Fitting: A Subroutine to Fit Four-Moment Probability Distributions to Data

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FITTING: A SUBROUTINE TO FIT FOUR-MOMENT PROBABILITY DISTRIBUTIONS TO DATA

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Abstract

fitting is a Fortran subroutine that constructs a smooth, generalized fourparameter probability distribution model. It is fit to the first four statistical moments of the random variable X (i.e., average values of X, X^2 , X^3 , and X^4) which can be calculated from data using the associated subroutine calmom. The generalized model is produced from a cubic distortion of the parent model, calibrated to match the first four moments of the data. This four-moment matching is intended to provide models that are more faithful to the data in the upper tail of the distribution. Examples are shown for two specific cases.

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Executive Summary

fitting is a Fortran subroutine that constructs a smooth, generalized four-parameter probability distribution model. It is fit to the first four statistical moments of the random variable X (i.e., average values of X, X^2, X^3 , and X^4) which can be calculated from data using the associated subroutine calmom.

This distribution is said to be "generalized" in that it generalizes three conventional, standard two-parameter "parent" distribution models. The user may select here between Gaussian, Gumbel, or Weibull parent models. The generalized model is produced from a cubic distortion of the parent model, calibrated to match the first four moments of the data. This four-moment matching is intended to provide models that are more faithful to the data in the upper tail of the distribution.

Examples are shown here for two specific cases: modelling rainflow-counted load ranges and extreme wave heights, based respectively on Weibull and Gumbel parent models. To use fitting to fit a distribution to data, a separate subroutine, calmom, is included to determine the first four statistical moments of the input data set. Because these moments are required input to fitting, the routines calmom and fitting together serve as a general distribution fitting algorithm. A sample driver program is included to illustrate the usage and interpretation of fitting and calmom for the two examples.

Chapter 1

The fitting Subroutine

1.1 What fitting Does

fitting is a Fortran subroutine that constructs a smooth, generalized four-parameter probability distribution model. The first four statistical moments of the random variable X (i.e., average values of X, X^2 , X^3 , and X^4) are used by the subroutine to establish the generalized distribution. These moments can be based on theory; however, they are almost always derived from data. A separate subroutine calmom is provided to compute the required moments for an arbitrary data set.

This distribution is said to be "generalized" in that it generalizes three conventional, standard two-parameter "parent" distribution models. The user may select here between Gaussian, Gumbel, or Weibull parent models. The generalized model is then produced from a cubic distortion of the parent model, calibrated to match the first four moments of the data. (Depending on the numerical values of the moments, an inverse cubic distortion may also be used.) This four-moment matching is intended to provide models that are more faithful to the extreme values of the data, commonly referred to as the upper tail region.

By invoking various parent models, the user is able to reflect reasonable "prior" probability distribution choices based on the context at hand. For example, values from a random process may be assigned Gaussian distribution if sampled at an arbitrary time, Weibull distribution if sampled at an arbitrary peak, or Gumbel distribution if sampled at a global peak in a fixed duration (Benjamin and Cornell, 1970). These three distributions are included here as possible parent distribution choices.

Examples are shown here for two specific cases: modelling rainflow-counted load ranges and extreme wave heights, based respectively on Weibull and Gumbel parent models. Notably, we find that over a range of practical values, these applications are controlled by the four moment values and are relatively insensitive to the underlying parent distribution choice. Because this conclusion may change with the application,

Values x_i [kip-ft]:	Probabilities $p_i = F(x_i)$:
9.250	0.004
9.500	0.058
9.750	0.146
10.000	0.251
10.250	0.360
10.500	0.465
10.750	0.561
11.000	0.645
12.000	0.862
13.000	0.949
14.000	0.981
15.000	0.993

Table 1.1: Predicted probabilities, p_i , of not exceeding various x levels.

fitting allows the user to implement various parent distributions and assess the sensitivity to this choice.

1.1.1 Overview of Capabilities

The subroutine fitting has two options. In the first option, the user can provide arbitrary values $x_1, ..., x_N$ of the physical variable, and the routine returns corresponding probability values, p_i , that the random variable is less than the value x_i . Formally, p_i is known as $F(x_i)$, the cumulative distribution function (CDF) of X. The second option works in the opposite direction: the user provides specified cumulative probability values p_i , and the routine returns levels x_i of the physical variable. In this case, the output levels x_i are known as specific fractiles of the probability distribution. Note that both options require the first four statistical moments of X to be input.

As a simple example, consider the edgewise bending moment range X on a wind turbine blade (Coleman, 1989). Figure 1.1 shows the cycle counts (rainflow counted) for a 71 minute time history of observed edgewise moments. The clustering of counts in the moment ranges around 9-15 and 0-5 kip-ft is attributed to the dominant gravity induced loading combined with the turbulent effects of the wind respectively. From the viewpoint of fatigue damage, ranges less than 9 kip-ft contribute less than 5% to the total damage and are considered insignificant. Table 1.1 shows the cumulative distribution, F(x), of applied loads above this level as predicted by fitting.

For example, Table 1.1 shows that among all loads above xmin=9 [kip-ft], the load level 9.5 [kip-ft] is not exceeded 5.8% of the time—and hence exceeded the remaining



Figure 1.1: Histogram of Edgewise Bending Moment Time Series Data

94.2% of the time. Similarly, this table shows that a typical, central load value is around 10.5 [kip-ft]. Strictly, this value is not exceeded 46.5% of the time; i.e., the *median* value of the load X—which has 50% chance of being exceeded—is between 10.5 and 10.75 [kip-ft]. We show in Section 2.2 how these values are estimated from the fitting routines. We also show how, if we invoke the second option of fitting, we can directly estimate the median level (for which $F(x)=p_i$ is specified to be 0.5) to be 10.59 [kip-ft]. Notice also from Table 1.1 that probabilities for values that exceed the range of observed values can be requested.

