

APPENDIX B: CARBON DIOXIDE CAPTURE TECHNOLOGY SHEETS
ADVANCED COMPRESSION

THERMAL INTEGRATION OF CO₂ COMPRESSION PROCESSES WITH COAL-FIRED POWER PLANTS EQUIPPED WITH CARBON CAPTURE

Primary Project Goals

Lehigh University is developing systems analysis models to study the benefits of improved thermal integration for coal-fired power plants equipped with post- or oxy-combustion carbon dioxide (CO₂) capture systems.

Technical Goals

- Gather technical and performance information from compressor manufacturers and the technical literature in order to calculate compressor power requirements, performance of interstage heat transfer, and interstage pressure changes.
- Develop and validate ASPEN Plus models of coal-fired power plants with solvent-based post-combustion CO₂ capture to simulate the effects of different thermal integration options on power plant efficiency and net power output.
- Develop and validate ASPEN Plus models of oxy-combustion coal power plants to simulate the effects of different thermal integration options on power plant efficiency and net power output.

Technical Content

Coal-based power plants equipped for CO₂ capture require a compression system to increase the pressure of the CO₂ to the level needed for geological storage [approximately 2,200 pounds per square inch absolute (psia)]. In addition to its relatively high capital cost, the CO₂ compression system requires a significant amount of auxiliary power for operation. The technology options available for CO₂ compression include:

- A multistage in-line centrifugal compressor with interstage and post-compression cooling.
- A multistage integrally geared centrifugal compressor with interstage cooling.
- A multistage supersonic shockwave compressor with interstage and post-compression cooling.
- A compression process involving gas phase compression to approximately 200 psia, cryogenic cooling through the two-phase region, and increase in pressure of the liquid CO₂ to the final pressure using a liquid cryogenic pump.

For some of these technology options, there is the potential for utilization of waste heat from the CO₂ compressors within the power plant. This project uses first-principle engineering analyses and computer simulations to determine the increase in power output and improvement in net unit heat rate which could occur by thermal integration of the CO₂ compression process with the CO₂ capture system, boiler, and turbine cycle. The study includes gathering information on compressor internal geometry and compressor stage efficiencies. The aerodynamic conditions and flow

Technology Maturity:
Systems analysis models

Project Focus:
Thermal Integration of CO₂ Compression Processes

Participant:
Lehigh University

Project Number:
FE0002146

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Partners:
None

Performance Period:
10/1/09 – 6/29/12

geometry change from the low-pressure to high-pressure end of the compressor, very likely resulting in significant variations in isentropic stage efficiency from inlet to outlet. Correct values for isentropic stage efficiency are needed in order to obtain realistic values of compressor power and CO₂ exit temperature for each stage. In addition, fluid flow and heat transfer analyses will be performed to estimate CO₂ pressure drop in the intercoolers and the exit temperature of the cooling fluid as a function of coolant flow rate. While the literature suggests that most CO₂ compressors are air-cooled, analyses will be performed to determine the feasibility of using liquid-cooled heat exchangers for interstage cooling.

Once the analyses of the compressors are complete, the results will be linked to models of the power plant for analysis of various thermal integration options. The compressor and power plant simulations will be performed using the ASPEN Plus software. Each of the following cases will be analyzed using bituminous, Powder River Basin (PRB), and lignite coals:

- Pulverized coal-fired boiler with post-combustion solvent-based capture systems using both amine and ammonia scrubbers.
- Oxy-combustion pulverized coal boiler.

The thermal integration options which will be considered include pre-drying of low-rank coals, regeneration of CO₂ solvent, and boiler feedwater preheating. Table 1 presents the matrix of analyses which will be performed.

Table 1: Systems Analysis Matrix for CO₂ Compression Heat Integration

| Use of Recovered Heat From CO ₂ Compressor | | | |
|-------------------------------------------------------------|-----------------------|------------------------------------|--------------------------|
| Integration Method | Pre-Dry Low Rank Coal | Regenerate CO ₂ Solvent | Preheat Boiler Feedwater |
| Post-Combustion Solvent-Based CO₂ Capture | | | |
| Bituminous | No | Yes | Yes |
| PRB | Yes | Yes | Yes |
| Lignite | Yes | Yes | Yes |
| Oxy-Combustion | | | |
| Bituminous | No | No | Yes |
| PRB | Yes | No | Yes |
| Lignite | Yes | No | Yes |

Technology Advantages

- Determine the best way to utilize waste heat from CO₂ compression.
- Improve power plant efficiency and increase the net power output.
- Reduce capital and operating cost for CO₂ capture and compression systems.

R&D Challenges

Implementation of the thermal integration opportunities as cost-effective technology options.

Results To Date/Accomplishments

- Obtained compressor design and performance information from CO₂ compressor vendors.
- Compared analysis algorithms to vendor data and verified analytical results.
- Initiated analysis of heat transfer and pressure drops for the pre-compression and interstage coolers.
- Developed ASPEN Plus models to analyze the effects of thermal integration on post-combustion capture and oxy-combustion systems.

