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FINAL REPORT FOR THE
EVALUATION OF UNEXPLODED ORDNANCE (UXO)
DETECTION TECHNOLOGY AT THE
STANDARDIZED UXO TEST SITES
ABERDEEN AND YUMA PROVING GROUNDS
MILITARY ENVIRONMENTAL TECHNOLOGY DEMONSTRATION CENTER
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| 14. ABSTRACT The U.S. Army Environmental Command (USAEC) issued a Test Execution Directive to Aberdeen Test Center (ATC), Aberdeen Proving Ground (APG), Maryland, to plan, perform, and report the evaluation of unexploded ordnance (UXO) detection technology. The standardized UXO test sites at APG and Yuma Proving Ground (YPG) were used to (1) determine detection and discrimination effectiveness under realistic scenarios that varied targets, geology, clutter, topography, and vegetation; (2) determine cost, time, and manpower requirements to operate the technology; (3) determine the demonstrator's ability to analyze survey data in a timely manner and provide prioritized "target lists" with associated confidence levels; and (4) provide independent site management to enable the collection of high quality, Ground Truth (GT), geo-referenced data for postdemonstration analysis. Testing emphasized the demonstration and evaluation of government and private industry ordnance detection systems. | | | | | |
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SECTION 1. EXECUTIVE DIGEST

1.1 SUMMARY

1.1.1 Introduction

a. Technologies under development for the detection and discrimination of Munitions and Explosives of Concern (MEC), which include Unexploded Ordnance (UXO) and Discarded Military Munitions (DMM), require testing so that the performance can be characterized. To that end, Standardized Test Sites have been developed at Aberdeen Proving Ground (APG), Maryland, and Yuma Proving Ground (YPG), Arizona. The test sites provide a diversity of geology, climate, terrain, and weather as well as diversity in ordnance and clutter. Testing at the sites has been independently administered and analyzed by the government for the purposes of characterizing technologies, tracking performance with system development, comparing performance of different systems, and comparing performance in different environments. By hosting the demonstration of detection systems since 2001 and publishing performance results in a standard format on the Internet, the program has served as a tool to quickly assess the abilities of off-the-shelf (OTS), developmental, and state-of-the-art (SOTA) technologies. The following is a summary of where UXO detection technology stands based on the results from the program through May, 2006.

b. The task of assessing the performance ability of detection systems is difficult. One reason for this is that in real world UXO remediation sites, no two sites contain the same type, distribution, depth, and orientation of ordnance. Clutter distributions and anomalous magnetic signals also vary at each site. Lastly, terrain varies from site to site. Therefore, one system may excel at one site and perform poorly at another, depending on the system's abilities. This variability has also existed over the years at different UXO test sites and can bias the results when comparing different detection systems demonstrated at different test areas. Further, different performance metrics used between these areas can make comparisons difficult. For these and other reasons, the standardized sites have been established. The sites provide a continuing test bed with standardized test metrics to evaluate detection systems. Because of the large number and variety of Ground Truth (GT) items (GT simply refers to a test group of buried ordnance and clutter) at the sites, general performance merit can be evaluated with good confidence in results.

c. A summary of basic system types and test configurations used at the sites are set forth as follows. Three basic sensor types were tested at the sites, which include electromagnetic induction (EMI or EM), magnetometer (MAG), and radar varieties. These sensors were sometimes combined so that two types would be a part of one system. Such a system is referred to as a dual system. The sensors were typically mounted on one of five platform types for carriage. These types were towed, pushcart, hand held, sling, and litter (will be referred to as 2-man) varieties. The latter three types are considered man-portable types. The basic types of test areas used include open field (flat open), mogul (small mounds), wooded, and extreme desert types of terrains with YPG providing a sand soil and APG a silty loam type soil. A test grid, referred to as a blind grid, where potential item positions are known, is also part of the test areas. All test areas typically contained 14 standard ordnance types ranging from small submunitions to

155-mm projectiles. Many types of ferrous-based clutter items typically ranging in mass from approximately 0.005 to 25 kg were inter-dispersed in the test areas with the ordnance items.

d. Results from the sites should be viewed as those gained from a unique test instance. The merit of a system may not be fully represented because of variables such as system health, human error, operator skill levels, and environmental conditions. Nonetheless, results presented represent “what is possible” in various arrangements of the GT used and in that sense characterize SOTA technology.

e. The reader should be aware that detection rules at the sites were set up so that a “detection” is considered the ability to “discern” an “individual” item in the ground. The problem with this approach is that some items are very close together in the ground and signal returns from the combined items appear as “one” anomalous signal. Thus, if two items are side by side in the ground and the detection system indicates one anomaly, then only one detection is granted. These rules apply when items are closer than one meter to each other or equivalently, when half meter radii around each item “overlap”. While the number of ordnance with overlap are small in the GT, the use of these rules will reduce and hence misrepresent detection scores if it is only desired to see if signals, whether from single or combined items, were detected. For the reader wanting to see results free from the effects of overlaps, GT variants have been created and are noted as having “no overlaps” or noted that distances between items are greater than one meter (all blind grid test areas inherently have no overlaps). Such results are the best indicator of detection ability for individual items. Conversely, results with overlaps have merit when comparing the performance of multiple systems to see if one system can better discern multiple items in close proximity than another. Also, comparing scores with and without overlaps gives some indication of the effect of signal masking from items in close proximity to each other.

f. The GT at the standardized sites contain items at or beyond (in some cases) the detection depth range of SOTA detection systems. This allows system limits to be determined. In real world cleanup sites, systems are not typically required to detect beyond ordnance depths of 11 diameters. Further, systems are typically evaluated in GT configurations that do not exceed this depth. Therefore, a majority of the results shown will use this GT depth limit when possible.

g. Finally, it is noted that sometimes discussion of GT details and their effect on scores are intentionally kept vague so proprietary GT information is not disclosed. This prevents gaming by demonstrators still using the sites. In time, as the sites are reconfigured, detailed information will be released.

1.1.2 Results/Findings

a. For the benefit of readers unfamiliar with the scoring metrics to be presented, the following short list of definitions is provided for easy reference (a more comprehensive list can be found in section 2.1.3). Further, to promote understanding of the naming conventions used in the plots, legend names consist of a basic sensor or system name followed by a platform type followed by a published report number (see section 2.3.1d for more details). Lastly, MAG systems can only detect ferrous (iron) items, so for these systems all non-ferrous items are removed from the GT for scoring unless otherwise noted.

(1) Probability of Detection in the Response Stage (P_d^{res}) - the number of ordnance detected divided by the total number of ordnance present in a test area (alternately, the percentage of ordnance detected divided by 100).

(2) Background Alarm - similar to a false alarm, a system response indicating an ordnance or clutter item is present where none exists.

(3) Probability of Background Alarm in the Response Stage ($P_{\text{ba}}^{\text{res}}$) - used only in blind grid test areas, the metric is the number of empty grid cells in which the system indicates an item is present, divided by the total number of empty cells (alternately, the percentage of empty cells indicated not to be empty divided by 100).

(4) Background Alarm Rate (BAR^{res}) - the number of system background alarms in a test area divided by an undisclosed constant and multiplied by an acreage ratio (open field/test area). The measure allows relative comparisons to be made between systems and test areas at a given proving ground.

(5) False Positive - a clutter item indicated to be an ordnance item after discrimination has occurred.

b. Blind grid values of P_d^{res} typically ranged from 0.7 to 1.0 at APG and 0.8 to 1.0 at YPG for all systems demonstrated when the GT was limited to an 11 diameter (D) depth. The lower scores at APG are attributed to a greater average GT depth. The APG results are shown in Figure 1. The APG blind grid results are shown because the grid had the highest number of systems demonstrated when compared with all other test areas and reflects a large cross section of UXO detection systems available. It is noted that the APG blind grid was dug up and reconfigured in the November, 2004 to April, 2005 time frame. Demonstrators with report numbers 680 and higher tested in the post-reconfiguration version of the blind grid. The new configuration is very similar to the old, so results should be comparable and are plotted for the reader's benefit (use for general comparison only).

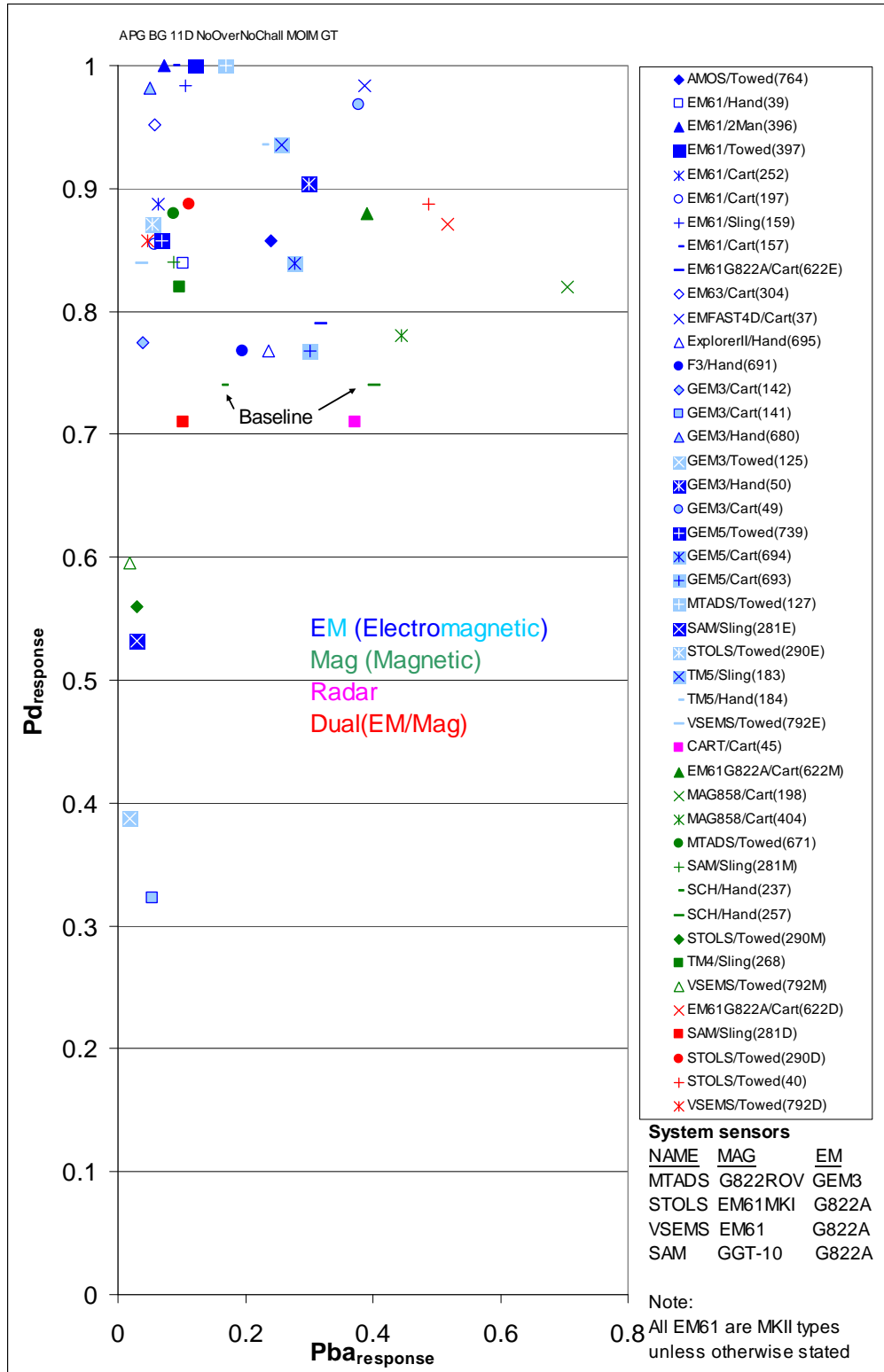


Figure 1. P_d^{res} , versus probability of background alarm (P_{ba}^{res}), APG blind grid results.

c. The blind grids at APG and YPG contain well spaced (2 meter) ordnance and clutter items buried at the center of grid cells in a flat, open area. Cell locations are known by demonstrators; therefore, their systems need only discern whether or not an item is present from a sensor response. Based on the results from both sites, it can be said that the best detection system sensors can find 100 percent of ordnance items in these simplest of test areas at the sites. The better systems had a 0.1 or less P_{ba}^{res} score, which means about 10 percent of empty cells were incorrectly declared to be occupied by an item. EM61 MKII and GEM3 sensors proved to be the best performers in the blind grid areas (both are EM types) with perfect detection rates and a small fraction of background alarms (in some cases zero).

d. A common result seen not only in the blind grids but also most test areas was that Schonstedt systems (the most common hand held system used in real-world applications, technically a flux-gate-type MAG) were outperformed by more complex systems with integrated Global Positioning System (GPS) and sensor data (digital geophysical mapping ability). Two Schonstedts were tested to provide a baseline result, which is shown in Figures 1 and 2.

e. Values of P_d^{res} versus BAR^{res} are shown in Figure 2 for systems demonstrated at the APG open field. This 13.7-acre field is filled with a much larger population of ordnance and clutter than the blind grids and has items at varying distances from one another. The results in Figure 2 are from a GT limited to an 11 D depth and with no items within 1 meter of each other (no overlap). Further, any areas of the field with power-lines, fences or wet areas are eliminated in the GT. A small portion of the field was reconfigured in the November, 2004 to April, 2005 time frame but was kept characteristically similar except for background noise (many items causing background alarms were removed). Demonstrators with report numbers 740 and 802 tested in the new version of the field. Their results are shown for general comparison only and likely have lower BAR scores than they would have had in the original field configuration (also, some noisy items were removed in an exploratory phase prior to reconfiguration which may have slightly reduced the BAR scores of report numbers 657, 298, 802, 740, 231, 406, 411 and 229).

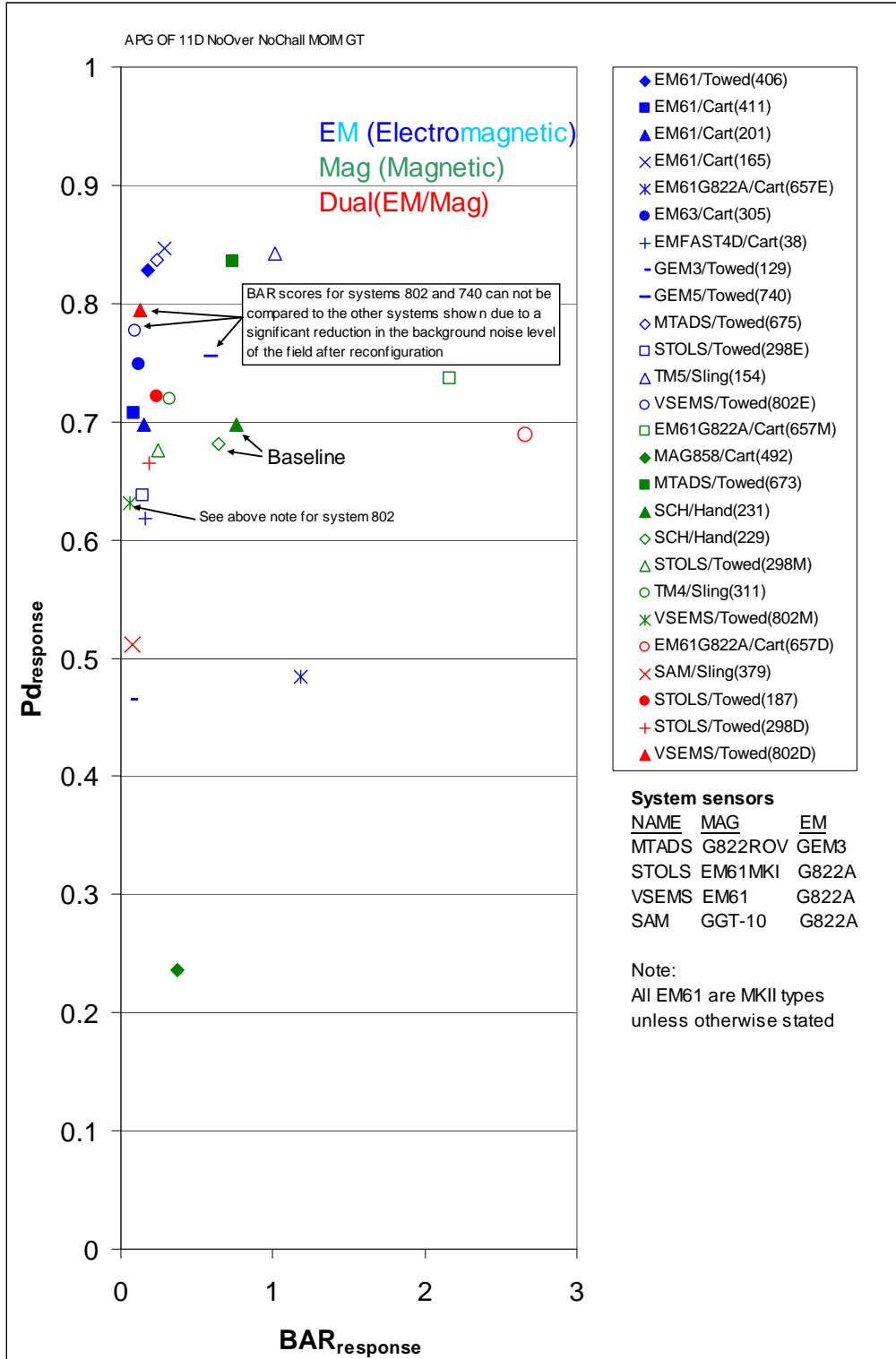


Figure 2. P_d^{res} versus BAR^{res} , APG open field results.

f. A significant reduction (~15%) in P_d^{res} when compared with the blind grid results is shown in Figure 2. This reduction is primarily driven by the potential locations of items being unknown (potential locations were known for blind grid), items closer to other GT causing signal interference (1 meter minimum spacing for open field, 2 meter minimum for blind grid), and a greater population of items of small mass/size. These and other drivers are discussed in greater detail later in this section.

g. As shown in Figure 2, better performers can keep the number of background alarms they produce to a relatively low level compared with all other systems demonstrated in the field. The number of background alarms at the APG open field was typically a few thousand or less for most systems. This number changed little after demonstrators reviewed their response stage lists to reject what they thought were non-ordnance items (termed “discrimination” stage processing).

h. Better performers in the open field areas were typically GEM-3, EM61 MKII, and TM-5 types of EM sensors, and an 822ROV MAG sensor. The 822ROV sensor had a relatively high (3x) background alarm value compared to the EM systems. An EM61 MKII/G822A dual system (EM/MAG) performed well but not as well as systems with the same sensors operating independently. All of the better performers were typically on a towed, cart, or sling type platform.

i. All systems demonstrated generally detected the same percentage, or less (APG), of intentionally buried clutter as ordnance in the open fields.

j. Relative performance results, as expressed by the percent difference from open field P_d^{res} results (100% represents twice the open field Pd result) for the various test areas, are shown in Figure 3, which are included to demonstrate the impact of various terrains on detection performance. Not all systems demonstrated are included in the figure. The GT used in the figure between a given test area and the open field baseline is the same (number, type, depth, orientation). Compared to performance in the open field, most systems experience an approximate 30 percent reduction in detection ability in rough or brush-laden terrains. Schonstedt systems are the exception to this generalization. It is also seen that the blind grids are much easier for systems than the open fields.

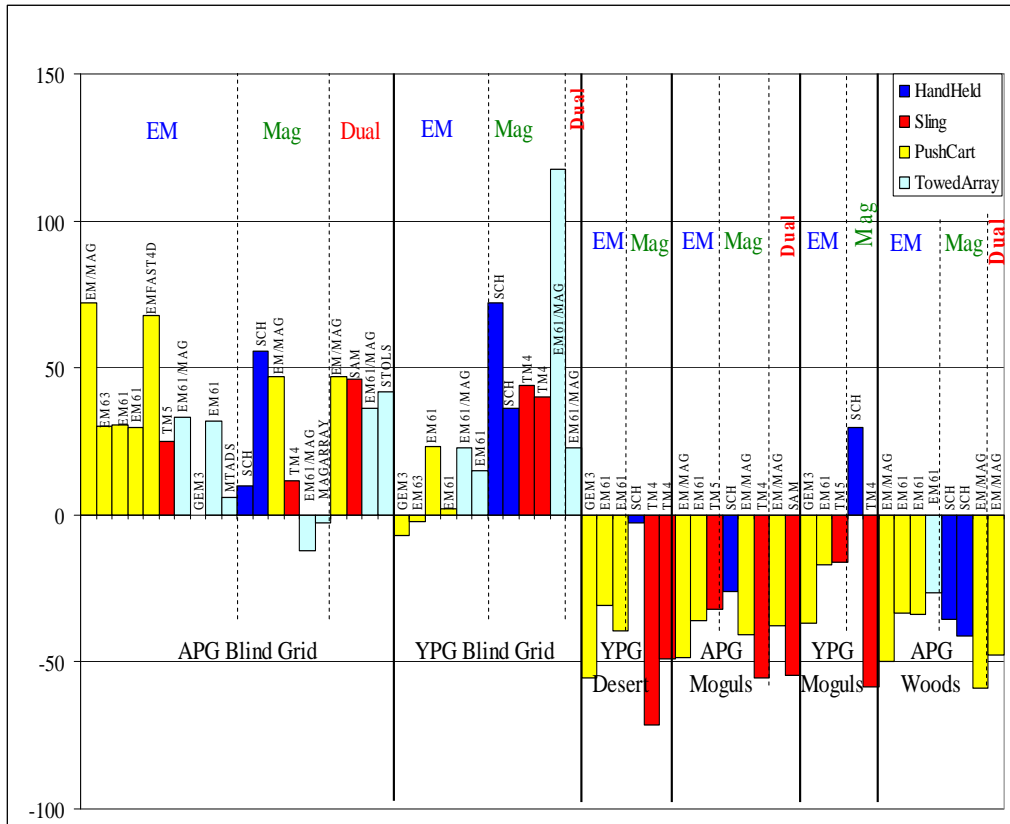


Figure 3. Percent difference in P_d^{res} score from open field baseline performance.

k. It was observed that towed array systems performed very well in both open field test areas and had some of the best detection scores. This platform technology is mature and has proven itself at the test sites. Further, it offers time and cost savings in large open terrains. The platforms do have accessibility issues as terrain becomes increasingly rough or filled with obstacles. In the more difficult areas to traverse or access, both carts and man-portable platforms typically performed best. In extremely rough or obstructed terrain like the woods or the moguls at APG, it appears that man-portable platforms perform best.

l. The discrimination abilities (ability to reject non-ordnance responses; see section 2.1.3 for more details) of the demonstrators/systems was minimal at best for the GT configurations at the sites. A test area with a more rudimentary GT configuration is needed at the sites to better evaluate what the technologies are capable of.

m. Analysis was performed on how well systems were maintaining proper lane spacing (spacing specified by the demonstrator). Most systems miss 1 to 5 percent of items they are capable of finding by not maintaining proper spacing. This is manifest as a quality control (QC) issue related to navigation for systems demonstrating.

n. Location error manifest by detection systems at the sites typically averaged from 0.15 to 0.35 m. One configuration achieved a 0.09-m value of average location error in the YPG open field. This system is the multi-sensor towed array detection system (MTADS) GEM-3/towed configuration (report no. 245). Uncertainty in the location of the GT by the test authority is estimated to be about 0.06 m. Therefore, the best location error may approach 0.03 m when this uncertainty is accounted for. Further analysis is needed to discern location error from signal interpretation error (in the sense of pinpointing the center of ordnance).

o. While location errors were in a good range for most systems, they tended to be distributed about their mean value in such a way that from 1 to 3 percent of the detectable population was not being scored as a hit. The location error in such instances exceeded the set radius about the GT, 0.5 m, which was considered a valid detection range. Better QC may eliminate this trend in the test results.

p. Detection rates at various depths were analyzed in terms of ordnance diameters, and results are presented in Figure 4 for the APG open field test area. In general, most systems start to experience a reduction in detection rates at depths between 5 and 11D. The GT used in Figure 4 contains no items within one meter of each other or items in challenge and wet areas. A more in-depth analysis of probability of detection versus depth was performed for systems demonstrated at the standardized sites (ref 5).

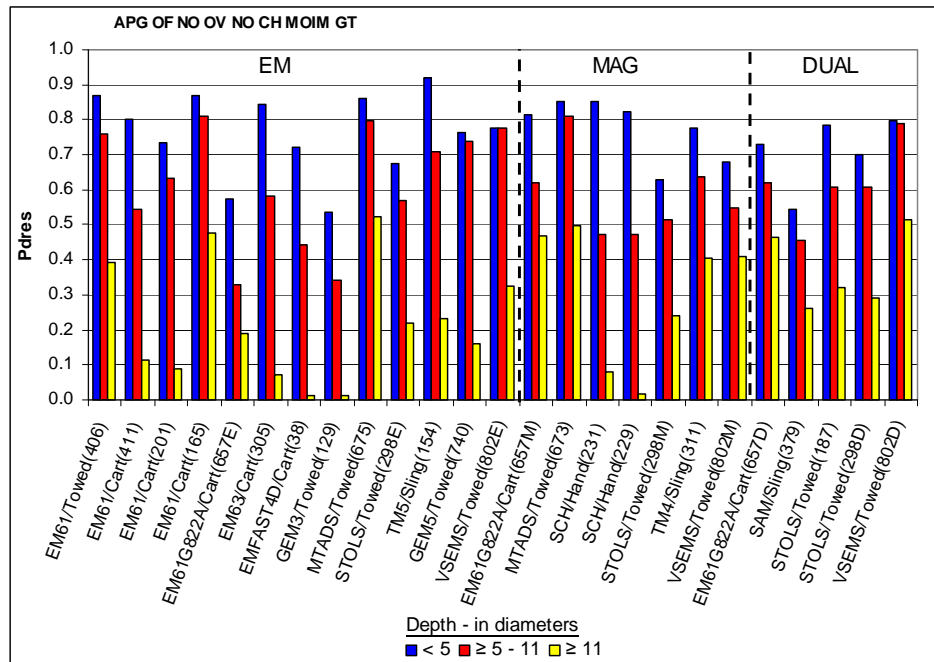


Figure 4. P_d^{res} as a function of depth in ordnance diameters, APG open field.

q. Detection rates for ordnance items at various distances to other ordnance or clutter items were examined for all systems. When an ordnance or clutter item is within approximately 1.5 m from a target ordnance item, P_d^{res} will typically start to decrease.

r. Two ordnance types were problematic for the detection systems tested: 20-mm projectiles and MK118 rocket submunitions. Analysis of 20-mm projectile signals (magnetic field strengths) from MAGs indicates that signal-to-noise ratios of 2 to 1 or less are not uncommon for the deeper (>0.13-m) items. Further, a good portion of these items are affected by signal bleed over (i.e., signals from nearby items confusing detection) from items in close proximity. The MK118 items are aluminum-based and are not detectable by MAGs. Notable performance difficulties for these items were observed in the EM systems.

s. Detection rates for each ordnance type for all systems demonstrated at the open fields are included in Appendix G. The GT used was limited to 11D depth and contained items minimally spaced at 1 meter. Further, items in areas that were intermittently underwater, as well as items located next to fences and power lines, were removed from the GT used.

t. To account for all performance drivers affecting the detection systems, a limited (LIM) GT subset was created for the APG open field. This subset eliminates all identified contributors to performance degradation to see if resulting detection scores will approach 100 percent. The adjustments made are as follows.

(1) A minimum spacing of 1.5 meters was required for GT items (i.e., if an item was within 1.5 m of another item, both items were eliminated from the GT).

(2) If a GT item was not within one-half of the lane spacing (specified by the demonstrator) from a sensor of a system, it was eliminated from the GT set for that system. This could be done only for geophysical mapping systems, which provided proper data.

(3) GT depth was limited to 11D (i.e., items below 11D were eliminated from the GT).

(4) 20-mm projectiles and MK118 submunitions were eliminated from the GT.

(5) Items in challenge areas (e.g., power line, metal fence) were eliminated from the GT. Items in wet areas that were sometimes difficult to traverse were also eliminated.

u. Results for the LIM GT set at the APG open field are shown in Figure 5. APG LIM blind grid results, using GT modifications 2, 3, and 4 above, are also shown for comparison. New P_d^{res} levels in the open field are not at 1.0 but are higher, 30 to 66 percent, than standard GT results and ~10% higher than Figure 2 results. Four systems detected between a 0.92 and 0.94 level (see fig. 2 for background alarm scores). Other analysis shows that some of the P_d deficiency remaining is due to depth issues between 5 and 11D depths. It also seen that four systems achieve $P_d^{\text{res}} = 1.0$ in the blind grids using the modified GT (same as fig. 1). Some LIM predictions are not shown because raw data were not in a format conducive to processing.

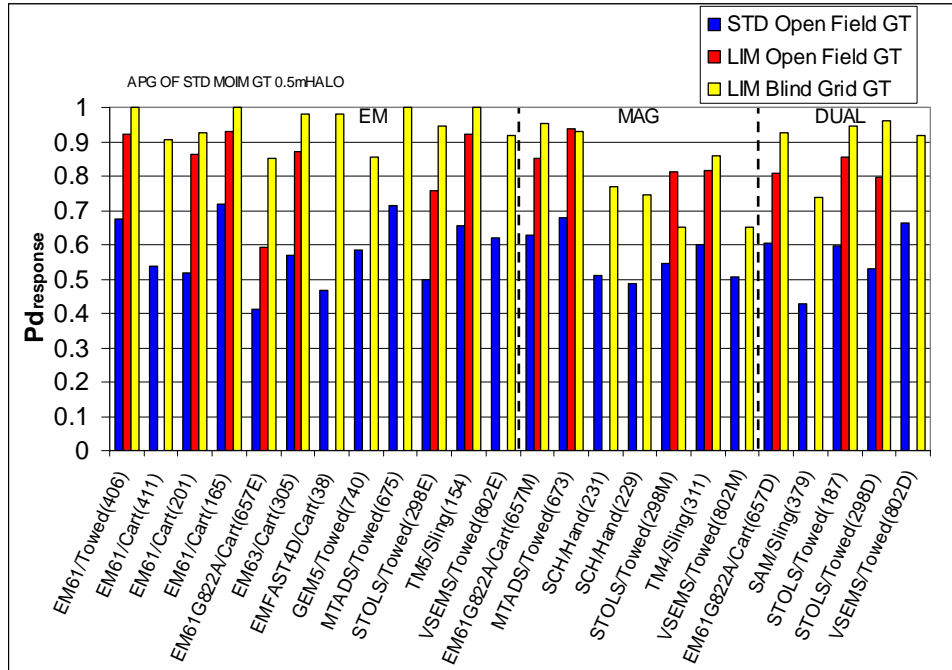


Figure 5. P_d^{res} for standard and LIM GT sets at APG.

v. Estimated production costs for the better performing systems are presented in Table 1 for each test area. The costs include setup, calibration, and demobilization efforts but not data processing, travel expenses, or costs to reacquire targets for flagging (i.e., mark for digging), as these excluded costs are highly variable. A wide range of costs due to terrain requirements are presented in Table 1; costs increased as terrain became rougher or more cluttered with brush. All costs shown are based on time, and number of personnel used (as demonstrated), and are estimated from the testing authority, not the demonstrators.

w. An estimate of site cleanup costs using a towed array system for UXO detection in the APG open field is shown in Figure 6. The system had a background alarm rate and false positive rate consistent with the best technologies demonstrated at the field. Reacquisition costs, digging costs for the false positives, and background alarms drove the overall site cleanup cost (43 percent). Thus, the need for better discrimination to reduce these numbers is evident.

TABLE 1. APPROXIMATE PRODUCTION COSTS BASED ON BEST P_d^{res}

| Test Site Area | Cost/Acre | Associated Platform |
|----------------|---------------------|-------------------------|
| APG open field | \$500 | Towed |
| YPG open field | \$700 | Sling, towed, cart |
| YPG moguls | \$900 | Sling |
| APG moguls | ^a \$1900 | ^a Sling |
| Desert extreme | \$3000 | 2-man |
| Woods | \$3200 | Sling, 2-man, hand held |

^aThis data point represents the second-best P_d score. The system with the best P_d score (32 percent above second-best) had a very high background alarm rate associated with it and took a very long time to survey. The cost would be about \$10,700 per acre.

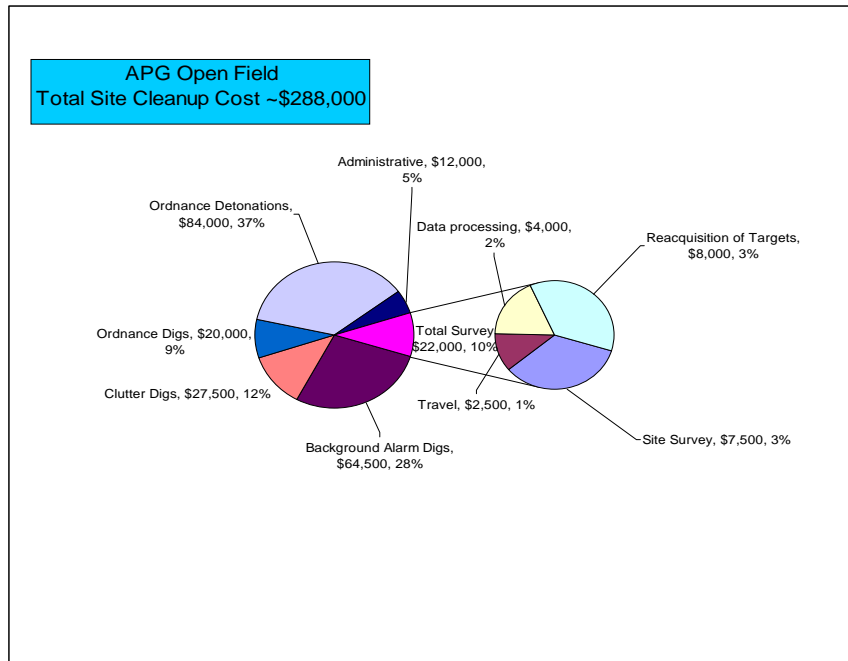


Figure 6. Total cost estimate for site cleanup.

x. Ranges of current production rates for the SOTA systems demonstrated at the sites are shown in Figure 7. The towed array systems in open field areas are leading the way for efficient use of time. Conversely, in the most extreme terrains, where man-portable units provide the only access, the best detection performance requires the most time (low production rate) in surveying. Production rates include setup, calibration, and demobilization. The rates shown will likely increase for larger site sizes as setup, calibration, and demobilization become a smaller part of overall time spent. Further, the test environment may have been somewhat more relaxed than a production environment, in which cost and time are of greater importance. The same considerations should be applied to cost estimates.

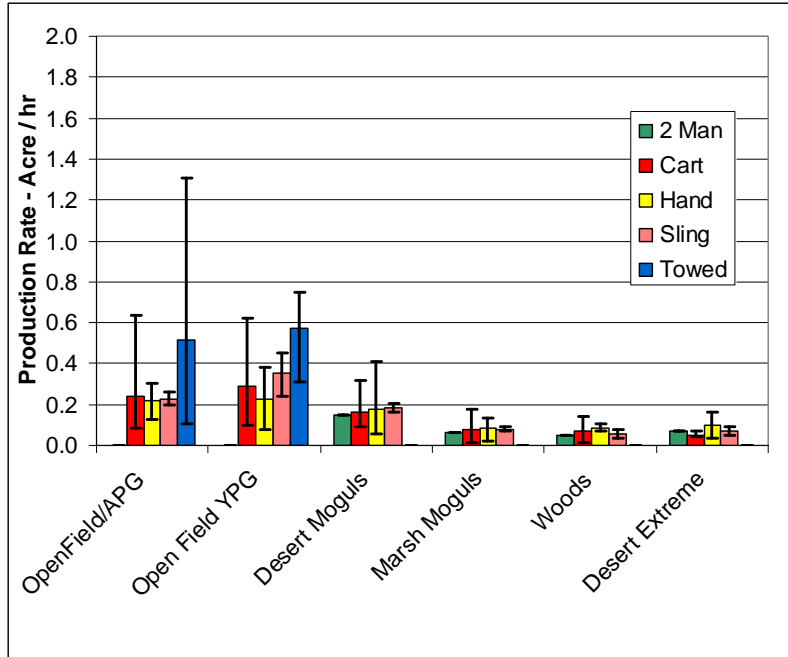


Figure 7. Production rates demonstrated at standardized sites.

y. Digital Geophysical Mapping (DGM) technology (mapping signal strength versus GPS derived location and then interpreting data) was typically used by more than 90 percent of the systems demonstrating. These systems commonly outperformed MAG and flag technology represented by two Schonstedt baseline systems. The Schonstedt systems performed well in harsh terrains and demonstrated some of the best location errors. Trade-off studies on reacquisition cost requirements for geophysical systems versus flagging systems were performed (flagging technology marks targets in real time and does not need to reacquire positions). A total cost analysis for a geophysical mapping system, as shown in Figure 6, indicated reacquisition costs were significant. However, it was found that the reacquisition costs for geophysical mapping systems were much less than the increase in dig costs from high false positive, and background alarm rates produced by a MAG and flag system (Schonstedt), in the APG open field.

z. Dual system technology first demonstrated at the standardized sites had detection rates that were near average when compared with all systems demonstrated. The fusing of data in these systems yielded performance gains when compared with constituent sensor performance from the same platform, but by a few percentage points or less. The most recent dual system brought into the sites performed well above average, and fused data results yielded significant improvement, 8 percent, over best constituent performance. Typical detection scores of SOTA dual systems are shown in Figure 8 for the APG open field. The full standard GT is used for the EM and MAG constituents, as well as the fused “dual” result, and contains both ferrous and non-ferrous items (MAG constituents can detect only ferrous items, which is why the scores are lower). This was done so the performance contributions of the parts and the whole could be

compared. It is noted that the VSEMS system shown was tested after the APG open field reconfiguration. The new field configuration is very similar to the original except that a large amount of items causing background noise were extracted. This likely contributed to the lower BAR score that the VSEMS demonstrated (see section 2.3.9.1 for further details).

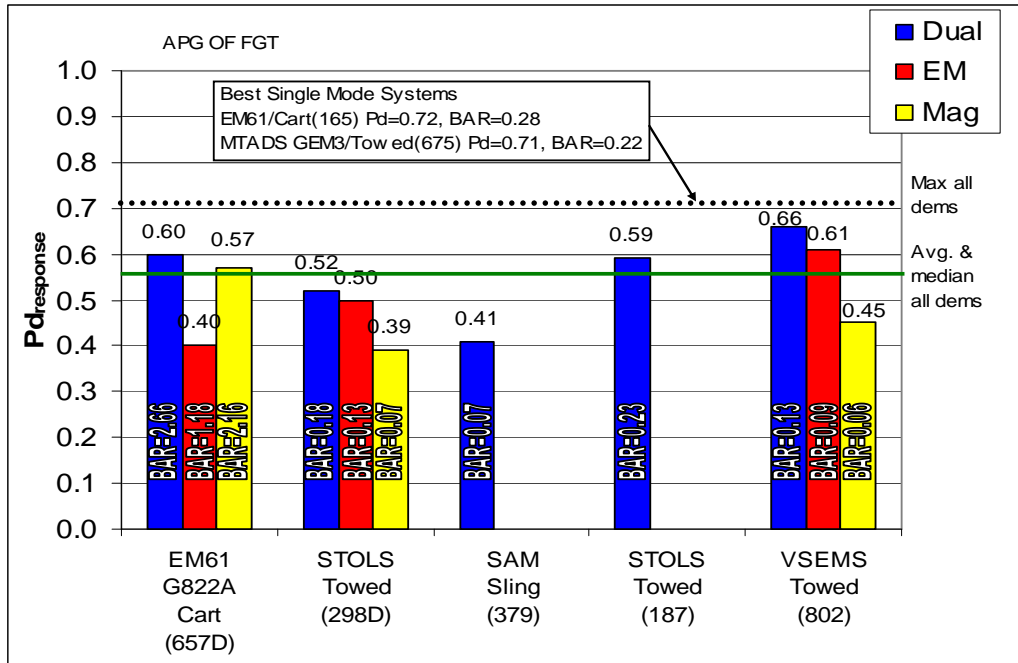


Figure 8. Dual system performance at APG open field, ferrous and non-ferrous items in GT.

aa. Data sampling trends for the detection systems demonstrated were analyzed. The purpose of the analysis was to look for a correlation between the number of data samples taken within a 0.5-meter radius (detection halo radius) of a target, versus the probability of a target's being detected. The number of samples divided by the halo area was defined as sample density. For the better performing EM systems, a well-defined trend existed between P_d^{res} and sample density. The best performer had the highest sample density. More analysis is needed with regard to parameters that drive sample density and how they relate to detecting GT at the sites for given sensor characteristics. Such trends may provide insight into design considerations or operational considerations for detection systems. More data are needed from MAG systems to establish trends.

bb. An analysis was also performed on combining dig lists from different systems to see how many systems were needed to optimize detection at a site (assuming best combinations). At the YPG open field, three systems were required before diminishing P_d^{res} gains resulted. If the GT spacing is set at a minimum of 1.5 meters, the number of systems required approached two. The best combinations were different EM systems.

1.1.3 Recommendations

a. Navigation Quality. Educate vendors on performance penalties possible when lane spacing is not rigidly maintained at the test sites. Encourage vendors to implement or improve quality checks on sensor coverage at survey sites.

b. Discrimination and Test Site.

(1) The most challenging aspect of the test sites for discrimination may be the large number of ordnance types that demonstrators are expected to handle at one time. The standardized test sites need easier GT configurations (at graduated levels of difficulty) set aside for the development of discrimination ability. More robust calibration lanes with items mimicking exact depths and orientations of items in the test areas may be helpful. Periodic releases of GT are needed from the test sites to provide demonstrators with data to refine discrimination algorithms.

(2) A possible QC would be to require real-time processing/discrimination at the test sites in the future and require resurvey of low confidence items in the discrimination stage.

c. Test Site.

(1) As the standardized test sites will have continued use, any reconfiguration efforts should strive to retain an area in which the original GT configurations are maintained so that technology advancement can be tracked in the coming years by comparative means.

(2) Implement better emplacement controls upon reconfiguration efforts at the standardized sites to ensure less positional error in the GT.

1.1.4 Conclusions

a. The SOTA UXO detection systems are currently challenged by targets close to other ordnance/clutter, by targets at depths approaching 11D and beyond, and by the smallest of munitions (20-mm projectiles). Such target distributions are site-specific; thus, the level of their occurrence in real-world cleanup sites will dictate development emphasis. When these types of targets do not exist at a survey or test site, and good QCs are in place for navigation, detection rates of 0.90 to 0.95 would be expected by the best detection technologies in a UXO field of “diverse” composition. In the same type of UXO field with only large types (>~105mm) of ordnance, probability of detection would be at or near 1.0. Detection rates may drop by as much as 30 to 40 percent in severe terrains.

b. The percentage of GT detected at a site similar to the test sites can be increased by employing additional systems to survey the site. Results from the test sites indicate that the benefits of this practice diminish past the addition of one or two systems depending on the spacing or density of the GT.

c. Geophysical mapping technology has consistently outperformed Schonstedt systems in all but the most severe of terrains. Results have demonstrated that this technology should be used when at all possible/practical.

d. Minimal discrimination ability of SOTA UXO detection systems is seen at the standardized sites. Based on cost payoffs of any discrimination ability, justification for investments in the sites to promote the development of this ability appears warranted.

e. Performance measures of detection and discrimination ability for UXO detection systems representing the SOTA were evaluated, and the results presented were based on testing performed at the standardized UXO testing sites. The standard GT composition and test metrics at the sites allowed comparative analysis of various system technologies. Insight was gained into identifying parameters affecting system performance. Possible QC issues were identified. Optimal configurations were identified. Furthermore, improvements to the test sites have been suggested on the basis of the test result findings. In summary, SOTA UXO detection technology, as demonstrated at the standardized UXO testing sites, has been characterized and evaluated on a broad but general level. Therefore, the objectives of the standardized UXO test sites have been met.

1.2 TEST OBJECTIVES

a. The objective of the Standardized UXO Technology Demonstration Site Program is to evaluate the detection and discrimination capabilities of a given technology. The evaluation is to take place under various field and soil conditions using inert munitions and clutter items positioned in various orientations and depths in the ground.

b. The evaluation objectives are as follows:

(1) To determine detection and discrimination effectiveness under realistic scenarios that vary targets, geology, clutter, topography, and vegetation.

(2) To determine cost, time, and manpower requirements to operate the technology.

(3) To determine the demonstrator's ability to analyze survey data in a timely manner and provide prioritized target lists with associated confidence levels.

(4) To provide independent site management to enable the collection of high quality, GT, geo-referenced data for post-demonstration analysis.

1.3 TESTING AUTHORITY

a. The Standardized UXO Technology Demonstration Site Program is a multiagency program spearheaded by the U.S. Army Environmental Command (USAEC). The U.S. Army Aberdeen Test Center (ATC), Aberdeen Proving Ground (APG), Maryland, and the U.S. Army Corps of Engineers Engineering Research and Development Center (ERDC) provide programmatic support. The program is funded and supported by the Environmental Security Technology Certification Program (ESTCP), the Strategic Environmental Research and Development Program (SERDP), and the Army Environmental Quality Technology Program (EQT).

b. USAEC issued a Test Execution Directive (app H, ref, 1) to ATC, APG, Maryland, to plan, perform, and report the evaluation of UXO detection technology at the Standardized UXO Test Sites, DTC Project No. 8-CO-160-UXO-021.

1.4 TEST CONCEPT

This test utilized the UXO test sites created at APG and YPG with emphasis on the demonstration and evaluation of government and private industry ordnance detection systems.

1.5 SYSTEM DESCRIPTION

a. Sensor Types.

(1) EM induction. EM sensors are typically packaged with one or more induction coils, which typically include transmitter and receiver types. When varying current is passed through the transmitter coil(s), current will be induced in any metallic object nearby. The nearby metallic objects will therefore change the inductance of the coils in the sensor. Mutual induction between the receiver and transmitter coils is often determined by sending large pulses of current through the transmitter coils and then measuring the electric potential induced in the receiver coil as a function of time. Another method is to measure the electric potential induced in the receiver coil as a function of frequency while alternating current (AC) at several frequencies is passed through the transmitter coil. EM sensors not only detect all metallic objects, but they can also begin to measure material properties such as the conductivity of buried objects. By mapping the measurements of an EM system as a function of location, it is possible to estimate the depth and some geometric parameters of any metallic object that is buried in the ground.

(2) MAG. MAGs utilize the characteristic of most UXO items being made with iron (ferromagnetic material). MAGs passively measure the magnitude of the magnetic field around an item as a function of location over the area to be surveyed. By taking into account the magnetic field of the earth, the magnetic field of ferromagnetic items buried in the ground can be calculated. There are numerous ways a MAG can measure a magnetic field in a given direction. One popular method is to measure the optical transmissivity of a chamber filled with a gas whose absorption coefficient varies as a function of the applied magnetic field. Another popular method is to build an inductor around a material whose magnetic permeability varies as a function of the total applied magnetic field. MAG systems typically consist of at least three

devices measuring the magnitude of the magnetic field in different directions so that the total magnitude and direction of the magnetic field vector can be accurately measured. By measuring the magnitude of the magnetic field as a function of location, it is possible to estimate the depth and shape of any ferromagnetic item buried in the ground.

(3) Dual mode. As both EM and MAG sensors have advantages and disadvantages, it is often advisable to survey a site using both sensor types. It would save time and money to conduct both surveys simultaneously by mounting EM and MAG sensors on the same platform. Such an arrangement must overcome the fact that the magnetic field induced by the EM sensor's transmitter coils will interfere with the MAG sensor's measurements. However, system designers have produced several methods to overcome this limitation. One method is to synchronize the MAG measurements with the pulses sent through the transmitter coil of the EM sensor so that the effects of the EM sensor can be taken into account. Another method is to mount the MAG sensor in locations near the EM sensor where the magnetic field produced by the transmitter coils is minimized. Such dual mode systems are designed so that they combine the advantages of both the EM and MAG sensors.

(4) Ground-penetrating radar (GPR). GPR systems work by transmitting electromagnetic radiation into the ground (frequency ranges are typically between 50 and 700 MHz). This radiation will bounce off of any metallic object buried in the ground or any dielectric discontinuity and then return to the surface. By analyzing the signal that returns from the ground, GPR systems can estimate the size, shape, and depth of the objects that are buried.

b. Platforms. Depending on the size of the sensors, performance considerations, and the terrain to be surveyed, it becomes necessary to configure UXO detection systems in many different ways. The platforms on which sensors are mounted can affect accessibility, ease of navigation, and, ultimately, detection performance. The platforms of the systems that have surveyed the Standardized UXO Test Sites are classified based on their architecture. Below is a list of the different platform types that have surveyed the sites:

(1) "Hand held" platforms are small enough for a single person to carry the detection system. Although some operators may attach these platforms to their body, the platforms are small enough that this is unnecessary. They can be operated by holding them with hands alone.

(2) "Sling" platforms are small enough to be carried by a single person but are large enough that it is not possible to carry them without attaching them to the operator's body with a sling or some other device.

(3) "2-man" platforms are small enough to be carried by hand but large enough to require more than one person. Only one type has been used at the sites to date and is more properly referred to as a "litter" platform (resembling a rigid hospital stretcher).

(4) "Cart" or "pushcart" platforms are large enough to require wheels to support the size or weight of the system but small enough that the operator can still push or pull the detection system without the need of a vehicle.

(5) “Towed” (often referred to as “towed array”) platforms are so large that they must be towed using some type of vehicle. Usually, multiple sensors (typically in an array) drive the size requirement.

c. Some systems have separate data processing units connected by a cable to the survey platform and carried by an individual. The above definitions refer only to the platform carrying the sensors.

d. Systems that can be carried are also typically designated as “man-portable” systems. Thus, the three general types of platforms used are man-portable, cart, and towed platforms.

SECTION 2. SUBTESTS

2.1 STANDARDIZED UXO TEST AND EVALUATION PROGRAM

2.1.1 Introduction

a. Technologies under development for the detection and discrimination of munitions and explosives of concern (MEC) (i.e., unexploded ordnance (UXO) and discarded military munitions (DMM)) require testing to characterize performance. To that end, Standardized Test Sites were developed at APG and U.S. Army Yuma Proving Ground (YPG), Arizona. The test sites provide diversity in geology, climate, terrain, and weather as well as in ordnance and clutter. Testing at the sites was independently administered and analyzed by the government to characterize technologies, track performance with system development, and compare performance of different systems in different environments. Daily weather logs were maintained and are provided in Appendix B.

b. The Standardized UXO Technology Demonstration Site Program is a multiagency program spearheaded by the USAEC. ATC and ERDC provide programmatic support. The program is funded and supported by ESTCP, SERDP, and EQT.

2.1.2 Test Site Description

Tests were performed at APG and YPG. Each test center contains one calibration area and four test areas for evaluating UXO detection systems. The APG and YPG sites are shown in Figures 2.1-1 and 2.1-2. Descriptions of the test sites are presented in Tables 2.1-1 and 2.1-2.



Figure 2.1-1. Layout of the APG UXO test site.

TABLE 2.1-1. APG TEST SITE AREAS

| Area | Description |
|------------------|--|
| Calibration grid | Contains 14 standard ordnance items buried in six positions at various angles and depths to allow demonstrator to calibrate their equipment. |
| Blind grid | Contains 400 grid cells in a 0.48-acre site. The center of each grid cell contains ordnance, clutter, or nothing. |
| Open field | A 13.68-acre site containing open areas, dips, ruts, and obstructions that challenge platform systems or hand held detectors. The challenges include a gravel road, wet areas, and trees. The vegetation height varies from 15 to 25 cm. |
| Woods | 1.35-acre area consisting of cleared woods (tree removal with only stumps remaining), partially cleared woods (including all underbrush and fallen trees), and virgin woods (i.e., woods in natural state with all trees, underbrush, and fallen trees left in place). |
| Mogul | A 1.30-acre area consisting of two areas (the rectangular or driving portion of the course and the triangular section with more difficult, non-drivable terrain). A series of craters (as deep as 0.91 m) and mounds (as high as 0.91 m) encompass this section. |

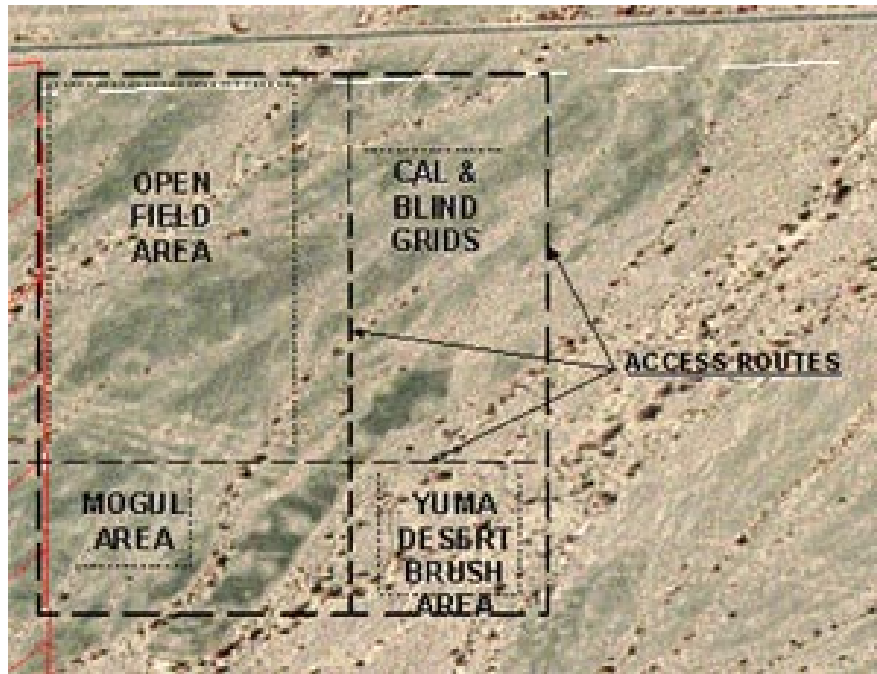


Figure 2.1-2. Layout of the YPG UXO test site.

TABLE 2.1-2. YPG TEST SITE AREAS

| Area | Description |
|------------------|--|
| Calibration grid | Contains the 15 standard ordnance items buried in six positions at various angles and depths to allow demonstrator equipment calibration. |
| Blind grid | Contains 400 grid cells in a 0.43-acre site. The center of each grid cell contains ordnance, clutter, or nothing. |
| Open field | A 15.38-acre site containing open areas, dips, ruts, and obstructions, including vegetation. |
| Desert extreme | A 1.23-acre area consisting of a sequence of man-made depressions, covered with desert-type vegetation. |
| Mogul | A 2.64-acre area consisting of two areas (the rectangular or driving portion of the course and the triangular section with more difficult, non-drivable terrain). A series of craters (as deep as 0.91 m) and trenches (as deep as 0.91 m) encompass this section. |

2.1.3 Scoring Methodology

a. Terms and definitions relevant to scoring can be found in Appendix A. The appendix is an excerpt from The Standardized UXO Technology Demonstration Site Scoring Records that are produced and published by ATC. The following paragraphs are a summary of metrics from the appendix that are most relevant to analysis performed in this report.

b. Scoring in its most basic form requires the understanding of three definitions, which are:

(1) Ground Truth (GT) - Represents a set of items buried (emplaced) by the test authority at known locations, depths, and orientations in a given test area. The GT comprises both ordnance (submunitions, grenades, mortars, and projectiles) and clutter (scrap steel) items.

(2) Anomaly - Location of a response (signal) from a detection system deemed to warrant further investigation by the demonstrator for consideration as an emplaced ordnance item.

(3) Detection Radius or Halo Radius - The radius about the center of a ground truth item which traces out a detection circle or halo. An anomaly within this radius is considered a detection. This radius is set at 0.5 meter at the standardized sites. For ordnance items that are greater than 0.6 meter long, an elliptical halo is used. The minor axis of the halo is 1 meter wide and the major axis is the length of the ordnance projected onto the horizontal plane plus 1 meter (0.5 m on each end).

c. A demonstrator will submit a diglist of anomalies to the test authority for scoring. The list will typically contain “response stage” data, which include location coordinates and signal strengths from anomalies in a given test area. When the scoring committee processes the list it counts the number of ordnance and clutter items in the GT with anomalies located within their halos. These numbers are respectively divided by the total number of ordnance and clutter in the GT for the area. The result is P_d^{res} (probability of detection in the response stage or fraction of overall ordnance detected) and $P_{\text{fp}}^{\text{res}}$ (probability of false positive in the response stage or fraction of overall clutter detected).

d. All anomalies outside of halos are considered background alarms (similar to false alarms). The total number of background alarms is divided by a constant (known only by the scoring committee) proportional to the test area size and the resulting metric is termed BAR^{res} (background alarm rate in the response stage). Since the constant used in the calculation is unknown, BAR^{res} can only be used as a relative means of comparing background alarm rates between areas or between systems.

e. Based on the configuration of the GT at the standardized sites and the defined scoring methodology; there exists the possibility of having anomalies within the overlaps of halos and/or multiple anomalies within a single halo. Overlaps typically occur in dense areas of GT called “clusters” where items are closer than one meter to each other. The challenge to score such areas is whether to consider an anomaly representing the combined signals of multiple items as a detection of all GT items involved or to allow only one anomaly to be associated with one GT item (closest to the anomaly) in the cluster. The former approach is a legitimate means of detecting multiple items. The latter approach has been used to date in scoring reports from the sites and is used in this report. This approach provides a measure of how well individual items can be “discerned” in such difficult areas. It can be argued that the drawback of the approach is that a system may not be able to discern many items in a cluster, consequently getting a low Pd, but it may very well be detecting all of the items, through one combined signal, and therefore the Pd is misrepresentative. Further, it can be argued that cluster results should be separate, regardless of scoring approach, because they bias the measurement of true ability to detect an

individual ordnance item (this problem is addressed in this report by creating an alternate GT set which does not include overlapping items, i.e. closer than one meter to each other). The following scoring logic is implemented for overlaps and multiple anomalies:

(1) When multiple anomalies exist within a single halo, the anomaly with the strongest response is assigned to that particular GT item (smallest distance from GT item is used if strengths are equal).

(2) For overlapping halo situations, ordnance has precedence over clutter (anomalies are first matched with ordnance, remaining anomalies are matched with clutter). The anomaly with the strongest response is first assigned to a GT item (smallest distance from GT item is used next). Remaining anomalies are retained until all matching is complete.

(3) If anomalies remain “within” halos after matching is complete they are thrown out (one anomaly allowed per GT item) and are not considered in the analysis. In a sense they are considered redundant (target halo they are in has already been detected).

f. The scoring methodology for the blind grids is slightly different. There are no “halos,” only one meter square grid cells. The grid cells contain either ordnance, clutter or are empty. If a cell contains an emplaced item, that item is located at the center of the cell. The demonstrators submit a list of cell addresses and indicate a response level for each cell. They also submit a threshold response value. Any response values above this threshold are considered anomalies and any at or below are considered noise (empty cell). If an anomaly exists in a cell with an emplaced GT item, the item is considered detected. Knowing the total number of ordnance and clutter emplaced in a grid, P_d^{res} and P_{fp}^{res} can be calculated. The background alarm metric for the grids is P_{ba}^{res} and is the total number of empty cells with anomalies in them divided by the total number of empty cells (or the fraction of total empty cells which were indicated “not” to be empty).

g. Demonstrators not only provide anomaly signal strengths and locations but they also provide a ranking of how likely any given anomaly is an ordnance item (higher number equals greater confidence level). This ranking may be based on algorithms or human judgment. A threshold ranking value is provided by the demonstrator above which it is believed all ordnance items are included. The scoring committee scores the list in what is termed “discrimination stage” processing.

h. In the discrimination stage, P_d is calculated again based on the number of detected ordnance in the dig list that are above the discrimination threshold value. The result is P_d^{disc} , which is the fraction of total ordnance in a testing area that have been detected and correctly identified.

i. P_{fp} is also calculated again counting all detected clutter items above the discrimination threshold value (clutter being called ordnance) and dividing by the total number of clutter. The result is, P_{fp}^{disc} , which is the fraction of total clutter in a test area that have been detected and called ordnance.

j. Background alarm metrics are calculated in a similar manner as above, counting all anomalies above the discrimination threshold for which no ordnance or clutter can be associated. This number is divided by the same constant as in the response stage to find BAR^{disc} . In the grids, the number of empty cells with anomaly rankings above the discrimination threshold is divided by the total number of empty cells to find a background alarm probability or P_{ba}^{disc} . P_{ba}^{disc} is the fraction of total empty cells in which it has been indicated that ordnance resides after discriminating.

k. Systems are also scored on EFFICIENCY (E) and REJECTION RATIOS (R_{fp} & R_{ba}), which measure the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of ordnance detections from the anomaly list while rejecting the maximum number of anomalies arising from non-ordnance items. E measures the fraction of detected ordnance (response stage) retained after discrimination while R_{fp} and R_{ba} measure the fraction of false positives and background alarms from the response stage that have been rejected. Optimum scores for these metrics are 1.0 (indicating 100 percent retention of ordnance and 100 percent rejection of false positives and background alarms after discriminating).

2.1.4. Description of Ordnance

Typical ordnance items embedded throughout the UXO test sites are shown in Figures 2.1-3 through 2.1-18. All ordnance together, with the exception of the 500-pound bomb and the M75 submunition (these two types are buried at limited test areas), is shown in Figure 2.1-19. A description of these ordnance items, as well as additional embedded clutter is presented in Table 2.1-3.



Figure 2.1-3. CTG, 81-mm, M374, mortar inert with fuze.



Figure 2.1-4. CTG, 60-mm, M49, mortar inert with fuze.



Figure 2.1-5. Projectile, 57-mm, inert.



Figure 2.1-6. Bomb, Mark (MK) 118 rockeye, submunition, inert (with plastic fin).



Figure 2.1-7. Bomb, BLU 26, inert submunition.



Figure 2.1-8. Warhead (WHD), M230 inert projectile for 2.75-inch rocket with inert fuze.



Figure 2.1-9. Projectile, 105-mm, HEAT, M456 A1, inert.



Figure 2.1-10. Projectile, 105-mm, M603, inert.



Figure 2.1-11. Bomb, inert submunition, BDU 28.



Figure 2.1-12. Projectile, 155-mm, M483A1, inert.



Figure 2.1-13. Projectile, 40-mm, MKII, inert.



Figure 2.1-14. Projectile, 20-mm, M55, inert.



Figure 2.1-15. Grenade, 40-mm, M385 inert.



Figure 2.1-16. Bomb, M42, submunition, inert.



Figure 2.1-17. Bomb, M75, submunition, inert (found only at YPG).



Figure 2.1-18. Bomb, 500-pound, inert.



Figure 2.1-19. Composite of ordnance items.

TABLE 2.1-3. MUNITION TARGETS

| Type | Nomenclature | Length, mm | Width, mm | Aspect Ratio | Weight, lb | Description | Size |
|--------|------------------|------------|-----------|--------------|------------|--|------|
| 20MM | 20MM M55 | 25 | 20 | 1.25 | 0.25 | The projectile is composed of alloy steel and has a small copper-rotating band. | S |
| 40MM | 40MM MK II | 179 | 40 | 4.48 | 1.55 | The thin-walled projectile is composed of steel. The projectile nose is internally threaded to receive the fuze. The projectile is assembled with either a brass or steel cartridge case containing a percussion primer that is crimped to the projectile by means of a 360° crimp. There is a thin copper-rotating band affixed at the base of the munitions. | S |
| 40MM | 40MM M385 | 80 | 40 | 2 | 0.55 | The cartridge is a fixed round of ammunition. It consists of a one-piece solid inert aluminum projectile body together with a copper-rotating band that is press-fitted into an aluminum bichambered cartridge case assembly. The chamber is sealed at the bottom with an aluminum base plug that is crimped to the base of the cartridge case. | S |
| M42 | SUBMUNITION | 62 | 40 | 1.55 | 0.35 | The projectile is composed of steel. | S |
| BDU-26 | SUBMUNITION | 66 | 66 | 1 | 0.95 | This item is composed of ferrous metal. | S |
| BDU-28 | SUBMUNITION | 97 | 67 | 1.45 | 1.7 | This item is composed of ferrous metal. | S |
| 57MM | 57MM M86 | 170 | 57 | 2.98 | 6 | The projectile is composed of steel and has a thin copper-rotating band affixed at the base of the munitions. | M |
| MK118 | MK118 ROCKEYE | 344 | 50 | 6.88 | 1.35 | This item is composed of cast aluminum with a thin ferrous ring. | M |
| 60MM | 60MM M49A3 | 243 | 60 | 4.05 | 2.9 | The projectile body is of pearlitic malleable iron/forged steel and is threaded internally at the nose to accept the fuze and at the base to accept the fin assembly. | M |
| 81MM | 81MM M374 | 480 | 81 | 5.93 | 8.75 | The projectile body is of pearlitic malleable iron/forged steel and is threaded internally at the nose to accept the fuze and at the base to accept the fin assembly. | M |

TABLE 2.1-3 (CONT'D)

| Type | Nomenclature | Length, mm | Width, mm | Aspect Ratio | Weight, lb | Description | Size |
|--------|--------------|---------------|--------------|-----------------|---------------|---|------|
| M230 | 2.75" ROCKET | 761 | 75 | 10.15 | 18.2 | The warhead consists of two main parts, a nose and a base, brazed together. The nose section is threaded to receive e fuze. The base is made of steel or cast iron and is threaded for the attachment to rocket motor. | M |
| 105MM | M456 HEAT RD | 640 | 105 | 6.1 | 19.65 | The forged steel body projectile is fitted with a plastic obturator, a threaded standoff spike assembly, a fin and boom assembly, and a point-initiating point-detonating fuze. There is a thin copper-rotating band affixed at the base of the munitions item. | L |
| 105MM | 105MM M60 | 426 | 105 | 4.06 | 28.35 | The projectile consists of forged hollow steel forging with a boat tail base, a streamlined ogive, and copper-rotating band. A steel nose adapter is threaded into the nose of the projectile providing a seal for the filler. | L |
| 155MM | 155MM M483A1 | 870 | 155 | 5.61 | 56.45 | The projectile is composed of forged steel/aluminum with a thin copper-rotating band affixed at the base of the munitions. | L |
| 500 LB | BOMB | 1680 | 273 | .163 | 500 | Cast iron, cylinder hollow. | L |
| M75 | SUBMUNITION | 69 | 64 | .928 | 1.19 | Steel. | S |

2.2 SYSTEMS TESTED

Various detection systems were demonstrated at both APG and YPG. A complete list of the systems tested is presented in Table 2.2-1. The table shows each system's test dates, demonstrator, areas surveyed, report numbers, basic sensor type, sensor technology (system name also included in parenthesis where applicable), and platform type. Detailed information about configurations can be found in the published reports on the Web at <http://aec.army.mil/usaec/technology/uxo03f.html>. Environmental conditions such as weather and soil moisture content are included in Appendixes B and C. Test logs (time, estimated costs) for each test are presented in Appendix D.

TABLE 2.2-1. SYSTEM/DEMONSTRATOR TEST

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | |
|---|---------------------|---------------------------------|---------------|------------------------|-----------------|
| Demo. Date | Demonstrator | Surveyed Area/(Rep. No.) | Sensor | Technology | Platform |
| Oct. 2002 | AETC | Blind Grid (39) | EM | EM61 | hand |
| Apr. 2005 | ARM | Blind Grid (695) | EM | Explorer II | hand |
| Apr. 2005 | ARM | Blind Grid (691) | EM | F3 | hand |
| Sep. 2004 | BH | Blind Grid (622) | Dual | EM61MKII G822A | cart |
| Sep. 2004 | BH | Moguls (642) | Dual | EM61MKII G822A | cart |
| Sep. 2004 | BH | Open Field (657) | Dual | EM61MKII G822A | cart |
| Sep. 2004 | BH | Woods (636) | Dual | EM61MKII G822A | cart |
| Apr. 2004 | ERDC | Blind Grid (304) | EM | EM63 | cart |
| Apr. 2004 | ERDC | Open Field (305) | EM | EM63 | cart |
| Sep. 2003 | ERDC | Blind Grid (142) | EM | GEM-3 | cart |
| Sep. 2003 | ERDC | Blind Grid (141) | EM | GEM-3 | cart |
| Oct. 2002 | Geocenters | Blind Grid (40) | Dual | EM61MKI G822A (STOLS) | towed |
| Aug. 2004 | Geocenters | Blind Grid (290) | Dual | EM61MKI G822A (STOLS) | towed |
| Oct. 2002 | Geocenters | Open Field (187) | Dual | EM61MKI G822A (STOLS) | towed |
| Aug. 2004 | Geocenters | Open Field (298) | Dual | EM61MKI G822A (STOLS) | towed |
| Apr. 2006 | Geocenters | Blind Grid (792) | Dual | EM61MKII G822A (VSEMS) | towed |
| Feb. 2006 | Geocenters | Open Field (802) | Dual | EM61MKII G822A (VSEMS) | towed |
| May. 2003 | Geophex | Blind Grid (50) | EM | GEM-3 | hand |
| Apr. 2005 | Geophex | Blind Grid (680) | EM | GEM-3 | hand |
| May. 2003 | Geophex | Blind Grid (125) | EM | GEM-3 | towed |
| May. 2003 | Geophex | Blind Grid (49) | EM | GEM-3 | cart |
| May. 2003 | Geophex | Moguls (451) | EM | GEM-3 | cart |
| Apr. 2005 | Geophex | Moguls (665) | EM | GEM-3 | hand |
| May. 2003 | Geophex | Open Field (129) | EM | GEM-3 | towed |
| May. 2003 | Geophex | Woods (449) | EM | GEM-3 | cart |
| Apr. 2005 | Geophex | Blind Grid (694) | EM | GEM-5 | cart |
| Oct. 2005 | Geophex | Blind Grid (739) | EM | GEM-5 | towed |
| Apr. 2005 | Geophex | Blind Grid (693) | EM | GEM-5 | cart |
| Oct. 2005 | Geophex | Open Field (740) | EM | GEM-5 | towed |
| Oct. 2003 | G-TEK | Blind Grid (184) | EM | TM-5 | hand |
| Oct. 2003 | G-TEK | Blind Grid (183) | EM | TM-5 | sling |
| Oct. 2003 | G-TEK | Mine Grid (146) | EM | TM-5 | sling |
| Oct. 2003 | G-TEK | Moguls (545) | EM | TM-5 | sling |

TABLE 2.2-1 (CONT'D)

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | |
|---|---------------------|---------------------------------|---------------|--------------------|-----------------|
| Demo. Date | Demonstrator | Surveyed Area/(Rep. No.) | Sensor | Technology | Platform |
| Oct. 2003 | G-TEK | Open Field (154) | EM | TM-5 | sling |
| Oct. 2003 | G-TEK | Woods (452) | EM | TM-5 | hand |
| Oct. 2003 | G-TEK | Blind Grid (268) | MAG | TM-4 | sling |
| Oct. 2003 | G-TEK | Moguls (547) | MAG | TM-4 | sling |
| Oct. 2003 | G-TEK | Open Field (311) | MAG | TM-4 | sling |
| Oct. 2003 | G-TEK | Woods (454) | MAG | TM-4 | sling |
| Jun. 2004 | G-TEK | Blind Grid (281) | Dual | GGT-10 G822A (SAM) | sling |
| May. 2004 | G-TEK | Moguls (380) | Dual | GGT-10 G822A (SAM) | sling |
| May. 2004 | G-TEK | Open Field (379) | Dual | GGT-10 G822A (SAM) | sling |
| Apr. 2004 | G-TEK | Woods (381) | Dual | GGT-10 G822A (SAM) | sling |
| Jul. 2004 | HFA | Blind Grid (237) | MAG | Schonstedt | hand |
| Jul. 2004 | HFA | Moguls (676) | MAG | Schonstedt | hand |
| Jul. 2004 | HFA | Open Field (231) | MAG | Schonstedt | hand |
| Jul. 2004 | HFA | Woods (486) | MAG | Schonstedt | hand |
| Aug. 2004 | NAEVA | Mine Grid (647) | EM | EM61MKII | towed |
| Aug. 2004 | NAEVA | Blind Grid (396) | EM | EM61MKII | 2man |
| Aug. 2004 | NAEVA | Blind Grid (397) | EM | EM61MKII | towed |
| Sep. 2004 | NAEVA | Moguls (597) | EM | EM61MKII | 2man |
| Aug. 2004 | NAEVA | Open Field (406) | EM | EM61MKII | towed |
| Aug. 2004 | NAEVA | Woods (494) | EM | EM61MKII | 2man |
| Sep. 2003 | NRL | Blind Grid (127) | EM | GEM3 (MTADS) | towed |
| Jun. 2004 | NRL | Open Field (675) | EM | GEM3 (MTADS) | towed |
| Jun. 2004 | NRL | Blind Grid (671) | MAG | G822ROV (MTADS) | towed |
| Jun. 2004 | NRL | Open Field (673) | MAG | G822ROV (MTADS) | towed |
| Oct. 2004 | Parsons | Blind Grid (252) | EM | EM61MKII | cart |
| Oct. 2004 | Parsons | Moguls (572) | EM | EM61MKII | cart |
| Oct. 2004 | Parsons | Open Field (411) | EM | EM61MKII | cart |
| Oct. 2004 | Parsons | Woods (496) | EM | EM61MKII | cart |
| Oct. 2004 | Parsons | Blind Grid (257) | MAG | Schonstedt | hand |
| Oct. 2004 | Parsons | Moguls (573) | MAG | Schonstedt | hand |
| Oct. 2004 | Parsons | Open Field (229) | MAG | Schonstedt | hand |
| Oct. 2004 | Parsons | Woods (499) | MAG | Schonstedt | hand |
| Dec. 2003 | Shaw | Blind Grid (197) | EM | EM61MKII | cart |
| Dec. 2003 | Shaw | Moguls (552) | EM | EM61MKII | cart |
| Dec. 2003 | Shaw | Open Field (201) | EM | EM61MKII | cart |
| Dec. 2003 | Shaw | Woods (461) | EM | EM61MKII | cart |
| Dec. 2003 | Shaw | Blind Grid (198) | MAG | MAG858 | cart |
| Dec. 2003 | Shaw | Blind Grid (404) | MAG | MAG858 | cart |
| Dec. 2003 | Shaw | Moguls (206) | MAG | MAG858 | cart |
| Dec. 2003 | Shaw | Open Field (492) | MAG | MAG858 | cart |
| Dec. 2003 | Shaw | Woods (376) | MAG | MAG858 | cart |
| Nov. 2003 | TTF | Blind Grid (157) | EM | EM61MKII | cart |
| Nov. 2003 | TTF | Blind Grid (159) | EM | EM61MKII | sling |
| Nov. 2003 | TTF | Moguls (549) | EM | EM61MKII | sling |
| Nov. 2003 | TTF | Open Field (165) | EM | EM61MKII | cart |
| Nov. 2003 | TTF | Woods (457) | EM | EM61MKII | sling |
| Jan. 2006 | VF Warner | Blind Grid (764) | EM | AMOS | towed |
| Dec. 2002 | Witten | Blind Grid (45) | GPR | Cart | cart |
| Dec. 2002 | Witten | Mine Grid (126) | GPR | Cart | cart |

TABLE 2.2-1 (CONT'D)

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | |
|---|---------------------|---------------------------------|---------------|-----------------------|-----------------|
| Demo. Date | Demonstrator | Surveyed Area/(Rep. No.) | Sensor | Technology | Platform |
| Aug. 2002 | Zonge | Blind Grid (37) | EM | EM FAST4D | cart |
| Aug. 2002 | Zonge | Open Field (38) | EM | EM FAST4D | cart |
| <i>Yuma Proving Ground Demonstrations</i> | | | | | |
| May. 2004 | BH | Blind Grid (383) | Dual | EM61MKII G822A | cart |
| May. 2004 | BH | Desert Ext (607) | Dual | EM61MKII G822A | cart |
| May. 2004 | BH | Moguls (655) | Dual | EM61MKII G822A | cart |
| May. 2004 | BH | Open Field (651) | Dual | EM61MKII G822A | towed |
| May. 2003 | ERDC | Blind Grid (216) | EM | EM63 | cart |
| May. 2003 | ERDC | Open Field (249) | EM | EM63 | cart |
| May. 2003 | ERDC | Blind Grid (134) | EM | GEM-3 | cart |
| May. 2003 | ERDC | Desert Ext (509) | EM | GEM-3 | cart |
| May. 2003 | ERDC | Moguls (136) | EM | GEM-3 | cart |
| May. 2003 | ERDC | Open Field (135) | EM | GEM-3 | cart |
| May. 2003 | ERDC | Blind Grid (362) | MAG | TM-4 | sling |
| May. 2003 | ERDC | Desert Ext (544) | MAG | TM-4 | sling |
| May. 2003 | ERDC | Moguls (571) | MAG | TM-4 | sling |
| May. 2003 | ERDC | Open Field (364) | MAG | TM-4 | sling |
| Feb. 2006 | Forester | Blind Grid (769) | MAG | FEREX | Sling |
| Feb. 2006 | Forester | Open Field (770) | MAG | FEREX | Sling |
| Oct. 2004 | Geocenters | Blind Grid (293) | Dual | EM61MKI G822A (STOLS) | towed |
| Oct. 2004 | Geocenters | Open Field (299) | Dual | EM61MKI G822A (STOLS) | towed |
| Oct. 2003 | G-TEK | Blind Grid (186) | EM | TM-5 | hand |
| Oct. 2003 | G-TEK | Desert Ext (144) | EM | TM-5 | sling |
| Oct. 2003 | G-TEK | Moguls (579) | EM | TM-5 | sling |
| Oct. 2003 | G-TEK | Open Field (148) | EM | TM-5 | sling |
| Oct. 2003 | G-TEK | Blind Grid (431) | MAG | TM-4 | sling |
| Oct. 2003 | G-TEK | Desert Ext (536) | MAG | TM-4 | sling |
| Oct. 2003 | G-TEK | Moguls (581) | MAG | TM-4 | sling |
| Oct. 2003 | G-TEK | Open Field (147) | MAG | TM-4 | sling |
| Apr. 2004 | HFA | Blind Grid (238) | MAG | Schonstedt | hand |
| Apr. 2004 | HFA | Desert Ext (528) | MAG | Schonstedt | hand |
| Jul. 2004 | HFA | Moguls (587) | MAG | Schonstedt | hand |
| Apr. 2004 | HFA | Open Field (442) | MAG | Schonstedt | hand |
| Dec. 2004 | NAEVA | Blind Grid (667) | EM | EM61MKII | towed |
| Dec. 2004 | NAEVA | Blind Grid (666) | EM | EM61MKII | 2man |
| Dec. 2004 | NAEVA | Desert Ext (670) | EM | EM61MKII | 2man |
| Dec. 2004 | NAEVA | Moguls (669) | EM | EM61MKII | 2man |
| Dec. 2004 | NAEVA | Open Field (668) | EM | EM61MKII | towed |
| Nov. 2003 | NRL | Blind Grid (213) | EM | GEM3 (MTADS) | towed |
| Nov. 2003 | NRL | Open Field (245) | EM | GEM3 (MTADS) | towed |
| Sep. 2004 | Parsons | Blind Grid (690) | EM | EM61MKII | cart |
| Sep. 2004 | Parsons | Desert Ext (532) | EM | EM61MKII | cart |
| Sep. 2004 | Parsons | Moguls (588) | EM | EM61MKII | cart |
| Sep. 2004 | Parsons | Open Field (425) | EM | EM61MKII | cart |
| Sep. 2004 | Parsons | Blind Grid (606) | MAG | Schonstedt | hand |
| Sep. 2004 | Parsons | Desert Ext (601) | MAG | Schonstedt | hand |
| Sep. 2004 | Parsons | Moguls (602) | MAG | Schonstedt | hand |

TABLE 2.2-1 (CONT'D)

| <i>Yuma Proving Ground Demonstrations</i> | | | | | |
|---|---------------------|---------------------------------|---------------|-------------------|-----------------|
| Demo. Date | Demonstrator | Surveyed Area/(Rep. No.) | Sensor | Technology | Platform |
| Sep. 2004 | Parsons | Open Field (426) | MAG | Schonstedt | hand |
| Jan. 2003 | Shaw | Blind Grid (199) | EM | EM61MKII | cart |
| Jan. 2003 | Shaw | Desert Ext (211) | EM | EM61MKII | cart |
| Jan. 2003 | Shaw | Moguls (207) | EM | EM61MKII | cart |
| Jan. 2003 | Shaw | Open Field (354) | EM | EM61MKII | cart |
| Jan. 2003 | Shaw | Blind Grid (312) | MAG | MAG858 | cart |
| Jan. 2003 | Shaw | Desert Ext (541) | MAG | MAG858 | cart |
| Jan. 2003 | Shaw | Moguls (594) | MAG | MAG858 | cart |
| Jan. 2003 | Shaw | Open Field (638) | MAG | MAG858 | cart |
| Dec. 2003 | TTF | Blind Grid (168) | EM | EM61MKII | cart |
| Dec. 2003 | TTF | Desert Ext (171) | EM | EM61MKII | cart |
| Dec. 2003 | TTF | Moguls (170) | EM | EM61MKII | sling |
| Dec. 2003 | TTF | Open Field (169) | EM | EM61MKII | cart |
| May. 2006 | USGS | Blind Grid (805) | EM | All TEM | towed |
| May. 2006 | USGS | Blind Grid (806) | MAG | TMGS | towed |

2.3 SYSTEM PERFORMANCE

2.3.1 Introduction

a. The following sections will present measures of performance for those detection systems demonstrated at the Standardized UXO Test Sites from the beginning of testing through the summer of 2006. The results are presented at a general level yet cover a broad spectrum of metrics. Because of time constraints associated with examining a large number of test parameters, which include variables associated with GT, system characteristics, and performance measures, discussion will be limited. Trends presented and analyzed will provide a snapshot of SOTA UXO detection capability.

b. All results that are presented should be understood to be those associated with a “test instance” that is characteristically unique. If tests were to be repeated, results would change. This change would be caused by but not limited to variations in environment, system health, human error, and human judgment. Because of expected variation in results, when best performers are mentioned or systems are ranked in any way, it should be understood to be pertaining to the one test instance the systems were demonstrated at.

c. The standardized sites are unique in configuration. While the standardized sites contain a variety of ordnance common to remediated sites, with depth distributions that are similar, the sites do not match the distribution of ordnance at any particular site. Varying the distribution of ordnance and clutter will cause detection results to vary to differing degrees from system to system. Therefore, any rankings noted or observed in this report are unique to the standardized sites and may change significantly for a real world site with its own distribution of clutter and ordnance at varied depths. Nonetheless, the standardized sites contain several thousand ordnance/clutter items and because of the quantity/variety of items they contain, they provide an outstanding tool to evaluate UXO detection technology in general.

d. Most data presentations will refer to a system using three descriptive fields. The first will include the sensor type or designator, the second will describe the platform type and the third will give a report number. If a system comprises dual sensor types, the report number will usually be followed by an E (EM), M (MAG), or D (dual) to indicate non-fused and fused results (note that E and M constituents of a dual system are not necessarily optimized for independent use). The report numbers can be used to find detailed information about a system by going to the Standardized UXO website (<http://aec.army.mil/usaec/technology/uxo03.html>) and clicking on the report number. The report number can also be correlated with detailed information presented in Table 2.2-1 of this report.

e. One of the GT sets used in the following sections is referred to as the “standard GT”. It represents all items in the ground (except when scoring MAG systems, only ferrous items used). Elsewhere in this report select items or areas within the standard GT are used as a subset and are noted as such. Results using the standard GT are those which are published on the standardized UXO web site. The standard GT contains a host of challenges that push the detection limits of current technology. Such challenges may include dense areas of clutter, overlapping halos (i.e., items within 1 m of each other), items (few) that are deeper than typically remediated, metallic

objects above ground, electromagnetic interference (minimal) from power lines, and a wet area. The wet area was not by design and proved to limit some demonstrators in the APG open field. The area was dry most of the time but at other times was marshy and under a couple inches of water. It comprises about 10 percent of the APG open field. This area is eliminated from scoring in the 11D, no challenge (wet area considered a challenge), no overlap GT variant commonly used throughout this report which allows a better comparison of performance of individual systems.

f. The standard GT is comprised of only ferrous items for MAG systems.(since these systems are incapable of detecting non-ferrous items). Ferrous and non-ferrous items are used in the GT for EM, radar, and dual systems. Plots will typically have a small acronym (MOIM, which stands for Magnetic Only If Magnetometer) on them to indicate that all ferrous GT was used only for the MAG systems. If the non-ferrous items are not removed then the MAG systems are penalized in performance by the proportion of non-ferrous items chosen.

g. Some of the GT subsets will commonly be limited in depth to 11D. In such cases, all GT items buried at depths greater than 11 times their diameter are eliminated from scoring. The 11D restriction is implemented to include items at depths that are commonly required for testing and, by doing so, to make results more comparable to typical GPOs. The 11D value is the industry rule (per ERDC) for range of depth within which current systems can detect ordnance. The rule defines depth from the ground surface to the highest point on a buried ordnance item in the ground. In this compilation of work, depth to the center of a buried ordnance item is used instead of the highest point in the ground. The effect is that the 11D GT will be slightly shallower. Sensitivity studies indicate P_d^{res} scores will be approximately 1 to 2 percent higher (APG open field site) when 11D is referenced to the center of the ordnance instead of the highest point of the ordnance in the ground.

h. One type of system in the results presented will be considered a baseline. This system, the Schonstedt, is a hand held MAG. The system is one of the most commonly used systems in current UXO remediation. Two Schonstedts were demonstrated to provide a comparison.

i. The reader should be aware that detection rules at the sites were set up so that a “detection” is considered the ability to “discern” an “individual” item in the ground. The problem with this approach is that some items are very close together in the ground and signal returns from the combined items appear as “one” anomalous signal. Thus, if two items are side by side in the ground and the detection system indicates one anomaly, then only one detection is granted. These rules apply when items are closer than one meter to each other or equivalently, when half meter radii around each item “overlap”. While the number of ordnance with overlap are small in the GT, the use of these rules will reduce and hence misrepresent detection scores if it is only desired to see if signals, whether from single or combined items, were detected. For the reader wanting to see results free from the effects of overlaps, GT variants have been created and are noted as having “no overlaps” or noted that distances between items are greater than one meter (all blind grid test areas inherently have no overlaps). Such results are the best indicator of detection ability for individual items. Conversely, results with overlaps have merit when comparing the performance of multiple systems to see if one system can better discern multiple

items in close proximity than another. Also, comparing scores with and without overlaps gives some indication of the effect of signal masking from items in close proximity to each other.

j. The blind grids and open fields at APG and YPG were reconfigured in the 2004-2005 time frame. The GT in these areas were fully extracted in the blind grids and partially extracted in the open fields. New items were put back into the ground in these areas with an overall characteristic that was similar to what was extracted. Some systems that were tested after the reconfiguration are included on the comparative plots shown in this report to add to the variety displayed. Their results should be adequate for general comparison but should not be used for decision making purposes beyond a general level. The post-reconfiguration systems are listed by report number as follows: 1) APG open field, 740 and 802, 2) APG blind grid, 680, 691, 693, 694, 695, 739, 764 and 792, 3) YPG open field, 770, 4) YPG blind grid, 769, 805 and 806. The APG open field had several hundred “noisy” items removed from it during reconfiguration which no doubt effects post-reconfiguration BAR scores. Therefore, for system numbers 740 and 802, BAR scores can not be compared with pre-reconfiguration results from other systems. It is also noted that some noisy items were removed in an exploratory phase prior to reconfiguration which “may” have slightly reduced the BAR scores of report numbers 657, 298, 802, 740, 231, 406, 411 and 229.

k. Finally, a note of caution when interpreting overall Pd results. Overall Pds are influenced by target mix and depths, presence of clusters, unsurveyable areas, etc. All of the identified factors will reduce overall Pd compared to a typical GPO. When possible, the effects on Pd by such factors are mitigated by the use of GT variants.

2.3.1.1 *Probability of Detecting Ordnance*

a. This section shows system results using P_d , and BAR (P_{ba} for blind grid), as measures of performance. P_d is in the response stage and therefore reflects the number of ordnance found divided by the total number of ordnance emplaced. BAR, also in the response stage, is a number that is proportional to the number of items declared to be potential ordnance (i.e., anomalies) that turn out to be neither ordnance nor clutter. The actual number of background alarms has not been given to help preclude discovery of GT proportion. Nonetheless, BAR allows relative comparisons between systems and between test areas (except blind grid) within a given proving ground.

b. P_d^{res} versus background alarm metrics for the systems demonstrated at the APG and YPG test sites using a GT variant are shown in Figures 2.3.1-1 through 2.3.1-8. The GT variant contains no items deeper than 11D, items closer than one meter to each other (no overlaps) or items in challenge areas (includes intermittently wet areas). The elimination of overlap items will help give a best estimate of P_d on individual items (not combined items). The elimination of challenge items will reduce environmental variability to give a more standard result.

c. Blind grid results are shown in Figures 2.3.1-1 and 2.3.1-2. The blind grids are set up to allow an objective binary type response from the sensors alone to indicate whether an anomaly is present or not. Potential locations of items are known beforehand. Further, the grids are free from overlap and dense areas of clutter to confuse signals. Albeit the APG blind grid did have some clutter items with signals that bled over into other grid locations even though the grids were spaced 2 meters apart. Thus, signal interpretation in the blind grids should be easier than in other test areas and platform navigation issues minimized (since potential locations of the items are known). This ease of detection is manifest in the higher detection rates realized in the blind grid areas when compared to other test areas.

d. The best systems demonstrated a P_d^{res} of 1.0 in both blind grids. All systems typically performed better at the YPG blind grid than they did at the APG blind grid. This is likely because of the greater GT depth at the APG grid. EM61 MKII sensors, irrespective of platform type, and the MTADS GEM3 sensor typically did best in the YPG blind grid with P_d^{res} scores as high as 1.0 and P_{ba} as low as 0.0. The same sensors were the best demonstrated at the APG blind grid also with P_d^{res} scores as high as 1.0 but with P_{ba} scores higher than at YPG at 0.07 to 0.17.

e. The best P_d^{res} scores with lowest P_{ba} that were achieved by MAG systems were 0.88 at APG with a G822ROV towed system and 0.95-0.98 at YPG with a TMGS towed and an TM-4 sling system.

f. The only ground penetrating radar system analyzed was demonstrated at the APG blind grid. The performance of this system was along the lower P_d^{res} vs. P_{ba} boundary of all other system types. More of these systems are needed to evaluate the technology better.

g. The dual systems did not excel in either of the blind grids. More analysis of dual systems is included in section 2.3.9.1.

h. Two Schonstedts were typically demonstrated in most areas. The majority of the technologies surpassed Schonstedt performance in the blind grids. This is a favorable indicator regarding the SOTA of the sensor community in general.