In general, one may consider three distinct ways to use fitting:

- One option of the subroutine fitting takes input values x_i and estimates the cumulative probability p_i of falling below each x_i . For example, data in the first column of Table 1.1) are input and the second column values are output.
- With this same option, the differences $p_i p_{i-1}$ between these cumulative probabilities can be used to give estimates of a theoretical histogram (i.e., probability content in various discretized "cells" or "bins.") For example, Table 1.1 can be used to directly produce a histogram, with probability .032 assigned to the interval (9.25, 9.50), probability .126-.032=.094 to the interval (9.50, 9.75), and so forth.
- The other option of the subroutine fitting takes input values p_i and returns corresponding values x_i . For example, data in the second column of Table 1.1

are input and the first column values are output. This is useful, for example, if the user can more easily specify interesting values of p_i rather than x_i values a priori.

1.1.2 Subroutine calmom

fitting requires the first four statistical moments of the random variable, X, as input. These moments can be based on either theoretical considerations or derived from a particular set of data. To use fitting to fit a distribution to data, a separate subroutine, calmom, is included to accurately estimate the first four statistical moments of the input data set. Input and output for the calmom subroutine are described in Section 1.3.

Because these moments are required input to fitting, the routines calmom and fitting together serve as a general distribution fitting algorithm. A sample driver program is included to illustrate the usage and interpretation of fitting and calmom for two example problems given in Chapters 2 and 3.

1.1.3 How to Read or Not Read This Manual

We recognize that there are two distinct types of computer users: those who read manuals thoroughly and those who go to great lengths to avoid doing so. For this latter group, who prefer to learn by example, we have included a driver program with detailed comments, and the sample input and output used to generate Table 1.1. Those users may wish to proceed to the driver source code listing, also given in Appendix A. Additional description of the driver and this example, based on a generalized Weibull model, is given in Chapter 2. Chapter 3 describes an alternate application to extreme wave height levels, using a generalized Gumbel model.

Those who prefer a more precise overview of fitting are referred to the remainder of Chapter 1. Section 1.2 describes its input and output arguments and calling syntax, while Section 1.3 discusses the usage and arguments of the subroutine calmom which computes statistical moments for a given data set.

Finally, Chapter 4 brings together a number of more detailed technical issues concerning fitting. These range from underlying motivation (Section 4.1) to the basic methodology underlying fitting (Section 4.2) and calmom (Section 4.3). Section 4.4 includes various additional practical notes on their usage, limitations and potential error conditions.

1.2 fitting Input and Output

The user can call fitting with the following command:

```
call fitting(itype,xmom,ndata,xmin,x,cdf,nx,pmom,iflag,ioout,etol)
```

Each component of the fitting argument list is defined below. Output quantities include the array pmom and, depending on the value of iflag, either x or cdf. All other quantities are input.

- itype: index used to define the parent distribution used by fitting
 - **itype** = 1: Gaussian distribution

itype = 2: Gumbel distribution

itype = 3: Weibull distribution

- xmom(1)¹: mean, $\mu_x = E[X] = \int_{all x} xf(x)dx$; f(x) = PDF of X
- xmom(2)¹: standard deviation, $\sigma_x = \{E[(x-\mu_x)^2]\}^{1/2} = \{\int_{all x} (x-\mu_x)^2 f(x) dx\}^{1/2}$
- xmom(3)¹: skewness, $\alpha_3 = E[(\frac{x-\mu_x}{\sigma_x})^3] = \int_{all x} (\frac{x-\mu_x}{\sigma_x})^3 f(x) dx$
- xmom(4)¹: kurtosis, $\alpha_4 = E[(\frac{x-\mu_x}{\sigma_x})^4] = \int_{all x} (\frac{x-\mu_x}{\sigma_x})^4 f(x) dx$
- ndata¹: Number of sample data used to estimate moments in xmom. If ndata< 100, fitting checks by simulation that these moments do not have excessive bias (Section 4.3). The user can avoid this simulation check by setting ndata \geq 100 on input.
- xmin: Optional shift parameter to be applied in the Weibull case (itype=3). Note that the standard Weibull model produces values for $X \ge 0$, while the Gaussian and Gumbel models are unbounded. If the user inputs a nonzero value of xmin, a shifted Weibull model (standard Weibull model of X - xmin) is then used as a parent distribution. Accordingly, in this case xmom(1) ... xmom(4) should contain moments of the shifted variable X - xmin. (This is precisely what is returned by the routine calmom when xmin is nonzero.) The data shown in figure 1.1 is a good example of using this variable (xmin ≈ 9.0) when only the upper portion of the data is important. Note finally that fitting ignores the value of xmin if the Gaussian or Gumbel distribution is selected.
- x: array containing values of the physical variable.

¹Section 1.3 explains these moments further and subroutine calmom used to compute them

- cdf: array containing the cumulative (non-exceedance) probabilities corresponding to each x_i in the x array above.
- nx: number of x or cdf values requested.
- pmom: array of the absolute moments of the fitted distribution:

pmom(n): the *n*-th absolute moment, $E[X^n] = \int_{all \ x} x^n f(x) dx$

The first four moments will be consistent with the input moments given in **xmom**, within the error tolerance described below. Higher moments may be of interest in other applications; e.g., fatigue damage of various materials. Here n=10 moments are output, using the probability density function f(x) estimated by the Generalized distribution model.

• iflag: index used to define the type of calculation to be performed by fitting

iflag = 0: returns output estimates of x for each of the cumulative probabilities input in the array cdf.

iflag = 1: returns output estimates of probabilities cdf for each of the physical values input in the array x.

- ioout: logical unit number for writing error messages. The calling program should make a file available for error messages by opening a file with ioout as its logical unit number. (The sample driver illustrates this in Chapter 2.)
- etol: the error tolerance in matching higher moments. This is defined formally in Eq. 4.2. In general, there is a tradeoff between moment accuracy and computation time. Based on experience with various tolerances, we use the value etol=.01 in our examples. This may be changed by the user.