Next Steps

- Complete analyses of thermal integration options for post-combustion capture system.
- Complete analyses of thermal integration options for oxy-combustion system.
- Complete analyses of pre-compression and interstage coolers.

Available Reports/Technical Papers/Presentations

No reports, technical papers, or presentations are yet available.

RAMGEN SUPERSONIC SHOCK WAVE COMPRESSION AND ENGINE TECHNOLOGY

Technology Maturity:
Pilot, 1,680 tonnes/day CO₂

Primary Project Goals

Ramgen Power Systems is designing and developing a unique compressor technology based upon aerospace shock wave compression theory for use as a carbon dioxide (CO₂) compressor. A shock wave-based gas turbine engine is also being developed.

Project Focus:
Shock Wave Compression

Participant:
Ramgen Power Systems, LLC

Technical Goals

Phase I:

- Complete testing of a high-pressure ratio (10:1) air compressor rotor for the Ram 2 program.
- Demonstrate the feasibility of high-pressure shock wave compression.
- Develop and detail a viable commercialization path.

Project Number:
FE0000493
NT42651

NETL Project Manager:
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Phase II:

- Perform critical success factors risk reduction validation and test program to identify and reduce technical risk areas.
- Complete general assessment, preliminary, and final design of a demonstration CO₂ supersonic shock compressor approximately 13,000 hp in size.

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Technical Content

Shock Wave CO₂ Compressor

Ramgen Power Systems is developing a supersonic shock wave compression technology, similar in concept to an aircraft's ramjet engine, for use in a stationary compressor. Ramgen's compressor design, known as a Rampressor, features a rotating disk that operates at high peripheral speeds to generate shock waves that compress the CO₂. Compared to conventional compressor technologies, shock compression offers several potential advantages: high compression efficiency; high, single-stage compression ratios; opportunity for waste heat recovery; and low capital cost. For example, Ramgen's shock compression has the potential to develop compression ratios from 2.0 to 15.0 per stage with an associated adiabatic efficiency of 85–90%. For CO₂ applications, Ramgen anticipates using a nominal, two-stage 100:1 compression ratio, featuring a matched pair of 10:1 compression stages with an intercooler located between the stages. Prototype testing completed in 2007 achieved a 7.8:1 compression ratio.

When shock waves pass through a gas they cause a localized compression. Figure 1 shows that the rotating rotor rim has small, shallow angles which, when rotating at high speeds, will produce supersonic shock waves both prior to and post-peak. These shock waves, modeled in the 3-D Euler Computational Fluid Dynamics (CFD) image shown, are first oblique, then normal. Additionally, strakes (ridges) are incorporated into the design of the rotor to form sidewalls. The strakes are utilized as shock compression ducts, as well as to separate high-pressure discharge from low-pressure suction. The combination of shocks and strakes result in a compressed fluid delivered from a stationary discharge duct with compression efficiencies comparable to conventional industrial turbo-compressors, but with much higher single-stage pressure ratios and therefore higher quality heat of compression that combine to deliver significant installed and operational cost savings versus existing turbo-compressors.

Partners:
Dresser-Rand

Performance Period:
5/10/06 – 12/31/13

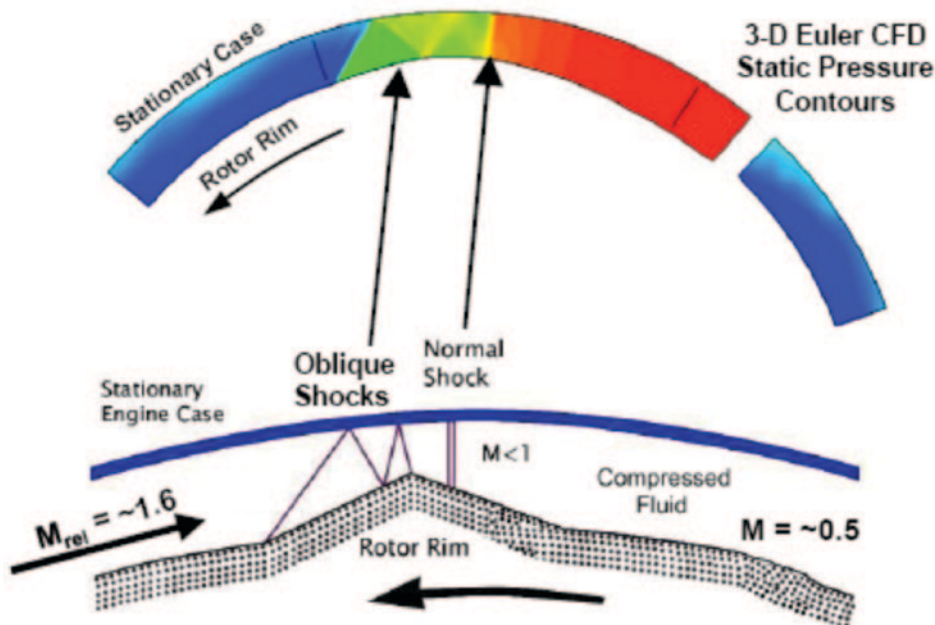


Figure 1: Schematic of Rotor Rim and Engine Case and 3-D Euler CFD Image Depicting Shock Wave Behavior

Two stages of compression are used with an intercooler located between the stages to optimize the efficiency of the compression process. Figure 2 shows the energy required as shaft work and the thermal energy lost to the cooling stream for a 200-MW coal plant with 90% CO₂ capture. The numbers found in the figure represent a stage in the process; each stage is driven independently through an external gearbox.

