, "SAS2H: The SCALE-4 Analysis Sequence for LWR Fuel Depletion," *Proc. Seminar on SCALE-4 and Related Modular Systems for the Evaluation of Nuclear Fuel Facilities and Package Design Featuring Criticality, Shielding, and Heat Transfer Capabilities*, September 17-19, 1991, OECD NEA Data Bank, Saclay, 1995.

11. O. W. Hermann and R. M. Westfall, "ORIGEN-S: SCALE System Module to Calculate Fuel Depletion, Actinide Transmutation, Fission Product Buildup and Decay, and Associated Radiation Source Terms," Sect. F7 of *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, Vols. I-III, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4) (April 1995). Available from Radiation Shielding Information Center at Oak Ridge National Laboratory as CCC-545.
12. Y. Naito, M. Kurosawa, and T. Kaneko, *Data Book of the Isotopic Composition of Spent Fuel in Light Water Reactors*, JAERI-M 94-034, Japan Atomic Energy Research Institute, 1994.
13. A. M. Bresesti et al., *Post-Irradiation Analysis of Trino Vercelles Reactor Fuel Elements*, EUR-4909e, Joint Nuclear Research Centre Ispra and Karlsruhe Establishments, 1972.
14. P. Barbero et al., *Post-Irradiation Examination of the Fuel Discharged from the Trino Vercelles Reactor After the 2nd Irradiation Cycle*, *Nuclear Science and Technology*, EUR5605e, Joint Research Centre Ispra and Karlsruhe Establishments, 1977.
15. S. D. Atkin, *Destructive Examination of 3-Cycle LWR Fuel Rods from Turkey Point Unit 3 for the CLIMAX-Spent Fuel Test*, HEDL-TME 80-89, Hanford Engineering Development Laboratory, 1981.
16. J. C. Ryman et al., *Fuel Inventory and Afterheat Power Studies of Uranium-Fueled Pressurized Water Reactor Fuel Assemblies Using the SAS2 and ORIGEN-S Modules of SCALE with an ENDF/B-V Updated Cross Section Library*, NUREG/CR-2397 (ORNL/CSD-90), U.S. Nuclear Regulatory Commission, September 1982.
17. *The Evaluated Nuclear Data File, Versions IV, V, and VI (ENDF/B-IV, V, and VI)*, maintained by the National Data Center at Brookhaven National Laboratory.
18. M. D. DeHart and S. M. Bowman, *Validation of the SCALE Broad Structure 44-Group ENDF/B-V Cross-Section Library for Use in Criticality Safety Analyses*, NUREG/CR-6102 (ORNL/TM-12460), U.S. Nuclear Regulatory Commission, 1994.
19. R. Q. Wright, "Fission Product Evaluations for ENDF/B-VI," *Trans. Am. Nucl. Soc.* **61**, 398-399 (1990).
20. J. B. Melehan, *Yankee Core Evaluation Program Final Report*, WCAP-3017-6094, Westinghouse Electric Corp., 1971.
21. O. W. Hermann, C. V. Parks, and J. P. Renier, "A Proposed Regulatory Guide Basis for Spent Fuel Decay Heat," *Proc. Second Annual International Conference on High Level Radioactive Waste Management*, Vol. 2, Las Vegas, Nevada, April 28-May 3, 1991; also see O. W. Hermann, C. V. Parks, and J. P. Renier, *Technical Support for a Proposed Decay*

Heat Guide Using SAS2H/ORIGEN-S Data, NUREG/CR-5625 (ORNL-6698), U.S. Nuclear Regulatory Commission, 1994.

22. J. W. Roddy et al., *Physical and Decay Characteristics of Commercial LWR Spent Fuel*, ORNL/TM-9591, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., October 1985.

APPENDIX A

DESCRIPTION OF THE SCALE SAS2H DEPLETION APPROACH

SCALE is a well-established code system that has been widely used in away-from-reactor (AFR) applications for spent fuel characterization via the SAS2H analysis sequence.^{A.1} SAS2H is a multicode sequence that determines the isotopic composition of spent fuel using the ORIGEN-S code^{A.2} for depletion and decay calculations and a 1-D neutronics model of an LWR fuel assembly to prepare burnup-dependent cross sections for ORIGEN-S. Isotopic concentrations used in the subsequent spent fuel criticality calculations are based on the results of SAS2H calculations.

The SAS2H control module was originally developed for the SCALE code system to provide a sequence that generated radiation source terms for spent fuel and subsequently utilized these sources with a 1-D shielding analysis of a shipping cask. However, in addition to the calculation of source terms, SAS2H is now often used to obtain decay heat and spent fuel isotopics. Within the scope of validation activities described in this report, SAS2H is used solely for the prediction of spent fuel isotopics.

Six different modules are invoked by the SAS2H sequence for performing a complete fuel depletion analysis. The SCALE-4 system driver provides automated data handling and code execution for each step of the process. This procedure begins with the SCALE Material Information Processor^{A.3} which generates number densities and related information, prepares geometry data for resonance self-shielding and flux-weighting cell calculations, and creates data input files for the cross-section processing codes. BONAMI^{A.4} applies the Bondarenko method of resonance self-shielding for nuclides which have Bondarenko data included in the cross-section library. NITAWL-II^{A.5} performs Nordheim resonance self-shielding corrections for nuclides that have resonance parameters included with their cross-section data. XSDRNPM^{A.6} is a 1-D discrete ordinates code that performs radiation transport calculations based on geometric data passed to it by SAS2H and produces cell-weighted cross sections for fuel depletion calculations. The COUPLE code^{A.7} updates cross-section constants included on the ORIGEN-S nuclear data library with data from the cell-weighted cross-section library produced by XSDRNPM. COUPLE also uses the XSDRNPM-computed weighting spectrum to update nuclide cross sections for remaining nuclides. Finally, the ORIGEN-S code is used to perform nuclide generation and depletion calculations for a specified reactor fuel history.

The process used by SAS2H in calculation of spent fuel isotopics is illustrated schematically in Fig. A.1. The calculation starts with input-specified data describing a fuel assembly as it is initially loaded into a reactor. The initial composition, average temperatures, geometry, and time-dependent specific power of the fuel assembly are required. The SAS2H sequence performs 1-D neutron transport analysis of the reactor fuel assembly using XSDRNPM and a two-part procedure with two separate unit-cell-lattice models. The first model (Path A of Fig. 1) is a unit fuel-pin cell from which cell-weighted cross sections are obtained. The second model (Path B of Fig. 1) represents a larger unit cell (e.g., an assembly) within an infinite lattice. The larger unit cell zones can be structured for different assembly designs to account for assembly-specific attributes (i.e., water holes, burnable poison rods, etc.). Problem-dependent resonance self-shielding of cross sections is performed prior to each XSDRNPM calculation using the BONAMI and NITAWL-II codes. The neutron flux spectrum obtained from the second (assembly) unit-cell model is used to determine the appropriate nuclide cross sections for the burnup-dependent fuel composition. The cross sections derived from XSDRNPM calculations at each time step are used in an ORIGEN-S point-depletion computation that produces the burnup-dependent fuel compositions to be used in the next spectrum calculation. This sequence is repeated in user-specified burnup steps for a complete assembly operating history. The buildup and decay of nuclides in the fuel assembly is then computed by ORIGEN-S in a final pass based on the assembly's cooling time (i.e., the period of time after final exposure time). Note that ORIGEN-S calculations have no spatial dependence. The neutron flux used to produce the ORIGEN-S cross sections is based on a radial average of an infinitely long uniform assembly with characteristics per input specifications. These specifications (e.g., burnup, specific power, moderator temperature, etc.) can be representative of any axial location along the fuel assembly or an axial average of the fuel assembly.

More than 1000 nuclides are tracked by ORIGEN-S during depletion and decay calculations. (Note that ORIGEN-S tracks all decay chains, but does not account for the loss of volatile isotopes; however, any released nuclides represent an insignificant fraction of the total fission-product inventory, and their inclusion should have an insignificant effect on the isotopic calculations.)

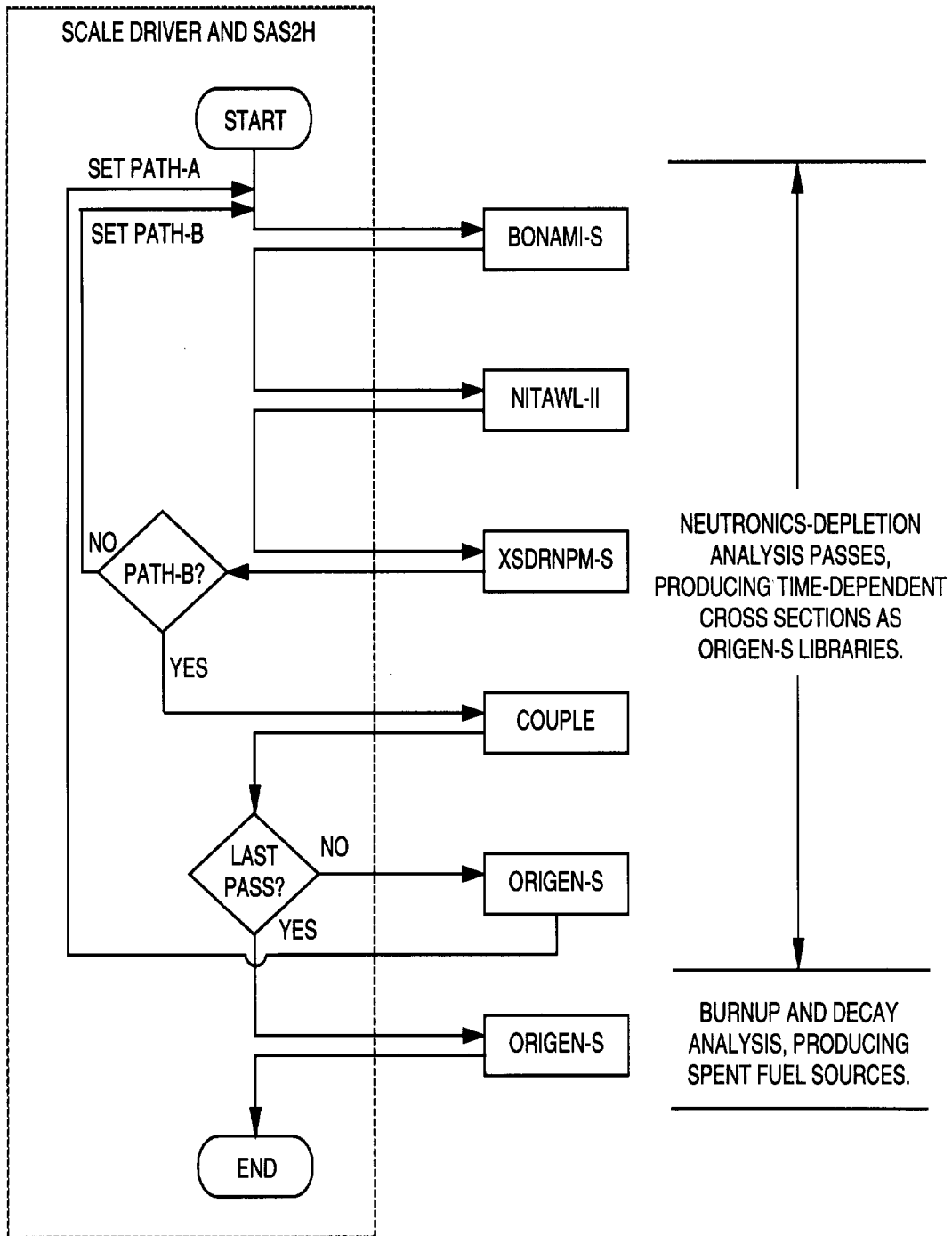


Fig. A.1. Flow path invoked in SAS2H depletion and decay sequences.

Burnup-dependent cross sections are processed by SAS2H only for a select set of user-specified nuclides. These nuclides are those found to be most important for depletion calculations in LWR fuels and are listed in Table A.1. Cross sections for remaining isotopes are obtained from the ORIGEN-S one-group LWR library and are adjusted with burnup using ORIGEN-S spectral parameters (THERM, RES, and FAST)^{A,2} calculated using fluxes determined by XSDRNPM. The ORIGEN-S one-group LWR library available in SCALE-4 has been updated to use cross sections from the SCALE-4 27-group burnup library for all 193 nuclides in that library. The update was performed by extracting one-group cross sections from the output of a low-burnup LWR-type fuel.

Table A.1. List of fuel nuclides automatically included by SAS2 for neutronics processing^a

¹³⁵ Xe	²³⁸ Pu	^{242m} Am
¹³³ Cs	²³⁹ Pu	²⁴³ Am
²³⁴ U	²⁴⁰ Pu	²⁴² Cm
²³⁵ U	²⁴¹ Pu	²⁴³ Cm
²³⁶ U	²⁴² Pu	²⁴⁴ Cm
²³⁸ U	²⁴¹ Am	1/v-absorber ^b
²³⁷ Np		

^aUnless overridden by user input, these nuclides are added to the initial fuel mixture with a number density of 10⁻²⁰ atoms/b-cm.

^bUsed to calculate the THERM parameters applied in ORIGEN-S (see Sect. F7 of ref. 1).

References

- A.1 O. W. Hermann and C. V. Parks, "SAS2H: A Coupled One-Dimensional Depletion and Shielding Analysis Code," Sect. S2 of *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4), Vols. I, II, and III (April 1995). Available from Radiation Shielding Information Center as CCC-545.
- A.2 O. W. Hermann and R. M. Westfall, "ORIGEN-S: A SCALE System Module to Calculate Fuel-Depletion, Actinide Transmutation, Fission Product Buildup and Decay, and Associated Radiation Source Terms," Sect. F7 of *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4), Vols. I, II, and III (April 1995). Available from Radiation Shielding Information Center as CCC-545.
- A.3 N. F. Landers et al., "The Material Information Processor for SCALE," Sect. M7 of *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4), Vols. I, II, and III (April 1995). Available from Radiation Shielding Information Center as CCC-545.
- A.4 N. M. Greene, "BONAMI: Resonance Self-Shielding by the Bondarenko Method," Sect. F1 of *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4), Vols. I, II, and III (April 1995). Available from Radiation Shielding Information Center as CCC-545.
- A.5 N. M. Greene, "NITAWL-II: SCALE System Module for Performing Resonance Shielding and Working Library Production," Sect. F2 of *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4), Vols. I, II, and III (April 1995). Available from Radiation Shielding Information Center as CCC-545.
- A.6 N. M. Greene and L. M. Petrie, "XSDRNPM: A One-Dimensional Discrete-Ordinates Code for Transport Analysis," Sect. F3 of *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4), Vols. I, II, and III (April 1995). Available from Radiation Shielding Information Center as CCC-545.
- A.7 O. W. Hermann, "COUPLE: SCALE System Module to Process Problem-Dependent Cross Sections and Neutron Spectral Data for ORIGEN-S Analyses," Sect. F6 of *SCALE: A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation*, NUREG/CR-0200, Rev. 4 (ORNL/NUREG/CSD-2/R4), Vols. I, II, and III (April 1995). Available from Radiation Shielding Information Center as CCC-545.

