November 10, 1995

Cheri Miller Tennessee Valley Authority Fossil Fuels Group 1101 Market Street Chattanooga, Tennessee 37402-2801

Subject:

FINAL REPORT TRANSMITTAL

Fly Ash, Bottom Ash and Scrubber Gypsum Study Contract No. TV-92657V, Phase 1 Law Engineering - Knoxville Project No. 50385-5-0400 (Phase 1) Law Engineering - Atlanta Project No. 5810860101

Dear Cheri:

I've sent a special messenger (courier) to deliver this final report. The package consists of five final report letters (for distribution to all who received the five sets I brought up last month) and the original test reports for all the work performed in this test phase. I've also copied the Excel spreadsheet files that you may find helpful. They are: Prgrm.xls - *contains all the information you see in the 11x17 fold-out sheets*; and 29 additional .xls files which contain a summary of results for each individual material/source tested, which are shown in each of the sections following a colored sheet of paper.

In speaking with Don Armour, he made a lot of sense when describing why the gypsums, a water soluble material, behaved the way they did. Essentially, the air-dry method of achieving an air-dried condition most certainly chemically altered the material. Additionally, because of the water soluble nature of the material, he recommends using gypsum saturated water when performing the saturation steps for the majority of the geotechnical tests performed. There is apparently some literature available in the Electric Power Research Institute (EPRI). I suggest that if we research the gypsum materials further, we retain Mr. Armour as a technical consultant to help us understand what is going on.

Thank you for the opportunity to be of service to you on this project. If you have any questions or require any additional information, please contact me.

Sincerely, LAW ENGINEERING, INC.

Mit

Richard L. Boudreau, P.E. Senior Materials Engineer



Tennessee Valley Authority Fossil Fuels Group 1101 Market Street Chattanooga, Tennessee 37402-2801

Subject:

FINAL REPORT Fly Ash, Bottom Ash and Scrubber Gypsum Study Contract No. TV-92657V, Phase 1 Law Engineering - Knoxville Project No. 50385-5-0400 (Phase 1) Law Engineering - Atlanta Project No. 5810860101

Dear Sir/Madam:

Law Engineering has completed the testing program outlined in the Scope of Work - Phase 1 of Contract TV-92657V. This letter provides a brief background of the test program. In addition, a descriptive summary of the test procedures used is presented. The summary provides discussion pertaining to clarifications or deviations from the procedures. Finally, general observations made while preparing samples or performing tests that are not represented on the test reports are discussed, and the results of the test program are presented.

BACKGROUND

The purpose of this laboratory testing program was to provide classification and engineering properties characterization of several of the Tennessee Valley Authority's (TVA) sources of fly ash, bottom ash, boiler slag and scrubber gypsum. Twenty-nine materials from eleven coal burning power generation steam plants were included in this study. The materials received were tested through a broad range of test procedures outlined by the American Society for Testing and Materials (ASTM), the American Association of State Highway and Transportation Officials (AASHTO), the Strategic Highway Research Program (SHRP), and Law Engineering. Each test in the program was chosen to illustrate the engineering properties of each material to determine their suitability for structural embankment fill in highway construction.

In all, thirteen sources of fly ash, nine sources of bottom ash, two sources of boiler slag and three sources of scrubber gypsum (FGD - flue gas desulfurization) were received for testing. In addition, a Spent Bed Material and Char material were received from the single unit atmospheric fluidized bed boiler at Shawnee. Each source material was provided to us in six 5-gallon plastic buckets, labeled A through F.

LAW ENGINEERING, INC.

396 PLASTERS AVENUE, N.E. • ATLANTA, GA 30324 (404) 873-4761 • FAX (404) 881-0508

Soils Classification System (USCS) symbol are provided based on the Particle-Size Analysis and Atterberg Limits results. Similarly, an AASHTO classification is provided based on guidelines set forth in *The Classification of Soils and Soil-Aggregate Mixtures for Highway Construction Purposes, AASHTO M145.*

Volumetric Testing

Several tests were performed to provide the general volumetric properties of each material. The tests outlined below were performed on one composite sample from each of the twenty-seven fly ash, bottom ash, boiler slag and scrubber gypsum sources.

Test Method for Laboratory Compaction Characteristics of Soil Using Standard Effort (12,400 ft-lbf/ft³) (600 kN-m/m³), ASTM D 698. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Standard Proctor.

Test Method for Laboratory Compaction Characteristics of Soil Using Modified Effort (56,000 ft-lbf/ft³) (2,700 kN-m/m³), ASTM D 1557. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Modified Proctor.

Test Method for Maximum Index Density and Unit Weight of Soils Using a Vibratory Table, ASTM D 4253 and Test Method for Minimum Index Density and Unit Weight of Soils and Calculation of Relative Density, ASTM D 4254. Because the Standard and Modified Proctors do not necessarily define a good relationship between dry density and moisture content (typically because of the free draining nature of granular materials), the minimum and maximum index densities were determined for the nine bottom ash samples.

Test Method for One-Dimensional Consolidation Properties of Soils, ASTM D 2435. Samples of the fly ash, boiler slag and scrubber gypsum were remolded in nominal 2.5-inch diameter by 1.0-inch high rings to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor. Nominal load increments of 0.5, 1.0, 2.0, 4.0, 8.0 and 16.0 ksf were applied. Moist porous stones were used; however, samples were not inundated for the test.

Hydraulic Conductivity and Static Strength Testing

Test Method for Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter, ASTM D 5084. The fly ash, boiler slag and scrubber gypsum materials were remolded to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor and tested for hydraulic conductivity. An effective confining pressure of 14 psi was used as the standard for all tests. The samples were remolded to a nominal 2.88-inch diameter by 6.0-in high specimen.

Electro-Chemical Testing

Determining the Minimum Laboratory Soil Resistivity, AASHTO T 288. A supersaturated slurry was prepared for each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) and the minimum resistivity value was measured.

Determining pH of Soil for Use in Corrosion Testing, AASHTO T 289. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the pH value was measured.

Determining Water Soluble Sulfate Ion Content in Soil, AASHTO T 290. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble sulfate ion content was measured using the Turbidimetric Method (Method B).

Determining Water Soluble Chloride Ion Content in Soil, AASHTO T 291. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble chloride ion content was measured using the pH/mV Meter Method (Method B).

PECULIARITIES AND TEST RESULTS

Based on our years of experience with the testing of geotechnical materials and our experience derived from this test program, we have highlighted some instances in which these materials behaved differently than others, either visually or by test results that varied significantly from results calculated for similar materials.

- Both the spent bed material (Shawnee) and the char (Shawnee) were observed to react upon treatment with water. This phenomenon created complications with all the geotechnical tests (classification, volumetric, and strength test). Only the electro-chemical tests were performed on these materials. Because of the highly reactive nature of the spent bed material, the resistivity test was unable to be performed.
- The scrubber gypsum materials were observed to react upon treatment with water following the air dry preparation of these materials. The samples were air-dried overnight in a temperature controlled room set at 140 °F. This phenomenon created complications with the successful completion of the classification tests, although we were able to perform a specific gravity test on a composite sample of each source. We note that the scrubber gypsum materials exhibit relatively more strength than the other materials tested in this program when tested under dynamic conditions at **low applied strains (Resilient Modulus)**. This may indicate that a weak chemical bond is created between particles.

• Beside the noticeable color difference of the Cumberland Dry Fly Ash (tan/brown as opposed to gray for all other fly ashes in this program) that was sampled from Units 1 and 2 on April 17, 18 and 19, 1995, several of the observations and test results are worth noting:



Tennessee Valley Authority Fossil Fuels Group 1101 Market Street Chattanooga, Tennessee 37402-2801

Subject:

FINAL REPORT Fly Ash, Bottom Ash and Scrubber Gypsum Study Contract No. TV-92657V, Phase 1 Law Engineering - Knoxville Project No. 50385-5-0400 (Phase 1) Law Engineering - Atlanta Project No. 5810860101

Dear Sir/Madam:

Law Engineering has completed the testing program outlined in the Scope of Work - Phase 1 of Contract TV-92657V. This letter provides a brief background of the test program. In addition, a descriptive summary of the test procedures used is presented. The summary provides discussion pertaining to clarifications or deviations from the procedures. Finally, general observations made while preparing samples or performing tests that are not represented on the test reports are discussed, and the results of the test program are presented.

BACKGROUND

The purpose of this laboratory testing program was to provide classification and engineering properties characterization of several of the Tennessee Valley Authority's (TVA) sources of fly ash, bottom ash, boiler slag and scrubber gypsum. Twenty-nine materials from eleven coal burning power generation steam plants were included in this study. The materials received were tested through a broad range of test procedures outlined by the American Society for Testing and Materials (ASTM), the American Association of State Highway and Transportation Officials (AASHTO), the Strategic Highway Research Program (SHRP), and Law Engineering. Each test in the program was chosen to illustrate the engineering properties of each material to determine their suitability for structural embankment fill in highway construction.

In all, thirteen sources of fly ash, nine sources of bottom ash, two sources of boiler slag and three sources of scrubber gypsum (FGD - flue gas desulfurization) were received for testing. In addition, a Spent Bed Material and Char material were received from the single unit atmospheric fluidized bed boiler at Shawnee. Each source material was provided to us in six 5-gallon plastic buckets, labeled A through F.

LAW ENGINEERING, INC.

396 PLASTERS AVENUE, N.E. • ATLANTA, GA 30324 (404) 873-4761 • FAX (404) 881-0508

Soils Classification System (USCS) symbol are provided based on the Particle-Size Analysis and Atterberg Limits results. Similarly, an AASHTO classification is provided based on guidelines set forth in *The Classification of Soils and Soil-Aggregate Mixtures for Highway Construction Purposes, AASHTO M145*.

Volumetric Testing

Several tests were performed to provide the general volumetric properties of each material. The tests outlined below were performed on one composite sample from each of the twenty-seven fly ash, bottom ash, boiler slag and scrubber gypsum sources.

