# SANDIA REPORT

SAND79-1753 • Unlimited Release • UC-60

Reprinted August 1982

# Aerodynamic Performance of the 17-M-Diameter Darrieus Wind Turbine in the Three-Bladed Configuration: An Addendum

Mark H. Worstell

Prepared by
Sandia National Laboratories
Albuquerque, New Mexico 87185 and Livermore, California 94550
for the United States Department of Energy
under Contract DE-AC04-76DP00789

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Printed in the United States of America Available from National Technical Information Service U.S. Department of Commerce 5285 Port Royal Road Springfield, VA 22161

NTIS price codes Printed copy: A04 Microfiche copy: A01

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AERODYNAMIC PERFORMANCE OF THE 17-M-DIAMETER DARRIEUS WIND TURBINE IN THE THREE-BLADED CONFIGURATION: AN ADDENDUM

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## ABSTRACT

The U.S. Department of Energy (DOE)/Sandia 17-m wind turbine has been tested in the three-bladed configuration at five rotational speeds. These data are presented along with some fundamental comparisons to the earlier two-bladed results. Also included is the theoretical output of the three-bladed 17-m wind turbine at two selected rotational speeds.

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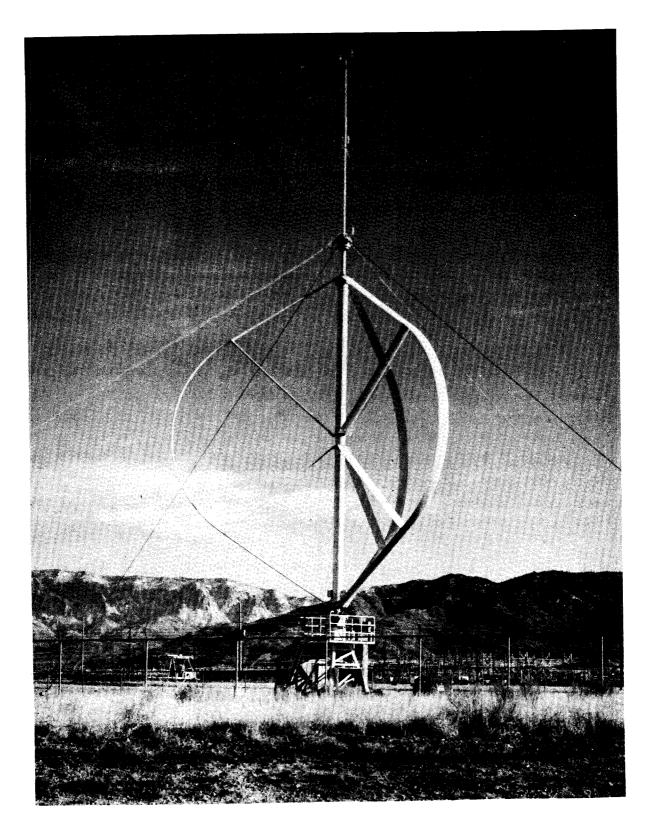


Figure 1. DOE/Sandia 17-m Wind Turbine

# AERODYNAMIC PERFORMANCE OF THE 17-M-DIAMETER DARRIEUS WIND TURBINE IN THE THREE-BLADED CONFIGURATION: AN ADDENDUM

#### Introduction

This report is an addendum to an earlier published report. The first report covered the performance of the DOE/Sandia 17-m turbine in the strutted two-bladed mode. This machine incorporates the flexibility of testing with either two or three blades. The effect of adding a third blade was to increase rotor solidity -- in this case, from  $\sigma = 0.14$  to  $\sigma = 0.21$ . The third blade is identical to the other two.

Testing in the three-bladed mode began in January 1978 and continued ~ 1 year, of which 6 months were lost for repair of the low-speed torque sensor. Aerodynamic performance data were accumulated for five rotational speeds. The nature of data assimilation and reduction is identical to that described in Reference 1. The descriptions, notations, equations, and references in Reference 1 are directly applicable to this report.

This report presents aerodynamic performance test data for the three-bladed 17-m turbine and makes some comparisons with the earlier two-bladed test data in order to identify the trends and characteristics of increasing the rotor solidity. In aerodynamic terms, there is a difference in changing solidity through the addition of more blades or by increasing the chord of the original number of blades, although the calculated value of solidity may be the same in either case. For example, Rec will change. The test results and data comparisons of this report are attributable only to the former case. Reference 2 presents wind tunnel test results of a 2-m turbine in both two- and three-bladed modes with varying blade chords.

## Test Results

Appendix A presents aerodynamic performance data of the 17-m turbine in the strutted three-bladed mode. Rotor speeds tested were 37, 42, 45.5, 48.4, and 52.5 rpm. As in Reference 1, the printed data, wind frequency,  $C_p$ , power, and  $K_p$  curves are presented for each rotational speed. Table 1 presents a summary of these test data. The  $K_{pmax}$  and  $P_{max}$  figures stated in Table 1 are 95% of the observed highest test data numbers.

In general, the  $_{\rm p}^{\rm c}$ , power, and  $_{\rm p}^{\rm c}$  curves of the test data exhibited smooth contours, which is quite encouraging for field test data.  $_{\rm pmax}^{\rm c}$  ranged from a high of 0.368 @ X = 5 for 37 rpm to a low of 0.323 @ X = 4.45 at 42 rpm. The windspeed at which the turbine rotor would begin producing power increases steadily from 9.5 mph at 37 rpm to 13.5 mph for 52.5 rpm. The highest aerodynamic power output achieved

Table 1
Three-Bladed Test Data Summary

	Breakeven V (mph)	C	K @ J Prnax	$\begin{array}{c} P & \otimes V \\ (k \mathbb{W}) & (mph) \end{array}$
37.0	9.5	.368 @ 5.00	.00775 @ .324	24.69 @ 23.5
l2.0	9.5	.323 @ 4.45	.00852 @ .346	39.70 @ 28.5
45.5	10.5	.340 @ 4.57	.00925 @ .353	54.77 @ 31.5
48.4	11.5	.352 @ 4.41	.00866 @ .332	61.75 @ 31.5
52.5	13.5	.346 @ 4.38	.00895 @ .335*	81.44 @ 34.5*

 $\mathbf{V}_{\infty}$  is at 44 foot reference height.

