



Semiannual Performance Report September 2003 through March 2004 for the Shiprock, New Mexico, Site

September 2004



U.S. Department
of Energy



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September 2003 through March 2004
for the Shiprock, New Mexico, Site**

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Work Performed by S.M. Stoller Corporation under DOE Contract No. DE-AC01-02GJ79491
for the U.S. Department of Energy Office of Legacy Management, Grand Junction, Colorado

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1.0 Introduction

This report evaluates the performance of the ground water remediation system at the Uranium Mill Tailings Remedial Action (UMTRA) Project site in Shiprock, New Mexico, for the period of September 2003 through March 2004. This evaluation is based upon comparison of the site conditions in March 2004 to the baseline site conditions presented in the Shiprock Baseline Performance Report (DOE 2003a). The baseline conditions were established using data collected primarily from March 2003. A detailed description of the site conditions is presented in the Site Observational Work Plan (SOWP) (DOE 2000), and the compliance strategy is presented in the Ground Water Compliance Action Plan (GCAP) (DOE 2002).

The Shiprock site is divided into two distinct areas, the floodplain and the terrace. An escarpment forms the boundary between the two areas. The terrace is further divided into terrace west and terrace east. Initially the remediation system (Figure 1) consisted of two floodplain ground water extraction wells, four terrace east ground water extraction wells, two interceptor drains (one installed in Bob Lee Wash and the other installed in Many Devils Wash), a lined evaporation pond, and a terrace drainage channel diversion structure. The terrace ground water extraction wells and interceptor drains became operational in late February 2003, and the floodplain extraction wells became operational in March 2003. Four additional extraction wells were installed on the terrace east portion of the site in July 2003; they were piped into the remediation system in early August 2003 in an attempt to increase the volume of ground water removed from the terrace.

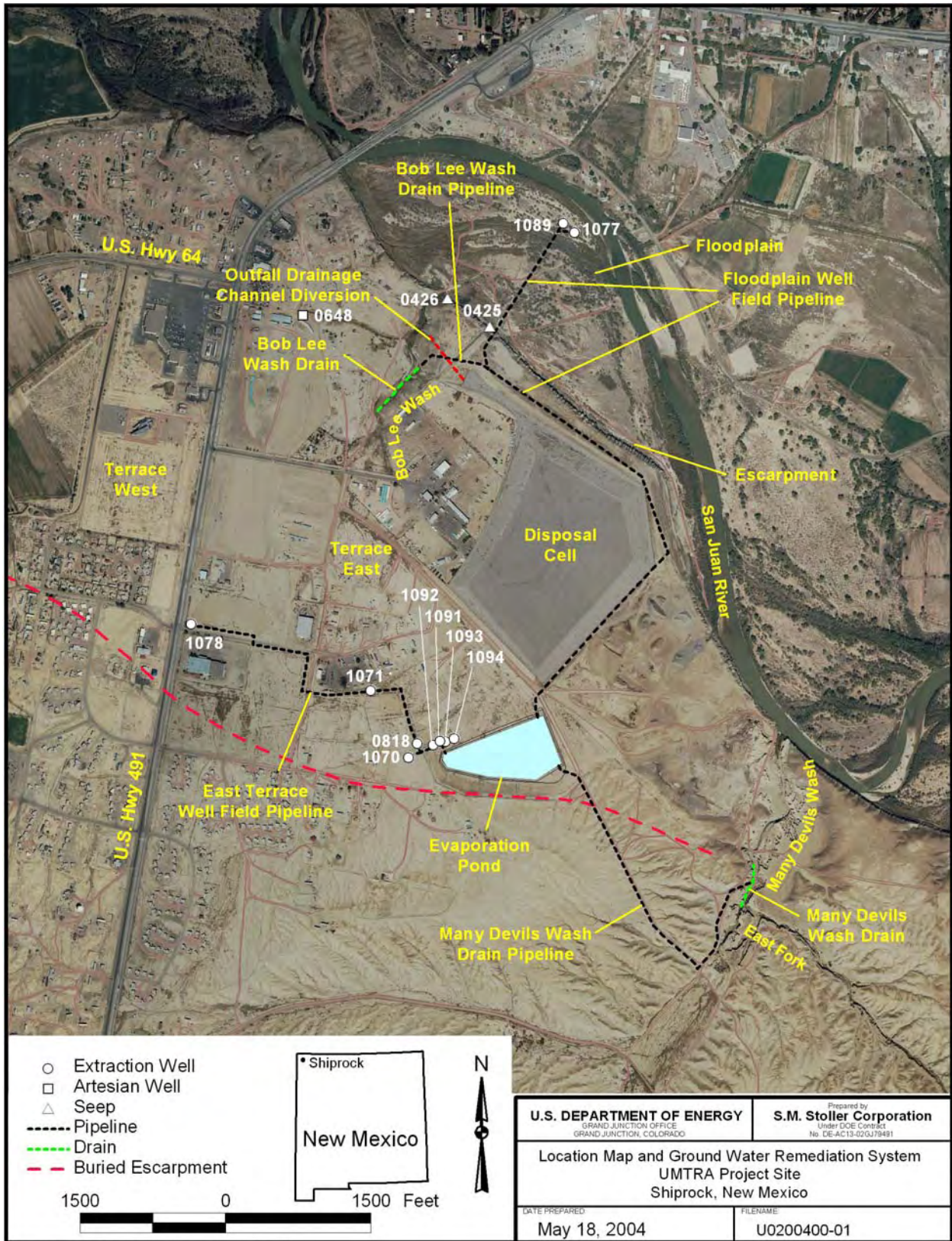
1.1 Remediation System Performance Standards

This performance assessment is based on the analysis of water quality and water level data obtained from site monitoring wells in addition to ground water flow rates associated with the drains and seeps. Specific performance standards as established for the Shiprock floodplain ground water remediation system in the Baseline Performance Report (DOE 2003a) are summarized as follows:

- Ground water flow directions in the vicinity of the extraction wells should be toward the extraction wells.
- Pumping on the floodplain should intercept contaminants of concern (COCs) that would otherwise discharge to the San Juan River.

Specific performance standards as established for the Shiprock terrace ground water remediation system (Section 3.2) in the Baseline Performance Report (DOE 2003a) are summarized as follows:

- Terrace ground water surface elevations should decrease as water is removed from the terrace system.
- Ground water flow directions in the vicinity of the extraction wells should be toward the extraction wells.
- The volume of water discharging to the interceptor drains located in Bob Lee and Many Devils Washes should decrease over time as ground water levels on the terrace decline.
- The flow rates of seeps located at the escarpment face (locations 0425 and 0426) should decrease over time as ground water levels on the terrace decline.



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Figure 1. Location Map

1.2 Contaminants of Concern and Remediation Goals

Ground water at the site is contaminated as a result of uranium milling activities between 1954 and 1968. The COCs for both the floodplain and terrace are ammonium, manganese, nitrate, selenium, strontium, sulfate, and uranium. Ground water compliance for the terrace is based on hydrologic control and concentration standards do not apply.

Floodplain compliance standards for uranium and nitrate are their respective UMTRA standards of 0.044 and 44 milligrams per liter (mg/L).

A secondary standard of 250 mg/L for sulfate exists under the Safe Drinking Water Act. However, studies conducted by the Centers for Disease Control in conjunction with the U.S. Environmental Protection Agency (EPA) have shown that no adverse effects from sulfate ingestion occur at concentrations of up to 1,200 mg/L (EPA 1999). The report notes that other studies have shown that concentrations of sulfate exceeding 2,000 mg/L may have little to no adverse effect on humans and animals. Because of the presence of high background sulfate concentrations at the site in the floodplain (up to 1,920 mg/L) and the high sulfate concentration of water entering the floodplain from flowing artesian well 0648 (up to 2,340 mg/L), the proposed cleanup goal for floodplain sulfate is 2,000 mg/L.

Relatively high selenium concentrations in the floodplain make it unlikely that the UMTRA standard of 0.01 mg/L for this constituent can be met while contaminated terrace water is still providing a source. An alternate concentration limit is proposed for selenium of 0.05 mg/L, which is the maximum contaminant level established by EPA.

The cleanup objective for manganese is the maximum background concentration for the floodplain, which is currently 2.74 mg/L. There are no cleanup standards or background concentrations established for ammonium and strontium.

1.3 Hydrogeological Setting

Sections 1.3.1 and 1.3.2 provide a summary of the floodplain and terrace ground water systems, respectively. A more detailed description is provided in the SOWP (DOE 2000).

1.3.1 Floodplain Ground Water System

The thick Mancos Shale of Cretaceous age forms the bedrock underlying the entire site. Floodplain ground water (floodplain alluvial aquifer) occurs in unconsolidated medium- to coarse-grained sand, gravel, and cobbles that were deposited in former channels of the San Juan River above the Mancos Shale. The floodplain aquifer is hydraulically connected to the San Juan River; the river contributes water to the floodplain in some areas, and receives ground water discharge in others. The floodplain aquifer also receives inflow from an artificial ground water system in the terrace area created during milling activities. The floodplain alluvium is up to 20 feet (ft) thick and overlies Mancos Shale, which is typically soft and weathered for the first several feet below the alluvium.

Most ground water contamination in the floodplain lies close to the escarpment east and north of the disposal cell. A plume extends northward from this contaminated area in an arc-shape as it

crosses the floodplain and reaches the San Juan River near the two floodplain extraction wells (1089 and 1077, Figure 1). This plume configuration is best characterized by elevated concentrations of sulfate and uranium. Contamination does not occur along the escarpment base in the northwest part of the floodplain because relatively uncontaminated surface water from Bob Lee Wash discharges into the floodplain, recharging local ground water and then flowing to the north and west. Water that enters the floodplain from Bob Lee Wash consists mainly of deep nonpotable ground water from flowing (approximately 65 gallons per minute [gpm]) artesian well 0648 that drains eastward into lower Bob Lee Wash. Background ground water quality in the floodplain aquifer has been defined by monitor wells installed in the floodplain about 1 mile upriver from the site.

1.3.2 Terrace Ground Water System

The terrace ground water system occurs partly in unconsolidated alluvium in the form of medium- to coarse-grained sand, gravel, and cobbles deposited in the floodplain of the ancestral San Juan River. Terrace alluvial material is Quaternary in age, typically 10 to 20 ft thick, and caps the Mancos Shale. Though less well mapped, some terrace ground water also occurs in weathered Mancos Shale underlying the alluvium. The Mancos Shale is exposed in the escarpment overlooking the present floodplain.

The terrace alluvial aquifer extends southwestward from the escarpment separating the terrace from the floodplain for up to 1 mile where it is abruptly bounded by a buried escarpment. Terrace alluvial material is exposed at the terrace/floodplain escarpment, but southwestward from there it is covered by an increasing thickness of silt, which was deposited by wind as loess. At the southwest edge of the terrace aquifer, along the base of the buried escarpment, up to 40 ft of loess overlies the alluvium. The alluvium in this latter area consists of coarse, ancestral San Juan River deposits.

Mancos Shale in the terrace area is weathered (fractured and soft) for up to several feet below its contact with alluvium. Ground water is known to occur in the weathered shale, and may flow through deeper portions of the shale that might be fractured.

2.0 Subsurface Conditions

This section summarizes hydraulic and water quality characteristics of the floodplain and terrace ground water systems in March 2004, approximately 1 year after startup of the treatment system. The response of the floodplain is evaluated in Section 2.1, and the terrace response is evaluated in Section 2.2.

2.1 Floodplain Subsurface Conditions

Performance standards provided in the Baseline Performance Report (DOE 2003a) and presented in Section 1.1 regarding the floodplain are designed to evaluate the effectiveness of the floodplain treatment system. An analysis of the horizontal hydraulic gradients and contaminant distributions in the floodplain are discussed in Sections 2.1.1 and 2.1.2, respectively.

2.1.1 Horizontal Hydraulic Gradients

The Baseline Performance Report contains a map of horizontal hydraulic gradients in the floodplain as determined from three-point analyses of March 2003 water level data. This figure, which represents conditions prior to the start-up of the floodplain extraction wells, is presented as Figure A-1 in Appendix A of this report. Figure A-2 (Appendix A) presents comparable horizontal gradients developed from a three-point analysis of water level data collected in March 2004. Comparison of the two maps shows that the ground water flow directions have changed in response to ground water extraction between March 2003 and March 2004. The river flow on the day the March 2003 water level data were measured was 649 cubic feet per second (cfs), while the flow on the day the March 2004 data were collected was 1,540 cfs. Despite the higher river level, which should increase flow to the floodplain, ground water is directed more toward the extraction wells in 2004.

Appendix B contains graphs of floodplain ground water elevation fluctuations between January 2003 and March 2004 collected using data loggers installed in wells 0617, 0736, 0857, and 1008. A data logger was also installed in well 0854 but it malfunctioned after the instrument was downloaded in August 2003 and the data collected between August 2003 and March 2004 were lost; therefore, its data are not included in Appendix B. This instrument was re-started in March 2004 and will provide ground water elevation data in the next performance report.

Well 0617 is located approximately 600 ft from the river. Wells 0736, 0857, and 1008 are located approximately 200 ft from the river. The ground water elevation data collected from these wells located on the floodplain are plotted with the San Juan River flow data (in cfs) collected from U.S. Geological Survey Gaging Station 09368000 (located in Shiprock) to show how the elevation fluctuates in response to changes in the river stage. The wells located near the river responded quickly to river level fluctuations; however, the river influence was apparently subdued within 600 ft inland.

2.1.2 Contaminant Distributions

Ground water samples were collected from selected floodplain wells in March 2004. The resulting COC concentrations were compared to baseline concentrations measured in March 2003 during the last sampling effort prior to full operation of the treatment system. Table 1 lists both floodplain baseline and March 2004 concentrations for the COCs.

In order to compare the data sets, it was necessary to convert the baseline ammonium and nitrate concentrations. Ammonium concentrations were converted from “ammonia total as NH_4 ” to “ammonia as total nitrogen.” The baseline nitrate concentrations were converted from “nitrate as NO_3 ” to “nitrate plus nitrite as nitrogen.” These conversions were made in response to different analyses being requested with a change in laboratories. As a result, the baseline concentrations in Table 1 are not consistent with the previous semiannual report (DOE 2003b).

The data show that the majority of the contaminant concentrations have not significantly changed compared to the baseline concentrations. Five samples had increases greater than 100 percent compared to the baseline concentrations. Of these five samples (well 0734 ammonium, manganese, nitrate, and selenium concentrations plus well 0736 nitrate concentration) all except the well 0734 nitrate concentration deal with concentrations below 1 mg/L. Of the wells that have changed significantly, it is believed that the concentration

Table 1. March 2004 COC Concentration Comparison to Baseline Data

Well	Ammonium			Manganese			Nitrate			Selenium			Strontium			Sulfate			Uranium		
	Baseline ^a Concentration (mg/L)	March 2004 Concentration (mg/L)	Difference (%)	Baseline Concentration (mg/L)	March 2004 Concentration (mg/L)	Difference (%)	Baseline ^b Concentration (mg/L)	March 2004 Concentration (mg/L)	Difference (%)	Baseline Concentration (mg/L)	March 2004 Concentration (mg/L)	Difference (%)	Baseline Concentration (mg/L)	March 2004 Concentration (mg/L)	Difference (%)	Baseline Concentration (mg/L)	March 2004 Concentration (mg/L)	Difference (%)	Baseline Concentration (mg/L)	March 2004 Concentration (mg/L)	Difference (%)
0608	303	220	-27.3	7.8	4.4	-43.6	524	510	-2.7	0.0065	0.0055	-15.4	10.7	12	12.1	10,500	11,000	4.8	1.78	1.8	1.1
0614	39	32	-18.5	6.01	5.1	-15.1	958	950	-0.8	0.291	0.06	-79.4	13.1	12	-8.4	14,400	13,000	-9.7	2.43	2.3	-5.3
0615	40	17	-57.1	5.56	3.4	-38.8	940	950	1.1	1.16	0.64	-44.8	14.4	14	-2.8	19,900	20,000	0.5	3.78	3.8	0.5
0618	604	54	-91.1	11.3	9.48	-16.1	278	200	-28.0	0.352	0.468	33.0	11.2	11.3	0.9	13,300	14,000	5.3	3.12	3.0	-3.8
0619	2.3	1.7	-24.6	3.13	2.02	-35.5	4.95	0.65	-86.9	0.213	0.0596	-72.0	7.32	5.7	-22.1	6,280	4,400	-29.9	0.48	0.345	-28.1
0734	0.003	0.1	3114.2	0.656	1.37	108.8	1.68	5.5	227.7	0.0086	0.0309	259.3	6.63	9.52	43.6	4,940	6,570	33.0	0.0735	0.0637	-13.3
0735	12	14	21.6	3.47	3.1	-10.7	454	530	16.7	0.159	0.041	-74.2	9.3	8.7	-6.5	6,980	7,500	7.4	0.24	0.25	4.2
0736	0.072	0.1	39.6	1.54	0.33	-78.6	0.019	0.23	1125.2	0.0007	0.0009	28.6	6.79	6.1	-10.2	3,480	5,200	49.4	0.146	0.15	2.7
1008	22	17	-23.6	6.61	6.0	-9.2	39	47	21.0	0.169	0.24	42.0	10.2	9.5	-6.9	13,900	12,000	-13.7	2.05	1.6	-22.0

Notes: a = Baseline ammonium concentrations were converted from "Ammonia Total as NH₄" to "Ammonia as Total N" for comparison purposes
 b = Baseline nitrate concentrations were converted from "Nitrate as NO₃" to "Nitrate + Nitrite as N" for comparison purposes

variations may be attributed to other factors (i.e., seasonal fluctuations) as opposed to ground water extraction.

Figure 2 through Figure 8 illustrate the spatial distribution of concentrations measured in March 2004 for ammonium, manganese, nitrate, selenium, strontium, sulfate, and uranium, respectively.

As previously mentioned, the site conceptual model suggests that pumping from the floodplain will not strongly affect COC concentrations. Consequently, concentrations measured in March 2004 were not expected to be significantly different from baseline concentrations. As a result, contouring of contaminant levels in March 2004 did not seem warranted at this time. Sampling is currently ongoing to develop a baseline for contaminant mass removal from both the floodplain and terrace. Future performance reports may include contoured contaminant plume maps as pumping from the floodplain continues.

2.2 Terrace System

Performance standards provided in the Baseline Performance Report (DOE 2003a) and presented in Section 1.1 for the terrace are designed to evaluate the effectiveness of the terrace treatment system. Analyses of horizontal hydraulic gradients, water level trends, drain flow rates, and seep flow rates associated with the terrace are discussed in Sections 2.2.1, 2.2.2, 2.2.3, and 2.2.4, respectively. There are no contaminant concentration performance standards because compliance is based on hydrologic control. As a best management practice, selected contaminant concentrations are being measured for the extraction system. Estimates of mass removal will be presented in the next performance report.

2.2.1 Horizontal Hydraulic Gradients

The Baseline Performance Report (DOE 2003a) contains a map of horizontal hydraulic gradients in the terrace as determined from three-point analyses of March 2003 water level data. This figure, which represents the baseline condition prior to the start-up of the terrace extraction wells, is presented as Figure A-5 of Appendix A in this report. Figure A-6 (Appendix A) presents comparable horizontal gradients developed from three-point analysis of the water level data collected in March 2004.

Comparison of the two gradient maps shows that the flow directions during the two periods are generally the same, except in the vicinity of the terrace extraction wells. The ground water flow direction in the vicinity of well 0604 (which is located near extraction well 0818) has shifted from the northeast in March 2003 to the northwest in March 2004. The impact of the ground water withdrawal in the vicinity of well 0604 from nearby extraction well 0818 is evident based on the datalogger data from well 0604 in Appendix B.

2.2.2 Water Level Trends

The March 2004 water level data were compared to terrace baseline ground water elevations presented in Table 1 of the Baseline Performance Report (DOE 2003a). Table 2 summarizes the resulting changes in ground water levels and Figure 9 presents a map view of ground water elevation increases and decreases. In general, the ground water elevation appears to be consistent or slightly decreasing in the vicinity of the terrace extraction wells and decreasing in the terrace west area.

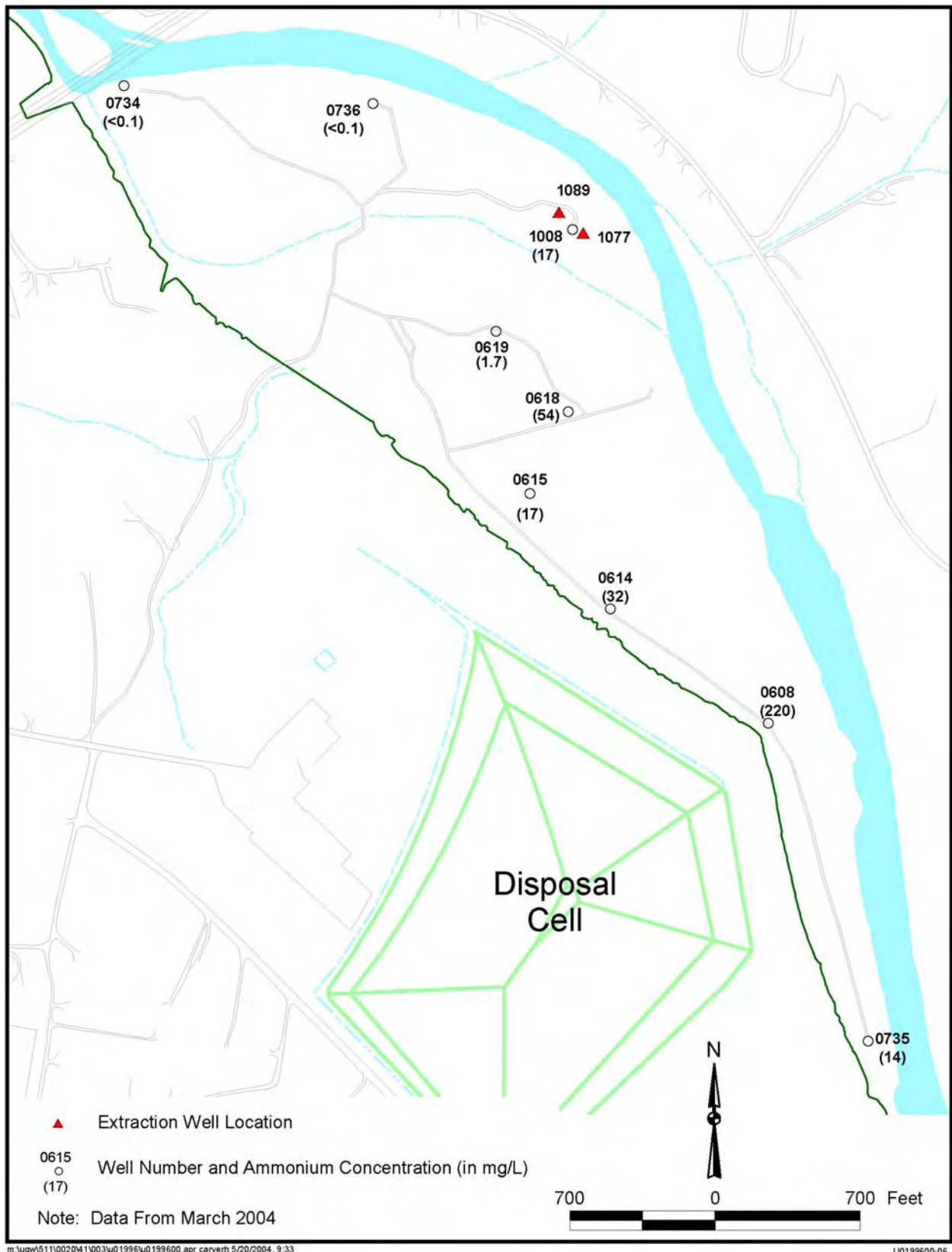
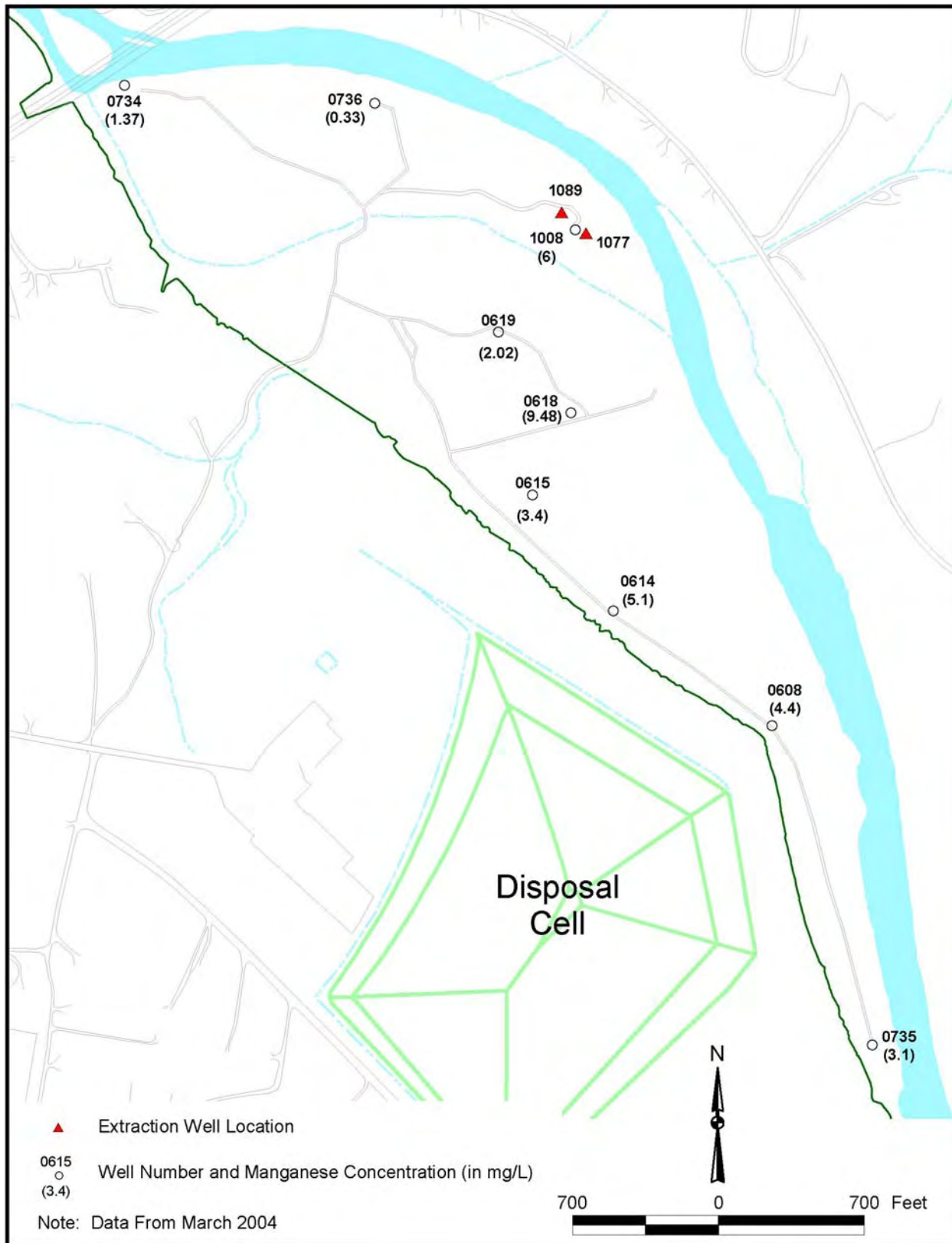