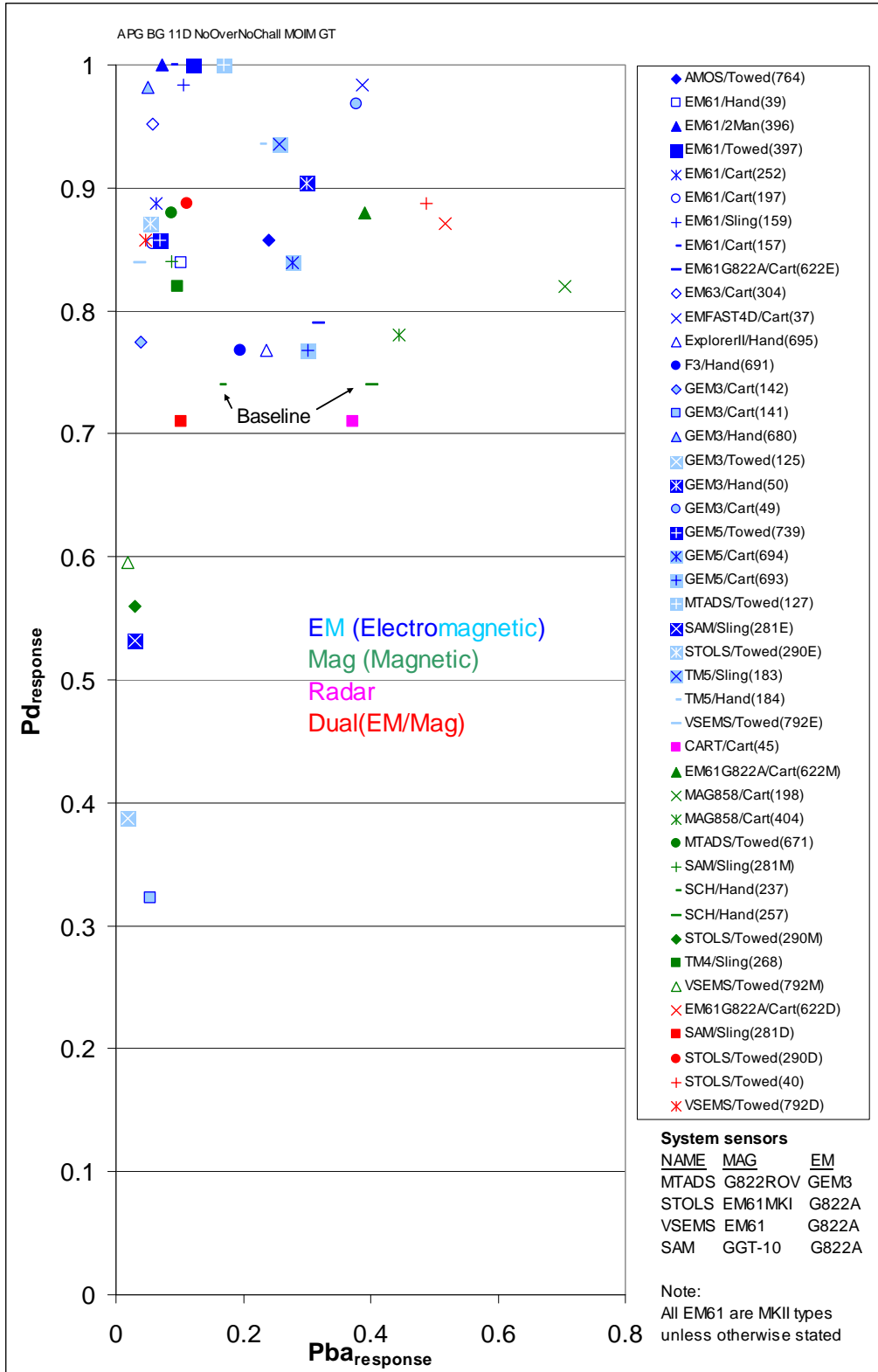


Figure 2.3.1-1. P_d^{res} versus P_{ba}^{res} , APG blind grid, 11D, No Overlap, No Challenge GT.

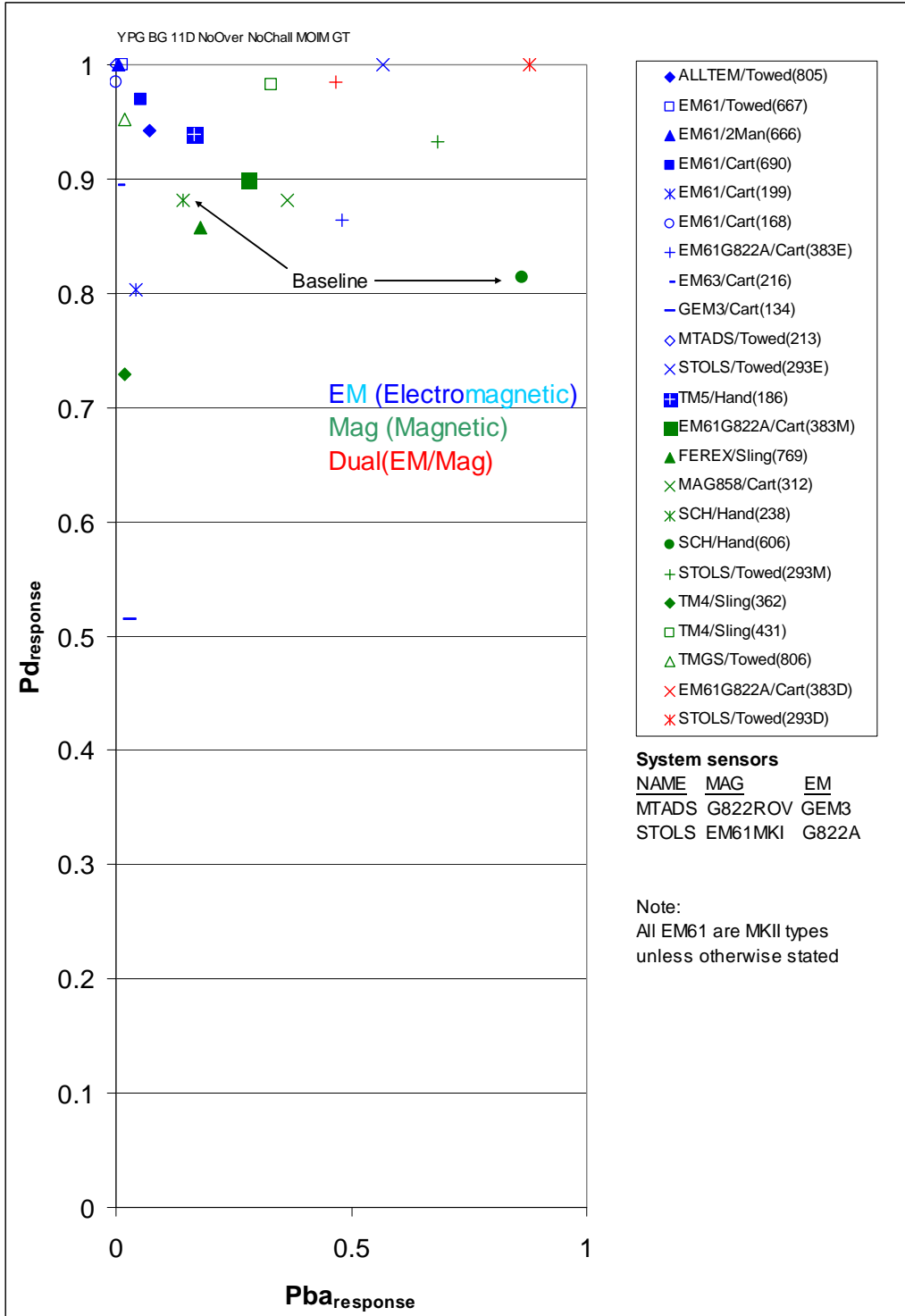


Figure 2.3.1-2. P_d^{res} versus P_{ba}^{res} , YPG blind grid, 11D, No Overlap, No Challenge GT.

i. P_d versus BAR results for the APG and YPG open field areas are shown in Figures 2.3.1-3 and 2.3.1-4.

j. In the open fields, the P_d^{res} of the systems are substantially lower when compared to the blind grid results. Based on the fact that the positions of potential ordnance/clutter are known beforehand in the blind grids, it has to be concluded that this advantage in the blind grids contributes some measure to the observed disparity. The terrain has little influence on the disparity since the open fields are indeed open and relatively flat like the blind grids. The GT in the intermittently wet area in the APG open field has been eliminated so no performance degradation is expected. Therefore, the remaining parameter likely driving disparity is the GT configuration/distribution differences between the two areas. Contributors to this and other disparities will be examined throughout this report.

k. Approximately 84 percent ($P_d^{res} = 0.84$) of the ordnance was found by the best performers in the APG open field (fig. 2.3.1-3). An EM61 MKII pushcart and MTADS GEM-3 towed array system achieved this level with a relatively low BAR score. The best score achieved in the YPG open field (fig. 2.3.1-4) was a P_d^{res} of 0.96 by the MTADS GEM-3 towed system with TM-5, EM61MKII and EM63 systems not far behind. The GEM-3 and EM61 systems had better BAR scores. Thus, P_d scores in the APG area were about 10% lower than in the YPG area. The BAR scores are very low and very tight for the YPG open field suggesting environmental noise in the YPG field may have been at a lower level than at APG.

l. The dual systems performed slightly above average in the open fields when compared to all other systems demonstrated. They typically trend between the EM and MAG sensors with regard to performance. Analysis performed later in section 2.3.9.1 will show that the performance of the dual systems surpasses the separate EM and MAG constituent performance of those same systems. Therefore, better combinations of systems may prove to have superior performance once matched up.

m. In the APG open field an MTADS towed system of eight 822ROV sensors was the best performer among MAG systems with a $P_d = 0.84$. The MAG constituent, G822A sensor, of a dual system, had the best MAG P_d^{res} score, 0.85, in the YPG open field however, the BAR value was extremely high relative to other systems demonstrated. The next best MAG system at YPG was a TM-4 sling with a $P_d^{res} = 0.77$ but also with a high BAR (about 20 times greater than EMs).

n. Again, most systems out performed the Schondstedt baseline results.

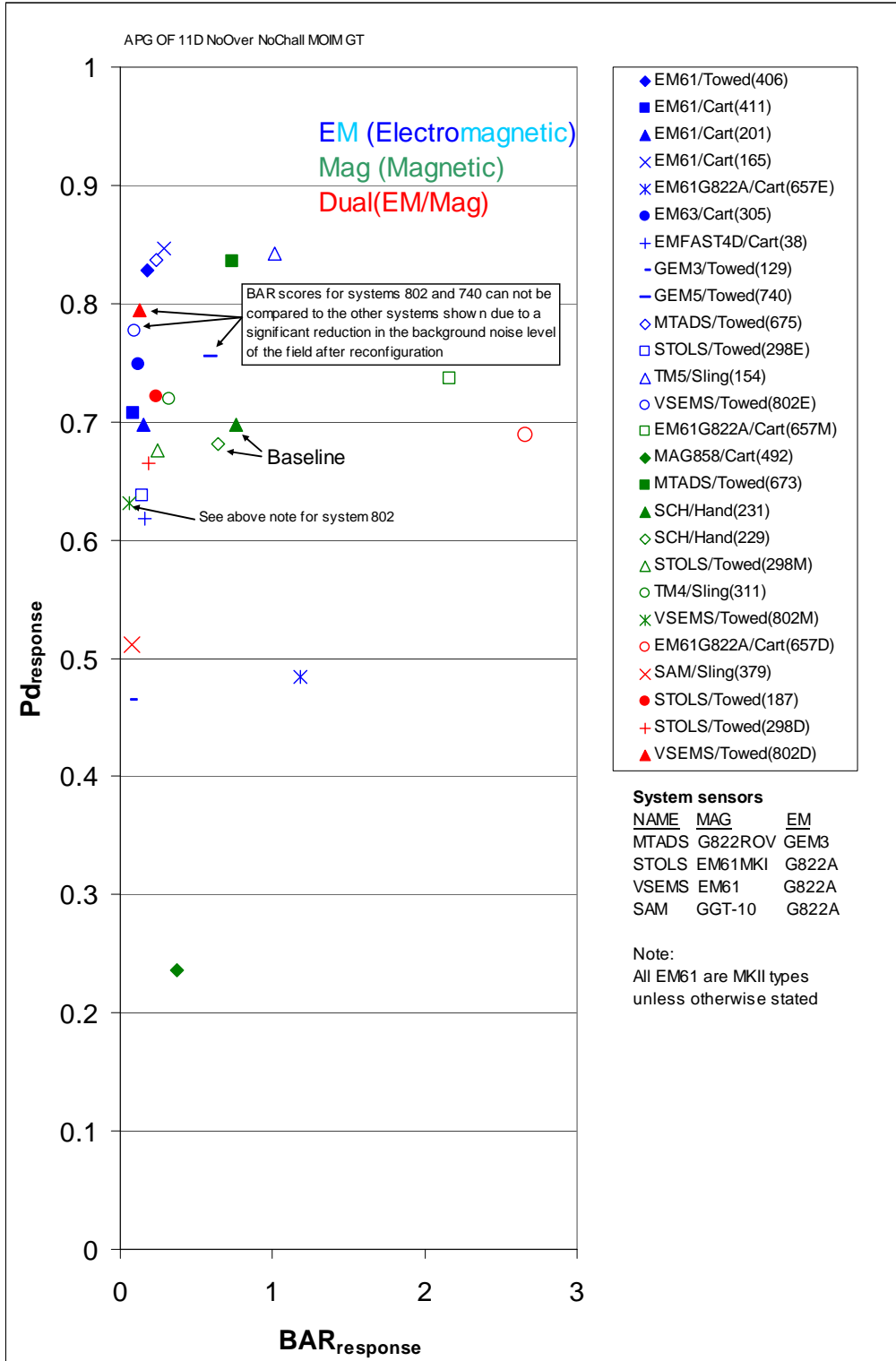


Figure 2.3.1-3. P_d^{res} versus BAR^{res} , APG open field, 11D, No Overlap, No Challenge GT.

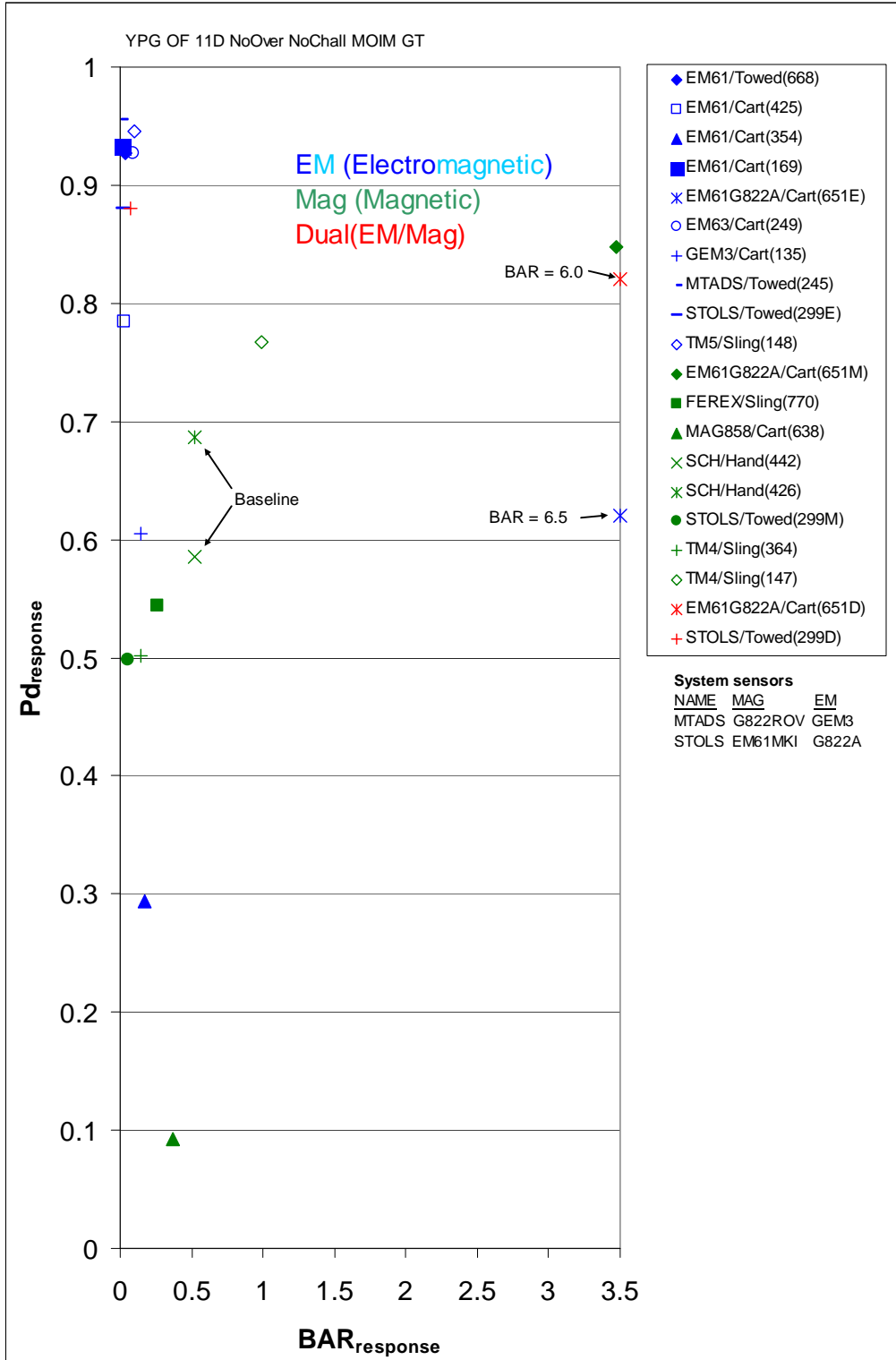


Figure 2.3.1-4. P_d^{res} versus BAR^{res} , YPG open field, 11D, No Overlap, No Challenge GT.

- o. P_d^{res} versus BAR^{res} results for the mogul areas are shown in Figures 2.3.1-5 and 2.3.1-6.
- p. A significant reduction in P_d^{res} occurs when comparing the APG mogul results to the APG blind grid results. The reduction is about twice that realized in the APG open field. This reduction is understandable when the APG mogul terrain is inspected first hand. The APG moguls are not able to be traversed by most wheeled vehicles. There are no moguls higher than about 1 meter but they have very steep sides kept from erosion by large clumps of grass. Further the valleys between moguls can fill up with water and become marsh like.
- q. The highest P_d^{res} achieved in the APG moguls was 0.82. This score was produced by a GEM-3 hand held unit. The next closest P_d^{res} value is 24 percent lower and the overall average P_d^{res} is about 0.45 for all systems combined. The only other hand held units demonstrated in the APG moguls were Schonstedts (MAG systems), which yielded P_d^{res} scores of 0.42 and 0.48. The GEM-3 hand held unit outperformed pushcarts and slings of EM and MAG varieties. The GEM-3 system has a BAR that is about six times greater than the next best system result. As will be shown in section 2.3.8, the GEM-3 system spent much more time surveying than did other systems. No towed platforms were tried in the area. If such platforms did try to survey these moguls they would likely destroy the terrain in an effort to negotiate it. All results demonstrated in the APG moguls are currently unacceptable.
- r. The results in the YPG moguls were comparable to YPG open field results. This is because the variation in the grade at the YPG moguls is not that severe. The sand mounds originally constructed were easily eroded and thus smoothed over time. Erosion was not monitored but it is likely earlier demonstrators had more difficulty traversing the moguls. Further analysis should date the demonstrations to look for trends.
- s. The Schonstedt baseline performance falls in the mid detection range of technologies demonstrated at the moguls. This is a better result for the Schonstedts, relative to other systems, than is exhibited in the open fields and blind grids. This in combination with the GEM-3 hand held performance shows how the platform is becoming a driver (hand held's exhibiting better performances) in detection ability for the rougher terrains.

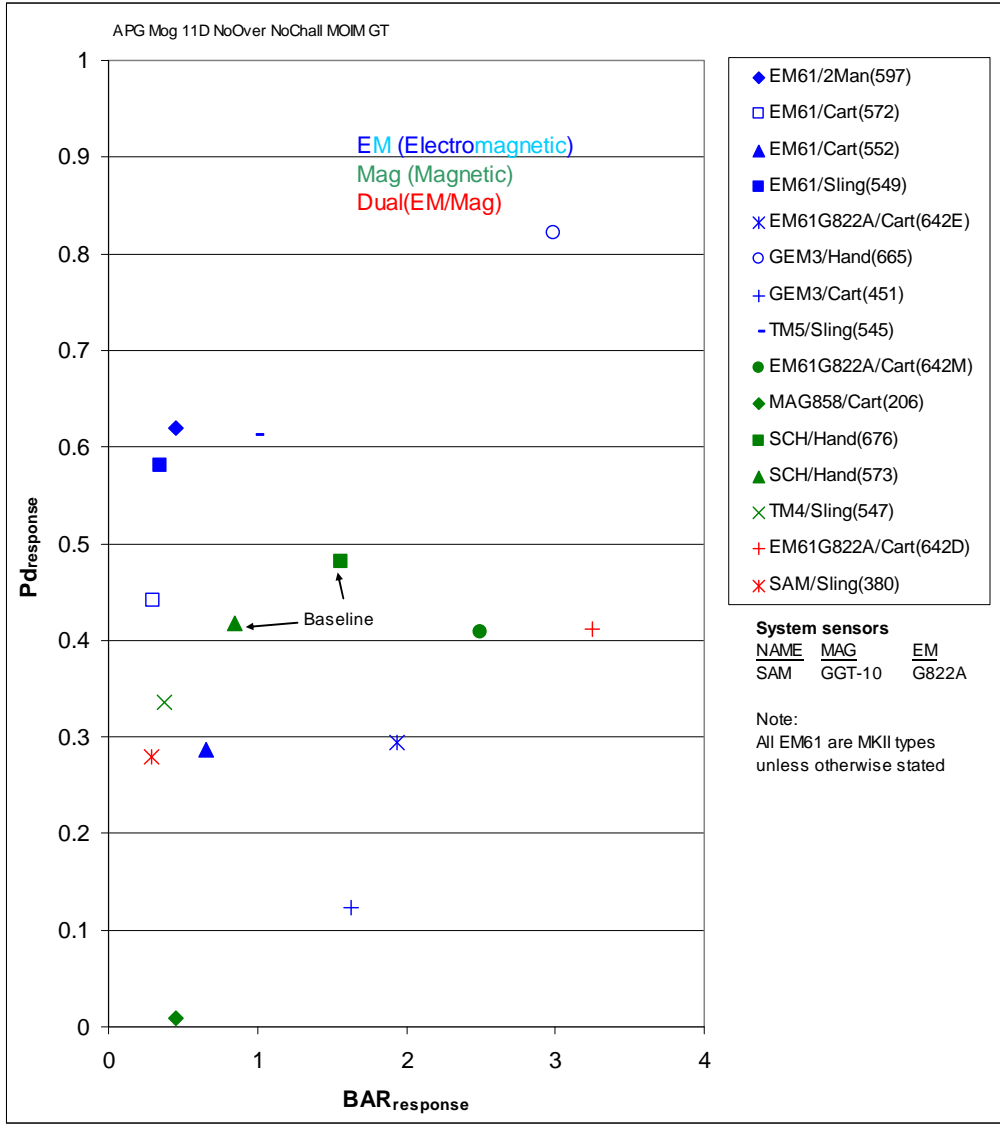


Figure 2.3.1-5. P_d^{res} versus BAR^{res} , APG moguls, 11D, No Overlap, No Challenge GT.

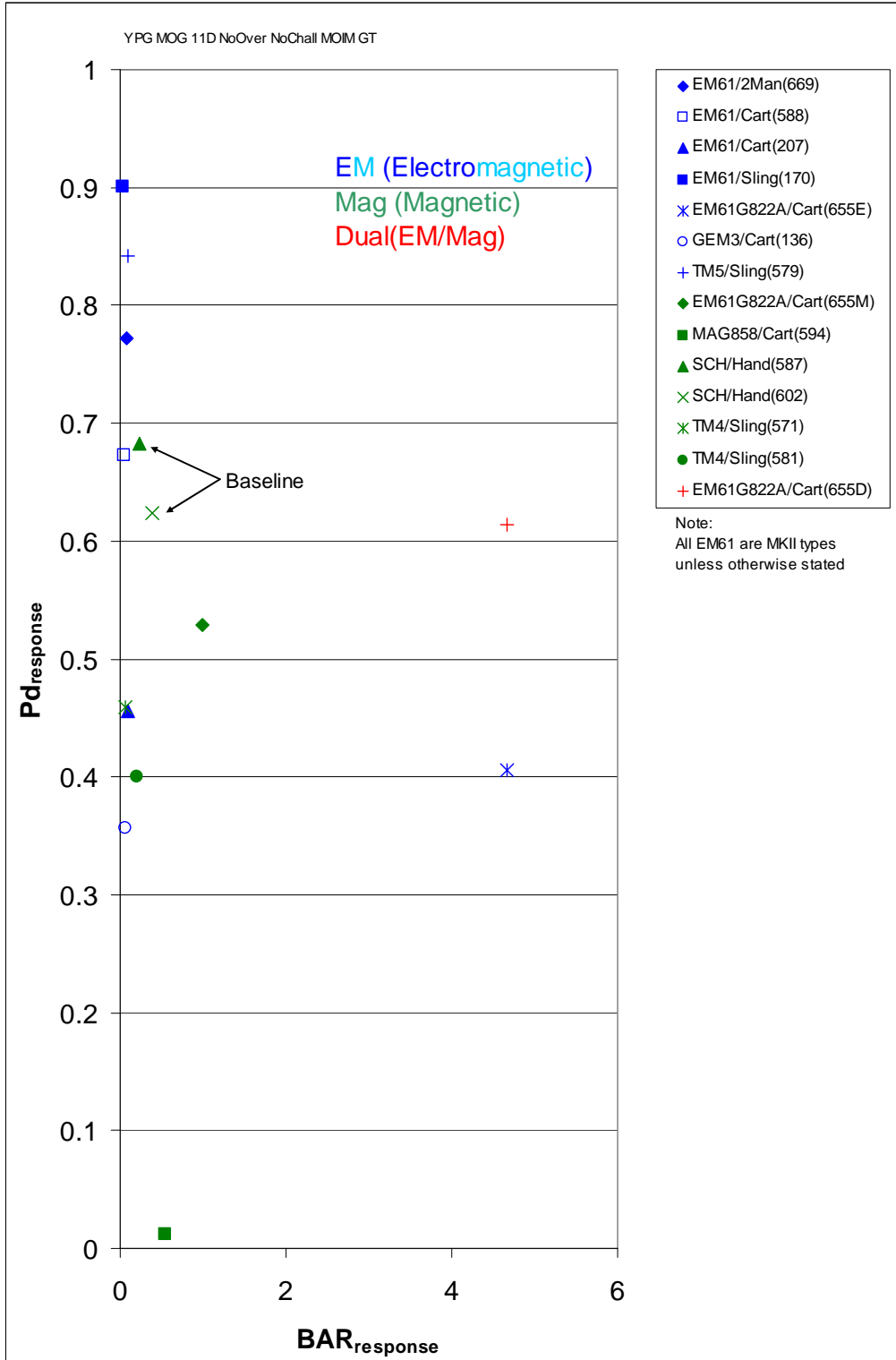


Figure 2.3.1-6. Pd^{res} versus BAR^{res} , YPG moguls, 11D, No Overlap, No Challenge GT.

t. P_d^{res} versus BAR is shown in Figure 2.3.1-7 for systems demonstrated at the desert extreme area at YPG. The performance of the systems in the extreme area decreased by about 30 percent compared to the YPG open field performance. The extreme area comprises uneven terrain characterized by gulleys and also contains brush.

u. The best performer in the desert extreme used an EM61 MKII sensor on a 2-man platform (litter type) and had a P_d^{res} of 0.67. The next best performer was a Schonstedt followed by an EM61 MKII push cart system, both with a P_d^{res} of about 0.6. BARs for these systems were about the same except for the pushcart system which had a very low value relative to the others.

v. Again, with more extreme terrain, hand held units are among top performers.

w. P_d^{res} versus BAR is shown in Figure 2.3.1-8 for the APG wooded area. This area along with the APG moguls turned out to be the most difficult of all the areas in the Standardized Test Sites. The best performers in the woods were the EM61 MKII/2-man and EM61 MKII/sling systems, both with a P_d^{res} score of approximately 0.64. The sling had a BAR score that was three times less than the 2-man platform system. A TM-5 hand held unit was close behind as one of the better performers. The next best performer was an EM61 cart system with a P_d^{res} score about 30 percent lower. The wooded area is actually very flat but is cluttered with large trees both living and fallen. Root systems also pervade the area. Further the area has standing water at times and contains brush. Navigation is very difficult. The results indicate pushcarts are not well suited for such close-in terrains and that man-portable platforms provide the best access. All results indicate a level of performance that would be unacceptable for ordnance detection.

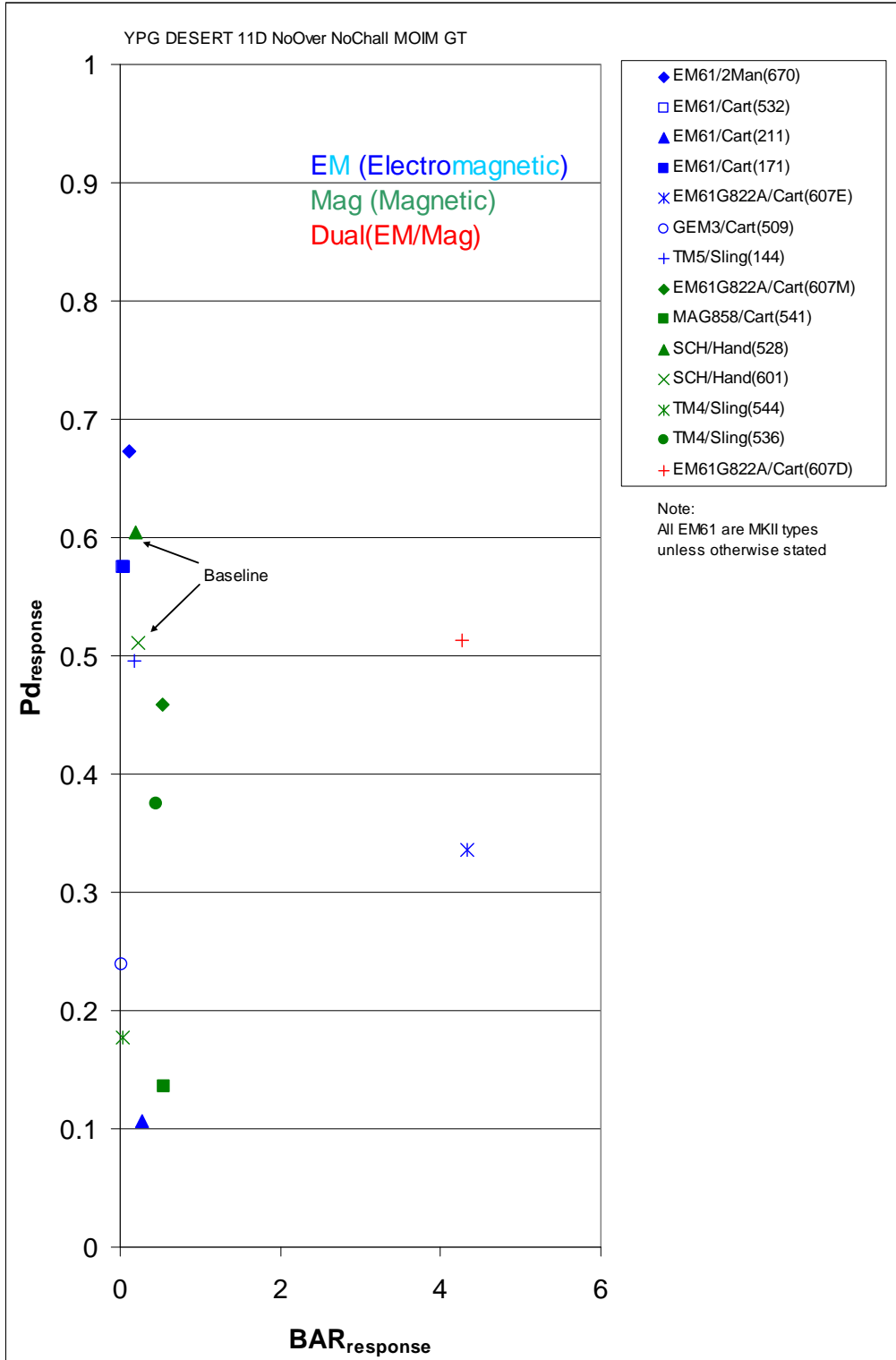


Figure 2.3.1-7. Pd^{res} versus BAR^{res}, YPG desert extreme, 11D, No Overlap, No Challenge GT.

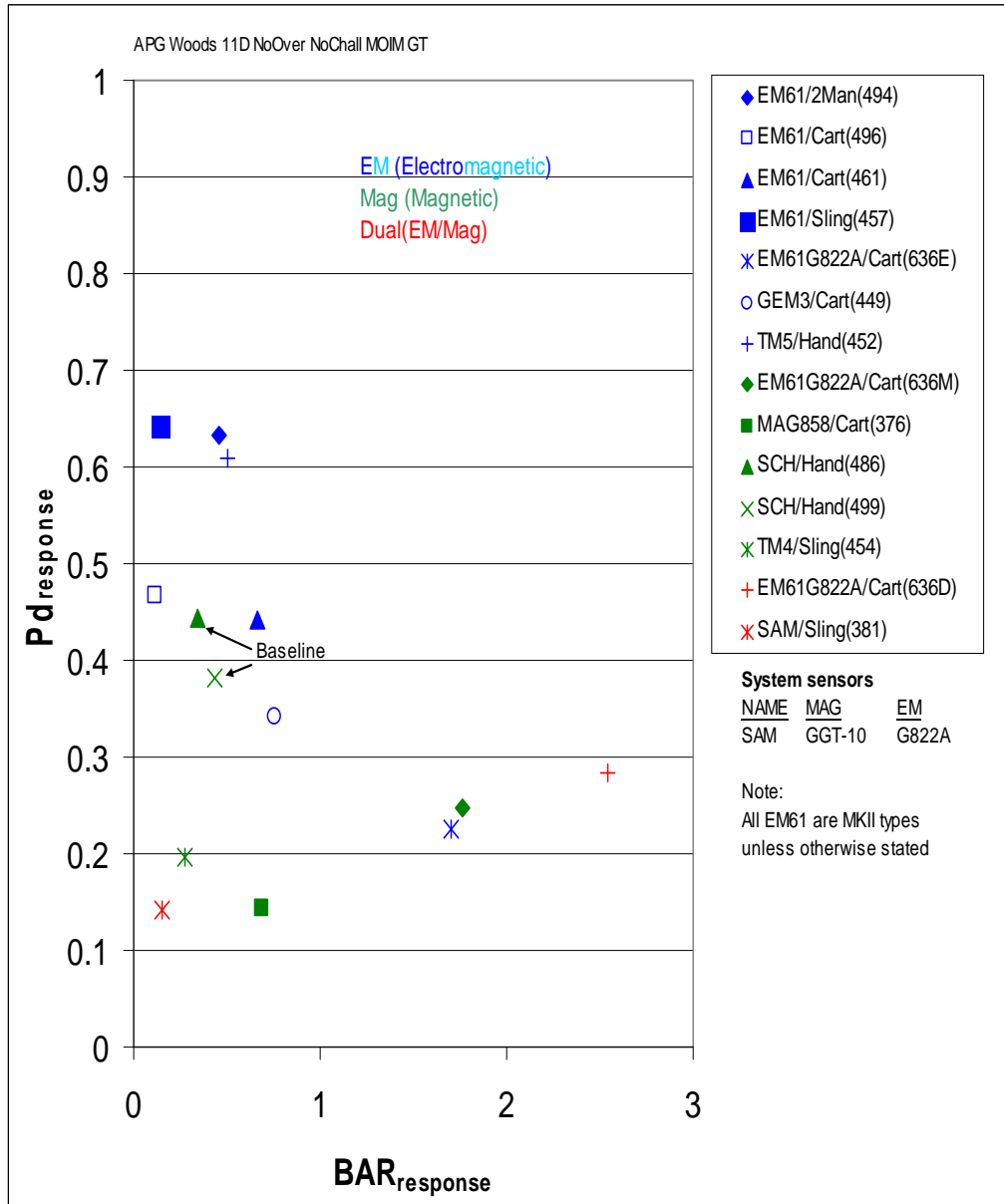


Figure 2.3.1-8. P_d^{res} versus BAR^{res} , APG woods, 11D, No Overlap, No Challenge GT.

2.3.1.2 Performance Using All Ferrous GT

a. P_d^{res} versus BAR results are shown in Figures 2.3.1-9 and 2.3.1-10 for all systems demonstrated in the APG and YPG open fields, respectively, using an all ferrous GT. This variant of the GT allows a direct comparison between EM and MAG systems since the same GT set is used for each (no longer ferrous and non-ferrous GT used for EM and ferrous GT used for MAG). Since the same GT is applied to both types of sensors, dual system component results can be compared with the fused results found in an all ferrous environment. This GT is similar to the one used in the previous section in that there are no items buried below 11D, no items in challenge areas (including wet areas) and no items within one meter of each other (no overlaps).

b. The results indicate that the EM based systems typically performed better than all other basic system types when using the same all ferrous GT.

c. The best dual systems were typically among the better performers in the all ferrous GT. In the APG open field the VSEMS/towed configuration was the best dual performer and benefited from combining its EM and MAG counterparts. The combined P_d^{res} score was 0.83, while the EM component score was $P_d^{\text{res}} = 0.81$ and the MAG score $P_d^{\text{res}} = 0.63$. The VSEMS uses the EM61 MKII (EM) and the G822A (MAG) sensors. The VSEMS tested after the APG open field was reconfigured and a large number of items causing background noise were extracted. Because of this, the BAR score for the VSEMS system (system 740 also) could be as much as 0.2 lower than a pre-reconfiguration result.

d. The best performing MAG system demonstrated at APG had a P_d^{res} score of 0.84. This score was near the best EM score (0.87) and was from a towed array of eight geometrics 822ROV sensors (MTADS, report No. 673). The BAR score, however, was about three times higher than the best EM system.

e. When comparing the all ferrous results for the EM against the ferrous/nonferrous results of Figures 2.3.1-3 and 2.3.1-4, the P_d^{res} scores improve a few percent in the all ferrous GT. This indicates that the EM sensors are having a more difficult time detecting the non-ferrous items than they are the ferrous items (the non-ferrous items are M385 aluminum grenades and aluminum MK118 submunitions). Size may be a contributing factor to this result.

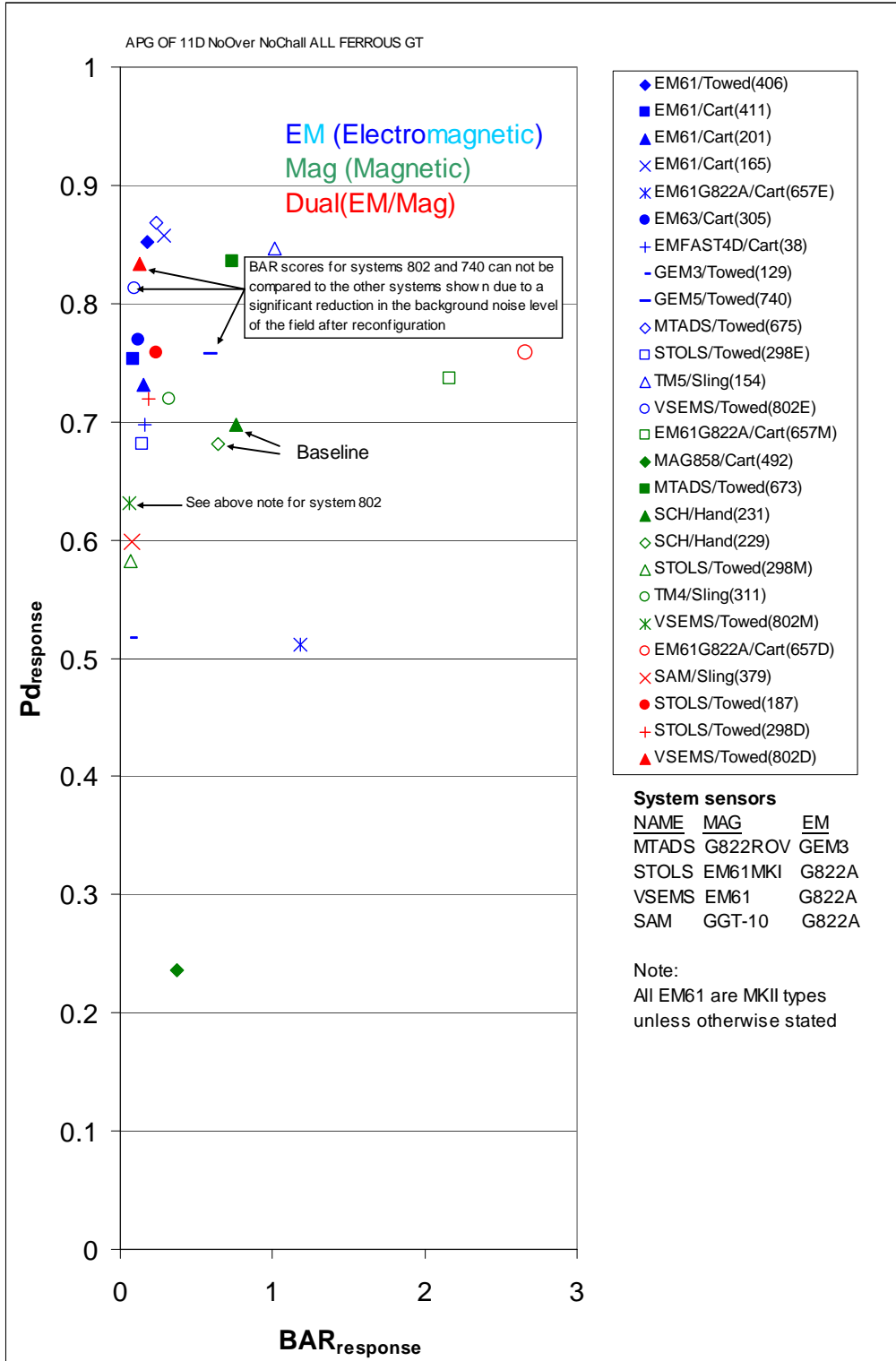


Figure 2.3.1-9. P_d^{res} versus BAR^{res} , APG open field, All ferrous, 11D, No Overlap, No Challenge GT.

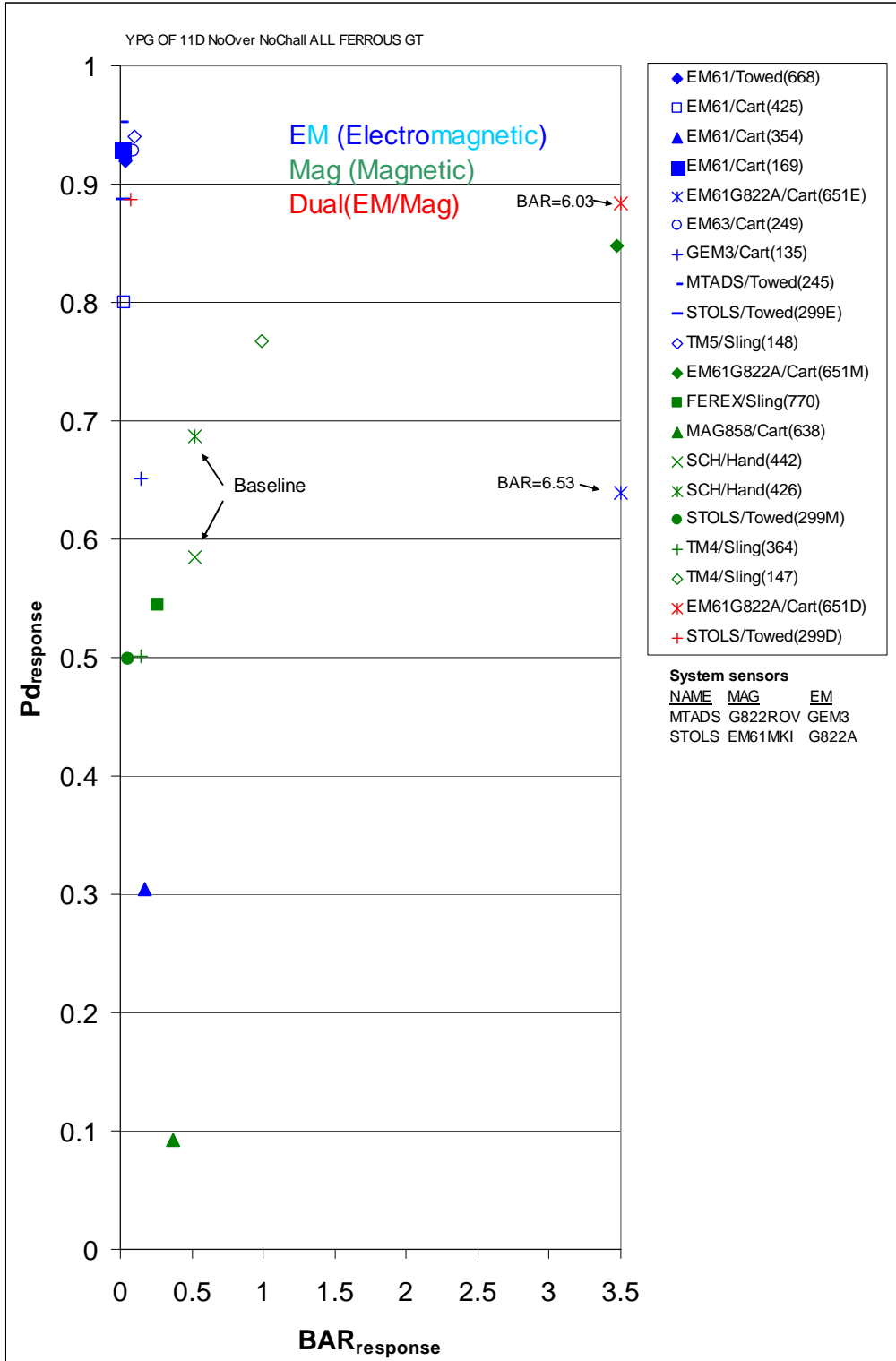


Figure 2.3.1-10. P_d^{res} versus BAR^{res} , YPG open field, All ferrous, 11D, No Overlap, No Challenge GT.

2.3.1.3 *Performance Using the Standard GT*

a. System results in the APG and YPG open fields using the standard GT are shown in Figures 2.3.1-11 and 2.3.1-12.

b. The figures show that most of the systems realized a P_d^{res} decrease of about 0.10 to 0.20 when compared with section 2.3.1.1 results. Nonetheless with this GT, trends between the EM, MAG, and dual systems are, for the most part, maintained. The EM systems are still outperforming the MAG systems.

c. The standard GT is more difficult since items are closer together (harder to discern individual signals) and deeper (harder to discern signals). Further, challenges such as power lines and fences are present to interfere with signals. This GT is more suited to test system limits. Unfortunately, in the APG open field, this GT included items in intermittently wet areas (prohibited ~5% of total area from being surveyed for some systems). Therefore comparisons between systems are restricted for this GT at APG open field. Systems that had to survey when the field was wet in these areas included those represented by report numbers 231, 298, 406, 673, and 675.

d. It is noted that one system that performed relatively (compared to results in previous sections) better in the more difficult standard GT was the TM5 sling system (report 148) at YPG open field.

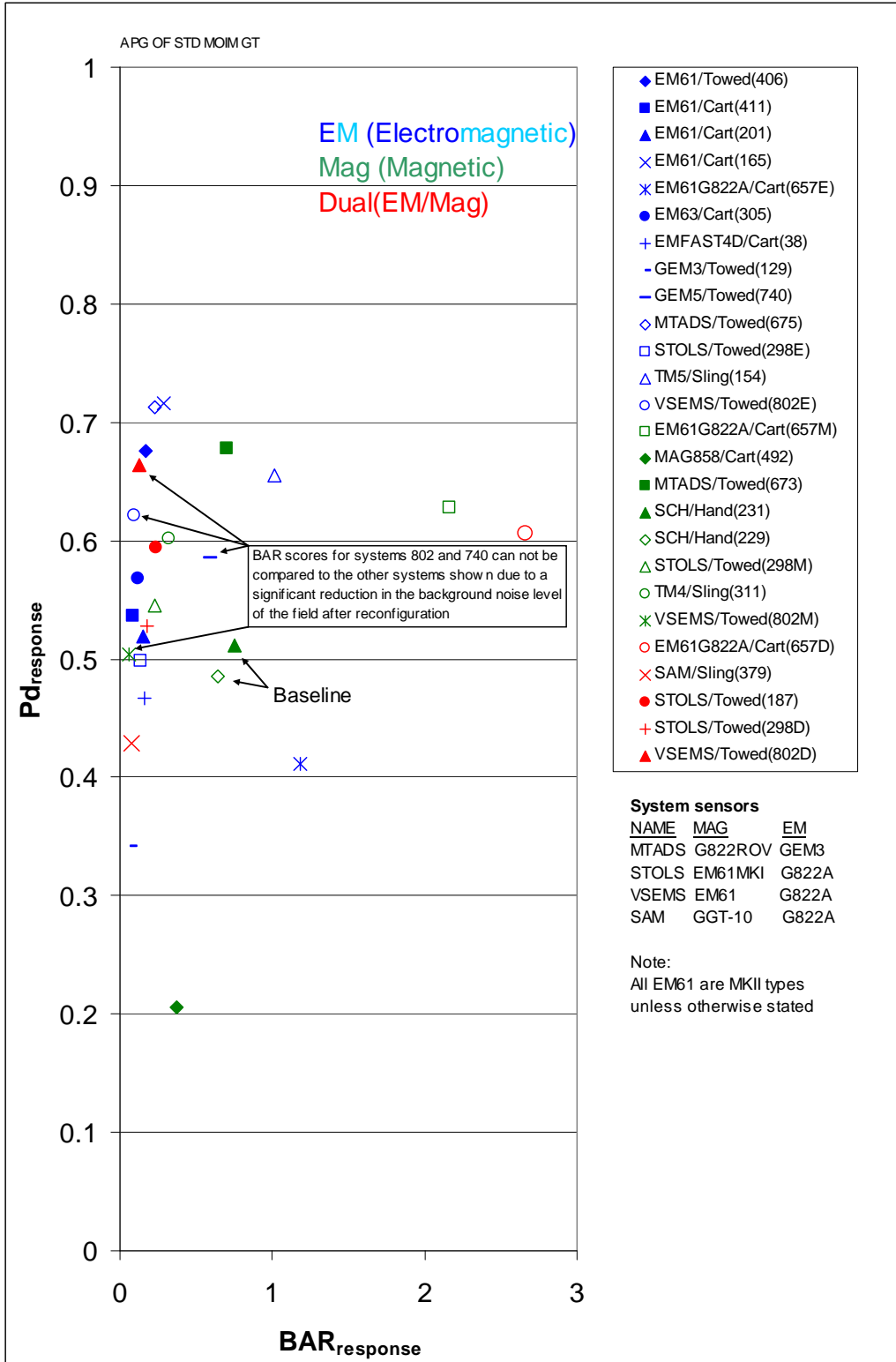


Figure 2.3.1-11. P_d^{res} versus BAR^{res} , APG open field, Standard GT.

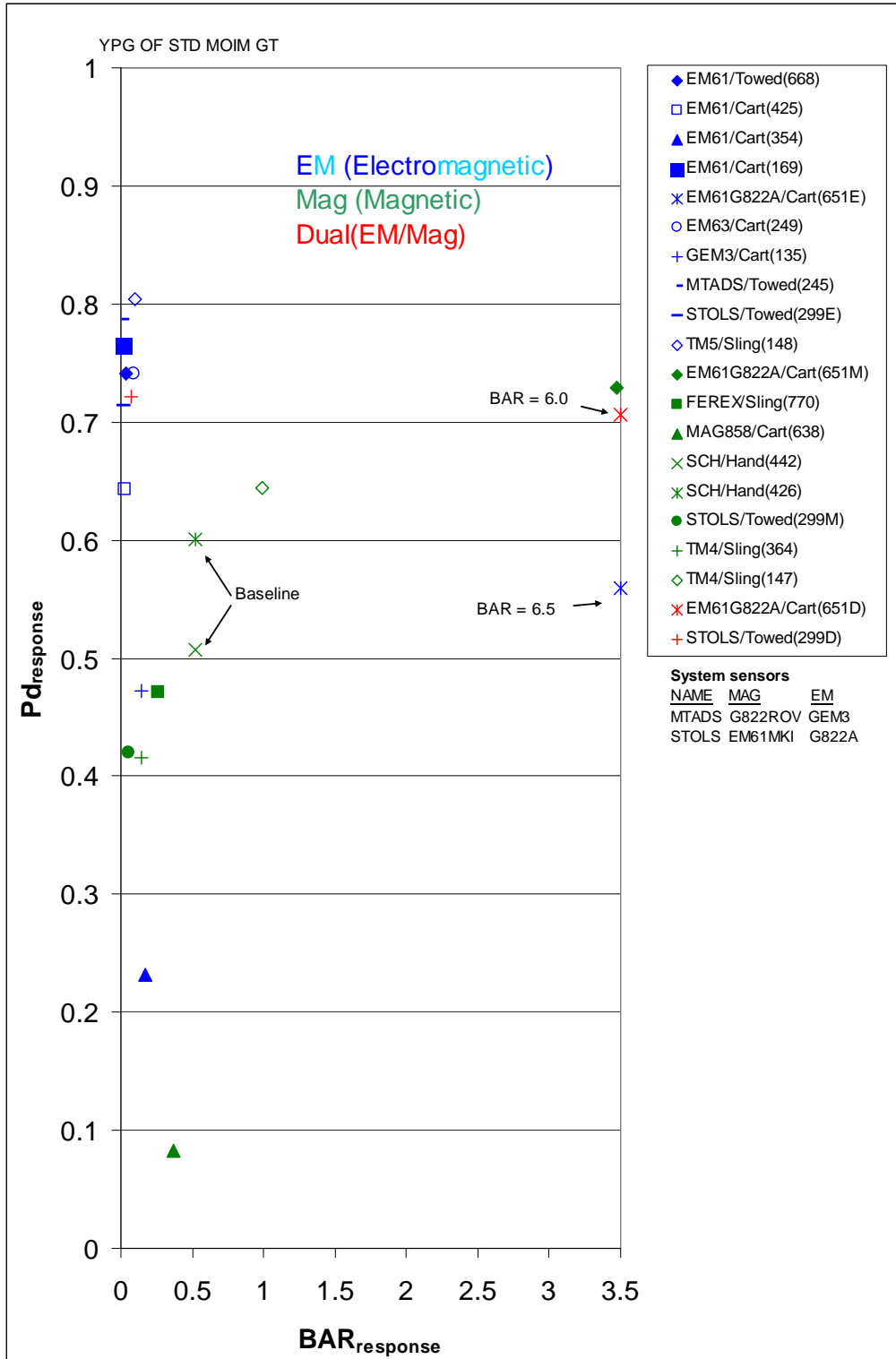


Figure 2.3.1-12. P_d^{res} versus BAR^{res} , YPG open field, Standard GT.

2.3.2 Probability of Detecting Clutter

a. Figures 2.3.2-1 through 2.3.2-8 are plots of the probability of false positive in the response stage (P_{fp}^{res}) versus BAR for all systems in all test areas. P_{fp}^{res} is the fraction of emplaced clutter items in a test area that have been detected by a system. The GT used contains no items in challenge areas or wet areas and has no items closer than one meter to another item (no overlaps). An 11D depth restriction could not be applied to the clutter since the objects buried were not cylindrical or spherical and could not be characterized by a common dimension. It can be said that only the most massive clutter (~18kg) were buried the deepest and that average depths of the larger clutter did not exceed 0.6 meters.

b. Results in the blind grids, Figures 2.3.2-1 and 2.3.2-2, APG and YPG respectively, show that clutter was less readily detected than ordnance when compared with Figures 2.3.1-1 and 2.3.1-2 of the previous section. This is likely due to a majority of clutter items being of small mass (<2kg) relative to the ordnance mass.

c. When comparing APG results versus YPG results in the blind grid, the clutter at YPG was more readily detected. At YPG most systems had P_{fp}^{res} scores above 0.95, with scores mostly below 0.9 at APG. This is likely due to the shallower depths of the clutter at YPG (0.21-m average) versus APG (0.31-m average).

d. The dual systems demonstrated in the blind grid areas typically exhibited average performance in relation to the other systems. At the YPG blind grid the dual systems had some of the highest P_{fp}^{res} scores but at the price of a very high BAR value.

e. The radar system demonstrated at the APG blind grid was one of the poorer performers when finding clutter items. This is one radar system in one test instance. More systems are needed to properly assess the technology.

f. The Schonstedt baselines were outperformed by a majority of the systems at the APG blind grid. At YPG one Schonstedt performed at a level similar to most other systems demonstrated.

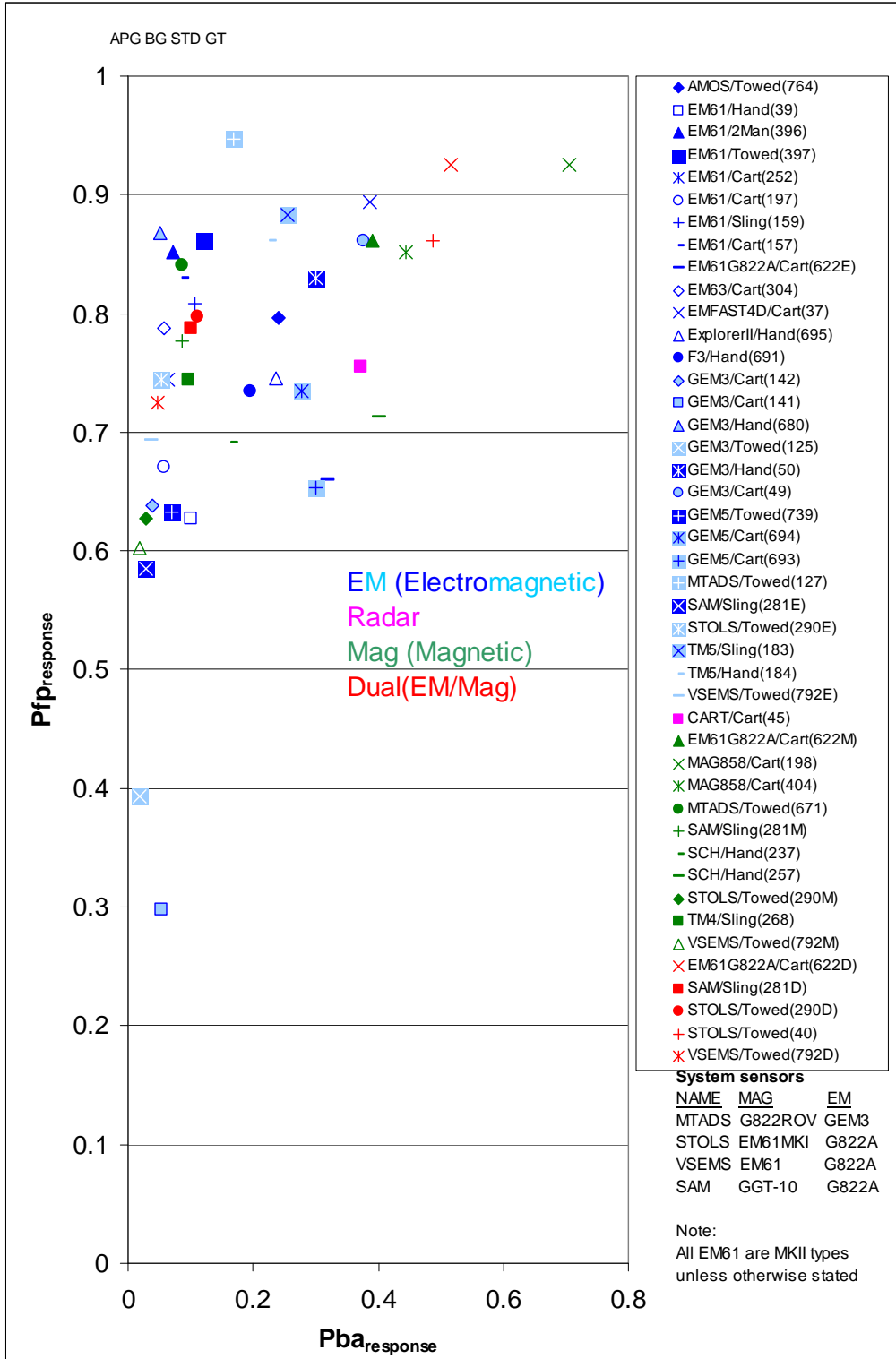


Figure 2.3.2-1. P_{fp}^{res} versus P_{ba}^{res} , APG blind grid, STD GT

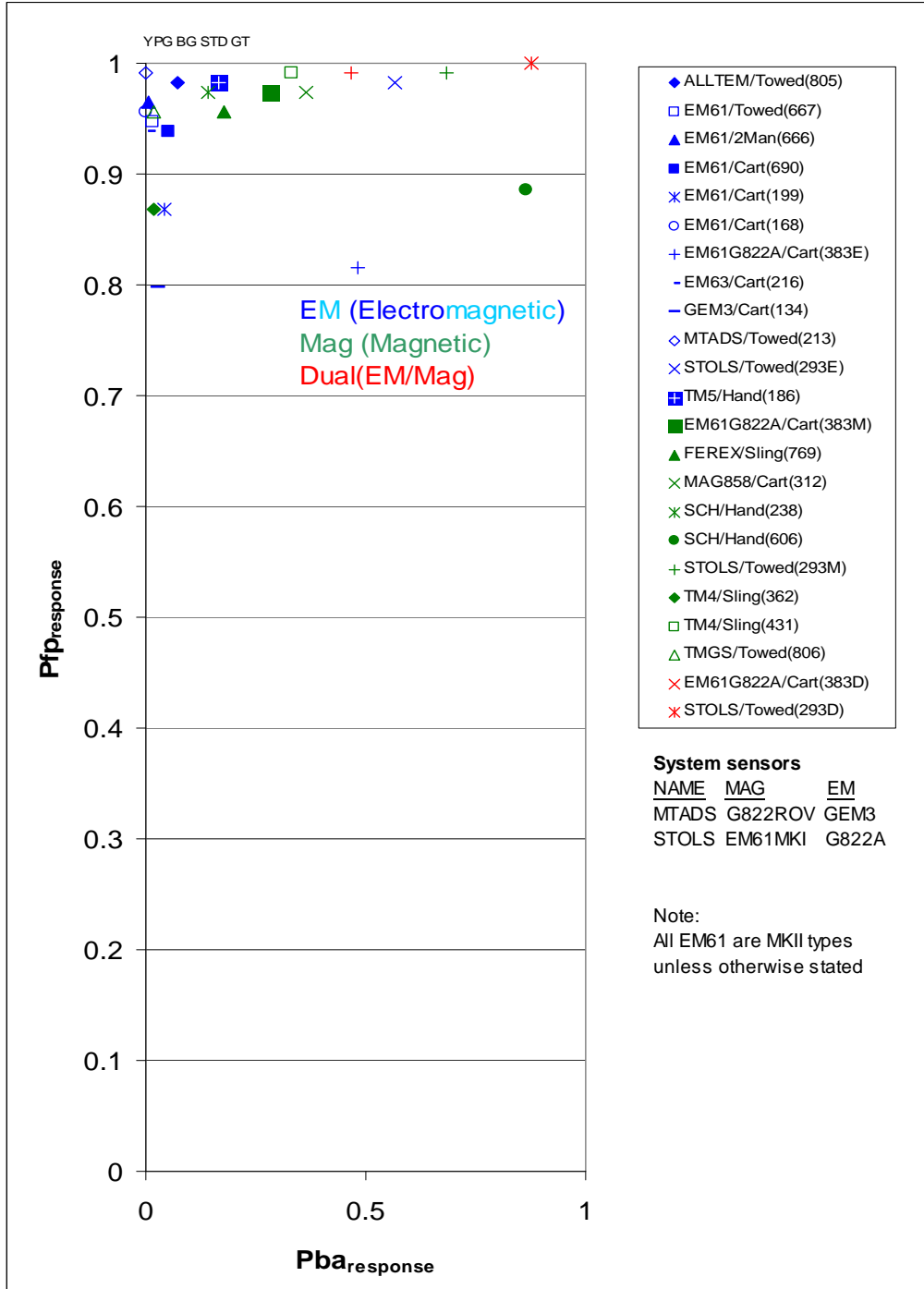


Figure 2.3.2-2. P_{fp}^{res} versus P_{ba}^{res} , YPG blind grid, STD GT

g. P_{fp}^{res} versus BAR^{res} results from the open field test areas are shown in Figures 2.3.2-3 and 2.3.2-4. The YPG open field P_{fp}^{res} results are, on average, about 20 percent lower than the YPG blind grid results. The APG open field P_{fp}^{res} results are typically about 25 percent lower than the APG blind grid results. Only about 68 percent ($P_{fp}^{res} = 0.68$) of the clutter items were detected at the APG open field by the best performers. The average clutter depth at APG is 0.37 m.

h. The best EM, MAG, and dual systems had similar P_{fp}^{res} scores in the APG open field. However, the MAG system had a significantly higher BAR^{res} value.

i. P_{fp}^{res} versus BAR^{res} for all the systems in the mogul areas are shown in Figures 2.3.2-5 and 2.3.2-6 for the APG and YPG areas, respectively. Similar trends existing in the open field areas are seen in the moguls in terms of P_{fp}^{res} and BAR^{res} . The exception is the GEM-3 hand held system that had a much higher P_{fp}^{res} than the other systems (0.68 versus 0.54 for next best) at the APG moguls. This score came at the price of a BAR^{res} value that was almost seven times greater than the next best performer..

j. Hand carried systems were among the top performers in the APG moguls which had a very challenging terrain.

k. It appears that no system currently exhibits performance that would be acceptable in a mogul environment.

l. P_{fp}^{res} versus BAR^{res} results for the YPG desert extreme test area are shown in Figure 2.3.2-7. Clutter was more easily detected than ordnance in this test area (P_{fp}^{res} about 0.2 greater than P_d^{res} , on average). A Schonstedt had the best score in this area with a $P_{fp}^{res} = 0.85$ with a relatively low BAR^{res} .

m. P_{fp}^{res} versus BAR^{res} results are shown in Figure 2.3.2-8 for the APG woods. The P_{fp}^{res} results are about 0.1 lower than P_d^{res} results for ordnance in the same area. The highest P_{fp}^{res} value, 0.54, with the lowest relative BAR^{res} value was achieved by an EM61 MKII/Sling system. It appears no system is demonstrating acceptable performance in the wooded area.

Note: Section 2.3.5.8 provides further analysis of clutter results by mass categories.

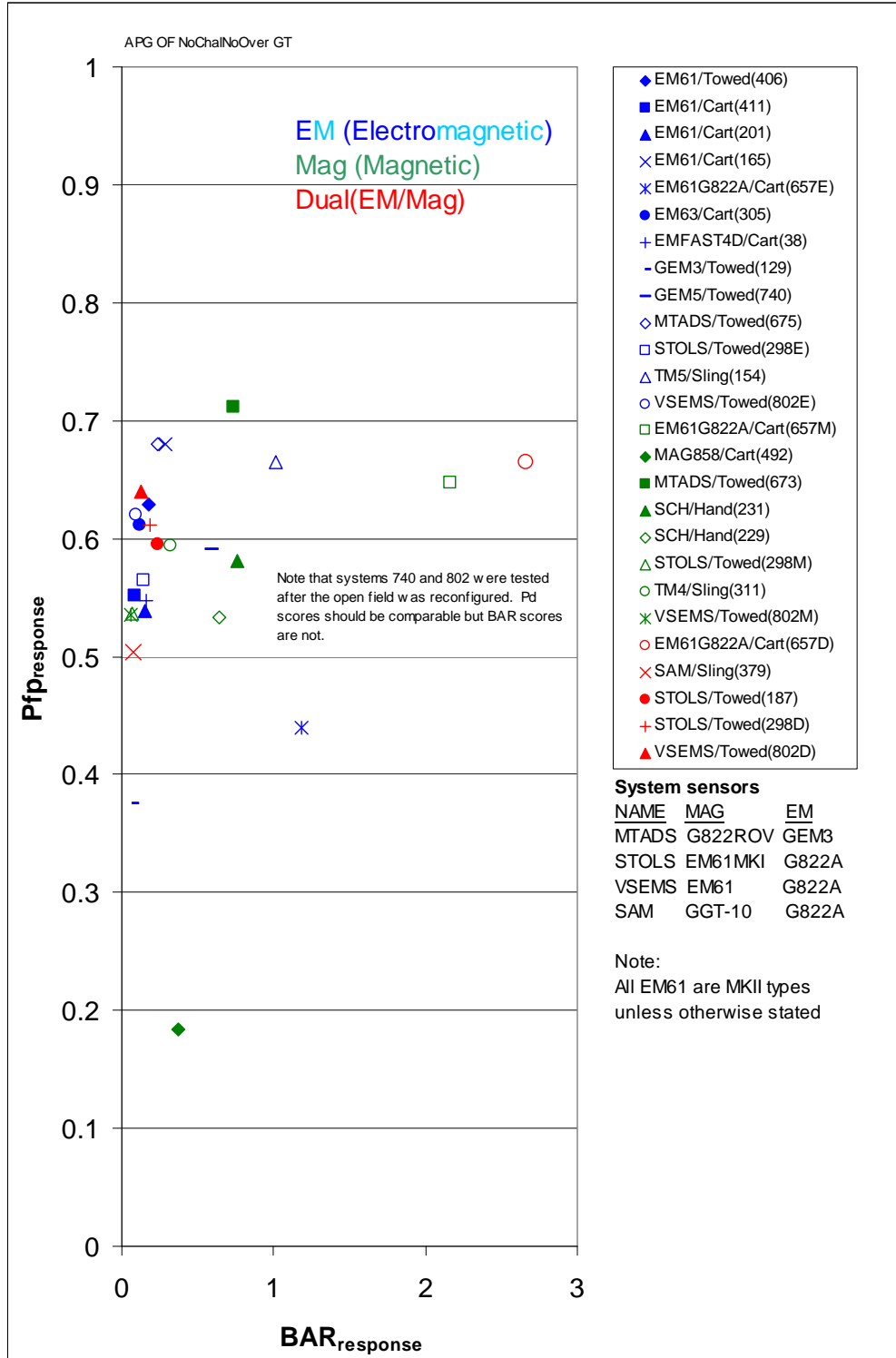


Figure 2.3.2-3. P_{fp}^{res} versus BAR^{res} , APG open field, No Challenge, No Overlaps GT

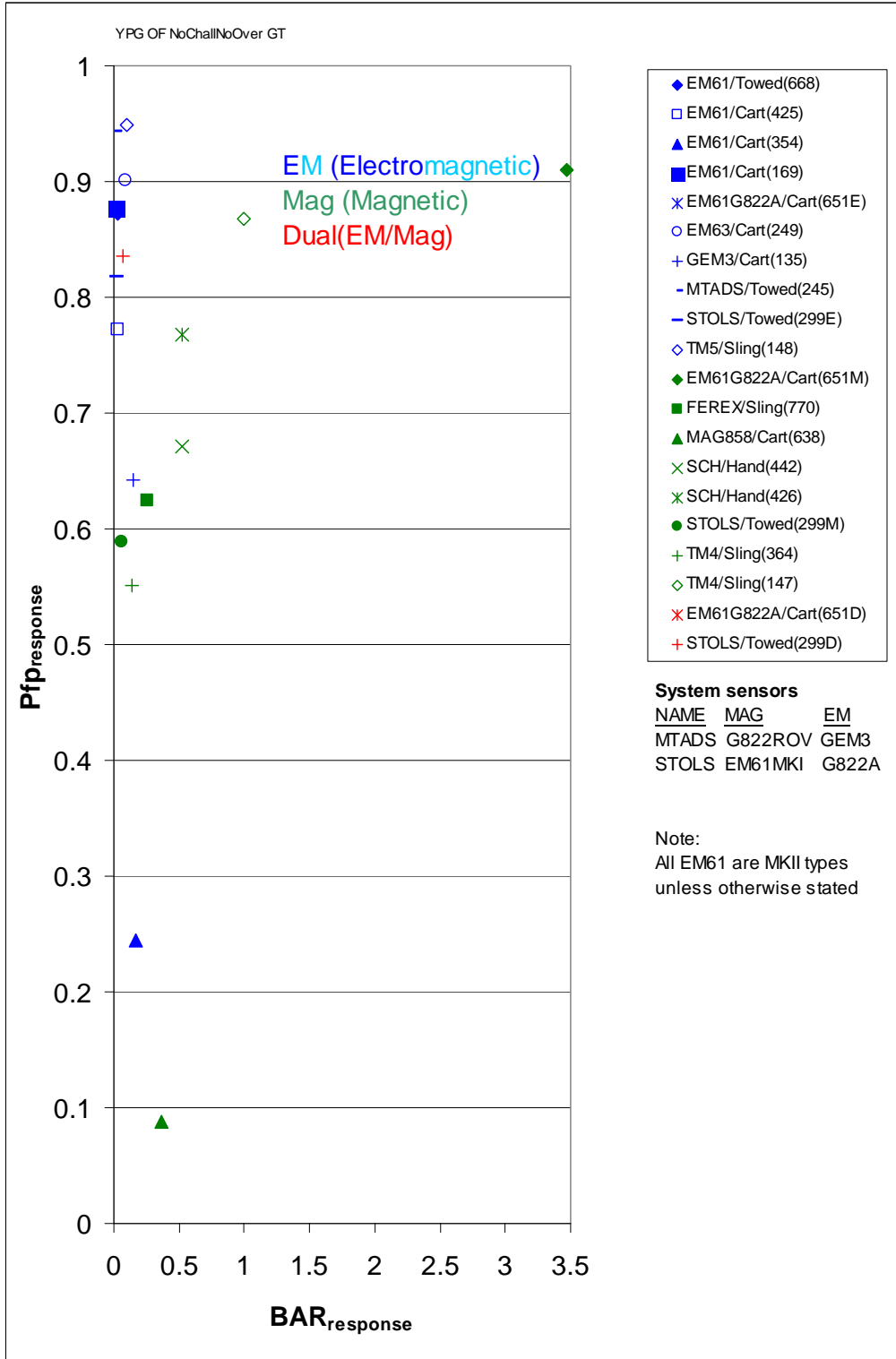


Figure 2.3.2-4. P_{fp}^{res} versus BAR^{res} , YPG open field, No Challenge, No Overlaps GT

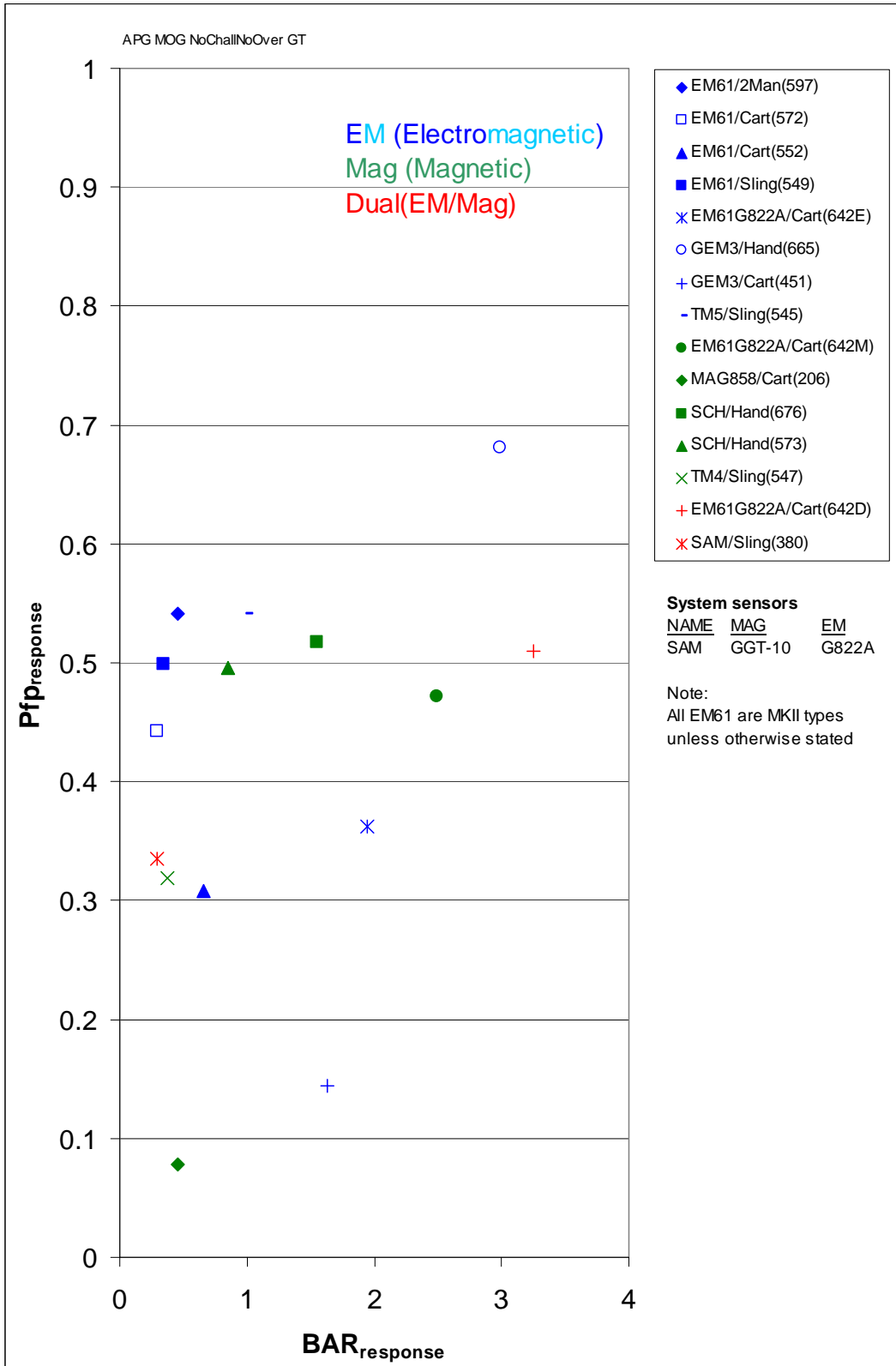


Figure 2.3.2-5. P_{fp}^{res} versus BAR^{res} , APG moguls, No Challenge, No Overlaps GT

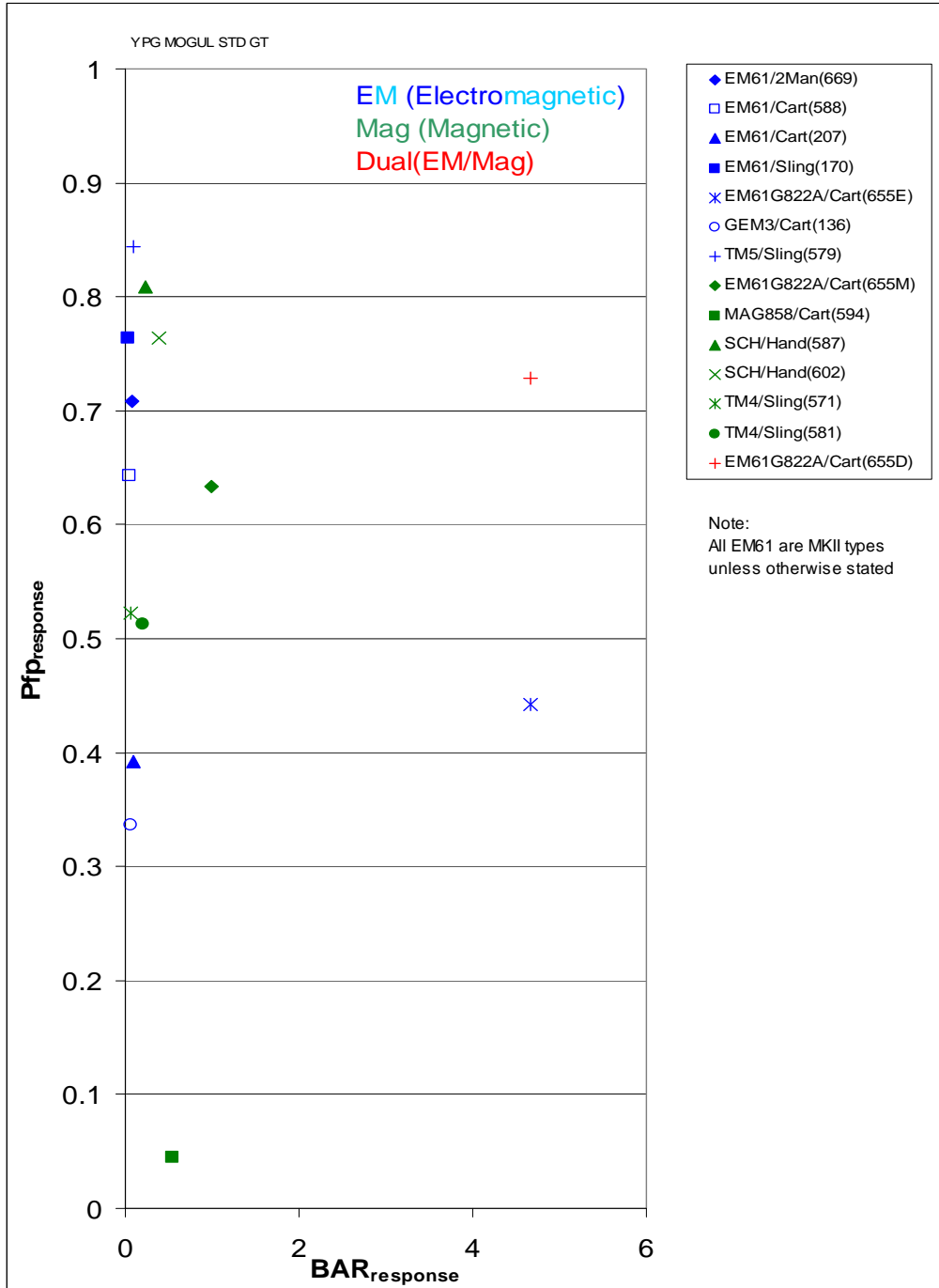


Figure 2.3.2-6. P_{fp}^{res} versus BAR^{res} , YPG moguls, No Challenge, No Overlaps GT

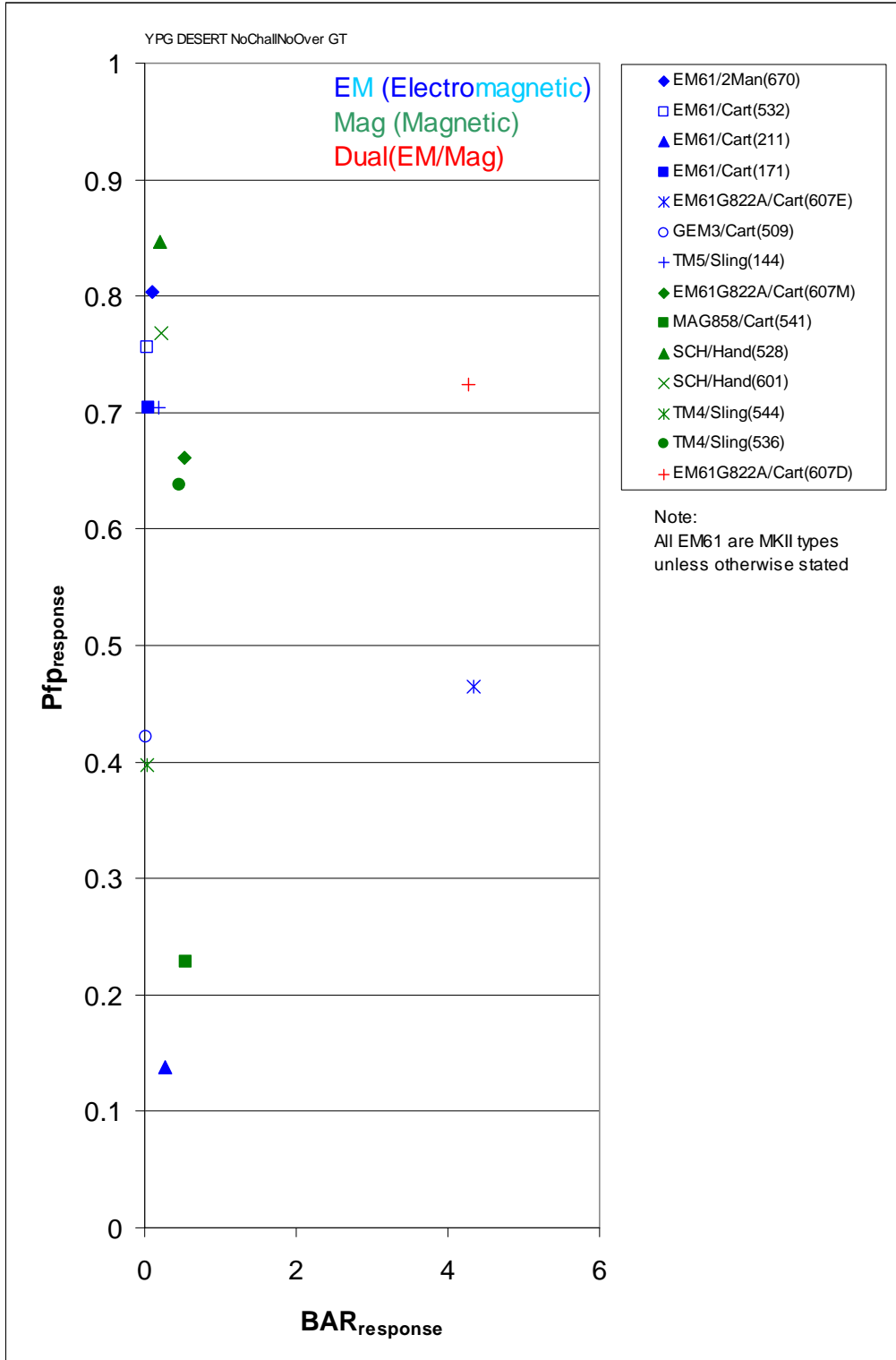


Figure 2.3.2-7. P_{fp}^{res} versus BAR^{res} , YPG desert extreme, No Challenge, No Overlaps GT

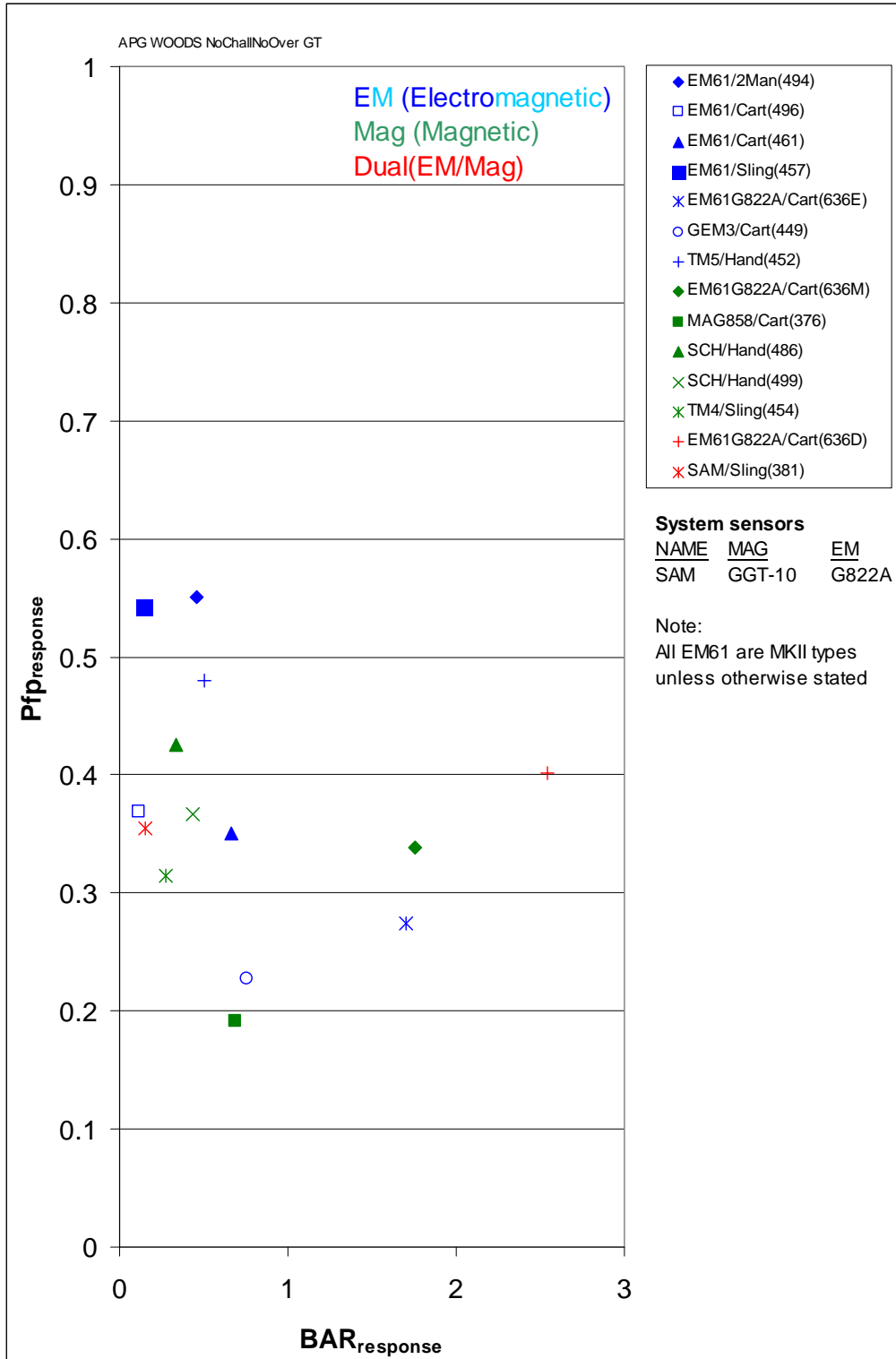


Figure 2.3.2-8. P_{fp}^{res} versus BAR^{res} , APG woods, No Challenge, No Overlaps GT

2.3.3 Ability to Discriminate

In this section various metrics will be used to show how well demonstrators were able to discriminate the items they detected using their systems. Results from standard GT sets are typically used. Time prohibited a full development of 11D, no challenge, no overlap results. However, section 2.3.3.2 will show results from both GT sets and it will be seen that little difference exists in the overall conclusion. Discrimination is defined as that ability to separate out ordnance items from clutter items in a list of anomalous targets (i.e., dig list) identified in the response stage. In the response stage, a list of potential ordnance items is submitted. In the discrimination stage, the items are identified as ordnance or nonordnance.

