

SNL Structural Modeling Overview

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Sandia is a multiprogram laboratory operated by Sandia Corporation, a Lockheed Martin Company,
for the United States Department of Energy's National Nuclear Security Administration
under contract DE-AC04-94AL85000.



Sandia National Laboratories

Outline

- **Background of blade concepts at Sandia**
- **Blade structural design and analysis**
- **Wind turbine system analysis**
- **Experiments for blade and system model validation**
- **Improving models using experimental data**
- **List analysis tools used in the industry**
- **Topics for future modeling and simulation**

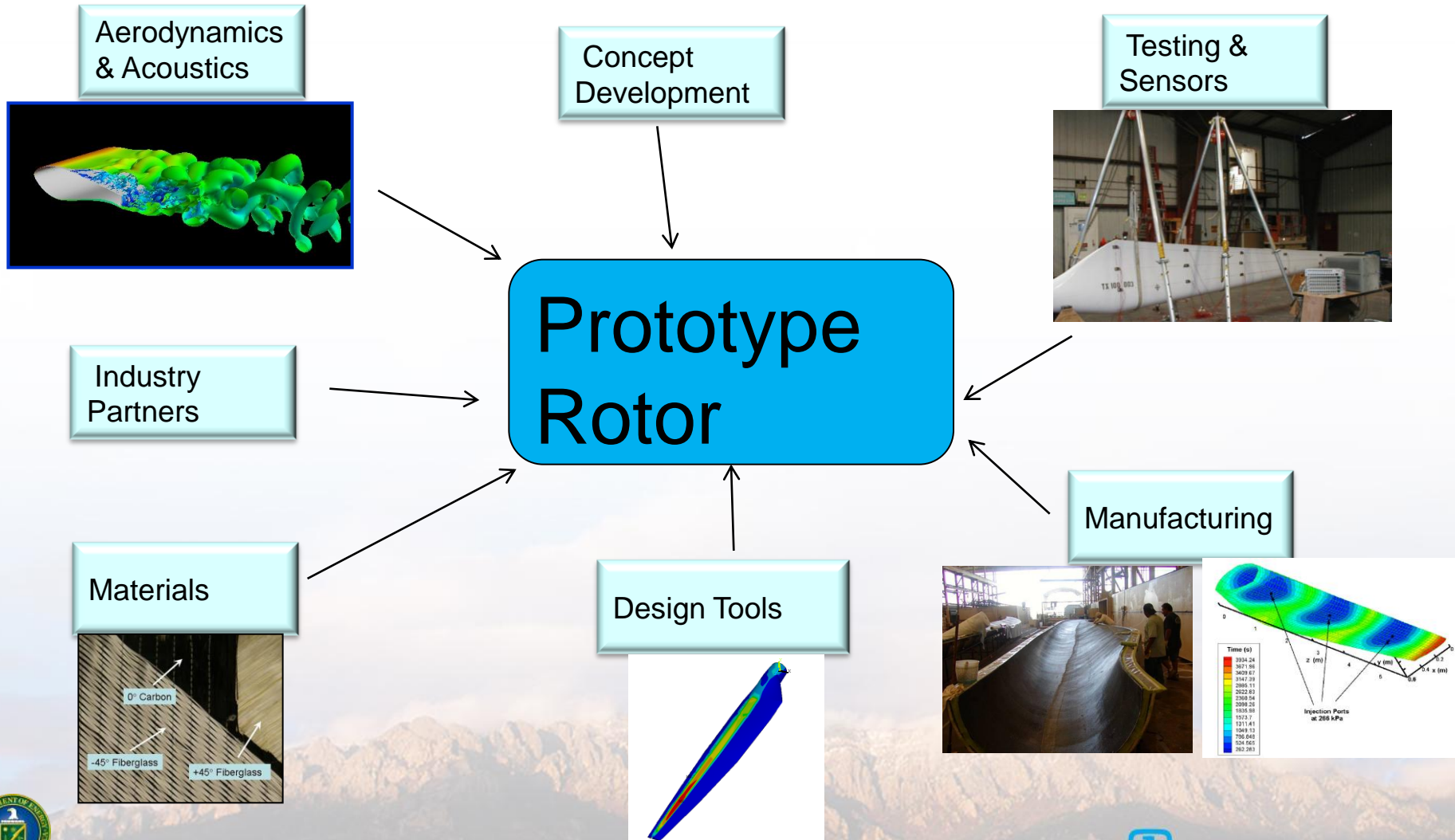


Innovative Blade Research: Major Focus

- Innovations that lead to longer & lighter blades that reduce COE
- Working with industry, have designed, built & tested several blade prototypes to demonstrate a variety of innovations



Rotor & Blade Innovation

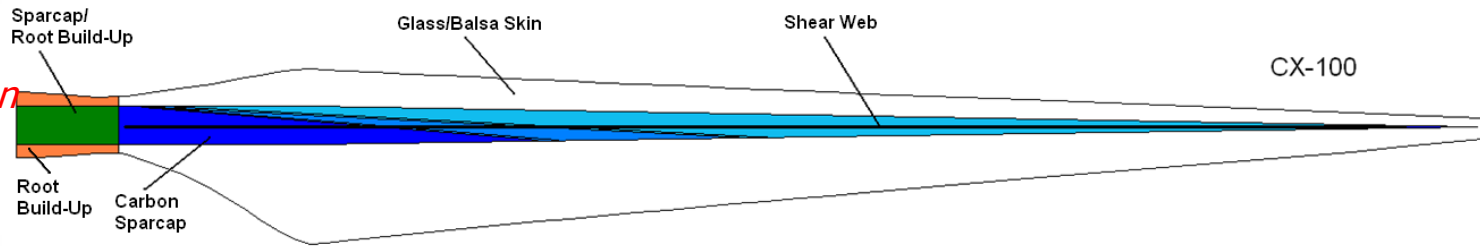


Historical SNL Research Blades

Research Goal

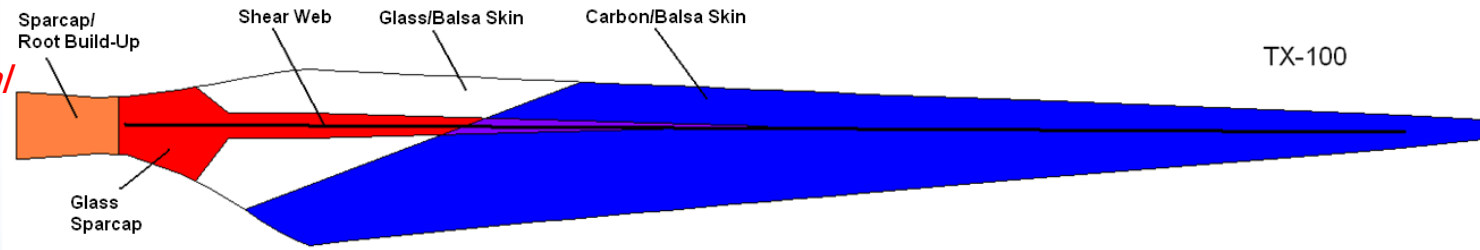
Strategic use of carbon for weight reduction

CX-100



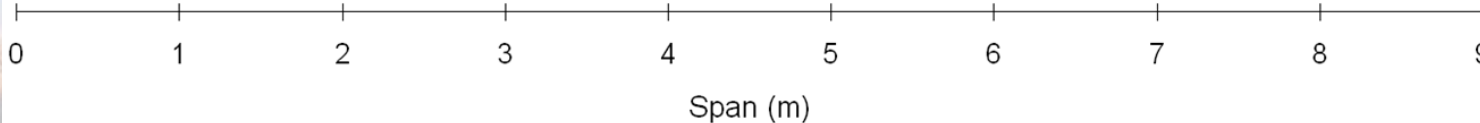
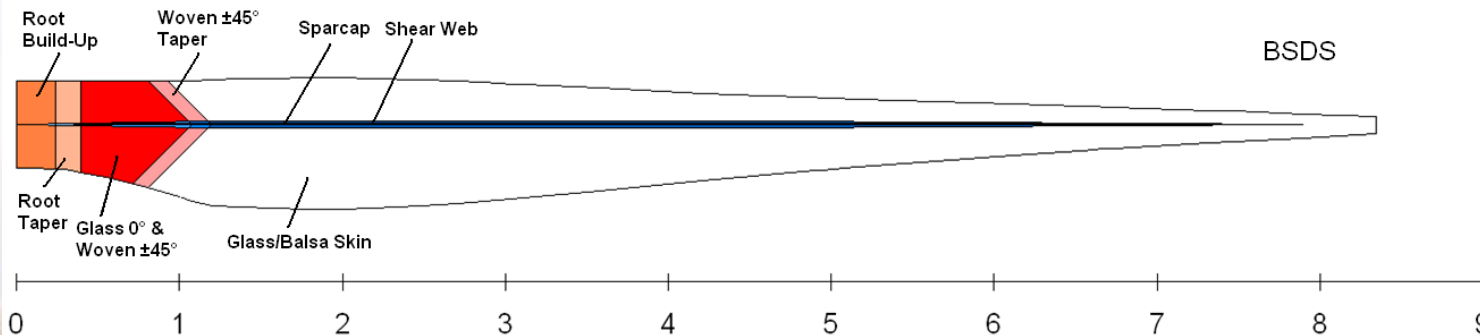
Passive aero-structural load mitigation