<sup>\*</sup>Higher ambient windspeeds needed.

by the 17-m turbine was 81.4 kW at 34.5 mph and 52.5 rpm. This figure might have been higher if ambient winds greater than 35 mph had been available.

The inherent characteristic of the constant-speed Darrieus turbine to level off in power output for increasing wind velocity (X < 3) is particularly evident in the power curve for 37 rpm. This is also seen at the other rotational speeds. Maximum turbine output power increased for higher rotational speeds, occurring at progressively higher ambient wind velocities.

One bothersome area of the field-test data was the  $C_p$  curve for 42 rpm. Unlike the other  $C_p$  curves, this one appears quite rough with no clearly defined maximum. (Note that the power curve for 42 rpm is indeed smooth, with a clearly defined maximum that does not depend upon a  $V^3$  calculation as does  $C_p$ .) The range in question is 4 < X < 10 (20 mph to 8 mph). A review of the individual test records of 42 rpm showed that seven records were in this particular range, with the majority of sample points confined to three records. Each of the seven records was examined; no clear-cut errors were apparent. One noteworthy fact was that all seven records were taken in the last three days of testing before retrofit work began on the 17-m turbine.

Because there were no anomalies present in the data taken before the last three days of testing, it is suspected that some aberration, such as unusual wind conditions and/or instrument error, occurred during these last three days. Due to lack of further data, the combined performance record for 42 rpm is presented in its entirely with the wind range in question to be noted.

# Data Trends and Comparison With Two-Bladed Results

It is the intent here to provide both the trends of the three-bladed data and to make a fundamental comparison with the earlier two-bladed data presented in Reference 1. The figures presented here combine both two- and three-bladed data at two selected rotational speeds of the turbine rotor.

Figure 2 plots the results of field testing of the DOE/Sandia 17-m turbine in both the two- and three-bladed modes at 37 and 52.5 rpm. The first impression of Fig. 2 is that the  $\rm C_p$  curves for the three-bladed mode are shifted towards lower tipspeed ratios (higher  $\rm V_{\infty}$ ) relative to those of the two-bladed configuration. This indicates that the 17-m turbine with three blades can produce more power in higher

<sup>\*</sup>This was the changeover to unstrutted aluminum-extruded blades with other modifications.

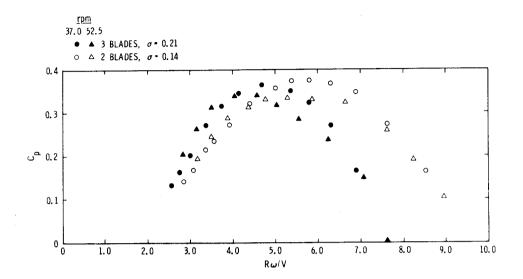


Figure 2.  $C_{D}$  as a Function of Tipspeed Ratio

ambient winds than with two blades at the same rpm, but less at lower  $V_{\infty}$ .  $C_{pmax}$  of both two and three blades was higher at 37 rpm than at 52.5 rpm. The similarity of the relationship between the  $C_{p}$  curves is also particularly striking.

Figure 3 plots  $C_{pmax}$  for both the two- and three-bladed configurations over the

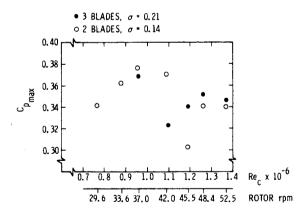


Figure 3.  $c_{p_{max}}$  as a Function of Reynolds Number

range of rotational speeds tested. Although two data points of this figure are in question (45.5 rpm,  $\sigma$  = 0.14 as described in Reference 1, and 42 rpm,  $\sigma$  = 0.21 as described earlier), this figure is still presented as a matter of consistency. With

these points excluded, no definite conclusions can be drawn other than that  $c_{pmax}$  for both solidities is roughly the same, and the highest  $c_{pmax}$  for both solidities occurred at 37 rpm.

Figure  $^{1}\!\!4$  shows a plot of  $^{K_0}\!\!_{p}$  as a function of advance ratio for both solidities

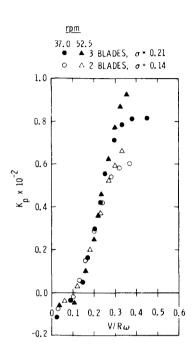


Figure 4.  $K_{D}$  as a Function of Advance Ratio

at 37 and 52.5 rpm. What is clearly evident in this figure is that for V/Rw > 0.26,  $K_p$  is decidedly higher for  $\sigma$  = 0.21 than for  $\sigma$  = 0.14, with  $K_p$  favoring the higher rotational speeds for both solidities. At lower advance ratios,  $K_p$  slightly favors  $\sigma$  = 0.14 at 37 rpm. Not clearly evident in Fig. 4 is that  $K_p$  for the higher solidity mode is slightly shifted towards higher values of advance ratios relative to the lower solidity.

In conjunction with Fig. 4, Fig. 5 presents  $K_{\rm pmax}$  as a function of Reynolds number, correlated to turbine rotational speed. Two distinct trends are apparent in Fig. 5. One is that  $K_{\rm pmax}$  increases for increasing rpm for both solidities. Second,  $K_{\rm pmax}$  for the higher solidity configuration is greater than for the lower solidity over the entire test range of turbine rotational speeds. Note that at 52.5 rpm, higher ambient winds than those encountered during testing are necessary to establish actual  $K_{\rm pmax}$ ; the points shown are the highest for the available winds.