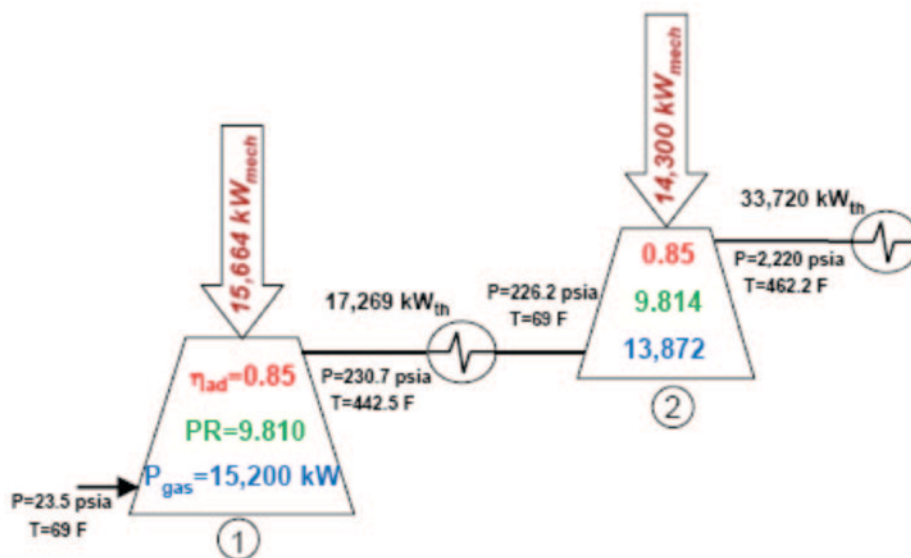


Figure 2: Series Process Schematic

As seen in Figure 2, the total shaft power is 29,964 kW_{mech}, which corresponds to a heat of compression of 50,989 kW_{th}. Approximately 28,986 kW_{th} of the heat of compression lost is recoverable down to 93 °C (200 °F).

Shock Wave Gas Turbine Engine

Ramgen is also developing a unique shock wave-based gas turbine engine that is expected to significantly improve energy efficiency. The Ramgen Integrated Supersonic Component Engine (ISCE) consolidates the compressor, combustor, and turbine of a conventional gas turbine into a single wheel that operates based on the same Brayton thermodynamic cycle as a conventional gas turbine; however, the mechanical implementation of the process is quite different. One important advantage is that because the compression, combustion, and expansion processes are all integrated into a single constant speed rotor, there is no physical acceleration of the rotating components required as the system transitions from idle to full power. The output torque and power are modulated from the full-speed, no load condition to the full-speed, full power condition by adjusting the fuel flow. As a result, the system can transition from idle to full power as quickly as the fuel flow can be adjusted. Testing has demonstrated a transition from combustor heat release levels consistent with a power variation from idle (pilot fuel only) to full power (full fuel/air premix) in periods as short as 150–200 milli-seconds (ms). The ISCE will have the ability to load follow from idle to full power in time scales as short as a few hundred ms compared with a response rate of 7–10 seconds for most intermediate sized gas turbine electric power generating systems.

The initial proof of concept Ramgen engine used an un-shrouded rotor configuration mounted on a single high-speed shaft driving a generator/starter motor through a speed reducing gearbox. The ISCE system will incorporate a fully shrouded flowpath power-wheel configuration. The power wheel now proposed will be directly supported by a magnetic bearing system and will incorporate permanent magnets into the inner diameter of the rotor. This rotor mounted magnet system will rotate around a central stator winding to form an integrated high-speed permanent magnet motor/starter system on the inner hub of the power wheel. This configuration will eliminate the need for a speed-reducing gearbox and the discrete separate motor/generator. This consolidation will result in a significantly more compact, lightweight, low-cost generation system compared to any other conventional turbo-generator system. This integrated power-wheel system is illustrated in Figure 4 and shows the engine feature of a propulsive flowpath that is fully shrouded and formed by a series of nested rim segments supported by a metal-matrix or polyimide composite outside diameter support ring.