Test Method for Laboratory Compaction Characteristics of Soil Using Standard Effort (12,400 $ft-lbf/ft^3$) (600 kN-m/m³), ASTM D 698. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Standard Proctor.

Test Method for Laboratory Compaction Characteristics of Soil Using Modified Effort (56,000 ft-lbf/ft³) (2,700 kN-m/m³), ASTM D 1557. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Modified Proctor.

Test Method for Maximum Index Density and Unit Weight of Soils Using a Vibratory Table. ASTM D 4253 and Test Method for Minimum Index Density and Unit Weight of Soils and Calculation of Relative Density, ASTM D 4254. Because the Standard and Modified Proctors do not necessarily define a good relationship between dry density and moisture content (typically because of the free draining nature of granular materials), the minimum and maximum index densities were determined for the nine bottom ash samples.

Test Method for One-Dimensional Consolidation Properties of Soils, ASTM D 2435. Samples of the fly ash, boiler slag and scrubber gypsum were remolded in nominal 2.5-inch diameter by 1.0-inch high rings to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor. Nominal load increments of 0.5, 1.0, 2.0, 4.0, 8.0 and 16.0 ksf were applied. Moist porous stones were used; however, samples were not inundated for the test.

Hydraulic Conductivity and Static Strength Testing

Test Method for Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter, ASTM D 5084. The fly ash, boiler slag and scrubber gypsum materials were remolded to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor and tested for hydraulic conductivity. An effective confining pressure of 14 psi was used as the standard for all tests. The samples were remolded to a nominal 2.88-inch diameter by 6.0-in high specimen.

Electro-Chemical Testing

Determining the Minimum Laboratory Soil Resistivity, AASHTO T 288. A supersaturated slurry was prepared for each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) and the minimum resistivity value was measured.

Determining pH of Soil for Use in Corrosion Testing, AASHTO T 289. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the pH value was measured.

Determining Water Soluble Sulfate Ion Content in Soil, AASHTO T 290. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble sulfate ion content was measured using the Turbidimetric Method (Method B).

Determining Water Soluble Chloride Ion Content in Soil, AASHTO T 291. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble chloride ion content was measured using the pH/mV Meter Method (Method B).

PECULIARITIES AND TEST RESULTS

Based on our years of experience with the testing of geotechnical materials and our experience derived from this test program, we have highlighted some instances in which these materials behaved differently than others, either visually or by test results that varied significantly from results calculated for similar materials.

- Both the spent bed material (Shawnee) and the char (Shawnee) were observed to react upon treatment with water. This phenomenon created complications with all the geotechnical tests (classification, volumetric, and strength test). Only the electro-chemical tests were performed on these materials. Because of the highly reactive nature of the spent bed material, the resistivity test was unable to be performed.
- The scrubber gypsum materials were observed to react upon treatment with water following the air dry preparation of these materials. The samples were air-dried overnight in a temperature controlled room set at 140 °F. This phenomenon created complications with the successful completion of the classification tests, although we were able to perform a specific gravity test on a composite sample of each source. We note that the scrubber gypsum materials exhibit relatively more strength than the other materials tested in this program when tested under dynamic conditions at low applied strains (Resilient Modulus). This may indicate that a weak chemical bond is created between particles.

• Beside the noticeable color difference of the Cumberland Dry Fly Ash (tan/brown as opposed to gray for all other fly ashes in this program) that was sampled from Units 1 and 2 on April 17, 18 and 19, 1995, several of the observations and test results are worth noting:



Tennessee Valley Authority Fossil Fuels Group 1101 Market Street Chattanooga, Tennessee 37402-2801

Subject:

FINAL REPORT Fly Ash, Bottom Ash and Scrubber Gypsum Study Contract No. TV-92657V, Phase 1 Law Engineering - Knoxville Project No. 50385-5-0400 (Phase 1) Law Engineering - Atlanta Project No. 5810860101

Dear Sir/Madam:

Law Engineering has completed the testing program outlined in the Scope of Work - Phase 1 of Contract TV-92657V. This letter provides a brief background of the test program. In addition, a descriptive summary of the test procedures used is presented. The summary provides discussion pertaining to clarifications or deviations from the procedures. Finally, general observations made while preparing samples or performing tests that are not represented on the test reports are discussed, and the results of the test program are presented.

BACKGROUND

The purpose of this laboratory testing program was to provide classification and engineering properties characterization of several of the Tennessee Valley Authority's (TVA) sources of fly ash, bottom ash, boiler slag and scrubber gypsum. Twenty-nine materials from eleven coal burning power generation steam plants were included in this study. The materials received were tested through a broad range of test procedures outlined by the American Society for Testing and Materials (ASTM), the American Association of State Highway and Transportation Officials (AASHTO), the Strategic Highway Research Program (SHRP), and Law Engineering. Each test in the program was chosen to illustrate the engineering properties of each material to determine their suitability for structural embankment fill in highway construction.

In all, thirteen sources of fly ash, nine sources of bottom ash, two sources of boiler slag and three sources of scrubber gypsum (FGD - flue gas desulfurization) were received for testing. In addition, a Spent Bed Material and Char material were received from the single unit atmospheric fluidized bed boiler at Shawnee. Each source material was provided to us in six 5-gallon plastic buckets, labeled A through F.

LAW ENGINEERING, INC.

396 PLASTERS AVENUE, N.E. • ATLANTA, GA 30324 (404) 873-4761 • FAX (404) 881-0508

November 7, 1995

Soils Classification System (USCS) symbol are provided based on the Particle-Size Analysis and Atterberg Limits results. Similarly, an AASHTO classification is provided based on guidelines set forth in *The Classification of Soils and Soil-Aggregate Mixtures for Highway Construction Purposes, AASHTO M145.*

Volumetric Testing

Several tests were performed to provide the general volumetric properties of each material. The tests outlined below were performed on one composite sample from each of the twenty-seven fly ash, bottom ash, boiler slag and scrubber gypsum sources.

Test Method for Laboratory Compaction Characteristics of Soil Using Standard Effort (12,400 $ft-lbf/ft^3$) (600 kN-m/m³), ASTM D 698. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Standard Proctor.

Test Method for Laboratory Compaction Characteristics of Soil Using Modified Effort (56,000 ft-lbf/ft³) (2,700 kN-m/m³), ASTM D 1557. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Modified Proctor.

Test Method for Maximum Index Density and Unit Weight of Soils Using a Vibratory Table. ASTM D 4253 and Test Method for Minimum Index Density and Unit Weight of Soils and Calculation of Relative Density, ASTM D 4254. Because the Standard and Modified Proctors do not necessarily define a good relationship between dry density and moisture content (typically because of the free draining nature of granular materials), the minimum and maximum index densities were determined for the nine bottom ash samples.

Test Method for One-Dimensional Consolidation Properties of Soils, ASTM D 2435. Samples of the fly ash, boiler slag and scrubber gypsum were remolded in nominal 2.5-inch diameter by 1.0-inch high rings to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor. Nominal load increments of 0.5, 1.0, 2.0, 4.0, 8.0 and 16.0 ksf were applied. Moist porous stones were used; however, samples were not inundated for the test.

Hydraulic Conductivity and Static Strength Testing

Test Method for Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter, ASTM D 5084. The fly ash, boiler slag and scrubber gypsum materials were remolded to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor and tested for hydraulic conductivity. An effective confining pressure of 14 psi was used as the standard for all tests. The samples were remolded to a nominal 2.88-inch diameter by 6.0-in high specimen.

Electro-Chemical Testing

Determining the Minimum Laboratory Soil Resistivity, AASHTO T 288. A supersaturated slurry was prepared for each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) and the minimum resistivity value was measured.

Determining pH of Soil for Use in Corrosion Testing, AASHTO T 289. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the pH value was measured.

Determining Water Soluble Sulfate Ion Content in Soil, AASHTO T 290. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble sulfate ion content was measured using the Turbidimetric Method (Method B).

Determining Water Soluble Chloride Ion Content in Soil, AASHTO T 291. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble chloride ion content was measured using the pH/mV Meter Method (Method B).

PECULIARITIES AND TEST RESULTS

Based on our years of experience with the testing of geotechnical materials and our experience derived from this test program, we have highlighted some instances in which these materials behaved differently than others, either visually or by test results that varied significantly from results calculated for similar materials.

- Both the spent bed material (Shawnee) and the char (Shawnee) were observed to react upon treatment with water. This phenomenon created complications with all the geotechnical tests (classification, volumetric, and strength test). Only the electro-chemical tests were performed on these materials. Because of the highly reactive nature of the spent bed material, the resistivity test was unable to be performed.
- The scrubber gypsum materials were observed to react upon treatment with water following the air dry preparation of these materials. The samples were air-dried overnight in a temperature controlled room set at 140 °F. This phenomenon created complications with the successful completion of the classification tests, although we were able to perform a specific gravity test on a composite sample of each source. We note that the scrubber gypsum materials exhibit relatively more strength than the other materials tested in this program when tested under dynamic conditions at low applied strains (Resilient Modulus). This may indicate that a weak chemical bond is created between particles.
- Beside the noticeable color difference of the Cumberland Dry Fly Ash (tan/brown as opposed to gray for all other fly ashes in this program) that was sampled from Units 1 and 2 on April 17, 18 and 19, 1995, several of the observations and test results are worth noting:



Tennessee Valley Authority Fossil Fuels Group 1101 Market Street Chattanooga, Tennessee 37402-2801

Subject:

FINAL REPORT Fly Ash, Bottom Ash and Scrubber Gypsum Study Contract No. TV-92657V, Phase 1 Law Engineering - Knoxville Project No. 50385-5-0400 (Phase 1) Law Engineering - Atlanta Project No. 5810860101

Dear Sir/Madam:

Law Engineering has completed the testing program outlined in the Scope of Work - Phase 1 of Contract TV-92657V. This letter provides a brief background of the test program. In addition, a descriptive summary of the test procedures used is presented. The summary provides discussion pertaining to clarifications or deviations from the procedures. Finally, general observations made while preparing samples or performing tests that are not represented on the test reports are discussed, and the results of the test program are presented.