Figure 2. Floodplain Ammonium Ground Water Concentrations



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Figure 3. Floodplain Manganese Ground Water Concentrations

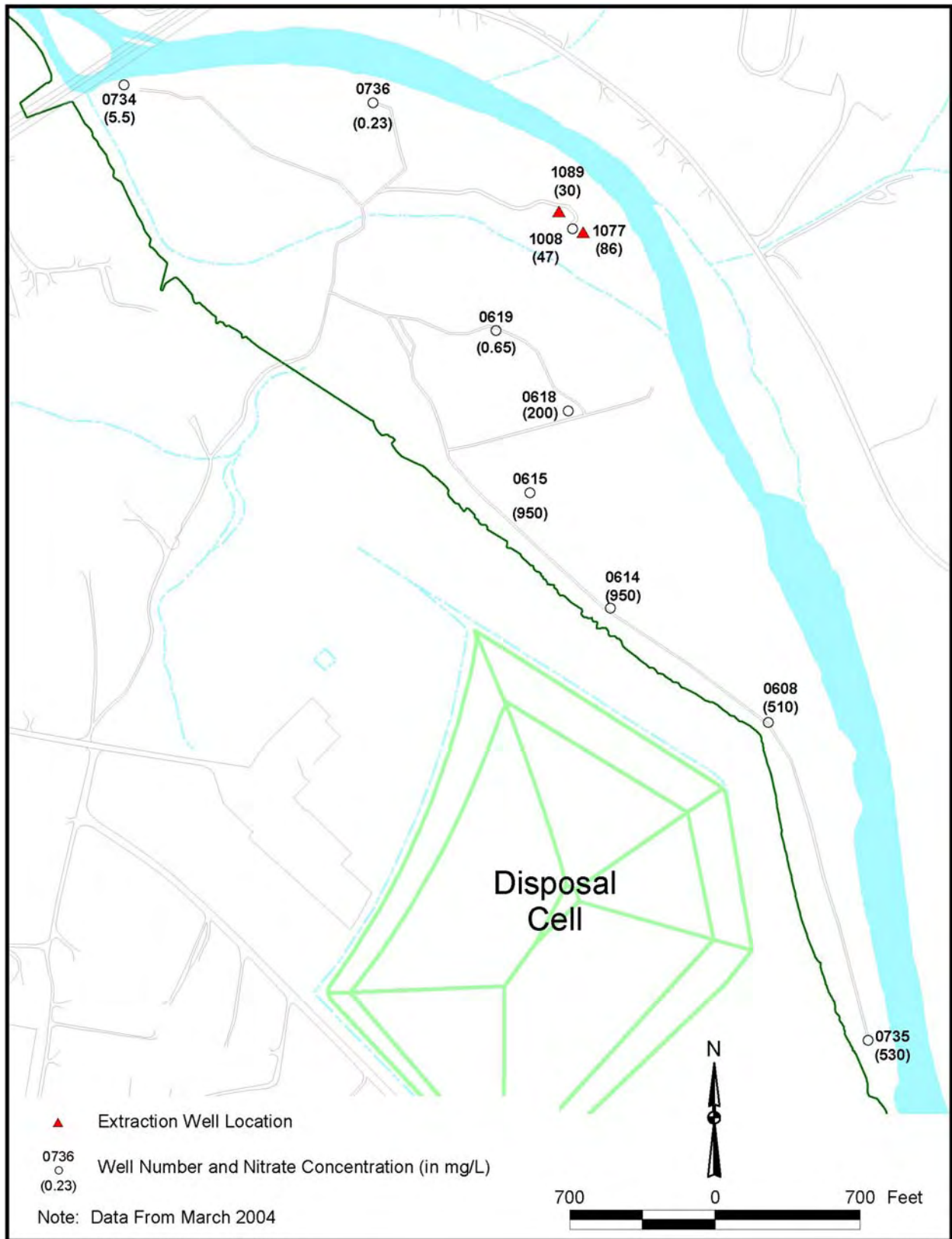
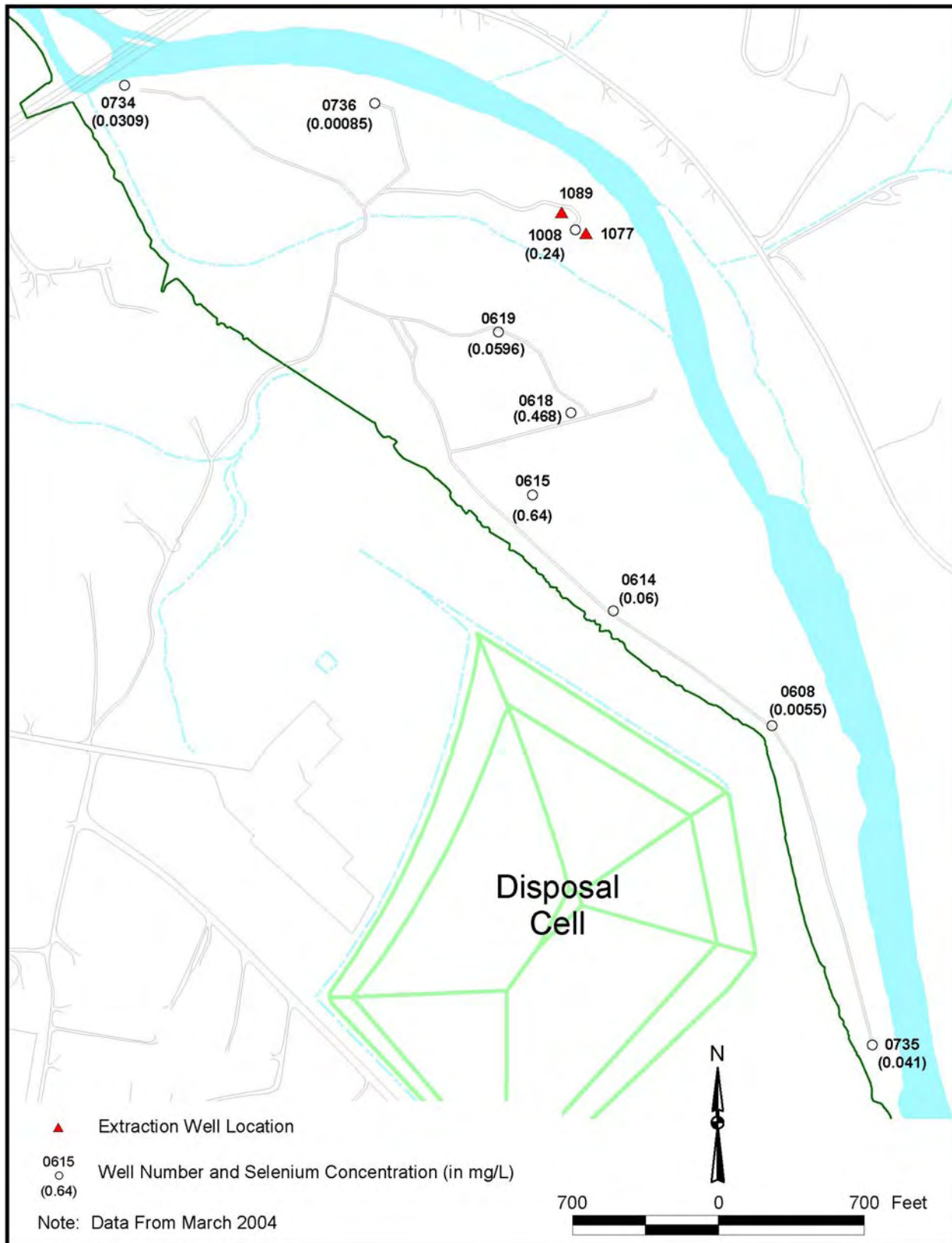


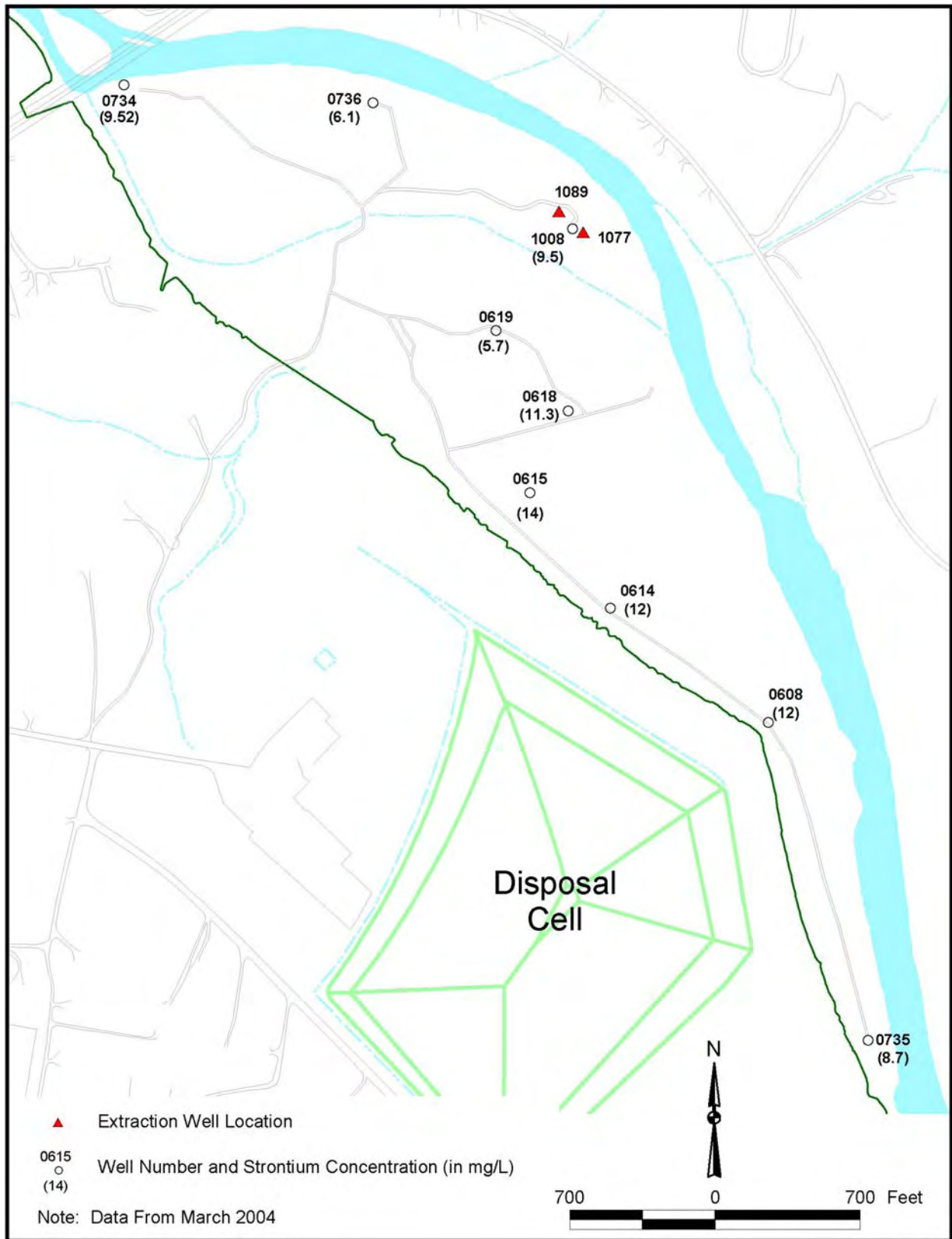
Figure 4. Floodplain Nitrate Ground Water Concentrations



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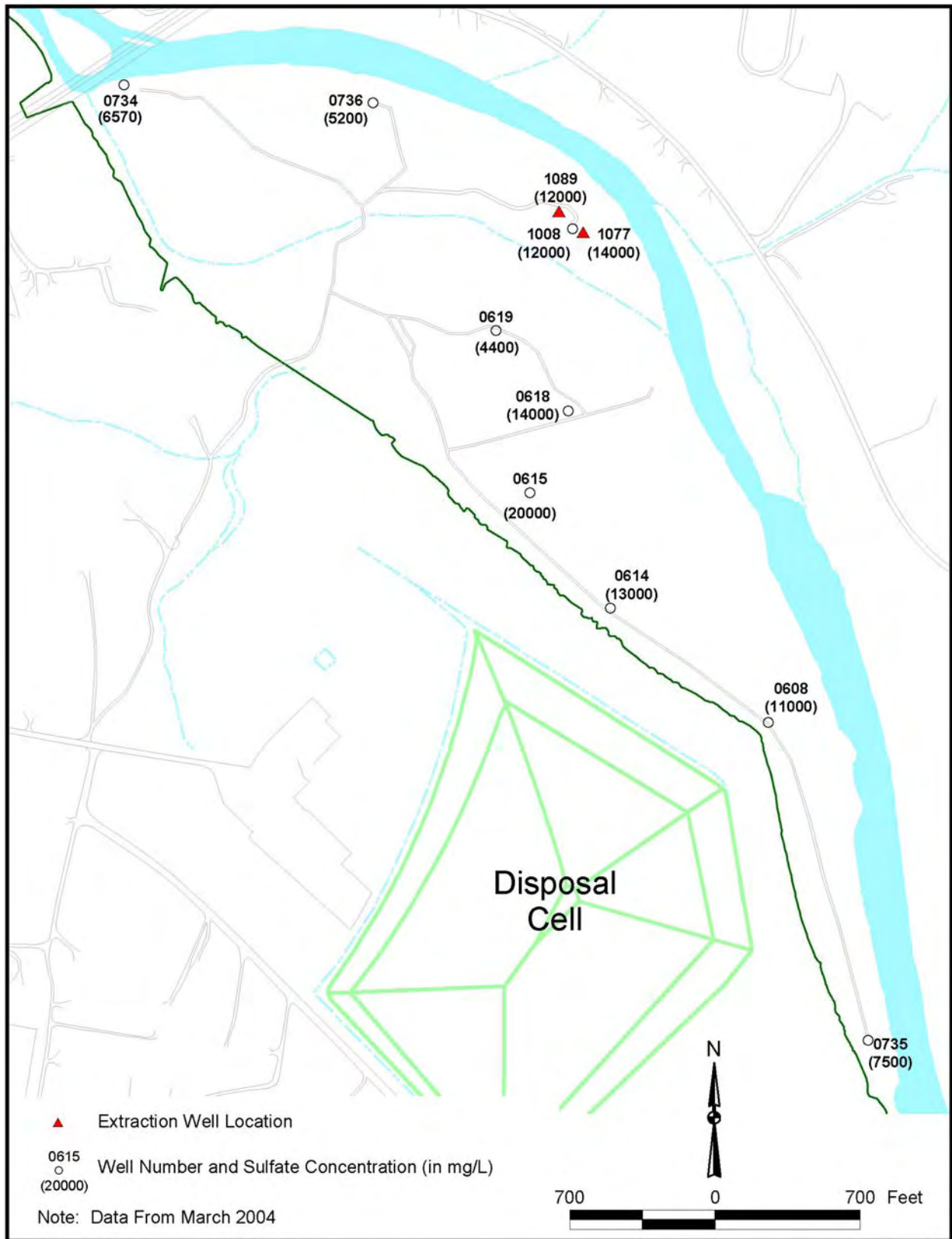
Figure 5. Floodplain Selenium Ground Water Concentrations



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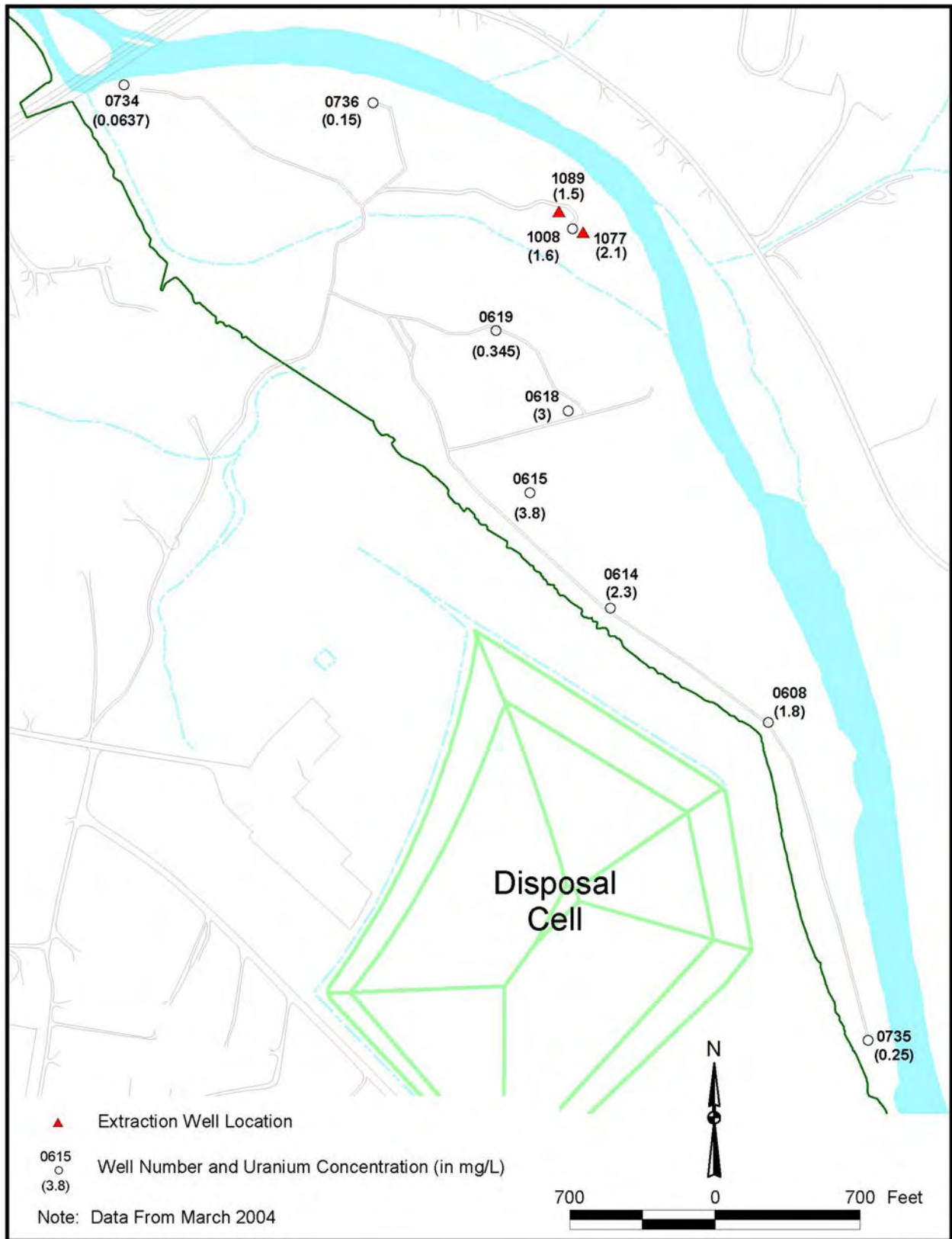
Figure 6. Floodplain Strontium Ground Water Concentrations



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Figure 7. Floodplain Sulfate Ground Water Concentrations



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Figure 8. Floodplain Uranium Ground Water Concentrations

Table 2. Comparison of Terrace March 2004 Water Level Data to Baseline Conditions

Well	Zone of Completion	Baseline Ground Water Elevation ^a (ft msl)	March 2004 Ground Water Elevation (ft msl)	Difference in Elevation ^b (ft)
0604*	Mancos	4,944.48	4,943.22	-1.26
0727	Mancos	4,933.89	4,933.70	-0.19
0728*	Alluvium / Mancos	4,940.25	4,940.19	-0.06
0730	Alluvium / Mancos	4,946.26	4,945.08	-1.18
0812*	Alluvium / Mancos	4,944.62	4,944.31	-0.31
0813*	Alluvium / Mancos	4,941.03	4,941.12	0.09
0814*	Alluvium / Mancos	4,936.27	4,936.23	-0.04
0815*	Alluvium / Mancos	4,927.78	4,927.80	0.02
0817*	Mancos	4,938.68	4,938.59	-0.09
0819*	Mancos	4,935.68	4,935.65	-0.03
0826*	Alluvium / Mancos	4,933.02	4,932.83	-0.19
0827	Alluvium / Mancos	4,920.12	4,920.11	-0.01
0828*	Alluvium / Mancos	4,934.83	4,934.17	-0.66
0832*	Alluvium / Mancos	4,936.26	4,936.22	-0.04
0835*	Alluvium	4,911.10	4,910.89	-0.21
0836*	Alluvium	4,878.25	4,878.86	0.61
0838*	Alluvium	4,911.73	4,911.12	-0.61
0839*	Alluvium / Mancos	4,917.32	4,916.76	-0.56
0841*	Alluvium	4,939.06	4,938.65	-0.41
0846*	Alluvium / Mancos	4,910.93	4,910.10	-0.83
1007*	Alluvium / Mancos	4,917.91	4,917.41	-0.50
1057*	Alluvium	4,948.32	4,948.32	0.00
1059*	Mancos	4,947.64	4,947.47	-0.17
1060*	Alluvium / Mancos	4,932.64	4,932.23	-0.41
1067*	Alluvium / Mancos	dry	dry	na
1068*	Alluvium / Mancos	4,920.71	4,920.61	-0.10
1069*	Alluvium / Mancos	4,920.15	4,916.99	-3.16
1073	Alluvium	4,941.99	4,941.63	-0.36
1079*	Alluvium	4,909.89	4,909.39	-0.50

^aBaseline Water Levels Measured In All Wells In March 2003 With The Exception Of Well 1073 (September 2002)

^bMarch 2004 Water Level – Baseline Water Level

Notes: na = not applicable, water level not measured

* = designates a well included in the long-term monitoring plan

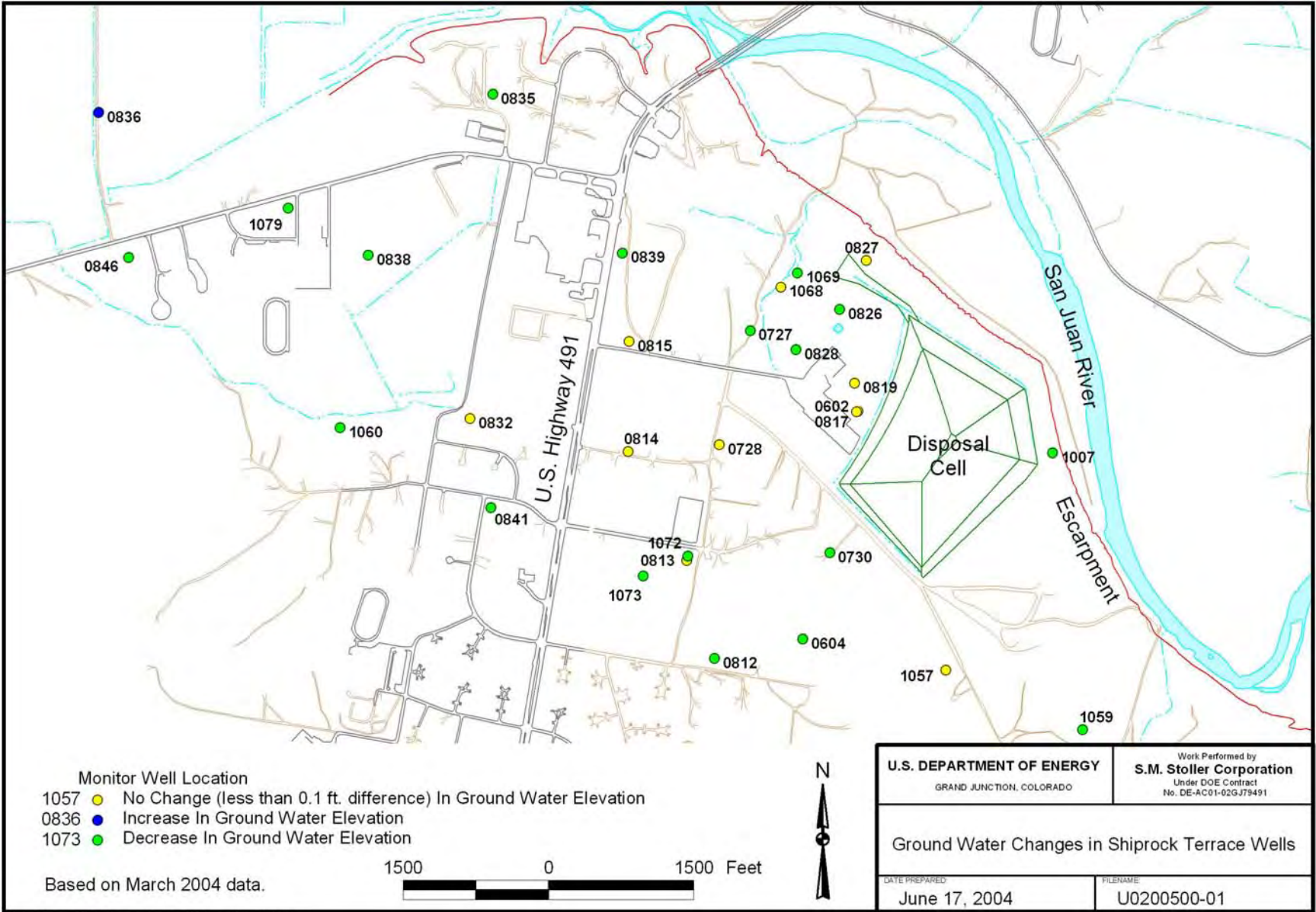


Figure 9. Terrace Ground Water Elevation Changes Between Baseline Conditions and March 2004

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Water levels have also been monitored using pressure transducers that had been installed in selected wells on the terrace prior to treatment system startup. Appendix B contains plots of ground water elevation data collected from pressure transducers connected to dataloggers in terrace east wells 0602, 0604, 0731, 0813, 0819, 0826, 0827, and 0830. These graphs indicate that water levels in the terrace east area from March 2003 to March 2004 in general do not fluctuate significantly and exhibit a slight (approximately a 0.5 ft decrease across the site) declining trend.

