

① March 23, 1993 thru March 27, 1993

COMPUTED _____ DATE _____

CHECKED _____ DATE _____

STORAGE VOLUME = 1,733,233 cf

PUMPING CAP

11500 gpm

= 12031 ft³/hr

11200 gpm

= 9625 ft³/hr

①A 5.43" in 5 days

DAY 1 3.84" = 1,355,029 cf

= 378,204
+ 577,488 (PUMPING)

avail. 955,692 cf

DAY 2 .22" = -77,030

+ 577,488 (PUMPING)
1,456,150 cf

DAY 3 0" + 577,488 (PUMPING)

= 1,733,233 (BACK UP TO MAX. STORAGE)

①B DAY 1 3.87" = 1,355,029

= 378,204 11200 gpm (100 ft³/hr)
+ 288,744 (PUMPING)
666,948

DAY 2 .22" = -77,030

+ 288,744 (PUMPING)
878,662

DAY 3 0" = + 288,744

1,167,406

DAY 4 .51" -178,570

+ 288,744 (PUMPING)
1,277,580

DAY 5 1.13" -395,654

+ 288,744 (PUMPING)
1,170,670

slightly more than 2 days to max. storage

TVA 11030 (WM-7-75)

(1C)

$$\begin{array}{r}
 1,733,233 \\
 \text{DAY 1 } 3.87'' - 1,355,029 \\
 \hline
 378,204 \\
 + 462,000 \text{ (pumping)} \\
 \hline
 840,000
 \end{array}$$

$$\begin{array}{r}
 \text{DAY 2 } .22'' - 77,030 \\
 + 462,000 \text{ (pumping)} \\
 \hline
 1,224,970
 \end{array}$$

$$\begin{array}{r}
 \text{DAY 3 } 0'' + 462,000 \text{ (pumping)} \\
 \hline
 1,686,970
 \end{array}$$

$$\begin{array}{r}
 \text{DAY 4 } .51'' - 178,570 \\
 + 462,000 \text{ (pumping)} \\
 \hline
 1,733,233 \text{ (back up to max. storage)}
 \end{array}$$

(1D)

$$\begin{array}{r}
 1,733,233 \\
 \text{DAY 1 } 3.84'' - 1,355,029 \\
 \hline
 378,204 \\
 + 231,000 \text{ (pumping)} \\
 \hline
 609,204
 \end{array}$$

$$\begin{array}{r}
 \text{DAY 2 } .22'' - 77,030 \\
 + 231,000 \text{ (pumping)} \\
 \hline
 763,174
 \end{array}$$

$$\begin{array}{r}
 \text{DAY 3 } 0'' + 231,000 \text{ (pumping)} \\
 \hline
 994,174
 \end{array}$$

$$\begin{array}{r}
 \text{DAY 4 } .51'' - 178,570 \text{ (pumping)} \\
 + 231,000 \\
 \hline
 1,046,604
 \end{array}$$

$$\begin{array}{r}
 \text{DAY 5 } 1.13'' - 395,654 \\
 + 231,000 \text{ (pumping)} \\
 \hline
 801,950
 \end{array}$$

more than 3 1/2 days to max. storage

TVA 11030 (WM-7-75)

①

Peaks

STORAGE VOLUME = 1,733,233 cf

4.09" in 30 hrs = 1,432,059 cf

left = 301,174
+ pumping

2721,860	=	1,023,034
360,930		662,104
577,500		878,674
1,288,750		589,924

3.87" in 18 hrs = 1,355,029

left = 378,204
+ pumping

433,116	=	811,320
216,558		594,762
346,500		724,704
173,250		551,454

② Dec 4, 1993 thru Dec 10, 1993

SHEET

OF

COMPUTED

DATE

STORAGE VOLUME - 1,733,233 cf

CHECKED

DATE

②A

[6.03" in 7 days]

DAY 1 4.32" = 1,512,590 cf
 = 220,643 cf
 + 577,488 (PUMPING)
 798131

DAY 2 .4" -140,055
 + 577,488 (PUMPING)
 1,235,564

DAY 3 0" + 577,488 (PUMPING)
 1,733,233 back up to max. storage

②B

DAY 1 4.32" = 1,512,590 cf
 = 220,643 cf
 + 288,744 cf (pumping)
 509,387 cf

DAY 2 .4" -140,055 cf
 + 288,744 (PUMPING)
 658,076

DAY 3 0" + 288,744 (PUMPING)
 946,820

DAY 4 0" + 288,744 (PUMPING)
 1,235,564

DAY 5 0" + 288,744 (PUMPING)
 1,524,308

DAY 6 0" + 288,744 (PUMPING)
 1,733,233 (back up to max. storage)

2

20

$$\begin{aligned}
 \text{DAY 1 } 4.32'' &= 1,512,590 \text{ cf} \\
 &= 220,643 \text{ cf} \\
 &+ \underline{462,000} \text{ (PUMPING)} \\
 &682,643
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 2 } .4'' &-140,055 \\
 &+ \underline{462,000} \text{ (PUMPING)} \\
 &1,004,588
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 3 } 0'' &+ \underline{462,000} \text{ (PUMPING)} \\
 &1,466,588
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 4 } 0'' &+ \underline{462,000} \text{ (PUMPING)} \\
 &1,733,233 \text{ (back up to max. storage)}
 \end{aligned}$$

21

$$\begin{aligned}
 \text{DAY 1 } 4.32'' &1,512,590 \text{ cf} \\
 &= 220,643 \text{ cf} \\
 &+ \underline{231,000} \text{ (PUMPING)} \\
 &451,643
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 2 } .4'' &-140,055 \\
 &+ \underline{231,000} \text{ (PUMPING)} \\
 &542,588
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 3 } 0'' &+ \underline{231,000} \text{ (PUMPING)} \\
 &773,588
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 4 } 0'' &+ \underline{231,000} \text{ (PUMPING)} \\
 &1,004,588
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 5 } 0'' &+ \underline{231,000} \text{ (PUMPING)} \\
 &1,235,588
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 6 } 0'' &+ \underline{231,000} \text{ (PUMPING)} \\
 &1,466,588
 \end{aligned}$$

$$\begin{aligned}
 \text{DAY 7 } 1.18'' &- 458,679 \\
 &+ \underline{231,000} \text{ (PUMPING)} \\
 &1,238,909
 \end{aligned}$$

slightly more than 2 days to max. storage

2

Plate

STORAGE VOLUME = 1,733,233 cf

4.72" in 30 hrs = 1,652,645

left = 80,588

+ pumping

(4721,860) =	802,448
	360,930		441,518
	577,500		658,088
	288,750		369,338

4.32" in 18 hrs = 1,512,590

left = 220,643

+ pumping

(433,116) =	653,759
	216,558		437,201
	346,500		567,143
	173,250		393,893

③ Feb 8, 1994 thru Feb 11, 1994

STORAGE VOLUME = 1,733,233 cf

6.67" in 3 1/4 days

3A	DAY 1	.4"	140,055	
		avail	= 1,593,178	
			+ 288,744 (pumping)	2,150,000
			<u>1,733,233</u>	
	DAY 2	1.48"	- 518,202	
			+ 577,480 (pumping)	
			<u>1,733,233</u>	
	DAY 3	1.37"	- 479,687	
			+ 577,480 (pumping)	
			<u>1,733,233</u>	
	DAY 4	3.42"	- 1,197,467	
			+ 577,480 (pumping)	
			<u>1,113,246</u>	

slightly more than 1 day to pump out to max storage

3B	DAY 1	.4"	140,055	
		avail	1,593,178	
			+ 144,372 (pumping)	1,881,605
			<u>1,733,233</u>	
	DAY 2	1.48"	- 518,202	
			+ 288,744 (pumping)	
			<u>1,503,775</u>	
	DAY 3	1.37"	- 479,687	
			+ 288,744 (pumping)	
			<u>1,312,832</u>	
	DAY 4	3.42"	- 1,197,467	
			+ 288,744 (pumping)	
			<u>404,109</u>	

take slight more than 4 1/2 days to pump out to max. storage

(2)

STORAGE VOLUME = 1,733,233 cf

(3C)

DAY 1	.4"	140,055	
	avail	1,593,178	
		+ 462,000	(pumping)
		<u>1,733,233</u>	
DAY 2	1.48"	-518,202	
		+ 462,000	(pumping)
		<u>1,677,031</u>	
DAY 3	1.37"	-479,687	
		+ 462,000	(pumping)
		<u>1,659,344</u>	
DAY 4	3.42"	-1,197,467	
		+ 462,000	(pumping)
		<u>923,877</u>	

take 1 3/4 days to pump out to max storage

(3D)

DAY 1	.4"	140,055	
	avail	1,593,178	
		+ 231,000	(pumping)
		<u>1,733,233</u>	
DAY 2	1.48"	-518,202	
		+ 231,000	(pumping)
		<u>1,330,531</u>	
DAY 3	1.37"	-479,687	
		+ 231,000	(pumping)
		<u>1,081,844</u>	
DAY 4	3.42	-1,197,467	
		+ 231,000	(pumping)
		<u>115,377</u>	

take 7 days to pump out to max eff.

within an inch of flooding

3

Peak

COMPUTED _____ DATE _____

STORAGE VOLUME = 1,733,233 cf

CHECKED _____ DATE _____

3.42" in 18 hrs. = 1,197,467 cf

left = 535,766

+ pumping

433,116
216,558
346,500
173,250

=	968,882
	752,324
	882,266
	709,016

④ Mon 27, 1994 thru Mar 31, 1994

SHEET _____ OF _____

COMPUTED _____ DATE _____

CHECKED _____ DATE _____

STORAGE VOLUME = 1,733,233

④A [6.18" in 5 days]

DAY 1 4.78" = 1,673,653
 available = 59,580
 + 577,488 (pumping)
 637,068

DAY 2 .96" 336,131
 + 577,488 (pumping)
 878,425

DAY 3 .04" - 14,006
 + 577,488 (pumping)
 1,441,907

less than 1 day to pump
back down to max. storage

④B

DAY 1 4.78" = 1,673,653
 59,580
 + 288,744 (pumping)
 348,324

DAY 2 .96" - 336,131
 288,744 (pumping)
 300,937

Day 3 .04" - 14,006
 + 288,488 (pumping)
 575,419

Day 4 0" + 288,488 (pumping)
 863,907

Day 5 .4" - 140,055
 + 288,488 (pumping)
 1,012,340

2 1/2 days to pump back
down to max. storage

TVA 11030 (WM-7-75)

STORAGE VOLUME = 1,733,233 cf

4C

DAY 1 4.78" = 1,673,653
 available = 59,580
 462,000 (pumping)
 521,580
 Day 2 .96" - 336,131
 + 462,000 (pumping)
 647,449
 Day 3 .04" - 14,006
 + 462,000 (pumping)
 1,095,443
 Day 4 0" 462,000 (pumping)
 1,557,443
 Day 5 .4" - 140,055
 + 462,000 (pumping)
 1,733,233
 max storage