BACKGROUND

The purpose of this laboratory testing program was to provide classification and engineering properties characterization of several of the Tennessee Valley Authority's (TVA) sources of fly ash, bottom ash, boiler slag and scrubber gypsum. Twenty-nine materials from eleven coal burning power generation steam plants were included in this study. The materials received were tested through a broad range of test procedures outlined by the American Society for Testing and Materials (ASTM), the American Association of State Highway and Transportation Officials (AASHTO), the Strategic Highway Research Program (SHRP), and Law Engineering. Each test in the program was chosen to illustrate the engineering properties of each material to determine their suitability for structural embankment fill in highway construction.

In all, thirteen sources of fly ash, nine sources of bottom ash, two sources of boiler slag and three sources of scrubber gypsum (FGD - flue gas desulfurization) were received for testing. In addition, a Spent Bed Material and Char material were received from the single unit atmospheric fluidized bed boiler at Shawnee. Each source material was provided to us in six 5-gallon plastic buckets, labeled A through F.

LAW ENGINEERING, INC.

396 PLASTERS AVENUE, N.E. • ATLANTA, GA 30324 (404) 873-4761 • FAX (404) 881-0508

Soils Classification System (USCS) symbol are provided based on the Particle-Size Analysis and Atterberg Limits results. Similarly, an AASHTO classification is provided based on guidelines set forth in *The Classification of Soils and Soil-Aggregate Mixtures for Highway Construction Purposes, AASHTO M145*.

Volumetric Testing

Several tests were performed to provide the general volumetric properties of each material. The tests outlined below were performed on one composite sample from each of the twenty-seven fly ash, bottom ash, boiler slag and scrubber gypsum sources.

Test Method for Laboratory Compaction Characteristics of Soil Using Standard Effort (12,400 $ft-lbf/ft^3$) (600 kN-m/m³), ASTM D 698. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Standard Proctor.

Test Method for Laboratory Compaction Characteristics of Soil Using Modified Effort (56,000 ft-lbf/ft³) (2,700 kN-m/m³), ASTM D 1557. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Modified Proctor.

Test Method for Maximum Index Density and Unit Weight of Soils Using a Vibratory Table. ASTM D 4253 and Test Method for Minimum Index Density and Unit Weight of Soils and Calculation of Relative Density, ASTM D 4254. Because the Standard and Modified Proctors do not necessarily define a good relationship between dry density and moisture content (typically because of the free draining nature of granular materials), the minimum and maximum index densities were determined for the nine bottom ash samples.

Test Method for One-Dimensional Consolidation Properties of Soils, ASTM D 2435. Samples of the fly ash, boiler slag and scrubber gypsum were remolded in nominal 2.5-inch diameter by 1.0-inch high rings to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor. Nominal load increments of 0.5, 1.0, 2.0, 4.0, 8.0 and 16.0 ksf were applied. Moist porous stones were used; however, samples were not inundated for the test.

Hydraulic Conductivity and Static Strength Testing

Test Method for Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter, ASTM D 5084. The fly ash, boiler slag and scrubber gypsum materials were remolded to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor and tested for hydraulic conductivity. An effective confining pressure of 14 psi was used as the standard for all tests. The samples were remolded to a nominal 2.88-inch diameter by 6.0-in high specimen.

Electro-Chemical Testing

Determining the Minimum Laboratory Soil Resistivity, AASHTO T 288. A supersaturated slurry was prepared for each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) and the minimum resistivity value was measured.

Determining pH of Soil for Use in Corrosion Testing, AASHTO T 289. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the pH value was measured.

Determining Water Soluble Sulfate Ion Content in Soil, AASHTO T 290. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble sulfate ion content was measured using the Turbidimetric Method (Method B).

Determining Water Soluble Chloride Ion Content in Soil, AASHTO T 291. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble chloride ion content was measured using the pH/mV Meter Method (Method B).

PECULIARITIES AND TEST RESULTS

Based on our years of experience with the testing of geotechnical materials and our experience derived from this test program, we have highlighted some instances in which these materials behaved differently than others, either visually or by test results that varied significantly from results calculated for similar materials.

- Both the spent bed material (Shawnee) and the char (Shawnee) were observed to react upon treatment with water. This phenomenon created complications with all the geotechnical tests (classification, volumetric, and strength test). Only the electro-chemical tests were performed on these materials. Because of the highly reactive nature of the spent bed material, the resistivity test was unable to be performed.
- The scrubber gypsum materials were observed to react upon treatment with water following the air dry preparation of these materials. The samples were air-dried overnight in a temperature controlled room set at 140 °F. This phenomenon created complications with the successful completion of the classification tests, although we were able to perform a specific gravity test on a composite sample of each source. We note that the scrubber gypsum materials exhibit relatively more strength than the other materials tested in this program when tested under dynamic conditions at low applied strains (Resilient Modulus). This may indicate that a weak chemical bond is created between particles.
- Beside the noticeable color difference of the Cumberland Dry Fly Ash (tan/brown as opposed to gray for all other fly ashes in this program) that was sampled from Units 1 and 2 on April 17, 18 and 19, 1995, several of the observations and test results are worth noting:



Tennessee Valley Authority Fossil Fuels Group 1101 Market Street Chattanooga, Tennessee 37402-2801

Subject:

FINAL REPORT

Fly Ash, Bottom Ash and Scrubber Gypsum Study Contract No. TV-92657V, Phase 1 Law Engineering - Knoxville Project No. 50385-5-0400 (Phase 1) Law Engineering - Atlanta Project No. 5810860101

Dear Sir/Madam:

Law Engineering has completed the testing program outlined in the Scope of Work - Phase 1 of Contract TV-92657V. This letter provides a brief background of the test program. In addition, a descriptive summary of the test procedures used is presented. The summary provides discussion pertaining to clarifications or deviations from the procedures. Finally, general observations made while preparing samples or performing tests that are not represented on the test reports are discussed, and the results of the test program are presented.

BACKGROUND

The purpose of this laboratory testing program was to provide classification and engineering properties characterization of several of the Tennessee Valley Authority's (TVA) sources of fly ash, bottom ash, boiler slag and scrubber gypsum. Twenty-nine materials from eleven coal burning power generation steam plants were included in this study. The materials received were tested through a broad range of test procedures outlined by the American Society for Testing and Materials (ASTM), the American Association of State Highway and Transportation Officials (AASHTO), the Strategic Highway Research Program (SHRP), and Law Engineering. Each test in the program was chosen to illustrate the engineering properties of each material to determine their suitability for structural embankment fill in highway construction.

In all, thirteen sources of fly ash, nine sources of bottom ash, two sources of boiler slag and three sources of scrubber gypsum (FGD - flue gas desulfurization) were received for testing. In addition, a Spent Bed Material and Char material were received from the single unit atmospheric fluidized bed boiler at Shawnee. Each source material was provided to us in six 5-gallon plastic buckets, labeled A through F.

LAW ENGINEERING, INC.

396 PLASTERS AVENUE, N.E. • ATLANTA, GA 30324 (404) 873-4761 • FAX (404) 881-0508

November 7, 1995

Soils Classification System (USCS) symbol are provided based on the Particle-Size Analysis and Atterberg Limits results. Similarly, an AASHTO classification is provided based on guidelines set forth in *The Classification of Soils and Soil-Aggregate Mixtures for Highway Construction Purposes, AASHTO M145.*

Volumetric Testing

Several tests were performed to provide the general volumetric properties of each material. The tests outlined below were performed on one composite sample from each of the twenty-seven fly ash, bottom ash, boiler slag and scrubber gypsum sources.

Test Method for Laboratory Compaction Characteristics of Soil Using Standard Effort (12,400 $ft-lbf/ft^3$) (600 kN-m/m³), ASTM D 698. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Standard Proctor.

Test Method for Laboratory Compaction Characteristics of Soil Using Modified Effort (56,000 ft- lbf/ft^3) (2,700 kN-m/m³), ASTM D 1557. This method defines the moisture content versus dry density relationship of the material using the standard specified level of energy. The method is commonly referred to as the Modified Proctor.

Test Method for Maximum Index Density and Unit Weight of Soils Using a Vibratory Table. ASTM D 4253 and Test Method for Minimum Index Density and Unit Weight of Soils and Calculation of Relative Density, ASTM D 4254. Because the Standard and Modified Proctors do not necessarily define a good relationship between dry density and moisture content (typically because of the free draining nature of granular materials), the minimum and maximum index densities were determined for the nine bottom ash samples.

Test Method for One-Dimensional Consolidation Properties of Soils, ASTM D 2435. Samples of the fly ash, boiler slag and scrubber gypsum were remolded in nominal 2.5-inch diameter by 1.0-inch high rings to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor. Nominal load increments of 0.5, 1.0, 2.0, 4.0, 8.0 and 16.0 ksf were applied. Moist porous stones were used; however, samples were not inundated for the test.

Hydraulic Conductivity and Static Strength Testing

Test Method for Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter, ASTM D 5084. The fly ash, boiler slag and scrubber gypsum materials were remolded to approximately 95 percent of the maximum dry density at the optimum moisture content as determined by the Standard Proctor and tested for hydraulic conductivity. An effective confining pressure of 14 psi was used as the standard for all tests. The samples were remolded to a nominal 2.88-inch diameter by 6.0-in high specimen.

Electro-Chemical Testing

Determining the Minimum Laboratory Soil Resistivity, AASHTO T 288. A supersaturated slurry was prepared for each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) and the minimum resistivity value was measured.

Determining pH of Soil for Use in Corrosion Testing, AASHTO T 289. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the pH value was measured.

Determining Water Soluble Sulfate Ion Content in Soil, AASHTO T 290. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble sulfate ion content was measured using the Turbidimetric Method (Method B).

