



# Novel Concepts for the Compression of Large Volumes of CO<sub>2</sub>

Dr. Jeffrey Moore Dr. Klaus Brun Ms. Marybeth Nored Mr. Ryan Gernentz Southwest Research Institute

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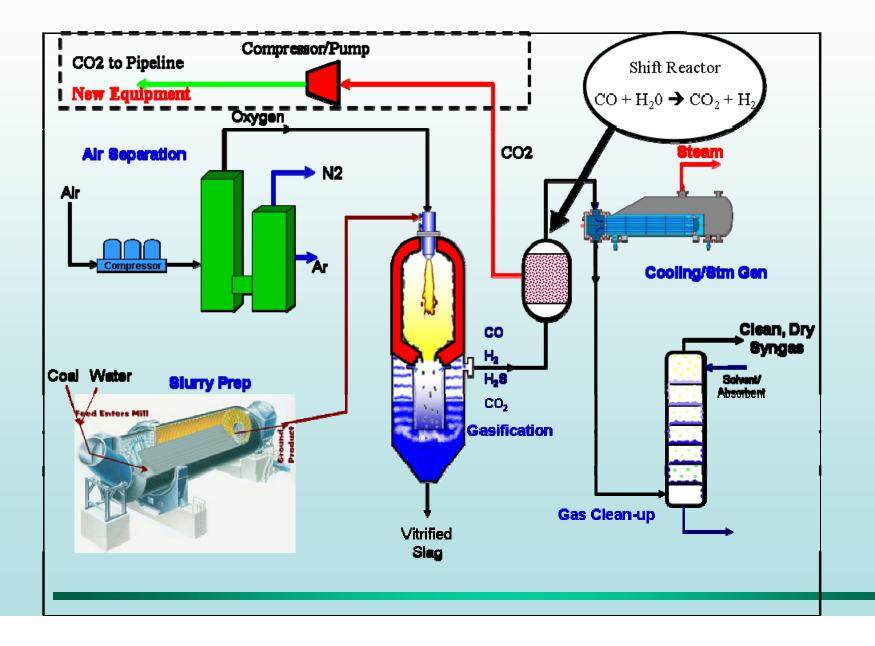
- CO<sub>2</sub> capture has significant compression penalty
  - As high as 8-12%
- Final pressure around 1500-2200 psi for pipeline transport or re-injection
- Typical flow rate 600,000 700,000 lbm/hr
  - Based on 400 MW IGCC plant
- Goal of this project is to minimize compression power penalty
- Many thermodynamic processes studied
- Several challenges with application discussed



- Type of compressor highly dependent on starting pressure (15 or 300 psia)
  - Approx 20-500 psia for CO<sub>2</sub> scrubbing of fuel stream (IGCC)
  - Approx 15 psia from CT or boiler exhaust scrubber
- High pressure ratio results in significant heat of compression
- Various compressor types considered
- Isothermal compression one concept considered to reduce power of compression
- Liquefaction of CO<sub>2</sub> also studied



#### **IGCC Process with Carbon Capture**



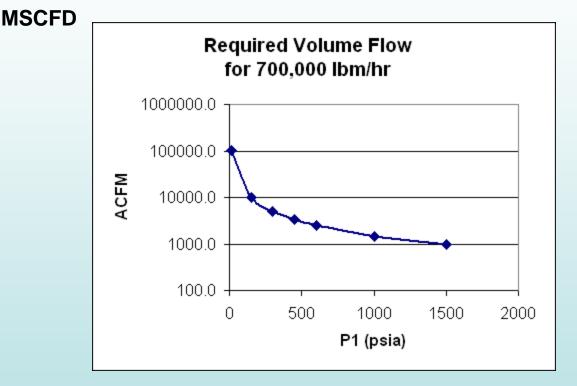


**Mass Flow** 

#### **Required Inlet Volume Flow for C0<sub>2</sub> Compressor**

	=144.89	M
Pressure	Volume Flow	
(psia)	ACFM	
14.7	100595.2	
150	9858.3	
300	4929.2	
450	3286.1	
600	2464.6	
1000	1478.8	
1500	985.8	