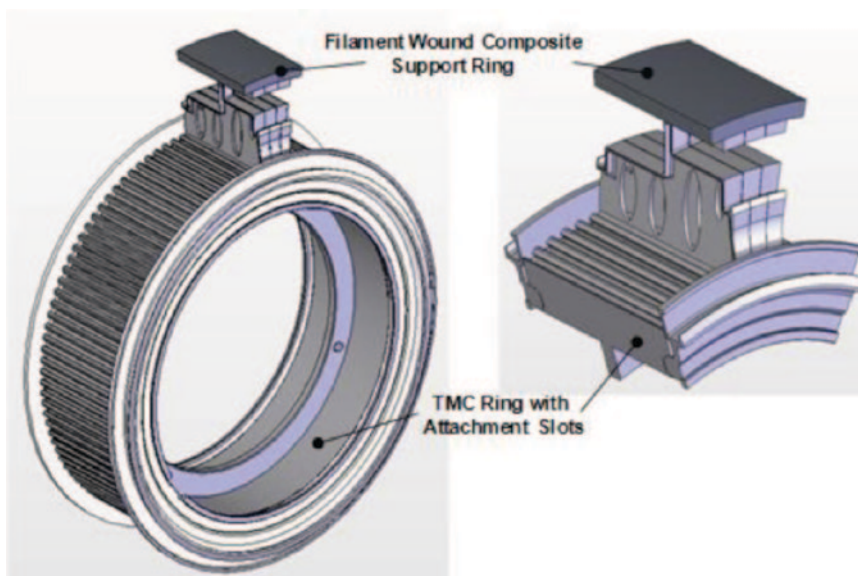


Figure 4: Integrated Power Wheel

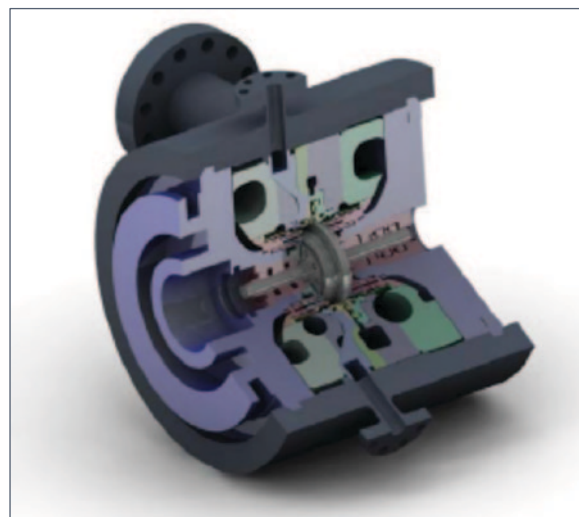


Figure 3: Cross Sectional Model of a 1/10th Scale Single Stage Supersonic Shock Wave Compressor

Technology Advantages

- Competitive operating efficiency and reduced installed capital cost (approximately 50%) over multi-stage bladed turbo compressors.
- High-stage discharge temperature enables cost-effective recovery of heat of compression.
 - Improves carbon capture and sequestration (CCS) efficiency.
 - Reduces power plant de-rate.

R&D Challenges

- Complicated shock wave aerodynamics on the flowpath requires intensive computing capabilities and model development.
- High rotational speeds and the resulting stresses can result in expensive rotor manufacturing techniques.
- High-pressure ratio compressors yield high rotor thrust loads on bearings and structure.

Results To Date/Accomplishments

- Finalized the CO₂ compressor rotor and static hardware geometry.
- Completed the preliminary conceptual design of the CO₂ compressor.
- Completed flowpath validation test conceptual design review.
- Completed CO₂ compressor demonstration unit feasibility study.
- Prepared a detailed systems analysis of the CO₂ compression technology.
- Prepared a rigorous comparative economic analysis based on the systems analysis of the CO₂ compressor.
- Achieved breakthrough rotor pressure ratio of approximately 7.9:1 in air.
- Demonstrated tip speeds up to ~2,200 ft/s and M_{rels} up to ~2.7.
- Successfully modeled full flowpath 3-D viscous CFD.
- Matched performance prediction/design tools to test.
- Obtained benign surge characteristics.
- Gathered data for preliminary compressor maps.
- Developed and demonstrated bearing designs suitable for product application.
- Completed CO₂ compressor stage configuration simulations.
- Completed CO₂ compressor preliminary design review.

Next Steps

- Improve understanding of the supersonic aerodynamics needed to achieve product performance levels in the CO₂ compressor.
- Continue to develop high-speed performance computing capability at Oak Ridge National Laboratory.
- Finalize design of the rotor and all other rig components and systems.
- Fabricate and retrofit the inlet guide vanes and diffuser.
- Install and test 13,000 hp CO₂ compressor.
- Complete ISCE preliminary design review.
- Test ISCE subcomponents.

