

# **Measurement of Three Critical Parameters As A Basis for A Simple Thermal Barrier Coating Life Prediction Methodology**

*University of Connecticut*



**Eric Jordan and Maurice Gell**

**SCIES Project 02- 01- SR 097**

**DOE COOPERATIVE AGREEMENT DE-FC26-02NT41431**

**Tom J. George, Program Manager, DOE/NETL**

**Richard Wenglarz, Manager of Research, SCIES**

**Project Awarded (05/01/02, 36 Month Duration)**

**\$ 478,495 Total Contract Value (\$ 478,495 DOE)**

# Gas Turbine Need

- **Industrial Gas Turbine Performance & Durability Depend Strongly On Use Of Thermal Barrier Coatings**
- **Aggressive Application of TBCs Limited By Lack of NDI And Lifing Methods**



# Gas Turbine Need

## **Non-Destructive Assessment of Remaining Life Strongly Impacts Operating Cost**

- **Reduce occurrence of unplanned shut down**
- **Reduce wasteful precautionary part replacement for parts that don't need it, increasing part utilization**
- **Increase understanding of failure mechanisms leading to coating with improved durability and provide a physical basis for NDI**



# Project Objectives

**To develop and experimentally validate a method for the nondestructive prediction of remaining life of by measurement of :**

- **Initial Surface Geometry**
- **Thermally Grown Oxide (TGO) Stress**
- **TGO Thickness**



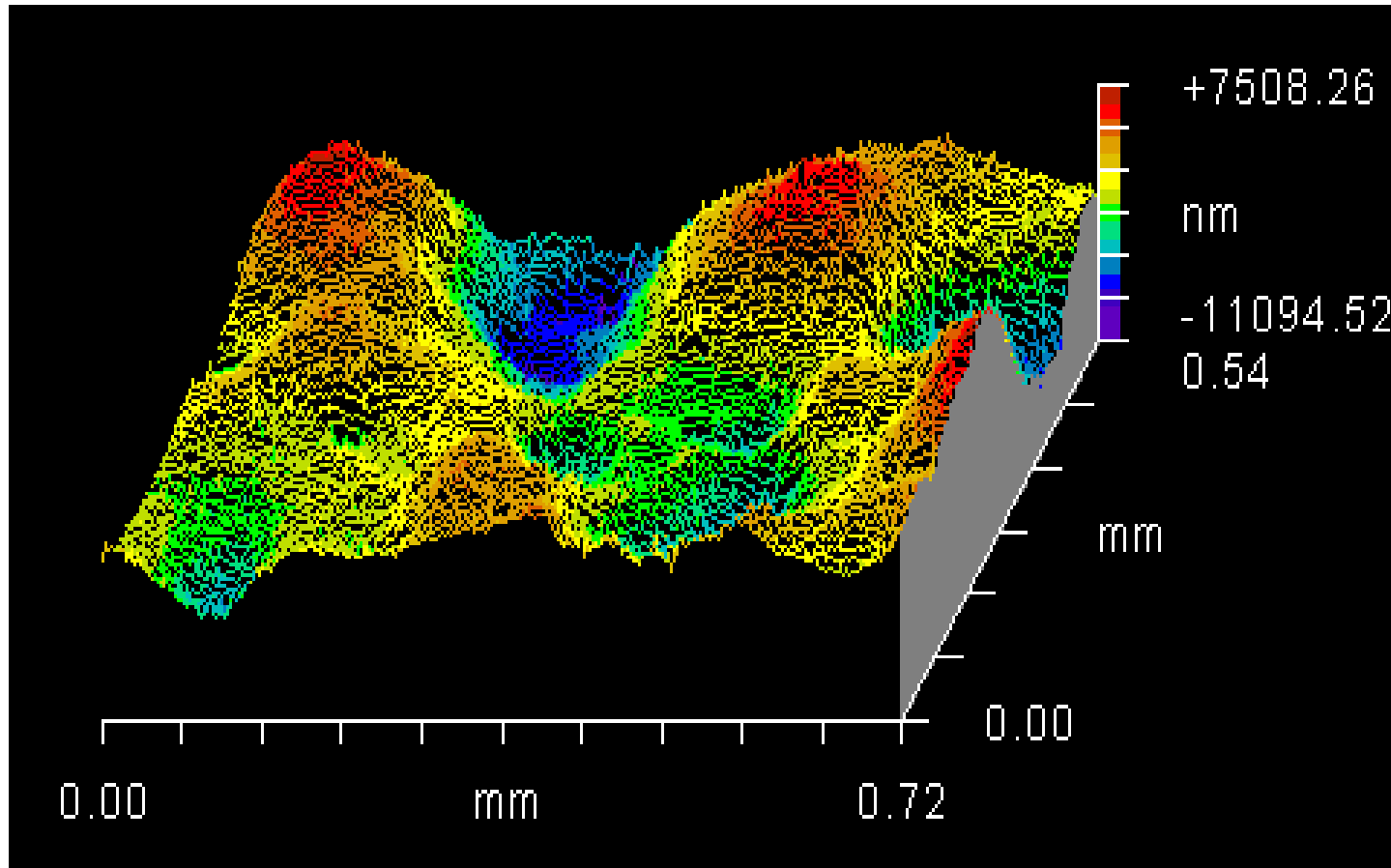
# ACOMPLISHMENTS

- **An accurate remain life NDI based on TGO Stress measurement**
  - **Showed a direct relation to damage and failure**
- **A new surface metric more related to damage than RMS etc.**
- **Transferred Technology to Industry**

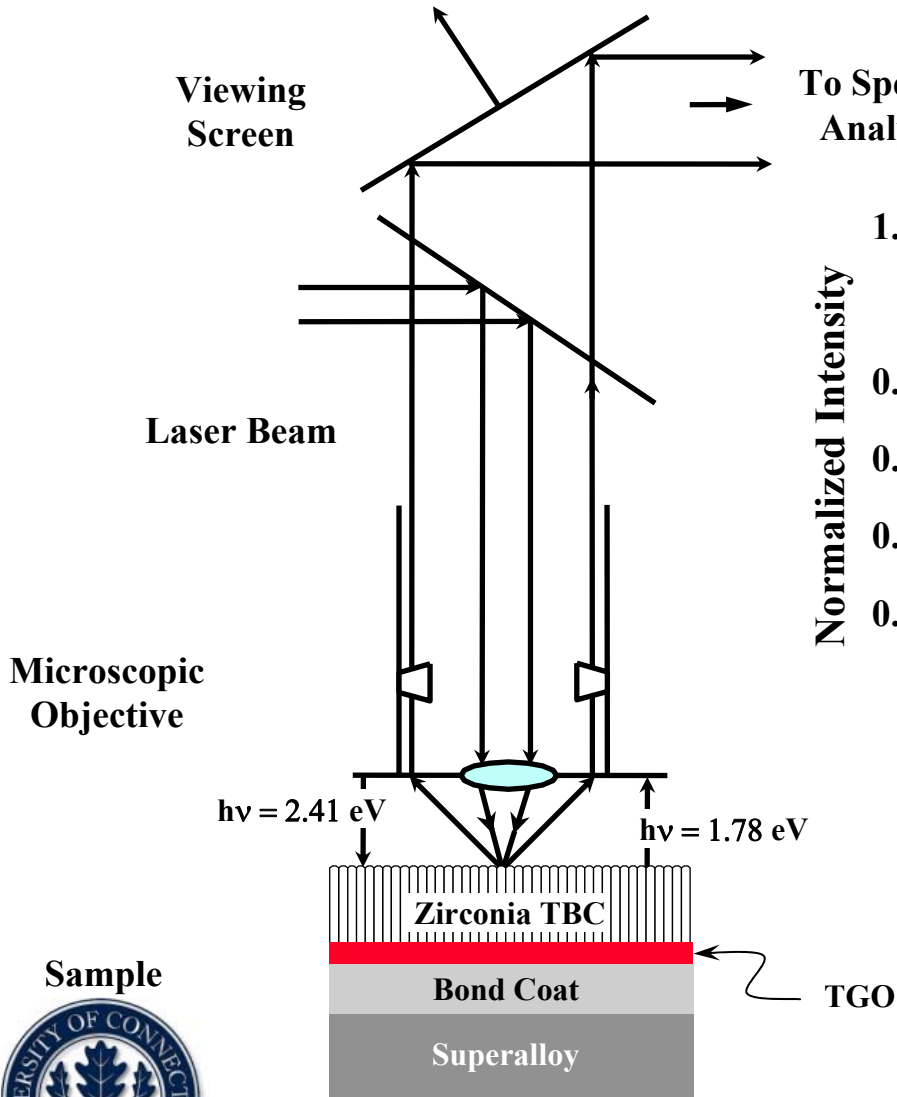
# ACOMPLISHMENTS

- **Two Ph D and two masters  $\frac{3}{4}$  female**
  - **Swetha Sridharan**
  - **Mei Wen**
  - **Jessica Shen**
  - **Manish Madhwal**

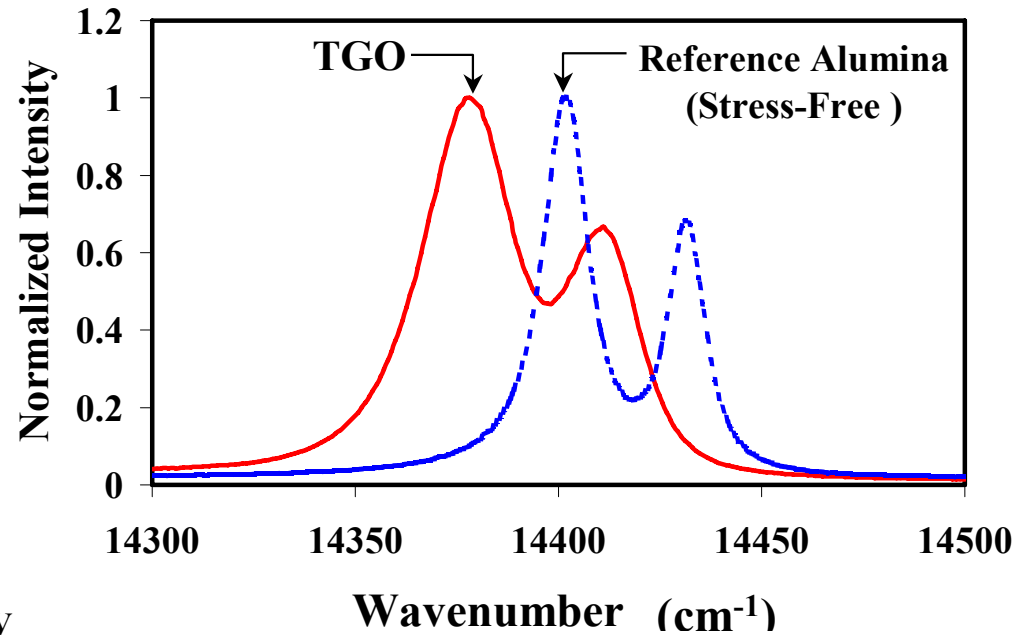
# Surface Geometry Determined by Interferometer Surface Profiler



# Photoluminescence Piezospectroscopy (PLPS) for Measuring TGO Stress



To Spectral Analyzer

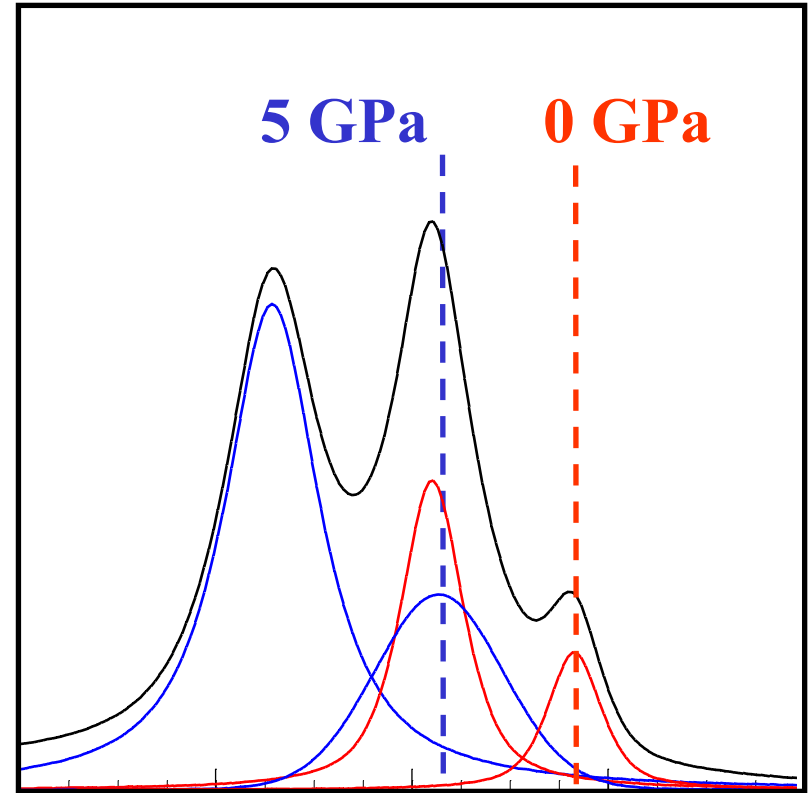
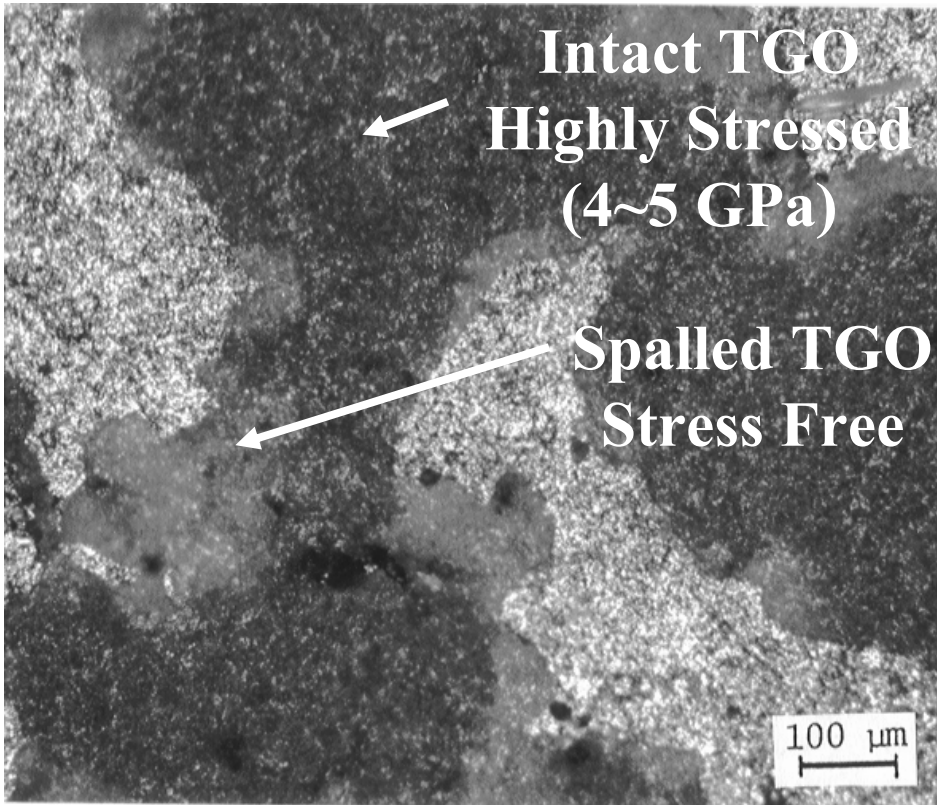


$$\overline{\Delta\nu_{\text{stress}}} = \frac{2}{3} \Pi_{ij} \sigma_o$$





# Bimodal Spectra



Top of MCrAlY Bond Coat Surface After Spallation of 7YSZ

14320 14360 14400 14440 14480

Wavenumber ( $\text{cm}^{-1}$ )