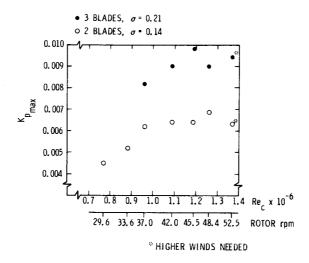


Figure 5.  $K_{pmax}$  as a Function of Reynolds Number

Figure 6 shows the power output of the DOE/Sandia 17-m turbine as a function of

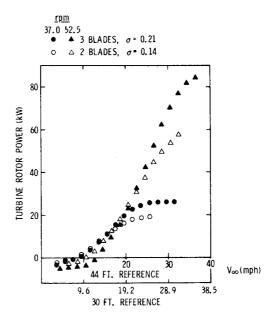


Figure 6. Power Output as a Function of Ambient Wind Velocity

wind velocity. This is essentially analogous to Fig. 4, which was expressed in dimensionless parameters. This clearly shows the effect of shifting the  $\frac{C}{p}$  curves

of Fig. 2 towards a lower tipspeed ratio for the higher solidity configuration. At higher  $V_{\infty}$  (lower X)  $C_p$  for  $\sigma$  = 0.21 is greater than for  $\sigma$  = 0.14, which manifests itself as increased rotor power output. The converse is also true; at lower  $V_{\infty}$ ,  $C_p$  for  $\sigma$  = 0.14 is greater. This can also be seen in Fig. 6, although not as distinctly.

#### Conclusions

Field-test results of the DOE/Sandia 17-m wind turbine appeared to be quite acceptable and exhibited basic trends and characteristics seen in the earlier two-bladed data of Reference 1. Comparing the two- and three-bladed data revealed several interesting (though predictable) trends. For the same rpm:

- 1. The peak turbine power output was higher for three blades than two.
- 2.  $C_{\text{pmax}}$  was roughly the same for both two and three blades.
- 3. The C curves for three blades were shifted towards lower X relative to two blades. This manifests itself as increased turbine power output at high winds and less output in low winds when compared to two blades.

Again, the results presented in this report are based upon a rotor solidity increase through the addition of a third blade, not by increasing the chord of the two-bladed rotor.

The predicted and experimental power output of the three-bladed DOE/Sandia wind turbine is presented in Figs. 7 and 8 for 37 and 52.5 rpm, respectively. The theoretical prediction is based upon the aerodynamic computer model PAREP, described in References 3 and 4. Very good agreement was obtained for 37 rpm, with the theoretical model tending to overpredict at 52.5 rpm.

As stated earlier, the DOE/Sandia 17-m turbine was refitted with unstrutted extruded aluminum blades. These blades are of a NACA 0015 airfoil section with a 24-in. chord. The geometry of the rotor is the same as that described in Reference 1 except for the struts. Current testing is in the two-bladed mode. Test results obtained to date indicate a significant improvement in performance over the original strutted NACA 0012 21-in. chord blades.

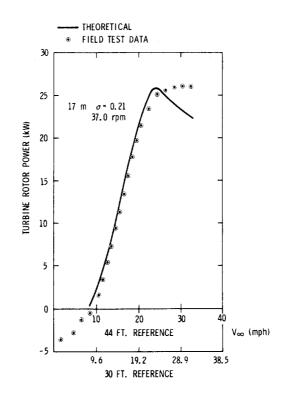


Figure 7. Comparison of Predicted and Experimental Power Output at 37 rpm

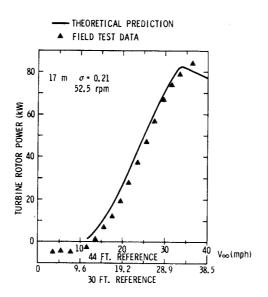


Figure 8. Comparison of Predicted and Experimental Power Output at 52.5 rpm

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- 1. M. H. Worstell, Aerodynamic Performance of the 17-Metre-Diameter Darrieus Wind Turbine, SAND78-1737, Sandia Laboratories, Albuquerque, NM, January 1979.
- 2. B. F. Blackwell, R. E. Sheldahl, and L. V. Feltz, <u>Wind Tunnel Performance Data</u> for the Darrieus Wind Turbine with NACA 0012 Blades, SAND76-0130, Sandia Laboratories, Albuquerque, NM, March 1977.
- 3. P. C. Klimas and R. E. Sheldahl, Four Aerodynamic Prediction Schemes for Vertical-Axis Wind Turbines: A Compendium, SAND78-0014, Sandia Laboratories, Albuquerque, NM, June 1978.
- 4. T. M. Leonard, <u>A User's Manual for the Computer Code PAREP</u>, SAND79-0431, Sandia Laboratories, Albuquerque, NM, April 1979.

