Development of Nanofiller-Modulated Polymeric Oxygen Enrichment Membranes for Reduction of Nitrogen Oxides in Coal Combustion

Dr. Jianzhong Lou North Carolina A&T State University DE-FG26-06NT42742



#### **Commercial Membrane Cartridges**





Figure 12-7 Illustration of the membrane transport of two differently sized molecules by various mechanisms. From left to right: A viscous flow through large pores of radii, r<sub>p</sub> (no separation); B Knudsen flow (separation based upon difference in molecular weights); C molecular sieving (separation due to relative diffusive rates and surface sorption on pore walls); and D solution-diffusion through a dense membrane (separation based upon relative solubility and diffusivity).



### **PDMS Carbon Nanotube Membrane**





# **Molecular Modeling and Simulations**

#### Nanofiller

#### Nanocomposite



#### Modified GROMOS force field

$E_{PE} = \sum k_r (r)$	$(-r_0) + \sum k_0$	$_{\theta}\left( \theta - \theta_{0} \right) +$	$\sum k_{\xi} (\xi$	$-\xi_0)$	
bonds					
$+\sum_{torsional}k_{\Phi}\left[1+c\right]$	$\cos(n\theta - \delta)] +$	$-\sum_{i}\sum_{j>i}f_{ij}\left\{rac{q_{i}}{2} ight.$	$\frac{q_j e^2}{r_{ij}} + 4\varepsilon_{ij}$	$\left[\left(\frac{\sigma_{ij}}{r_{ij}}\right)^{12}-\right.$	$\left(\frac{\sigma_{ij}}{r_{ij}}\right)^{6}$

Bonds	$k_b~(10^{\rm 5}/\rm{kJ~mol^{-1}~nm^{-2}})$			b <sub>0</sub> (nm)			
Si–O		2.5080			0.160		
Si-CH <sub>3</sub>		2.5080	_		0.188		
Angles		$k_{\Theta}  (\text{kJ/mol}^{-1}  \text{rad}^{-1})$	2)	$\Theta_0$ (deg)			
Si–O–Si		118.4		114.0			
O-Si-O		791.2			109.5		
O-Si-CH <sub>3</sub>		418.4			109.5		
CH <sub>3</sub> -Si-CH <sub>3</sub>		418.4			109.5		
Dihedrals		$k_\varphi~(\rm kJ~mol^{-1})$		n	δ		
CH3-Si-O-Si		3.77		3	0		
Si-O-Si-CH3		3.77		3	0		
Si-O-Si-O		3.77		3	0		
O-Si-O-Si		3.77		3	0		
Nonbonded	$\epsilon \; (\rm kJ \: mol^{-1})$		$\sigma \; (\rm nm)$	q(e)	(a.m.u)		
Si	2.4480		0.3385	0.3	28.080		
0	0.8493		0.2955	-0.3	15.999		
CH <sub>3</sub> (PDMS)	0.7532		0.3786	0	15.035		
He	0.0850		0.2580	0	4.003		
H <sub>2</sub>	0.3076		0.2950	0	2.016		
Ar	0.9977		0.3400	0	39.948		
N <sub>2</sub>	0.7898		0.3700	0	28.013		
O2	0.9145		0.3500	0	31.998		
CH <sub>4</sub>	1.2466		0.3733	0	16.043		

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Mass transfer flux 
$$J_A = P_A \left(\frac{dp_A}{dx}\right) = D_A \left(\frac{dc_A}{dx}\right)$$

- $p_A$  partial pressure of gas molecule A
- $c_A$  concentration of gas molecule A
- $P_A$  Permeability of polymer for gas molecule A
- $D_A$  Difusion coefficient of gas molecule A inside polymer

$$S_A = \frac{c_A}{p_A}$$

 $S_A$  Solubility of gas molecule A inside polymer

Separation factor (also called selectivity)  $\alpha_{A/B} = \frac{P_A}{P_B}$ 

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Separations	Suitable Polymers		
O <sub>2</sub> /N <sub>2</sub>	Silicone rubber		
	Polysiloxane-block-polycarbonate		
	Polysulfone		
	Ethylcellulose		
	Poly[(1-trimethylsilyl)-1-propyne]		
	Polypyrrolone		
	Polytriazole		
	Polyaniline		
H <sub>2</sub> from CO, CH <sub>4</sub> , N <sub>2</sub>	Polysulfone		
Acid gases (CO <sub>2</sub> and $H_2S$ ) from hydrocarbons	Cellulose acetate		
(e.g., natural gas and enhanced oil-recovery)	<sup>')</sup> Poly(vinyl chloride)		
	Polysulfone		
	Polyetherimide		

#### Table 12-4 Applications for Polymeric Membranes in Gas Separations

Hydrocarbon vapors from air

Silicone rubber

# Table 12-7 Kinetic Diameters and Lennard-Jones Potential Well Depth\* of Important Gases

Gas:	He	H <sub>2</sub>	C02	02	N <sub>2</sub>	CO	CH4
Kinetic diameter (Å)	2.6	2.89	3.3	3.46	3.64	3.76	3.80
<i>ɛ/k</i> (K)	10.2	59.7	195	107	71.4	91.7	149
σ(Å)	2.55	2.83	3.94	3.47	3.80	3.69	3.76

\*See text footnote for identification of the Lennard-Jones  $\varepsilon/k$  and  $\sigma$  parameters.