TX-100

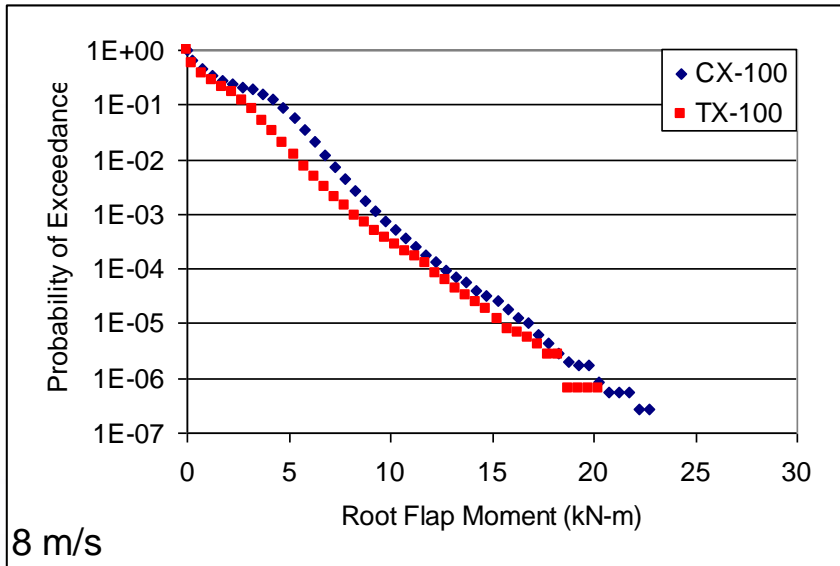


Structural efficiency improvement

BSDS

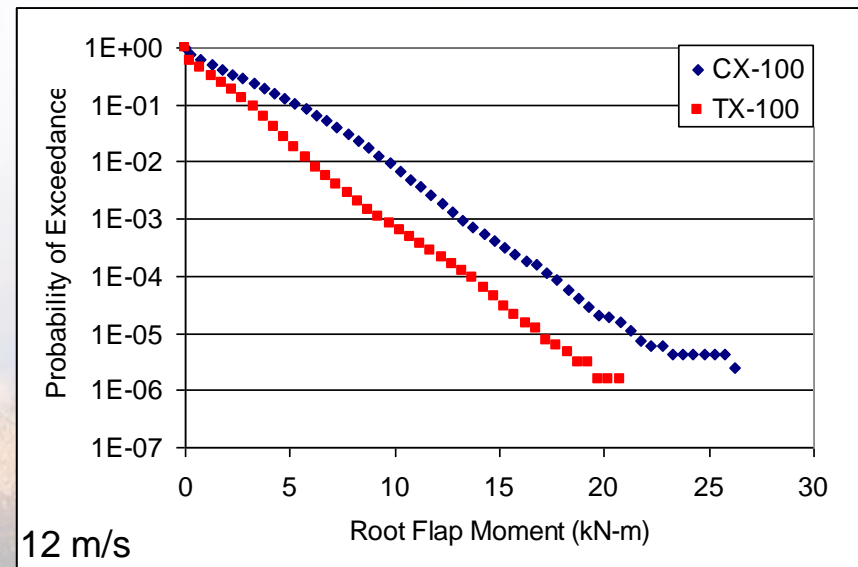
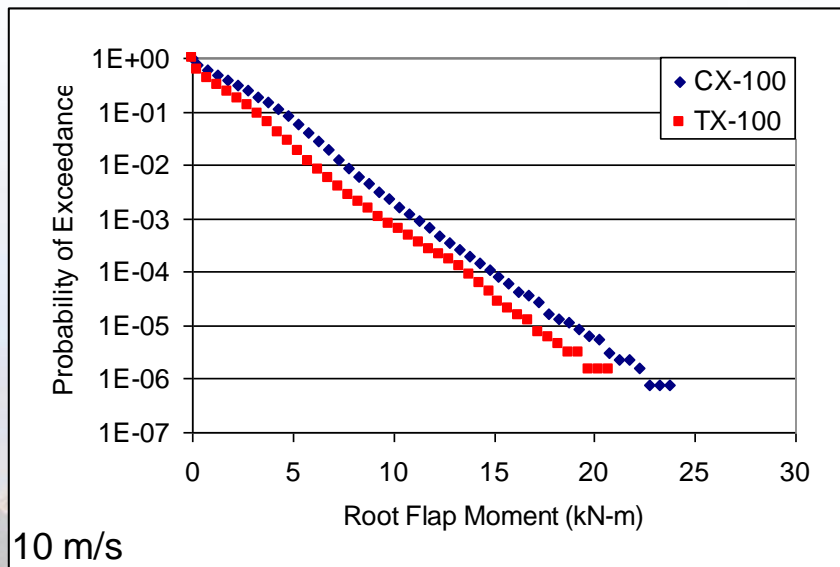


Fatigue Damage Reduction



Wind Speed (m/s)	Relative Damage Rate (%)	Relative Damage Equivalent Load (%)
7-9	-53.8%	-7.4%
9-11	-69.1%	-11.1%
11-13	-93.6%	-24.0%

Fatigue Damage Summary (TX vs. CX)



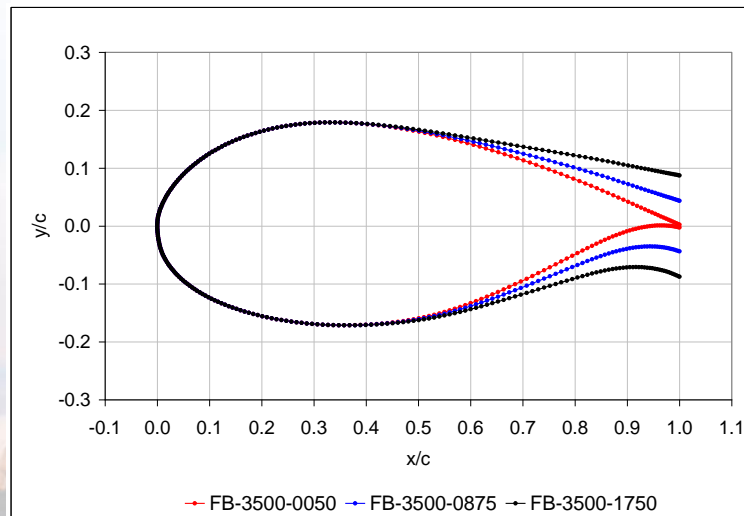
Structural Efficiency: Geometry

- Flatback airfoils created by symmetric expansion about camber line
- Less soiling sensitivity than other thick foils
- Higher structural efficiency
 - *Delayed Buckling → better material usage at failure*

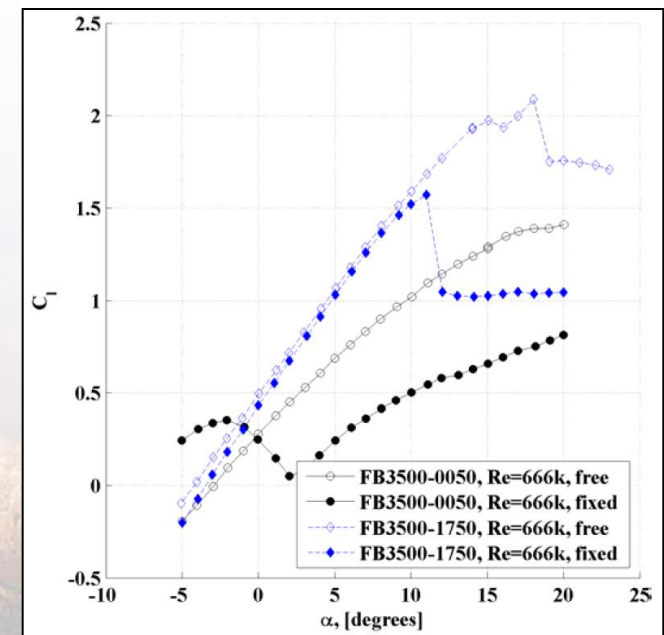
Structural Properties

Property	CX-100	TX-100	BSDS
Root Failure Moment (kN-m)	128.6	121.4	203.9
Max. Carbon Tensile Strain at Failure (%)	0.31%	0.59%	0.81%
Max. Carbon Compressive Strain at Failure (%)	0.30%	0.73%	0.87%

Flatback Airfoil Creation



Effect of Soiling



Knight & Carver STAR Blade

Cost-shared project “Sweep-Twist Adaptive Blade” began in November 2004

Goal – use geometric sweep to reduce loads through passive bend twist coupling

- **Enables a larger rotor for a given design, leading to an overall increase in energy capture**
 - ◆ **2.6 meter longer blade (24.5 → 27.1)**
 - ◆ **Predicted 5-8% increase in overall energy capture**



Advanced Rotor Development: 100-m Sandia Blade Design

- **Goal:** Provide technology research to produce innovations and advanced design concepts to develop very large utility-grade blade and rotor designs for offshore and onshore (where possible).



- **Methodology:**

- Develop and apply scaling laws to scale-up of 5 MW turbine system.
- Create 13.2 MW Sandia Baseline (100 m long blade) with detailed composite laminates
- Apply innovative concepts to baseline to reduce weight, and improve performance & cost effectiveness

- **Partners: European UpWind Program and NREL**



Challenges & Opportunities for Large Blade Development

Challenges:

Blade weight growth
Manufacturing &
reliability issues
Material volumes & cost
Transportation

Opportunities:

Very thick airfoils for structural efficiency
Material lay-up & choices
Multidisciplinary design optimization
Blade joints
Load alleviation concepts (active &
passive)
Other innovations

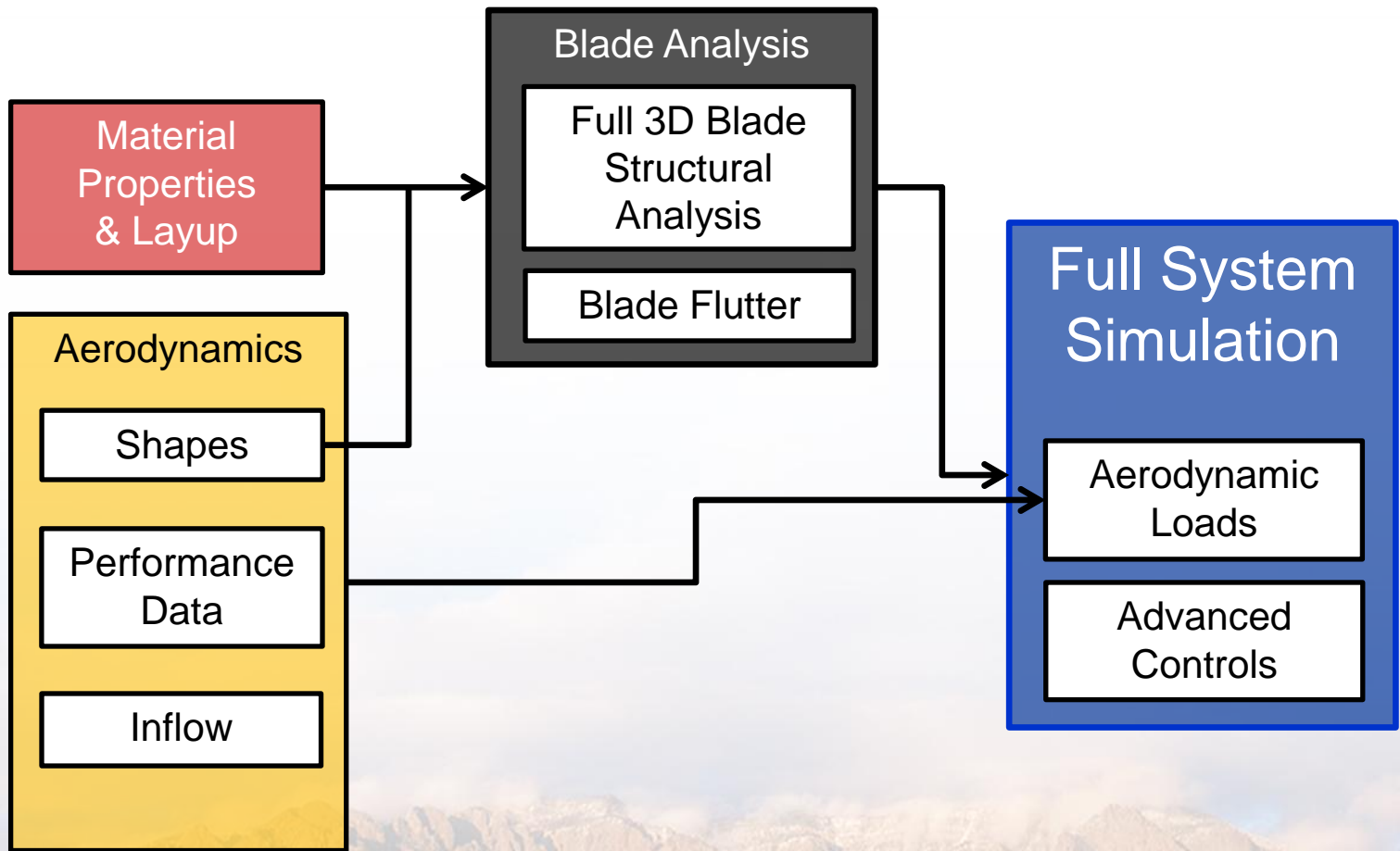


Outline

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- **Blade structural design and analysis**
- Wind turbine system analysis
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Wind Turbine Design/Analysis Elements