APPENDIX B

INPUT LISTINGS FOR TRINO VERCELLES SAS2H DEPLETION CALCULATION

Assembly 509-104, Rod M11, Axial Level 7, with a Burnup of 12.042 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
trino vercelles pwr, 509-104, rod m11 7, 12.042 gwd/mtu, b4, July-95
'
  Input File Name: trino104m1117b4
'
-----
  cooled 10 d, axial-dependent h2o density & temperature
'
  in reactor for cycle 1 only
'
  using ag-in-cd absorber in mix 6, estimated densities
  applying an effective control-rod mockup, period dependent, with uo2
'
  ***** endf/b-4 *****
  .....SCALE Version 4.2p, /scale4.2p/ .....
'
-----
  mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.079 1 1001
    92234 0.035 92235 3.897 92236 0.018 92238 96.050  end
co-59 3 0 1-20 543  end
zr-94 1 0 1-20 1001  end
mo-94 1 0 1-20 1001  end
nb-95 1 0 1-20 1001  end
mo-95 1 0 1-20 1001  end
tc-99 1 0 1-20 1001  end
rh-103 1 0 1-20 1001  end
rh-105 1 0 1-20 1001  end
ru-106 1 0 1-20 1001  end
sn-126 1 0 1-20 1001  end
xe-131 1 0 1-20 1001  end
cs-134 1 0 1-20 1001  end
cs-135 1 0 1-20 1001  end
cs-137 1 0 1-20 1001  end
pr-143 1 0 1-20 1001  end
nd-143 1 0 1-20 1001  end
ce-144 1 0 1-20 1001  end
nd-144 1 0 1-20 1001  end
nd-145 1 0 1-20 1001  end
nd-146 1 0 1-20 1001  end
nd-147 1 0 1-20 1001  end
pm-147 1 0 1-20 1001  end
sm-147 1 0 1-20 1001  end
nd-148 1 0 1-20 1001  end
pm-148 1 0 1-20 1001  end
sm-148 1 0 1-20 1001  end
pm-149 1 0 1-20 1001  end
sm-149 1 0 1-20 1001  end
nd-150 1 0 1-20 1001  end
sm-150 1 0 1-20 1001  end
sm-151 1 0 1-20 1001  end
eu-151 1 0 1-20 1001  end
sm-152 1 0 1-20 1001  end
eu-153 1 0 1-20 1001  end
eu-154 1 0 1-20 1001  end
gd-154 1 0 1-20 1001  end
eu-155 1 0 1-20 1001  end
gd-155 1 0 1-20 1001  end
gd-157 1 0 1-20 1001  end
gd-158 1 0 1-20 1001  end
gd-160 1 0 1-20 1001  end
h2o 3 den=0.7795 1 543  end
```

```

arbm-bormod 0.7795 1 1 0 0 5000 100 3 1175.0e-6 543 end
'
' 1175 ppm boron (wt) in moderator
' -----
ss304 2 1 570 end
arbm-ag 10.159 1 1 0 1 47000 100 6 0.80 543 end
arbm-in 10.159 1 1 0 1 49000 100 6 0.15 543 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 543 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=3 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=10.390 burn=226 down=86 end
power=16.138 burn=263 down=51 bfrac=0.7234 end
power=18.663 burn=292 down=10 bfrac=0.2766 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-032, Rod E11, Axial Level 4, with a Burnup of 15.377 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
trino vercelles pwr, 509-032, rod e11, level 4, 15.377 gwd/mtu, b4, july-95
'
'   Input File Name: trino32e1114b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2  1 den=10.079  1 1015
    92234 0.028 92235 3.13  92236 0.014 92238 96.828  end
co-59  3 0 1-20 557  end
zr-94  1 0 1-20 1015  end
mo-94  1 0 1-20 1015  end
nb-95  1 0 1-20 1015  end
mo-95  1 0 1-20 1015  end
tc-99  1 0 1-20 1015  end
rh-103 1 0 1-20 1015  end
rh-105 1 0 1-20 1015  end
ru-106 1 0 1-20 1015  end
sn-126 1 0 1-20 1015  end
xe-131 1 0 1-20 1015  end
cs-134 1 0 1-20 1015  end
cs-135 1 0 1-20 1015  end
cs-137 1 0 1-20 1015  end
pr-143 1 0 1-20 1015  end
nd-143 1 0 1-20 1015  end
ce-144 1 0 1-20 1015  end
nd-144 1 0 1-20 1015  end
nd-145 1 0 1-20 1015  end
nd-146 1 0 1-20 1015  end
nd-147 1 0 1-20 1015  end
pm-147 1 0 1-20 1015  end
sm-147 1 0 1-20 1015  end
nd-148 1 0 1-20 1015  end
pm-148 1 0 1-20 1015  end
sm-148 1 0 1-20 1015  end
pm-149 1 0 1-20 1015  end
sm-149 1 0 1-20 1015  end
nd-150 1 0 1-20 1015  end
sm-150 1 0 1-20 1015  end
sm-151 1 0 1-20 1015  end
eu-151 1 0 1-20 1015  end
sm-152 1 0 1-20 1015  end
eu-153 1 0 1-20 1015  end
eu-154 1 0 1-20 1015  end
gd-154 1 0 1-20 1015  end
eu-155 1 0 1-20 1015  end
gd-155 1 0 1-20 1015  end
gd-157 1 0 1-20 1015  end
gd-158 1 0 1-20 1015  end
gd-160 1 0 1-20 1015  end
ss304  2 1  570  end
h2o  3 den=0.7554  1  557  end
arbm-bormod  0.7554 1 1 0 0 5000 100 3 1175.0e-6  557  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag  10.159 1 1 0 1 47000 100 6 0.80  557  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 557 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 557 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=3 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.268 burn=226 down=86 end
power=20.607 burn=263 down=51 bfrac=0.7234 end
power=23.831 burn=292 down=10 bfrac=0.2766 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-032, Rod E11, Axial Level 7, with a Burnup of 15.898 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
trino vercelles pwr, 509-032, rod e11 7, 15.898 gwd/mtu, b4, july-95
'
'   Input File Name: trino32e1117b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 only
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2  1 den=10.079  1 1001
    92234 0.028 92235 3.13  92236 0.014 92238 96.828  end
co-59  3 0 1-20 543  end
zr-94  1 0 1-20 1001  end
mo-94  1 0 1-20 1001  end
nb-95  1 0 1-20 1001  end
mo-95  1 0 1-20 1001  end
tc-99  1 0 1-20 1001  end
rh-103 1 0 1-20 1001  end
rh-105 1 0 1-20 1001  end
ru-106 1 0 1-20 1001  end
sn-126 1 0 1-20 1001  end
xe-131 1 0 1-20 1001  end
cs-134 1 0 1-20 1001  end
cs-135 1 0 1-20 1001  end
cs-137 1 0 1-20 1001  end
pr-143 1 0 1-20 1001  end
nd-143 1 0 1-20 1001  end
ce-144 1 0 1-20 1001  end
nd-144 1 0 1-20 1001  end
nd-145 1 0 1-20 1001  end
nd-146 1 0 1-20 1001  end
nd-147 1 0 1-20 1001  end
pm-147 1 0 1-20 1001  end
sm-147 1 0 1-20 1001  end
nd-148 1 0 1-20 1001  end
pm-148 1 0 1-20 1001  end
sm-148 1 0 1-20 1001  end
pm-149 1 0 1-20 1001  end
sm-149 1 0 1-20 1001  end
nd-150 1 0 1-20 1001  end
sm-150 1 0 1-20 1001  end
sm-151 1 0 1-20 1001  end
eu-151 1 0 1-20 1001  end
sm-152 1 0 1-20 1001  end
eu-153 1 0 1-20 1001  end
eu-154 1 0 1-20 1001  end
gd-154 1 0 1-20 1001  end
eu-155 1 0 1-20 1001  end
gd-155 1 0 1-20 1001  end
gd-157 1 0 1-20 1001  end
gd-158 1 0 1-20 1001  end
gd-160 1 0 1-20 1001  end
h2o  3 den=0.7795  1 543  end
arbm-bormod  0.7795 1 1 0 0 5000 100 3 1175.0e-6  543  end
'
'   1175 ppm boron (wt) in moderator
'-----
ss304  2 1 570  end
arbm-ag  10.159 1 1 0 1 47000 100 6 0.80  543  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 543 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 543 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=3 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.717 burn=226 down=86 end
power=21.306 burn=263 down=51 bfrac=0.7234 end
power=24.639 burn=292 down=10 bfrac=0.2766 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-032, Rod E11, Axial Level 9, with a Burnup of 11.529 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
trino vercelles pwr, 509-032, rod e11 9, 11.529 gwd/mtu, b4, july-95
'
'   Input File Name: trino32e1119b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 only
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.079 1 927
    92234 0.028 92235 3.13 92236 0.014 92238 96.828  end
co-59 3 0 1-20 537  end
zr-94 1 0 1-20 927  end
mo-94 1 0 1-20 927  end
nb-95 1 0 1-20 927  end
mo-95 1 0 1-20 927  end
tc-99 1 0 1-20 927  end
rh-103 1 0 1-20 927  end
rh-105 1 0 1-20 927  end
ru-106 1 0 1-20 927  end
sn-126 1 0 1-20 927  end
xe-131 1 0 1-20 927  end
cs-134 1 0 1-20 927  end
cs-135 1 0 1-20 927  end
cs-137 1 0 1-20 927  end
pr-143 1 0 1-20 927  end
nd-143 1 0 1-20 927  end
ce-144 1 0 1-20 927  end
nd-144 1 0 1-20 927  end
nd-145 1 0 1-20 927  end
nd-146 1 0 1-20 927  end
nd-147 1 0 1-20 927  end
pm-147 1 0 1-20 927  end
sm-147 1 0 1-20 927  end
nd-148 1 0 1-20 927  end
pm-148 1 0 1-20 927  end
sm-148 1 0 1-20 927  end
pm-149 1 0 1-20 927  end
sm-149 1 0 1-20 927  end
nd-150 1 0 1-20 927  end
sm-150 1 0 1-20 927  end
sm-151 1 0 1-20 927  end
eu-151 1 0 1-20 927  end
sm-152 1 0 1-20 927  end
eu-153 1 0 1-20 927  end
eu-154 1 0 1-20 927  end
gd-154 1 0 1-20 927  end
eu-155 1 0 1-20 927  end
gd-155 1 0 1-20 927  end
gd-157 1 0 1-20 927  end
gd-158 1 0 1-20 927  end
gd-160 1 0 1-20 927  end
h2o 3 den=0.7885 1 537  end
arbm-bormod 0.7885 1 1 0 0 5000 100 3 1175.0e-6 537  end
'
'   1175 ppm boron (wt) in moderator
'-----
ss304 2 1 570  end
arbm-ag 10.159 1 1 0 1 47000 100 6 0.80 537  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 537 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 537 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=3 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=9.947 burn=226 down=86 end
power=15.451 burn=263 down=51 bfrac=0.7234 end
power=17.868 burn=292 down=10 bfrac=0.2766 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```