Determining Water Soluble Chloride Ion Content in Soil, AASHTO T 291. Each of the fly ash, bottom ash, boiler slag and gypsum/spent bed/char materials (fraction passing the #10 sieve) was prepared and the water soluble chloride ion content was measured using the pH/mV Meter Method (Method B).

PECULIARITIES AND TEST RESULTS

Based on our years of experience with the testing of geotechnical materials and our experience derived from this test program, we have highlighted some instances in which these materials behaved differently than others, either visually or by test results that varied significantly from results calculated for similar materials.

- Both the spent bed material (Shawnee) and the char (Shawnee) were observed to react upon treatment with water. This phenomenon created complications with all the geotechnical tests (classification, volumetric, and strength test). Only the electro-chemical tests were performed on these materials. Because of the highly reactive nature of the spent bed material, the resistivity test was unable to be performed.
- The scrubber gypsum materials were observed to react upon treatment with water following the air dry preparation of these materials. The samples were air-dried overnight in a temperature controlled room set at 140 °F. This phenomenon created complications with the successful completion of the classification tests, although we were able to perform a specific gravity test on a composite sample of each source. We note that the scrubber gypsum materials exhibit relatively more strength than the other materials tested in this program when tested under dynamic conditions at low applied strains (Resilient Modulus). This may indicate that a weak chemical bond is created between particles.

• Beside the noticeable color difference of the Cumberland Dry Fly Ash (tan/brown as opposed to gray for all other fly ashes in this program) that was sampled from Units 1 and 2 on April 17, 18 and 19, 1995, several of the observations and test results are worth noting:

LAW

Technical Procedures for Tennessee Valley Authortiy

TITLE: DETERMINING THE ANGLE OF REPOSE OF NON-COHESIVE GRANULAR SAMPLES

These procedures meet the Quality Assurance Program requirements for this project. LAW's Quality Assurance Program Description and all of its invoked documents govern the preparation, approval, and use of these procedures.

Copy Number _____

PREPARED BY:

Auburd P. Boudrown

Richard L. Boudreau, P.E.

APPROVALS:

James W. Niehoff,

Chief Engineer

9/11/95 Date

9/19/95

Date

Date

Date

Procedure: TP6-TVA Page 1 of 4

Revision 0 August 28, 1995

lab\forms\tp6-tva.doc

TP - 6: DETERMINING THE ANGLE OF REPOSE OF NON-COHESIVE GRANULAR SAMPLES

3.1.6 Calculate the angle of repose, using the average of the 2 measurements taken, using the following equations:

 $\phi_1 = \operatorname{Tan}^{-1} [(V_1 - V_0)/H_1]$ $\phi_2 = \operatorname{Tan}^{-1} [(V_2 - V_1)/(H_2 - H_1)]$

 $\phi_{\rm avg} = (\phi_1 + \phi_2)/2$

where: $H_{1,2}$ = Horizontal distance from mound peak along horizontal plane, inches

 $V_{0,1,2}$ = Vertical distance from horizontal offset along horizontal plane to the surface of the mound, inches

4.0 REPORTING

- 4.1 The following information shall be reported:
 - Sample I.D.
 - Visual description
 - Average angle of repose value

Revision 0 August 28, 1995 Procedure: TP6-TVA Page 3 of 4

11/4 - Fly Ash, Bottom Ash and Scrubber Sludge Sludy Classification (Index Property) Summary Law Engineering Project Na, 5810860101

					Moisture	Grs	Grain Size • ASTM D422	H22	Atterber	Atterberg Limits ASTMI D4318	11 D4318	Specific	USCS	ASHTO
Source	Code	Material	Bucket Code	Date Collected	Content, %	%Ret. on No. 4	%Pass No. 200	%Pass 0.005mm	11	ЪГ	Ы	Gravity	Classification	Classification
Allen	ALF	Boiler Slag - Fine Reed Rejects	A-B	\$6/11/5	0.06	0.0	18.2	0.8	ЯГ	dN	N/N	2.75	SM	A-2-4(0.0)
			C-D		0.12	0.0	14.6	0.8	۶ſ	٩Ż	N/A	2.79	SM	A-2-4(0.0)
			<u>е</u> -е		0.10	0.0	16.0	0.8	NL	ŝ	N'A	2.81	SNI	A-2-4(0.0)
Buil Run	BRF	Drv Fly Ash	A-B	4/4/95	0.02	0.0	91.2	16.6	NL	ŝ	N/A	2.36	ML	A-4(0.0)
			C-D	4/5/95	0.05	0.0	91.2	19.5	NL	άŻ	N/A	2.28	ML	A-4(0.0)
			E-F	4/6/95	0.03	0.0	90.7	17.5	NL	dΝ	N/N	2.37	NIL	A-4(0.0)
		Bottom Ash - From Pond	A-B	3/29/95	6.99	23.0	4.0		JI,	٩Z	N/A	2.31	SW	A-1-b
			C-D	1	6.07	21.3	6.9		NL	ďV	N/A	2.29	MS-WS	A-1-b
			E-F		6.74	17.9	5.9		ЯГ	ď	N/A	2.35	SW-SM	A-1-b
Colbert	COF	Dry Fly Ash - Units 1&2	<	5/25/95										-
		- Units 3&4	8	\$/25/95	0.01	0.0	81.6	14.9	ŊĘ	dN	N/A	2.02	ML	A-4(0.0)
		- Units 1&2	Ċ	5/26/95										
		- Units 3&4	D	5/26/95	0.01	0.0	6.69	11.5	N	٩X	N/A	2.00	ML	A-4(0.0)
		- Units L&2	ш	5/30/95		ć	Š	v .	;	5		20.		10 07 1
		- Units 364	-	26/00/2	21.0	0.0	0.00	6.0	ž		VA.	21.0	ML	A-4(0.0)
		Bottom ASA - From Pond	4-V	66/07/0	20.0	7./	0.01			UN NI	V/N	00 C	INC INC	A-1-0
				,	107	12.2	10.5		Z	av	V/N	2 10	INS-10	A-1-6
					47.1	0.44						21-2	5	
Cumberland	CUF	Dry Fly Ash	A-B	4/17/95	0.31	0.0	95,1	30.0	JZ	dz	N/A	2.57	ML	A-4(0.0)
		- Units 1&2	C-D	4/18/95		0.0	92.0	20.7	NL	ďZ	N/A	2.64	ML	A-4(0.0)
		- Units 1&2	E-F	4/19/95	0.01	0.0	93.2	29.8	N	đ	N/A	2.65	ML	A-4(0.0)
		Bottom Ash - From Pond	A-B	4/6/95	14.32	30.9	1.1	*	NL	ď	N/A	2.59	SW	A-I-a
			C-D		13.66	46.2	2.2		NL	dX	V/N	2.66	SW	A-1-a
			н-н Н		5.08	32.2	2.8		NL	ďŻ	N/A	2.63	SW	A-I-a
		Scrubber Gypsum	A-B	4/6/95	30.44	••••			٦٢	ΔN	N/A	••••		****
			C-D		30.39				NL	٩N	N/A	3.41	,	
			Е-F		29.41			:	NL	đ	N/A		1	-
Gallatin	GAF	Drv Fly Ash - Unit 2 Hoppers	A-B	6/9/95	0.03	0.0	94.2	12.0	M	å	N/A	2.37	NL	A-4(0.0)
			C-D		0.01	0.0	95.2	13.8	Лſ	ďŇ	N/A	2.40	ML	A-4(0.0)
			E-F		0.01	0.0	95.5	14.8	N	dZ	N/A	2.39	ML	A-4(0.0)
		Bettom Ash - From Pond	A-B	6/9/95	19.11	18.2	5.9	****	NL	٩N	N/A	2.56	SP-SNI	A-1-b
			C-D		7.32	27.0	4.0		NL	ďŻ	N/A	2.57	SW	A-1-b
			E-F		10.20	18.8	5.6		NL	dN	N/A	2.52	SW-SM	A-I-b
John Sevier	JSL	Dry Fly Ash - Unit 4, Hoppers 11&12	ĸ	\$/25/95					;				:	
		- Unit 3, Hoppers 11&12	8		0.06	0.0	94.2	17.4	NL	dz	N/A	2.27	ML	A-4(0.0)
		- Unit 4, Hoppers 9, 10&13 - Unit 3, Hoppers 9&10	υŌ	5/25/95	0.0	0.0	96.1	22.1	NL	đX	Y/N	2.35	ML	A-4(0.0)
		Unit 4, Hopper 15,	E	5/25/95										
		- Unit 3, Hopper 16	<u>.</u>		0.20	0.0	94.1	28.0	ΊN	ź	N N	2.43	NIL	A-4(0.0)
		Bottom Ash - From Pond	A-B	4/12/95	26.68	22.8	6,4		NI.	Ż	N N	2.25	SP	A-1-a
			0-D		27.22	22.2	3.3		Z	âŻ	V-N	2 24	SW	A-1-a
			E-F		30.70	27.8	3.7		N.	άŻ	N.A	2.22	ŚW	в-1-А

TVA-00012400

117A - Fiy Ash, Batam Ash and Scrubber Sludge Sludy Classification (Indes Property) Summary Law Engineering Project No. 8810860101