= 700,000 lbm/hr



• High volume reduction adds to challenge in compressor selection

T=60 F

### Example IGCC CO<sub>2</sub> Separator Conditions

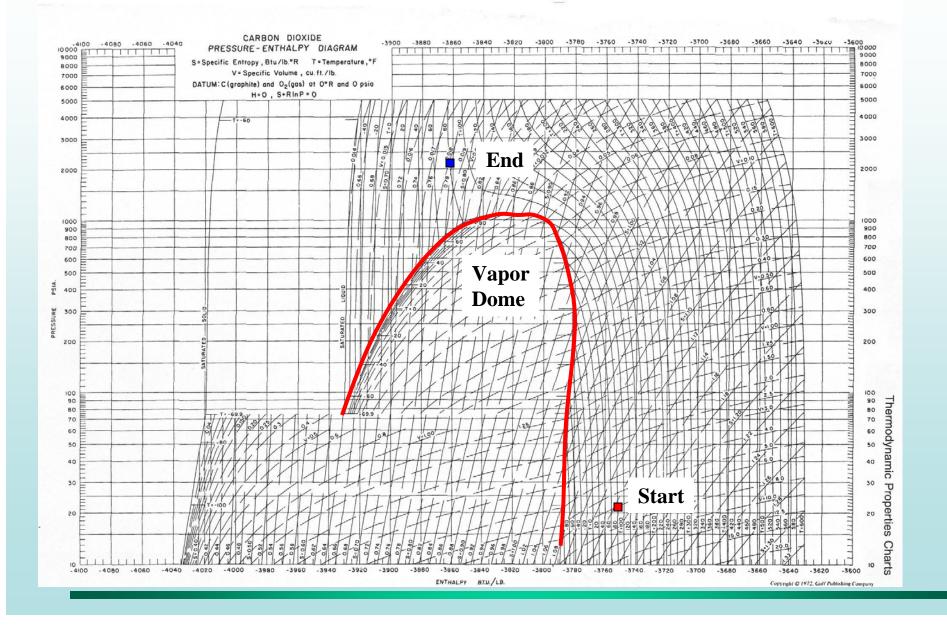
Uncompressed CO<sub>2</sub> Streams in typical IGCC plant with physical absorption separation method using Selexol solvent.

CO2 Gas Streams	LP	MP	HP 1	HP 2
Pressure (psia)	21.9	160.0	250.0	299.0
Temperature (°F)	51.0	68.0	90.0	75.0
Density (lbm/ft <sup>3</sup> )	0.177	1.3	1.87	2.088
Flow Rate (acfm)	33,257	2,158	3,374	1,073

Higher pressure streams help reduce volume reduction allowing more uniform frame size in compressor selection



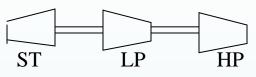
### $\mathbf{P}_{\mathbf{P}}$ Pressure-Enthalpy Chart for $\mathbf{C}_{\mathbf{O}_2}$





### **D-R** Selection Using Conventional Centrifugal Compressors (Baseline)

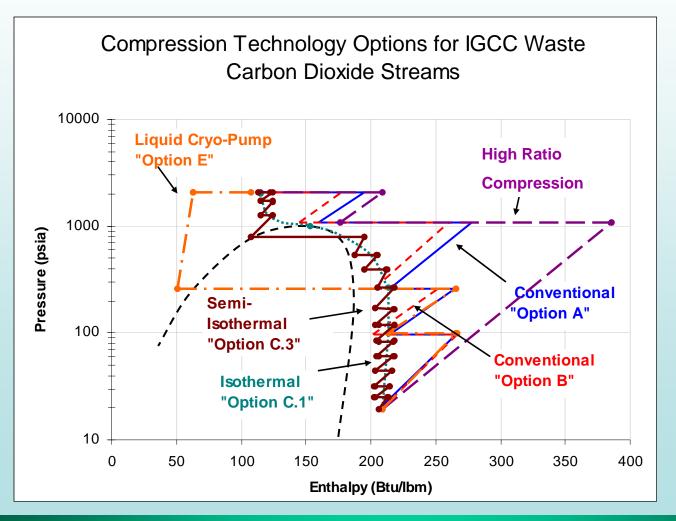
- Requires 2 Parallel Trains
- Intercooling Between Each Section