Note: Refer to section 2.1.3 for a thorough description of the discrimination process.

2.3.3.1 P_d^{disc} versus P_{fp}^{disc} Standard GT

a. Two of the more common metrics used (in published scoring reports from the sites) for evaluating discrimination capability are P_d^{disc} and P_{fp}^{disc} . While not the best metrics for showing discrimination ability alone, they do show “effective” detection results if discrimination is used. For review, P_d^{disc} is the number of ordnance items detected and correctly identified as ordnance, divided by the total number of ordnance in the GT. Up to this point only P_d^{res} has been used which looks only at the percentage of ordnance items detected, not the percentage detected and correctly identified. Similarly P_{fp}^{res} is a measure of the percentage of clutter items found. P_{fp}^{disc} is a measure of the number of clutter items detected and misidentified as ordnance (after discrimination has occurred) divided by the total number of clutter items in the GT. Thus, if P_{fp}^{disc} is greater than 0.5, a majority of the clutter items in the field are being detected and misidentified as ordnance.

b. When a demonstrator has no ability to discriminate or identify the anomalies that have been found, that demonstrator will likely err on the side of caution and identify all anomalies as ordnance. Thus, the demonstrator’s P_d^{disc} score will be the best possible ($= P_d^{res}$) but lack of discrimination ability will be manifest by the highest value of P_{fp}^{disc} possible ($= P_{fp}^{res}$).

c. If a demonstrator is detecting ordnance and clutter at the same level in the response stage, no discrimination ability will be manifest in a ratio of P_d^{disc}/P_{fp}^{disc} that is about equal to one. For example, if a demonstrator detects all of the GT ($P_d^{res} = P_{fp}^{res} = 1$) and randomly rejects half of the GT during discrimination, then the resulting P_d^{disc} and P_{fp}^{disc} values will be approximately 0.5. The ratio of P_d^{disc}/P_{fp}^{disc} will be close to 1.0 indicating no discrimination ability. However, if nearly all the items are discriminated correctly (i.e. high P_d^{disc} , low P_{fp}^{disc}) then the ratio will be substantially larger than 1.

d. P_d versus P_{fp} in the discrimination stage is shown in Figures 2.3.3-1 through 2.3.3-4 for open field and blind grid test areas at both proving grounds using the standard GT. When all four figures are looked at as a whole the community of demonstrators in general are performing near levels of equal probability (i.e., $P_d^{disc} = P_{fp}^{disc}$ or $P_d^{disc}/P_{fp}^{disc} = 1$), indicating little to no ability to discriminate.

e. In the figures, most plotted points trend parallel to the equal probability line. These points are consistently on one side of the line or the other. It is likely these trends are related to how easily clutter is being “detected” relative to ordnance. For example, clutter is harder to find at APG because the smaller items are buried relatively deep, therefore, P_{fp}^{res} scores are usually lower than P_d^{res} scores. If the same percentage of ordnance and clutter are correctly identified by the systems, P_d^{disc}/P_{fp}^{disc} will be greater than one and plotted points will typically fall above the equal probability line for most systems.

f. While P_d^{disc} and the P_{fp}^{disc} indicate a final percentage of items both detected and properly identified, the metrics are not the best way to measure discrimination ability alone. A more accurate way to determine how well a demonstrator is discriminating is by analyzing the shape of his receiver-operating characteristic (ROC) curve in the discrimination stage, as shown in section 2.3.3.3.

g. One of the more obvious results shown in Figures 2.3.3-1 through 2.3.3-4 is that after discriminating, the amount of false positives present is high, especially for those systems with the highest ordnance detection scores.

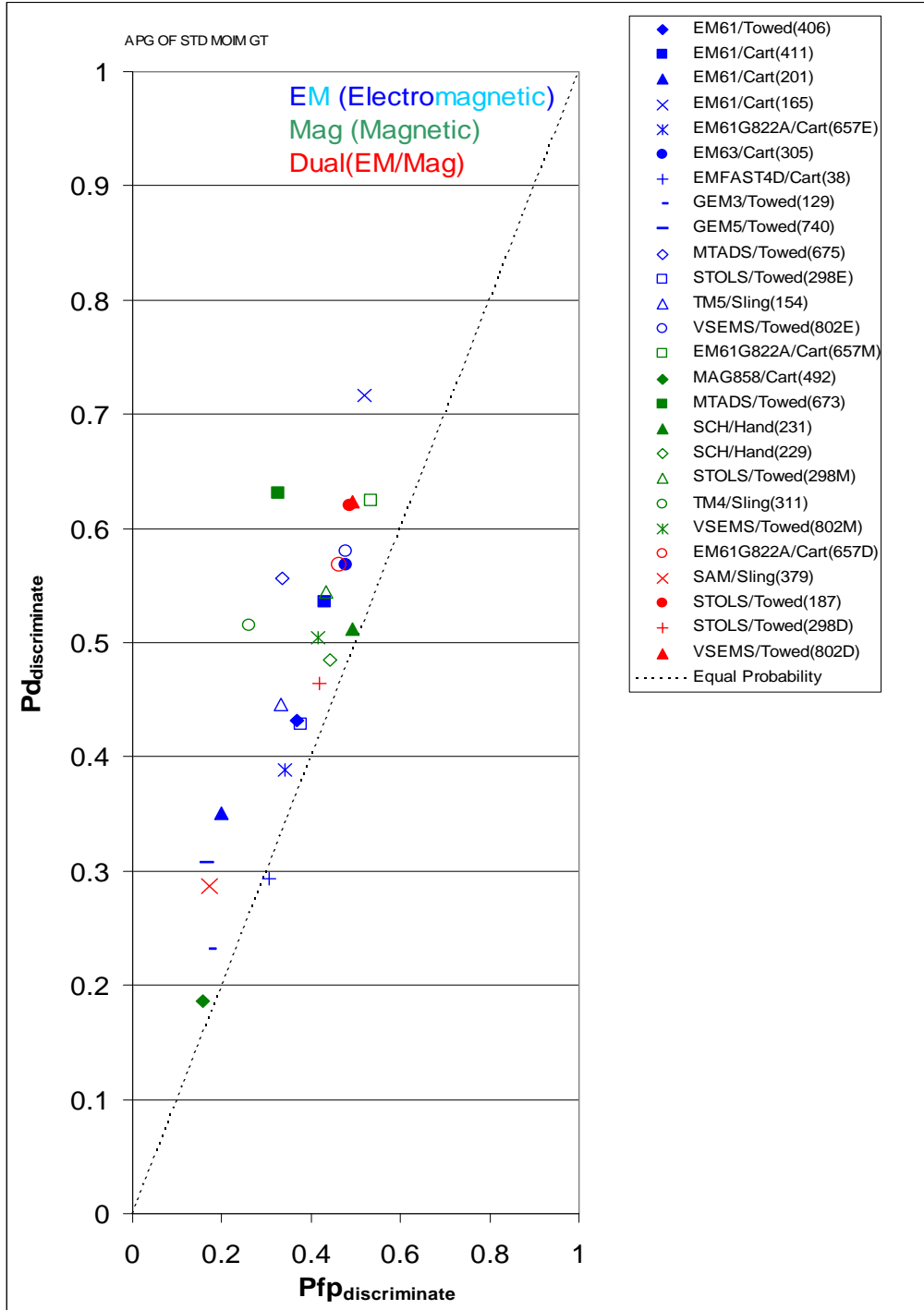


Figure 2.3.3-1. P_d^{disc} versus P_{fp}^{disc} , APG open field.

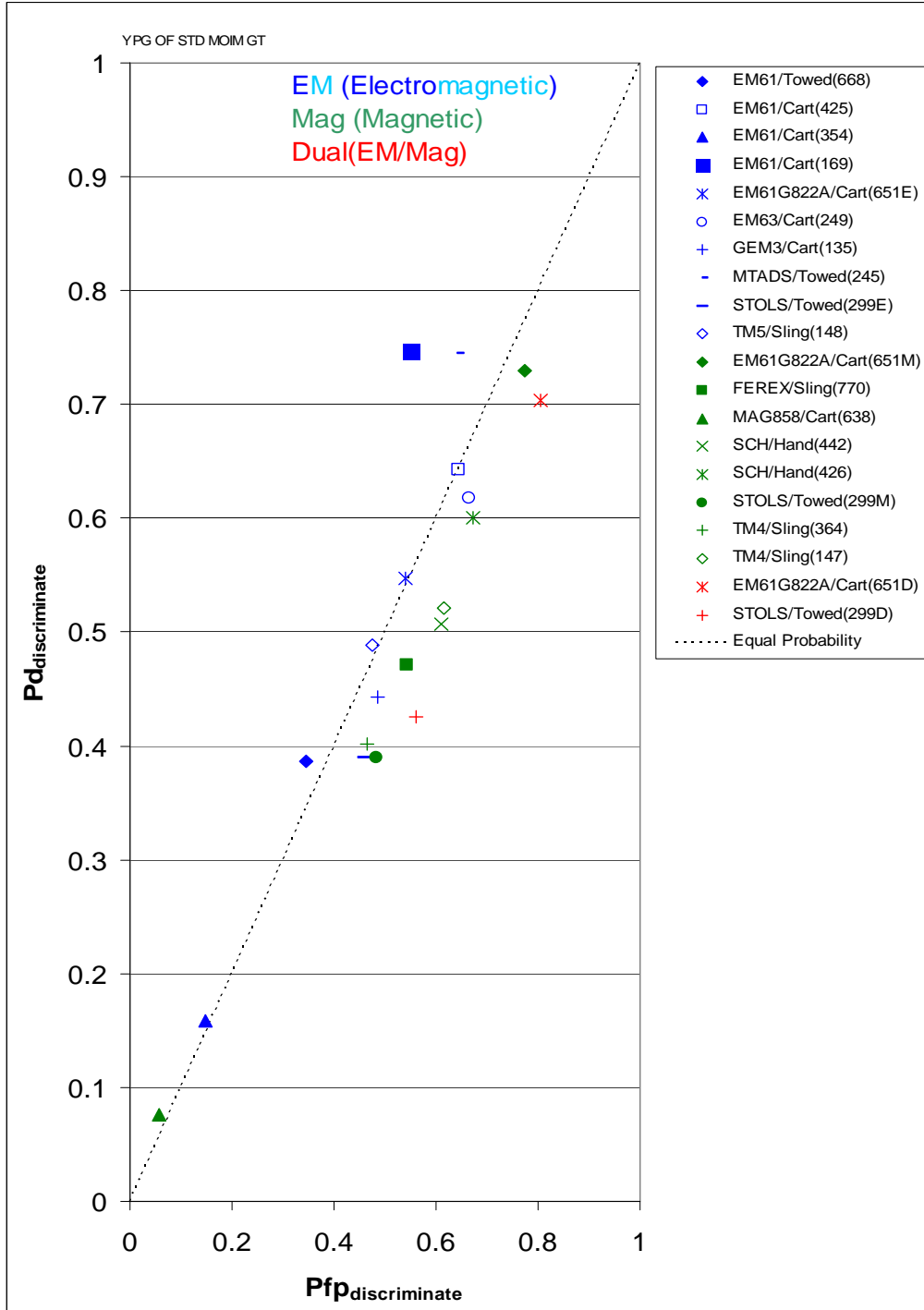


Figure 2.3.3-2. P_d^{disc} versus P_{fp}^{disc} , YPG open field.

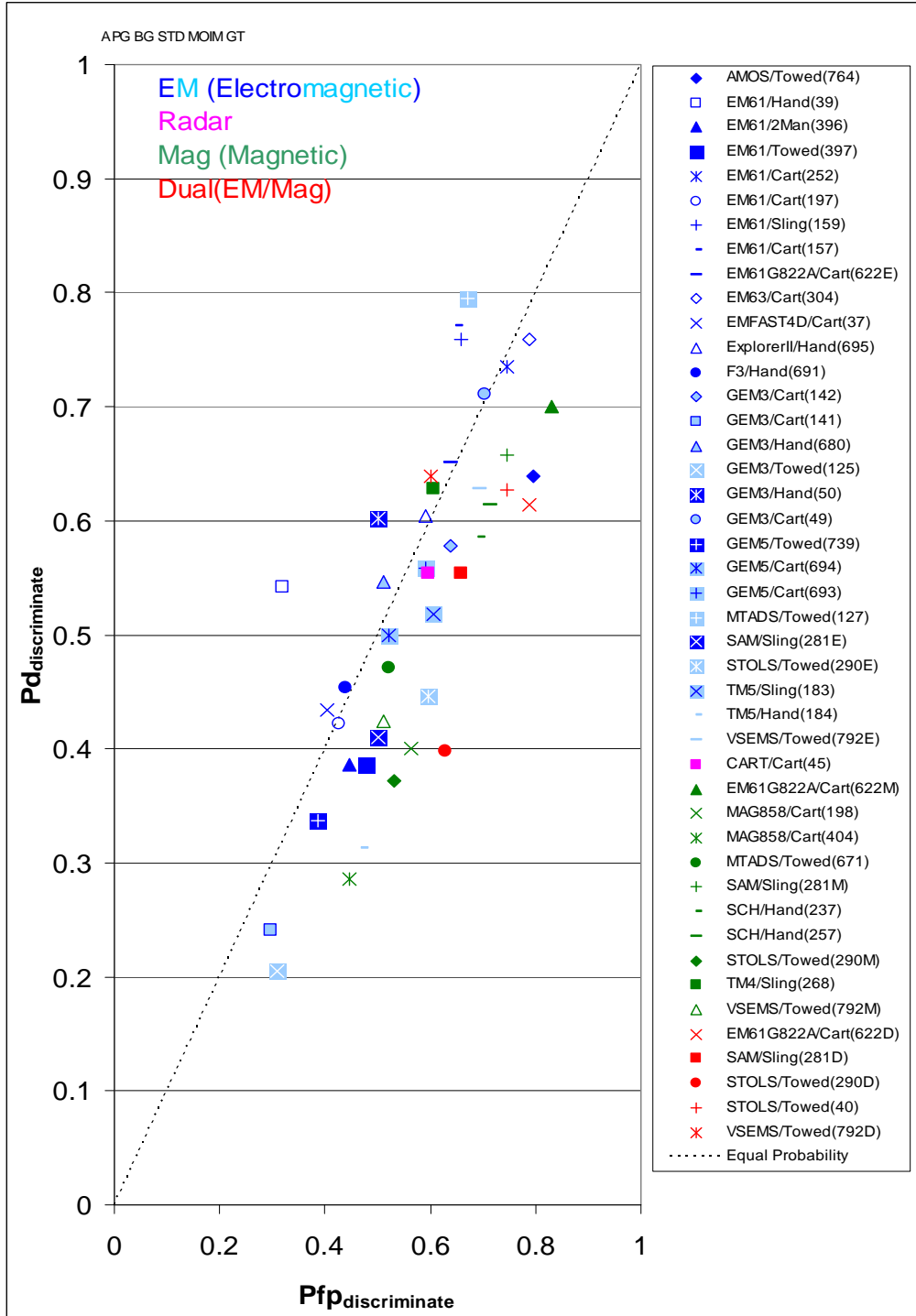


Figure 2.3.3-3. P_d^{disc} versus P_{fp}^{disc} , APG blind grid.

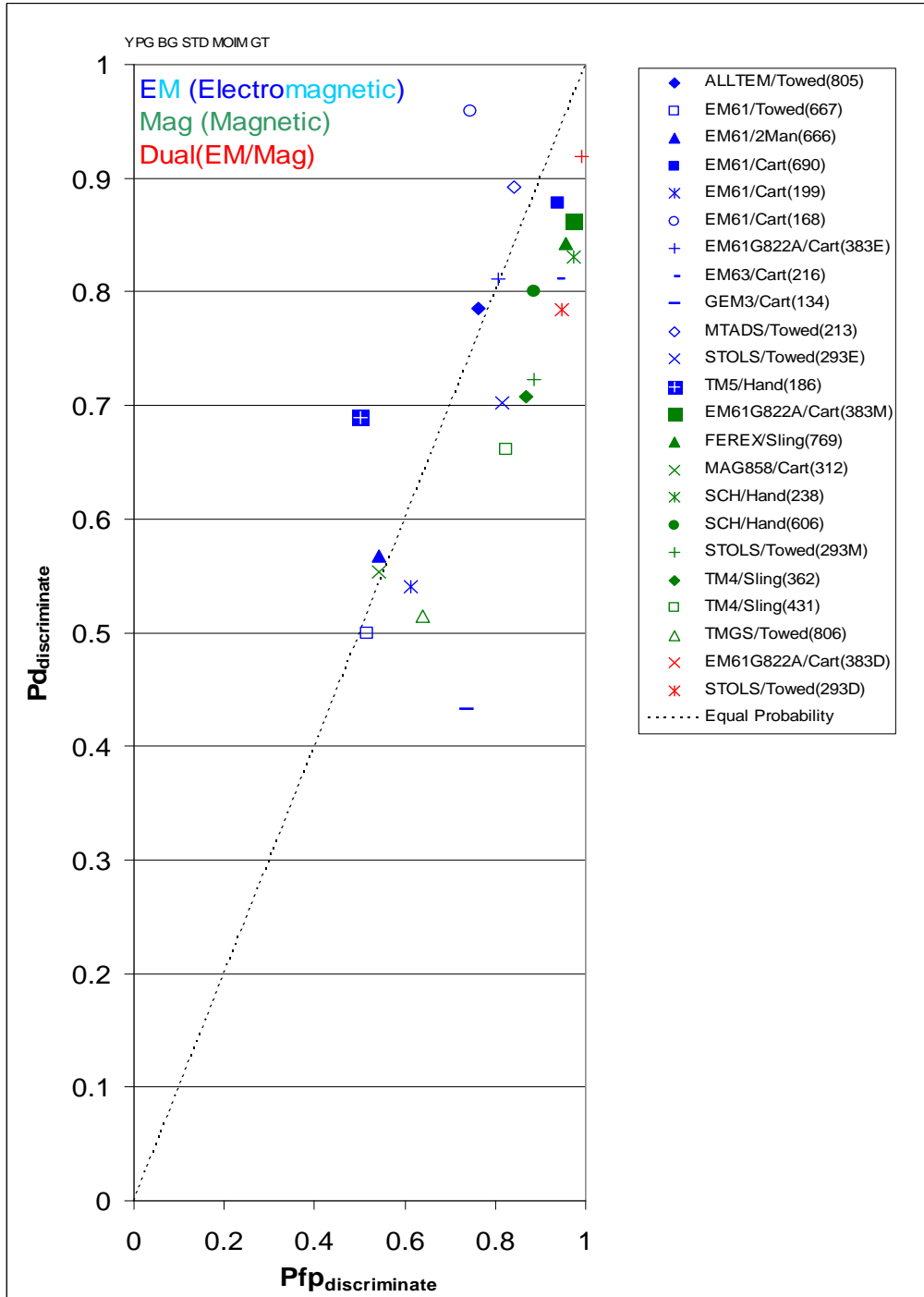


Figure 2.3.3-4. P_d^{disc} versus P_{fp}^{disc} , YPG blind grid.

2.3.3.2 Efficiency (E), R_{fp} , R_{ba} , and P_d^{res}

a. Three additional metrics were developed to help evaluate discrimination ability for the Standardized UXO program. These measures are efficiency (E) (the ability to retain ordnance), false positive rejection rate (R_{fp}), and background alarm rejection rate (R_{ba}). In effect, all three values are a measure of how efficiently items are being kept or rejected, where a value of 1.0 indicates optimum performance.

b. A demonstrator creates a list of anomalies believed to be potential ordnance in the response stage. In the discrimination stage the list is taken and reduced in size by rejecting items thought not to be ordnance. If all ordnance items from the response stage list are kept the demonstrator will be given an E score equal to 1.0 (100 percent of ordnance found are kept). If all of the clutter items are rejected and not carried forward into the discrimination stage list the demonstrator will have a R_{fp} of 1.0 (100 percent of clutter items are eliminated). Similarly, if all anomalies from the response stage list that were actually noise are eliminated in the discrimination stage list the demonstrator will have a R_{ba} score of 1.0 (100 percent of background alarms are rejected). Whereas P_d^{disc} and P_{fp}^{disc} relate the number of items properly and improperly identified to the entire amount possible in the GT, the above measures relate the number of items kept and rejected to the number of items of that type identified as anomalies in the response stage.

c. When all of these measures are plotted side-by-side, a better picture of the amount of effort exerted in discriminating is manifest. For example, a demonstrator may not discriminate at all and carry all anomalies over into the discrimination stage list and say they are ordnance. It appears the demonstrator has discriminated because the E (retaining ordnance) score for the effort is 1.0. However, when the percentage of clutter and background alarms rejected is examined by looking at associated rejection rates, these values will be zero.

d. E , R_{fp} , R_{ba} , and P_d^{res} (P_d^{res} showing the initial amount of ordnance detected) scores for systems demonstrated at the APG open field using the standard GT set are shown in Figure 2.3.3-6. The results are sorted on the measure of E , in descending order going from left to right. For the highest E scores on the left, no clutter or background alarms are being rejected as witnessed by the low scores for these measures. This indicates that discrimination was not attempted or was minimal in effort. As rejection rates for clutter and background alarms increase, the E value associated with retaining ordnance decreases (moving right on plot) until all three values meet at about 0.50. This indicates that clutter and anomalous noise currently cannot be discriminated by SOTA systems in the standardized test area configuration without significant ordnance rejection.

e. As shown in Figure 2.3.3-6, demonstrators have more success identifying and rejecting background alarms than they do clutter.

f. Results for the same test area as in Figure 2.3.3-6 but using an easier GT set are shown in Figure 2.3.3-7. The GT variant used is an 11D version where no ordnance depths exceed 11Ds. Further any items with overlapping halos (items within 1 m of another) and items in challenge areas (fence, power line, wet, etc.) are eliminated. This should serve to increase the signal to noise ratio of the GT set and eliminate items from the set that are difficult to access at times. Further, all non-ferrous ordnance are eliminated to allow direct capability comparisons between all sensor types.

g. As shown in Figure 2.3.3-7, the E level changed for various systems so that the sort order has changed. However, the overall trend is about the same as shown in Figure 2.3.3-6, with the exception that the P_d^{res} scores have improved. This indicates that the 11D depth limit and removal of overlaps had little effect on the ability to discriminate.

h. E scores for different ordnance types are addressed in section 2.3.5.6.

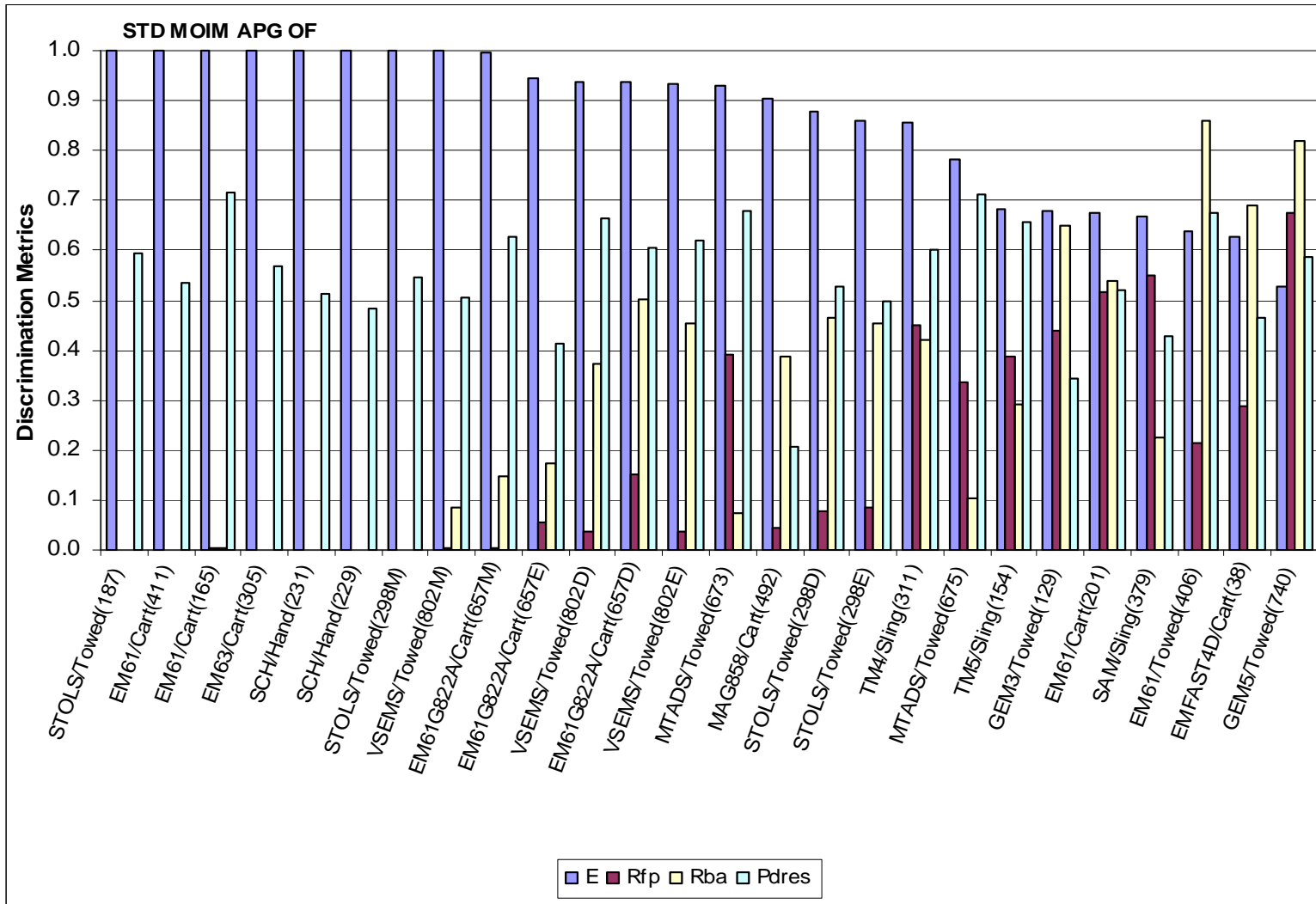


Figure 2.3.3-6. Discrimination metrics, E, R_{fp} , R_{ba} , and P_d^{res} , for various demonstrators at APG open field.

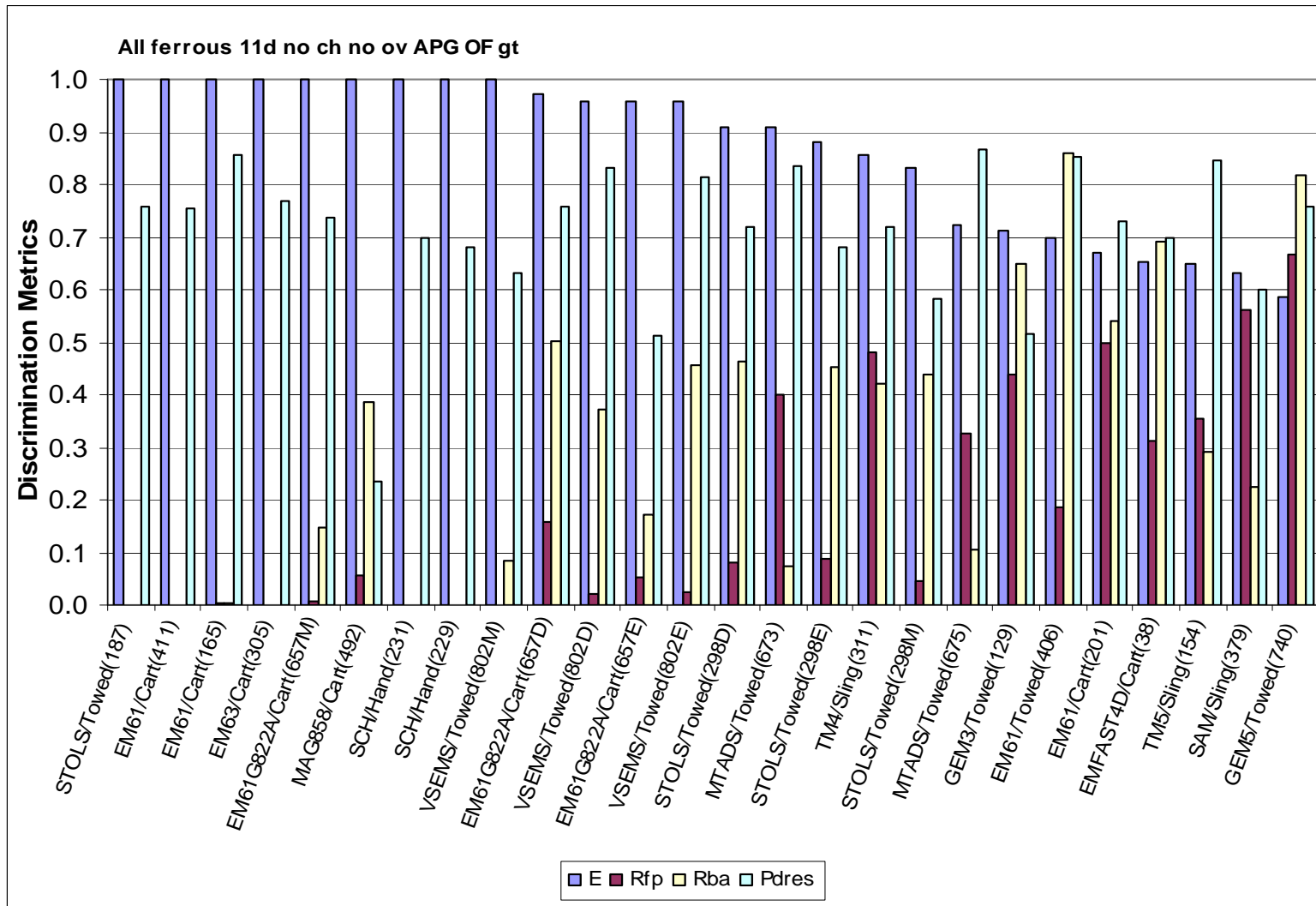


Figure 2.3.3-7. Discrimination metrics, E, R_{fp} , R_{ba} , and P_d^{res} , for various demonstrators at APG open field, all ferrous, 11D depth limit, no challenge area, no overlaps..

2.3.3.3 ROC Curves

a. In the discrimination stage, demonstrators are asked to refine their response stage anomaly list so those items likely to be ordnance are identified. The list is to be prioritized in descending order of likelihood that items are ordnance. This order allows the demonstrator to establish a threshold level where items above threshold are considered to be ordnance. All items below the threshold are considered likely to be clutter. The scoring authority will vary this threshold value to see if discrimination metrics improve or not. Results of varying the threshold values are included in published scoring reports and are also included in Figure 2.3.3-8 for APG open field results using the standard GT (report numbers are shown in the legend, refer to Table 2.2-1 to correlate with system types).

b. The metrics used in Figure 2.3.3-8 are P_d^{disc} versus $P_{\text{fp}}^{\text{disc}}$. Specifically, the figure shows a curve of how the metrics vary when the discrimination threshold value is varied from maximum to minimum (moving left to right on the plot). The curve is termed a ROC curve. An optimal curve is a vertical line with a $P_{\text{fp}}^{\text{res}}$ value of 0.0 that peaks at the fraction of ordnance detected and then goes horizontally to the right, ending at the fraction of clutter detected. If demonstrators have mostly ordnance at the top of their list, then a mix of ordnance and clutter for the remainder, the ROC curve will start out near vertical and then project out to the right at an angle. This type of curve shows some discrimination ability. If the demonstrators have a uniform distribution of ordnance and clutter throughout their list, the ROC curve will project out at a slope ~ 1 from the origin (assuming the percentage of ordnance and clutter detected are approximately the same). This type of curve indicates no discrimination was performed or no discrimination ability exists.

c. As shown in Figure 2.3.3-8, a majority of the curves have slopes near 1.0 indicating minimal to no discrimination ability. Two of the curves (reports No. 311 and No. 740) start out with a high slope that diminishes as $P_{\text{fp}}^{\text{disc}}$ increases. This indicates that most of the items on the top of the discrimination lists, which were most confidently affirmed to be ordnance, were indeed ordnance. Four of the curves start off with a slope near or below 1.0 but finish with a high slope and a respectable P_d^{disc} score. These curves are numbers 675, 165, 406, and 802D. These trends show that confidence rankings were deficient (in reverse order). Curve 673 starts with a slope near 1.0, but with a significant portion of the remaining curve at a characteristically good shape.

d. As indicated by the curves shown in Figure 2.3.3-8, changing the threshold values for most system results will not generally help or hinder the ratio of $P_d^{\text{disc}}/P_{\text{fp}}^{\text{disc}}$. Thus, feedback from the scoring authority on the effects of varying threshold values has not provided much aid in helping demonstrators refine their discrimination algorithms.

e. In summary, little discrimination ability is exhibited in the ROC curves of the detection system community. The TM-4/sling (report No. 311, G-TEK) and the GEM-3/towed (report No. 740, Geophex) systems were able to discriminate the best. Their ROC curves demonstrated trends somewhat consistent with proper confidence level rankings. The MTADs MAG system (report No. 673, Naval Research Laboratory (NRL)) also demonstrated noticeable discrimination ability. The large variety of ordnance and clutter at the sites, along with highly

dense areas of emplacement proved to make discrimination extremely challenging. It is expected that ability improves as the variety of items decrease and spacing increase.

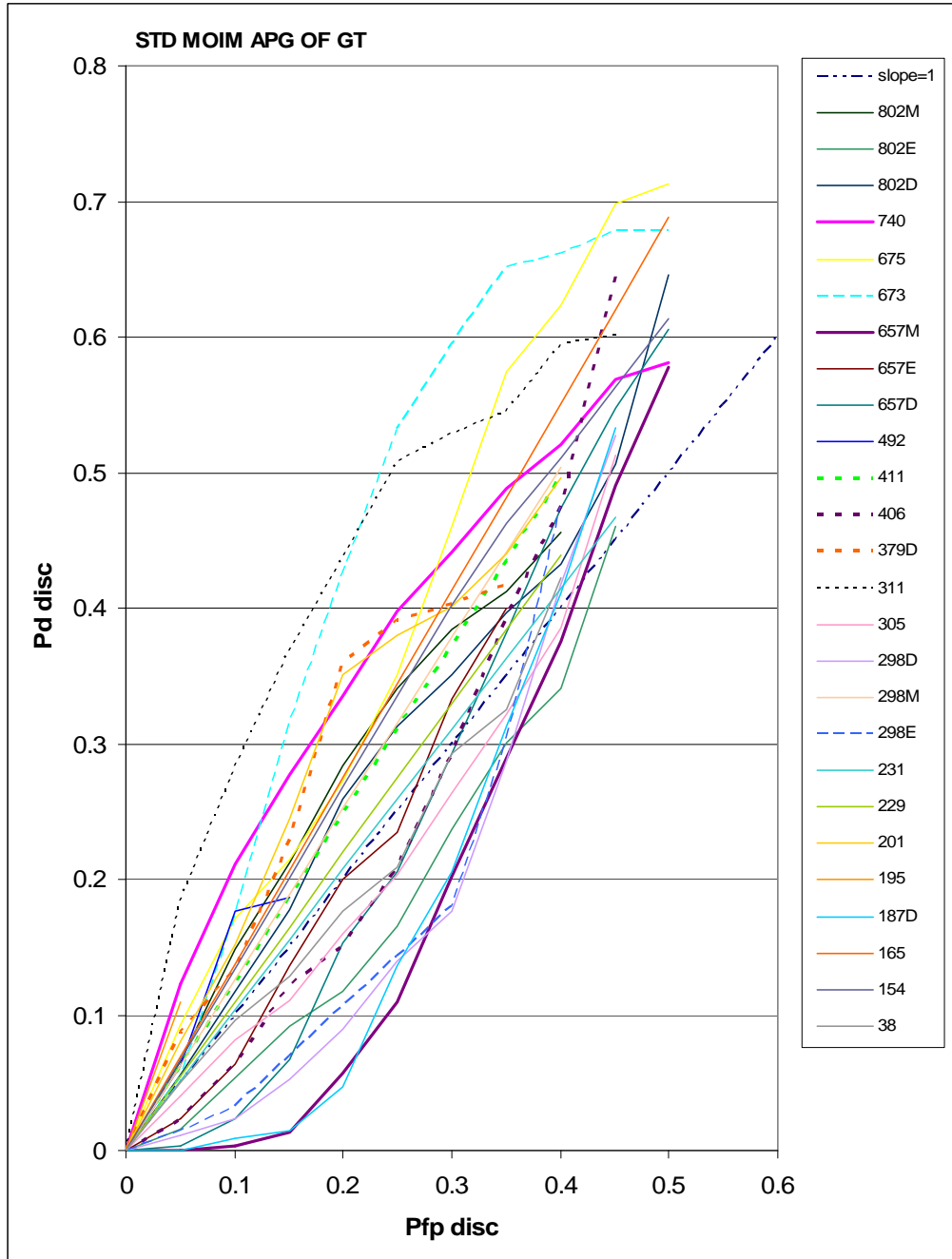


Figure 2.3.3-8. ROC curve, P_d^{disc} vs. P_{fp}^{disc} , for systems demonstrated at APG open field.

2.3.3.4 R_{fp} and R_{ba} Values at Optimum Efficiency (E)

a. The prioritized discrimination stage lists, of likely ordnance for each system demonstrated in the open fields, were processed to find the minimum threshold values that allowed all ordnance items from the response stage anomaly list to be retained. The percentage of clutter and background alarms that would be rejected at these threshold values were then calculated. These values, measured as R_{fp} and R_{ba} , are shown in Figures 2.3.3-9 and 2.3.3-10 for the APG and YPG open field. They are denoted as “optimum” values in the sense that no ordnance is rejected when discriminated and the maximum amount of clutter and background alarms below threshold are rejected. The values are shown beside values associated with threshold values chosen by the demonstrators.

b. When examining the optimum values of R_{fp} and R_{ba} , it is found that a very small portion of clutter and background alarms, typically much less than 15 percent, are rejected for a vast majority of the systems. Thus, if optimum thresholds could accurately be determined, it would be currently required that about 85 percent of clutter and background alarms found be dug up for SOTA technologies. This result is specific to the GT configurations at the test sites.

c. As shown in Figure 2.3.3-10, the EM61 MKII/pushcart combination (report No. 169) demonstrated by Tetra Tech Foster Wheeler (TTFW) not only performed best in the optimized list, but also had selected a threshold that was close to the optimum value. This system had the third best P_d^{res} score (= 0.76) at the YPG open field. The other systems that had some of the best rejection rates at optimum threshold did not have the best P_d^{res} scores (see section 2.3.1 results).

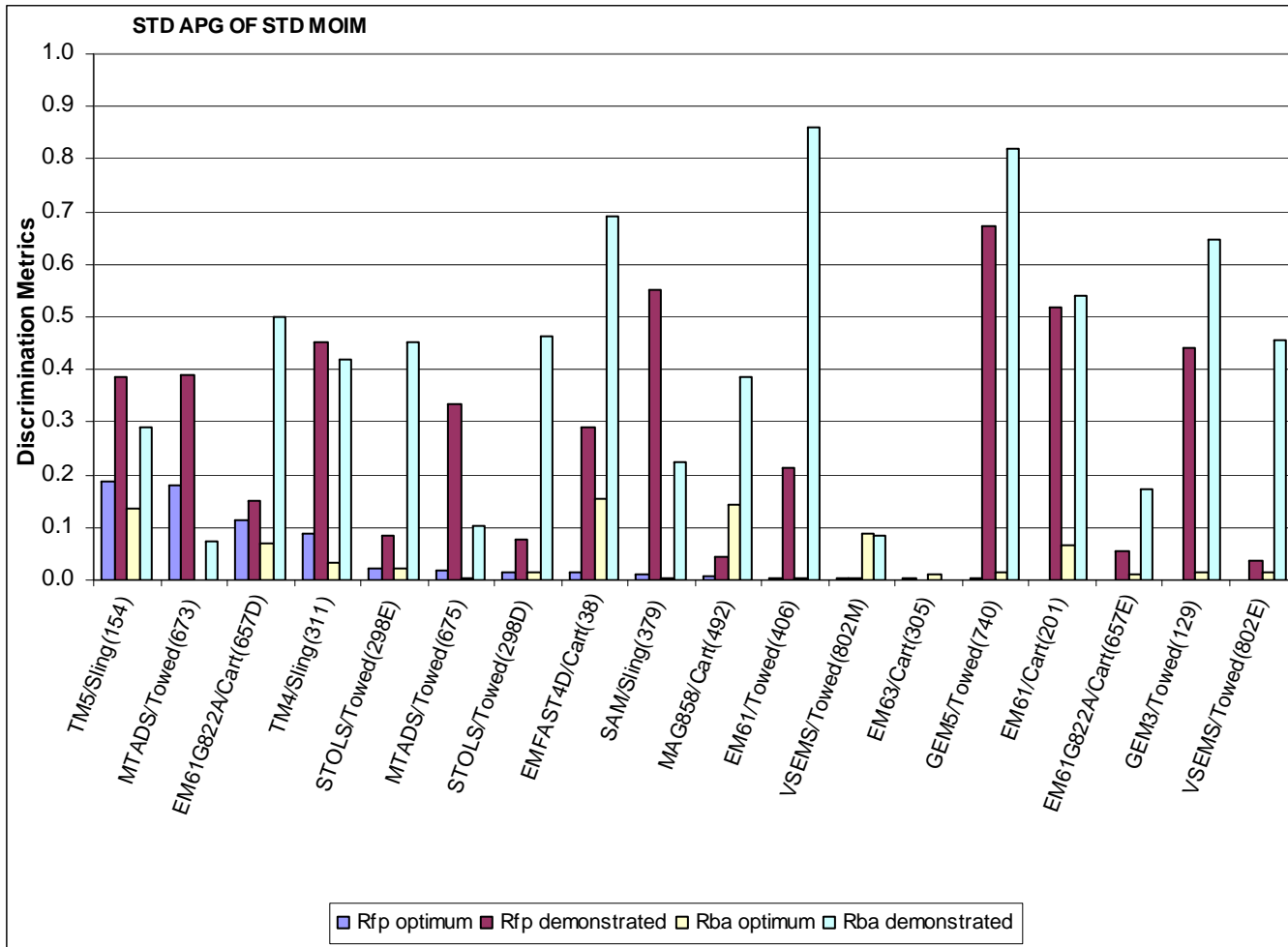


Figure 2.3.3-9. Discrimination metrics, R_{fp} optimum, R_{fp} demonstrated, R_{ba} optimum, and R_{ba} demonstrated, for various demonstrators at APG open field.

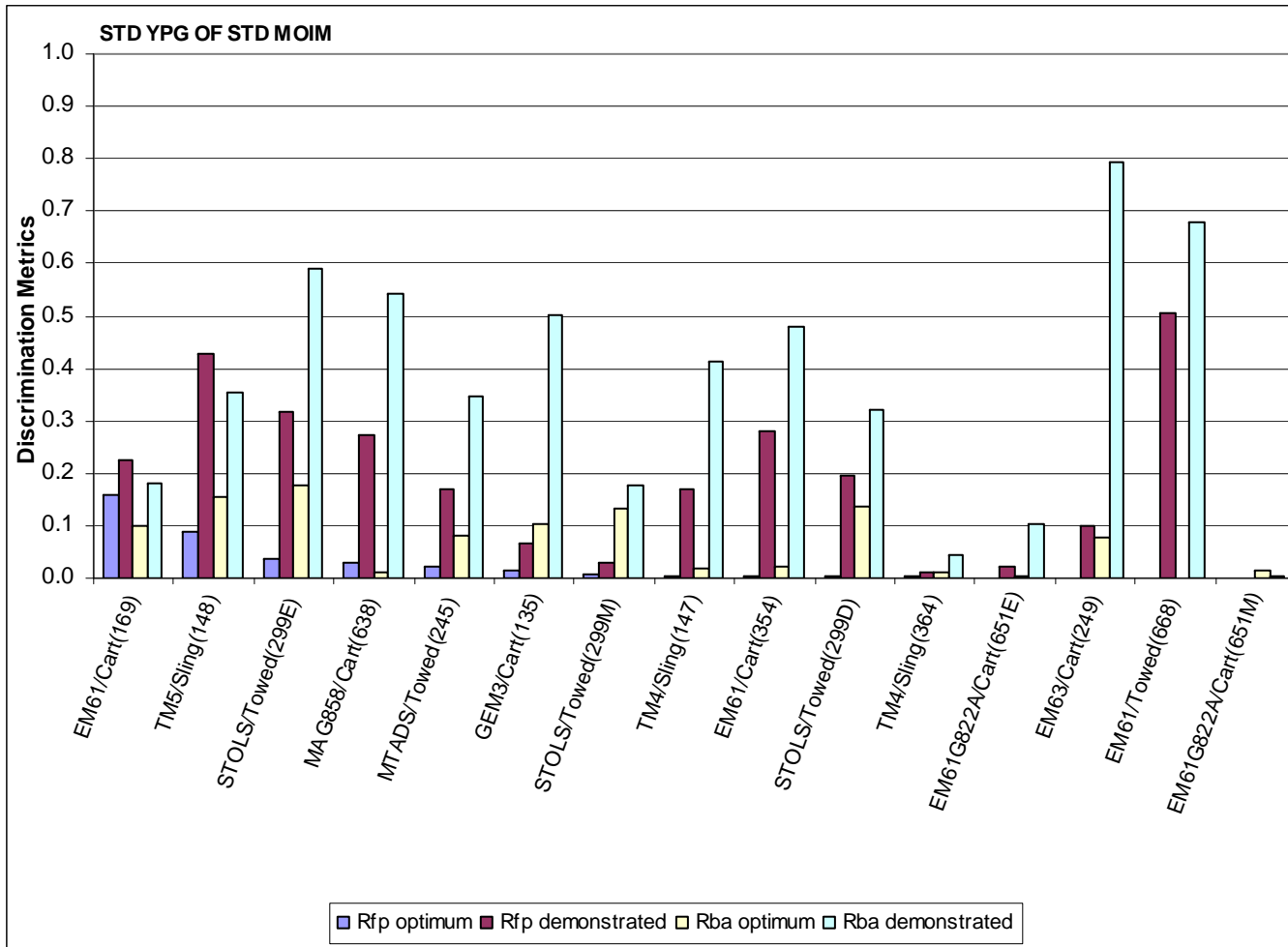


Figure 2.3.3-10. Discrimination metrics, R_{fp} optimum, R_{fp} demonstrated, R_{ba} optimum, and R_{ba} demonstrated, for various demonstrators at YPG open field.

2.3.4 Influence of Platform/Navigation/Location

Inaccuracies in the measurement of the location of the dig list at the sites can lead to lower P_d scores in the response stage. If the error in the determined location of a GT item is greater than 0.5 meter, then the anomaly will be outside of the scoring halo of the GT item and not considered a detection. Errors in navigation (guiding the platform) can lead to parts of the site not being surveyed. This could also lead to a lower P_d^{res} . These location and navigation errors can vary as a function of the platform type that is used, the area that is surveyed and the navigation/positioning system itself. This section analyzes the navigation and location errors of the detection systems demonstrated at the standardized sites.

2.3.4.1 *Improvement in P_d^{res} (When Only Ground Covered is Used)*

a. All demonstrators who survey the standardized UXO test sites are required to supply their minimally processed raw data, if such is available. In most cases the data are in a standard form that can be loaded into a large database so that the data from each vendor can be compared. Typically, the data includes the location where each measurement is taken. In addition to these minimally processed data, the vendor supplies the lane spacing that is used while surveying the site. When vendors survey the sites they typically take data while moving back and forth over the site in relatively straight lines. The lane spacing is the distance between these lines.

b. By comparing the location of the GT with the location where the demonstrator collected each data point, it is possible to measure the minimum distance between the GT item and where data has been collected. If that distance is greater than one half the demonstrator's lane spacing, it is assumed that the vendor did not collect enough data to properly survey the item. So for each vendor who supplied data in a standard format it is possible to tabulate a list of GT items where insufficient data was collected to accurately survey. It is then possible to create a custom GT for which each vendor collected adequate data to properly survey. In this way it is possible to explore the effects of incomplete coverage on the vendor's P_d^{res} score.

c. P_d^{res} results with and without the items that were not (based on lane spacing) properly surveyed as part of the GT are shown in Figures 2.3.4-1a through 2.3.4-1c. In each of these figures, items that were buried deeper than 11 times their diameter, items that are closer than 1.0 meter to another item, and items in challenge areas were eliminated from the GT. The figures show results for the APG open field, woods, and moguls, respectively. Both sets of results are not present for all systems because of insufficient data.

d. In most cases there is an increase in P_d^{res} , typically 0.01 to 0.05, when the items inadequately surveyed are eliminated. If there is no increase in P_d^{res} after these items are removed, then this would indicate that either the vendor surveyed the entire site or that the sensor used was capable of properly surveying beyond the lane spacing used.

e. In addition to incomplete coverage, the terrain of the site could make it impossible for some vendors to survey some parts of the site using a chosen platform. In the open field, areas that were difficult for vendors to survey (i.e., wet and fenced areas) were deemed challenges and were eliminated from the GT when generating Figure 2.3.4-1a. However, much of the woods and moguls are meant to be difficult for vendors to survey. This difficult terrain may lead to the slightly larger increases in P_d^{res} seen in Figures 2.3.4-1b and 2.3.4-1c.

f. The figures below conclude that better quality controls on navigation would benefit the detection rates of many systems.

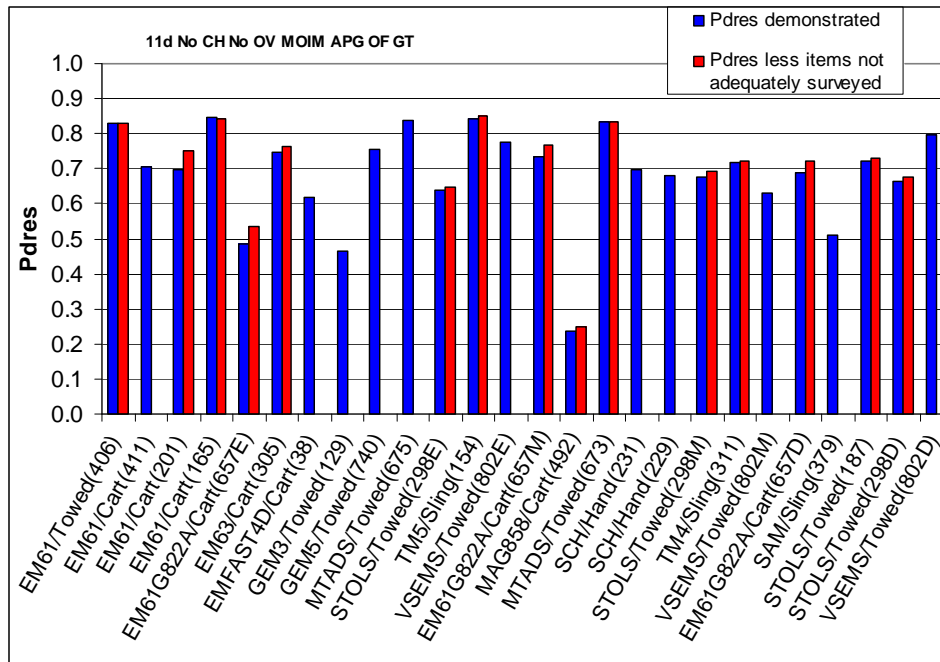


Figure 2.3.4-1a. P_d^{res} with and without items that were not adequately surveyed for each platform type, APG open field, 11D limit, no challenges, no overlaps.

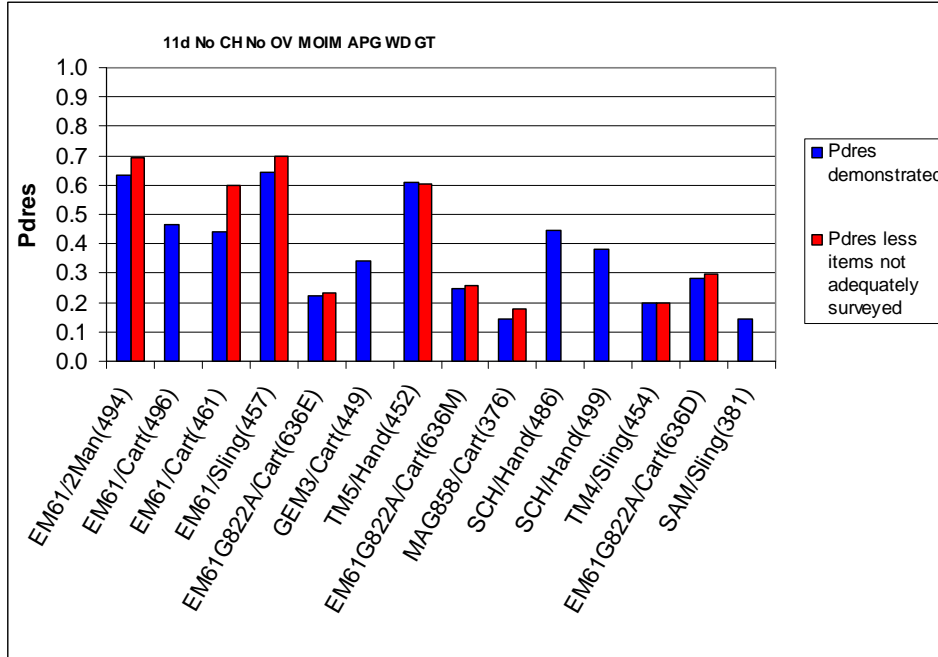


Figure 2.3.4-1b. P_d^{res} with and without items that were not adequately surveyed for each platform type, APG woods, 11D limit, no challenges, no overlaps.

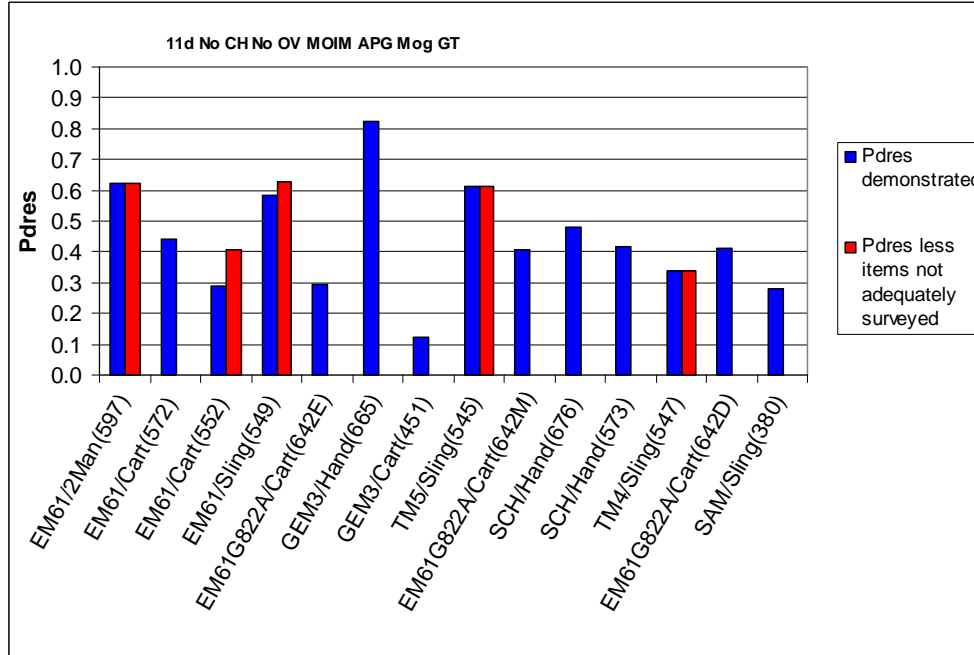


Figure 2.3.4-1c. P_d^{res} with and without items that were not adequately surveyed for each platform type, APG moguls, 11D limit, no challenges, no overlaps.

2.3.4.2 Location Error for Demonstrators Tested

a. This section examines the location errors demonstrated by the detection systems at the test sites. By comparing the location of a demonstrator's anomalies to the location of the matching GT items it is possible to study location error. It is difficult to account for location error if the distance between the anomaly and the intended matching GT item is sufficiently large to make the anomaly a background alarm. In this study, an anomaly exceeding a 0.5-meter distance to a GT item will not be counted toward the demonstrator's P_d^{res} but will be assumed a background alarm by virtue of scoring criteria. Therefore, location error will only be calculated for each anomaly that is within 0.5 meter of its intended matching GT item.

b. When the GT items were buried at the UXO sites, great care was taken to accurately record the location of each item. However, some error in measurement of the location of each GT item can still be expected. In addition, once these items are buried, phenomena such as frost heave, or the effect of heavy surface equipment traversing the area, may change the location of the items. Settling may also contribute to GT migration. When the UXO sites were reconfigured from 2004 through 2005, many GT items were extracted from the ground. The locations of the items were measured during this process so that effects of migration and error in measuring location could be bounded after calculating distances from the original burial positions. The mean difference calculated represents inaccuracy of the GT locations. The inaccuracy value represents the minimum location error that the vendors could be expected to obtain when they are surveying the site. The values obtained from the reconfiguration effort were 0.06 meter for inaccuracy and 0.07 meter for the corresponding standard deviation (may be termed uncertainty). These values were obtained from part of the GT in the APG open field.

c. Location error versus the standard deviation in location error between the vendors' anomalies and matching GT items in different test areas is shown in Figures 2.3.4-2 through 2.3.4-7. The inaccuracy and uncertainty in GT location is also shown in Figure 2.3.4-2 for reference.

d. In each figure, the location error and the standard deviation of that error for the systems decrease together toward the inaccuracy and uncertainty in the location of the GT. These trends are indicated by the lines bounding a majority of the points, which trend not toward (0, 0) but some finite value. One laser based system will typically not trend with a majority of systems that are GPS based.

e. Some of the smallest location errors were obtained by vendors using towed arrays or those who were using MAG and Flag or EM and Flag systems. It is likely that the towed array systems are yielding more accurate location measurements because the stability of the platforms makes it easier to produce more accurate GPS measurements. The MAG and Flag vendors are likely producing smaller location errors because when the operator finds an anomaly the vendor can immediately resurvey the area in order to place his flag as accurately as possible. Once the flag is placed the locations of the flags can be accurately measured by a non-moving system.

f. The smallest location error, 0.09 meter, was produced by a towed array system in the YPG open field. Otherwise, minimum location errors were typically about 0.15 meter. This minimum is slightly higher at the APG moguls. If the 0.06-meter inaccuracy in the GT location in the APG open field is taken into account, the best location errors by the systems will be lower in that test area.

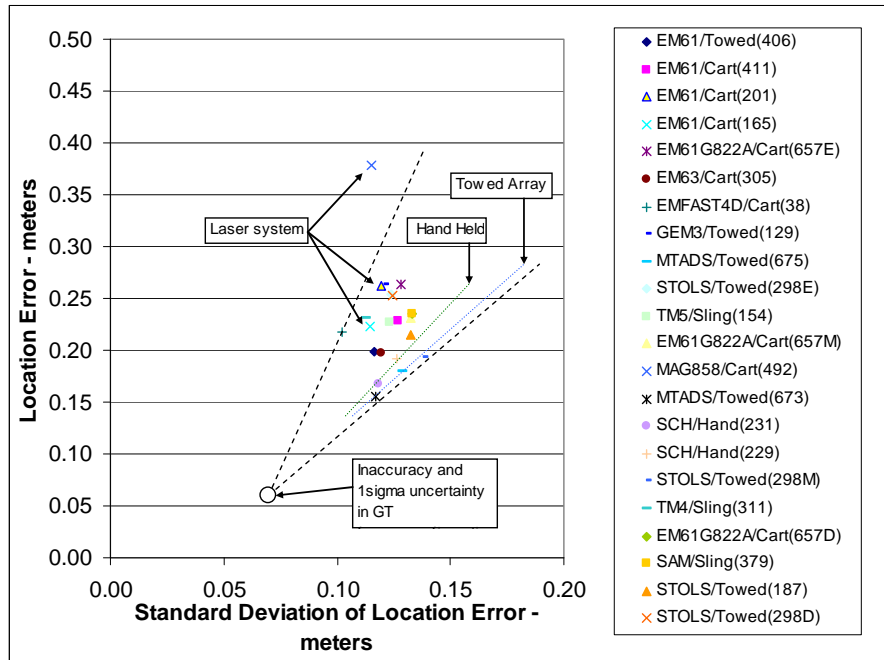


Figure 2.3.4-2. Location error versus standard deviation of location error for all systems, APG open field.

g. Demonstrators were asked to give the location of the center of the anomaly they detected. An element of signal interpretation that plays into the location errors is inevitable. Analysis of this is beyond the scope of this work.

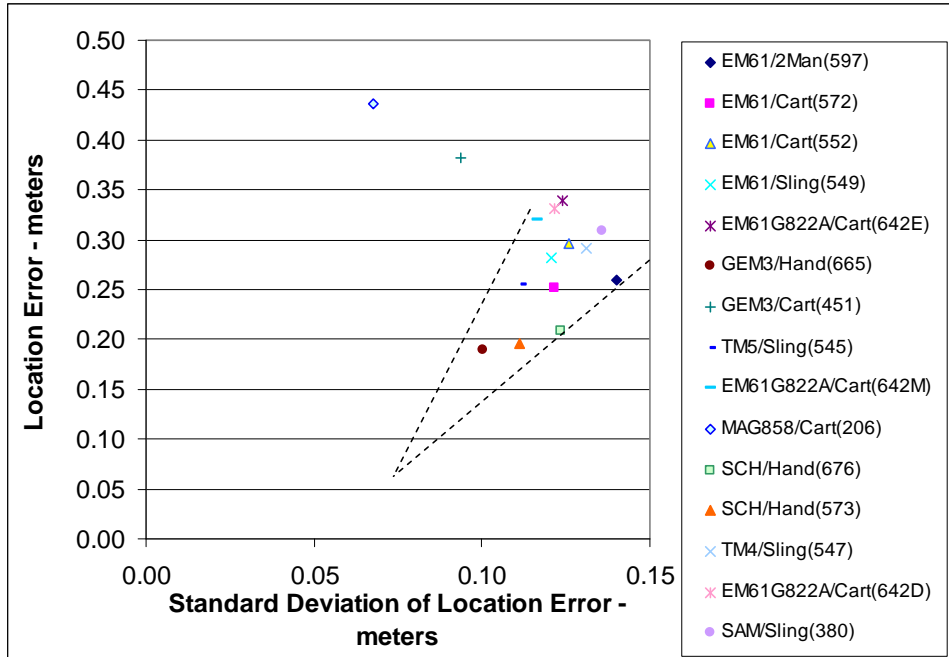


Figure 2.3.4-3. Location error versus standard deviation of location error for all systems, APG moguls.

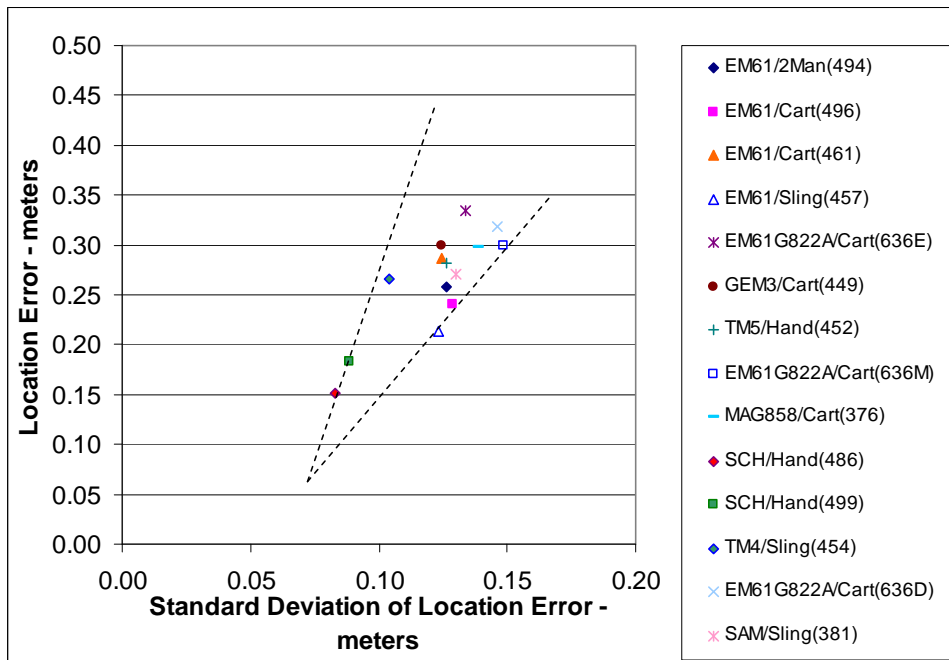


Figure 2.3.4-4. Location error versus standard deviation of location error for all systems, APG woods.

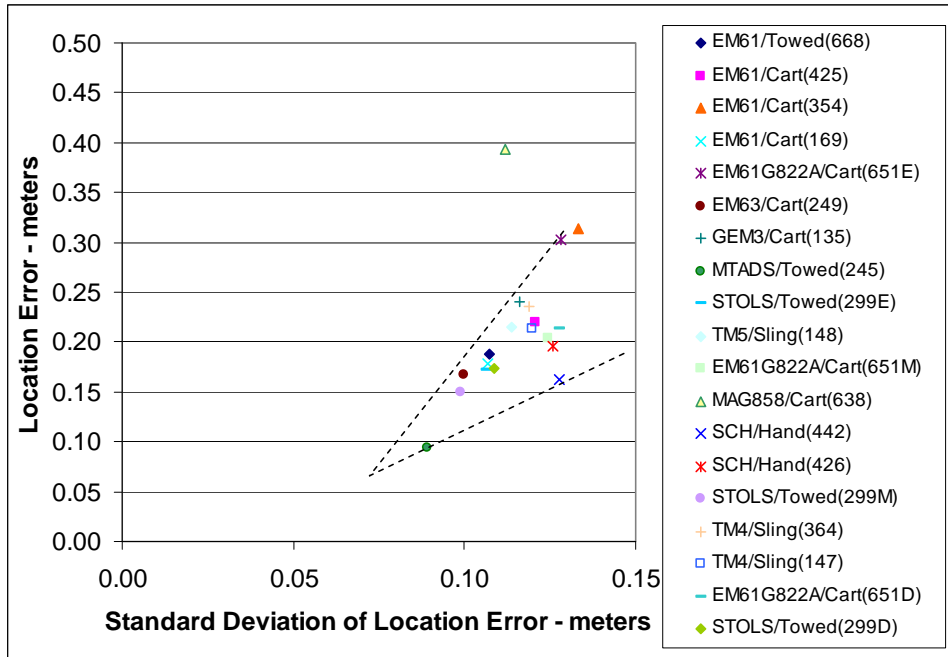


Figure 2.3.4-5. Location error versus standard deviation of location error for all systems, YPG open field.

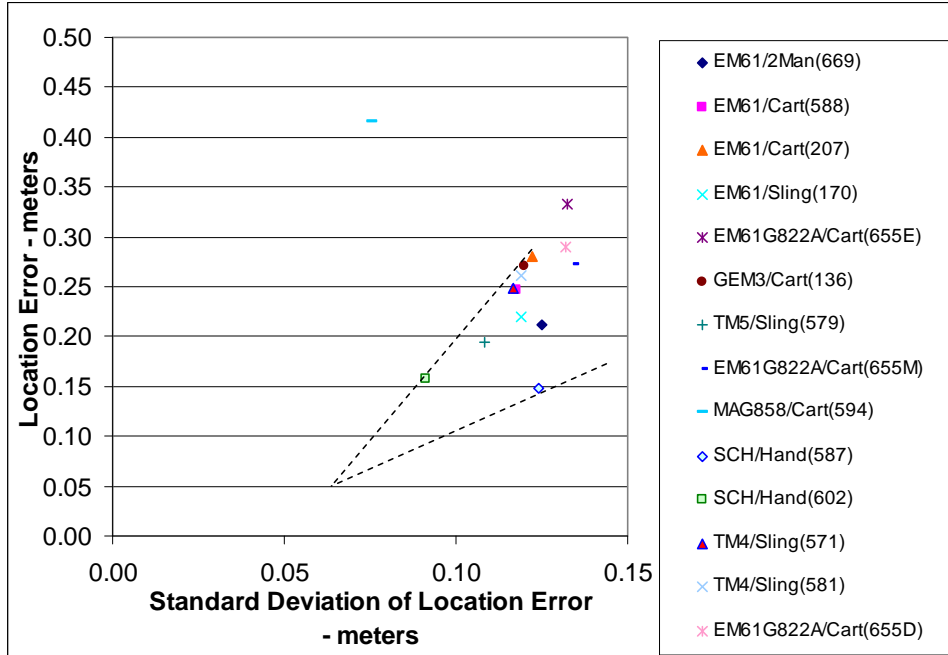


Figure 2.3.4-6. Location error versus standard deviation of location error for all systems, YPG moguls.

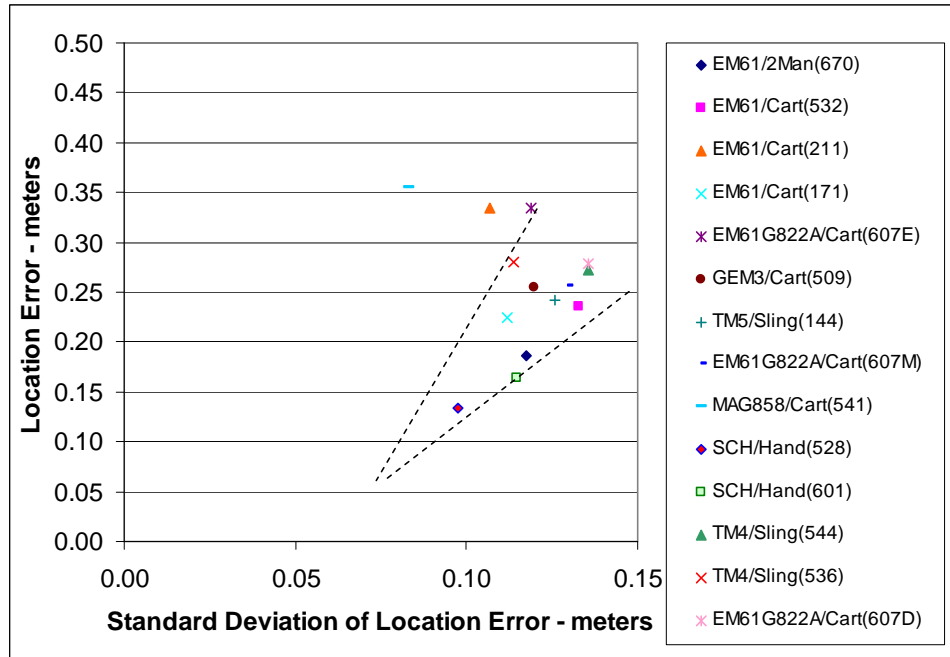


Figure 2.3.4-7. Location error versus standard deviation of location error for all systems, YPG desert.

2.3.4.3 Comparative Results for Platform and Areas

a. Once the location error for each vendor that surveyed the UXO sites was analyzed, a comparison of the minimum location error that demonstrators produced as a function of the platform and the site being surveyed was made. A location error scale was created to allow a quick look at relationships.

b. A comparison of the minimum location error for each type of platform in each area at the UXO sites is presented in Table 2.3.4-1. Consistent with section 2.3.4.2, the towed array and hand held systems allow a good or excellent minimum location error for each area that was surveyed. The hand held units accessed all areas whereas the towed array units did not. In the open field, demonstrators produced a lower minimum location error using a pushcart than a sling. This may have been due to the greater stability of the pushcart platform. As terrain becomes more difficult to traverse, as in the YPG desert moguls, the lowest location error was produced using a hand held unit. In the most difficult terrains such as YPG desert extreme, APG moguls, and APG woods, the hand held units still had the best error. As the terrain changed, the ability of systems to accurately determine the location of GT items was largely a function of platform type.

TABLE 2.3.4-1. BEST LOCATION ERROR RESULTS FOR PLATFORM/AREA

| Terrain | Site | Towed Array | Pushcart | 2 Man | Sling | Hand Held |
|----------------------------------|------|-----------------------------|----------------------------|----------------------------|----------------------------|------------------------|
| Wooded | APG | No data Min= N/A N= 0 | Marginal Min= 0.24 N= 7 | Marginal Min= 0.26 N= 1 | Marginal Min= 0.21 N= 3 | Good Min= 0.15 N= 3 |
| Moguls - Marsh | APG | No data Min= N/A N= 0 | Marginal Min= 0.25 N= 7 | Marginal Min= 0.26 N= 1 | Marginal Min= 0.25 N= 4 | Good Min= 0.19 N= 3 |
| Moguls - Desert | YPG | No data Min= N/A N= 0 | Marginal Min= 0.25 N= 7 | Marginal Min= 0.21 N= 1 | Good Min= 0.19 N= 4 | Good Min= 0.15 N= 2 |
| Open Field - Loam | APG | Good Min= 0.16 N= 8 | Good Min= 0.20 N= 9 | No data Min= N/A N= 0 | Marginal Min= 0.23 N= 3 | Good Min= 0.17 N= 2 |
| Open Field - Desert | YPG | Excellent Min= 0.09 N= 5 | Good Min= 0.17 N= 9 | No data Min= N/A N= 0 | Marginal Min= 0.21 N= 3 | Good Min= 0.16 N= 2 |
| Desert Extreme - Brush/Eroded | YPG | No data Min= N/A N= 0 | Marginal Min= 0.22 N= 8 | Good Min= 0.19 N= 1 | Marginal Min= 0.24 N= 3 | Good Min= 0.13 N= 2 |

Location Error Scale

| | |
|-----------|-----------|
| Excellent | 0-0.1 m |
| Good | 0.1-0.2 m |
| Marginal | 0.2-0.3 m |
| Poor | 0.3-0.4 m |

← Indicates best error value among systems demonstrated and number of systems tested

2.3.4.4 Percentage of Ordnance Possibly Missed Because of Location Error

a. Many of the systems would have a slightly increased P_d^{res} value if their location error were better. The variation in their existing location error extends beyond 0.5 m and therefore precludes some anomalies from being considered a hit. It is difficult to determine the difference between a true background alarm and a legitimate hit as distance from a GT item increases. An effort to estimate the reduction in P_d^{res} being caused by location error was made so that P_d^{res} increases possible with improving locating methods/technologies might be quantified.

b. To estimate the reduction in P_d^{res} resulting from location error, histograms of location error within the allowable halo radius were plotted. Next, a characteristic distribution that best described the histograms was found. It was determined that a Weibull distribution that is skewed right fitted most system results best. The estimated cumulative probability of location error was then plotted on a Weibull chart. Total population was based upon the fit of the distribution which typically extended beyond 0.5 meter. The cumulative probability at the intersection of the line fitting the distribution and a line denoting a 0.5-meter halo radius was used as an estimate of the ordnance population that will be found at location errors below 0.5 meter. The difference between that value and 100 percent was used as an estimate of the percentage of ordnance likely missed given the 0.5-meter criterion. Populations of items less than 0.6 meter long were used since these items do not require an elliptical halo which can exceed a 0.5-meter radius. These items comprise approximately 84 percent of the APG open field GT (used for study).

c. A typical histogram for one of the systems processed is shown in Figure 2.3.4-8, and the corresponding probability plot is shown in Figure 2.3.4-9. The data are from an NRL system demonstrated at APG open field. Past 0.5 meter, for the distribution of location error shown in the histogram, there is still area under the characteristic curve representing the trend. Further, from the probability plot, the population found at 0.5 meter would be estimated to be 98.9 percent, and the population not found estimated at $100 - 98.9 = 1.1$ percent. Since the population used comprises 84 percent of the GT, the percentage missed comprises $1.1 \text{ percent} \times 0.84 = 0.9$ percent of the overall ordnance population. The P_d^{res} score could be

improved by 0.009 (0.01 when rounded) if location error was sufficiently improved. This is a small percentage for this example. Greater values will be seen for other systems.

d. The vertical axis in the histogram is unlabeled to help preserve GT information related to quantity.

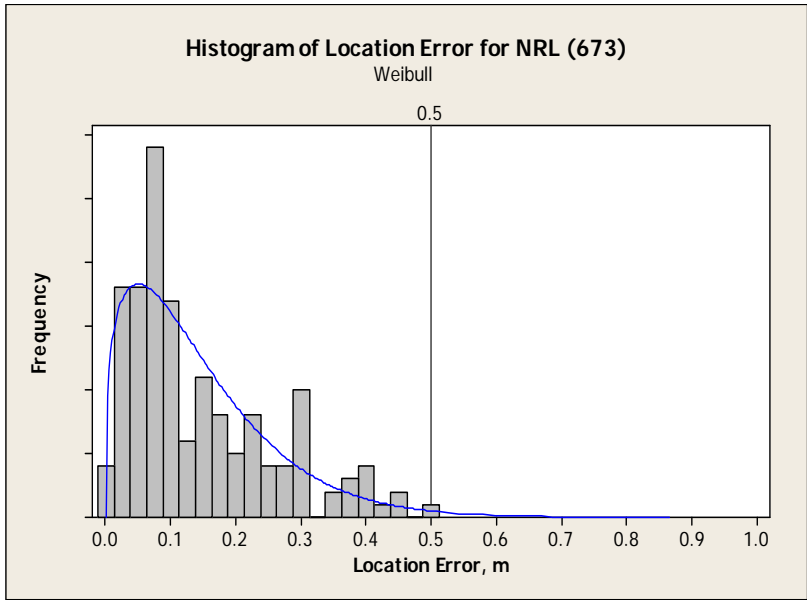


Figure 2.3.4-8. Histogram of location error for NRL towed system (report No. 673) at APG open field.

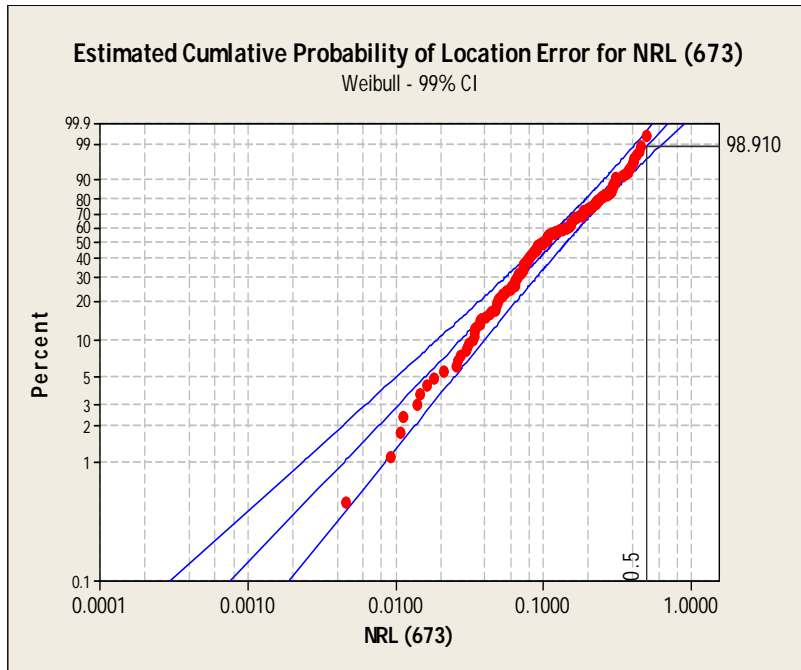


Figure 2.3.4-9. Estimated cumulative probability of location error for NRL towed system (report No. 673) at APG open field.

e. The percentage of the population of ordnance not found because of location error is estimated for all systems at APG open field using the above method, and the results are summarized in Figure 2.3.4-10 (estimates based on general trends). The systems are represented by report numbers in the plots. Most systems may be missing approximately 1 to 3 percent of the ordnance in the ground because of location error and the scoring criteria of 0.5 meter used at the sites. If the inaccuracy of the GT location is factored in, the values may decrease slightly.

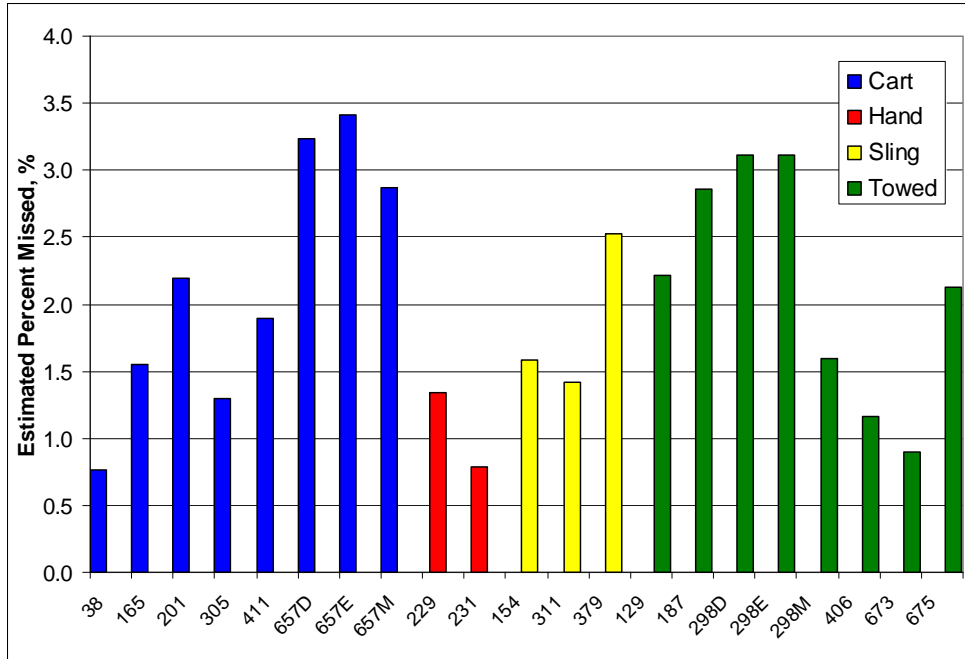


Figure 2.3.4-10. Estimated percentage of ordnance missed because of location error, APG open field.

f. The plot in Figure 2.3.4-9 shows that probabilities can be chosen such as 99.9 or 99.99 percent. These percentages would represent 1 in 1,000 and 1 in 10,000 items being left in the ground, respectively. When these values are correlated with the radius on the horizontal axis, radial dig limits can be estimated. These values for the systems demonstrated at APG open field are shown in Figures 2.3.4-11 and 2.3.4-12 (systems are represented by report numbers). The estimates are for GT items less than 0.6 meter long.

g. As shown in Figures 2.3.4-11 and 2.3.4-12, no well defined trends between platform types are evident. As shown in Figure 2.3.4-12, a 1-meter dig radius encompasses all location error results for a 1 in 10,000 miss. The geophysical prove-outs (GPOs) typically use a 1-meter detection radius for scoring.

h. Histograms and probability plots of location error for all demonstrators at APG open field are presented in Appendixes E and F.

i. See section 2.3.6 for an examination of how BARs may inflate a P_d score as the scoring radius is increased.

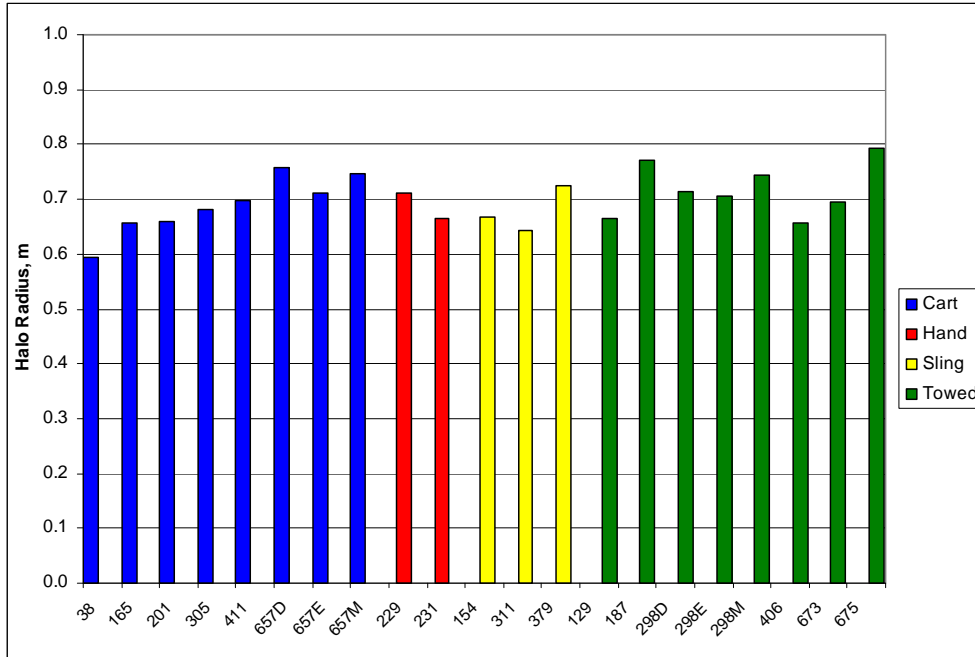


Figure 2.3.4-11. Estimated halo radius at which 1 in 1,000 items would be left in the ground because of location error, APG open field.

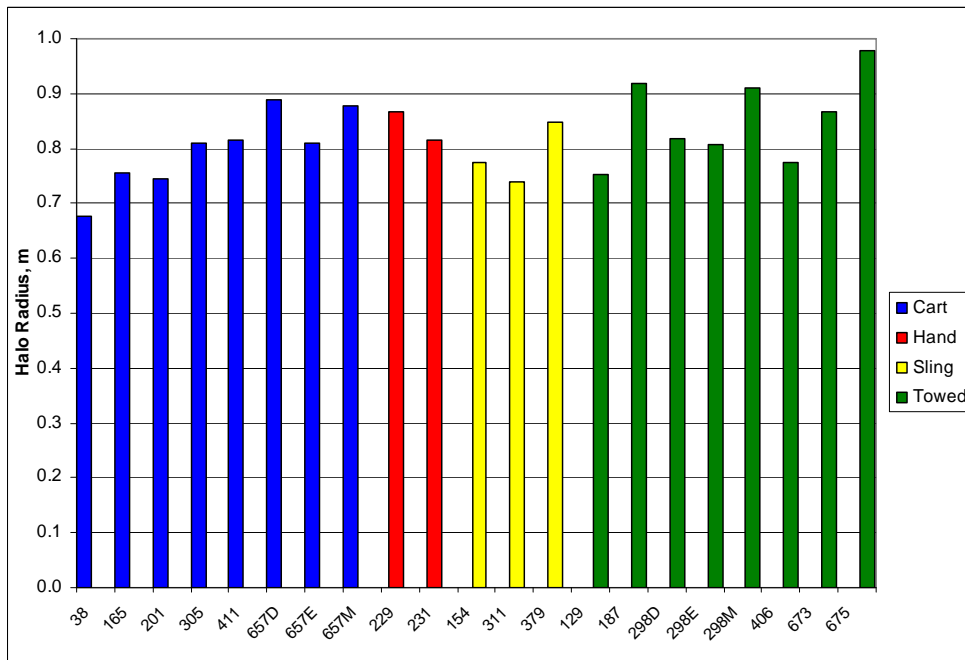


Figure 2.3.4-12. Estimated halo radius at which 1 in 10,000 items would be left in the ground because of location error, APG open field.