Number Control Control <th< th=""><th></th><th></th><th></th><th></th><th></th><th>Moisture</th><th>ō</th><th>rain Size - ASTM I</th><th>D422</th><th>Atterber</th><th>g Limits AST</th><th>VE D4318</th><th>_</th><th>USCS</th><th>AASHTO</th></th<>						Moisture	ō	rain Size - ASTM I	D422	Atterber	g Limits AST	VE D4318	_	USCS	AASHTO
Int Out Made (y, xh) (wor) bacy (xcl), Fr Made Made (y, xh) (wor) bacy (xcl), Fr Made	Source	Code	Material	Bucket Code	Date Collected	Content, %	%Ret. on No. 4	%, Pass No. 200	%Pass 0.005mm	FT -	ЪГ	Ы	Gravity	Classification	Classification
Ander by Ant, An (Add Frieder(ed) Col No	Johnsonville	JOF	Ponded Fly Ash (New Dredge Cell)	Λ-Β	6/7/95	28.82	3.2	47.1	2.4	NL	NP	N/A	2.36	SM	A-4(0.0)
And Mudd by, wh (hold bedge(c1)) EF 07/3 1310 13 93 93 94				C-D		39.10	0.0	54.4	4.2	NL	dN	N/A	2.56	NL	A-4(0.0)
Inductify Ant Out Reduct ANTONIN CP3 U201				Ę.F		31.07	1.8	59.2	3.5	٦٢	ď	N/A	2.31	NL	A-4(0.0)
CF CF<			Ponded Fly Ash (Old Dredge Cell)	A-B	6:7:95	13.61	3.6	33.6	0.0	NF	٨p	N/N	2.41	SM	A-2-4(0.0)
Tound Fy, Anh Levin An Theory Exp Orang 201 101 101 101 NM 201 NM 201 Read Fy, Anh Levin An Theorem C.D 2010 1012 201 101 NM NM NM 201 Read Fy, Anh Levin And Theorem C.D 2011 201 101 201 NM NM NM NM NM 201 201 Read Fy, Anh Cotal 11 C.D 201 202 203 203 201 NM NM NM NM NM 201				C-D		10.98	8.7	42.2	4,1	NL	٩N	N/A	2.43	SM	A-2-4(0.0)
Flowed fb, An I, Adir, And Motic, And Tandy Case 3307 3307 900 930 110 N N N N N N N N 239 Read (I), An I, Adir, Fam Thai 60 923 923 930 <t< td=""><td></td><th></th><td></td><th>Ч</th><td></td><td>15.11</td><td>2.5</td><td>41.4</td><td>2.1</td><td>ЯĽ</td><td>đZ</td><td>N/A</td><td>2.23</td><td>SN</td><td>A-4(0.0)</td></t<>				Ч		15.11	2.5	41.4	2.1	ЯĽ	đZ	N/A	2.23	SN	A-4(0.0)
C0 312 00 913 114 NL			Ponded Fly Ash (Active Ash Pond)	A-B	6/1/95	28.09	0.0	95.0	15.6	NL	đz	N/A	2.48	NL	A-4(0.0)
Index (A) Index (A) <t< td=""><td></td><th></th><td></td><th>C-D</th><td></td><td>31.07</td><td>0.0</td><td>94.8</td><td>14.8</td><td>ž</td><td>ź</td><td>N/A</td><td>2.48</td><td>ML</td><td>A-4(0.0)</td></t<>				C-D		31.07	0.0	94.8	14.8	ž	ź	N/A	2.48	ML	A-4(0.0)
Memoritati renarioat CD 10.2 20.0 60.0 10.2 20.0 60.0 <td></td> <th></th> <td></td> <th>- E</th> <td></td> <td>32.70</td> <td>0.0</td> <td>93.9</td> <td>16.8</td> <td>z;</td> <td>dz ;</td> <td>N/A</td> <td>2.50</td> <td>ML</td> <td>A-4(0.0)</td>				- E		32.70	0.0	93.9	16.8	z;	dz ;	N/A	2.50	ML	A-4(0.0)
Nf Imade (F) Add (Cal (1)) CD 11/1 21/2 0.00			Bottom Ash - From Pond	A-B	6/1/95	13.28	15.6	26.3		JZ :	ź	N/A	2.39	SM	A-1-b
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				C-D		11.92	23.0	16.8		Z Z	dz dz	N/A N/A	2.39	SM	A-1-b
Nft Twoold fly, Ani (cit1) Cut1 203 223 00 951 112 Ni							0.77			-			<u>, , , , , , , , , , , , , , , , , , , </u>	MC	
Ford CP 393 C0 971 NI NI NI NI NI 201 Pondsthy AntCal III) CP 30.93 90.91 91.01 NI	Kingston	KIF	Ponded Fly Ash (Cell 1)	A-B	5/3/95	28.28	0.0	86.4	13.6	NL	ŊŊ	N/A	2.28	ML	A-4(0.0)
Funded Fly, Ahr (Call 11) EF 939 949 731 NN NN NN 231 Model Fly, Ahr (Call 11) CO 939 939 939 939 939 939 939 939 939 931				C-D	,	33.95	0.0	1.79	13.2	۶ľ	đz	N/A	2.31	ML	A-4(0.0)
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				EF		30.95	0.0	94.0	13.1	ŊĘ	ą	N/A	2.30	ML	A-4(0.0)
$ \ \ \ \ \ \ \ \ \ \ \ \ \ $			Ponded Fly Ash (Cell 111)	A-B	5/3/95	36.09	0.0	96.5	22.6	NL	ЧN	N/A	2.31	ML	A-4(0.0)
$ \ \ \ \ \ \ \ \ \ \ \ \ \ $,	C-D			0.0	98.3	25.0	NL	NP	N/A	2.29	ML	A-4(0.0)
$ \left $				E-F		36.19	0.0	96.1	18.4	ß	dz	N/A	2.34	ML	A-4(0.0)
$ \left \mbox{ red} $			Bettom Ash - From Pond	A-B	5/3/95	9.62	21.9	9.7		N	٨P	N/N	2.37	SW-SM	A-1-b
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				C-D		10.01	19.3	10.7	:	Z	ďz	N/A	2.34	SP-SM	A-1-b
$ \left. \begin{array}{cccccccccccccccccccccccccccccccccccc$				EF		17.15	18.4	11.3	1	ž	đ	N/A	2.33	SP-SM	A-I-b
	Paradise	PAF	Ponded Fly Ash (East Cell)	A-B	56/11/95		0.0	99.4	20.9	NL	ΝP	N/A	2.82	ML	A-4(0.0)
$ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$				C-D			0.0	98.1	11.4	βĽ	dN	N/A	2.77	ML	A-4(0.0)
$ \left \begin{array}{cccccccccccccccccccccccccccccccccccc$				E-F			0.0	98.5	18.7	ŊĹ	٩N	N/A	2.93	ML	A-4(0.0)
$ \ \ \ \ \ \ \ \ \ \ \ \ \ $			Boiler Slag (Reed Rejects)	A-B	56/8t/S		0.0	5.8	0.0	NL	NP	N/A	2.78	SP-SM	A-1-b
$ \ \ \ \ \ \ \ \ \ \ \ \ \ $				СĐ			0.0	12.5	0.0	M	NP	N/A	2.84	SM	A-2-4(0.0)
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				ш		1	1.0	10.2	0.0	NL	dN	N/A	2.73	SW-SM	A-1-b
			Scrubber Gypsum	A-B	5/17/95	****				NL	NP	N/A			
				C-D						۶Ľ	dN	N/A	3.00		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				в			-			NL	ЧN	N/A	1		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Shawnee	SHF		A-B	4/6/95	0.14	0.0	91.6	7.6	N	٩N	N/A	2.14	ML	A-4(0.0)
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		5		C-D	4/7/95	0.13	0.0	91.2	6.4	, NL	NP	N/A	2.09	ML	A-4(0.0)
				É-F	4/10/95	0.16	0.0	90.1	7.5	NL	ŊŊ	N/A	2.11	NIL	A-4(0.0)
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			Bottom Ash - From Pond	A-B	4/5/95	23.64	20.0	11.2		NL	ЧN	N/A	2.14	SP-SM	A-1-b
$ \begin{array}{l l l l l l l l l l l l l l l l l l l $		_		C-D		23.83	14.7	9.1		NL	٩N	N/A	2.14	SP-SM	A-1-b
				E-F		21.11	18.3	9.3		NL	NP	N/A	2.09	SP-SM	A-1-b
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			Spent Bed Material (SBM)	A-B	4,6,95	000				NL	٩N	N/A	2.93		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				c.D	4/7/95	00.0		**-*		NL	٩N	N/A	2.86		****
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				E-F	4:10:95	0.00	;			NL	Ż	N/A	2.92		•
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			Char	A-B	4/6/95	0.00				NL	z	V/N	3.00		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				3	4/7/4	000	•••			R	Ż	N/N	2.99		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					C6.01/F	0.00	1			NL	ž	N/A	00.0		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Widows Creek	WCF	-	A-B	4/28/95	42.20	0.0	84.5	6.7	NL	٩N	N/A	2.38	NL	A-4(0.0)
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				C-D		75.19	1.5	84.6	8.2	NL	aN	N'A	2.40	ML	A-4(0.0)
Studber Gpsum A.B 4.28.95 ML NP NA C-D ML NP NA NA E-F NL NP NA 3.01 Batom Ash - From Pould A.B 4.28 3.37 4.8 NL NP NA 2.01 C-D A.B 3.37 4.8 NL NP NA 2.01 C-D 2.36 2.99 4.1 NL NP NA 2.01 E-F 4.03 4.09 4.5 NL NP NA 2.60				E-F		63.46	0.0	92.9	3.6	NL	ż	N/A	2.22	NIL	A-4(0.0)
C-D ML NP MA 3.01 Bstom Ash - From Pond A-B 128-95 4.25 33.7 48 NL NP NA 3.01 Bstom Ash - From Pond A-B 128-95 4.25 33.7 48 NL NP NA 2.01 C-D C-D 23.9 4.1 NL NP NA 2.61 E-F 4.03 40.9 4.5 NL NP NA 2.67			Scrubber Gypsum	A-B	4/28-95	•••				NL	đN	N/A			
Battom Ash From Pould E-F N-1 N-1 N-1 N-1 N-2 N-1				0-2-						R	dN	N/A	3.01		
Battom Ash From Pond A-B 4.28-95 4.25 3.37 4.8 NL NP NA 2.74 C-D C-D 2.36 29.9 4.1 NL NP NA 2.06 E-F 4.03 40.9 4.5 NL NP NA 2.60			1							II :	ż :	N/A			
C-D 2.30 29.9 4.1 NL NP NA 2.00 E-F 4.03 40.9 4.5 NL NP NA 2.67			Bottom Ash · From Pond	A-B	4/28/95	4.25	33.7	4.8		N,	e s	N/A	2.74	SW .	A-1-a
E-F 403 409 45 1 1 NL 1 NP 1 267 1						2.36	29.9	4.1		NL	AN 9	N/A	097	SW	A-1-a
				E-F		4.03	40.9	4.5		NL	Ń	A/A	2.67	SW	A-1-a