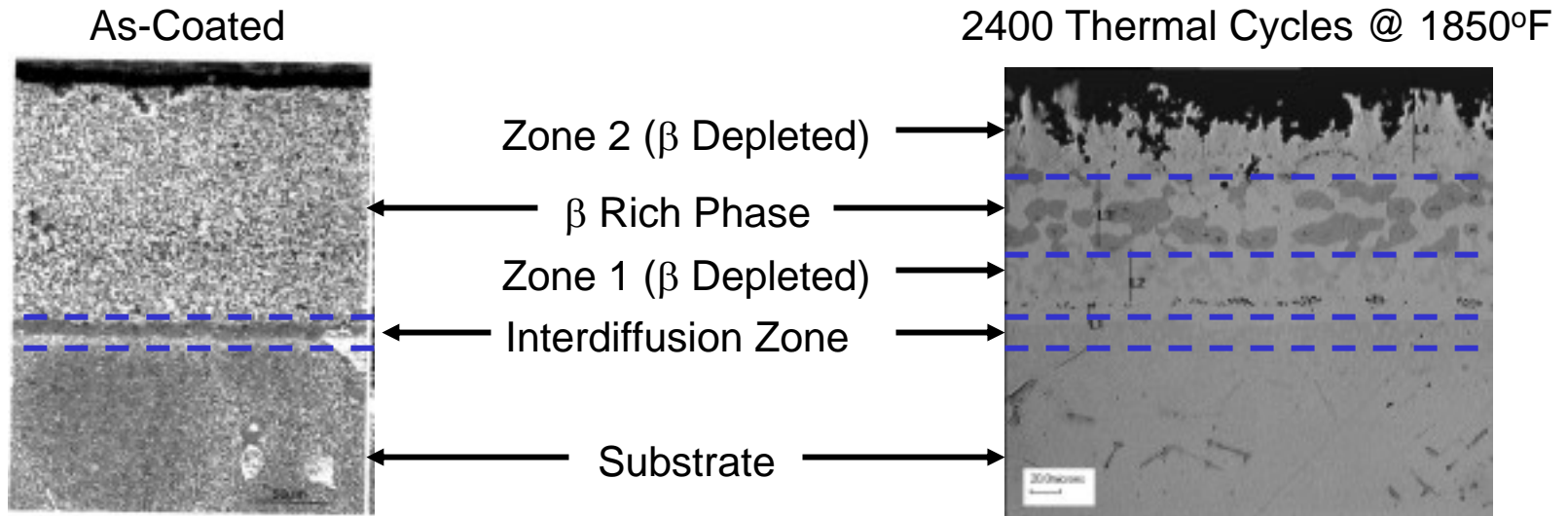
# Automated Deconvolution of PLPS Spectra

- **Solution- Optimized fit to R1-R2 peak pairs with enforced spacing**
- **Benefit- 100X reduced user effort and reduced user training level**



# TGO Thickness Measured by Advanced AC Potential Drop

- Beta depletion zone thickness determined from electrical resistivity vs. depth inferred from AC Potential Drop.
- JENTEK measurement system deemed best in Round-Robin Test



# Different Type of Specimens Used In The Program

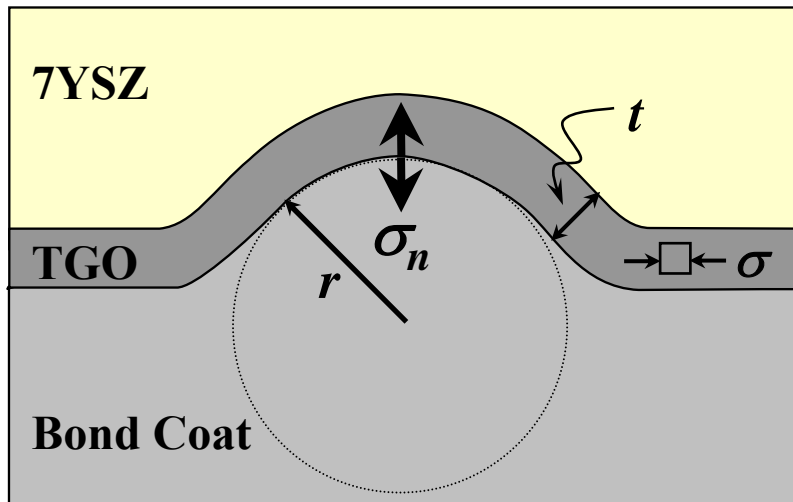
Type	Superalloy Substrate	Bond Coat		Ceramic (7YSZ)	
		Type	Thickness (μm)	Type	Thickness (μm)
I	Single Crystal CMSX-4	Ni-20Co-18Cr-12.5Al-0.6 Y-0.4 Si-0.25 Hf wt.%	100	EB-PVD	145
II	Single Crystal CMSX-4	Grit Blasted-[(Ni,Pt) Al]-Ni-21 Al-20 Pt wt.%	50	EB-PVD	140
III a,b	Single Crystal CMSX-4	Grit Blasted-[(Ni,Pt) Al]-Ni-21 Al-20 Pt wt.%	75	EB-PVD	150

# **Type I. Specimen Life Prediction**

## **Use all 3 Parameters**

# Failure Occurs at Constant Value of Out of Plane Interface Stress

$$\sigma_n = \sigma t (1/r_x + 1/r_y) = \sigma t (1/r_{mean})$$



$t =$  TGO thickness

$r_y, r_x =$  Principal radii of curvature

$\sigma_n =$  Normal tensile stress at asperity

$\sigma_y, \sigma_x =$  in-plane compressive stress

If  $\sigma_y = \sigma_x = \sigma$

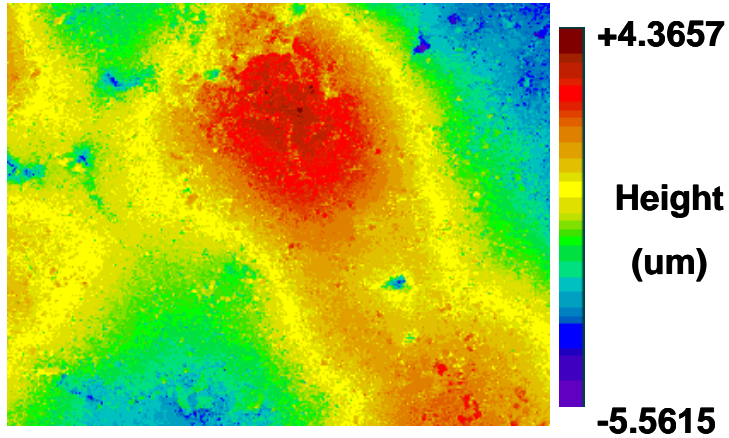


# Development of Geometry Feature Extraction Software

- **Smooth the Raw Data by Filtering**
- **Cubic Splines Are Used to Fit the Data**
- **Compute Mean Curvature from Derivatives**