If the theoretical moments xmom(i) are known, the fitting routine can be applied directly. In practice, it is often necessary to estimate these statistical moments from a set of data. A separate subroutine, calmom, is supplied here to compute the required moments from data; i.e., to act as a pre-processor for fitting routine. The procedure used to compute these moments is discussed in section 4.3, and its use is demonstrated in Chapter 2.

The Role of the Lower Threshold xmin. In most applications of the Weibull model we seek to model all possible values of a positive quantity (e.g., stress range, number of cycles to failure, etc.). In certain applications, however, the user may wish to impose a non-zero lower-bound xmin. This is useful, for example, if we wish to exclude lower values as non-physical, or due to a fundamentally different probability distribution. We have found this useful, for example, in modelling some edgewise bending loads on a turbine blade. In this case, we seek to exclude small, non-damaging loads produced by a different mechanism: low amplitude (turbulence induced) cycles superimposed on marked gravity-driven bending moment ranges. This case is illustrated further in the example of Chapter 2.

1.3 calmom Input and Output

The subroutine calmom estimates the first four statistical moments xmom(i), i=1...4, from an input data set. It can thus serve as a preprocessor to fitting.

The calmom argument list is:

```
subroutine calmom(xmom,data,ndata,nrmax,xmin,itype)
```

The input to calmom are the following:

- data: array containing the data for which the moments are to be calculated.
- ndata: number of data points in array data.
- nrmax: dimension size of array data (should be consistent with that used in calling program).
- xmin: threshold value of the physical variable, as used in fitting (see description of xmin in section 1.2 and the example problem in Chapter 2).
- itype: index used to define the parent distribution used by fitting

itype = 1: Gaussian distribution
itype = 2: Gumbel distribution
itype = 3: Weibull distribution

The sample data input via the array data, can be arranged in any order and does not need to be sorted in increasing magnitude as shown in the example input of Table 2.1. Also, calmom screens the array data removing any values that are below the threshold xmin.

On output the array xmom contains the sample moments of the data, as defined in section 1.2. These can then be used directly as input to the routine fitting. The theoretical background for calmom is described in Section 4.3.

1.4 The Driver Program

A single driver program is used to demonstrate the use of subroutines fitting and calmom for two examples.

In general, the source code is distributed in three separate files:

calmom.for: The calmom subroutine to estimate moments from an input data set.

- fitting.for: The fitting subroutine, to use these moments to estimate the entire distribution function of X.
- **driver.for:** A separate driver program that calls these routines (listing in Appendix A).

This driver program is included to help speed the reader's understanding and implementation of fitting. The example shown here can thus be run without creating any additional source code. One needs merely to compile and link the three source codes listed above, and execute with the input files provided.

Of course, prospective users are encouraged to modify the driver program according to their needs. Toward that end, it is hoped that driver.for can provide a useful template. For those users who prefer to learn by example, we recommend reading the source code of driver.for as a useful starting point.

Analysis Steps. As implemented in driver.for, the analysis proceeds in the following steps:

- 1. Read control data: itype, xmin, iflag, and the array cdf or x used as input to fitting.
- 2. Read input data: the array data used as input to calmom, which calculates the necessary moment input for fitting.
- 3. Call calmom to estimate moments.
- 4. Call fitting to estimate the corresponding full distribution function.
- 5. Write results.

These steps are clearly delineated in comments contained within the source code of driver.

File Architecture. In the current coding of the driver (Appendix A), two input files are expected:

driver.in: Input file containing control data read in step 1 above.

driver.dat: Input file containing physical data read in step 2 above.

Together with the three source code files, we are distributing input files for two examples: (1) weibull.in, weibull.dat; and (2) gumbel.in, gumbel.dat. The user

should note that to implement one of these examples, the input files *.in and *.dat (*='weibull' or 'gumbel') should be copied to driver.in and driver.dat before executing. The corresponding output file, driver.out, should then agree with the file *.out that has been distributed.

The examples described in Chapters 2 and 3 provide tables that identify more clearly the contents of the files driver.in and driver.dat.

Chapter 2

Fatigue Load Modelling: A Generalized Weibull Example

This chapter describes the first example, which relates to fatigue load modelling. The next chapter describes an alternate application to extreme wave height modelling.

2.1 Wind Turbine Loads Example

This example concerns the edgewise bending moments shown in figure 1.1 of Chapter 1 (Coleman, 1989). We consider here 8913 values of X= bending moment range [kip-ft], as found by rainflow counting (Fuchs and Stephens, 1980). The data are stored in the file weibull.dat. Table 2.1 gives a partial listing of these values. For the sake of clarity they are input in increasing order; however, this is not required by the program.

A separate analysis of these data (Winterstein and Lange, 1994) has shown that bending moment ranges below 9 kip-ft do not contribute to the total fatigue damage given by this data set. Since the application for the load model is a fatigue analysis of the HAWT blade, we choose to fit the model above a lower threshold xmin=9 [kip-ft]. Note that only 4819 ranges are above this threshold.

This threshold is set in the first line of the input file weibull.in. Table 2.2 lists this file. The first line also contains the values iflag=1 and itype=3. The value iflag=1 indicates that values of x are to follow on the subsequent lines in the file, and the program is to calculate corresponding cdf values. The value itype=3 tells the fitting routine to select Weibull as the parent distribution. The remaining lines list the actual x values requested, which are the same as in column 1 of Table 1.1.

Output. The driver produces a single output file, driver.out, which we have stored here as weibull.out. Table 2.3 lists weibull.out for our example. The

Line number i:	Data x_i [kip-ft]:
1	0.0190
2	0.0190
3	0.0190
•	
	•
4092	8.9810
4093	8.9820
4094	8.9820
4095	9.0010
4096	9.0010
4097	9.0010
8911	18.0420
8912	18.9290
8913	20.4990

Table 2.1: Abridged listing of edgewise moment ranges [kip-ft] from weibull.dat. File contains column 2 data only; line numbers are inserted here for clarity.