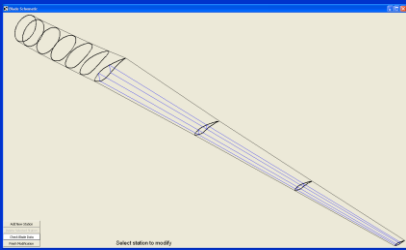


Blade Design with NuMAD

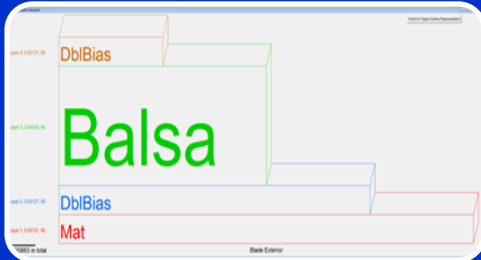
NuMAD

NuMAD:
Numerical Manufacturing
And Design Tool

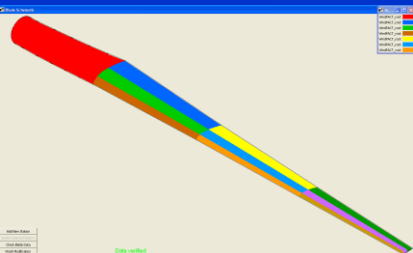
Blade Geometry



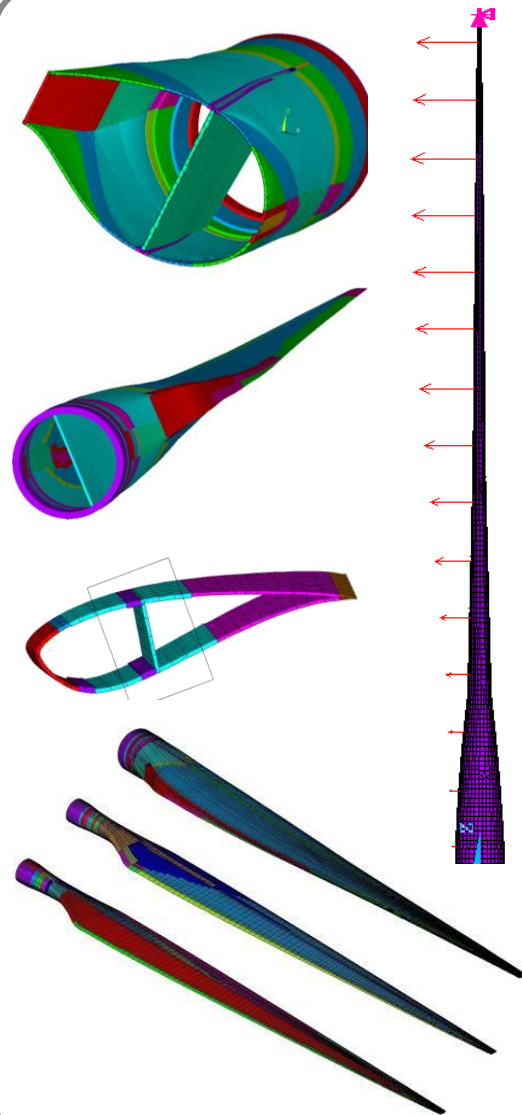
Materials & Layups



Stack Placement

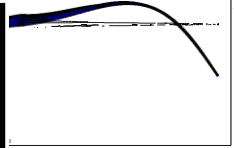
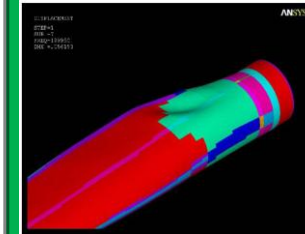


ANSYS FE Model



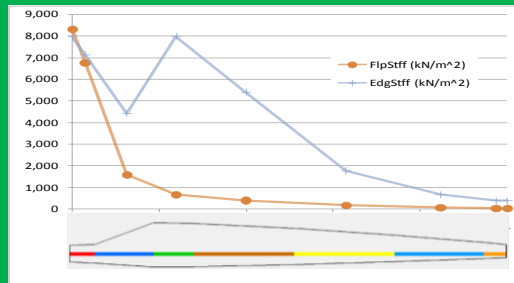
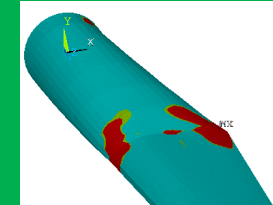
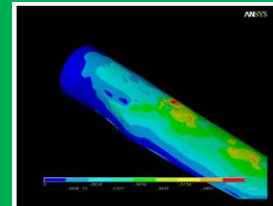
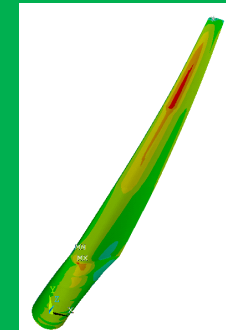
ANSYS Analysis

Modal



Buckling

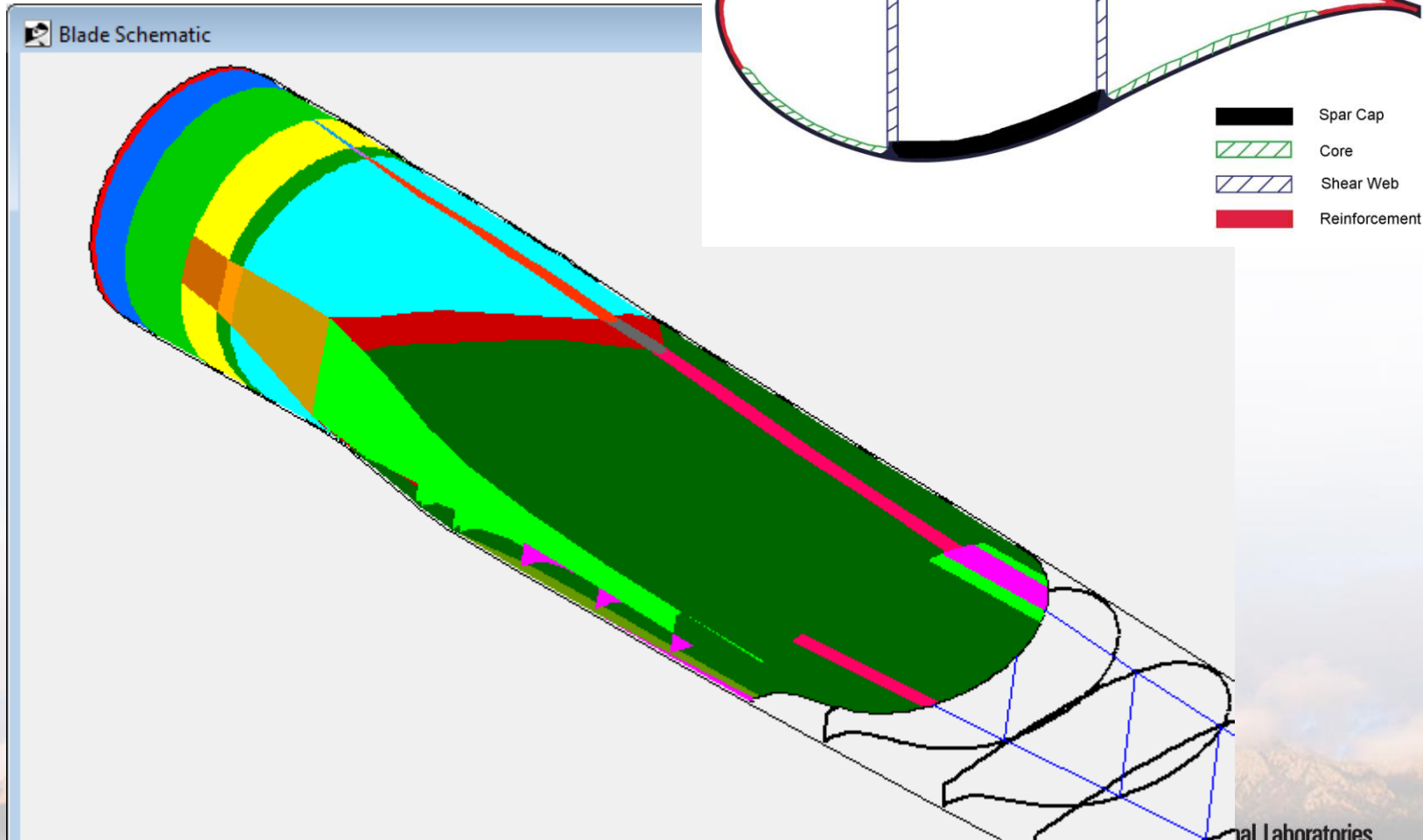
Stress & Strain



Beam Properties

NuMAD Geometry and Materials

- A complicated example:



Use of Offset-Thickness Shell Nodes

- Offset-thickness nodes are most desirable for wind turbine blade FE models because the outer blade surface is the specified surface

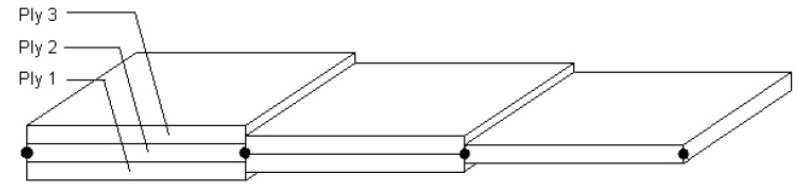


Figure 2. Schematic of physical representation of layered shell elements with nodes positioned at the mid-thickness.

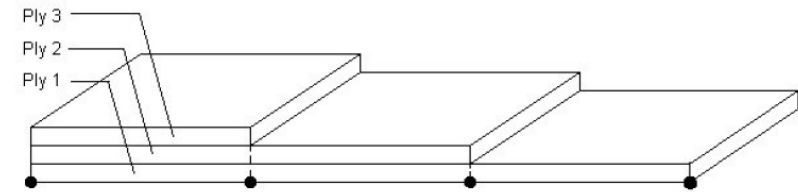
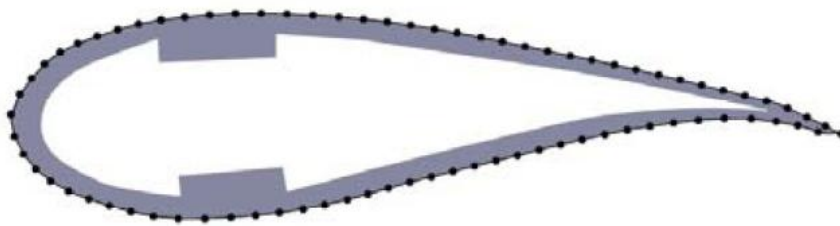


Figure 3. Schematic of physical representation of layered shell elements with nodes offset to the bottom surface.¹



(a)

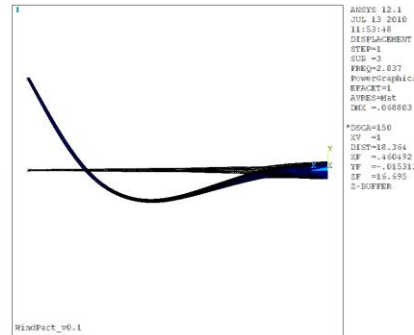
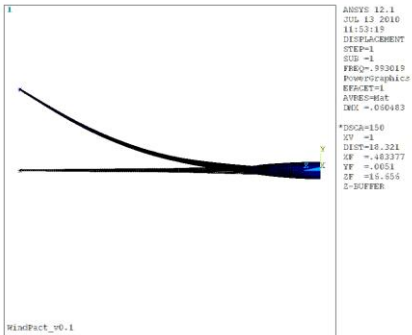


(b)

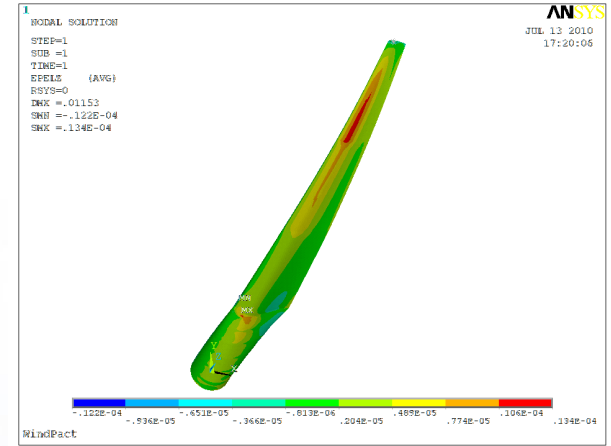
Figure 4. Blade cross-sections with nodes located at the exterior surface (a) and the mid-thickness (b).