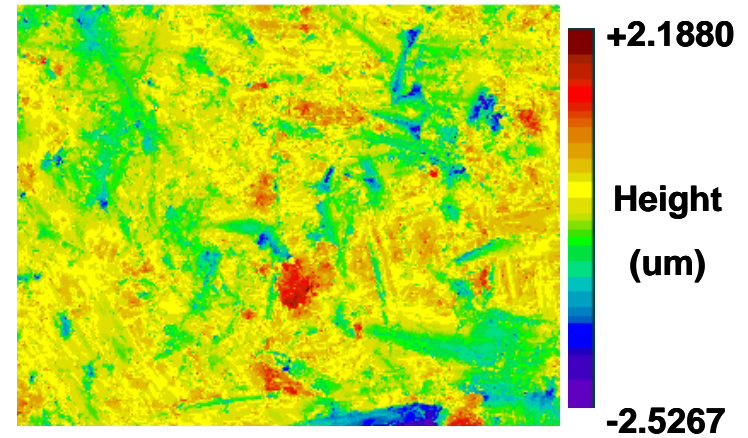


# Curvature Map Superior to RMS in Characterizing Surface Geometry



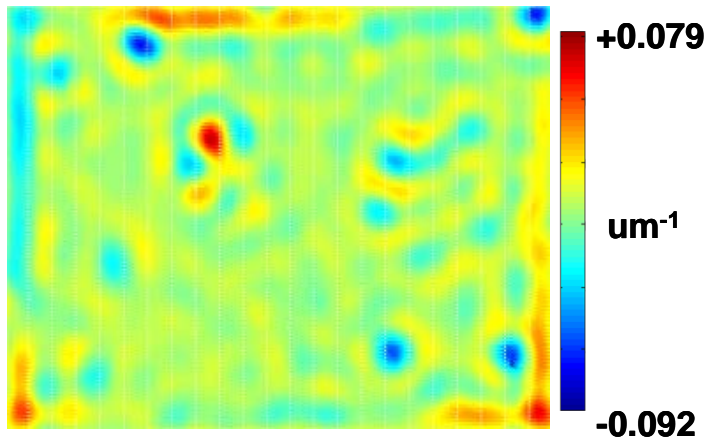
Surface of As-received

RMS=1.456  $\mu\text{m}$

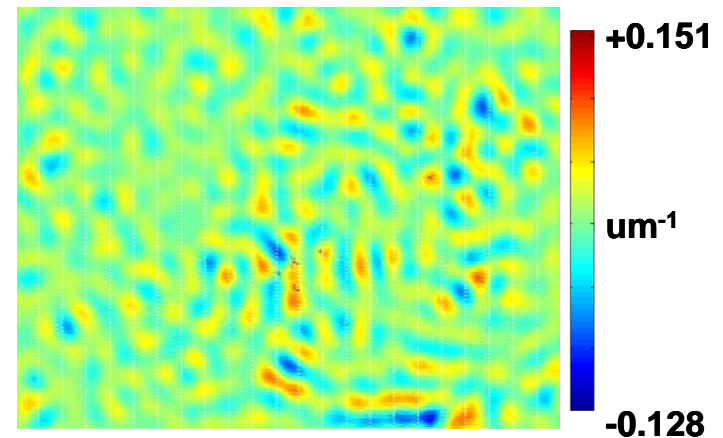


Surface of Barrel Finish

RMS=0.452  $\mu\text{m}$



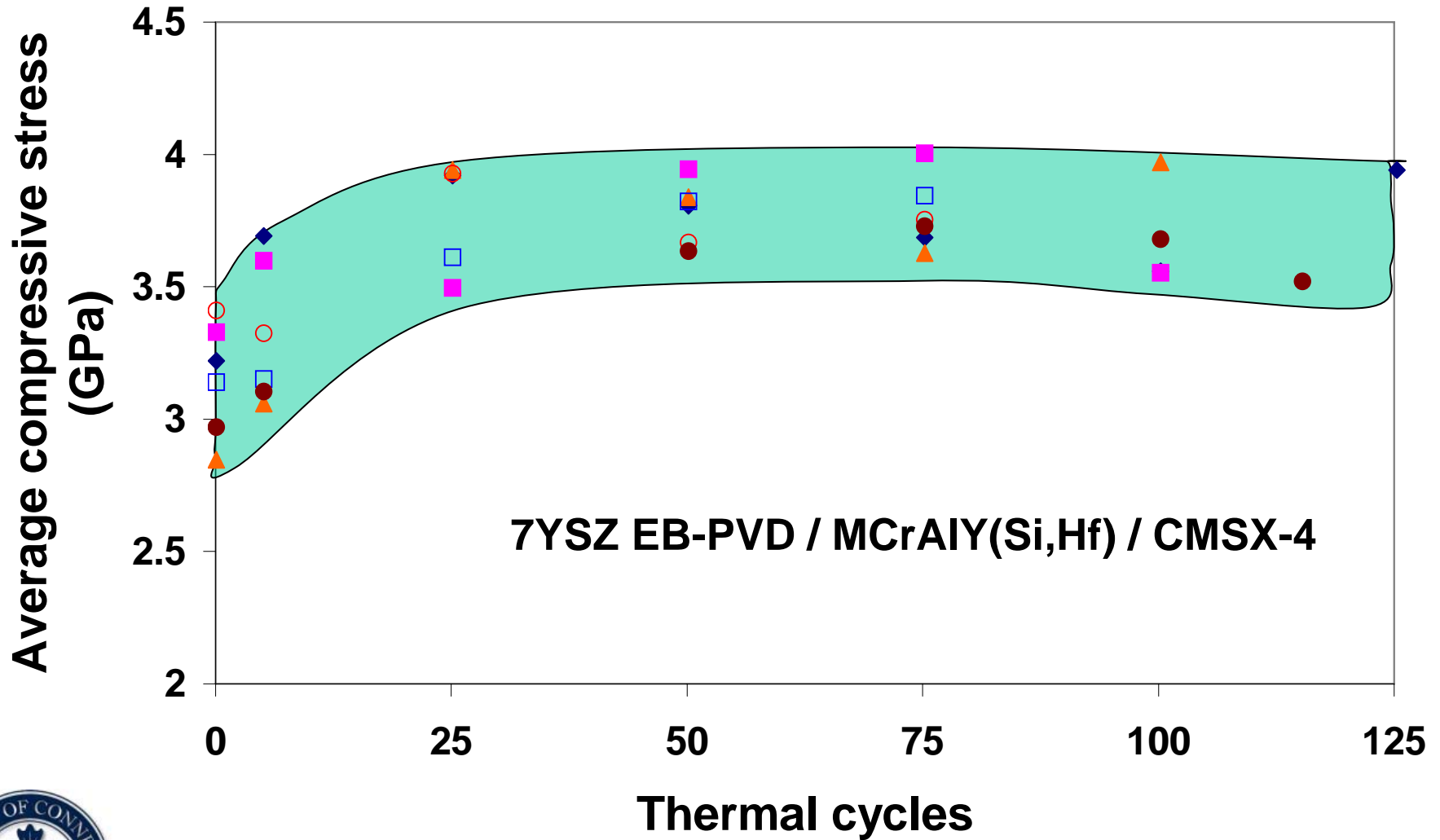
Curvature of As-received Surface



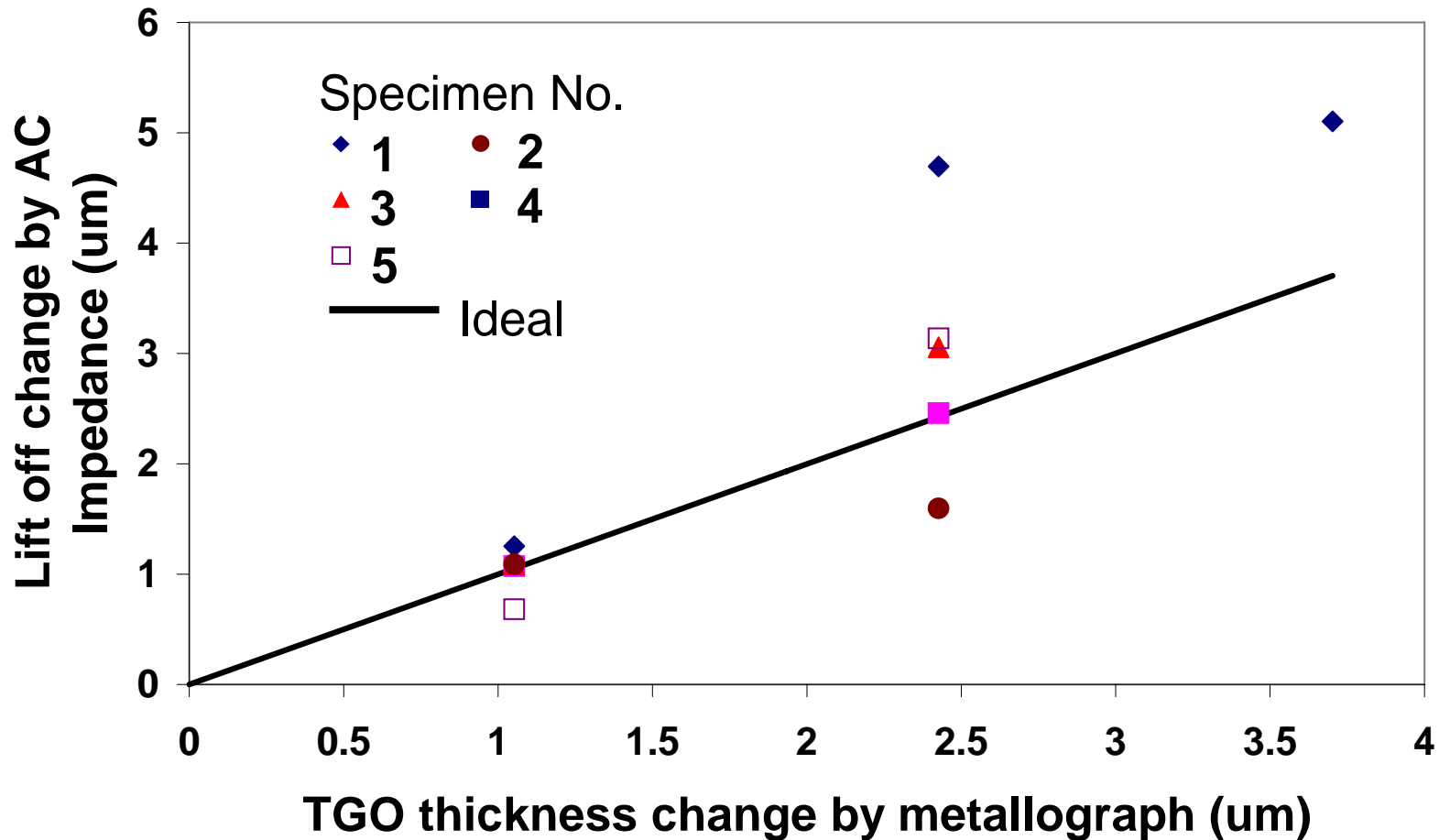
Curvature of Barrel Finish Surface



# Evolution of TGO Stress throughout Thermal Cycling



# TGO Thickness Measured by AC Impedance Method



Oxide growth rate  $h = 0.3859 t^{1/2} + 0.742$

# Life Prediction Methodology

**Compute  
curvature  
of surface**



**Determine  
the  
continuous  
debond  
region size  
based on  $\sigma$ ,  
 $r$ ,  $\sigma_n$**



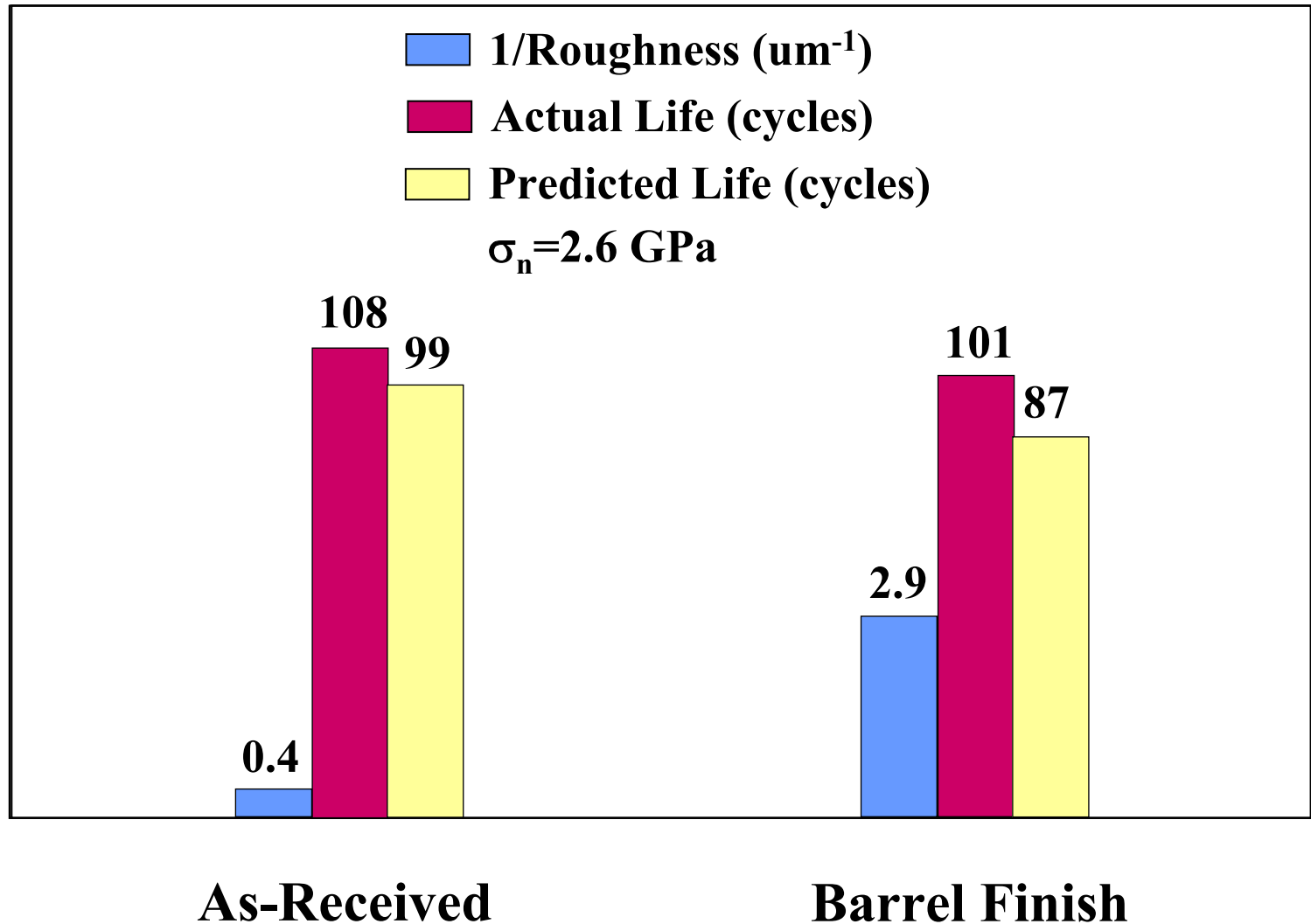
**Determine  
the minimum  
TGO  
thickness to  
spallation  
from fracture  
mechanics**



**Predict life  
based on  
TGO growth  
rate**



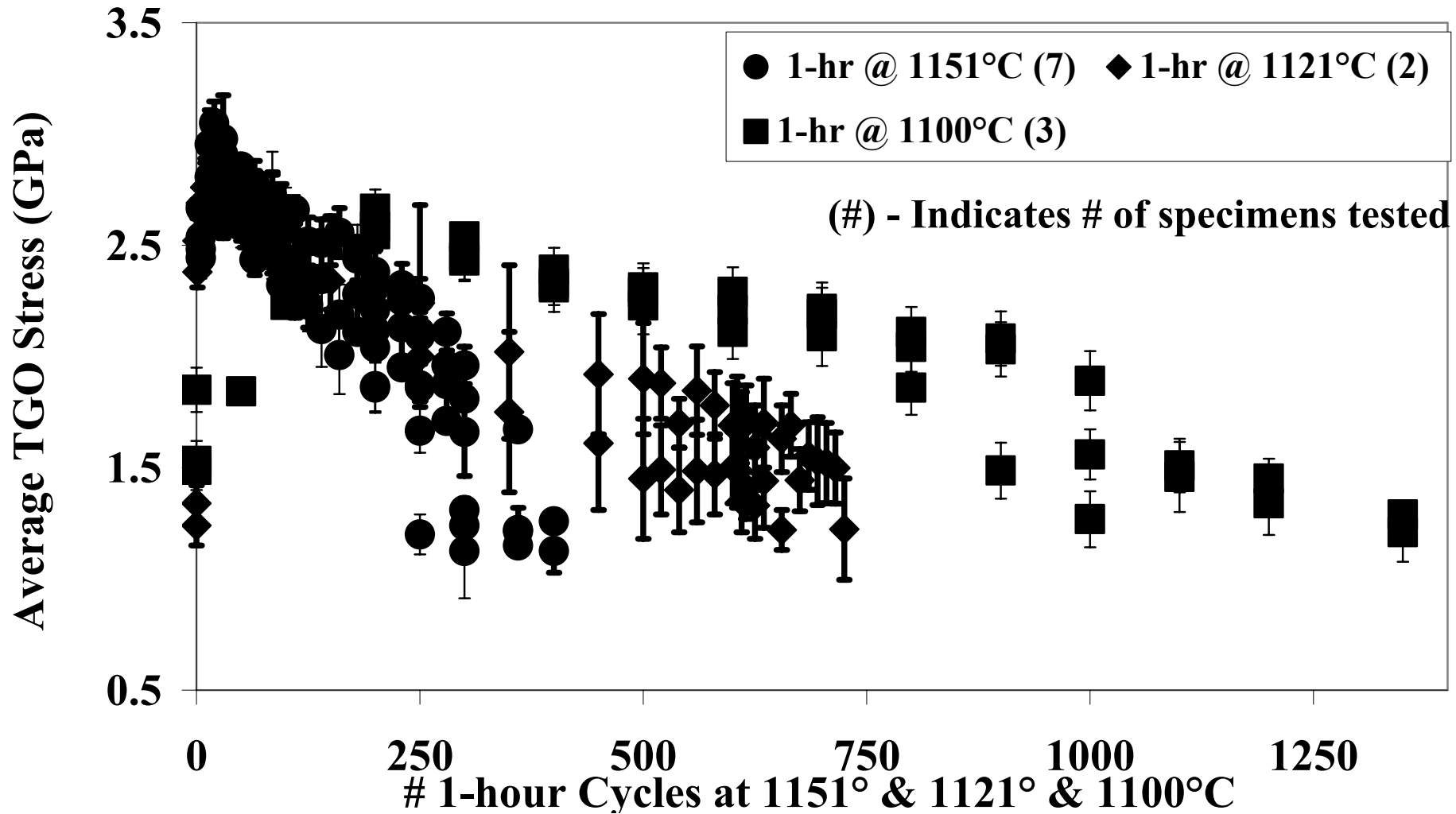
# Summary of Surface Roughness, Real Life and Predicted Life



**Type II & III a,b Specimen Use  
TGO Stress Only**

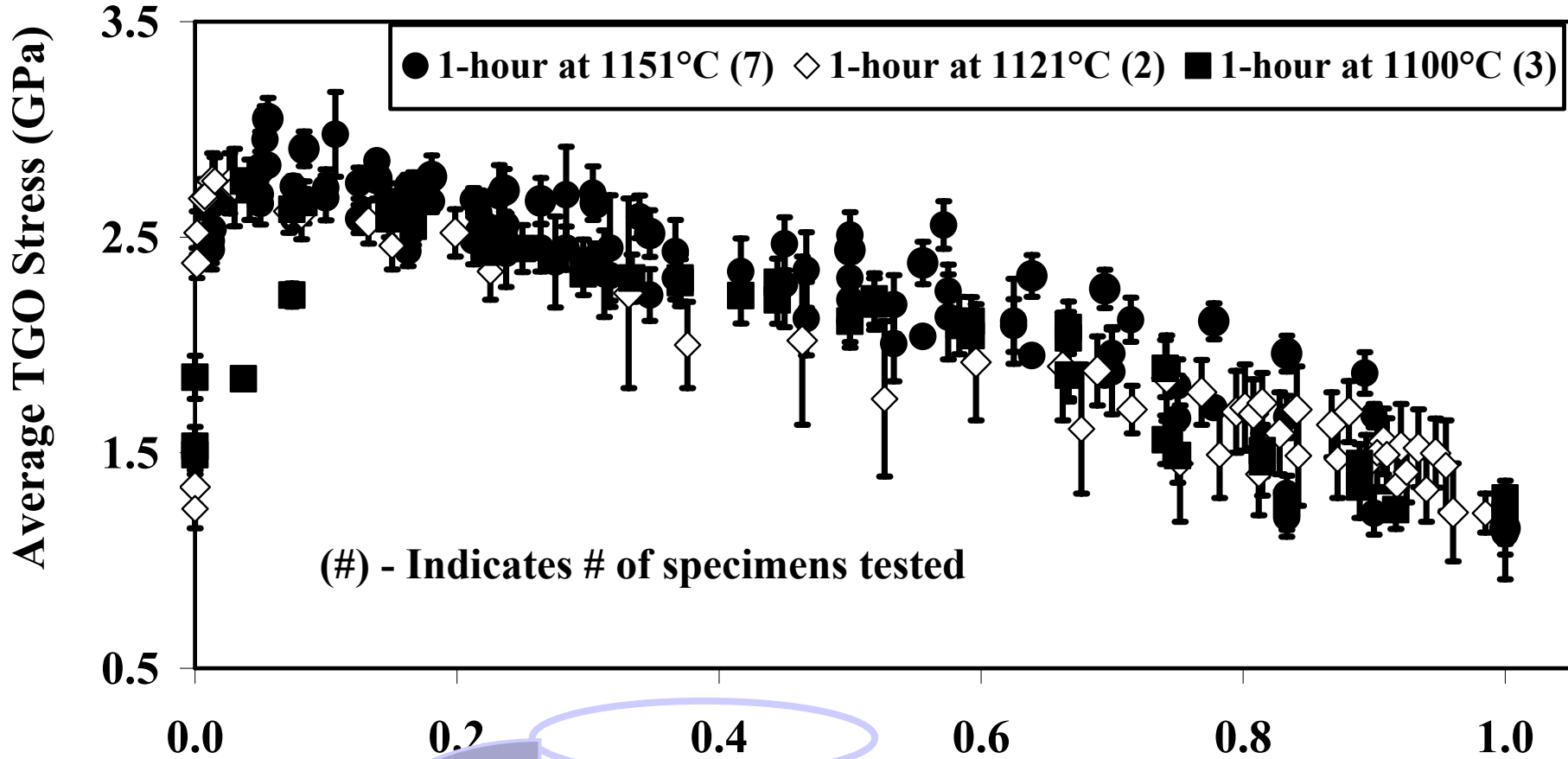
# Type I TBC – TGO Stress Versus Cycles

## 1-hour Tests



# Type I TBC – TGO Stress Versus Cyclic Life Fraction

## 1-hour Tests

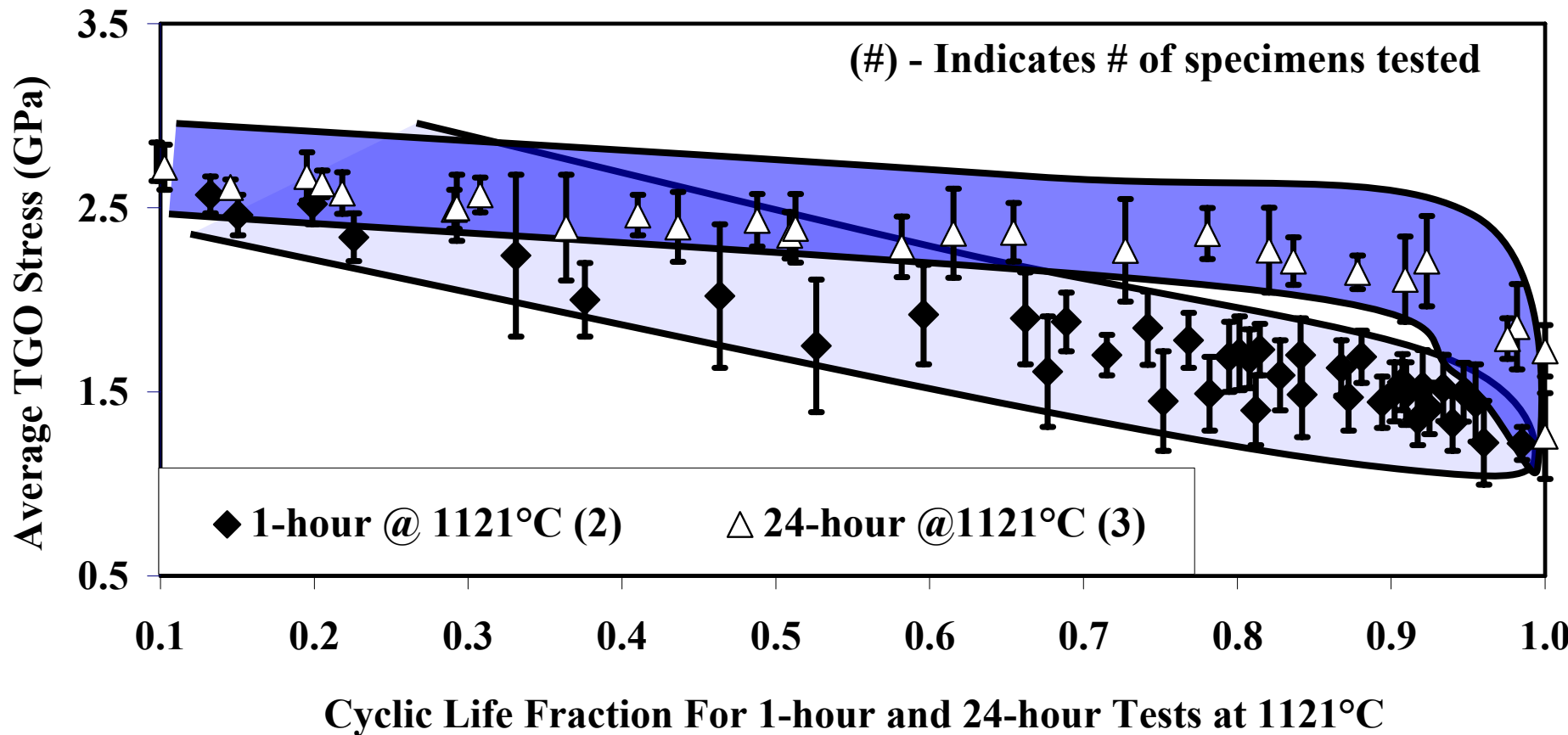


Cyclic Life Fraction During 1-hour Cycles at 1151° & 1121° & 1100°C

# of Cycles / # of Cycles To Failure

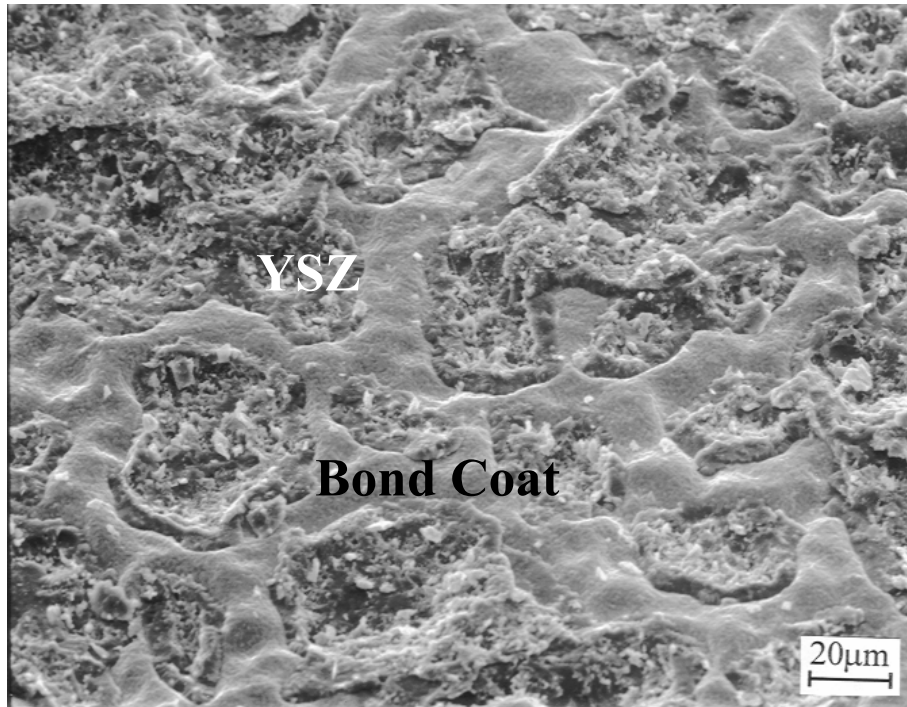
# Type I TBC – TGO Stress Versus Cyclic Life Fraction