4D

DAY 1 4.78" = 1,673,653
 avail = 59,580
 231,000 (pumping)
 290,580
 DAY 2 .96" - 336,131
 + 231,000 (pumping)
 195,449
 Day 3 .04" - 14,006
 231,000 (pumping)
 402,443
 Day 4 0" + 231,000 (pumping)
 633,443
 Day 5 .4" - 140,055
 + 231,000 (pumping)
 724,388

nearly 4 1/2 days to max. storage

5) April 12

thru April 16, 1994

COMPUTED

DATE

CHECKED

DATE

STORAGE VOLUME = 1,733,233 cf

[4.58" in 4 1/2 days]

5A)

DAY 1 .05" = 17,507

left = 1,718,726

+ 288,744 (pumping)

1,733,233

DAY 2 2.41"

- 843,829

+ 577,488 (pumping)

1,466,892

DAY 3 0"

+ 577,488 (pumping)

1,733,233

DAY 4 1.30"

455,178

+ 288,744 (pumping)

1,566,799

DAY 5 .82"

- 287,112

+ 577,488 (pumping)

1,733,233

back up to max storage

5B)

DAY 1 .05" = 17,507

left = 1,718,726

+ 144,372 (pumping)

1,733,233

DAY 2 2.41"

- 843,829

+ 288,744 (pumping)

1,178,148

DAY 3 0"

+ 288,744 (pumping)

1,466,892

DAY 4 1.30"

- 455,178

+ 288,744 (pumping)

1,300,458

DAY 5 .82"

- 287,112

+ 288,744 (pumping)

1,302,090

1 1/2 days to pump out to maximum storage

STORAGE VOLUME = 1,733,233 cf

(52)

DAY 1 .05" = 17,507
 left = 1,718,726
231,000 (pumping)

DAY 2 2.41"
 1,733,233
 - 843,829
+ 462,000 (pumping)
 1,351,404

DAY 3 0" =
+ 462,000 (pumping)
 1,733,233

DAY 4 1.30"
 455,178
+ 231,000 (pumping)

DAY 5 .82"
 1,509,055
 - 287,112
+ 462,000 (pumping)
 1,683,943

about 2 1/2 hrs to pump back up to max storage

DAY 1 .05" = 17,507
 left = 1,718,726
+ 115,500 (pumping)

DAY 2 2.41" =
 1,733,233
 - 843,829
231,000 (pumping)
 1,120,404

DAY 3 0" =
231,000 (pumping)
 1,351,404

DAY 4 1.30"
 - 455,178
231,000 (pumping)

DAY 5 .82"
 1,127,226
 - 287,112
+ 231,000 (pumping)
 1,071,114

= 2 days 2 hrs to pump out to max. storage

KIF-COAL YARD RUNOFF POND

2 lines

Time (hr)	10 yr (cf)	1500 gpm 1200 gpm		² 1500 gpm 1200 gpm	
		1500 gpm	1200 gpm	1500 gpm	1200 gpm
0.5	619742	6016	4813	12032	9626
1	777303	12031	9625	24064	19252
2	875340	24063	19250	48128	38504
3	1032905	36094	28875	72192	57756
6	1232480	72188	57750	144384	115512
12	1470573	144375	115500	288768	231024
24	1680657	288750	231000	577536	462048

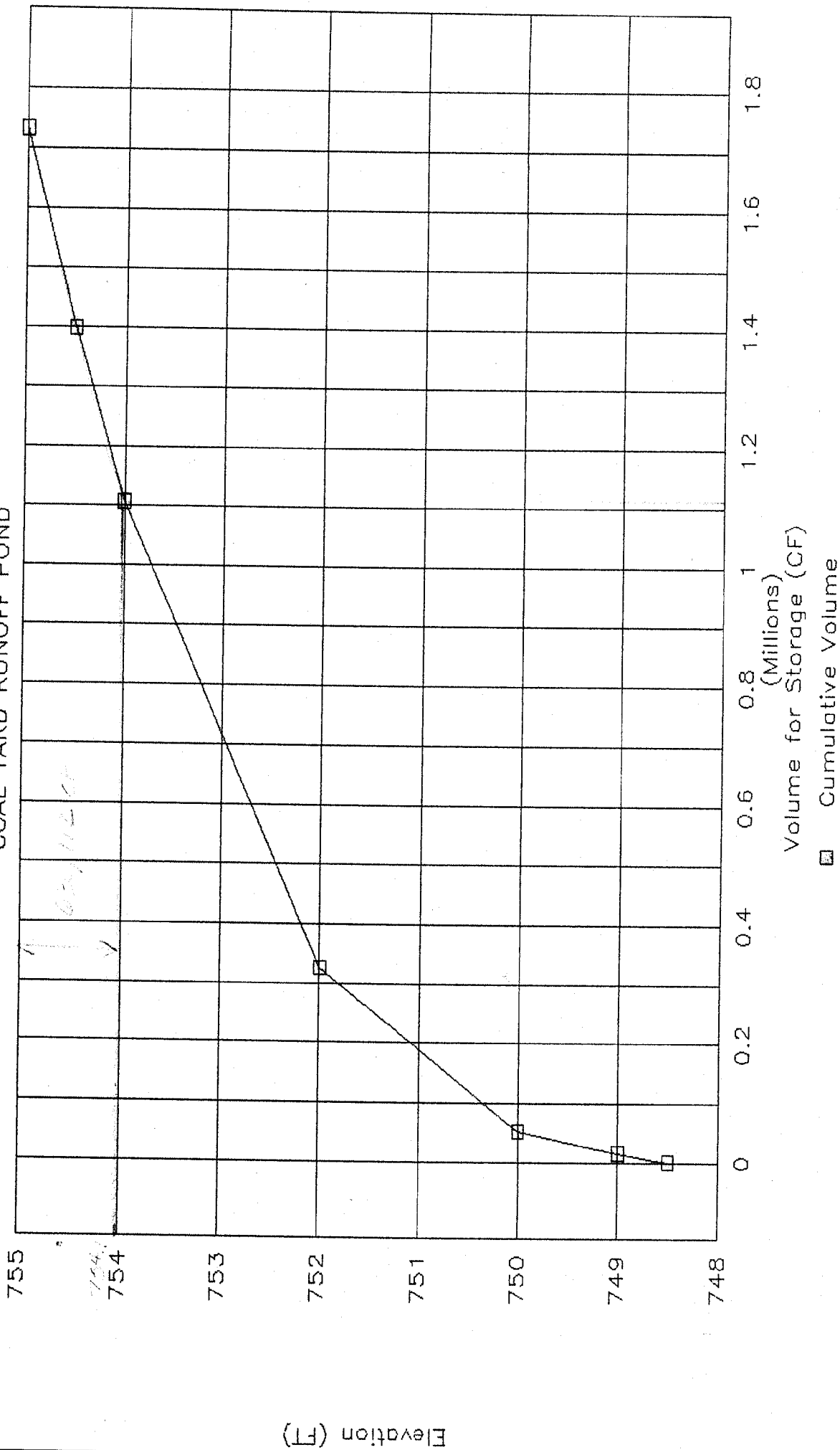
KINGSTON FOSSIL PLANT

RAINFALL DATA (US Weather Bureau Technical Paper No. 40)

Rainfall Duration (hr)	5 yr Rainfall Depth(in)	2 yr Rainfall Depth (in)	1 yr Rainfall Depth (in)
0.5	1.52	1.2	1.05
1	1.91	1.55	1.3
2	2.4	1.95	1.6
3	2.6	2.1	1.65
6	3.25	2.5	2.1
12	3.75	2.85	2.5
24	4.25	3.4	2.9