Example ANSYS Analyses

■ Modal

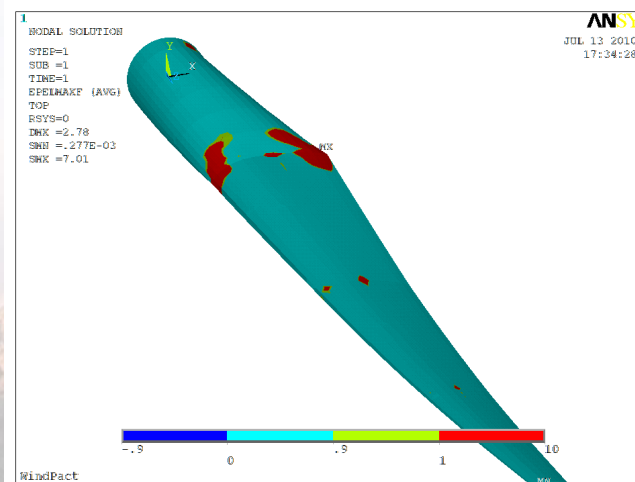


■ Strains



■ View material failure

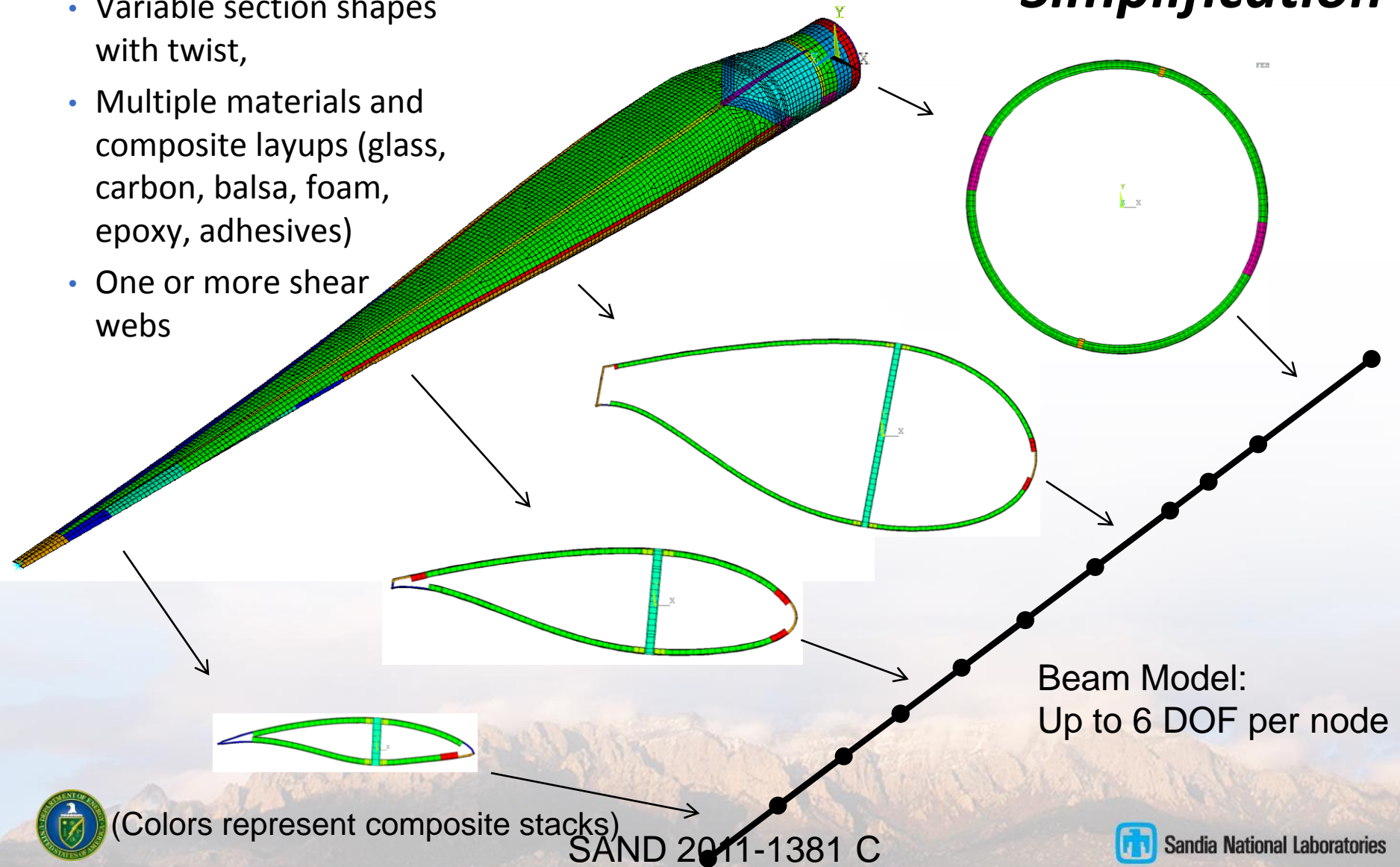
- Ultimate
- Fatigue



Blade Structural Model Simplification

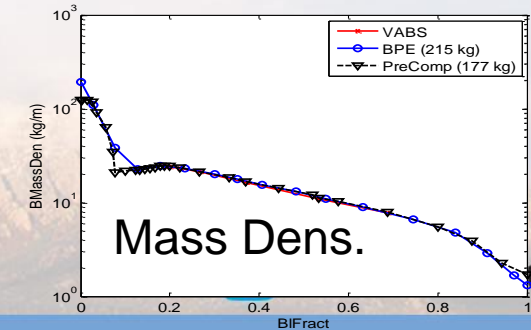
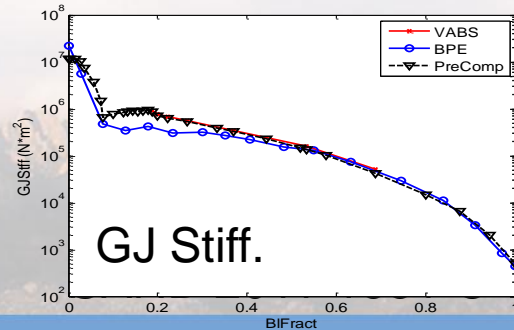
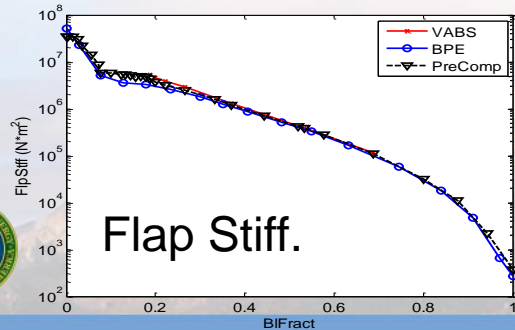
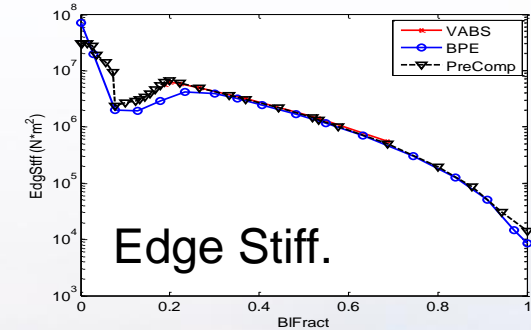
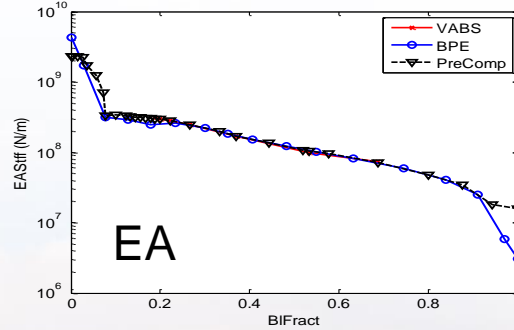
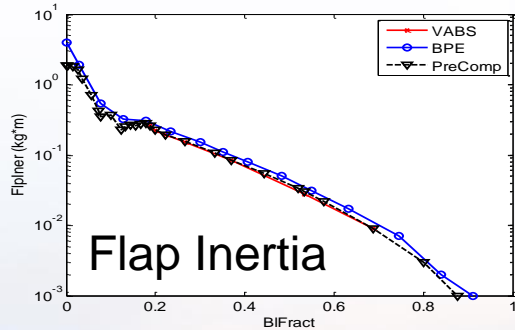
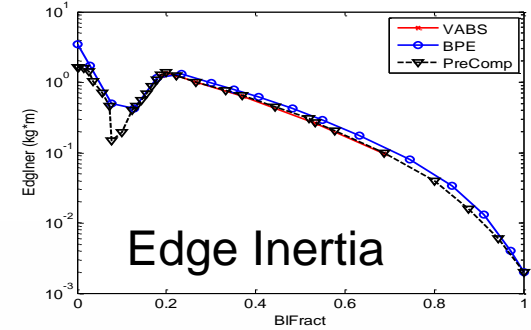
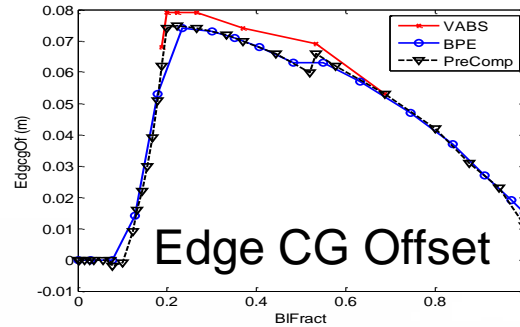
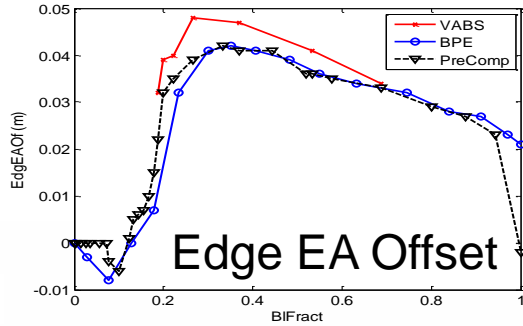
■ Wind turbine blades include

- Variable section shapes with twist,
- Multiple materials and composite layups (glass, carbon, balsa, foam, epoxy, adhesives)
- One or more shear webs