## 24-hour Tests



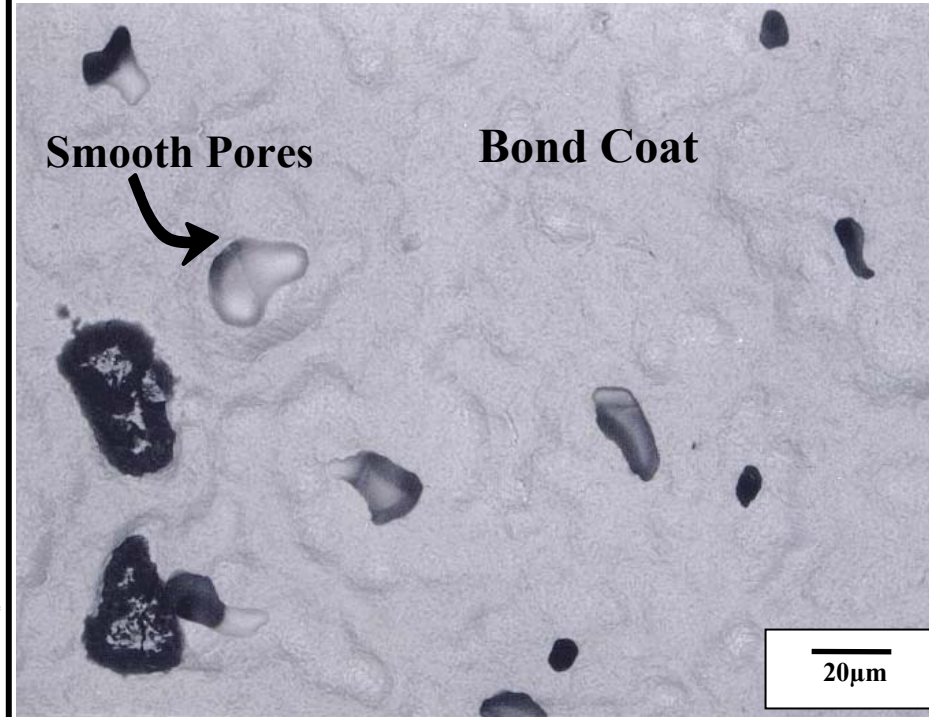


# *RESULTS -1-hour Versus 24-hour Tests*



**1-hour Tests: Failure**

**Predominantly In The  
YSZ At or Near the  
TBC/TGO Interface**



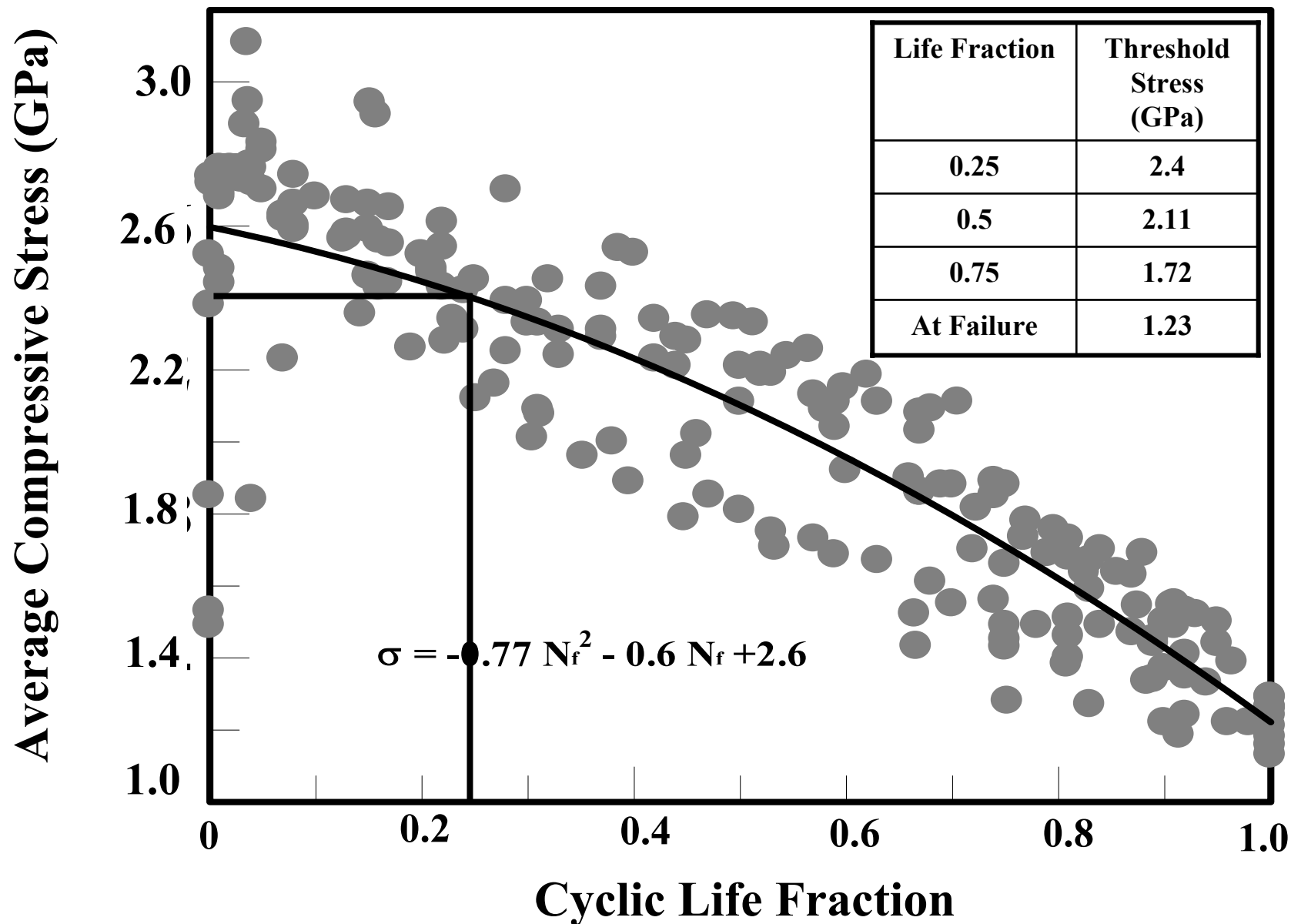
**Failed after 33 24-hour  
Cycles @ 1121°C**

**24-hour Tests: Failure**

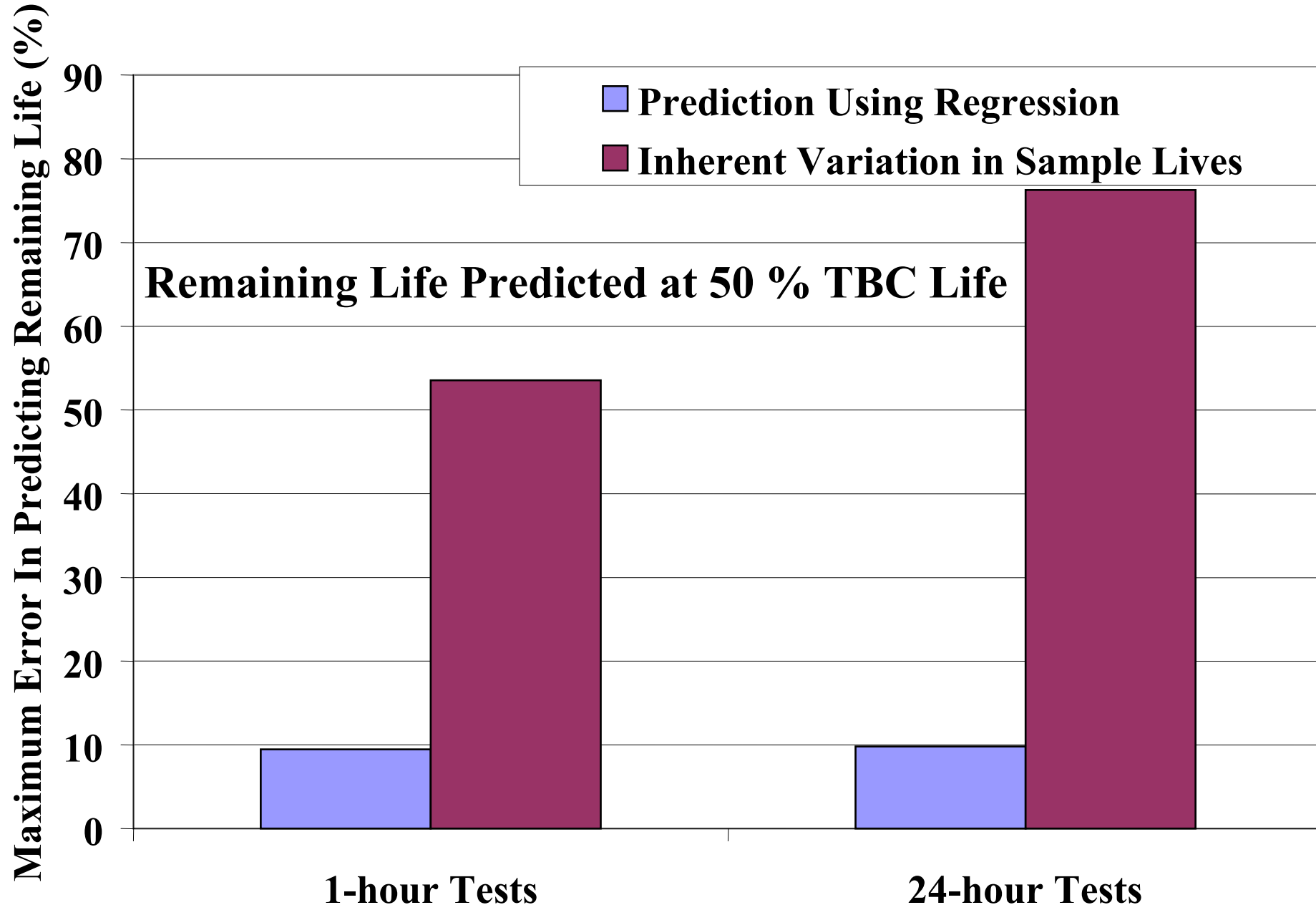
**Predominantly At  
TGO/Bond Coat Interface**

**Remaining Life Prediction  
Based on PLPS Data without  
knowledge of temperature  
I. Regression Method  
For Type III**