Based on previous datalogger results, well 0730 has shown an increasing ground water elevation (DOE 2003b). The surface casing of well 0730 was destroyed shortly after the datalogger was downloaded in August 2003, and the data logger was removed. The well was reconditioned and the datalogger was re-installed in March 2004, and the data will be included in the next performance report.

Appendix B also contains plots of ground water elevation data collected by dataloggers in terrace west wells 0837, 0841, 0843, 0846, and 1060. The graphs indicate ground water elevations in the vicinity of terrace west fluctuate in response to irrigation practices in that area.

2.2.3 Seep Flow Rates

Rates of ground water discharge at seeps 0425 and 0426 were also measured in March 2004. The flow rate at seep 0425 was only 0.04 gpm, which is significantly lower than the rate measured in March 2003 (0.5 gpm). Between October 2002 and March 2003, the minimum flow rate measured was 0.4 gpm. With only 1 year of active remediation from the terrace, it is unlikely that the reduced seep 0425 flow rate is a direct result of the terrace ground water extraction. Rather, it is more likely the rate decreased in March 2004 due to recent drought conditions in the region.

The flow measured at seep 0426 in March 2004 was 2.2 gpm, which is higher than the rate measured in March 2003 (1.8 gpm). Between October 2002 and March 2003, the maximum flow rate measured at seep 0426 was 2.1 gpm, suggesting that flow at the seep has not changed significantly since initiation of the extraction system.

2.2.4 Drain Flow Rates

As discussed in the Baseline Performance Report, the flow rate of the pump removing water from the drains installed in Bob Lee and Many Devils Washes was expected to decrease as ground water levels in the terrace decline. The flow rate data collected over the first 6 months of drain collection (i.e., March through August 2003) indicate the pump in Bob Lee Wash initially was pumping approximately 7 gpm, and that the water pump could not keep up with the water flowing into the drain.

During May 2003, ponded water was no longer on the surface, indicating the pump at that time was removing water from the system as fast as the system recharged the drain. Over the 6-month evaluation period (August 2003 to March 2004), the flow rate decreased at a relatively constant rate. At the end of March 2004, approximately 3.5 gpm was being pumped from the drain. Figure 10 was generated using ground water elevation data collected from wells 1067, 1068, and 1069, all of which are located adjacent to Bob Lee Wash. As this figure shows the ground water

elevations decreased significantly in well 1068 after March 2003, when the drain extraction system became operational. The ground water elevation in the vicinity of well 1069 has been more gradual, while well 1067 became dry starting in March 2003, has been dry since that time.

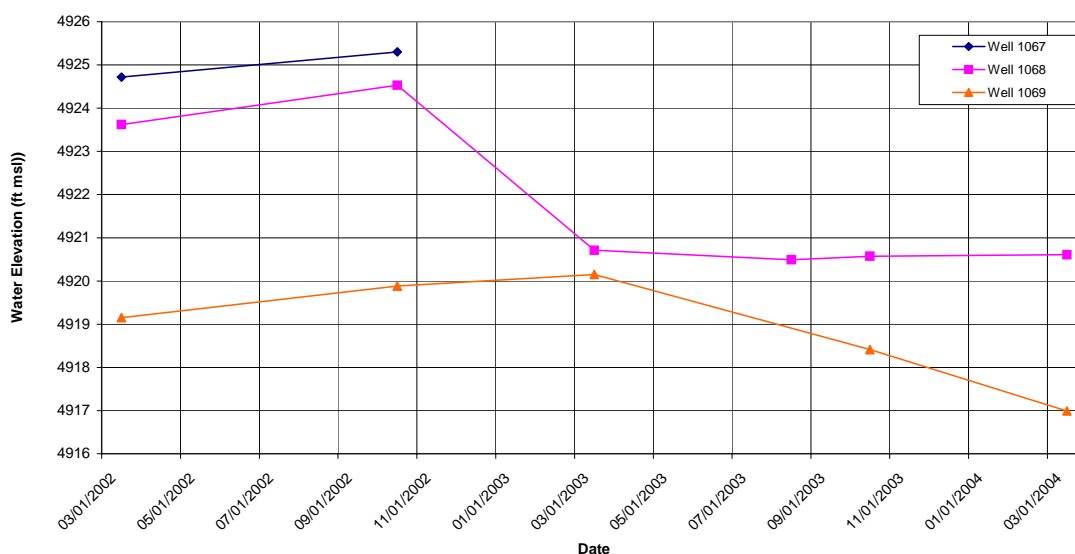


Figure 10. Ground Water Elevation Decrease in the Vicinity of Bob Lee Wash

While the pump at the Many Devils Wash drain removed water at an average rate of about 0.14 gpm between March and August 2003, the average between August 2003 and March 2004 was 0.48 gpm. This increase may be attributed to modifications made to the drain system in June 2003.

3.0 Remediation System Performance

The following sections provide a brief description of the components of the floodplain and terrace ground water remediation systems, and summarize their performance between baseline conditions and March 2004.

3.1 Floodplain Remediation System

The objective of the floodplain ground water extraction system is to remove ground water from the parts of the COC plumes near the San Juan River. Pumping is focused at this location to lessen exposure risk to aquatic life. All ground water collected from the floodplain extraction wells is piped south to the terrace where it discharges into the evaporation pond. A more complete description of the floodplain extraction system is presented in the Baseline Performance Report (DOE 2003a).

This system initially consisted of wells 1075 and 1077. These wells were drilled to approximately 20 ft below ground surface and had saturated alluvial thicknesses of 8 to 10 ft. After nearly 4 months of pumping, neither well was producing more than 3 gpm, far below the goal of 10 to 20 gpm per well. Both wells were re-developed a number of times in an attempt to increase the extraction rates. Ultimately, well 1075 was replaced with well 1089, which was

installed just north of 1075 using alternative methods. Specifically, well 1089 was constructed using a slotted culvert placed in a trench excavated to bedrock. After installation of the culvert, the pump was removed from well 1075 and placed inside the new well.

3.1.1 Extraction Well Performance

Figure 11 presents measured pumping rates and cumulative volume of ground water pumped from well 1089 from between September 2003 and March 2004. Increases in the pumping rates during late March 2004 can be attributed to the higher river stage of the nearby San Juan River (at higher river stages the pumping rate tends to increase due to the increased saturated thickness). By the end of March 2004, well 1089 had removed more than 2,512,300 gallons of water from the floodplain ground water system.

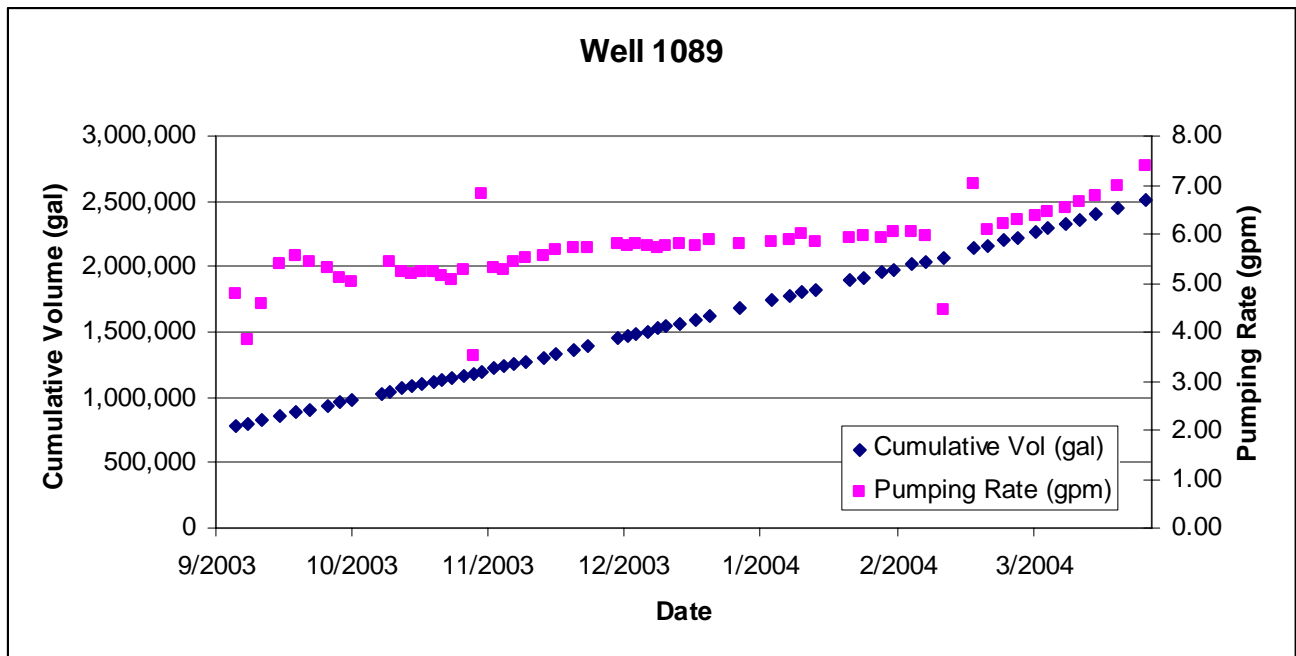


Figure 11. Well 1089 Pumping Rate and Cumulative Ground Water Volume Extracted

Well 1077 has not performed as efficiently as well 1089 (Figure 12). Between September 2003 and March 2004 the average pumping rate was only approximately 0.5 gpm (compared to an average of 5.7 from well 1089), and only approximately 305,131 gallons of ground water had been pumped from this well at the end of the period. Appendix C lists measured flow rates and corresponding volumes of ground water removed from floodplain extraction wells 1089 and 1077.

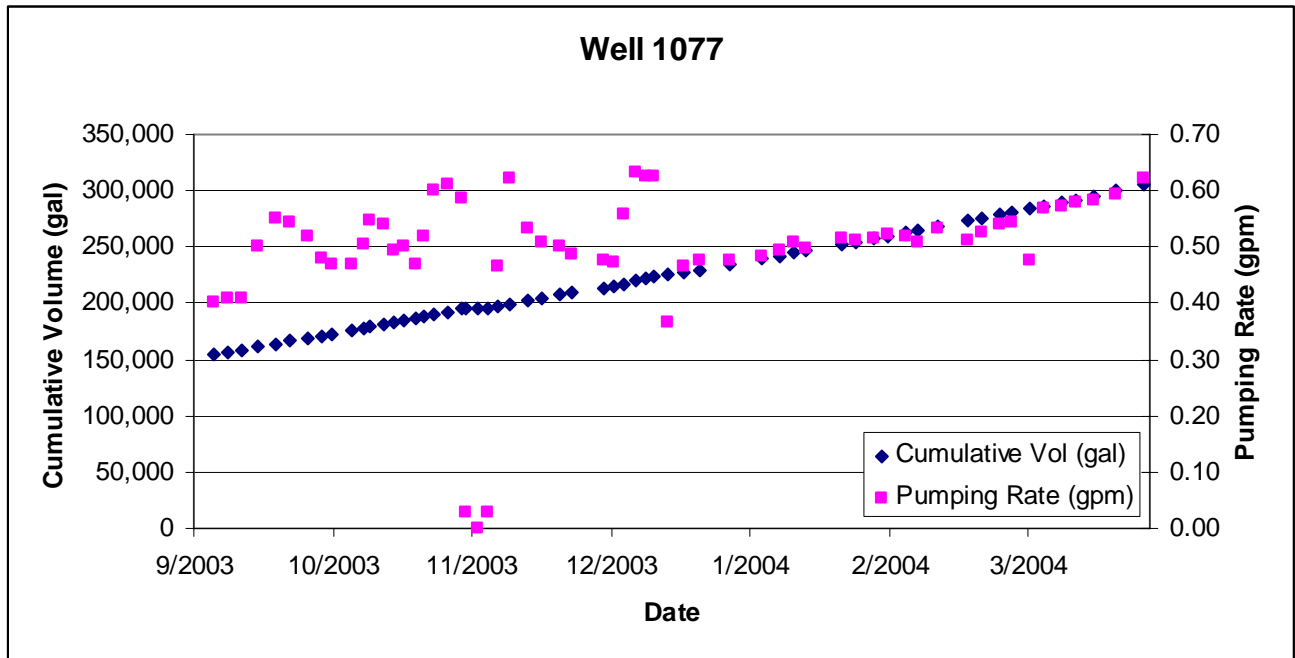


Figure 12. Well 1077 Pumping Rate and Cumulative Ground Water Volume Extracted

3.2 Terrace Remediation System

The terrace remediation system consists of four components: the terrace extraction wells, the terrace drains (Bob Lee and Many Devils Washes), the evaporation pond, and the terrace outfall drainage channel diversion (Figure 1).

Extraction Wells

Three wells (1070, 1071, and 1078) were initially installed for the purposes of ground water extraction on the terrace. In addition, monitor well 0818 was converted to a pumping well. All of the wells, whose total depths range from 40 to 60 ft below ground surface, were located within the terrace east portion of the site. Saturated thickness in the wells ranged from 3 to 7 ft. Ground water extracted from these wells was collected in a pipeline and transported eastward to the evaporation pond.

After 5 months of pumping, and a number of efforts to increase the flow from the initial four extraction wells, additional wells were installed in an attempt to reach a total terrace extraction rate of 10 gpm. Wells 1091, 1092, 1093, and 1094 were installed in July 2003 just north of the west part of the evaporation pond (Figure 1).

Terrace Drain System

The terrace extraction system is also designed to collect seepage along Bob Lee and Many Devils Washes using subsurface interceptor drains. These drains, which consist of perforated pipe surrounded by drain rock and are lined with impermeable geomembrane and geotextile filter fabric, are offset from the centerline of each wash to minimize infiltration of surface water. All water collected by these drains is pumped through a pipeline to the evaporation pond.

Evaporation Pond

The selected method for treating ground water from the interceptor drains and extraction wells is solar evaporation. The contaminated ground water is pumped to a lined evaporation pond in the south part of the radon cover borrow pit area (Figure 1). This pond, with a surface area of approximately 11 acres, has a geosynthetic liner underlain by a compacted soil base.

Terrace Drainage Channel Diversion

During infrequent high-intensity rainfall events, surface water shed from the disposal cell has historically drained northwest to a rock-lined dissipation area, eventually reaching upper Bob Lee Wash. In some instances the water has become ponded in the rock-lined dissipation area, from whence it potentially recharged the aquifer and fed the escarpment seeps.

The outfall drainage channel diversion was installed to better drain surface water from the dissipation area and convey it northwest to the lower part of Bob Lee Wash. It is located such that it will not interfere with the interceptor drain in upper Bob Lee Wash.

A more detailed description of remediation system components are contained in the Baseline Performance Report (DOE 2003a) and GCAP (DOE 2002). The following sections discuss the performance of the extraction wells (3.2.1), terrace drain system (3.2.2), and evaporation pond (3.2.3) between late September 2003 and March 2004. Performance of the outfall drainage channel is omitted because flows in the channel are not being measured.

3.2.1 Extraction Well Performance

The pumping rates and corresponding ground water volumes removed from wells 0818, 1070, 1071, 1078, 1091, 1092, 1093, and 1094 through March 2004 are presented in Figure 13 through Figure 20, respectively. Table 3 lists each well's average pumping rate and total ground water volume removed as of March 2004. The average pumping rates range from 0.03 (well 1094) to 1.38 gpm (well 0818), and the total ground water volume removed from each well during this same time period ranged from 10,819 (well 1094) to 770,697 gallons (well 0818).

Appendix C lists measured pumping rates and corresponding volumes of ground water removed from all eight terrace ground water extraction wells.