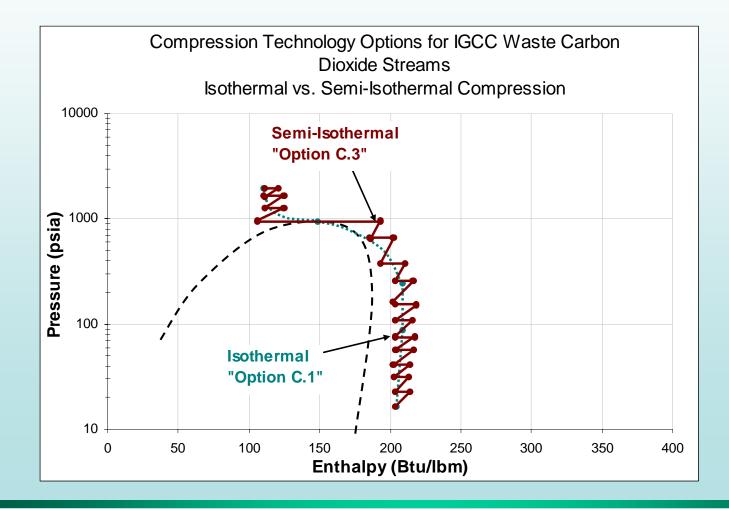
9	OPERATING CONDITIONS					
10						
11	(ALL DATA ON PER UNIT BASIS)			Base		
12		D18R7B D16R9B				R9B
13		SEC #1	SS In	SEC #2	SEC #1	SEC #2
14	<ul> <li>GAS HANDLED (ALSO SEE PAGE )</li> </ul>	LP	MP		Ble	end
17	● WEIGHT FLOW, (Lb/Hr) (WET)	176,649	168,445	260,872	517,475	517,475
18						
19	PRESSURE (PSIA)	21.90	170.0	96.58	248.0	1,087
20	TEMPERATURE (°F)	51.00	68.00	90.21	100.00	100.0
22	MOLECULAR WEIGHT	43.88	43.13	43.63	41.61	41.61
25	■ INLET VOLUME, (ACFM)(WET)	16,634		5,908	4,694	745.0
26	DISCHARGE CONDITI					
27	PRESSURE (PSIA)	106.6		258.0	1,097	2,215
28	■ TEMPERATURE (°F)	299.3		258.1	369.8	231.4
29	Cp/Cv(Kavg)	1.271		1.272	1.274	1.230
30	COMPRESSIBILITY (ZAvg)	0.9910		0.9685	0.9334	0.6919
36						
37	GHP REQUIRED (HP)	3,684		3,656	12,126	5,180
40	SPEED (RPM)			5,166		

Total Power = 49,292 hp (37 MW, 5.2% of 700MW Output)

#### All Processes

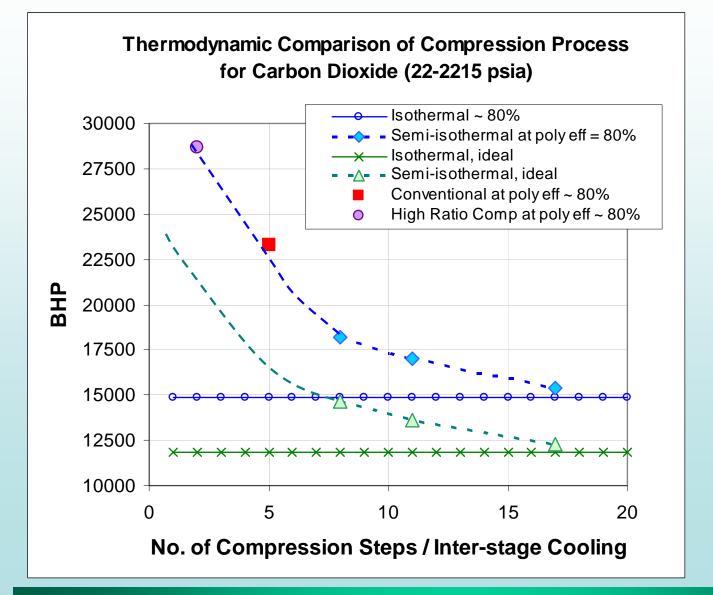


#### Semi-Isothermal Process



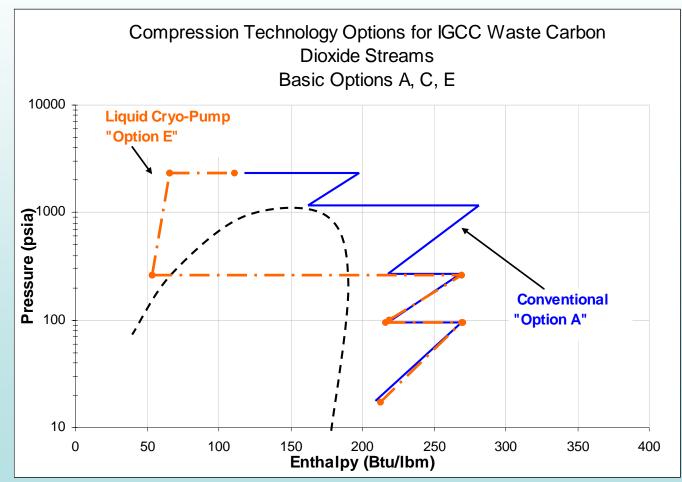
## SR.