# Type I TBC - Quadratic Curve Fit For Multiple History Data

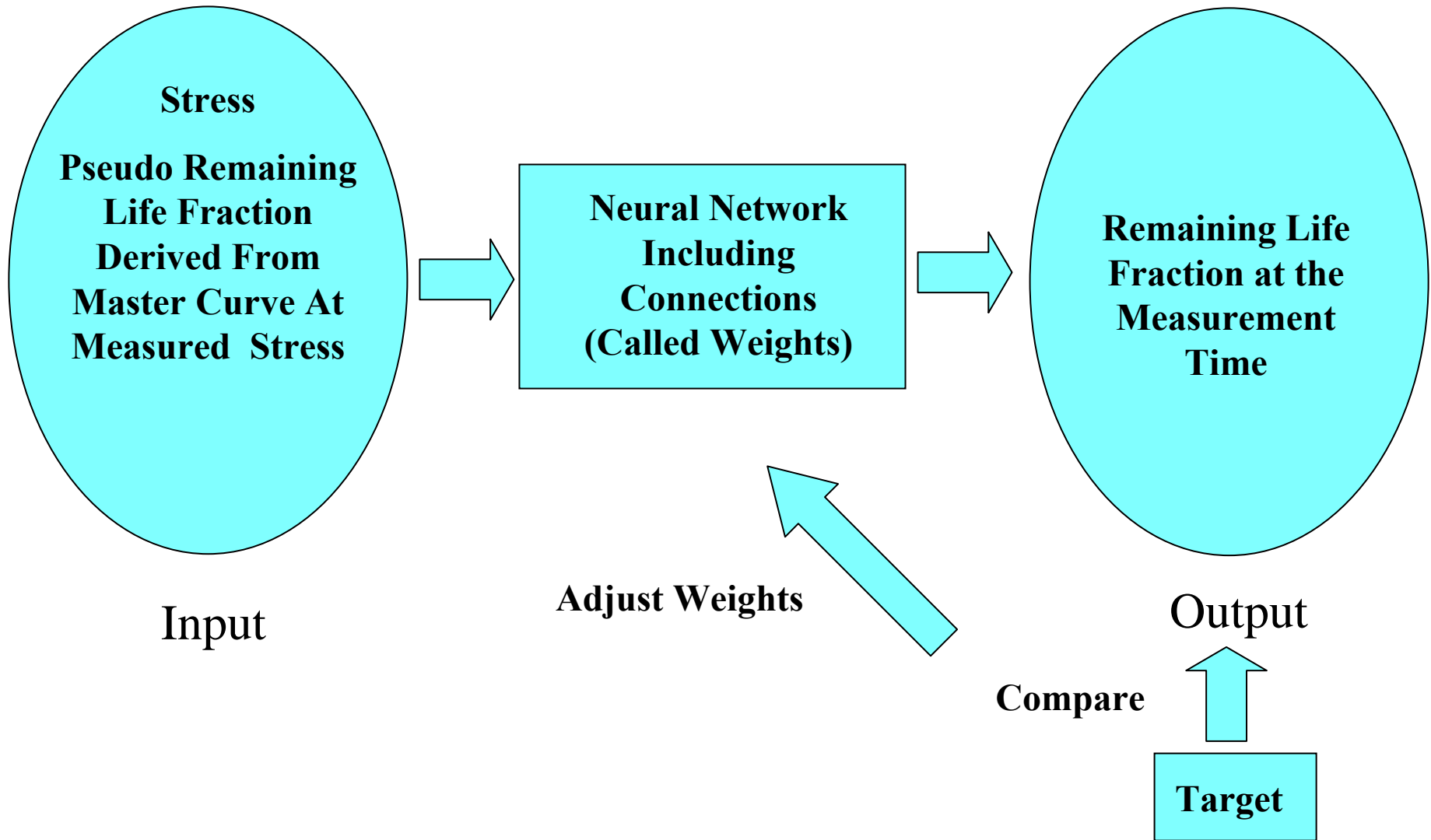


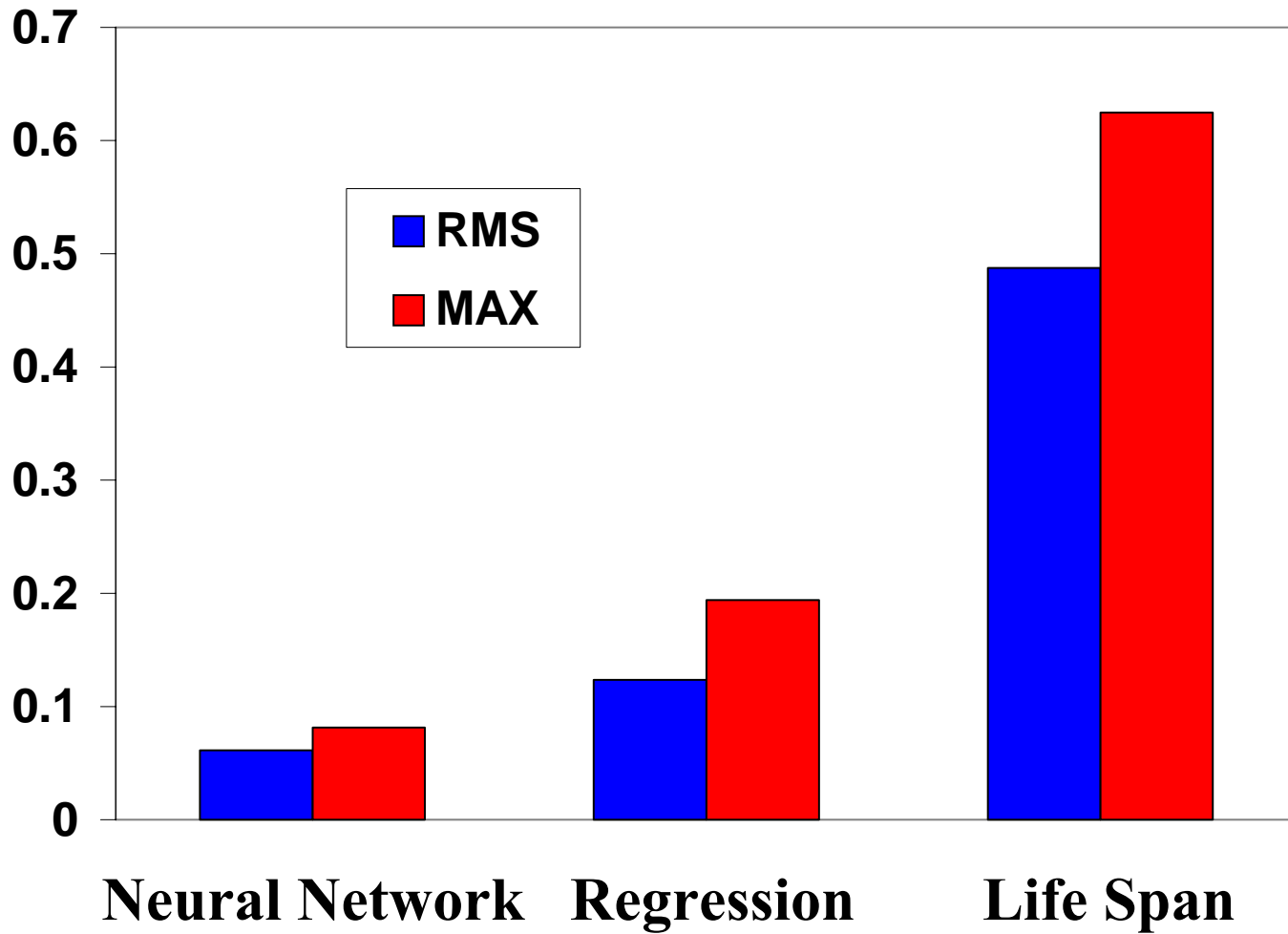
# *Remaining Life Predictions Versus TBC Life Scatter*



**Remaining Life Prediction  
Based on PLPS Data without  
knowledge of temperature  
II. Neural Network Method  
For Type II**

# Method II. Stress with Master Curve





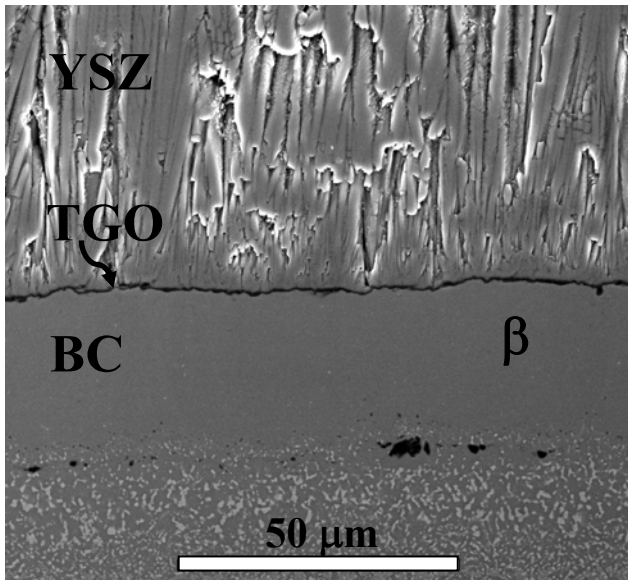
# Type III Had Bimodal

- **Bimodal can be mapped and used as a indication that failure is near**

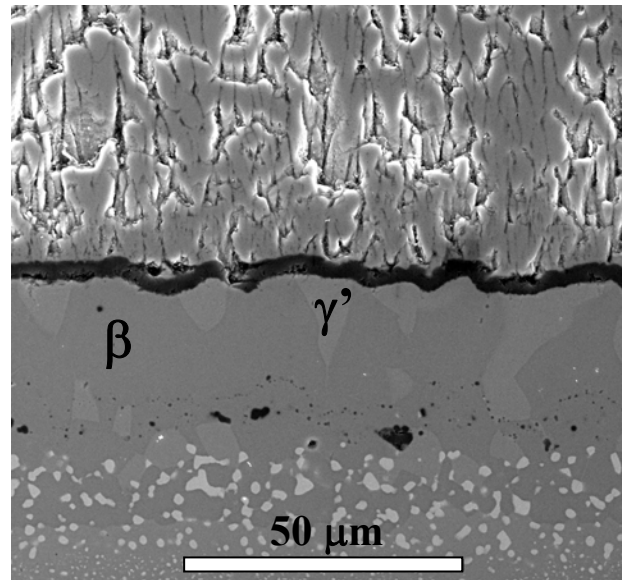


**Claim: Rumpling Primary  
Causes of Stress Drop**

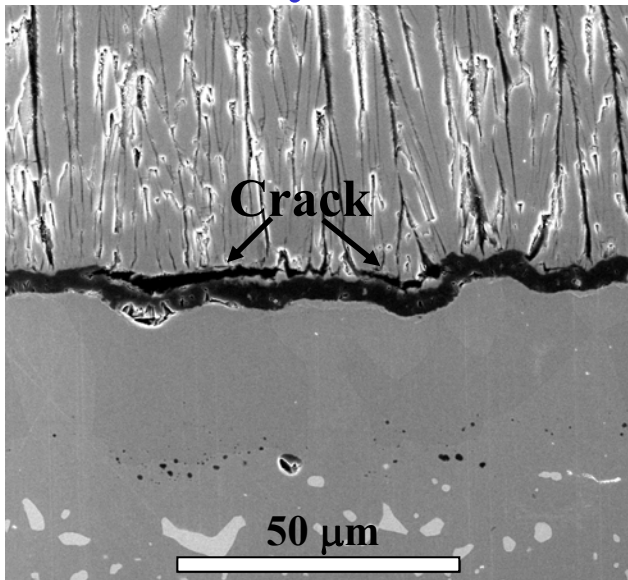
# Microstructural Evolution



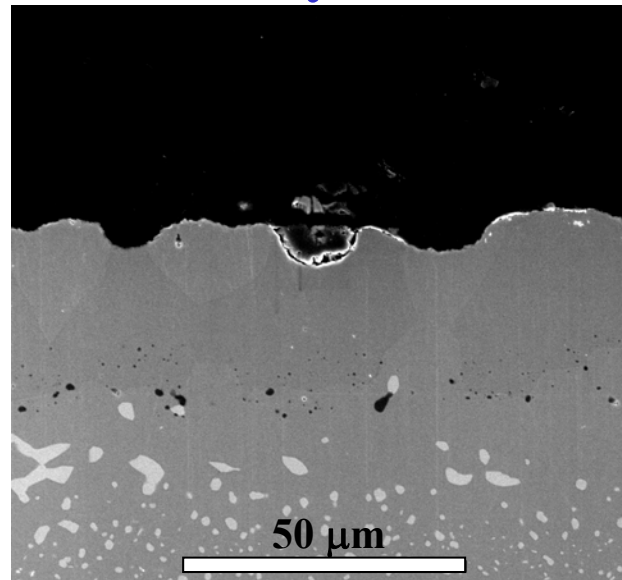
0 cycles



60 cycles



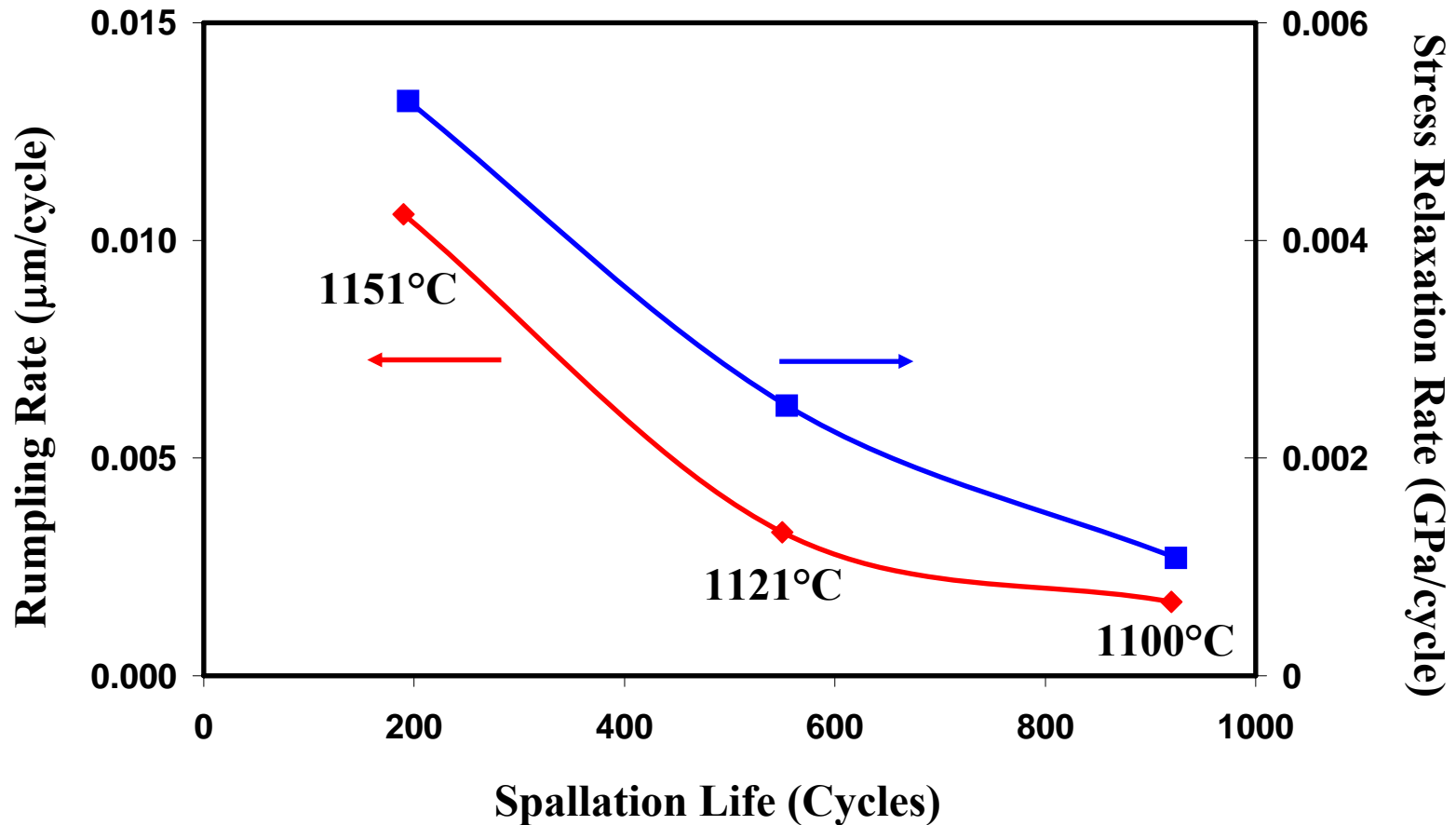
125 cycles



190 cycles

- Interface Rumpling
- TGO Thickening
- $\beta$ -(Ni,Pt)Al  $\rightarrow$   $\gamma'$ -Ni<sub>3</sub>Al
- Cracking

# Relationships Among Life, Rumpling And TGO Stress



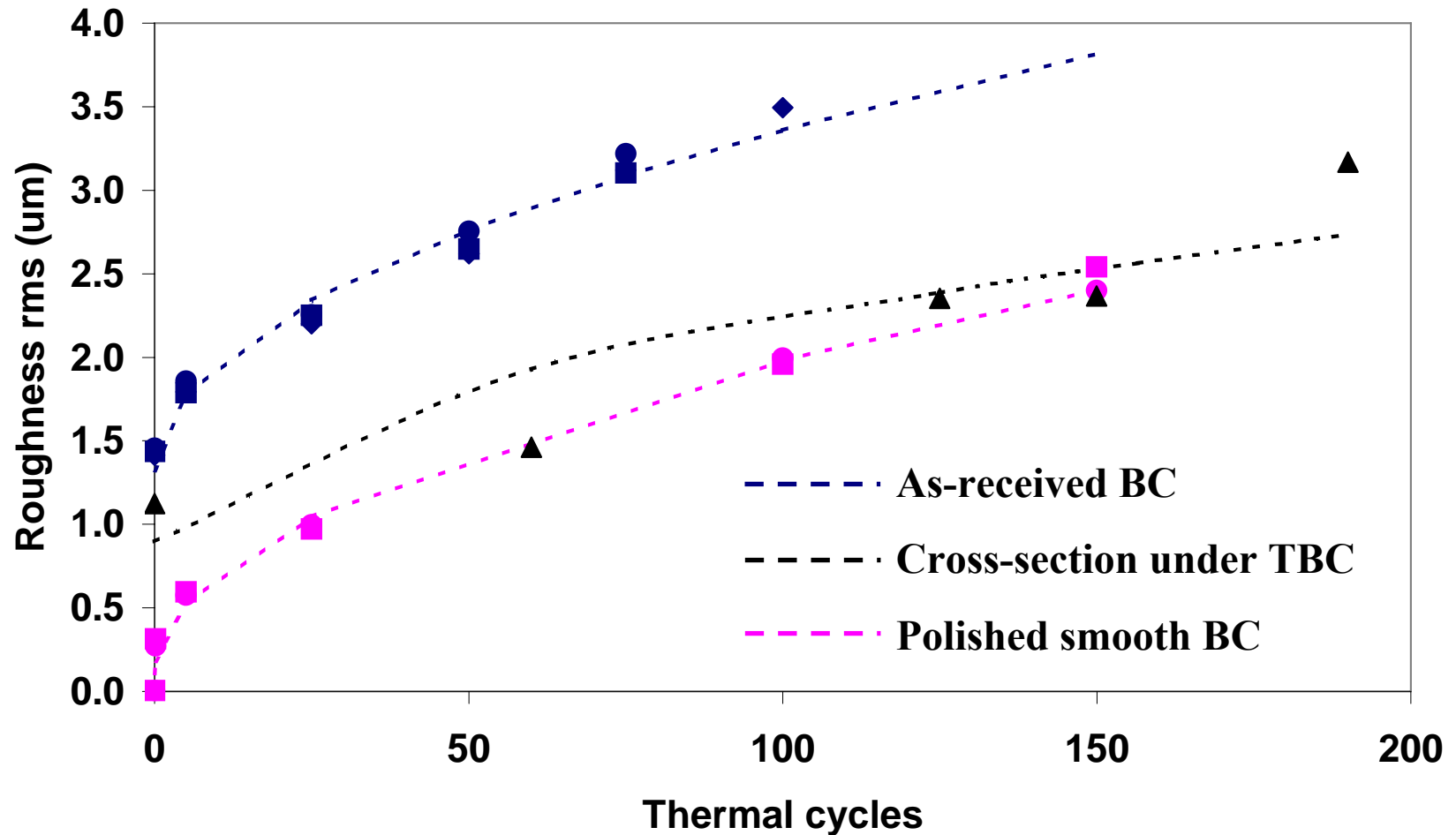
- Life Prediction Is Possible Based on TGO Stress