2.3.5 Effects of Field Configurations/Item Type

2.3.5.1 *Standard and Non-standard Items*

a. Ordnance items buried at the sites are designed to fit into one of two categories, standard or nonstandard. Standard items are members of a set whose physical properties are identical and that resemble a complete production configuration. Some examples of the physical properties that must conform in order for an item to be categorized as being standard are, caliber, configuration, size, weight, aspect ratio, material filler, and nomenclature. Items whose physical properties do not conform are categorized as being nonstandard. Nonstandard items can have missing parts such as fuses or fins, they could have lost mass from already having been buried in the ground for several years or they could simply be filled with a different filler material. The degree to which nonstandard items do not conform to the standard physical properties varies depending on the particular item.

b. It was originally intended that all standard items be degaussed. In review of records, it was found that both standard and non-standard items had been degaussed to varying degrees. Therefore, this characteristic is variable.

c. Standard and non-standard items comprise the overall standard GT sets used in this report. Standard GT sets examined thus far are not to give the impression that only standard items, as defined above, were used.

d. The P_d^{res} for standard and nonstandard items in the APG open field is shown in Figure 2.3.5-1. The standard and nonstandard GT used in the figure are a duplicate in quantity, round type (whether in part or whole), azimuth, dip, and depth. In addition, the distance to the next closest item is similar for a standard and its nonstandard counterpart in GTs.

e. With the characteristics of depth and orientation being the same, the relative abilities of systems to detect standard versus nonstandard items are shown in Figure 2.3.5-1. For some systems, the standard items may be easier to detect because they are slightly larger or are not missing any parts. In addition, standard items are buried in the calibration lanes and it may be easier to identify the standard items. As shown in Figure 2.3.5-1, no well defined trends exist between standard and nonstandard items for the basic sensor types. This indicates that the detection systems are not thrown off by the absence of part of a round to a noticeable degree in the APG open field environment. It may also simply indicate an insufficient sample size (15 items in this case) to make adequate comparisons.

f. The P_d^{res} for standard and nonstandard items at the YPG open field is shown in Figure 2.3.5-2. Even though the standard and nonstandard GTs shown in Figure 2.3.5-2 are duplicates (in terms of round type, depth, and orientation, etc.), the GTs shown in Figure 2.3.5-2 are not identical to those shown in Figure 2.3.5-1. So the differences between the two figures could be caused by differences in the GTs, such as the basic round types used, population, depth, and orientation. The differences may also be a result of a better test statistic. The population size used for YPG is 38, which is much better for making comparisons (for $P_d = 0.95$, upper confidence level = 0.99 and lower confidence level = 0.87 at 80% confidence).

g. As shown in Figure 2.3.5-2, most EM systems are finding the standard items at a greater frequency than nonstandard items. The reverse is true for the MAG systems; however, the MAG systems are finding less of the standard and nonstandard items as a whole when compared to the EM results. It is likely that the aluminum fuzes and tails present in standard items but not present in non-standard items are causing these trends (MAG systems are not sensitive to these parts). More analysis needs to be done to confirm this. Differences between the GT at both testing sites need to be examined.

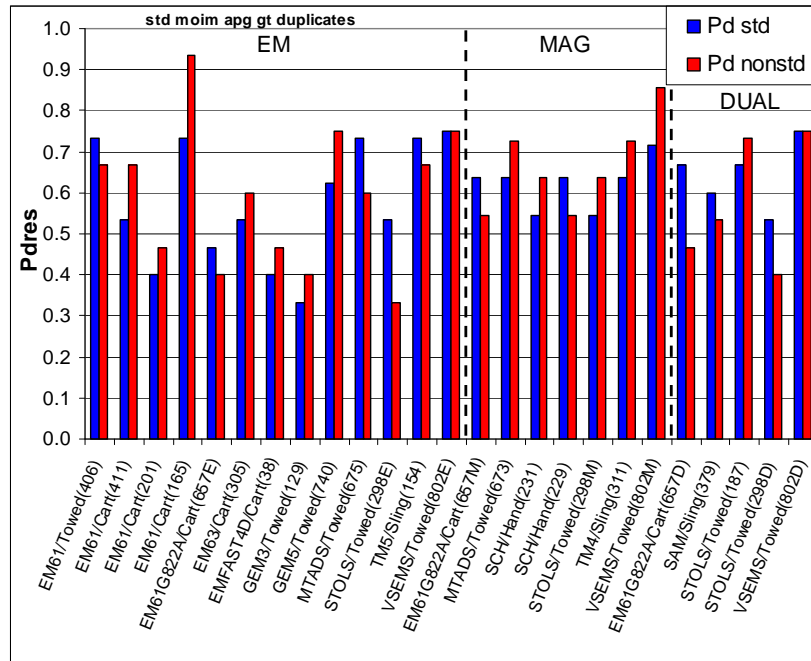


Figure 2.3.5-1. P_d^{res} versus demonstrator for standard and nonstandard GT, APG open field.

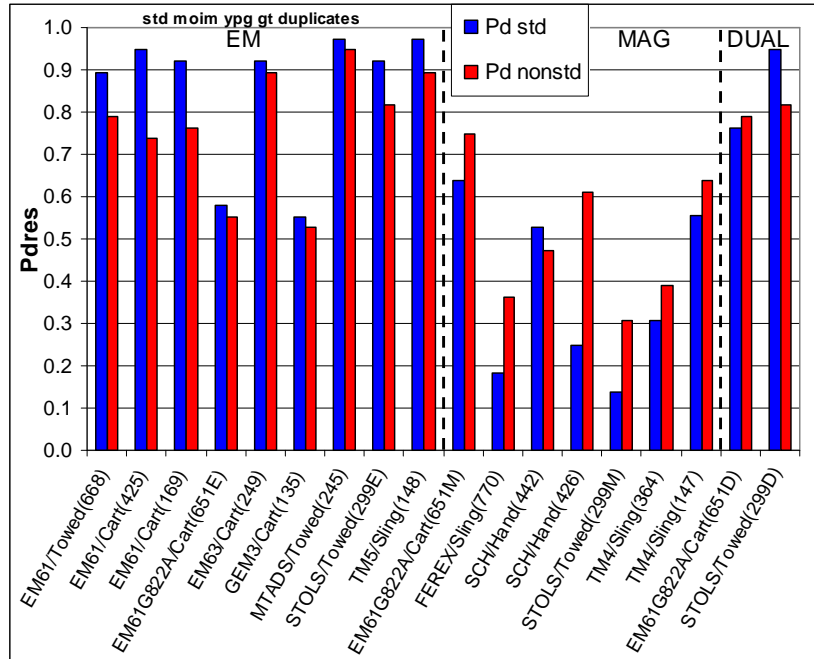


Figure 2.3.5-2. P_d^{res} versus configuration for standard and nonstandard GT, YPG open field.

2.3.5.2 Depth

a. Items at the standardized UXO sites are buried at a variety of depths. In general, as items are buried deeper and signal levels decrease, the items become more difficult to detect. The effects of depth on the ability of vendors to detect GT items are shown in Figures 2.3.5-3a, 2.3.5-3b, 2.3.5-4a, and 2.3.5-4b. The first two figures are APG open field results, and the latter two figures are YPG open field results. To achieve a result more representative of the ability to detect individual items, GT items that are closer than 1.0 meter to another item, and items that are in challenge areas (including wet areas), were removed from the GT used to generate results.

b. Depths are separated into ranges that were typically analyzed for published reports in Figures 2.3.5-3a and 2.3.5-4a. The figures show the P_d^{res} as a function of depth. The figures indicate that as the ordnance items are emplaced deeper the items become more difficult to detect. However, the figures do not take into account the size of the item which is typically proportional to signal return. In this respect, Figures 2.3.5-3b and 2.3.5-4b are more useful because they show the P_d^{res} as a function of depth divided by the diameter of an item.

c. The results show that for items greater than 1 meter deep there is a marked decrease in P_d^{res} . While not disclosing critical GT information, typically, with few exceptions, a small amount of only large items are buried at depths greater than 1 meter.

d. Some magnetometers show better detection rates between 0.3 and 1 meter than at 0.0 to 0.3 meter. This is not the case with the Schonstedt.

e. No systems with high P_d^{res} values were able to see across all depth ranges with near equal detection ability. The VSEMS dual system shown in Figure 2.3.5-3a, however, was close.

f. A large drop in P_d^{res} for depths greater than 11D for all systems was demonstrated, as expected.

g. Items buried between 5 and 11D typically had approximately a 0.05 to 0.20 drop in P_d^{res} when compared to 0 to 5D performances for the better systems. This indicates that sensing at this depth range still has room for improvement within the community of systems demonstrated. At YPG open field (fig 2.3.5-4b), the MTADS/towed array system (report No. 245, GEM-3 sensor) had only a ~ 0.01 decrease in performance going to the 5 to 11D depth range.

h. Finally, the depth distributions at YPG tended to be shallower than at APG because of difficulty burying items in the sand at YPG. This in part explains differences in performance between the two grounds.

i. For the influence of depth on clutter results, see section 2.3.5.8.

j. The Institute for Defense Analysis (IDA) has done extensive work on detection rates as a function of depth at the sites. Their work is reproduced in part in reference 5. An independent report is expected to follow.

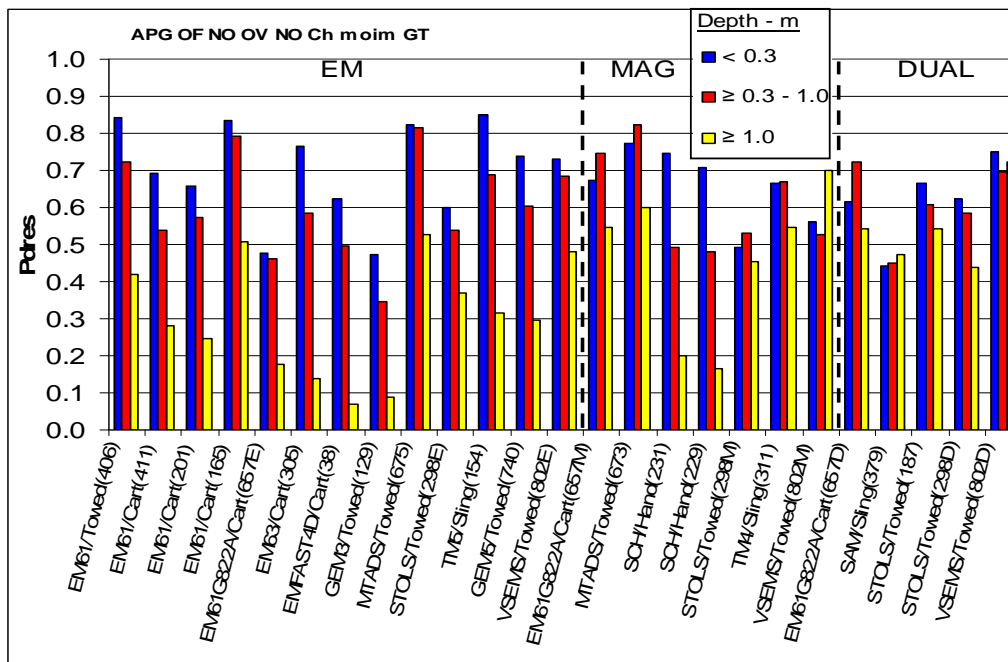


Figure 2.3.5-3a. P_d^{res} versus configurations for different depth ranges (< 0.3 m, ≥ 0.3 m to < 1 m, ≥ 1 m), APG open field, no challenge areas, no overlaps.

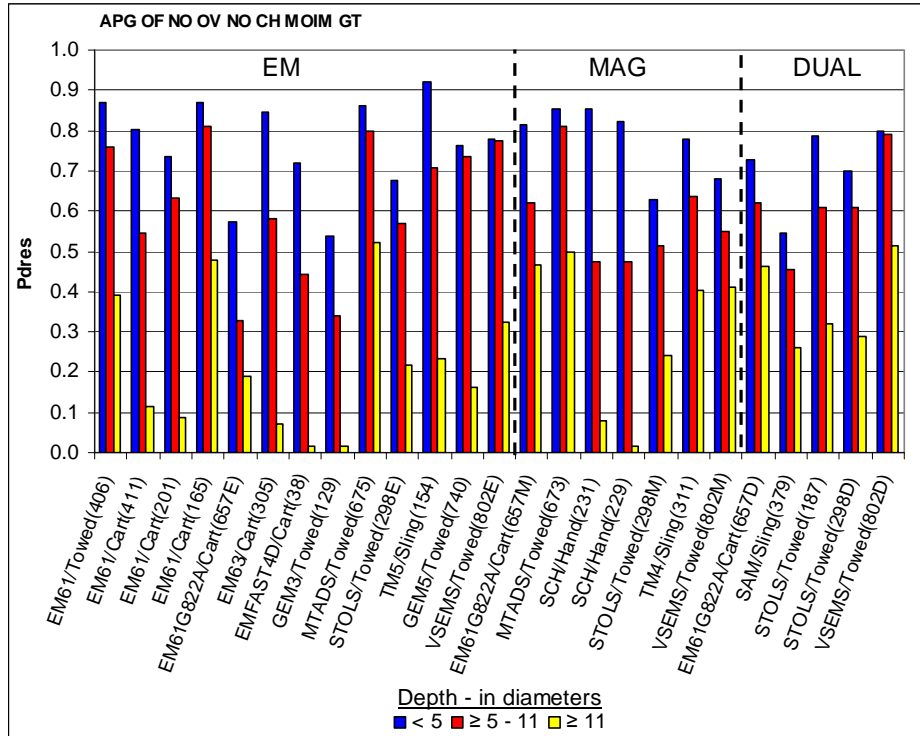


Figure 2.3.5-3b. P_d^{res} versus configurations for different depth ranges ($< 5D$, $\geq 5D$ to $< 11D$, $\geq 11D$), APG open field, no challenge area, no overlaps.

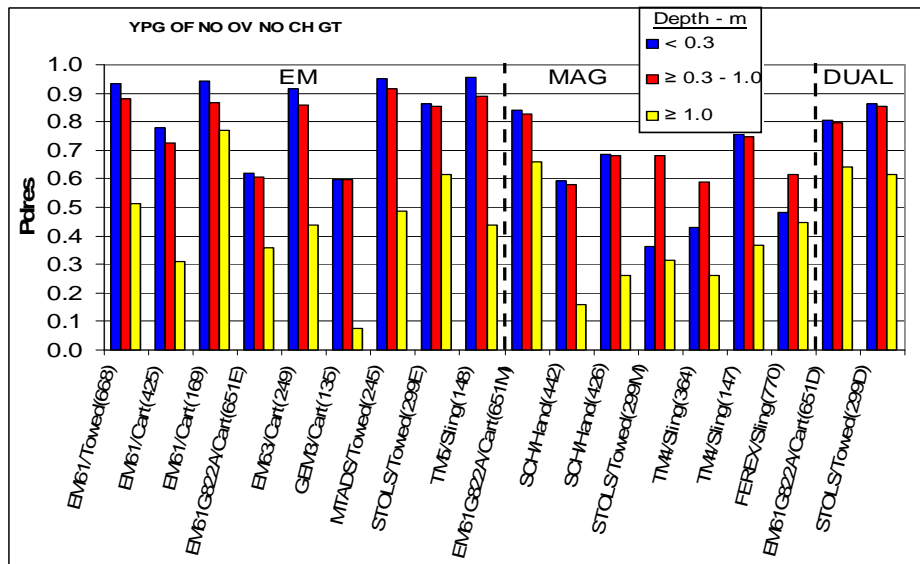


Figure 2.3.5-4a. P_d^{res} versus configurations for different depth ranges (< 0.3 m, ≥ 0.3 m to < 1 m, ≥ 1 m), YPG open field, no challenge area, no overlaps.

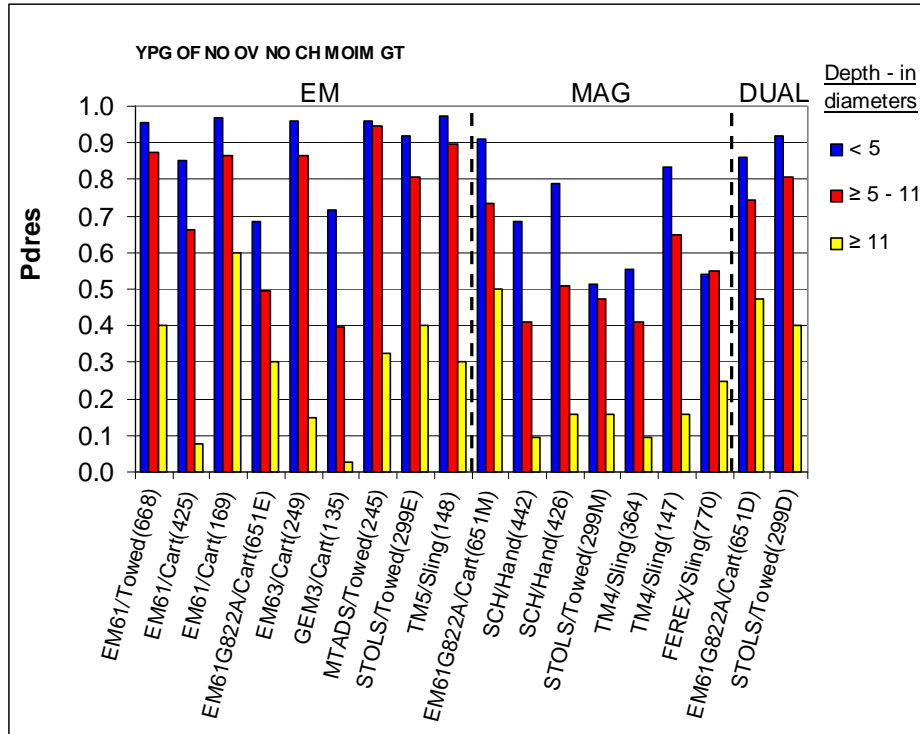


Figure 2.3.5-4b. P_d^{res} versus configurations for different depth ranges (< 5D, ≥ 5D to < 11D, ≥ 11D), YPG open field, no challenge area, no overlaps.

2.3.5.3 Size

a. A total of 14 different types of inert ordnance items have been buried at all of the standardized demonstration sites. An additional two types of ordnance can be found at limited test areas. These items have been categorized into small, medium, and large size groups for general analysis. Small items include 20-mm projectiles, 40-mm projectiles, 40-mm grenades, M42 submunitions, BLU-26 submunitions, and BDU-28 submunitions. Medium size ordnance items include 57-mm projectiles, MK118 Rockeye submunitions, 60-mm projectiles, 64-mm M75 submunition (only at YPG), 81-mm projectiles, and 2.75-inch rockets. Large items include 105-mm heat rounds, 105-mm projectiles, 155-mm projectiles, and 500-pound bombs (only in open fields).

b. P_d^{res} as a function of ordnance size for the systems tested at the standardized sites is shown in Figures 2.3.5-5 and 2.3.5-6. To help to remove the influence of extreme depths, overlapping halos, and challenge areas (including wet areas), the figures do not include results from items that are deeper than 11 times their diameter, items that are closer than 1.0 meter to another item, or items in challenge areas. The results for the APG open field are shown in Figure 2.3.5-5; the results for the YPG open field are shown in Figure 2.3.5-6.

c. The figures indicate that, in general, it is easier for most systems to detect large items than it is to detect small and medium sized items, small items being the most difficult. Because the 11D GT was used (i.e., items should be within sensor range), and the GT approximates depths of items at remediated sites, the finding suggests a deficiency exists in detecting small items at <11D for many of the SOTA systems. An examination of which small ordnances in particular are driving the results is discussed in section 2.3.5-6. Some EM systems at YPG found all three size ranges of ordnance with near equal ability: the MTADS/towed array (GEM-3), TM-5/sling, and EM61/cart configurations (EM61 MK11).

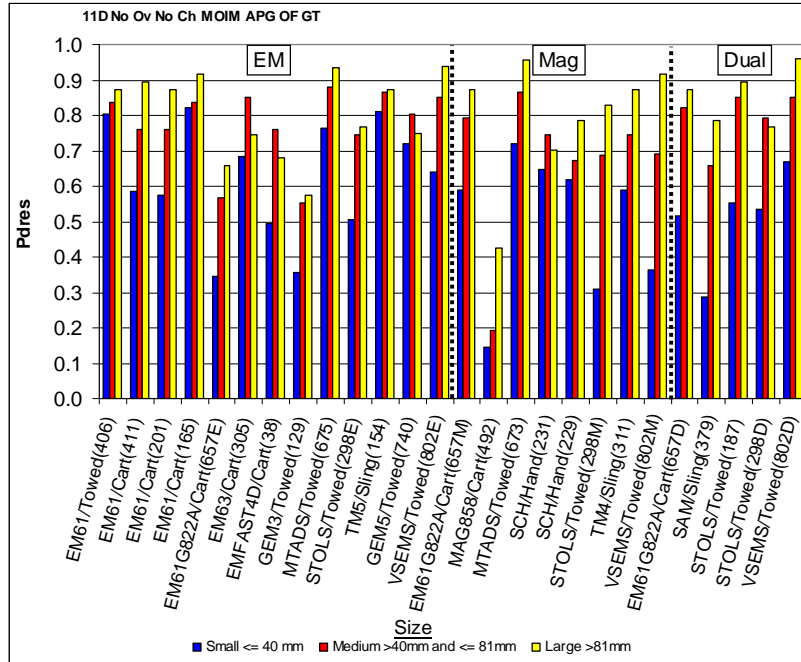


Figure 2.3.5-5. P_d^{res} versus demonstrator for size ranges, APG open field, 11D depth limit, no challenge area, no overlaps.

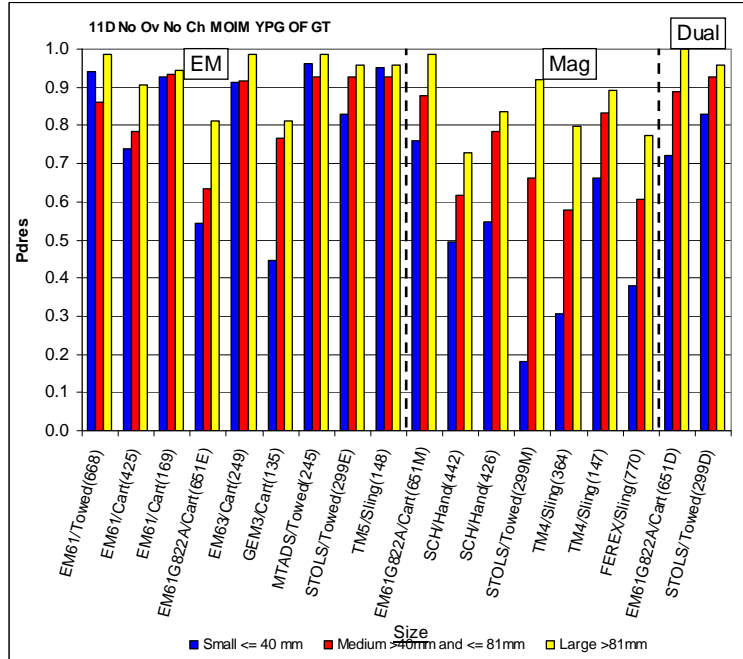


Figure 2.3.5-6. P_d^{res} versus demonstrator for size ranges, YPG open field, 11D depth limit, no challenge area, no overlaps.

2.3.5.4 Overlap and Items in Proximity

a. When items are buried close enough to each other, the signal from one item may bleed over into the area of its neighboring item. When bleed-over (may also be referred to as overlapping signal or shadow effect) occurs, it can become difficult to accurately detect all items in that area. To study this effect, both the APG and YPG sites were designed to have areas where several GT items were buried close to other items.

b. To analyze the effects of items in proximity, six GT subsets were broken out of the entire GT for the APG open field test area. Each subset represents ranges of proximity in increments of 0.5 meter. Thus, for the first subset, 0.0 to <0.5 meter, all ordnance in the GT within 0 to <0.5 meter of another item (item includes ordnance or clutter) were grouped together. For the next subset, if ordnance are within ≥ 0.5 to <1.0 meter of another item they were separated out as a group. This method is repeated up to 2.5 meters at increments of 0.5 meter. The last subset includes all ordnance that have items no closer than 2.5 meters to them.

c. By scoring each subset of ordnance as a GT in itself, a relationship of P_d^{res} versus item proximity or distance to next closest item can be calculated.

d. P_d^{res} and discrimination ability as a function of distance to the next closest item at the APG open field are shown in Figures 2.3.5-7 and 2.3.5-8. The GT subsets used in the figures do not go beyond 11D in depth and do not contain items in challenge areas (including wet areas). This was done to help isolate effects of proximity.

e. As shown in Figure 2.3.5-7, most systems experience a marked decrease in P_d^{res} when a GT item is within 1.5 meters or less of another item.

f. The percentage of demonstrators that experienced a decrease in P_d results after discriminating for the different proximity ranges is shown in Figure 2.3.5-8. Alternately, this is the same as the percentage of demonstrators that did not retain all ordnance in a group when discriminating. The plot indicates that more difficulty exists when discriminating ordnance items with greater distance between them and another item. This seems counterintuitive. A possible explanation is that items very close to one another were more difficult to discriminate and that most demonstrators erred on the side of caution and declared them ordnance. A more in-depth analysis is needed to explain this trend.

g. The sample sizes are small for the groups that were close together. Confidence limits are not shown to preserve GT information from disclosure. Results from the proximity study should be viewed as indicative of general trends.

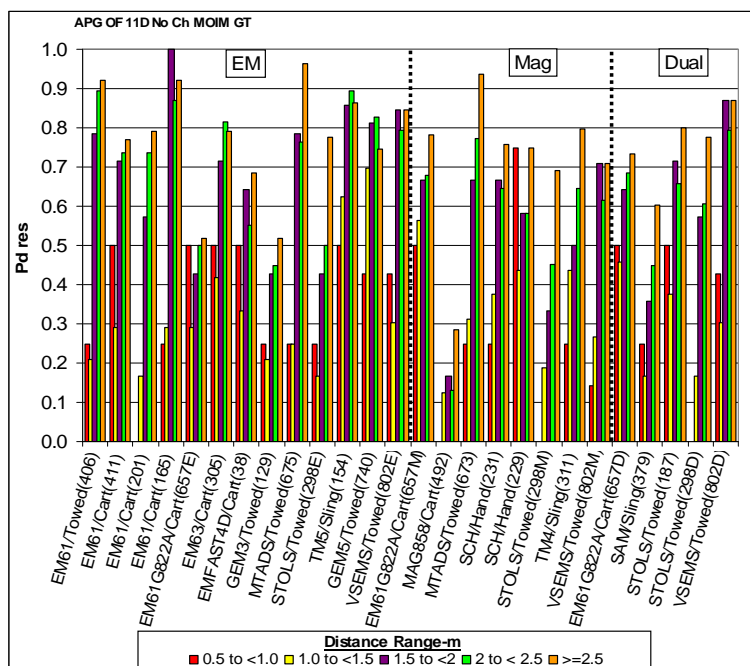


Figure 2.3.5-7. P_d^{res} for various systems versus distance to closest GT item, APG open field, 11D depth limit, no challenge area.

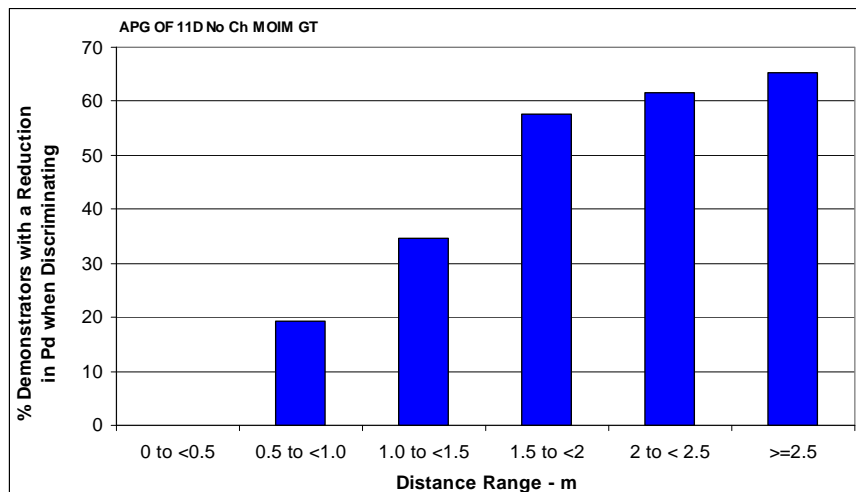


Figure 2.3.5-8. Percentage of demonstrators with a reduction in P_d when discriminating for various distance ranges to next to closest GT item, APG open field, 11D depth limit, no challenge area.

2.3.5.5 Challenge Areas

a. To accurately measure the effects that the different challenge areas have on P_d^{res} , it is necessary to have a statistically significant number of items in each challenge area that are identical to other items in the open fields in non-challenge areas for comparison. In addition, these items need to be far enough apart to remove the effects of overlapping halos and depths needs to be well within range of detection. In 2005, a statistically significant number of items did not exist.

b. After the 2004 through 2005 reconfiguration, such groups of items were buried in the open field (control) as well as in all of the challenge areas (test). However, since the reconfiguration, few demonstrators have surveyed the sites.

c. In the fence challenge area, a chain-link fence was installed over an area where a number of GT items were buried. The area will help evaluate how detection abilities are affected by the fence.

d. In the power line area, the same items were buried directly underneath domestic power lines. The magnetic field produced from the 60-Hz alternating current flowing through these 13,000-volt lines may interfere with a system's ability to detect items in this area as well. The lines are about 7 meters off the ground (at the lowest point).

e. P_d^{res} results, for the challenge areas to date are shown in Figures 2.3.5-9 and 2.3.5-10. If it is assumed that the number of ordnance successfully detected is a binomially distributed random variable, it can be said with an 80 percent confidence that results will fall within the intervals displayed in the figures. The results are for two systems, a GEM-5/towed array and a VSEMS dual mode (EM61 MK11/G822A) towed array that surveyed the area after the 2005

reconfiguration. To see if the results are significantly different, a chi-square test was performed. It was found that at a 0.1 significance level (2-sided test), the power line and fence results could not be said to be significantly different from the control results for the GEM-5. For the VSEMS the fence results are significantly different but the power line results are not.

f. As shown in Figure 2.3.5-11, efficiencies (E = fraction of ordnance retained after discrimination) were calculated from the GEM-5 results. The GEM-5 vendor was aggressive in attempting to discriminate and thus provided a good test case to evaluate challenge area effects. An E of 1 means 100 percent of the ordnance were correctly identified or retained. The figure shows that about 90 percent of ordnance items were retained after discriminating the control and power line group. However, only 38 percent of the ordnance items were retained in the fence test area. This is significantly different from the control group. The VSEMS results are not shown because little effort was made in discrimination (i.e., high E , low false positive rejection).

g. Therefore, preliminary results indicate the power lines are not significantly effecting results. However, the fence has significantly affected the performance of a dual mode system in terms of detection and an EM system in terms of discrimination. Further analysis needs to be performed to see what part navigation around the fence played in the reduced scores. More details about the GT will be provided after the challenge areas are reconfigured.

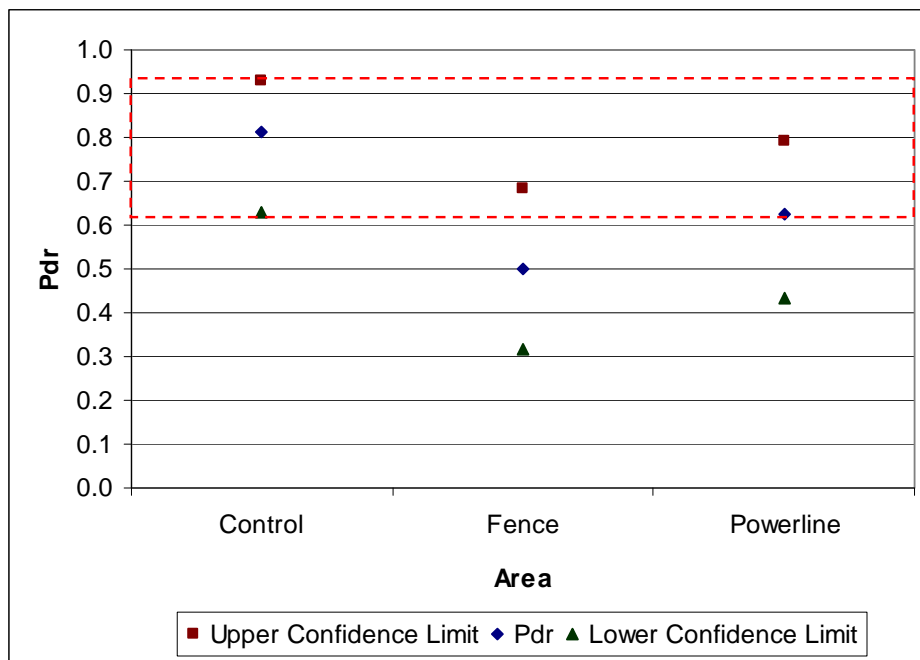


Figure 2.3.5-9. P_d^{res} for different challenge areas, with upper and lower confidence limits for GEM-5 towed array, report No. 740, APG.

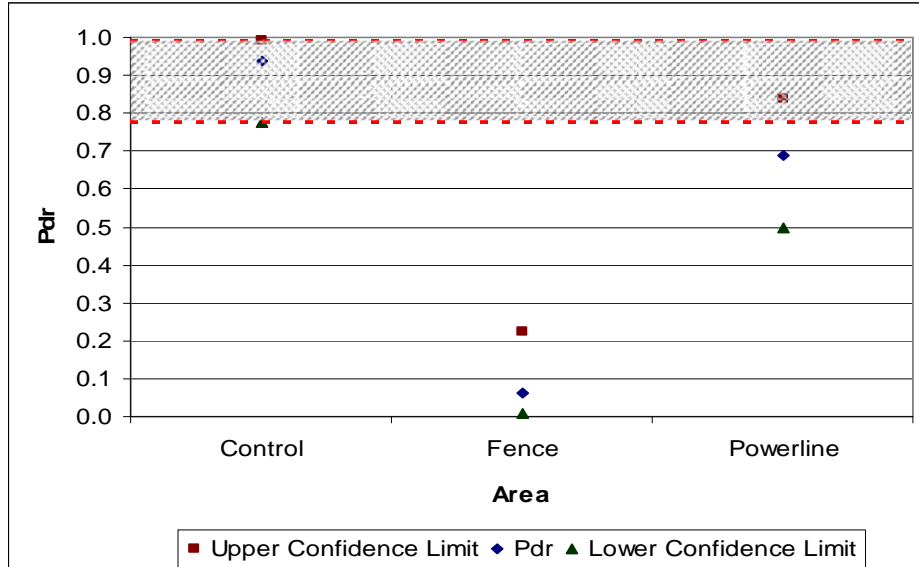


Figure 2.3.5-10. P_d^{res} for different challenge areas, with upper and lower confidence limits for VSEMS towed array, report No. 802D, APG.

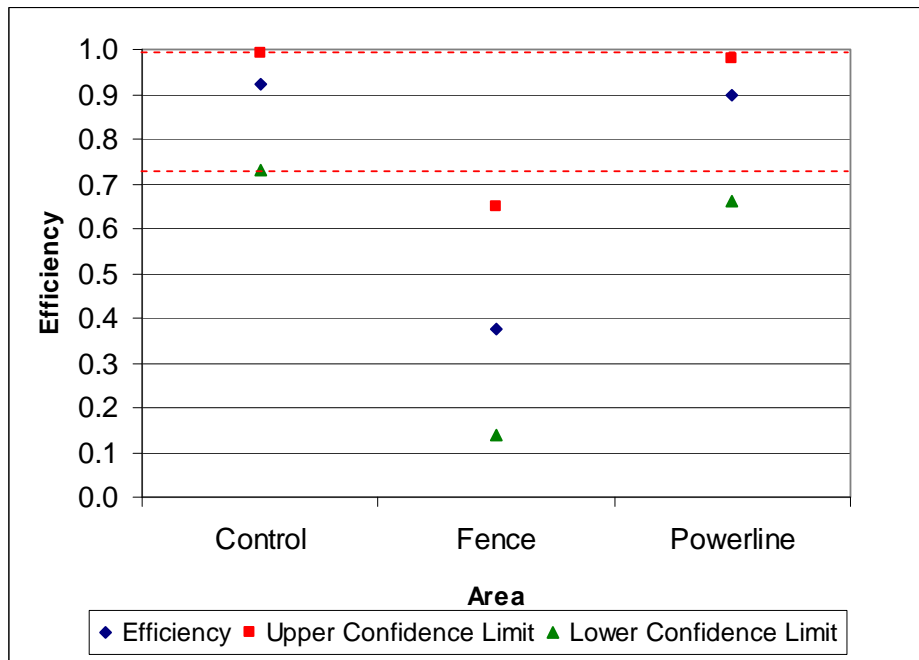


Figure 2.3.5-11. E versus challenge area for GEM-5 towed array, report No. 740, APG.

2.3.5.6 Ordnance Type

a. The following section examines how easily the demonstrated detection systems found and identified individual ordnance types at the standardized sites. As indicated in section 2.3.5-3, in general, smaller ordnance were more difficult to detect. By looking at types it will be determined if some or all of the small ordnance types are driving this trend.

b. The P_{dres} scores for some of the relatively better performing EM and MAG systems at the APG open field are shown (EM blue, MAG green) in Figure 2.3.5-12. The GT used has no items in challenge areas (including wet areas), items closer than 1.0 meter to another item (no overlaps), or items deeper than 11D. BAR values (all ordnance) for the systems are included in the plot as the first group on the horizontal axis.

c. As shown in Figure 2.3.5-12, the magnetometers have no result showing for the 40-mm grenades and MK118 Rockeye submunition. This is because the standard GT for magnetometers does not include non-ferrous items.

d. Of the small ordnance types (which include 20-mm projectiles, 40-mm projectiles, 40-mm grenades, M42 submunitions, BLU-26 submunitions, and BDU 28 submunitions), the 20-mm projectiles are approximately 20 to 30 percent more difficult to detect than other items in this group for EM systems. This margin is even greater for MAG systems. The 20-mm projectiles are driving detection scores for smaller items. The ordnance is the smallest type in the GT configuration. A possible reason for this performance shortfall by the systems is discussed in section 2.3.7.3.

e. One other ordnance type that is relatively difficult to detect is the MK118 Rockeye submunition. It is part of the medium sized ordnance group. This ordnance type does not drive the medium group results like the 20-mm projectiles drive the small group results, as seen in section 2.3.5.3. This is due to the smaller population of the MK118s at the APG open field.

f. The largest ordnance are easiest to find, especially since an 11D limit is in place. However, one small ordnance type, BLU 26 submunition, was also easy to find; it is the only type that is round. It could be that the depths associated with its burial are causing this ease of detection. Further study needs to be done to determine causes.

g. Values of P_d^{res} for each system and ordnance type at APG and YPG open fields using an 11D, no challenge (including wet areas), no overlap GT are included in Appendix G. The tables should provide a quick look at what systems may (some systems might have underachieved for some reason specific to the test instance) be best suited to detect a particular ordnance type. Unfortunately, time prohibited the updating of the tables to show corresponding BAR values. The reader is referred to figures 2.3.1-11 and 2.3.1-12 for this information (a high P_d may not necessarily be good if the corresponding BAR value is high). Scores in the tables are rounded to the nearest 0.05 level to help keep GT quantities from being discovered. The GT used for the tables is the same for both EM and MAG systems and includes non-ferrous items. Therefore, the MAG systems will justifiably have low scores for the 40-mm grenades and MK118 Rockeye submunitions.

h. An E score is shown in Figure 2.3.5-13 for the different ordnance types in the APG open field using the same GT limitations as Figure 2.3.5-12. The same systems are also used with the exception of the EM61/Cart(165) and SCH/Hand(229) which did not discriminate. For the group of systems examined it is seen that the BDU28 and 20mmP ordnance types were most difficult to discriminate. In general the small ordnance types gave the demonstrators the most difficulty.

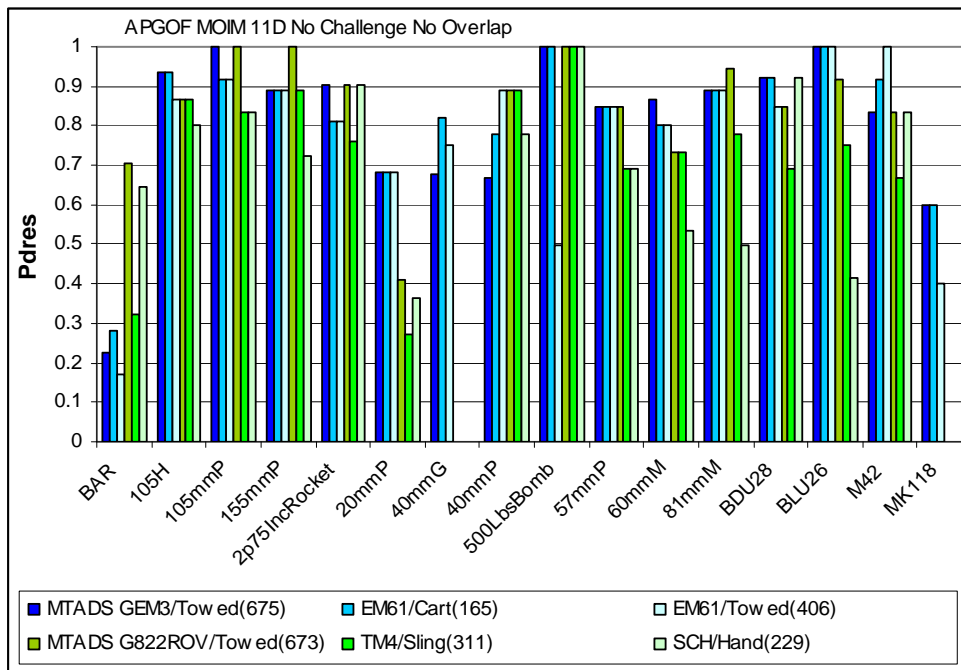


Figure 2.3.5-12. P_d^{res} , per ordnance type and sensor type, APG open field, 11D depth limit, no challenge area, no overlaps.

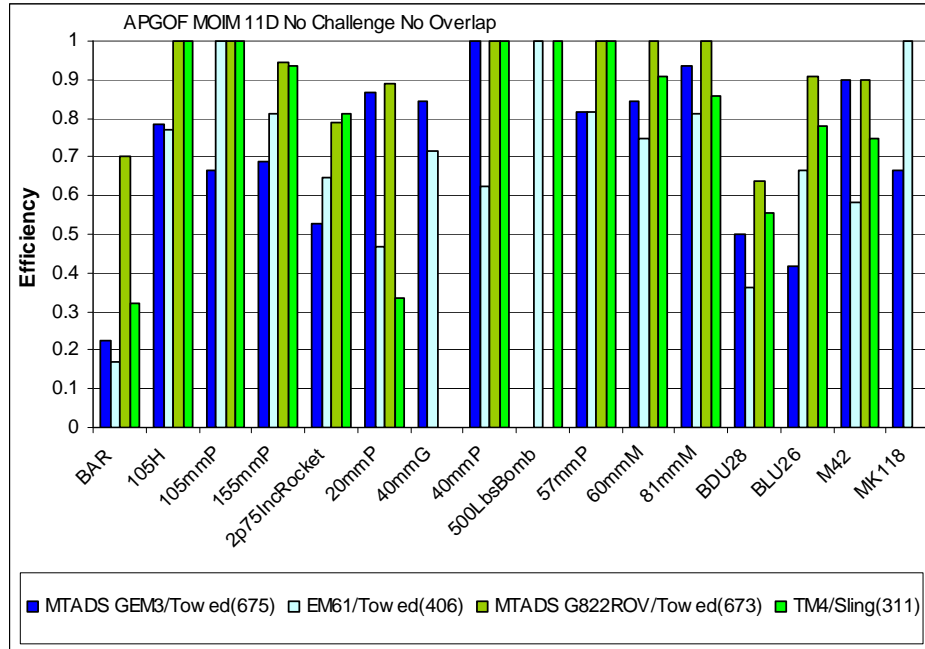


Figure 2.3.5-13. E for systems per ordnance type for APG open field, 11D depth limit, no challenge area, no overlaps.

2.3.5.7 Combined Effects

a. Different influences on P_d^{res} have been examined. The following contributors to reduced P_d^{res} values have been identified.

(1) Item depths beyond 11D have been proven to cause significant detection problems. Even depths from 5 to 11D have been problematic for systems.

(2) Small size ordnance and, to a lesser degree, medium size ordnance had lower detection rates. The rates were found to be driven primarily by 20-mm projectiles and to a lesser degree by MK118 submunitions.

(3) Items in proximity to the GT have been found to reduce detection rates. It appears when items are within 1.5 meter or less from a GT item that marked decreases in detection rates typically occur.

(4) Location error may be causing some systems to have potential detections nullified because they are just outside of the allowed 0.5-meter detection radius. Judging from error distribution characteristics, a lower value (typically no more than 3.5% reduction, in most cases not significant) of P_d^{res} occurred for many systems.

(5) It appears that coverage deficiencies may be causing some systems to have a decrease in P_d^{res} rates of up to 0.05.

(6) Metallic ground obstacles such as fences in the challenge areas cause P_d^{res} reduction if GT items are in proximity. More testing is needed to quantify distance, depth, mass, etc., relationships with P_d^{res} .

b. All of the above considerations were taken into account to create an adjusted GT or LIM (limited) GT subset to see how much P_d^{res} scores can be improved.

(1) Items deeper than 11D are eliminated.

(2) 20-mm projectiles and MK118 submunitions are eliminated.

(3) GT items that have a neighboring item within 1.5 meter are eliminated.

(4) Items missed because of lack of sensor coverage are eliminated (varies from demonstrator to demonstrator).

(5) Estimated percentages of missed population due to location error were not added on to detection scores (varies from demonstrator to demonstrator). This is because some of the location error was likely related to coverage and overlapping halo effects, which are accounted for in above items 3 and 4.

(6) Items in challenge areas are eliminated.

c. The new P_d^{res} results for demonstrators in the APG open field, using the LIM GT, are shown in Figure 2.3.5-11 alongside standard results and an LIM version of the blind grid results. Some LIM results are not calculated, because of data formatting issues and time restrictions in processing the data. Nonetheless, all systems are represented on the graph.

d. The LIM GT promotes a drastic increase in P_d^{res} results (30 to 66 percent) for the APG open field. The top four performers using the LIM GT have scores between $P_d^{\text{res}} = 0.92$ and 0.94, which are 6 to 8 percent shy of 100 percent detection. Six systems are at or near 100 percent detection for the LIM blind grid results.

e. It is likely that another means of increasing P_d^{res} scores would be to further decrease the maximum depth (into the 5D to 11D range) of the GT.

f. This exercise is not meant to make the detection systems look good or to excuse deficiencies but is meant to try to account for or identify causes of deficiencies to give direction to development efforts and understand current system limitations. Further, this exercise shows the full potential of the systems in detecting individual (not clustered) items within expected (11D depth, accessible environment, etc.) system limits, allowing a more objective means of evaluation. Lastly, comparative analysis should not be done without considering BAR scores for the systems presented earlier in the report.

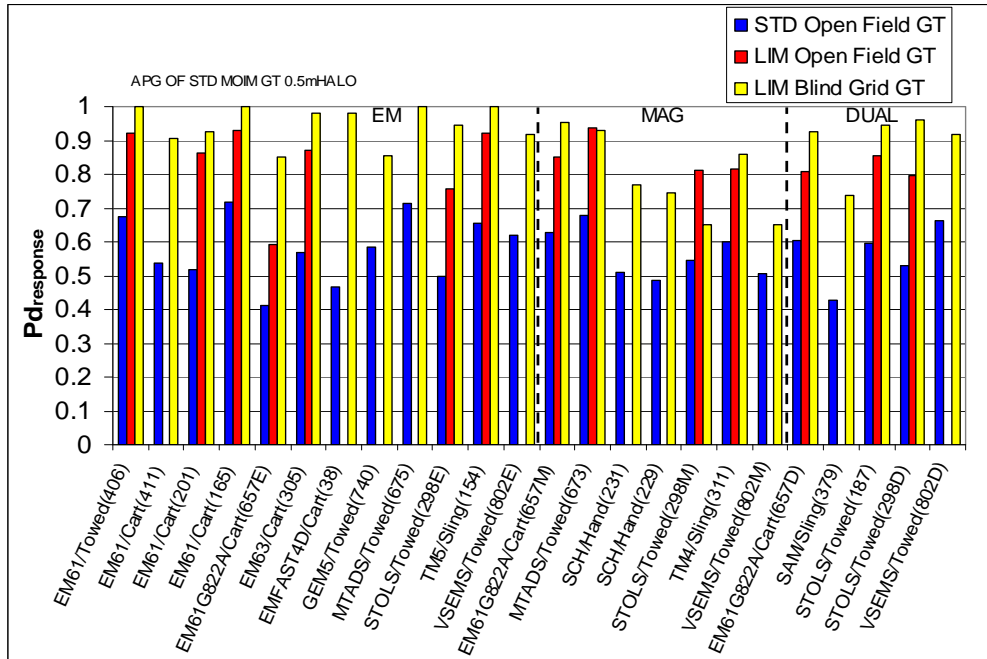


Figure 2.3.5-14. P_d^{res} for all systems in the APG open field using an LIM GT set.

2.3.5.8 Clutter Type

a. A large number of ferrous items that were not ordnance were also buried at the standardized UXO sites. These clutter items are categorized based upon their mass. No dimensional details were recorded. This is because of the wide variation in shapes and sizes of the clutter. At the time of emplacement, greater emphasis was placed on mass than is now as a driver in detectability. The mass categories include, in kilograms, the following ranges: 0.0-0.25, >0.25-0.7, >0.7-1.0, >1.0-4.0, >4.0-10.0, and >10.0.

b. Probability of false positive in the response stage, P_{fp}^{res} , as a function of the average mass of the clutter groups in the APG and YPG open field for all vendors is shown in Figures 2.3.5-15a and 2.3.5-15b. P_{fp}^{res} is in effect a measure of the percentage (where 1.0 = 100 percent) of clutter items detected. The GT used for the plotted results excluded clutter items if they were less than 1.0 meter from another object (no overlaps) and if they were in the challenge areas (including wet areas). Detectability increases up to about 1 kg, then drops off slightly, increasing again as mass increases for APG results. A more consistent increasing trend with mass is seen in P_{fp}^{res} when YPG results are viewed.

c. The average depths of the mass categories are plotted as a dashed line using the scale on the right vertical axis in the figures. This was done to see to what degree mass or depth are driving detectability trends.

d. An interesting trend in the figures is that at APG the groups at the smallest value of mass are more difficult to detect than at YPG. This appears to be driven by depth since the APG items at this mass range are approximately two times deeper than the YPG items.

e. Since the APG P_{fp}^{res} values are so low for the minimal mass group it appears that the limits of the SOTA systems are being manifest. Items less than ~0.5 kg at depths greater than ~0.25 meter are very difficult to detect. Otherwise, in general, the systems performed well when detecting clutter.

f. The average false positive rejection rate (R_{fp}), for all demonstrators, for the same GT used as in Figures 2.3.5-15a and 2.3.5-15b, is shown in Figure 2.3.5-16. $R_{fp} \times 100$ is the percentage of clutter items rejected (i.e., declared not to be ordnance) during discrimination, where 100 percent is optimum. The figure shows that a small percentage of detected clutter items were rejected as clutter (i.e., most clutter items were called ordnance by SOTA systems). On average, for both proving grounds and all clutter masses, ~25 percent of clutter is typically rejected (identified as clutter) during discrimination. The exception to the trend is the larger mass items at APG which had an R_{fp} that averaged around 0.46. This value still indicates an inability to properly discriminate clutter. The more massive items at YPG did not have the higher R_{fp} value even though they were at similar depths. This is likely due to the type clutter items, type systems, or type soil differences between APG and YPG.

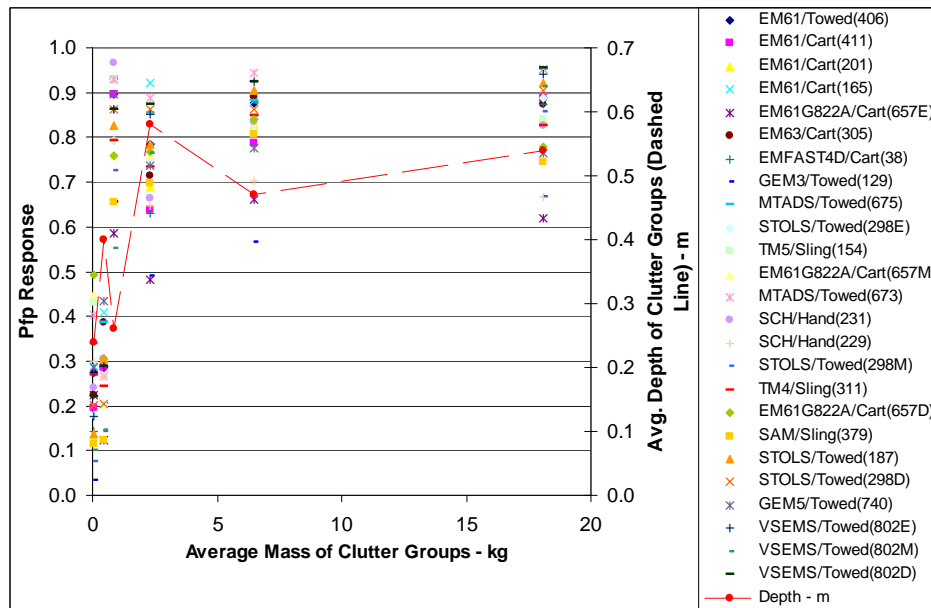


Figure 2.3.5-15a. P_{fp}^{res} , for different groups of clutter mass, APG open field, no challenge area, no overlaps.

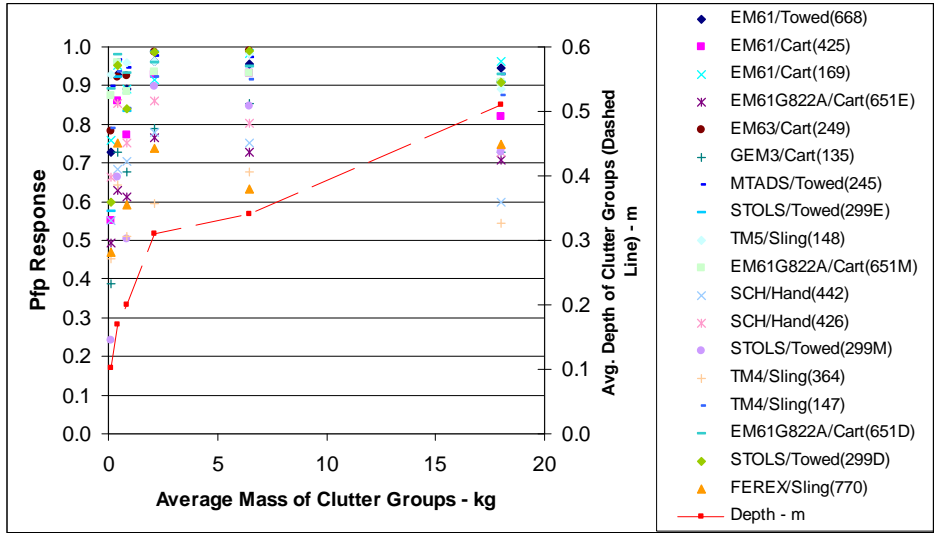


Figure 2.3.5-15b. P_{fp}^{res} , for different groups of clutter mass, YPG open field, no challenge area, no overlaps.

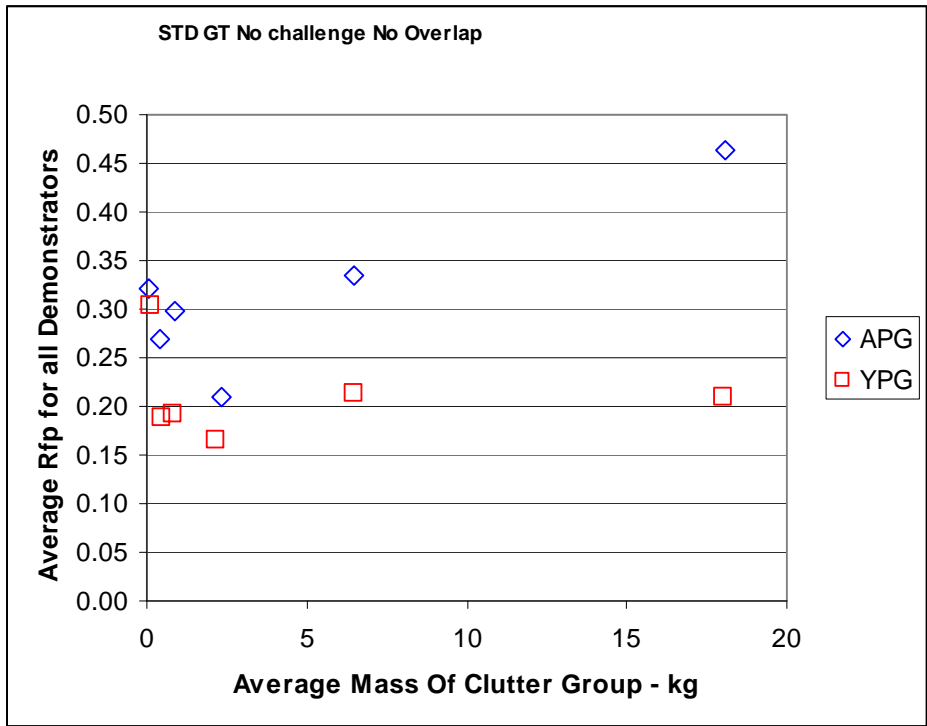


Figure 2.3.5-16. R_{fp} for different groups of clutter mass, APG and YPG open field, no challenge, no overlaps.

2.3.6 Effects of Scoring Methodologies

a. In this section, P_d^{res} versus halo size around GT items will be examined. If the location of an item on a dig list is within 0.5 meter of a GT item, the standardized site rules dictate that the two items be associated and the GT item be considered detected (general case). The 0.5-meter radius around the GT traces out a circle that in standardized site terminology is called a halo. A quick analysis was performed to see what effects varying this halo size would have on scoring.

b. A subset of the GT was created which contained ordnance with no neighboring items within 4 meters. This allowed the halo radius to be increased to 2 meters while limiting interference on detection by neighboring GT. Items no deeper than 11D were selected for the subset used.

c. The trends of P_d^{res} versus halo radius for the GT subset are shown in Figure 2.3.6-1 for a representative number of systems demonstrated in the APG open field.

d. As shown in Figure 2.3.6-1, trends start with a high-sloped-linear region then begin transitioning to a low slope region as halo size increases. The high slope region represents true detections, while the low slope region represents background alarms being counted as detections. As a system experiences a greater location error, the transition between high slope and low slope will shift right (many systems have this characteristic). As discussed in section 2.3.4.4, estimates of P_d^{res} increases that can be afforded by eliminating location error, greater than 0.5 meter, typically run from 1 to 3 percent. Further study is needed to look at the number of anomalies as a function of distance from GT to better understand the transition region of the curves.

e. The best performers (reports No. 673 and 675, both NRL MTADS systems, G822ROV and GEM3 sensors respectively) have a sharp transition between slopes at or below a halo radius of 0.5 meter.

f. The figure indicates that the chosen halo radius of 0.5 meter is a good value to use to show true detection ability. Most system results enter a transition region near this radius. GPOs typically use a 1-meter detection radius. As shown in Figure 2.3.6-1, detection scores at the standardized UXO sites would be inflated using a value of 1-meter due to background alarms becoming legitimate detections. However, as discussed in section 2.3.4.4, from a margin of error standpoint, 1 meter is a good number to use when digging.

g. As shown in Figure 2.3.6-1, P_d^{res} scores are much higher than those from standard GT results. This is a result of the large, 4-meter minimum spacing between GT items that is limiting signal interference from other items and causing the items to stand out better. It may be these items are also larger because they are well spaced in the GT.

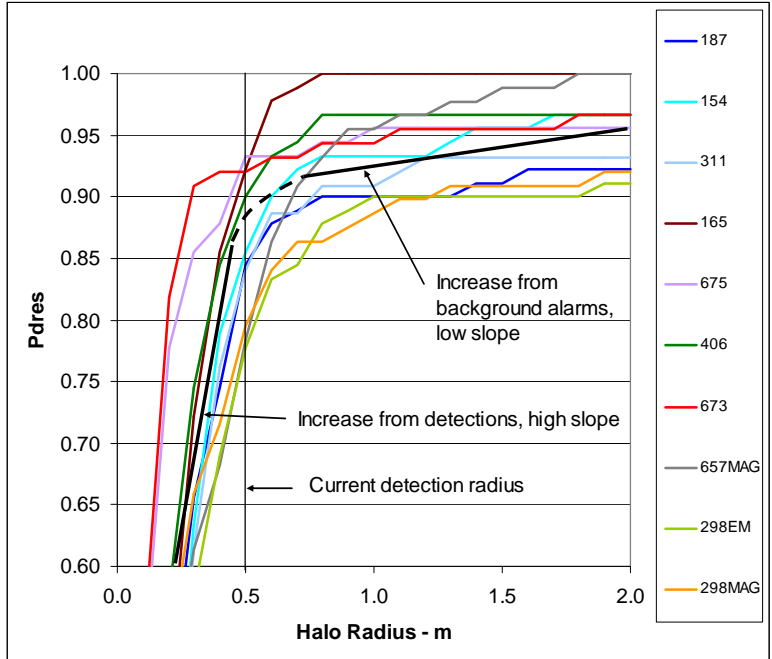


Figure 2.3.6-1. P_d^{res} , versus halo size, 11D depth limit, APG open field, reduced GT size (no items within 4 m).

2.3.7 Environmental Effects

This section will show that system performance was affected by various environments.

2.3.7.1 *Comparing Performance in Different Terrains for Similar GT*

a. The GT for each test area at the UXO test sites is unique. This means that the distributions of ordnance types, orientations and depths are not duplicated as a whole in any other test area. It can be difficult to analyze the effects of a change of terrain by simply looking at the change in P_d using the standard GTs in the different areas. A drop in P_d^{res} from one area to the next could be caused by the change of the terrain in the different areas, or it could be caused by the change in GT distribution for the different areas. To compare the effects of the terrain in the different areas, both the GT distribution in each area and the systems the vendors are using in each area must be identical.

b. By carefully analyzing each GT item in each of the test areas it is possible to select a subset of GT items in one area that have an identical set of GT in another area. Two GT items are defined to be identical if they are of the same type, are both standard or nonstandard, if the closest item to both of them is either greater than or less than 1 meter away, and if the difference between the depth, dip angle, and azimuth angle of the two are within the margin of error for which these quantities can be measured.

c. If a common set of GT were found between all sites this GT set would be very small. So, to maximize the population of items to be compared between terrains, two baseline areas were established: the APG and YPG open fields. Items in each test area identical to items in the baseline areas were selected for analysis at each proving ground. Populations of identical items varied from 55 items to 177 items for the different areas. The blind grids could have been selected as baseline areas but since they are much smaller than the open fields, finding populations of identical items between sites adequate for analysis would be difficult.

d. The percentage change in P_d^{res} going from the open field baselines to other test areas at each proving ground for various systems is shown in Figure 2.3.7-1. Not all systems demonstrated are included in this figure because of time restrictions in analyzing the data, and because not everyone used an identical system at each area.

e. As shown in Figure 2.3.7-1, for the more difficult terrains to navigate (e.g., APG woods, APG moguls, and YPG desert extreme), the detection rates typically drop from 25 to 60 percent when compared to open field performance at the same proving ground. The exception to this rule is the Schonstedt unit at the YPG desert extreme area; that unit's performance decreased by 3 percent.

f. The performance as measured by percentage change in P_d^{res} at the YPG moguls was not as pronounced as in the APG moguls. This is no doubt due to the lower slope and height of the moguls at YPG. There is much variation in performance degradation between demonstrators at this test area and in general a decrease in performance. The exception to this trend is the Schondstedt whose performance improved in the YPG moguls when compared with open field performance.

g. As expected, performance in the blind grids was typically better than in the open fields. This is driven by the fact that the demonstrators know the potential locations of the GT in this test area.

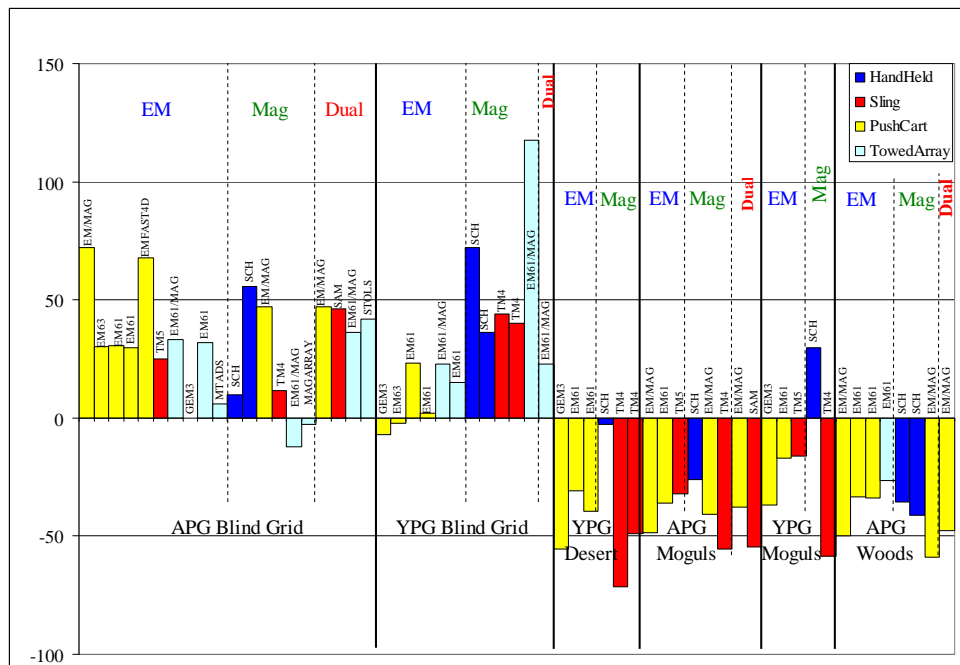


Figure 2.3.7-1. Percentage change in detection rate from open field baselines at APG and YPG for different test terrains and platforms, same comparative GT used.

2.3.7.2 Power Line and Fence Effects

See section 2.3.5.5 for discussion.

2.3.7.3 *Noise Level/Bleed-over Effects*

a. This section will examine the effects of background noise (environmental, not system) level on detection rate for 20-mm projectiles. Background noise levels are specific to each test area and are contributed to by natural and man-made items/disturbances. Earlier, it was determined that 20-mm items were more difficult to find, and it is speculated that due to their size/mass they were likely falling within the noise limits of the test areas. Due to time considerations, this will be the only ordnance type used to study this effect.

b. In order to study noise effects, a method was needed to characterize a background noise level. The method used was to map out a test area, in this case the YPG open field, into grid cells 1 x 1 m². If no ordnance or clutter were within a grid box, that box would be considered blank. All blank boxes were assigned 0.5-meter halos at their center. Raw signal data were then processed for each system, and all signals within the 0.5-meter halos were selected. Only magnetometers were considered; therefore, magnetic field strength data were used (unprocessed). Absolute values of the signals were sorted through for maximum values occurring in the blank halos. All maximums were then averaged and standard deviations found. The averages represent maximum field levels, in an absolute sense, to expect from background noise in any given halo in the field. All data will be compared relative to the same system since it is not known what processing had been performed with each data set and because system noise levels are not known. Inherent system noise was assumed constant across the field.

c. The same methodology was performed for determining signal levels in the 20-mm projectile halos. Absolute values were found and maximum values averaged.

d. The results of the exercise for the 20-mm projectile round are shown in Figure 2.3.7-2. Signal returns are broken down into groups from two depth regimes:

- (1) Less than 0.133-meter depth.
- (2) Greater than or equal to 0.133-m depth.

e. All bars represent the average of the absolute maximum signal values for the halos in the labeled groups. The results from three MAG systems are shown. The signal levels from the rounds are indeed close to the background noise level, especially the group at depths greater than 0.133 meter (this is the median depth; items deeper than this value represent 50 percent of the population). The lines in the plot represent 1 standard deviation. When ranges of signal values within 1 standard deviation are compared, it is apparent that a good portion of 20-mm signals fall within the background noise range. As discussed in reference 5, signal-to-noise ratios below 2:1 are typically problematic. The deeper 20-mm population, >0.133 meter, are at this level, on average. As discussed in section 2.3.5.7, the MAG systems were missing more than 60 percent of the 20-mm projectiles at the APG open field. YPG MAG results were similar, except for system 651M, which found 70 percent of the 20-mm items, but with a very high BAR.

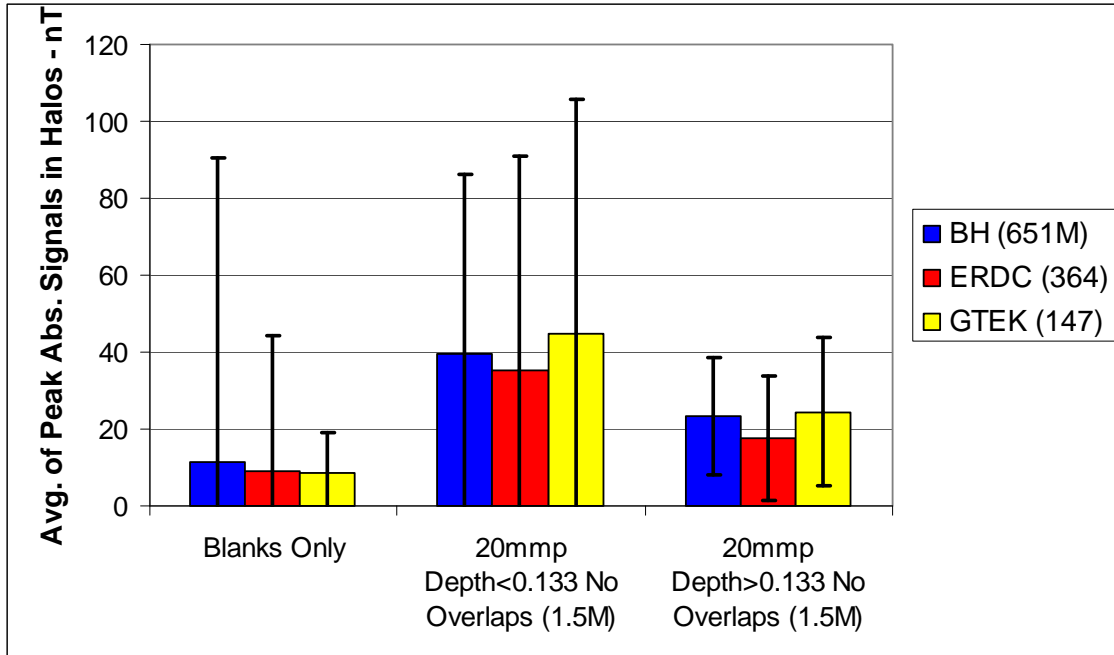


Figure 2.3.7-2. Signal (average peak absolute) to noise comparisons for the 20-mm projectile at YPG open field.

f. The GT used for the above exercise had no items within 1.5 meters to confuse signals. The value of 1.5 meters is borrowed from section 2.3.5.4 and represents where items in proximity begin to affect P_d^{res} scores in general. Initially, the exercise did not use the proximity criteria, and it was found that the average peak absolute signal from the 20-mm halos was approximately 25 times greater or more than the background noise level calculated. This did not make sense until the population of 20-mm items in proximity to other items was examined. A significant portion (actual percentage not given to preserve GT discovery) of the 20-mm population have items within 1.5 meters of them. Therefore, two drivers affect the low 20-mm detection rates: low signal-to-noise ratios and high levels of signal bleed over from items in proximity. If line spacing were decreased for the systems the signal-to-noise ratio may improve (analysis beyond the scope of this report).

g. Round-by-round analysis must be done to complete this study.

2.3.8 Production and Cost Rates

a. The following section will cover measures of time and cost as they relate to detection system performance. During the testing of the systems, a test log of hours spent setting up, calibrating, surveying, and demobilizing was kept as well as the number of personnel involved in the effort. Standard cost rates were applied to an assumed hierarchy of the personnel to generate total production costs. These values, along with acreage and time data, were used to calculate cost per acre and production rates.

b. The data in this section are based on test performance and not an actual production survey. It could be that more or less time and personnel would be used in actual production. Further, downtime due to maintenance and repair are included in the numbers. It is likely this may cause values to be inflated. In short, the potential of some systems may not be realized by the time and cost numbers shown.

c. What the numbers should show are rough order of magnitude cost and time estimates. The lowest values show what “is possible.” Also, because of the quantity of systems and test areas, general trends between basic system types and test area should be seen. Cost and time are shown along with P_d^{res} scores from the standard GT (GT exceeds system limits in some cases). It is difficult to show corresponding BAR scores on the plots without making them difficult to read. Therefore it is left to the reader to make finer comparisons using BAR scores and P_d^{res} scores shown in Figures 2.3.3-1 to 2.3.3-6 which use an 11D, no overlap, no challenge area GT. A low cost rate is not significant unless it is accompanied by a relatively low BAR score.

2.3.8.1 P_d^{res} versus Man-Hours/Acre

a. The total man-hours spent in setup, calibration, survey, and demobilization for a given test area were found for each system demonstrated. These values were divided by the corresponding test site acreages and plotted against P_d^{res} (fig. 2.3.8-1 through 2.3.8-6). The purpose of the plots is to show how labor intensive it is to operate the various systems.

b. When minimal man-hours per acre to achieve best P_d^{res} scores are compared between all test areas, two levels of effort are manifest. The APG and YPG open fields and YPG moguls show around 10 to 15 man-hours per acre are required. The remaining areas, which include APG woods, APG moguls, and YPG desert extreme, require twice the effort or more with minimal rates of about 25 man-hours per acre. One system defies this generalization which is the GEM-3 hand held system demonstrated at the APG moguls. This system had a good P_d score but a poor BAR score in the area and expended much labor, about 220 man-hours per acre.

c. If man-hours for the systems are compared in the open field areas (figs. 2.3.8-1 and 2.3.8-4), at first glance it will appear that from best to least best the platform trend is towed, sling, cart, and then hand held (symbols are color coded for platform type). Minimal man-hour rates for the towed systems are at approximately 2.5 hours per acre. However, when P_d^{res} values are considered, best scores appear to require 10 to 14 man-hours per acre and differences between towed, sling, and cart platforms are not as great. Hand held units in the open fields typically have lower P_d^{res} and higher man-hour values than other platform types.

d. All figures show an hour per acre annotation for one Schonstedt hand held unit that flagged anomalies but did not locate them in local geographic coordinates. The annotated value represents an estimate of how much more effort was required to locate the positions of the anomalies, via the flags, using surveying equipment. The cost is based on time to perform such tasks by proving ground personnel. This effort was required to give tabulated dig list locations for scoring at the test sites. At actual site surveys, flagging systems do not need to supply this data since the flags mark the dig location. Therefore, if one wants to subtract off the effort it will be in the order of a couple hours per acre.

e. Typically, three systems flagged targets in the test areas. They are indicated by a flag on their symbols in the plots below. In actual site surveys, no reacquisition of targets would be required for the systems that flagged. Rather, the systems that did not flag would incur additional expense to mark (flag) targets for digging. Depending on the number of false positives and BARs, this reacquisition cost/labor would vary. Therefore, when comparing non-flagging systems with flagging systems, time to reacquire targets is not shown for non-flagging systems. It is likely that a few hours or more per acre would be needed to reacquire and mark target positions (based on time to locate Schonstedt flag positions).

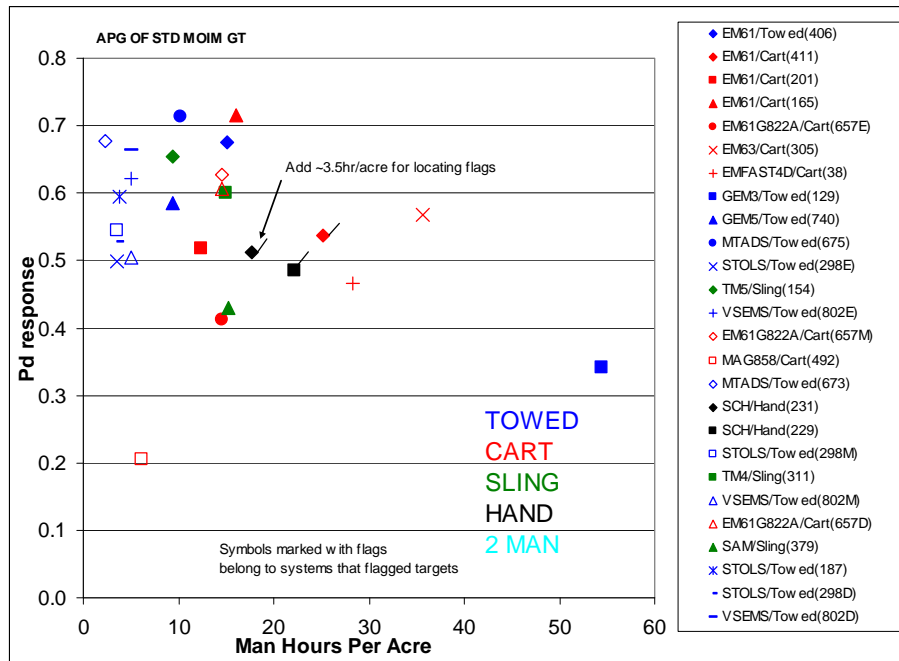


Figure 2.3.8-1. P_d^{res} , versus man-hours per acre, APG open field.

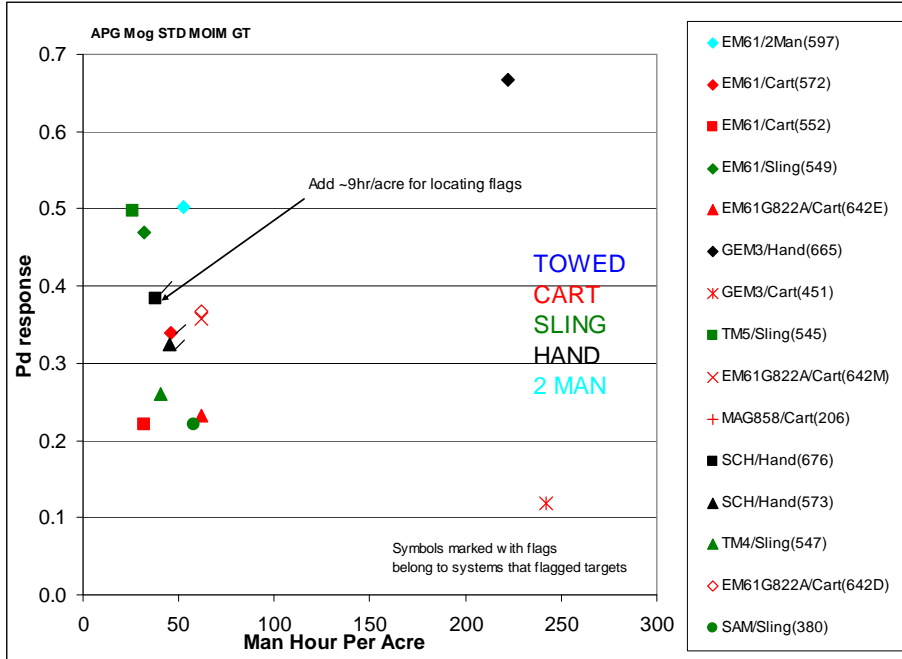


Figure 2.3.8-2. P_d^{res} , versus man-hours per acre, APG moguls.

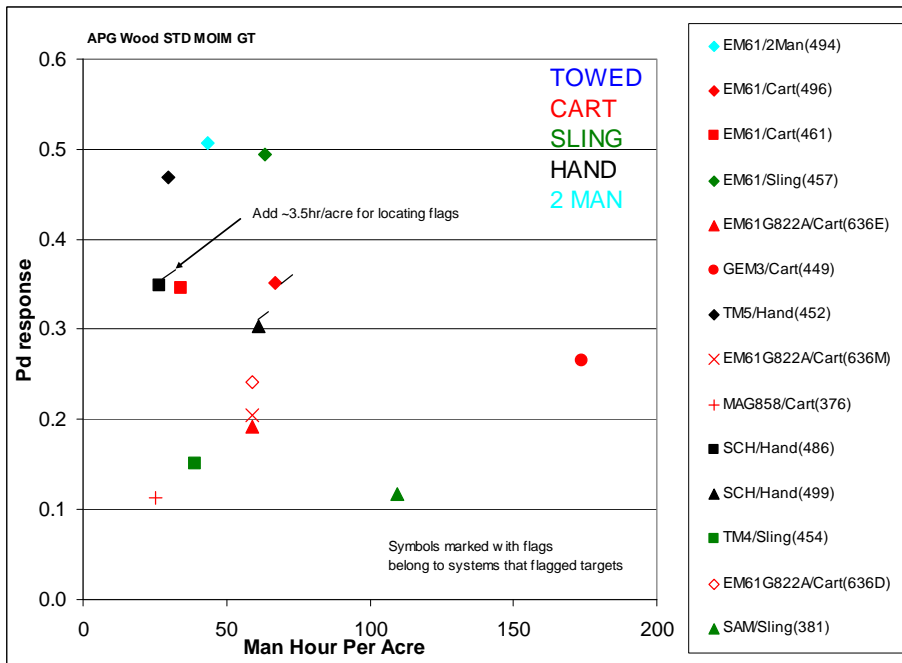


Figure 2.3.8-3. P_d^{res} , versus man-hours per acre, APG woods.

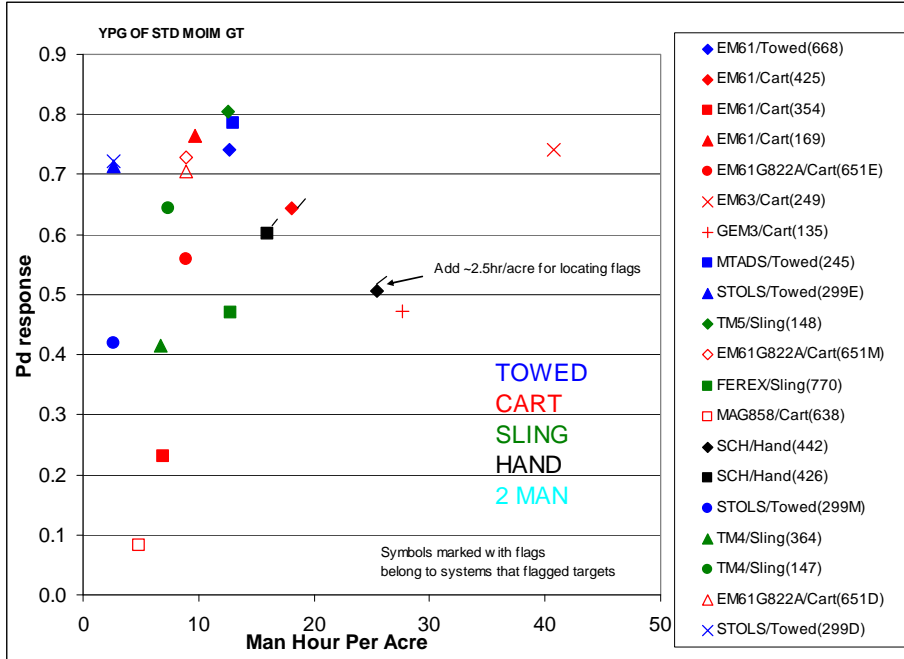


Figure 2.3.8-4. P_d^{res} , versus man-hours per acre, YPG open field.

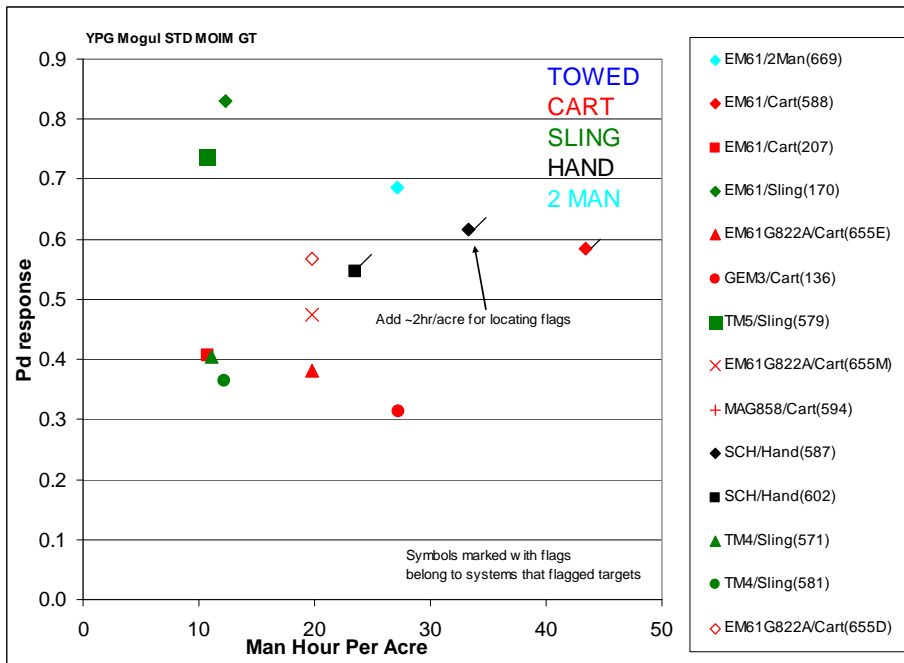


Figure 2.3.8-5. P_d^{res} , versus man-hours per acre, YPG moguls.

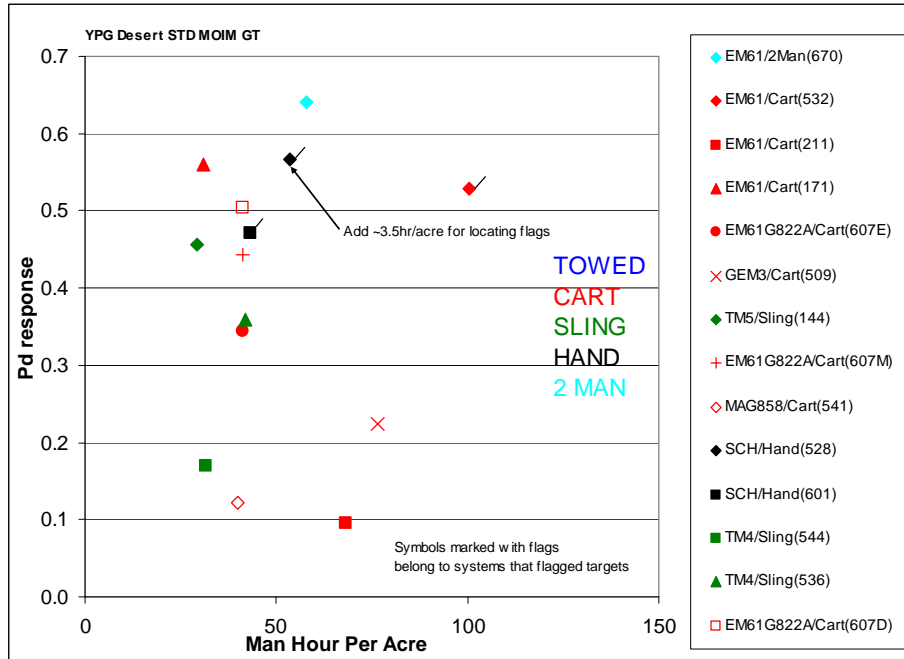


Figure 2.3.8-6. P_d^{res} , versus man-hours per acre, YPG desert extreme.

2.3.8.2 P_d^{res} versus Cost/Acre

a. Plots of P_d^{res} versus cost per acre for all demonstrators at the various UXO test areas are shown in Figures 2.3.8-7 through 2.3.8-12. Costs represent total production values for survey (from setup to demobilization). They do not include any type of post processing costs for the data taken, travel expenses, or reacquisition costs (only applicable to systems that did not flag, see section 2.3.8.1e). Cost was calculated using the following labor rates: supervisor = \$95.00 per hour, data analyst = \$57.00 per hour, and field support = \$28.50 per hour. A hierarchy of position was assumed for personnel using the following rules.

- (1) There must be only one supervisor.
- (2) If more than one person is in the work crew, there must be only one data analyst.
- (3) If more than two people are in the work crew, these remaining personnel will be considered field support.

b. Knowing the time spent in each phase (setup, calibration, survey, and demobilization) of testing and the number of personnel working in each phase of testing, total production costs were calculated using the above rules and rates. These costs were in turn divided by the acreage of each corresponding test site to get cost per acre values or operating costs.

c. This cost estimation is the product of the test site organization and does not represent any cost estimate data given by the demonstrators. The costs are rough order of magnitude and should provide a means of comparison of system operating costs between test areas and between system types. If flagging and non-flagging system costs are to be compared in a non-test environment, some adjustments need to be made to the costs shown. In general, a few hundred dollars per acre should be added to non-flagging system costs for reacquisition of target and a similar amount subtracted off of flagging system costs because of the test requirement to provide GPS derived coordinates.

d. The cost-per-acre trends are not necessarily proportional to man-hour-per acre trends since labor rates are not constant for each type of personnel nor are the amount of personnel the same between systems. However, similarities will be observed for both.

e. The best P_d^{res} scores (approximately 0.71 APG and 0.8 YPG) produced in the open fields have operating costs associated with them of about \$500 to \$700 per acre. These were produced by towed, cart, and sling based systems. Towed systems with performance that is about 3 to 10 percent off of the best P_d^{res} values are yielding costs of about \$140 and \$200 per acre, respectively. There may be a correlation between the towed platform speeds, cost, sampling rates per area and P_d^{res} . Such analysis will not be made but the reader is referred to section 2.3.11 to view sampling data characteristics versus P_d^{res} .

f. There is greater variation in cost than in man-hours expended from test area to test area. The following are the systems with highest P_d^{res} in each non-open field test area and their associated operating cost.

(1) APG moguls, GEM-3/hand held, P_d^{res} maximum = 0.67, cost/acre = \$10,660 (note the GEM3 had a high BAR score, the next best P_d^{res} = 0.50, cost/acre = \$1,950, TM-5/sling).