Assembly 509-069, Rod E11, Axial Level 1, with a Burnup of 12.859 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod e11, level 1, 12.859 gwd/mtu, b4, july-95
'
'   Input File Name: trino69e1111b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.079 1 915
    92234 0.028 92235 3.13 92236 0.014 92238 96.828  end
co-59 3 0 1-20 563  end
zr-94 1 0 1-20 915  end
mo-94 1 0 1-20 915  end
nb-95 1 0 1-20 915  end
mo-95 1 0 1-20 915  end
tc-99 1 0 1-20 915  end
rh-103 1 0 1-20 915  end
rh-105 1 0 1-20 915  end
ru-106 1 0 1-20 915  end
sn-126 1 0 1-20 915  end
xe-131 1 0 1-20 915  end
cs-134 1 0 1-20 915  end
cs-135 1 0 1-20 915  end
cs-137 1 0 1-20 915  end
pr-143 1 0 1-20 915  end
nd-143 1 0 1-20 915  end
ce-144 1 0 1-20 915  end
nd-144 1 0 1-20 915  end
nd-145 1 0 1-20 915  end
nd-146 1 0 1-20 915  end
nd-147 1 0 1-20 915  end
pm-147 1 0 1-20 915  end
sm-147 1 0 1-20 915  end
nd-148 1 0 1-20 915  end
pm-148 1 0 1-20 915  end
sm-148 1 0 1-20 915  end
pm-149 1 0 1-20 915  end
sm-149 1 0 1-20 915  end
nd-150 1 0 1-20 915  end
sm-150 1 0 1-20 915  end
sm-151 1 0 1-20 915  end
eu-151 1 0 1-20 915  end
sm-152 1 0 1-20 915  end
eu-153 1 0 1-20 915  end
eu-154 1 0 1-20 915  end
gd-154 1 0 1-20 915  end
eu-155 1 0 1-20 915  end
gd-155 1 0 1-20 915  end
gd-157 1 0 1-20 915  end
gd-158 1 0 1-20 915  end
gd-160 1 0 1-20 915  end
ss304 2 1 570  end
h2o 3 den=0.7365 1 563  end
arbm-bormod 0.7365 1 1 0 0 5000 100 3 1175.0e-6 563  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag 10.159 1 1 0 1 47000 100 6 0.80 563  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 563 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 563 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=7.148 burn=226 down=86 end
power=11.101 burn=263 down=51 bfrac=0.7234 end
power=12.840 burn=292 down=1117 bfrac=0.2766 end
power=10.997 burn=416 down=10 bfrac=0.5532 h2ofrac=1.026 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-069, Rod E11, Axial Level 2, with a Burnup of 20.602 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod e11, level 2, 20.602 gwd/mtu, b4, july-95
'
'   Input File Name: trino69e1112b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.079 1 968
    92234 0.028 92235 3.13 92236 0.014 92238 96.828  end
co-59 3 0 1-20 561  end
zr-94 1 0 1-20 968  end
mo-94 1 0 1-20 968  end
nb-95 1 0 1-20 968  end
mo-95 1 0 1-20 968  end
tc-99 1 0 1-20 968  end
rh-103 1 0 1-20 968  end
rh-105 1 0 1-20 968  end
ru-106 1 0 1-20 968  end
sn-126 1 0 1-20 968  end
xe-131 1 0 1-20 968  end
cs-134 1 0 1-20 968  end
cs-135 1 0 1-20 968  end
cs-137 1 0 1-20 968  end
pr-143 1 0 1-20 968  end
nd-143 1 0 1-20 968  end
ce-144 1 0 1-20 968  end
nd-144 1 0 1-20 968  end
nd-145 1 0 1-20 968  end
nd-146 1 0 1-20 968  end
nd-147 1 0 1-20 968  end
pm-147 1 0 1-20 968  end
sm-147 1 0 1-20 968  end
nd-148 1 0 1-20 968  end
pm-148 1 0 1-20 968  end
sm-148 1 0 1-20 968  end
pm-149 1 0 1-20 968  end
sm-149 1 0 1-20 968  end
nd-150 1 0 1-20 968  end
sm-150 1 0 1-20 968  end
sm-151 1 0 1-20 968  end
eu-151 1 0 1-20 968  end
sm-152 1 0 1-20 968  end
eu-153 1 0 1-20 968  end
eu-154 1 0 1-20 968  end
gd-154 1 0 1-20 968  end
eu-155 1 0 1-20 968  end
gd-155 1 0 1-20 968  end
gd-157 1 0 1-20 968  end
gd-158 1 0 1-20 968  end
gd-160 1 0 1-20 968  end
ss304 2 1 570  end
h2o 3 den=0.7407 1 561  end
arbm-bormod 0.7407 1 1 0 0 5000 100 3 1175.0e-6 561  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag 10.159 1 1 0 1 47000 100 6 0.80 561  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 561 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 561 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=11.452 burn=226 down=86 end
power=17.786 burn=263 down=51 bfrac=0.7234 end
power=20.571 burn=292 down=1117 bfrac=0.2766 end
power=17.619 burn=416 down=10 bfrac=0.5532 h2ofrac=1.025 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-069, Rod E11, Axial Level 4, with a Burnup of 23.718 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod e11, level 4, 23.718 gwd/mtu, b4, july-95
'
'   Input File Name: trino69e1114b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.079 1 1015
    92234 0.028 92235 3.13 92236 0.014 92238 96.828  end
co-59 3 0 1-20 553  end
zr-94 1 0 1-20 1015  end
mo-94 1 0 1-20 1015  end
nb-95 1 0 1-20 1015  end
mo-95 1 0 1-20 1015  end
tc-99 1 0 1-20 1015  end
rh-103 1 0 1-20 1015  end
rh-105 1 0 1-20 1015  end
ru-106 1 0 1-20 1015  end
sn-126 1 0 1-20 1015  end
xe-131 1 0 1-20 1015  end
cs-134 1 0 1-20 1015  end
cs-135 1 0 1-20 1015  end
cs-137 1 0 1-20 1015  end
pr-143 1 0 1-20 1015  end
nd-143 1 0 1-20 1015  end
ce-144 1 0 1-20 1015  end
nd-144 1 0 1-20 1015  end
nd-145 1 0 1-20 1015  end
nd-146 1 0 1-20 1015  end
nd-147 1 0 1-20 1015  end
pm-147 1 0 1-20 1015  end
sm-147 1 0 1-20 1015  end
nd-148 1 0 1-20 1015  end
pm-148 1 0 1-20 1015  end
sm-148 1 0 1-20 1015  end
pm-149 1 0 1-20 1015  end
sm-149 1 0 1-20 1015  end
nd-150 1 0 1-20 1015  end
sm-150 1 0 1-20 1015  end
sm-151 1 0 1-20 1015  end
eu-151 1 0 1-20 1015  end
sm-152 1 0 1-20 1015  end
eu-153 1 0 1-20 1015  end
eu-154 1 0 1-20 1015  end
gd-154 1 0 1-20 1015  end
eu-155 1 0 1-20 1015  end
gd-155 1 0 1-20 1015  end
gd-157 1 0 1-20 1015  end
gd-158 1 0 1-20 1015  end
gd-160 1 0 1-20 1015  end
ss304 2 1 570  end
h2o 3 den=0.7554 1 553  end
arbm-bormod 0.7554 1 1 0 0 5000 100 3 1175.0e-6 553  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag 10.159 1 1 0 1 47000 100 6 0.80 553  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 553 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 553 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.184 burn=226 down=86 end
power=20.476 burn=263 down=51 bfrac=0.7234 end
power=23.683 burn=292 down=1117 bfrac=0.2766 end
power=20.283 burn=416 down=10 bfrac=0.5532 h2ofrac=1.023 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-069, Rod E11, Axial Level 7, with a Burnup of 24.304 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod e11, level 7, 24.304 gwd/mtu, b5, july-95
'
'   Input File Name: trino69e1117b5
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-5 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.079 1 1001
    92234 0.028 92235 3.13 92236 0.014 92238 96.828  end
co-59 3 0 1-20 540  end
zr-94 1 0 1-20 1001  end
mo-94 1 0 1-20 1001  end
nb-95 1 0 1-20 1001  end
mo-95 1 0 1-20 1001  end
tc-99 1 0 1-20 1001  end
rh-103 1 0 1-20 1001  end
rh-105 1 0 1-20 1001  end
ru-106 1 0 1-20 1001  end
sn-126 1 0 1-20 1001  end
xe-131 1 0 1-20 1001  end
cs-134 1 0 1-20 1001  end
cs-135 1 0 1-20 1001  end
cs-137 1 0 1-20 1001  end
pr-143 1 0 1-20 1001  end
nd-143 1 0 1-20 1001  end
ce-144 1 0 1-20 1001  end
nd-144 1 0 1-20 1001  end
nd-145 1 0 1-20 1001  end
nd-146 1 0 1-20 1001  end
nd-147 1 0 1-20 1001  end
pm-147 1 0 1-20 1001  end
sm-147 1 0 1-20 1001  end
nd-148 1 0 1-20 1001  end
pm-148 1 0 1-20 1001  end
sm-148 1 0 1-20 1001  end
pm-149 1 0 1-20 1001  end
sm-149 1 0 1-20 1001  end
nd-150 1 0 1-20 1001  end
sm-150 1 0 1-20 1001  end
sm-151 1 0 1-20 1001  end
eu-151 1 0 1-20 1001  end
sm-152 1 0 1-20 1001  end
eu-153 1 0 1-20 1001  end
eu-154 1 0 1-20 1001  end
gd-154 1 0 1-20 1001  end
eu-155 1 0 1-20 1001  end
gd-155 1 0 1-20 1001  end
gd-157 1 0 1-20 1001  end
gd-158 1 0 1-20 1001  end
gd-160 1 0 1-20 1001  end
ss304 2 1 570  end
h2o 3 den=0.7795 1 540  end
arbm-bormod 0.7795 1 1 0 0 5000 100 3 1175.0e-6 540  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag 10.159 1 1 0 1 47000 100 6 0.80 540  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 540 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 540 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.509 burn=226 down=86 end
power=20.982 burn=263 down=51 bfrac=0.7234 end
power=24.268 burn=292 down=1117 bfrac=0.2766 end
power=20.785 burn=416 down=10 bfrac=0.5532 h2ofrac=1.020 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```


Assembly 509-069, Rod E5, Axial Level 4, with a Burnup of 23.867 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod e5, level 4, 23.867 gwd/mtu, b4, july-95
'
'   Input File Name: trino69e514b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2  1 den=10.079  1 1015
    92234 0.028 92235 3.13  92236 0.014 92238 96.828  end
co-59  3 0 1-20 553  end
zr-94  1 0 1-20 1015  end
mo-94  1 0 1-20 1015  end
nb-95  1 0 1-20 1015  end
mo-95  1 0 1-20 1015  end
tc-99  1 0 1-20 1015  end
rh-103 1 0 1-20 1015  end
rh-105 1 0 1-20 1015  end
ru-106 1 0 1-20 1015  end
sn-126 1 0 1-20 1015  end
xe-131 1 0 1-20 1015  end
cs-134 1 0 1-20 1015  end
cs-135 1 0 1-20 1015  end
cs-137 1 0 1-20 1015  end
pr-143 1 0 1-20 1015  end
nd-143 1 0 1-20 1015  end
ce-144 1 0 1-20 1015  end
nd-144 1 0 1-20 1015  end
nd-145 1 0 1-20 1015  end
nd-146 1 0 1-20 1015  end
nd-147 1 0 1-20 1015  end
pm-147 1 0 1-20 1015  end
sm-147 1 0 1-20 1015  end
nd-148 1 0 1-20 1015  end
pm-148 1 0 1-20 1015  end
sm-148 1 0 1-20 1015  end
pm-149 1 0 1-20 1015  end
sm-149 1 0 1-20 1015  end
nd-150 1 0 1-20 1015  end
sm-150 1 0 1-20 1015  end
sm-151 1 0 1-20 1015  end
eu-151 1 0 1-20 1015  end
sm-152 1 0 1-20 1015  end
eu-153 1 0 1-20 1015  end
eu-154 1 0 1-20 1015  end
gd-154 1 0 1-20 1015  end
eu-155 1 0 1-20 1015  end
gd-155 1 0 1-20 1015  end
gd-157 1 0 1-20 1015  end
gd-158 1 0 1-20 1015  end
gd-160 1 0 1-20 1015  end
ss304  2 1  570  end
h2o  3 den=0.7554  1  553  end
arbm-bormod  0.7554 1 1 0 0 5000 100 3 1175.0e-6  553  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag  10.159 1 1 0 1 47000 100 6 0.80  553  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 553 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 553 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.266 burn=226 down=86 end
power=20.605 burn=263 down=51 bfrac=0.7234 end
power=23.832 burn=292 down=1117 bfrac=0.2766 end
power=20.411 burn=416 down=10 bfrac=0.5532 h2ofrac=1.023 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-069, Rod E5, Axial Level 7, with a Burnup of 24.548 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod e5, level 7, 24.548 gwd/mtu, b4, july-95
'
'   Input File Name: trino69e517b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2  1 den=10.079  1 1001
    92234 0.028 92235 3.13  92236 0.014 92238 96.828  end
co-59  3 0 1-20 540  end
zr-94  1 0 1-20 1001  end
mo-94  1 0 1-20 1001  end
nb-95  1 0 1-20 1001  end
mo-95  1 0 1-20 1001  end
tc-99  1 0 1-20 1001  end
rh-103 1 0 1-20 1001  end
rh-105 1 0 1-20 1001  end
ru-106 1 0 1-20 1001  end
sn-126 1 0 1-20 1001  end
xe-131 1 0 1-20 1001  end
cs-134 1 0 1-20 1001  end
cs-135 1 0 1-20 1001  end
cs-137 1 0 1-20 1001  end
pr-143 1 0 1-20 1001  end
nd-143 1 0 1-20 1001  end
ce-144 1 0 1-20 1001  end
nd-144 1 0 1-20 1001  end
nd-145 1 0 1-20 1001  end
nd-146 1 0 1-20 1001  end
nd-147 1 0 1-20 1001  end
pm-147 1 0 1-20 1001  end
sm-147 1 0 1-20 1001  end
nd-148 1 0 1-20 1001  end
pm-148 1 0 1-20 1001  end
sm-148 1 0 1-20 1001  end
pm-149 1 0 1-20 1001  end
sm-149 1 0 1-20 1001  end
nd-150 1 0 1-20 1001  end
sm-150 1 0 1-20 1001  end
sm-151 1 0 1-20 1001  end
eu-151 1 0 1-20 1001  end
sm-152 1 0 1-20 1001  end
eu-153 1 0 1-20 1001  end
eu-154 1 0 1-20 1001  end
gd-154 1 0 1-20 1001  end
eu-155 1 0 1-20 1001  end
gd-155 1 0 1-20 1001  end
gd-157 1 0 1-20 1001  end
gd-158 1 0 1-20 1001  end
gd-160 1 0 1-20 1001  end
ss304  2 1  570  end
h2o  3 den=0.7795  1  540  end
arbm-bormod  0.7795 1 1 0 0 5000 100 3 1175.0e-6  540  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag  10.159 1 1 0 1 47000 100 6 0.80  540  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 540 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 540 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.645 burn=226 down=86 end
power=21.193 burn=263 down=51 bfrac=0.7234 end
power=24.512 burn=292 down=1117 bfrac=0.2766 end
power=20.993 burn=416 down=10 bfrac=0.5532 h2ofrac=1.020 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-069, Rod L11, Axial Level 4, with a Burnup of 23.928 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod l11, level 4, 23.928 gwd/mtu, b5, july-95
'
'   Input File Name: trino6911114b5
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-5 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2  1 den=10.079  1 1015
    92234 0.028 92235 3.13  92236 0.014 92238 96.828  end
co-59  3 0 1-20 553  end
zr-94  1 0 1-20 1015  end
mo-94  1 0 1-20 1015  end
nb-95  1 0 1-20 1015  end
mo-95  1 0 1-20 1015  end
tc-99  1 0 1-20 1015  end
rh-103 1 0 1-20 1015  end
rh-105 1 0 1-20 1015  end
ru-106 1 0 1-20 1015  end
sn-126 1 0 1-20 1015  end
xe-131 1 0 1-20 1015  end
cs-134 1 0 1-20 1015  end
cs-135 1 0 1-20 1015  end
cs-137 1 0 1-20 1015  end
pr-143 1 0 1-20 1015  end
nd-143 1 0 1-20 1015  end
ce-144 1 0 1-20 1015  end
nd-144 1 0 1-20 1015  end
nd-145 1 0 1-20 1015  end
nd-146 1 0 1-20 1015  end
nd-147 1 0 1-20 1015  end
pm-147 1 0 1-20 1015  end
sm-147 1 0 1-20 1015  end
nd-148 1 0 1-20 1015  end
pm-148 1 0 1-20 1015  end
sm-148 1 0 1-20 1015  end
pm-149 1 0 1-20 1015  end
sm-149 1 0 1-20 1015  end
nd-150 1 0 1-20 1015  end
sm-150 1 0 1-20 1015  end
sm-151 1 0 1-20 1015  end
eu-151 1 0 1-20 1015  end
sm-152 1 0 1-20 1015  end
eu-153 1 0 1-20 1015  end
eu-154 1 0 1-20 1015  end
gd-154 1 0 1-20 1015  end
eu-155 1 0 1-20 1015  end
gd-155 1 0 1-20 1015  end
gd-157 1 0 1-20 1015  end
gd-158 1 0 1-20 1015  end
gd-160 1 0 1-20 1015  end
ss304  2 1  570  end
h2o  3 den=0.7554  1  553  end
arbm-bormod  0.7554 1 1 0 0 5000 100 3 1175.0e-6  553  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag  10.159 1 1 0 1 47000 100 6 0.80  553  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 553 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 553 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.300 burn=226 down=86 end
power=20.657 burn=263 down=51 bfrac=0.7234 end
power=23.893 burn=292 down=1117 bfrac=0.2766 end
power=20.463 burn=416 down=10 bfrac=0.5532 h2ofrac=1.023 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-069, Rod L11, Axial Level 7, with a Burnup of 24.362 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod l11, level 7, 24.362 gwd/mtu, b4, july-95
'
'   Input File Name: trino6911117b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.079 1 1001
    92234 0.028 92235 3.13 92236 0.014 92238 96.828  end
co-59 3 0 1-20 540  end
zr-94 1 0 1-20 1001  end
mo-94 1 0 1-20 1001  end
nb-95 1 0 1-20 1001  end
mo-95 1 0 1-20 1001  end
tc-99 1 0 1-20 1001  end
rh-103 1 0 1-20 1001  end
rh-105 1 0 1-20 1001  end
ru-106 1 0 1-20 1001  end
sn-126 1 0 1-20 1001  end
xe-131 1 0 1-20 1001  end
cs-134 1 0 1-20 1001  end
cs-135 1 0 1-20 1001  end
cs-137 1 0 1-20 1001  end
pr-143 1 0 1-20 1001  end
nd-143 1 0 1-20 1001  end
ce-144 1 0 1-20 1001  end
nd-144 1 0 1-20 1001  end
nd-145 1 0 1-20 1001  end
nd-146 1 0 1-20 1001  end
nd-147 1 0 1-20 1001  end
pm-147 1 0 1-20 1001  end
sm-147 1 0 1-20 1001  end
nd-148 1 0 1-20 1001  end
pm-148 1 0 1-20 1001  end
sm-148 1 0 1-20 1001  end
pm-149 1 0 1-20 1001  end
sm-149 1 0 1-20 1001  end
nd-150 1 0 1-20 1001  end
sm-150 1 0 1-20 1001  end
sm-151 1 0 1-20 1001  end
eu-151 1 0 1-20 1001  end
sm-152 1 0 1-20 1001  end
eu-153 1 0 1-20 1001  end
eu-154 1 0 1-20 1001  end
gd-154 1 0 1-20 1001  end
eu-155 1 0 1-20 1001  end
gd-155 1 0 1-20 1001  end
gd-157 1 0 1-20 1001  end
gd-158 1 0 1-20 1001  end
gd-160 1 0 1-20 1001  end
ss304 2 1 570  end
h2o 3 den=0.7795 1 540  end
arbm-bormod 0.7795 1 1 0 0 5000 100 3 1175.0e-6 540  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag 10.159 1 1 0 1 47000 100 6 0.80 540  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 540 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 540 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.542 burn=226 down=86 end
power=21.032 burn=263 down=51 bfrac=0.7234 end
power=24.326 burn=292 down=1117 bfrac=0.2766 end
power=20.834 burn=416 down=10 bfrac=0.5532 h2ofrac=1.020 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```