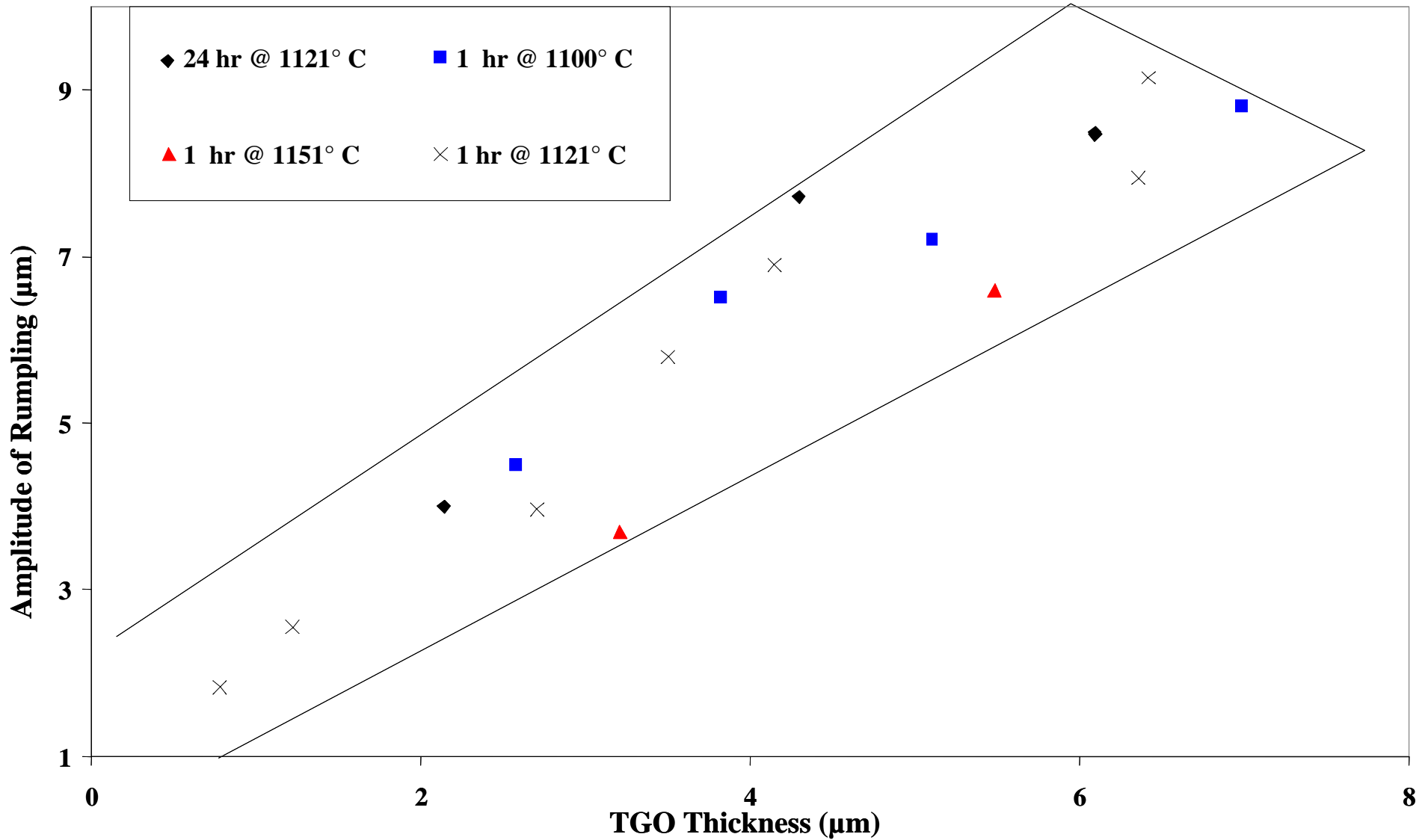
# **Stress Based NDI has Physical Basis**

- **Rumpling Causes Stress Drop**
- **Rumpling causes failure**
- **Rumpling is important**

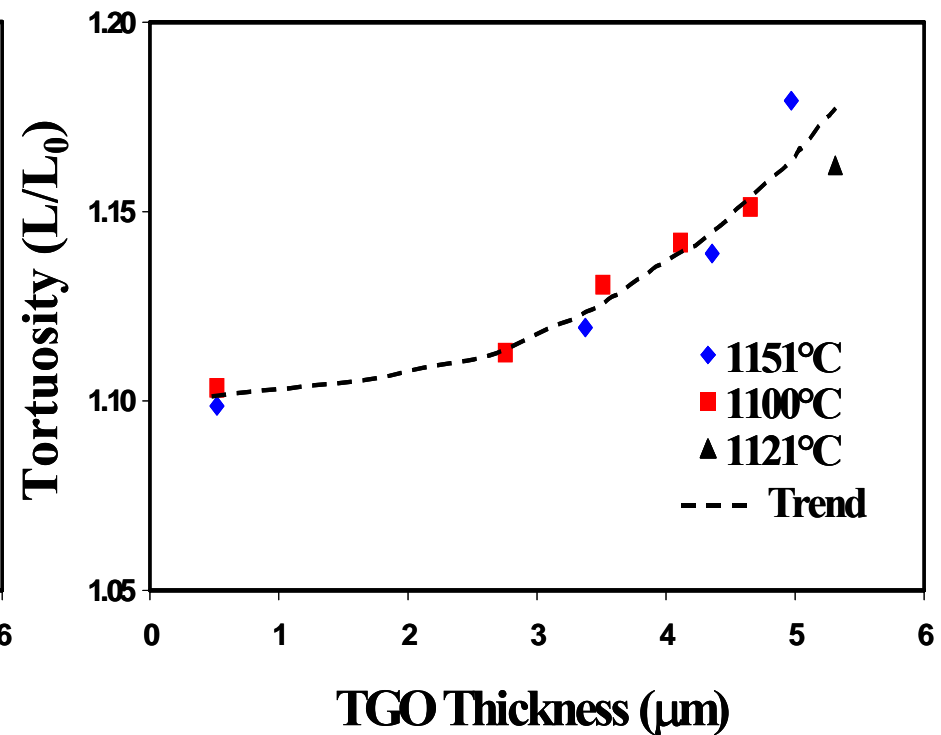
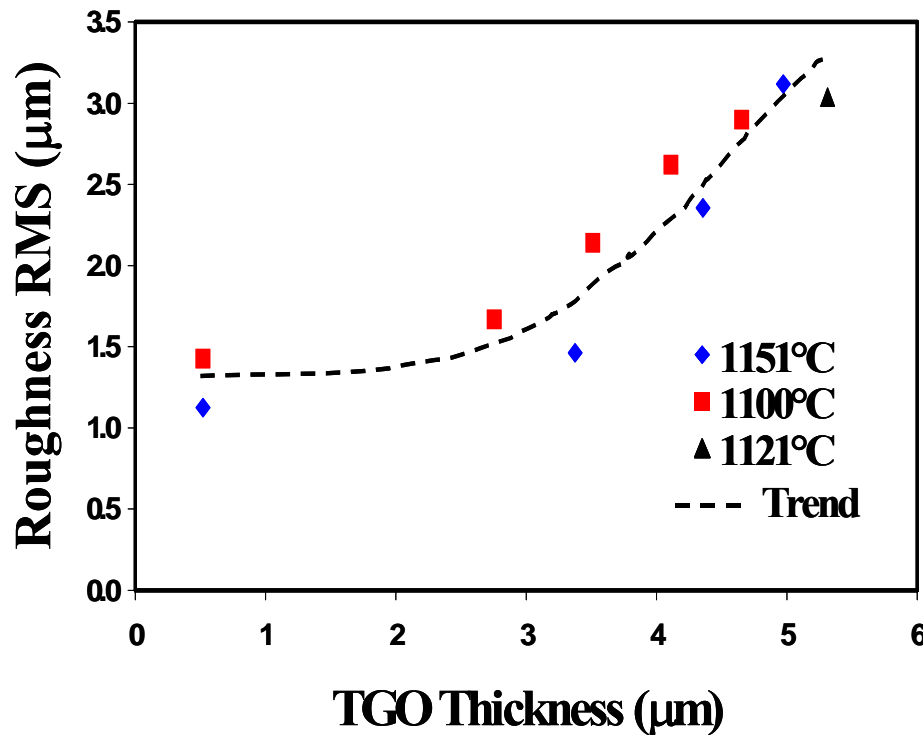
# Roughness vs. thermal cycling: Type II



# Single Valued Relation Between Rumpling Amplitudes And TGO Thickness Type II



# Rumpling Dependence On TGO Growth Type III



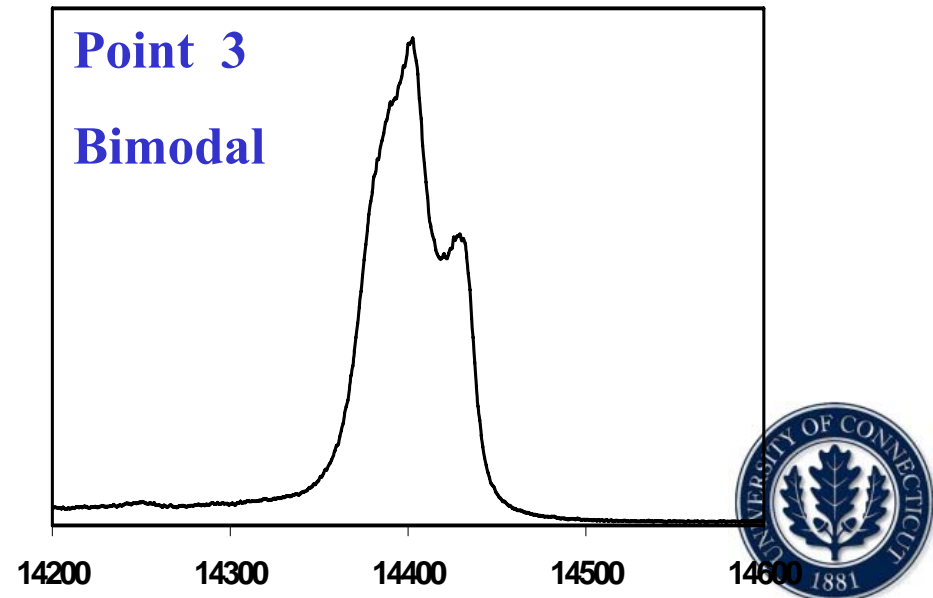
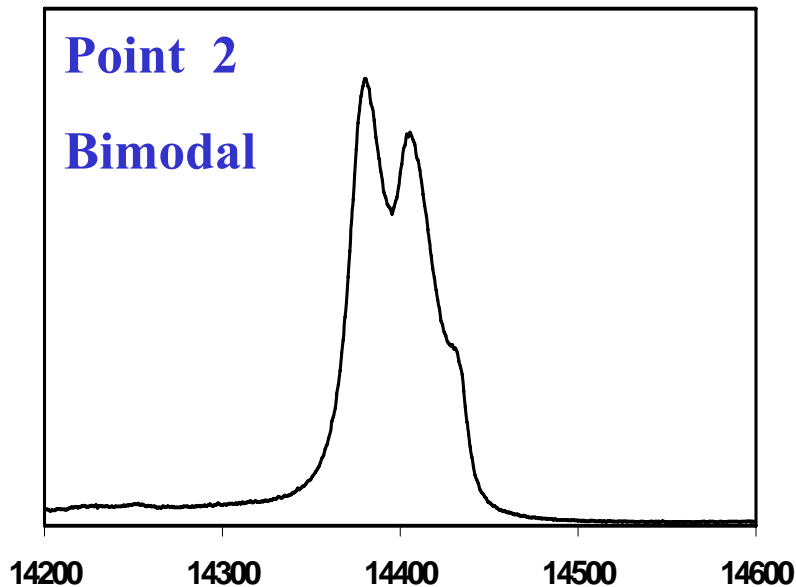
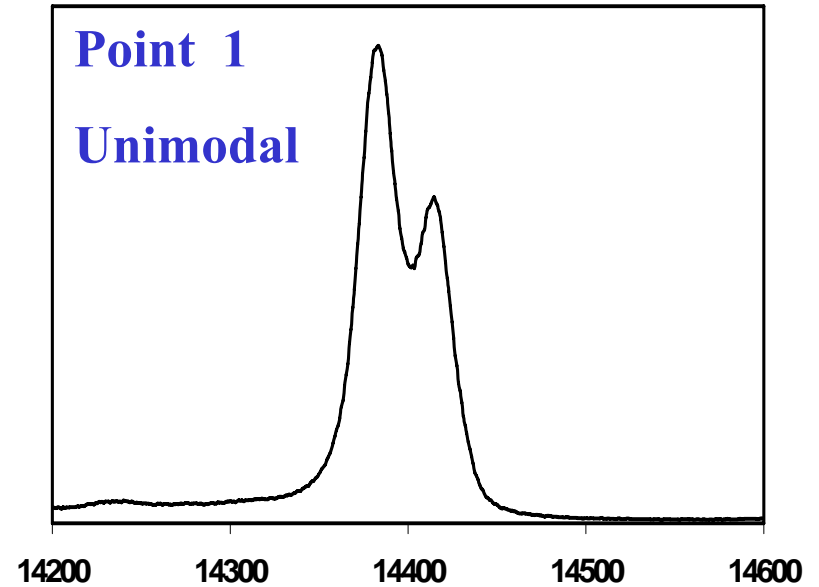
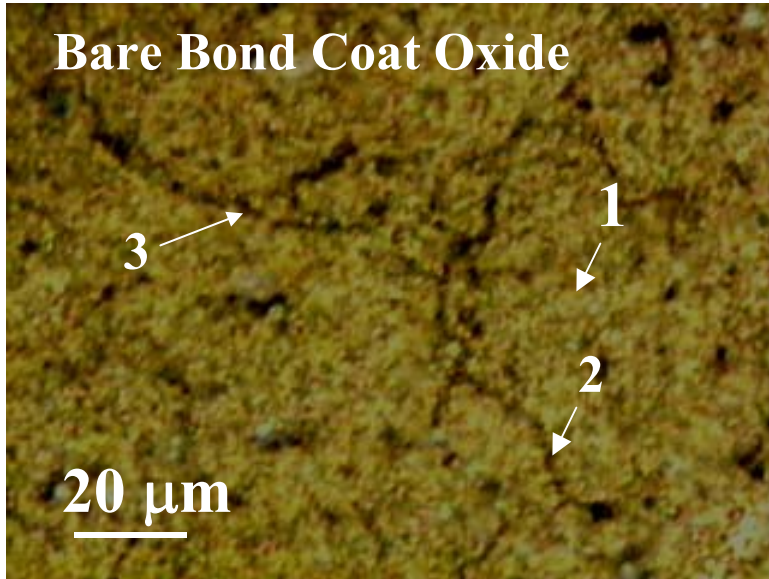
• TGO Growth Controls Rumpling



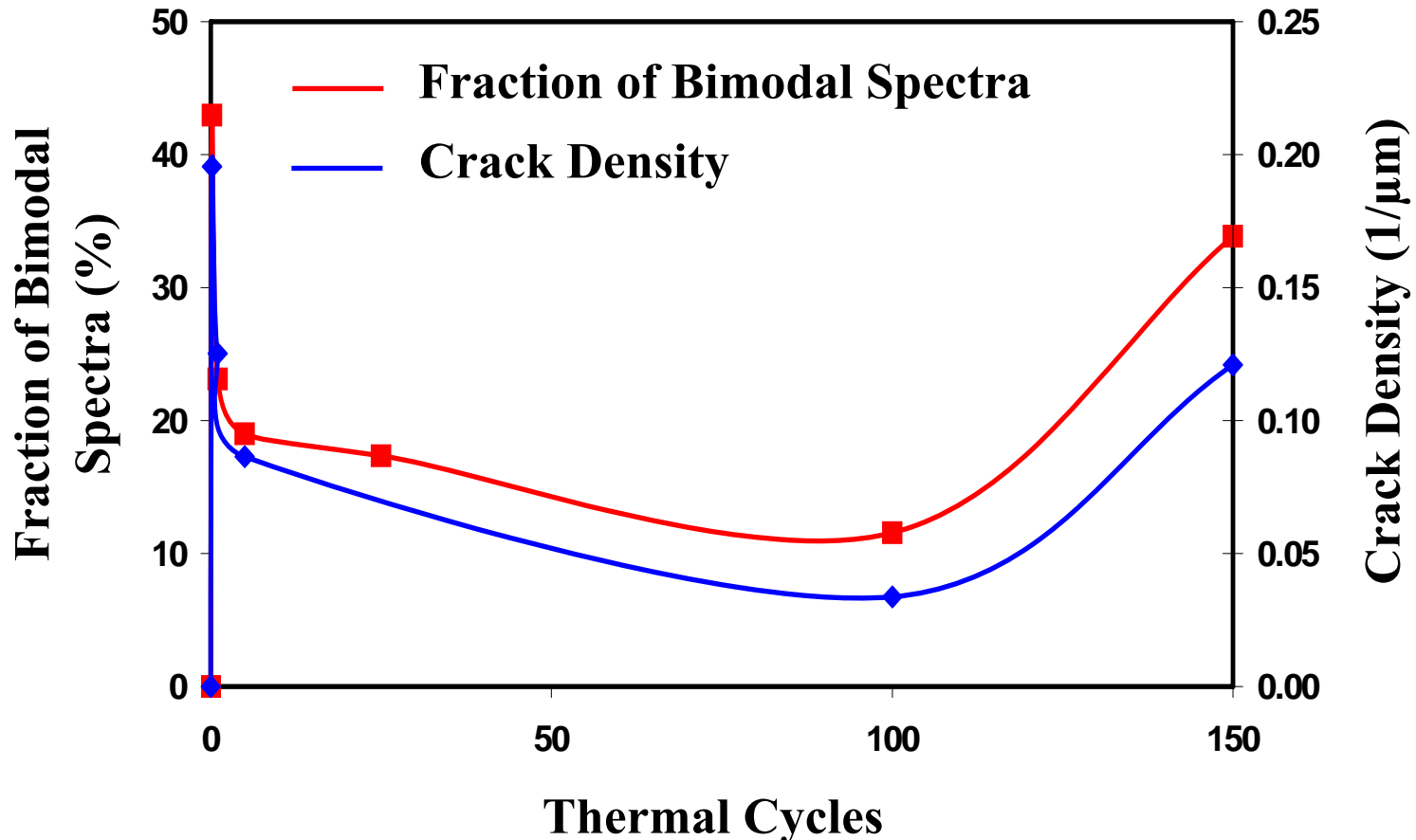
**We have Proved Bimodal  
Spectra Come from Cracking**