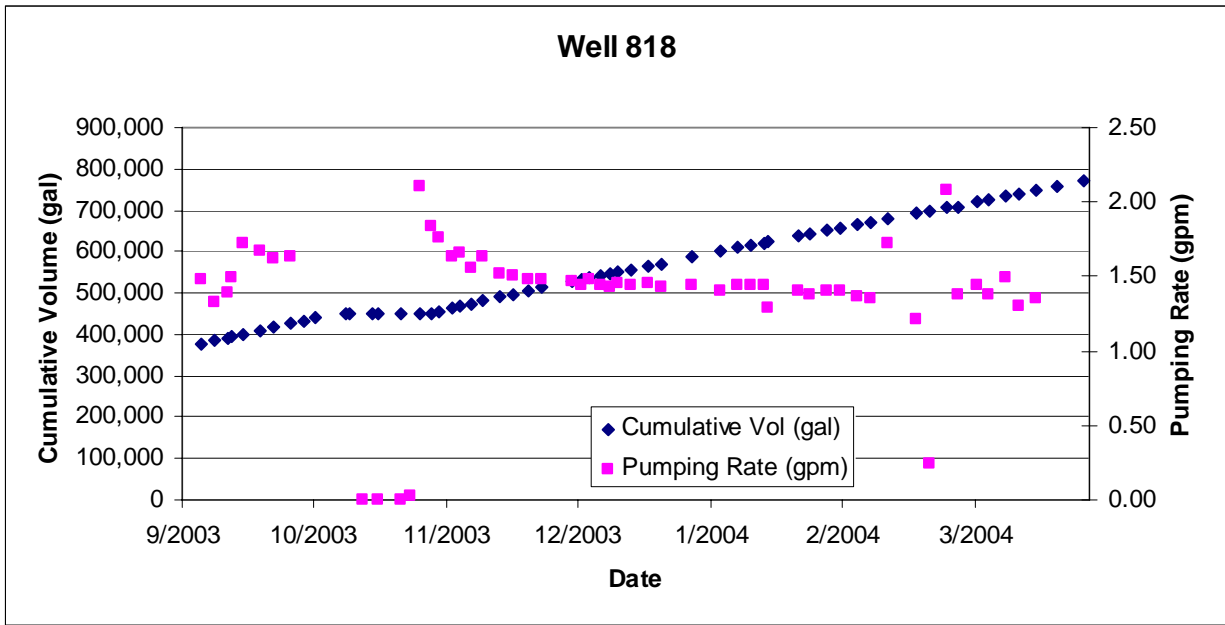


Figure 13. Well 0818 Pumping Rate and Cumulative Ground Water Volume Extracted

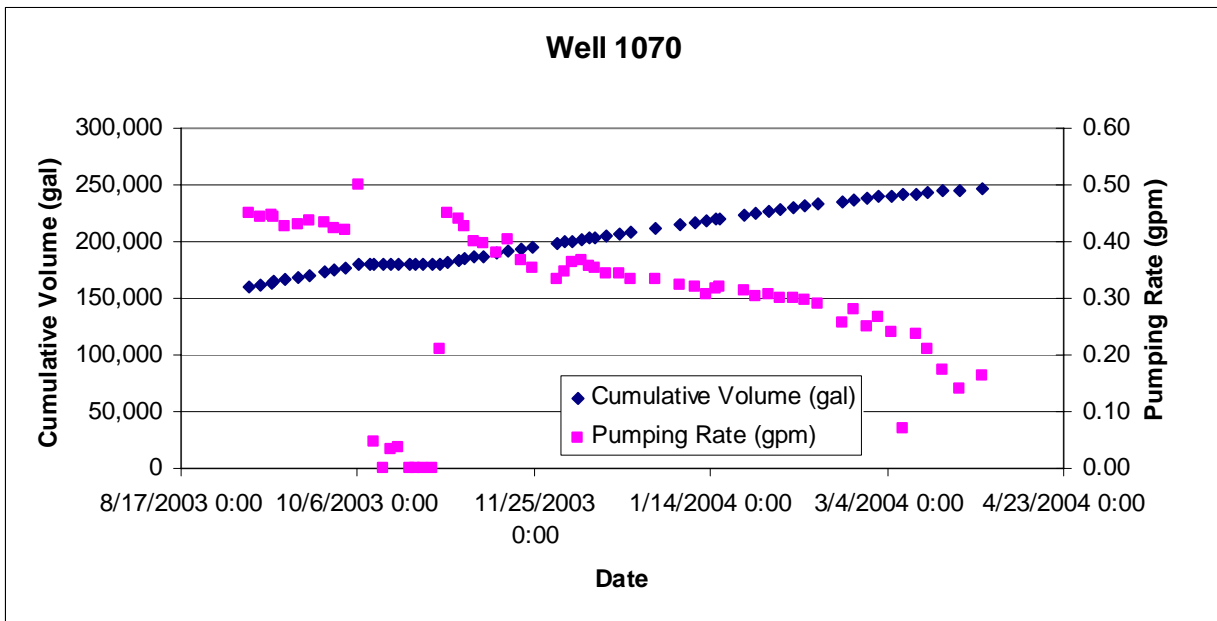


Figure 14. Well 1070 Pumping Rate and Cumulative Ground Water Volume Extracted

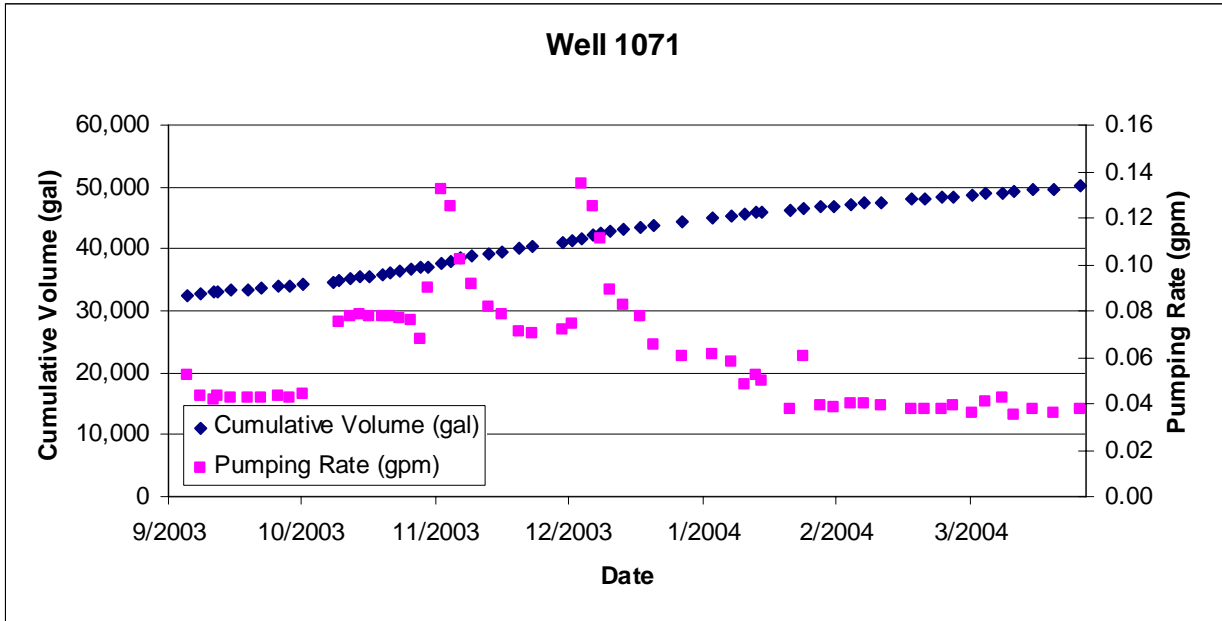


Figure 15. Well 1071 Pumping Rate and Cumulative Ground Water Volume Extracted

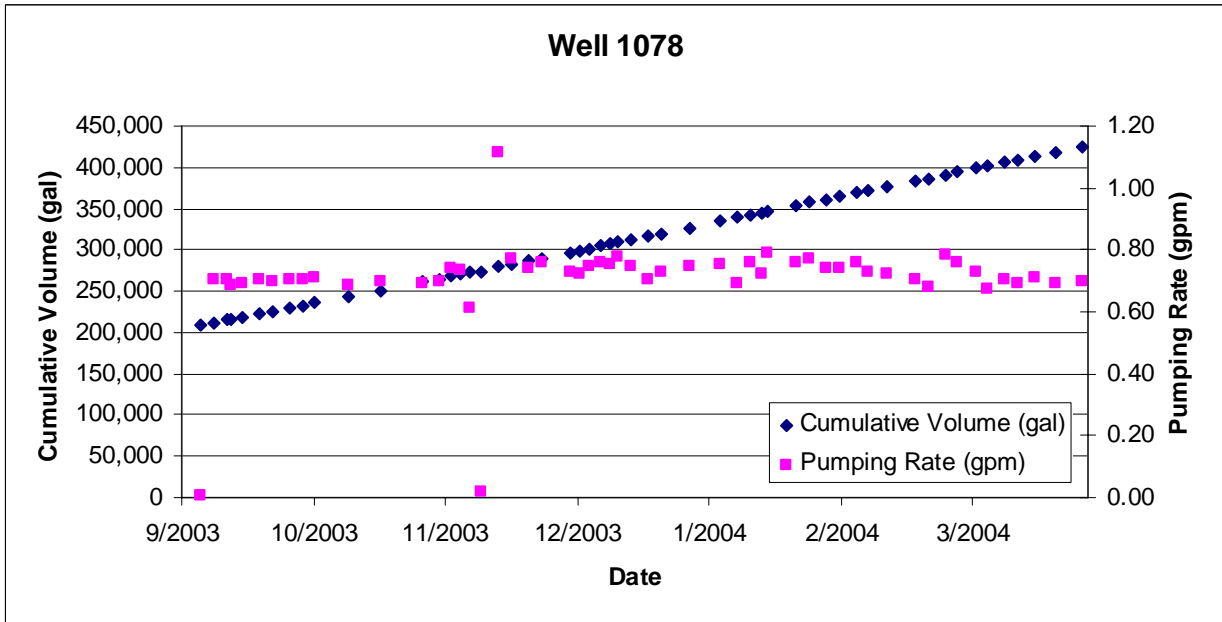


Figure 16. Well 1078 Pumping Rate and Cumulative Ground Water Volume Extracted

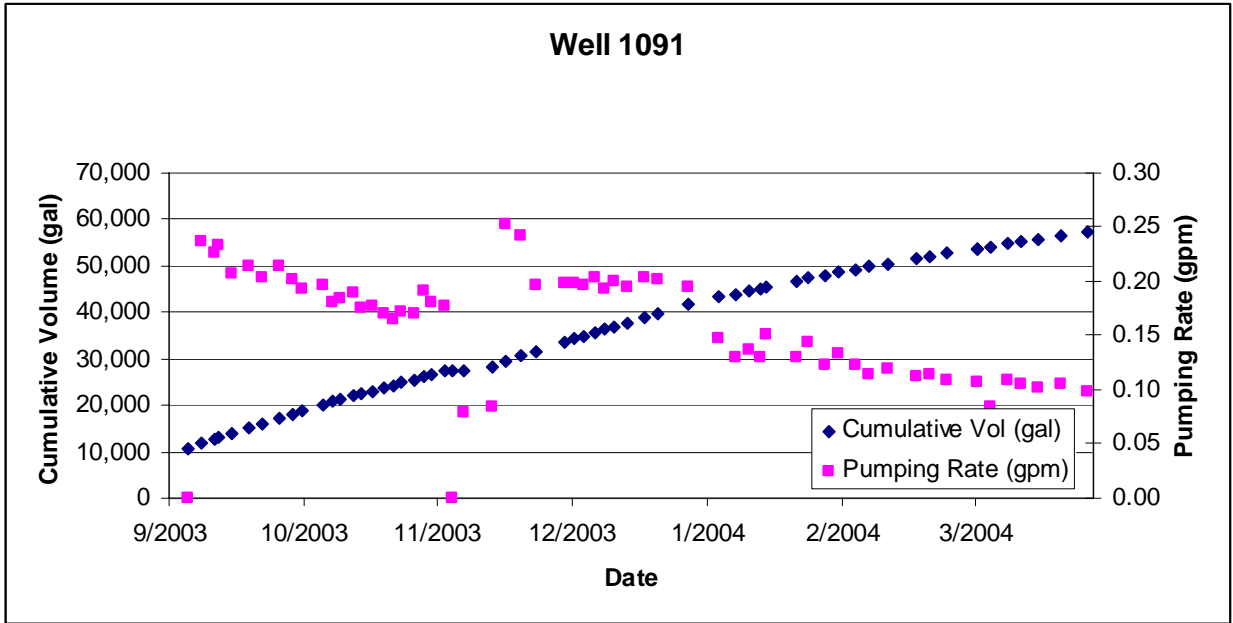


Figure 17. Well 1091 Pumping Rate and Cumulative Ground Water Volume Extracted

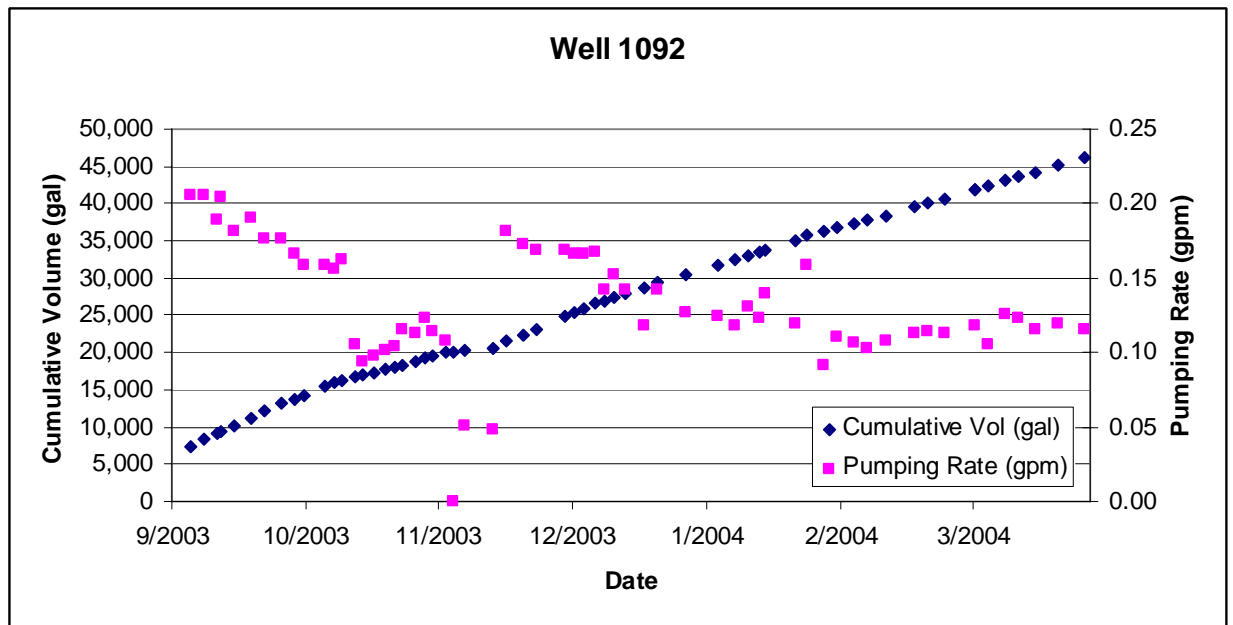


Figure 18. Well 1092 Pumping Rate and Cumulative Ground Water Volume Extracted

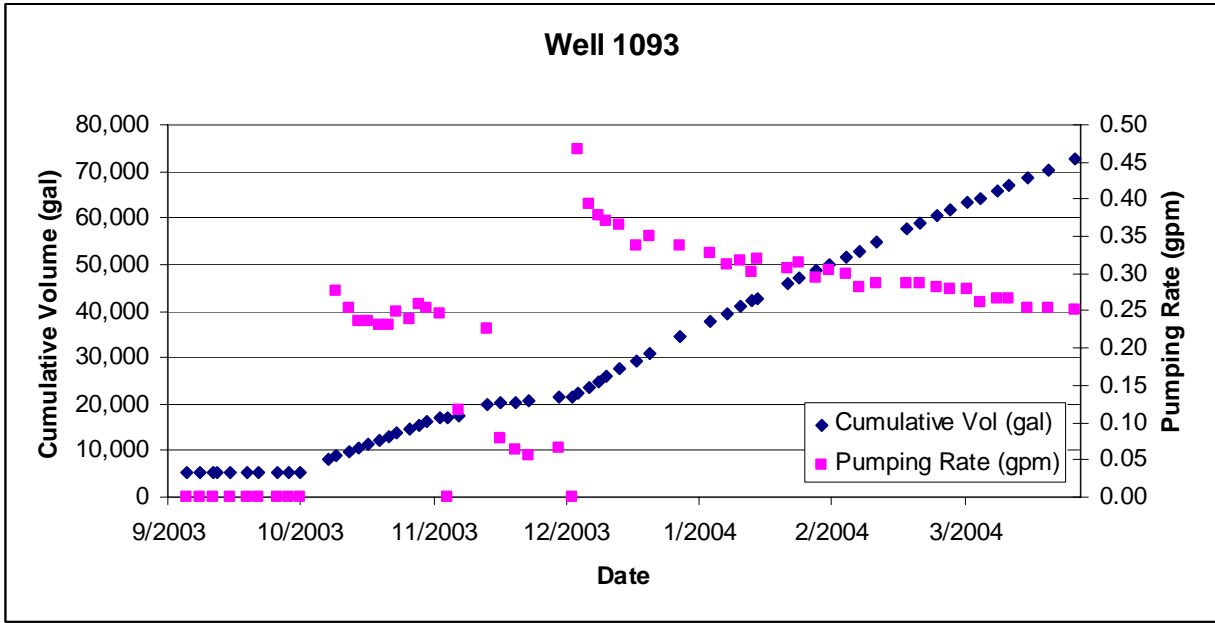


Figure 19. Well 1093 Pumping Rate and Cumulative Ground Water Volume Extracted

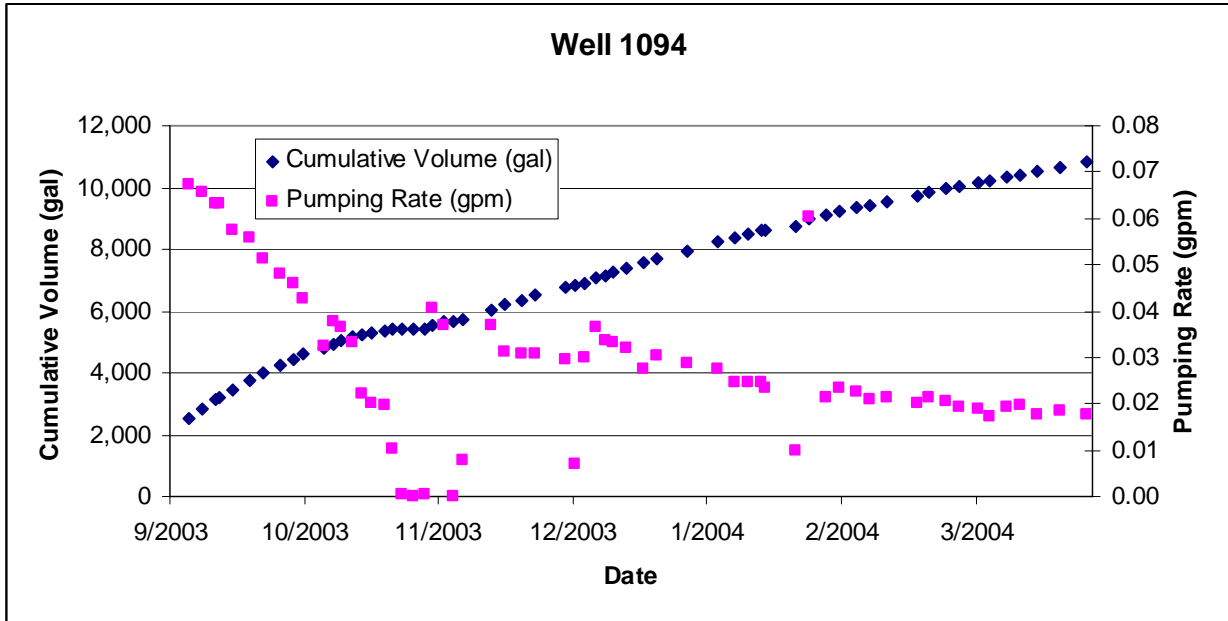


Figure 20. Well 1094 Pumping Rate and Cumulative Ground Water Volume Extracted

Table 3. Terrace Extraction Well Average Pumping Rate and Total Ground Water Volume Removed

Well	Average Pumping Rate, September 2003 through March 2004 (gpm)	Total Ground Water Volume Removed, March 2004 (gallons)
0818	1.38	770,697
1070	0.29	246,641
1071	0.06	50,074
1078	0.70	423,626
1091	0.16	57,467
1092	0.13	46,144
1093	0.22	72,591
1094	0.03	10,819
Total	2.97	1,678,059

3.2.2 Terrace Drain System Performance

Figure 21 presents extraction rates and cumulative flow volumes for the pump installed in the Bob Lee Wash drain. The data clearly indicate a continued uniform decline in drain flow since startup of the system in late February 2003. The flow rate by the end of March 2004 was 3.3 gpm. During the 6-month performance period (September 2003 to March 2004), the average flow rate was 3.58 gpm, with over 2.3 million gallons of water removed by the drain.

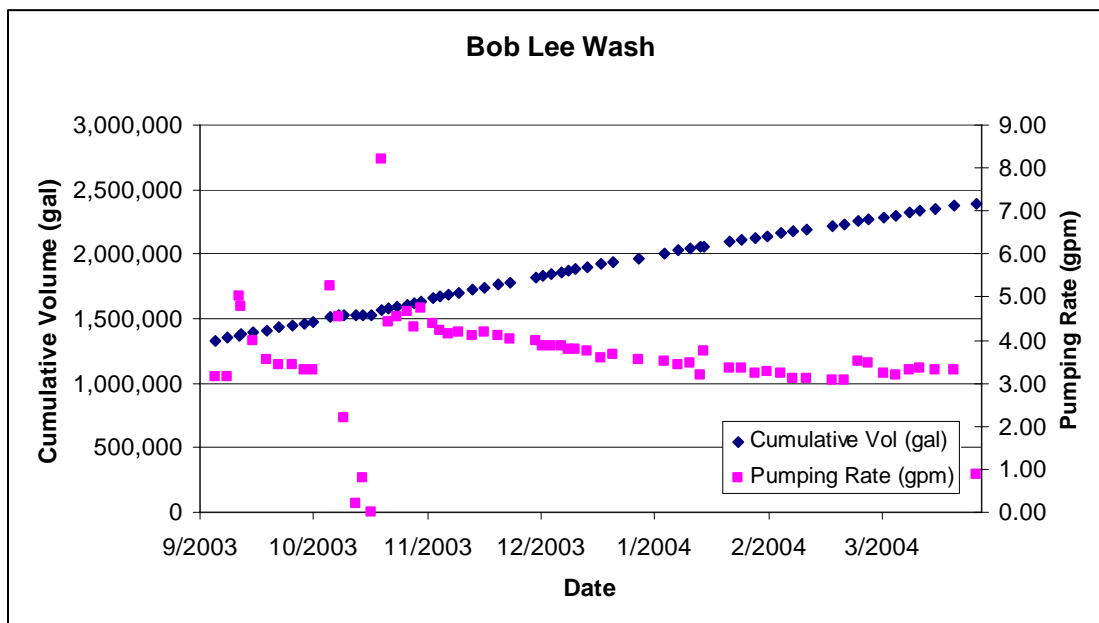


Figure 21. Bob Lee Wash Pumping Rate and Cumulative Ground Water Volume Extracted

As previously discussed, inflow to the drain during its first few months of operation was greater than the ability of the pump installed in the drain to remove the water, as evidence by ponded water present on the surface near the base of the sump containing the pump. By early May 2003, the ponded water was gone, suggesting that the pump discharge was equal to the drain inflow.

During summer months the drain filter at Bob Lee Wash appeared to be affected by scaling that had likely reduced the ability of the ground water to enter the drain. Attempts were made to remove this material and increase the flow rate in July 2003.

The pumping rates and volumes of water removed from the drain installed in Many Devils Wash are presented in Figure 22. Ponded water was present along the wash bottom just east of the buried drain intermittently between September 2003 and March 2004. The flow rate increased in mid-January 2004 from approximately 0.5 to 0.8 gpm and remained at this level through March 2004. By the end of March 2004 the total volume removed by this drain was 207,674 gallons. Appendix C lists the measured pumping rates and corresponding volumes of ground water removed from the Bob Lee Wash and Many Devils Wash drains.

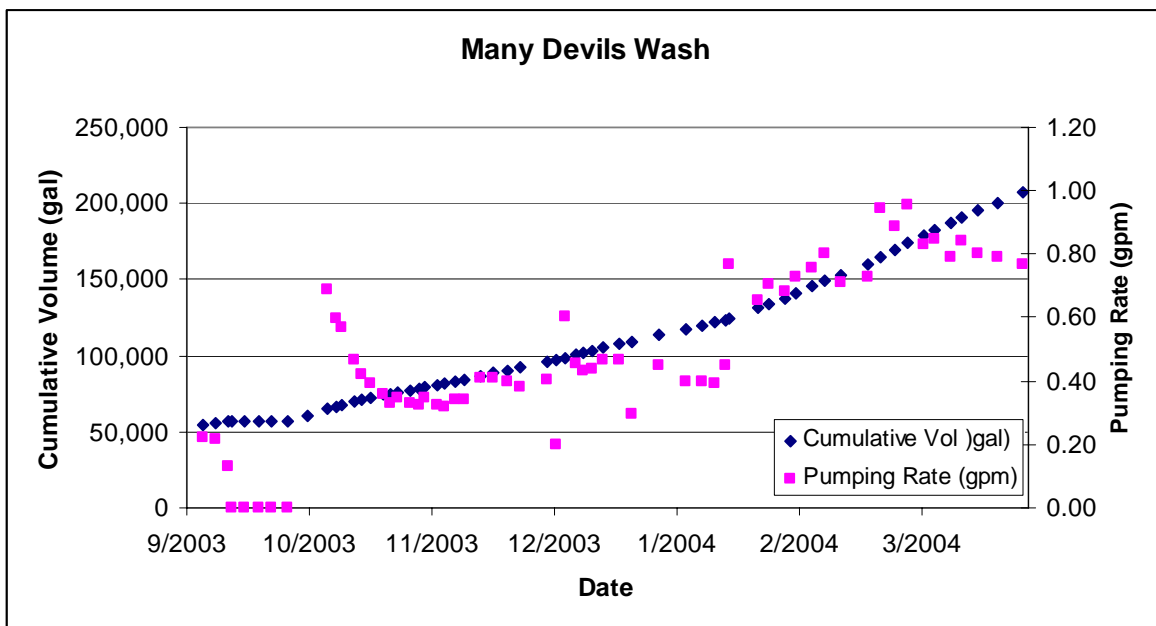


Figure 22. Many Devils Wash Pumping Rate and Cumulative Ground Water Volume Extracted

3.2.3 Evaporation Pond

The bottom of the evaporation pond became completely covered during the 2003/2004 winter, when evaporation rates decreased significantly compared to the summer rates. However, despite the lower evaporation rates, the depth of water in the pond never exceeded more than 0.5 ft in some places of the pond due to limited pumpage from both the floodplain and the terrace. Figure 23 presents the total volume of water transported to the pond, and the relative contributions from the floodplain and terrace systems.

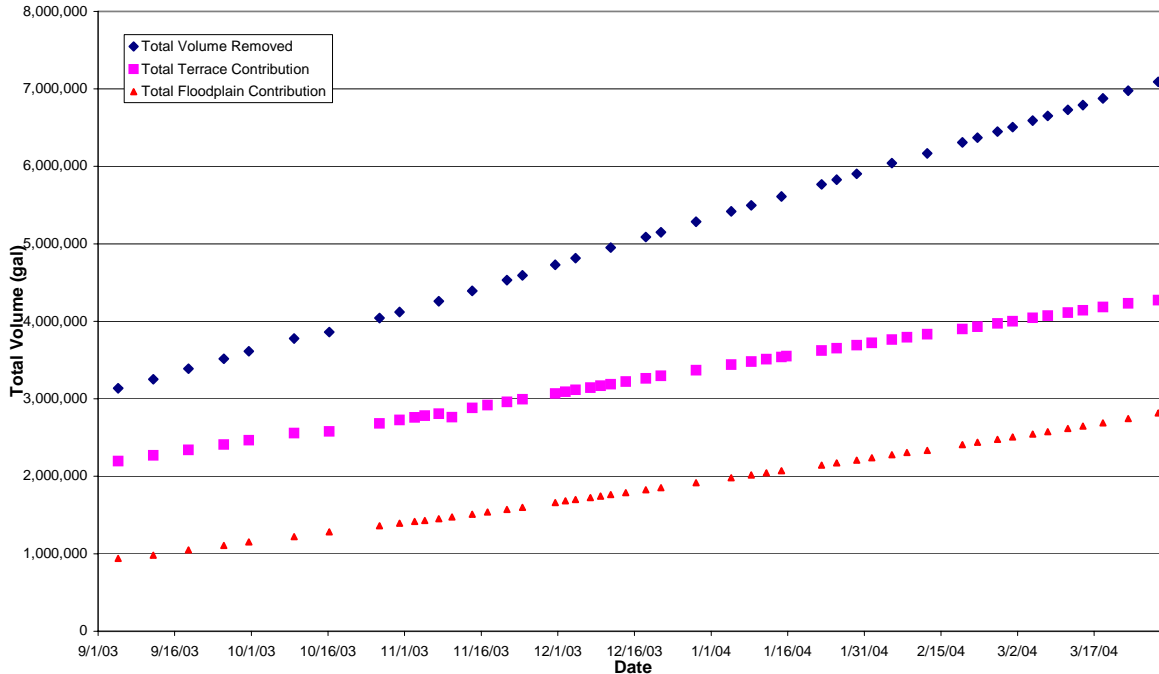


Figure 23. Total Ground Water Volume Transported to the Evaporation Pond

4.0 Performance Summary

No significant changes were expected at the Shiprock site during the initial 12 months of remedial system operation. Findings from the September 2003 through March 2004 performance evaluation of the floodplain remediation system at the site are as follows:

- Three-point analysis of March 2004 water level data in the vicinity of the two floodplain extraction wells indicates that ground water is locally flowing toward the wells in response to pumping.
- No significant reductions in COC concentrations are observed in the floodplain; however, the extraction wells removed some contamination that would have otherwise discharged to the San Juan River.

Findings from the September 2003 through March 2004 performance evaluation of the terrace remediation system are as follows:

- Three-point analysis of the August 2003 water level data indicates the extraction wells are inducing ground water flow towards them.
- The terrace east ground water elevations have been decreasing over the past 5 years, and the March 2004 data indicate the elevations have continued to decline during the previous 6 months. Ground water elevation data collected using data loggers confirm the decline. The terrace west water levels continue to fluctuate in response to irrigation practices in that portion of the site.

- Ground water elevations in the vicinity of the Bob Lee Wash drain have been declining since March 2003, when the ground water extraction system became operational.
- Flow rate data from the pump installed in the Many Devils Wash drain indicate that the average flow rate has more than doubled compared to the average flow rate associated with the first six months of operation. The flow rate increased significantly in mid January 2004.
- The flow rates measured in March 2004 from seeps 0425 and 0426 were below the range measured since October 2002.

5.0 Recommendations

On the basis of the preceding review and the analysis presented in DOE 2004, the following recommendations are provided as means to improve the performance of the Shiprock remediation system and to improve evaluation of the system:

- Increase the volume of ground water extracted from the floodplain to fill the evaporation pond. Well 1077 might be replaced with a new well in a similar manner to which well 1075 was replaced with well 1089.
- Evaluate the effects of well inefficiency on limited pumping rates for wells installed in the floodplain aquifer to remove contaminant mass available to the river; devise methods to reduce well inefficiencies so that better capture of floodplain aquifer contaminants is achieved.
- Assess the potential for ground water flow and contaminant transport in Mancos Shale, both on the terrace and beneath the floodplain, to be affected by preferred flow paths associated with fractures, differential weathering, etc. Develop methods to determine effectiveness of improving contaminant recovery associated with such paths.
- Apply techniques to better understand the migration of contaminated Mancos Shale ground water to the floodplain aquifer, particularly along the escarpment separating the terrace from the floodplain (e.g., at seeps 0425 and 0426). Use associated findings to improve interception of floodplain contaminants via extraction wells, drain trenches, etc.
- Analyze pumping data from wells in alluvium in the southern part of the terrace ground water system to identify possible barrier boundary effects; if possible, revise ground water volume estimates for this area based on the pumping data, and use accordingly for performance evaluation in the terrace ground water system.
- Because ground water extraction rates have been less than anticipated, consider the installation of two to four additional extraction wells in the south part of the terrace east, in an arc between the highest-producing existing extraction wells 0818 and 1078. This spread, or optimization, of extraction wells should result in an increase of the volume of ground water extracted from the south part of terrace east.

6.0 References

Laase, A.D., J.E. Wilson, and D.W. Green, 2002. "Evaluation of Natural Flushing Using Three-Point and Partitioning Theory Analysis," in *Proceedings for the Third International Conference on Remediation of Chlorinated and Recalcitrant Compounds*, May.

U.S. Department of Energy (DOE), 2000. *Final Site Observational Work Plan for the Shiprock, New Mexico, UMTRA Project Site*, Rev. 2, GJO-2001-169-TAR, MAC-GWSHP 1.1, U.S. Department of Energy Grand Junction Office, Grand Junction, Colorado, November.

———, 2002. *Final Ground Water Compliance Action Plan for Remediation at the Shiprock, New Mexico, UMTRA Project Site*, GJO-2001-297-TAR, MAC-GWSHP 1.9, U.S. Department of Energy Grand Junction Office, Grand Junction, Colorado, July.

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———, 2003b. *Semiannual Performance Report February 2003 through August 2003 for the Shiprock, New Mexico, UMTRA Project Site*, GJO-2003-490-TAC, U.S. Department of Energy Grand Junction Office, Grand Junction, Colorado, September.

———, 2004. *Refinement of Conceptual Model and Recommendations for Improving Remediation Efficiency at the Shiprock, New Mexico, Site*, GJO-2004-579-TAC, U.S. Department of Energy Grand Junction Office, Grand Junction, Colorado, March.

U.S. Environmental Protection Agency (EPA), 1999. *Health Effects from Exposure to High Levels of Sulfate in Drinking Water Study*, EPA 815-R-99-001, Office of Water, January.

