

# SOP 24

## Calculation of the fugacity of carbon dioxide in pure carbon dioxide gas or in air

### 1. Scope and field of application

This procedure describes a method for the calculation of the fugacity of carbon dioxide in pure carbon dioxide gas or in air. The fugacity,  $f(\text{CO}_2)$ , is expressed either in Pascals or in atmospheres<sup>1</sup>.

### 2. Definition

The chemical potential ( $\mu_B$ ) of an individual component of a vapor phase can be expressed in terms of its fugacity ( $f_B$ ). This is defined by the equation

$$RT \ln f_B = \mu_B - \lim_{p \rightarrow 0} [\mu_B - RT \ln(x_B p / p^\circ)] \quad (1)$$

where  $x_B$  is the mole fraction of B in the gaseous mixture and thus  $x_B p$  is the partial pressure of B ( $p_B$ ) in the vapor phase and  $p^\circ$  is a standard pressure (typically 101325 Pa, *i.e.*, 1 atm). The term

$$\lim_{p \rightarrow 0} [\mu_B - RT \ln(x_B p / p^\circ)] \quad (2)$$

is thus a standard chemical potential,  $\mu_B^\circ(T)$ .

### 3. Principle

The vapor phase fugacity of either a pure gas ( $x_B = 1$ ) or of a component in a mixture of gases can be calculated from the equation

$$f_B = x_B p \exp\left(\frac{1}{RT} \int_0^p (V_B - RT/p') dp'\right). \quad (3)$$

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<sup>1</sup> 1 atm = 101325 Pa.

$V_B$  is obtained from

$$V_B = \left( \frac{\partial V}{\partial n_B} \right)_{T,p}, \quad (4)$$

where  $V$  is given by an equation of state for the vapor,

$$V = f(T, p). \quad (5)$$

### 3.1 The ideal gas equation

The simplest equation of state is the expression for a perfect gas mixture,

$$V = \frac{RT}{p} \sum_B n_B. \quad (6)$$

The integral in equation (3) is then equal to zero and

$$f_B = x_B p. \quad (7)$$

### 3.2 The virial equation

More generally, the equation of state can be represented by a virial expression,

$$\frac{pV_B}{RT} = 1 + \frac{B(T)}{V_B} + \frac{C(T)}{V_B^2} + \dots \quad (8)$$

This equation, truncated after the second virial coefficient, is usually adequate to represent  $p$ - $V$ - $T$  properties at pressures up to a few atmospheres. It also has the advantage that the coefficient,  $B(T)$ , can be related to the intermolecular potential energy function of the molecules concerned.

In a mixture of gases,

$$B(T) = \sum_l \sum_m x_l x_m B_{lm}(T) \quad (9)$$

where  $B_{lm} = B_{ml}$ . The total volume can then be written as

$$V = \sum_k n_k V_k = \sum_k n_k \frac{RT}{p} + \frac{\sum_l \sum_m n_l n_m B_{lm}(T)}{\sum_k n_k}. \quad (10)$$

The partial molar volume of an individual component is

$$V_B = \frac{RT}{p} - \frac{\sum_l \sum_m n_l n_m B_{lm}(T)}{\left( \sum_k n_k \right)^2} + \frac{2 \sum_m n_m B_{Bm}(T)}{\sum_k n_k} \quad (11)$$

and thus

$$V_B = \frac{RT}{p} + \sum_l \sum_m x_l x_m [2B_{Bm}(T) - B_{lm}(T)]p. \quad (12)$$

The fugacity is then given by

$$f_B = x_B p \exp\left(\frac{\sum_l \sum_m x_l x_m (2B_{Bm}(T) - B_{lm}(T))p}{RT}\right). \quad (13)$$

For a pure gas, this reduces to

$$f_B = p \exp\left(\frac{B_{BB}(T)p}{RT}\right) \quad (14)$$

where  $B_{BB}(T)$  is the virial coefficient for the pure gas, B.