9.00	$1\ 3\ ;$ xmin=lower threshold; iflag=1 to get cdf for given x; itype=3 to fit generalized weibull
9.25	
9.50	
9.75	
10.00	
10.25	
10.50	
10.75	
11.00	
12.00	
13.00	
14.00	
15.00	

Table 2.2: Listing of input file, weibull.in, with control data for driver program.



Figure 2.1: Generalized Weibull Distribution for Fatigue Loads-4819 Data.

fractile results reported by fitting are precisely those given in Chapter 1 (Table 1.1). Note also that the output confirms that 4819 data points have been found above the input lower threshold of x=9. It also reports the first four moments from these data, as estimated by calmom, that are used as input to fitting. Finally, the model predicts the first 10 absolute moments, $E[X^n]$. Note that these are consistent with the first four moments found for the data. For example, $E[X^1]=1.831$, the mean value μ_x , while $E[X^2]=\sigma_X^2 + \mu_X^2$, or $1.154^2 + 1.831^2 = 4.685$. Similarly, the predicted third and fourth moments can be shown to be consistent with those estimated from the data. The main virtue of the routine, of course, is that it seeks to predict still higher moments more accurately—through introduction of a smooth distribution model—than would be possible from the data alone.

Figure 2.1 compares the fitted distribution function F(x) with the data. (These results have been obtained by running the fitting routine over a larger range of x values than shown in the example.) Results are shown on "Weibull probability scale," on which the parent Weibull model appears as a straight line. It appears that the generalized Weibull model reflects the curvature of the data shown on this scale, particularly in the upper tail of interest (which is most heavily weighted by the third and fourth moments).

Lower Threshold Value: 9.000 Number of Data Processed: 4819 ** MOMENT RESULTS ** Mean: 1.831 Standard Deviation: 1.154 Skewness: 1.552 7.449 Kurtosis: ****** FRACTILE RESULTS (FITTING) ****** Χ: CDF: 9.250 0.004 9.500 0.058 9.750 0.146 10.000 0.251 10.250 0.360 10.500 0.465 10.750 0.561 11.000 0.645 12.000 0.862 13.000 0.949 14.000 0.981 15.000 0.993 ****** PREDICTED MOMENTS (FITTING) ****** N : E[X**N]: 1.000 0.183E+01 2.000 0.469E+01 3.000 0.159E+02 4.000 0.688E+02 5.000 0.377E+03 6.000 0.259E+04 7.000 0.221E+05 8.000 0.234E+06

9.000 0.302E+07 10.000 0.472E+08

Table 2.3: Listing of output file, weibull.out, produced by driver program.

9.00	0.3; xmin=lower threshold; iflag=0 to get x for given CDF; itype=3 to fit generalized weibull
0.10	
0.20	
0.30	
0.40	
0.50	
0.60	
0.70	
0.80	
0.90	
0.99	
0.999	

Table 2.4: Listing of input file for iflag=0 option.

2.2 Alternate Usage of fitting

Finally, we illustrate the iflag=0 option of fitting. For example, if the weibull.in content is modified as shown in Table 2.4, Table 2.5 shows the corresponding output. The data file weibull.dat remains the same, and hence all moment results are unchanged. The only difference is that in this case, the distribution fractiles x have been evaluated at the requested probability levels given in the input file driver.in (Table 2.4). For example, as noted in Chapter 1, the median value of X (with 50% chance of being exceeded) is found to be 10.589. The values of bending moment that are not exceeded 99% and 99.9% of the time were also determined.

- Lower Threshold Value: 9.000 Number of Data Processed: 4819 **** MOMENT RESULTS **** Mean: 1.831 Standard Deviation: 1.154 Skewness: 1.552 7.449 Kurtosis: ****** FRACTILE RESULTS (FITTING) ****** X : CDF: 9.627 0.100 9.882 0.200 10.114 0.300 10.345 0.400 10.589 0.500 10.861 0.600 11.188 0.700 11.620 0.800 12.324 0.900 14.664 0.990 17.255 0.999 ****** PREDICTED MOMENTS (FITTING) ****** N : E[X**N]: 1.000 0.183E+01 2.000 0.469E+01 3.000 0.159E+02 4.000 0.688E+02 5.000 0.377E+03 6.000 0.259E+04 7.000 0.221E+05
 - 8.000 0.234E+06 9.000 0.302E+07 10.000 0.472E+08

Table 2.5: Listing of output file, generated from iflag=0 input file given in Table 2.4.

Chapter 3

Extreme Values: A Generalized Gumbel Example

This chapter illustrates the use of the fitting routine to fit a generalized Gumbel distribution to extreme values. The driver program used for this demonstration is described in Chapter 1. This driver program reads the relevant input data for this example and passes them to the calmom and fitting routines to construct the generalized Gumbel distribution.

This example concerns the significant wave height H_s in a Southern North Sea location, for which 19 years of hindcast data are available (Danish Hydraulic Institute, 1989). For each of these 19 years, a single storm event has been identified with maximum significant wave height H_s (i.e. the extreme values). This value ranges from $H_s = 6.92m$ (1972/1973) to 9.66m (1981/1982). A sorted list of all 19 values is reported in Table 3.1.

This chapter has two sections. The first section deals with the generalized Gumbel model for the significant wave height data. The second section compares the three different generalized distribution models for the same data set.

Finally, it should be noted that a generalized Gumbel model has previously been fit to this data set (Winterstein and Haver, 1991). The results shown here are an improvement in two senses: (1) fitting permits greater accuracy to be achieved in matching moments; and (2) fitting includes an inverse cubic transformation, which is particularly important in reflecting the narrower-than-Gumbel tails similar to the data in Table 3.1.

·····	
Line number i:	Data H_{si} [m]:
1	9.66
2	9.44
3	9.18
4	9.17
5	8.85
6	8.79
7	8.60
8	8.58
9	8.54
10	8.49
11	8.09
12	8.08
13	8.06
14	7.47
15	7.42
16	7.41
17	7.31
18	7.16
19	6.92

Table 3.1: Listing of annual significant wave height [m] from gumbel.dat. File contains column 2 data only; line numbers are inserted here for clarity.