# Bimodal Luminescence Related To TGO Cracking



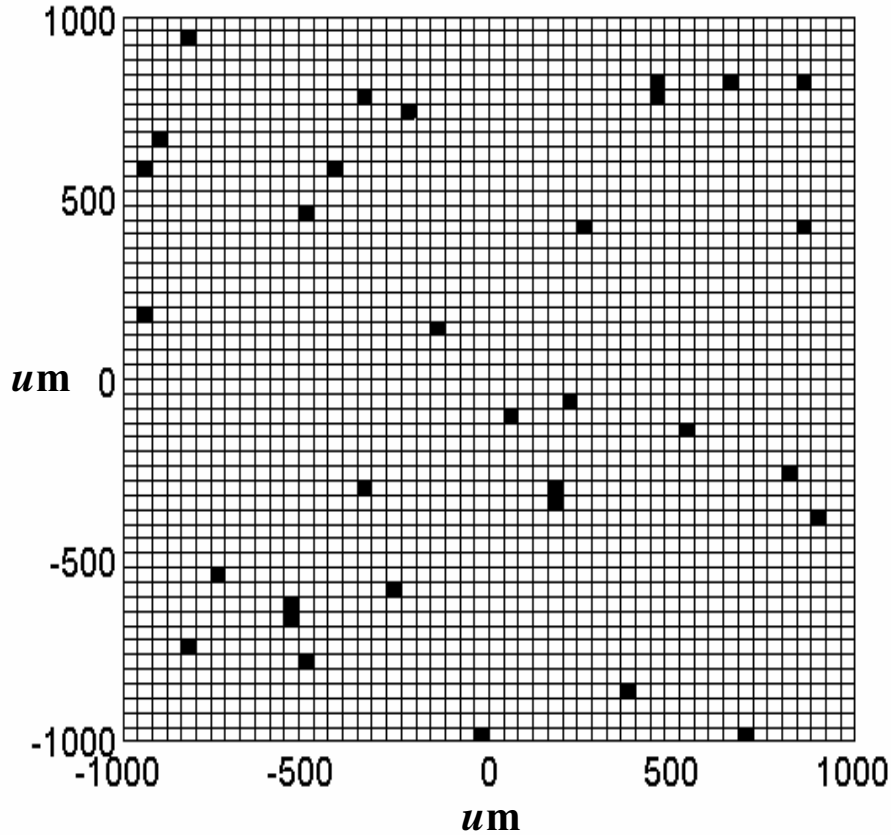
# Fraction of Bimodal Spectra and Crack Density



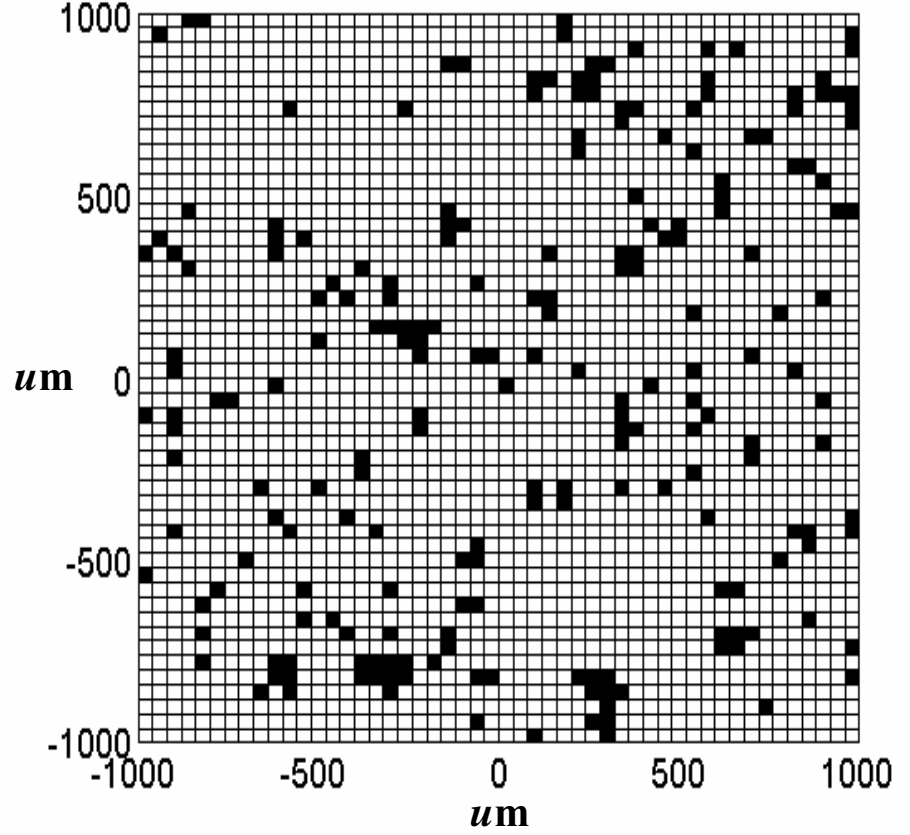
- Fraction of Bimodal Spectra and Crack Density Change in a Similar Manner with Thermal Cycles



# Area Mapping – Damage Accumulation



27 cycle



470 cycle

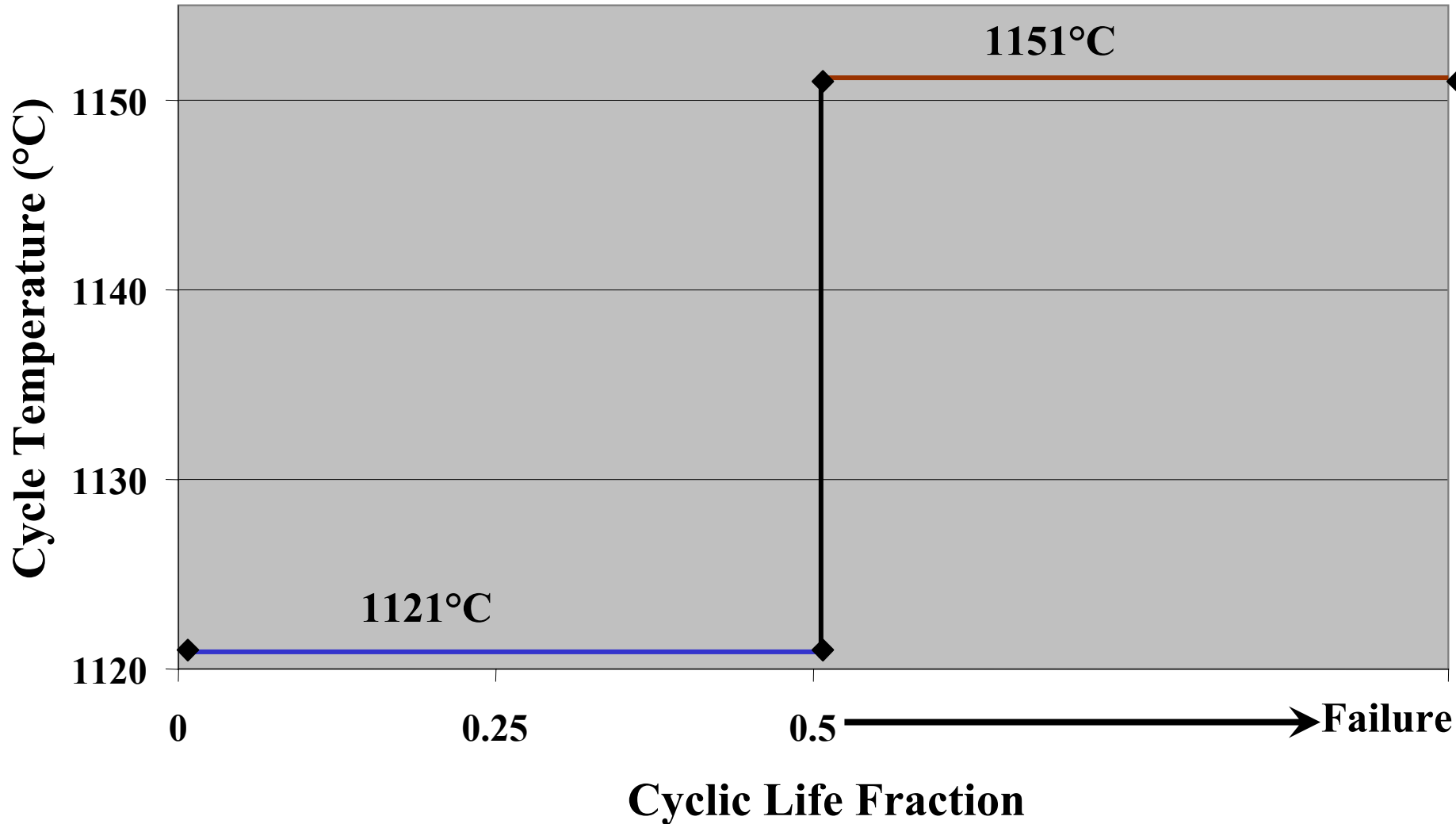
■ Damage (Bi-modal)

□ Intact



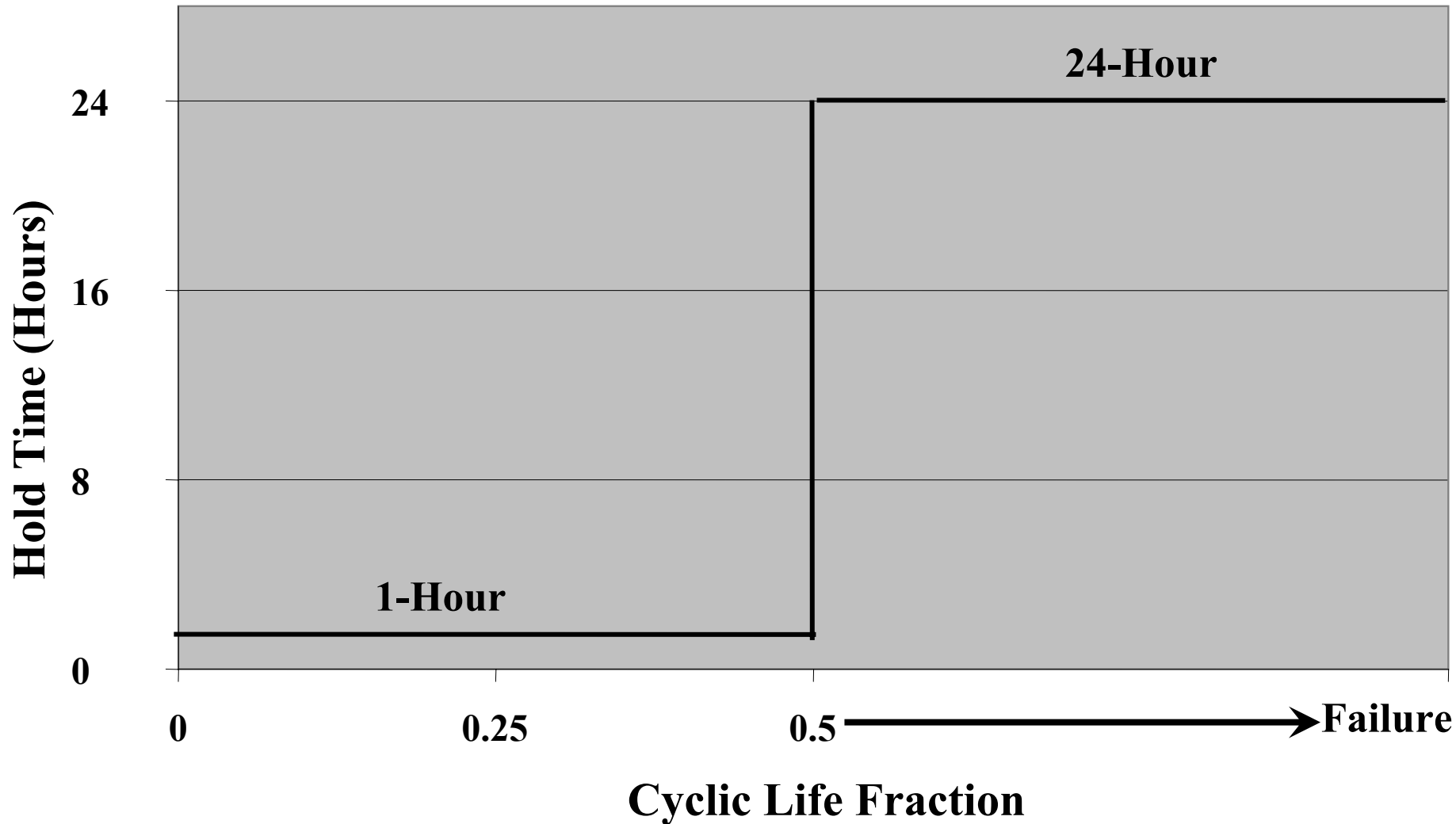
# *Non-Constant Amplitude Tests*

## *Two Temperature Cyclic Tests*



# *Non-Constant Amplitude Tests*

## *Two Hold Time Cyclic Tests*

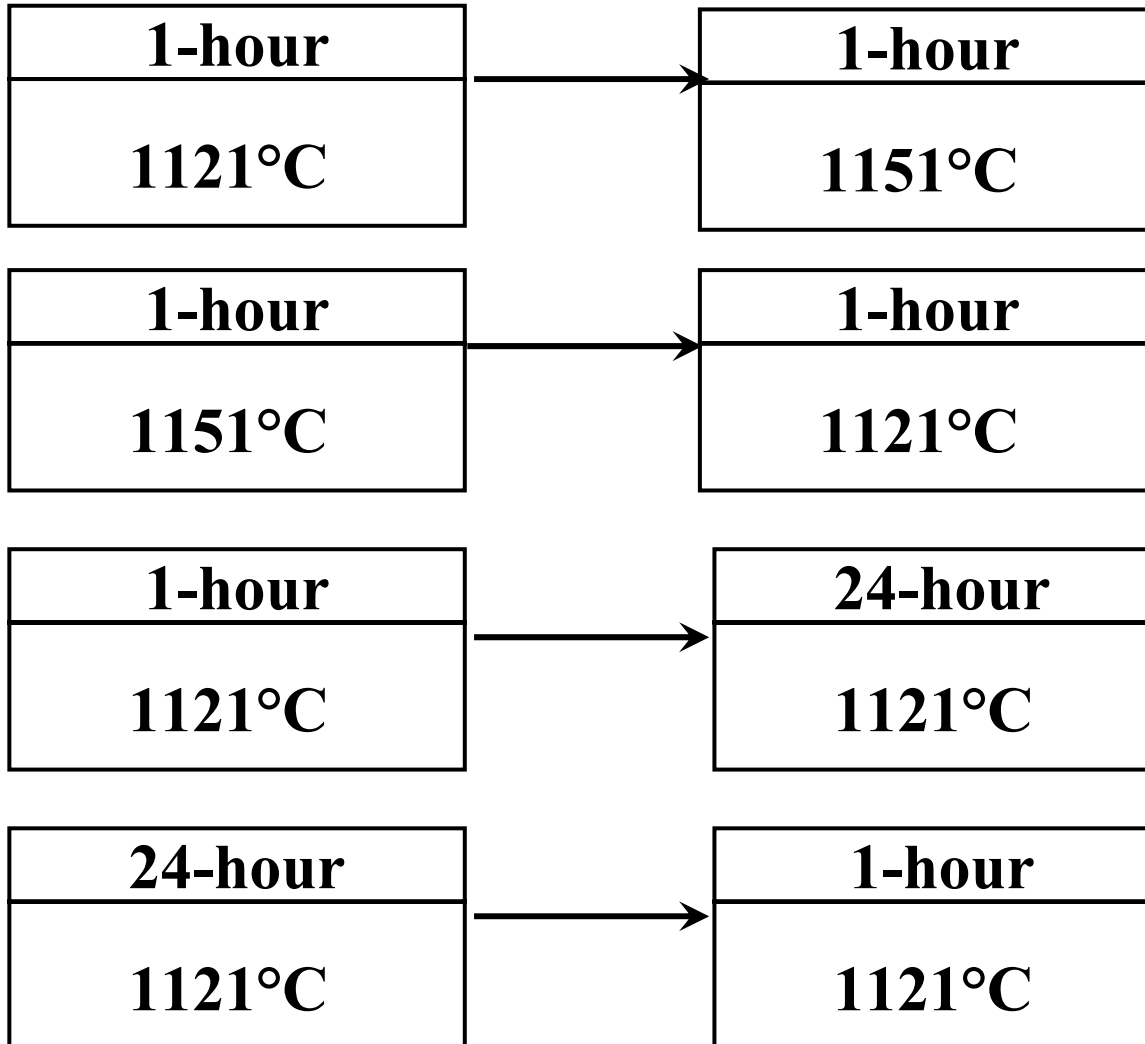


# Linear Damage Example 1121° C followed by 1151° C

- Failure life at 1121°C  $N_{f1}=677$
- Cycles run  $n_1= 335$
- Life fraction  $=335/677=0.49$
- $N_1/N_{f1}+n_2/N_{f2}=1$
- At 1151°C  $N_{f2}=358$
- Predicted life= $0.51*358=$