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND

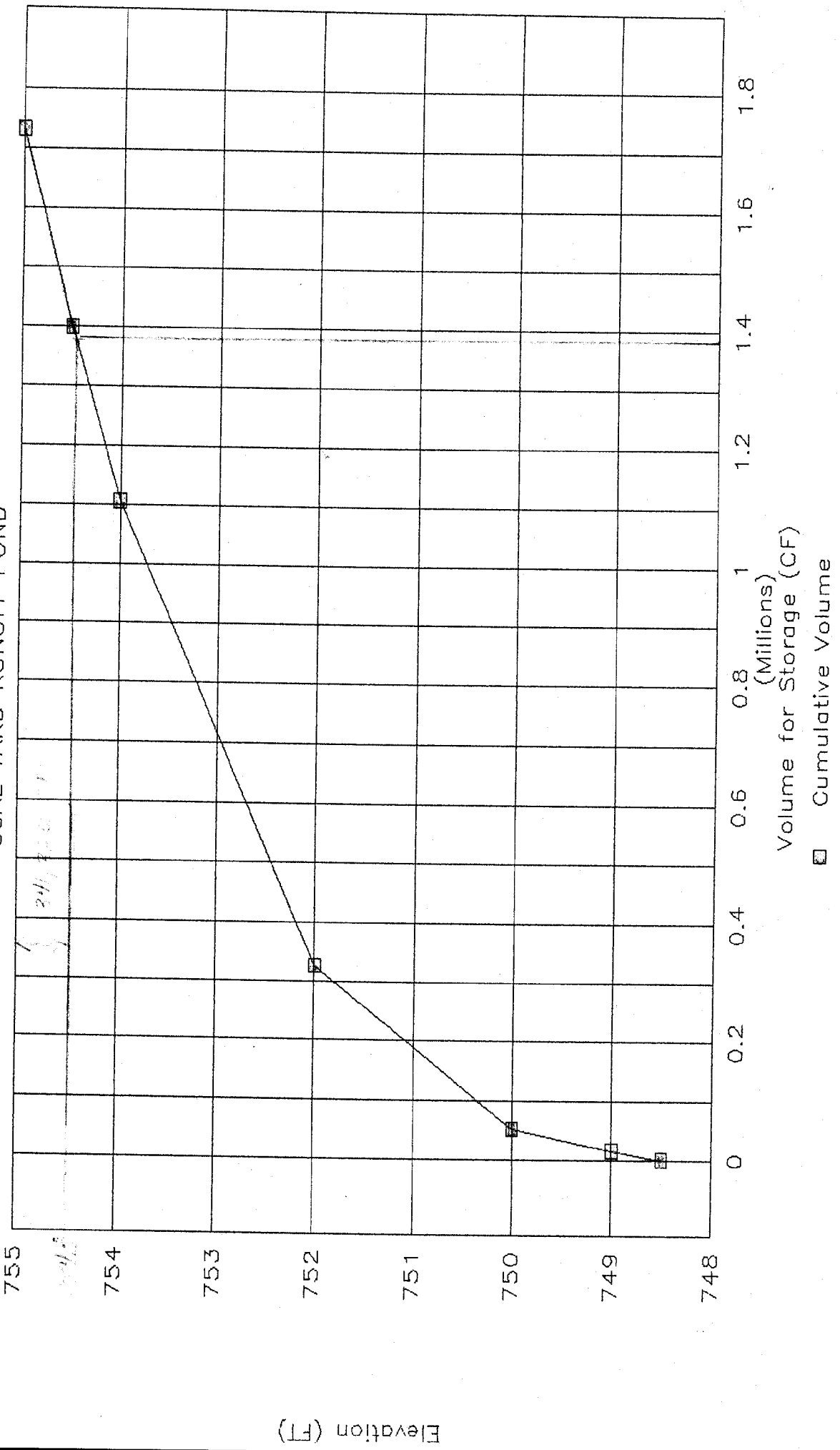


STORAGE AVAILABLE AT TIME OF 11-24-78
WITH 1,000 GPM PUMP

CLM
6-20-91

KINGSTON FOSSIL PLANT

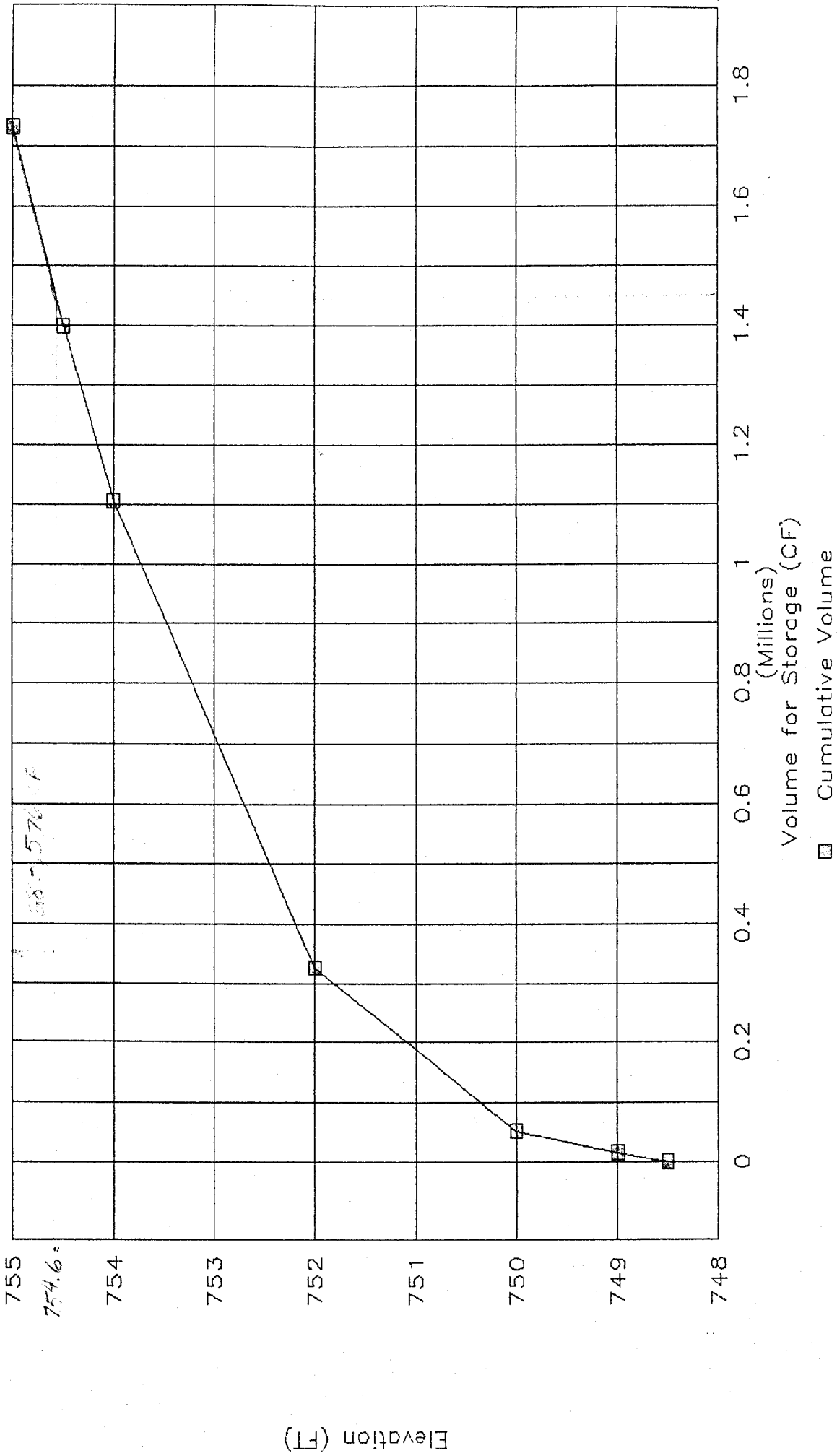
COAL YARD RUNOFF POND



- Storage capacity at time of 100% runoff
with 1,000 cfs inflow

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND



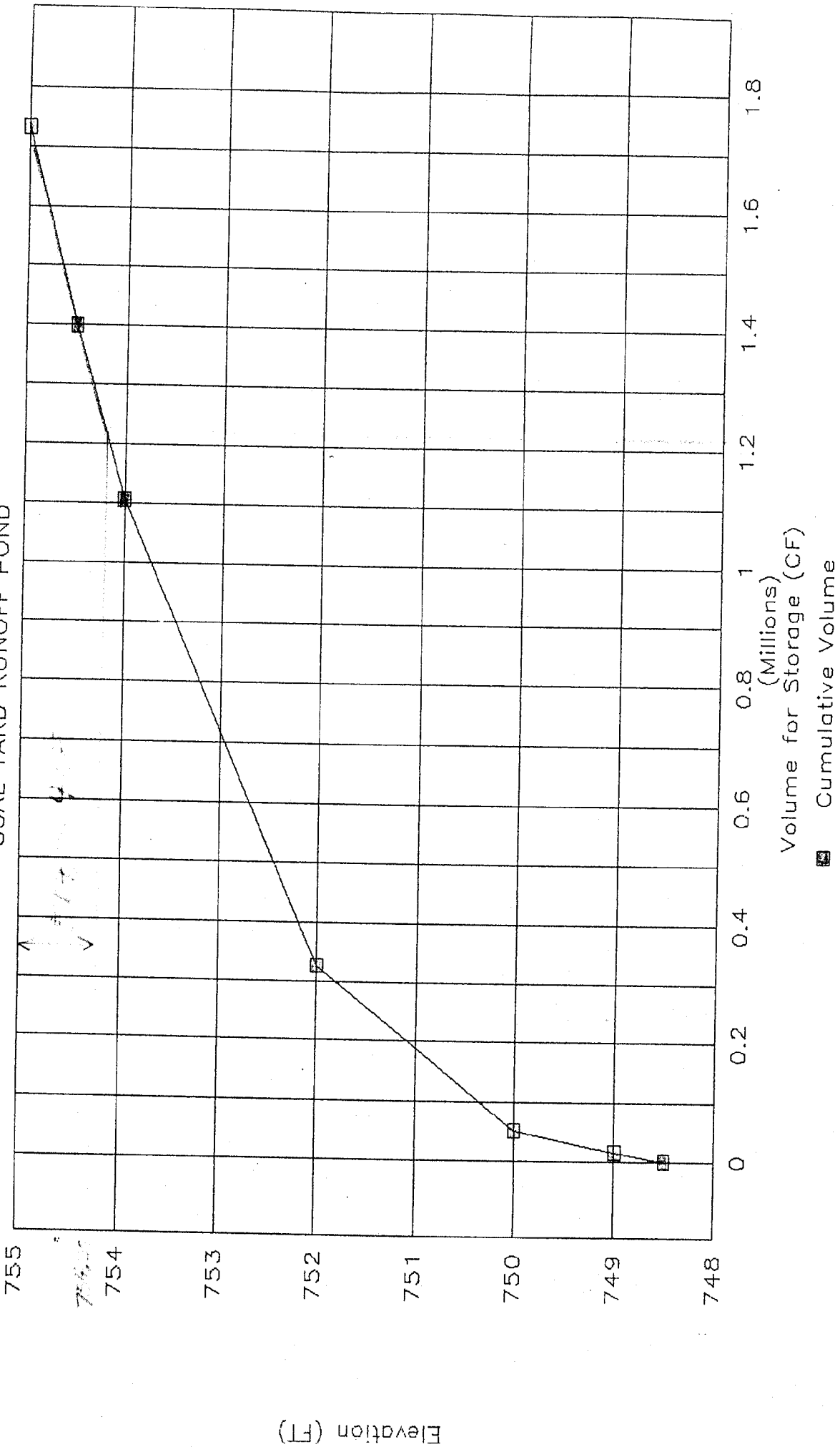
□ Cumulative Volume

— CURVES AVAILABLE AT TWP FOR 1974 AND 1975
WITH 1/2000 SCALE PLAN

CLP
8-20-74

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND

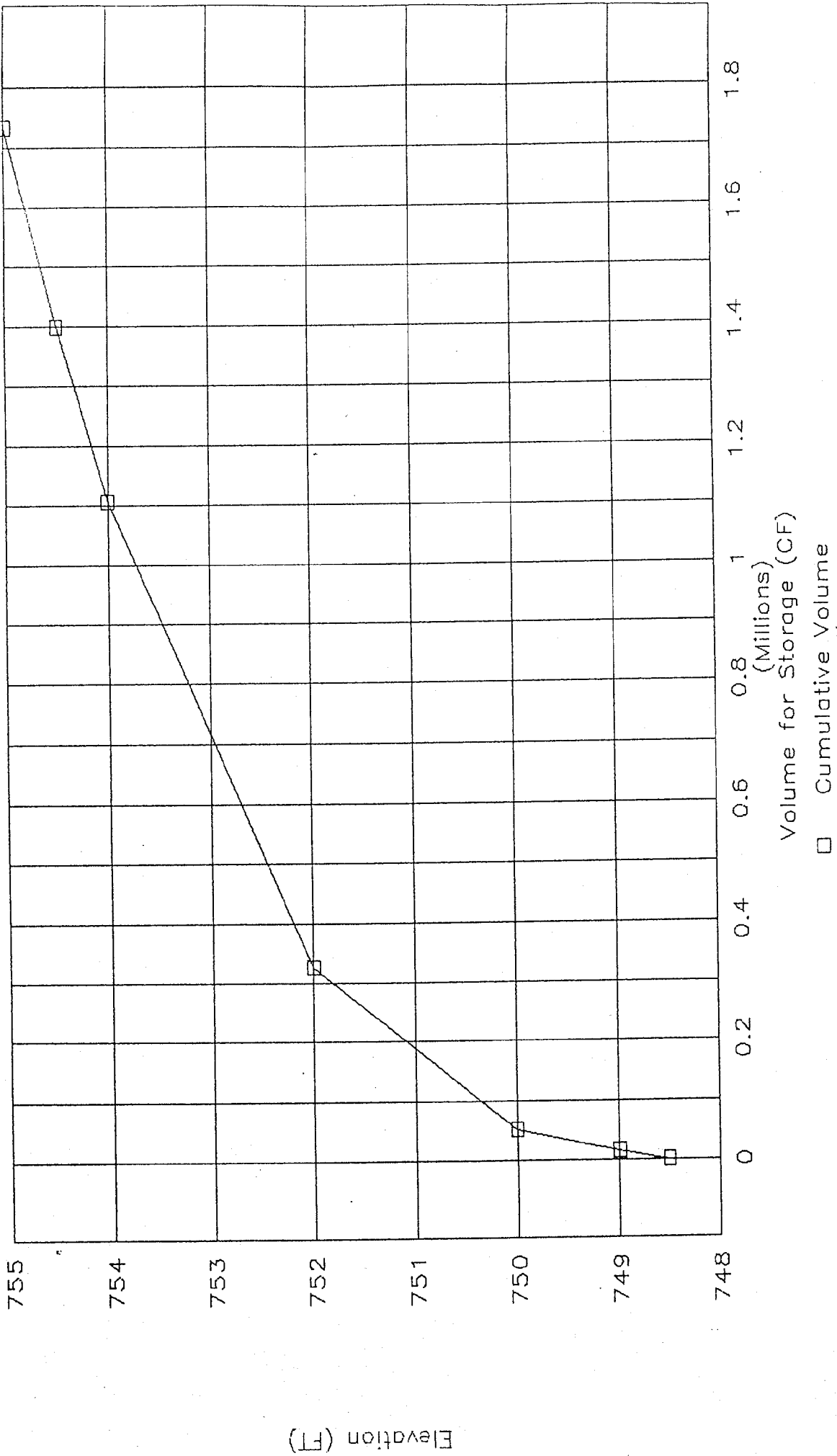


— STORAGE CAPABLE AT END OF 1.9 MILLION CF
 WITH 2 1200 gpm pumps

6.11
 6.30

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND



KINGSTON FOSSIL PLANT
COAL YARD RUNOFF POND

SHEET _____ OF _____

COMPUTED CLM DATE 6-20-94

CHECKED _____ DATE _____

1 1500 gpm pump

AT END OF 10 YR STORM
24 HR

$$1680657 - 288750 = 1,391,907 \text{ cf}$$

@ EL 754.5

$$\text{STORAGE LEFT} = 1,733,233 - 1,391,907 = 341,326 \text{ cf}$$

RAINS AGAIN..
could contain..

$$341,326 = 350,137 \times$$
$$+ 288,750$$

24 hr pumping capacity

$$x = 1.8'' \text{ (can't handle a 1 yr - 24 hr storm)}$$

1 1200 gpm pump

AT END OF 10 YR STORM
24 HR

$$1680657 - 231,000 = 1,449,657 \text{ cf}$$

@ EL 754.6

$$\text{STORAGE LEFT} = 1,733,233 - 1,449,657 = 283,576 \text{ cf}$$

RAINS AGAIN..
could contain..

$$283,576 = 350,137 \times$$
$$+ 231,000$$
$$x = 1.47'' \text{ (can't handle a 1 yr - 24 hr storm)}$$

TVA 11030 (WM-7-75)

KINGSTON FOSSIL PLANT
COAL YARD RUNOFF POND

SHEET _____ OF _____