3.1 Generalized Gumbel Results

The annual significant wave height data consists of 19 values listed in Table 3.1. The data are stored in the file gumbel.dat. For the sake of clarity they are input in decreasing order; however, this is not required by the program.

The control data are stored in gumbel.in. Table 3.2 lists this file. The first line of this file contains three values. The first value is xmin=0.0, which sets the lower threshold value. Note, however, that this is not used in this case of Gumbel distribution since there is no cutoff value. This threshold value is used when generalized Weibull distribution is fit to the data (see Chapter 2). The second argument, iflag=1, indicates that x values are to follow in the file and the program will calculate corresponding cdf values. The third argument, itype=2, indicates that a generalized Gumbel distribution is to be fit to the data in file gumbel.dat. The remaining lines list the actual x values requested.

Output. Table 3.3 lists the corresponding output file gumbel.out for this example. It also reports the first four moments from these data, as estimated by calmom,

0.00	12; XMIN=LOWER THRESHOLD; IFLAG=1 TO GET CDF FOR GIVEN X; ITYPE=2 TO FIT GENERALIZED GUMBEL
10.00	
9.66	
9.44	
9.18	
9.17	
8.85	
8.79	
8.60	
8.58	
8.54	
8.49	
8.09	
8.08	
8.06	

Table 3.2: Listing of input file, gumbel.in, with control data for driver program.

which are used as input to fitting. Finally, the model predicts the first 10 absolute moments, $E[X^n]$. Note that these are consistent with the first four moments found for the data. For example, $E[X^1] = 8.275$, the mean value μ_x , while $E[X^2] = \sigma_X^2 + \mu_X^2$, or $.819^2 + 8.275^2 = 69.1$. Similarly, the predicted third and fourth moments can be shown consistent with those estimated from the data.

As discussed in Chapter 2, note that to use the input files gumbel.in and gumbel.dat with the driver program they must be copied to the files driver.in and driver.dat respectively. The output, written to driver.out, should then be comparable to gumbel.out.

In order to generate a smooth plot of the generalized Gumbel distribution, an input file similar to driver.in with a greater number of input values to compute corresponding CDF values was used. This distribution is plotted in Figure 3.1 along with the observed data values. It appears to capture fairly well the systematic curvature of the data on the Gumbel probability scale used.

3.2 Comparison of Three Generalized Distributions for Wave Height

Because we deal here with annual extreme values, the Gumbel distribution is the natural choice of parent distribution. We may ask, however, what effect is achieved if

```
Number of Data Processed: 19
      ** MOMENT RESULTS **
                    Mean:
                               8.275
      Standard Deviation:
                               0.819
                Skewness:
                              -0.053
                               1.905
                Kurtosis:
   ** FRACTILE RESULTS (FITTING) **
                    X :
                                CDF:
                    10.000
                               0.998
                    9.660
                               0.978
                    9.440
                               0.937
                    9.180
                               0.846
                    9.170
                               0.842
                               0.690
                    8.850
                    8.790
                               0.662
                    8.600
                               0.580
                    8.580
                               0.572
                               0.557
                    8.540
                    8.490
                               0.539
                    8.090
                               0.427
                    8.080
                               0.424
                    8.060
                               0.419
  ** PREDICTED MOMENTS (FITTING) **
                            E[X**N]:
                    N :
                     1.000 0.827E+01
                    2.000 0.691E+02
                    3.000 0.583E+03
                    4.000 0.496E+04
                    5.000 0.426E+05
                    6.000 0.369E+06
                    7.000 0.322E+07
```

8.000 0.282E+08 9.000 0.250E+09 10.000 0.222E+10

Table 3.3: Listing of output file, gumbel.out, produced by driver program.



Figure 3.1: Generalized Gumbel Distribution for Annual Extreme Wave Height-19 Data.



Figure 3.2: Comparison of Generalized Gaussian, Gumbel, and Weibull Distributions for Annual Extreme Wave Height.

a different choice of parent distribution is selected. This is investigated in this section.

We again use the same data set as listed in Table 3.1. Thus the input data file is same as driver.dat of Section 3.1. However, the control input file driver.in is varied so that itype is either 1, 2, or 3. These three different values of itype give three generalized distributions: generalized Gaussian (itype = 1), generalized Gumbel (itype = 2), and generalized Weibull (itype = 3).

The three distribution are shown in Figure 3.2. The figure shows wave height results up to the 1000-year fractile, i.e. for which p=.999 and hence $-\ln(-\ln(p))=6.9$. The pattern of variation follows that of the underlying parent distributions: the Weibull has the narrowest upper tail and hence predicts the lowest extreme values, while the Gumbel predicts the largest. Most notably, however, all three parent distributions predict quite similar wave heights over this domain of interest.

This suggests that knowledge of four moments is sufficient to control the tail behavior of interest. This apparent robustness of the four-moment description is encouraging, particularly in cases where the optimal parent distribution is not obvious. Of course this conclusion may be problem-dependent; the user is encouraged to vary the choice of itype for the problem at hand.

Chapter 4

Technical Background and Additional Details

4.1 Motivation

The fitting routine has been developed to modify standard, commonly used distributions to better match observed tail behavior. In particular, cubic distortions of these standard "parent" distributions are sought to match the first four moments of the data. We may then ask why precisely *four* moments are used to fit the probability distribution of X—and not two, three, five, ten, etc. Conventional models are of lower order, requiring only one or two moments. The problem is that a number of plausible models, with very different tail behavior and hence fatigue reliability, can be fit to the same first two moments. This scatter in reliability estimates is said to be produced by *model uncertainty*. This is prevalent in low-order, one- or two-moment models. (Note that many common fatigue load models include only one parameter; e.g., the Rayleigh and exponential models.)