APPENDIX A

Performance Data

37 rpm 3 Blades,  $\sigma$  = 0.21 Wind Range 2.5 to 31.5 mph

```
AIR DENSITY* .0625 LBS PER CU FT
17. M TURBINE, COMBINED DATA, RPM*37.0
NUMBER SAMPLES IN ACCUMULATION = 123392.
DATA RECORD MAME(S)* 130721. 131221. 131222. 120.

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1.5 284. .002 -3.6655 48.32-129.843 .021 -.0
2.5 845. .007 -3.6290 28.99 -27.766 .034 -.7
937. .008 -3.6439 20.71 -9.882 .048 -
1092. .009 -2.7829 16.11 -3.651 .062
1092. .009 -2.7829 16.11 -3.651 .062
1092. .009 -2.7829 16.11 -3.651 .062
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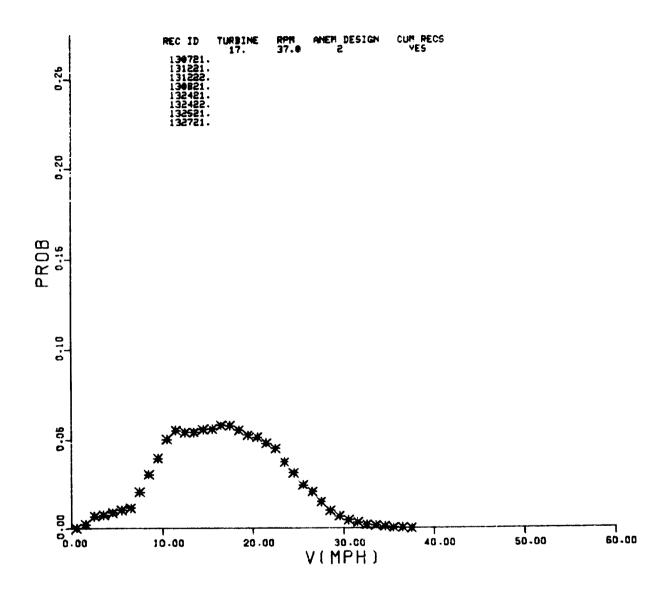
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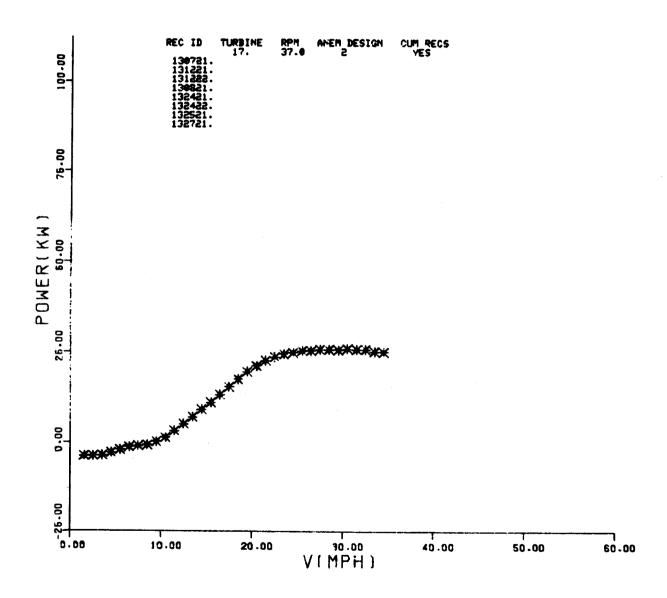
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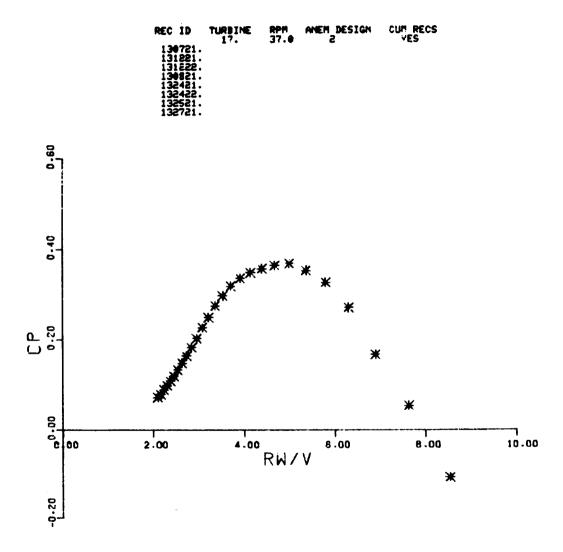
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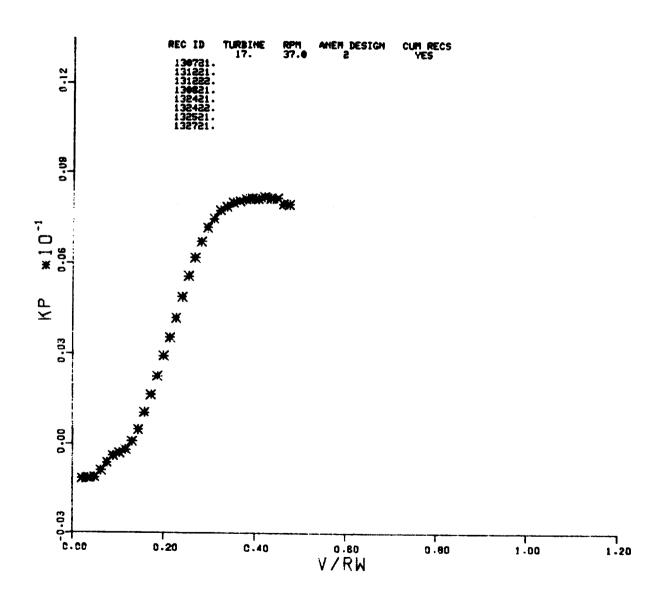
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42 rpm  $\text{3 Blades, } \sigma = \text{0.21}$  Wind Range 4.5 to 37.5 mph