COMPUTED CUM DATE 6-20-74

CHECKED _____ DATE _____

2 1500 gpm pumps

AT END OF 10 YR STORM
24-HR

$$1,680,657 - 577,536 = 1,103,121 \text{ cf}$$

@ eL 754.1

$$\text{STORAGE LEFT} = 1,733,233 - 1,103,121 = 630,112 \text{ cf}$$

RAINS AGAIN,
could contain..

$$630,112 = 350,137x$$
$$+ 577,536$$

$x = 3.45''$ (could handle a
2 yr - 24 hr storm)

2 1200 gpm pumps

AT END OF 10 YR STORM
24 HR

$$1,680,657 - 462,048 = 1,218,609 \text{ cf}$$

@ eL 754.25

$$\text{STORAGE LEFT} = 1,733,233 - 1,218,609 = 514,624 \text{ cf}$$

$$514,624 = 350,137x$$
$$+ 462,048$$

$x = 2.79''$ (can't handle a
1 yr - 24 hr storm)

SHEET _____ OF _____

COMPUTED _____ DATE _____

CHECKED _____ DATE _____

TVA 11030 (WM-7-75)

TVA-00006703

KINGSTON FOSSIL PLANT
COAL YARD RUNOFF POND

SHEET _____ OF _____

COMPUTED CLM DATE 6-30-94

CHECKED _____ DATE _____

10YR-12HR (AT END OF DAY)

TRY: 1 1500gpm pump

10YR-12HR (4.2" RAIN)

$$1470573 - 144375 = 1,326,198 \text{ f}$$

$$\begin{matrix} 1 \\ 12\text{HR} \end{matrix} @ 754.4$$

STORAGE LEFT = $1,733,233 - 1,326,198 = 407,035 \text{ f}$
RAINS AGAIN..

could contain.. $407,035 = 350,137 \times$
 $+ 288,750$

$$\begin{matrix} \uparrow \\ 24\text{HR} \end{matrix} x = 1.99'' \quad (\text{can't handle a } 1 \text{ yr - 24 hr storm})$$

2 1500 gpm pumps

10YR-12HR (4.2" RAIN)

$$1470573 - 288,768 = 1,181,805 \text{ cf}$$

$$@ 754.15$$

$$\text{STORAGE LEFT} = 1733233 - 1181805 = 551,428 \text{ cf}$$

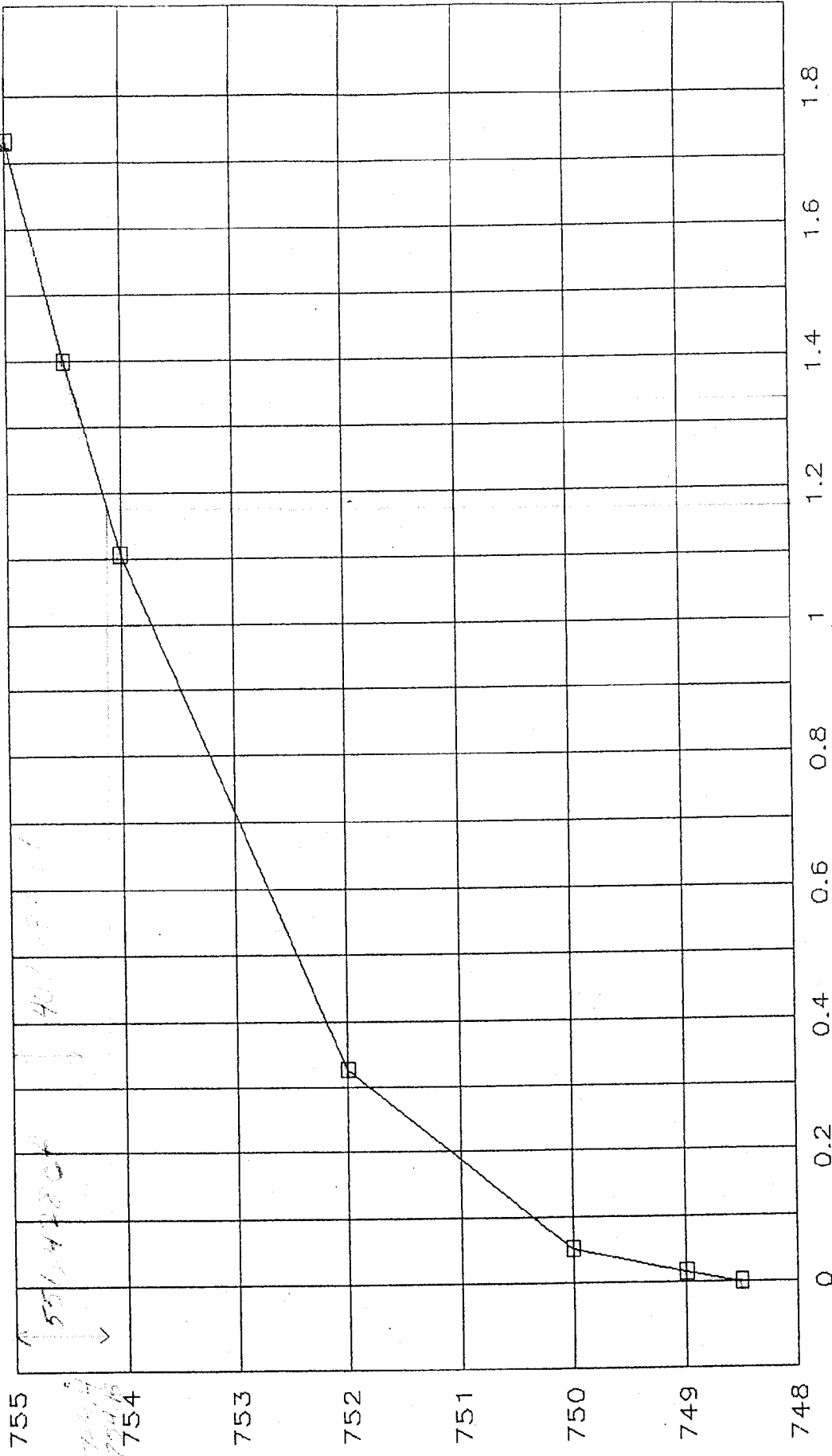
$$\begin{matrix} 551,428 \\ + 577,536 \end{matrix} = 350,137 \times$$

$$x = 3.22''$$

(can handle a 1 yr - 24 hr storm)