Assembly 509-069, Rod L5, Axial Level 4, with a Burnup of 24.330 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod l5, level 4, 24.330 gwd/mtu, b4, july-95
'
'   Input File Name: trino691514b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2  1 den=10.079  1 1015
    92234 0.028 92235 3.13  92236 0.014 92238 96.828  end
co-59  3 0 1-20 553  end
zr-94  1 0 1-20 1015  end
mo-94  1 0 1-20 1015  end
nb-95  1 0 1-20 1015  end
mo-95  1 0 1-20 1015  end
tc-99  1 0 1-20 1015  end
rh-103 1 0 1-20 1015  end
rh-105 1 0 1-20 1015  end
ru-106 1 0 1-20 1015  end
sn-126 1 0 1-20 1015  end
xe-131 1 0 1-20 1015  end
cs-134 1 0 1-20 1015  end
cs-135 1 0 1-20 1015  end
cs-137 1 0 1-20 1015  end
pr-143 1 0 1-20 1015  end
nd-143 1 0 1-20 1015  end
ce-144 1 0 1-20 1015  end
nd-144 1 0 1-20 1015  end
nd-145 1 0 1-20 1015  end
nd-146 1 0 1-20 1015  end
nd-147 1 0 1-20 1015  end
pm-147 1 0 1-20 1015  end
sm-147 1 0 1-20 1015  end
nd-148 1 0 1-20 1015  end
pm-148 1 0 1-20 1015  end
sm-148 1 0 1-20 1015  end
pm-149 1 0 1-20 1015  end
sm-149 1 0 1-20 1015  end
nd-150 1 0 1-20 1015  end
sm-150 1 0 1-20 1015  end
sm-151 1 0 1-20 1015  end
eu-151 1 0 1-20 1015  end
sm-152 1 0 1-20 1015  end
eu-153 1 0 1-20 1015  end
eu-154 1 0 1-20 1015  end
gd-154 1 0 1-20 1015  end
eu-155 1 0 1-20 1015  end
gd-155 1 0 1-20 1015  end
gd-157 1 0 1-20 1015  end
gd-158 1 0 1-20 1015  end
gd-160 1 0 1-20 1015  end
ss304  2 1  570  end
h2o  3 den=0.7554  1  553  end
arbm-bormod  0.7554 1 1 0 0 5000 100 3 1175.0e-6  553  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag  10.159 1 1 0 1 47000 100 6 0.80  553  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 553 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 553 end
' cadmium fraction corrected from 0.15 to 0.05
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.524 burn=226 down=86 end
power=21.004 burn=263 down=51 bfrac=0.7234 end
power=24.294 burn=292 down=1117 bfrac=0.2766 end
power=20.807 burn=416 down=10 bfrac=0.5532 h2ofrac=1.023 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

Assembly 509-069, Rod L5, Axial Level 7, with a Burnup of 24.313 GWd/MTU

```
=sas2      parm='halt04,skipshipdata'
trino vercelles pwr, 509-069, rod l5, level 7, 24.313 gwd/mtu, b4, july-95
'
'   Input File Name: trino691517b4
'
'-----
'   cooled 10 d, axial-dependent h2o density & temperature
'
'       in reactor for cycle 1 and 2
'
'       using ag-in-cd absorber in mix 6, estimated densities
'   applying an effective control-rod mockup, period dependent, with uo2
'
'       ***** endf/b-4 *****
'   .....SCALE Version 4.2p, /scale4.2p/ .....
'-----
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2  1 den=10.079  1 1001
    92234 0.028 92235 3.13  92236 0.014 92238 96.828  end
co-59  3 0 1-20 540  end
zr-94  1 0 1-20 1001  end
mo-94  1 0 1-20 1001  end
nb-95  1 0 1-20 1001  end
mo-95  1 0 1-20 1001  end
tc-99  1 0 1-20 1001  end
rh-103 1 0 1-20 1001  end
rh-105 1 0 1-20 1001  end
ru-106 1 0 1-20 1001  end
sn-126 1 0 1-20 1001  end
xe-131 1 0 1-20 1001  end
cs-134 1 0 1-20 1001  end
cs-135 1 0 1-20 1001  end
cs-137 1 0 1-20 1001  end
pr-143 1 0 1-20 1001  end
nd-143 1 0 1-20 1001  end
ce-144 1 0 1-20 1001  end
nd-144 1 0 1-20 1001  end
nd-145 1 0 1-20 1001  end
nd-146 1 0 1-20 1001  end
nd-147 1 0 1-20 1001  end
pm-147 1 0 1-20 1001  end
sm-147 1 0 1-20 1001  end
nd-148 1 0 1-20 1001  end
pm-148 1 0 1-20 1001  end
sm-148 1 0 1-20 1001  end
pm-149 1 0 1-20 1001  end
sm-149 1 0 1-20 1001  end
nd-150 1 0 1-20 1001  end
sm-150 1 0 1-20 1001  end
sm-151 1 0 1-20 1001  end
eu-151 1 0 1-20 1001  end
sm-152 1 0 1-20 1001  end
eu-153 1 0 1-20 1001  end
eu-154 1 0 1-20 1001  end
gd-154 1 0 1-20 1001  end
eu-155 1 0 1-20 1001  end
gd-155 1 0 1-20 1001  end
gd-157 1 0 1-20 1001  end
gd-158 1 0 1-20 1001  end
gd-160 1 0 1-20 1001  end
ss304  2 1  570  end
h2o  3 den=0.7795  1  540  end
arbm-bormod  0.7795 1 1 0 0 5000 100 3 1175.0e-6  540  end
'
'   1175 ppm boron (wt) in moderator at start (1st segment)
'-----
arbm-ag  10.159 1 1 0 1 47000 100 6 0.80  540  end
```

```

arbm-in 10.159 1 1 0 1 49000 100 6 0.15 540 end
arbm-cd 10.159 8 0 0 1
48108 0.85 48110 12.21 48111 12.63 48112 24.02
48113 12.27 48114 29.11 48601 1-20 48116 7.72
6 0.05 540 end
'
end comp
'
' -----
'
' fuel-pin-cell geometry:
'
squarepitch 1.303 0.9020 1 3 0.9786 2 end
'
' -----
'
' assembly and cycle parameters:
'
npin/assm=214 fuelnght=823.10 ncycles=4 nlib/cyc=1
printlevel=4 lightel=8 inplevel=2 numztotal=5 mxrepeats=0 end
3 0.73514 500 10.779 6 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
3 0.73514 500 10.779 3 10.809 3 11.273 2 11.340
power=13.514 burn=226 down=86 end
power=20.990 burn=263 down=51 bfrac=0.7234 end
power=24.277 burn=292 down=1117 bfrac=0.2766 end
power=20.792 burn=416 down=10 bfrac=0.5532 h2ofrac=1.020 end
o 135 cr 35.7 mn 3.5
fe 121 co 0.20 ni 24
zr 3.0 nb 0.71
'
' -----
'
end

```

APPENDIX C

SAMPLE INPUT FOR A TURKEY POINT UNIT 3 SAS2H DEPLETION CALCULATION

Assembly D01, Rod G9, with a Burnup of 30.72 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
turkey point 3 pwr, assembly d01 rod g9, 30.72 gwd/mtu, b4, june-95
'   cooled 927 days
'
'-----
'   in reactor for cycles 2, 3 and 4
'
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.235 1 922
    92234 0.023 92235 2.556 92236 0.012 92238 97.409  end
co-59 3 0 1-20 570  end
zr-94 1 0 1-20 922  end
mo-94 1 0 1-20 922  end
nb-95 1 0 1-20 922  end
mo-95 1 0 1-20 922  end
tc-99 1 0 1-20 922  end
rh-103 1 0 1-20 922  end
rh-105 1 0 1-20 922  end
ru-106 1 0 1-20 922  end
sn-126 1 0 1-20 922  end
xe-131 1 0 1-20 922  end
cs-134 1 0 1-20 922  end
cs-135 1 0 1-20 922  end
cs-137 1 0 1-20 922  end
pr-143 1 0 1-20 922  end
nd-143 1 0 1-20 922  end
ce-144 1 0 1-20 922  end
nd-144 1 0 1-20 922  end
nd-145 1 0 1-20 922  end
nd-146 1 0 1-20 922  end
nd-147 1 0 1-20 922  end
pm-147 1 0 1-20 922  end
sm-147 1 0 1-20 922  end
nd-148 1 0 1-20 922  end
pm-148 1 0 1-20 922  end
sm-148 1 0 1-20 922  end
pm-149 1 0 1-20 922  end
sm-149 1 0 1-20 922  end
nd-150 1 0 1-20 922  end
sm-150 1 0 1-20 922  end
sm-151 1 0 1-20 922  end
eu-151 1 0 1-20 922  end
sm-152 1 0 1-20 922  end
eu-153 1 0 1-20 922  end
eu-154 1 0 1-20 922  end
gd-154 1 0 1-20 922  end
eu-155 1 0 1-20 922  end
gd-155 1 0 1-20 922  end
gd-157 1 0 1-20 922  end
gd-158 1 0 1-20 922  end
gd-160 1 0 1-20 922  end
'   need the following to use endf/b4 library:
zircalloy 2 1 595  end
'   need the following to use endf/b5 library:
'arbmzirc 6.44 4 0 0 1 40000 97.91 26000 0.5 50116 0.86 50120 0.73 2 1 595  end
h2o 3 den=0.731 1 570  end
arbm-bormod 0.731 1 1 0 0 5000 100 3 450.0e-6 570  end
'
'   450 ppm boron (wt) in moderator at start (1st segment)
'-----
end comp
```