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AIR DENSITY - .0625 LBS PER CU FT
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NUMBER SAMPLES IN ACCUMULATION - 105366.
DATA RECORD NAME(S) = 140821. 141421.

V POWER(KU) RU/V
2.5 1. .000 - .5135 32.91
                                                                                                                                                          141422.
CP
                                                                                                                   | • 105366.

141421.

1(KU) PU/U

35 32.91

58 23.51

58 23.51

665 12.66

673 10.97

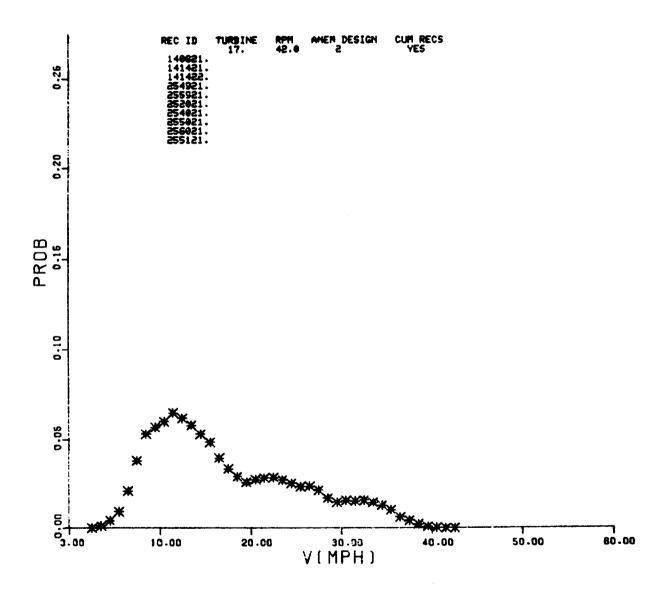
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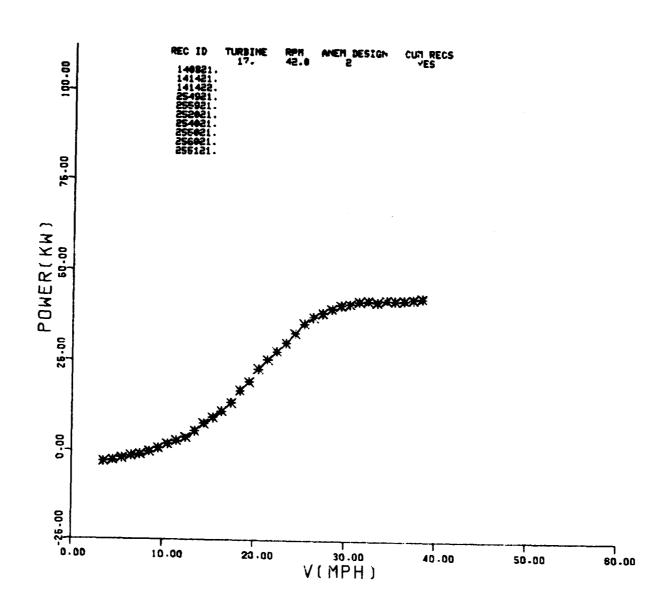
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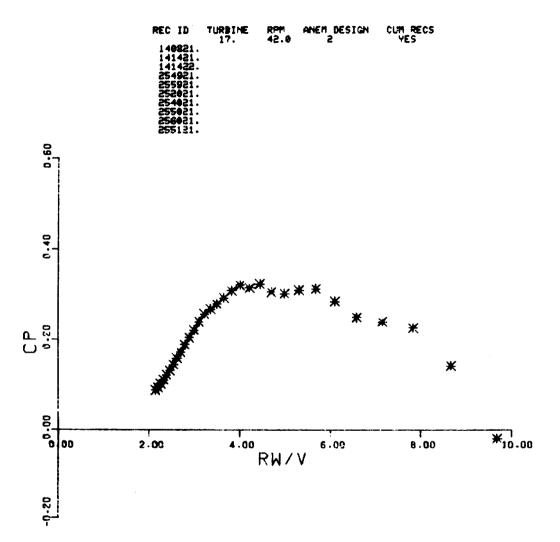
105 7.84

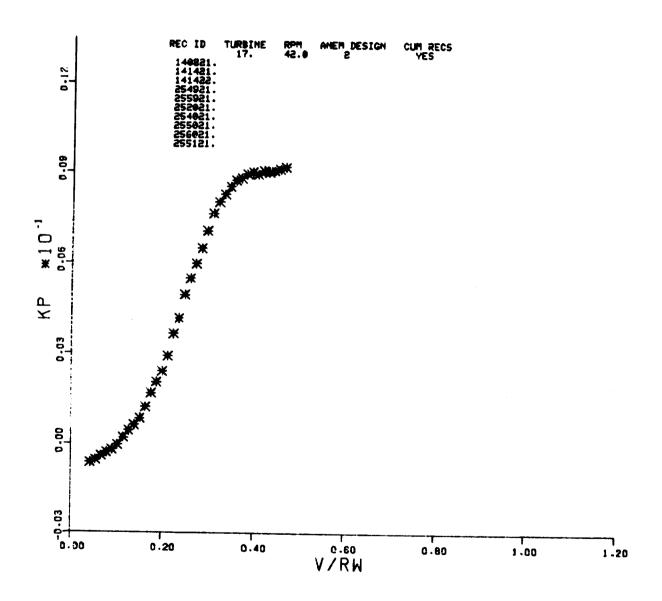
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45.5 rpm 3 Blades,  $\sigma$  = 0.21 Wind Range 6.5 to 34.5 mph

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AIR DENSITY - .0626 LBS PER CU FT