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND



Volume for Storage (CF)
 Cumulative Volume

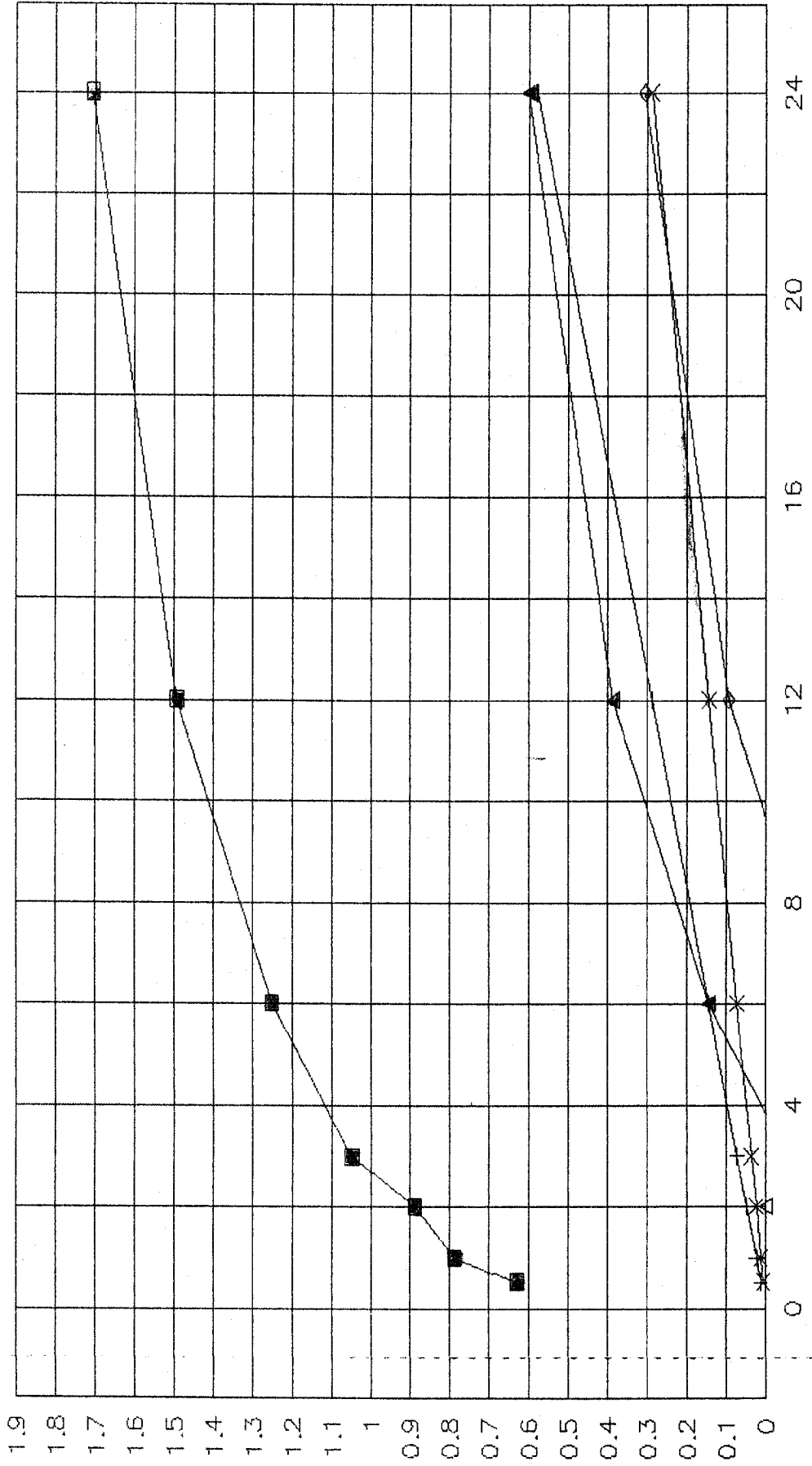
— STORAGE AVAILABLE IN POND CF 10 YR 10% REPLENISHMENT W/1 INCH YEAR
 — STORAGE AVAILABLE AT END OF 10 YR 10% REPLENISHMENT W/3 INCH YEAR

Elevation (FT)

CLM
6-8-94

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND



Time (hrs)

■ 10 yr storm + 2 1500 gpm pumps ◇ El 748.5-754.5 ▲ El 748.5-754

X 1 Discharge Line

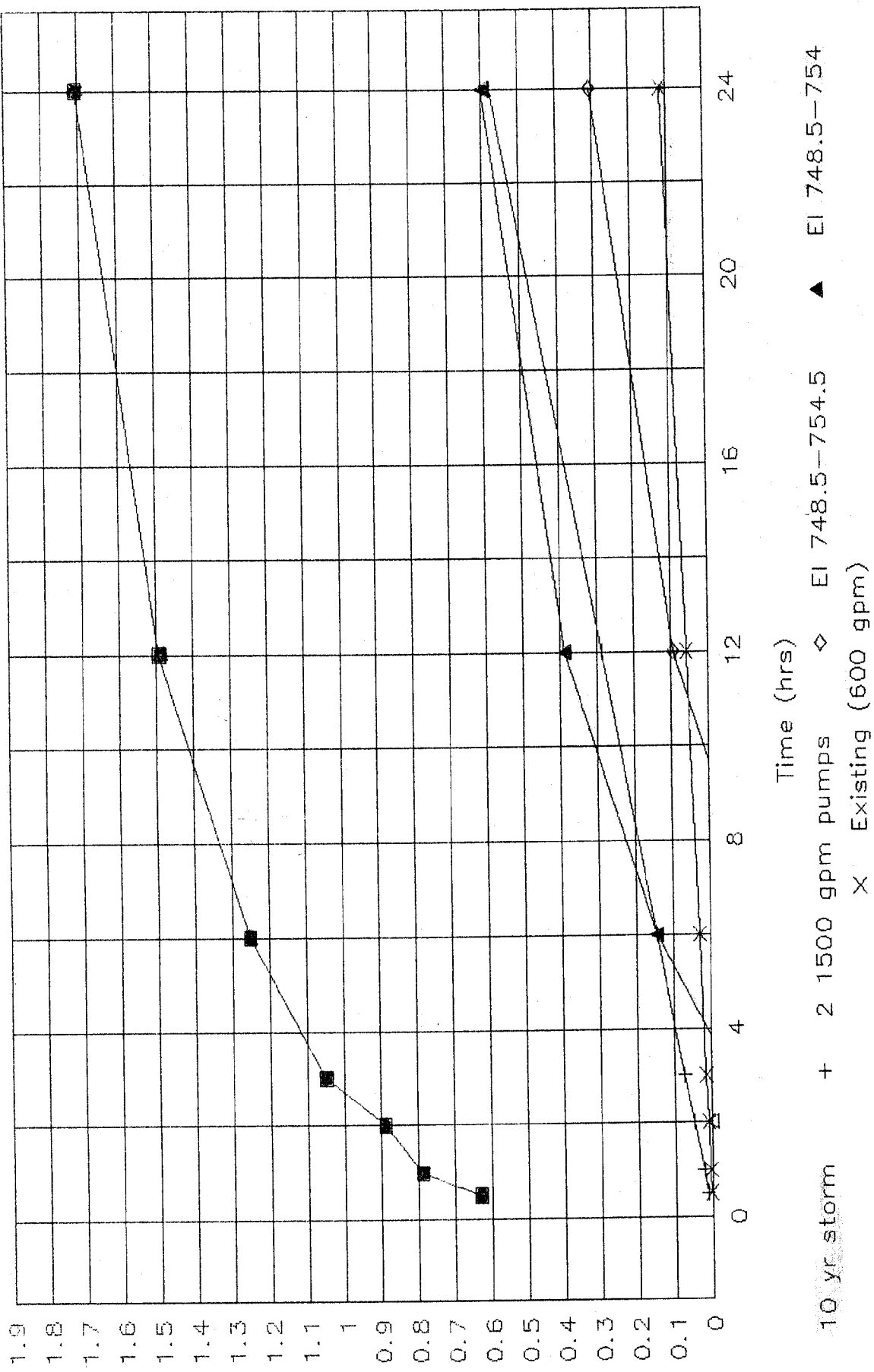
↳ * will contain up to El 755

46-02
70

WLM
6-8-94

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND



■ 10 yr storm + 2 1500 gpm pumps ◆ EI 748.5-754.5 ▲ EI 748.5-754
 X Existing (600 gpm)

The existing pump is adequate in containing a 10 YR - 24 hr flood, which does not even fall on the graph (1,733,233)

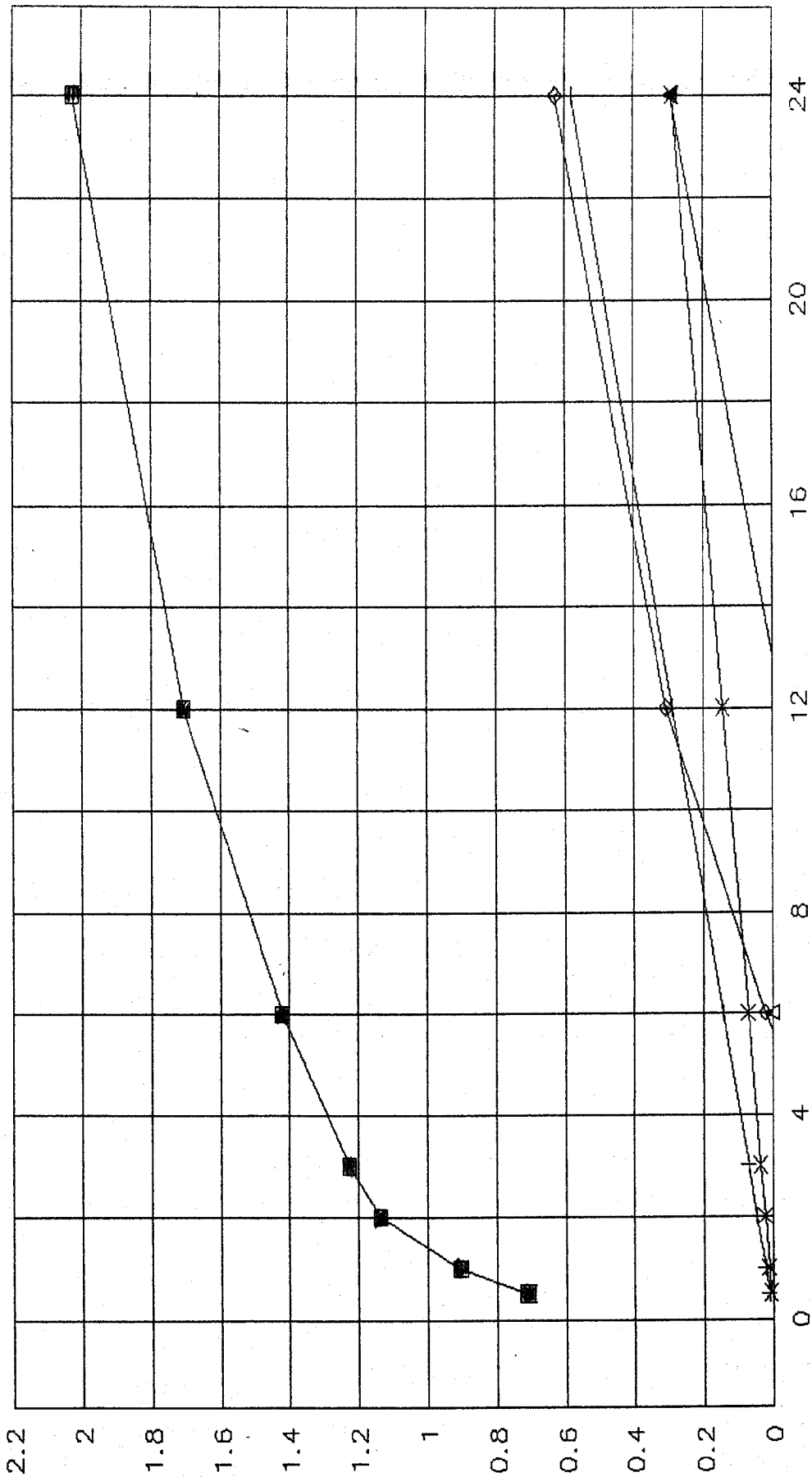
Cumulative Inflow of Pond (cf) (Millions)

WLM
6-8-94

CLM
6-6-94

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND



Cumulative Inflow of Pond (cf) (Millions)

Time (hrs)

- 25 yr storm
- + 2 1500 gpm pumps
- ◇ EI 748.5-754.5
- ▲ EI 748.5-755
- X 1 Discharge Line

* 1 DISCHARGE LINE WILL CONTAIN 25% STORAGE IN EL 745

CLM
6-6-94

July earliest start

May 6, 1994

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND

COST ESTIMATE REQUEST No.:

*Memo Dan Scott to R G Johnson
~~KIP93-1218~~ PO dated March 22, 1994 (465 940322
103)*

CIVIL SITE ENGINEERING

Phase II Scope of Work:

During periods of heavy rainfall, the existing Coal Yard Runoff Pond is inadequate in containing the flood waters.