(2) APG woods, EM61/2-man-portable, P_d^{res} maximum = 0.51, cost/acre = \$3,250.

(3) YPG moguls, EM61/sling, P_d^{res} maximum = 0.83, cost/acre = \$940.

(4) YPG desert extreme, EM61/2-man-portable, P_d^{res} maximum = 0.64, cost/acre = \$3,030.

g. From the above costs, it is seen that terrains like the APG moguls, which are not navigable by towed platforms and are difficult even for carts, may very well cost approximately \$10,000/acre just to survey.

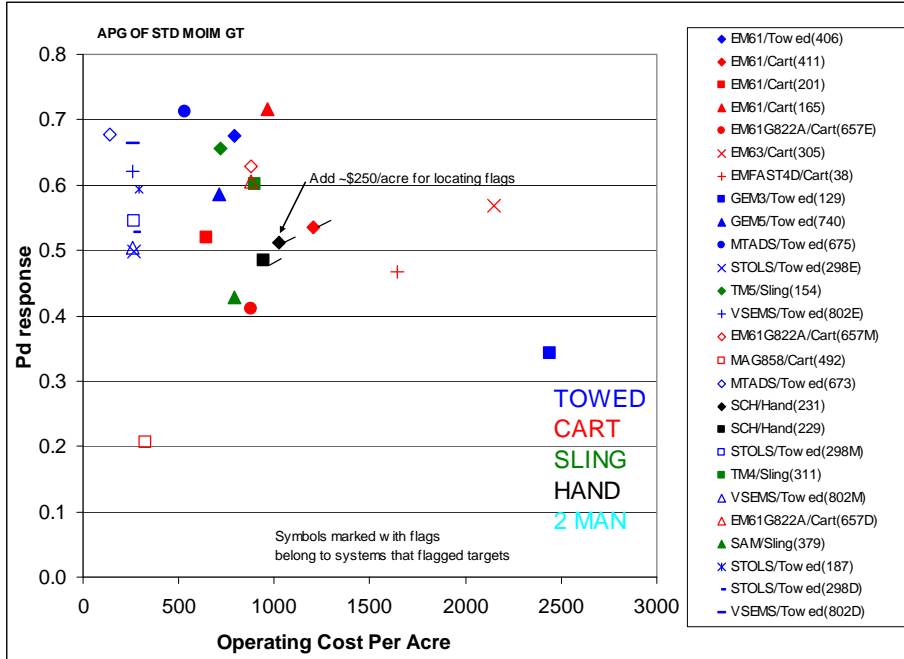


Figure 2.3.8-7. P_d^{res} , versus operating cost per acre, APG open field.

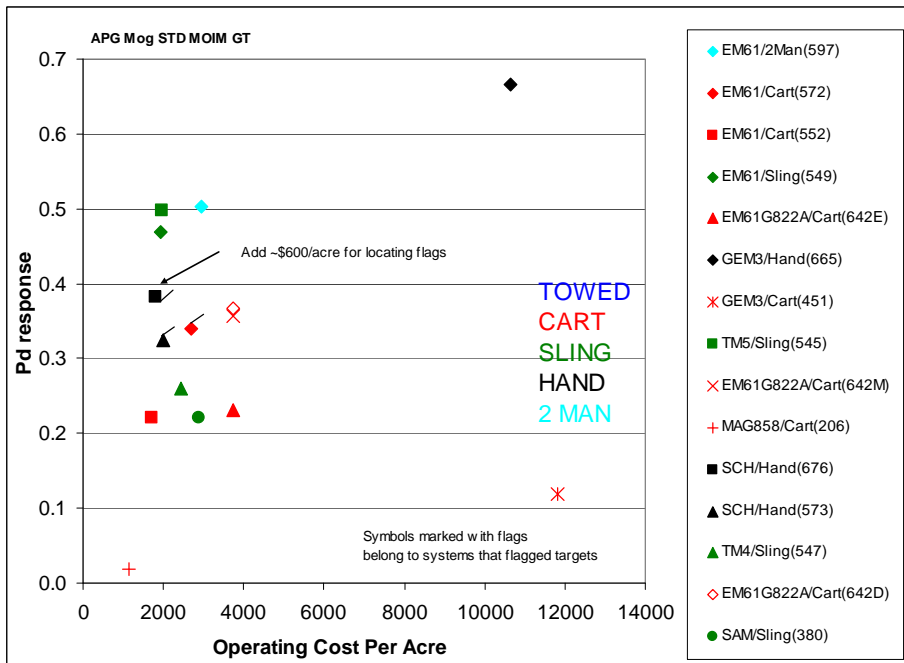


Figure 2.3.8-8. P_d^{res} , versus operating cost per acre, APG moguls.

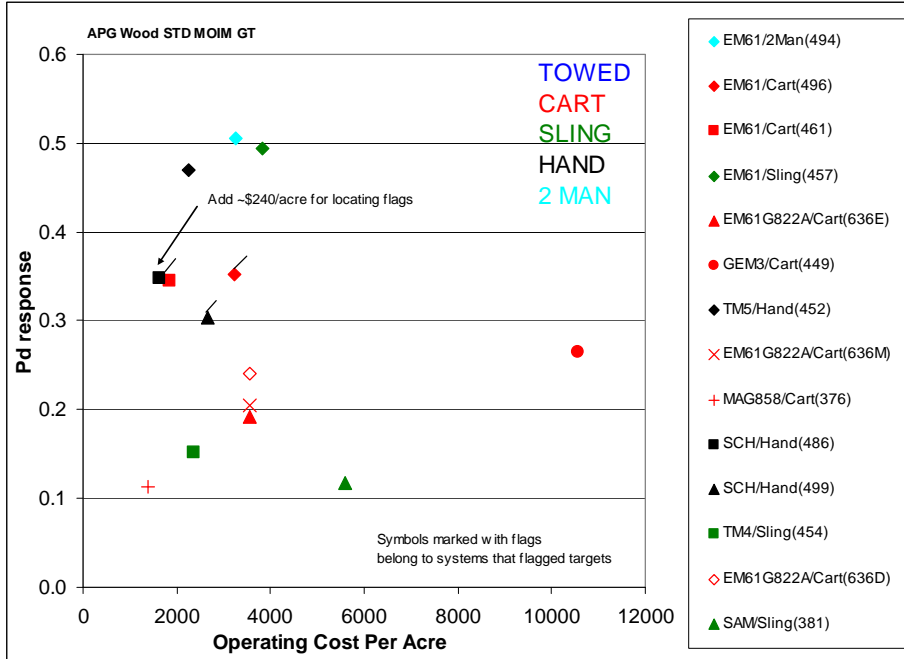


Figure 2.3.8-9. P_d^{res} , versus operating cost per acre, APG woods.

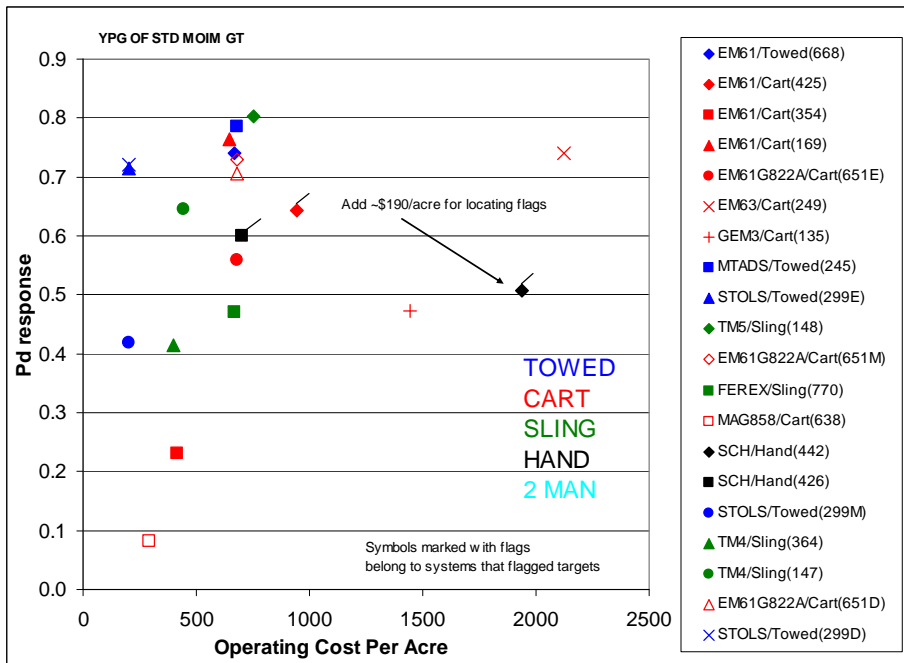


Figure 2.3.8-10. P_d^{res} , versus operating cost per acre, YPG open field.

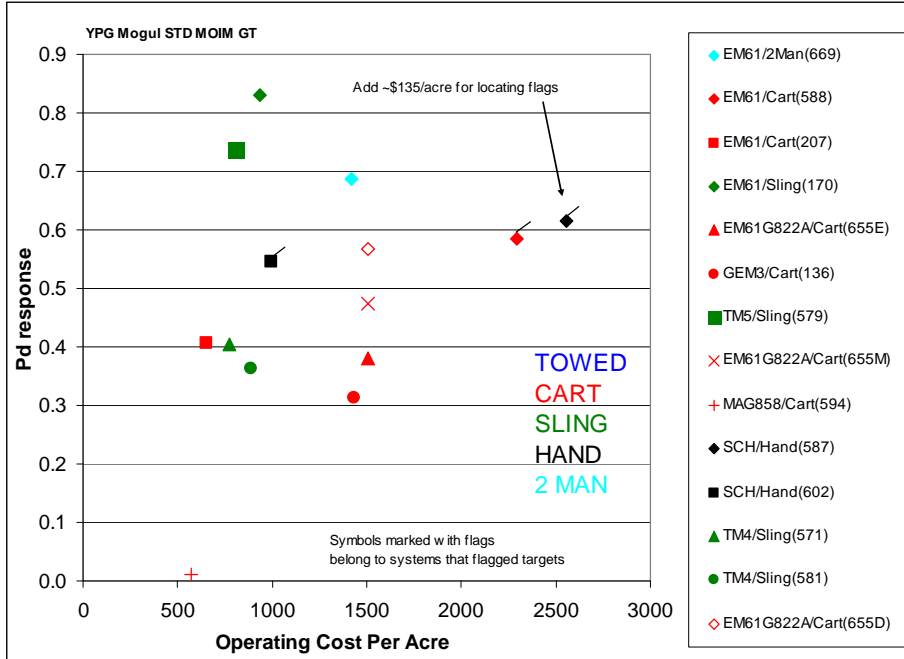


Figure 2.3.8-11. P_d^{res} , versus operating cost per acre, YPG moguls.

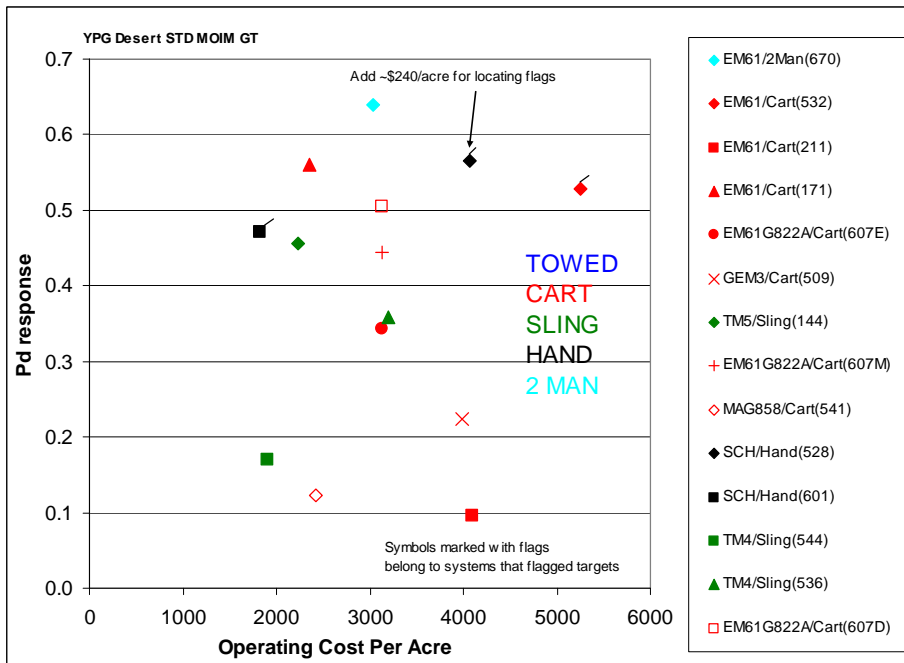


Figure 2.3.8-12. P_d^{res} , versus operating cost per acre, YPG desert extreme.

2.3.8.3 Total Cost

a. To show the effect of system performance on total site cleanup costs, a short analysis of these costs was performed for the APG open field. The system considered first is the EM version of MTADS demonstrated by NRL. The towed array system is one of the best performers at APG open field in terms of P_d^{res} and background alarm scores. A total site cleanup cost breakdown using the MTADS results are shown in Figure 2.3.8-13, except that a 100 percent detection rate was assumed for ordnance items. This will increase the dig and detonation costs to reflect a complete site cleanup cost. All costs shown are estimates of the test authority and are based on performance and not on demonstrator input.

b. The site survey cost shown is based upon personnel used and time spent. This survey cost, \$7500 (actual rounded to the nearest \$500), does not include target reacquisition, travel, or data processing costs. Reacquisition was estimated to cost about \$8000 and is based upon reacquiring all targets (ordnance, clutter and background alarms). Response stage targets are used since discrimination ability is insufficient. Travel costs were estimated for four people traveling (by road) 2 half days and surveying 2 days. Meal and hotel expenses were included. The travel costs were estimated at \$2,500. Data processing costs were estimated on the low side at \$4,000. These costs could be as high \$20,000 or more. Thus, the total site survey package was estimated to cost about \$22,000.

c. Using time and manpower data from current dig and detonate operations at APG, costs were estimated for removal of ordnance and clutter along with discovery of background alarms. Again, it was assumed that a 100 percent detection of ordnance occurred. It is estimated that it would take approximately \$20,000 to unearth all the ordnance in the APG open field and \$80,000 to detonate these items. To unearth the clutter items it is estimated that it would cost about \$27,500 and to discover the background alarms (false alarms) it is estimated that it would cost \$64,500. The amount of clutter assumed is the amount detected by the MTADS system. Further, the number of background alarms that would be discovered to be such upon digging are those coming from the MTADS system.

d. Administrative costs are considered to include planning, documentation, and coordination components. Total cost is estimated at \$12,000.

e. When all costs are summed, the total site cleanup cost is estimated to be about \$288,000. This cost is likely on the low side but should represent most major costs at a rough order of magnitude. In a real world scenario, one or two additional systems would survey (sweep operation) and hence further increase the total cost (would probably approach ~\$400,000).

f. When the total site survey cost is compared to the total site cleanup cost, it is seen that the survey package comprises about 10 percent of the total cost.

g. The ordnance removal costs in total comprise about 45 percent of the total costs and effectively should not change. The administrative costs would also be fixed. Thus, about 50 percent of the total costs cannot be affected by detection technology. The part that is affected is a product of detection technology, namely the number of background alarms followed by the number of non-rejected clutter items. Costs to reacquire and discover these items comprise approximately 40 percent of total cost. Thus, it is seen how important development of discrimination technology is from a cost standpoint.

h. Finally, it should be kept in mind that the cost comparison performed here is site specific and is subject to change for other sites depending on GT composition.

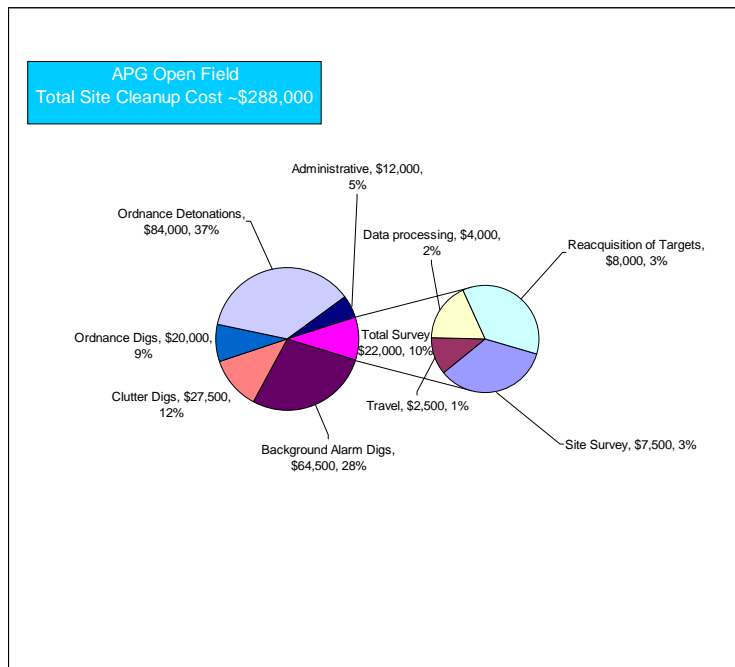


Figure 2.3.8-13. P_d^{res} , versus operating and dig cost per acre, APG open field.

i. The top performing EM and MAG systems in the APG open field are next considered along side the Schonstedt baselines. All non-fixed costs (clutter digs, background alarm digs, travel, data processing, reacquisition, and site survey) will be compared. One hundred percent ordnance detection is assumed to calculate reacquisition costs. Travel costs are estimated for carts and slings to be 60 percent of that for towed platforms and costs for hand held units to be 30 percent of towed platform values. Data processing costs are assumed to be \$4000 for all but the Schonstedts, which effectively have none (any that was done would be reflected in survey costs). The total costs are divided by the test area acreage and should approximate rates for a similar sized site with a similar GT configuration. The GT used is an 11D, no challenge area (wet areas eliminated), no overlap (no items closer than 1 meter) version. The cost comparisons are shown in Figure 2.3.8-14.

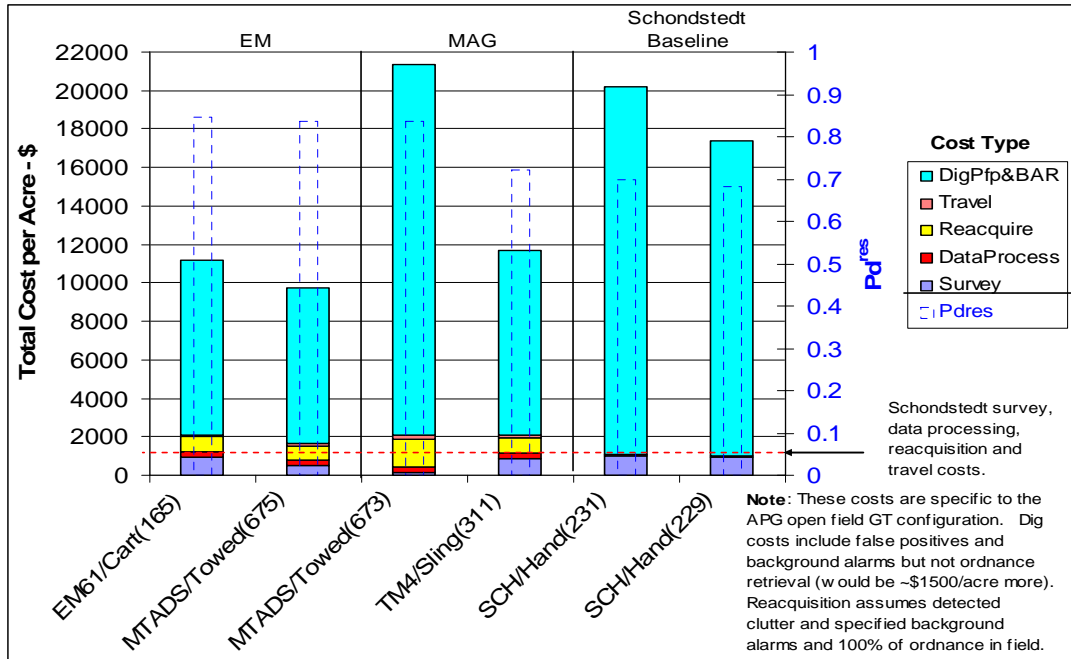


Figure 2.3.8-14. P_d^{res} versus operating and dig cost per acre, APG open field.

j. The systems are separated by basic sensor type in Figure 2.3.8-14. P_d^{res} scores are on the right vertical axis and are represented on the plot by dashed rectangles. It is seen that the best EM and MAG P_d^{res} scores are about 0.85 (85 percent ordnance detection), and the Schonstedt scores are about 0.7 (70 percent ordnance detection). Thus, the best systems have about a 20% greater detection score than the Schonstedts in the open field (Schonstedts do relatively better in rougher terrains and small areas).

k. As shown in Figure 2.3.8-14, when the total of all of the non-dig costs (travel, reacquire, data process, and survey) are compared, the Schonstedts are the least expensive system. However, when the dig costs are factored in for clutter and background alarm discovery, the Schonstedts become among the most expensive systems in overall result.

l. In the APG open field test area, which contains challenging varieties, depths, and densities of ordnance and clutter, the best detection systems find about 20 percent more ordnance than Schonstedt systems at about one-half the overall resulting cost. When deeper and more dense GT are added (as in the standard GT), the relative Schonstedt results become worse. These results should help the reader to have a greater appreciation for parameters governing overall costs.

2.3.8.4 Production Rate

a. The average, maximum, and minimum production rates for all systems in all areas were found and are shown in Figure 2.3.8-15. The values represent the time to survey an area from setup to demobilization, including calibration.

b. As shown in Figure 2.3.8-15, the towed array systems break away from the pack on flat grassy terrains, as in the APG open field. The best rate in that area, by the MAG version of NRL's MTADS system, is about 1.3 acres per hour. The P_d^{res} for this system was 0.68 (third best for area using standard GT) but it had a relatively high BAR score compared to better performing EM systems.

c. Rates of less than 0.2 acre per hour are all that could be achieved in terrains with brush, trees, gulleys, or pronounced moguls.

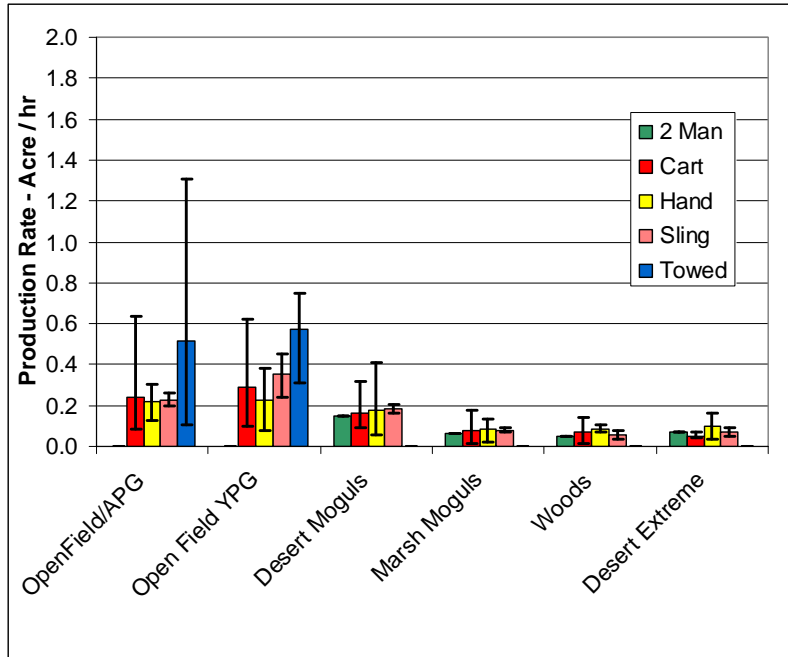


Figure 2.3.8-15. Production rates.

d. A plot of survey rates that exclude calibration, setup, and demobilization time is shown in Figure 2.3.8-16 for all systems. Production rates will likely approach survey rates for larger sites where setup and calibration are a smaller part of total time spent.

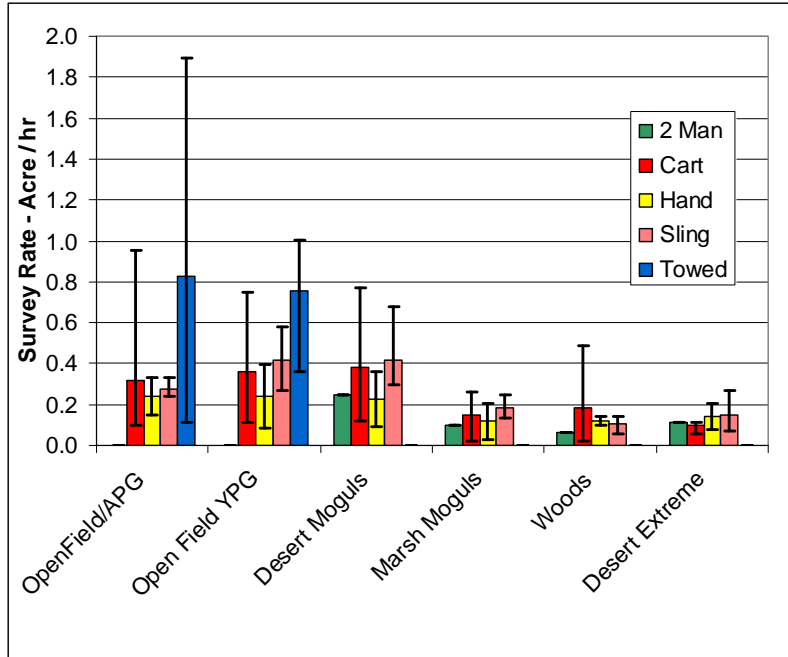


Figure 2.3.8-16. Survey rates.

2.3.9 Technology Comparisons

2.3.9.1 *Dual versus Non-dual Systems*

a. Dual mode systems are composed of two sensor types operating in tandem on the same platform. EM and MAG sensors were typically combined and demonstrated at the standardized sites. The details of how the demonstrators combined or fused their data are beyond the scope of this report. The demonstrators that used dual systems were asked to submit three dig lists, one for each component system and one for the combined system. The purpose of this request was to allow direct comparison of performance between component and combined components of the systems. (It is not known to what extent single components were optimized for dual use.)

b. The probability of detection for the dual systems demonstrated at the APG and YPG open fields in the response stage is shown in Figures 2.3.9-1 and 2.3.9-2. BAR scores are also shown in the figures. Individual and combined sensor performance results are shown. Also shown are the results of all systems (including non-dual) demonstrated at the respective sites, as represented by maximum, median, and average values of P_d^{res} . The GT used contains both ferrous and non-ferrous items; thus, the MAG scores are biased on the low side.

c. The figures show that a 0.01 to 0.05 P_d^{res} increase above the best constituent performance is afforded by combining sensor data in a dual mode. The best P_d^{res} result is from the VSEMS system in the APG open field. It is noted that this system was tested after the open field GT was reconfigured. While clutter and ordnance distributions remained essentially the same as the old configuration, many items contributing to background noise ended up being removed. Therefore BAR scores from the VSEMS can not be compared directly with all other values shown in Figure 2.3.9-1. The BAR score is likely on the low side for the VSEMS and could not increase more than 0.2 if the items were put back in the ground and all flagged as anomalies. It is also noted that system scores for report numbers 675 and 298 are not corrected for wet areas that were not surveyed (Pd and BAR would increase) as is done when the 11D, no overlap, no challenge GT variant is used. The standard GT result is used here because it shows a greater benefit from the dual system combination. The standard GT has items closer together and deeper than the 11D variant.

d. In general, community wide, dual systems perform above average.

e. It is not known to what extent dual system performance benefits are resulting simply from increased data density.

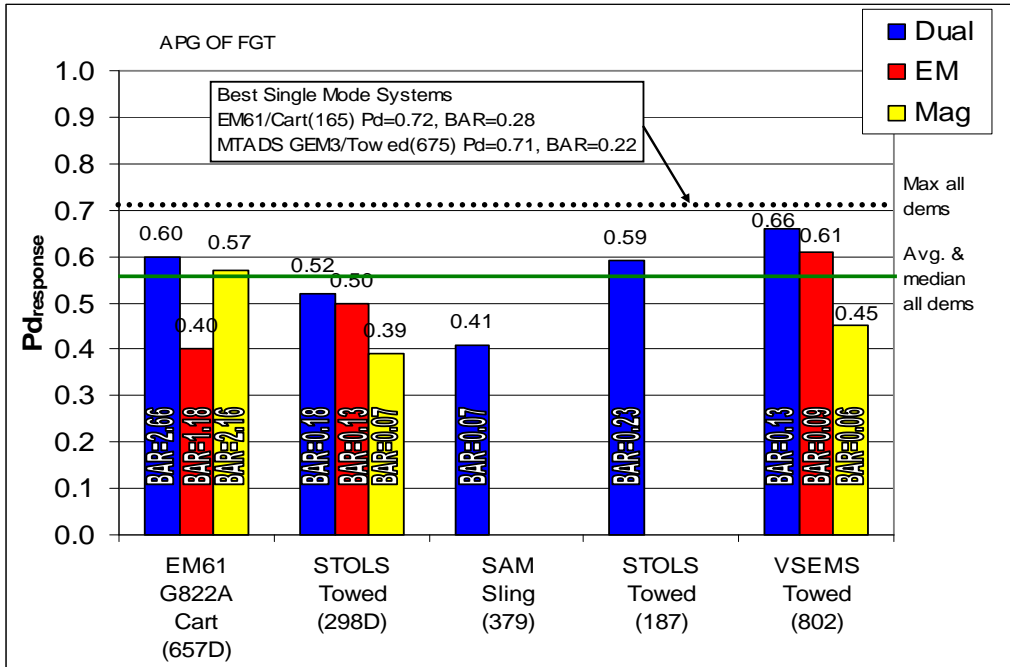


Figure 2.3.9-1. P_d^{res} , for dual and single counterparts in APG open field.

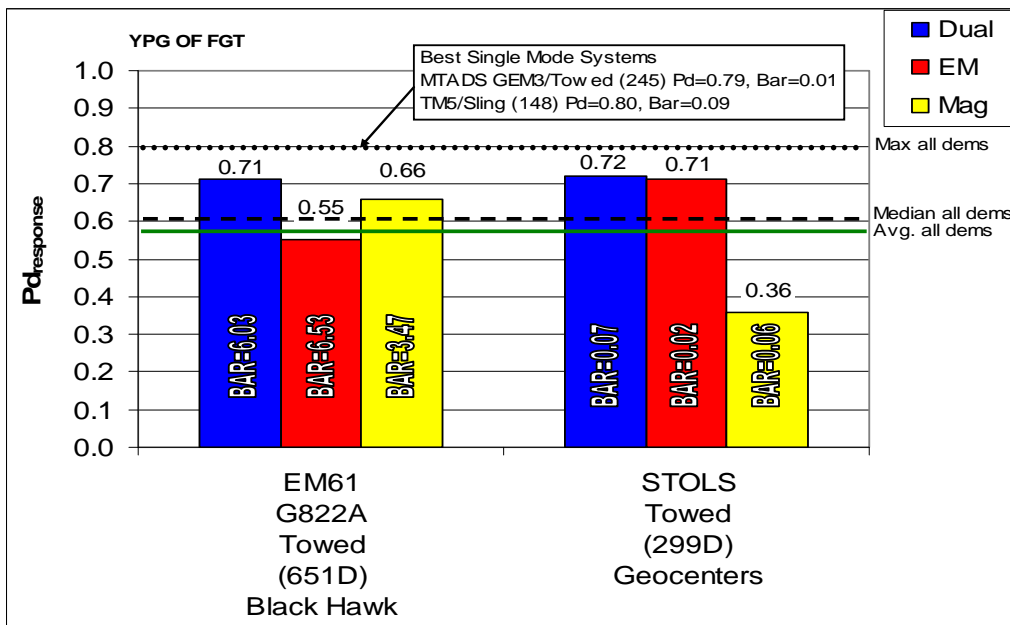


Figure 2.3.9-2. P_d^{res} , for dual and single counterparts in YPG open field.

2.3.9.2 *Digital Geophysical Mapping (DGM) versus Flag*

a. One of the more common ways to detect buried UXO is to use MAG and Flag or EM and flag techniques with a hand held unit. With these flag techniques, typically the operator surveys over the area using an instrument that does not collect and store data. If the instrument detects an object then the instrument informs the operator (usually by emitting an audible signal). Once the instrument alerts the operator to the presence of an object, the operator can immediately resurvey the area to get an accurate fix on the location of the item. Typically, an operator will place a flag into the ground directly over the suspected object. Then the area around the flag can later be excavated in order to find the buried object. If such a system/technique is used at the standardized UXO detection sites, after the operator is finished placing the flags, the flags must be surveyed so that their locations can be tabulated as part of a dig list.

b. One major advantage of this system/technique is that it excels in very difficult terrains. A disadvantage is that large areas can become cumbersome to survey and as a result quality may suffer. Another disadvantage is the extra time/cost it takes to survey the location of the flags if needed. Also, the operator is dependent on his own memory and skill to locate and identify an item.

c. Another technique for surveying an area where UXO is suspected to be buried is the use of DGM. With DGM, an operator will survey the site with an instrument that is continuously collecting signal, location and time data. Location data is typically provided by a GPS system. The data that are collected will typically be sent to a skilled geophysicist to be processed. The geophysicist will apply a variety of algorithms to the data in order to compile a dig list of locations where suspected UXO like items are buried.

d. The advantage of this technique is that it offers a large picture of signal returns to be viewed at one time which permits better interpretation of the sensor data. The disadvantage of this technique is that if additional information is needed a resurvey may not be convenient depending on whether or not real-time processing was performed. Further, for rough terrains, more elaborate instrumentation is required to orient/locate a sensor platform relative to the topography being surveyed. Finally, extra cost is required to mark dig locations after the survey unless real-time processing is used.

e. Up to this point in the report, the results of all system configurations have been compared side-by-side, and it has been seen that often MAG and Flag, and EM and flag, systems are outperformed by systems that geophysically map items in the ground. Some of the performance differences may be due to sensor and platform differences. To better isolate trends, a plot of only hand held platform performance, as measured by P_d^{res} and P_{ba} in the APG blind grid, is shown in Figure 2.3.9-3 (no depth limits are imposed). When EM systems are compared, the systems that used geophysical mapping to locate anomalies typically performed better. To what degree the different system types are contributing to performance differences cannot be established.

f. In terms of location error, the flagging technique used by hand held units works very well, only surpassed by towed platforms using the geophysical technique on flat terrains (see section 2.3.4.2).

g. In summary, it appears that geophysical mapping and processing has proven itself not only a viable technology but a reliable technology for all terrains. This is attested to by all best performers in each test area using the technology. Further the technology consistently, when configured with different sensors, outperforms flagging technology in these terrains.

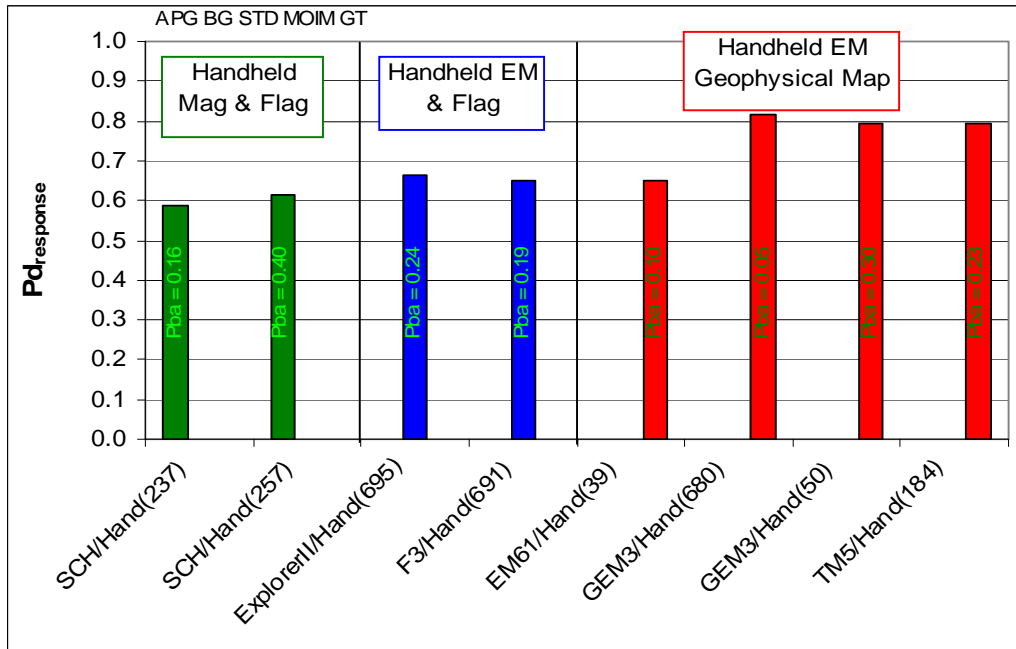


Figure 2.3.9-3. P_d^{res} for systems that Flag and that process geophysical data, APG blind grid.

2.3.10 *Operational Requirements Document (ORD) Evaluation*

a. The U.S. Army, through their Environmental Quality Technology (EQT) Program established an ORD in April 2002 (ref 6). The document gives guidance to the type of systems to be developed and demonstrated at the Standardized UXO Demonstration sites in light of expected operational requirements. The ORD also sets forth threshold and objective requirements for performance that are considered a leap ahead of year 2002 technologic capability and deemed necessary for practical use. The following section will evaluate how the technologies demonstrated at the standardized sites relate to the ORD metrics. Not all requirements will be evaluated since some pertain to the transfer of government developed technology to the contract community. Nonetheless, where applicable, an assessment of how development and performance requirements in the ORD are being met by the demonstrated technologies will be made.

b. In section 4.1.2 of the ORD, a table of “threshold” and “objective” metrics are established in six categories of performance. The threshold values represent acceptable measures of performance while the objective values represent developmental targets. Demonstrated performance at the sites will be compared with these values. Results for one GT variant will be shown from the sites. The variant uses only items less than 11D deep and contains no items in challenge areas (including wet areas) or items within 1 meter of a GT item (i.e., no overlapping halos). Only open field results will be examined, since this area is more common and is the easiest of terrains to detect ordnance.

c. The first performance category evaluated is P_d^{res} . A 0.95 threshold and a 0.98 objective value are specified in the ORD. The P_d^{res} value for each system tested in the open field at APG and YPG using the GT variant discussed above are plotted to see how the demonstrated technologies compare to these values. The plots are shown in Figures 2.3.10-1 through 2.3.10-2.

d. As shown in Figures 2.3.10-1 and 2.3.10-2, the P_d^{res} threshold value of 0.95 is currently being met by SOTA systems at YPG, The threshold value is not being met at APG, however, when the MK118 and 20mm items are eliminated from the GT and better ground coverage quality controls are employed, better systems are within .01 to .02 from the value (see Figure 2.3.5-14). If “individual” ordnance results in a no challenge, no overlap (1 m), <11D depth environment are examined (app G), it will be found that 8 of the 14 ordnance types can be detected at or above threshold value in both open fields. Four ordnance types can be detected at or above objective values at both open fields. Finally, it is noted that a majority of systems meeting the requirements have relatively low BAR scores. Therefore SOTA system designers appear to be on track for the development of needed detection capability.

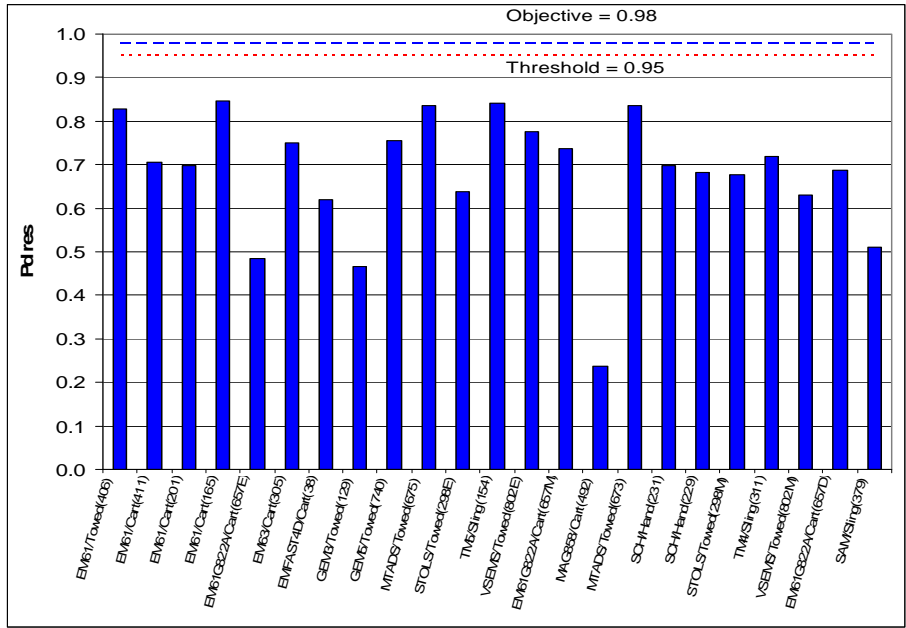


Figure 2.3.10-1. P_d^{res} , for systems demonstrated at APG open field, 11D depth limit, no overlap, no challenge area, all ferrous GT used for MAG systems.

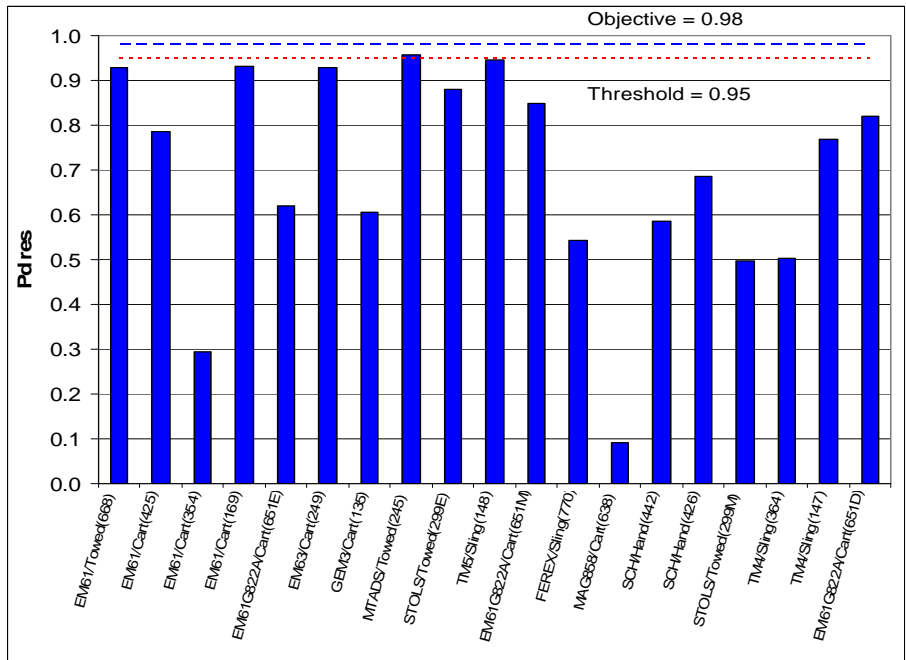


Figure 2.3.10-2. P_d^{res} , for systems demonstrated at YPG open field, 11D depth limit, no overlaps, no challenge area, all ferrous GT used for MAG systems.

e. The second performance category evaluated is discrimination as measured by the clutter rejection rate. Ideally, when a demonstrator discriminates the items in the list of response stage anomalies, the goal is to eliminate or reject 100 percent of the non-ordnance or clutter items. A 75 percent threshold and 90 percent objective value are specified in the ORD. A comparison of these requirements against demonstrated performance at APG and YPG open fields is shown in Figures 2.3.10-3 and 2.3.10-4.

f. Upon examination of Figures 2.3.10-3 and 2.3.10-4, it is seen that the best clutter rejection rates fall about 9 percent below the threshold at APG and about 25 percent below the threshold at YPG. However, the next group of figures show that the clutter rejection rates come at the cost of rejecting significant amounts of ordnance.

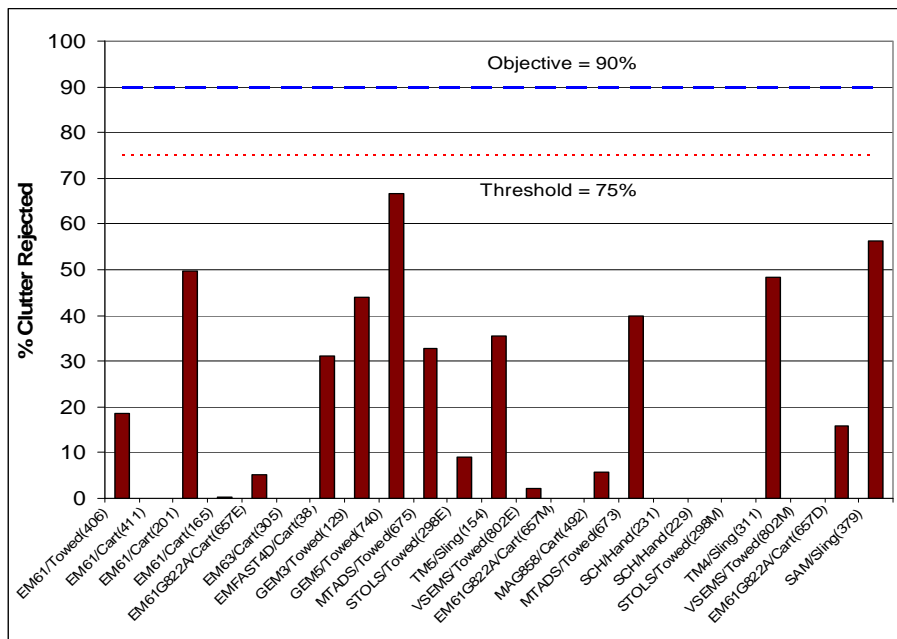


Figure 2.3.10-3. Percentage of clutter rejected, $R_{fp}^{disc} \times 100$, for systems demonstrated at APG open field, 11D, no overlap, no challenge area.

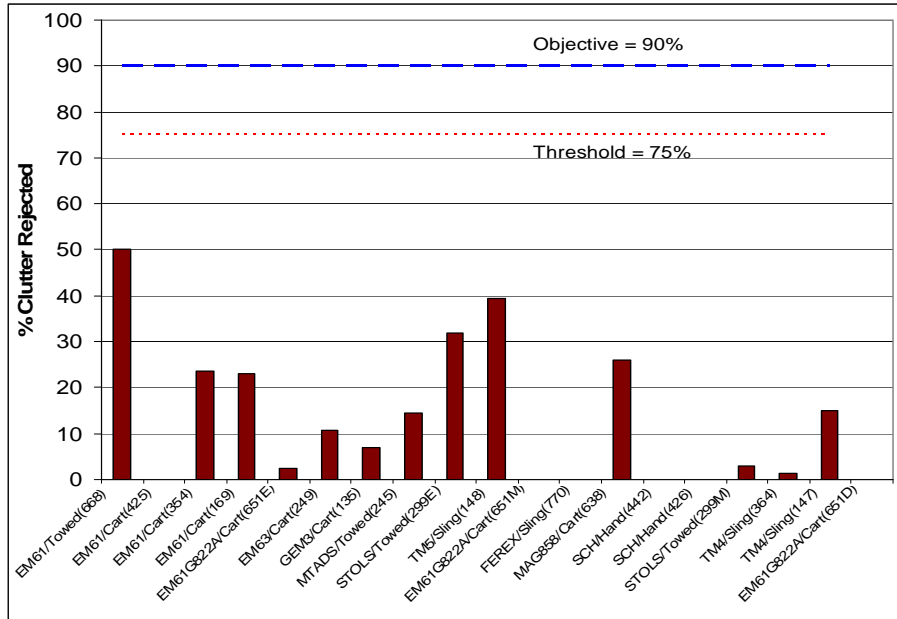


Figure 2.3.10-4. Percentage of clutter rejected, $R_{fp}^{disc} \times 100$, for systems demonstrated at YPG open field, 11D, no overlap, no challenge area.

g. One other measure of discrimination ability, false negative rejection rate (R_{fn}^{disc}), is also evaluated. This rate is the amount of ordnance detected that is called clutter by a demonstrator upon discrimination. A 5 percent threshold and 0.5 percent objective value are specified in the ORD. A comparison of these requirements against demonstrated performance at APG and YPG open fields is shown in Figures 2.3.10-5 and 2.3.10-6.

h. The figures show that the threshold and objective values can be met by systems, but it is known that if a demonstrator makes little effort to discriminate, most anomalies will be called ordnance and the false negative rates will be low. So, the results should be looked at in light of other detection and discrimination metrics for balance. When results are compared with figures 2.3.10-3 and 2.3.10-4, it will be seen that when small amounts of ordnance are misidentified (false negative), large amounts of clutter end up being misidentified. In summary, discrimination ability demonstrated at the sites does not meet threshold requirements for discrimination as a whole as specified in the ORD. Future test sites with a smaller variety of ordnance may reveal a more favorable result for SOTA discrimination ability.

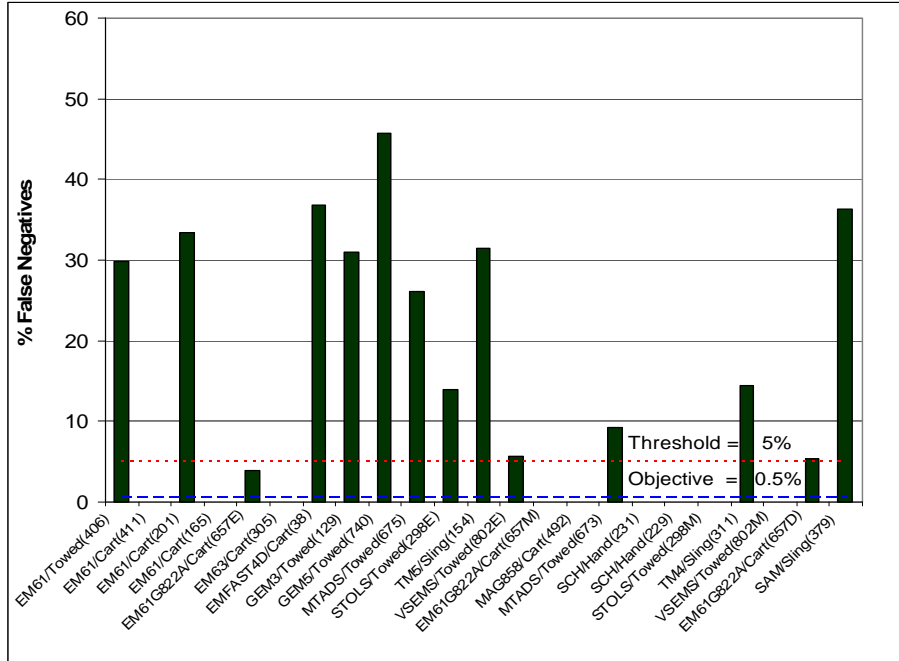


Figure 2.3.10-5. Percentage of $R_{fn}^{disc} \times 100$, for systems demonstrated at APG open field, 11D depth limit, no overlap, no challenge area, all ferrous GT used for MAG systems.

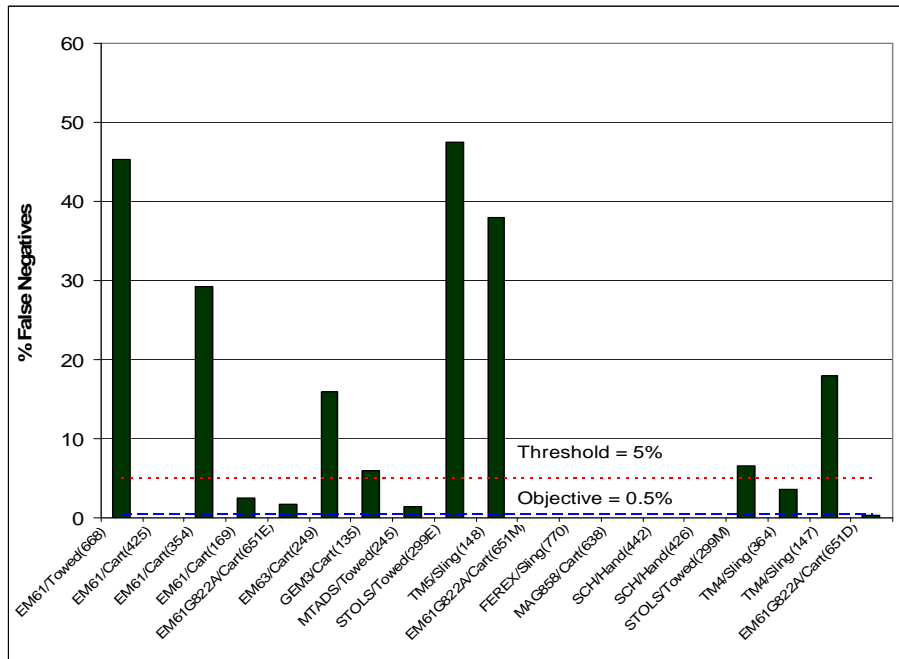


Figure 2.3.10-6. Percentage of $R_{fn}^{disc} \times 100$, for systems demonstrated at YPG open field, 11D, no overlap, no challenge area, all ferrous GT used for MAG systems.

i. The third performance category evaluated is reacquisition error. This error was not truly measured for systems at the sites. The geophysical mapping systems were not made to physically reacquire their target locations once identified, they were only asked to submit calculated locations in a dig list. If ATC personnel had to reacquire the target locations from the systems, location error of surveying equipment would average about 0.01 meter using best surveying practices. This would meet the objective reacquisition error requirement of 0.1 meter. It would also have a negligible impact on the overall location error of the systems. If reacquisition error is meant as overall location error from the GT after reacquisition, then the error is closely approximated by the location error of the systems alone. The best values demonstrated at each test area are shown in Figure 2.3.10-7.

j. As shown in Figure 2.3.10-7, the best location error in each test area falls within the threshold requirement of the ORD for reacquisition. One value, 0.09 meter, falls within the objective value. This value is from the MTADS towed array system (EM, report No. 245).

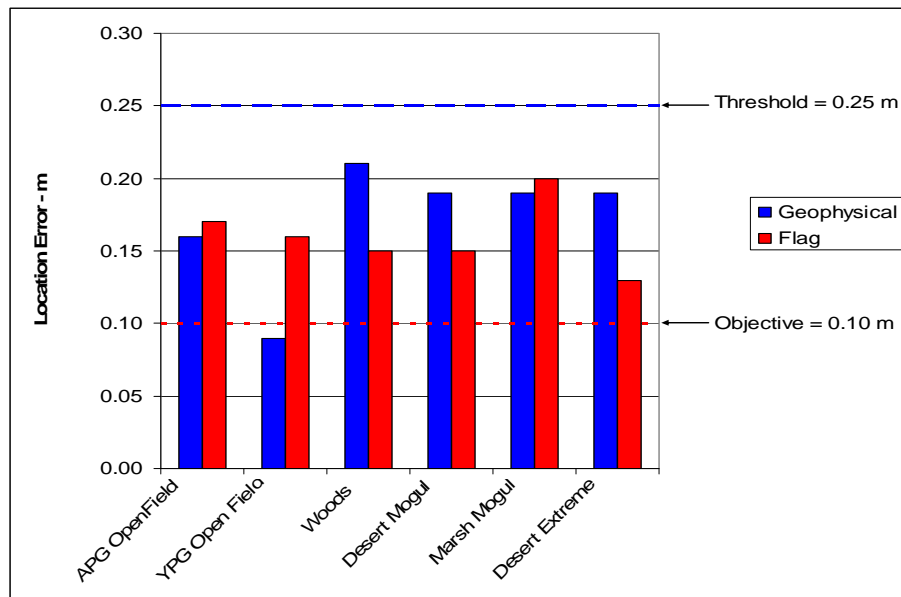


Figure 2.3.10-7. Best location/reacquisition error demonstrated in test areas at the standardized sites.

k. The fourth performance category evaluated is cost rate, which is a measure of production cost, based on time spent (including setup, calibration, and demobilization) in the open field and number/type of personnel working, divided by acreage. A \$4000/acre threshold and \$400/acre objective value are specified in the ORD. A comparison of these requirements against demonstrated performance at APG and YPG open fields is shown in Figure 2.3.10-8. The costs shown do not include travel, post-processing, and reacquisition costs.

1. The values shown in Figure 2.3.10-8 are average costs for the whole community of systems demonstrated, along with maximum and minimum values. The minimum values for all three basic sensor types at both open fields are within objective values. Further all maximums are within threshold requirements. Reacquisition costs are not a part of the calculated cost values, as stated above. Such costs are estimated to be as high as \$600/acre for the better performers at APG open field and will likely bring survey costs above the objective threshold. Further, if data processing costs are included, additional costs of approximately \$300 to \$2000 per acre are possible. Future tests at the sites should require demonstrators to supply data processing costs.

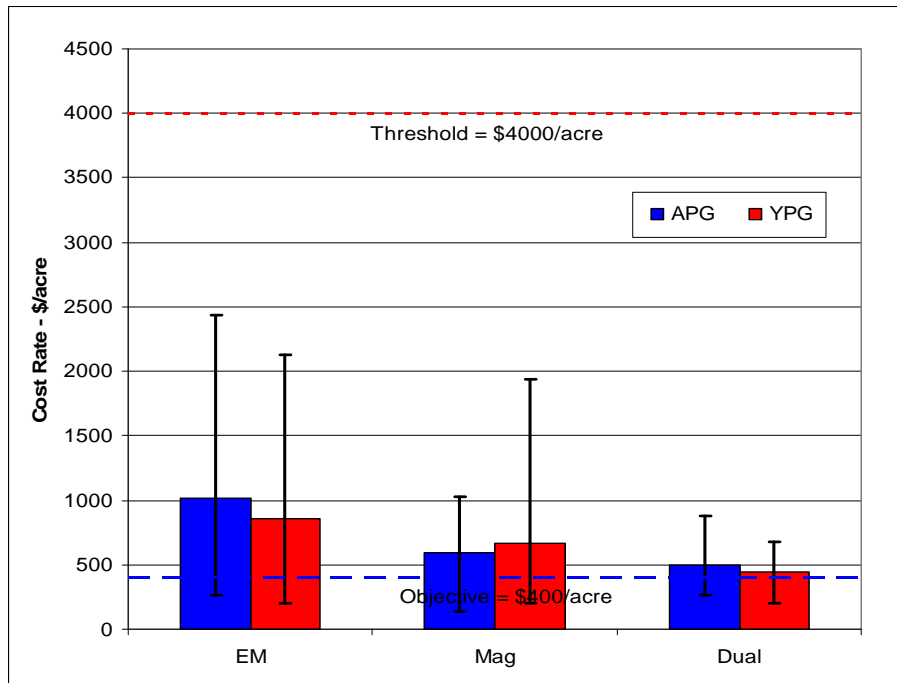


Figure 2.3.10-8. Average cost rates with maximums and minimums, APG and YPG open fields for all demonstrators.

m. The fifth performance category evaluated is the ability of detection technology to operate in all test areas at the standardized sites. The test areas represented at the sites are moguls (desert and marsh), desert terrain, open field (desert and grass), and woods. The threshold metric is simply the ability to operate in the areas, and the objective metric is to have unhindered access to all of the areas. By observation of test site personnel, the former requirement can be met by SOTA technology, but the latter requirement is not being met in desert extreme and wooded areas (the major hindrance being brush).

n. The sixth and final performance category evaluated is production rate. The threshold value required is 5 acres per day (0.625 acre per hour for 8-hr workday), and the objective value targeted is 50 acres per day (6.25 acres per hr). A comparison of these values is made in Figure 2.3.10-9 against average production rates, as well as maximums and minimums, for all systems demonstrated at the various test areas. In the open fields, some systems (towed arrays) meet the threshold requirement; however, no systems meet the objective requirement.

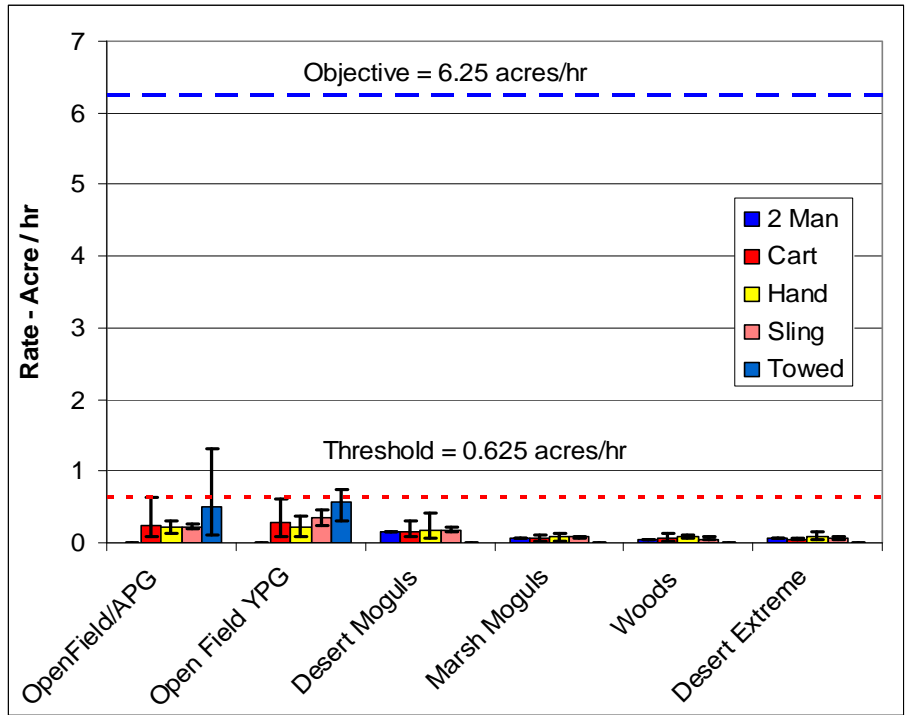


Figure 2.3.10-9. Production rates for all APG demonstrated systems at various test areas.

2.3.11 Optimization

a. Given the data available, efforts have been made to look at different ways system performance might be optimized. From a discrimination standpoint, it was shown that optimizing threshold values in the discrimination stage did not make much difference in results (see section 2.3.3.3). No attempt was made to optimize response stage thresholds to see how much detection rates increase, since most demonstrators supplied no data below threshold values. Optimum halo sizes were examined for digging and scoring (section 2.3.4.4 and 2.3.6). It is suggested in section 2.3.4.1 that if quality controls are optimized to verify coverage, minor gains in P_d^{res} may result. Finally, one area not yet considered is the determination of the minimum number of systems required to survey an area to give optimum detection rates.

b. The practice of having multiple systems come in to survey a site in order to increase the number of detected ordnance is not a new concept. The benefit of this practice primarily results from effectively increasing the sample density (samples per area) of signal returns. However, this is not in a fused sense, for the “results” are being superimposed, not the raw data. This mode of thought brings to light a second means of optimization, namely finding the value of sample density by which systems will achieve maximum or diminishing returns in P_d^{res} .

c. The optimum number of systems to survey an area and possible optimum sample densities will be examined in this section. It is realized that coil size, sample rate, translation speed, and transmitting power (EM), operating modes, etc., will affect sample density considerations. Further, GT characteristics (depth, density, and size) will affect system configurations. Results presented represent general trends at best and apply to “similar” systems.

d. The raw/unprocessed data from the detection systems are required to determine the average number of samples taken per square meter in the ordnance halos. These raw data files are huge and prohibit, because of time considerations, analyzing all systems at all test sites. For this reason, only systems demonstrated at the YPG open field are examined (standard GT). Also, not all systems had raw data in a format that was conducive to processing and therefore not all systems could be analyzed at the YPG open field. All data associated with one time value and one sensor is considered to comprise one sample. The number of samples in each ordnance halo were averaged and divided by the halo area to calculate sample density (samples/square meter).

e. A plot of P_d^{res} versus data samples per m^2 is shown in Figure 2.3.11-1. Results are in blue for EM and in green for MAG. If only the top performers for the EM systems are examined and a trend line fitted (blue solid line), it can be seen that P_d^{res} increases as the number of samples per m^2 increases. Insufficient data exists at very low densities to fit a trend line to, but it is apparent that a high slope line will exist for the EM systems at very low densities and that a sharp transition or “corner” to a low sloped region will occur. It appears that most of the EM systems have “turned the corner” from a high sloped trend to a low sloped trend (at ~ 8 samples per m^2). The low slope region indicates some improvement in Pd may be possible by increasing data density. It is not apparent whether the MAG systems have such a sharp transition. If they have not, a moderate slope may exist and improvement may be possible by increasing their data density. MAG systems with higher sample densities are needed to make this determination.

f. A plot of the detection rate for clutter in the response stage, P_{fp}^{res} , versus sample density is shown in Figure 2.3.11-2. It is seen that the detection trends are similar to those in Figure 2.3.11-1 for the ordnance. BAR scores from Figure 2.3.11-1 apply to Figure 2.3.11-2.

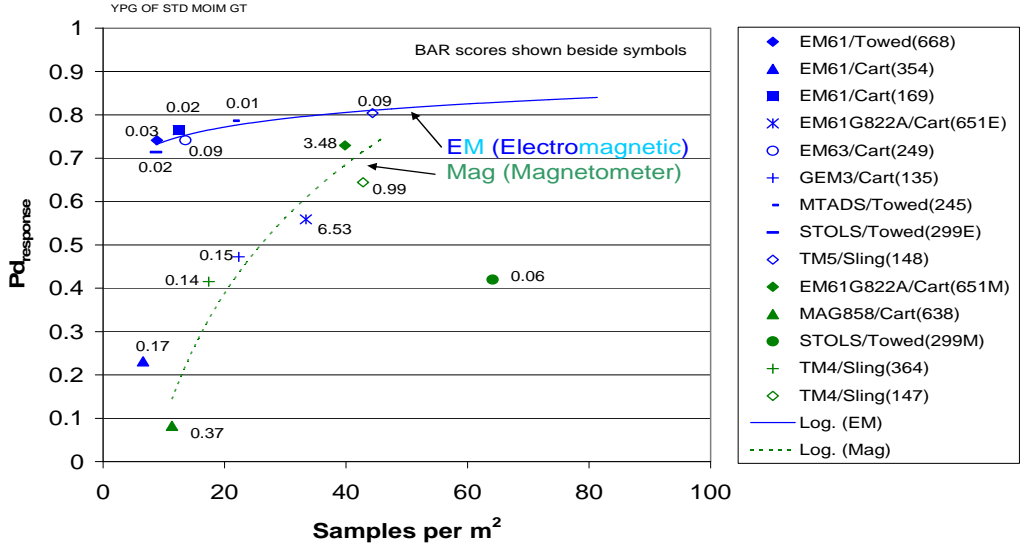


Figure 2.3.11-1. P_d^{res} versus samples per m^2 , BAR score labeled, YPG open field.

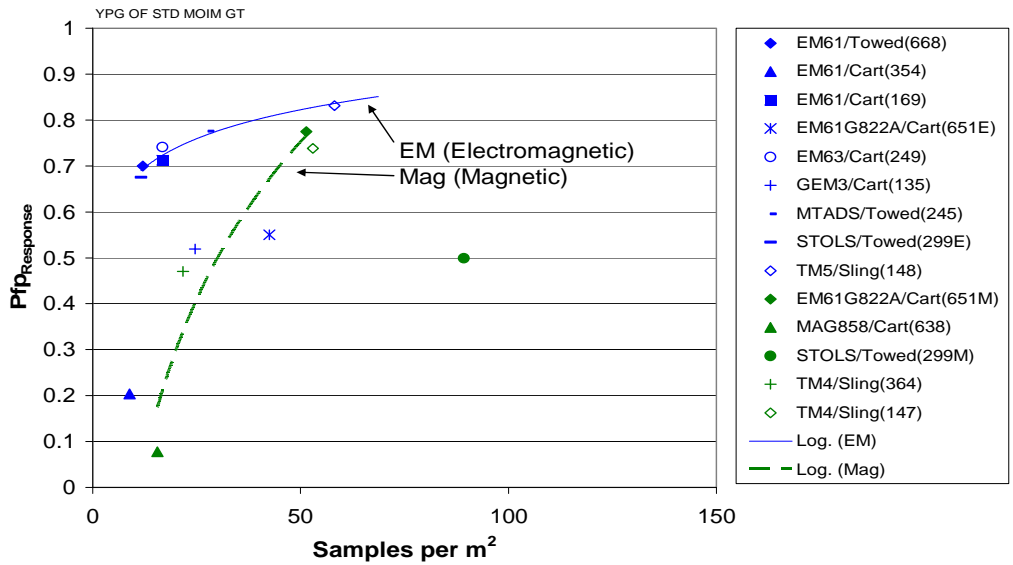


Figure 2.3.11-2. P_{fp}^{res} versus samples per m^2 , YPG open field.

g. The results of combining (all combinations, up to three different systems) system dig lists are shown in Figure 2.3.11-3. This should be the same as having multiple demonstrators come in to survey a site. The GT used contains ferrous and non-ferrous items, and both EM and MAG systems are being combined. A trend line has been fitted to the best combination of systems. It is seen that the effects of combining results yields a greater increase in P_d^{res} than is realized by the trends in single system results, given their current design configurations. Further, increases in P_d^{res} diminish at about three systems, or at about 100 samples per square meter. The combined systems are effectively giving better site coverage at a higher sampling density. However, results are improving at the cost of an increased background alarm rate (will not be analyzed here).

h. Combining results is advantageous for P_d results but not for BAR results and cost. It would be interesting to fuse the raw data of multiple systems (multiple platforms) to see if an even greater increase in detection rates will occur after processing and determine what the resulting BAR will be.

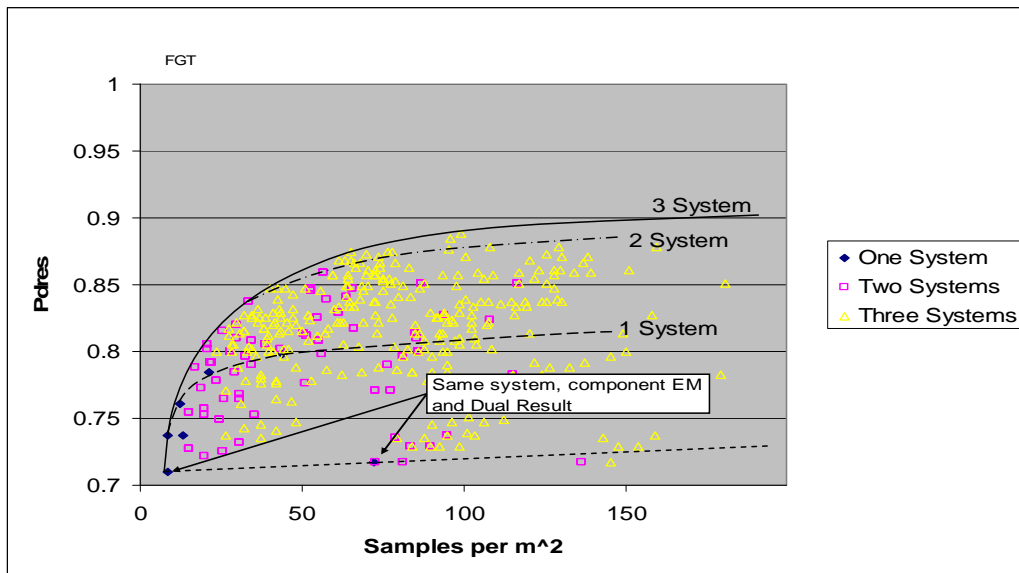


Figure 2.3.11-3. YPG open field, Combined results

i. Combined results, from a GT with items spaced at least 1.5 meters apart from the next closest item, are shown in Figure 2.3.11-4. The P_d^{res} trends turn the corner better in such a GT configuration, with diminishing returns when using approximately two systems at a sample density of about 50 samples per square meter. This indicates that for a field with ordnance/clutter that are less densely packed, spaced greater than 1.5 meters apart, data resolution requirements can be relaxed. Also, for the field with greater spacing, fewer systems are required to achieve optimum detection.

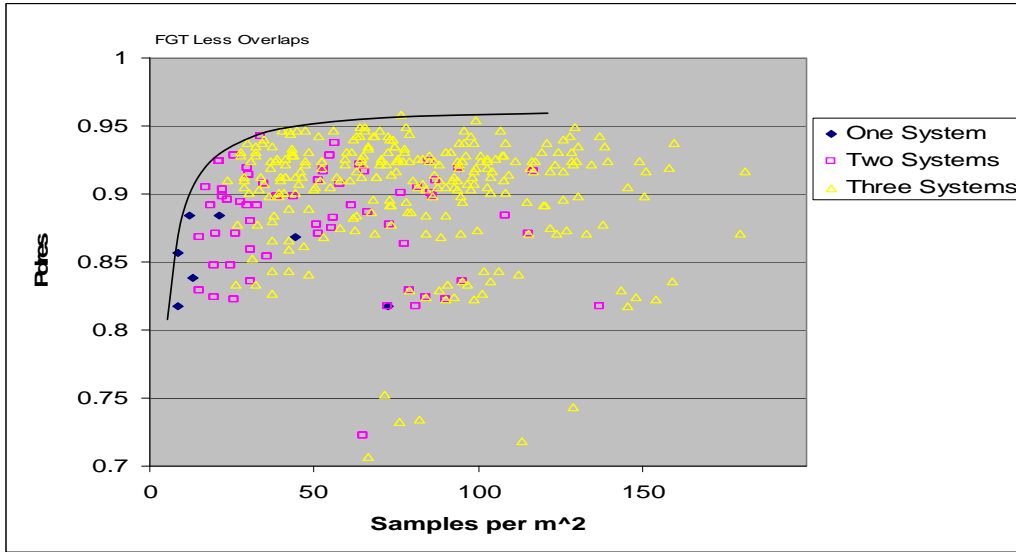


Figure 2.3.11-4. YPG open field ,Combined results for GT spaced at least 1.5 meters apart.

j. The sensor/platform combinations that were most effective when combined are presented in Table 2.3.11-1. The results are for the >1.5-meter spaced GT. It is noted that the 651D, 651M, and 651E systems had very high BAR values.

TABLE 2.3.11-1. COMBINED SYSTEM RESULTS

| Single/Single | Pdres | Sample Density | System 1 | System 2 | |
|----------------------|-------|----------------|--------------------|-----------------------|-----------------------|
| 1 | 0.94 | 43 | MTADS/Towed(245) | EM61/Cart(169) | |
| 2 | 0.93 | 33 | EM63/Cart(249) | EM61/Cart(169) | |
| 3 | 0.93 | 70 | TM4/Sling(147) Mag | EM61/Cart(169) | |
| Single/Dual | Pdres | Sample Density | System 1 | System 2 | |
| 1 | 0.94 | 109 | EM61/Cart(169) | EM61G822A/Towed(651D) | |
| 2 | 0.94 | 105 | EM61/Towed(668) | EM61G822A/Towed(651D) | |
| 3 | 0.94 | 121 | MTADS/Towed(245) | EM61G822A/Towed(651D) | |
| 4 | 0.94 | 150 | TM5/Sling(148) | EM61G822A/Towed(651D) | |
| Single/Single/Single | Pdres | Sample Density | System 1 | System 2 | System 3 |
| 1 | 0.97 | 109 | EM61/Cart(169) | EM61G822A/Towed(651E) | EM61G822A/Towed(651M) |
| 2 | 0.97 | 105 | EM61/Towed(668) | EM61G822A/Towed(651E) | EM61G822A/Towed(651M) |
| 3 | 0.96 | 113 | TM4/Sling(147) Mag | EM61/Cart(169) | EM61G822A/Towed(651E) |
| Single/Single/Dual | Pdres | Sample Density | System 1 | System 2 | System 3 |
| 1 | 0.97 | 136 | MTADS/Towed(245) | EM61/Cart(169) | EM61G822A/Towed(651D) |
| 2 | 0.97 | 166 | TM5/Sling(148) | EM61/Cart(169) | EM61G822A/Towed(651D) |

k. The relationships between P_d^{res} and sample density are plotted for individual EM and MAG sensor types, as shown in Figures 2.3.11-5 and 2.3.11-6, respectively, using the GT spaced at a minimum of 1.5 meters.

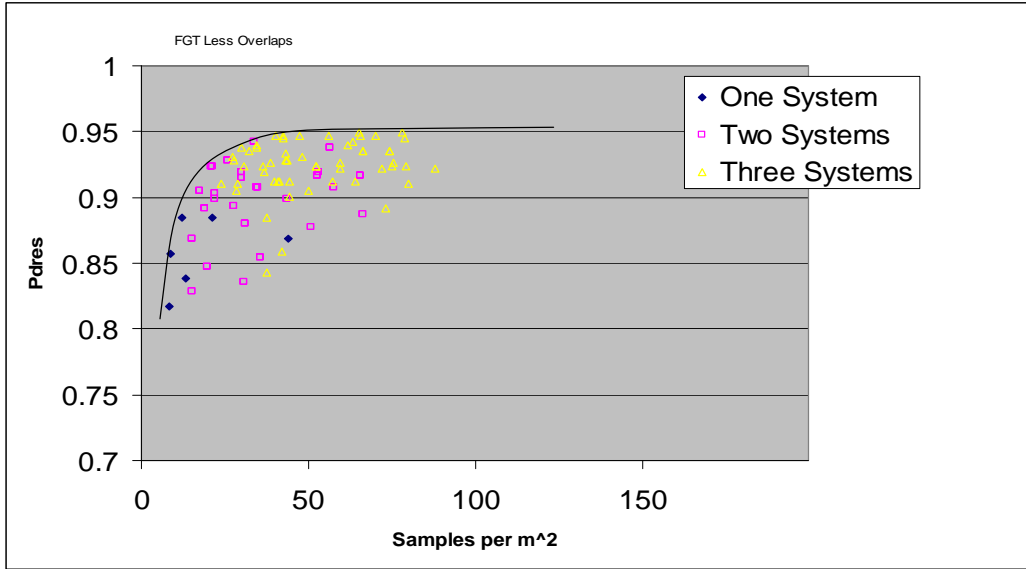


Figure 2.3.11-5. YPG open field, Combined results for GT spaced at least 1.5 meters apart, EM sensors only.

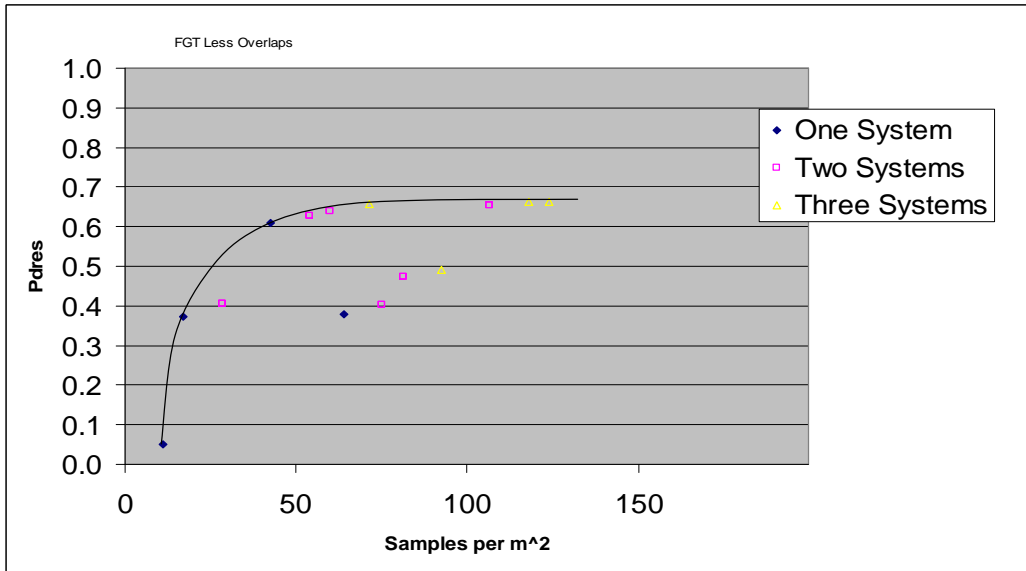


Figure 2.3.11-6. YPG open field, Combined results for GT spaced at least 1.5 meters apart, MAG sensors only.

l. When comparing the EM results shown in Figure 2.3.11-5 against those in Figure 2.3.11-4 (which contains all sensor combinations), the trend line is practically the same. Therefore, the best combinations of sensors are turning out to be combinations of different types of EM sensors, not combinations of EM and MAG sensors. Further, when Figures 2.3.11-5 and 2.3.11-6 are compared, it is seen that greater increases in P_d occur when different EM systems are combined than occur when MAG systems are combined. Also, the number of EM systems and sample density required to optimize P_d are less.

m. Discrimination trends with sampling density could not be discerned in preliminary analysis, so they are not included for consideration.

SECTION 3. APPENDIXES

APPENDIX A. TERMS AND DEFINITIONS

GENERAL DEFINITIONS

Anomaly: Location of a system response deemed to warrant further investigation by the demonstrator for consideration as an emplaced ordnance item.

Detection: An anomaly location that is within R_{halo} of an emplaced ordnance item.

Munitions and Explosives Of Concern (MEC): Specific categories of military munitions that may pose unique explosive safety risks, including UXO as defined in 10 USC 101(e)(5), DMM as defined in 10 USC 2710(e)(2) and/or munitions constituents (e.g. TNT, RDX) as defined in 10 USC 2710(e)(3) that are present in high enough concentrations to pose an explosive hazard.

Emplaced Ordnance: An ordnance item buried by the government at a specified location in the test site.

Emplaced Clutter: A clutter item (i.e., non-ordnance item) buried by the government at a specified location in the test site.

R_{halo} : A pre-determined radius about the periphery of an emplaced item (clutter or ordnance) within which a location identified by the demonstrator as being of interest is considered to be a response from that item. If multiple declarations lie within R_{halo} of any item (clutter or ordnance), the declaration with the highest signal output within the R_{halo} will be utilized. For the purpose of this program, a circular halo 0.5 meters in radius will be placed around the center of the object for all clutter and ordnance items less than 0.6 meters in length. When ordnance items are longer than 0.6 meters, the halo becomes an ellipse where the minor axis remains 1 meter and the major axis is equal to the length of the ordnance plus 1 meter.

Small Ordnance: Caliber of ordnance less than or equal to 40 mm (includes 20-mm projectile, 40-mm projectile, submunitions BLU-26, BLU-63, and M42).

Medium Ordnance: Caliber of ordnance greater than 40 mm and less than or equal to 81 mm (includes 57-mm projectile, 60-mm mortar, 2.75 in. Rocket, MK118 Rockeye, 81-mm mortar).

Large Ordnance: Caliber of ordnance greater than 81 mm (includes 105-mm HEAT, 105-mm projectile, 155-mm projectile, 500-pound bomb).

Shallow: Items buried less than 0.3 meter below ground surface.

Medium: Items buried greater than or equal to 0.3 meter and less than 1 meter below ground surface.

Deep: Items buried greater than or equal to 1 meter below ground surface.

Response Stage Noise Level: The level that represents the point below which anomalies are not considered detectable. Demonstrators are required to provide the recommended noise level for the Blind Grid test area.

Discrimination Stage Threshold: The demonstrator selected threshold level that they believe provides optimum performance of the system by retaining all detectable ordnance and rejecting the maximum amount of clutter. This level defines the subset of anomalies the demonstrator would recommend digging based on discrimination.

Binomially Distributed Random Variable: A random variable of the type which has only two possible outcomes, say success and failure, is repeated for n independent trials with the probability p of success and the probability $1-p$ of failure being the same for each trial. The number of successes x observed in the n trials is an estimate of p and is considered to be a binomially distributed random variable.

RESPONSE AND DISCRIMINATION STAGE DATA

The scoring of the demonstrator's performance is conducted in two stages. These two stages are termed the **RESPONSE STAGE** and **DISCRIMINATION STAGE**. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver operating characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of false positive (P_{fp}) and those that do not correspond to any known item, termed background alarms.

The **RESPONSE STAGE** scoring evaluates the ability of the system to detect emplaced targets without regard to ability to discriminate ordnance from other anomalies. For the **RESPONSE STAGE**, the demonstrator provides the scoring committee with the location and signal strength of all anomalies that the demonstrator has deemed sufficient to warrant further investigation and/or processing as potential emplaced ordnance items. This list is generated with minimal processing (e.g., this list will include all signals above the system noise threshold). As such, it represents the most inclusive list of anomalies.

The **DISCRIMINATION STAGE** evaluates the demonstrator's ability to correctly identify ordnance as such, and to reject clutter. For the same locations as in the **RESPONSE STAGE** anomaly list, the **DISCRIMINATION STAGE** list contains the output of the algorithms applied in the discrimination-stage processing. This list is prioritized based on the demonstrator's determination that an anomaly location is likely to contain ordnance. Thus, higher output values are indicative of higher confidence that an ordnance item is present at the specified location. For electronic signal processing, priority ranking is based on algorithm output. For other systems, priority ranking is based on human judgment. The demonstrator also selects the threshold that the demonstrator believes will provide "optimum" system performance, (i.e., that retains all the detected ordnance and rejects the maximum amount of clutter).

Note: The two lists provided by the demonstrator contain identical numbers of potential target locations. They differ only in the priority ranking of the declarations.

RESPONSE STAGE DEFINITIONS

Response Stage Probability of Detection (P_d^{res}): $P_d^{\text{res}} = (\text{No. of response-stage detections})/(\text{No. of emplaced ordnance in the test site})$.

Response Stage False Positive (fp^{res}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Response Stage Probability of False Positive (P_{fp}^{res}): $P_{fp}^{\text{res}} = (\text{No. of response-stage false positives})/(\text{No. of emplaced clutter items})$.

Response Stage Background Alarm (ba^{res}): An anomaly in a blind grid cell that contains neither emplaced ordnance nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced ordnance or emplaced clutter item.

Response Stage Probability of Background Alarm (P_{ba}^{res}): Blind Grid only: $P_{ba}^{\text{res}} = (\text{No. of response-stage background alarms})/(\text{No. of empty grid locations})$.

Response Stage Background Alarm Rate (BAR^{res}): Open Field only: $BAR^{\text{res}} = (\text{No. of response-stage background alarms})/(\text{arbitrary constant})$.

Note that the quantities P_d^{res} , P_{fp}^{res} , P_{ba}^{res} , and BAR^{res} are functions of t^{res} , the threshold applied to the response-stage signal strength. These quantities can therefore be written as $P_d^{\text{res}}(t^{\text{res}})$, $P_{fp}^{\text{res}}(t^{\text{res}})$, $P_{ba}^{\text{res}}(t^{\text{res}})$, and $BAR^{\text{res}}(t^{\text{res}})$.

DISCRIMINATION STAGE DEFINITIONS

Discrimination: The application of a signal processing algorithm or human judgment to response-stage data that discriminates ordnance from clutter. Discrimination should identify anomalies that the demonstrator has high confidence correspond to ordnance, as well as those that the demonstrator has high confidence correspond to non-ordnance or background returns. The former should be ranked with highest priority and the latter with lowest.

Discrimination Stage Probability of Detection (P_d^{disc}): $P_d^{\text{disc}} = (\text{No. of discrimination-stage detections})/(\text{No. of emplaced ordnance in the test site})$.

Discrimination Stage False Positive (fp^{disc}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Discrimination Stage Probability of False Positive (P_{fp}^{disc}): $P_{fp}^{\text{disc}} = (\text{No. of discrimination stage false positives})/(\text{No. of emplaced clutter items})$.

Discrimination Stage Background Alarm (ba^{disc}): An anomaly in a blind grid cell that contains neither emplaced ordnance nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced ordnance or emplaced clutter item.

Discrimination Stage Probability of Background Alarm (P_{ba}^{disc}): $P_{ba}^{disc} = (\text{No. of discrimination-stage background alarms})/(\text{No. of empty grid locations})$.

Discrimination Stage Background Alarm Rate (BAR^{disc}): $BAR^{disc} = (\text{No. of discrimination-stage background alarms})/(\text{arbitrary constant})$.

Note that the quantities P_d^{disc} , P_{fp}^{disc} , P_{ba}^{disc} , and BAR^{disc} are functions of t^{disc} , the threshold applied to the discrimination-stage signal strength. These quantities can therefore be written as $P_d^{disc}(t^{disc})$, $P_{fp}^{disc}(t^{disc})$, $P_{ba}^{disc}(t^{disc})$, and $BAR^{disc}(t^{disc})$.

RECEIVER-OPERATING CHARACTERISTIC (ROC) CURVES

ROC curves at both the response and discrimination stages can be constructed based on the above definitions. The ROC curves plot the relationship between P_d versus P_{fp} and P_d versus BAR or P_{ba} as the threshold applied to the signal strength is varied from its minimum (t_{min}) to its maximum (t_{max}) value.¹ Figure A-1 shows how P_d versus P_{fp} and P_d versus BAR are combined into ROC curves. Note that the “res” and “disc” superscripts have been suppressed from all the variables for clarity.

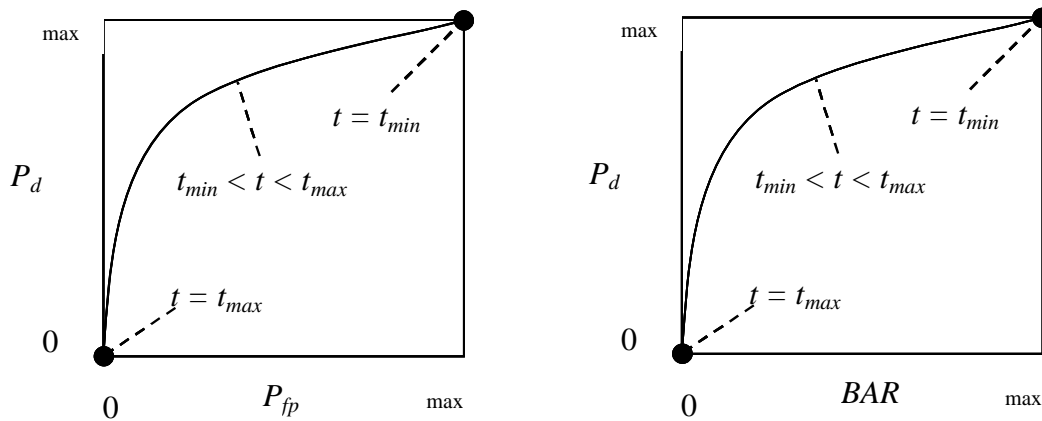


Figure A-1. ROC curves for open field testing. Each curve applies to both the response and discrimination stages.