```

'
' -----
'
'      fuel-pin-cell geometry:
'
squarepitch  1.4300  0.92964 1  3  1.0719  2  0.9484  0  end
'
' -----
'
'      assembly and cycle parameters:
'
npin/assm=204 fuelnght=800.53 ncycles=3  nlib/cyc=1
printlevel=4 lightel=9  inplevel=2 numztotal=4  end
3  0.6502  2  0.6934  3  0.80679  500  2.5146
power=32.235  burn=314  down=58  end
power=32.235  burn=327  down=62  end
power=32.235  burn=312  down=927  end
  o 135  cr  5.9  mn  0.33
  fe 12.9 co 0.075 ni  9.9
  zr 221 nb  0.71 sn  3.6
'
' -----
'
end

```

Assembly D01, Rod G10, with a Burnup of 30.510 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
turkey point 3 pwr, assembly d01 rod g10, 30.51 gwd/mtu, b4, june-95
'   cooled 927 days
'   -----
'   in reactor for cycles 2, 3 and 4
'
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.235 1 922
    92234 0.023 92235 2.556 92236 0.012 92238 97.409  end
co-59 3 0 1-20 570  end
zr-94 1 0 1-20 922  end
mo-94 1 0 1-20 922  end
nb-95 1 0 1-20 922  end
mo-95 1 0 1-20 922  end
tc-99 1 0 1-20 922  end
rh-103 1 0 1-20 922  end
rh-105 1 0 1-20 922  end
ru-106 1 0 1-20 922  end
sn-126 1 0 1-20 922  end
xe-131 1 0 1-20 922  end
cs-134 1 0 1-20 922  end
cs-135 1 0 1-20 922  end
cs-137 1 0 1-20 922  end
pr-143 1 0 1-20 922  end
nd-143 1 0 1-20 922  end
ce-144 1 0 1-20 922  end
nd-144 1 0 1-20 922  end
nd-145 1 0 1-20 922  end
nd-146 1 0 1-20 922  end
nd-147 1 0 1-20 922  end
pm-147 1 0 1-20 922  end
sm-147 1 0 1-20 922  end
nd-148 1 0 1-20 922  end
pm-148 1 0 1-20 922  end
sm-148 1 0 1-20 922  end
pm-149 1 0 1-20 922  end
sm-149 1 0 1-20 922  end
nd-150 1 0 1-20 922  end
sm-150 1 0 1-20 922  end
sm-151 1 0 1-20 922  end
eu-151 1 0 1-20 922  end
sm-152 1 0 1-20 922  end
eu-153 1 0 1-20 922  end
eu-154 1 0 1-20 922  end
gd-154 1 0 1-20 922  end
eu-155 1 0 1-20 922  end
gd-155 1 0 1-20 922  end
gd-157 1 0 1-20 922  end
gd-158 1 0 1-20 922  end
gd-160 1 0 1-20 922  end
'   need the following to use endf/b4 library:
zircalloy 2 1 595  end
'   need the following to use endf/b5 library:
'arbmzirc 6.44 4 0 0 1 40000 97.91 26000 0.5 50116 0.86 50120 0.73 2 1 595  end
h2o 3 den=0.731 1 570  end
arbm-bormod 0.731 1 1 0 0 5000 100 3 450.0e-6 570  end
'
'   450 ppm boron (wt) in moderator at start (1st segment)
'   -----
end comp
'
'   -----
'   fuel-pin-cell geometry:
'
squarepitch 1.4300 0.92964 1 3 1.0719 2 0.9484 0  end
'
```

```
' - - - - -  
'  
      assembly and cycle parameters:  
'  
npin/assm=204 fuelnght=800.53 ncycles=3  nlib/cyc=1  
printlevel=4 lightel=9  inplevel=2 numzttotal=4  end  
3 0.6502 2 0.6934 3 0.80679 500 2.5146  
power=32.015 burn=314 down=58 end  
power=32.015 burn=327 down=62 end  
power=32.015 burn=312 down=927 end  
  o 135 cr 5.9 mn 0.33  
  fe 12.9 co 0.075 ni 9.9  
  zr 221 nb 0.71 sn 3.6  
'  
' - - - - -  
'  
end
```


Assembly D01, Rod H9, with a Burnup of 31.560 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
turkey point 3 pwr, assembly d01 rod h9, 31.56 gwd/mtu, b4, june-95
'   cooled 927 days
'   -----
'   in reactor for cycles 2, 3 and 4
'
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.235 1 922
    92234 0.023 92235 2.556 92236 0.012 92238 97.409  end
co-59 3 0 1-20 570  end
zr-94 1 0 1-20 922  end
mo-94 1 0 1-20 922  end
nb-95 1 0 1-20 922  end
mo-95 1 0 1-20 922  end
tc-99 1 0 1-20 922  end
rh-103 1 0 1-20 922  end
rh-105 1 0 1-20 922  end
ru-106 1 0 1-20 922  end
sn-126 1 0 1-20 922  end
xe-131 1 0 1-20 922  end
cs-134 1 0 1-20 922  end
cs-135 1 0 1-20 922  end
cs-137 1 0 1-20 922  end
pr-143 1 0 1-20 922  end
nd-143 1 0 1-20 922  end
ce-144 1 0 1-20 922  end
nd-144 1 0 1-20 922  end
nd-145 1 0 1-20 922  end
nd-146 1 0 1-20 922  end
nd-147 1 0 1-20 922  end
pm-147 1 0 1-20 922  end
sm-147 1 0 1-20 922  end
nd-148 1 0 1-20 922  end
pm-148 1 0 1-20 922  end
sm-148 1 0 1-20 922  end
pm-149 1 0 1-20 922  end
sm-149 1 0 1-20 922  end
nd-150 1 0 1-20 922  end
sm-150 1 0 1-20 922  end
sm-151 1 0 1-20 922  end
eu-151 1 0 1-20 922  end
sm-152 1 0 1-20 922  end
eu-153 1 0 1-20 922  end
eu-154 1 0 1-20 922  end
gd-154 1 0 1-20 922  end
eu-155 1 0 1-20 922  end
gd-155 1 0 1-20 922  end
gd-157 1 0 1-20 922  end
gd-158 1 0 1-20 922  end
gd-160 1 0 1-20 922  end
'   need the following to use endf/b4 library:
zircalloy 2 1 595  end
'   need the following to use endf/b5 library:
'arbmzirc 6.44 4 0 0 1 40000 97.91 26000 0.5 50116 0.86 50120 0.73 2 1 595  end
h2o 3 den=0.731 1 570  end
arbm-bormod 0.731 1 1 0 0 5000 100 3 450.0e-6 570  end
'
'   450 ppm boron (wt) in moderator at start (1st segment)
'   -----
end comp
'
'   -----
'   fuel-pin-cell geometry:
'
squarepitch 1.4300 0.92964 1 3 1.0719 2 0.9484 0  end
'
```

```
' - - - - -  
'  
assembly and cycle parameters:  
'  
npin/assm=204 fuelnght=800.53 ncycles=3 nlib/cyc=1  
printlevel=4 lightel=9 inplevel=2 numzttotal=4 end  
3 0.6502 2 0.6934 3 0.80679 500 2.5146  
power=33.116 burn=314 down=58 end  
power=33.116 burn=327 down=62 end  
power=33.116 burn=312 down=927 end  
o 135 cr 5.9 mn 0.33  
fe 12.9 co 0.075 ni 9.9  
zr 221 nb 0.71 sn 3.6  
'  
' - - - - -  
'  
end
```

Assembly D04, Rod G9, with a Burnup of 31.260 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
turkey point 3 pwr, assembly d04 rod g9, 31.26 gwd/mtu, b4, june-95
'   cooled 927 days
'   -----
'   in reactor for cycles 2, 3 and 4
'
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.235 1 922
    92234 0.023 92235 2.556 92236 0.012 92238 97.409  end
co-59 3 0 1-20 570  end
zr-94 1 0 1-20 922  end
mo-94 1 0 1-20 922  end
nb-95 1 0 1-20 922  end
mo-95 1 0 1-20 922  end
tc-99 1 0 1-20 922  end
rh-103 1 0 1-20 922  end
rh-105 1 0 1-20 922  end
ru-106 1 0 1-20 922  end
sn-126 1 0 1-20 922  end
xe-131 1 0 1-20 922  end
cs-134 1 0 1-20 922  end
cs-135 1 0 1-20 922  end
cs-137 1 0 1-20 922  end
pr-143 1 0 1-20 922  end
nd-143 1 0 1-20 922  end
ce-144 1 0 1-20 922  end
nd-144 1 0 1-20 922  end
nd-145 1 0 1-20 922  end
nd-146 1 0 1-20 922  end
nd-147 1 0 1-20 922  end
pm-147 1 0 1-20 922  end
sm-147 1 0 1-20 922  end
nd-148 1 0 1-20 922  end
pm-148 1 0 1-20 922  end
sm-148 1 0 1-20 922  end
pm-149 1 0 1-20 922  end
sm-149 1 0 1-20 922  end
nd-150 1 0 1-20 922  end
sm-150 1 0 1-20 922  end
sm-151 1 0 1-20 922  end
eu-151 1 0 1-20 922  end
sm-152 1 0 1-20 922  end
eu-153 1 0 1-20 922  end
eu-154 1 0 1-20 922  end
gd-154 1 0 1-20 922  end
eu-155 1 0 1-20 922  end
gd-155 1 0 1-20 922  end
gd-157 1 0 1-20 922  end
gd-158 1 0 1-20 922  end
gd-160 1 0 1-20 922  end
'   need the following to use endf/b4 library:
zircalloy 2 1 595  end
'   need the following to use endf/b5 library:
'arbmzirc 6.44 4 0 0 1 40000 97.91 26000 0.5 50116 0.86 50120 0.73 2 1 595  end
h2o 3 den=0.731 1 570  end
arbm-bormod 0.731 1 1 0 0 5000 100 3 450.0e-6 570  end
'
'   450 ppm boron (wt) in moderator at start (1st segment)
'   -----
end comp
'
'   -----
'   fuel-pin-cell geometry:
'
squarepitch 1.4300 0.92964 1 3 1.0719 2 0.9484 0  end
'
```

```
' - - - - -  
'  
      assembly and cycle parameters:  
'  
npin/assm=204 fuelnght=800.53 ncycles=3  nlib/cyc=1  
printlevel=4 lightel=9  inplevel=2 numzttotal=4  end  
3 0.6502 2 0.6934 3 0.80679 500 2.5146  
power=32.802 burn=314 down=58 end  
power=32.802 burn=327 down=62 end  
power=32.802 burn=312 down=927 end  
  o 135 cr 5.9 mn 0.33  
  fe 12.9 co 0.075 ni 9.9  
  zr 221 nb 0.71 sn 3.6  
'  
' - - - - -  
'  
end
```

Assembly D04, Rod G10, with a Burnup of 31.310 GWd/MTU

```
=sas2      parm='halt03,skipshipdata'
turkey point 3 pwr, assembly d04 rod g10, 31.31 gwd/mtu, b4, june-95
' cooled 927 days
' -----
'   in reactor for cycles 2, 3 and 4
'
'   mixtures of fuel-pin-unit-cell:
'
27burnuplib  latticecell
uo2 1 den=10.235 1 922
    92234 0.023 92235 2.556 92236 0.012 92238 97.409  end
co-59 3 0 1-20 570  end
zr-94 1 0 1-20 922  end
mo-94 1 0 1-20 922  end
nb-95 1 0 1-20 922  end
mo-95 1 0 1-20 922  end
tc-99 1 0 1-20 922  end
rh-103 1 0 1-20 922  end
rh-105 1 0 1-20 922  end
ru-106 1 0 1-20 922  end
sn-126 1 0 1-20 922  end
xe-131 1 0 1-20 922  end
cs-134 1 0 1-20 922  end
cs-135 1 0 1-20 922  end
cs-137 1 0 1-20 922  end
pr-143 1 0 1-20 922  end
nd-143 1 0 1-20 922  end
ce-144 1 0 1-20 922  end
nd-144 1 0 1-20 922  end
nd-145 1 0 1-20 922  end
nd-146 1 0 1-20 922  end
nd-147 1 0 1-20 922  end
pm-147 1 0 1-20 922  end
sm-147 1 0 1-20 922  end
nd-148 1 0 1-20 922  end
pm-148 1 0 1-20 922  end
sm-148 1 0 1-20 922  end
pm-149 1 0 1-20 922  end
sm-149 1 0 1-20 922  end
nd-150 1 0 1-20 922  end
sm-150 1 0 1-20 922  end
sm-151 1 0 1-20 922  end
eu-151 1 0 1-20 922  end
sm-152 1 0 1-20 922  end
eu-153 1 0 1-20 922  end
eu-154 1 0 1-20 922  end
gd-154 1 0 1-20 922  end
eu-155 1 0 1-20 922  end
gd-155 1 0 1-20 922  end
gd-157 1 0 1-20 922  end
gd-158 1 0 1-20 922  end
gd-160 1 0 1-20 922  end
'   need the following to use endf/b4 library:
zircalloy 2 1 595  end
'   need the following to use endf/b5 library:
'arbmzirc 6.44 4 0 0 1 40000 97.91 26000 0.5 50116 0.86 50120 0.73 2 1 595  end
h2o 3 den=0.731 1 570  end
arbm-bormod 0.731 1 1 0 0 5000 100 3 450.0e-6 570  end
'
'   450 ppm boron (wt) in moderator at start (1st segment)
' -----
end comp
'
' -----
'   fuel-pin-cell geometry:
'
squarepitch 1.4300 0.92964 1 3 1.0719 2 0.9484 0  end
'
```

```
' - - - - -  
'  
      assembly and cycle parameters:  
'  
npin/assm=204 fuelnght=800.53 ncycles=3  nlib/cyc=1  
printlevel=4 lightel=9  inplevel=2 numzttotal=4  end  
3 0.6502 2 0.6934 3 0.80679 500 2.5146  
power=32.854 burn=314 down=58 end  
power=32.854 burn=327 down=62 end  
power=32.854 burn=312 down=927 end  
  o 135 cr 5.9 mn 0.33  
  fe 12.9 co 0.075 ni 9.9  
  zr 221 nb 0.71 sn 3.6  
'  
' - - - - -  
'  
end
```

APPENDIX D

MEASURED AND COMPUTED ISOTOPIC CONCENTRATIONS FOR TRINO VERCELLES FUEL SAMPLES

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-104, rod m11, level 7, 12.042 gwd/mtu
run july 1995
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	2.662E+01	2.695E+01	(1.2%)	2.694E+01	(1.2%)
92 u236	2.736E+00	2.450E+00	(-10.4%)	2.446E+00	(-10.6%)
92 u238	9.513E+02	9.519E+02	(.1%)	9.519E+02	(.1%)
94 pu239	4.586E+00	4.418E+00	(-3.7%)	4.400E+00	(-4.1%)
94 pu240	7.165E-01	6.665E-01	(-7.0%)	6.704E-01	(-6.4%)
94 pu241	3.475E-01	3.318E-01	(-4.5%)	3.062E-01	(-11.9%)
94 pu242	3.135E-02	2.534E-02	(-19.2%)	2.680E-02	(-14.5%)
units: curies/gram U					
44 ru106	1.403E-01	1.293E-01	(-7.8%)	1.281E-01	(-8.7%)
58 ce144	5.777E-01	5.626E-01	(-2.6%)	5.633E-01	(-2.5%)
55 cs134	2.728E-02	2.091E-02	(-23.3%)	2.018E-02	(-26.0%)
55 cs137	3.895E-02	3.937E-02	(1.1%)	3.937E-02	(1.1%)

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-032, rod e11, level 4, 15.377 gwd/mtu
run july 1995
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.728E+01	1.786E+01	(3.4%)	1.795E+01	(3.9%)
92 u236	2.834E+00	2.614E+00	(-7.8%)	2.606E+00	(-8.1%)
92 u238	9.558E+02	9.559E+02	(.0%)	9.560E+02	(.0%)
94 pu239	5.266E+00	5.201E+00	(-1.2%)	4.987E+00	(-5.3%)
94 pu240	1.118E+00	1.069E+00	(-4.4%)	1.136E+00	(1.7%)
94 pu241	6.140E-01	6.321E-01	(2.9%)	6.055E-01	(-1.4%)
94 pu242	8.638E-02	7.661E-02	(-11.3%)	8.772E-02	(1.6%)
units: curies/gram U					
44 ru106	2.118E-01	2.151E-01	(1.5%)	2.167E-01	(2.3%)
58 ce144	7.165E-01	6.886E-01	(-3.9%)	6.877E-01	(-4.0%)
55 cs134	4.656E-02	3.748E-02	(-19.5%)	3.606E-02	(-22.5%)
55 cs137	4.949E-02	5.018E-02	(1.4%)	5.018E-02	(1.4%)