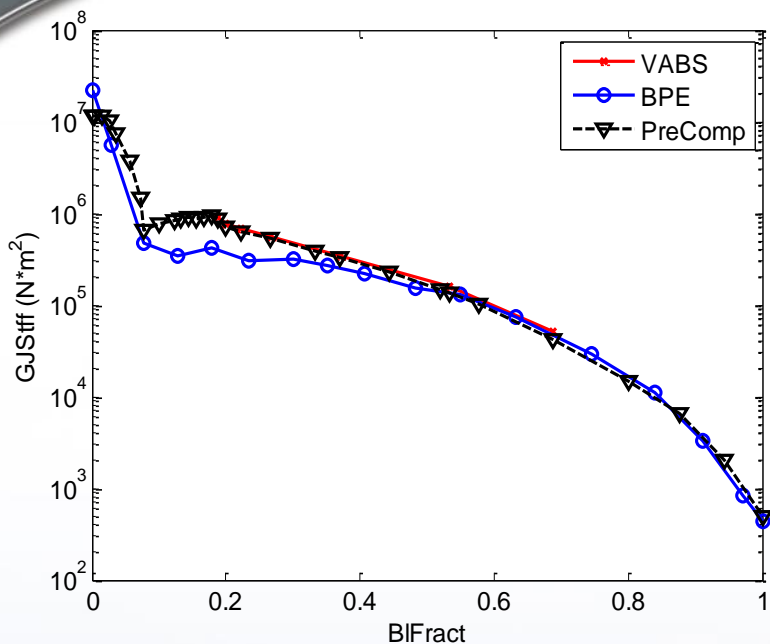


Calculate Beam Properties

Comparing three techniques: BPE, 2D Section & VABS



Torsional Stiffness and Flutter



Inputs used in classical flutter prediction

Parameter	Description
EI_flap	Flapwise bending stiffness
EI_edge	Edgewise bending stiffness
GJ	Torsional stiffness
Twist	Blade pretwist
Tiner	Torsional inertia
LCS	Lift curve slope
Elastax	Distance along the chord the elastic axis is aft of the pitch axis
Aerocntr	Fraction of the chord that the aerodynamic center is aft of the leading edge.
Masscntr	Distance the mass center is aft of the elastic axis
Chord	Section chord length

How sensitive is flutter speed to torsional stiffness?



Sandia Classical Flutter Capability

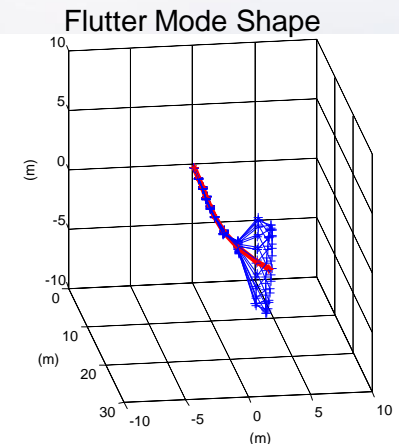
■ Current capability utilizes:

- MSC.Nastran 2005
- FAST2NAST.m (Matlab routine)
 - ◆ Required inputs: lift curve slope and pitch axis location along with information taken from ad.IPT and blade.DAT files utilized by FAST
- Fortran executable
 - ◆ Determines necessary mass, stiffness, and damping matrix additions due to aerodynamic effects (Theodorsen)
 - ◆ Generates additional Nastran decks for the **complex eigenvalue solve**

■ Iterates on operating speed, following the complex modes, to find the flutter speed

$$[M + M_a(\Omega)]\{\ddot{u}\} + [C_C(\Omega) + C_a(\omega, \Omega)]\{\dot{u}\} + [K(u_0, \Omega) + K_{tc} + K_{cs}(\Omega) + K_a(\omega, \Omega)]\{u\} = 0$$

Matrix	Description
M, C, K	Conventional matrices (with centrifugal stiffening)
$M_a(\Omega)$, $C_a(\omega, \Omega)$, $K_a(\omega, \Omega)$	Aeroelastic matrices
$C_C(\Omega)$	Coriolis
$K_{cs}(\Omega)$	Centrifugal softening
K_{tc}	Bend-twist coupling



Outline

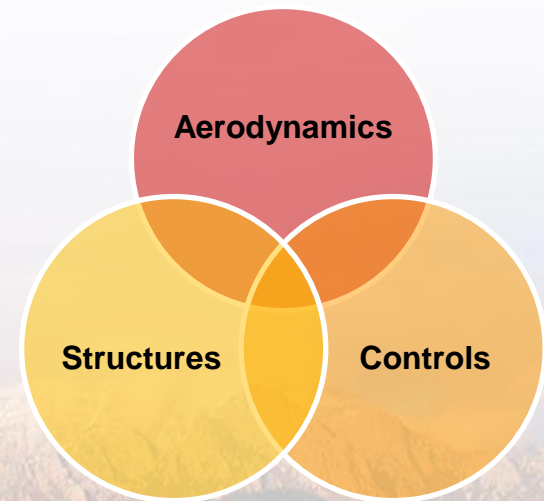
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Importance of System Analysis

- Full system analysis is required in order to evaluate the capability of the design to withstand loads prescribed by certification standards
- It is just as important to understand and report the cost of an innovation as well as the benefit; Common system costs include
 - Increased forces and moments in the system
 - Increased complexity
 - Decreased energy capture

$$COE = \frac{FCR * ICC + (O \& M)}{AEP}$$



Design Criteria Examples

Design Requirements

- Usually governed by IEC or GL Standards
- Conditions:
 - 20 year minimum design life
 - Normal wind conditions
 - Extreme wind conditions
 - Wind defined by average wind speed and turbulence intensity
- Loads
 - Ultimate loads – can the system withstand the largest expected loads?
 - Fatigue – can it withstand the combination of all loads?
 - Functional requirements – deflections (tower clearance)

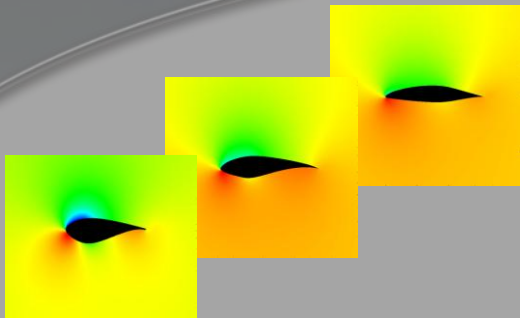
Example Load Cases

- Normal production: Fatigue and/or ultimate loads due to
 - Normal turbulence
 - Extreme turbulence
 - Extreme gust
 - ◆ Extreme wind speed
 - ◆ Extreme direction change
 - ◆ Extreme wind shear
 - Start up and shut down
- Normal production with faults
 - Yaw system fault
 - Pitch system fault
 - Loss of electrical load, etc.
- Parked Turbine
 - Extreme loads
 - Normal loads
- Transportation loads

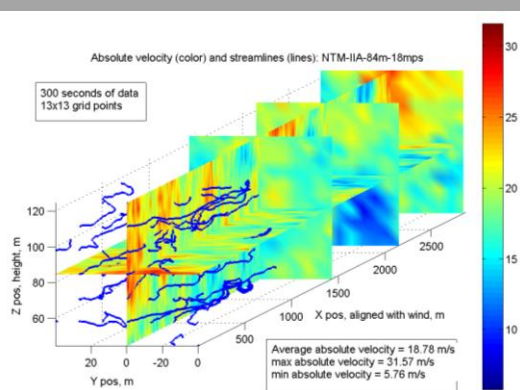


System Analysis with Wind Turbine Aeroelastic Simulation

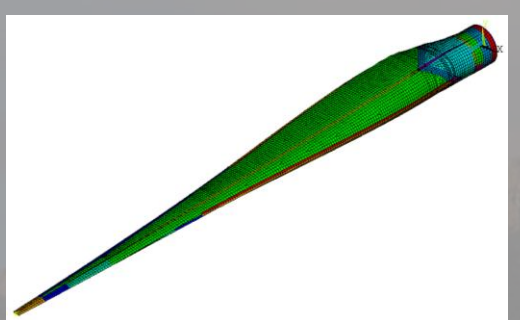
Aerodynamic Performance



Turbulent Wind Input



Structure and Materials

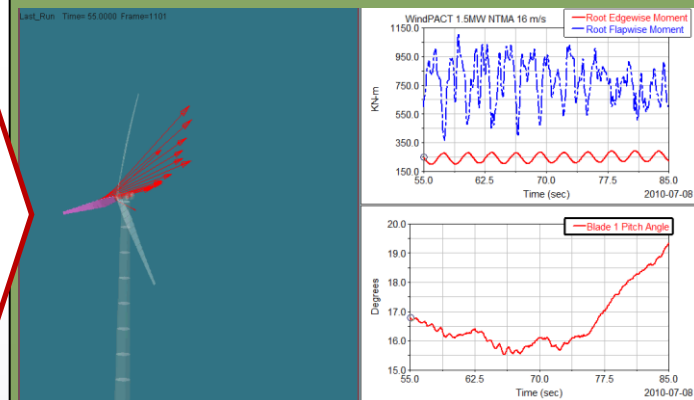


Aeroelastic System Dynamics Model

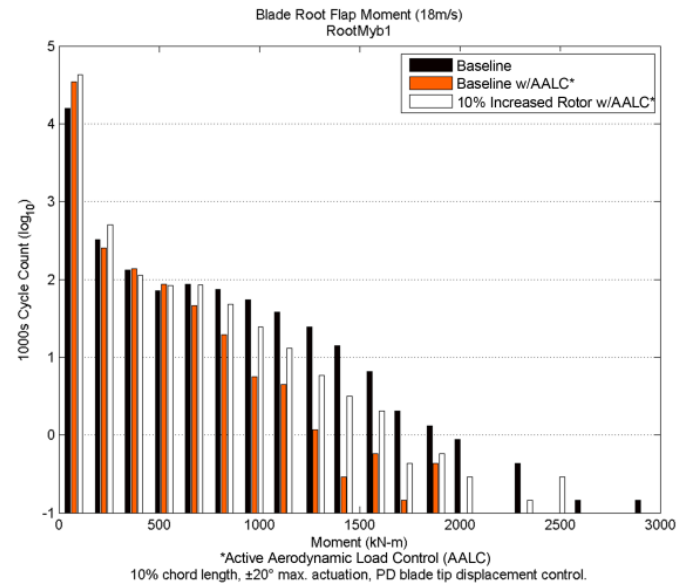
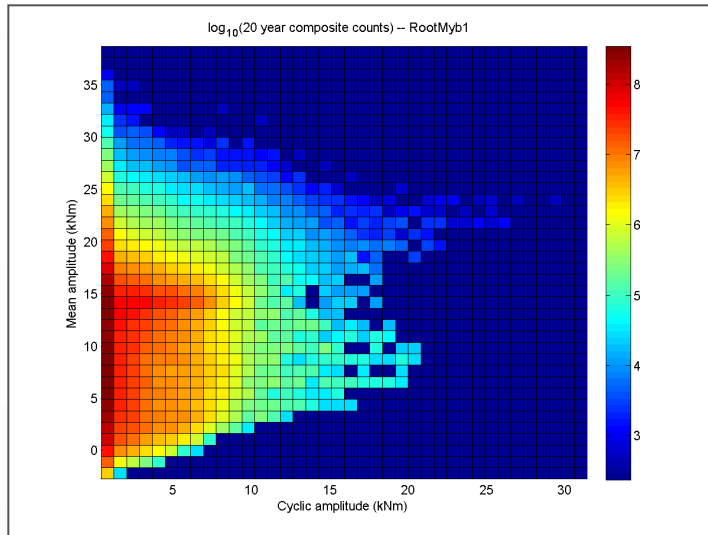