Available Reports/Technical Papers/Presentations

General project information is available on DOE/NETL website at: <http://www.netl.doe.gov/technologies/coalpower/ewr/co2/co2compression/supersonic.html>

“CO₂ Compression Using Supersonic Shock Wave Technology,” Annual NETL CO₂ Capture Technology for Existing Plants R&D Meeting, Pittsburgh, PA, September 2010, <http://www.netl.doe.gov/publications/proceedings/10/co2capture/index.html>

“CO₂ Compression Using Supersonic Shock Wave Technology,” Annual NETL CO₂ Capture Technology for Existing Plants R&D Meeting, Pittsburgh, PA, May 2009, <http://www.netl.doe.gov/technologies/coalpower/ewr/co2/co2compression/supersonic.html>

“Ramgen Power Systems Low-Cost, High-Efficiency CO₂ Compressor,” Seventh Annual Conference on Carbon Capture and Sequestration, May 2008, <http://www.netl.doe.gov/technologies/coalpower/ewr/co2/co2compression/supersonic.html>

NOVEL CONCEPTS FOR THE COMPRESSION OF LARGE VOLUMES OF CO₂

Primary Project Goals

Southwest Research Institute (SwRI) is developing two novel compression technology concepts to reduce carbon dioxide (CO₂) compression power requirements by 35% compared to conventional compressor designs. The first concept is a semi-isothermal compression process where the CO₂ is continually cooled using an internal cooling jacket rather than using conventional inter-stage cooling. The second concept involves the use of refrigeration to liquefy the CO₂ so that its pressure can be increased using a pump rather than a compressor. The project includes prototype testing and a full-scale demonstration of each concept.

Technical Goals

- Conduct thermodynamic and economic analysis to determine the preferred CO₂ state for compression.
- Identify and evaluate intercooling concepts.
- Develop preliminary intercooling design.
- Calculate total potential energy savings.
- Complete a comprehensive thermodynamic and cost analysis of an integrated gasification combined cycle (IGCC) plant incorporating the new compression technology.
- Design a single-stage compressor test rig based on the analyses and design studies.
- Design, fabricate, and test a multi-stage pump test rig based on the analyses and design studies.

Technical Content

In the first concept, semi-isothermal compression, the gas is continually cooled after each stage in the path through the compressor. A cooling jacket insert is used in the diaphragm of each stage to provide continuous cooling. Figure 1 shows a design for an internally cooled compressor. The flow of the CO₂ is shown in red, while the cooling liquid is shown in blue.

In the second concept, compression is achieved by a combination of partial compression, liquefaction, and pumping. The liquefaction process utilizes a refrigeration system to condense CO₂ at 250 pounds per square inch gauge (psig) and -12 °F. The liquid CO₂ is then pumped from 250 to 2,200 psig. The primary power requirements are the initial compression required to boost the CO₂ to approximately 250 pounds per square inch absolute (psia) and the refrigeration power required to liquefy the gas. The pumping power to boost the pressure to pipeline supply pressure is minimal after the CO₂ is liquefied.

SwRI examined a number of different compression options to find the ones that would consume the least amount of power. Figure 2 shows how two hypothetical compression processes can achieve the same pressure, but still consume different quantities of power. The isothermal compression, even at 60% efficiency, is preferable to isentropic compression at 100% efficiency. Figure 3 shows the pressure/enthalpy curves for six of the options examined by SwRI. Table 1

Technology Maturity:

Pilot-scale, 90 tonnes/hr

Project Focus:

Evaluation of Compression Efficiency Improvements

Participant:

Southwest Research Institute

Project Number:

NT42650

NETL Project Manager:

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Principal Investigator:

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 Southwest Research Institute
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Partners:

Dresser-Rand

Performance Period:

9/28/05 – 12/31/13

presents a description of the compression and cooling technology options and the resultant power requirements for a 400-MW IGCC power plant (~700,000 lb/hr CO₂ stream). The optimal solution combines interstage cooling and a liquefaction approach (Option E.2).