To avoid this model uncertainty, which is difficult to quantify, one is led to try to preserve higher moments as well. This will help to discriminate between various models, and hence reduce model uncertainty. The benefit does not come without cost, however: higher moments are more sensitive to rare extreme outcomes, and hence are more difficult to estimate from a limited data set. This is known as *statistical uncertainty*, which reflects the limitations of our data set.

Thus, our search for an "optimal" model reflects an attempt at balance between model and statistical uncertainties. Practical experience (e.g., Winterstein, 1988) suggests that four moments are often sufficient to define upper distribution tails over the range of interest. This experience motivates the generalized models developed here. It is again supported by the results of Section 3.2, in which extreme wave heights are insensitive to the choice of parent distribution, once four moments have been specified.

4.2 Underlying Methodology: fitting

The fitting routine begins with a theoretical, 2-parameter "parent" distribution. In the current implementation, the user may choose Gaussian, Gumbel, or Weibull parent distributions. Denoting this parent variable as U, fitting then models the physical random variable X through a cubic transformation of U:

$$X = c_0 + c_1 U + c_2 U^2 + c_3 U^3$$
(4.1)

The optimizer adjusts the coefficients c_n through an iterative scheme until the difference between the requested skewness, α_3 , and kurtosis, α_4 , (see xmom(3) and xmom(4), section 1.2) and those of the generalized model in Eq. 4.1 (α_{3X} and α_{4X}) are minimized.

The optimizer also restricts the coefficients so that Eq. 4.1 remains monotonically increasing, producing a well-behaved model that only mildly modifies the underlying parent distribution. This leads, for example, to requiring $c_3 \ge 0$ so that X in Eq. 4.1 continues to grow as U becomes large. This in turn makes it difficult to model cases with tails that are narrower than those of the parent distribution. In particular, it is difficult to use Eq. 4.1, with positive c_3 , to model situations in which the desired kurtosis, α_4 , is less than that of the parent variable, α_{4U} . In this case fitting inverts the model, seeking to fit a model analogous to Eq. 4.1 in which the roles of X and U are interchanged. (In this view, one seeks to expand the distribution tail of the actual variable X to produce a parent variable U, so that c_3 becomes positive.)

Note that this switching between two dual models, based on the size of α_4 , occurs automatically within fitting and should be of no consequence to the user. Adding such a dual model, however, has has been found to greatly increase modelling flexibility for small kurtosis cases. These have been found to arise both in extreme and fatigue loading applications.

Finally, in whichever form the model is defined, the coefficients c_n are chosen to minimize the error ϵ , defined as

$$\epsilon = \sqrt{(\alpha_3 - \alpha_{3X})^2 + (\alpha_4 - \alpha_{4X})^2}$$
(4.2)

The speed of executing fitting is governed largely by the speed of this optimization; i.e., by the amount of effort (trial c_n values) needed to achieve an acceptably small tolerance, ϵ_{tol} . The driver program sets $\epsilon_{tol}=.01$ for the examples shown. The user can vary this tolerance, with the resulting change in computation time to be expected.

4.3 Underlying Methodology: calmom

To motivate the need for this routine, we must consider a brief background in statistical moment estimation. If we seek to estimate the ordinary mean value $E[X] = \mu$ from data $X_1...X_n$, a natural estimate is the simple average value $\overline{X} = \sum_{i=1}^n X_i/n$. Similarly, the k-th order "ordinary" moment, $E[X^k]$, is naturally estimated by the corresponding average $\sum_{i=1}^n X_i^k/n$.

The difficulties arise when we instead seek, as in many applications, to estimate not ordinary but *central* moments; i.e., of the form $\mu_k = E[(X - \mu)^k]$ for k=2, 3, 4... (Note that fitting input stops at k=4: $\sigma_x = \mu_2^{1/2}$, $\alpha_3 = \mu_3/\mu_2^{1.5}$, and $\alpha_4 = \mu_4/\mu_2^2$.)

The problem here lies in its circular aspect: we must first estimate the unknown first moment μ before seeking to estimate $\mu_k = E[(X - \mu)^k]$. And, if we use the same data set for both purposes, we typically find too-low estimates of μ_2 , μ_3 , μ_4 , etc. because our μ value is artificially tuned to best match the mean of the observations. Those exposed to a standard statistics course will best recognize this phenomenon when estimating the variance μ_2 : to inflate the sample variance to account for this bias, the sum of squared deviations is divided by n-1 rather than n.

While unbiased estimates of the higher moments μ_3 , μ_4 , ... are less familiar, they are available in the statistical literature (Fisher, 1928):

$$\mu = \overline{X} = \frac{1}{n} \sum_{i=1}^{n} X_i \tag{4.3}$$

$$\mu_2 = \frac{n}{n-1}m_2 \tag{4.4}$$

$$\mu_3 = \frac{n^2}{(n-1)(n-2)}m_3 \tag{4.5}$$

$$\mu_4 - 3\mu_2^2 = \frac{n^2}{(n-1)(n-2)(n-3)} [(n+1)m_4 - 3(n-1)m_2^2]$$
(4.6)

in terms of the sample central moment $m_k = \sum_{i=1}^n (X_i - \overline{X})^k / n$. Eq. 4.4 is the conventional result for the sample variance.

Remaining Bias. Finally, the routine calmom uses these results to estimate the quantities σ_x by $\mu_2^{0.5}$, α_3 by $\mu_3/(\mu_2^{1.5})$, and α_4 by $\mu_4/(\mu_2^2)$. Because these vary nonlinearly with μ_n , they may still contain some bias although the μ_n estimates do not.

For example, if we fit a Gumbel model to the 19 wave height data from Chapter 3, the true skewness and kurtosis values are 1.14 and 5.40. However, simulating 10000 data sets of size n=19 and running each through calmom, we find on average the skewness 0.79 and kurtosis 3.89 (Winterstein and Haver, 1991).

To address this problem, the fitting routine has an automatic check for remaining bias through simulation. This is why ndata is given as an input parameter. After fitting constructs a distribution with moments from the input array xmom, many similar data sets (of size ndata) are simulated from this distribution. If the moments



Figure 4.1: Effect of Ignoring Bias: Wave Height Example.

predicted from calmom differ appreciably on average from the input values, new theoretical estimates of the moments are constructed. This estimation-simulation loop is continued iteratively until satisfactory convergence is found.