Includes Controls Implementation

System Response



Analyze System Response w.r.t Fatigue

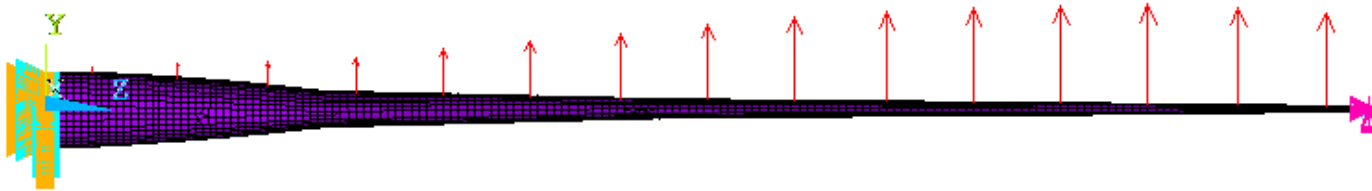


Percent Change in Equivalent Fatigue Load	9 m/s	11 m/s	18 m/s	Avg. Wind 5.5m/s	Avg. Wind 7m/s
Low Speed Shaft Torque	-1.7	-4.9	-33.5	-3.1	-7.3
Blade Root Edge Moment	1.7	1.9	-2.5	0.8	0.8
Blade Root Flap Moment	-31.2	-27.1	-30.4	-23.1	-26.3
Tower Base Side-Side Moment	-0.1	-8	-7.2	-0.9	-2.9
Tower Base Fore-Aft Moment	-18.6	-16.5	-13.8	-5	-8
Tower Top Yaw Moment	-53.2	-42.9	-43.4	-25.1	-32.2

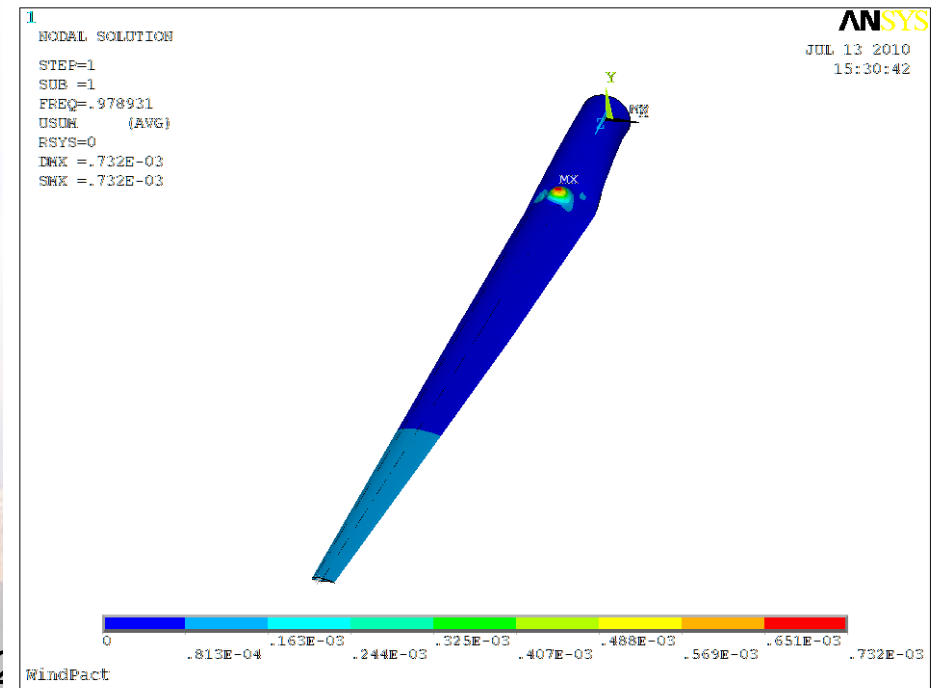


Buckling in ANSYS

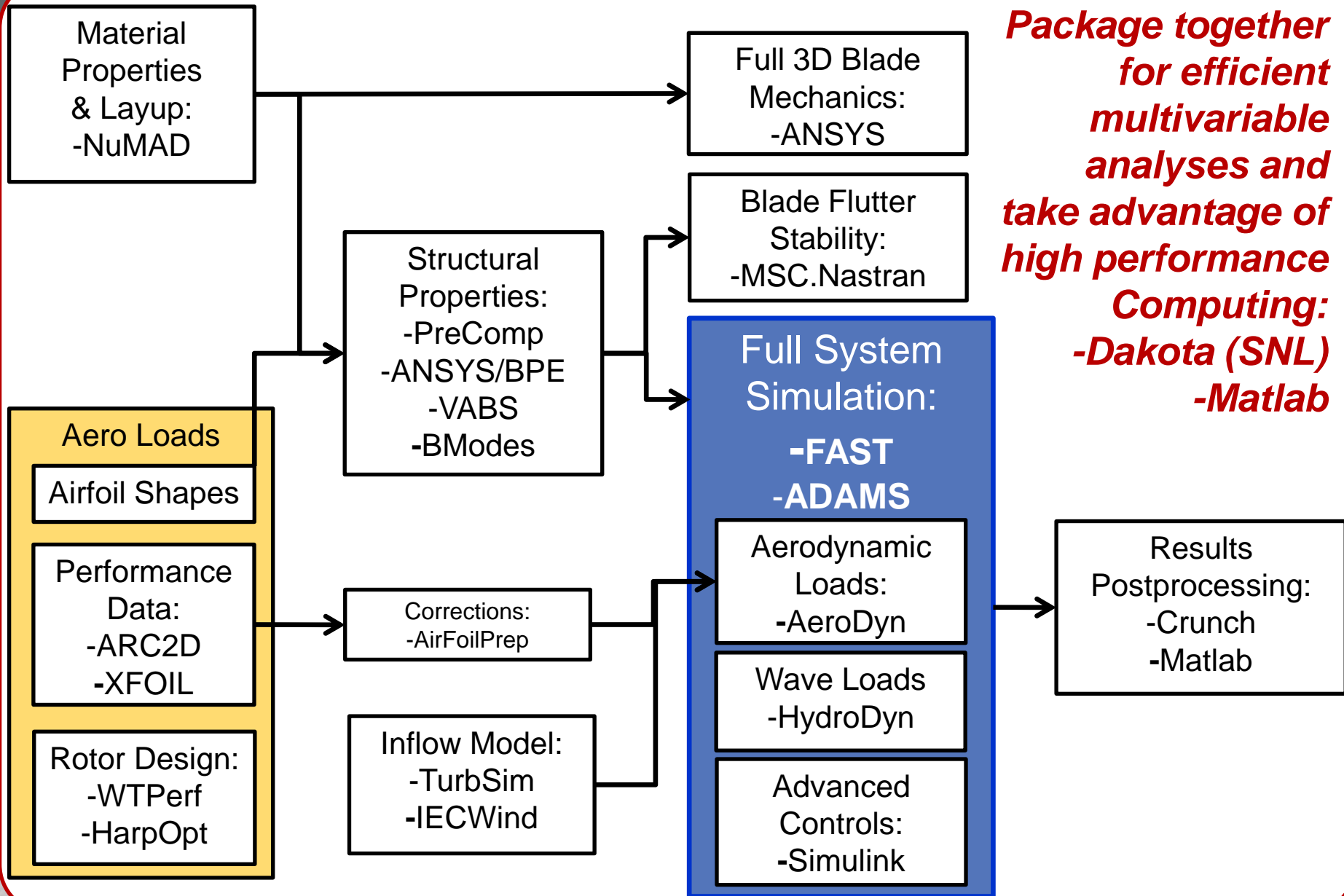
- Apply forces to nodes using aeroelastic simulation data



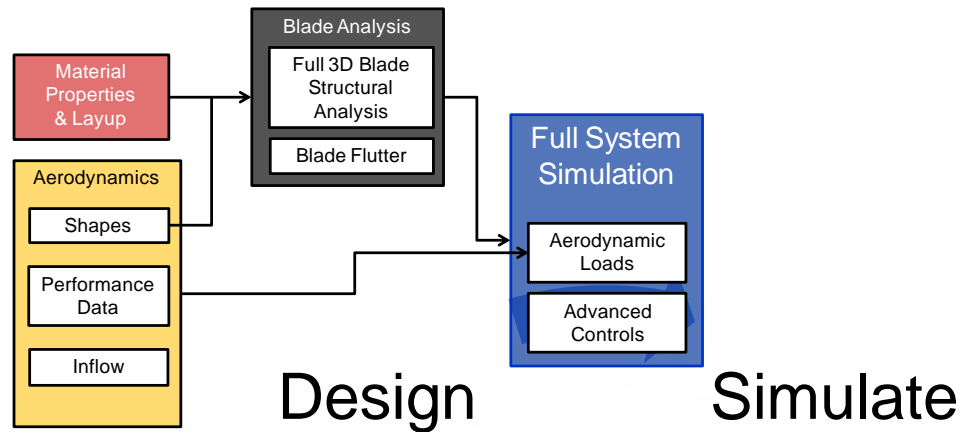
- Buckles at 0.9789 x Applied load
 - Design iteration required!



Wind Turbine Design Tools in Use at Sandia



Design & Test Loop at SNL



*Calibrate the model
or
Include missing physics*

Measure

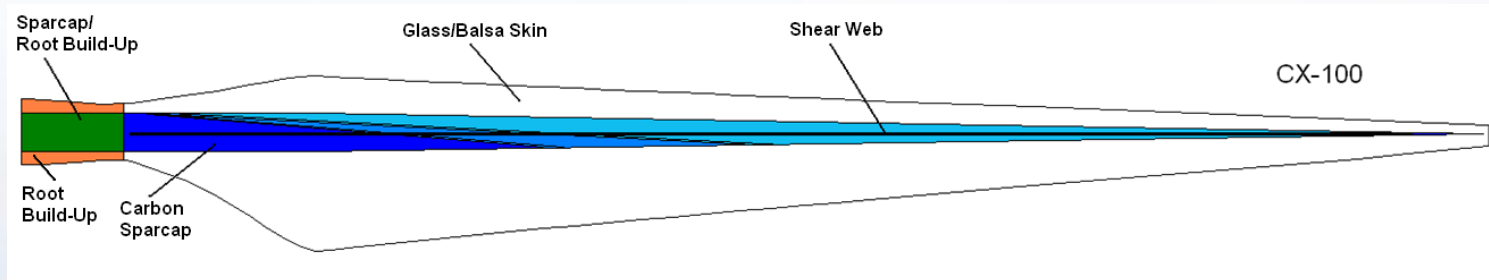
Test



Example 1



Micon turbine with 9m CX-100 blades

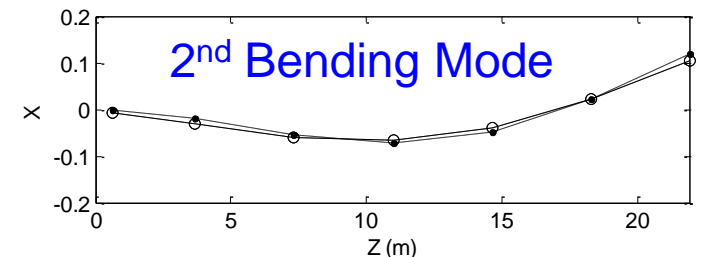
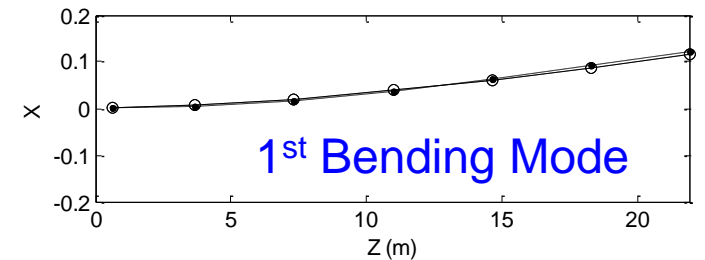