Our involvement in the Phase II study will include providing for the following:

- 40 — 1. Provide for earthfill in low areas and crushed stone surface on roadway where required.
 - 24 — 2. Provide for grading of new areas, including area and roadway around pumphouse.
 - 24 — 3. Perform a field survey in the area to obtain recent topographical data. *(assume site does this) (2 trips)* ^{at} Monday
 - 8 — 4. Develop a Phase III scope of work.
 - 24 — 5. Make site visits as necessary to obtain plant input to the proposed scheme and to obtain necessary field information. *(3 trips)* → { 1 lead north
2 pits
 - 25 — Lead Section
- 12/ say 125 hrs.

K.W. Burnett
Manager, Site Engineering
LP 2G-C

Phase 3 — 40 hrs.

May 6, 1994

KINGSTON FOSSIL PLANT

COAL YARD RUNOFF POND

COST ESTIMATE REQUEST No.: Memo- Dan Scott to R G Johnson dated
March 22, 1994 (B65 940322 103)

CIVIL SITE ENGINEERING

Phase II Scope of Work:

During periods of heavy rainfall, the existing Coal Yard Runoff Pond is inadequate in containing the flood waters.

Our involvement in the Phase II study will include providing for the following:

1. Provide for earthfill in low areas and crushed stone surface on roadway where required.
2. Provide for grading of new areas, including area and roadway around pumphouse.
3. Perform a field survey in the area to obtain recent topographical data.
4. Provide for removal of pumphouse and platform.
5. Develop a Phase III scope of work.
6. Make site visits as necessary to obtain plant input to the proposed scheme and to obtain necessary field information.

K.W. Burnett
Manager, Site Engineering
LP 2G-C

FILL QUANTITIES

1) ROAD AROUND PUMPING STATION ($\approx 153' \rightarrow 1756'$)

3' { $2\frac{1}{2}'$ depth earthfill
 $\frac{1}{2}'$ crushed stone surface } for road

20' road width

300' length

(+ room to turn around)

10' width

20' length

EARTH FILL -

$$(2.5' \times 20' \times 300') + (2.5' \times 10' \times 20') = 15,500 \text{ CF} \\ = 575 \text{ CY}$$

CRUSHED STONE SURFACE (6" thick)

$$(.5' \times 20' \times 300') + (.5' \times 10' \times 20') = 3100 \text{ CF}$$

125-
 $\approx 135 \text{ lb/CF}$

$$135 \text{ lb/CF} \times 3100 \text{ CF} = 418,500 \text{ lbs} \\ = 210 \text{ tons}$$

2) 20' x 20' area around pumphouse

EARTH FILL

$$20' \times 20' \times 3' = 1200 \text{ CF} \\ = 45 \text{ CY}$$

$$\text{TOTAL EARTH FILL} = 620 \text{ CY} \Rightarrow \boxed{700 \text{ CY}}$$

$$\text{TOTAL CRUSHED STONE SURFACE} = 210 \text{ tons} \Rightarrow \boxed{230 \text{ tons}}$$

Drawings

KINGSTON FOSSIL PLANT (KIF) - COAL YARD RUNOFF POND

Calculate the Ordinates to Plot the Cumulative Inflow to the Storage Area for a (100, 50, 25, 10) yr-24 hr Storm

Time (hr)	Rainfall Storms (in)				Conv. to ft	Drainage Area (SF)	Runoff coeff.	Volume			
	100 yr	50 yr	25 yr	10 yr				100 yr	50 yr	25 yr	10 yr
.5	2.505	2.2	2	1.77	0.0833	5795280	0.7	846497	743430	675846	598123
1	3.1	2.8	2.55	2.22	0.0833	5795280	0.7	1047561	946184	861703	750189
2	3.6	3.4	3.2	2.5	0.0833	5795280	0.7	1216522	1148937	1081353	844807
3	4.2	3.75	3.45	2.95	0.0833	5795280	0.7	1419276	1267210	1165834	996872
6	4.9	4.7	4	3.52	0.0833	5795280	0.7	1655822	1588237	1351691	1189488
12	5.9	5.5	4.8	4.2	0.0833	5795280	0.7	1993744	1858575	1622029	1419276
24	6.6	6.3	5.7	4.8	0.0833	5795280	0.7	2230290	2128913	1926160	1622029

RAILROAD AREA

293250	0.5	30596	26870	24428	21619
293250	0.5	37863	34199	31145	27115
293250	0.5	43970	41527	39084	30535
293250	0.5	51298	45802	42138	36031
293250	0.5	59848	57405	48855	42993
293250	0.5	72062	67176	58627	51298
293250	0.5	80611	76947	69619	58627

TOTAL

877092	770301	700273	619742
1085424	980383	892848	777303
1260492	1190465	1120437	875342
1470574	1313012	1207971	1032903
1715670	1645642	1400547	1232481
2065806	1925752	1680656	1470574
2310902	2205861	1995779	1680656

KINGSTON FOSSIL PLANT - (KIF)

RAINFALL DATA (US Weather Bureau Technical Paper No. 40)

Rainfall Duration (hr)	100 yr Rainfall Depth (in)	Rainfall rate (in/hr)	50 yr Rainfall Depth (in)	Rainfall rate (in/hr)	25 yr Rainfall depth (in)	Rainfall rate (in/hr)	10 yr Rainfall depth (in)	Rainfall rate (in/hr)
0.5	2.505	5.01	2.2	4.4	2	4	1.77	3.54
1	3.1	3.1	2.8	2.8	2.55	2.55	2.22	2.22
2	3.6	1.8	3.4	1.7	3.2	1.6	2.5	1.25
3	4.2	1.4	3.75	1.25	3.45	1.15	2.95	0.983
6	4.9	0.817	4.7	0.783	4	0.667	3.52	0.587
12	5.9	0.492	5.5	0.458	4.8	0.4	4.2	0.35
24	6	0.275	6.3	0.263	5.7	0.238	4.8	0.2