Note that the fitting routine does not perform this simulation if its input parameter ndata ≥ 100 . This value can be hard-wired if the user wishes to bypass this option. Figure 4.1 shows the effect of enabling this "unbiased" option (the default) and disabling it (using "raw" moments from calmom directly) for the generalized Gumbel model produced for the example given in Chapter 3. There is relatively little difference found in these cases. Larger effects may be found for cases of (1) fewer data and/or (2) distributions with broader tails.

4.4 Notes on Usage

The fitting routine has limiting conditions that users should note. When these conditions are encountered, appropriate error messages are written to the output file/device corresponding to the input logical unit number ioout. This section explains the meaning of these messages and discusses other details regarding fitting usage.

4.4.1 Errors in Matching Moments

Note that in most practical cases, the coefficients c_n in Eq. 4.1 can be chosen so that the error ϵ , as given in Eq. 4.2, falls within the user-defined tolerance limit ϵ_{tol} . In rare cases the minimized error exceeds ϵ_{tol} . In these cases fitting writes an error message indicating the magnitude of ϵ , the error norm of the skewness and kurtosis in Eq. 4.2.

4.4.2 Lower Tail Limiting Values

Lower tail limiting values are only a problem when the parent distribution is Weibull. In this case the variable U in Eq. 4.1 has Weibull distribution, and hence a minimum value of 0. Because Eq. 4.1 is monotonic, the corresponding smallest possible value of the physical variable X is c_0 . This physical lower limit c_0 can be either greater or less than zero, since the optimized Weibull model in Eq. 4.1 will not in general have its x intercept at exactly zero.

This may lead to situations that seem anomalous. If the lower limit c_0 is negative, for example, fitting may estimate negative values of X for probabilities near zero. Conversely, if the lowest possible value c_0 is positive, an input X value below c_0 cannot occur and fitting will return a zero cumulative probability (CDF=0). When xmin is not zero the situation is entirely analogous: c_0 may be greater or less than xmin.

In practice we believe this to be a minor issue for the following reasons:

- The routine fitting is intended for applications where large X values (upper distribution tails) are crucial. This is the motivation for preserving higher moments. Its accuracy at the lower end of the distribution may not be of great concern.
- If we wish to preserve a positive range of values, one can easily introduce a transformation to the data. For example, apply fitting not to the physical variable X but rather $Y=\ln(X)$, based on the first four moments of Y. Then the reverse transformation $X=\exp(Y)$ will still be positive.
- The routine fitting is intended for applications where the true distribution is not too different than a Weibull model would predict. In such cases we may expect the nonlinear terms (proportional to c_0 , c_2 , and c_3) in Eq. 4.1 to be relatively small on average relative to the linear term. Thus, compared to the range of likely variation of X values, c_0 may seem to lie rather "close" to zero.

References

Ang, A., and W. Tang, 1975, Probability Concepts in Engineering Planning and Design, Volume I Basic Principles, John Wiley and Sons, Inc.

Benjamin, J.R., and C.A. Cornell, 1970, Probability, Statistics, and Decision for Civil Engineers, McGraw-Hill Book Co.

Coleman, C., and B. McNiff, 1989, Final Report: Dynamic Response Testing of the Northwind 100 Wind Turbine, Subcontractor Report, SERI Cooperative Research Agreement No. DE-FC02-86CH10311, Solar Energy Research Institute, Golden, CO, 40pp.

Danish Hydraulic Institute, 1989, Environmental Design Conditions and Design Procedures for Offshore Structures, Copenhagen.

Fisher, R.A., 1928, "Moments and Product Moments of Sampling Distributions," Proceedings of the London Mathematical Society, Vol. 30, pp. 199-238.

Fuchs, H., and R. Stephens, 1980, Metal Fatigue in Engineering, John Wiley and Sons, Inc.

Veers, P.S., C.H. Lange, S.R. Winterstein, and T.A. Wilson, 1994, Users Manual for FAROW: A Computer Analysis of the Fatigue and Reliability of Wind Turbine Components, SAND94-2460, Sandia National Laboratories, Albuquerque, New Mexico.

Winterstein, S. R. 1988, "Nonlinear Vibration Models for Extremes and Fatigue," Journal of Engineering Mechanics, Vol. 114, No. 10, October, 1988.

Winterstein, S. R., and S. Haver, 1991, "Statistical Uncertainties in Wave Heights and Combined Loads on Offshore Structures," 9th International Symposium on Offshore Mechanics and Arctic Engineering, Houston, Texas, ASME.

Winterstein, S.R., and C.H. Lange, 1994, "Load Models for Fatigue Reliability from Limited Data," Wind Energy - 1994, ASME.