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-032, rod e11, level 7, 15.898 gwd/mtu
run july 1995
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.661E+01	1.746E+01 (5.1%)		1.741E+01 (4.8%)	
92 u236	2.739E+00	2.672E+00 (-2.4%)		2.669E+00 (-2.6%)	
92 u238	9.558E+02	9.556E+02 (.0%)		9.558E+02 (.0%)	
94 pu239	5.234E+00	5.168E+00 (-1.3%)		5.169E+00 (-1.2%)	
94 pu240	1.137E+00	1.102E+00 (-3.1%)		1.116E+00 (-1.8%)	
94 pu241	6.180E-01	6.530E-01 (5.7%)		6.044E-01 (-2.2%)	
94 pu242	9.487E-02	8.321E-02 (-12.3%)		8.787E-02 (-7.4%)	
units: curies/gram U					
44 ru106	2.263E-01	2.240E-01 (-1.0%)		2.215E-01 (-2.1%)	
58 ce144	7.012E-01	7.114E-01 (1.5%)		7.126E-01 (1.6%)	
55 cs134	4.927E-02	3.948E-02 (-19.9%)		3.808E-02 (-22.7%)	
55 cs137	5.014E-02	5.191E-02 (3.5%)		5.190E-02 (3.5%)	

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-032, rod e11, level 9, 11.529 gwd/mtu
run july 1995
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	2.017E+01	2.045E+01 (1.4%)		2.042E+01 (1.3%)	
92 u236	2.502E+00	2.140E+00 (-14.5%)		2.136E+00 (-14.6%)	
92 u238	9.595E+02	9.593E+02 (.0%)		9.594E+02 (.0%)	
94 pu239	4.418E+00	4.338E+00 (-1.8%)		4.330E+00 (-2.0%)	
94 pu240	7.750E-01	7.436E-01 (-4.0%)		7.476E-01 (-3.5%)	
94 pu241	3.690E-01	3.684E-01 (-.2%)		3.391E-01 (-8.1%)	
94 pu242	3.803E-02	3.324E-02 (-12.6%)		3.477E-02 (-8.6%)	
units: curies/gram U					
44 ru106	1.552E-01	1.389E-01 (-10.5%)		1.373E-01 (-11.5%)	
58 ce144	5.570E-01	5.291E-01 (-5.0%)		5.299E-01 (-4.9%)	
55 cs134	2.711E-02	2.086E-02 (-23.0%)		2.020E-02 (-25.5%)	
55 cs137	3.635E-02	3.763E-02 (3.5%)		3.763E-02 (3.5%)	

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-069, rod e11, level 1, 12.859 gwd/mtu
run july 1995
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.946E+01	1.949E+01 (.1%)		1.956E+01 (.5%)	
92 u236	2.453E+00	2.319E+00 (-5.4%)		2.312E+00 (-5.8%)	
92 u238	9.587E+02	9.581E+02 (-.1%)		9.582E+02 (.0%)	
94 pu239	4.580E+00	4.695E+00 (2.5%)		4.511E+00 (-1.5%)	
94 pu240	8.400E-01	8.540E-01 (1.7%)		9.089E-01 (8.2%)	
94 pu241	4.000E-01	4.310E-01 (7.7%)		4.145E-01 (3.6%)	
94 pu242	4.600E-02	4.443E-02 (-3.4%)		5.072E-02 (10.3%)	
units: curies/gram U					
55 cs134	2.494E-02	1.913E-02 (-23.3%)		1.847E-02 (-25.9%)	
55 cs137	3.939E-02	3.967E-02 (.7%)		3.967E-02 (.7%)	
63 eu154	1.370E-03	1.490E-03 (8.7%)		1.019E-03 (-25.6%)	

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-069, rod e11, level 2, 20.602 gwd/mtu
run july 1995
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.436E+01	1.463E+01 (1.9%)		1.472E+01 (2.5%)	
92 u236	3.317E+00	3.152E+00 (-5.0%)		3.143E+00 (-5.2%)	
92 u238	9.518E+02	9.516E+02 (.0%)		9.518E+02 (.0%)	
94 pu239	5.755E+00	5.808E+00 (.9%)		5.546E+00 (-3.6%)	
94 pu240	1.520E+00	1.466E+00 (-3.6%)		1.555E+00 (2.3%)	
94 pu241	8.850E-01	9.131E-01 (3.2%)		8.707E-01 (-1.6%)	
94 pu242	1.720E-01	1.578E-01 (-8.3%)		1.790E-01 (4.0%)	
60 nd148	2.307E-01	2.271E-01 (-1.6%)		2.272E-01 (-1.5%)	
95 am242	1.388E-03	2.226E-03 (60.4%)		1.656E-03 (19.3%)	
95 am243	2.394E-02	2.293E-02 (-4.2%)		2.568E-02 (7.3%)	
96 cm242	1.769E-02	1.391E-02 (-21.4%)		1.274E-02 (-28.0%)	
96 cm244	4.675E-03	3.391E-03 (-27.5%)		4.224E-03 (-9.6%)	
units: curies/gram U					
55 cs134	6.059E-02	4.837E-02 (-20.2%)		4.651E-02 (-23.2%)	
55 cs137	6.337E-02	6.356E-02 (.3%)		6.356E-02 (.3%)	
63 eu154	3.664E-03	4.141E-03 (13.0%)		2.704E-03 (-26.2%)	

trino vercelles pwr
 measured and computed irradiated fuel composition
 fuel assembly 509-069, rod e11, level 4, 23.718 gwd/mtu
 run july 1995

..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

units: milligrams/gram U

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
92 u235	1.248E+01	1.295E+01	(3.8%)	1.305E+01	(4.5%)
92 u236	3.610E+00	3.411E+00	(-5.5%)	3.403E+00	(-5.7%)
92 u238	9.493E+02	9.491E+02	(.0%)	9.492E+02	(.0%)
94 pu239	5.895E+00	6.038E+00	(2.4%)	5.756E+00	(-2.4%)
94 pu240	1.755E+00	1.683E+00	(-4.1%)	1.784E+00	(1.6%)
94 pu241	1.030E+00	1.095E+00	(6.3%)	1.042E+00	(1.1%)
94 pu242	2.435E-01	2.227E-01	(-8.5%)	2.521E-01	(3.5%)
60 nd148	2.655E-01	2.611E-01	(-1.7%)	2.612E-01	(-1.6%)
95 am242	2.125E-03	2.622E-03	(23.4%)	1.934E-03	(-9.0%)
95 am243	4.533E-02	3.715E-02	(-18.0%)	4.139E-02	(-8.7%)
96 cm242	2.435E-02	1.906E-02	(-21.7%)	1.750E-02	(-28.1%)
96 cm244	9.017E-03	6.459E-03	(-28.4%)	7.967E-03	(-11.6%)

units: curies/gram U

55 cs134	7.605E-02	6.326E-02	(-16.8%)	6.078E-02	(-20.1%)
55 cs137	7.242E-02	7.318E-02	(1.1%)	7.317E-02	(1.0%)
63 eu154	4.643E-03	5.524E-03	(19.0%)	3.538E-03	(-23.8%)

trino vercelles pwr
 measured and computed irradiated fuel composition
 fuel assembly 509-069, rod e11, level 7, 24.304 gwd/mtu
 run july 1995

..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.235E+01	1.255E+01 (1.7%)		1.247E+01 (1.0%)	
92 u236	3.638E+00	3.459E+00 (-4.9%)		3.456E+00 (-5.0%)	
92 u238	9.492E+02	9.488E+02 (.0%)		9.490E+02 (.0%)	
94 pu239	6.070E+00	5.941E+00 (-2.1%)		5.965E+00 (-1.7%)	
94 pu240	1.825E+00	1.711E+00 (-6.2%)		1.744E+00 (-4.4%)	
94 pu241	1.060E+00	1.108E+00 (4.5%)		1.034E+00 (-2.5%)	
94 pu242	2.575E-01	2.357E-01 (-8.5%)		2.499E-01 (-2.9%)	
60 nd148	2.719E-01	2.676E-01 (-1.6%)		2.677E-01 (-1.5%)	
95 am242	2.257E-03	2.602E-03 (15.3%)		1.820E-03 (-19.4%)	
95 am243	4.584E-02	3.968E-02 (-13.4%)		4.112E-02 (-10.3%)	
96 cm242	2.664E-02	1.977E-02 (-25.8%)		1.719E-02 (-35.5%)	
96 cm244	9.904E-03	7.015E-03 (-29.2%)		7.982E-03 (-19.4%)	
units: curies/gram U					
55 cs134	7.793E-02	6.573E-02 (-15.7%)		6.335E-02 (-18.7%)	
55 cs137	7.352E-02	7.502E-02 (2.0%)		7.500E-02 (2.0%)	
63 eu154	4.305E-03	5.753E-03 (33.6%)		3.753E-03 (-12.8%)	

trino vercelles pwr
 measured and computed irradiated fuel composition
 fuel assembly 509-069, rod e5, level 4, 23.867 gwd/mtu
 run july 1995

..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.291E+01	1.288E+01	(-.2%)	1.297E+01	(.5%)
92 u236	3.520E+00	3.423E+00	(-2.8%)	3.415E+00	(-3.0%)
92 u238	9.492E+02	9.489E+02	(.0%)	9.491E+02	(.0%)
94 pu239	5.950E+00	6.050E+00	(1.7%)	5.766E+00	(-3.1%)
94 pu240	1.760E+00	1.693E+00	(-3.8%)	1.794E+00	(1.9%)
94 pu241	1.050E+00	1.104E+00	(5.1%)	1.050E+00	(.0%)
94 pu242	2.400E-01	2.261E-01	(-5.8%)	2.559E-01	(6.6%)
60 nd148	2.666E-01	2.627E-01	(-1.5%)	2.628E-01	(-1.4%)
96 cm242	2.318E-02	1.933E-02	(-16.6%)	1.775E-02	(-23.4%)
96 cm244	8.960E-03	6.650E-03	(-25.8%)	8.200E-03	(-8.5%)
units: curies/gram U					
55 cs134	1.028E-01	6.404E-02	(-37.7%)	6.152E-02	(-40.2%)
55 cs137	7.277E-02	7.364E-02	(1.2%)	7.363E-02	(1.2%)
63 eu154	4.607E-03	5.596E-03	(21.5%)	3.582E-03	(-22.3%)

trino vercelles pwr
 measured and computed irradiated fuel composition
 fuel assembly 509-069, rod e5, level 7, 24.548 gwd/mtu
 run july 1995

..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.221E+01	1.243E+01 (1.8%)		1.235E+01 (1.1%)	
92 u236	3.540E+00	3.477E+00 (-1.8%)		3.474E+00 (-1.9%)	
92 u238	9.483E+02	9.486E+02 (.0%)		9.488E+02 (.0%)	
94 pu239	5.980E+00	5.958E+00 (-.4%)		5.983E+00 (.0%)	
94 pu240	1.785E+00	1.727E+00 (-3.2%)		1.761E+00 (-1.3%)	
94 pu241	1.055E+00	1.122E+00 (6.4%)		1.047E+00 (-.8%)	
94 pu242	2.540E-01	2.414E-01 (-5.0%)		2.560E-01 (.8%)	
60 nd148	2.740E-01	2.702E-01 (-1.4%)		2.704E-01 (-1.3%)	
95 am242	2.440E-03	2.630E-03 (7.8%)		1.840E-03 (-24.6%)	
95 am243	4.615E-02	4.107E-02 (-11.0%)		4.255E-02 (-7.8%)	
96 cm242	2.512E-02	2.021E-02 (-19.5%)		1.758E-02 (-30.0%)	
96 cm244	9.422E-03	7.350E-03 (-22.0%)		8.361E-03 (-11.3%)	
units: curies/gram U					
55 cs134	7.959E-02	6.703E-02 (-15.8%)		6.460E-02 (-18.8%)	
55 cs137	7.581E-02	7.577E-02 (-.1%)		7.576E-02 (-.1%)	
63 eu154	5.001E-03	5.872E-03 (17.4%)		3.827E-03 (-23.5%)	

trino vercelles pwr
 measured and computed irradiated fuel composition
 fuel assembly 509-069, rod l11, level 4, 23.928 gwd/mtu
 run july 1995

..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.282E+01	1.285E+01 (.2%)		1.294E+01 (1.0%)	
92 u236	3.753E+00	3.428E+00 (-8.7%)		3.419E+00 (-8.9%)	
92 u238	9.485E+02	9.489E+02 (.0%)		9.490E+02 (.1%)	
94 pu239	6.060E+00	6.054E+00 (-.1%)		5.771E+00 (-4.8%)	
94 pu240	1.790E+00	1.697E+00 (-5.2%)		1.799E+00 (.5%)	
94 pu241	1.050E+00	1.108E+00 (5.5%)		1.053E+00 (.3%)	
94 pu242	2.470E-01	2.275E-01 (-7.9%)		2.575E-01 (4.2%)	
60 nd148	2.676E-01	2.634E-01 (-1.6%)		2.635E-01 (-1.5%)	
95 am242	1.962E-03	2.648E-03 (35.0%)		1.952E-03 (-.5%)	
95 am243	4.452E-02	3.829E-02 (-14.0%)		4.265E-02 (-4.2%)	
96 cm242	2.796E-02	1.944E-02 (-30.5%)		1.785E-02 (-36.2%)	
96 cm244	9.155E-03	6.729E-03 (-26.5%)		8.296E-03 (-9.4%)	

trino vercelles pwr
 measured and computed irradiated fuel composition
 fuel assembly 509-069, rod 111, level 7, 24.362 gwd/mtu
 run july 1995