Appendix A

Three-Point Analyses of Floodplain and Terrace Ground Water Elevation Data

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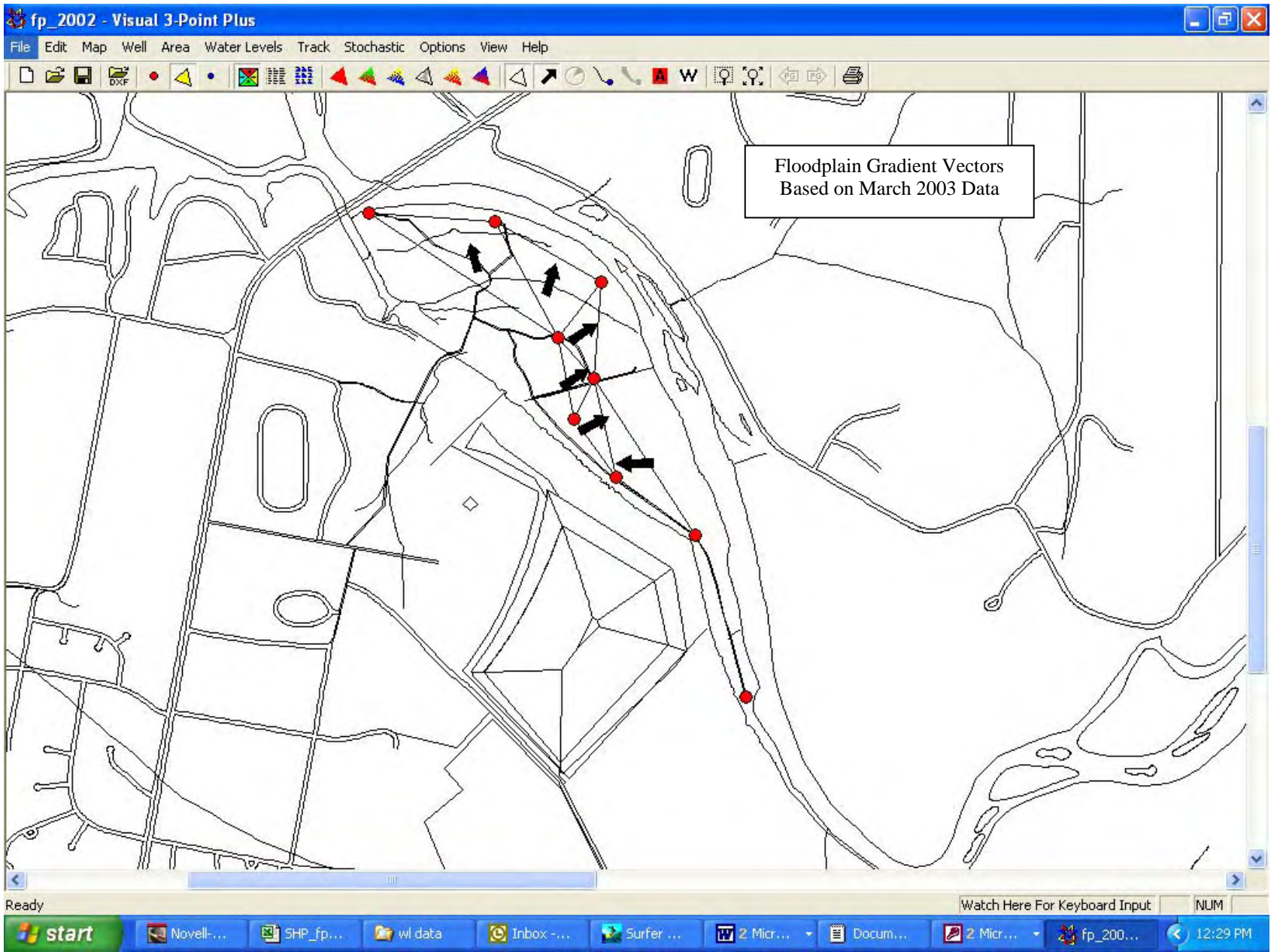


Figure A-1

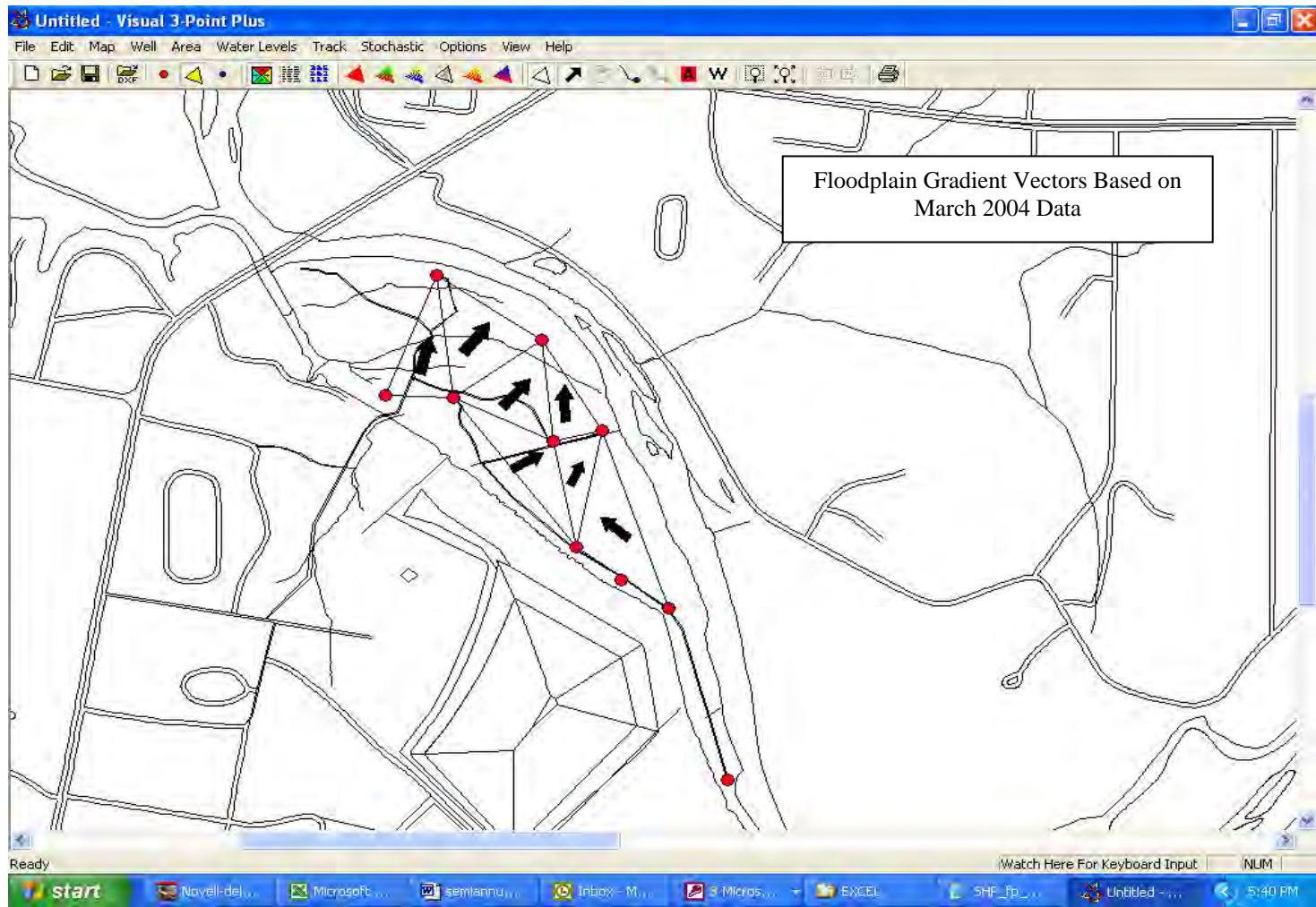


Figure A-2

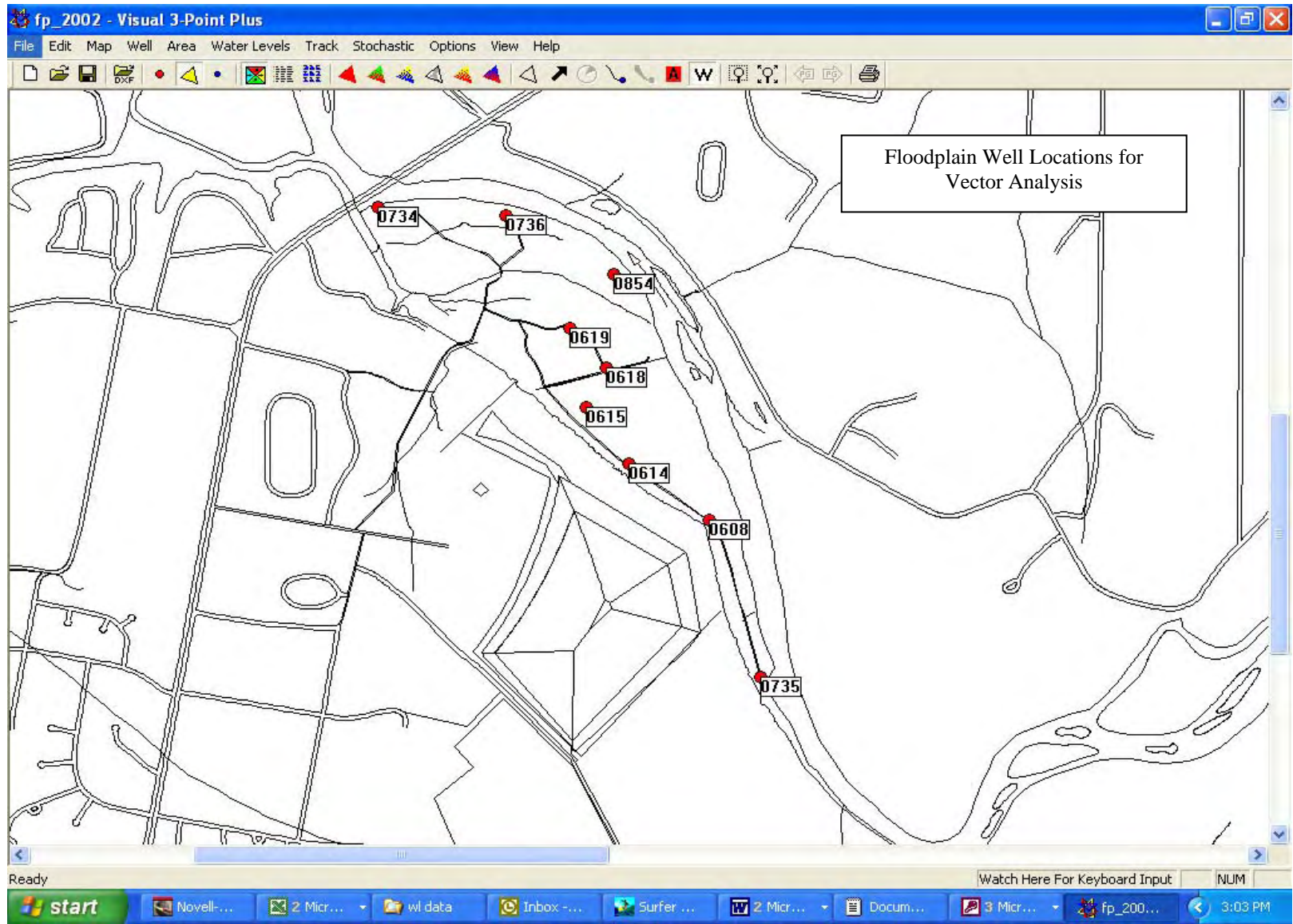


Figure A-3

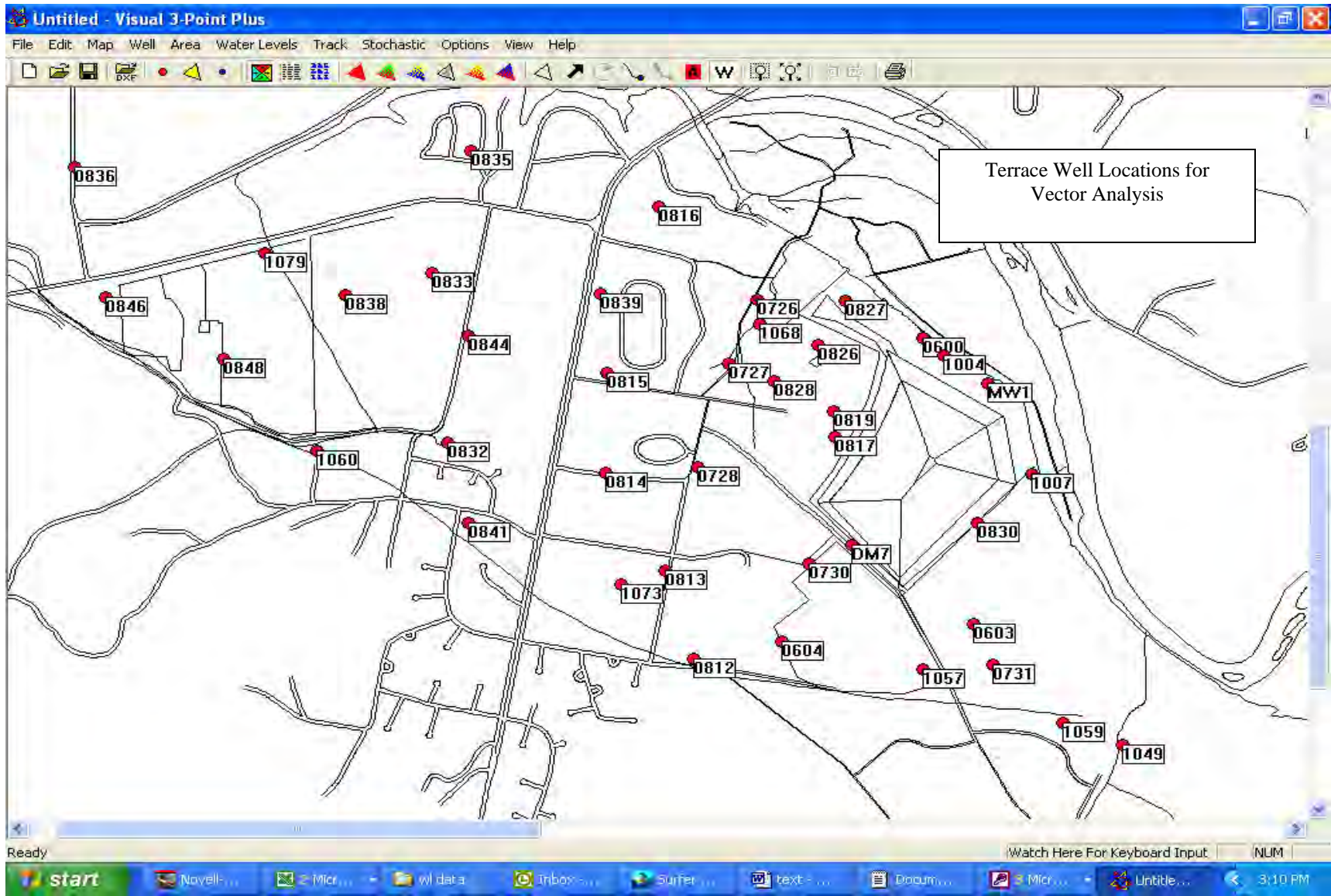


Figure A-4

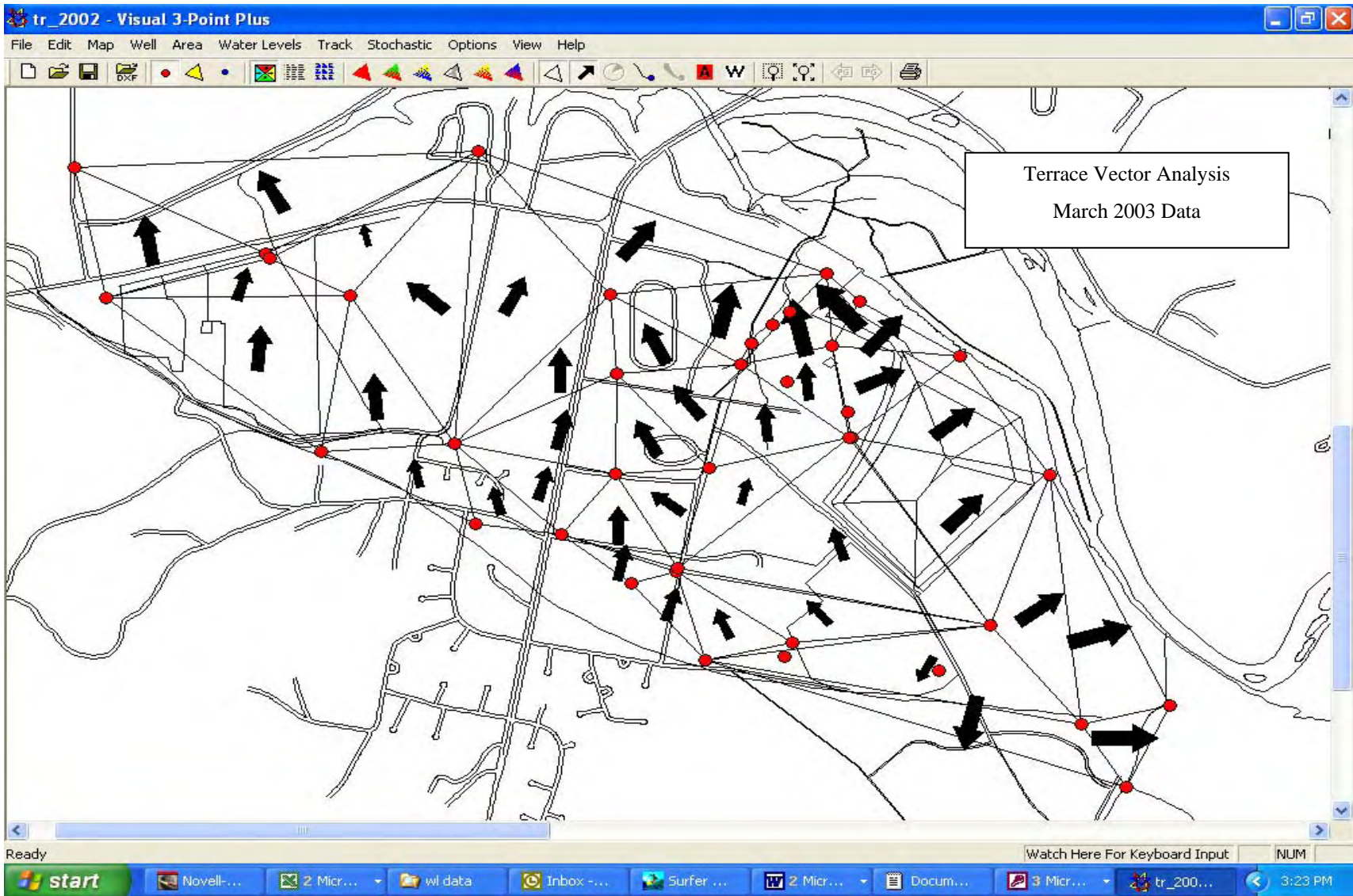


Figure A-5

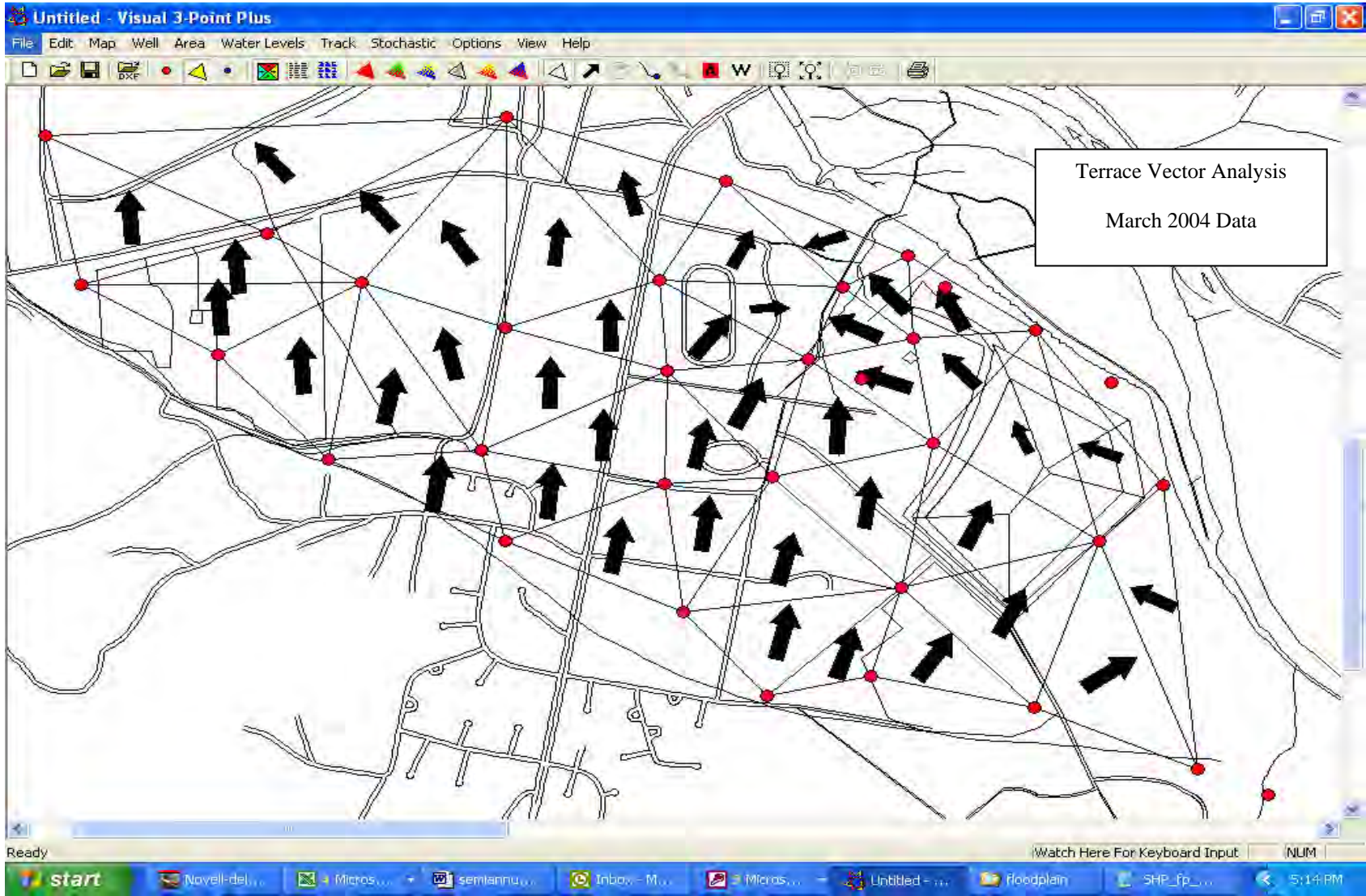


Figure A-6

Appendix B

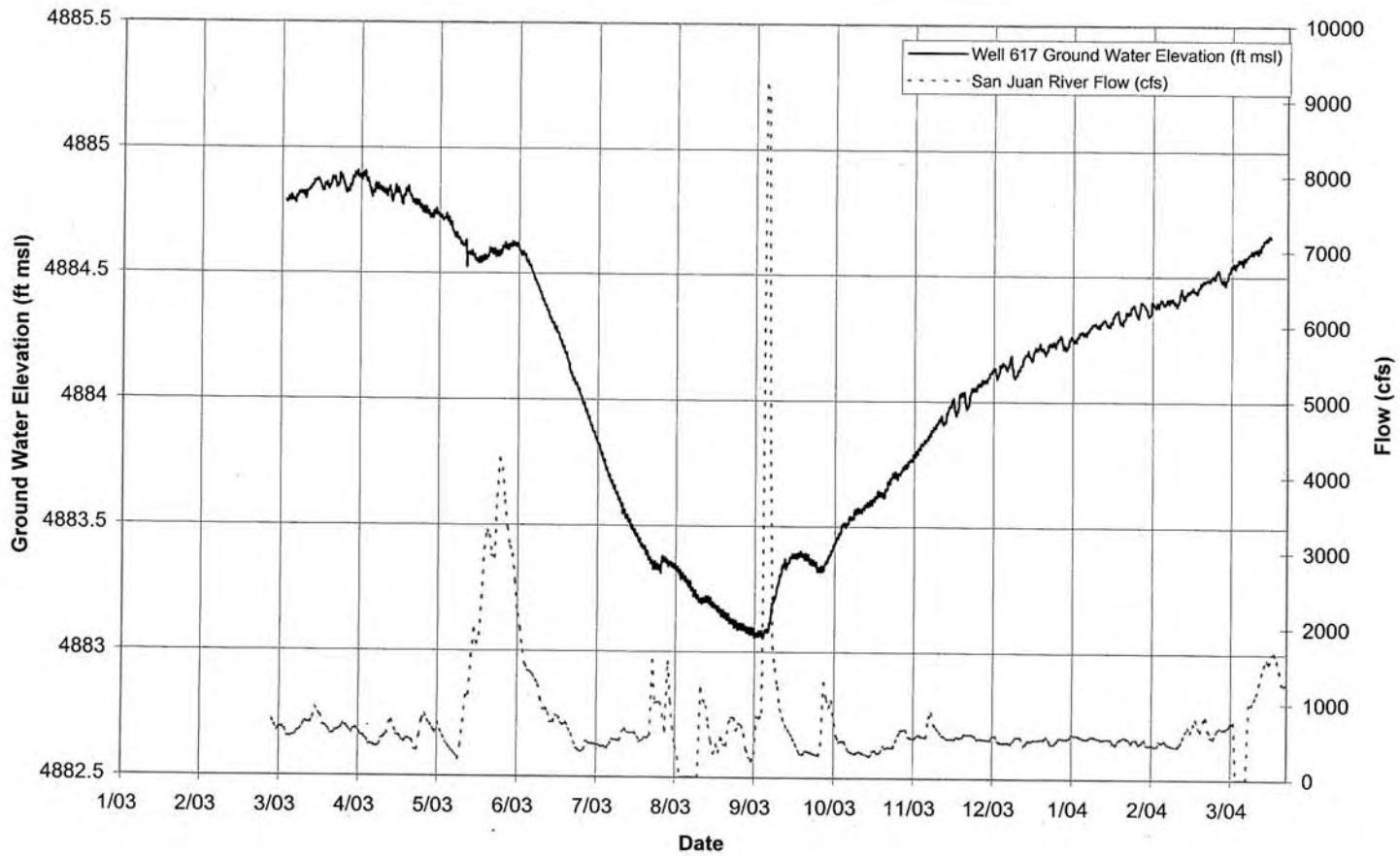
Shiprock Data Logger Ground Water Elevation Data