Appendix A

Driver Source Code Listing

```
С
С
   THIS PROGRAM DEMONSTRATES THE USE OF THE SUBROUTINES
С
С
       CALMOM ... CALCULATES FOUR MOMENTS OF A GIVEN INPUT DATA SET
       FITTING... USES THESE
                                        FIT A GENERALIZED
С
                            MOMENTS
                                    TO
                  (GAUSSIAN, GUMBEL, WEIBULL) DISTRIBUTION FUNCTION
С
С
С
   INPUT FILES:
                 DRIVER.DAT... INPUT DATA USED TO ESTIMATE MOMENTS
                  DRIVER. IN... CONTROL DATA USED IN CALLING FITTING
С
С
                  (NOTE: SAMPLE EXAMPLE FILES *.DAT AND *.IN SHOULD
С
                  BE COPIED TO DRIVER.DAT AND DRIVER.IN
С
                                                   BEFORE
С
                  EXECUTING)
С
С
   OUTPUT FILE:
                 DRIVER.OUT
С
С
                 COMPILE AND LINK DRIVER, CALMOM, AND FITTING
   USAGE:
С
PROGRAM DRIVER
IMPLICIT REAL*8 (A-H,O-Z)
    PARAMETER ( NDMAX = 20000 , NXMAX = 2000 )
    DIMENSION DATA(NDMAX), CDF(NXMAX), X(NXMAX), XMOM(4), PMOM(10)
С
C----
               -----OPEN FILES FOR INPUT AND OUTPUT
    IODAT = 10
    IOIN = 11
    IOOUT = 12
    OPEN(IODAT,FILE='driver.dat')
```

```
OPEN( IOIN, FILE='driver.in')
     OPEN(IOOUT,FILE='driver.out')
C
    -----READ CONTROL DATA
C-
С
                    LOWER THRESHOLD DATA VALUE USED IN THE ANALYSIS
С
         XMIN
         IFLAG INPUT/OUTPUT FLAG:
С
                           IFLAG = 0....FINDS X FOR INPUT CDF VALUES
С
С
                           IFLAG = 1....FINDS CDF FOR INPUT X VALUES
                     CONTROL VARIABLE TO CHOOSE THE GENERALIZED
С
         ITYPE
С
                     DISTRIBUTION TYPE
                    ITYPE = 1 :FIT GENERALIZED GAUSSIAN DISTRIBUTION
С
                    ITYPE = 2 :FIT GENERALIZED GUMBEL DISTRIBUTION
С
                    ITYPE = 3 :FIT GENERALIZED WEIBULL DISTRIBUTION
С
         X(NXMAX) LEVELS OF X AT WHICH DISTRIBUTION IS REPORTED
С
         CDF(NXMAX) CDF VALUES (NON-EXCEEDENCE PROBABILITIES) FOR
С
С
                           EACH X LEVEL
                    MAXIMUM NUMBER OF X OR CDF VALUES REQUESTED
С
         NXMAX
                    ACTUAL NUMBER OF X OR CDF VALUES REQUESTED
С
         NX
С
     READ(IOIN,*) XMIN, IFLAG, ITYPE
     IF (ITYPE .NE. 3) XMIN = 0.d0
     IF (IFLAG.EQ.0) THEN
         DO 10 IX = 1, NXMAX
         READ(IOIN, *, ERR=30, END=30) CDF(IX)
  10
                                         READ CDF VALUES IF IFLAG=0
С
     ELSE
         DO 20 IX = 1.NXMAX
         READ(IOIN, *, ERR=30, END=30) X(IX)
  20
                                         READ X VALUES IF IFLAG=1
С
     ENDIF
  30 NX = IX - 1
С
              -----READ INPUT DATA
C-----
С
         DATA (NDMAX) ARRAY OF INPUT DATA FOR WHICH MOMENTS ARE FOUND
С
        NDMAX MAXIMUM NUMBER OF INPUT DATA PERMISSIBLE
С
        NDATA
                    ACTUAL NUMBER OF INPUT DATA
С
C
     NDATA=0
  40 READ(IODAT, *, ERR=50, END=50) X1
     NDATA=NDATA+1
     DATA(NDATA) = X1
     GO TO 40
```

50 CONTINUE С C-----CALL CALMOM TO ESTIMATE MOMENTS С С XMOM(4) ARRAY OF FOUR MOMENTS COMPUTED FROM DATA: XMOM(1) = MEANС С XMOM(2) = STANDARD DEVIATIONС XMOM(3) = SKEWNESSС XMOM(4) = KURTOSISС CALL CALMOM(XMOM, DATA, NDATA, NDMAX, XMIN, ITYPE) С C-----WRITE OUTPUT С IF (ITYPE .EQ. 3) THEN WRITE(IOOUT,900) ' Lower Threshold Value:', XMIN ENDIF WRITE(IOOUT, *) ' Number of Data Processed:', NDATA WRITE(IOOUT, *) ' ' WRITE(IOOUT, *) ' ** MOMENT RESULTS **' WRITE(IOOUT, *) ' ' WRITE(I00UT,900) ' Mean:', XMOM(1) Standard Deviation:', XMOM(2) WRITE(IOOUT,900) ' WRITE(100UT,900) ' Skewness:', XMOM(3) WRITE(IOOUT,900) ' Kurtosis:', XMOM(4) WRITE(IOOUT, *) '' С C-----CALL FITTING TO ESTIMATE X FOR GIVEN CDF (IFLAG=0) С OR CDF FOR GIVEN X (IFLAG=1) С С ETOL ERROR TOLERANCE IN MATCHING OBSERVED MOMENTS С ... HERE WE ACCEPT 0.01 ERROR---USER CAN ALTER С С PMOM(10) ARRAY OF PREDICTED ABSOLUTE MOMENTS FROM MODEL С PMOM(I) = PREDICTED AVERAGE OF X**N, N=1..10С ETOL = .01DOCALL FITTING(ITYPE, XMOM, NDATA, XMIN, X, CDF, NX, PMOM, IFLAG, IOOUT, ETOL) С C-----WRITE OUTPUT С WRITE(IOOUT, *) ' ** FRACTILE RESULTS (FITTING) **' WRITE(IOOUT, *) ' ' WRITE(IOOUT, *) ' X: CDF:' WRITE(IOOUT, *) ' '

```
DO 60 IX = 1 , NX
          WRITE(IOOUT,901) X(IX),CDF(IX)
 60
    WRITE(IOOUT, * ) ' '
    WRITE(IOOUT, * ) ' ** PREDICTED MOMENTS (FITTING) **'
    WRITE(IOOUT, * ) ' '
                                                   E[X**N]:'
                                            N :
    WRITE(IOOUT, * ) '
    wRITE(IOOUT, * ) ' '
          DO \ 70 \ IX = 1, 10
          wRITE(IOOUT,902) REAL(IX),PMOM(IX)
 70
900 FORMAT(A26, F10.3)
901 FORMAT(16X,2F10.3)
902 FORMAT(16X, F10.3,E10.3)
    STOP
    END
```

С

С

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