17. N TURBINE, COMBINED DATA, RPM-45.5
NUMBER SAMPLES IN ACCUMULATION - 87978.

DATA FECORD NAME($) = 142721. 142722. 15

V 5. 38. .000 -3.9004 16.21

6.5 459. .005 -3.5223 13.71

7.5 1930. .022 -2.9673 11.88

8.5 2668. .030 -2.5660 10.49

9.5 1737. .020 -1.5961 8.49

10.5 1069. .012 -.6810 8.49

11.5 753. .009 2.0669 7.75

12.5 1526. .017 3.4983 7.13

12.5 1526. .017 3.4983 7.13

13.5 2174. .036 5.1257 6.60

14.5 4577. .052 6.9954 6.15

15.5 5856. .067 9.1922 5.75

16.5 7097. .081 11.6436 5.40

17.5 7255. .082 14.4413 5.09

18.5 7106. .081 17.6451 4.82

19.5 6725. .077 21.0566 4.57

20.5 6517. .074 24.3810 4.35

21.5 5797. .066 27.9986 4.15

22.5 5032. .057 31.0806 3.36

23.5 3823. .044 34.4732 2.79

24.5 3209. .036 37.5928 3.64

25.5 2408. .027 46.5758 3.56

26.5 1527. .022 43.1552 3.36

27.5 1450. .017 46.4126 3.24

30.5 684. .027 46.5758 3.54

20.5 684. .027 46.5758 3.54

20.5 684. .027 46.5758 3.54

32.5 532. .010 50.6074 3.02

33.5 532. .004 58.2511 2.66

34.5 261. .004 58.1547 2.58

35.5 242. .003 58.1708 2.51

36.5 37. .006 58.2511 2.66

34.5 261. .004 58.1547 2.58