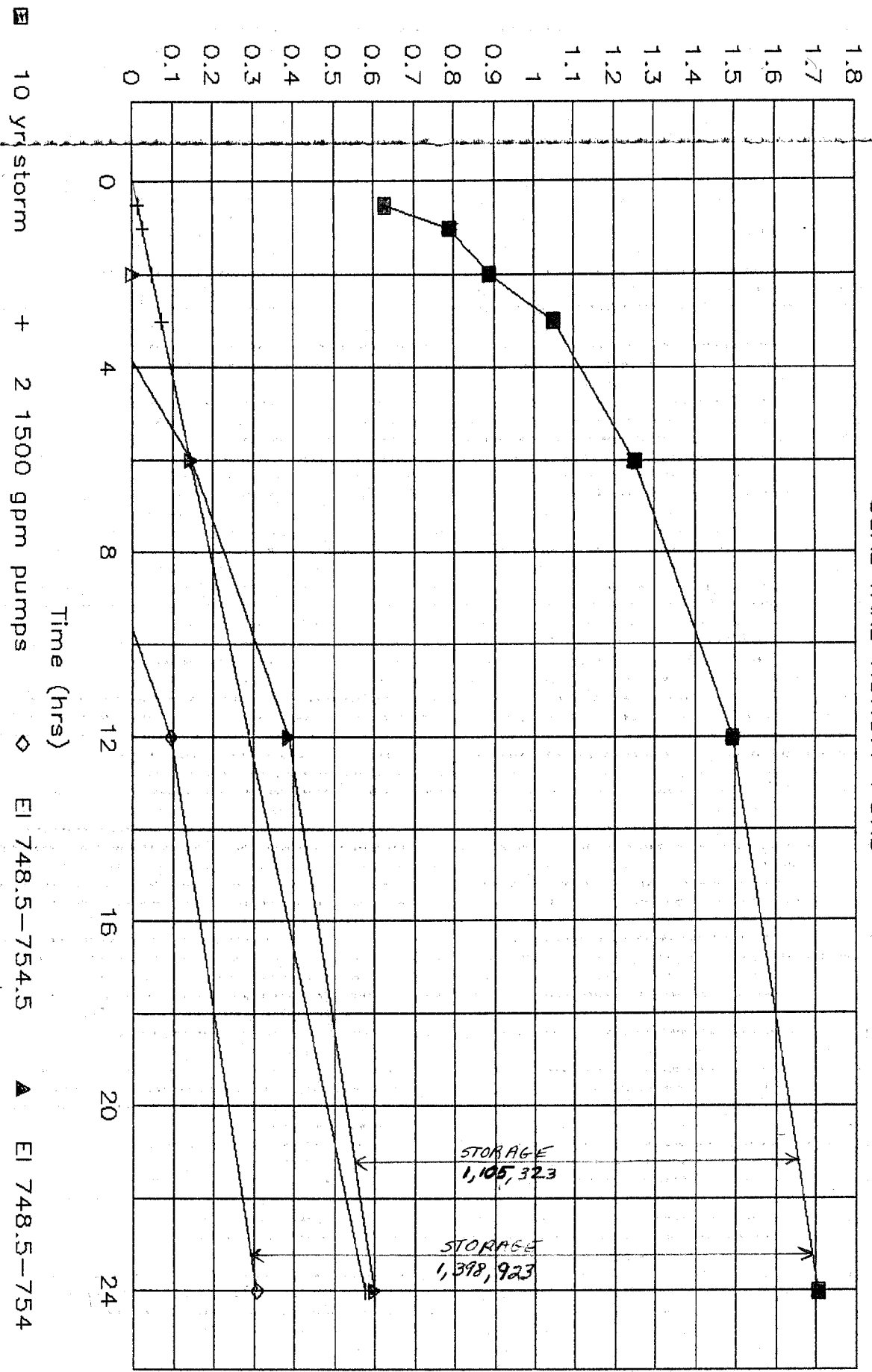
Inches

1 yr 24hr	2.6
2 yr 24hr	3.25
5 yr 24hr	3.9

CLM
4-21-94

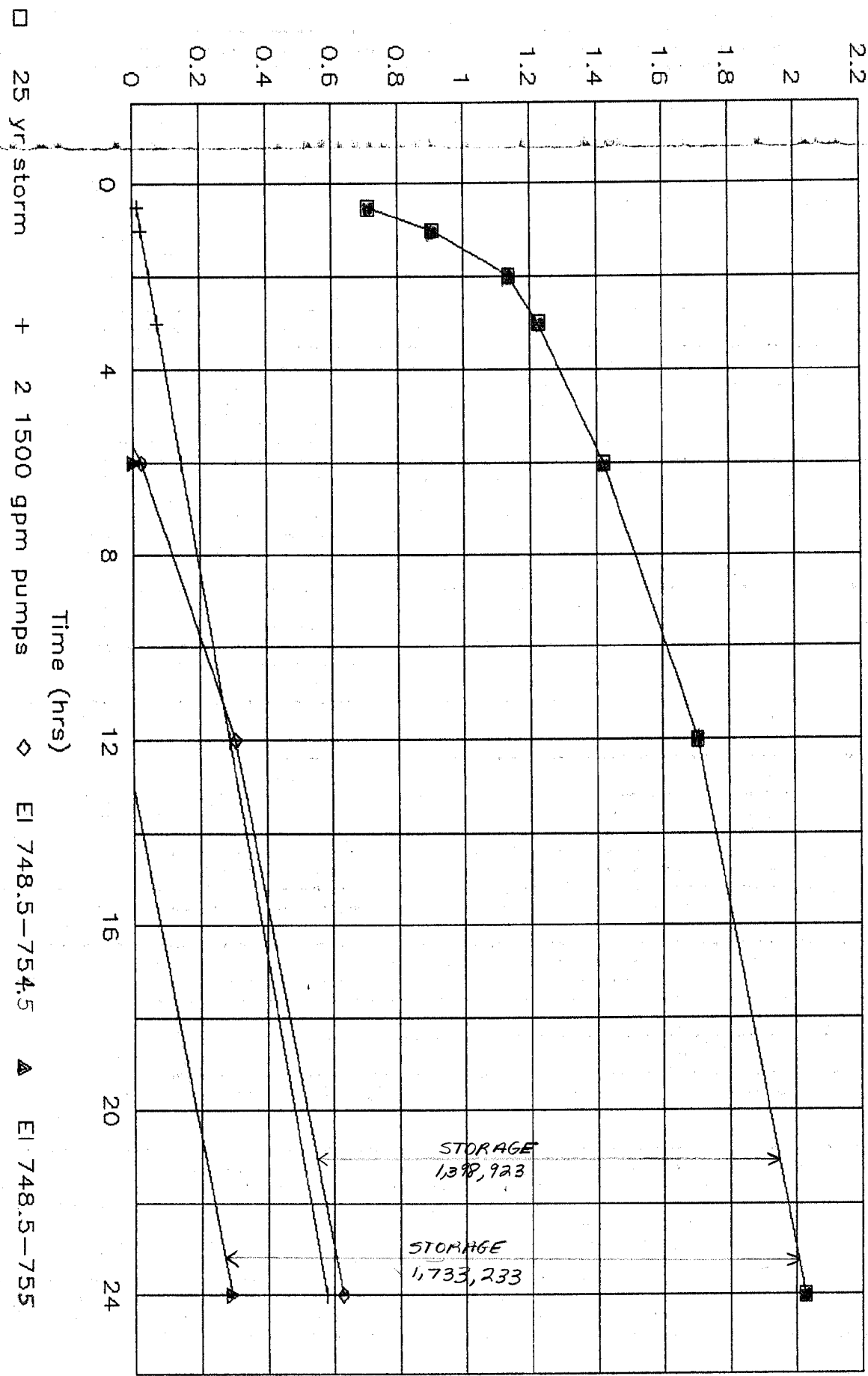
Cumulative Inflow of Pond (cf) (Millions)

KINGSTON FOSSIL PLANT COAL YARD RUNOFF POND



Cumulative Inflow of Pond (cf) (Millions)

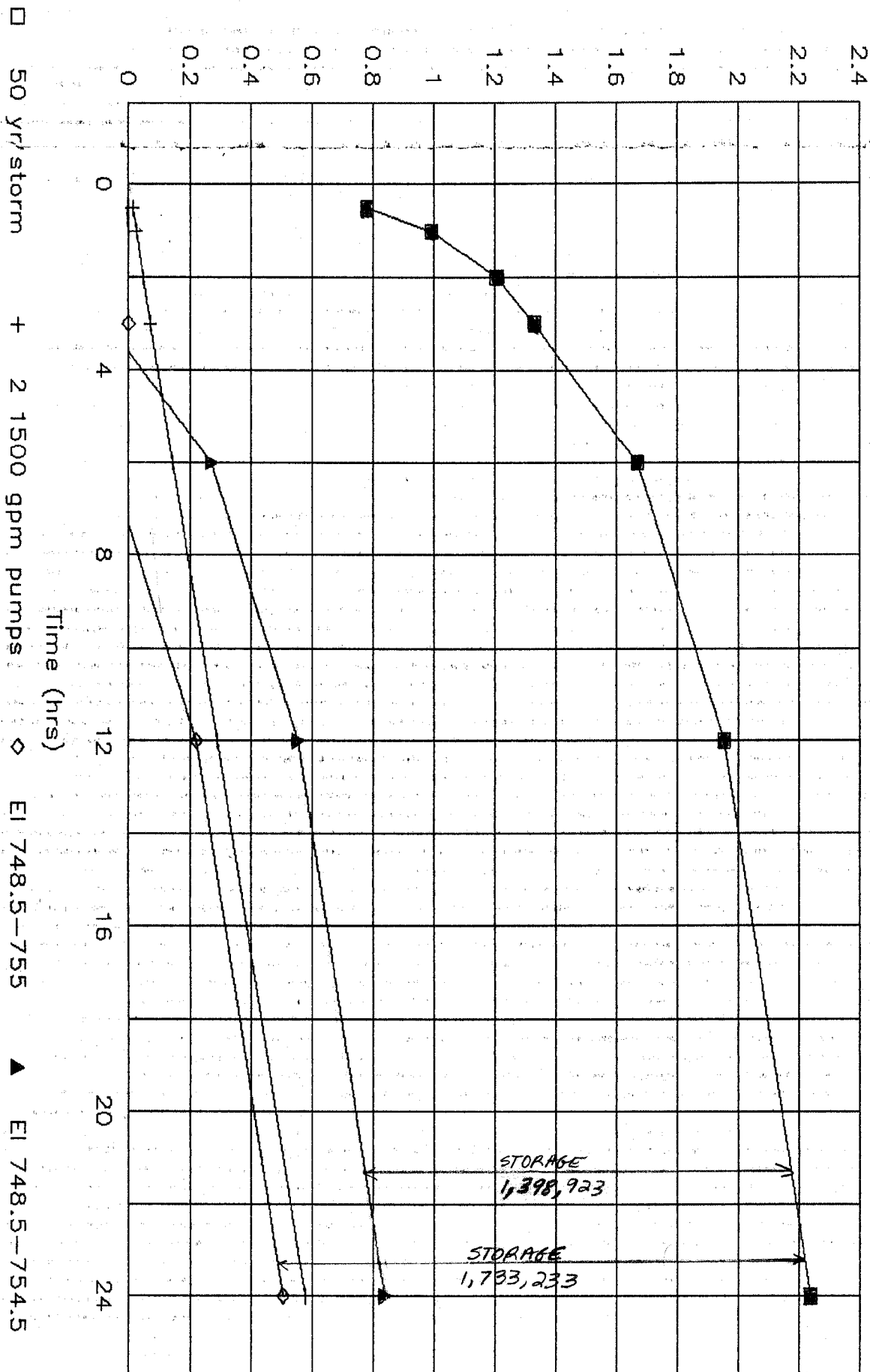
KINGSTON FOSSIL PLANT COAL YARD RUNOFF POND



Cumulative inflow of Pond (ct)
(Millions)

CLM
5-10-94

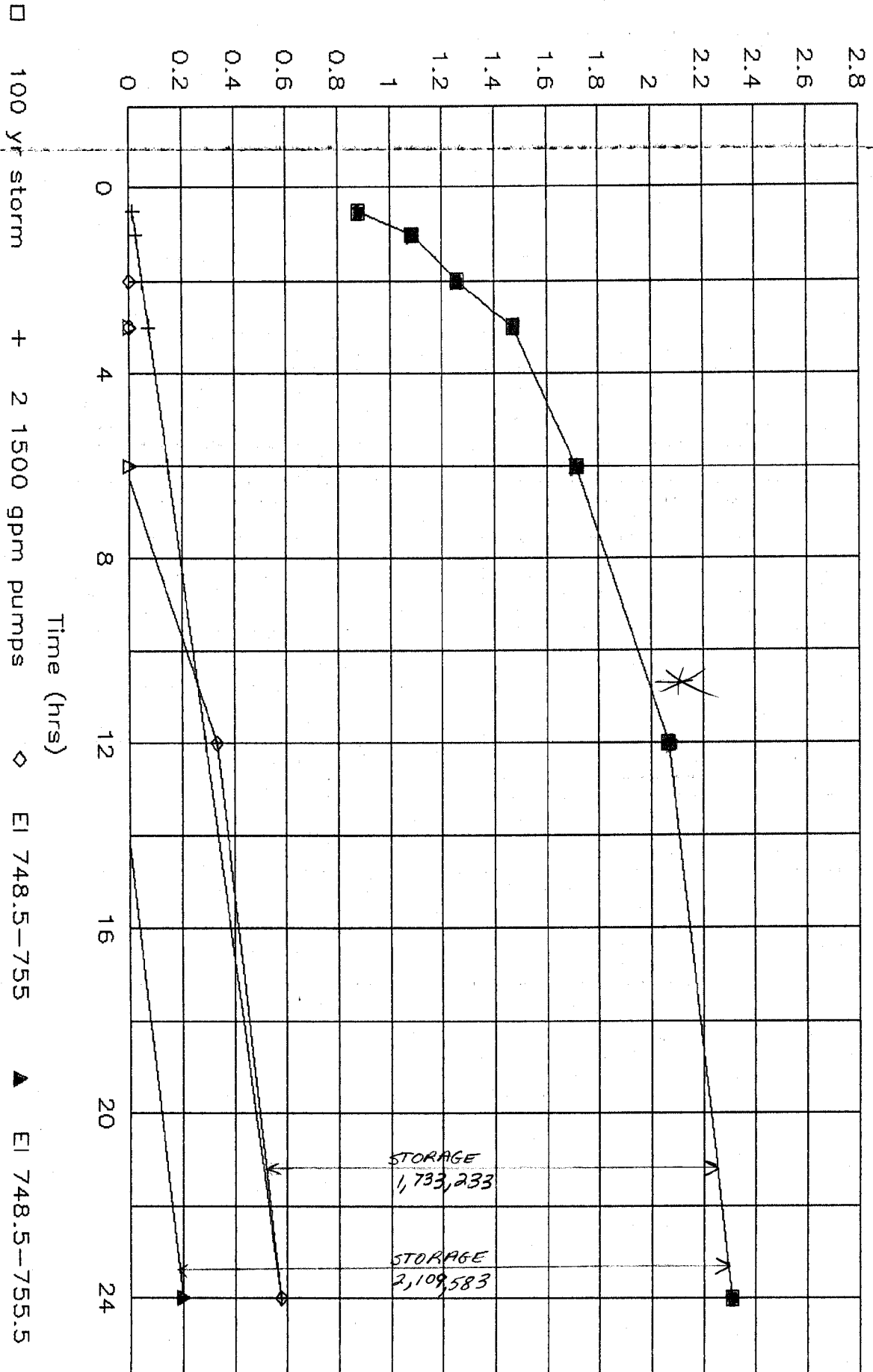
KINGSTON FOSSIL PLANT COAL YARD RUNOFF POND