A further particular case of equation (13) is the expression for a component of a binary mixture,

$$f_B = x_B p \exp\left[\left(B_{BB}(T) + 2x_C^2 \delta_{B-C}(T)\right) \frac{p}{RT}\right] \quad (15)$$

where

$$\delta_{B-C} = B_{BC} - \frac{1}{2}(B_{BB} + B_{CC}). \quad (16)$$

Many of the cross-virial coefficients for the practical computation of fugacity in vapor mixtures have never been measured experimentally. However, a number of empirical approaches can be used.

The simplest of these is the Lewis and Randall rule,

$$f_B = x_B f_B^* \quad (17)$$

where  $f_B^*$  is the fugacity of pure component, B, at the same temperature and total pressure as the mixture (equation 14).

An alternate method of predicting  $B(T)$ , based on statistical–mechanical arguments, is to use the expression

$$B(T) = 2\pi L \int_0^{\infty} [1 - \exp(-u(r)/kT)] r^2 dr \quad (18)$$

where  $L$  is the Avogadro constant and  $k$  the Boltzmann constant. Here,  $u(r)$ —the pair-interaction energy—is assumed to depend only on the separation,  $r$ , of the centers of mass of two molecules.

## 4. Calculation and expression of results

### 4.1 Virial coefficient of pure carbon dioxide gas

The first virial coefficient of CO<sub>2</sub>,  $B(\text{CO}_2, T)$ , is given by the expression (Weiss, 1974) which is based on values reported by Levelt Sengers *et al.* (1971):

$$\frac{B(\text{CO}_2, T)}{\text{cm}^3 \text{ mol}^{-1}} = -1636.75 + 12.0408 \left( \frac{T}{\text{K}} \right) - 3.27957 \times 10^{-2} \left( \frac{T}{\text{K}} \right)^2 + 3.16528 \times 10^{-5} \left( \frac{T}{\text{K}} \right)^3 \quad (19)$$

where  $265 < T/\text{K} < 320$ .

This expression can then be used in equation (14) to calculate the fugacity of pure CO<sub>2</sub> provided that the pressure and temperature of the CO<sub>2</sub> are known.

### 4.2 Virial coefficient of carbon dioxide in air

In addition, Weiss used the Lennard–Jones (6–12) potential to estimate  $u(r)$  and hence calculate values for  $\delta_{\text{BC}}$  for the binary mixture: CO<sub>2</sub>–air. He found that the temperature dependence of this parameter is represented by the equation

$$\frac{\delta(\text{CO}_2 - \text{air})}{\text{cm}^3 \text{ mol}^{-1}} = 57.7 - 0.118 \left( \frac{T}{\text{K}} \right) \quad (20)$$

where  $273 < T/\text{K} < 313$ .

This expression can then be used in equation (15), together with equation (19), to calculate the fugacity of CO<sub>2</sub> in air.

### 4.3 Example calculations

#### 4.3.1 Fugacity of pure CO<sub>2</sub>

$$T = 298.15 \text{ K},$$

$$p = 101.325 \text{ kPa (1 atm)}.$$

Then,

$$B(T) = -123.2 \text{ cm}^3 \text{ mol}^{-1},$$

$$f(\text{CO}_2) = 101325 \exp\left(\frac{-123.2 \times 10^{-6} \times 101325}{8.31447 \times 298.15}\right)$$

$$= 100.816 \text{ kPa}$$

or

$$f(\text{CO}_2) = 100.816 / 101.325 = 0.99498 \text{ atm}.$$

### 4.3.2 Fugacity of CO<sub>2</sub> in air

$$T = 298.15 \text{ K},$$

$$p = 101.325 \text{ kPa (1 atm)},$$

$$x(\text{CO}_2) = 350 \times 10^{-6}.$$

Then,

$$B(T) = -123.2 \text{ cm}^3 \text{ mol}^{-1},$$

$$\delta(\text{CO}_2\text{-air}) = 22.5 \text{ cm}^3 \text{ mol}^{-1},$$

$$f(\text{CO}_2) = (350 \times 10^{-6})(101325)$$

$$\times \exp \left\{ \frac{\left[ -123.2 \times 10^{-6} + 2(1 - 350 \times 10^{-6})^2 (22.5 \times 10^{-6}) \right] \times 101325}{8.31447 \times 298.15} \right\}$$

$$= 35.35 \text{ Pa (348.9} \times 10^{-6} \text{ atm)}.$$

## 5. Bibliography

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