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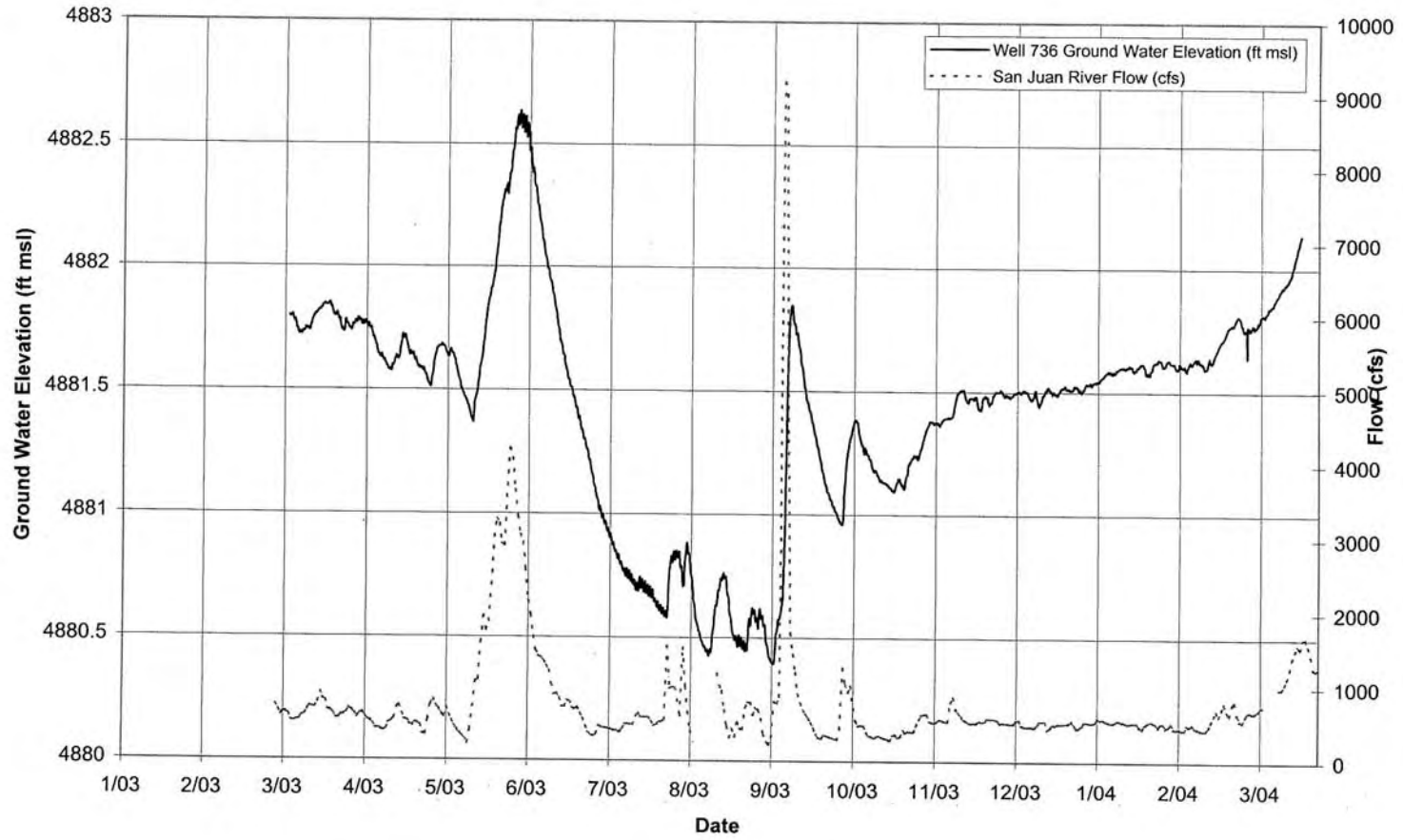
**Floodplain Ground Water Elevation Data
(January 2003 through March 2004)**

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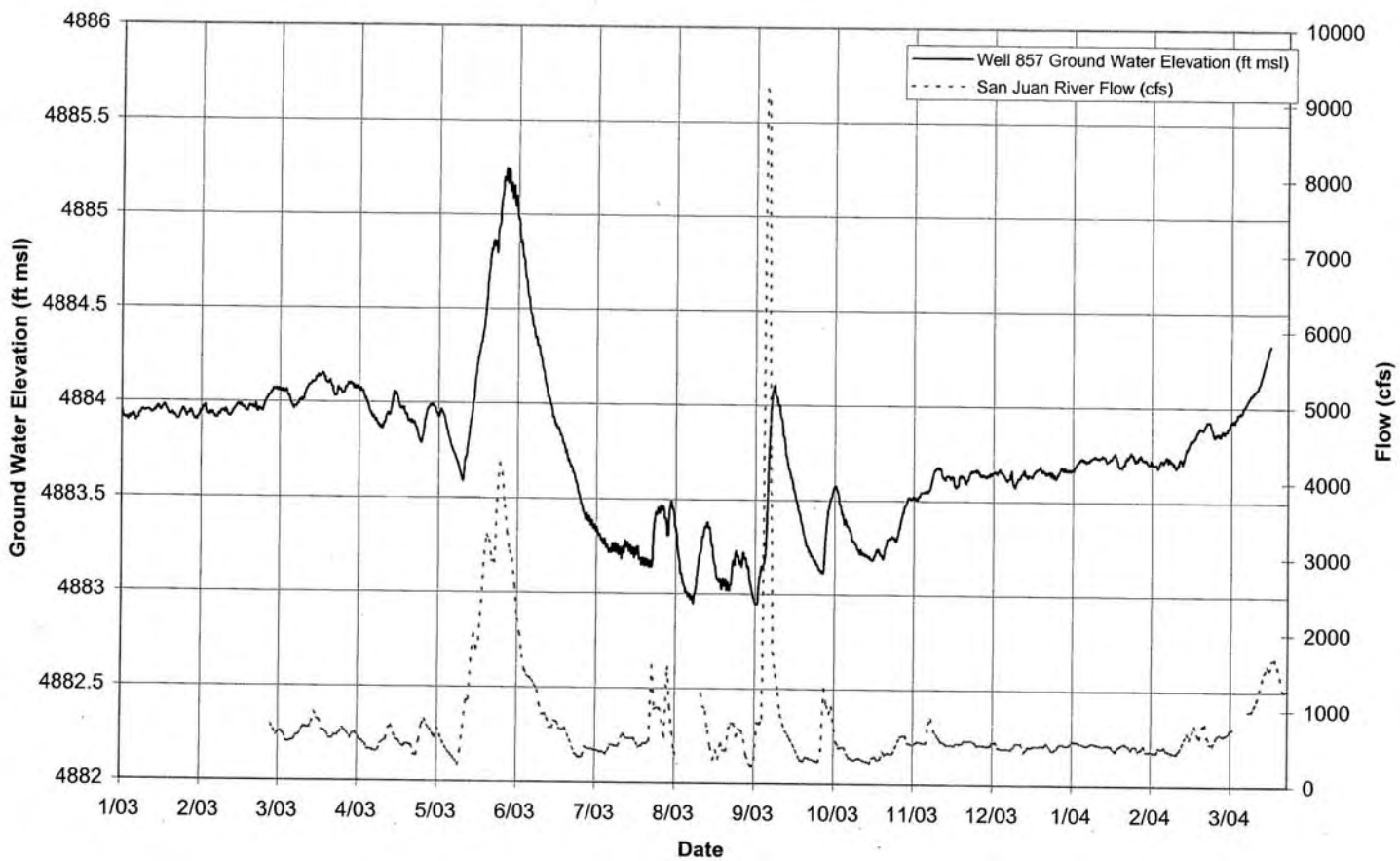
Well 0617 - Floodplain



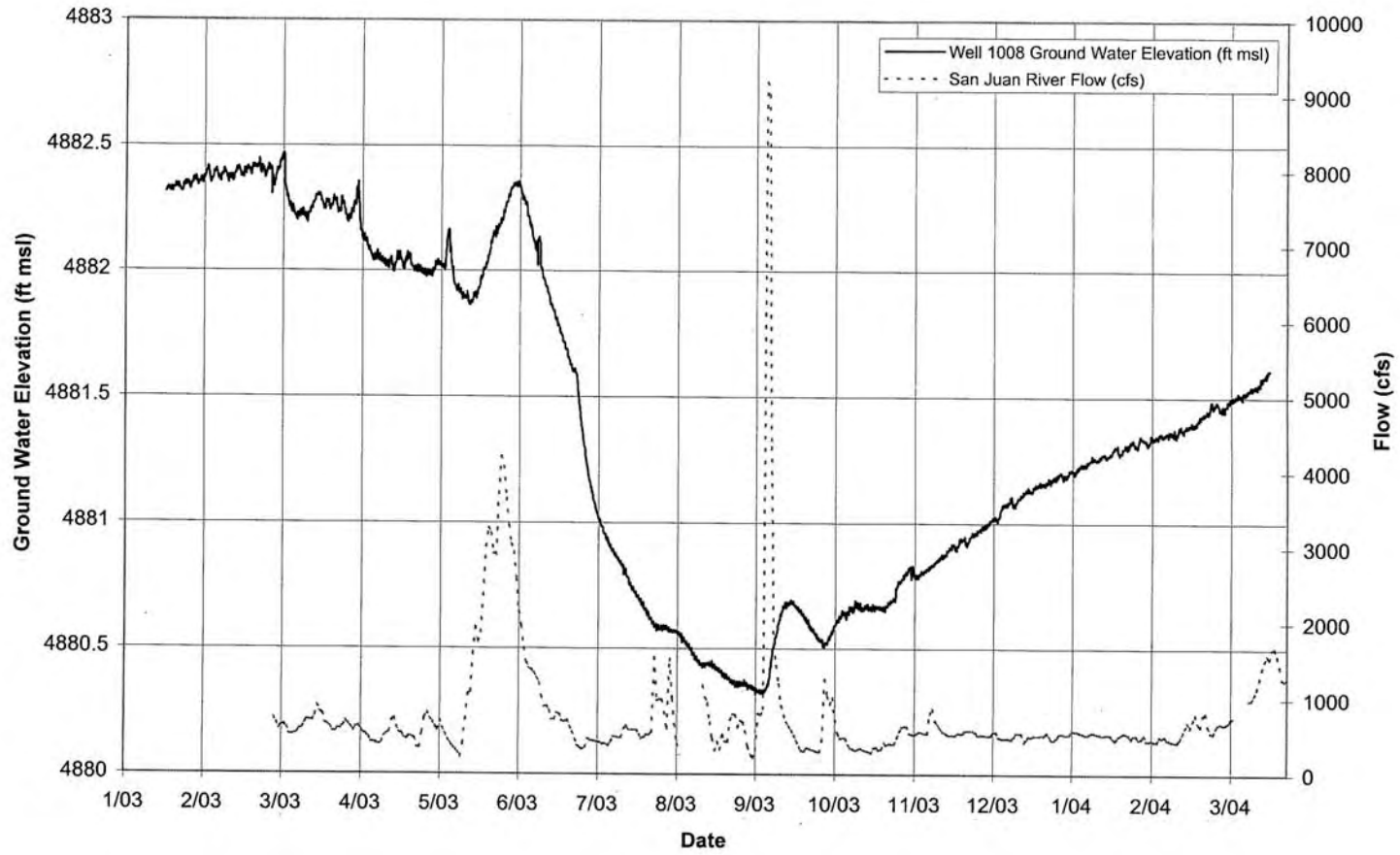
Well 0736 - Floodplain



Well 0857 - Floodplain



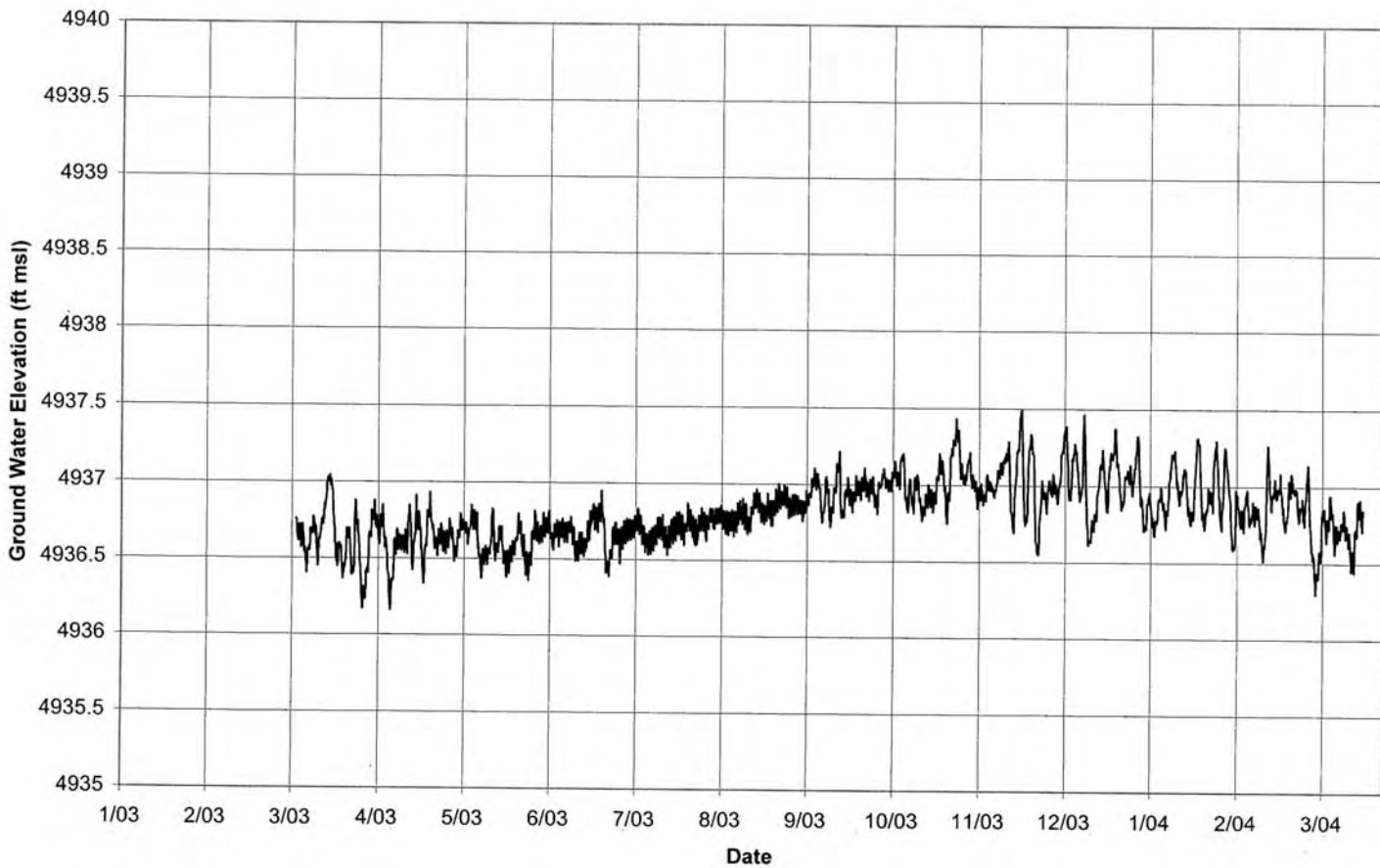
Well 1008 - Floodplain



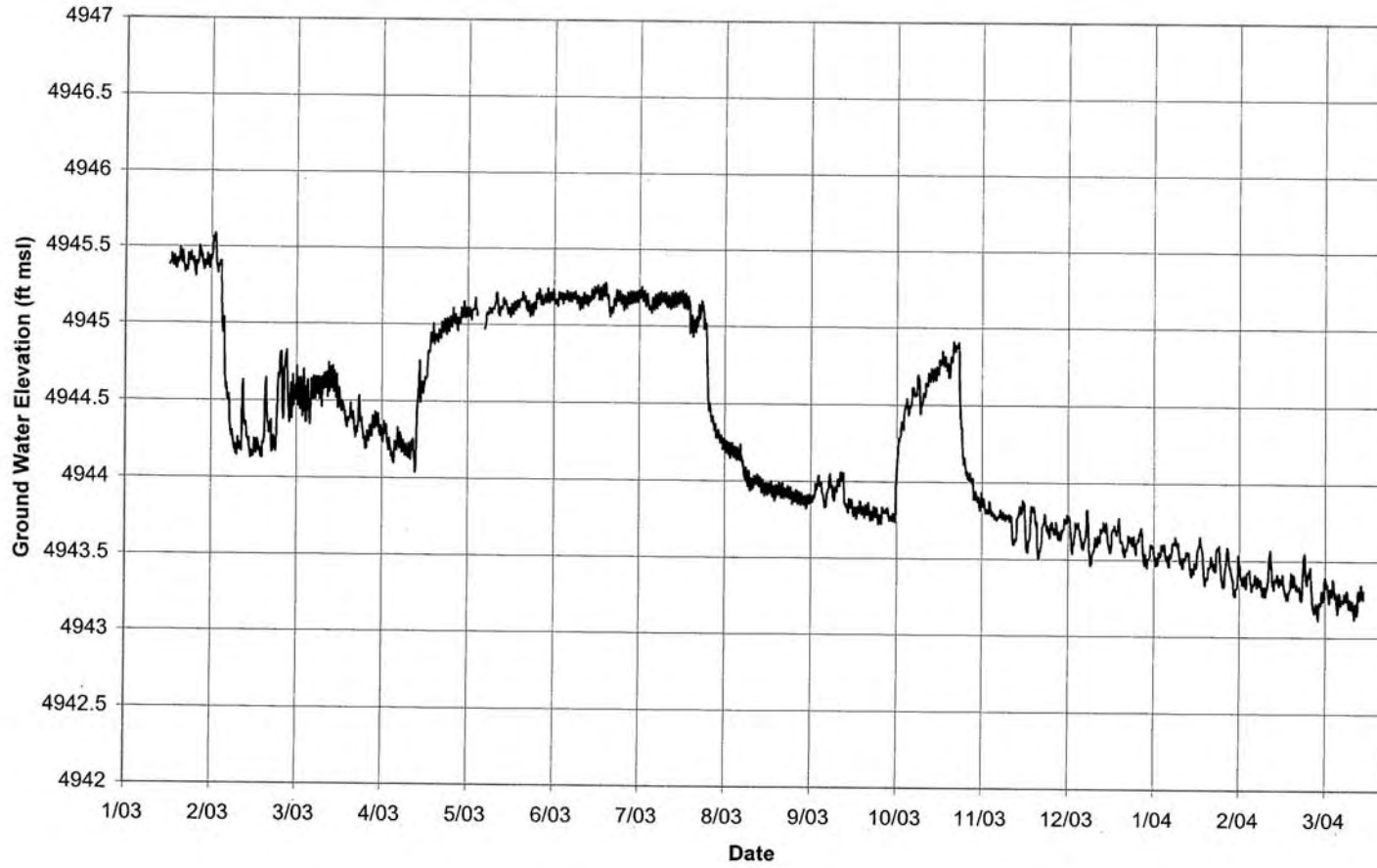
**Terrace East Ground Water Elevation Data
(January 2003 through March 2004)**

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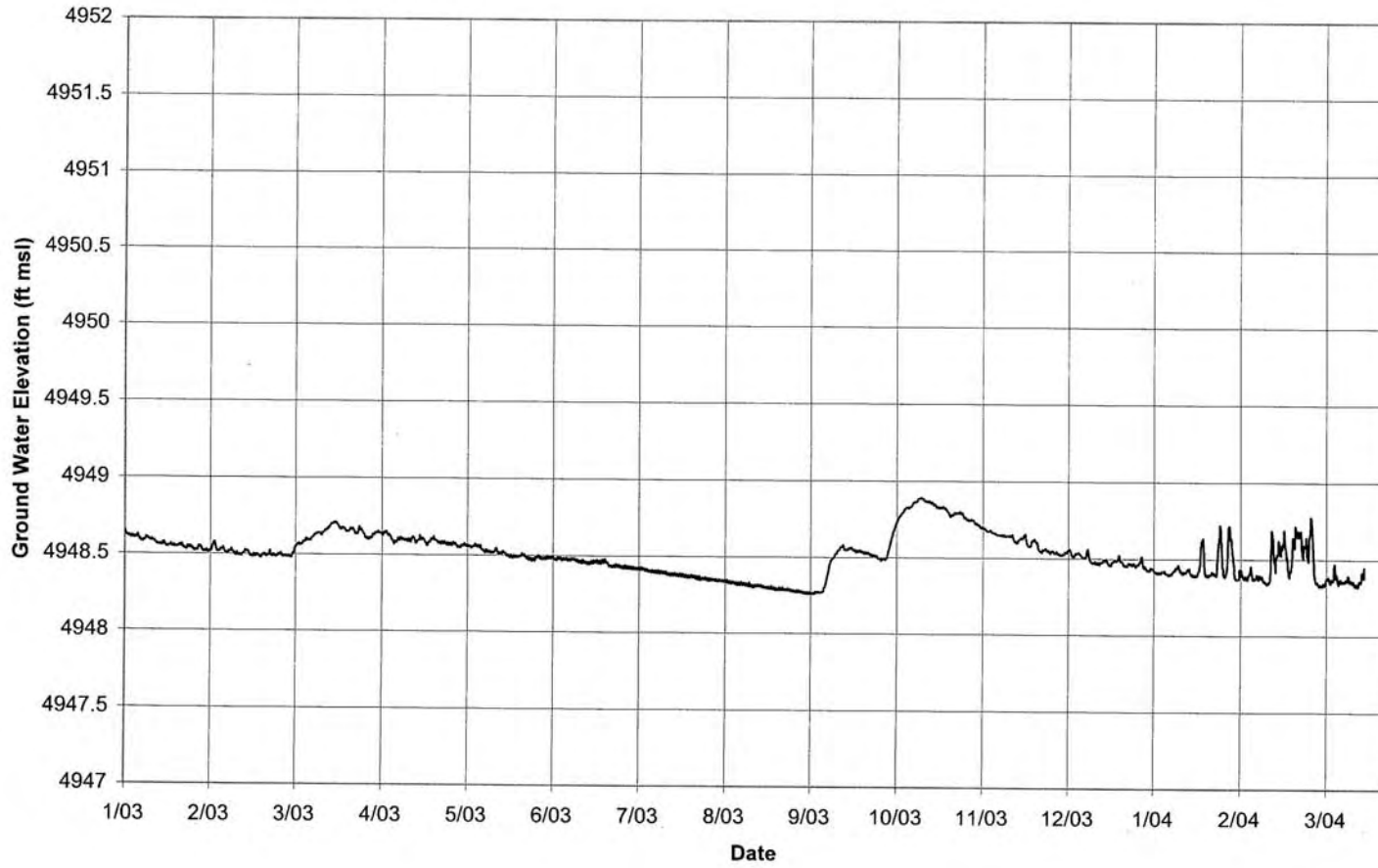
Well 0602 - Terrace East (NECA Yard, NW of Disposal Cell)



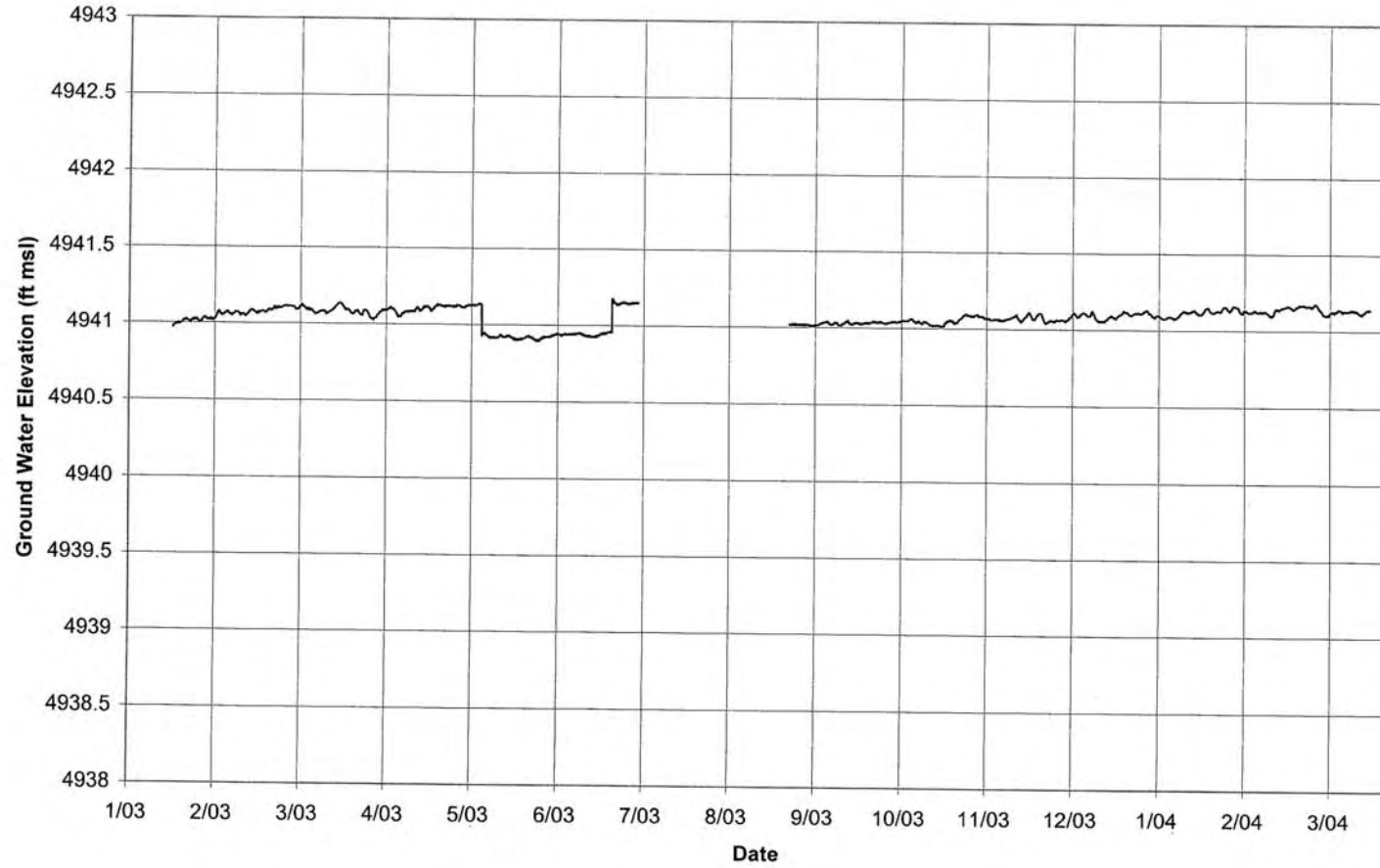
Well 0604 - Terrace East (Off Extraction Well 0818)