..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.225E+01	1.253E+01	(2.2%)	1.244E+01	(1.5%)
92 u236	3.465E+00	3.463E+00	(-.1%)	3.460E+00	(-.1%)
92 u238	9.482E+02	9.488E+02	(.1%)	9.489E+02	(.1%)
94 pu239	5.995E+00	5.945E+00	(-.8%)	5.969E+00	(-.4%)
94 pu240	1.810E+00	1.715E+00	(-5.3%)	1.748E+00	(-3.4%)
94 pu241	1.055E+00	1.111E+00	(5.3%)	1.037E+00	(-1.7%)
94 pu242	2.590E-01	2.371E-01	(-8.5%)	2.514E-01	(-2.9%)
60 nd148	2.722E-01	2.682E-01	(-1.5%)	2.683E-01	(-1.4%)
95 am242	2.191E-03	2.609E-03	(19.1%)	1.825E-03	(-16.7%)
95 am243	4.247E-02	4.001E-02	(-5.8%)	4.146E-02	(-2.4%)
96 cm242	2.466E-02	1.988E-02	(-19.4%)	1.728E-02	(-29.9%)
96 cm244	9.734E-03	7.094E-03	(-27.1%)	8.071E-03	(-17.1%)
units: curies/gram U					
55 cs134	7.942E-02	6.604E-02	(-16.9%)	6.365E-02	(-19.9%)
55 cs137	7.507E-02	7.519E-02	(.2%)	7.518E-02	(.2%)
63 eu154	4.477E-03	5.781E-03	(29.1%)	3.770E-03	(-15.8%)

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-069, rod 15, level 4, 24.330 gwd/mtu
run july 1995
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.297E+01	1.265E+01	(-2.4%)	1.275E+01	(-1.7%)
92 u236	3.471E+00	3.458E+00	(-.4%)	3.450E+00	(-.6%)
92 u238	9.486E+02	9.485E+02	(.0%)	9.487E+02	(.0%)
94 pu239	6.060E+00	6.085E+00	(.4%)	5.799E+00	(-4.3%)
94 pu240	1.770E+00	1.724E+00	(-2.6%)	1.827E+00	(3.2%)
94 pu241	1.060E+00	1.131E+00	(6.7%)	1.075E+00	(1.5%)
94 pu242	2.440E-01	2.367E-01	(-3.0%)	2.678E-01	(9.8%)
60 nd148	2.706E-01	2.678E-01	(-1.0%)	2.679E-01	(-1.0%)
96 cm242	2.522E-02	2.016E-02	(-20.0%)	1.853E-02	(-26.5%)
96 cm244	9.524E-03	7.271E-03	(-23.7%)	8.956E-03	(-6.0%)
units: curies/gram U					
55 cs134	7.667E-02	6.649E-02	(-13.3%)	6.387E-02	(-16.7%)
55 cs137	7.360E-02	7.507E-02	(2.0%)	7.506E-02	(2.0%)
63 eu154	4.612E-03	5.822E-03	(26.2%)	3.719E-03	(-19.4%)

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-069, rod 15, level 7, 24.313 gwd/mtu
run july 1995
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u235	1.231E+01	1.255E+01	(1.9%)	1.246E+01	(1.2%)
92 u236	3.569E+00	3.460E+00	(-3.1%)	3.457E+00	(-3.1%)
92 u238	9.472E+02	9.488E+02	(.2%)	9.490E+02	(.2%)
94 pu239	5.970E+00	5.941E+00	(-.5%)	5.966E+00	(-.1%)
94 pu240	1.790E+00	1.712E+00	(-4.4%)	1.745E+00	(-2.5%)
94 pu241	1.060E+00	1.109E+00	(4.6%)	1.034E+00	(-2.4%)
94 pu242	2.500E-01	2.359E-01	(-5.6%)	2.501E-01	(.1%)
96 cm242	2.481E-02	1.979E-02	(-20.2%)	1.720E-02	(-30.7%)
96 cm244	8.786E-03	7.027E-03	(-20.0%)	7.995E-03	(-9.0%)
units: curies/gram U					
55 cs134	7.823E-02	6.578E-02	(-15.9%)	6.340E-02	(-19.0%)
55 cs137	7.451E-02	7.504E-02	(.7%)	7.503E-02	(.7%)
63 eu154	4.814E-03	5.757E-03	(19.6%)	3.756E-03	(-22.0%)

APPENDIX E

MEASURED AND COMPUTED ISOTOPIC CONCENTRATIONS FOR TURKEY POINT UNIT 3 FUEL SAMPLES

turkey point unit 3 pwr
measured and computed irradiated fuel composition
fuel assembly d01, rod g9, 30.72 gwd/mtu
run june 1995
....measured and calculated at 927 day cooling time....
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..
nuclide, z & name measured 27BURNUPLIB %diff 44GROUPNDF5 %diff
units: milligrams/gram U

92	u234	1.321E-01	1.379E-01 (4.4%)	1.345E-01 (1.8%)
92	u235	5.865E+00	5.447E+00 (-7.1%)	5.522E+00 (-5.8%)
92	u236	3.254E+00	3.353E+00 (3.0%)	3.350E+00 (3.0%)
92	u238	9.502E+02	9.493E+02 (-.1%)	9.495E+02 (-.1%)
94	pu238	1.365E-01	1.465E-01 (7.3%)	1.384E-01 (1.4%)
94	pu239	4.838E+00	5.080E+00 (5.0%)	4.808E+00 (-.6%)
94	pu240	2.266E+00	2.147E+00 (-5.2%)	2.278E+00 (.5%)
94	pu241	1.061E+00	1.161E+00 (9.4%)	1.091E+00 (2.8%)
94	pu242	5.020E-01	5.146E-01 (2.5%)	5.716E-01 (13.9%)
60	nd148	3.342E-01	3.396E-01 (1.6%)	3.397E-01 (1.7%)

turkey point unit 3 pwr
measured and computed irradiated fuel composition
fuel assembly d01, rod g10, 30.51 gwd/mtu
run june 1995
....measured and calculated at 927 day cooling time....
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..
nuclide, z & name measured 27BURNUPLIB %diff 44GROUPNDF5 %diff
units: milligrams/gram U

92	u234	1.321E-01	1.385E-01 (4.8%)	1.350E-01 (2.2%)
92	u235	5.676E+00	5.512E+00 (-2.9%)	5.589E+00 (-1.5%)
92	u236	3.255E+00	3.346E+00 (2.8%)	3.343E+00 (2.7%)
92	u238	9.506E+02	9.495E+02 (-.1%)	9.496E+02 (-.1%)
94	pu238	1.360E-01	1.445E-01 (6.2%)	1.365E-01 (.4%)
94	pu239	4.840E+00	5.076E+00 (4.9%)	4.805E+00 (-.7%)
94	pu240	2.294E+00	2.137E+00 (-6.9%)	2.267E+00 (-1.2%)
94	pu241	1.068E+00	1.154E+00 (8.1%)	1.085E+00 (1.6%)
94	pu242	5.248E-01	5.071E-01 (-3.4%)	5.634E-01 (7.3%)
60	nd148	3.320E-01	3.373E-01 (1.6%)	3.374E-01 (1.6%)

turkey point unit 3 pwr
measured and computed irradiated fuel composition
fuel assembly d01, rod h9, 31.56 gwd/mtu
run june 1995
...measured and calculated at 927 day cooling time...
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u234	1.225E-01	1.359E-01	(10.9%)	1.324E-01	(8.1%)
92 u235	5.584E+00	5.190E+00	(-7.1%)	5.263E+00	(-5.7%)
92 u236	3.174E+00	3.381E+00	(6.5%)	3.379E+00	(6.5%)
92 u238	9.495E+02	9.485E+02	(-.1%)	9.487E+02	(-.1%)
94 pu238	1.426E-01	1.547E-01	(8.5%)	1.462E-01	(2.6%)
94 pu239	4.930E+00	5.093E+00	(3.3%)	4.819E+00	(-2.3%)
94 pu240	2.295E+00	2.188E+00	(-4.7%)	2.321E+00	(1.1%)
94 pu241	1.104E+00	1.186E+00	(7.4%)	1.114E+00	(.9%)
94 pu242	5.477E-01	5.446E-01	(-.6%)	6.049E-01	(10.4%)
60 nd148	3.434E-01	3.488E-01	(1.6%)	3.490E-01	(1.6%)

turkey point unit 3 pwr
measured and computed irradiated fuel composition
fuel assembly d04, rod g9, 31.26 gwd/mtu
run june 1995
...measured and calculated at 927 day cooling time...
..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u234	1.131E-01	1.366E-01	(20.8%)	1.332E-01	(17.7%)
92 u235	5.509E+00	5.280E+00	(-4.2%)	5.354E+00	(-2.8%)
92 u236	3.156E+00	3.371E+00	(6.8%)	3.369E+00	(6.7%)
92 u238	9.499E+02	9.488E+02	(-.1%)	9.490E+02	(-.1%)
94 pu238	1.382E-01	1.518E-01	(9.8%)	1.434E-01	(3.8%)
94 pu239	4.941E+00	5.088E+00	(3.0%)	4.815E+00	(-2.6%)
94 pu240	2.320E+00	2.174E+00	(-6.3%)	2.306E+00	(-.6%)
94 pu241	1.124E+00	1.177E+00	(4.7%)	1.106E+00	(-1.6%)
94 pu242	5.428E-01	5.338E-01	(-1.6%)	5.929E-01	(9.2%)
60 nd148	3.400E-01	3.455E-01	(1.6%)	3.457E-01	(1.7%)

turkey point unit 3 pwr
 measured and computed irradiated fuel composition
 fuel assembly d04, rod g10, 31.31 gwd/mtu
 run june 1995

...measured and calculated at 927 day cooling time....

..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram U					
92 u234	1.320E-01	1.365E-01	(3.4%)	1.331E-01	(.8%)
92 u235	5.662E+00	5.265E+00	(-7.0%)	5.339E+00	(-5.7%)
92 u236	3.252E+00	3.373E+00	(3.7%)	3.370E+00	(3.6%)
92 u238	9.498E+02	9.488E+02	(-.1%)	9.489E+02	(-.1%)
94 pu238	1.372E-01	1.523E-01	(11.0%)	1.439E-01	(4.9%)
94 pu239	4.788E+00	5.089E+00	(6.3%)	4.816E+00	(.6%)
94 pu240	2.278E+00	2.176E+00	(-4.5%)	2.308E+00	(1.3%)
94 pu241	1.072E+00	1.179E+00	(10.0%)	1.107E+00	(3.3%)
94 pu242	5.235E-01	5.356E-01	(2.3%)	5.949E-01	(13.6%)
60 nd148	3.405E-01	3.461E-01	(1.6%)	3.462E-01	(1.7%)

APPENDIX F

EFFECT OF INCORRECT ABSORBER SPECIFICATION FOR TRINO VERCELLES CALCULATIONS

After completion of analyses included in this report, an error was identified in the input for all Trino Vercelles models. Specifically, the composition of the Ag-In-Cd absorber material was defined as 80% Ag, 15% In, and **15%** Cd, rather than the correct composition of 80% Ag, 15% In, and **5%** Cd. Because the absorber material was specified in SCALE input as an arbitrary material, which allows considerable latitude in user input specifications, no error was detected by SCALE. Thus calculations were performed using 150% of the nominal cadmium content in the absorber material. However, despite the magnitude of this error, it was expected to result in very little effect on the isotopic predictions performed based on the erroneous specification. This appendix discusses briefly why no significant effect is expected and provides the results of supplementary scoping calculations performed to determine the net effect. These scoping calculations confirm that the effect of the error is indeed small. Because of the time and effort that would be required to redo all Trino calculations and revise the contents of the body of this report relative to the inconsequential changes that would result, it was decided to forego a revision and instead simply demonstrate that the effect of the error was negligible.

As discussed in Sect. 2.1 and shown in Table 5, absorber rod insertion was modeled only during the first of three subcycles in the first cycle; the absorber was not present during the last two-thirds of the first subcycle and all of the second subcycle. Thus the effect of the error was diluted by subsequent burnup. In addition, the error introduced by the overspecification of cadmium is likely to be on the order of error introduced by assumptions made in the development of the assembly model. First, absorber rod positions were not known explicitly and were assumed to be uniformly distributed around the core. Second, although the spent fuel samples were obtained primarily from axial locations distant from the partially inserted rod, the one-dimensional nature of SAS2H necessitated the approximation of a homogenized 30% absorber/70% moderator material to represent the effect of a rod that was axially inserted by 30%. Thus models for samples located near the top of the core and therefore near the absorber rod would see less

absorber than was present in reality, while samples located further from the top of the core would see more absorber effects than were actually present.

Table F.1 lists the results of a revised calculation performed for a single fuel sample with the corrected cadmium fraction in the input. These can be compared with the results listed for the same pin using the erroneous cadmium fraction, as given in Appendix D. Table F.2 provides a side-by-side comparison of the results of the reported (body of report and Appendix D) and corrected (Table F.1) results for this fuel sample. Note that the corrected results are all within 1% of the earlier results, and that for the most part the largest effect is seen for nuclides for which there is already a large uncertainty/bias between measured and computed isotopic concentrations (e.g., ^{242}Am or ^{244}Cm).