Polymer	$P(\mathbf{O}_2)^*$	$\frac{P(O_2)}{P(N_2)}$	$P(\mathbf{CO}_2)$	$\frac{P(\text{CO}_2)}{P(\text{CH}_1)}$
	Petrologia	- (2)		- (()4)
Rubbery Polymers	12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Calles		
High-density polyethylene ( $\rho = 0.964$ )	0.4	2.9	1.7	4.4
Butyl rubber	1.3	3.9	5.8	6.6
Low-density polyethylene ( $\rho = 0.914$ )	2.9	3.0	12.6	4.3
Natural rubber	24	3.0	134	4.7
Silicone rubber	610	2.2	4,553	3.4
Glassy Polymers				
Poly(ethylene terephthalate) ( $X_c = 0.50$ )	0.06	4.5	0.30	ns <u>on</u> brinklik
Cellulose acetate	0.68	3.4	5.5	28
Polysulfone	1.3	5.2	4.9	23
Polycarbonate	1.5	5.2	6.0	23
Polystyrene	2.6	3.3	10.5	a <u>my</u> orla.at
Poly(2,6-dimethyl-1,4-phenylene oxide)	18	5.0	59	15
Poly(4-methylpentene-1)	29	4.4	93	Trainin wi
Poly[1-(trimethylsilyl)-1-propyne]	7,200	1.7	19,000	4.4



### Permeability of Polydimethylsiloxane

Table 12-1 Permeability Coefficients of Selected Polymers at 25°C\* CH. P(0,)<sup>†</sup> Polymer ~0.0001 CH, Poly(vinyl alcohol) ~0.002 Polyacrylonitrile CH 0.012 Poly(vinylidene chloride) CH 0.012 Polymethacrylonitrile 0.42 Poly(ethylene terephthalate) 0.48 Poly(vinyl chloride)  $-0 - Si - CH = (CH_{2} + H)$ - CH\_- CH\_ 3.3 Poly(vinyl acetate) R 10.8 Polypropylene R - Si - R- R 30.0 Polyethylene (LDPE) 90.0 Polyisobutylene R - Si - RR - Si - R ~3000 Polydimethylsiloxane - Si - CH = (CH + H)-\*Data taken from ref. 1.  $^{\dagger}P \times 10^{11} \text{ cm}^3\text{-cm/cm}^2\text{-sec cmHg at 0\% humidity}$  $^{\ddagger}P \times 10^{11} \text{ g-cm/cm}^2 \text{ sec cmHg}$ Polymer Crosslinker

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#### **Measurement of Diffusion Coefficient**



**Figure 12-10** Plot of the amount of permeant versus time for a flat film illustrated at the left. The slope of the linear portion of the curve gives the steady-state permeability, while the intercept with the time axis yields the time lag,  $\theta$ , from which the apparent diffusion coefficient can be obtained (eq. 12.22). The increase in permeant concentration in the film up to the attainment of steady state is illustrated at the left.



# Measurement of Solubility



Figure 12-8 Sorption isotherm of CO₂ in silicone rubber at 35°C. Data points give CO₂ concentrations measured at different pressures during sorption (○) and desorption (●). The solid line represents the fit by the Flory–Huggins equation; the broken line represents Henry's law behavior. (Reprinted with permission from G. K. Fleming and W. J. Koros, *Macromolecules*, 19, 2285 (1986). Copyright 1986 American Chemical Society.)



#### **Experimental set up**



- Preferred method for application of thin, uniform films to flat substrates.
- The polymer solution placed on the substrate is rotated at high speed in order to spread the fluid by centrifugal force.
- Rotation is continued for some time, with fluid being spun off the edges of the substrate, until the desired film thickness is achieved.



Neat polymer 18 µm thick DE-FG26-06NT42742



Filled polymer 28 µm thick

Figure 1: SEM picture of neat polymer and filled polymer on metallic substrate

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# **PDMS Carbon Nanotube Membrane**



Selectivity	Neat PDMS	PDMS+MWNT
Oxygen/Nitrogen	1.97	0.86
Hydrogen/Oxygen	1.01	2.05

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#### **PDMS-Silica Membrane**



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# **Difficulty in Measuring Diffusion Coefficient**



**Response of permeate pressure for neat PDMS- time lag method**  **Response of permeate pressure** for filled PDMS- time lag method

Selectivity of O2/N2	PDMS	Filled PDMS
CL <sub>A/B</sub>	2.04	8.54

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- Nanofillers have significant impact on both permeability and permselectivity of polymers.
- Whether or not the selectivity was controlled by the size of the molecules and the interactions between the molecules and the surfaces of the fillers remain to be investigated.
- Since silicone polymers are well known for their high free volume characteristics, this trade-off of slight reduction in permeability and drastic increase in selectivity seems to be commercially attractive.
- Molecular dynamics simulation model has been established to further the study of diffusion and solution of oxygen molecules in a nanofiller (nanotube and nanosilica) filled polymer system. This will lead to better understanding of filled polymer and guide the further experimental development of novel membrane in the next project period.

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Thank you for your attention.

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