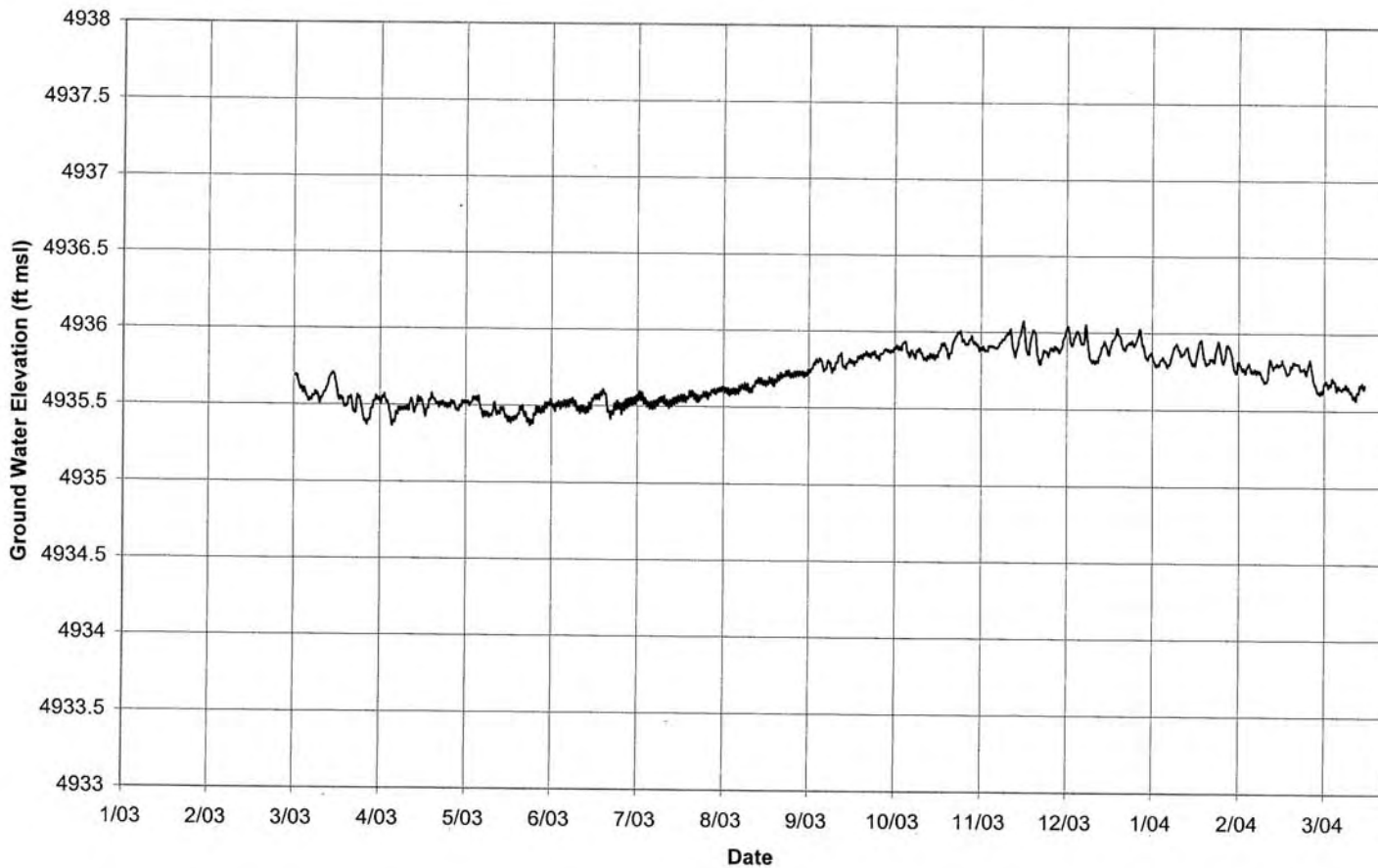
Well 0731 - Terrace East (East of the Evaporation Pond)



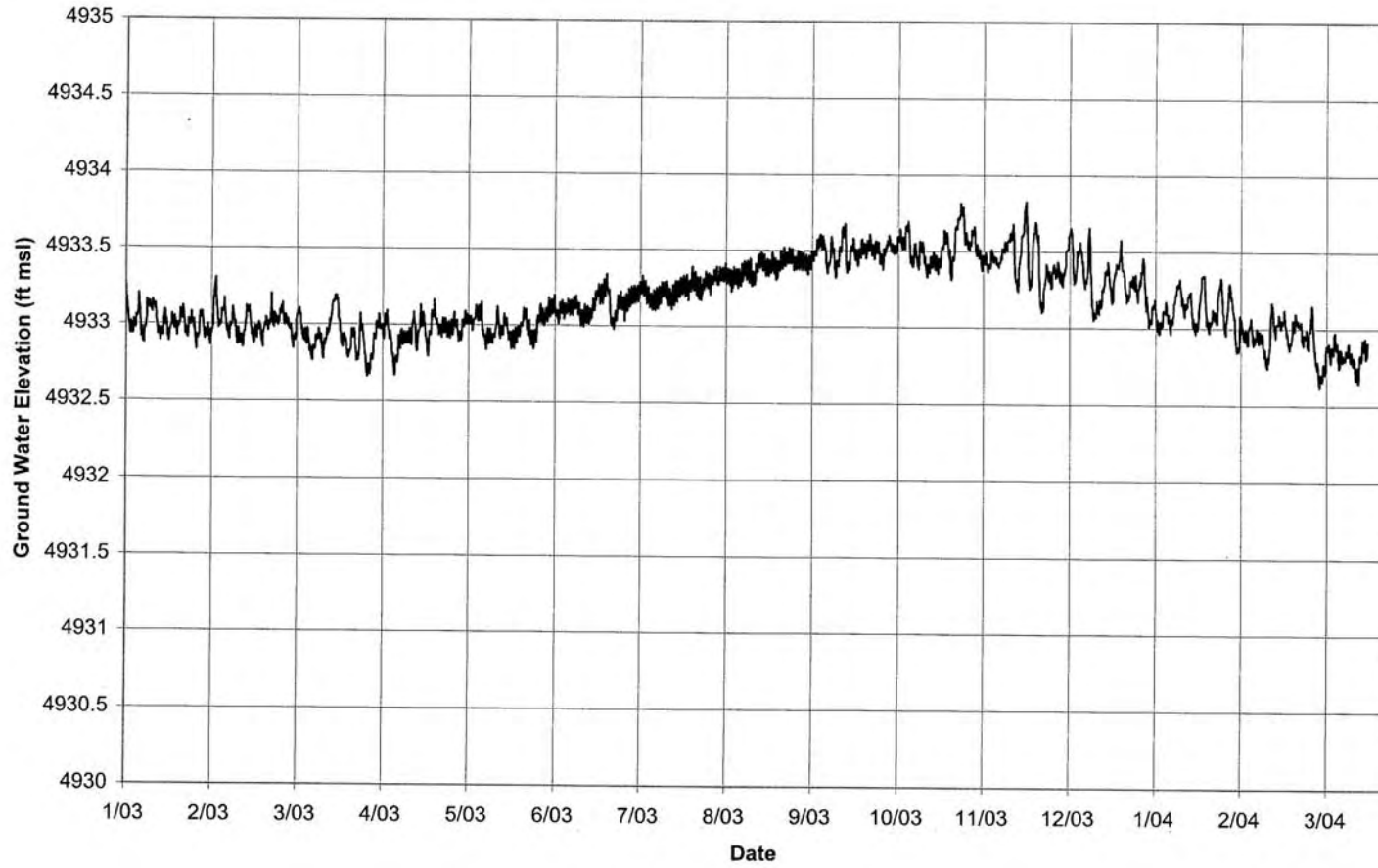
Well 0813 - Terrace East (Southern Area)



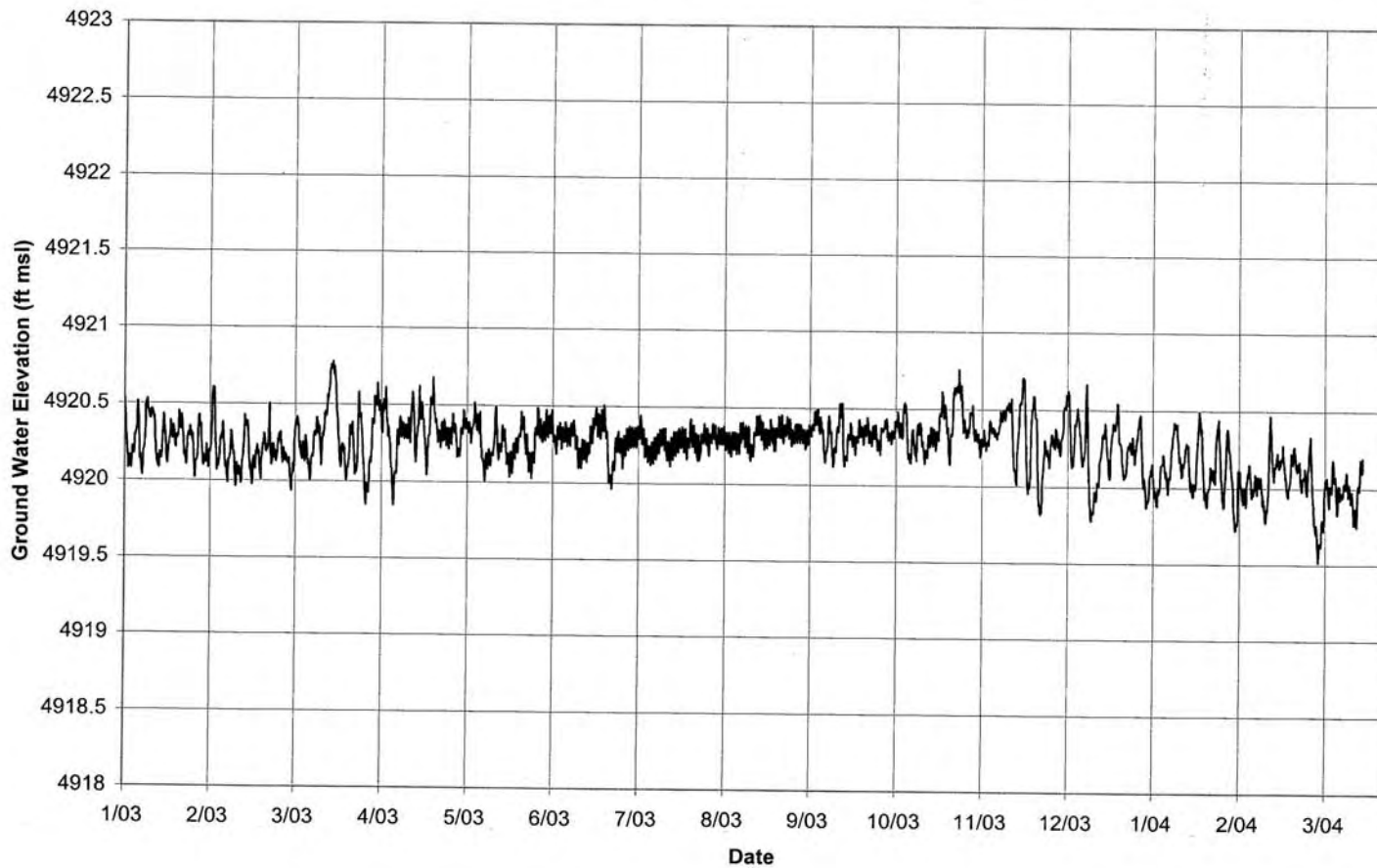
Well 0819 - Terrace East (NECA Yard, NW of Disposal Cell)



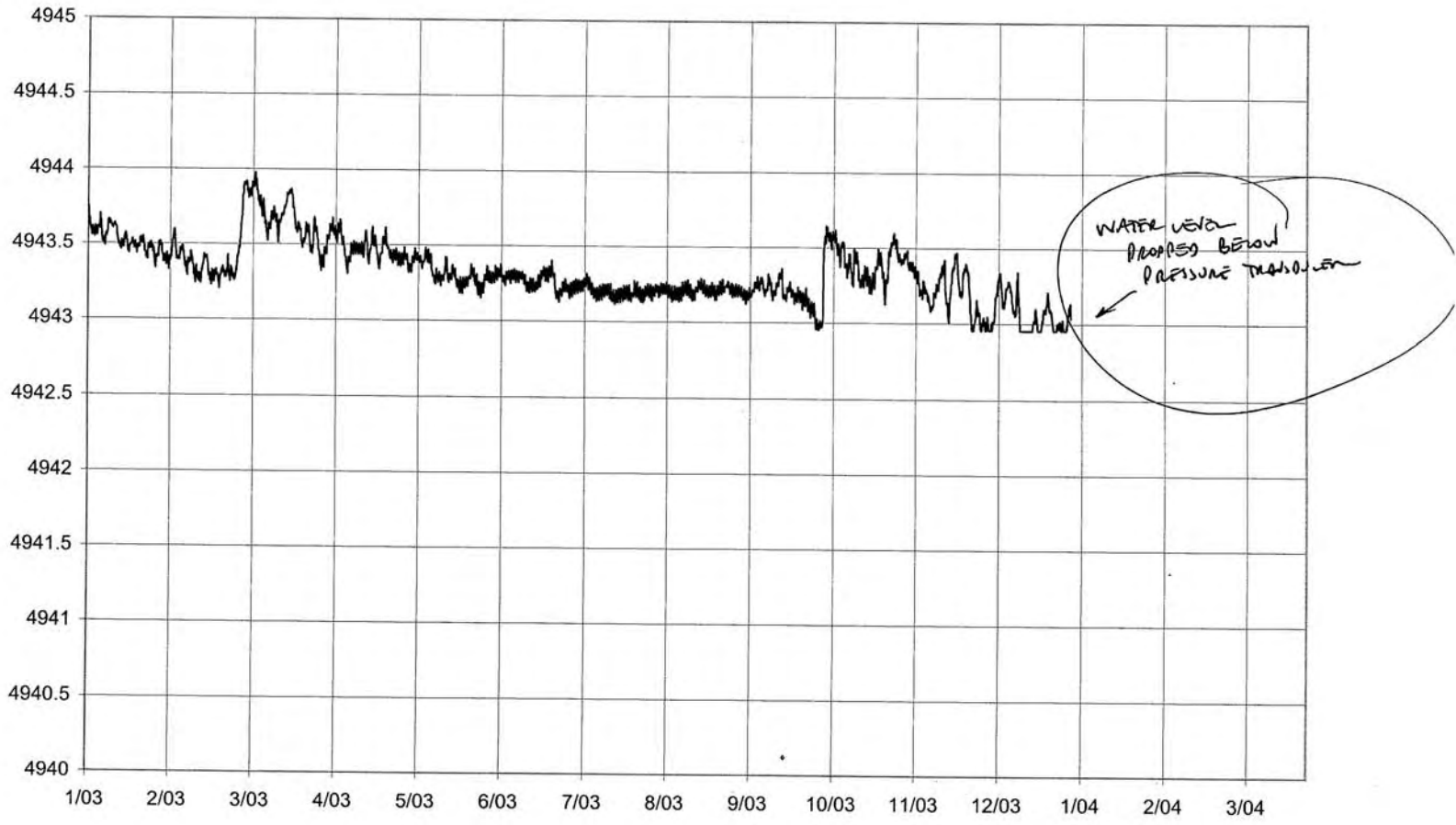
Well 0826 - Terrace East (NECA Yard)



Well 0827 - Terrace East (Off NW Corner of Disposal Cell)



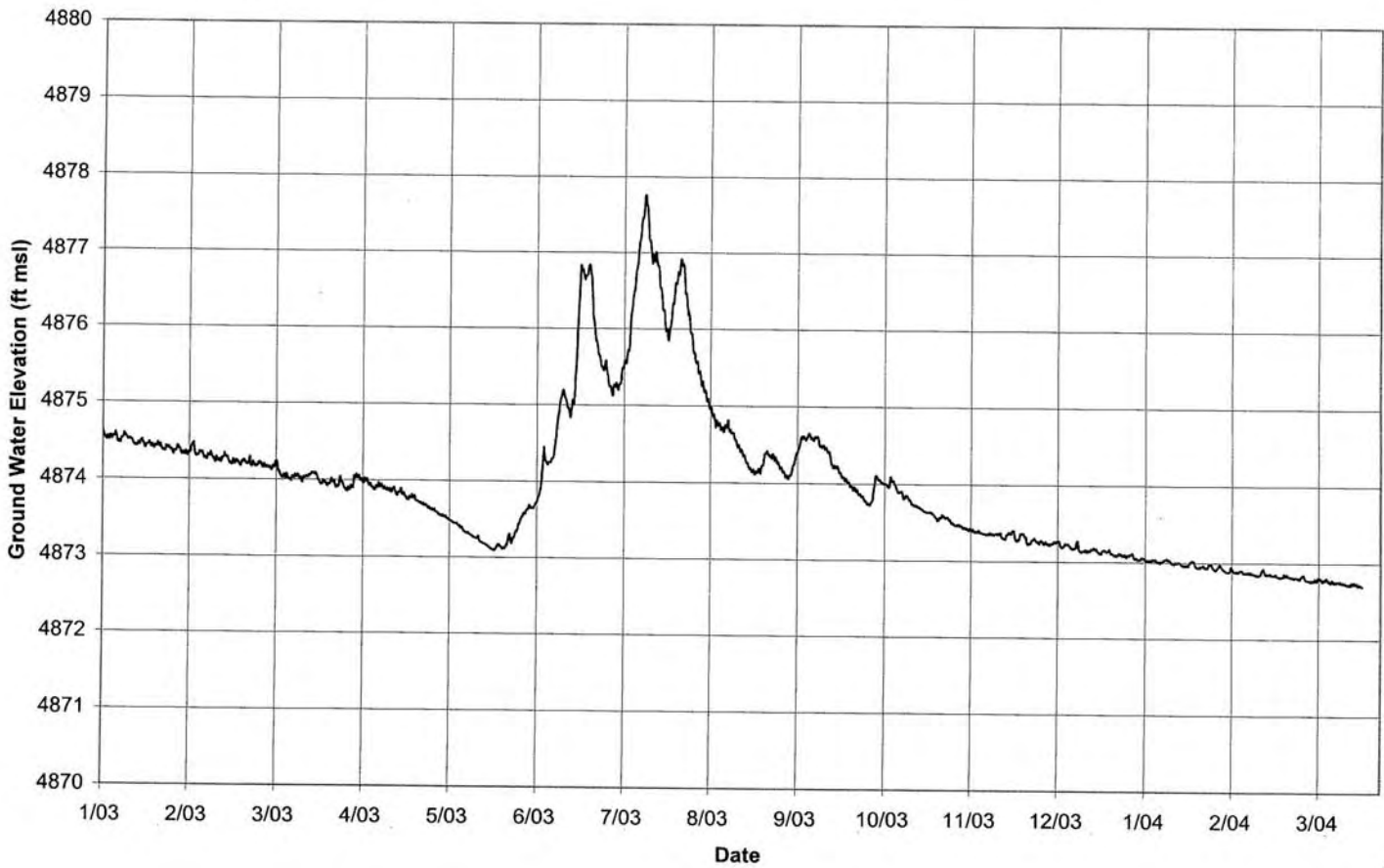
Well 0830 - Terrace East (SE of Disposal Cell)



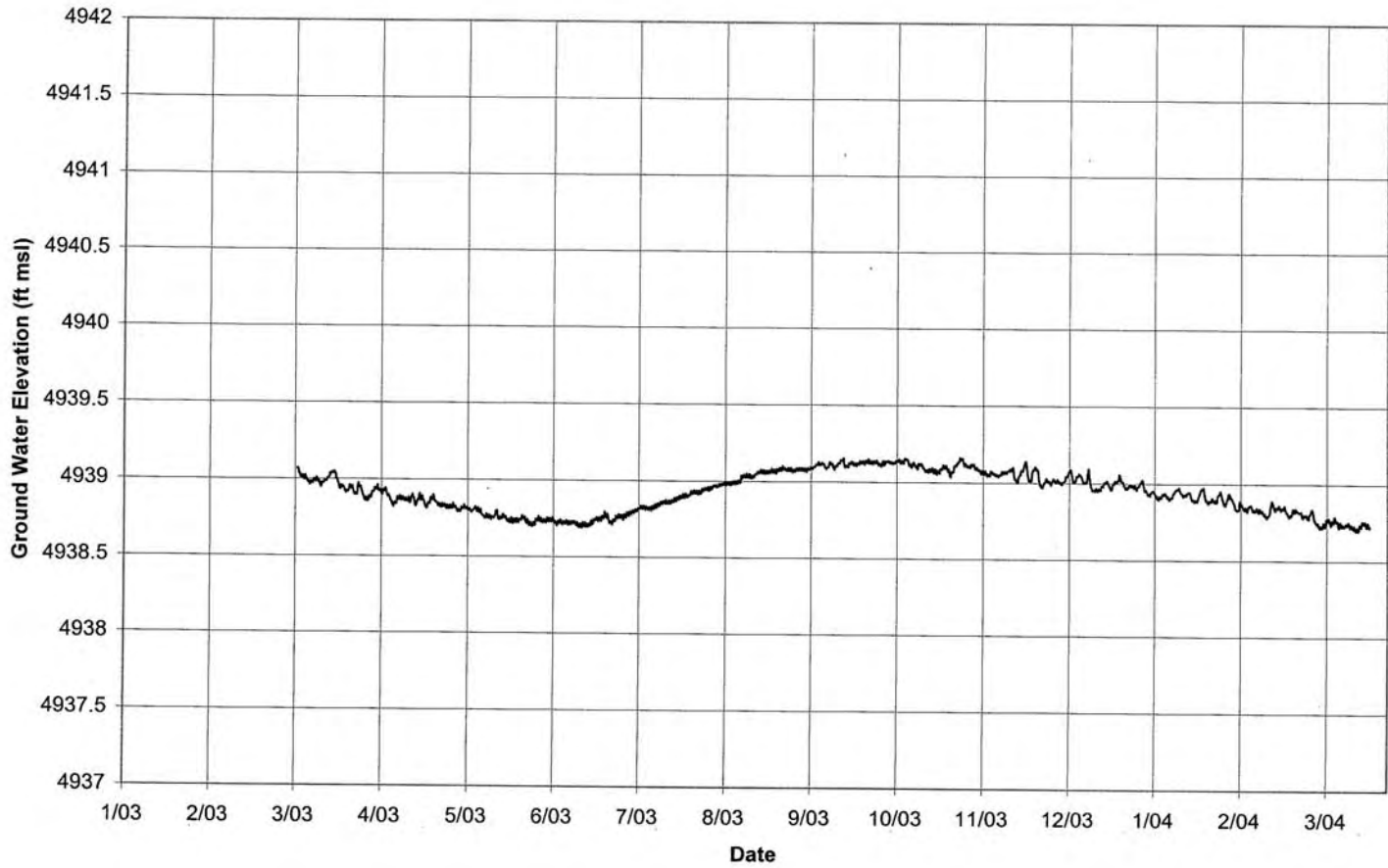
**Terrace West Ground Water Elevation Data
(January 2003 through March 2004)**