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ADVANCED COMPRESSION

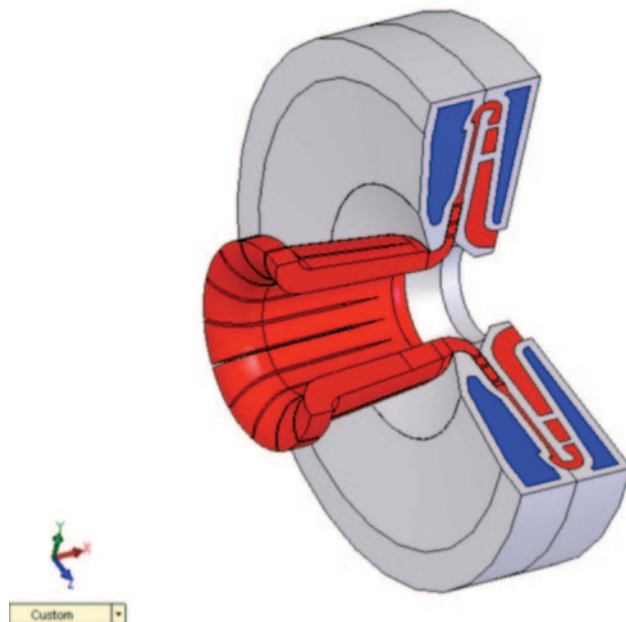


Figure 1: Design for an Internally Cooled Compressor

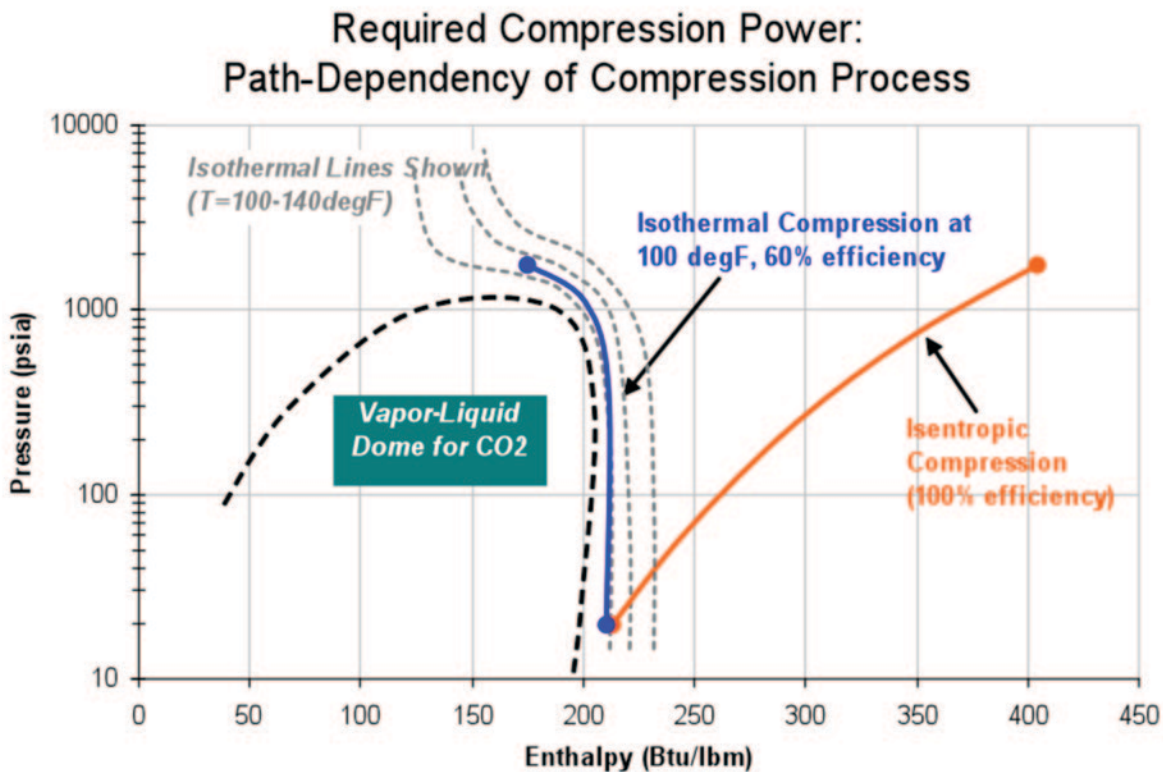


Figure 2: The Path Dependency of Compression Power

Compression Technology Options for IGCC Waste Carbon Dioxide Streams

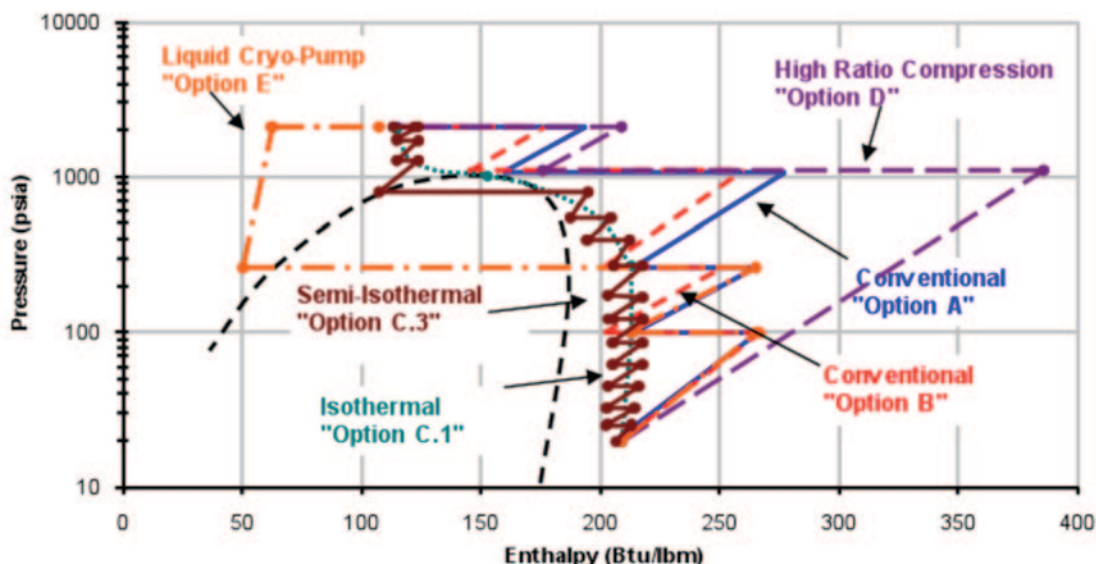


Figure 3: Required Compression Power for the Investigated Technology Options

Table 1: Comparison of Compression Technologies

| Option | Compression Technology | Power Requirements | % Difference from Option A | Cooling Technology |
|--------|-----------------------------------------------------------------------------------------------------------------------|---------------------------------------------------|----------------------------|------------------------------------------------------------------------------------------------------------------|
| A | Conventional Dresser-Rand Centrifugal 10-stage Compression | 23,251 BHP | 0.00% | Air-cool streams between separate stages |
| B | Conventional Dresser-Rand Centrifugal 10-stage Compression with additional cooling | 21,522 BHP | -7.44% | Air-cool streams between separate stages using ASU cool N ₂ stream |
| C.1 | Isothermal compression at 70 °F and 80% efficiency | 14,840 BHP | -36.17% | T _c = 70 °F inlet temp throughout |
| C.4 | Semi-isothermal compression at 70 °F, pressure ratio ~1.55 | 17,025 BHP (required cooling power TBD) | -26.78% | T _c = 70 °F in between each stage. |
| C.7 | Semi-isothermal compression at 100 °F, pressure Ratio ~1.55 | 17,979 BHP (required cooling power TBD) | -22.67% | T _c = 100 °F in between each stage. |
| D.3 | High ratio compression at 90% efficiency—no inter-stage cooling | 34,192 BHP | 47.06% | Air cool at 2,215 psia only |
| D.4 | High ratio compression at 90% efficiency - intercooling on final compression stage | 24,730 BHP | 6.36% | Air cool at 220 and 2,215 psia |