¹Strictly speaking, ROC curves plot the P_d versus P_{ba} over a pre-determined and fixed number of detection opportunities (some of the opportunities are located over ordnance and others are located over clutter or blank spots). In an open field scenario, each system suppresses its signal strength reports until some bare-minimum signal response is received by the system. Consequently, the open field ROC curves do not have information from low signal-output locations, and, furthermore, different contractors report their signals over a different set of locations on the ground. These ROC curves are thus not true to the strict definition of ROC curves as defined in textbooks on detection theory. Note, however, that the ROC curves obtained in the Blind Grid test sites are true ROC curves.

METRICS TO CHARACTERIZE THE DISCRIMINATION STAGE

The demonstrator is also scored on efficiency and rejection ratio, which measure the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of ordnance detections from the anomaly list, while rejecting the maximum number of anomalies arising from non-ordnance items. The efficiency measures the amount of detected ordnance retained by the discrimination, while the rejection ratio measures the fraction of false alarms rejected. Both measures are defined relative to the entire response list, i.e., the maximum ordnance detectable by the sensor and its accompanying false positive rate or background alarm rate.

Efficiency (E): $E = P_d^{\text{disc}}(t^{\text{disc}})/P_d^{\text{res}}(t_{\text{min}}^{\text{res}})$; Measures (at a threshold of interest), the degree to which the maximum theoretical detection performance of the sensor system (as determined by the response stage t_{min}) is preserved after application of discrimination techniques. Efficiency is a number between 0 and 1. An efficiency of 1 implies that all of the ordnance initially detected in the response stage was retained at the specified threshold in the discrimination stage, t^{disc} .

False Positive Rejection Rate (R_{fp}): $R_{\text{fp}} = 1 - [P_{\text{fp}}^{\text{disc}}(t^{\text{disc}})/P_{\text{fp}}^{\text{res}}(t_{\text{min}}^{\text{res}})]$; Measures (at a threshold of interest), the degree to which the sensor system's false positive performance is improved over the maximum false positive performance (as determined by the response stage t_{min}). The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all emplaced clutter initially detected in the response stage were correctly rejected at the specified threshold in the discrimination stage.

Background Alarm Rejection Rate (R_{ba}):

Blind Grid: $R_{\text{ba}} = 1 - [P_{\text{ba}}^{\text{disc}}(t^{\text{disc}})/P_{\text{ba}}^{\text{res}}(t_{\text{min}}^{\text{res}})]$.

Open Field: $R_{\text{ba}} = 1 - [\text{BAR}^{\text{disc}}(t^{\text{disc}})/\text{BAR}^{\text{res}}(t_{\text{min}}^{\text{res}})]$.

Measures the degree to which the discrimination stage correctly rejects background alarms initially detected in the response stage. The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all background alarms initially detected in the response stage were rejected at the specified threshold in the discrimination stage.

CHI-SQUARE COMPARISON EXPLANATION:

The Chi-square test for differences in probabilities (or 2 x 2 contingency table) is used to analyze two samples drawn from two different populations to see if both populations have the same or different proportions of elements in a certain category. More specifically, two random samples are drawn, one from each population, to test the null hypothesis that the probability of event A (some specified event) is the same for both populations (ref 3).

A 2 x 2 contingency table is used in the Standardized UXO Technology Demonstration Site Program to determine if there is reason to believe that the proportion of ordnance correctly detected/discriminated by demonstrator X's system is significantly degraded by the more challenging terrain feature introduced. The test statistic of the 2 x 2 contingency table is the

Chi-square distribution with one degree of freedom. Since an association between the more challenging terrain feature and relatively degraded performance is sought, a one-sided test is performed. A significance level of 0.05 is chosen which sets a critical decision limit of 2.71 from the Chi-square distribution with one degree of freedom. It is a critical decision limit because if the test statistic calculated from the data exceeds this value, the two proportions tested will be considered significantly different. If the test statistic calculated from the data is less than this value, the two proportions tested will be considered not significantly different.

An exception must be applied when either a 0 or 100 percent success rate occurs in the sample data. The Chi-square test cannot be used in these instances. Instead, Fischer’s test is used and the critical decision limit for one-sided tests is the chosen significance level, which in this case is 0.05. With Fischer’s test, if the test statistic is less than the critical value, the proportions are considered to be significantly different.

Standardized UXO Technology Demonstration Site examples, where blind grid results are compared to those from the open field and open field results are compared to those from one of the scenarios, follow. It should be noted that a significant result does not prove a cause and effect relationship exists between the two populations of interest; however, it does serve as a tool to indicate that one data set has experienced a degradation in system performance at a large enough level than can be accounted for merely by chance or random variation. Note also that a result that is not significant indicates that there is not enough evidence to declare that anything more than chance or random variation within the same population is at work between the two data sets being compared.

Demonstrator X achieves the following overall results after surveying each of the three progressively more difficult areas using the same system (results indicate the number of ordnance detected divided by the number of ordnance emplaced):

| | Blind Grid | Open Field | Moguls |
|--------------|---------------|------------|-------------|
| P_d^{res} | 100/100 = 1.0 | 8/10 = .80 | 20/33 = .61 |
| P_d^{disc} | 80/100 = 0.80 | 6/10 = .60 | 8/33 = .24 |

P_d^{res} : BLIND GRID versus OPEN FIELD. Using the example data above to compare probabilities of detection in the response stage, all 100 ordnance out of 100 emplaced ordnance items were detected in the blind grid while 8 ordnance out of 10 emplaced were detected in the open field. Fischer’s test must be used since a 100 percent success rate occurs in the data. Fischer’s test uses the four input values to calculate a test statistic of 0.0075 that is compared against the critical value of 0.05. Since the test statistic is less than the critical value, the smaller response stage detection rate (0.80) is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause and effect relationship exists between the change in survey area and degradation in performance, it does indicate that the detection ability of demonstrator X’s system seems to have been degraded in the open field relative to results from the blind grid using the same system.

P_d^{disc} : BLIND GRID versus OPEN FIELD. Using the example data above to compare probabilities of detection in the discrimination stage, 80 out of 100 emplaced ordnance items were correctly discriminated as ordnance in blind grid testing while 6 ordnance out of 10 emplaced were correctly discriminated as such in open field-testing. Those four values are used to calculate a test statistic of 1.12. Since the test statistic is less than the critical value of 2.71, the two discrimination stage detection rates are considered to be not significantly different at the 0.05 level of significance.

P_d^{res} : OPEN FIELD versus MOGULS. Using the example data above to compare probabilities of detection in the response stage, 8 out of 10 and 20 out of 33 are used to calculate a test statistic of 0.56. Since the test statistic is less than the critical value of 2.71, the two response stage detection rates are considered to be not significantly different at the 0.05 level of significance.

P_d^{disc} : OPEN FIELD versus MOGULS. Using the example data above to compare probabilities of detection in the discrimination stage, 6 out of 10 and 8 out of 33 are used to calculate a test statistic of 2.98. Since the test statistic is greater than the critical value of 2.71, the smaller discrimination stage detection rate is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause and effect relationship exists between the change in survey area and degradation in performance, it does indicate that the ability of demonstrator X to correctly discriminate seems to have been degraded by the mogul terrain relative to results from the flat open field using the same system.

APPENDIX B. DAILY WEATHER LOGS

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|-------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 39 | EM | Blind Grid | hand | AETC | 21 October | 54.2 °F | 0" |
| 39 | EM | Blind Grid | hand | AETC | 22 October | 51.6 °F | 0" |
| 39 | EM | Blind Grid | hand | AETC | 23 October | 52.8 °F | 0" |
| 695 | EM | Blind Grid | hand | ARM | 4 April | 58 °F | 0" |
| 695 | EM | Blind Grid | hand | ARM | 5 April | 59.63 °F | 0" |
| 695 | EM | Blind Grid | hand | ARM | 6 April | 68.93 °F | 0" |
| 695 | EM | Blind Grid | hand | ARM | 7 April | 70.5 °F | 0" |
| 695 | EM | Blind Grid | hand | ARM | 14 April | 56.02 °F | 0" |
| 691 | EM | Blind Grid | hand | ARM | 4 April | 58 °F | 0" |
| 691 | EM | Blind Grid | hand | ARM | 5 April | 59.63 °F | 0" |
| 691 | EM | Blind Grid | hand | ARM | 6 April | 68.93 °F | 0" |
| 691 | EM | Blind Grid | hand | ARM | 7 April | 70.5 °F | 0" |
| 691 | EM | Blind Grid | hand | ARM | 14 April | 56.02 °F | 0" |
| 622 | dual | Blind Grid | cart | BH | 24 August | 79.06 °F | 0" |
| 642 | dual | Moguls | cart | BH | 1 September | 78.51 °F | 0" |
| 657 | dual | Open Field | cart | BH | 25 August | 75.63 °F | 0" |
| 657 | dual | Open Field | cart | BH | 26 August | 77.89 °F | 0" |
| 657 | dual | Open Field | cart | BH | 27 August | 81.12 °F | 0" |
| 657 | dual | Open Field | cart | BH | 28 August | 83.4 °F | 0" |
| 657 | dual | Open Field | cart | BH | 30 August | 79.17 °F | 0" |
| 657 | dual | Open Field | cart | BH | 31 August | 79.5 °F | 0" |
| 657 | dual | Open Field | cart | BH | 2 September | 76.44 °F | 0" |
| 636 | dual | Woods | cart | BH | 31 August | 79.5 °F | 0" |
| 636 | dual | Woods | cart | BH | 2 September | 76.44 °F | 0" |
| 304 | EM | Blind Grid | cart | ERDC | 31 March | 46.63 °F | 0.09" |
| 304 | EM | Blind Grid | cart | ERDC | 1 April | 49.1 °F | 1.03" |
| 305 | EM | Open Field | cart | ERDC | 30 March | 41.85 °F | 0.04" |
| 305 | EM | Open Field | cart | ERDC | 31 March | 46.64 °F | 0.1" |
| 305 | EM | Open Field | cart | ERDC | 1 April | 49.1 °F | 1.03" |
| 305 | EM | Open Field | cart | ERDC | 2 April | 46.39 °F | 0.69" |
| 305 | EM | Open Field | cart | ERDC | 3 April | 47.2 °F | 0.04" |
| 305 | EM | Open Field | cart | ERDC | 4 April | 43.66 °F | 0.21" |
| 305 | EM | Open Field | cart | ERDC | 5 April | 37.98 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 6 April | 48.55 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 7 April | 64.87 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 8 April | 49.39 °F | 0.02" |
| 305 | EM | Open Field | cart | ERDC | 9 April | 57.32 °F | 0.03" |
| 305 | EM | Open Field | cart | ERDC | 10 April | 55.36 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 11 April | 46.46 °F | 0.02" |
| 305 | EM | Open Field | cart | ERDC | 12 April | 47.28 °F | 1.15" |
| 305 | EM | Open Field | cart | ERDC | 13 April | 49.45 °F | 0.4" |
| 305 | EM | Open Field | cart | ERDC | 14 April | 51.19 °F | 0.14" |
| 305 | EM | Open Field | cart | ERDC | 15 April | 55.89 °F | 0.01" |
| 305 | EM | Open Field | cart | ERDC | 16 April | 55.66 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 17 April | 65.43 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 18 April | 76.4 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 19 April | 76.19 °F | 0" |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|---------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 305 | EM | Open Field | cart | ERDC | 20 April | 72.25 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 21 April | 63.16 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 22 April | 73.65 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 23 April | 73.75 °F | 0.15" |
| 305 | EM | Open Field | cart | ERDC | 24 April | 66.28 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 25 April | 57.54 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 26 April | 63.65 °F | 0.72" |
| 305 | EM | Open Field | cart | ERDC | 27 April | 61.05 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 28 April | 52.69 °F | 0" |
| 305 | EM | Open Field | cart | ERDC | 29 April | 61.74 °F | 0" |
| 142 | EM | Blind Grid | cart | ERDC | 8 September 8 | 75.9 °F | 0" |
| 142 | EM | Blind Grid | cart | ERDC | 9 September 9 | 72.3 °F | 0" |
| 142 | EM | Blind Grid | cart | ERDC | 10 September | 71.7 °F | 0" |
| 142 | EM | Blind Grid | cart | ERDC | 11 September | 76.1 °F | 0" |
| 142 | EM | Blind Grid | cart | ERDC | 12 September | 65.1 °F | 0.55" |
| 141 | EM | Blind Grid | cart | ERDC | 8 September | 75.9 °F | 0" |
| 141 | EM | Blind Grid | cart | ERDC | 9 September | 72.3 °F | 0" |
| 141 | EM | Blind Grid | cart | ERDC | 10 September | 71.7 °F | 0" |
| 141 | EM | Blind Grid | cart | ERDC | 11 September | 76.1 °F | 0" |
| 141 | EM | Blind Grid | cart | ERDC | 12 September | 65.1 °F | 0.55" |
| 40 | dual | Blind Grid | towed | Geocenters | 8 October | 57.6 °F | 0" |
| 40 | dual | Blind Grid | towed | Geocenters | 9 October | 58.9 °F | 0" |
| 290 | dual | Blind Grid | towed | Geocenters | 4 October | 84.55 °F | 0.06" |
| 187 | dual | Open Field | towed | Geocenters | 7 October | 72.6 °F | 0" |
| 187 | dual | Open Field | towed | Geocenters | 8 October | 57.6 °F | 0" |
| 187 | dual | Open Field | towed | Geocenters | 9 October | 58.9 °F | 0" |
| 187 | dual | Open Field | towed | Geocenters | 10 October | 63.5 °F | 0.61" |
| 187 | dual | Open Field | towed | Geocenters | 11 October | 64.9 °F | 2.59" |
| 298 | dual | Open Field | towed | Geocenters | 4 August | 84.55 °F | 0.06" |
| 298 | dual | Open Field | towed | Geocenters | 5 August | 72.91 °F | 0.03" |
| 298 | dual | Open Field | towed | Geocenters | 6 August | 66.7 °F | 0" |
| 792 | dual | Blind Grid | towed | Geocenters | 17 April | 58.8 °F | 0" |
| 792 | dual | Blind Grid | towed | Geocenters | 18 April | 59.4 °F | 0" |
| 802 | dual | Open Field | towed | Geocenters | 18 April | 61.4 °F | 0" |
| 802 | dual | Open Field | towed | Geocenters | 19 April | 68.5 °F | 0" |
| 50 | EM | Blind Grid | hand | Geophex | 29 April | 66.65 °F | 0" |
| 50 | EM | Blind Grid | hand | Geophex | 30 April | 66.81 °F | 0" |
| 680 | EM | Blind Grid | hand | Geophex | 26 April | 64.94 °F | 0" |
| 680 | EM | Blind Grid | hand | Geophex | 27 April | 65.79 °F | 0.02" |
| 125 | EM | Blind Grid | towed | Geophex | 1 May | 67.04 °F | 0.05" |
| 125 | EM | Blind Grid | towed | Geophex | 2 May | 71.07 °F | 0" |
| 125 | EM | Blind Grid | towed | Geophex | 3 May | 60.28 °F | 0" |
| 125 | EM | Blind Grid | towed | Geophex | 5 May | 51.19 °F | 0.03" |
| 49 | EM | Blind Grid | cart | Geophex | 28 April | 66.74 °F | 0" |
| 49 | EM | Blind Grid | cart | Geophex | 29 April | 66.65 °F | 0" |
| 451 | EM | Moguls | cart | Geophex | 9 December | 25.67 °F | 0" |
| 451 | EM | Moguls | cart | Geophex | 10 December | 27.49 °F | 0" |
| 451 | EM | Moguls | cart | Geophex | 11 December | 35.5 °F | 1.5" |
| 451 | EM | Moguls | cart | Geophex | 12 December | 41.55 °F | 0.03" |
| 451 | EM | Moguls | cart | Geophex | 13 December | 34.4 °F | 0.67" |
| 665 | EM | Moguls | hand | Geophex | 18 April | 72.39 °F | 0" |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|-------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 665 | EM | Moguls | hand | Geophex | 19 April | 73.97 °F | 0" |
| 665 | EM | Moguls | hand | Geophex | 20 April | 78.07 °F | 0" |
| 665 | EM | Moguls | hand | Geophex | 21 April | 60.02 °F | 0" |
| 665 | EM | Moguls | hand | Geophex | 22 April | 52.29 °F | 0" |
| 665 | EM | Moguls | hand | Geophex | 25 April | 54.31 °F | 0" |
| 665 | EM | Moguls | hand | Geophex | 26 April | 64.94 °F | 0" |
| 665 | EM | Moguls | hand | Geophex | 27 April | 65.79 °F | 0.02" |
| 129 | EM | Open Field | towed | Geophex | 28 April | 71.55 °F | 0" |
| 129 | EM | Open Field | towed | Geophex | 29 April | 71.49 °F | 0" |
| 129 | EM | Open Field | towed | Geophex | 30 April | 67.62 °F | 0" |
| 129 | EM | Open Field | towed | Geophex | 1 May | 71.11 °F | 0.05" |
| 129 | EM | Open Field | towed | Geophex | 2 May | 78.35 °F | 0" |
| 129 | EM | Open Field | towed | Geophex | 3 May | 65.32 °F | 0" |
| 129 | EM | Open Field | towed | Geophex | 4 May | 62.76 °F | 0" |
| 129 | EM | Open Field | towed | Geophex | 5 May | 53.09 °F | 0.03" |
| 129 | EM | Open Field | towed | Geophex | 6 May | 57.36 °F | 0.02" |
| 129 | EM | Open Field | towed | Geophex | 7 May | 69.85 °F | 0.56" |
| 449 | EM | Woods | cart | Geophex | 28 April | 66.74 °F | 0" |
| 449 | EM | Woods | cart | Geophex | 29 April | 66.65 °F | 0" |
| 449 | EM | Woods | cart | Geophex | 30 April | 66.81 °F | 0" |
| 449 | EM | Woods | cart | Geophex | 1 May | 67.04 °F | 0.05" |
| 694 | EM | Blind Grid | cart | Geophex | 18 April | 72.39 °F | 0" |
| 694 | EM | Blind Grid | cart | Geophex | 19 April | 73.97 °F | 0" |
| 694 | EM | Blind Grid | cart | Geophex | 20 April | 78.07 °F | 0" |
| 694 | EM | Blind Grid | cart | Geophex | 26 April | 64.94 °F | 0" |
| 694 | EM | Blind Grid | cart | Geophex | 27 April | 65.79 °F | 0.02" |
| 739 | EM | Blind Grid | towed | Geophex | 5 October | 70.2 °F | 0" |
| 739 | EM | Blind Grid | towed | Geophex | 6 October | 71.6 °F | 0" |
| 693 | EM | Blind Grid | cart | Geophex | 18 April | 72.39 °F | 0" |
| 693 | EM | Blind Grid | cart | Geophex | 19 April | 73.97 °F | 0" |
| 693 | EM | Blind Grid | cart | Geophex | 20 April | 78.07 °F | 0" |
| 693 | EM | Blind Grid | cart | Geophex | 26 April | 64.94 °F | 0" |
| 693 | EM | Blind Grid | cart | Geophex | 27 April | 65.79 °F | 0.02" |
| 740 | EM | Open Field | towed | Geophex | 7 October | 75.1 °F | 1.21" |
| 740 | EM | Open Field | towed | Geophex | 17 October | 59.2 °F | 0" |
| 740 | EM | Open Field | towed | Geophex | 18 October | 67.1 °F | 0" |
| 740 | EM | Open Field | towed | Geophex | 19 October | 61.7 °F | 0" |
| 740 | EM | Open Field | towed | Geophex | 20 October | 55.1 °F | 0" |
| 184 | EM | Blind Grid | hand | G-TEK | 24 October | 49.45 °F | 0" |
| 183 | EM | Blind Grid | sling | G-TEK | 14 October | 62.05 °F | 1.28" |
| 545 | EM | Moguls | sling | G-TEK | 22 October | 55.09 °F | 0" |
| 154 | EM | Open Field | sling | G-TEK | 15 October | 61.12 °F | 0.11" |
| 154 | EM | Open Field | sling | G-TEK | 16 October | 61.73 °F | 0" |
| 154 | EM | Open Field | sling | G-TEK | 17 October | 55.15 °F | 0.05" |
| 154 | EM | Open Field | sling | G-TEK | 18 October | 54.36 °F | 0" |
| 154 | EM | Open Field | sling | G-TEK | 20 October | 55.24 °F | 0" |
| 154 | EM | Open Field | sling | G-TEK | 21 October | 67.51 °F | 0" |
| 452 | EM | Woods | hand | G-TEK | 23 October | 44.38 °F | 0" |
| 452 | EM | Woods | hand | G-TEK | 24 October | 49.45 °F | 0.01" |
| 268 | MAG | Blind Grid | sling | G-TEK | 14 October | 62 °F | 0" |
| 268 | MAG | Blind Grid | sling | G-TEK | 24 October | 49.4 °F | 0" |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|-------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 547 | MAG | Moguls | sling | G-TEK | 23 October | 44.38 °F | 0" |
| 547 | MAG | Moguls | sling | G-TEK | 24 October | 49.45 °F | 0.01" |
| 311 | MAG | Open Field | sling | G-TEK | 15 October | 61.12 °F | 0.11" |
| 311 | MAG | Open Field | sling | G-TEK | 16 October | 61.73 °F | 0" |
| 311 | MAG | Open Field | sling | G-TEK | 17 October | 55.15 °F | 0.05" |
| 311 | MAG | Open Field | sling | G-TEK | 18 October | 54.36 °F | 0" |
| 311 | MAG | Open Field | sling | G-TEK | 20 October | 55.24 °F | 0" |
| 311 | MAG | Open Field | sling | G-TEK | 21 October | 67.51 °F | 0" |
| 454 | MAG | Woods | sling | G-TEK | 22 October | 55.09 °F | 0" |
| 281 | dual | Blind Grid | sling | G-TEK | 24 May | 83.75 °F | 0" |
| 281 | dual | Blind Grid | sling | G-TEK | 4 June | 69.63 °F | 0" |
| 380 | dual | Moguls | sling | G-TEK | 3 June | 73.6 °F | 0.01" |
| 379 | dual | Open Field | sling | G-TEK | 24 May | 83.75 °F | 0" |
| 379 | dual | Open Field | sling | G-TEK | 25 May | 81.02 °F | 0.07" |
| 379 | dual | Open Field | sling | G-TEK | 26 May | 74.81 °F | 0.02" |
| 379 | dual | Open Field | sling | G-TEK | 27 May | 75.67 °F | 0.25" |
| 379 | dual | Open Field | sling | G-TEK | 1 June | 72.01 °F | 0.19" |
| 379 | dual | Open Field | sling | G-TEK | 2 June | 74.14 °F | 0.08" |
| 379 | dual | Open Field | sling | G-TEK | 3 June | 73.6 °F | 0.01" |
| 379 | dual | Open Field | sling | G-TEK | 4 June | 69.63 °F | 0" |
| 381 | dual | Woods | sling | G-TEK | 28 May | 76.62 °F | 0.01" |
| 381 | dual | Woods | sling | G-TEK | 29 May | 66.15 °F | 0" |
| 381 | dual | Woods | sling | G-TEK | 1 June | 72.01 °F | 0.19" |
| 237 | MAG | Blind Grid | hand | HFA | 14 June | 78.67 °F | 2.02" |
| 676 | MAG | Moguls | hand | HFA | 19 July | 75.45 °F | 0" |
| 676 | MAG | Moguls | hand | HFA | 20 July | 80.23 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 15 June | 82.61 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 16 June | 80.71 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 17 June | 82.6 °F | 0.18" |
| 231 | MAG | Open Field | hand | HFA | 18 June | 84.72 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 28 June | 78.6 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 29 June | 72.46 °F | 0.03" |
| 231 | MAG | Open Field | hand | HFA | 30 June | 78.69 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 1 July | 79.14 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 2 July | 84.18 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 6 July | 79.96 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 7 July | 81.65 °F | 0.34" |
| 231 | MAG | Open Field | hand | HFA | 12 July | 76.69 °F °F | 3.56" |
| 231 | MAG | Open Field | hand | HFA | 13 July | 74.89 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 14 July | 75.09 °F | 1.12" |
| 231 | MAG | Open Field | hand | HFA | 15 July | 77.74 °F | 0" |
| 231 | MAG | Open Field | hand | HFA | 16 July | 78.06 °F | 0" |
| 486 | MAG | Woods | hand | HFA | 8 July | 82.19 °F | 0" |
| 486 | MAG | Woods | hand | HFA | 9 July | 79.53 °F | 0" |
| 647 | EM | Mine Grid | towed | NAEVA | 12 August | 80.04 °F | 0.74" |
| 396 | EM | Blind Grid | 2-man | NAEVA | 18 August | 78.07 °F | 0.05" |
| 396 | EM | Blind Grid | 2-man | NAEVA | 22 August | 71.96 °F | 0" |
| 397 | EM | Blind Grid | towed | NAEVA | 10 August | 79.22 °F | 0" |
| 597 | EM | Moguls | 2-man | NAEVA | 19 August | 80.65 °F | 0" |
| 597 | EM | Moguls | 2-man | NAEVA | 20 August | 85.59 °F | 0" |
| 406 | EM | Open Field | towed | NAEVA | 10 August | 79.22 °F | 0" |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|--------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 406 | EM | Open Field | towed | NAEVA | 11 August | 79.94 °F | 0.02" |
| 406 | EM | Open Field | towed | NAEVA | 12 August | 80.04 °F | 0.74" |
| 406 | EM | Open Field | towed | NAEVA | 16 August | 77.95 °F | 0.01" |
| 406 | EM | Open Field | towed | NAEVA | 17 August | 76.25 °F | 0.02" |
| 406 | EM | Open Field | towed | NAEVA | 18 August | 78.07 °F | 0.05" |
| 406 | EM | Open Field | towed | NAEVA | 22 August | 71.96 °F | 0" |
| 494 | EM | Woods | 2-man | NAEVA | 18 August | 78.07 °F | 0.05" |
| 494 | EM | Woods | 2-man | NAEVA | 20 August | 85.59 °F | 0" |
| 494 | EM | Woods | 2-man | NAEVA | 21 August | 79.17 °F | 0.09" |
| 494 | EM | Woods | 2-man | NAEVA | 22 August | 71.96 °F | 0" |
| 127 | EM | Blind Grid | towed | NRL | 24 September | 68.3 °F | 0" |
| 127 | EM | Blind Grid | towed | NRL | 25 September | 72.6 °F | 0.04" |
| 127 | EM | Blind Grid | towed | NRL | 2 October | 53.2 °F | 0" |
| 127 | EM | Blind Grid | towed | NRL | 6 October | 57.3 °F | 0" |
| 675 | EM | Open Field | towed | NRL | 7 June | 72.68 °F | 0" |
| 675 | EM | Open Field | towed | NRL | 8 June | 78.2 °F | 0" |
| 675 | EM | Open Field | towed | NRL | 9 June | 84.74 °F | 0" |
| 671 | MAG | Blind Grid | towed | NRL | 21 June | 74.14 °F | 0" |
| 671 | MAG | Blind Grid | towed | NRL | 22 June | 79.78 °F | 0.24" |
| 673 | MAG | Open Field | towed | NRL | 21 June | 74.14 °F | 0" |
| 673 | MAG | Open Field | towed | NRL | 22 June | 79.78 °F | 0.24" |
| 252 | EM | Blind Grid | cart | Parsons | 14 September | 73.41 °F | 0" |
| 572 | EM | Moguls | cart | Parsons | 21 September | 73.12 °F | 0" |
| 572 | EM | Moguls | cart | Parsons | 22 September | 77.3 °F | 0" |
| 411 | EM | Open Field | cart | Parsons | 15 September | 68.05 °F | 0.05" |
| 411 | EM | Open Field | cart | Parsons | 16 September | 74.77 °F | 0" |
| 411 | EM | Open Field | cart | Parsons | 17 September | 75.57 °F | 0.1" |
| 411 | EM | Open Field | cart | Parsons | 20 September | 64.25 °F | 0" |
| 411 | EM | Open Field | cart | Parsons | 21 September | 73.12 °F | 0" |
| 496 | EM | Woods | cart | Parsons | 22 September | 77.3 °F | 0" |
| 496 | EM | Woods | cart | Parsons | 23 September | 79.92 °F | 0" |
| 257 | MAG | Blind Grid | hand | Parsons | 21 September | 73.12 °F | 0" |
| 573 | MAG | Moguls | hand | Parsons | 28 September | 73.65 °F | 2.69" |
| 573 | MAG | Moguls | hand | Parsons | 29 September | 69.37 °F | 0.01" |
| 229 | MAG | Open Field | hand | Parsons | 21 September | 73.12 °F | 0" |
| 229 | MAG | Open Field | hand | Parsons | 22 September | 77.3 °F | 0" |
| 229 | MAG | Open Field | hand | Parsons | 23 September | 79.92 °F | 0" |
| 229 | MAG | Open Field | hand | Parsons | 24 September | 73.14 °F | 0" |
| 229 | MAG | Open Field | hand | Parsons | 27 September | 71.18 °F | 0" |
| 229 | MAG | Open Field | hand | Parsons | 28 September | 73.65 °F | 2.69" |
| 229 | MAG | Open Field | hand | Parsons | 29 September | 69.37 °F | 0.01" |
| 499 | MAG | Woods | hand | Parsons | September 29 | 69.37 °F | 0.01" |
| 499 | MAG | Woods | hand | Parsons | September 30 | 68.96 °F | 0.02" |
| 197 | EM | Blind Grid | cart | Shaw | 8 December 8 | 31.64 °F | 0" |
| 197 | EM | Blind Grid | cart | Shaw | 9 December 9 | 33.68 °F | 0.12" |
| 552 | EM | Moguls | cart | Shaw | 18 December | 34.33 °F | 0" |
| 201 | EM | Open Field | cart | Shaw | 10 December | 39.8 °F | 0.39" |
| 201 | EM | Open Field | cart | Shaw | 11 December | 52.37 °F | 0.57" |
| 201 | EM | Open Field | cart | Shaw | 12 December | 39.33 °F | 0" |
| 201 | EM | Open Field | cart | Shaw | 13 December | 32.55 °F | 0" |
| 201 | EM | Open Field | cart | Shaw | 15 December | 40.5 °F | 0" |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|-------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 461 | EM | Woods | cart | Shaw | 15 December | 40.59 °F | 0" |
| 461 | EM | Woods | cart | Shaw | 16 December | 40.21 °F | 0" |
| 198 | MAG | Blind Grid | cart | Shaw | 8 December | 31.64 °F | 0" |
| 198 | MAG | Blind Grid | cart | Shaw | 9 December | 33.68 °F | 0.12" |
| 404 | MAG | Blind Grid | cart | Shaw | 19 December | 33.9 °F | 0" |
| 206 | MAG | Moguls | cart | Shaw | 19 December | 33.94 °F | 0" |
| 492 | MAG | Open Field | cart | Shaw | 9 December | 33.68 °F | 0.12" |
| 492 | MAG | Open Field | cart | Shaw | 16 December | 40.21 °F | 0" |
| 492 | MAG | Open Field | cart | Shaw | 18 December | 34.33 °F | 0" |
| 492 | MAG | Open Field | cart | Shaw | 19 December | 33.94 °F | 0" |
| 376 | MAG | Woods | cart | Shaw | 19 December | 33.9 °F | 0" |
| 157 | EM | Blind Grid | cart | TT | 3 November | 68.7 °F | 0" |
| 159 | EM | Blind Grid | sling | TT | 5 November | 65.78 °F | 0.2" |
| 549 | EM | Moguls | sling | TT | 11 November | 51.3 °F | 0" |
| 549 | EM | Moguls | sling | TT | 12 November | 54.64 °F | 0.68" |
| 165 | EM | Open Field | cart | TT | 4 November | 67.54 °F | 0" |
| 165 | EM | Open Field | cart | TT | 5 November | 65.78 °F | 0.2" |
| 165 | EM | Open Field | cart | TT | 6 November | 63.46 °F | 0.31" |
| 165 | EM | Open Field | cart | TT | 7 November | 57.17 °F | 0.03" |
| 165 | EM | Open Field | cart | TT | 10 November | 42.05 °F | 0" |
| 165 | EM | Open Field | cart | TT | 11 November | 51.3 °F | 0" |
| 457 | EM | Woods | sling | TT | 11 November | 51.3 °F | 0" |
| 457 | EM | Woods | sling | TT | 12 November | 54.64 °F | 0.68" |
| 457 | EM | Woods | sling | TT | 13 November | 48.05 °F | 0" |
| 764 | EM | Blind Grid | towed | VF Warner | 23 January | 40.7 °F | 0.89" |
| 764 | EM | Blind Grid | towed | VF Warner | 24 January | 40.7 °F | 0.08" |
| 764 | EM | Blind Grid | towed | VF Warner | 25 January | 39.4 °F | 0.02" |
| 45 | GPR | Blind Grid | cart | Witten | 2 December | 38.6 °F | 0" |
| 45 | GPR | Blind Grid | cart | Witten | 3 December | 25 °F | 0" |
| 126 | GPR | Mine Grid | cart | Witten | 2 December | 38.6 °F | 0" |
| 126 | GPR | Mine Grid | cart | Witten | 3 December | 25 °F | 0" |
| 37 | EM | Blind Grid | cart | Zonge | 19 August | 87 °F | 0" |
| 37 | EM | Blind Grid | cart | Zonge | 20 August | 84.2 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 19 August | 87 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 20 August | 84.2 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 21 August | 81.6 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 22 August | 82.2 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 23 August | 80.8 °F | 0.07" |
| 38 | EM | Open Field | cart | Zonge | 24 August | 78 °F | 0.84" |
| 38 | EM | Open Field | cart | Zonge | 25 August | 80.2 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 26 August | 78.1 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 27 August | 79.6 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 28 August | 71.2 °F | 0.64" |
| 38 | EM | Open Field | cart | Zonge | 29 August | 65.2 °F | 0.2" |
| 38 | EM | Open Field | cart | Zonge | 30 August | 67.5 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 31 August | 74.3 °F | 0" |
| 38 | EM | Open Field | cart | Zonge | 1 September | 64.1 °F | 0.92" |
| 38 | EM | Open Field | cart | Zonge | 2 September | 70.5 °F | 0" |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|-------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 383 | dual | Blind Grid | cart | BH | 18 May | 30.6 °F | 0" |
| 607 | dual | Desert Ext | cart | BH | 26 May | 26.9 °F | 0" |
| 607 | dual | Desert Ext | cart | BH | 27 May | 29.7 °F | 0" |
| 655 | dual | Moguls | cart | BH | 25 May | 28.5 °F | 0" |
| 655 | dual | Moguls | cart | BH | 26 May | 26.9 °F | 0" |
| 655 | dual | Moguls | cart | BH | 27 May | 29.7 °F | 0" |
| 655 | dual | Moguls | cart | BH | 28 May | 31.5 °F | 0" |
| 651 | dual | Open Field | towed | BH | 19 May | 30.5 °F | 0" |
| 651 | dual | Open Field | towed | BH | 20 May | 30.3 °F | 0" |
| 651 | dual | Open Field | towed | BH | 21 May | 27 °F | 0" |
| 651 | dual | Open Field | towed | BH | 22 May | 25.8 °F | 0" |
| 651 | dual | Open Field | towed | BH | 24 May | 28.3 °F | 0" |
| 651 | dual | Open Field | towed | BH | 25 May | 28.5 °F | 0" |
| 651 | dual | Open Field | towed | BH | 26 May | 26.9 °F | 0" |
| 216 | EM | Blind Grid | cart | ERDC | 6 May | 76.5 °F | 0" |
| 216 | EM | Blind Grid | cart | ERDC | 7 May | 66.1 °F | 0" |
| 216 | EM | Blind Grid | cart | ERDC | 8 May | 59.4 °F | 0" |
| 216 | EM | Blind Grid | cart | ERDC | 10 May | 75.25 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 6 May | 76.5 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 7 May | 66.1 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 8 May | 59.4 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 9 May | 68.2 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 12 May | 87.4 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 14 May | 88.9 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 15 May | 78.3 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 16 May | 91.3 °F | 0" |
| 249 | EM | Open Field | cart | ERDC | 19 May | 93.2 °F | 0" |
| 134 | EM | Blind Grid | cart | ERDC | 6 May | 76.5 °F | 0" |
| 134 | EM | Blind Grid | cart | ERDC | 7 May | 66.1 °F | 0" |
| 134 | EM | Blind Grid | cart | ERDC | 8 May | 59.4 °F | 0" |
| 509 | EM | Desert Ext | cart | ERDC | 20 May | 81 °F | 0" |
| 136 | EM | Moguls | cart | ERDC | 21 May | 81 °F | 0" |
| 135 | EM | Open Field | cart | ERDC | 7 May | 72.1 °F | 0" |
| 135 | EM | Open Field | cart | ERDC | 8 May | 70.7 °F | 0" |
| 135 | EM | Open Field | cart | ERDC | 9 May | 68.2 °F | 0" |
| 135 | EM | Open Field | cart | ERDC | 12 May | 87.4 °F | 0" |
| 135 | EM | Open Field | cart | ERDC | 14 May | 88.9 °F | 0" |
| 135 | EM | Open Field | cart | ERDC | 15 May | 78.3 °F | 0" |
| 135 | EM | Open Field | cart | ERDC | 16 May | 91.3 °F | 0" |
| 135 | EM | Open Field | cart | ERDC | 19 May | 93.2 °F | 0" |
| 362 | MAG | Blind Grid | sling | ERDC | 12 May | 87.2 °F | 0" |
| 544 | MAG | Desert Ext | sling | ERDC | 17 May | 81 °F | 0" |
| 571 | MAG | Moguls | sling | ERDC | 16 May | 91.2 °F | 0" |
| 364 | MAG | Open Field | sling | ERDC | 14 May | 88.96 °F | 0" |
| 364 | MAG | Open Field | sling | ERDC | 15 May | 78.35 °F | 0" |
| 364 | MAG | Open Field | sling | ERDC | 16 May | 91.25 °F | 0" |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|-------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 769 | MAG | Blind Grid | hand | Forester | 30 January | 17.4 °F | 0" |
| 769 | MAG | Blind Grid | hand | Forester | 6 February | 19.7 °F | 0" |
| 770 | MAG | Open Field | hand | Forester | 30 January | 63.3 °F | 0" |
| 770 | MAG | Open Field | hand | Forester | 31 January | 64.2 °F | 0" |
| 770 | MAG | Open Field | hand | Forester | 1 February | 64.6 °F | 0" |
| 770 | MAG | Open Field | hand | Forester | 2 February | 69.3 °F | 0" |
| 770 | MAG | Open Field | hand | Forester | 3 February | 65.5 °F | 0" |
| 770 | MAG | Open Field | hand | Forester | 6 February | 67.5 °F | 0" |
| 770 | MAG | Open Field | hand | Forester | 7 February | 67.1 °F | 0" |
| 293 | dual | Blind Grid | towed | Geocenters | 18 October | 75.9 °F | 0" |
| 293 | dual | Blind Grid | towed | Geocenters | 19 October | 74.93 °F | 0" |
| 293 | dual | Blind Grid | towed | Geocenters | 20 October | 76.5 °F | 0" |
| 299 | dual | Open Field | towed | Geocenters | 18 October | 75.9 °F | 0" |
| 299 | dual | Open Field | towed | Geocenters | 19 October | 74.93 °F | 0" |
| 299 | dual | Open Field | towed | Geocenters | 20 October | 76.5 °F | 0" |
| 186 | EM | Blind Grid | hand | G-TEK | 28 October | 73.65 °F | 0" |
| 144 | EM | Desert Ext. | hand | G-TEK | 3 November | 63.29 °F | 0" |
| 144 | EM | Desert Ext. | hand | G-TEK | 5 November | 64.97 °F | 0" |
| 579 | EM | Moguls | sling | G-TEK | 4 November | 62.6 °F | 0" |
| 148 | EM | Open Field | sling | G-TEK | 28 October | 82.11 °F | 0" |
| 148 | EM | Open Field | sling | G-TEK | 29 October | 79.61 °F | 0" |
| 148 | EM | Open Field | sling | G-TEK | 30 October | 73.98 °F | 0" |
| 148 | EM | Open Field | sling | G-TEK | 31 October | 67.55 °F | 0" |
| 148 | EM | Open Field | sling | G-TEK | 3 November | 63.3 °F | 0" |
| 148 | EM | Open Field | sling | G-TEK | 4 November | 62.65 °F | 0" |
| 148 | EM | Open Field | sling | G-TEK | 5 November | 64.99 °F | 0" |
| 148 | EM | Open Field | sling | G-TEK | 6 November | 67.03 °F | 0" |
| 431 | MAG | Blind Grid | sling | G-TEK | 28 October | 73.65 °F | 0" |
| 431 | MAG | Blind Grid | sling | G-TEK | 6 November | 62.73 °F | 0" |
| 536 | MAG | Desert Ext. | sling | G-TEK | 3 November | 63.29 °F | 0" |
| 536 | MAG | Desert Ext. | sling | G-TEK | 4 November | 62.59 °F | 0" |
| 536 | MAG | Desert Ext. | sling | G-TEK | 5 November | 64.97 °F | 0" |
| 536 | MAG | Desert Ext. | sling | G-TEK | 6 November | 67.02 °F | 0" |
| 581 | MAG | Moguls | sling | G-TEK | 31 October | 67.5 °F | 0" |
| 581 | MAG | Moguls | sling | G-TEK | 3 November | 63.2 °F | 0" |
| 581 | MAG | Moguls | sling | G-TEK | 5 November | 64.9 °F | 0" |
| 147 | MAG | Open Field | sling | G-TEK | 28 October | 82.08 °F | 0" |
| 147 | MAG | Open Field | sling | G-TEK | 29 October | 79.62 °F | 0" |
| 147 | MAG | Open Field | sling | G-TEK | 30 October | 74 °F | 0" |
| 147 | MAG | Open Field | sling | G-TEK | 31 October | 67.51 °F | 0" |
| 147 | MAG | Open Field | sling | G-TEK | 4 November | 62.6 °F | 0" |
| 147 | MAG | Open Field | sling | G-TEK | 5 November | 64.98 °F | 0" |
| 238 | MAG | Blind Grid | hand | HFA | 20 April | 24.8 °F | 0" |
| 238 | MAG | Blind Grid | hand | HFA | 21 April | 27.3 °F | 0" |
| 528 | MAG | Desert Ext. | hand | HFA | 7 May | 32.6 °F | 0" |
| 528 | MAG | Desert Ext. | hand | HFA | 10 May | 32 °F | 0" |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|--------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 528 | MAG | Desert Ext. | hand | HFA | 11 May | 28.2 °F | 0" |
| 587 | MAG | Moguls | hand | HFA | 11 May | 28.2 °F | 0" |
| 587 | MAG | Moguls | hand | HFA | 12 May | 27.2 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 22 April | 25.2 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 23 April | 26.3 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 26 April | 34.1 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 27 April | 33.7 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 28 April | 32.6 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 29 April | 26.6 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 30 April | 26.3 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 3 May | 35.4 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 4 May | 35.3 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 5 May | 33.8 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 6 May | 33 °F | 0" |
| 442 | MAG | Open Field | hand | HFA | 7 May | 37.8 °F | 0" |
| 667 | EM | Blind Grid | towed | NAEVA | 6 December | 53.78 °F | 0" |
| 667 | EM | Blind Grid | towed | NAEVA | 8 December | 48.4 °F | 0" |
| 666 | EM | Blind Grid | 2-man | NAEVA | 15 December | 56.7 °F | 0" |
| 670 | EM | Desert Ext. | 2-man | NAEVA | 14 December | 60.42 °F | 0" |
| 670 | EM | Desert Ext. | 2-man | NAEVA | 15 December | 56.7 °F | 0" |
| 669 | EM | Moguls | 2-man | NAEVA | 13 December | 57.83 °F | 0" |
| 669 | EM | Moguls | 2-man | NAEVA | 14 December | 60.42 °F | 0" |
| 668 | EM | Open Field | towed | NAEVA | 6 December | 53.78 °F | 0" |
| 668 | EM | Open Field | towed | NAEVA | 8 December | 48.4 °F | 0" |
| 668 | EM | Open Field | towed | NAEVA | 9 December | 47.61 °F | 0" |
| 668 | EM | Open Field | towed | NAEVA | 10 December | 58.35 °F | 0" |
| 668 | EM | Open Field | towed | NAEVA | 13 December | 57.83 °F | 0" |
| 668 | EM | Open Field | towed | NAEVA | 14 December | 60.42 °F | 0" |
| 668 | EM | Open Field | towed | NAEVA | 15 December | 56.7 °F | 0" |
| 213 | EM | Blind Grid | towed | NRL | 13 November | 68.9 °F | 0" |
| 213 | EM | Blind Grid | towed | NRL | 14 November | 62.9 °F | 0" |
| 213 | EM | Blind Grid | towed | NRL | 19 November | 72.1 °F | 0" |
| 245 | EM | Open Field | towed | NRL | 14 November | 17.2 °F | 0" |
| 245 | EM | Open Field | towed | NRL | 17 November | 17.1 °F | 0" |
| 245 | EM | Open Field | towed | NRL | 18 November | 19.2 °F | 0" |
| 245 | EM | Open Field | towed | NRL | 19 November | 18.5 °F | 0" |
| 690 | EM | Blind Grid | cart | Parsons | 29 September | 26.4 °F | 0" |
| 532 | EM | Desert Ext. | cart | Parsons | 29 September | 26.4 °F | 0" |
| 532 | EM | Desert Ext. | cart | Parsons | 30 September | 24.6 °F | 0" |
| 532 | EM | Desert Ext. | cart | Parsons | 1 October | 28.1 °F | 0" |
| 532 | EM | Desert Ext. | cart | Parsons | 4 October | 29.8 °F | 0" |
| 532 | EM | Desert Ext. | cart | Parsons | 7 October | 29.6 °F | 0" |
| 588 | EM | Moguls | cart | Parsons | 29 September | 26.4 °F | 0" |
| 588 | EM | Moguls | cart | Parsons | 30 September | 22.7 °F | 0" |
| 588 | EM | Moguls | cart | Parsons | 1 October | 26.8 °F | 0" |
| 588 | EM | Moguls | cart | Parsons | 4 October | 29.8 °F | 0" |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|-------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 425 | EM | Open Field | cart | Parsons | 1 October | 28.1 °F | 0" |
| 425 | EM | Open Field | cart | Parsons | 4 October | 29.8 °F | 0" |
| 425 | EM | Open Field | cart | Parsons | 5 October | 27.9 °F | 0" |
| 425 | EM | Open Field | cart | Parsons | 6 October | 30.5 °F | 0" |
| 425 | EM | Open Field | cart | Parsons | 7 October | 29.6 °F | 0" |
| 606 | MAG | Blind Grid | hand | Parsons | 12 October | 26.6 °F | 0" |
| 601 | MAG | Desert Ext. | hand | Parsons | 19 October | 23 °F | 0" |
| 601 | MAG | Desert Ext. | hand | Parsons | 20 October | 23.9 °F | 0" |
| 602 | MAG | Moguls | hand | Parsons | 18 October | 23.6 °F | 0" |
| 602 | MAG | Moguls | hand | Parsons | 19 October | 23 °F | 0" |
| 426 | MAG | Open Field | hand | Parsons | 12 October | 26.7 °F | 0" |
| 426 | MAG | Open Field | hand | Parsons | 13 October | 26.6 °F | 0" |
| 426 | MAG | Open Field | hand | Parsons | 14 October | 30.4 °F | 0" |
| 426 | MAG | Open Field | hand | Parsons | 15 October | 27.1 °F | 0" |
| 426 | MAG | Open Field | hand | Parsons | 18 October | 23.6 °F | 0" |
| 199 | EM | Blind Grid | cart | Shaw | 12 January | 17.9 °F | 0" |
| 199 | EM | Blind Grid | cart | Shaw | 13 January | 18.5 °F | 0" |
| 211 | EM | Desert Ext. | cart | Shaw | 16 January | 17.8 °F | 0" |
| 211 | EM | Desert Ext. | cart | Shaw | 23 January | 14.3 °F | 0" |
| 211 | EM | Desert Ext. | cart | Shaw | 26 January | 13.7 °F | 0" |
| 211 | EM | Desert Ext. | cart | Shaw | 27 January | 13.6 °F | 0" |
| 207 | EM | Moguls | cart | Shaw | 16 January | 17.8 °F | 0" |
| 354 | EM | Open Field | cart | Shaw | 12 January | 18.2 °F | 0" |
| 354 | EM | Open Field | cart | Shaw | 13 January | 29.8 °F | 0" |
| 354 | EM | Open Field | cart | Shaw | 14 January | 21.1 °F | 0" |
| 354 | EM | Open Field | cart | Shaw | 15 January | 19.2 °F | 0" |
| 354 | EM | Open Field | cart | Shaw | 27 January | 13.6 °F | 0" |
| 312 | MAG | Blind Grid | cart | Shaw | 20 January | 15.74 °F | 0" |
| 312 | MAG | Blind Grid | cart | Shaw | 22 January | 14.55 °F | 0" |
| 312 | MAG | Blind Grid | cart | Shaw | 26 January | 13.7 °F | 0" |
| 541 | MAG | Desert Ext. | cart | Shaw | 23 January | 14.3 °F | 0" |
| 541 | MAG | Desert Ext. | cart | Shaw | 26 January | 13.7 °F | 0" |
| 594 | MAG | Moguls | cart | Shaw | 22 January | 14.5 °F | 0" |
| 638 | MAG | Open Field | cart | Shaw | 20 January | 15.7 °F | 0.1" |
| 638 | MAG | Open Field | cart | Shaw | 21 January | 14.4 °F | 0.1" |
| 638 | MAG | Open Field | cart | Shaw | 22 January | 14.5 °F | 0" |
| 638 | MAG | Open Field | cart | Shaw | 23 January | 14.3 °F | 0" |
| 638 | MAG | Open Field | cart | Shaw | 26 January | 13.7 °F | 0" |
| 168 | EM | Blind Grid | cart | TT | 1 December | 59.7 °F | 0" |
| 171 | EM | Desert Ext. | cart | TT | 4 December | 64.1 °F | 0" |
| 171 | EM | Desert Ext. | cart | TT | 5 December | 63.8 °F | 0" |
| 171 | EM | Desert Ext. | cart | TT | 8 December | 63.7 °F | 0" |
| 170 | EM | Moguls | sling | TT | 4 December | 64 °F | 0" |
| 170 | EM | Moguls | sling | TT | 5 December | 63.8 °F | 0" |
| 169 | EM | Open Field | cart | TT | 2 December | 64.3 °F | 0" |
| 169 | EM | Open Field | cart | TT | 3 December | 64.5 °F | 0" |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-------------|-----------------|---------------|-------------|--------------------|----------------------|
| Report | Sensor | Area | Platform | Vendor | Date | Temperature | Precipitation |
| 169 | EM | Open Field | cart | TT | 4 December | 64.1 °F | 0" |
| 169 | EM | Open Field | cart | TT | 8 December | 63.7 °F | 0" |

APPENDIX C. SOIL MOISTURE

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 39 | EM | hand | AETC | Open Field | 0 to 6 | 32.78 | 7.04 |
| 39 | EM | hand | AETC | Open Field | 6 to 12 | 27.95 | 9.71 |
| 39 | EM | hand | AETC | Open Field | 12 to 24 | 11.63 | 3.86 |
| 39 | EM | hand | AETC | Open Field | 24 to 36 | 30.93 | 17.65 |
| 39 | EM | hand | AETC | Open Field | 36 to 48 | 11.95 | 8.49 |
| 695 | EM | hand | ARM | Wet Probe | 0 to 6 | 0 | 0 |
| 695 | EM | hand | ARM | Wet Probe | 6 to 12 | 0 | 0 |
| 695 | EM | hand | ARM | Wet Probe | 12 to 24 | 0 | 0 |
| 695 | EM | hand | ARM | Wet Probe | 24 to 36 | 0 | 0 |
| 695 | EM | hand | ARM | Wet Probe | 36 to 48 | 0 | 0 |
| 695 | EM | hand | ARM | Woods | 0 to 6 | 0 | 0 |
| 695 | EM | hand | ARM | Woods | 6 to 12 | 0 | 0 |
| 695 | EM | hand | ARM | Woods | 12 to 24 | 0 | 0 |
| 695 | EM | hand | ARM | Woods | 24 to 36 | 0 | 0 |
| 695 | EM | hand | ARM | Woods | 36 to 48 | 0 | 0 |
| 695 | EM | hand | ARM | Open Field | 0 to 6 | 0 | 0 |
| 695 | EM | hand | ARM | Open Field | 6 to 12 | 0 | 0 |
| 695 | EM | hand | ARM | Open Field | 12 to 24 | 0 | 0 |
| 695 | EM | hand | ARM | Open Field | 24 to 36 | 0 | 0 |
| 695 | EM | hand | ARM | Open Field | 36 to 48 | 0 | 0 |
| 695 | EM | hand | ARM | Calibration | 0 to 6 | 6.187 | 0.183 |
| 695 | EM | hand | ARM | Calibration | 6 to 12 | 37.738 | 0.581 |
| 695 | EM | hand | ARM | Calibration | 12 to 24 | 50.55 | 0.132 |
| 695 | EM | hand | ARM | Calibration | 24 to 36 | 44.875 | 0.334 |
| 695 | EM | hand | ARM | Calibration | 36 to 48 | 40.075 | 0.399 |
| 695 | EM | hand | ARM | Blind Grid | 0 to 6 | 3.767 | 0.137 |
| 695 | EM | hand | ARM | Blind Grid | 6 to 12 | 24.267 | 0.262 |
| 695 | EM | hand | ARM | Blind Grid | 12 to 24 | 38.033 | 0.149 |
| 695 | EM | hand | ARM | Blind Grid | 24 to 36 | 35.167 | 0.189 |
| 695 | EM | hand | ARM | Blind Grid | 36 to 48 | 39.833 | 0.229 |
| 691 | EM | hand | ARM | Wet Probe | 0 to 6 | 0 | 0 |
| 691 | EM | hand | ARM | Wet Probe | 6 to 12 | 0 | 0 |
| 691 | EM | hand | ARM | Wet Probe | 12 to 24 | 0 | 0 |
| 691 | EM | hand | ARM | Wet Probe | 24 to 36 | 0 | 0 |
| 691 | EM | hand | ARM | Wet Probe | 36 to 48 | 0 | 0 |
| 691 | EM | hand | ARM | Woods | 0 to 6 | 0 | 0 |
| 691 | EM | hand | ARM | Woods | 6 to 12 | 0 | 0 |
| 691 | EM | hand | ARM | Woods | 12 to 24 | 0 | 0 |
| 691 | EM | hand | ARM | Woods | 24 to 36 | 0 | 0 |
| 691 | EM | hand | ARM | Woods | 36 to 48 | 0 | 0 |
| 691 | EM | hand | ARM | Open Field | 0 to 6 | 0 | 0 |
| 691 | EM | hand | ARM | Open Field | 6 to 12 | 0 | 0 |
| 691 | EM | hand | ARM | Open Field | 12 to 24 | 0 | 0 |
| 691 | EM | hand | ARM | Open Field | 24 to 36 | 0 | 0 |
| 691 | EM | hand | ARM | Open Field | 36 to 48 | 0 | 0 |
| 691 | EM | hand | ARM | Calibration | 0 to 6 | 6.187 | 0.183 |
| 691 | EM | hand | ARM | Calibration | 6 to 12 | 37.738 | 0.581 |