35.5 242. .003 58.1708 2.51

36.5 37. .006 58.2717 2.05

41.5 18. .006 57.7481 2.15

42.5 6. .006 57.7481 2.15

44.5 4. .006 63.7428 2.00

45.5 2.000 55.2828 1.96
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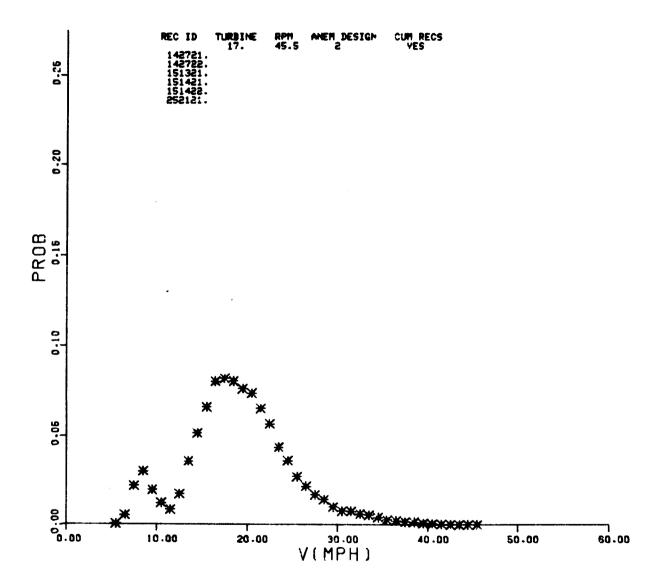
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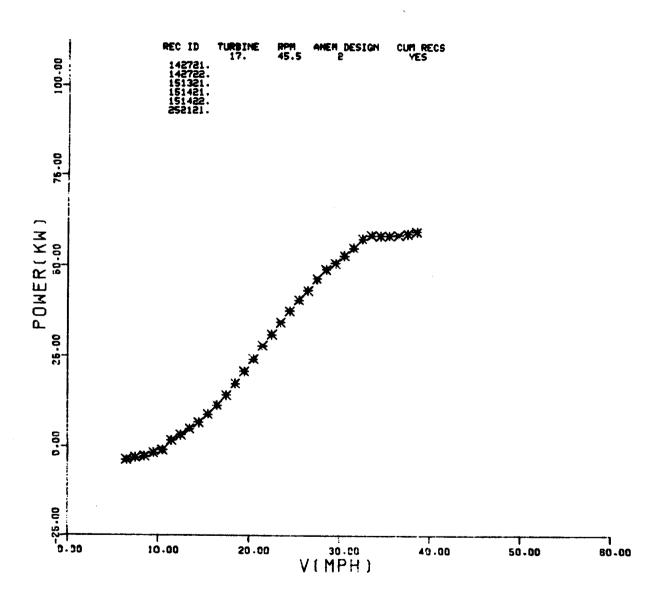
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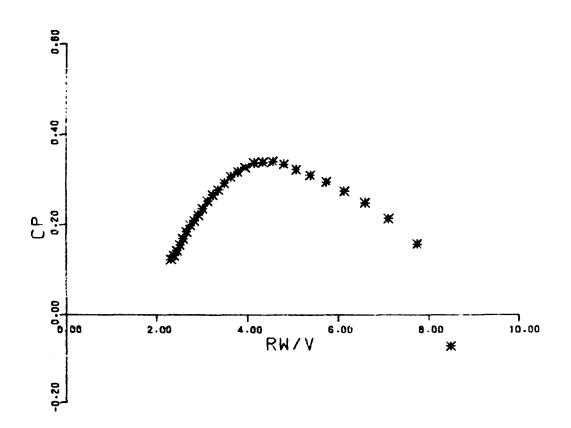
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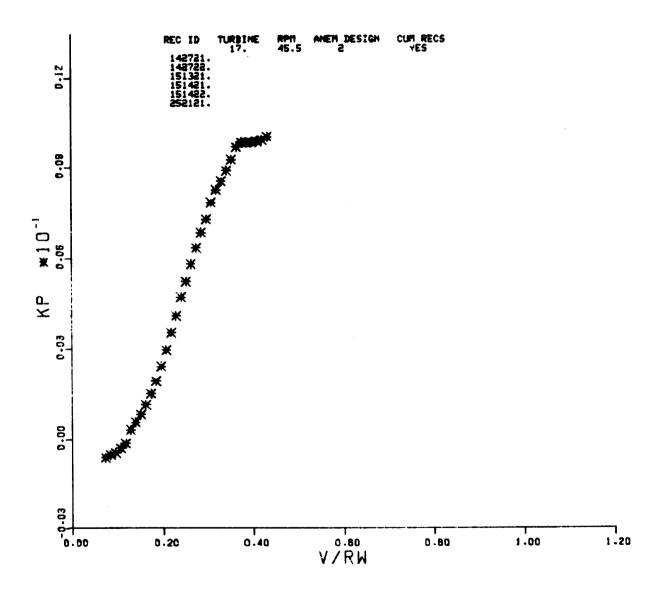
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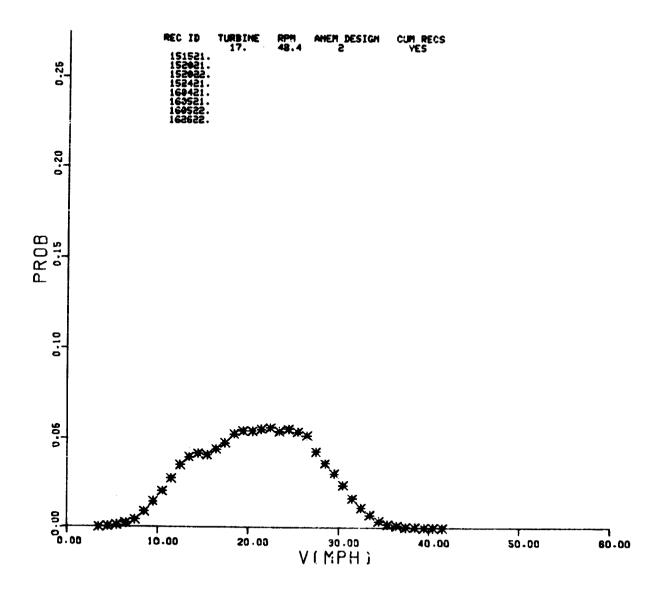


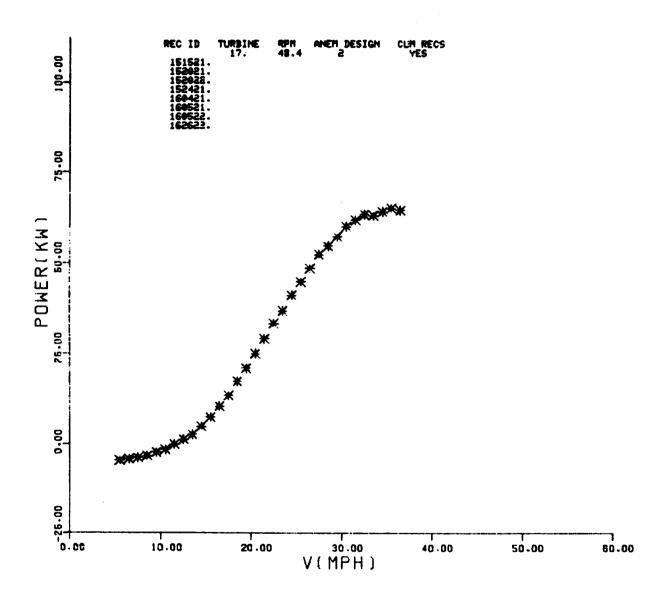


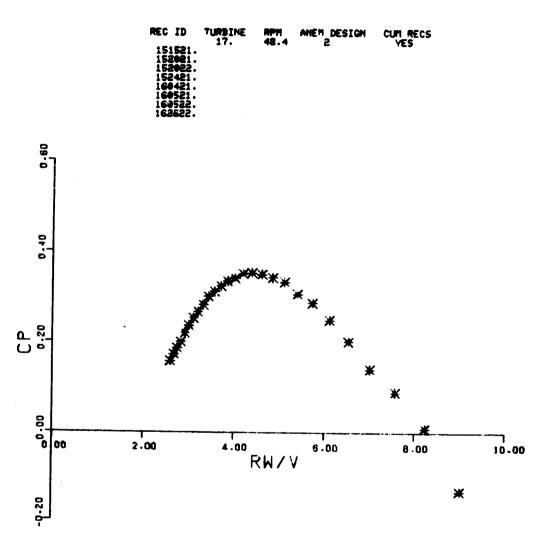


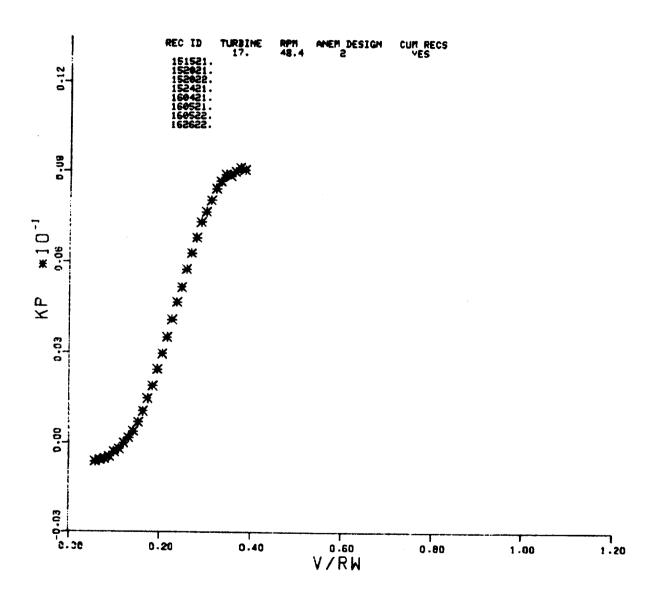
48.4 rpm  $\text{3 Blades, } \sigma = \text{0.21}$  Wind Range 6.5 to 34.5 mph

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52.5 rpm 3 Blades,  $\sigma$  = 0.21 Wind Range 4.5 to 36.5 mph

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AIR DENSITY - .0625 LBS PER CU FT
17. N TURBINE, COMBINED DATA, RPM-52.5