| E.1 | Centrifugal compression to 250 psia, Liquid cryo-pump from 250 to 2,215 psia | 16,198 BHP (includes 7,814 BHP for refrigeration) | -30.33% | Air cool up to 250 psia, refrigeration to reduce CO ₂ to -25 °F to liquify |
| E.2 | Centrifugal compression to 250 psia with semi-isothermal cooling at 100 degF, Liquid cryo-pump from 250 to 2,215 psia | 15,145 BHP (includes 7,814 BHP for refrigeration) | -34.86% | Air cool up to 250 psia between centrifugal stages, refrigeration to reduce CO ₂ to -25 °F to liquify |



Figure 4: Existing Liquid CO₂ Pump Loop Constructed at SwRI

The Option E.2 compression concepts were tested in Phase 2 of the project, which included construction of a dedicated liquid CO₂ flow loop to qualify an industrial turbo-pump. Also, a cooled diaphragm was tested in a compressor test rig that verified successful performance in a single-stage test. Figure 4 shows a photograph of the liquid CO₂ pump loop including the 12-stage vertical pump that was tested. Performance and mechanical testing was performed for a range of speeds, flows, and pressures. The pump met the design conditions with a discharge pressure in excess of 2,200 psig and showed good mechanical behavior. Figure 5 shows the performance map that was measured indicating good correlation to factory measurements using liquid nitrogen.

Figure 6 shows a photograph of the internally cooled compressor diaphragm, which routes cooling fluid through the diaphragm to remove the heat of compression. This prototype was installed into a closed-loop compressor test facility at SwRI and tested for a range of speeds, flows, pressures, and cooling fluid conditions. The testing agreed well with computational fluid dynamics (CFD) predictions for the heat transfer characteristics. Figure 7 shows a comparison between measured and predicted heat exchanger effectiveness for the diaphragm, which shows good agreement. Unlike external heat exchangers, no additional pressure drop occurs between stages. Implementation of the cooled diaphragm technology into a multi-stage application can reduce the power requirements of the compressor by 20% compared to adiabatic compression.