### Summary of Thermodynamic Analysis



• 17 intercooled stages provide near isothermal performance

#### Liquefaction Process



## SR .

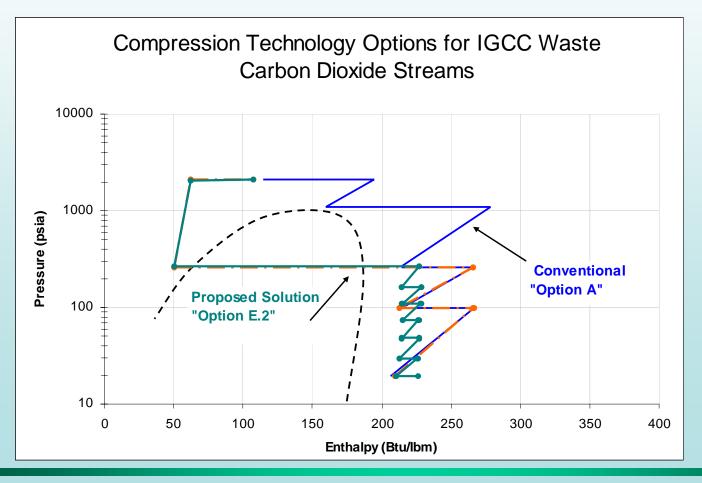
### Summary of Thermodynamic Analysis

#### Liquefaction Process

- Utilize a refrigeration system to condense CO<sub>2</sub> at about 250 psia and -20F
- Liquid then pumped from 250 to 2215 psia
- Requires significantly less power to pump liquid than compress a gas
- Cost of refrigeration system must be accounted for

#### Proposed Optimal Solution

Combines interstage cooling and liquefaction approach





Option	Compression Technology	Power Requirements	% Diff from Option A	Cooling Technology
A	Conventional Dresser-Rand Centrifugal 10-stage Compression	23,251 BHP	0.00%	Air-cool streams between separate stages
В	Conventional Dresser-Rand Centrifugal 10-stage Compression with additional cooling	21,522 BHP	-7.44%	Air-cool streams between separate stages using ASU cool N2 stream
C.1	Isothermal compression at 70 degF and 80% efficiency	14,840 BHP	-36.17%	Tc = 70 degF inlet temp throughout
C.4	Semi-isothermal compression at 70 degF, Pressure Ratio ~ 1.55	17,025 BHP (Required Cooling Power TBD)	-26.78%	Tc = 70degF in between each stage.
C.7	Semi-isothermal compression at 100 degF, Pressure Ratio ~ 1.55	17,979 BHP (Required Cooling Power TBD)	-22.67%	Tc = 100degF in between each stage.



Option	Compression Technology	Power Requirements	% Diff from Option A	Cooling Technology
D.3	High ratio compression at 90% efficiency - no inter-stage cooling	34,192 BHP	47.06%	Air cool at 2215 psia only
D.4	High ratio compression at 90% efficiency - intercooling on final compression stage	24,730 BHP	6.36%	Air cool at 220 and 2215 psia
E.1	Centrifugal compression to 250 psia, Liquid cryo-pump from 250- 2215 psia	16,198 BHP (Includes 7,814 BHP for Refrigeration) <sup>1</sup>	-30.33%	Air cool up to 250 psia, Refrigeration to reduce CO2 to -25degF to liquify
E.2	Centrifugal compression to 250 psia with semi-isothermal cooling at 100 degF, Liquid cryo-pump from 250- 2215 psia	15,145 BHP (Includes 7,814 BHP for Refrigeration) <sup>1</sup>	-34.86%	Air cool up to 250 psia between centrifugal stages, Refrigeration to reduce CO2 to -25degF to liquify



- Provide enabling technology to compress CO<sub>2</sub> from a coal fed IGCC power plant cost effectively minimizing the financial impact of CO<sub>2</sub> sequestration
- Supports carbon capture to eliminate green-house gas emissions from power plants, which make up 35% of total CO<sub>2</sub> emissions
- Minimize financial impact to US industry and consumers of electricity
- This program identified up to 35% power savings over a conventional CO<sub>2</sub> compression solution
- Thermodynamic process more important than compressor efficiency
- Program proceeding into Phase 2 to perform validation testing



## **Questions???**

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Dr. J. Jeffrey Moore Southwest Research Institute (210) 522-5812 Jeff.Moore@swri.org