NUMBER SAMPLES IN ACCUMULATION - 108573.
DATA RECORD NAME(S) - 161721. 161821. 162021.

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2.5 23. .000 -5.5790 4: 14 -42.687
3.5 231. .002 -5.2073 29.38 -14.520
4.5 1130. .010 -5.2052 22.85 -6.829
5.5 1720. .016 -5.2052 22.85 -6.829
5.5 1720. .016 -5.0393 18.70 -3.621
6.5 1832. .017 -4.7425 15.82 -2.0521
6.5 1832. .017 -4.7425 15.82 -2.0521
6.5 1832. .017 -4.7425 15.82 -2.0521
6.5 1832. .018 -4.7327 13.71 -1.358
8.5 2172. .020 -4.6984 12.10 -915
9.5 2254. .021 -4.3820 10.83 -611
10.5 2118. .020 -3.9812 9.79 -411
11.5 1399. .013 -2.5675 8.94 -202
12.5 1115. .010 -1.2964 8.23 -075
13.5 1144. .011 1.1672 7.62 .057
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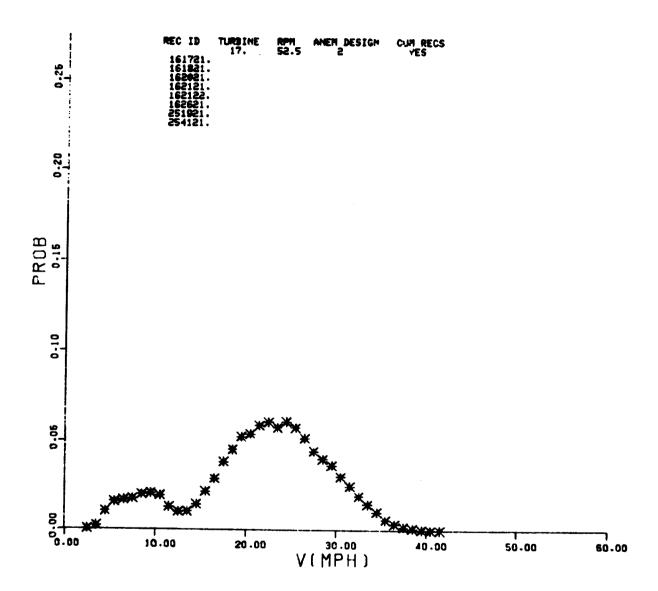
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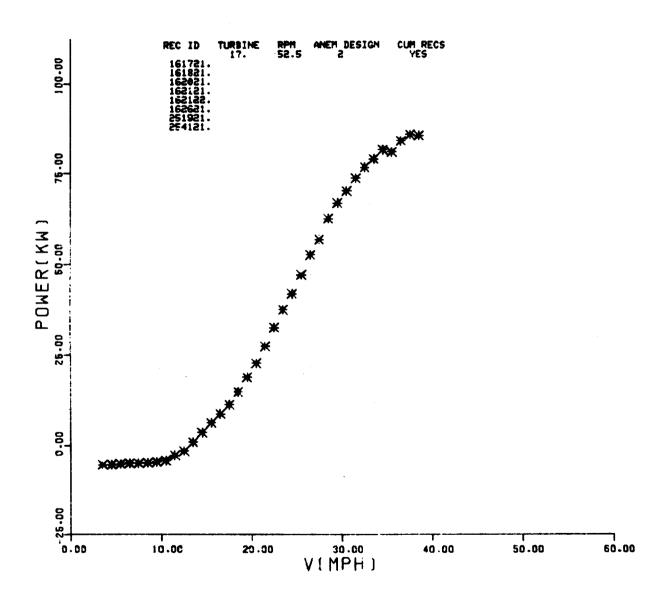
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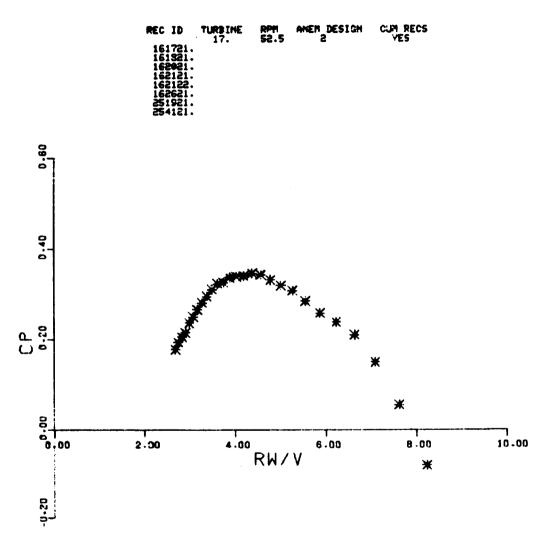
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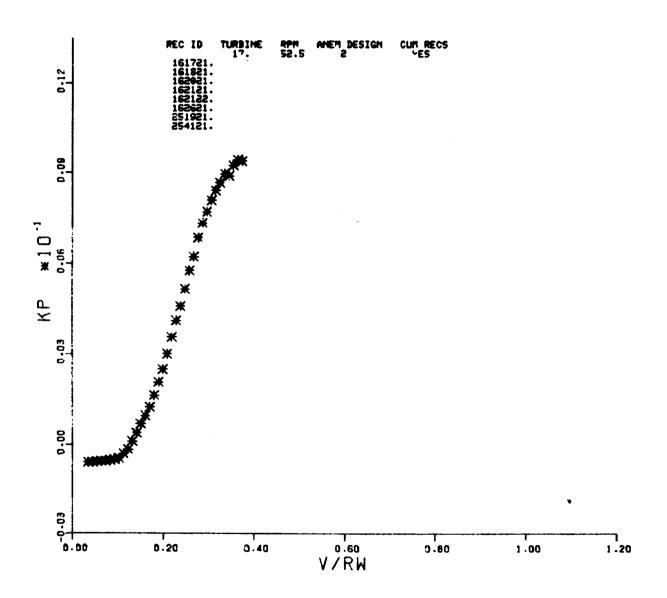
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