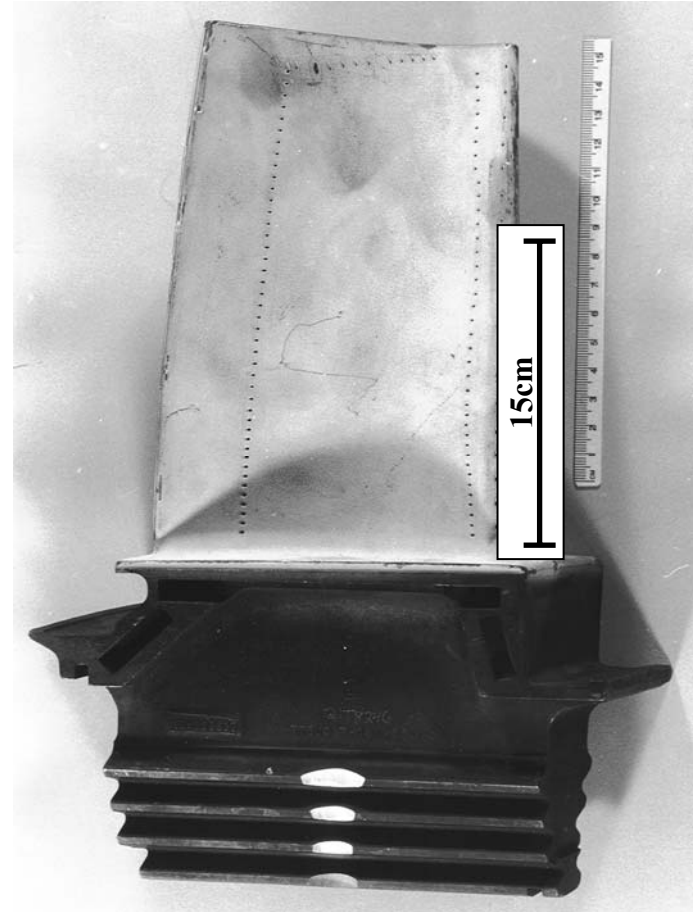
# *First Ever Sequence Effect Tests*

## *Linear Damage Fractions – Type I TBC*



<b>Linear Damage Sum</b> $= N_1/N_{1f} + N_2/N_{2f}$
<b>1.08</b>
<b>1.10</b>
<b>0.75</b>
<b>0.93</b>

# Portable PLPS NDI Instrument Available





# ACOMPLISHMENTS

- **An accurate remain life NDI based on TGO Stress measurement**
  - **Showed a direct relation to damage and failure**
- **A new surface metric more related to damage than RMS etc.**
- **Tested the linear damage rule for TBC life prediction for the first time**
- **Revealed failure mechanisms**

# ACOMPLISHMENTS

- **Transferred technology to industry**
- **Two Ph D and two masters  $\frac{3}{4}$  female**
  - **Swetha Sridharan**
  - **Mei Wen**
  - **Jessica Shen**
  - **Manish Madhwal**

# **Goal Was to Develop Practical Tool**

- **We are one year into an industrial contract to apply Stress Measurement Method developed under HEET/AGTSR funding to blade retirement for cause.**

**Thank You**

# Approach

**Task I : Specimen Procurement**

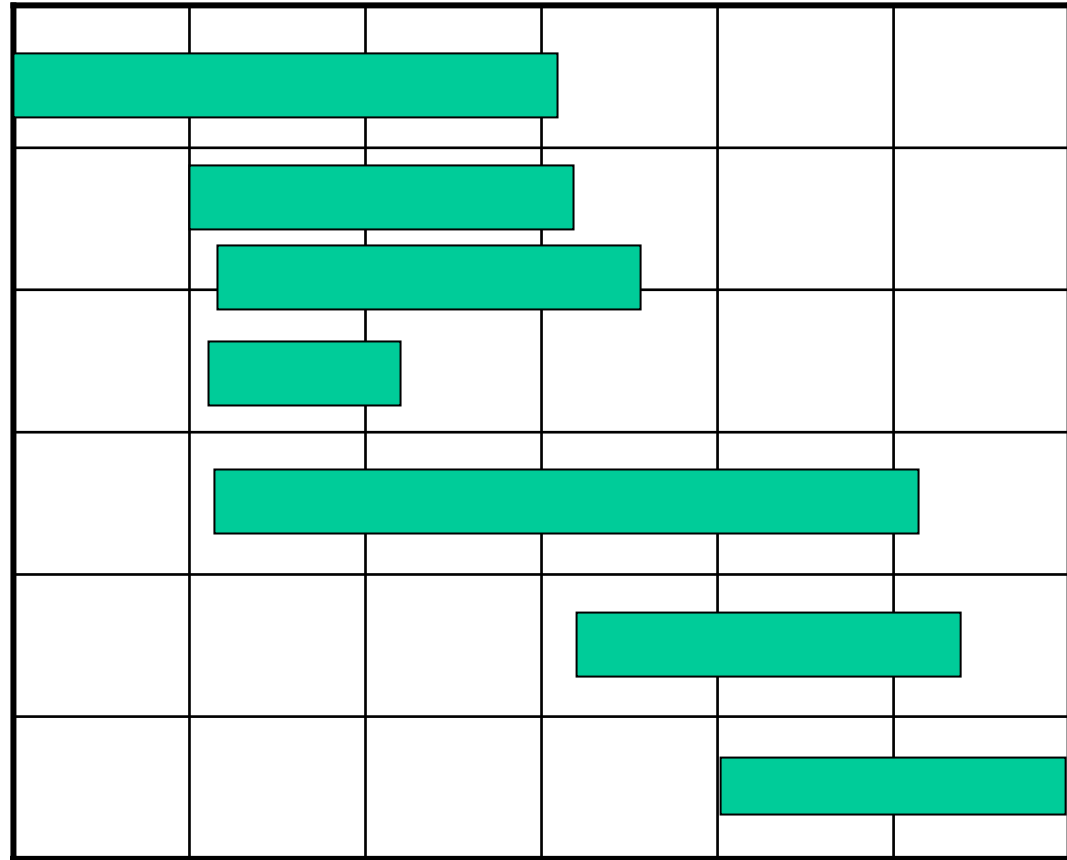
**Task II : (a) Bond Coat Surface Geometry  
(b) TBC Coating**

**Task III : Geometric Feature Software  
Development**

**Task IV : Cyclic Furnace Tests**

**Task V : Measurements of Engine Blades**

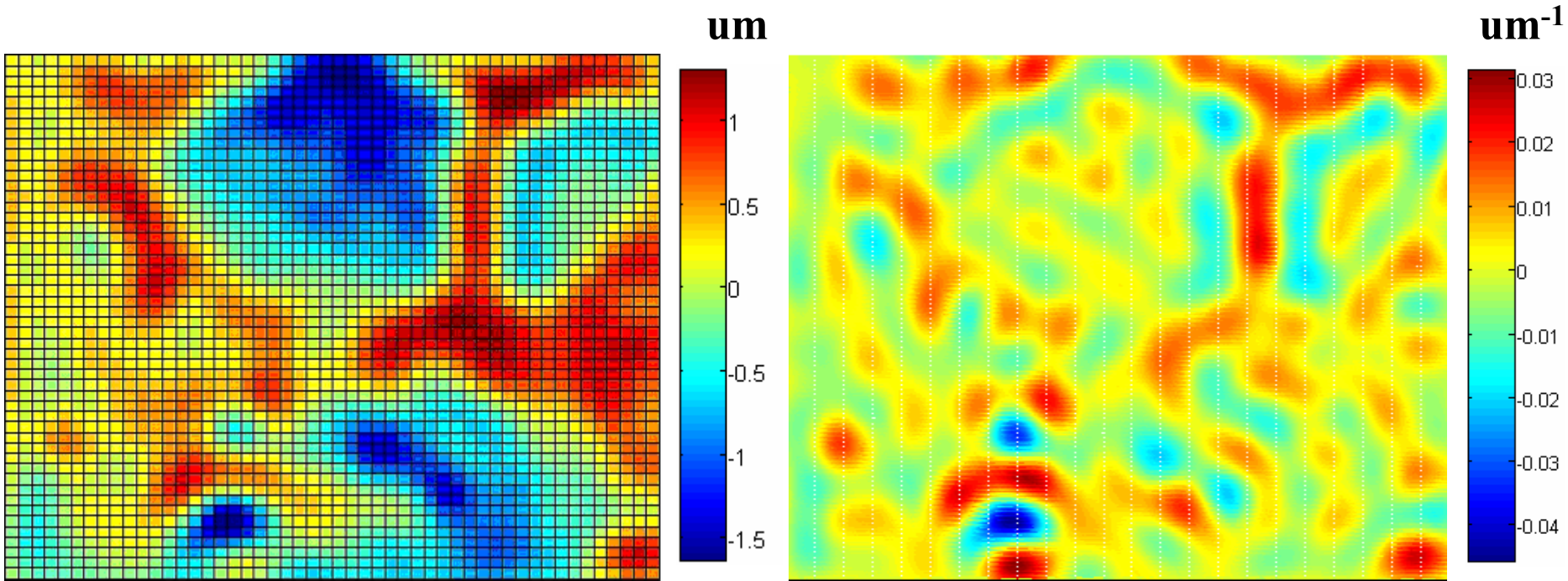
**Task VI : Development of Lifetime  
Prediction Methodology**



05/02 11/02 05/03 11/03 05/04 11/04 05/05  
Date



# Mapping of Curvature by MATLAB



Original Surface

Curvature



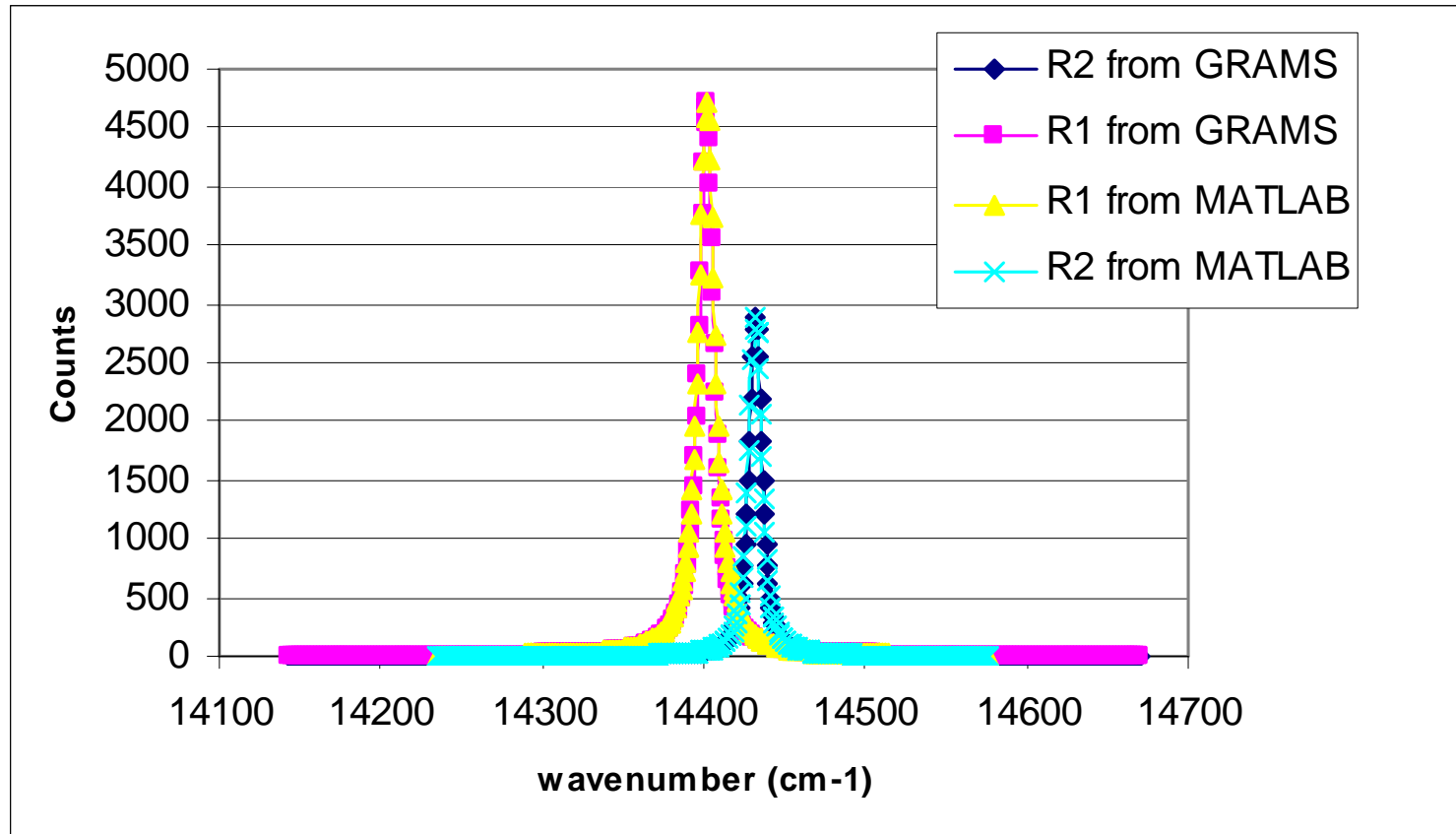
# Project Objectives

**To develop and experimentally validate a method for the nondestructive prediction of remaining life of by measurement of :**

- **Initial Surface Geometry**
- **Thermally Grown Oxide (TGO) Stress**
- **TGO Thickness**



# Results of Automated Analyzing PLPS Spectra



	$L_{R2}$	$V_{R2}$	$W_{R2}$	$H_{R2}$	$L_{R1}$	$H_{R1}$
<b>Grams</b>	0.7581	14432	9.6300	1.4690e5	0.9898	2.3452e5
<b>Matlab</b>	0.7290	14432	9.7534	1.4617e5	0.9990	2.3492e5





# Results of Multi-Temperature Cyclic Tests – 1-hour @ 1121°C Followed By 1-hour @ 1151°C

Exposure Condition	Cycled To		Average Failure Life		Linear Damage Fraction	
	# Cycles	Hot Time (Hours)	# Cycles	Hot Time (Hours)	Based on Cycles	Based On Hot Time (Hours)
1-hour @ 1121°C	335	251	<b>677</b> ± 55	<b>508</b>	<b>0.49</b>	<b>0.49</b>
	335	251			<b>0.49</b>	<b>0.49</b>
1-hour @ 1151°C	<b>205</b> (Failed)	154	<b>358</b> ± 65	<b>269</b>	<b>0.57</b>	<b>0.57</b>
	<b>225</b> (Failed)	169			<b>0.63</b>	<b>0.63</b>
	<b>Total = 356 Cycles</b>	<b>Total = 520 Hours</b>			<b>Total = 1.06</b>	<b>Total = 1.12</b>