Table F.1 Results of corrected depletion calculations for
Assembly 509-069, Rod E11, Level 2

trino vercelles pwr
measured and computed irradiated fuel composition
fuel assembly 509-069, rod e11, level 2, 20.602 gwd/mtu

run June 1996

..compares cases using 27BURNUPLIB and 44GROUPNDF5 libraries..

nuclide, z & name	measured	27BURNUPLIB	%diff	44GROUPNDF5	%diff
units: milligrams/gram u					
92 u235	1.436E+01	1.457E+01	(1.4%)	1.465E+01	(2.0%)
92 u236	3.317E+00	3.152E+00	(-5.0%)	3.144E+00	(-5.2%)
92 u238	9.518E+02	9.517E+02	(0.0%)	9.519E+02	(0.0%)
94 pu239	5.755E+00	5.787E+00	(0.5%)	5.523E+00	(-4.0%)
94 pu240	1.520E+00	1.458E+00	(-4.1%)	1.547E+00	(1.8%)
94 pu241	8.850E-01	9.080E-01	(2.6%)	8.656E-01	(-2.2%)
94 pu242	1.720E-01	1.568E-01	(-8.8%)	1.778E-01	(3.4%)
60 nd148	2.307E-01	2.272E-01	(-1.5%)	2.273E-01	(-1.5%)
95 am242	1.388E-03	2.197E-03	(58.3%)	1.633E-03	(17.6%)
95 am243	2.394E-02	2.274E-02	(-5.0%)	2.546E-02	(6.3%)
96 cm242	1.769E-02	1.378E-02	(-22.1%)	1.262E-02	(-28.6%)
96 cm244	4.675E-03	3.357E-03	(-28.2%)	4.179E-03	(-10.6%)
units: curies/gram u					
55 cs134	6.059E-02	4.847E-02	(-20.0%)	4.660E-02	(-23.1%)
55 cs137	6.337E-02	6.359E-02	(0.3%)	6.358E-02	(0.3%)
63 eu154	3.664E-03	4.140E-03	(13.0%)	2.701E-03	(-26.3%)

Table F.2 Differences between reported and corrected calculated isotopic concentrations

nuclide	Reported (27BURNUPLIB)	Corrected (27BURNUPLIB)	%diff	Reported (44GROUPNDF5)	Corrected (44GROUPNDF5)	%diff
units: milligrams/gram u						
u235	1.463E+01	1.457E+01	0.41%	1.472E+01	1.465E+01	0.48%
u236	3.152E+00	3.152E+00	0.00%	3.143E+00	3.144E+00	-0.03%
u238	9.516E+02	9.517E+02	-0.01%	9.518E+02	9.519E+02	-0.01%
pu239	5.808E+00	5.787E+00	0.36%	5.546E+00	5.523E+00	0.41%
pu240	1.466E+00	1.458E+00	0.55%	1.555E+00	1.547E+00	0.51%
pu241	9.131E-01	9.080E-01	0.56%	8.707E-01	8.656E-01	0.59%
pu242	1.578E-01	1.568E-01	0.63%	1.790E-01	1.778E-01	0.67%
ndl48	2.271E-01	2.272E-01	-0.04%	2.272E-01	2.273E-01	-0.04%
am242	2.226E-03	2.197E-03	1.30%	1.656E-03	1.633E-03	1.39%
am243	2.293E-02	2.274E-02	0.83%	2.568E-02	2.546E-02	0.86%
cm242	1.391E-02	1.378E-02	0.93%	1.274E-02	1.262E-02	0.94%
cm244	3.391E-03	3.357E-03	1.00%	4.224E-03	4.179E-03	1.07%
units: curies/gram u						
cs134	4.837E-02	4.847E-02	-0.21%	4.651E-02	4.660E-02	-0.19%
cs137	6.356E-02	6.359E-02	-0.05%	6.356E-02	6.358E-02	-0.03%
eu154	4.141E-03	4.140E-03	0.02%	2.704E-03	2.701E-03	0.11%

INTERNAL DISTRIBUTION

- | | |
|-------------------------|---------------------------------|
| 1. C. W. Alexander | 26-30. C. V. Parks |
| 2. S. M. Bowman | 31. L. M. Petrie |
| 3. B. L. Broadhead | 32. R. T. Primm |
| 4. J. A. Bucholz | 33. J.-P. Renier |
| 5. R. D. Dabbs | 34. J. W. Roddy |
| 6-10. M. D. DeHart | 35. R. W. Roussin |
| 7. M. B. Emmett | 36. J. C. Ryman |
| 8-12. O. W. Hermann | 37. C. H. Shappert |
| 13. M. Kuliasha | 38. C. O. Slater |
| 14. L. C. Leal | 39. R. M. Westfall |
| 15. J. J. Lichtenwalter | 40. B. A. Worley |
| 16. S. B. Ludwig | 41. R. Q. Wright |
| 17. S. K. Martin | 42-43. Laboratory Records Dept. |
| 18. G. E. Michaels | 44. Laboratory Records, |
| 19. B. D. Murphy | 45. Document Reference Sect. |
| 20-24. L. F. Norris | 46. ORNLY-12 Research Library |
| 25. J. V. Pace | 47. Central Research Library |
| | 48. ORNL Patent Section |

EXTERNAL DISTRIBUTION

49. R. Anderson, General Nuclear Systems, Inc., 220 Stoneridge Dr., Columbia, SC 29210
50. M. G. Bailey, Office of Nuclear Material Safety & Safeguards, U.S. Nuclear Regulatory Commission, MS OWFN 6 G22, Washington, DC 20555
51. L. Barrett, Office of Civilian Radioactive Waste Management, RW-232 20545, U.S. Department of Energy, Washington, DC 20545
52. P. Baylor, Office of Civilian Radioactive Waste Management, RW-36, U.S. Department of Energy, Washington, DC 20545
53. C. J. Benson, Bettis Atomic Power Laboratory, P.O. Box 79, West Mifflin, PA 15122
54. J. Bickel, U.S. Department of Energy, Albuquerque Operations Office, P.O. Box 5400, Albuquerque, NM 87115
55. J. Boshoven, GA Technologies, Inc., P.O. Box 85608, 10955 John J. Hopkins Dr., San Diego, CA 92121
56. M. C. Brady, Sandia National Laboratories, 1261 Town Center Drive, Room 421A, Las Vegas, NV 89134
57. P. Bunton, U.S. Department of Energy, RW-1, Washington, DC 20545
58. R. J. Cacciapouti, Yankee Atomic Electric Co., 1617 Worcester Rd., Framington, MA 01701
59. D. E. Carlson, U.S. Nuclear Regulatory Commission, Spent Fuel Project Office, OWFN 6 G22, Washington, DC 20555
60. R. D. Carlson, Argonne National Laboratory, 9700 S. Cass Ave., Bldg.308, Argonne, IL 60439-4825
61. C. R. Chappell, U.S. Nuclear Regulatory Commission, Office of Nuclear Material Safety and Safeguards, TWFN 8F5, Washington, DC 20555

62. J. S. Choi, Lawrence Livermore National Laboratory, P.O. Box 808, Livermore, CA 94550
63. J. Clark, 2650 Park Tower Drive, Suite 800, Vienna, VA 22180
64. J. Conde, Consejo de Seguridad Nuclear, Justo Dorado, 11, 28040 Madrid, Spain
65. D. R. Conners, Bettis Atomic Power Laboratory, P.O. Box 79, West Mifflin, PA 15122
66. M. Conroy, U.S. Department of Energy, M-261 Quince Orchard, Washington, DC 20585-0002
67. W. Davis, Cogema, 101 Convention Center Drive, Suite 527, MS 423, Las Vegas, NV 89109
68. D. Dawson, Transnuclear, Inc., 2 Skyline Dr., Hawthorne, NY 10532-2120
69. T. W. Doering, Cogema, MS 423, Suite 527, P.O. Box 98608, 101 Convention Center Drive, Las Vegas, NV 89109
70. R. Doman, Nuclear Packaging, Inc., 1010 S. 336th St., Suite 220, Federal Way, WA 98003
71. E. P. Easton, U.S. Nuclear Regulatory Commission, Office of Nuclear Materials Safety and Safeguards, OWFN 6 F18, Washington, DC 20555
72. R. C. Ewing, Sandia National Laboratories, P.O. Box 5800, Div. 6643, MS 0716, Albuquerque, NM 87185-0716
73. I. Gauld, Whiteshell Laboratories, AECL Research, Pinawa Manitoba R0E1L0 Canada
74. G. Gualdrini, ENEA-TIB/FICS, C.R.E. "E. Clementel," Via Mazzini, 2, I-40139 Bologna, Italy
75. H. Geiser, Wissenschaftlich-Technische Ingenieurberatung GmbH, P.O. Box 13 40, 52410 Julich, Federal Republic of Germany
- 76-78. D. E. Hampton, Sandia National Laboratories, P.O. Box 5800, Div. 6302, MS 1333, Albuquerque, NM 87185-0716
79. S. Hanauer, U.S. Department of Energy, RW-22, Washington, DC 20545
80. K. J. Hardin, U.S. Nuclear Regulatory Commission, TWFN 10 C9, Washington, DC 20555
81. C. J. Haughney, U.S. Nuclear Regulatory Commission, Spent Fuel Project Office, OWFN 6 F18, Washington, DC 20555
82. L. Hassler, Babcock & Wilcox, P.O. Box 10935, Lynchburg, VA 24506-0935
83. C. A. Hrabel, U.S. Nuclear Regulatory Commission, TWFN 10 C9, Washington, DC 20555
84. U. Jenquin, Battelle Pacific Northwest Laboratory, P.O. Box 999, Richland, WA 99352
85. E. Johnson, E. R. Johnson Associates, Inc., 9302 Lee Hwy, Suite 200, Fairfax, VA 22031
86. G. Kirchner, University of Bremen, FB 1 Postfach 330440, D-W-2800 Bremen 33, Federal Republic of Germany
87. C. Kouts, Office of Civilian Radioactive Waste Management, RW-36, U.S. Department of Energy, Washington, DC 20545
88. S. Kraft, Nuclear Energy Institute, 1776 I Street, Suite 400, Washington, DC 20086
89. P. Krishna, TRW Environmental Safety Systems, 600 Maryland Ave. S.W., Suite 695, Washington, DC 20024
90. A. Kubo, 2650 Park Tower Drive, Suite 800, Vienna, VA 22180
91. W. H. Lake, Office of Civilian Radioactive Waste Management, U.S. Department of Energy, RW-46, Washington, DC 20585
92. R. Lambert, Electric Power Research Institute, 3412 Hillview Ave., Palo Alto, CA 94304
- 93-97. D. Lancaster, 2650 Park Tower Drive, Suite 800, Vienna, VA 22180
98. D. Langstaff, U.S. Department of Energy, Richland Operations Office, P.O. Box 550, Richland, WA 99352

99. C. Marotta, 1504 Columbia Ave., Rockville, MD 20850
100. M. Mason, Transnuclear, Two Skyline Drive, Hawthorne, NY 10532-2120
101. J. Massey, Sierra Nuclear Corporation, 5619 Scotts Valley Drive, Number 240, Scotts Valley, CA 95066
102. W. Mings, U.S. Department of Energy, Idaho Operations Office, 550 2nd St., Idaho Falls, ID 83401
103. A. Mobashevan, Roy F. Weston, Inc., 955 L'Enfant Plaza, SW, 8th Floor, Washington, DC 20024
104. M. Mount, Lawrence Livermore National Laboratory, P.O. Box 808, Livermore, CA 94550
105. P. K. Nair, Manager, Engineered Barrier System, Center for Nuclear Waste Regulatory Analyses, Southwest Research Institute, 6220 Culebra Road, San Antonio, TX 78238-5166
106. D. Napolitano, Nuclear Assurance Corp., 5720 Peachtree Parkway, Norcross, GA 30092
107. C. W. Nilsen, Office of Nuclear Material Safety and Safeguards, U.S. Nuclear Regulatory Commission, MS TWFN-9F29, Washington, DC 20555
- 108-109. Office of Scientific and Technical Information, U.S. Department of Energy, P.O. Box 62, Oak Ridge, TN 37831
110. Office of the Assistant Manager for Energy Research and Development, Department of Energy Oak Ridge Operations (DOE-ORO), P.O. Box 2008, Oak Ridge, TN 37831
111. N. L. Osgood, U.S. Nuclear Regulatory Commission, Office of Nuclear Materials Safety and Safeguards, OWFN 6 G22, Washington, DC 20555
112. O. Ozer, Electric Power Research Institute, 3412 Hillview Ave., Palo Alto, CA 94304
113. P. Pacquin, General Nuclear Systems, Inc., 220 Stoneridge Dr., Columbia, SC 29210
114. T. Parish, Department of Nuclear Engineering, Texas A & M University, College Station, TX 77843-3313
115. F. Prohammer, Argonne National Laboratory, 9700 S. Cass Ave., Bldg.308, Argonne, IL 60439-4825
- 116-118. M. Rahimi, 2650 Park Tower Drive, Suite 800, Vienna, VA 22180
119. B. Reid, Battelle Pacific Northwest Laboratory, P.O. Box 999, Richland, WA 99352
120. C. Rombough, CTR Technical Services, Inc., 5619 Misty Crest Dr., Arlington, TX 76017-4147
121. T. L. Sanders, Sandia National Laboratories, P.O. Box 5800, Div. 6609, MS 0720, Albuquerque, NM 87185-0716
122. M. Schaeffer, Brookhaven National Laboratory, Plant Engineering, Building 134C, P.O. Box 5000, Upton, NY 11973-5000
123. M. Smith, U.S. Department of Energy, Yucca Mountain Project Office, 101 Convention Center Dr., Las Vegas, NV 89190
124. M. Smith, Virginia Power Co., P.O. Box 2666, Richmond, VA 23261
125. K. B. Sorenson, Sandia National Laboratories, P.O. Box 5800, Div. 6643, MS 0716, Albuquerque, NM 87185-0716
126. J. B. Stringer, Duke Engineering & Services, 230 S. Tryon St., P.O. Box 1004, Charlotte, NC 28201-1004
127. F. C. Sturz, Office of Nuclear Material Safety & Safeguards, U.S. Nuclear Regulatory Commission, MS OWFN 6 G22, Washington, DC 20555
128. J. Sun, Florida Power & Light Co., P.O. Box 029100, Miami, FL 33102
129. T. Suto, Power Reactor and Nuclear Fuel Development Corp., 1-9-13, Akasaka, Minato-Ku, Tokyo, Japan
130. R. J. Talbert, Battelle Pacific Northwest Laboratory, P.O. Box 999, Richland, WA 99352
131. H. Taniuchi, Kobe Steel, Ltd., 2-3-1 Shinhamma, Arai-Cho, Takasago, 676 Japan
132. T. Taylor, INEL, P.O. Box 4000, MS 3428, Idaho Falls, ID 83403

133. B. Thomas, VECTRA Technologies, Inc., 6203 San Ignacio Ave., Suite 100, San Jose, CA 95119
134. D. A. Thomas, Cogema, 101 Convention Center Drive, Suite 527, MS 423, Las Vegas, NV 89109
135. J. R. Thornton, TRW Environmental Safety Systems, 2650 Park Tower Dr., Suite 800, Vienna, VA 22180
136. J. Vujic, Department of Nuclear Engineering, University of California at Berkeley, Berkeley, CA 94720
137. G. Walden, Duke Power Co., P.O. Box 33189, Charlotte, NC 28242
138. M. E. Wangler, U.S. Department of Energy, EH-33.2, Washington, DC 20585-0002
139. R. M. Weller, U.S. Nuclear Regulatory Commission, TWFN 7 C6, Washington, DC 20555
140. A. Wells, 2846 Peachtree Walk, Duluth, GA 30136
141. W. Weyer, Wissenschaftlich-Technische Ingenieurberatung GMBH, Mozartstrasse 13, 5177 Titz-Rodingen, Federal Republic of Germany
142. B. H. White, U.S. Nuclear Regulatory Commission, Spent Fuel Project Office, OWFN 6 F18, Washington, DC 20555
143. J. Williams, Office of Civilian Radioactive Waste Management, U.S. Department of Energy, RW-46, Washington, DC 20545
144. M. L. Williams, LSU Nuclear Science Center, Baton Rouge, LA 70803
145. C. J. Withee, U.S. Nuclear Regulatory Commission, Spent Fuel Project Office, OWFN 6 G22, Washington, DC 20555
146. R. Yang, Electric Power Research Institute, 3412 Hillview Ave., Palo Alto, CA 94304