Micon Tower Modal Analysis

- Simmermacher et al. (1999) Performed Impact Test of Tower "C"



Mode	Experimental Frequency (Hz)	Analytical Beam Frequency (Hz)	Difference	Description
1	3.3	3.13	-4.9%	1st Fore-Aft Bending
2	3.3	3.13	-5.4%	1st Side-Side Bending
3	15.3	16.31	6.8%	2nd Fore-Aft Bending
4	15.8	16.31	3.5%	2nd Side-Side Bending

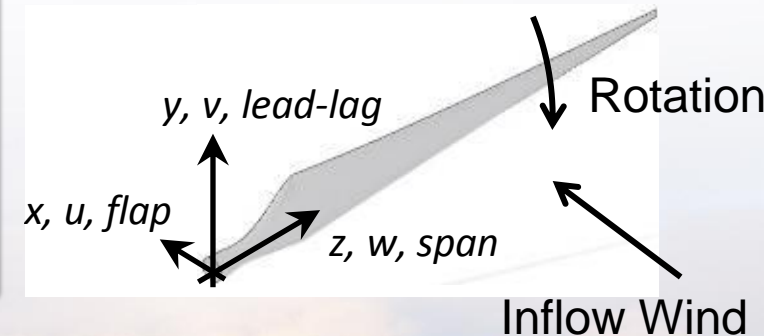


CX-100 Modal Analysis

■ Impact Test of Free-free CX-100 Sensored Rotor Blade



Mode	Experimental Frequency (Hz)	Analytical Beam Frequency (Hz)	Difference	Description
1	8.2	8.30	1.0%	1st Flap Bending
2	16.8	17.17	2.3%	1st Edge Bending
3	20.3	18.96	-6.5%	2nd Flap Bending
4	33.8	34.22	1.1%	3rd Flap Bending
5	42.2	42.19	0.0%	2nd Edge Bending
6	52.2	56.77	8.8%	4th Flap Bending

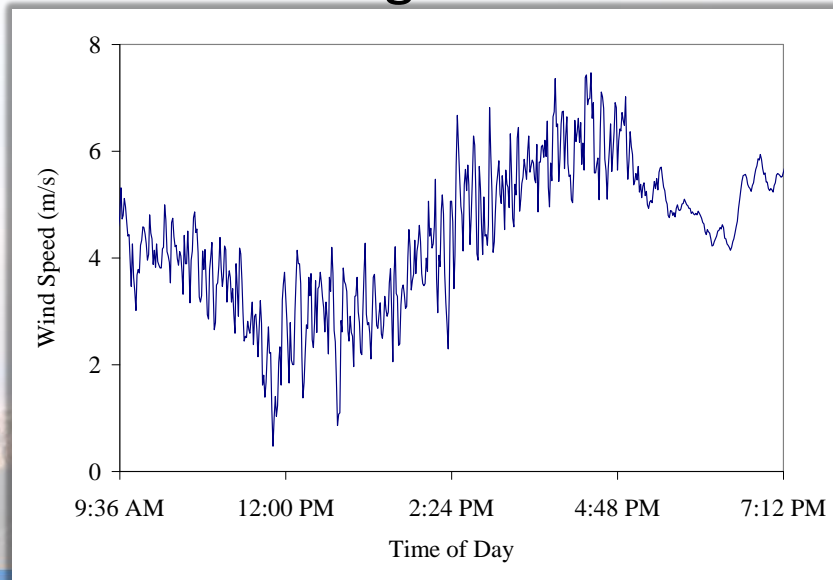


Micon 65/13M Wind Turbine Modal Analysis

■ Impact Test of Micon 65/13M Wind Turbine at Rest



■ Wind Speed Profile During Test



Ambient Excitation Makes
Experimental Testing Difficult



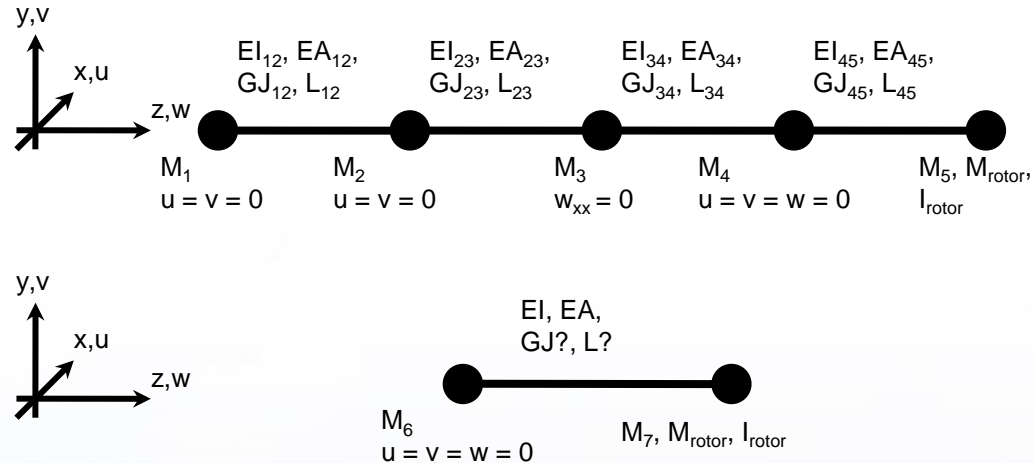
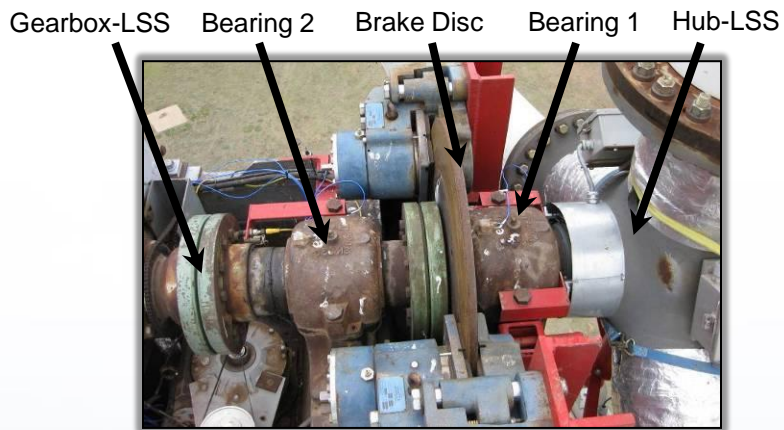
Micon 65/13M Model Comparison

Mode	Experimental Frequency (Hz)	Rigid LSS Frequency (Hz)	% Diff.	Description
1	1.30	1.33	2.3%	1st Side-Side Tower
2	1.34	1.35	0.7%	1st Fore-Aft Tower
3	3.19	3.31	4.0%	1st Rotor Torsion
4	3.26	3.61	10.8%	1st Flap Antisymmetric (about vertical axis)
5	3.45	4.21	22.2%	1st Flap Antisymmetric (about horizontal axis)
6	4.51	4.29	-4.9%	1st Flap Symmetric
7	5.35	5.86	9.6%	1st Edge Symmetric, In-phase
8	5.51	6.00	8.9%	1st Edge Symmetric, Out-phase
9	6.57	6.52	-0.7%	2nd Flap Antisymmetric (about vertical axis), Tower In-phase
10	7.17	10.13	41.2%	2nd Flap Antisymmetric (about horizontal axis), Tower In-phase
11	10.01	11.35	13.4%	2nd Flap Antisymmetric (about horizontal axis), Tower Out-phase
12	10.34	10.96	6.0%	2nd Flap Antisymmetric (about vertical axis), Tower Out-phase
13	11.49	10.90	-5.1%	2nd Flap Symmetric
14	15.41	14.85	-3.6%	2nd Rotor Torsion
Average			7.48%	
1 Std. Dev.			12.39%	



System Model Additions

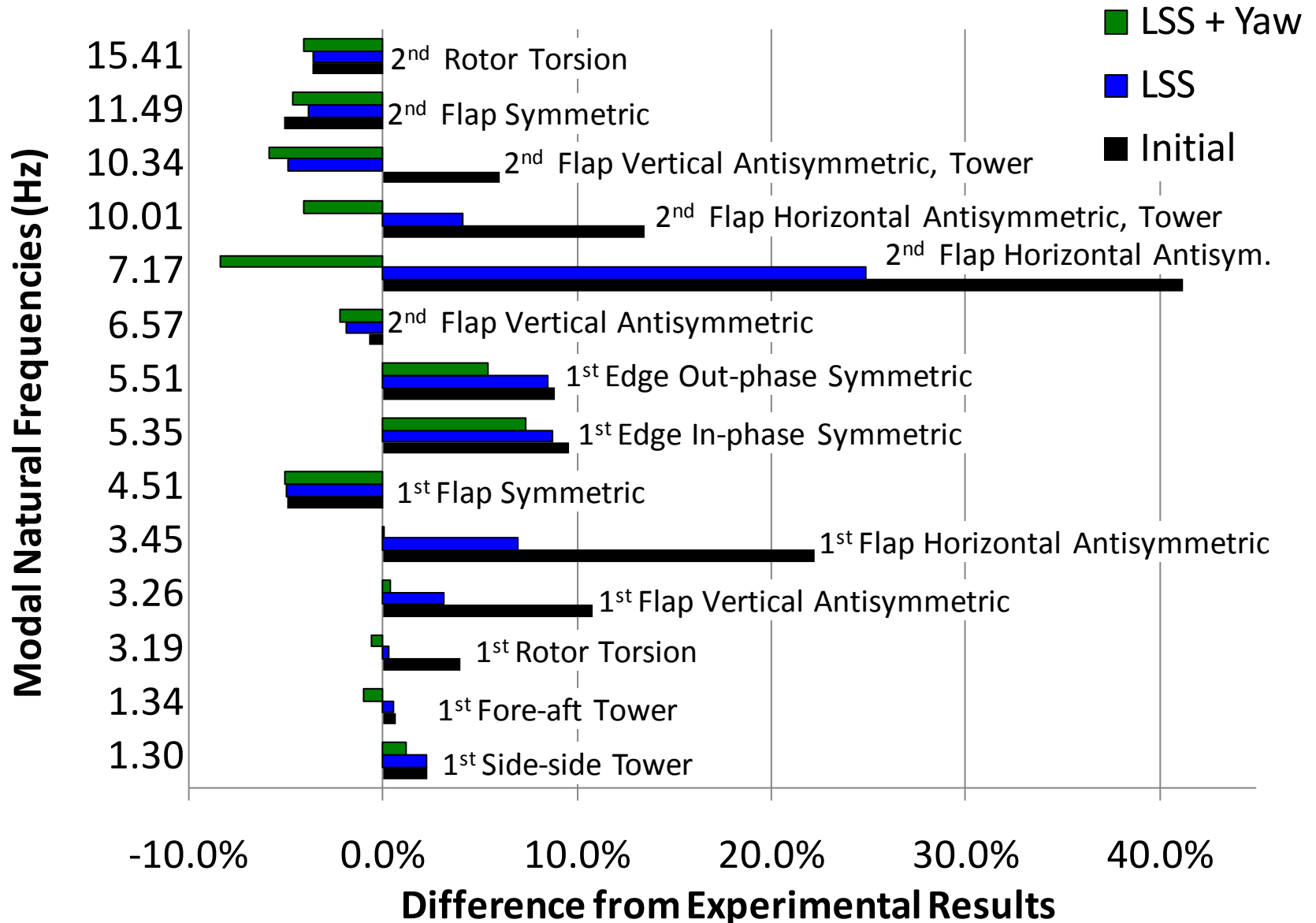
■ Develop Single Element Flexible LSS Model