Т

TVA - Fly Ash, Bottom Ash and Scrubber Sludge Study Volumetric Testing Summary Law Engineering Project No. 5810860101

			Standard Proctor	Proctor	Modified Proctor	Proctor	Relative Densit	Relative Density, Dry Method (pcf)
Source	Code	Material	Max. Drv Dens. (ncf)	Ont. Moisture (%)	Max. Drv Dens. (nef)	Out. Maisture (%)	Minimum	Maximum
Allen	A1 F	Boiler Slan (Fine Reed Rejects)	05.3	516	100 6	ς ες		
INIT	70	DUIN DIAS (1 1110 NOVA IN DOUD)	C.C/	C:17	10.201	7.67		
Bull Run	BRF	Dry Fly Ash	91.6	17.4	95.7	15.1		
		Bottom Ash - From Pond	91.9	22.6	98.7	18.5	73.9	92.1
Colbert	COF	Dry Fly Ash (Units 1-4)	56.7	45.4	62.9	40.3		-
		Bottom Ash - From Pond	64.2	27.4	73.2	17.2	55.7	71.2
Cumberland	CUF	Dry Fly Ash (Units 1-2)	111.4	13.2	116.3	11.5		
		Bottom Ash - From Pond	90.1	15.4	103.3	15.7	67.0	87.1
		Scrubber Gypsum	77.6	40.6	85.9	29.7		
Gallatin	GAF	Dry Fly Ash (Unit 2 Hoppers)	86.6	21.4	88.9	18.8	1	•
		Bottom Ash - From Pond	92.0	25.5	102.5	20.9	71.3	6.7
John Sevier	JSF	Dry Fly Ash (Units 3-4)	83.7	18.6	86.7	17.8		
		Bottom Ash - From Pond	78.9	30.3	96.2	21.9	55.7	73.9
Johnsonville	JOF	Ponded Fly Ash (New Dredge Cell)	75.8	31.4	92.5	20.6		l
		Ponded Fly Ash (Old Dredge Cell)	89.5	20.5	96.0	16.1		
		Ponded Fly Ash (Active Ash Pond)	86.6	22.8	91.7	18.0		
		Bottom Ash - From Pond	99.2	18.0	104.1	12.0	80.2	99.2
Kingston	KIF	Ponded Fly Ash (Cell I)	81.0	25.2	84.7	24.1	-	1
		Ponded Fly Ash (Cell III)	81.0	23.5	84.4	23.7		
		Bottom Ash - From Pond	89.0	24.1	97.6	21.0	71.0	88.4
Paradise	PAF	Ponded Fly Ash (East Cell)	110.0	16.5	114.4	13.7		
		Boiler Slag (Reed Rejects)	112.5	18.2	116.0	18.7		
		Scrubber Gypsum	85.7	31.7	87.4	30.8		
Shawnee	SHF	Dry Fly Ash	72.4	28.3	77.2	24.4	-	-
		Bottom Ash - From Pond	71.7	30.5	81.4	26.1	57.4	74.0
		Spent Bed Material (SBM)	1					
		Char						
Widows Creek	WCF	Ponded Fly Ash (Ash Pond)	67.0	39.8	73.5	27.8		
		Scrubber Gypsum	92.0	23.1	6.99	19.4		
		Bottom Ash - From Pond	106.2	17.6	120.8	15.8	83.0	103.3

lab' soil wa'prgrm.xls (Proctor)

TVA - Fly Ash, Bottom Ash and Scrubber Sludge Study	Consolidation/Hydraulic Conductivity/Chemical Testing Summary	Law Engineering Project No. 5810860101
---	---	--