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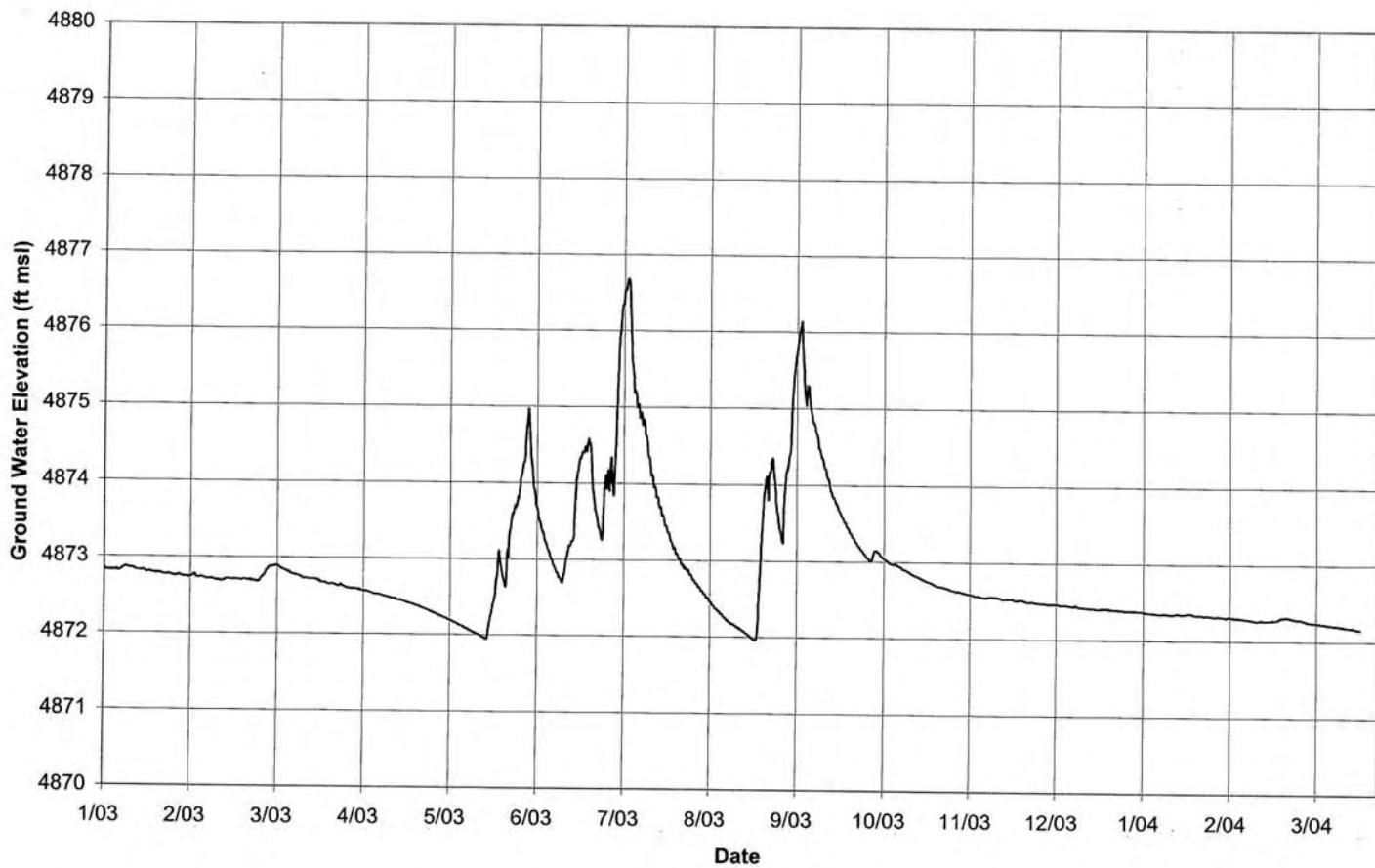
Well 0837 - Terrace West (Irrigated Area)



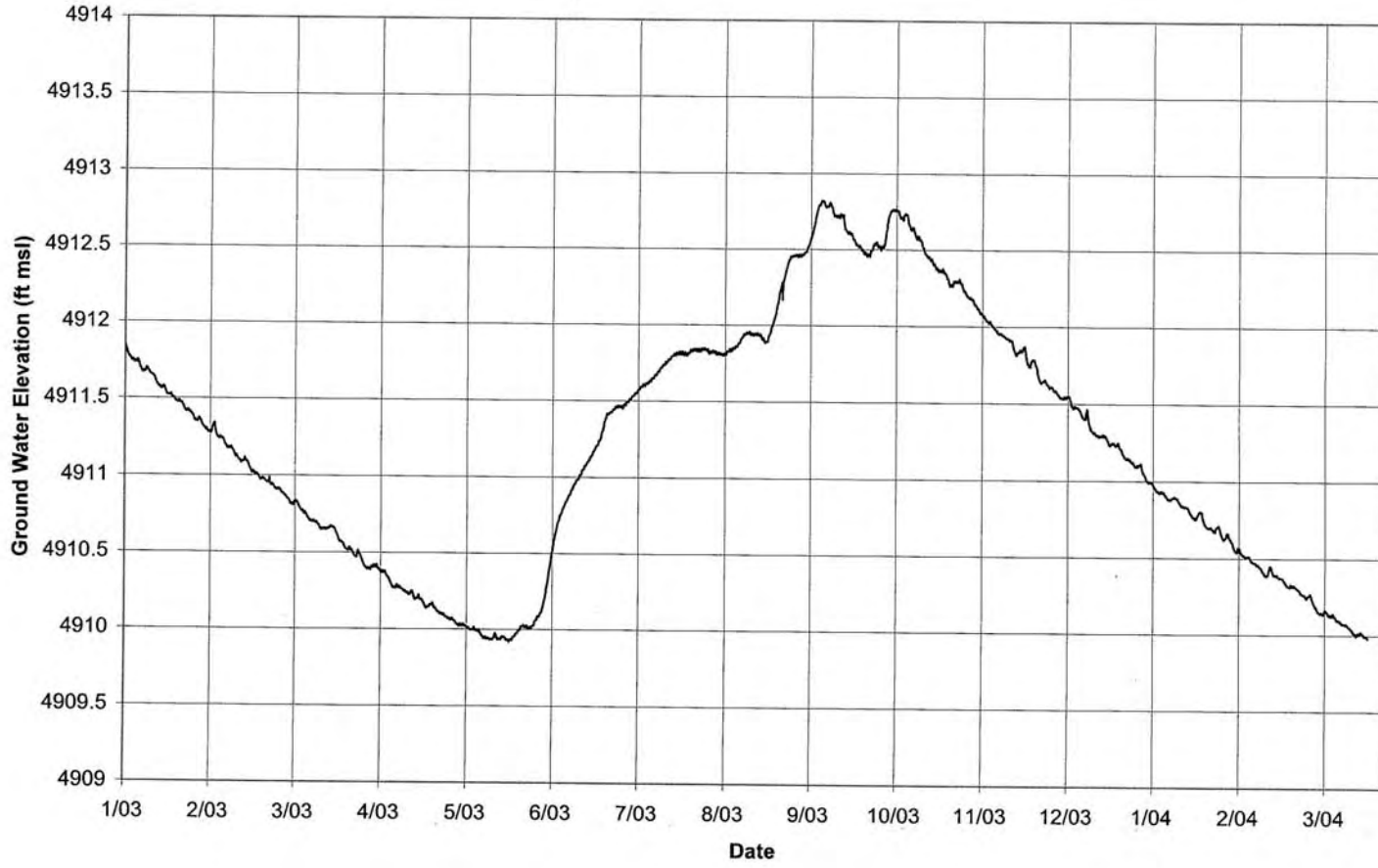
Well 0841 - Terrace West (Across Highway 491 from Terrace East)



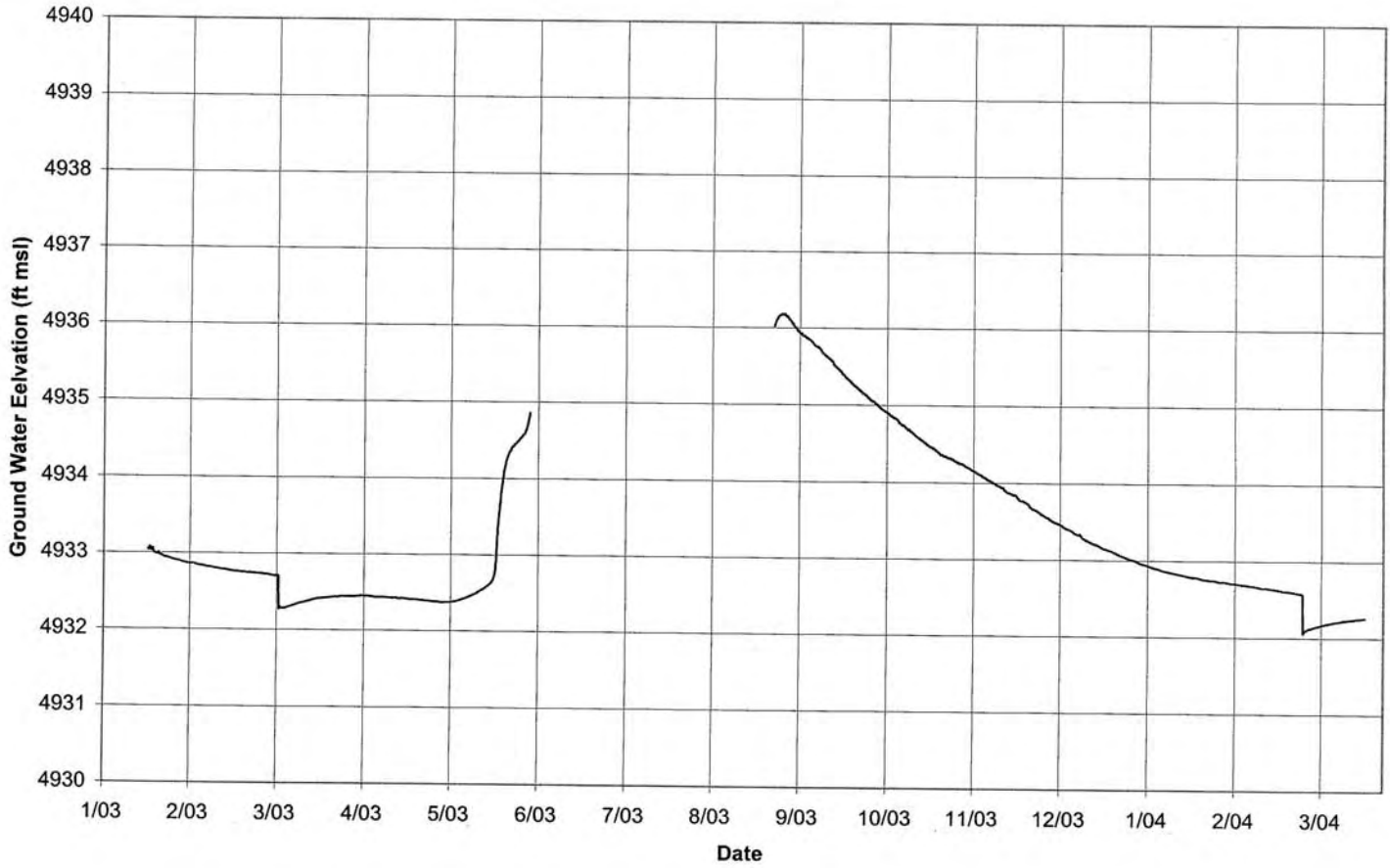
Well 0843 - Terrace West (Irrigated Area)



Well 0846 - Terrace West (Just South of Hwy 64)



Well 1060 - Terrace West



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Appendix C

Floodplain and Terrace Ground Water Extraction Well Data (September 2003 through March 2004)

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Shiprock Terrace Well Field Pumping Rates

well	date/time	reading cum_vol (gal)	added vol prev meter	actual cum_vol (gal)	delta vol (gal)	delta t (min)	avg gpm	
1070	8/29/2003 11:40	155,632		155,632				
	9/5/2003 9:30	160,114		160,114	4,482	9950	0.45	
	9/8/2003 12:21	162,105		162,105	1,991	4491	0.44	
	9/11/2003 14:07	164,075		164,075	1,970	4426	0.45	
	9/12/2003 9:33	164,590		164,590	515	1166	0.44	
	9/15/2003 10:31	166,456		166,456	1,866	4378	0.43	
	9/19/2003 9:31	168,907		168,907	2,451	5700	0.43	
	9/22/2003 10:17	170,807		170,807	1,900	4366	0.44	
	9/26/2003 10:59	173,315		173,315	2,508	5802	0.43	
	9/29/2003 9:15	175,093		175,093	1,778	4216	0.42	
	10/2/2003 9:40	176,915		176,915	1,822	4345	0.42	
	10/6/2003 10:19	179,819		179,819	2,904	5799	0.50	
	10/9/2003 9:35	179,321		179,321				
	10/10/2003 10:00	179,389		179,389	68	1465	0.05	inadvertantly shut off at times
	10/13/2003 10:00	179,389		179,389	0	4320	0.00	inadvertantly shut off at times
	10/15/2003 11:21	179,492		179,492	103	2961	0.03	inadvertantly shut off at times
	10/17/2003 18:11	179,617		179,617	125	3290	0.04	inadvertantly shut off at times
	10/20/2003 13:59	179,617		179,617	0	4068	0.00	inadvertantly shut off at times
	10/22/2003 11:35	179,617		179,617	0	2736	0.00	inadvertantly shut off at times
	10/24/2003 12:15	179,617		179,617	0	2920	0.00	inadvertantly shut off at times
	10/27/2003 10:40	179,617		179,617	0	4225	0.00	
	10/29/2003 13:30	180,254		180,254	637	3050	0.21	
	10/31/2003 11:27	181,494		181,494	1,240	2757	0.45	
	11/3/2003 11:11	183,382		183,382	1,888	4304	0.44	
	11/5/2003 8:14	184,537		184,537	1,155	2703	0.43	changed flow meter batteries
	11/7/2003 19:33	1,420	184,537	185,957	1,420	3559	0.40	
	11/10/2003 10:00	2,906	184,537	187,443	1,486	3747	0.40	
	11/14/2003 11:20	5,116	184,537	189,653	2,210	5840	0.38	
	11/17/2003 12:15	6,877	184,537	191,414	1,761	4375	0.40	
	11/21/2003 9:20	8,921	184,537	193,458	2,044	5585	0.37	
	11/24/2003 11:15	10,486	184,537	195,023	1,565	4435	0.35	
	12/1/2003 10:57	13,832	184,537	198,369	3,346	10062	0.33	
	12/3/2003 13:20	14,884	184,537	199,421	1,052	3023	0.35	
	12/5/2003 18:12	16,041	184,537	200,578	1,157	3172	0.36	
	12/8/2003 10:24	17,456	184,537	201,993	1,415	3852	0.37	
	12/10/2003 12:00	18,519	184,537	203,056	1,063	2976	0.36	
	12/12/2003 10:55	19,516	184,537	204,053	997	2815	0.35	
	12/15/2003 11:47	21,023	184,537	205,560	1,507	4372	0.34	
	12/19/2003 9:50	22,961	184,537	207,498	1,938	5643	0.34	
	12/22/2003 14:38	24,501	184,537	209,038	1,540	4608	0.33	
	12/29/2003 11:55	27,803	184,537	212,340	3,302	9917	0.33	
	1/5/2004 12:39	31,093	184,537	215,630	3,290	10124	0.32	
	1/9/2004 12:19	32,935	184,537	217,472	1,842	5740	0.32	
	1/12/2004 13:55	34,292	184,537	218,829	1,357	4416	0.31	
	1/15/2004 13:30	35,651	184,537	220,188	1,359	4295	0.32	
	1/16/2004 13:21	36,110	184,537	220,647	459	1431	0.32	inaccurate reading
	1/23/2004 11:45	39,250	184,537	223,787	3,140	9984	0.31	used historical data
	1/26/2004 11:46	40,555	184,537	225,092	1,305	4321	0.30	
	1/30/2004 9:12	42,265	184,537	226,802	1,710	5606	0.31	
	2/2/2004 11:22	43,596	184,537	228,133	1,331	4450	0.30	
	2/6/2004 12:33	45,348	184,537	229,885	1,752	5831	0.30	
	2/9/2004 11:51	46,611	184,537	231,148	1,263	4278	0.30	
	2/13/2004 13:22	48,314	184,537	232,851	1,703	5851	0.29	
	2/20/2004 11:55	50,886	184,537	235,423	2,572	9993	0.26	
	2/23/2004 12:24	52,110	184,537	236,647	1,224	4349	0.28	
	2/27/2004 10:15	53,526	184,537	238,063	1,416	5631	0.25	
	3/1/2004 9:22	54,669	184,537	239,206	1,143	4267	0.27	
	3/5/2004 12:47	56,099	184,537	240,636	1,430	5965	0.24	
	3/8/04 13:00	56,409	184,537	240,946	310	4333	0.07	
	3/12/2004 10:48	57,739	184,537	242,276	1,330	5628	0.24	
	3/15/2004 11:00	58,642	184,537	243,179	903	4332	0.21	
	3/19/2004 11:42	59,644	184,537	244,181	1,002	5802	0.17	
	3/24/2004 10:38	60,640	184,537	245,177	996	7136	0.14	
	3/30/2004 17:33	62,104	184,537	246,641	1,464	9055	0.16	

avg 0.29

Shiprock Terrace Well Field Pumping Rates

well	date/time	reading (gpm)reading	added vol prev meter	actual cum_vol (gal)	delta vol (gal)	delta t (min)	avg gpm
1078	8/29/2003 10:50	201,917		201,917			
	9/5/2003 8:53	208,779		208,779	208,779	54531893	0.00
	9/8/2003 12:09	211,945		211,945	3,166	4516	0.70
	9/11/2003 14:24	215,093		215,093	3,148	4455	0.71
	9/12/2003 9:00	215,858		215,858	765	1116	0.69
	9/15/2003 10:14	218,907		218,907	3,049	4394	0.69
	9/19/2003 8:49	222,894		222,894	3,987	5675	0.70
	9/22/2003 10:00	225,955		225,955	3,061	4391	0.70
	9/26/2003 10:20	230,033		230,033	4,078	5780	0.71
	9/29/2003 8:50	233,003		233,003	2,970	4230	0.70
	10/2/2003 7:54	236,027		236,027	3,024	4264	0.71
	10/6/2003 10:19						
	10/9/2003 12:15						
	10/10/2003 9:20	244,000		244,000	7,973	11606	0.69
	10/13/2003 9:45						
	10/15/2003 10:45						
	10/17/2003 18:00	251,400		251,400	7,400	10600	0.70
	10/20/2003 13:40						
	10/22/2003 12:10						
	10/24/2003 12:05						
	10/27/2003 10:05	261,000		261,000	9,600	13925	0.69
	10/30/2003 10:30						
	10/31/2003 11:10	1,063	264,000	265,063	4,063	5825	0.70
	11/3/2003 10:30	4,238	264,000	268,238	3,175	4280	0.74
	11/5/2003 8:40	6,279	264,000	270,279	2,041	2770	0.74
	11/7/2003 19:01	8,428	264,000	272,428	2,149	3501	0.61
	11/10/2003 9:37	8,501	264,000	272,501	73	3756	0.02
	11/14/2003 10:51	15,012	264,000	279,012	6,511	5834	1.12
	11/17/2003 12:02	18,395	264,000	282,395	3,383	4391	0.77
	11/21/2003 8:44	22,514	264,000	286,514	4,119	5562	0.74
	11/24/2003 10:45	25,895	264,000	289,895	3,381	4441	0.76
	12/1/2003 10:25	33,195	264,000	297,195	7,300	10060	0.73
	12/3/2003 13:45	35,427	264,000	299,427	2,232	3080	0.72
	12/5/2003 17:58	37,776	264,000	301,776	2,349	3133	0.75
	12/8/2003 10:05	40,690	264,000	304,690	2,914	3847	0.76
	12/10/2003 12:18	42,966	264,000	306,966	2,276	3013	0.76
	12/12/2003 10:41	45,127	264,000	309,127	2,161	2783	0.78
	12/15/2003 11:15	48,373	264,000	312,373	3,246	4354	0.75
	12/19/2003 9:33	52,364	264,000	316,364	3,991	5658	0.71
	12/22/2003 13:45	55,686	264,000	319,686	3,322	4572	0.73
	12/29/2003 11:18	63,117	264,000	327,117	7,431	9933	0.75
	1/5/2004 12:11	70,769	264,000	334,769	7,652	10133	0.76
	1/9/2004 12:06	74,750	264,000	338,750	3,981	5755	0.69
	1/12/2004 13:15	78,080	264,000	342,080	3,330	4389	0.76
	1/15/2004 12:35	81,182	264,000	345,182	3,102	4280	0.72
	1/16/2004 11:27	82,263	264,000	346,263	1,081	1372	0.79
	1/23/2004 11:45	89,900	264,000	353,900	7,637	10098	0.76
	1/26/2004 11:15	93,205	264,000	357,205	3,305	4290	0.77
	1/30/2004 8:59	97,360	264,000	361,360	4,155	5624	0.74
	2/2/2004 11:00	100,660	264,000	364,660	3,300	4441	0.74
	2/6/2004 12:00	105,073	264,000	369,073	4,413	5820	0.76
	2/9/2004 11:40	108,195	264,000	372,195	3,122	4300	0.73
	2/13/2004 13:12	112,407	264,000	376,407	4,212	5852	0.72
	2/20/2004 11:10	119,419	264,000	383,419	7,012	9958	0.70
	2/23/2004 12:15	122,411	264,000	386,411	2,992	4385	0.68
	2/27/2004 9:38	126,786	264,000	390,786	4,375	5603	0.78
	3/1/2004 9:16	130,051	264,000	394,051	3,265	4298	0.76
	3/5/2004 12:00	134,385	264,000	398,385	4,334	5924	0.73
	3/8/2004 12:18	137,314	264,000	401,314	2,929	4338	0.68
	3/12/2004 10:35	141,281	264,000	405,281	3,967	5657	0.70
	3/15/2004 10:29	144,270	264,000	408,270	2,989	4314	0.69
	3/19/2004 11:32	148,392	264,000	412,392	4,122	5823	0.71
	3/24/2004 10:22	153,319	264,000	417,319	4,927	7130	0.69
	3/30/2004 17:20	159,626	264,000	423,626	6,307	9058	0.70
	avg						0.70

Shiprock Terrace Well Field Pumping Rates

well	date/time	reading cum vol (gal)	added vol prev meter	actual cum vol (gal)	delta vol (gal)	delta t (min)	avg gpm
1091	8/29/2003 9:02			8,440			
	9/5/2003 6:47			10,715	10715	54531767	0.00
	9/8/2003 11:21			11,803	1088	4594	0.24
	9/11/2003 15:04			12,832	1029	4543	0.23
	9/12/2003 6:50			13,053	221	946	0.23
	9/15/2003 9:34			13,982	929	4484	0.21
	9/19/2003 6:56			15,185	1203	5602	0.21
	9/22/2003 9:09			16,090	905	4453	0.20
	9/26/2003 8:25			17,315	1225	5716	0.21
	9/29/2003 7:15			18,175	860	4250	0.20
	10/1/2003 17:08			18,845	670	3473	0.19
	10/6/2003 9:23			20,165	1320	6735	0.20
	10/8/2003 16:08			20,759	594	3285	0.18
	10/10/2003 7:55			21,200	441	2387	0.18
	10/13/2003 7:50			22,018	818	4315	0.19
	10/15/2003 9:19			22,539	521	2969	0.18
	10/17/2003 16:30			23,126	587	3311	0.18
	10/20/2003 12:53			23,824	698	4103	0.17
	10/22/2003 13:15			24,301	477	2902	0.16
	10/24/2003 11:27			24,779	478	2772	0.17
	10/27/2003 9:18			25,492	713	4191	0.17
	10/29/2003 16:42			26,129	637	3324	0.19
	10/31/2003 9:50			26,574	445	2468	0.18
	11/3/2003 9:00			27,327	753	4270	0.18
	11/5/2003 7:55			27,327	0	2815	0.00
	11/7/2003 18:00			27,600	273	3485	0.08
	11/10/2003 9:15						
	11/14/2003 9:30	3,026	25,375	28,401	801	9570	0.08
	11/17/2003 11:07	4,143	25,375	29,518	1,117	4417	0.25
	11/21/2003 6:57	5,476	25,375	30,851	1,333	5510	0.24
	11/24/2003 8:50	6,350	25,375	31,725	874	4433	0.20
	12/1/2003 8:30	8,350	25,375	33,725	2,000	10060	0.20
	12/3/2003 12:56	621	33,725	34,346	621	3146	0.20
	12/5/2003 15:29	1,217	33,725	34,942	596	3033	0.20
	12/8/2003 9:12	2,022	33,725	35,747	805	3943	0.20
	12/10/2003 13:54	2,630	33,725	36,355	608	3162	0.19
	12/12/2003 9:48	3,159	33,725	36,884	529	2634	0.20
	12/15/2003 9:50	4,002	33,725	37,727	843	4322	0.20
	12/19/2003 9:02	938	37,950	38,888	1,161	5712	0.20
	12/22/2003 12:50	1,858	37,950	39,808	920	4548	0.20
	12/29/2003 10:20	3,800	37,950	41,750	1,942	9930	0.20
	1/5/2004 11:00	5,300	37,950	43,250	1,500	10120	0.15
	1/9/2004 11:28	750	43,250	44,000	750	5788	0.13
	1/12/2004 12:30	1,348	43,250	44,598	598	4382	0.14
	1/15/2004 9:15	1,886	43,250	45,136	538	4125	0.13
	1/16/2004 11:03	2,119	43,250	45,369	233	1548	0.15
	1/23/2004 11:36	3,429	43,250	46,679	1,310	10113	0.13
	1/26/2004 10:26	4,039	43,250	47,289	610	4250	0.14
	1/30/2004 8:17	4,728	43,250	47,978	689	5631	0.12
	2/2/2004 9:20	5,316	43,250	48,566	588	4383	0.13
	2/6/2004 10:00	6,031	43,250	49,281	715	5800	0.12
	2/9/2004 11:02	6,533	43,250	49,783	502	4382	0.11
	2/13/2004 12:32	7,228	43,250	50,478	695	5850	0.12
	2/20/2004 9:21	8,337	43,250	51,587	1,109	9889	0.11
	2/23/2004 9:27	8,831	43,250	52,081	494	4326	0.11
	2/27/2004 8:45	9,455	43,250	52,705	624	5718	0.11
	3/5/2004 10:20	10,540	43,250	53,790	1,085	10175	0.11
	3/5/2004 10:20	10,540	43,250	53,790			
	3/8/2004 11:12	10,910	43,250	54,160	370	4372	0.08
	3/12/2004 9:50	11,523	43,250	54,773	613	5678	0.11
	3/15/2004 8:51	11,974	43,250	55,224	451	4261	0.11
	3/19/2004 10:43	12,571	43,250	55,821	597	5872	0.10
	3/24/2004 9:16	13,314	43,250	56,564	743	7113	0.10
	3/30/2004 17:51	14,217	43,250	57,467	903	9155	0.10
	avg						0.16