■ Yaw Bearing and Brake Bending Flexibility was Un-modeled

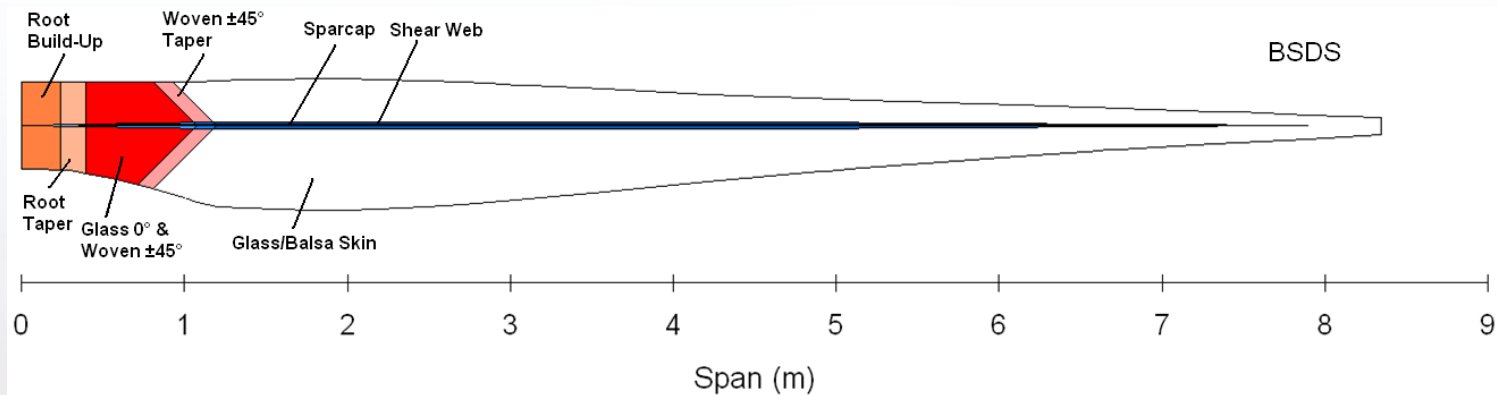


Model Update Results



Example 2

BSDS Blade

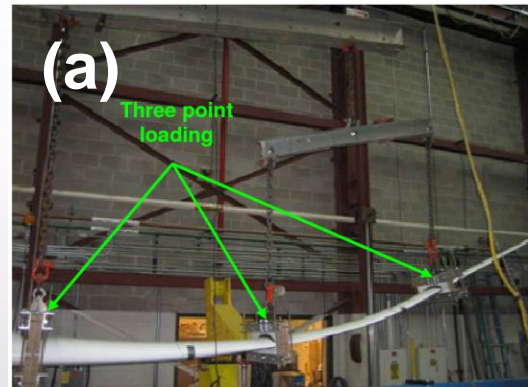
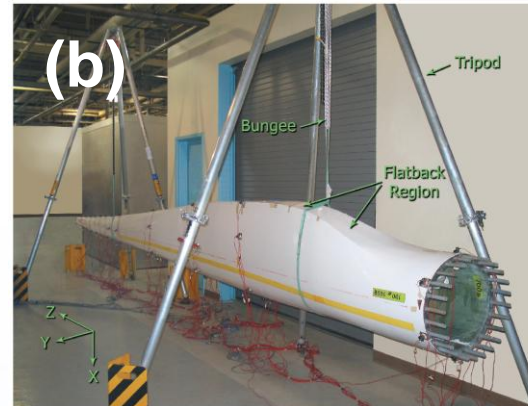


BSDS Experimentally Determined Properties

- Flap-wise stiffness distribution determined using three approaches

- (a) Static load-deflection testing
- (b) Free boundary condition modal test
- (c) Root boundary condition modal test: seismic mass on airbags

- Mass properties were measured directly from sliced sections of a BSDS blade which had been tested to failure

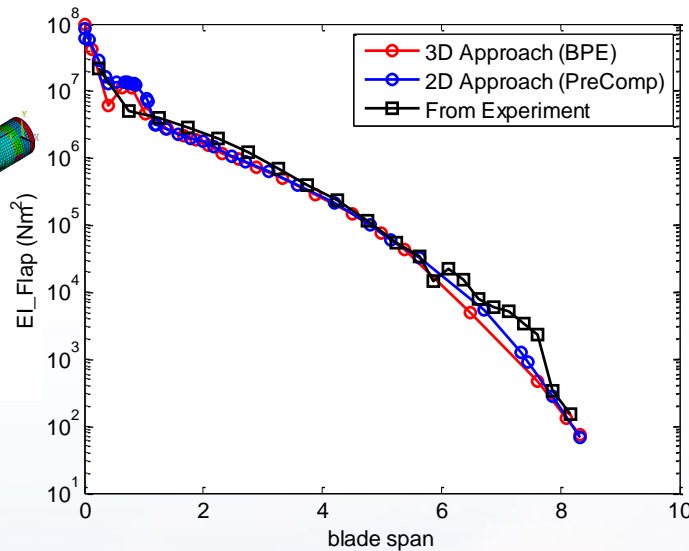


D.T.Griffith, et.al., SNL

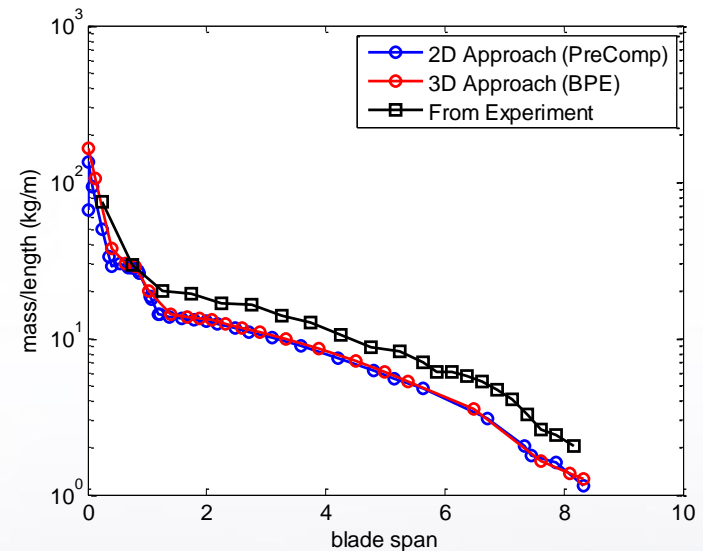


Compare Analysis and Experiment

Flapwise bending stiffness



Mass Distribution



Free-Free Beam Model	BSDS Hardware (Actual)	BPE	BPE/Hardware % Difference
Mass (kg)	127	105.6	-16.8%
1st Flap (Hz)	5.25	5.43	3.4%
2nd Flap (Hz)	13.5	12.9	-4.4%
1st Edge (Hz)	17.2	14.0	-18.6%
3rd Flap (Hz)	24.5	23.8	-3.1%



Outline

- Background of blade concepts at Sandia
- Blade structural design and analysis
- Wind turbine system analysis
- Experiments for blade and system model validation
- Improving models using experimental data
- **List analysis tools used in the industry**
- Topics for future modeling and simulation



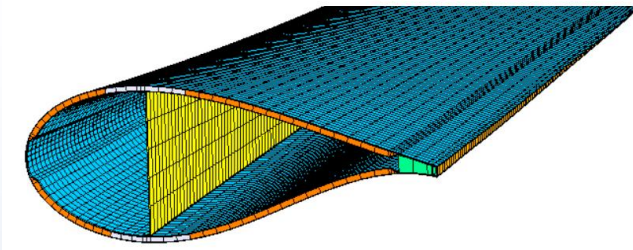
Blade Modeling Tools - Worldwide

■ Focus6

- Commercially available in modules from Knowledge Centre WMC & ECN, The Netherlands

■ ANSYS and ANSYS ACP

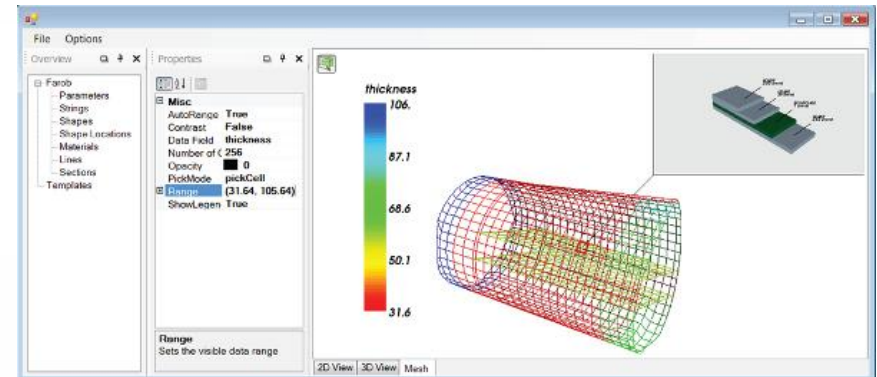
■ Abaqus



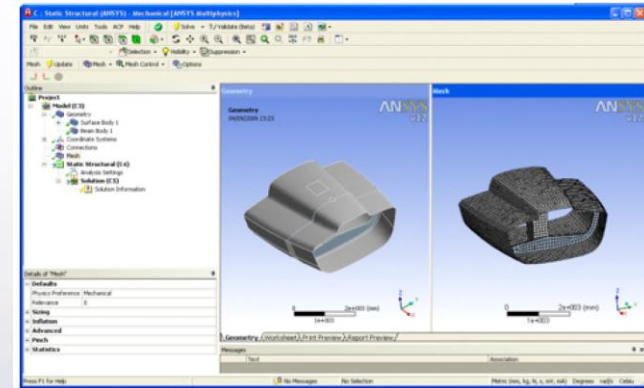
■ VABS

- There are several different efforts to look at design environments that take advantage of VABS

Focus6



ANSYS ACP



Aeroelastic Simulation Tools - Worldwide

- **Bladed, Garrad Hassan, UK**
 - Mainstream tool
- **Focus 6, WMC/ECN, The Netherlands**
 - Mainstream tool
- **HAWC2, Riso National Lab, Denmark**
- **Flex5, DTU**
- **FAST and AeroDyn, NWTCC-NREL, United States**
 - Very popular in the research community
- **MSC.ADAMS and AeroDyn**
 - Used in some of the more challenging/innovative projects
- **Full Blade FE Model coupled with multibody dynamics (and possibly CFD)**
- **DU_SWAMP, TU-Delft, The Netherlands**
 - Simulink-based multibody dynamics for advanced controls simulation
 - A very young code



SNL Structural Tools Activities Moving Forward

In order of completion; near-term first

- **Application of blade loads from aeroelastic simulation to the NuMAD/ANSYS finite element blade model**
- **Implementation of NuMAD in Matlab: Experiencing increased usage by industry and researchers**
- **Creation of a parametric wind turbine system analysis toolbox in Matlab: For highly effective setup, execution and analysis of a very large numbers of simulations**
- **Detailed structural models from NuMAD: i.e. Brick elements**

Future research areas

- **Passive and active fatigue load mitigation concepts**
- **Damage and defect modeling**
- **Full system aeroelastic stability**