					THE ALL COMPLECTION AND A	
ALFBolten Sing (Fine Reed Rejects)004tinBRF $Dy Fly Ash$ 0.04Bottom Ash - From Pond0.04LtCvF $Dy Fly Ash (Units 1-4)$ 0.08Bottom Ash - From Pond0.01Bottom Ash - From Pond0.05ServierJSFDry Fly Ash (Unit 3.4)0.05JSFDry Fly Ash (Unit 3.4)0.05ServierJSFDry Fly Ash (Ond Dredge Cell)0.01OnvilleJOFPonded Fly Ash (Coll Dredge Cell)0.01Donded Fly Ash (Coll Dredge Cell)0.010.01ItomKIFPonded Fly Ash (Cell 11)0.05ItomKIFPonded Fly Ash (Cell 11)0.05ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13ItomStrubber Gypsum0.13Itom </th <th>Compression index, C.</th> <th>(cm/sec)</th> <th>(Ohm-cm)</th> <th></th> <th>(mg/kg)</th> <th>(mg/kg)</th>	Compression index, C.	(cm/sec)	(Ohm-cm)		(mg/kg)	(mg/kg)
BRF Dyr Fly Ash 0.04 BOItom Ash - From Pond COF Dyr Fly Ash (Units 1-4) 0.08 Bottom Ash - From Pond Bottom Ash - From Pond CUF Dyr Fly Ash (Units 1-2) 0.01 Bottom Ash - From Pond 0.12 CUF Dyr Fly Ash (Units 1-2) 0.01 Bottom Ash - From Pond Scrubber Gypsum 0.12 0.05 Bottom Ash - From Pond JSF Dyr Fly Ash (Unit 3-4) 0.05 Bottom Ash - From Pond JOF Ponded Fly Ash (Coll Dredge Cell) 0.06 Ponded Fly Ash (Coll Dredge Cell) 0.06 JOF Ponded Fly Ash (Cell I) 0.05 Rtl: Ponded Fly Ash (Cell I) 0.05 Ponded Fly Ash (Cell I) 0.05 Rtl: Ponded Fly Ash (Cell I) 0.11 Ponded Fly Ash (Cell I) 0.05 Rtl: Ponded Fly Ash (Cell I) 0.05 Ponded Fly Ash (Cell I) 0.13 Rtl: Ponded Fly Ash (Cell I) 0.05 Ponded Fly Ash (Cell I) 0.05 Bo	0.04	9.0E-4	30000	7.5	43	<10
Bottom Ash - From PondCOF $Dyr Fly Ash (Units 1-4)$ 0.08Bottom Ash - From PondBottom Ash - From PondCUF $Dyr Fly Ash (Units 1-2)$ 0.01Bottom Ash - From PondSeubber Gypsum0.12CMF $Dyr Fly Ash (Units 1-2)$ 0.05Bottom Ash - From PondJSF $Dyr Fly Ash (Unit 2 Hoppers)$ 0.05Bottom Ash - From PondJOFPonded Fly Ash (Units 3-4)Ponded Fly Ash (Units 3-4)0.05Ponded Fly Ash (Units 3-4)Ponded Fly Ash (Cell 1)0.06Ponded Fly Ash (Cell 1)0.05Ponded Fly Ash (Cell 1)Ponded Fly Ash (Cell 1)0.05Ponded Fly Ash (Cell 1)0.05<	0.04	4.0E-5	690	8.4	4630	<10
COF Dry Fly Ash (Units 1-4) 0.08 Bottom Ash - Froin Pond CUF Dry Fly Ash (Units 1-2) 0.01 Bottom Ash - Froin Pond Bottom Ash - Froin Pond Bottom Ash - Froin Pond Bottom Ash - Froin Pond 0.12 Scrubber Gypsum 0.05 Bottom Ash - Froin Pond JSF Dry Fly Ash (Unit 2 Hoppers) 0.05 Bottom Ash - Froin Pond 0.05 JSF Dry Fly Ash (Unit 2 4-4) 0.05 Ponded Fly Ash (Old Dredge Cell) 0.10 0.06 Ponded Fly Ash (Cell 1) 0.10 0.10 Ponded Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond RIF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond Bottom Ash - From Pond RIF Ponded Fly Ash (Cell 11) 0.05 Ponded Fly Ash (Cell 11) 0.05 Bottom Ash - From Pond Scrubber Gypsum 0.13 Scrubber Gypsum 0.13 <		1.8E-2	7300	7.2	370	<10
KIF Bottom Ash - From Pond CUF Dry Fly Ash (Units 1-2) 0.01 Bottom Ash - From Pond Serubber Gypsum 0.12 GAF Dry Fly Ash (Units 1-1) Bottom Ash - From Pond JSF Dry Fly Ash (Units 3.4) 0.05 Bottom Ash - From Pond 0.05 JSF Dry Fly Ash (Units 3.4) 0.05 Jor Ponded Fly Ash (New Dredge Cell) 0.06 JOF Ponded Fly Ash (Old Dredge Cell) 0.10 Ponded Fly Ash (Cell 1) 0.10 0.11 Ponded Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond RtF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond RtF Ponded Fly Ash (Cell 1) 0.05 Partod Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond Scubber Gypsum 0.13 Stiff Dyf Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond Scubber	0.08	2.8E-4	850	9.4	1660	<10
CUF Dry Fly Ash (Units 1-2) 0.01 Bottom Ash - From Pond Serubber Gypsum 0.12 GAF Dry Fly Ash (Units 3-4) 0.05 Bottom Ash - From Pond 0.05 JSF Dry Fly Ash (Units 3-4) 0.05 Bottom Ash - From Pond 0.05 JOF Ponded Fly Ash (Units 3-4) 0.05 Ponded Fly Ash (Units 3-4) 0.06 JOF Ponded Fly Ash (Old Dredge Cell) 0.10 Ponded Fly Ash (Cell 1) 0.06 RIF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond RIF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond Strubber Gypsum 0.13 Strubber Gypsum 0.13 Strubber Gypsum 0.13 Strubber Gypsum Strubber Gypsum Strubber Gypsum Strubber Gypsum Strubber Gypsu		1.6E-2	4500	5.4	215	<10
Bottom Ash - From Pond Scrubber Gypsum 0.12 GAF Dry Fly Ash (Unit 2 Hoppers) 0.05 Bottom Ash - From Pond JOF Dry Fly Ash (Unit 3.4) 0.05 Bottom Ash - From Pond JOF Ponded Fly Ash (Unit 3.4) 0.06 Ponded Fly Ash (Old Dredge Cell) 0.06 Ponded Fly Ash (Old Dredge Cell) 0.10 RIF Ponded Fly Ash (Cell 11) 0.10 RIF Ponded Fly Ash (Cell 11) 0.05 RIF Ponded Fly Ash (Cell 11) 0.05 RIF Ponded Fly Ash (Cell 11) 0.05 PAF Ponded Fly Ash (East Cell) 0.05 Ponded Fly Ash (East Cell) 0.05 Ponded Fly Ash (East Cell) 0.05 Ponded Fly Ash (East Cell) 0.05 Ponded Fly Ash (East Cell) 0.05 Ponded Fly Ash (East Cell) Boitom Ash - From Pond Stubber Gypsum 0.13 Shift D	0.01	2.2E-5	2600	11.6	5020	<10 <
Art Scrubber Gypsum 0.12 GAF Dry Fly Ash (Unit 2 Hoppers) 0.05 Bottom Ash - From Pond JOF Dry Fly Ash (Units 3-4) 0.05 Bottom Ash - From Pond JOF Ponded Fly Ash (Units 3-4) 0.06 Ponded Fly Ash (New Dredge Cell) 0.06 JOF Ponded Fly Ash (New Dredge Cell) 0.10 Ponded Fly Ash (Active Ash Pond) 0.11 0.10 RIF Ponded Fly Ash (Cell 11) 0.05 RIF Ponded Fly Ash (Cell 11) 0.05 Ponded Fly Ash (Cell 11) 0.05 RIF Ponded Fly Ash (East Cell) 0.01 Ponded Fly Ash (East Cell) 0.05 Rottom Ash - From Pond Ponded Fly Ash (East Cell) 0.05 Ponded Fly Ash (East Cell) 0.01 Ponded Fly Ash (East Cell) Boitom Ash - From Pond Ponded Fly Ash (East Cell) Setubber Gypsum 0.13 Shift Dry Fly Ash Boitom Ash - From Pond Shift Dry Fly Ash (Ash Pond) </td <td></td> <td>6.8E-2</td> <td>1200</td> <td>2.7</td> <td>4790</td> <td><10</td>		6.8E-2	1200	2.7	4790	<10
GAF Dry Fly Ash (Unit 2 Hoppers) 0.05 Bottom Ash - From Poud JSF Dry Fly Ash (Unit 3.4) 0.05 Bottom Ash - From Poud 0.05 Bottom Ash - From Poud 0.06 JOF Ponded Fly Ash (Units 3.4) 0.06 Ponded Fly Ash (Old Dredge Cell) 0.10 0.10 Ponded Fly Ash (Old Dredge Cell) 0.10 0.11 Bottom Ash - From Poud RIF Ponded Fly Ash (Cell 11) 0.10 Ponded Fly Ash (Cell 11) 0.05 RIF Ponded Fly Ash (Cell 11) 0.05 Ponded Fly Ash (Cell 11) 0.05 RIF Ponded Fly Ash (Cell 11) 0.05 Ponded Fly Ash (Cell 11) 0.05 Rottom Ash - From Pond PAF Ponded Fly Ash (East Cell) 0.04 PAF Ponded Fly Ash (East Cell) PAF Ponded Fly Ash (East Cell) 0.05 Portom Ash - From Pond Ponded Fly Ash (East Cell) 0.13 Ponded Fly Ash (East Cell) <t< td=""><td>0.12</td><td>1.2E-3</td><td>0011</td><td>7.8</td><td>4830</td><td>01></td></t<>	0.12	1.2E-3	0011	7.8	4830	01>
ISF Bottom Ash - From Pond JSF Dry Fly Ash (Units 3-4) 0.05 Bottom Ash - From Pond JOF Ponded Fly Ash (New Dredge Cell) 0.10 Ponded Fly Ash (Old Dredge Cell) 0.10 Ponded Fly Ash (Active Ash Pond) 0.11 Bottom Ash - From Pond KIF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 RIF Ponded Fly Ash (Cell 1) 0.05 Ruther Erom Pond Bottom Ash - From Pond Ruther Grysum 0.13 Strubber Gysum Strubber Gysum 0.13 Strubber Gysum Strubber Gysum Strubber Gysum Strubber Gysum Strubber Gyby Ash (Ash Pond)	0.05	7.7E-5	420	10.6	5800	<10
JSF Dry Fly Ash (Units 3.4) 0.05 Bottom Ash - From Pond JOF Ponded Fly Ash (New Dredge Cell) 0.06 Ponded Fly Ash (Old Dredge Cell) 0.10 Ponded Fly Ash (Old Dredge Cell) 0.11 Rottom Ash - From Pond RIF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.06 Ponded Fly Ash (Cell 1) 0.05 RIF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1) 0.05 Rottom Ash - From Pond Bottom Ash - From Pond Bottom Ash - From Pond Bottom Ash - From Pond Draft Fly Ash (Edel Rejects) Serubber Gypsum 0.13 Strubbert Gypsum 0.13 MCF Donded Fly Ash (Ash Pond) Att Ponded Fly Ash (Ash Pond)	9 * * * * *	2.9E-2	1600	2.8	0991	01>
A bottom Ash - From Pond JOF Ponded Fly Ash (New Dredge Cell) 0.06 Ponded Fly Ash (Old Dredge Cell) 0.10 Ponded Fly Ash (Active Ash Pond) 0.11 Rottom Ash - From Pond 0.11 Rottom Ash - From Pond 0.11 Rottom Ash - From Pond 0.11 Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 11) 0.05 Ponded Fly Ash (Cell 11) 0.05 PAF Ponded Fly Ash (Cell 11) Ponded Fly Ash (East Cell) 0.04 Bottom Ash - From Pond Rubber Gypsum 0.13 Stubber Gypsum 0.13 Spent Bed Material (SBM) Char Morded Fly Ash (Ash Pond) 0.12	0.05	5.5E-5 ·	440	4.1	4910	<10
JOF Ponded Fly Ash (New Dredge Cell) 0.06 Ponded Fly Ash (Old Dredge Cell) 0.10 Ponded Fly Ash (Active Ash Pond) 0.11 Bottom Ash - From Pond KIF Ponded Fly Ash (Cell 11) 0.05 Ponded Fly Ash (Cell 11) 0.06 PAF Ponded Fly Ash (Cell 11) 0.06 Ponded Fly Ash (East Cell) 0.13 Sturbber Gypsum 0.13 Sturbber Gypsum 0.13 Spent Bed Material (SBM) Act		2.6E-2	5200	6.8	285	<10
Ponded Fly Ash (Old Dredge Cell) 0.10 Ponded Fly Ash (Active Ash Pond) 0.11 Bottom Ash - From Pond KIF Ponded Fly Ash (Cell 1) 0.05 Bottom Ash - From Pond Bottom Ash - From Pond Stubber Gysum 0.13 Stubber Gysum 0.13 Stubber Gysum 0.13 Char Spent Bed Material (SBM) Char Morded Fly Ash (Ash Pond) 0.12		5.0E-4	2800		83	<10
Ponded Fly Ash (Active Ash Pond) 0.11 Bottom Ash - From Pond Bottom Ash - From Pond Ponded Fly Ash (Cell 11) 0.05 Ponded Fly Ash (Cell 11) 0.05 Bottom Ash - From Pond PAF Ponded Fly Ash (East Cell) 0.04 Botter Slag (Reed Rejects) Scrubber Gypsum 0.13 SHF Dry Fly Ash Botter Bad Material (SBM) Spent Bed Material (SBM) MCF Ponded Fly Ash Pondi		5.8E-4	2600	6.8	1520	20
Bottom Ash - From Pond KIF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 11) 0.05 Bottom Ash - From Pond PAF Ponded Fly Ash (East Cell) 0.04 Botter Slag (Reed Rejects) Scrubber Gypsum 0.13 SHF Dry Fly Ash Bottom Ash - From Pond Sturbber Gypsum 0.04 Sturbber Gypsum 0.13 Char MCF Ponded Fly Ash (Ash Pond) O.12		3.5E-S	069	8.4	2960	60
KIF Ponded Fly Ash (Cell 1) 0.05 Ponded Fly Ash (Cell 1II) 0.05 Bottom Ash - From Pond 0.05 PAF Ponded Fly Ash (Cell 1II) 0.05 PAF Ponded Fly Ash (Cell 1II) 0.04 PAF Ponded Fly Ash (East Cell) 0.04 Boiler Slag (Reed Rejects) Stuff Dry Fly Ash 0.13 Bottom Ash - From Pond 0.13		4.7E-3	740	6.0	2200	<10
Ponded Fly Ash (Cell III) 0.05 Bottom Ash - From Pond Bottom Ash - From Pond PAF Ponded Fly Ash (East Cell) 0.04 Boiler Slag (Reed Rejects) Scrubber Gypsum 0.13 SHF Dry Fly Ash Bottom Ash - From Pond Stert Bed Material (SBM) Char MCF Ponded Fly Ash Pondi O 0.12	0.05	8.3E-5	7700	7.6	200	<10
Bottom Ash - From Pond PAF Bottom Ash (East Cell) 0.04 Boiler Slag (Reed Rejects) Scrubber Gypsum 0.13 SHF Dry Fly Ash 0.04 Bottom Ash - From Pond Spent Bed Material (SBM) Char Morded Fly Ash (Ash Pond) 0.12	0.05	3.4E-5	6400	6.8	140	<10
PAF Ponded Fly Ash (East Cell) 0.04 Boiler Slag (Reed Rejects) Scrubber Gypsum 0.13 SHF Dry Fly Ash Bottom Ash - From Pond Spent Bed Material (SBM) Char Creek WCF Ponded Fly Ash (Ash Pond) 0.12	1	9.1E-3	0061	4.0	490	<10
Boiler Slag (Reed Rejects) Scrubber Gypsum 0.13 Srubber Gypsum 0.13 SHF Dry Fly Ash Bottom Ash - From Pond Spent Bed Material (SBM) Char Char 0.12	0.04	1.0E-5	2600	8.1	340	<10
Scrubber Gypsum 0.13 SHF Dry Fly Ash 0.04 Bottom Ash - From Pond 0.04 Spent Bed Material (SBM) Char 0.12		1.3E-3	9700	4.3	220	<10
SHF Dry Fly Ash 0.04 Bottom Ash - From Poud Spent Bed Material (SBM) Char Char Creek WCF Ponded Fly Ash (Ash Pond) 0.12	0.13	1.5E-4	1100	7.7	4630	10
Bottom Ash - From Pond Spent Bed Material (SBM) Char WCF Ponded Fly Ash (Ash Pond) 0.12	0.04	9.2E-5	1000	11.5	2270	<10
Spent Bed Material (SBM) Char CF Ponded Flv Ash (Ash Pond) 0.12		8.9E-3	3000	8.1	4200	10
Char				12.0	4190	150
WCF Ponded Fly Ash (Ash Pond) 0.12	•		190	12.0	4130	086
	0.12	1.8E-4	1400	9.2	1060	<10
Scrubber Gypsum 0.07 3.9E-4	0.07	3.9E-4	1200	6.7	3050	<10
Bottom Ash - From Pond 3.4E-2 3.4E-2		3.4E-2	3100	8.0	4070	130