Aberdeen Proving Ground Demonstrations

| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
|---------------|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| 691 | EM | hand | ARM | Calibration | 12 to 24 | 50.55 | 0.132 |
| 691 | EM | hand | ARM | Calibration | 24 to 36 | 44.875 | 0.334 |
| 691 | EM | hand | ARM | Calibration | 36 to 48 | 40.075 | 0.399 |
| 691 | EM | hand | ARM | Blind Grid | 0 to 6 | 3.767 | 0.137 |
| 691 | EM | hand | ARM | Blind Grid | 6 to 12 | 24.267 | 0.262 |
| 691 | EM | hand | ARM | Blind Grid | 12 to 24 | 38.033 | 0.149 |
| 691 | EM | hand | ARM | Blind Grid | 24 to 36 | 35.167 | 0.189 |
| 691 | EM | hand | ARM | Blind Grid | 36 to 48 | 39.833 | 0.229 |
| 622 | dual | cart | BH | Wet Probe | 0 to 6 | 64.133 | 0.634 |
| 622 | dual | cart | BH | Wet Probe | 6 to 12 | 72.947 | 0.56 |
| 622 | dual | cart | BH | Wet Probe | 12 to 24 | 77.727 | 0.742 |
| 622 | dual | cart | BH | Wet Probe | 24 to 36 | 54.033 | 0.753 |
| 622 | dual | cart | BH | Wet Probe | 36 to 48 | 51.373 | 0.249 |
| 622 | dual | cart | BH | Woods | 0 to 6 | 13.65 | 0.357 |
| 622 | dual | cart | BH | Woods | 6 to 12 | 5.625 | 0.179 |
| 622 | dual | cart | BH | Woods | 12 to 24 | 5.8 | 0.122 |
| 622 | dual | cart | BH | Woods | 24 to 36 | 55.55 | 0.112 |
| 622 | dual | cart | BH | Woods | 36 to 48 | 57.45 | 0.15 |
| 622 | dual | cart | BH | Open Field | 0 to 6 | 19.953 | 0.741 |
| 622 | dual | cart | BH | Open Field | 6 to 12 | 5.187 | 0.365 |
| 622 | dual | cart | BH | Open Field | 12 to 24 | 18.273 | 0.621 |
| 622 | dual | cart | BH | Open Field | 24 to 36 | 25.413 | 0.534 |
| 622 | dual | cart | BH | Open Field | 36 to 48 | 51.467 | 0.282 |
| 622 | dual | cart | BH | Calibration | 0 to 6 | 0.9 | 0.1 |
| 622 | dual | cart | BH | Calibration | 6 to 12 | 20.1 | 0.1 |
| 622 | dual | cart | BH | Calibration | 12 to 24 | 28.25 | 0.05 |
| 622 | dual | cart | BH | Calibration | 24 to 36 | 35.3 | 0.1 |
| 622 | dual | cart | BH | Calibration | 36 to 48 | 39 | 0 |
| 622 | dual | cart | BH | Blind Grid | 0 to 6 | 3.175 | 0.286 |
| 622 | dual | cart | BH | Blind Grid | 6 to 12 | 24.825 | 0.179 |
| 622 | dual | cart | BH | Blind Grid | 12 to 24 | 38.925 | 0.228 |
| 622 | dual | cart | BH | Blind Grid | 24 to 36 | 35.9 | 0.158 |
| 622 | dual | cart | BH | Blind Grid | 36 to 48 | 39.475 | 0.396 |
| 642 | dual | cart | BH | Wet Probe | 0 to 6 | 64.133 | 0.634 |
| 642 | dual | cart | BH | Wet Probe | 6 to 12 | 72.947 | 0.56 |
| 642 | dual | cart | BH | Wet Probe | 12 to 24 | 77.727 | 0.742 |
| 642 | dual | cart | BH | Wet Probe | 24 to 36 | 54.033 | 0.753 |
| 642 | dual | cart | BH | Wet Probe | 36 to 48 | 51.373 | 0.249 |
| 642 | dual | cart | BH | Woods | 0 to 6 | 13.65 | 0.357 |
| 642 | dual | cart | BH | Woods | 6 to 12 | 5.625 | 0.179 |
| 642 | dual | cart | BH | Woods | 12 to 24 | 5.8 | 0.122 |
| 642 | dual | cart | BH | Woods | 24 to 36 | 55.55 | 0.112 |
| 642 | dual | cart | BH | Woods | 36 to 48 | 57.45 | 0.15 |
| 642 | dual | cart | BH | Open Field | 0 to 6 | 19.953 | 0.741 |
| 642 | dual | cart | BH | Open Field | 6 to 12 | 5.187 | 0.365 |
| 642 | dual | cart | BH | Open Field | 12 to 24 | 18.273 | 0.621 |
| 642 | dual | cart | BH | Open Field | 24 to 36 | 25.413 | 0.534 |
| 642 | dual | cart | BH | Open Field | 36 to 48 | 51.467 | 0.282 |
| 642 | dual | cart | BH | Calibration | 0 to 6 | 0.9 | 0.1 |
| 642 | dual | cart | BH | Calibration | 6 to 12 | 20.1 | 0.1 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 642 | dual | cart | BH | Calibration | 12 to 24 | 28.25 | 0.05 |
| 642 | dual | cart | BH | Calibration | 24 to 36 | 35.3 | 0.1 |
| 642 | dual | cart | BH | Calibration | 36 to 48 | 39 | 0 |
| 642 | dual | cart | BH | Blind Grid | 0 to 6 | 3.175 | 0.286 |
| 642 | dual | cart | BH | Blind Grid | 6 to 12 | 24.825 | 0.179 |
| 642 | dual | cart | BH | Blind Grid | 12 to 24 | 38.925 | 0.228 |
| 642 | dual | cart | BH | Blind Grid | 24 to 36 | 35.9 | 0.158 |
| 642 | dual | cart | BH | Blind Grid | 36 to 48 | 39.475 | 0.396 |
| 657 | dual | cart | BH | Wet Probe | 0 to 6 | 64.133 | 0.634 |
| 657 | dual | cart | BH | Wet Probe | 6 to 12 | 72.947 | 0.56 |
| 657 | dual | cart | BH | Wet Probe | 12 to 24 | 77.727 | 0.742 |
| 657 | dual | cart | BH | Wet Probe | 24 to 36 | 54.033 | 0.753 |
| 657 | dual | cart | BH | Wet Probe | 36 to 48 | 51.373 | 0.249 |
| 657 | dual | cart | BH | Woods | 0 to 6 | 13.65 | 0.357 |
| 657 | dual | cart | BH | Woods | 6 to 12 | 5.625 | 0.179 |
| 657 | dual | cart | BH | Woods | 12 to 24 | 5.8 | 0.122 |
| 657 | dual | cart | BH | Woods | 24 to 36 | 55.55 | 0.112 |
| 657 | dual | cart | BH | Woods | 36 to 48 | 57.45 | 0.15 |
| 657 | dual | cart | BH | Open Field | 0 to 6 | 19.953 | 0.741 |
| 657 | dual | cart | BH | Open Field | 6 to 12 | 5.187 | 0.365 |
| 657 | dual | cart | BH | Open Field | 12 to 24 | 18.273 | 0.621 |
| 657 | dual | cart | BH | Open Field | 24 to 36 | 25.413 | 0.534 |
| 657 | dual | cart | BH | Open Field | 36 to 48 | 51.467 | 0.282 |
| 657 | dual | cart | BH | Calibration | 0 to 6 | 0.9 | 0.1 |
| 657 | dual | cart | BH | Calibration | 6 to 12 | 20.1 | 0.1 |
| 657 | dual | cart | BH | Calibration | 12 to 24 | 28.25 | 0.05 |
| 657 | dual | cart | BH | Calibration | 24 to 36 | 35.3 | 0.1 |
| 657 | dual | cart | BH | Calibration | 36 to 48 | 39 | 0 |
| 657 | dual | cart | BH | Blind Grid | 0 to 6 | 3.175 | 0.286 |
| 657 | dual | cart | BH | Blind Grid | 6 to 12 | 24.825 | 0.179 |
| 657 | dual | cart | BH | Blind Grid | 12 to 24 | 38.925 | 0.228 |
| 657 | dual | cart | BH | Blind Grid | 24 to 36 | 35.9 | 0.158 |
| 657 | dual | cart | BH | Blind Grid | 36 to 48 | 39.475 | 0.396 |
| 636 | dual | cart | BH | Wet Probe | 0 to 6 | 64.133 | 0.634 |
| 636 | dual | cart | BH | Wet Probe | 6 to 12 | 72.947 | 0.56 |
| 636 | dual | cart | BH | Wet Probe | 12 to 24 | 77.727 | 0.742 |
| 636 | dual | cart | BH | Wet Probe | 24 to 36 | 54.033 | 0.753 |
| 636 | dual | cart | BH | Wet Probe | 36 to 48 | 51.373 | 0.249 |
| 636 | dual | cart | BH | Woods | 0 to 6 | 13.65 | 0.357 |
| 636 | dual | cart | BH | Woods | 6 to 12 | 5.625 | 0.179 |
| 636 | dual | cart | BH | Woods | 12 to 24 | 5.8 | 0.122 |
| 636 | dual | cart | BH | Woods | 24 to 36 | 55.55 | 0.112 |
| 636 | dual | cart | BH | Woods | 36 to 48 | 57.45 | 0.15 |
| 636 | dual | cart | BH | Open Field | 0 to 6 | 19.953 | 0.741 |
| 636 | dual | cart | BH | Open Field | 6 to 12 | 5.187 | 0.365 |
| 636 | dual | cart | BH | Open Field | 12 to 24 | 18.273 | 0.621 |
| 636 | dual | cart | BH | Open Field | 24 to 36 | 25.413 | 0.534 |
| 636 | dual | cart | BH | Open Field | 36 to 48 | 51.467 | 0.282 |
| 636 | dual | cart | BH | Calibration | 0 to 6 | 0.9 | 0.1 |
| 636 | dual | cart | BH | Calibration | 6 to 12 | 20.1 | 0.1 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 636 | dual | cart | BH | Calibration | 12 to 24 | 28.25 | 0.05 |
| 636 | dual | cart | BH | Calibration | 24 to 36 | 35.3 | 0.1 |
| 636 | dual | cart | BH | Calibration | 36 to 48 | 39 | 0 |
| 636 | dual | cart | BH | Blind Grid | 0 to 6 | 3.175 | 0.286 |
| 636 | dual | cart | BH | Blind Grid | 6 to 12 | 24.825 | 0.179 |
| 636 | dual | cart | BH | Blind Grid | 12 to 24 | 38.925 | 0.228 |
| 636 | dual | cart | BH | Blind Grid | 24 to 36 | 35.9 | 0.158 |
| 636 | dual | cart | BH | Blind Grid | 36 to 48 | 39.475 | 0.396 |
| 304 | EM | cart | ERDC | Wet Probe | 0 to 6 | 78.479 | 2.922 |
| 304 | EM | cart | ERDC | Wet Probe | 6 to 12 | 77.262 | 1.753 |
| 304 | EM | cart | ERDC | Wet Probe | 12 to 24 | 69.7 | 0.726 |
| 304 | EM | cart | ERDC | Wet Probe | 24 to 36 | 52.641 | 0.596 |
| 304 | EM | cart | ERDC | Wet Probe | 36 to 48 | 49.741 | 0.516 |
| 304 | EM | cart | ERDC | Woods | 0 to 6 | 0 | 0 |
| 304 | EM | cart | ERDC | Woods | 6 to 12 | 0 | 0 |
| 304 | EM | cart | ERDC | Woods | 12 to 24 | 0 | 0 |
| 304 | EM | cart | ERDC | Woods | 24 to 36 | 0 | 0 |
| 304 | EM | cart | ERDC | Woods | 36 to 48 | 0 | 0 |
| 304 | EM | cart | ERDC | Open Field | 0 to 6 | 12.772 | 1.325 |
| 304 | EM | cart | ERDC | Open Field | 6 to 12 | 2.421 | 0.697 |
| 304 | EM | cart | ERDC | Open Field | 12 to 24 | 15.679 | 1.027 |
| 304 | EM | cart | ERDC | Open Field | 24 to 36 | 21.548 | 0.302 |
| 304 | EM | cart | ERDC | Open Field | 36 to 48 | 27.245 | 0.964 |
| 304 | EM | cart | ERDC | Calibration | 0 to 6 | 39.5 | 0.3 |
| 304 | EM | cart | ERDC | Calibration | 6 to 12 | 37.6 | 0.1 |
| 304 | EM | cart | ERDC | Calibration | 12 to 24 | 0.9 | 0 |
| 304 | EM | cart | ERDC | Calibration | 24 to 36 | 4.6 | 0.1 |
| 304 | EM | cart | ERDC | Calibration | 36 to 48 | 5.05 | 0.15 |
| 304 | EM | cart | ERDC | Blind Grid | 0 to 6 | 4.65 | 0.25 |
| 304 | EM | cart | ERDC | Blind Grid | 6 to 12 | 9.65 | 0.15 |
| 304 | EM | cart | ERDC | Blind Grid | 12 to 24 | 35.1 | 0.2 |
| 304 | EM | cart | ERDC | Blind Grid | 24 to 36 | 36.45 | 0.25 |
| 304 | EM | cart | ERDC | Blind Grid | 36 to 48 | 38.8 | 0.1 |
| 305 | EM | cart | ERDC | Wet Probe | 0 to 6 | 78.479 | 2.922 |
| 305 | EM | cart | ERDC | Wet Probe | 6 to 12 | 77.262 | 1.753 |
| 305 | EM | cart | ERDC | Wet Probe | 12 to 24 | 69.7 | 0.726 |
| 305 | EM | cart | ERDC | Wet Probe | 24 to 36 | 52.641 | 0.596 |
| 305 | EM | cart | ERDC | Wet Probe | 36 to 48 | 49.741 | 0.516 |
| 305 | EM | cart | ERDC | Woods | 0 to 6 | 0 | 0 |
| 305 | EM | cart | ERDC | Woods | 6 to 12 | 0 | 0 |
| 305 | EM | cart | ERDC | Woods | 12 to 24 | 0 | 0 |
| 305 | EM | cart | ERDC | Woods | 24 to 36 | 0 | 0 |
| 305 | EM | cart | ERDC | Woods | 36 to 48 | 0 | 0 |
| 305 | EM | cart | ERDC | Open Field | 0 to 6 | 12.772 | 1.325 |
| 305 | EM | cart | ERDC | Open Field | 6 to 12 | 2.421 | 0.697 |
| 305 | EM | cart | ERDC | Open Field | 12 to 24 | 15.679 | 1.027 |
| 305 | EM | cart | ERDC | Open Field | 24 to 36 | 21.548 | 0.302 |
| 305 | EM | cart | ERDC | Open Field | 36 to 48 | 27.245 | 0.964 |
| 305 | EM | cart | ERDC | Calibration | 0 to 6 | 39.5 | 0.3 |
| 305 | EM | cart | ERDC | Calibration | 6 to 12 | 37.6 | 0.1 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 305 | EM | cart | ERDC | Calibration | 12 to 24 | 0.9 | 0 |
| 305 | EM | cart | ERDC | Calibration | 24 to 36 | 4.6 | 0.1 |
| 305 | EM | cart | ERDC | Calibration | 36 to 48 | 5.05 | 0.15 |
| 305 | EM | cart | ERDC | Blind Grid | 0 to 6 | 4.65 | 0.25 |
| 305 | EM | cart | ERDC | Blind Grid | 6 to 12 | 9.65 | 0.15 |
| 305 | EM | cart | ERDC | Blind Grid | 12 to 24 | 35.1 | 0.2 |
| 305 | EM | cart | ERDC | Blind Grid | 24 to 36 | 36.45 | 0.25 |
| 305 | EM | cart | ERDC | Blind Grid | 36 to 48 | 38.8 | 0.1 |
| 142 | EM | cart | ERDC | Wet Probe | 0 to 6 | 0 | 0 |
| 142 | EM | cart | ERDC | Wet Probe | 6 to 12 | 0 | 0 |
| 142 | EM | cart | ERDC | Wet Probe | 12 to 24 | 0 | 0 |
| 142 | EM | cart | ERDC | Wet Probe | 24 to 36 | 0 | 0 |
| 142 | EM | cart | ERDC | Wet Probe | 36 to 48 | 0 | 0 |
| 142 | EM | cart | ERDC | Woods | 0 to 6 | 0 | 0 |
| 142 | EM | cart | ERDC | Woods | 6 to 12 | 0 | 0 |
| 142 | EM | cart | ERDC | Woods | 12 to 24 | 0 | 0 |
| 142 | EM | cart | ERDC | Woods | 24 to 36 | 0 | 0 |
| 142 | EM | cart | ERDC | Woods | 36 to 48 | 0 | 0 |
| 142 | EM | cart | ERDC | Open Field | 0 to 6 | 39.812 | 0.276 |
| 142 | EM | cart | ERDC | Open Field | 6 to 12 | 38.138 | 0.387 |
| 142 | EM | cart | ERDC | Open Field | 12 to 24 | 8.462 | 0.628 |
| 142 | EM | cart | ERDC | Open Field | 24 to 36 | 5.412 | 0.713 |
| 142 | EM | cart | ERDC | Open Field | 36 to 48 | 5.525 | 1.015 |
| 141 | EM | cart | ERDC | Wet Probe | 0 to 6 | 0 | 0 |
| 141 | EM | cart | ERDC | Wet Probe | 6 to 12 | 0 | 0 |
| 141 | EM | cart | ERDC | Wet Probe | 12 to 24 | 0 | 0 |
| 141 | EM | cart | ERDC | Wet Probe | 24 to 36 | 0 | 0 |
| 141 | EM | cart | ERDC | Wet Probe | 36 to 48 | 0 | 0 |
| 141 | EM | cart | ERDC | Woods | 0 to 6 | 0 | 0 |
| 141 | EM | cart | ERDC | Woods | 6 to 12 | 0 | 0 |
| 141 | EM | cart | ERDC | Woods | 12 to 24 | 0 | 0 |
| 141 | EM | cart | ERDC | Woods | 24 to 36 | 0 | 0 |
| 141 | EM | cart | ERDC | Woods | 36 to 48 | 0 | 0 |
| 141 | EM | cart | ERDC | Open Field | 0 to 6 | 39.812 | 0.276 |
| 141 | EM | cart | ERDC | Open Field | 6 to 12 | 38.138 | 0.387 |
| 141 | EM | cart | ERDC | Open Field | 12 to 24 | 8.462 | 0.628 |
| 141 | EM | cart | ERDC | Open Field | 24 to 36 | 5.412 | 0.713 |
| 141 | EM | cart | ERDC | Open Field | 36 to 48 | 5.525 | 1.015 |
| 40 | dual | towed | Geocenters | Open Field | 0 to 6 | 17.37 | 6.83 |
| 40 | dual | towed | Geocenters | Open Field | 6 to 12 | 10.17 | 2.03 |
| 40 | dual | towed | Geocenters | Open Field | 12 to 24 | 0.35 | 0.1 |
| 40 | dual | towed | Geocenters | Open Field | 24 to 36 | 26.52 | 0.34 |
| 40 | dual | towed | Geocenters | Open Field | 36 to 48 | 9.75 | 0.17 |
| 290 | dual | towed | Geocenters | Wet Probe | 0 to 6 | 65.367 | 0.287 |
| 290 | dual | towed | Geocenters | Wet Probe | 6 to 12 | 75.3 | 0.408 |
| 290 | dual | towed | Geocenters | Wet Probe | 12 to 24 | 79.5 | 0.327 |
| 290 | dual | towed | Geocenters | Wet Probe | 24 to 36 | 55.5 | 0.327 |
| 290 | dual | towed | Geocenters | Wet Probe | 36 to 48 | 52.4 | 0.374 |
| 290 | dual | towed | Geocenters | Woods | 0 to 6 | 0 | 0 |
| 290 | dual | towed | Geocenters | Woods | 6 to 12 | 0 | 0 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 290 | dual | towed | Geocenters | Woods | 12 to 24 | 0 | 0 |
| 290 | dual | towed | Geocenters | Woods | 24 to 36 | 0 | 0 |
| 290 | dual | towed | Geocenters | Woods | 36 to 48 | 0 | 0 |
| 290 | dual | towed | Geocenters | Open Field | 0 to 6 | 22.133 | 0.189 |
| 290 | dual | towed | Geocenters | Open Field | 6 to 12 | 6.833 | 0.094 |
| 290 | dual | towed | Geocenters | Open Field | 12 to 24 | 19.433 | 0.368 |
| 290 | dual | towed | Geocenters | Open Field | 24 to 36 | 26.3 | 0.356 |
| 290 | dual | towed | Geocenters | Open Field | 36 to 48 | 52.567 | 0.33 |
| 290 | dual | towed | Geocenters | Calibration | 0 to 6 | 1.2 | 0 |
| 290 | dual | towed | Geocenters | Calibration | 6 to 12 | 20.8 | 0 |
| 290 | dual | towed | Geocenters | Calibration | 12 to 24 | 28.9 | 0 |
| 290 | dual | towed | Geocenters | Calibration | 24 to 36 | 36.3 | 0 |
| 290 | dual | towed | Geocenters | Calibration | 36 to 48 | 39.2 | 0 |
| 290 | dual | towed | Geocenters | Blind Grid | 0 to 6 | 2.9 | 0.1 |
| 290 | dual | towed | Geocenters | Blind Grid | 6 to 12 | 25.15 | 0.15 |
| 290 | dual | towed | Geocenters | Blind Grid | 12 to 24 | 39.1 | 0.1 |
| 290 | dual | towed | Geocenters | Blind Grid | 24 to 36 | 34.9 | 0.1 |
| 290 | dual | towed | Geocenters | Blind Grid | 36 to 48 | 40.35 | 0.15 |
| 298 | dual | towed | Geocenters | Wet Probe | 0 to 6 | 65.367 | 0.287 |
| 298 | dual | towed | Geocenters | Wet Probe | 6 to 12 | 75.3 | 0.408 |
| 298 | dual | towed | Geocenters | Wet Probe | 12 to 24 | 79.5 | 0.327 |
| 298 | dual | towed | Geocenters | Wet Probe | 24 to 36 | 55.5 | 0.327 |
| 298 | dual | towed | Geocenters | Wet Probe | 36 to 48 | 52.4 | 0.374 |
| 298 | dual | towed | Geocenters | Woods | 0 to 6 | 0 | 0 |
| 298 | dual | towed | Geocenters | Woods | 6 to 12 | 0 | 0 |
| 298 | dual | towed | Geocenters | Woods | 12 to 24 | 0 | 0 |
| 298 | dual | towed | Geocenters | Woods | 24 to 36 | 0 | 0 |
| 298 | dual | towed | Geocenters | Woods | 36 to 48 | 0 | 0 |
| 298 | dual | towed | Geocenters | Open Field | 0 to 6 | 22.133 | 0.189 |
| 298 | dual | towed | Geocenters | Open Field | 6 to 12 | 6.833 | 0.094 |
| 298 | dual | towed | Geocenters | Open Field | 12 to 24 | 19.433 | 0.368 |
| 298 | dual | towed | Geocenters | Open Field | 24 to 36 | 26.3 | 0.356 |
| 298 | dual | towed | Geocenters | Open Field | 36 to 48 | 52.567 | 0.33 |
| 298 | dual | towed | Geocenters | Calibration | 0 to 6 | 1.2 | 0 |
| 298 | dual | towed | Geocenters | Calibration | 6 to 12 | 20.8 | 0 |
| 298 | dual | towed | Geocenters | Calibration | 12 to 24 | 28.9 | 0 |
| 298 | dual | towed | Geocenters | Calibration | 24 to 36 | 36.3 | 0 |
| 298 | dual | towed | Geocenters | Calibration | 36 to 48 | 39.2 | 0 |
| 298 | dual | towed | Geocenters | Blind Grid | 0 to 6 | 2.9 | 0.1 |
| 298 | dual | towed | Geocenters | Blind Grid | 6 to 12 | 25.15 | 0.15 |
| 298 | dual | towed | Geocenters | Blind Grid | 12 to 24 | 39.1 | 0.1 |
| 298 | dual | towed | Geocenters | Blind Grid | 24 to 36 | 34.9 | 0.1 |
| 298 | dual | towed | Geocenters | Blind Grid | 36 to 48 | 40.35 | 0.15 |
| 792 | dual | towed | Geocenters | Wet Probe | 0 to 6 | 13.45 | 0 |
| 792 | dual | towed | Geocenters | Wet Probe | 6 to 12 | 32.6 | 0 |
| 792 | dual | towed | Geocenters | Wet Probe | 12 to 24 | 30.675 | 0 |
| 792 | dual | towed | Geocenters | Wet Probe | 24 to 36 | 22.575 | 0 |
| 792 | dual | towed | Geocenters | Wet Probe | 36 to 48 | 43.6 | 0 |
| 792 | dual | towed | Geocenters | Woods | 0 to 6 | 0 | 0 |
| 792 | dual | towed | Geocenters | Woods | 6 to 12 | 0 | 0 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 792 | dual | towed | Geocenters | Woods | 12 to 24 | 0 | 0 |
| 792 | dual | towed | Geocenters | Woods | 24 to 36 | 0 | 0 |
| 792 | dual | towed | Geocenters | Woods | 36 to 48 | 0 | 0 |
| 792 | dual | towed | Geocenters | Open Field | 0 to 6 | 1.925 | 0 |
| 792 | dual | towed | Geocenters | Open Field | 6 to 12 | 11.25 | 0 |
| 792 | dual | towed | Geocenters | Open Field | 12 to 24 | 12.275 | 0 |
| 792 | dual | towed | Geocenters | Open Field | 24 to 36 | 15.7 | 0 |
| 792 | dual | towed | Geocenters | Open Field | 36 to 48 | 16.575 | 0 |
| 792 | dual | towed | Geocenters | Calibration | 0 to 6 | 3.4 | 0 |
| 792 | dual | towed | Geocenters | Calibration | 6 to 12 | 18.6 | 0 |
| 792 | dual | towed | Geocenters | Calibration | 12 to 24 | 19.4 | 0 |
| 792 | dual | towed | Geocenters | Calibration | 24 to 36 | 21.4 | 0 |
| 792 | dual | towed | Geocenters | Calibration | 36 to 48 | 18.7 | 0 |
| 792 | dual | towed | Geocenters | Blind Grid | 0 to 6 | 3.2 | 0 |
| 792 | dual | towed | Geocenters | Blind Grid | 6 to 12 | 14.3 | 0 |
| 792 | dual | towed | Geocenters | Blind Grid | 12 to 24 | 15.5 | 0 |
| 792 | dual | towed | Geocenters | Blind Grid | 24 to 36 | 12.6 | 0 |
| 792 | dual | towed | Geocenters | Blind Grid | 36 to 48 | 18.7 | 0 |
| 802 | dual | towed | Geocenters | Wet Probe | 0 to 6 | 13.45 | 0 |
| 802 | dual | towed | Geocenters | Wet Probe | 6 to 12 | 32.6 | 0 |
| 802 | dual | towed | Geocenters | Wet Probe | 12 to 24 | 30.675 | 0 |
| 802 | dual | towed | Geocenters | Wet Probe | 24 to 36 | 22.575 | 0 |
| 802 | dual | towed | Geocenters | Wet Probe | 36 to 48 | 43.6 | 0 |
| 802 | dual | towed | Geocenters | Woods | 0 to 6 | 0 | 0 |
| 802 | dual | towed | Geocenters | Woods | 6 to 12 | 0 | 0 |
| 802 | dual | towed | Geocenters | Woods | 12 to 24 | 0 | 0 |
| 802 | dual | towed | Geocenters | Woods | 24 to 36 | 0 | 0 |
| 802 | dual | towed | Geocenters | Woods | 36 to 48 | 0 | 0 |
| 802 | dual | towed | Geocenters | Open Field | 0 to 6 | 1.925 | 0 |
| 802 | dual | towed | Geocenters | Open Field | 6 to 12 | 11.25 | 0 |
| 802 | dual | towed | Geocenters | Open Field | 12 to 24 | 12.275 | 0 |
| 802 | dual | towed | Geocenters | Open Field | 24 to 36 | 15.7 | 0 |
| 802 | dual | towed | Geocenters | Open Field | 36 to 48 | 16.575 | 0 |
| 802 | dual | towed | Geocenters | Calibration | 0 to 6 | 3.4 | 0 |
| 802 | dual | towed | Geocenters | Calibration | 6 to 12 | 18.6 | 0 |
| 802 | dual | towed | Geocenters | Calibration | 12 to 24 | 19.4 | 0 |
| 802 | dual | towed | Geocenters | Calibration | 24 to 36 | 21.4 | 0 |
| 802 | dual | towed | Geocenters | Calibration | 36 to 48 | 18.7 | 0 |
| 802 | dual | towed | Geocenters | Blind Grid | 0 to 6 | 3.2 | 0 |
| 802 | dual | towed | Geocenters | Blind Grid | 6 to 12 | 14.3 | 0 |
| 802 | dual | towed | Geocenters | Blind Grid | 12 to 24 | 15.5 | 0 |
| 802 | dual | towed | Geocenters | Blind Grid | 24 to 36 | 12.6 | 0 |
| 802 | dual | towed | Geocenters | Blind Grid | 36 to 48 | 18.7 | 0 |
| 50 | EM | hand | Geophex | Wet Probe | 0 to 6 | 77.9 | 0.458 |
| 50 | EM | hand | Geophex | Wet Probe | 6 to 12 | 65.675 | 0.936 |
| 50 | EM | hand | Geophex | Wet Probe | 12 to 24 | 74.525 | 1.53 |
| 50 | EM | hand | Geophex | Wet Probe | 24 to 36 | 61.8 | 0.943 |
| 50 | EM | hand | Geophex | Wet Probe | 36 to 48 | 51.375 | 0.545 |
| 50 | EM | hand | Geophex | Woods | 0 to 6 | 84.6 | 0.3 |
| 50 | EM | hand | Geophex | Woods | 6 to 12 | 64.85 | 0.05 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 50 | EM | hand | Geophex | Woods | 12 to 24 | 63.15 | 0.25 |
| 50 | EM | hand | Geophex | Woods | 24 to 36 | 88.1 | 0.2 |
| 50 | EM | hand | Geophex | Woods | 36 to 48 | 48.5 | 0.2 |
| 50 | EM | hand | Geophex | Open Field | 0 to 6 | 15.325 | 1.295 |
| 50 | EM | hand | Geophex | Open Field | 6 to 12 | 1.125 | 0.311 |
| 50 | EM | hand | Geophex | Open Field | 12 to 24 | 22.6 | 0.412 |
| 50 | EM | hand | Geophex | Open Field | 24 to 36 | 29.65 | 0.45 |
| 50 | EM | hand | Geophex | Open Field | 36 to 48 | 42.625 | 0.444 |
| 680 | EM | hand | Geophex | Wet Probe | 0 to 6 | 0 | 0 |
| 680 | EM | hand | Geophex | Wet Probe | 6 to 12 | 0 | 0 |
| 680 | EM | hand | Geophex | Wet Probe | 12 to 24 | 0 | 0 |
| 680 | EM | hand | Geophex | Wet Probe | 24 to 36 | 0 | 0 |
| 680 | EM | hand | Geophex | Wet Probe | 36 to 48 | 0 | 0 |
| 680 | EM | hand | Geophex | Woods | 0 to 6 | 0 | 0 |
| 680 | EM | hand | Geophex | Woods | 6 to 12 | 0 | 0 |
| 680 | EM | hand | Geophex | Woods | 12 to 24 | 0 | 0 |
| 680 | EM | hand | Geophex | Woods | 24 to 36 | 0 | 0 |
| 680 | EM | hand | Geophex | Woods | 36 to 48 | 0 | 0 |
| 680 | EM | hand | Geophex | Open Field | 0 to 6 | 0 | 0 |
| 680 | EM | hand | Geophex | Open Field | 6 to 12 | 0 | 0 |
| 680 | EM | hand | Geophex | Open Field | 12 to 24 | 0 | 0 |
| 680 | EM | hand | Geophex | Open Field | 24 to 36 | 0 | 0 |
| 680 | EM | hand | Geophex | Open Field | 36 to 48 | 0 | 0 |
| 680 | EM | hand | Geophex | Calibration | 0 to 6 | 5 | 0.305 |
| 680 | EM | hand | Geophex | Calibration | 6 to 12 | 36.536 | 0.199 |
| 680 | EM | hand | Geophex | Calibration | 12 to 24 | 49.929 | 0.228 |
| 680 | EM | hand | Geophex | Calibration | 24 to 36 | 43.457 | 0.425 |
| 680 | EM | hand | Geophex | Calibration | 36 to 48 | 38.286 | 0.307 |
| 680 | EM | hand | Geophex | Blind Grid | 0 to 6 | 2.707 | 0.296 |
| 680 | EM | hand | Geophex | Blind Grid | 6 to 12 | 22.986 | 0.346 |
| 680 | EM | hand | Geophex | Blind Grid | 12 to 24 | 36.436 | 0.381 |
| 680 | EM | hand | Geophex | Blind Grid | 24 to 36 | 33.714 | 0.493 |
| 680 | EM | hand | Geophex | Blind Grid | 36 to 48 | 38.043 | 0.344 |
| 125 | EM | towed | Geophex | Wet Probe | 0 to 6 | 77.661 | 4.526 |
| 125 | EM | towed | Geophex | Wet Probe | 6 to 12 | 67.856 | 3.49 |
| 125 | EM | towed | Geophex | Wet Probe | 12 to 24 | 74.606 | 1.141 |
| 125 | EM | towed | Geophex | Wet Probe | 24 to 36 | 61.8 | 1.197 |
| 125 | EM | towed | Geophex | Wet Probe | 36 to 48 | 49.561 | 4.433 |
| 125 | EM | towed | Geophex | Woods | 0 to 6 | 76.979 | 7.626 |
| 125 | EM | towed | Geophex | Woods | 6 to 12 | 66.536 | 3.353 |
| 125 | EM | towed | Geophex | Woods | 12 to 24 | 78.307 | 13.289 |
| 125 | EM | towed | Geophex | Woods | 24 to 36 | 73.057 | 12.473 |
| 125 | EM | towed | Geophex | Woods | 36 to 48 | 49.936 | 1.25 |
| 125 | EM | towed | Geophex | Open Field | 0 to 6 | 10.694 | 3.779 |
| 125 | EM | towed | Geophex | Open Field | 6 to 12 | 0.665 | 0.407 |
| 125 | EM | towed | Geophex | Open Field | 12 to 24 | 19.994 | 1.682 |
| 125 | EM | towed | Geophex | Open Field | 24 to 36 | 27.376 | 1.736 |
| 125 | EM | towed | Geophex | Open Field | 36 to 48 | 40.159 | 1.83 |
| 49 | EM | cart | Geophex | Wet Probe | 0 to 6 | 77.9 | 0.458 |
| 49 | EM | cart | Geophex | Wet Probe | 6 to 12 | 65.675 | 0.936 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 49 | EM | cart | Geophex | Wet Probe | 12 to 24 | 74.525 | 1.53 |
| 49 | EM | cart | Geophex | Wet Probe | 24 to 36 | 61.8 | 0.943 |
| 49 | EM | cart | Geophex | Wet Probe | 36 to 48 | 51.375 | 0.545 |
| 49 | EM | cart | Geophex | Woods | 0 to 6 | 84.6 | 0.3 |
| 49 | EM | cart | Geophex | Woods | 6 to 12 | 64.85 | 0.05 |
| 49 | EM | cart | Geophex | Woods | 12 to 24 | 63.15 | 0.25 |
| 49 | EM | cart | Geophex | Woods | 24 to 36 | 88.1 | 0.2 |
| 49 | EM | cart | Geophex | Woods | 36 to 48 | 48.5 | 0.2 |
| 49 | EM | cart | Geophex | Open Field | 0 to 6 | 15.325 | 1.295 |
| 49 | EM | cart | Geophex | Open Field | 6 to 12 | 1.125 | 0.311 |
| 49 | EM | cart | Geophex | Open Field | 12 to 24 | 22.6 | 0.412 |
| 49 | EM | cart | Geophex | Open Field | 24 to 36 | 29.65 | 0.45 |
| 49 | EM | cart | Geophex | Open Field | 36 to 48 | 42.625 | 0.444 |
| 451 | EM | cart | Geophex | Wet Probe | 0 to 6 | 76.2 | 7.063 |
| 451 | EM | cart | Geophex | Wet Probe | 6 to 12 | 68.1 | 0.566 |
| 451 | EM | cart | Geophex | Wet Probe | 12 to 24 | 75.567 | 0.17 |
| 451 | EM | cart | Geophex | Wet Probe | 24 to 36 | 63.3 | 0.283 |
| 451 | EM | cart | Geophex | Wet Probe | 36 to 48 | 51.967 | 0.125 |
| 451 | EM | cart | Geophex | Woods | 0 to 6 | 21.333 | 0.85 |
| 451 | EM | cart | Geophex | Woods | 6 to 12 | 21.933 | 1.621 |
| 451 | EM | cart | Geophex | Woods | 12 to 24 | 27.533 | 0.419 |
| 451 | EM | cart | Geophex | Woods | 24 to 36 | 4.2 | 0 |
| 451 | EM | cart | Geophex | Woods | 36 to 48 | 25.767 | 0.205 |
| 451 | EM | cart | Geophex | Open Field | 0 to 6 | 43.517 | 27.513 |
| 451 | EM | cart | Geophex | Open Field | 6 to 12 | 44.367 | 42.298 |
| 451 | EM | cart | Geophex | Open Field | 12 to 24 | 36.133 | 26.382 |
| 451 | EM | cart | Geophex | Open Field | 24 to 36 | 39.067 | 19.048 |
| 451 | EM | cart | Geophex | Open Field | 36 to 48 | 40.083 | 20.226 |
| 665 | EM | hand | Geophex | Wet Probe | 0 to 6 | 0 | 0 |
| 665 | EM | hand | Geophex | Wet Probe | 6 to 12 | 0 | 0 |
| 665 | EM | hand | Geophex | Wet Probe | 12 to 24 | 0 | 0 |
| 665 | EM | hand | Geophex | Wet Probe | 24 to 36 | 0 | 0 |
| 665 | EM | hand | Geophex | Wet Probe | 36 to 48 | 0 | 0 |
| 665 | EM | hand | Geophex | Woods | 0 to 6 | 0 | 0 |
| 665 | EM | hand | Geophex | Woods | 6 to 12 | 0 | 0 |
| 665 | EM | hand | Geophex | Woods | 12 to 24 | 0 | 0 |
| 665 | EM | hand | Geophex | Woods | 24 to 36 | 0 | 0 |
| 665 | EM | hand | Geophex | Woods | 36 to 48 | 0 | 0 |
| 665 | EM | hand | Geophex | Open Field | 0 to 6 | 0 | 0 |
| 665 | EM | hand | Geophex | Open Field | 6 to 12 | 0 | 0 |
| 665 | EM | hand | Geophex | Open Field | 12 to 24 | 0 | 0 |
| 665 | EM | hand | Geophex | Open Field | 24 to 36 | 0 | 0 |
| 665 | EM | hand | Geophex | Open Field | 36 to 48 | 0 | 0 |
| 665 | EM | hand | Geophex | Calibration | 0 to 6 | 5 | 0.305 |
| 665 | EM | hand | Geophex | Calibration | 6 to 12 | 36.536 | 0.199 |
| 665 | EM | hand | Geophex | Calibration | 12 to 24 | 49.929 | 0.228 |
| 665 | EM | hand | Geophex | Calibration | 24 to 36 | 43.457 | 0.425 |
| 665 | EM | hand | Geophex | Calibration | 36 to 48 | 38.286 | 0.307 |
| 665 | EM | hand | Geophex | Blind Grid | 0 to 6 | 2.707 | 0.296 |
| 665 | EM | hand | Geophex | Blind Grid | 6 to 12 | 22.986 | 0.346 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 665 | EM | hand | Geophex | Blind Grid | 12 to 24 | 36.436 | 0.381 |
| 665 | EM | hand | Geophex | Blind Grid | 24 to 36 | 33.714 | 0.493 |
| 665 | EM | hand | Geophex | Blind Grid | 36 to 48 | 38.043 | 0.344 |
| 129 | EM | towed | Geophex | Wet Probe | 0 to 6 | 77.661 | 4.526 |
| 129 | EM | towed | Geophex | Wet Probe | 6 to 12 | 67.856 | 3.49 |
| 129 | EM | towed | Geophex | Wet Probe | 12 to 24 | 74.606 | 1.141 |
| 129 | EM | towed | Geophex | Wet Probe | 24 to 36 | 61.8 | 1.197 |
| 129 | EM | towed | Geophex | Wet Probe | 36 to 48 | 49.561 | 4.433 |
| 129 | EM | towed | Geophex | Woods | 0 to 6 | 76.979 | 7.626 |
| 129 | EM | towed | Geophex | Woods | 6 to 12 | 66.536 | 3.353 |
| 129 | EM | towed | Geophex | Woods | 12 to 24 | 78.307 | 13.289 |
| 129 | EM | towed | Geophex | Woods | 24 to 36 | 73.057 | 12.473 |
| 129 | EM | towed | Geophex | Woods | 36 to 48 | 49.936 | 1.25 |
| 129 | EM | towed | Geophex | Open Field | 0 to 6 | 10.694 | 3.779 |
| 129 | EM | towed | Geophex | Open Field | 6 to 12 | 0.665 | 0.407 |
| 129 | EM | towed | Geophex | Open Field | 12 to 24 | 19.994 | 1.682 |
| 129 | EM | towed | Geophex | Open Field | 24 to 36 | 27.376 | 1.736 |
| 129 | EM | towed | Geophex | Open Field | 36 to 48 | 40.053 | 1.922 |
| 449 | EM | cart | Geophex | Wet Probe | 0 to 6 | 77.661 | 4.526 |
| 449 | EM | cart | Geophex | Wet Probe | 6 to 12 | 67.856 | 3.49 |
| 449 | EM | cart | Geophex | Wet Probe | 12 to 24 | 74.606 | 1.141 |
| 449 | EM | cart | Geophex | Wet Probe | 24 to 36 | 61.8 | 1.197 |
| 449 | EM | cart | Geophex | Wet Probe | 36 to 48 | 49.561 | 4.433 |
| 449 | EM | cart | Geophex | Woods | 0 to 6 | 76.979 | 7.626 |
| 449 | EM | cart | Geophex | Woods | 6 to 12 | 66.536 | 3.353 |
| 449 | EM | cart | Geophex | Woods | 12 to 24 | 78.307 | 13.289 |
| 449 | EM | cart | Geophex | Woods | 24 to 36 | 73.057 | 12.473 |
| 449 | EM | cart | Geophex | Woods | 36 to 48 | 49.936 | 1.25 |
| 449 | EM | cart | Geophex | Open Field | 0 to 6 | 10.694 | 3.779 |
| 449 | EM | cart | Geophex | Open Field | 6 to 12 | 0.665 | 0.407 |
| 449 | EM | cart | Geophex | Open Field | 12 to 24 | 19.994 | 1.682 |
| 449 | EM | cart | Geophex | Open Field | 24 to 36 | 27.376 | 1.736 |
| 449 | EM | cart | Geophex | Open Field | 36 to 48 | 40.159 | 1.83 |
| 694 | EM | cart | Geophex | Wet Probe | 0 to 6 | 0 | 0 |
| 694 | EM | cart | Geophex | Wet Probe | 6 to 12 | 0 | 0 |
| 694 | EM | cart | Geophex | Wet Probe | 12 to 24 | 0 | 0 |
| 694 | EM | cart | Geophex | Wet Probe | 24 to 36 | 0 | 0 |
| 694 | EM | cart | Geophex | Wet Probe | 36 to 48 | 0 | 0 |
| 694 | EM | cart | Geophex | Woods | 0 to 6 | 0 | 0 |
| 694 | EM | cart | Geophex | Woods | 6 to 12 | 0 | 0 |
| 694 | EM | cart | Geophex | Woods | 12 to 24 | 0 | 0 |
| 694 | EM | cart | Geophex | Woods | 24 to 36 | 0 | 0 |
| 694 | EM | cart | Geophex | Woods | 36 to 48 | 0 | 0 |
| 694 | EM | cart | Geophex | Open Field | 0 to 6 | 0 | 0 |
| 694 | EM | cart | Geophex | Open Field | 6 to 12 | 0 | 0 |
| 694 | EM | cart | Geophex | Open Field | 12 to 24 | 0 | 0 |
| 694 | EM | cart | Geophex | Open Field | 24 to 36 | 0 | 0 |
| 694 | EM | cart | Geophex | Open Field | 36 to 48 | 0 | 0 |
| 694 | EM | cart | Geophex | Calibration | 0 to 6 | 5.125 | 0.323 |
| 694 | EM | cart | Geophex | Calibration | 6 to 12 | 36.525 | 0.233 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 694 | EM | cart | Geophex | Calibration | 12 to 24 | 49.963 | 0.245 |
| 694 | EM | cart | Geophex | Calibration | 24 to 36 | 43.588 | 0.457 |
| 694 | EM | cart | Geophex | Calibration | 36 to 48 | 38.425 | 0.338 |
| 694 | EM | cart | Geophex | Blind Grid | 0 to 6 | 2.812 | 0.344 |
| 694 | EM | cart | Geophex | Blind Grid | 6 to 12 | 23.125 | 0.367 |
| 694 | EM | cart | Geophex | Blind Grid | 12 to 24 | 36.625 | 0.402 |
| 694 | EM | cart | Geophex | Blind Grid | 24 to 36 | 33.95 | 0.48 |
| 694 | EM | cart | Geophex | Blind Grid | 36 to 48 | 38.137 | 0.409 |
| 739 | EM | towed | Geophex | Wet Probe | 0 to 6 | 4.317 | 1.025 |
| 739 | EM | towed | Geophex | Wet Probe | 6 to 12 | 7.708 | 1.787 |
| 739 | EM | towed | Geophex | Wet Probe | 12 to 24 | 14.808 | 3.109 |
| 739 | EM | towed | Geophex | Wet Probe | 24 to 36 | 4.242 | 1.096 |
| 739 | EM | towed | Geophex | Wet Probe | 36 to 48 | 4.367 | 1.091 |
| 739 | EM | towed | Geophex | Woods | 0 to 6 | 0 | 0 |
| 739 | EM | towed | Geophex | Woods | 6 to 12 | 0 | 0 |
| 739 | EM | towed | Geophex | Woods | 12 to 24 | 0 | 0 |
| 739 | EM | towed | Geophex | Woods | 24 to 36 | 0 | 0 |
| 739 | EM | towed | Geophex | Woods | 36 to 48 | 0 | 0 |
| 739 | EM | towed | Geophex | Open Field | 0 to 6 | 5.092 | 1.107 |
| 739 | EM | towed | Geophex | Open Field | 6 to 12 | 5.975 | 1.461 |
| 739 | EM | towed | Geophex | Open Field | 12 to 24 | 3.792 | 0.866 |
| 739 | EM | towed | Geophex | Open Field | 24 to 36 | 11.767 | 2.491 |
| 739 | EM | towed | Geophex | Open Field | 36 to 48 | 20.9 | 4.365 |
| 739 | EM | towed | Geophex | Calibration | 0 to 6 | 0.35 | 0.05 |
| 739 | EM | towed | Geophex | Calibration | 6 to 12 | 14.05 | 0.112 |
| 739 | EM | towed | Geophex | Calibration | 12 to 24 | 21.625 | 0.349 |
| 739 | EM | towed | Geophex | Calibration | 24 to 36 | 26.275 | 0.164 |
| 739 | EM | towed | Geophex | Calibration | 36 to 48 | 27.15 | 0.087 |
| 739 | EM | towed | Geophex | Blind Grid | 0 to 6 | 1.95 | 0.05 |
| 739 | EM | towed | Geophex | Blind Grid | 6 to 12 | 4.075 | 0.083 |
| 739 | EM | towed | Geophex | Blind Grid | 12 to 24 | 22.25 | 0.112 |
| 739 | EM | towed | Geophex | Blind Grid | 24 to 36 | 2.925 | 0.13 |
| 739 | EM | towed | Geophex | Blind Grid | 36 to 48 | 2.275 | 0.083 |
| 693 | EM | cart | Geophex | Wet Probe | 0 to 6 | 0 | 0 |
| 693 | EM | cart | Geophex | Wet Probe | 6 to 12 | 0 | 0 |
| 693 | EM | cart | Geophex | Wet Probe | 12 to 24 | 0 | 0 |
| 693 | EM | cart | Geophex | Wet Probe | 24 to 36 | 0 | 0 |
| 693 | EM | cart | Geophex | Wet Probe | 36 to 48 | 0 | 0 |
| 693 | EM | cart | Geophex | Woods | 0 to 6 | 0 | 0 |
| 693 | EM | cart | Geophex | Woods | 6 to 12 | 0 | 0 |
| 693 | EM | cart | Geophex | Woods | 12 to 24 | 0 | 0 |
| 693 | EM | cart | Geophex | Woods | 24 to 36 | 0 | 0 |
| 693 | EM | cart | Geophex | Woods | 36 to 48 | 0 | 0 |
| 693 | EM | cart | Geophex | Open Field | 0 to 6 | 0 | 0 |
| 693 | EM | cart | Geophex | Open Field | 6 to 12 | 0 | 0 |
| 693 | EM | cart | Geophex | Open Field | 12 to 24 | 0 | 0 |
| 693 | EM | cart | Geophex | Open Field | 24 to 36 | 0 | 0 |
| 693 | EM | cart | Geophex | Open Field | 36 to 48 | 0 | 0 |
| 693 | EM | cart | Geophex | Calibration | 0 to 6 | 5.125 | 0.323 |
| 693 | EM | cart | Geophex | Calibration | 6 to 12 | 36.525 | 0.233 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 693 | EM | cart | Geophex | Calibration | 12 to 24 | 49.963 | 0.245 |
| 693 | EM | cart | Geophex | Calibration | 24 to 36 | 43.588 | 0.457 |
| 693 | EM | cart | Geophex | Calibration | 36 to 48 | 38.425 | 0.338 |
| 693 | EM | cart | Geophex | Blind Grid | 0 to 6 | 2.812 | 0.344 |
| 693 | EM | cart | Geophex | Blind Grid | 6 to 12 | 23.125 | 0.367 |
| 693 | EM | cart | Geophex | Blind Grid | 12 to 24 | 36.625 | 0.402 |
| 693 | EM | cart | Geophex | Blind Grid | 24 to 36 | 33.95 | 0.48 |
| 693 | EM | cart | Geophex | Blind Grid | 36 to 48 | 38.137 | 0.409 |
| 740 | EM | towed | Geophex | Wet Probe | 0 to 6 | 4.317 | 1.025 |
| 740 | EM | towed | Geophex | Wet Probe | 6 to 12 | 7.708 | 1.787 |
| 740 | EM | towed | Geophex | Wet Probe | 12 to 24 | 14.808 | 3.109 |
| 740 | EM | towed | Geophex | Wet Probe | 24 to 36 | 4.242 | 1.096 |
| 740 | EM | towed | Geophex | Wet Probe | 36 to 48 | 4.367 | 1.091 |
| 740 | EM | towed | Geophex | Woods | 0 to 6 | 0 | 0 |
| 740 | EM | towed | Geophex | Woods | 6 to 12 | 0 | 0 |
| 740 | EM | towed | Geophex | Woods | 12 to 24 | 0 | 0 |
| 740 | EM | towed | Geophex | Woods | 24 to 36 | 0 | 0 |
| 740 | EM | towed | Geophex | Woods | 36 to 48 | 0 | 0 |
| 740 | EM | towed | Geophex | Open Field | 0 to 6 | 5.092 | 1.107 |
| 740 | EM | towed | Geophex | Open Field | 6 to 12 | 5.975 | 1.461 |
| 740 | EM | towed | Geophex | Open Field | 12 to 24 | 3.792 | 0.866 |
| 740 | EM | towed | Geophex | Open Field | 24 to 36 | 11.767 | 2.491 |
| 740 | EM | towed | Geophex | Open Field | 36 to 48 | 20.9 | 4.365 |
| 740 | EM | towed | Geophex | Calibration | 0 to 6 | 0.35 | 0.05 |
| 740 | EM | towed | Geophex | Calibration | 6 to 12 | 14.05 | 0.112 |
| 740 | EM | towed | Geophex | Calibration | 12 to 24 | 21.625 | 0.349 |
| 740 | EM | towed | Geophex | Calibration | 24 to 36 | 26.275 | 0.164 |
| 740 | EM | towed | Geophex | Calibration | 36 to 48 | 27.15 | 0.087 |
| 740 | EM | towed | Geophex | Blind Grid | 0 to 6 | 1.95 | 0.05 |
| 740 | EM | towed | Geophex | Blind Grid | 6 to 12 | 4.075 | 0.083 |
| 740 | EM | towed | Geophex | Blind Grid | 12 to 24 | 22.25 | 0.112 |
| 740 | EM | towed | Geophex | Blind Grid | 24 to 36 | 2.925 | 0.13 |
| 740 | EM | towed | Geophex | Blind Grid | 36 to 48 | 2.275 | 0.083 |
| 184 | EM | hand | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 184 | EM | hand | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 184 | EM | hand | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 184 | EM | hand | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 184 | EM | hand | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 184 | EM | hand | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 184 | EM | hand | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 184 | EM | hand | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 184 | EM | hand | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 184 | EM | hand | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 184 | EM | hand | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 184 | EM | hand | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 184 | EM | hand | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 184 | EM | hand | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 184 | EM | hand | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 184 | EM | hand | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 184 | EM | hand | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 184 | EM | hand | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 184 | EM | hand | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 184 | EM | hand | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 184 | EM | hand | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 184 | EM | hand | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 184 | EM | hand | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 184 | EM | hand | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 184 | EM | hand | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 183 | EM | sling | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 183 | EM | sling | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 183 | EM | sling | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 183 | EM | sling | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 183 | EM | sling | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 183 | EM | sling | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 183 | EM | sling | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 183 | EM | sling | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 183 | EM | sling | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 183 | EM | sling | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 183 | EM | sling | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 183 | EM | sling | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 183 | EM | sling | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 183 | EM | sling | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 183 | EM | sling | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 183 | EM | sling | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 183 | EM | sling | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |
| 183 | EM | sling | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 183 | EM | sling | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 183 | EM | sling | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 183 | EM | sling | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 183 | EM | sling | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 183 | EM | sling | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 183 | EM | sling | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 183 | EM | sling | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 545 | EM | sling | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 545 | EM | sling | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 545 | EM | sling | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 545 | EM | sling | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 545 | EM | sling | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 545 | EM | sling | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 545 | EM | sling | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 545 | EM | sling | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 545 | EM | sling | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 545 | EM | sling | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 545 | EM | sling | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 545 | EM | sling | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 545 | EM | sling | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 545 | EM | sling | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 545 | EM | sling | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 545 | EM | sling | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 545 | EM | sling | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 545 | EM | sling | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 545 | EM | sling | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 545 | EM | sling | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 545 | EM | sling | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 545 | EM | sling | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 545 | EM | sling | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 545 | EM | sling | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 545 | EM | sling | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 154 | EM | sling | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 154 | EM | sling | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 154 | EM | sling | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 154 | EM | sling | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 154 | EM | sling | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 154 | EM | sling | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 154 | EM | sling | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 154 | EM | sling | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 154 | EM | sling | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 154 | EM | sling | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 154 | EM | sling | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 154 | EM | sling | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 154 | EM | sling | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 154 | EM | sling | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 154 | EM | sling | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 154 | EM | sling | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 154 | EM | sling | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |
| 154 | EM | sling | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 154 | EM | sling | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 154 | EM | sling | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 154 | EM | sling | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 154 | EM | sling | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 154 | EM | sling | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 154 | EM | sling | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 154 | EM | sling | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 452 | EM | hand | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 452 | EM | hand | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 452 | EM | hand | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 452 | EM | hand | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 452 | EM | hand | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 452 | EM | hand | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 452 | EM | hand | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 452 | EM | hand | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 452 | EM | hand | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 452 | EM | hand | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 452 | EM | hand | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 452 | EM | hand | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 452 | EM | hand | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 452 | EM | hand | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 452 | EM | hand | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 452 | EM | hand | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 452 | EM | hand | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 452 | EM | hand | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 452 | EM | hand | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 452 | EM | hand | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 452 | EM | hand | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 452 | EM | hand | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 452 | EM | hand | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 452 | EM | hand | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 452 | EM | hand | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 268 | MAG | sling | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 268 | MAG | sling | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 268 | MAG | sling | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 268 | MAG | sling | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 268 | MAG | sling | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 268 | MAG | sling | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 268 | MAG | sling | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 268 | MAG | sling | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 268 | MAG | sling | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 268 | MAG | sling | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 268 | MAG | sling | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 268 | MAG | sling | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 268 | MAG | sling | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 268 | MAG | sling | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 268 | MAG | sling | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 268 | MAG | sling | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 268 | MAG | sling | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |
| 268 | MAG | sling | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 268 | MAG | sling | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 268 | MAG | sling | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 268 | MAG | sling | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 268 | MAG | sling | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 268 | MAG | sling | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 268 | MAG | sling | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 268 | MAG | sling | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 547 | MAG | sling | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 547 | MAG | sling | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 547 | MAG | sling | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 547 | MAG | sling | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 547 | MAG | sling | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 547 | MAG | sling | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 547 | MAG | sling | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 547 | MAG | sling | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 547 | MAG | sling | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 547 | MAG | sling | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 547 | MAG | sling | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 547 | MAG | sling | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 547 | MAG | sling | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 547 | MAG | sling | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 547 | MAG | sling | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 547 | MAG | sling | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 547 | MAG | sling | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 547 | MAG | sling | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 547 | MAG | sling | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 547 | MAG | sling | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 547 | MAG | sling | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 547 | MAG | sling | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 547 | MAG | sling | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 547 | MAG | sling | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 547 | MAG | sling | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 311 | MAG | sling | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 311 | MAG | sling | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 311 | MAG | sling | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 311 | MAG | sling | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 311 | MAG | sling | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 311 | MAG | sling | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 311 | MAG | sling | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 311 | MAG | sling | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 311 | MAG | sling | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 311 | MAG | sling | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 311 | MAG | sling | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 311 | MAG | sling | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 311 | MAG | sling | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 311 | MAG | sling | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 311 | MAG | sling | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 311 | MAG | sling | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 311 | MAG | sling | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |
| 311 | MAG | sling | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 311 | MAG | sling | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 311 | MAG | sling | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 311 | MAG | sling | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 311 | MAG | sling | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 311 | MAG | sling | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 311 | MAG | sling | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 311 | MAG | sling | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 454 | MAG | sling | G-TEK | Wet Probe | 0 to 6 | 70.858 | 6.235 |
| 454 | MAG | sling | G-TEK | Wet Probe | 6 to 12 | 73.775 | 1.371 |
| 454 | MAG | sling | G-TEK | Wet Probe | 12 to 24 | 71.592 | 2.525 |
| 454 | MAG | sling | G-TEK | Wet Probe | 24 to 36 | 53.083 | 0.906 |
| 454 | MAG | sling | G-TEK | Wet Probe | 36 to 48 | 49.192 | 0.671 |
| 454 | MAG | sling | G-TEK | Woods | 0 to 6 | 12.033 | 0.149 |
| 454 | MAG | sling | G-TEK | Woods | 6 to 12 | 6 | 0.516 |
| 454 | MAG | sling | G-TEK | Woods | 12 to 24 | 4.583 | 0.227 |
| 454 | MAG | sling | G-TEK | Woods | 24 to 36 | 52.1 | 0.424 |
| 454 | MAG | sling | G-TEK | Woods | 36 to 48 | 54.483 | 0.414 |
| 454 | MAG | sling | G-TEK | Open Field | 0 to 6 | 15.9 | 3.209 |
| 454 | MAG | sling | G-TEK | Open Field | 6 to 12 | 1.908 | 2.029 |
| 454 | MAG | sling | G-TEK | Open Field | 12 to 24 | 17.1 | 1.922 |
| 454 | MAG | sling | G-TEK | Open Field | 24 to 36 | 22.3 | 1.888 |
| 454 | MAG | sling | G-TEK | Open Field | 36 to 48 | 31.8 | 8.579 |
| 454 | MAG | sling | G-TEK | Calibration | 0 to 6 | 39.35 | 0.15 |
| 454 | MAG | sling | G-TEK | Calibration | 6 to 12 | 36.95 | 0.75 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 454 | MAG | sling | G-TEK | Calibration | 12 to 24 | 0.65 | 0.15 |
| 454 | MAG | sling | G-TEK | Calibration | 24 to 36 | 4.3 | 0.2 |
| 454 | MAG | sling | G-TEK | Calibration | 36 to 48 | 4.2 | 0.4 |
| 454 | MAG | sling | G-TEK | Blind Grid | 0 to 6 | 4.071 | 0.587 |
| 454 | MAG | sling | G-TEK | Blind Grid | 6 to 12 | 11.514 | 4.854 |
| 454 | MAG | sling | G-TEK | Blind Grid | 12 to 24 | 35.071 | 0.641 |
| 454 | MAG | sling | G-TEK | Blind Grid | 24 to 36 | 36.3 | 0.293 |
| 454 | MAG | sling | G-TEK | Blind Grid | 36 to 48 | 38.314 | 0.36 |
| 281 | dual | sling | G-TEK | Wet Probe | 0 to 6 | 58.99 | 2.85 |
| 281 | dual | sling | G-TEK | Wet Probe | 6 to 12 | 74.65 | 4.932 |
| 281 | dual | sling | G-TEK | Wet Probe | 12 to 24 | 76.88 | 0.807 |
| 281 | dual | sling | G-TEK | Wet Probe | 24 to 36 | 58.6 | 6.273 |
| 281 | dual | sling | G-TEK | Wet Probe | 36 to 48 | 51.06 | 1.589 |
| 281 | dual | sling | G-TEK | Woods | 0 to 6 | 15.233 | 0.125 |
| 281 | dual | sling | G-TEK | Woods | 6 to 12 | 6.233 | 0.249 |
| 281 | dual | sling | G-TEK | Woods | 12 to 24 | 4.817 | 0.241 |
| 281 | dual | sling | G-TEK | Woods | 24 to 36 | 52.933 | 0.461 |
| 281 | dual | sling | G-TEK | Woods | 36 to 48 | 55.35 | 0.594 |
| 281 | dual | sling | G-TEK | Open Field | 0 to 6 | 21.29 | 0.277 |
| 281 | dual | sling | G-TEK | Open Field | 6 to 12 | 5.97 | 0.287 |
| 281 | dual | sling | G-TEK | Open Field | 12 to 24 | 19.35 | 0.766 |
| 281 | dual | sling | G-TEK | Open Field | 24 to 36 | 27.98 | 0.584 |
| 281 | dual | sling | G-TEK | Open Field | 36 to 48 | 52.59 | 0.375 |
| 281 | dual | sling | G-TEK | Calibration | 0 to 6 | 39.1 | 0.1 |
| 281 | dual | sling | G-TEK | Calibration | 6 to 12 | 37.75 | 0.25 |
| 281 | dual | sling | G-TEK | Calibration | 12 to 24 | 1.55 | 0.05 |
| 281 | dual | sling | G-TEK | Calibration | 24 to 36 | 4.15 | 0.05 |
| 281 | dual | sling | G-TEK | Calibration | 36 to 48 | 5.4 | 0.1 |
| 281 | dual | sling | G-TEK | Blind Grid | 0 to 6 | 3.283 | 0.203 |
| 281 | dual | sling | G-TEK | Blind Grid | 6 to 12 | 23.75 | 0.275 |
| 281 | dual | sling | G-TEK | Blind Grid | 12 to 24 | 37.65 | 0.754 |
| 281 | dual | sling | G-TEK | Blind Grid | 24 to 36 | 35.983 | 0.811 |
| 281 | dual | sling | G-TEK | Blind Grid | 36 to 48 | 38.317 | 0.241 |
| 380 | dual | sling | G-TEK | Wet Probe | 0 to 6 | 58.99 | 2.85 |
| 380 | dual | sling | G-TEK | Wet Probe | 6 to 12 | 74.65 | 4.932 |
| 380 | dual | sling | G-TEK | Wet Probe | 12 to 24 | 76.88 | 0.807 |
| 380 | dual | sling | G-TEK | Wet Probe | 24 to 36 | 58.6 | 6.273 |
| 380 | dual | sling | G-TEK | Wet Probe | 36 to 48 | 51.06 | 1.589 |
| 380 | dual | sling | G-TEK | Woods | 0 to 6 | 15.233 | 0.125 |
| 380 | dual | sling | G-TEK | Woods | 6 to 12 | 6.233 | 0.249 |
| 380 | dual | sling | G-TEK | Woods | 12 to 24 | 4.817 | 0.241 |
| 380 | dual | sling | G-TEK | Woods | 24 to 36 | 52.933 | 0.461 |
| 380 | dual | sling | G-TEK | Woods | 36 to 48 | 55.35 | 0.594 |
| 380 | dual | sling | G-TEK | Open Field | 0 to 6 | 21.29 | 0.277 |
| 380 | dual | sling | G-TEK | Open Field | 6 to 12 | 5.97 | 0.287 |
| 380 | dual | sling | G-TEK | Open Field | 12 to 24 | 19.35 | 0.766 |
| 380 | dual | sling | G-TEK | Open Field | 24 to 36 | 27.98 | 0.584 |
| 380 | dual | sling | G-TEK | Open Field | 36 to 48 | 52.59 | 0.375 |
| 380 | dual | sling | G-TEK | Calibration | 0 to 6 | 39.1 | 0.1 |
| 380 | dual | sling | G-TEK | Calibration | 6 to 12 | 37.75 | 0.25 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 380 | dual | sling | G-TEK | Calibration | 12 to 24 | 1.55 | 0.05 |
| 380 | dual | sling | G-TEK | Calibration | 24 to 36 | 4.15 | 0.05 |
| 380 | dual | sling | G-TEK | Calibration | 36 to 48 | 5.4 | 0.1 |
| 380 | dual | sling | G-TEK | Blind Grid | 0 to 6 | 3.283 | 0.203 |
| 380 | dual | sling | G-TEK | Blind Grid | 6 to 12 | 23.75 | 0.275 |
| 380 | dual | sling | G-TEK | Blind Grid | 12 to 24 | 37.65 | 0.754 |
| 380 | dual | sling | G-TEK | Blind Grid | 24 to 36 | 35.983 | 0.811 |
| 380 | dual | sling | G-TEK | Blind Grid | 36 to 48 | 38.317 | 0.241 |
| 379 | dual | sling | G-TEK | Wet Probe | 0 to 6 | 58.99 | 2.85 |
| 379 | dual | sling | G-TEK | Wet Probe | 6 to 12 | 74.65 | 4.932 |
| 379 | dual | sling | G-TEK | Wet Probe | 12 to 24 | 76.88 | 0.807 |
| 379 | dual | sling | G-TEK | Wet Probe | 24 to 36 | 58.6 | 6.273 |
| 379 | dual | sling | G-TEK | Wet Probe | 36 to 48 | 51.06 | 1.589 |
| 379 | dual | sling | G-TEK | Woods | 0 to 6 | 15.233 | 0.125 |
| 379 | dual | sling | G-TEK | Woods | 6 to 12 | 6.233 | 0.249 |
| 379 | dual | sling | G-TEK | Woods | 12 to 24 | 4.817 | 0.241 |
| 379 | dual | sling | G-TEK | Woods | 24 to 36 | 52.933 | 0.461 |
| 379 | dual | sling | G-TEK | Woods | 36 to 48 | 55.35 | 0.594 |
| 379 | dual | sling | G-TEK | Open Field | 0 to 6 | 21.29 | 0.277 |
| 379 | dual | sling | G-TEK | Open Field | 6 to 12 | 5.97 | 0.287 |
| 379 | dual | sling | G-TEK | Open Field | 12 to 24 | 19.35 | 0.766 |
| 379 | dual | sling | G-TEK | Open Field | 24 to 36 | 27.98 | 0.584 |
| 379 | dual | sling | G-TEK | Open Field | 36 to 48 | 52.59 | 0.375 |
| 379 | dual | sling | G-TEK | Calibration | 0 to 6 | 39.1 | 0.1 |
| 379 | dual | sling | G-TEK | Calibration | 6 to 12 | 37.75 | 0.25 |
| 379 | dual | sling | G-TEK | Calibration | 12 to 24 | 1.55 | 0.05 |
| 379 | dual | sling | G-TEK | Calibration | 24 to 36 | 4.15 | 0.05 |
| 379 | dual | sling | G-TEK | Calibration | 36 to 48 | 5.4 | 0.1 |
| 379 | dual | sling | G-TEK | Blind Grid | 0 to 6 | 3.283 | 0.203 |
| 379 | dual | sling | G-TEK | Blind Grid | 6 to 12 | 23.75 | 0.275 |
| 379 | dual | sling | G-TEK | Blind Grid | 12 to 24 | 37.65 | 0.754 |
| 379 | dual | sling | G-TEK | Blind Grid | 24 to 36 | 35.983 | 0.811 |
| 379 | dual | sling | G-TEK | Blind Grid | 36 to 48 | 38.317 | 0.241 |
| 381 | dual | sling | G-TEK | Wet Probe | 0 to 6 | 58.99 | 2.85 |
| 381 | dual | sling | G-TEK | Wet Probe | 6 to 12 | 74.65 | 4.932 |
| 381 | dual | sling | G-TEK | Wet Probe | 12 to 24 | 76.88 | 0.807 |
| 381 | dual | sling | G-TEK | Wet Probe | 24 to 36 | 58.6 | 6.273 |
| 381 | dual | sling | G-TEK | Wet Probe | 36 to 48 | 51.06 | 1.589 |
| 381 | dual | sling | G-TEK | Woods | 0 to 6 | 15.233 | 0.125 |
| 381 | dual | sling | G-TEK | Woods | 6 to 12 | 6.233 | 0.249 |
| 381 | dual | sling | G-TEK | Woods | 12 to 24 | 4.817 | 0.241 |
| 381 | dual | sling | G-TEK | Woods | 24 to 36 | 52.933 | 0.461 |
| 381 | dual | sling | G-TEK | Woods | 36 to 48 | 55.35 | 0.594 |
| 381 | dual | sling | G-TEK | Open Field | 0 to 6 | 21.29 | 0.277 |
| 381 | dual | sling | G-TEK | Open Field | 6 to 12 | 5.97 | 0.287 |
| 381 | dual | sling | G-TEK | Open Field | 12 to 24 | 19.35 | 0.766 |
| 381 | dual | sling | G-TEK | Open Field | 24 to 36 | 27.98 | 0.584 |
| 381 | dual | sling | G-TEK | Open Field | 36 to 48 | 52.59 | 0.375 |
| 381 | dual | sling | G-TEK | Calibration | 0 to 6 | 39.1 | 0.1 |
| 381 | dual | sling | G-TEK | Calibration | 6 to 12 | 37.75 | 0.25 |

Aberdeen Proving Ground Demonstrations

| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
|---------------|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| 381 | dual | sling | G-TEK | Calibration | 12 to 24 | 1.55 | 0.05 |
| 381 | dual | sling | G-TEK | Calibration | 24 to 36 | 4.15 | 0.05 |
| 381 | dual | sling | G-TEK | Calibration | 36 to 48 | 5.4 | 0.1 |
| 381 | dual | sling | G-TEK | Blind Grid | 0 to 6 | 3.283 | 0.203 |
| 381 | dual | sling | G-TEK | Blind Grid | 6 to 12 | 23.75 | 0.275 |
| 381 | dual | sling | G-TEK | Blind Grid | 12 to 24 | 37.65 | 0.754 |
| 381 | dual | sling | G-TEK | Blind Grid | 24 to 36 | 35.983 | 0.811 |
| 381 | dual | sling | G-TEK | Blind Grid | 36 to 48 | 38.317 | 0.241 |
| 237 | MAG | hand | HFA | Wet Probe | 0 to 6 | 64.138 | 1.283 |
| 237 | MAG | hand | HFA | Wet Probe | 6 to 12 | 75.121 | 1.556 |
| 237 | MAG | hand | HFA | Wet Probe | 12 to 24 | 79.214 | 0.827 |
| 237 | MAG | hand | HFA | Wet Probe | 24 to 36 | 59.666 | 2.15 |
| 237 | MAG | hand | HFA | Wet Probe | 36 to 48 | 52.931 | 2.22 |
| 237 | MAG | hand | HFA | Woods | 0 to 6 | 14.7 | 0.255 |
| 237 | MAG | hand | HFA | Woods | 6 to 12 | 6.1 | 0.122 |
| 237 | MAG | hand | HFA | Woods | 12 to 24 | 5.875 | 0.043 |
| 237 | MAG | hand | HFA | Woods | 24 to 36 | 54.5 | 0.274 |
| 237 | MAG | hand | HFA | Woods | 36 to 48 | 57.225 | 0.217 |
| 237 | MAG | hand | HFA | Open Field | 0 to 6 | 21.352 | 1.172 |
| 237 | MAG | hand | HFA | Open Field | 6 to 12 | 7.431 | 1.139 |
| 237 | MAG | hand | HFA | Open Field | 12 to 24 | 22.11 | 2.682 |
| 237 | MAG | hand | HFA | Open Field | 24 to 36 | 26.597 | 0.965 |
| 237 | MAG | hand | HFA | Open Field | 36 to 48 | 56.855 | 2.603 |
| 237 | MAG | hand | HFA | Calibration | 0 to 6 | 0 | 0 |
| 237 | MAG | hand | HFA | Calibration | 6 to 12 | 0 | 0 |
| 237 | MAG | hand | HFA | Calibration | 12 to 24 | 0 | 0 |
| 237 | MAG | hand | HFA | Calibration | 24 to 36 | 0 | 0 |
| 237 | MAG | hand | HFA | Calibration | 36 to 48 | 0 | 0 |
| 237 | MAG | hand | HFA | Blind Grid | 0 to 6 | 4.16 | 0.602 |
| 237 | MAG | hand | HFA | Blind Grid | 6 to 12 | 12.64 | 10.012 |
| 237 | MAG | hand | HFA | Blind Grid | 12 to 24 | 20.18 | 15.613 |
| 237 | MAG | hand | HFA | Blind Grid | 24 to 36 | 36.76 | 0.692 |
| 237 | MAG | hand | HFA | Blind Grid | 36 to 48 | 39.76 | 0.185 |
| 676 | MAG | hand | HFA | Wet Probe | 0 to 6 | 64.138 | 1.283 |
| 676 | MAG | hand | HFA | Wet Probe | 6 to 12 | 75.121 | 1.556 |
| 676 | MAG | hand | HFA | Wet Probe | 12 to 24 | 79.214 | 0.827 |
| 676 | MAG | hand | HFA | Wet Probe | 24 to 36 | 59.666 | 2.15 |
| 676 | MAG | hand | HFA | Wet Probe | 36 to 48 | 52.931 | 2.22 |
| 676 | MAG | hand | HFA | Woods | 0 to 6 | 14.7 | 0.255 |
| 676 | MAG | hand | HFA | Woods | 6 to 12 | 6.1 | 0.122 |
| 676 | MAG | hand | HFA | Woods | 12 to 24 | 5.875 | 0.043 |
| 676 | MAG | hand | HFA | Woods | 24 to 36 | 54.5 | 0.274 |
| 676 | MAG | hand | HFA | Woods | 36 to 48 | 57.225 | 0.217 |
| 676 | MAG | hand | HFA | Open Field | 0 to 6 | 21.352 | 1.172 |
| 676 | MAG | hand | HFA | Open Field | 6 to 12 | 7.431 | 1.139 |
| 676 | MAG | hand | HFA | Open Field | 12 to 24 | 22.11 | 2.682 |
| 676 | MAG | hand | HFA | Open Field | 24 to 36 | 26.597 | 0.965 |
| 676 | MAG | hand | HFA | Open Field | 36 to 48 | 56.855 | 2.603 |
| 676 | MAG | hand | HFA | Calibration | 0 to 6 | 0 | 0 |
| 676 | MAG | hand | HFA | Calibration | 6 to 12 | 0 | 0 |

Aberdeen Proving Ground Demonstrations

| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
|---------------|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| 676 | MAG | hand | HFA | Calibration | 12 to 24 | 0 | 0 |
| 676 | MAG | hand | HFA | Calibration | 24 to 36 | 0 | 0 |
| 676 | MAG | hand | HFA | Calibration | 36 to 48 | 0 | 0 |
| 676 | MAG | hand | HFA | Blind Grid | 0 to 6 | 4.16 | 0.602 |
| 676 | MAG | hand | HFA | Blind Grid | 6 to 12 | 12.64 | 10.012 |
| 676 | MAG | hand | HFA | Blind Grid | 12 to 24 | 20.18 | 15.613 |
| 676 | MAG | hand | HFA | Blind Grid | 24 to 36 | 36.76 | 0.692 |
| 676 | MAG | hand | HFA | Blind Grid | 36 to 48 | 39.76 | 0.185 |
| 231 | MAG | hand | HFA | Wet Probe | 0 to 6 | 64.138 | 1.283 |
| 231 | MAG | hand | HFA | Wet Probe | 6 to 12 | 75.121 | 1.556 |
| 231 | MAG | hand | HFA | Wet Probe | 12 to 24 | 79.214 | 0.827 |
| 231 | MAG | hand | HFA | Wet Probe | 24 to 36 | 59.666 | 2.15 |
| 231 | MAG | hand | HFA | Wet Probe | 36 to 48 | 52.931 | 2.22 |
| 231 | MAG | hand | HFA | Woods | 0 to 6 | 14.7 | 0.255 |
| 231 | MAG | hand | HFA | Woods | 6 to 12 | 6.1 | 0.122 |
| 231 | MAG | hand | HFA | Woods | 12 to 24 | 5.875 | 0.043 |
| 231 | MAG | hand | HFA | Woods | 24 to 36 | 54.5 | 0.274 |
| 231 | MAG | hand | HFA | Woods | 36 to 48 | 57.225 | 0.217 |
| 231 | MAG | hand | HFA | Open Field | 0 to 6 | 20.569 | 3.994 |
| 231 | MAG | hand | HFA | Open Field | 6 to 12 | 7.436 | 1.159 |
| 231 | MAG | hand | HFA | Open Field | 12 to 24 | 22.218 | 2.667 |
| 231 | MAG | hand | HFA | Open Field | 24 to 36 | 26.593 | 0.982 |
| 231 | MAG | hand | HFA | Open Field | 36 to 48 | 56.979 | 2.564 |
| 231 | MAG | hand | HFA | Calibration | 0 to 6 | 0 | 0 |
| 231 | MAG | hand | HFA | Calibration | 6 to 12 | 0 | 0 |
| 231 | MAG | hand | HFA | Calibration | 12 to 24 | 0 | 0 |
| 231 | MAG | hand | HFA | Calibration | 24 to 36 | 0 | 0 |
| 231 | MAG | hand | HFA | Calibration | 36 to 48 | 0 | 0 |
| 231 | MAG | hand | HFA | Blind Grid | 0 to 6 | 4.16 | 0.602 |
| 231 | MAG | hand | HFA | Blind Grid | 6 to 12 | 12.64 | 10.012 |
| 231 | MAG | hand | HFA | Blind Grid | 12 to 24 | 20.18 | 15.613 |
| 231 | MAG | hand | HFA | Blind Grid | 24 to 36 | 36.76 | 0.692 |
| 231 | MAG | hand | HFA | Blind Grid | 36 to 48 | 39.76 | 0.185 |
| 486 | MAG | hand | HFA | Wet Probe | 0 to 6 | 64.138 | 1.283 |
| 486 | MAG | hand | HFA | Wet Probe | 6 to 12 | 75.121 | 1.556 |
| 486 | MAG | hand | HFA | Wet Probe | 12 to 24 | 79.214 | 0.827 |
| 486 | MAG | hand | HFA | Wet Probe | 24 to 36 | 59.666 | 2.15 |
| 486 | MAG | hand | HFA | Wet Probe | 36 to 48 | 52.931 | 2.22 |
| 486 | MAG | hand | HFA | Woods | 0 to 6 | 14.7 | 0.255 |
| 486 | MAG | hand | HFA | Woods | 6 to 12 | 6.1 | 0.122 |
| 486 | MAG | hand | HFA | Woods | 12 to 24 | 5.875 | 0.043 |
| 486 | MAG | hand | HFA | Woods | 24 to 36 | 54.5 | 0.274 |
| 486 | MAG | hand | HFA | Woods | 36 to 48 | 57.225 | 0.217 |
| 486 | MAG | hand | HFA | Open Field | 0 to 6 | 21.352 | 1.172 |
| 486 | MAG | hand | HFA | Open Field | 6 to 12 | 7.431 | 1.139 |
| 486 | MAG | hand | HFA | Open Field | 12 to 24 | 22.11 | 2.682 |
| 486 | MAG | hand | HFA | Open Field | 24 to 36 | 26.597 | 0.965 |
| 486 | MAG | hand | HFA | Open Field | 36 to 48 | 56.855 | 2.603 |
| 486 | MAG | hand | HFA | Calibration | 0 to 6 | 0 | 0 |
| 486 | MAG | hand | HFA | Calibration | 6 to 12 | 0 | 0 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 486 | MAG | hand | HFA | Calibration | 12 to 24 | 0 | 0 |
| 486 | MAG | hand | HFA | Calibration | 24 to 36 | 0 | 0 |
| 486 | MAG | hand | HFA | Calibration | 36 to 48 | 0 | 0 |
| 486 | MAG | hand | HFA | Blind Grid | 0 to 6 | 4.16 | 0.602 |
| 486 | MAG | hand | HFA | Blind Grid | 6 to 12 | 12.64 | 10.012 |
| 486 | MAG | hand | HFA | Blind Grid | 12 to 24 | 20.18 | 15.613 |
| 486 | MAG | hand | HFA | Blind Grid | 24 to 36 | 36.76 | 0.692 |
| 486 | MAG | hand | HFA | Blind Grid | 36 to 48 | 39.76 | 0.185 |
| 647 | EM | towed | NAEVA | Wet Probe | 0 to 6 | 66.909 | 0.761 |
| 647 | EM | towed | NAEVA | Wet Probe | 6 to 12 | 75.791 | 0.723 |
| 647 | EM | towed | NAEVA | Wet Probe | 12 to 24 | 79.373 | 0.277 |
| 647 | EM | towed | NAEVA | Wet Probe | 24 to 36 | 55.273 | 0.305 |
| 647 | EM | towed | NAEVA | Wet Probe | 36 to 48 | 53.264 | 0.503 |
| 647 | EM | towed | NAEVA | Woods | 0 to 6 | 14.45 | 0.206 |
| 647 | EM | towed | NAEVA | Woods | 6 to 12 | 5.425 | 0.192 |
| 647 | EM | towed | NAEVA | Woods | 12 to 24 | 5.55 | 0.166 |
| 647 | EM | towed | NAEVA | Woods | 24 to 36 | 55.5 | 0.316 |
| 647 | EM | towed | NAEVA | Woods | 36 to 48 | 57.675 | 0.179 |
| 647 | EM | towed | NAEVA | Open Field | 0 to 6 | 23.436 | 1.077 |
| 647 | EM | towed | NAEVA | Open Field | 6 to 12 | 6.473 | 0.289 |
| 647 | EM | towed | NAEVA | Open Field | 12 to 24 | 19.473 | 0.2 |
| 647 | EM | towed | NAEVA | Open Field | 24 to 36 | 27.091 | 0.557 |
| 647 | EM | towed | NAEVA | Open Field | 36 to 48 | 52.445 | 0.227 |
| 647 | EM | towed | NAEVA | Calibration | 0 to 6 | 1.2 | 0.163 |
| 647 | EM | towed | NAEVA | Calibration | 6 to 12 | 20.5 | 0.245 |
| 647 | EM | towed | NAEVA | Calibration | 12 to 24 | 28.667 | 0.205 |
| 647 | EM | towed | NAEVA | Calibration | 24 to 36 | 36.2 | 0.141 |
| 647 | EM | towed | NAEVA | Calibration | 36 to 48 | 38.867 | 0.34 |
| 647 | EM | towed | NAEVA | Blind Grid | 0 to 6 | 3.3 | 0.551 |
| 647 | EM | towed | NAEVA | Blind Grid | 6 to 12 | 24.9 | 0.306 |
| 647 | EM | towed | NAEVA | Blind Grid | 12 to 24 | 39 | 0.529 |
| 647 | EM | towed | NAEVA | Blind Grid | 24 to 36 | 36.183 | 0.43 |
| 647 | EM | towed | NAEVA | Blind Grid | 36 to 48 | 39.533 | 0.499 |
| 396 | EM | 2-man | NAEVA | Wet Probe | 0 to 6 | 66.909 | 0.761 |
| 396 | EM | 2-man | NAEVA | Wet Probe | 6 to 12 | 75.791 | 0.723 |
| 396 | EM | 2-man | NAEVA | Wet Probe | 12 to 24 | 79.373 | 0.277 |
| 396 | EM | 2-man | NAEVA | Wet Probe | 24 to 36 | 55.273 | 0.305 |
| 396 | EM | 2-man | NAEVA | Wet Probe | 36 to 48 | 53.264 | 0.503 |
| 396 | EM | 2-man | NAEVA | Woods | 0 to 6 | 14.45 | 0.206 |
| 396 | EM | 2-man | NAEVA | Woods | 6 to 12 | 5.425 | 0.192 |
| 396 | EM | 2-man | NAEVA | Woods | 12 to 24 | 5.55 | 0.166 |
| 396 | EM | 2-man | NAEVA | Woods | 24 to 36 | 55.5 | 0.316 |
| 396 | EM | 2-man | NAEVA | Woods | 36 to 48 | 57.675 | 0.179 |
| 396 | EM | 2-man | NAEVA | Open Field | 0 to 6 | 23.436 | 1.077 |
| 396 | EM | 2-man | NAEVA | Open Field | 6 to 12 | 6.473 | 0.289 |
| 396 | EM | 2-man | NAEVA | Open Field | 12 to 24 | 19.473 | 0.2 |
| 396 | EM | 2-man | NAEVA | Open Field | 24 to 36 | 27.091 | 0.557 |
| 396 | EM | 2-man | NAEVA | Open Field | 36 to 48 | 52.445 | 0.227 |
| 396 | EM | 2-man | NAEVA | Calibration | 0 to 6 | 1.2 | 0.163 |
| 396 | EM | 2-man | NAEVA | Calibration | 6 to 12 | 20.5 | 0.245 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 396 | EM | 2-man | NAEVA | Calibration | 12 to 24 | 28.667 | 0.205 |
| 396 | EM | 2-man | NAEVA | Calibration | 24 to 36 | 36.2 | 0.141 |
| 396 | EM | 2-man | NAEVA | Calibration | 36 to 48 | 38.867 | 0.34 |
| 396 | EM | 2-man | NAEVA | Blind Grid | 0 to 6 | 3.3 | 0.551 |
| 396 | EM | 2-man | NAEVA | Blind Grid | 6 to 12 | 24.9 | 0.306 |
| 396 | EM | 2-man | NAEVA | Blind Grid | 12 to 24 | 39 | 0.529 |
| 396 | EM | 2-man | NAEVA | Blind Grid | 24 to 36 | 36.183 | 0.43 |
| 396 | EM | 2-man | NAEVA | Blind Grid | 36 to 48 | 39.533 | 0.499 |
| 397 | EM | towed | NAEVA | Wet Probe | 0 to 6 | 66.909 | 0.761 |
| 397 | EM | towed | NAEVA | Wet Probe | 6 to 12 | 75.791 | 0.723 |
| 397 | EM | towed | NAEVA | Wet Probe | 12 to 24 | 79.373 | 0.277 |
| 397 | EM | towed | NAEVA | Wet Probe | 24 to 36 | 55.273 | 0.305 |
| 397 | EM | towed | NAEVA | Wet Probe | 36 to 48 | 53.264 | 0.503 |
| 397 | EM | towed | NAEVA | Woods | 0 to 6 | 14.45 | 0.206 |
| 397 | EM | towed | NAEVA | Woods | 6 to 12 | 5.425 | 0.192 |
| 397 | EM | towed | NAEVA | Woods | 12 to 24 | 5.55 | 0.166 |
| 397 | EM | towed | NAEVA | Woods | 24 to 36 | 55.5 | 0.316 |
| 397 | EM | towed | NAEVA | Woods | 36 to 48 | 57.675 | 0.179 |
| 397 | EM | towed | NAEVA | Open Field | 0 to 6 | 23.436 | 1.077 |
| 397 | EM | towed | NAEVA | Open Field | 6 to 12 | 6.473 | 0.289 |
| 397 | EM | towed | NAEVA | Open Field | 12 to 24 | 19.473 | 0.2 |
| 397 | EM | towed | NAEVA | Open Field | 24 to 36 | 27.091 | 0.557 |
| 397 | EM | towed | NAEVA | Open Field | 36 to 48 | 52.445 | 0.227 |
| 397 | EM | towed | NAEVA | Calibration | 0 to 6 | 1.2 | 0.163 |
| 397 | EM | towed | NAEVA | Calibration | 6 to 12 | 20.5 | 0.245 |
| 397 | EM | towed | NAEVA | Calibration | 12 to 24 | 28.667 | 0.205 |
| 397 | EM | towed | NAEVA | Calibration | 24 to 36 | 36.2 | 0.141 |
| 397 | EM | towed | NAEVA | Calibration | 36 to 48 | 38.867 | 0.34 |
| 397 | EM | towed | NAEVA | Blind Grid | 0 to 6 | 3.3 | 0.551 |
| 397 | EM | towed | NAEVA | Blind Grid | 6 to 12 | 24.9 | 0.306 |
| 397 | EM | towed | NAEVA | Blind Grid | 12 to 24 | 39 | 0.529 |
| 397 | EM | towed | NAEVA | Blind Grid | 24 to 36 | 36.183 | 0.43 |
| 397 | EM | towed | NAEVA | Blind Grid | 36 to 48 | 39.533 | 0.499 |
| 597 | EM | 2-man | NAEVA | Wet Probe | 0 to 6 | 66.909 | 0.761 |
| 597 | EM | 2-man | NAEVA | Wet Probe | 6 to 12 | 75.791 | 0.723 |
| 597 | EM | 2-man | NAEVA | Wet Probe | 12 to 24 | 79.373 | 0.277 |
| 597 | EM | 2-man | NAEVA | Wet Probe | 24 to 36 | 55.273 | 0.305 |
| 597 | EM | 2-man | NAEVA | Wet Probe | 36 to 48 | 53.264 | 0.503 |
| 597 | EM | 2-man | NAEVA | Woods | 0 to 6 | 14.45 | 0.206 |
| 597 | EM | 2-man | NAEVA | Woods | 6 to 12 | 5.425 | 0.192 |
| 597 | EM | 2-man | NAEVA | Woods | 12 to 24 | 5.55 | 0.166 |
| 597 | EM | 2-man | NAEVA | Woods | 24 to 36 | 55.5 | 0.316 |
| 597 | EM | 2-man | NAEVA | Woods | 36 to 48 | 57.675 | 0.179 |
| 597 | EM | 2-man | NAEVA | Open Field | 0 to 6 | 23.436 | 1.077 |
| 597 | EM | 2-man | NAEVA | Open Field | 6 to 12 | 6.473 | 0.289 |
| 597 | EM | 2-man | NAEVA | Open Field | 12 to 24 | 19.473 | 0.2 |
| 597 | EM | 2-man | NAEVA | Open Field | 24 to 36 | 27.091 | 0.557 |
| 597 | EM | 2-man | NAEVA | Open Field | 36 to 48 | 52.445 | 0.227 |
| 597 | EM | 2-man | NAEVA | Calibration | 0 to 6 | 1.2 | 0.163 |
| 597 | EM | 2-man | NAEVA | Calibration | 6 to 12 | 20.5 | 0.245 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 597 | EM | 2-man | NAEVA | Calibration | 12 to 24 | 28.667 | 0.205 |
| 597 | EM | 2-man | NAEVA | Calibration | 24 to 36 | 36.2 | 0.141 |
| 597 | EM | 2-man | NAEVA | Calibration | 36 to 48 | 38.867 | 0.34 |
| 597 | EM | 2-man | NAEVA | Blind Grid | 0 to 6 | 3.3 | 0.551 |
| 597 | EM | 2-man | NAEVA | Blind Grid | 6 to 12 | 24.9 | 0.306 |
| 597 | EM | 2-man | NAEVA | Blind Grid | 12 to 24 | 39 | 0.529 |
| 597 | EM | 2-man | NAEVA | Blind Grid | 24 to 36 | 36.183 | 0.43 |
| 597 | EM | 2-man | NAEVA | Blind Grid | 36 to 48 | 39.533 | 0.499 |
| 406 | EM | towed | NAEVA | Wet Probe | 0 to 6 | 66.909 | 0.761 |
| 406 | EM | towed | NAEVA | Wet Probe | 6 to 12 | 75.791 | 0.723 |
| 406 | EM | towed | NAEVA | Wet Probe | 12 to 24 | 79.373 | 0.277 |
| 406 | EM | towed | NAEVA | Wet Probe | 24 to 36 | 55.273 | 0.305 |
| 406 | EM | towed | NAEVA | Wet Probe | 36 to 48 | 53.264 | 0.503 |
| 406 | EM | towed | NAEVA | Woods | 0 to 6 | 14.45 | 0.206 |
| 406 | EM | towed | NAEVA | Woods | 6 to 12 | 5.425 | 0.192 |
| 406 | EM | towed | NAEVA | Woods | 12 to 24 | 5.55 | 0.166 |
| 406 | EM | towed | NAEVA | Woods | 24 to 36 | 55.5 | 0.316 |
| 406 | EM | towed | NAEVA | Woods | 36 to 48 | 57.675 | 0.179 |
| 406 | EM | towed | NAEVA | Open Field | 0 to 6 | 23.436 | 1.077 |
| 406 | EM | towed | NAEVA | Open Field | 6 to 12 | 6.473 | 0.289 |
| 406 | EM | towed | NAEVA | Open Field | 12 to 24 | 19.473 | 0.2 |
| 406 | EM | towed | NAEVA | Open Field | 24 to 36 | 27.091 | 0.557 |
| 406 | EM | towed | NAEVA | Open Field | 36 to 48 | 52.445 | 0.227 |
| 406 | EM | towed | NAEVA | Calibration | 0 to 6 | 1.2 | 0.163 |
| 406 | EM | towed | NAEVA | Calibration | 6 to 12 | 20.5 | 0.245 |
| 406 | EM | towed | NAEVA | Calibration | 12 to 24 | 28.667 | 0.205 |
| 406 | EM | towed | NAEVA | Calibration | 24 to 36 | 36.2 | 0.141 |
| 406 | EM | towed | NAEVA | Calibration | 36 to 48 | 38.867 | 0.34 |
| 406 | EM | towed | NAEVA | Blind Grid | 0 to 6 | 3.3 | 0.551 |
| 406 | EM | towed | NAEVA | Blind Grid | 6 to 12 | 24.9 | 0.306 |
| 406 | EM | towed | NAEVA | Blind Grid | 12 to 24 | 39 | 0.529 |
| 406 | EM | towed | NAEVA | Blind Grid | 24 to 36 | 36.183 | 0.43 |
| 406 | EM | towed | NAEVA | Blind Grid | 36 to 48 | 39.533 | 0.499 |
| 494 | EM | 2-man | NAEVA | Wet Probe | 0 to 6 | 66.909 | 0.761 |
| 494 | EM | 2-man | NAEVA | Wet Probe | 6 to 12 | 75.791 | 0.723 |
| 494 | EM | 2-man | NAEVA | Wet Probe | 12 to 24 | 79.373 | 0.277 |
| 494 | EM | 2-man | NAEVA | Wet Probe | 24 to 36 | 55.273 | 0.305 |
| 494 | EM | 2-man | NAEVA | Wet Probe | 36 to 48 | 53.264 | 0.503 |
| 494 | EM | 2-man | NAEVA | Woods | 0 to 6 | 14.45 | 0.206 |
| 494 | EM | 2-man | NAEVA | Woods | 6 to 12 | 5.425 | 0.192 |
| 494 | EM | 2-man | NAEVA | Woods | 12 to 24 | 5.55 | 0.166 |
| 494 | EM | 2-man | NAEVA | Woods | 24 to 36 | 55.5 | 0.316 |
| 494 | EM | 2-man | NAEVA | Woods | 36 to 48 | 57.675 | 0.179 |
| 494 | EM | 2-man | NAEVA | Open Field | 0 to 6 | 23.436 | 1.077 |
| 494 | EM | 2-man | NAEVA | Open Field | 6 to 12 | 6.473 | 0.289 |
| 494 | EM | 2-man | NAEVA | Open Field | 12 to 24 | 19.473 | 0.2 |
| 494 | EM | 2-man | NAEVA | Open Field | 24 to 36 | 27.091 | 0.557 |
| 494 | EM | 2-man | NAEVA | Open Field | 36 to 48 | 52.445 | 0.227 |
| 494 | EM | 2-man | NAEVA | Calibration | 0 to 6 | 1.2 | 0.163 |
| 494 | EM | 2-man | NAEVA | Calibration | 6 to 12 | 20.5 | 0.245 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 494 | EM | 2-man | NAEVA | Calibration | 12 to 24 | 28.667 | 0.205 |
| 494 | EM | 2-man | NAEVA | Calibration | 24 to 36 | 36.2 | 0.141 |
| 494 | EM | 2-man | NAEVA | Calibration | 36 to 48 | 38.867 | 0.34 |
| 494 | EM | 2-man | NAEVA | Blind Grid | 0 to 6 | 3.3 | 0.551 |
| 494 | EM | 2-man | NAEVA | Blind Grid | 6 to 12 | 24.9 | 0.306 |
| 494 | EM | 2-man | NAEVA | Blind Grid | 12 to 24 | 39 | 0.529 |
| 494 | EM | 2-man | NAEVA | Blind Grid | 24 to 36 | 36.183 | 0.43 |
| 494 | EM | 2-man | NAEVA | Blind Grid | 36 to 48 | 39.533 | 0.499 |
| 127 | EM | towed | NRL | Wet Probe | 0 to 6 | 0 | 0 |
| 127 | EM | towed | NRL | Wet Probe | 6 to 12 | 0 | 0 |
| 127 | EM | towed | NRL | Wet Probe | 12 to 24 | 0 | 0 |
| 127 | EM | towed | NRL | Wet Probe | 24 to 36 | 0 | 0 |
| 127 | EM | towed | NRL | Wet Probe | 36 to 48 | 0 | 0 |
| 127 | EM | towed | NRL | Woods | 0 to 6 | 0 | 0 |
| 127 | EM | towed | NRL | Woods | 6 to 12 | 0 | 0 |
| 127 | EM | towed | NRL | Woods | 12 to 24 | 0 | 0 |
| 127 | EM | towed | NRL | Woods | 24 to 36 | 0 | 0 |
| 127 | EM | towed | NRL | Woods | 36 to 48 | 0 | 0 |
| 127 | EM | towed | NRL | Open Field | 0 to 6 | 28.95 | 0.18 |
| 127 | EM | towed | NRL | Open Field | 6 to 12 | 0.55 | 0.112 |
| 127 | EM | towed | NRL | Open Field | 12 to 24 | 24.925 | 0.192 |
| 127 | EM | towed | NRL | Open Field | 24 to 36 | 33.7 | 0.274 |
| 127 | EM | towed | NRL | Open Field | 36 to 48 | 52.675 | 0.148 |
| 127 | EM | towed | NRL | Calibration | 0 to 6 | 38.733 | 1.084 |
| 127 | EM | towed | NRL | Calibration | 6 to 12 | 37.767 | 0.094 |
| 127 | EM | towed | NRL | Calibration | 12 to 24 | 7.9 | 0.216 |
| 127 | EM | towed | NRL | Calibration | 24 to 36 | 4.733 | 0.262 |
| 127 | EM | towed | NRL | Calibration | 36 to 48 | 4.733 | 0.189 |
| 127 | EM | towed | NRL | Blind Grid | 0 to 6 | 3.4 | 0.432 |
| 127 | EM | towed | NRL | Blind Grid | 6 to 12 | 17.667 | 0.403 |
| 127 | EM | towed | NRL | Blind Grid | 12 to 24 | 36.2 | 1.558 |
| 127 | EM | towed | NRL | Blind Grid | 24 to 36 | 36.567 | 1.793 |
| 127 | EM | towed | NRL | Blind Grid | 36 to 48 | 37.8 | 1.705 |
| 675 | EM | towed | NRL | Wet Probe | 0 to 6 | 63.183 | 0.418 |
| 675 | EM | towed | NRL | Wet Probe | 6 to 12 | 75.033 | 0.83 |
| 675 | EM | towed | NRL | Wet Probe | 12 to 24 | 77.917 | 0.555 |
| 675 | EM | towed | NRL | Wet Probe | 24 to 36 | 55.533 | 0.534 |
| 675 | EM | towed | NRL | Wet Probe | 36 to 48 | 50.517 | 1.218 |
| 675 | EM | towed | NRL | Woods | 0 to 6 | 0 | 0 |
| 675 | EM | towed | NRL | Woods | 6 to 12 | 0 | 0 |
| 675 | EM | towed | NRL | Woods | 12 to 24 | 0 | 0 |
| 675 | EM | towed | NRL | Woods | 24 to 36 | 0 | 0 |
| 675 | EM | towed | NRL | Woods | 36 to 48 | 0 | 0 |
| 675 | EM | towed | NRL | Open Field | 0 to 6 | 24.57 | 3.586 |
| 675 | EM | towed | NRL | Open Field | 6 to 12 | 3.76 | 2.63 |
| 675 | EM | towed | NRL | Open Field | 12 to 24 | 21 | 3.217 |
| 675 | EM | towed | NRL | Open Field | 24 to 36 | 29.17 | 3.743 |
| 675 | EM | towed | NRL | Open Field | 36 to 48 | 52.36 | 0.673 |
| 675 | EM | towed | NRL | Calibration | 0 to 6 | 38.733 | 1.084 |
| 675 | EM | towed | NRL | Calibration | 6 to 12 | 37.767 | 0.094 |

Aberdeen Proving Ground Demonstrations

| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
|---------------|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| 675 | EM | towed | NRL | Calibration | 12 to 24 | 7.9 | 0.216 |
| 675 | EM | towed | NRL | Calibration | 24 to 36 | 4.733 | 0.262 |
| 675 | EM | towed | NRL | Calibration | 36 to 48 | 4.733 | 0.189 |
| 675 | EM | towed | NRL | Blind Grid | 0 to 6 | 3.157 | 0.358 |
| 675 | EM | towed | NRL | Blind Grid | 6 to 12 | 21.529 | 3.36 |
| 675 | EM | towed | NRL | Blind Grid | 12 to 24 | 37.057 | 1.404 |
| 675 | EM | towed | NRL | Blind Grid | 24 to 36 | 35.771 | 1.405 |
| 675 | EM | towed | NRL | Blind Grid | 36 to 48 | 38.471 | 1.269 |
| 671 | MAG | towed | NRL | Wet Probe | 0 to 6 | 60.2 | 0.082 |
| 671 | MAG | towed | NRL | Wet Probe | 6 to 12 | 75.633 | 0.249 |
| 671 | MAG | towed | NRL | Wet Probe | 12 to 24 | 78.1 | 0.216 |
| 671 | MAG | towed | NRL | Wet Probe | 24 to 36 | 55.4 | 0.216 |
| 671 | MAG | towed | NRL | Wet Probe | 36 to 48 | 48.433 | 0.189 |
| 671 | MAG | towed | NRL | Woods | 0 to 6 | 0 | 0 |
| 671 | MAG | towed | NRL | Woods | 6 to 12 | 0 | 0 |
| 671 | MAG | towed | NRL | Woods | 12 to 24 | 0 | 0 |
| 671 | MAG | towed | NRL | Woods | 24 to 36 | 0 | 0 |
| 671 | MAG | towed | NRL | Woods | 36 to 48 | 0 | 0 |
| 671 | MAG | towed | NRL | Open Field | 0 to 6 | 21.2 | 0.082 |
| 671 | MAG | towed | NRL | Open Field | 6 to 12 | 6.533 | 0.205 |
| 671 | MAG | towed | NRL | Open Field | 12 to 24 | 18.267 | 0.17 |
| 671 | MAG | towed | NRL | Open Field | 24 to 36 | 26.3 | 0.163 |
| 671 | MAG | towed | NRL | Open Field | 36 to 48 | 54.1 | 0.163 |
| 671 | MAG | towed | NRL | Calibration | 0 to 6 | 40.25 | 0.05 |
| 671 | MAG | towed | NRL | Calibration | 6 to 12 | 38.45 | 0.05 |
| 671 | MAG | towed | NRL | Calibration | 12 to 24 | 1.65 | 0.15 |
| 671 | MAG | towed | NRL | Calibration | 24 to 36 | 4.1 | 0.1 |
| 671 | MAG | towed | NRL | Calibration | 36 to 48 | 4.4 | 0.1 |
| 671 | MAG | towed | NRL | Blind Grid | 0 to 6 | 3.95 | 0.05 |
| 671 | MAG | towed | NRL | Blind Grid | 6 to 12 | 25.9 | 0.2 |
| 671 | MAG | towed | NRL | Blind Grid | 12 to 24 | 36.1 | 0.2 |
| 671 | MAG | towed | NRL | Blind Grid | 24 to 36 | 37.65 | 0.15 |
| 671 | MAG | towed | NRL | Blind Grid | 36 to 48 | 38.45 | 0.05 |
| 673 | MAG | towed | NRL | Wet Probe | 0 to 6 | 60.2 | 0.082 |
| 673 | MAG | towed | NRL | Wet Probe | 6 to 12 | 75.633 | 0.249 |
| 673 | MAG | towed | NRL | Wet Probe | 12 to 24 | 78.1 | 0.216 |
| 673 | MAG | towed | NRL | Wet Probe | 24 to 36 | 55.4 | 0.216 |
| 673 | MAG | towed | NRL | Wet Probe | 36 to 48 | 48.433 | 0.189 |
| 673 | MAG | towed | NRL | Woods | 0 to 6 | 0 | 0 |
| 673 | MAG | towed | NRL | Woods | 6 to 12 | 0 | 0 |
| 673 | MAG | towed | NRL | Woods | 12 to 24 | 0 | 0 |
| 673 | MAG | towed | NRL | Woods | 24 to 36 | 0 | 0 |
| 673 | MAG | towed | NRL | Woods | 36 to 48 | 0 | 0 |
| 673 | MAG | towed | NRL | Open Field | 0 to 6 | 21.2 | 0.082 |
| 673 | MAG | towed | NRL | Open Field | 6 to 12 | 6.533 | 0.205 |
| 673 | MAG | towed | NRL | Open Field | 12 to 24 | 18.267 | 0.17 |
| 673 | MAG | towed | NRL | Open Field | 24 to 36 | 26.3 | 0.163 |
| 673 | MAG | towed | NRL | Open Field | 36 to 48 | 54.1 | 0.163 |
| 673 | MAG | towed | NRL | Calibration | 0 to 6 | 40.25 | 0.05 |
| 673 | MAG | towed | NRL | Calibration | 6 to 12 | 38.45 | 0.05 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 673 | MAG | towed | NRL | Calibration | 12 to 24 | 1.65 | 0.15 |
| 673 | MAG | towed | NRL | Calibration | 24 to 36 | 4.1 | 0.1 |
| 673 | MAG | towed | NRL | Calibration | 36 to 48 | 4.4 | 0.1 |
| 673 | MAG | towed | NRL | Blind Grid | 0 to 6 | 3.95 | 0.05 |
| 673 | MAG | towed | NRL | Blind Grid | 6 to 12 | 25.9 | 0.2 |
| 673 | MAG | towed | NRL | Blind Grid | 12 to 24 | 36.1 | 0.2 |
| 673 | MAG | towed | NRL | Blind Grid | 24 to 36 | 37.65 | 0.15 |
| 673 | MAG | towed | NRL | Blind Grid | 36 to 48 | 38.45 | 0.05 |
| 252 | EM | cart | Parsons | Wet Probe | 0 to 6 | 64.585 | 0.549 |
| 252 | EM | cart | Parsons | Wet Probe | 6 to 12 | 73.3 | 0.522 |
| 252 | EM | cart | Parsons | Wet Probe | 12 to 24 | 77.1 | 0.621 |
| 252 | EM | cart | Parsons | Wet Probe | 24 to 36 | 54.235 | 0.662 |
| 252 | EM | cart | Parsons | Wet Probe | 36 to 48 | 53.355 | 0.466 |
| 252 | EM | cart | Parsons | Woods | 0 to 6 | 13.3 | 0.818 |
| 252 | EM | cart | Parsons | Woods | 6 to 12 | 6.3 | 0.46 |
| 252 | EM | cart | Parsons | Woods | 12 to 24 | 6.771 | 0.198 |
| 252 | EM | cart | Parsons | Woods | 24 to 36 | 57.786 | 0.264 |
| 252 | EM | cart | Parsons | Woods | 36 to 48 | 59.371 | 0.377 |
| 252 | EM | cart | Parsons | Open Field | 0 to 6 | 20.37 | 0.603 |
| 252 | EM | cart | Parsons | Open Field | 6 to 12 | 7.535 | 0.338 |
| 252 | EM | cart | Parsons | Open Field | 12 to 24 | 21.445 | 0.264 |
| 252 | EM | cart | Parsons | Open Field | 24 to 36 | 28.25 | 0.398 |
| 252 | EM | cart | Parsons | Open Field | 36 to 48 | 54.56 | 0.365 |
| 252 | EM | cart | Parsons | Calibration | 0 to 6 | 2.05 | 0.75 |
| 252 | EM | cart | Parsons | Calibration | 6 to 12 | 14.95 | 0.65 |
| 252 | EM | cart | Parsons | Calibration | 12 to 24 | 25.05 | 0.65 |
| 252 | EM | cart | Parsons | Calibration | 24 to 36 | 32.2 | 1.3 |
| 252 | EM | cart | Parsons | Calibration | 36 to 48 | 38.1 | 1 |
| 252 | EM | cart | Parsons | Blind Grid | 0 to 6 | 5.162 | 0.908 |
| 252 | EM | cart | Parsons | Blind Grid | 6 to 12 | 1.675 | 0.614 |
| 252 | EM | cart | Parsons | Blind Grid | 12 to 24 | 25.938 | 0.831 |
| 252 | EM | cart | Parsons | Blind Grid | 24 to 36 | 35.937 | 0.394 |
| 252 | EM | cart | Parsons | Blind Grid | 36 to 48 | 40.838 | 0.817 |
| 572 | EM | cart | Parsons | Wet Probe | 0 to 6 | 64.585 | 0.549 |
| 572 | EM | cart | Parsons | Wet Probe | 6 to 12 | 73.3 | 0.522 |
| 572 | EM | cart | Parsons | Wet Probe | 12 to 24 | 77.1 | 0.621 |
| 572 | EM | cart | Parsons | Wet Probe | 24 to 36 | 54.235 | 0.662 |
| 572 | EM | cart | Parsons | Wet Probe | 36 to 48 | 53.355 | 0.466 |
| 572 | EM | cart | Parsons | Woods | 0 to 6 | 13.3 | 0.818 |
| 572 | EM | cart | Parsons | Woods | 6 to 12 | 6.3 | 0.46 |
| 572 | EM | cart | Parsons | Woods | 12 to 24 | 6.771 | 0.198 |
| 572 | EM | cart | Parsons | Woods | 24 to 36 | 57.786 | 0.264 |
| 572 | EM | cart | Parsons | Woods | 36 to 48 | 59.371 | 0.377 |
| 572 | EM | cart | Parsons | Open Field | 0 to 6 | 20.37 | 0.603 |
| 572 | EM | cart | Parsons | Open Field | 6 to 12 | 7.535 | 0.338 |
| 572 | EM | cart | Parsons | Open Field | 12 to 24 | 21.445 | 0.264 |
| 572 | EM | cart | Parsons | Open Field | 24 to 36 | 28.25 | 0.398 |
| 572 | EM | cart | Parsons | Open Field | 36 to 48 | 54.56 | 0.365 |
| 572 | EM | cart | Parsons | Calibration | 0 to 6 | 2.05 | 0.75 |
| 572 | EM | cart | Parsons | Calibration | 6 to 12 | 14.95 | 0.65 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 572 | EM | cart | Parsons | Calibration | 12 to 24 | 25.05 | 0.65 |
| 572 | EM | cart | Parsons | Calibration | 24 to 36 | 32.2 | 1.3 |
| 572 | EM | cart | Parsons | Calibration | 36 to 48 | 38.1 | 1 |
| 572 | EM | cart | Parsons | Blind Grid | 0 to 6 | 5.162 | 0.908 |
| 572 | EM | cart | Parsons | Blind Grid | 6 to 12 | 1.675 | 0.614 |
| 572 | EM | cart | Parsons | Blind Grid | 12 to 24 | 25.938 | 0.831 |
| 572 | EM | cart | Parsons | Blind Grid | 24 to 36 | 35.937 | 0.394 |
| 572 | EM | cart | Parsons | Blind Grid | 36 to 48 | 40.838 | 0.817 |
| 411 | EM | cart | Parsons | Wet Probe | 0 to 6 | 64.585 | 0.549 |
| 411 | EM | cart | Parsons | Wet Probe | 6 to 12 | 73.3 | 0.522 |
| 411 | EM | cart | Parsons | Wet Probe | 12 to 24 | 77.1 | 0.621 |
| 411 | EM | cart | Parsons | Wet Probe | 24 to 36 | 54.235 | 0.662 |
| 411 | EM | cart | Parsons | Wet Probe | 36 to 48 | 53.355 | 0.466 |
| 411 | EM | cart | Parsons | Woods | 0 to 6 | 13.3 | 0.818 |
| 411 | EM | cart | Parsons | Woods | 6 to 12 | 6.3 | 0.46 |
| 411 | EM | cart | Parsons | Woods | 12 to 24 | 6.771 | 0.198 |
| 411 | EM | cart | Parsons | Woods | 24 to 36 | 57.786 | 0.264 |
| 411 | EM | cart | Parsons | Woods | 36 to 48 | 59.371 | 0.377 |
| 411 | EM | cart | Parsons | Open Field | 0 to 6 | 20.37 | 0.603 |
| 411 | EM | cart | Parsons | Open Field | 6 to 12 | 7.535 | 0.338 |
| 411 | EM | cart | Parsons | Open Field | 12 to 24 | 21.445 | 0.264 |
| 411 | EM | cart | Parsons | Open Field | 24 to 36 | 28.25 | 0.398 |
| 411 | EM | cart | Parsons | Open Field | 36 to 48 | 54.56 | 0.365 |
| 411 | EM | cart | Parsons | Calibration | 0 to 6 | 2.05 | 0.75 |
| 411 | EM | cart | Parsons | Calibration | 6 to 12 | 14.95 | 0.65 |
| 411 | EM | cart | Parsons | Calibration | 12 to 24 | 25.05 | 0.65 |
| 411 | EM | cart | Parsons | Calibration | 24 to 36 | 32.2 | 1.3 |
| 411 | EM | cart | Parsons | Calibration | 36 to 48 | 38.1 | 1 |
| 411 | EM | cart | Parsons | Blind Grid | 0 to 6 | 5.162 | 0.908 |
| 411 | EM | cart | Parsons | Blind Grid | 6 to 12 | 1.675 | 0.614 |
| 411 | EM | cart | Parsons | Blind Grid | 12 to 24 | 25.938 | 0.831 |
| 411 | EM | cart | Parsons | Blind Grid | 24 to 36 | 35.937 | 0.394 |
| 411 | EM | cart | Parsons | Blind Grid | 36 to 48 | 40.838 | 0.817 |
| 496 | EM | cart | Parsons | Wet Probe | 0 to 6 | 64.585 | 0.549 |
| 496 | EM | cart | Parsons | Wet Probe | 6 to 12 | 73.3 | 0.522 |
| 496 | EM | cart | Parsons | Wet Probe | 12 to 24 | 77.1 | 0.621 |
| 496 | EM | cart | Parsons | Wet Probe | 24 to 36 | 54.235 | 0.662 |
| 496 | EM | cart | Parsons | Wet Probe | 36 to 48 | 53.355 | 0.466 |
| 496 | EM | cart | Parsons | Woods | 0 to 6 | 13.3 | 0.818 |
| 496 | EM | cart | Parsons | Woods | 6 to 12 | 6.3 | 0.46 |
| 496 | EM | cart | Parsons | Woods | 12 to 24 | 6.771 | 0.198 |
| 496 | EM | cart | Parsons | Woods | 24 to 36 | 57.786 | 0.264 |
| 496 | EM | cart | Parsons | Woods | 36 to 48 | 59.371 | 0.377 |
| 496 | EM | cart | Parsons | Open Field | 0 to 6 | 20.37 | 0.603 |
| 496 | EM | cart | Parsons | Open Field | 6 to 12 | 7.535 | 0.338 |
| 496 | EM | cart | Parsons | Open Field | 12 to 24 | 21.445 | 0.264 |
| 496 | EM | cart | Parsons | Open Field | 24 to 36 | 28.25 | 0.398 |
| 496 | EM | cart | Parsons | Open Field | 36 to 48 | 54.56 | 0.365 |
| 496 | EM | cart | Parsons | Calibration | 0 to 6 | 2.05 | 0.75 |
| 496 | EM | cart | Parsons | Calibration | 6 to 12 | 14.95 | 0.65 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 496 | EM | cart | Parsons | Calibration | 12 to 24 | 25.05 | 0.65 |
| 496 | EM | cart | Parsons | Calibration | 24 to 36 | 32.2 | 1.3 |
| 496 | EM | cart | Parsons | Calibration | 36 to 48 | 38.1 | 1 |
| 496 | EM | cart | Parsons | Blind Grid | 0 to 6 | 5.162 | 0.908 |
| 496 | EM | cart | Parsons | Blind Grid | 6 to 12 | 1.675 | 0.614 |
| 496 | EM | cart | Parsons | Blind Grid | 12 to 24 | 25.938 | 0.831 |
| 496 | EM | cart | Parsons | Blind Grid | 24 to 36 | 35.937 | 0.394 |
| 496 | EM | cart | Parsons | Blind Grid | 36 to 48 | 40.838 | 0.817 |
| 257 | MAG | hand | Parsons | Wet Probe | 0 to 6 | 64.585 | 0.549 |
| 257 | MAG | hand | Parsons | Wet Probe | 6 to 12 | 73.3 | 0.522 |
| 257 | MAG | hand | Parsons | Wet Probe | 12 to 24 | 77.1 | 0.621 |
| 257 | MAG | hand | Parsons | Wet Probe | 24 to 36 | 54.235 | 0.662 |
| 257 | MAG | hand | Parsons | Wet Probe | 36 to 48 | 53.355 | 0.466 |
| 257 | MAG | hand | Parsons | Woods | 0 to 6 | 13.3 | 0.818 |
| 257 | MAG | hand | Parsons | Woods | 6 to 12 | 6.3 | 0.46 |
| 257 | MAG | hand | Parsons | Woods | 12 to 24 | 6.771 | 0.198 |
| 257 | MAG | hand | Parsons | Woods | 24 to 36 | 57.786 | 0.264 |
| 257 | MAG | hand | Parsons | Woods | 36 to 48 | 59.371 | 0.377 |
| 257 | MAG | hand | Parsons | Open Field | 0 to 6 | 20.37 | 0.603 |
| 257 | MAG | hand | Parsons | Open Field | 6 to 12 | 7.535 | 0.338 |
| 257 | MAG | hand | Parsons | Open Field | 12 to 24 | 21.445 | 0.264 |
| 257 | MAG | hand | Parsons | Open Field | 24 to 36 | 28.25 | 0.398 |
| 257 | MAG | hand | Parsons | Open Field | 36 to 48 | 54.56 | 0.365 |
| 257 | MAG | hand | Parsons | Calibration | 0 to 6 | 2.05 | 0.75 |
| 257 | MAG | hand | Parsons | Calibration | 6 to 12 | 14.95 | 0.65 |
| 257 | MAG | hand | Parsons | Calibration | 12 to 24 | 25.05 | 0.65 |
| 257 | MAG | hand | Parsons | Calibration | 24 to 36 | 32.2 | 1.3 |
| 257 | MAG | hand | Parsons | Calibration | 36 to 48 | 38.1 | 1 |
| 257 | MAG | hand | Parsons | Blind Grid | 0 to 6 | 5.162 | 0.908 |
| 257 | MAG | hand | Parsons | Blind Grid | 6 to 12 | 1.675 | 0.614 |
| 257 | MAG | hand | Parsons | Blind Grid | 12 to 24 | 25.938 | 0.831 |
| 257 | MAG | hand | Parsons | Blind Grid | 24 to 36 | 35.937 | 0.394 |
| 257 | MAG | hand | Parsons | Blind Grid | 36 to 48 | 40.838 | 0.817 |
| 573 | MAG | hand | Parsons | Wet Probe | 0 to 6 | 64.585 | 0.549 |
| 573 | MAG | hand | Parsons | Wet Probe | 6 to 12 | 73.3 | 0.522 |
| 573 | MAG | hand | Parsons | Wet Probe | 12 to 24 | 77.1 | 0.621 |
| 573 | MAG | hand | Parsons | Wet Probe | 24 to 36 | 54.235 | 0.662 |
| 573 | MAG | hand | Parsons | Wet Probe | 36 to 48 | 53.355 | 0.466 |
| 573 | MAG | hand | Parsons | Woods | 0 to 6 | 13.3 | 0.818 |
| 573 | MAG | hand | Parsons | Woods | 6 to 12 | 6.3 | 0.46 |
| 573 | MAG | hand | Parsons | Woods | 12 to 24 | 6.771 | 0.198 |
| 573 | MAG | hand | Parsons | Woods | 24 to 36 | 57.786 | 0.264 |
| 573 | MAG | hand | Parsons | Woods | 36 to 48 | 59.371 | 0.377 |
| 573 | MAG | hand | Parsons | Open Field | 0 to 6 | 20.37 | 0.603 |
| 573 | MAG | hand | Parsons | Open Field | 6 to 12 | 7.535 | 0.338 |
| 573 | MAG | hand | Parsons | Open Field | 12 to 24 | 21.445 | 0.264 |
| 573 | MAG | hand | Parsons | Open Field | 24 to 36 | 28.25 | 0.398 |
| 573 | MAG | hand | Parsons | Open Field | 36 to 48 | 54.56 | 0.365 |
| 573 | MAG | hand | Parsons | Calibration | 0 to 6 | 2.05 | 0.75 |
| 573 | MAG | hand | Parsons | Calibration | 6 to 12 | 14.95 | 0.65 |