CLM
5-16-94

Cumulative Inflow of Pond (cf) (Millions)

KINGSTON FOSSIL PLANT COAL YARD RUNOFF POND



KINGSTON FOSSIL PLANT
 COAL YARD RUNOFF POND

SHEET _____ OF _____

COMPUTED CLM DATE 5-5-94

CHECKED _____ DATE _____

Calculate Storage Elevation (748.5 - 755.5)

@ 748.5 748 20,650 25863 = 748.5
 749 31,075

<u>EI</u>	<u>AREA(SF)</u>	<u>AVG AREA(SF)</u>	<u>DEPTH(FT)</u>	<u>VOLUME(CF)</u>
748.5	25863			
		28469	.5	14,235
749	31075			
		36288	1	36,288
750	41500			
		137450	2	274,900
752	233,400			
		389,950	2	779,900
754	546,500			
		627,900	1	627,900
755	709,300			
				→ 1,733,233 CF
		752,700	.5	376,350
755.5	796,100			
		833,050	.5	→ 2,109,583 CF
				416,525
756	870,000			→ 2,526,108 CF

TVA 11030 (WM-7-75)

Calculate Storage Elevation (10 yr) (748.5 - 754.5)

<u>EI</u>	<u>AREA (SF)</u>	<u>AVG AREA (SF)</u>	<u>DEPTH (FT)</u>	<u>VOLUME (CF)</u>
748.5	25863	28469	.5	14,235
749	31075	36288	1	36,288
750	41500	137450	2	274,900
752	233,400	389,950	2	779,900
754	546,500	587,200	5	293,600
754.5	627,900			
				1,398,923

KINGSTON FOSSIL PLANT
COAL YARD RUNOFF POND

SHEET _____ OF _____

COMPUTED CLM DATE 5-6-94

CHECKED _____ DATE _____

STORAGE
EL 755

77.61	76.74	00.97
<u>54.80</u>	<u>00.97</u>	<u>77.61</u>
22.81	24.03	23.36

$23.4 \text{ in}^2 = 234,000 \text{ ft}^2$

EL 755

91.95	44.44	96.25
<u>44.44</u>	<u>96.65</u>	<u>48.97</u>
47.51	47.179	47.28

$47.53 \text{ in}^2 = 475,300 \text{ ft}^2$

709,300 ft²

EI 755.5

49.50	14.87	43.70
<u>78.95</u>	<u>43.70</u>	<u>73.36</u>
29.45	28.83	29.66

$29.31 \text{ in}^2 = 293,100 \text{ ft}^2$

EI 755.5

22.02	72.06	22.80
<u>72.06</u>	<u>22.80</u>	<u>72.91</u>
50.04	50.74	50.11

$50.30 \text{ in}^2 = 503,000 \text{ ft}^2$

796,100 ft²

@ 756
EST = 875,000 ft²

KINGSTON FOSSIL PLANT COAL YARD RUNOFF POND

Drainage

COMPUTED CLM DATE 5-5-94

CHECKED _____ DATE _____

Meeting @ Kingston on 5/4/94

SAID TO DO AS LITTLE EXCAVATION AS POSSIBLE
use 2 1500gpm pumps w/separate discharge lines

DRAINAGE AREA

Due to PLUGGED PIPES INCREASE IN DRAINAGE AREA

① Railroad tracks
(runoff coeff. = .5)

Sheet M-7

$$\begin{array}{r} 98.34 \\ 15.35 \\ \hline 17.01 \end{array} \quad \begin{array}{r} 15.35 \\ 31.83 \\ \hline 16.48 \end{array} \quad 16.745 \text{ in}^2 = 167,450 \text{ ft}^2$$

Sheet M-6

$$4.43'' \times 2.84'' = 12.58 \text{ in}^2 = \underline{125,800 \text{ ft}^2}$$

(keep separate) DRAINAGE ADJ. 293,250 ft²

② Rest of DRAINAGE AREA

Sheet M-7

$$\begin{array}{r} 03.36 \\ 39.72 \\ \hline 36.36 \text{ in}^2 \end{array} + \frac{75.00}{82.4} + \frac{2.75 \text{ in} \times 7.55 \text{ in}}{7.4 \text{ in}^2} = 20.763 \text{ in}^2$$

$$\begin{array}{l} (-) \frac{4.7 \text{ in} \times 3.1 \text{ in}}{2} \\ = 7.285 \text{ in} \end{array} \Rightarrow \begin{array}{l} 57.248 \text{ in}^2 \\ = 572,480 \text{ ft}^2 \end{array}$$

Sheet M-6

$$\begin{array}{r} 26.87 \\ 42.93 \\ \hline 16.06 \text{ in} \end{array} = 16.06 \text{ in}^2 = 160,600 \text{ ft}^2$$

HARRIMAN QUADRANGLE TOPO

<u>66.19</u>	<u>66.51</u>	<u>66.90</u>	= 7.39 in ²
<u>66.51</u>	<u>66.90</u>	<u>67.29</u>	
.38	.39	.39	

1 in = 2000'
1 in² = 4,000,000 ft²
= 1,560,000 ft²

TOTAL DRAINAGE ADJUSTMENT

$$= 2,293,080 \text{ ft}^2$$

El ~~747~~^{changed} to 754.5 (to meet 7.5' max to pump start)

VOLUME FOR STORAGE (NO EXCAVATION)

<u>EI</u>	<u>AREA (SF)</u>	<u>AVG AREA (SF)</u>	<u>DEPTH (FT)</u>	<u>VOLUME (CF)</u>
747	18325	19488	1	19488
748	20650	31075	2	62150
750	41500	137,450	2	274900
752	233,400	389,950	2	779900
754	546500	597,000	.5	298,500
754.5	647,500			<u>1,434,938</u> CF

to 754' = 1,136,438 CF

KINGSTON FOSSIL PLANT
 COAL YARD RUNOFF POND

SHEET _____ OF _____
 COMPUTED CLM DATE 4-26-94
 CHECKED _____ DATE _____

E1 754.5

Area 1	93.98	14.65	Area 2	89.01	33.18
	<u>14.65</u>	35.06		<u>33.18</u>	<u>77.44</u>
	20.67	<u>30.41</u>		44.16	44.26
		20.54 in ²			44.21 in ²

64.75 in²
 = 647,500 ft²

Calculate TOTAL VOLUME TO E1 754.5

745 up to 754 (previously calculated) = 1,168,700 CF

<u>E1</u>	<u>AREA (SF)</u>	<u>AVG AREA (SF)</u>	<u>DEPTH (FT)</u>	<u>VOL (CF)</u>
754	546,500	597,000	.5	298,500
754.5	647,500			

TOTAL = 1,168,700_{CF} + 298,500_{CF} = 1,467,200 CF

KINGSTON FOSSIL PLANT
COAL YARD RUNOFF POND

SHEET _____ OF _____

COMPUTED CLM DATE 4-23-94

CHECKED _____ DATE _____

Volume for Storage (continued) actual

<u>E1</u>	<u>AREA(SF)</u>	<u>AVG AREA(SF)</u>	<u>DEPTH(FT)</u>	<u>VOLUME(CF)</u>
745	14,200			
		15,100	1	15,100
746	16,000			
		18,325	2	36,650
748	20,650			
		31,075	2	62,150
750	41,500			
		137,450	2	274,900
752	233,400			
		389,950	2	779,900
754	546,500			
		<u>Total</u>		<u>1,168,700</u> CF

KINGSTON FOSSIL PLANT
 COAL YARD RUNOFF POND

SHEET _____ OF _____

COMPUTED CLM DATE 4-22-94

CHECKED _____ DATE _____

VOLUME FOR STORAGE actual

E1 745 to E1 754

E1 745

20.80	23.49	1.41 in ² = 14,200 ft ²
<u>22.20</u>	<u>24.91</u>	
1.4	1.42	

E1 746

24.80	26.41	1.60 in ² = 16,000 ft ²
<u>26.41</u>	<u>28.00</u>	
1.61	1.59	

E1 748

28.47	26.41	2.065 in ² = 20,650 ft ²
<u>30.54</u>	<u>28.47</u>	
2.07	2.06	

E1 750

77.10	81.25	85.37	4.15 in ² = 41,500 ft ²
<u>81.25</u>	<u>85.37</u>	<u>89.56</u>	
4.15	4.12	4.19	

E1 752

(1) 0612	(2) 62.89	82.67	= 23.34 in ² = 233,400 ft ²
<u>0996</u>	82.67	<u>63.45</u>	
3.84	19.78	19.22	

E1 754

(1) 74.10	08.06	(2) 80.34	49.59	(3) 86.06	00.40
<u>01.26</u>	<u>34.19</u>	<u>66.75</u>	<u>63.48</u>	<u>00.40</u>	<u>14.87</u>
27.16	26.13	13.59	13.89	14.34	14.47
26.65		13.59		14.41	
54.65 in ² = 546,500 ft ²					

TVA 11030 (WM-7-75)

DRAINAGE AREA CALCULATIONS

Sheet 461K530 M-8

Area 1	43.02	73.10	02.05
	<u>73.10</u>	<u>02.05</u>	<u>31.80</u>
	30.08	28.95	29.75

Drainage

AVG = 29.59 in² => 295,900 ft²

Area 2

18.18	44.86
<u>44.86</u>	<u>72.18</u>
26.68	27.32

AVG = 27 in² => 270,000 ft²

565,900 ft²

Sheet 461K530 M-7

Area 1

80.41	00.29	60.36
<u>40.35</u>	<u>60.36</u>	<u>20.09</u>
40.06	39.93	40.27

AVG = 40.09 in² => 400,867 ft²

Area 2

10.10	09.50	09.50
<u>59.89</u>	<u>59.50</u>	<u>59.50</u>
49.79	50.00	50.00

AVG = 49.90 in² => 498,950 ft²
899,817 ft²

DRAINAGE AREA CALCULATIONS

Sheet 461K530 L-7

Area 1	91.78	23.49
	<u>14.64</u>	<u>45.71</u>
	22.86	22.22

AVG = 22.54 in² => 225,400 ft²

Area 2

05.46	40.21
<u>40.21</u>	<u>75.04</u>
34.75	34.83

AVG 34.79 in² => 347,900 ft²
573,300 ft²

Sheet 461K530 L-8

Area 1

36.53	75.10	84.23
<u>84.23</u>	<u>22.44</u>	<u>31.77</u>
47.70	47.34	47.54

AVG 47.53 in² => 475,300 ft²

Area 2

11.62 × 6.59 = 76.58 in²
in in

- .75 in (.53 in) / 2 = 76.38 in² => 763,800 ft²

Area 3

81.76	58.65	36.94
<u>58.65</u>	<u>36.94</u>	<u>14.55</u>
23.11	21.77	22.36

AVG 22.41 in² => 224,100 ft²
1,463,200 ft²