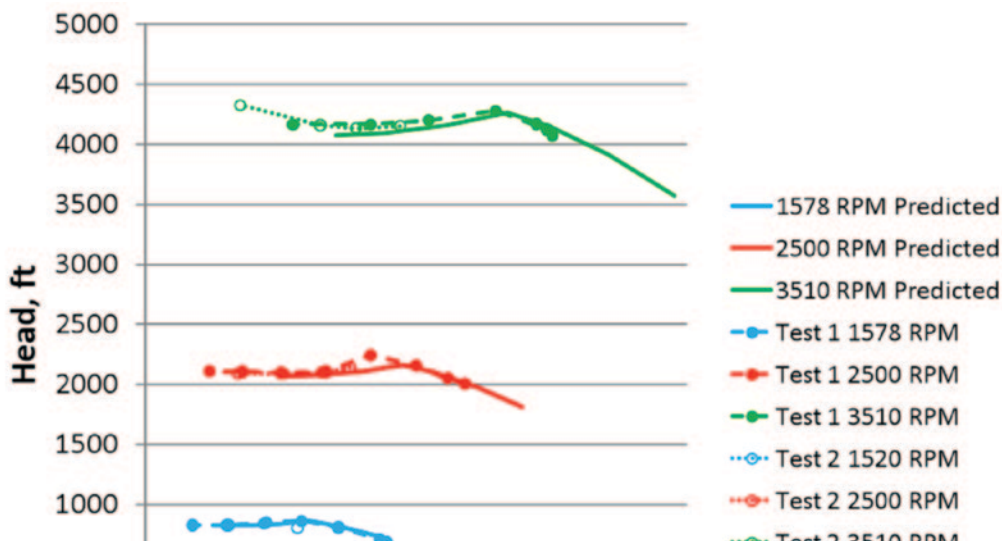


Figure 5: Pump Performance Plot (Head vs. Flow)



Figure 6: Internally Cooled Compressor Diaphragm

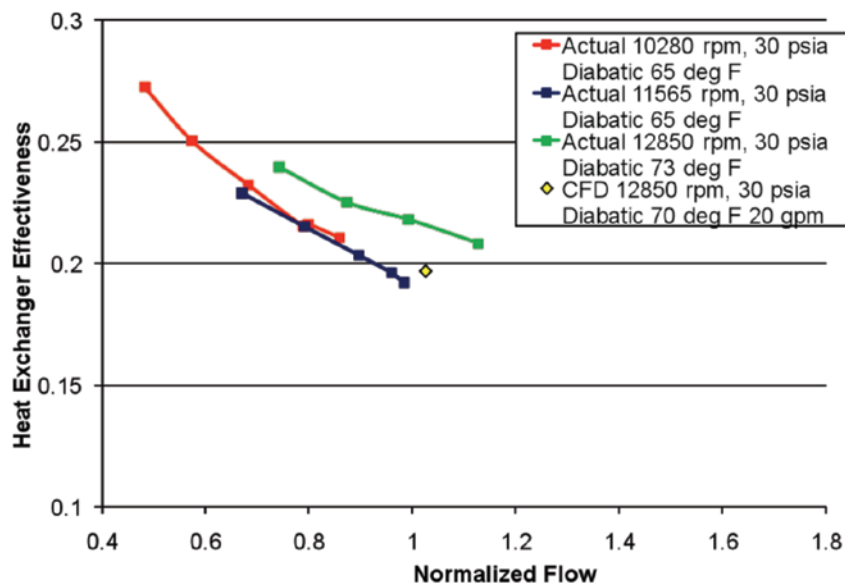


Figure 7: Heat Transfer Effectiveness of CFD and Test Results

Technology Advantages

- New compression process could use up to 35% less power combining semi-isothermal compression, liquefaction, and liquid pumping.
- Applicable to all types of power plants.
- Could result in significant capital savings compared to an integrally geared compressor.
- Pump operating costs will be lower than high-pressure compressor operating costs.

R&D Challenges

- There will be a wide range of CO₂ output from the power plant based on required electrical output.
- CO₂ compression technology must have high reliability.
- IGCC plants contain multiple CO₂ streams at different pressures.

Results To Date/Accomplishments

- Completed a thermodynamic and economic analysis to determine the preferred CO₂ state for compression. The optimal solution combines interstage cooling and a liquefaction approach (Option E.2).
- Designed, constructed, and tested pilot-scale prototype using a liquid CO₂ pumping loop.
 - Pump performed well matching the measured performance during factory testing on liquid nitrogen.
 - Achieved discharge pressure goals.
 - Liquid CO₂ introduced no mechanical issues for the pump.
 - Vibration levels were reasonable.
 - A sub-synchronous vibration occurred at minimum flow point, but only at very low flow rates.
- Designed, constructed, and tested pilot-scale prototype using a closed-loop CO₂ compressor with internal cooling.
 - Heat transfer effectiveness matched CFD predictions.
 - Up to 55% of the heat of compression was removed during testing with cooled diaphragm technology with no additional pressure drop.

Next Steps

In Phase 3 of this project, a full-scale CO₂ compression and pumping system will be engineered and installed at a power plant. This work will include:

- Detailed design and fabrication of the CO₂ compressor.
- Measurement of the CO₂ compressor performance.
- Testing to assess the actual field efficiency.
- Conduct long-term performance studies.

Final test results will not be available until the December 2013 project completion date.

Available Reports/Technical Papers/Presentations

General project information is available on DOE/NETL website at: <http://www.netl.doe.gov/technologies/coalpower/ewr/co2/co2compression/novelconcepts.html>

“Novel Concepts for the Compression of Large Volumes of CO₂,” Annual NETL CO₂ Capture Technology for Existing Plants R&D Meeting, Pittsburgh, PA, September 2010. <http://www.netl.doe.gov/publications/proceedings/10/co2capture/index.html>

“Novel Concepts for the Compression of Large Volumes of CO₂ - Phase II,” Annual NETL CO₂ Capture Technology for Existing Plants R&D Meeting, Pittsburgh, PA, March 2009.

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