Note: Cons

lab soil tva prgrm.xfs (Consel)

				Triaxial CU with nore pressure	h nore pressure		Direc	Direct Shear	
Source	Code	Material	Effecti	Effective Stress	T'otal	Fotal Stress	Cohesion, c (ksf)	Internal friction, \$	Angle of Repose
			Cohesion, c' (ksf)	Internal friction, \$'	Cohesion, c (ksf)	Internal friction, 🕸			
Allen	ALF	Boiler Slag (Fine Reed Rejects)	0.00	37.3	1.15	39.2	2.32	25.2	
Bull Run	BRF	Dry Fly Ash	0.31	27.7	1.12	21.2	1.36	27.4	1
		Bottom Ash - From Pond							32.4
Colbert	COF	Dry Fly Ash (Units 1-4)	0.34	27.6	0.69	19.9	1.31	28.6	
		Bottom Ash - From Pond		-					30.9
Cumberland	CUF	Dry Fly Ash (Units 1-2)	0.00	53.5	1.70	50.5	2.53	33.4	
		Bottom Ash - From Pond				1	****		30.8
		Scrubber Gypsum	0.00	38.1	3.33	33.4	1.32	41.4	-
Gallatin	GAF	Dry Fly Ash (Unit 2 Hoppers)	0.00	31.7	0.57	26.2	1.37	34.5	
		Bottom Ash - From Pond						-	31.8
John Sevier	JSF	Dry Fly Ash (Units 3-4)	0.22	22.4	0.26	17.7	1.11	33.6	
5	-	Bottom Ash - From Pond			****				27.4
Johnsonville	JOF	Ponded Fly Ash (New Dredge Cell)	0.23	32.4	1.26	25.8	1.29	32.4	
		Ponded Fly Ash (Old Dredge Cell)	0.12	30.5	0.66	15.2	2.14	39.3	,
		Ponded Fly Ash (Active Ash Pond)	0.00	22.6	0.01	15.8	1.41	36.6	-
		Bottom Ash - From Pond							30.8
Kingston	KIF	Ponded Fly Ash (Cell I)	0.14	26.1	0.36	19.6	0.82	39.1	
)		Ponded Fly Ash (Cell III)	0.03	24.4	0.00	17.8	1.47	37.6	
		Bottom Ash - From Pond					-	3	31.3
Paradise	PAF	Ponded Fly Ash (East Cell)	0.37	21.2	0.55	15.6	2.27	20.2	2
		Boiler Slag (Reed Rejects)	0.06	40.6	2.00	40.3			
		Scrubber Gypsum	0.00	39.7	3.07	35.5	0.97	45.7	
Shawnee	SHF	Dry Fly Ash	1.24	22.4	1.79	14.7	1.10	39.8	
		Bottom Ash - From Pond	-				-	••••	31.6
		Spent Bed Material (SBM)							
		Char						-	
Widows Creek	WCF	Ponded Fly Ash (Ash Pond)	1.85	25.5	1.94	21.5	1.70	31.2	
		Scrubber Gypsum	0.00	37.8	3.01	33.1	0.55	28.9	1
		Bottom Ash - From Pond							29.0
Note: Triaxial	CU and D	Note: Triaxial (U and Direct Shear test specimen were remolded to approximately 95 percent of the Standard Proctor maximum dry density at or near optimum moisture content	to approximately 95	percent of the Standard	Proctor maximum d	Iry density at or near o	ptimum moisture cont	tent	

lab soil wa prgmi.vls (Static)

TVA - Fly Ash, Bottom Ash and Scrubber Sludge Study Strength Testing Summary Law Engineering Project No. 5810860101

Note: CBR and Resilient Modulus test specimen were remolded to approximately 95 percent of the Standard Proctor (and Modified Proctor for Res. Mod.) maximum dry density at or near optimum moisture content M_R at S_c=4psi, S_i=4psi 13,079 17,515 16,325 6,368 5,917 5,199 5,807 5,529 5,030 5.500 4.788 6,110 5.500 3,480 6,372 19,021 6,945 5,671 6,095 6,352 4,917 6,247 4.309 9,421 4,731 7,541 6,901 ļ ł **Resilient Modulus (Modified Effort)** 0.26140 0.26147 0.76648 0.59309 0.56010 0.20492 0.41978 0.76224 0.38843 0.20475 0.42844 0.43051 0.76411 0.51069 0.38843 0.24877 0.76150 0.45133 0.61364 0.39276 0.69867 0.48836 0.65332 0.47386 0.64487 0.44309 0.53301 K5 0.20416 0.08396 -0.14235 -0.09252 -0.06155 0.08023 0.08137 -0.03472 0.08323 -0.09489 0.13323 -0.043880.19126 -0.016250.14322 -0.01625 0.13522 0.14896 0.13866 -0.12389 0.09702 -0.01211 0.09559 0.05337 0.28011 0.09488 0.01011 ; K2 11,738 1,715 10,977 1,558 8,454 2,260 10,959 3,254 2,427 2,255 3,980 1,822 2,774 3,283 1,977 2,455 1,994 3,602 4,033 2,108 2,389 2,374 5,551 1,639 2,468 3,283 2,541 1 ł Z M_k at S, =4psi, S,=4psi 15,110 2,384 12.513 11,612 4,938 5,460 6,244 7.379 15,646 4,657 4.350 4,222 6,949 3,553 6,419 5.370 6,378 2,918 6,264 6,417 4,598 6,545 4,813 3,769 3,844 6,169 9,071 ł 1 **Resilient Modulus (Standard Effort)** 0.76340 0.78260 0.75876 0.63430 0.66319 0.78070 0.65540 0.45385 0.60215 0.40269 0.79102 0.23790 0.73640 0.23891 0.58242 0.34550 0.67882 0.25471 0.43636 0.63725 0.51994 0.41203 0.48134 0.53980 0.54531 0.56321 0.47991 KS 0.20995 0.11134 -0.03317 -0.04340-0.02608 0.19103 -0.17750 0.11934 -0.18159 -0.09595 0.06737 0.08949 0.10936 0.09590 -0.09930 -0.08694 0.08085 -0.10787 -0.00868 0.03358 0.13665 0.10296 0.09516 0.09530 0.03707 0.16927 0.07728 1 K2 2,146 2,390 1,928 1,026 7,937 2.258 1,972 2,156 1,495 1,803 1,427 5,929 9,420 2,662 3,225 1,857 2,368 2,194 9,623 2,713 2,965 1,487 2,373 2,592 1,661 1,353 7,531 ł 1 ¥ CBR ļ 12 50 99 55 14 25 1 2 30 35 24 54 20 30 5 40 4 6 ŝ 37 ---~ % 2 6 -Ponded Fly Ash (New Dredge Cell) Ponded Fly Ash (Active Ash Pond) onded Fly Ash (Old Dredge Cell) Boiler Slag (Fine Reed Rejects) Dry Fly Ash (Unit 2 Hoppers) Ponded Fly Ash (Ash Pond) Ponded Fly Ash (East Cell) Spent Bed Material (SBM) Boiler Slag (Reed Rejects) Bottom Ash - From Pond Bottom Ash - From Pond Ponded Fly Ash (Cell III) **Bottom Ash - From Pond** Bottom Ash - From Pond **Bottom Ash - From Pond** Bottom Ash - From Pond Bottom Ash - From Pond **3ottom Ash - From Pond** Bottom Ash - From Pond Ponded Fly Ash (Cell I) Dry Fly Ash (Units 1-4) Dry Fly Ash (Units 1-2) Dry Fly Ash (Units 3-4) Scrubber Gypsum Scrubber Gypsum Scrubber Gypsum Dry Fly Ash Dry Fly Ash Material Char Code ALF WCF SHF BRF CUF GAF COF JOF KIF PAF JSF Widows Creek Johnsonville Cumberland John Sevier Kingston Shawnee **Bull Run** Paradise Gallatin Colbert Source Allen

lab soil tva prgrin.xls (Dynamic)