Aberdeen Proving Ground Demonstrations

| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
|---------------|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| 573 | MAG | hand | Parsons | Calibration | 12 to 24 | 25.05 | 0.65 |
| 573 | MAG | hand | Parsons | Calibration | 24 to 36 | 32.2 | 1.3 |
| 573 | MAG | hand | Parsons | Calibration | 36 to 48 | 38.1 | 1 |
| 573 | MAG | hand | Parsons | Blind Grid | 0 to 6 | 5.162 | 0.908 |
| 573 | MAG | hand | Parsons | Blind Grid | 6 to 12 | 1.675 | 0.614 |
| 573 | MAG | hand | Parsons | Blind Grid | 12 to 24 | 25.938 | 0.831 |
| 573 | MAG | hand | Parsons | Blind Grid | 24 to 36 | 35.937 | 0.394 |
| 573 | MAG | hand | Parsons | Blind Grid | 36 to 48 | 40.838 | 0.817 |
| 229 | MAG | hand | Parsons | Wet Probe | 0 to 6 | 64.585 | 0.549 |
| 229 | MAG | hand | Parsons | Wet Probe | 6 to 12 | 73.3 | 0.522 |
| 229 | MAG | hand | Parsons | Wet Probe | 12 to 24 | 77.1 | 0.621 |
| 229 | MAG | hand | Parsons | Wet Probe | 24 to 36 | 54.235 | 0.662 |
| 229 | MAG | hand | Parsons | Wet Probe | 36 to 48 | 53.355 | 0.466 |
| 229 | MAG | hand | Parsons | Woods | 0 to 6 | 13.3 | 0.818 |
| 229 | MAG | hand | Parsons | Woods | 6 to 12 | 6.3 | 0.46 |
| 229 | MAG | hand | Parsons | Woods | 12 to 24 | 6.771 | 0.198 |
| 229 | MAG | hand | Parsons | Woods | 24 to 36 | 57.786 | 0.264 |
| 229 | MAG | hand | Parsons | Woods | 36 to 48 | 59.371 | 0.377 |
| 229 | MAG | hand | Parsons | Open Field | 0 to 6 | 20.37 | 0.603 |
| 229 | MAG | hand | Parsons | Open Field | 6 to 12 | 7.535 | 0.338 |
| 229 | MAG | hand | Parsons | Open Field | 12 to 24 | 21.445 | 0.264 |
| 229 | MAG | hand | Parsons | Open Field | 24 to 36 | 28.25 | 0.398 |
| 229 | MAG | hand | Parsons | Open Field | 36 to 48 | 54.56 | 0.365 |
| 229 | MAG | hand | Parsons | Calibration | 0 to 6 | 2.05 | 0.75 |
| 229 | MAG | hand | Parsons | Calibration | 6 to 12 | 14.95 | 0.65 |
| 229 | MAG | hand | Parsons | Calibration | 12 to 24 | 25.05 | 0.65 |
| 229 | MAG | hand | Parsons | Calibration | 24 to 36 | 32.2 | 1.3 |
| 229 | MAG | hand | Parsons | Calibration | 36 to 48 | 38.1 | 1 |
| 229 | MAG | hand | Parsons | Blind Grid | 0 to 6 | 5.162 | 0.908 |
| 229 | MAG | hand | Parsons | Blind Grid | 6 to 12 | 1.675 | 0.614 |
| 229 | MAG | hand | Parsons | Blind Grid | 12 to 24 | 25.938 | 0.831 |
| 229 | MAG | hand | Parsons | Blind Grid | 24 to 36 | 35.937 | 0.394 |
| 229 | MAG | hand | Parsons | Blind Grid | 36 to 48 | 40.838 | 0.817 |
| 499 | MAG | hand | Parsons | Wet Probe | 0 to 6 | 64.585 | 0.549 |
| 499 | MAG | hand | Parsons | Wet Probe | 6 to 12 | 73.3 | 0.522 |
| 499 | MAG | hand | Parsons | Wet Probe | 12 to 24 | 77.1 | 0.621 |
| 499 | MAG | hand | Parsons | Wet Probe | 24 to 36 | 54.235 | 0.662 |
| 499 | MAG | hand | Parsons | Wet Probe | 36 to 48 | 53.355 | 0.466 |
| 499 | MAG | hand | Parsons | Woods | 0 to 6 | 13.3 | 0.818 |
| 499 | MAG | hand | Parsons | Woods | 6 to 12 | 6.3 | 0.46 |
| 499 | MAG | hand | Parsons | Woods | 12 to 24 | 6.771 | 0.198 |
| 499 | MAG | hand | Parsons | Woods | 24 to 36 | 57.786 | 0.264 |
| 499 | MAG | hand | Parsons | Woods | 36 to 48 | 59.371 | 0.377 |
| 499 | MAG | hand | Parsons | Open Field | 0 to 6 | 20.37 | 0.603 |
| 499 | MAG | hand | Parsons | Open Field | 6 to 12 | 7.535 | 0.338 |
| 499 | MAG | hand | Parsons | Open Field | 12 to 24 | 21.445 | 0.264 |
| 499 | MAG | hand | Parsons | Open Field | 24 to 36 | 28.25 | 0.398 |
| 499 | MAG | hand | Parsons | Open Field | 36 to 48 | 54.56 | 0.365 |
| 499 | MAG | hand | Parsons | Calibration | 0 to 6 | 2.05 | 0.75 |
| 499 | MAG | hand | Parsons | Calibration | 6 to 12 | 14.95 | 0.65 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 499 | MAG | hand | Parsons | Calibration | 12 to 24 | 25.05 | 0.65 |
| 499 | MAG | hand | Parsons | Calibration | 24 to 36 | 32.2 | 1.3 |
| 499 | MAG | hand | Parsons | Calibration | 36 to 48 | 38.1 | 1 |
| 499 | MAG | hand | Parsons | Blind Grid | 0 to 6 | 5.162 | 0.908 |
| 499 | MAG | hand | Parsons | Blind Grid | 6 to 12 | 1.675 | 0.614 |
| 499 | MAG | hand | Parsons | Blind Grid | 12 to 24 | 25.938 | 0.831 |
| 499 | MAG | hand | Parsons | Blind Grid | 24 to 36 | 35.937 | 0.394 |
| 499 | MAG | hand | Parsons | Blind Grid | 36 to 48 | 40.838 | 0.817 |
| 197 | EM | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 197 | EM | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 197 | EM | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 197 | EM | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 197 | EM | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 197 | EM | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 197 | EM | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 197 | EM | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 197 | EM | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 197 | EM | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 197 | EM | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 197 | EM | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 197 | EM | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 197 | EM | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 197 | EM | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 197 | EM | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 197 | EM | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |
| 197 | EM | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 197 | EM | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 197 | EM | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 197 | EM | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 197 | EM | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 197 | EM | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 197 | EM | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 197 | EM | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 552 | EM | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 552 | EM | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 552 | EM | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 552 | EM | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 552 | EM | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 552 | EM | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 552 | EM | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 552 | EM | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 552 | EM | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 552 | EM | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 552 | EM | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 552 | EM | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 552 | EM | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 552 | EM | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 552 | EM | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 552 | EM | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 552 | EM | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 552 | EM | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 552 | EM | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 552 | EM | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 552 | EM | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 552 | EM | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 552 | EM | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 552 | EM | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 552 | EM | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 201 | EM | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 201 | EM | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 201 | EM | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 201 | EM | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 201 | EM | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 201 | EM | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 201 | EM | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 201 | EM | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 201 | EM | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 201 | EM | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 201 | EM | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 201 | EM | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 201 | EM | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 201 | EM | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 201 | EM | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 201 | EM | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 201 | EM | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |
| 201 | EM | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 201 | EM | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 201 | EM | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 201 | EM | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 201 | EM | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 201 | EM | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 201 | EM | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 201 | EM | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 461 | EM | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 461 | EM | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 461 | EM | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 461 | EM | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 461 | EM | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 461 | EM | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 461 | EM | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 461 | EM | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 461 | EM | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 461 | EM | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 461 | EM | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 461 | EM | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 461 | EM | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 461 | EM | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 461 | EM | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 461 | EM | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 461 | EM | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 461 | EM | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 461 | EM | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 461 | EM | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 461 | EM | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 461 | EM | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 461 | EM | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 461 | EM | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 461 | EM | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 198 | MAG | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 198 | MAG | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 198 | MAG | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 198 | MAG | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 198 | MAG | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 198 | MAG | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 198 | MAG | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 198 | MAG | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 198 | MAG | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 198 | MAG | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 198 | MAG | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 198 | MAG | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 198 | MAG | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 198 | MAG | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 198 | MAG | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 198 | MAG | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 198 | MAG | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |
| 198 | MAG | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 198 | MAG | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 198 | MAG | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 198 | MAG | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 198 | MAG | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 198 | MAG | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 198 | MAG | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 198 | MAG | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 404 | MAG | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 404 | MAG | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 404 | MAG | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 404 | MAG | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 404 | MAG | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 404 | MAG | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 404 | MAG | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 404 | MAG | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 404 | MAG | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 404 | MAG | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 404 | MAG | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 404 | MAG | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 404 | MAG | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 404 | MAG | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 404 | MAG | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 404 | MAG | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 404 | MAG | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 404 | MAG | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 404 | MAG | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 404 | MAG | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 404 | MAG | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 404 | MAG | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 404 | MAG | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 404 | MAG | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 404 | MAG | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 206 | MAG | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 206 | MAG | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 206 | MAG | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 206 | MAG | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 206 | MAG | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 206 | MAG | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 206 | MAG | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 206 | MAG | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 206 | MAG | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 206 | MAG | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 206 | MAG | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 206 | MAG | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 206 | MAG | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 206 | MAG | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 206 | MAG | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 206 | MAG | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 206 | MAG | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |
| 206 | MAG | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 206 | MAG | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 206 | MAG | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 206 | MAG | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 206 | MAG | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 206 | MAG | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 206 | MAG | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 206 | MAG | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 492 | MAG | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 492 | MAG | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 492 | MAG | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 492 | MAG | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 492 | MAG | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 492 | MAG | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 492 | MAG | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 492 | MAG | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 492 | MAG | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 492 | MAG | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 492 | MAG | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 492 | MAG | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 492 | MAG | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 492 | MAG | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 492 | MAG | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 492 | MAG | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 492 | MAG | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 492 | MAG | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 492 | MAG | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 492 | MAG | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 492 | MAG | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 492 | MAG | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 492 | MAG | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 492 | MAG | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 492 | MAG | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 376 | MAG | cart | Shaw | Wet Probe | 0 to 6 | 88.072 | 0.881 |
| 376 | MAG | cart | Shaw | Wet Probe | 6 to 12 | 79.1 | 0.399 |
| 376 | MAG | cart | Shaw | Wet Probe | 12 to 24 | 70.056 | 0.679 |
| 376 | MAG | cart | Shaw | Wet Probe | 24 to 36 | 54.706 | 1.397 |
| 376 | MAG | cart | Shaw | Wet Probe | 36 to 48 | 51.606 | 1.306 |
| 376 | MAG | cart | Shaw | Woods | 0 to 6 | 79.883 | 0.318 |
| 376 | MAG | cart | Shaw | Woods | 6 to 12 | 69.75 | 0.678 |
| 376 | MAG | cart | Shaw | Woods | 12 to 24 | 94.017 | 0.414 |
| 376 | MAG | cart | Shaw | Woods | 24 to 36 | 68.517 | 0.515 |
| 376 | MAG | cart | Shaw | Woods | 36 to 48 | 58.867 | 0.309 |
| 376 | MAG | cart | Shaw | Open Field | 0 to 6 | 23.111 | 0.401 |
| 376 | MAG | cart | Shaw | Open Field | 6 to 12 | 3.461 | 0.73 |
| 376 | MAG | cart | Shaw | Open Field | 12 to 24 | 39.472 | 0.323 |
| 376 | MAG | cart | Shaw | Open Field | 24 to 36 | 60.911 | 0.683 |
| 376 | MAG | cart | Shaw | Open Field | 36 to 48 | 57.644 | 0.905 |
| 376 | MAG | cart | Shaw | Calibration | 0 to 6 | 39.5 | 0 |
| 376 | MAG | cart | Shaw | Calibration | 6 to 12 | 36.3 | 0 |
| 376 | MAG | cart | Shaw | Calibration | 12 to 24 | 7.7 | 0 |
| 376 | MAG | cart | Shaw | Calibration | 24 to 36 | 5.6 | 0 |
| 376 | MAG | cart | Shaw | Calibration | 36 to 48 | 5.8 | 0 |
| 376 | MAG | cart | Shaw | Blind Grid | 0 to 6 | 3.95 | 0.112 |
| 376 | MAG | cart | Shaw | Blind Grid | 6 to 12 | 17.075 | 0.164 |
| 376 | MAG | cart | Shaw | Blind Grid | 12 to 24 | 39.4 | 0.235 |
| 376 | MAG | cart | Shaw | Blind Grid | 24 to 36 | 41.05 | 0.572 |
| 376 | MAG | cart | Shaw | Blind Grid | 36 to 48 | 42 | 0.158 |
| 157 | EM | cart | TTF | Wet Probe | 0 to 6 | 85.875 | 3.549 |
| 157 | EM | cart | TTF | Wet Probe | 6 to 12 | 79.7 | 2.765 |
| 157 | EM | cart | TTF | Wet Probe | 12 to 24 | 72.625 | 2.24 |
| 157 | EM | cart | TTF | Wet Probe | 24 to 36 | 54.012 | 1.161 |
| 157 | EM | cart | TTF | Wet Probe | 36 to 48 | 50.213 | 0.878 |
| 157 | EM | cart | TTF | Woods | 0 to 6 | 82.65 | 7.577 |
| 157 | EM | cart | TTF | Woods | 6 to 12 | 68.55 | 5.752 |
| 157 | EM | cart | TTF | Woods | 12 to 24 | 92.8 | 1.002 |
| 157 | EM | cart | TTF | Woods | 24 to 36 | 66.35 | 1.404 |
| 157 | EM | cart | TTF | Woods | 36 to 48 | 60.775 | 3.031 |
| 157 | EM | cart | TTF | Open Field | 0 to 6 | 19.855 | 3.09 |
| 157 | EM | cart | TTF | Open Field | 6 to 12 | 1.964 | 0.808 |
| 157 | EM | cart | TTF | Open Field | 12 to 24 | 25.118 | 10.59 |
| 157 | EM | cart | TTF | Open Field | 24 to 36 | 33.291 | 19.37 |
| 157 | EM | cart | TTF | Open Field | 36 to 48 | 41.018 | 10.798 |
| 157 | EM | cart | TTF | Calibration | 0 to 6 | 24.9 | 13.8 |
| 157 | EM | cart | TTF | Calibration | 6 to 12 | 37.3 | 0.4 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 157 | EM | cart | TTF | Calibration | 12 to 24 | 8.1 | 0.3 |
| 157 | EM | cart | TTF | Calibration | 24 to 36 | 4.8 | 0.3 |
| 157 | EM | cart | TTF | Calibration | 36 to 48 | 4.95 | 0.35 |
| 157 | EM | cart | TTF | Blind Grid | 0 to 6 | 2.35 | 0.112 |
| 157 | EM | cart | TTF | Blind Grid | 6 to 12 | 24.55 | 9.711 |
| 157 | EM | cart | TTF | Blind Grid | 12 to 24 | 36.65 | 0.594 |
| 157 | EM | cart | TTF | Blind Grid | 24 to 36 | 36.425 | 0.303 |
| 157 | EM | cart | TTF | Blind Grid | 36 to 48 | 38.275 | 0.179 |
| 159 | EM | sling | TTF | Wet Probe | 0 to 6 | 85.875 | 3.549 |
| 159 | EM | sling | TTF | Wet Probe | 6 to 12 | 79.7 | 2.765 |
| 159 | EM | sling | TTF | Wet Probe | 12 to 24 | 72.625 | 2.24 |
| 159 | EM | sling | TTF | Wet Probe | 24 to 36 | 54.012 | 1.161 |
| 159 | EM | sling | TTF | Wet Probe | 36 to 48 | 50.213 | 0.878 |
| 159 | EM | sling | TTF | Woods | 0 to 6 | 82.65 | 7.577 |
| 159 | EM | sling | TTF | Woods | 6 to 12 | 68.55 | 5.752 |
| 159 | EM | sling | TTF | Woods | 12 to 24 | 92.8 | 1.002 |
| 159 | EM | sling | TTF | Woods | 24 to 36 | 66.35 | 1.404 |
| 159 | EM | sling | TTF | Woods | 36 to 48 | 60.775 | 3.031 |
| 159 | EM | sling | TTF | Open Field | 0 to 6 | 19.855 | 3.09 |
| 159 | EM | sling | TTF | Open Field | 6 to 12 | 1.964 | 0.808 |
| 159 | EM | sling | TTF | Open Field | 12 to 24 | 25.118 | 10.59 |
| 159 | EM | sling | TTF | Open Field | 24 to 36 | 33.291 | 19.37 |
| 159 | EM | sling | TTF | Open Field | 36 to 48 | 41.018 | 10.798 |
| 159 | EM | sling | TTF | Calibration | 0 to 6 | 24.9 | 13.8 |
| 159 | EM | sling | TTF | Calibration | 6 to 12 | 37.3 | 0.4 |
| 159 | EM | sling | TTF | Calibration | 12 to 24 | 8.1 | 0.3 |
| 159 | EM | sling | TTF | Calibration | 24 to 36 | 4.8 | 0.3 |
| 159 | EM | sling | TTF | Calibration | 36 to 48 | 4.95 | 0.35 |
| 159 | EM | sling | TTF | Blind Grid | 0 to 6 | 2.35 | 0.112 |
| 159 | EM | sling | TTF | Blind Grid | 6 to 12 | 24.55 | 9.711 |
| 159 | EM | sling | TTF | Blind Grid | 12 to 24 | 36.65 | 0.594 |
| 159 | EM | sling | TTF | Blind Grid | 24 to 36 | 36.425 | 0.303 |
| 159 | EM | sling | TTF | Blind Grid | 36 to 48 | 38.275 | 0.179 |
| 549 | EM | sling | TTF | Wet Probe | 0 to 6 | 85.875 | 3.549 |
| 549 | EM | sling | TTF | Wet Probe | 6 to 12 | 79.7 | 2.765 |
| 549 | EM | sling | TTF | Wet Probe | 12 to 24 | 72.625 | 2.24 |
| 549 | EM | sling | TTF | Wet Probe | 24 to 36 | 54.012 | 1.161 |
| 549 | EM | sling | TTF | Wet Probe | 36 to 48 | 50.213 | 0.878 |
| 549 | EM | sling | TTF | Woods | 0 to 6 | 82.65 | 7.577 |
| 549 | EM | sling | TTF | Woods | 6 to 12 | 68.55 | 5.752 |
| 549 | EM | sling | TTF | Woods | 12 to 24 | 92.8 | 1.002 |
| 549 | EM | sling | TTF | Woods | 24 to 36 | 66.35 | 1.404 |
| 549 | EM | sling | TTF | Woods | 36 to 48 | 60.775 | 3.031 |
| 549 | EM | sling | TTF | Open Field | 0 to 6 | 19.855 | 3.09 |
| 549 | EM | sling | TTF | Open Field | 6 to 12 | 1.964 | 0.808 |
| 549 | EM | sling | TTF | Open Field | 12 to 24 | 25.118 | 10.59 |
| 549 | EM | sling | TTF | Open Field | 24 to 36 | 33.291 | 19.37 |
| 549 | EM | sling | TTF | Open Field | 36 to 48 | 41.018 | 10.798 |
| 549 | EM | sling | TTF | Calibration | 0 to 6 | 24.9 | 13.8 |
| 549 | EM | sling | TTF | Calibration | 6 to 12 | 37.3 | 0.4 |

Aberdeen Proving Ground Demonstrations

| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
|---------------|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| 549 | EM | sling | TTF | Calibration | 12 to 24 | 8.1 | 0.3 |
| 549 | EM | sling | TTF | Calibration | 24 to 36 | 4.8 | 0.3 |
| 549 | EM | sling | TTF | Calibration | 36 to 48 | 4.95 | 0.35 |
| 549 | EM | sling | TTF | Blind Grid | 0 to 6 | 2.35 | 0.112 |
| 549 | EM | sling | TTF | Blind Grid | 6 to 12 | 24.55 | 9.711 |
| 549 | EM | sling | TTF | Blind Grid | 12 to 24 | 36.65 | 0.594 |
| 549 | EM | sling | TTF | Blind Grid | 24 to 36 | 36.425 | 0.303 |
| 549 | EM | sling | TTF | Blind Grid | 36 to 48 | 38.275 | 0.179 |
| 165 | EM | cart | TTF | Wet Probe | 0 to 6 | 85.875 | 3.549 |
| 165 | EM | cart | TTF | Wet Probe | 6 to 12 | 79.7 | 2.765 |
| 165 | EM | cart | TTF | Wet Probe | 12 to 24 | 72.625 | 2.24 |
| 165 | EM | cart | TTF | Wet Probe | 24 to 36 | 54.012 | 1.161 |
| 165 | EM | cart | TTF | Wet Probe | 36 to 48 | 50.213 | 0.878 |
| 165 | EM | cart | TTF | Woods | 0 to 6 | 82.65 | 7.577 |
| 165 | EM | cart | TTF | Woods | 6 to 12 | 68.55 | 5.752 |
| 165 | EM | cart | TTF | Woods | 12 to 24 | 92.8 | 1.002 |
| 165 | EM | cart | TTF | Woods | 24 to 36 | 66.35 | 1.404 |
| 165 | EM | cart | TTF | Woods | 36 to 48 | 60.775 | 3.031 |
| 165 | EM | cart | TTF | Open Field | 0 to 6 | 19.855 | 3.09 |
| 165 | EM | cart | TTF | Open Field | 6 to 12 | 1.964 | 0.808 |
| 165 | EM | cart | TTF | Open Field | 12 to 24 | 25.118 | 10.59 |
| 165 | EM | cart | TTF | Open Field | 24 to 36 | 33.291 | 19.37 |
| 165 | EM | cart | TTF | Open Field | 36 to 48 | 41.018 | 10.798 |
| 165 | EM | cart | TTF | Calibration | 0 to 6 | 24.9 | 13.8 |
| 165 | EM | cart | TTF | Calibration | 6 to 12 | 37.3 | 0.4 |
| 165 | EM | cart | TTF | Calibration | 12 to 24 | 8.1 | 0.3 |
| 165 | EM | cart | TTF | Calibration | 24 to 36 | 4.8 | 0.3 |
| 165 | EM | cart | TTF | Calibration | 36 to 48 | 4.95 | 0.35 |
| 165 | EM | cart | TTF | Blind Grid | 0 to 6 | 2.35 | 0.112 |
| 165 | EM | cart | TTF | Blind Grid | 6 to 12 | 24.55 | 9.711 |
| 165 | EM | cart | TTF | Blind Grid | 12 to 24 | 36.65 | 0.594 |
| 165 | EM | cart | TTF | Blind Grid | 24 to 36 | 36.425 | 0.303 |
| 165 | EM | cart | TTF | Blind Grid | 36 to 48 | 38.275 | 0.179 |
| 457 | EM | sling | TTF | Wet Probe | 0 to 6 | 85.875 | 3.549 |
| 457 | EM | sling | TTF | Wet Probe | 6 to 12 | 79.7 | 2.765 |
| 457 | EM | sling | TTF | Wet Probe | 12 to 24 | 72.625 | 2.24 |
| 457 | EM | sling | TTF | Wet Probe | 24 to 36 | 54.012 | 1.161 |
| 457 | EM | sling | TTF | Wet Probe | 36 to 48 | 50.213 | 0.878 |
| 457 | EM | sling | TTF | Woods | 0 to 6 | 82.65 | 7.577 |
| 457 | EM | sling | TTF | Woods | 6 to 12 | 68.55 | 5.752 |
| 457 | EM | sling | TTF | Woods | 12 to 24 | 92.8 | 1.002 |
| 457 | EM | sling | TTF | Woods | 24 to 36 | 66.35 | 1.404 |
| 457 | EM | sling | TTF | Woods | 36 to 48 | 60.775 | 3.031 |
| 457 | EM | sling | TTF | Open Field | 0 to 6 | 19.855 | 3.09 |
| 457 | EM | sling | TTF | Open Field | 6 to 12 | 1.964 | 0.808 |
| 457 | EM | sling | TTF | Open Field | 12 to 24 | 25.118 | 10.59 |
| 457 | EM | sling | TTF | Open Field | 24 to 36 | 33.291 | 19.37 |
| 457 | EM | sling | TTF | Open Field | 36 to 48 | 41.018 | 10.798 |
| 457 | EM | sling | TTF | Calibration | 0 to 6 | 24.9 | 13.8 |
| 457 | EM | sling | TTF | Calibration | 6 to 12 | 37.3 | 0.4 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 457 | EM | sling | TTF | Calibration | 12 to 24 | 8.1 | 0.3 |
| 457 | EM | sling | TTF | Calibration | 24 to 36 | 4.8 | 0.3 |
| 457 | EM | sling | TTF | Calibration | 36 to 48 | 4.95 | 0.35 |
| 457 | EM | sling | TTF | Blind Grid | 0 to 6 | 2.35 | 0.112 |
| 457 | EM | sling | TTF | Blind Grid | 6 to 12 | 24.55 | 9.711 |
| 457 | EM | sling | TTF | Blind Grid | 12 to 24 | 36.65 | 0.594 |
| 457 | EM | sling | TTF | Blind Grid | 24 to 36 | 36.425 | 0.303 |
| 457 | EM | sling | TTF | Blind Grid | 36 to 48 | 38.275 | 0.179 |
| 764 | EM | towed | VF Warner | Wet Probe | 0 to 6 | 0 | 0 |
| 764 | EM | towed | VF Warner | Wet Probe | 6 to 12 | 0 | 0 |
| 764 | EM | towed | VF Warner | Wet Probe | 12 to 24 | 0 | 0 |
| 764 | EM | towed | VF Warner | Wet Probe | 24 to 36 | 0 | 0 |
| 764 | EM | towed | VF Warner | Wet Probe | 36 to 48 | 0 | 0 |
| 764 | EM | towed | VF Warner | Woods | 0 to 6 | 0 | 0 |
| 764 | EM | towed | VF Warner | Woods | 6 to 12 | 0 | 0 |
| 764 | EM | towed | VF Warner | Woods | 12 to 24 | 0 | 0 |
| 764 | EM | towed | VF Warner | Woods | 24 to 36 | 0 | 0 |
| 764 | EM | towed | VF Warner | Woods | 36 to 48 | 0 | 0 |
| 764 | EM | towed | VF Warner | Open Field | 0 to 6 | 0 | 0 |
| 764 | EM | towed | VF Warner | Open Field | 6 to 12 | 0 | 0 |
| 764 | EM | towed | VF Warner | Open Field | 12 to 24 | 0 | 0 |
| 764 | EM | towed | VF Warner | Open Field | 24 to 36 | 0 | 0 |
| 764 | EM | towed | VF Warner | Open Field | 36 to 48 | 0 | 0 |
| 764 | EM | towed | VF Warner | Calibration | 0 to 6 | 2.9 | 0 |
| 764 | EM | towed | VF Warner | Calibration | 6 to 12 | 15.8 | 0 |
| 764 | EM | towed | VF Warner | Calibration | 12 to 24 | 24.8 | 0 |
| 764 | EM | towed | VF Warner | Calibration | 24 to 36 | 28.85 | 0 |
| 764 | EM | towed | VF Warner | Blind Grid | 0 to 6 | 3.55 | 0 |
| 764 | EM | towed | VF Warner | Blind Grid | 6 to 12 | 5.85 | 0 |
| 764 | EM | towed | VF Warner | Blind Grid | 12 to 24 | 1251.4 | 0 |
| 764 | EM | towed | VF Warner | Blind Grid | 24 to 36 | 5.05 | 0 |
| 764 | EM | towed | VF Warner | Blind Grid | 36 to 48 | 4.55 | 0 |
| 45 | GPR | cart | Witten | Open Field | 0 to 6 | 12.4 | 2.45 |
| 45 | GPR | cart | Witten | Open Field | 6 to 12 | 4.43 | 5.08 |
| 45 | GPR | cart | Witten | Open Field | 12 to 24 | 6.87 | 3.71 |
| 45 | GPR | cart | Witten | Open Field | 24 to 36 | 20.8 | 2.38 |
| 45 | GPR | cart | Witten | Open Field | 36 to 48 | 28.3 | 2.95 |
| 126 | GPR | cart | Witten | Open Field | 0 to 6 | 12.4 | 2.45 |
| 126 | GPR | cart | Witten | Open Field | 6 to 12 | 4.43 | 5.08 |
| 126 | GPR | cart | Witten | Open Field | 12 to 24 | 6.87 | 3.71 |
| 126 | GPR | cart | Witten | Open Field | 24 to 36 | 20.8 | 2.38 |
| 126 | GPR | cart | Witten | Open Field | 36 to 48 | 28.3 | 2.95 |
| 37 | EM | cart | Zonge | Open Field | 0 to 6 | 13.71 | 10.15 |
| 37 | EM | cart | Zonge | Open Field | 6 to 12 | 6.85 | 4.45 |
| 37 | EM | cart | Zonge | Open Field | 12 to 24 | 1.8 | 0.23 |
| 37 | EM | cart | Zonge | Open Field | 24 to 36 | 4.4 | 1.25 |
| 37 | EM | cart | Zonge | Open Field | 36 to 48 | 0.18 | 0.15 |
| 37 | EM | cart | Zonge | Wet Probe | 0 to 6 | 20.11 | 9.31 |
| 37 | EM | cart | Zonge | Wet Probe | 6 to 12 | 12.25 | 3.68 |
| 37 | EM | cart | Zonge | Wet Probe | 12 to 24 | 12.53 | 1.8 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 37 | EM | cart | Zonge | Wet Probe | 24 to 36 | 30.61 | 2.98 |
| 37 | EM | cart | Zonge | Wet Probe | 36 to 48 | 36.4 | 1.68 |
| 38 | EM | cart | Zonge | Open Field | 0 to 6 | 13.5 | 9.79 |
| 38 | EM | cart | Zonge | Open Field | 6 to 12 | 9.6 | 4.33 |
| 38 | EM | cart | Zonge | Open Field | 12 to 24 | 1.87 | 0.23 |
| 38 | EM | cart | Zonge | Open Field | 24 to 36 | 4.43 | 1.21 |
| 38 | EM | cart | Zonge | Open Field | 36 to 48 | 0.17 | 0.15 |
| 38 | EM | cart | Zonge | Wet Probe | 0 to 6 | 19.88 | 8.98 |
| 38 | EM | cart | Zonge | Wet Probe | 6 to 12 | 12.15 | 3.55 |
| 38 | EM | cart | Zonge | Wet Probe | 12 to 24 | 12.47 | 1.75 |
| 38 | EM | cart | Zonge | Wet Probe | 24 to 36 | 31.79 | 9.9 |
| 38 | EM | cart | Zonge | Wet Probe | 36 to 48 | 35.2 | 6.33 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 383 | dual | cart | BH | Calibration | 0 to 6 | 1.57 | 0.046 |
| 383 | dual | cart | BH | Calibration | 6 to 12 | 2.225 | 0.07 |
| 383 | dual | cart | BH | Calibration | 12 to 24 | 3.88 | 0.04 |
| 383 | dual | cart | BH | Calibration | 24 to 36 | 3.6 | 0 |
| 383 | dual | cart | BH | Calibration | 36 to 48 | 4 | 0 |
| 383 | dual | cart | BH | Moguls | 0 to 6 | 1.61 | 0.083 |
| 383 | dual | cart | BH | Moguls | 6 to 12 | 2.07 | 0.064 |
| 383 | dual | cart | BH | Moguls | 12 to 24 | 3.68 | 0.04 |
| 383 | dual | cart | BH | Moguls | 24 to 36 | 4 | 0 |
| 383 | dual | cart | BH | Moguls | 36 to 48 | 4 | 0 |
| 383 | dual | cart | BH | Desert Ext. | 0 to 6 | 1.63 | 0.09 |
| 383 | dual | cart | BH | Desert Ext. | 6 to 12 | 2.1 | 0.045 |
| 383 | dual | cart | BH | Desert Ext. | 12 to 24 | 3.5 | 0 |
| 383 | dual | cart | BH | Desert Ext. | 24 to 36 | 4 | 0 |
| 383 | dual | cart | BH | Desert Ext. | 36 to 48 | 4.095 | 0.022 |
| 607 | dual | cart | BH | Calibration | 0 to 6 | 1.57 | 0.046 |
| 607 | dual | cart | BH | Calibration | 6 to 12 | 2.235 | 0.073 |
| 607 | dual | cart | BH | Calibration | 12 to 24 | 3.88 | 0.04 |
| 607 | dual | cart | BH | Calibration | 24 to 36 | 3.6 | 0 |
| 607 | dual | cart | BH | Calibration | 36 to 48 | 4 | 0 |
| 607 | dual | cart | BH | Moguls | 0 to 6 | 1.6 | 0.077 |
| 607 | dual | cart | BH | Moguls | 6 to 12 | 2.08 | 0.06 |
| 607 | dual | cart | BH | Moguls | 12 to 24 | 3.68 | 0.04 |
| 607 | dual | cart | BH | Moguls | 24 to 36 | 4 | 0 |
| 607 | dual | cart | BH | Moguls | 36 to 48 | 4 | 0 |
| 607 | dual | cart | BH | Desert Ext. | 0 to 6 | 1.63 | 0.09 |
| 607 | dual | cart | BH | Desert Ext. | 6 to 12 | 2.095 | 0.038 |
| 607 | dual | cart | BH | Desert Ext. | 12 to 24 | 3.5 | 0 |
| 607 | dual | cart | BH | Desert Ext. | 24 to 36 | 4 | 0 |
| 607 | dual | cart | BH | Desert Ext. | 36 to 48 | 4.095 | 0.022 |
| 655 | dual | cart | BH | Calibration | 0 to 6 | 1.57 | 0.046 |
| 655 | dual | cart | BH | Calibration | 6 to 12 | 2.235 | 0.073 |

| | | | | | | | |
|-----|------|------|----|-------------|----------|------|------|
| 655 | dual | cart | BH | Calibration | 12 to 24 | 3.88 | 0.04 |
| 655 | dual | cart | BH | Calibration | 24 to 36 | 3.6 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 655 | dual | cart | BH | Calibration | 36 to 48 | 4 | 0 |
| 655 | dual | cart | BH | Moguls | 0 to 6 | 1.6 | 0.077 |
| 655 | dual | cart | BH | Moguls | 6 to 12 | 2.08 | 0.06 |
| 655 | dual | cart | BH | Moguls | 12 to 24 | 3.68 | 0.04 |
| 655 | dual | cart | BH | Moguls | 24 to 36 | 4 | 0 |
| 655 | dual | cart | BH | Moguls | 36 to 48 | 4 | 0 |
| 655 | dual | cart | BH | Desert Ext. | 0 to 6 | 1.63 | 0.09 |
| 655 | dual | cart | BH | Desert Ext. | 6 to 12 | 2.095 | 0.038 |
| 655 | dual | cart | BH | Desert Ext. | 12 to 24 | 3.5 | 0 |
| 655 | dual | cart | BH | Desert Ext. | 24 to 36 | 4 | 0 |
| 655 | dual | cart | BH | Desert Ext. | 36 to 48 | 4.095 | 0.022 |
| 651 | dual | towed | BH | Calibration | 0 to 6 | 1.57 | 0.046 |
| 651 | dual | towed | BH | Calibration | 6 to 12 | 2.235 | 0.073 |
| 651 | dual | towed | BH | Calibration | 12 to 24 | 3.88 | 0.04 |
| 651 | dual | towed | BH | Calibration | 24 to 36 | 3.6 | 0 |
| 651 | dual | towed | BH | Calibration | 36 to 48 | 4 | 0 |
| 651 | dual | towed | BH | Moguls | 0 to 6 | 1.6 | 0.077 |
| 651 | dual | towed | BH | Moguls | 6 to 12 | 2.08 | 0.06 |
| 651 | dual | towed | BH | Moguls | 12 to 24 | 3.68 | 0.04 |
| 651 | dual | towed | BH | Moguls | 24 to 36 | 4 | 0 |
| 651 | dual | towed | BH | Moguls | 36 to 48 | 4 | 0 |
| 651 | dual | towed | BH | Desert Ext. | 0 to 6 | 1.63 | 0.09 |
| 651 | dual | towed | BH | Desert Ext. | 6 to 12 | 2.095 | 0.038 |
| 651 | dual | towed | BH | Desert Ext. | 12 to 24 | 3.5 | 0 |
| 651 | dual | towed | BH | Desert Ext. | 24 to 36 | 4 | 0 |
| 651 | dual | towed | BH | Desert Ext. | 36 to 48 | 4.095 | 0.022 |
| 769 | MAG | hand | Forester | Calibration | 0 to 6 | 1.731 | 0 |
| 769 | MAG | hand | Forester | Calibration | 6 to 12 | 2.169 | 0 |
| 769 | MAG | hand | Forester | Calibration | 12 to 24 | 3.592 | 0 |
| 769 | MAG | hand | Forester | Calibration | 24 to 36 | 3.715 | 0 |
| 769 | MAG | hand | Forester | Calibration | 36 to 48 | 4.1 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 0 to 6 | 1.685 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 6 to 12 | 4.223 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 12 to 24 | 3.808 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 24 to 36 | 4.7 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 36 to 48 | 4.854 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 0 to 6 | 2.25 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 6 to 12 | 2.133 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 12 to 24 | 3.217 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 24 to 36 | 4 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 36 to 48 | 4 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 0 to 6 | 1.7 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 6 to 12 | 1.8 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 12 to 24 | 3.3 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 24 to 36 | 4 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 36 to 48 | 4 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 769 | MAG | hand | Forester | Calibration | 0 to 6 | 1.731 | 0 |
| 769 | MAG | hand | Forester | Calibration | 6 to 12 | 2.169 | 0 |
| 769 | MAG | hand | Forester | Calibration | 12 to 24 | 3.592 | 0 |
| 769 | MAG | hand | Forester | Calibration | 24 to 36 | 3.715 | 0 |
| 769 | MAG | hand | Forester | Calibration | 36 to 48 | 4.1 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 0 to 6 | 1.685 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 6 to 12 | 4.223 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 12 to 24 | 3.808 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 24 to 36 | 4.7 | 0 |
| 769 | MAG | hand | Forester | Mogul Area | 36 to 48 | 4.854 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 0 to 6 | 2.25 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 6 to 12 | 2.133 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 12 to 24 | 3.217 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 24 to 36 | 4 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 36 to 48 | 4 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 0 to 6 | 1.7 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 6 to 12 | 1.8 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 12 to 24 | 3.3 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 24 to 36 | 4 | 0 |
| 769 | MAG | hand | Forester | Desert Ext. | 36 to 48 | 4 | 0 |
| 293 | dual | towed | Geocenters | Calibration | 0 to 6 | 1.76 | 0.08 |
| 293 | dual | towed | Geocenters | Calibration | 6 to 12 | 2.2 | 0 |
| 293 | dual | towed | Geocenters | Calibration | 12 to 24 | 3.7 | 0 |
| 293 | dual | towed | Geocenters | Calibration | 24 to 36 | 3.6 | 0 |
| 293 | dual | towed | Geocenters | Calibration | 36 to 48 | 4.1 | 0 |
| 293 | dual | towed | Geocenters | Moguls | 0 to 6 | 1.6 | 0 |
| 293 | dual | towed | Geocenters | Moguls | 6 to 12 | 2.04 | 0.049 |
| 293 | dual | towed | Geocenters | Moguls | 12 to 24 | 3.44 | 0.08 |
| 293 | dual | towed | Geocenters | Moguls | 24 to 36 | 3.92 | 0.04 |
| 293 | dual | towed | Geocenters | Moguls | 36 to 48 | 4 | 0 |
| 293 | dual | towed | Geocenters | Desert Ext. | 0 to 6 | 1.64 | 0.049 |
| 293 | dual | towed | Geocenters | Desert Ext. | 6 to 12 | 1.98 | 0.183 |
| 293 | dual | towed | Geocenters | Desert Ext. | 12 to 24 | 3.28 | 0.098 |
| 293 | dual | towed | Geocenters | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 293 | dual | towed | Geocenters | Desert Ext. | 36 to 48 | 4.033 | 0.047 |
| 299 | dual | towed | Geocenters | Calibration | 0 to 6 | 1.76 | 0.08 |
| 299 | dual | towed | Geocenters | Calibration | 6 to 12 | 2.2 | 0 |
| 299 | dual | towed | Geocenters | Calibration | 12 to 24 | 3.7 | 0 |
| 299 | dual | towed | Geocenters | Calibration | 24 to 36 | 3.6 | 0 |
| 299 | dual | towed | Geocenters | Calibration | 36 to 48 | 4.1 | 0 |
| 299 | dual | towed | Geocenters | Moguls | 0 to 6 | 1.6 | 0 |
| 299 | dual | towed | Geocenters | Moguls | 6 to 12 | 2.04 | 0.049 |
| 299 | dual | towed | Geocenters | Moguls | 12 to 24 | 3.44 | 0.08 |
| 299 | dual | towed | Geocenters | Moguls | 24 to 36 | 3.92 | 0.04 |
| 299 | dual | towed | Geocenters | Moguls | 36 to 48 | 4 | 0 |
| 299 | dual | towed | Geocenters | Desert Ext. | 0 to 6 | 1.64 | 0.049 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 299 | dual | towed | Geocenters | Desert Ext. | 6 to 12 | 1.98 | 0.183 |
| 299 | dual | towed | Geocenters | Desert Ext. | 12 to 24 | 3.28 | 0.098 |
| 299 | dual | towed | Geocenters | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 299 | dual | towed | Geocenters | Desert Ext. | 36 to 48 | 4.033 | 0.047 |
| 238 | MAG | hand | HFA | Calibration | 0 to 6 | 1.759 | 0.072 |
| 238 | MAG | hand | HFA | Calibration | 6 to 12 | 2.278 | 0.047 |
| 238 | MAG | hand | HFA | Calibration | 12 to 24 | 3.824 | 0.043 |
| 238 | MAG | hand | HFA | Calibration | 24 to 36 | 3.6 | 0 |
| 238 | MAG | hand | HFA | Calibration | 36 to 48 | 4 | 0 |
| 238 | MAG | hand | HFA | Moguls | 0 to 6 | 1.595 | 0.061 |
| 238 | MAG | hand | HFA | Moguls | 6 to 12 | 2.089 | 0.045 |
| 238 | MAG | hand | HFA | Moguls | 12 to 24 | 3.689 | 0.031 |
| 238 | MAG | hand | HFA | Moguls | 24 to 36 | 4 | 0 |
| 238 | MAG | hand | HFA | Moguls | 36 to 48 | 4 | 0 |
| 238 | MAG | hand | HFA | Desert Ext. | 0 to 6 | 1.684 | 0.049 |
| 238 | MAG | hand | HFA | Desert Ext. | 6 to 12 | 2.092 | 0.036 |
| 238 | MAG | hand | HFA | Desert Ext. | 12 to 24 | 3.5 | 0 |
| 238 | MAG | hand | HFA | Desert Ext. | 24 to 36 | 3.995 | 0.023 |
| 238 | MAG | hand | HFA | Desert Ext. | 36 to 48 | 4.097 | 0.016 |
| 528 | MAG | hand | HFA | Calibration | 0 to 6 | 1.759 | 0.072 |
| 528 | MAG | hand | HFA | Calibration | 6 to 12 | 2.278 | 0.047 |
| 528 | MAG | hand | HFA | Calibration | 12 to 24 | 3.824 | 0.043 |
| 528 | MAG | hand | HFA | Calibration | 24 to 36 | 3.6 | 0 |
| 528 | MAG | hand | HFA | Calibration | 36 to 48 | 4 | 0 |
| 528 | MAG | hand | HFA | Moguls | 0 to 6 | 1.595 | 0.061 |
| 528 | MAG | hand | HFA | Moguls | 6 to 12 | 2.089 | 0.045 |
| 528 | MAG | hand | HFA | Moguls | 12 to 24 | 3.689 | 0.031 |
| 528 | MAG | hand | HFA | Moguls | 24 to 36 | 4 | 0 |
| 528 | MAG | hand | HFA | Moguls | 36 to 48 | 4 | 0 |
| 528 | MAG | hand | HFA | Desert Ext. | 0 to 6 | 1.684 | 0.049 |
| 528 | MAG | hand | HFA | Desert Ext. | 6 to 12 | 2.092 | 0.036 |
| 528 | MAG | hand | HFA | Desert Ext. | 12 to 24 | 3.5 | 0 |
| 528 | MAG | hand | HFA | Desert Ext. | 24 to 36 | 3.995 | 0.023 |
| 528 | MAG | hand | HFA | Desert Ext. | 36 to 48 | 4.097 | 0.016 |
| 587 | MAG | hand | HFA | Calibration | 0 to 6 | 1.759 | 0.072 |
| 587 | MAG | hand | HFA | Calibration | 6 to 12 | 2.278 | 0.047 |
| 587 | MAG | hand | HFA | Calibration | 12 to 24 | 3.824 | 0.043 |
| 587 | MAG | hand | HFA | Calibration | 24 to 36 | 3.6 | 0 |
| 587 | MAG | hand | HFA | Calibration | 36 to 48 | 4 | 0 |
| 587 | MAG | hand | HFA | Moguls | 0 to 6 | 1.595 | 0.061 |
| 587 | MAG | hand | HFA | Moguls | 6 to 12 | 2.089 | 0.045 |
| 587 | MAG | hand | HFA | Moguls | 12 to 24 | 3.689 | 0.031 |
| 587 | MAG | hand | HFA | Moguls | 24 to 36 | 4 | 0 |
| 587 | MAG | hand | HFA | Moguls | 36 to 48 | 4 | 0 |
| 587 | MAG | hand | HFA | Desert Ext. | 0 to 6 | 1.684 | 0.049 |
| 587 | MAG | hand | HFA | Desert Ext. | 6 to 12 | 2.092 | 0.036 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 587 | MAG | hand | HFA | Desert Ext. | 12 to 24 | 3.5 | 0 |
| 587 | MAG | hand | HFA | Desert Ext. | 24 to 36 | 3.995 | 0.023 |
| 587 | MAG | hand | HFA | Desert Ext. | 36 to 48 | 4.097 | 0.016 |
| 442 | MAG | hand | HFA | Calibration | 0 to 6 | 1.759 | 0.072 |
| 442 | MAG | hand | HFA | Calibration | 6 to 12 | 2.278 | 0.047 |
| 442 | MAG | hand | HFA | Calibration | 12 to 24 | 3.824 | 0.043 |
| 442 | MAG | hand | HFA | Calibration | 24 to 36 | 3.6 | 0 |
| 442 | MAG | hand | HFA | Calibration | 36 to 48 | 4 | 0 |
| 442 | MAG | hand | HFA | Moguls | 0 to 6 | 1.595 | 0.061 |
| 442 | MAG | hand | HFA | Moguls | 6 to 12 | 2.089 | 0.045 |
| 442 | MAG | hand | HFA | Moguls | 12 to 24 | 3.689 | 0.031 |
| 442 | MAG | hand | HFA | Moguls | 24 to 36 | 4 | 0 |
| 442 | MAG | hand | HFA | Moguls | 36 to 48 | 4 | 0 |
| 442 | MAG | hand | HFA | Desert Ext. | 0 to 6 | 1.684 | 0.049 |
| 442 | MAG | hand | HFA | Desert Ext. | 6 to 12 | 2.092 | 0.036 |
| 442 | MAG | hand | HFA | Desert Ext. | 12 to 24 | 3.5 | 0 |
| 442 | MAG | hand | HFA | Desert Ext. | 24 to 36 | 3.876 | 0.497 |
| 442 | MAG | hand | HFA | Desert Ext. | 36 to 48 | 3.995 | 0.429 |
| 667 | EM | towed | NAEVA | Calibration | 0 to 6 | 1.853 | 0.062 |
| 667 | EM | towed | NAEVA | Calibration | 6 to 12 | 2.787 | 0.088 |
| 667 | EM | towed | NAEVA | Calibration | 12 to 24 | 4.587 | 0.096 |
| 667 | EM | towed | NAEVA | Calibration | 24 to 36 | 3.7 | 0 |
| 667 | EM | towed | NAEVA | Calibration | 36 to 48 | 4.033 | 0.047 |
| 667 | EM | towed | NAEVA | Moguls | 0 to 6 | 1.713 | 0.034 |
| 667 | EM | towed | NAEVA | Moguls | 6 to 12 | 2.773 | 0.044 |
| 667 | EM | towed | NAEVA | Moguls | 12 to 24 | 4.487 | 0.034 |
| 667 | EM | towed | NAEVA | Moguls | 24 to 36 | 3.8 | 0 |
| 667 | EM | towed | NAEVA | Moguls | 36 to 48 | 3.9 | 0 |
| 667 | EM | towed | NAEVA | Desert Ext. | 0 to 6 | 1.513 | 0.034 |
| 667 | EM | towed | NAEVA | Desert Ext. | 6 to 12 | 2.087 | 0.034 |
| 667 | EM | towed | NAEVA | Desert Ext. | 12 to 24 | 3.633 | 0.249 |
| 667 | EM | towed | NAEVA | Desert Ext. | 24 to 36 | 3.7 | 0 |
| 667 | EM | towed | NAEVA | Desert Ext. | 36 to 48 | 3.9 | 0 |
| 666 | EM | 2-man | NAEVA | Calibration | 0 to 6 | 1.853 | 0.062 |
| 666 | EM | 2-man | NAEVA | Calibration | 6 to 12 | 2.787 | 0.088 |
| 666 | EM | 2-man | NAEVA | Calibration | 12 to 24 | 4.587 | 0.096 |
| 666 | EM | 2-man | NAEVA | Calibration | 24 to 36 | 3.7 | 0 |
| 666 | EM | 2-man | NAEVA | Calibration | 36 to 48 | 4.033 | 0.047 |
| 666 | EM | 2-man | NAEVA | Moguls | 0 to 6 | 1.713 | 0.034 |
| 666 | EM | 2-man | NAEVA | Moguls | 6 to 12 | 2.773 | 0.044 |
| 666 | EM | 2-man | NAEVA | Moguls | 12 to 24 | 4.487 | 0.034 |
| 666 | EM | 2-man | NAEVA | Moguls | 24 to 36 | 3.8 | 0 |
| 666 | EM | 2-man | NAEVA | Moguls | 36 to 48 | 3.9 | 0 |
| 666 | EM | 2-man | NAEVA | Desert Ext. | 0 to 6 | 1.513 | 0.034 |
| 666 | EM | 2-man | NAEVA | Desert Ext. | 6 to 12 | 2.087 | 0.034 |
| 666 | EM | 2-man | NAEVA | Desert Ext. | 12 to 24 | 3.633 | 0.249 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 666 | EM | 2-man | NAEVA | Desert Ext. | 24 to 36 | 3.7 | 0 |
| 666 | EM | 2-man | NAEVA | Desert Ext. | 36 to 48 | 3.9 | 0 |
| 670 | EM | 2-man | NAEVA | Calibration | 0 to 6 | 1.853 | 0.062 |
| 670 | EM | 2-man | NAEVA | Calibration | 6 to 12 | 2.787 | 0.088 |
| 670 | EM | 2-man | NAEVA | Calibration | 12 to 24 | 4.587 | 0.096 |
| 670 | EM | 2-man | NAEVA | Calibration | 24 to 36 | 3.7 | 0 |
| 670 | EM | 2-man | NAEVA | Calibration | 36 to 48 | 4.033 | 0.047 |
| 670 | EM | 2-man | NAEVA | Moguls | 0 to 6 | 1.713 | 0.034 |
| 670 | EM | 2-man | NAEVA | Moguls | 6 to 12 | 2.773 | 0.044 |
| 670 | EM | 2-man | NAEVA | Moguls | 12 to 24 | 4.487 | 0.034 |
| 670 | EM | 2-man | NAEVA | Moguls | 24 to 36 | 3.8 | 0 |
| 670 | EM | 2-man | NAEVA | Moguls | 36 to 48 | 3.9 | 0 |
| 670 | EM | 2-man | NAEVA | Desert Ext. | 0 to 6 | 1.513 | 0.034 |
| 670 | EM | 2-man | NAEVA | Desert Ext. | 6 to 12 | 2.087 | 0.034 |
| 670 | EM | 2-man | NAEVA | Desert Ext. | 12 to 24 | 3.633 | 0.249 |
| 670 | EM | 2-man | NAEVA | Desert Ext. | 24 to 36 | 3.7 | 0 |
| 670 | EM | 2-man | NAEVA | Desert Ext. | 36 to 48 | 3.9 | 0 |
| 669 | EM | 2-man | NAEVA | Calibration | 0 to 6 | 1.853 | 0.062 |
| 669 | EM | 2-man | NAEVA | Calibration | 6 to 12 | 2.787 | 0.088 |
| 669 | EM | 2-man | NAEVA | Calibration | 12 to 24 | 4.587 | 0.096 |
| 669 | EM | 2-man | NAEVA | Calibration | 24 to 36 | 3.7 | 0 |
| 669 | EM | 2-man | NAEVA | Calibration | 36 to 48 | 4.033 | 0.047 |
| 669 | EM | 2-man | NAEVA | Moguls | 0 to 6 | 1.713 | 0.034 |
| 669 | EM | 2-man | NAEVA | Moguls | 6 to 12 | 2.773 | 0.044 |
| 669 | EM | 2-man | NAEVA | Moguls | 12 to 24 | 4.487 | 0.034 |
| 669 | EM | 2-man | NAEVA | Moguls | 24 to 36 | 3.8 | 0 |
| 669 | EM | 2-man | NAEVA | Moguls | 36 to 48 | 3.9 | 0 |
| 669 | EM | 2-man | NAEVA | Desert Ext. | 0 to 6 | 1.513 | 0.034 |
| 669 | EM | 2-man | NAEVA | Desert Ext. | 6 to 12 | 2.087 | 0.034 |
| 669 | EM | 2-man | NAEVA | Desert Ext. | 12 to 24 | 3.633 | 0.249 |
| 669 | EM | 2-man | NAEVA | Desert Ext. | 24 to 36 | 3.7 | 0 |
| 669 | EM | 2-man | NAEVA | Desert Ext. | 36 to 48 | 3.9 | 0 |
| 668 | EM | towed | NAEVA | Calibration | 0 to 6 | 1.853 | 0.062 |
| 668 | EM | towed | NAEVA | Calibration | 6 to 12 | 2.787 | 0.088 |
| 668 | EM | towed | NAEVA | Calibration | 12 to 24 | 4.587 | 0.096 |
| 668 | EM | towed | NAEVA | Calibration | 24 to 36 | 3.7 | 0 |
| 668 | EM | towed | NAEVA | Calibration | 36 to 48 | 4.033 | 0.047 |
| 668 | EM | towed | NAEVA | Moguls | 0 to 6 | 1.713 | 0.034 |
| 668 | EM | towed | NAEVA | Moguls | 6 to 12 | 2.773 | 0.044 |
| 668 | EM | towed | NAEVA | Moguls | 12 to 24 | 4.487 | 0.034 |
| 668 | EM | towed | NAEVA | Moguls | 24 to 36 | 3.8 | 0 |
| 668 | EM | towed | NAEVA | Moguls | 36 to 48 | 3.9 | 0 |
| 668 | EM | towed | NAEVA | Desert Ext. | 0 to 6 | 1.513 | 0.034 |
| 668 | EM | towed | NAEVA | Desert Ext. | 6 to 12 | 2.087 | 0.034 |
| 668 | EM | towed | NAEVA | Desert Ext. | 12 to 24 | 3.633 | 0.249 |
| 668 | EM | towed | NAEVA | Desert Ext. | 24 to 36 | 3.7 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 668 | EM | towed | NAEVA | Desert Ext. | 36 to 48 | 3.9 | 0 |
| 213 | EM | towed | NRL | Calibration | 0 to 6 | 1.85 | 0.05 |
| 213 | EM | towed | NRL | Calibration | 6 to 12 | 2.588 | 0.105 |
| 213 | EM | towed | NRL | Calibration | 12 to 24 | 3.7 | 0 |
| 213 | EM | towed | NRL | Calibration | 24 to 36 | 3.6 | 0 |
| 213 | EM | towed | NRL | Calibration | 36 to 48 | 4 | 0 |
| 213 | EM | towed | NRL | Moguls | 0 to 6 | 1.6 | 0 |
| 213 | EM | towed | NRL | Moguls | 6 to 12 | 2.413 | 0.145 |
| 213 | EM | towed | NRL | Moguls | 12 to 24 | 3.5 | 0 |
| 213 | EM | towed | NRL | Moguls | 24 to 36 | 3.925 | 0.043 |
| 213 | EM | towed | NRL | Moguls | 36 to 48 | 3.975 | 0.043 |
| 213 | EM | towed | NRL | Desert Ext. | 0 to 6 | 1.675 | 0.083 |
| 213 | EM | towed | NRL | Desert Ext. | 6 to 12 | 2.387 | 0.06 |
| 213 | EM | towed | NRL | Desert Ext. | 12 to 24 | 3.3 | 0 |
| 213 | EM | towed | NRL | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 213 | EM | towed | NRL | Desert Ext. | 36 to 48 | 4.1 | 0 |
| 245 | EM | towed | NRL | Calibration | 0 to 6 | 1.85 | 0.05 |
| 245 | EM | towed | NRL | Calibration | 6 to 12 | 2.588 | 0.105 |
| 245 | EM | towed | NRL | Calibration | 12 to 24 | 3.7 | 0 |
| 245 | EM | towed | NRL | Calibration | 24 to 36 | 3.6 | 0 |
| 245 | EM | towed | NRL | Calibration | 36 to 48 | 4 | 0 |
| 245 | EM | towed | NRL | Moguls | 0 to 6 | 1.6 | 0 |
| 245 | EM | towed | NRL | Moguls | 6 to 12 | 2.413 | 0.145 |
| 245 | EM | towed | NRL | Moguls | 12 to 24 | 3.5 | 0 |
| 245 | EM | towed | NRL | Moguls | 24 to 36 | 3.925 | 0.043 |
| 245 | EM | towed | NRL | Moguls | 36 to 48 | 3.975 | 0.043 |
| 245 | EM | towed | NRL | Desert Ext. | 0 to 6 | 1.675 | 0.083 |
| 245 | EM | towed | NRL | Desert Ext. | 6 to 12 | 2.387 | 0.06 |
| 245 | EM | towed | NRL | Desert Ext. | 12 to 24 | 3.3 | 0 |
| 245 | EM | towed | NRL | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 245 | EM | towed | NRL | Desert Ext. | 36 to 48 | 4.1 | 0 |
| 690 | EM | cart | Parsons | Calibration | 0 to 6 | 1.786 | 0.035 |
| 690 | EM | cart | Parsons | Calibration | 6 to 12 | 2.286 | 0.035 |
| 690 | EM | cart | Parsons | Calibration | 12 to 24 | 3.7 | 0 |
| 690 | EM | cart | Parsons | Calibration | 24 to 36 | 3.65 | 0.05 |
| 690 | EM | cart | Parsons | Calibration | 36 to 48 | 4.1 | 0 |
| 690 | EM | cart | Parsons | Moguls | 0 to 6 | 1.7 | 0 |
| 690 | EM | cart | Parsons | Moguls | 6 to 12 | 2 | 0 |
| 690 | EM | cart | Parsons | Moguls | 12 to 24 | 3.6 | 0 |
| 690 | EM | cart | Parsons | Moguls | 24 to 36 | 3.9 | 0 |
| 690 | EM | cart | Parsons | Moguls | 36 to 48 | 4 | 0 |
| 690 | EM | cart | Parsons | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 690 | EM | cart | Parsons | Desert Ext. | 6 to 12 | 2 | 0 |
| 690 | EM | cart | Parsons | Desert Ext. | 12 to 24 | 3.4 | 0 |
| 690 | EM | cart | Parsons | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 690 | EM | cart | Parsons | Desert Ext. | 36 to 48 | 4.1 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 532 | EM | cart | Parsons | Calibration | 0 to 6 | 1.786 | 0.035 |
| 532 | EM | cart | Parsons | Calibration | 6 to 12 | 2.286 | 0.035 |
| 532 | EM | cart | Parsons | Calibration | 12 to 24 | 3.7 | 0 |
| 532 | EM | cart | Parsons | Calibration | 24 to 36 | 3.65 | 0.05 |
| 532 | EM | cart | Parsons | Calibration | 36 to 48 | 4.1 | 0 |
| 532 | EM | cart | Parsons | Moguls | 0 to 6 | 1.7 | 0 |
| 532 | EM | cart | Parsons | Moguls | 6 to 12 | 2 | 0 |
| 532 | EM | cart | Parsons | Moguls | 12 to 24 | 3.6 | 0 |
| 532 | EM | cart | Parsons | Moguls | 24 to 36 | 3.9 | 0 |
| 532 | EM | cart | Parsons | Moguls | 36 to 48 | 4 | 0 |
| 532 | EM | cart | Parsons | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 532 | EM | cart | Parsons | Desert Ext. | 6 to 12 | 2 | 0 |
| 532 | EM | cart | Parsons | Desert Ext. | 12 to 24 | 3.4 | 0 |
| 532 | EM | cart | Parsons | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 532 | EM | cart | Parsons | Desert Ext. | 36 to 48 | 3.771 | 0.805 |
| 588 | EM | cart | Parsons | Calibration | 0 to 6 | 1.786 | 0.035 |
| 588 | EM | cart | Parsons | Calibration | 6 to 12 | 2.286 | 0.035 |
| 588 | EM | cart | Parsons | Calibration | 12 to 24 | 3.7 | 0 |
| 588 | EM | cart | Parsons | Calibration | 24 to 36 | 3.657 | 0.049 |
| 588 | EM | cart | Parsons | Calibration | 36 to 48 | 4.1 | 0 |
| 588 | EM | cart | Parsons | Moguls | 0 to 6 | 1.7 | 0 |
| 588 | EM | cart | Parsons | Moguls | 6 to 12 | 2 | 0 |
| 588 | EM | cart | Parsons | Moguls | 12 to 24 | 3.6 | 0 |
| 588 | EM | cart | Parsons | Moguls | 24 to 36 | 3.9 | 0 |
| 588 | EM | cart | Parsons | Moguls | 36 to 48 | 4 | 0 |
| 588 | EM | cart | Parsons | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 588 | EM | cart | Parsons | Desert Ext. | 6 to 12 | 2 | 0 |
| 588 | EM | cart | Parsons | Desert Ext. | 12 to 24 | 3.4 | 0 |
| 588 | EM | cart | Parsons | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 588 | EM | cart | Parsons | Desert Ext. | 36 to 48 | 4.1 | 0 |
| 425 | EM | cart | Parsons | Calibration | 0 to 6 | 1.786 | 0.035 |
| 425 | EM | cart | Parsons | Calibration | 6 to 12 | 2.286 | 0.035 |
| 425 | EM | cart | Parsons | Calibration | 12 to 24 | 3.7 | 0 |
| 425 | EM | cart | Parsons | Calibration | 24 to 36 | 3.65 | 0.05 |
| 425 | EM | cart | Parsons | Calibration | 36 to 48 | 4.1 | 0 |
| 425 | EM | cart | Parsons | Moguls | 0 to 6 | 1.7 | 0 |
| 425 | EM | cart | Parsons | Moguls | 6 to 12 | 2 | 0 |
| 425 | EM | cart | Parsons | Moguls | 12 to 24 | 3.6 | 0 |
| 425 | EM | cart | Parsons | Moguls | 24 to 36 | 3.9 | 0 |
| 425 | EM | cart | Parsons | Moguls | 36 to 48 | 4 | 0 |
| 425 | EM | cart | Parsons | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 425 | EM | cart | Parsons | Desert Ext. | 6 to 12 | 2 | 0 |
| 425 | EM | cart | Parsons | Desert Ext. | 12 to 24 | 3.4 | 0 |
| 425 | EM | cart | Parsons | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 425 | EM | cart | Parsons | Desert Ext. | 36 to 48 | 4.1 | 0 |
| 606 | MAG | hand | Parsons | Calibration | 0 to 6 | 1.677 | 0.119 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 606 | MAG | hand | Parsons | Calibration | 6 to 12 | 2.2 | 0 |
| 606 | MAG | hand | Parsons | Calibration | 12 to 24 | 3.7 | 0 |
| 606 | MAG | hand | Parsons | Calibration | 24 to 36 | 3.6 | 0 |
| 606 | MAG | hand | Parsons | Calibration | 36 to 48 | 4.1 | 0 |
| 606 | MAG | hand | Parsons | Moguls | 0 to 6 | 1.654 | 0.05 |
| 606 | MAG | hand | Parsons | Moguls | 6 to 12 | 2.015 | 0.036 |
| 606 | MAG | hand | Parsons | Moguls | 12 to 24 | 3.6 | 0.13 |
| 606 | MAG | hand | Parsons | Moguls | 24 to 36 | 3.923 | 0.042 |
| 606 | MAG | hand | Parsons | Moguls | 36 to 48 | 4 | 0 |
| 606 | MAG | hand | Parsons | Desert Ext. | 0 to 6 | 1.623 | 0.042 |
| 606 | MAG | hand | Parsons | Desert Ext. | 6 to 12 | 2.008 | 0.1 |
| 606 | MAG | hand | Parsons | Desert Ext. | 12 to 24 | 3.354 | 0.075 |
| 606 | MAG | hand | Parsons | Desert Ext. | 24 to 36 | 3.869 | 0.072 |
| 606 | MAG | hand | Parsons | Desert Ext. | 36 to 48 | 4.054 | 0.075 |
| 601 | MAG | hand | Parsons | Calibration | 0 to 6 | 1.677 | 0.119 |
| 601 | MAG | hand | Parsons | Calibration | 6 to 12 | 2.2 | 0 |
| 601 | MAG | hand | Parsons | Calibration | 12 to 24 | 3.7 | 0 |
| 601 | MAG | hand | Parsons | Calibration | 24 to 36 | 3.6 | 0 |
| 601 | MAG | hand | Parsons | Calibration | 36 to 48 | 4.1 | 0 |
| 601 | MAG | hand | Parsons | Moguls | 0 to 6 | 1.654 | 0.05 |
| 601 | MAG | hand | Parsons | Moguls | 6 to 12 | 2.015 | 0.036 |
| 601 | MAG | hand | Parsons | Moguls | 12 to 24 | 3.6 | 0.13 |
| 601 | MAG | hand | Parsons | Moguls | 24 to 36 | 3.923 | 0.042 |
| 601 | MAG | hand | Parsons | Moguls | 36 to 48 | 4 | 0 |
| 601 | MAG | hand | Parsons | Desert Ext. | 0 to 6 | 1.623 | 0.042 |
| 601 | MAG | hand | Parsons | Desert Ext. | 6 to 12 | 2.008 | 0.1 |
| 601 | MAG | hand | Parsons | Desert Ext. | 12 to 24 | 3.354 | 0.075 |
| 601 | MAG | hand | Parsons | Desert Ext. | 24 to 36 | 3.869 | 0.072 |
| 601 | MAG | hand | Parsons | Desert Ext. | 36 to 48 | 4.054 | 0.075 |
| 602 | MAG | hand | Parsons | Calibration | 0 to 6 | 1.677 | 0.119 |
| 602 | MAG | hand | Parsons | Calibration | 6 to 12 | 2.2 | 0 |
| 602 | MAG | hand | Parsons | Calibration | 12 to 24 | 3.7 | 0 |
| 602 | MAG | hand | Parsons | Calibration | 24 to 36 | 3.6 | 0 |
| 602 | MAG | hand | Parsons | Calibration | 36 to 48 | 4.1 | 0 |
| 602 | MAG | hand | Parsons | Moguls | 0 to 6 | 1.654 | 0.05 |
| 602 | MAG | hand | Parsons | Moguls | 6 to 12 | 2.015 | 0.036 |
| 602 | MAG | hand | Parsons | Moguls | 12 to 24 | 3.6 | 0.13 |
| 602 | MAG | hand | Parsons | Moguls | 24 to 36 | 3.923 | 0.042 |
| 602 | MAG | hand | Parsons | Moguls | 36 to 48 | 4 | 0 |
| 602 | MAG | hand | Parsons | Desert Ext. | 0 to 6 | 1.623 | 0.042 |
| 602 | MAG | hand | Parsons | Desert Ext. | 6 to 12 | 2.008 | 0.1 |
| 602 | MAG | hand | Parsons | Desert Ext. | 12 to 24 | 3.354 | 0.075 |
| 602 | MAG | hand | Parsons | Desert Ext. | 24 to 36 | 3.869 | 0.072 |
| 602 | MAG | hand | Parsons | Desert Ext. | 36 to 48 | 4.054 | 0.075 |
| 426 | MAG | hand | Parsons | Calibration | 0 to 6 | 1.677 | 0.119 |
| 426 | MAG | hand | Parsons | Calibration | 6 to 12 | 2.2 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 426 | MAG | hand | Parsons | Calibration | 12 to 24 | 3.7 | 0 |
| 426 | MAG | hand | Parsons | Calibration | 24 to 36 | 3.6 | 0 |
| 426 | MAG | hand | Parsons | Calibration | 36 to 48 | 4.1 | 0 |
| 426 | MAG | hand | Parsons | Moguls | 0 to 6 | 1.654 | 0.05 |
| 426 | MAG | hand | Parsons | Moguls | 6 to 12 | 2.015 | 0.036 |
| 426 | MAG | hand | Parsons | Moguls | 12 to 24 | 3.6 | 0.13 |
| 426 | MAG | hand | Parsons | Moguls | 24 to 36 | 3.923 | 0.042 |
| 426 | MAG | hand | Parsons | Moguls | 36 to 48 | 4 | 0 |
| 426 | MAG | hand | Parsons | Desert Ext. | 0 to 6 | 1.623 | 0.042 |
| 426 | MAG | hand | Parsons | Desert Ext. | 6 to 12 | 2.008 | 0.1 |
| 426 | MAG | hand | Parsons | Desert Ext. | 12 to 24 | 3.354 | 0.075 |
| 426 | MAG | hand | Parsons | Desert Ext. | 24 to 36 | 3.869 | 0.072 |
| 426 | MAG | hand | Parsons | Desert Ext. | 36 to 48 | 3.708 | 0.817 |
| 199 | EM | cart | Shaw | Calibration | 0 to 6 | 1.73 | 0.09 |
| 199 | EM | cart | Shaw | Calibration | 6 to 12 | 2.32 | 0.04 |
| 199 | EM | cart | Shaw | Calibration | 12 to 24 | 3.7 | 0 |
| 199 | EM | cart | Shaw | Calibration | 24 to 36 | 3.6 | 0 |
| 199 | EM | cart | Shaw | Calibration | 36 to 48 | 3.93 | 0.046 |
| 199 | EM | cart | Shaw | Moguls | 0 to 6 | 1.61 | 0.03 |
| 199 | EM | cart | Shaw | Moguls | 6 to 12 | 2.04 | 0.08 |
| 199 | EM | cart | Shaw | Moguls | 12 to 24 | 3.58 | 0.04 |
| 199 | EM | cart | Shaw | Moguls | 24 to 36 | 3.9 | 0 |
| 199 | EM | cart | Shaw | Moguls | 36 to 48 | 3.9 | 0 |
| 199 | EM | cart | Shaw | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 199 | EM | cart | Shaw | Desert Ext. | 6 to 12 | 2.2 | 0.077 |
| 199 | EM | cart | Shaw | Desert Ext. | 12 to 24 | 3.38 | 0.04 |
| 199 | EM | cart | Shaw | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 199 | EM | cart | Shaw | Desert Ext. | 36 to 48 | 4.01 | 0.03 |
| 211 | EM | cart | Shaw | Calibration | 0 to 6 | 1.713 | 0.093 |
| 211 | EM | cart | Shaw | Calibration | 6 to 12 | 2.325 | 0.043 |
| 211 | EM | cart | Shaw | Calibration | 12 to 24 | 3.7 | 0 |
| 211 | EM | cart | Shaw | Calibration | 24 to 36 | 3.6 | 0 |
| 211 | EM | cart | Shaw | Calibration | 36 to 48 | 3.925 | 0.043 |
| 211 | EM | cart | Shaw | Moguls | 0 to 6 | 1.612 | 0.033 |
| 211 | EM | cart | Shaw | Moguls | 6 to 12 | 2.05 | 0.087 |
| 211 | EM | cart | Shaw | Moguls | 12 to 24 | 3.575 | 0.043 |
| 211 | EM | cart | Shaw | Moguls | 24 to 36 | 3.9 | 0 |
| 211 | EM | cart | Shaw | Moguls | 36 to 48 | 3.9 | 0 |
| 211 | EM | cart | Shaw | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 211 | EM | cart | Shaw | Desert Ext. | 6 to 12 | 2.2 | 0.087 |
| 211 | EM | cart | Shaw | Desert Ext. | 12 to 24 | 3.375 | 0.043 |
| 211 | EM | cart | Shaw | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 211 | EM | cart | Shaw | Desert Ext. | 36 to 48 | 4.012 | 0.033 |
| 207 | EM | cart | Shaw | Calibration | 0 to 6 | 1.713 | 0.093 |
| 207 | EM | cart | Shaw | Calibration | 6 to 12 | 2.325 | 0.043 |
| 207 | EM | cart | Shaw | Calibration | 12 to 24 | 3.7 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 207 | EM | cart | Shaw | Calibration | 24 to 36 | 3.6 | 0 |
| 207 | EM | cart | Shaw | Calibration | 36 to 48 | 3.925 | 0.043 |
| 207 | EM | cart | Shaw | Moguls | 0 to 6 | 1.612 | 0.033 |
| 207 | EM | cart | Shaw | Moguls | 6 to 12 | 2.05 | 0.087 |
| 207 | EM | cart | Shaw | Moguls | 12 to 24 | 3.575 | 0.043 |
| 207 | EM | cart | Shaw | Moguls | 24 to 36 | 3.9 | 0 |
| 207 | EM | cart | Shaw | Moguls | 36 to 48 | 3.9 | 0 |
| 207 | EM | cart | Shaw | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 207 | EM | cart | Shaw | Desert Ext. | 6 to 12 | 2.2 | 0.087 |
| 207 | EM | cart | Shaw | Desert Ext. | 12 to 24 | 3.375 | 0.043 |
| 207 | EM | cart | Shaw | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 207 | EM | cart | Shaw | Desert Ext. | 36 to 48 | 4.012 | 0.033 |
| 354 | EM | cart | Shaw | Calibration | 0 to 6 | 1.713 | 0.093 |
| 354 | EM | cart | Shaw | Calibration | 6 to 12 | 2.325 | 0.043 |
| 354 | EM | cart | Shaw | Calibration | 12 to 24 | 3.7 | 0 |
| 354 | EM | cart | Shaw | Calibration | 24 to 36 | 3.6 | 0 |
| 354 | EM | cart | Shaw | Calibration | 36 to 48 | 3.925 | 0.043 |
| 354 | EM | cart | Shaw | Moguls | 0 to 6 | 1.612 | 0.033 |
| 354 | EM | cart | Shaw | Moguls | 6 to 12 | 2.05 | 0.087 |
| 354 | EM | cart | Shaw | Moguls | 12 to 24 | 3.575 | 0.043 |
| 354 | EM | cart | Shaw | Moguls | 24 to 36 | 3.9 | 0 |
| 354 | EM | cart | Shaw | Moguls | 36 to 48 | 3.9 | 0 |
| 354 | EM | cart | Shaw | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 354 | EM | cart | Shaw | Desert Ext. | 6 to 12 | 2.2 | 0.087 |
| 354 | EM | cart | Shaw | Desert Ext. | 12 to 24 | 3.375 | 0.043 |
| 354 | EM | cart | Shaw | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 354 | EM | cart | Shaw | Desert Ext. | 36 to 48 | 4.012 | 0.033 |
| 312 | MAG | cart | Shaw | Calibration | 0 to 6 | 1.74 | 0.092 |
| 312 | MAG | cart | Shaw | Calibration | 6 to 12 | 2.4 | 0.089 |
| 312 | MAG | cart | Shaw | Calibration | 12 to 24 | 3.69 | 0.03 |
| 312 | MAG | cart | Shaw | Calibration | 24 to 36 | 3.6 | 0 |
| 312 | MAG | cart | Shaw | Calibration | 36 to 48 | 3.94 | 0.049 |
| 312 | MAG | cart | Shaw | Moguls | 0 to 6 | 1.64 | 0.049 |
| 312 | MAG | cart | Shaw | Moguls | 6 to 12 | 2.27 | 0.215 |
| 312 | MAG | cart | Shaw | Moguls | 12 to 24 | 3.5 | 0 |
| 312 | MAG | cart | Shaw | Moguls | 24 to 36 | 3.9 | 0 |
| 312 | MAG | cart | Shaw | Moguls | 36 to 48 | 3.9 | 0 |
| 312 | MAG | cart | Shaw | Desert Ext. | 0 to 6 | 1.64 | 0.08 |
| 312 | MAG | cart | Shaw | Desert Ext. | 6 to 12 | 2.26 | 0.136 |
| 312 | MAG | cart | Shaw | Desert Ext. | 12 to 24 | 3.3 | 0 |
| 312 | MAG | cart | Shaw | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 312 | MAG | cart | Shaw | Desert Ext. | 36 to 48 | 4 | 0 |
| 541 | MAG | cart | Shaw | Calibration | 0 to 6 | 1.74 | 0.092 |
| 541 | MAG | cart | Shaw | Calibration | 6 to 12 | 2.4 | 0.089 |
| 541 | MAG | cart | Shaw | Calibration | 12 to 24 | 3.69 | 0.03 |
| 541 | MAG | cart | Shaw | Calibration | 24 to 36 | 3.6 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 541 | MAG | cart | Shaw | Calibration | 36 to 48 | 3.94 | 0.049 |
| 541 | MAG | cart | Shaw | Moguls | 0 to 6 | 1.64 | 0.049 |
| 541 | MAG | cart | Shaw | Moguls | 6 to 12 | 2.27 | 0.215 |
| 541 | MAG | cart | Shaw | Moguls | 12 to 24 | 3.5 | 0 |
| 541 | MAG | cart | Shaw | Moguls | 24 to 36 | 3.9 | 0 |
| 541 | MAG | cart | Shaw | Moguls | 36 to 48 | 3.9 | 0 |
| 541 | MAG | cart | Shaw | Desert Ext. | 0 to 6 | 1.64 | 0.08 |
| 541 | MAG | cart | Shaw | Desert Ext. | 6 to 12 | 2.26 | 0.136 |
| 541 | MAG | cart | Shaw | Desert Ext. | 12 to 24 | 3.3 | 0 |
| 541 | MAG | cart | Shaw | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 541 | MAG | cart | Shaw | Desert Ext. | 36 to 48 | 4 | 0 |
| 594 | MAG | cart | Shaw | Calibration | 0 to 6 | 1.74 | 0.092 |
| 594 | MAG | cart | Shaw | Calibration | 6 to 12 | 2.4 | 0.089 |
| 594 | MAG | cart | Shaw | Calibration | 12 to 24 | 3.69 | 0.03 |
| 594 | MAG | cart | Shaw | Calibration | 24 to 36 | 3.6 | 0 |
| 594 | MAG | cart | Shaw | Calibration | 36 to 48 | 3.94 | 0.049 |
| 594 | MAG | cart | Shaw | Moguls | 0 to 6 | 1.64 | 0.049 |
| 594 | MAG | cart | Shaw | Moguls | 6 to 12 | 2.27 | 0.215 |
| 594 | MAG | cart | Shaw | Moguls | 12 to 24 | 3.5 | 0 |
| 594 | MAG | cart | Shaw | Moguls | 24 to 36 | 3.9 | 0 |
| 594 | MAG | cart | Shaw | Moguls | 36 to 48 | 3.9 | 0 |
| 594 | MAG | cart | Shaw | Desert Ext. | 0 to 6 | 1.64 | 0.08 |
| 594 | MAG | cart | Shaw | Desert Ext. | 6 to 12 | 2.26 | 0.136 |
| 594 | MAG | cart | Shaw | Desert Ext. | 12 to 24 | 3.3 | 0 |
| 594 | MAG | cart | Shaw | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 594 | MAG | cart | Shaw | Desert Ext. | 36 to 48 | 4 | 0 |
| 638 | MAG | cart | Shaw | Calibration | 0 to 6 | 1.74 | 0.092 |
| 638 | MAG | cart | Shaw | Calibration | 6 to 12 | 2.4 | 0.089 |
| 638 | MAG | cart | Shaw | Calibration | 12 to 24 | 3.69 | 0.03 |
| 638 | MAG | cart | Shaw | Calibration | 24 to 36 | 3.6 | 0 |
| 638 | MAG | cart | Shaw | Calibration | 36 to 48 | 3.94 | 0.049 |
| 638 | MAG | cart | Shaw | Moguls | 0 to 6 | 1.64 | 0.049 |
| 638 | MAG | cart | Shaw | Moguls | 6 to 12 | 2.27 | 0.215 |
| 638 | MAG | cart | Shaw | Moguls | 12 to 24 | 3.5 | 0 |
| 638 | MAG | cart | Shaw | Moguls | 24 to 36 | 3.9 | 0 |
| 638 | MAG | cart | Shaw | Moguls | 36 to 48 | 3.9 | 0 |
| 638 | MAG | cart | Shaw | Desert Ext. | 0 to 6 | 1.64 | 0.08 |
| 638 | MAG | cart | Shaw | Desert Ext. | 6 to 12 | 2.26 | 0.136 |
| 638 | MAG | cart | Shaw | Desert Ext. | 12 to 24 | 3.3 | 0 |
| 638 | MAG | cart | Shaw | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 638 | MAG | cart | Shaw | Desert Ext. | 36 to 48 | 4 | 0 |
| 168 | EM | cart | TTF | Calibration | 0 to 6 | 1.8 | 0 |
| 168 | EM | cart | TTF | Calibration | 6 to 12 | 2.4 | 0 |
| 168 | EM | cart | TTF | Calibration | 12 to 24 | 3.7 | 0 |
| 168 | EM | cart | TTF | Calibration | 24 to 36 | 3.6 | 0 |
| 168 | EM | cart | TTF | Calibration | 36 to 48 | 3.983 | 0.037 |

Yuma Proving Ground Demonstrations

| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
|---------------|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| 168 | EM | cart | TTF | Moguls | 0 to 6 | 1.65 | 0.05 |
| 168 | EM | cart | TTF | Moguls | 6 to 12 | 2.167 | 0.047 |
| 168 | EM | cart | TTF | Moguls | 12 to 24 | 3.517 | 0.037 |
| 168 | EM | cart | TTF | Moguls | 24 to 36 | 3.9 | 0 |
| 168 | EM | cart | TTF | Moguls | 36 to 48 | 3.9 | 0 |
| 168 | EM | cart | TTF | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 168 | EM | cart | TTF | Desert Ext. | 6 to 12 | 2.217 | 0.055 |
| 168 | EM | cart | TTF | Desert Ext. | 12 to 24 | 3.358 | 0.049 |
| 168 | EM | cart | TTF | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 168 | EM | cart | TTF | Desert Ext. | 36 to 48 | 4.083 | 0.055 |
| 171 | EM | cart | TTF | Calibration | 0 to 6 | 1.8 | 0 |
| 171 | EM | cart | TTF | Calibration | 6 to 12 | 2.4 | 0 |
| 171 | EM | cart | TTF | Calibration | 12 to 24 | 3.7 | 0 |
| 171 | EM | cart | TTF | Calibration | 24 to 36 | 3.6 | 0 |
| 171 | EM | cart | TTF | Calibration | 36 to 48 | 3.983 | 0.037 |
| 171 | EM | cart | TTF | Moguls | 0 to 6 | 1.65 | 0.05 |
| 171 | EM | cart | TTF | Moguls | 6 to 12 | 2.167 | 0.047 |
| 171 | EM | cart | TTF | Moguls | 12 to 24 | 3.517 | 0.037 |
| 171 | EM | cart | TTF | Moguls | 24 to 36 | 3.9 | 0 |
| 171 | EM | cart | TTF | Moguls | 36 to 48 | 3.9 | 0 |
| 171 | EM | cart | TTF | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 171 | EM | cart | TTF | Desert Ext. | 6 to 12 | 2.217 | 0.055 |
| 171 | EM | cart | TTF | Desert Ext. | 12 to 24 | 3.358 | 0.049 |
| 171 | EM | cart | TTF | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 171 | EM | cart | TTF | Desert Ext. | 36 to 48 | 4.083 | 0.055 |
| 170 | EM | sling | TTF | Calibration | 0 to 6 | 1.8 | 0 |
| 170 | EM | sling | TTF | Calibration | 6 to 12 | 2.4 | 0 |
| 170 | EM | sling | TTF | Calibration | 12 to 24 | 3.7 | 0 |
| 170 | EM | sling | TTF | Calibration | 24 to 36 | 3.6 | 0 |
| 170 | EM | sling | TTF | Calibration | 36 to 48 | 3.983 | 0.037 |
| 170 | EM | sling | TTF | Moguls | 0 to 6 | 1.65 | 0.05 |
| 170 | EM | sling | TTF | Moguls | 6 to 12 | 2.167 | 0.047 |
| 170 | EM | sling | TTF | Moguls | 12 to 24 | 3.517 | 0.037 |
| 170 | EM | sling | TTF | Moguls | 24 to 36 | 3.9 | 0 |
| 170 | EM | sling | TTF | Moguls | 36 to 48 | 3.9 | 0 |
| 170 | EM | sling | TTF | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 170 | EM | sling | TTF | Desert Ext. | 6 to 12 | 2.217 | 0.055 |
| 170 | EM | sling | TTF | Desert Ext. | 12 to 24 | 3.358 | 0.049 |
| 170 | EM | sling | TTF | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 170 | EM | sling | TTF | Desert Ext. | 36 to 48 | 4.083 | 0.055 |
| 169 | EM | cart | TTF | Calibration | 0 to 6 | 1.8 | 0 |
| 169 | EM | cart | TTF | Calibration | 6 to 12 | 2.4 | 0 |
| 169 | EM | cart | TTF | Calibration | 12 to 24 | 3.7 | 0 |
| 169 | EM | cart | TTF | Calibration | 24 to 36 | 3.6 | 0 |
| 169 | EM | cart | TTF | Calibration | 36 to 48 | 3.983 | 0.037 |
| 169 | EM | cart | TTF | Moguls | 0 to 6 | 1.65 | 0.05 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------------|-------------------|------------------------------------|---------------------------|
| Report | Sensor | Platform | Vendor | Area Measured | Layer, in. | Average Moisture Content, % | Standard Deviation |
| 169 | EM | cart | TTF | Moguls | 6 to 12 | 2.167 | 0.047 |
| 169 | EM | cart | TTF | Moguls | 12 to 24 | 3.517 | 0.037 |
| 169 | EM | cart | TTF | Moguls | 24 to 36 | 3.9 | 0 |
| 169 | EM | cart | TTF | Moguls | 36 to 48 | 3.9 | 0 |
| 169 | EM | cart | TTF | Desert Ext. | 0 to 6 | 1.6 | 0 |
| 169 | EM | cart | TTF | Desert Ext. | 6 to 12 | 2.217 | 0.055 |
| 169 | EM | cart | TTF | Desert Ext. | 12 to 24 | 3.358 | 0.049 |
| 169 | EM | cart | TTF | Desert Ext. | 24 to 36 | 3.9 | 0 |
| 169 | EM | cart | TTF | Desert Ext. | 36 to 48 | 4.083 | 0.055 |

APPENDIX D. DAILY ACTIVITY LOGS

Note: The cost column is represented in dollars.

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 39 | EM | hand | AETC | Initial Setup | Supervisor | 0.5 | 47.5 |
| 39 | EM | hand | AETC | Initial Setup | Data Analyst | 0 | 0 |
| 39 | EM | hand | AETC | Initial Setup | Field Support | 0 | 0 |
| 39 | EM | hand | AETC | Initial Setup | Subtotal | 0 | 47.5 |
| 39 | EM | hand | AETC | Calibration | Supervisor | 8.75 | 831.25 |
| 39 | EM | hand | AETC | Calibration | Data Analyst | 0 | 0 |
| 39 | EM | hand | AETC | Calibration | Field Support | 0 | 0 |
| 39 | EM | hand | AETC | Calibration | Subtotal | 0 | 831.25 |
| 39 | EM | hand | AETC | Site Survey | Supervisor | 18.33 | 1741.35 |
| 39 | EM | hand | AETC | Site Survey | Data Analyst | 0 | 0 |
| 39 | EM | hand | AETC | Site Survey | Field Support | 0 | 0 |
| 39 | EM | hand | AETC | Site Survey | Subtotal | 0 | 1741.35 |
| 39 | EM | hand | AETC | Demobilization | Supervisor | 0.25 | 23.75 |
| 39 | EM | hand | AETC | Demobilization | Data Analyst | 0 | 0 |
| 39 | EM | hand | AETC | Demobilization | Field Support | 0 | 0 |
| 39 | EM | hand | AETC | Demobilization | Subtotal | 0 | 23.75 |
| 39 | EM | hand | AETC | Total | Total | 0 | 2643.85 |
| 695 | EM | hand | ARM | Initial Setup | Supervisor | 1.58 | 150.1 |
| 695 | EM | hand | ARM | Initial Setup | Data Analyst | 1.58 | 90.06 |
| 695 | EM | hand | ARM | Initial Setup | Field Support | 1.58 | 0 |
| 695 | EM | hand | ARM | Initial Setup | Subtotal | 0 | 240.16 |
| 695 | EM | hand | ARM | Calibration | Supervisor | 11.66 | 1107.7 |
| 695 | EM | hand | ARM | Calibration | Data Analyst | 11.66 | 664.62 |
| 695 | EM | hand | ARM | Calibration | Field Support | 11.66 | 0 |
| 695 | EM | hand | ARM | Calibration | Subtotal | 0 | 1772.32 |
| 695 | EM | hand | ARM | Site Survey | Supervisor | 15.58 | 1480.1 |
| 695 | EM | hand | ARM | Site Survey | Data Analyst | 15.58 | 888.06 |
| 695 | EM | hand | ARM | Site Survey | Field Support | 15.58 | 0 |
| 695 | EM | hand | ARM | Site Survey | Subtotal | 0 | 2368.16 |
| 695 | EM | hand | ARM | Demobilization | Supervisor | 0.5 | 47.5 |
| 695 | EM | hand | ARM | Demobilization | Data Analyst | 0.5 | 28.5 |
| 695 | EM | hand | ARM | Demobilization | Field Support | 0.5 | 0 |
| 695 | EM | hand | ARM | Demobilization | Subtotal | 0 | 76 |
| 695 | EM | hand | ARM | Total | Total | 0 | 4456.64 |
| 691 | EM | hand | ARM | Initial Setup | Supervisor | 1.08 | 102.6 |
| 691 | EM | hand | ARM | Initial Setup | Data Analyst | 1.08 | 61.56 |
| 691 | EM | hand | ARM | Initial Setup | Field Support | 1.08 | 0 |
| 691 | EM | hand | ARM | Initial Setup | Subtotal | 0 | 164.16 |
| 691 | EM | hand | ARM | Calibration | Supervisor | 12.16 | 1155.2 |
| 691 | EM | hand | ARM | Calibration | Data Analyst | 12.16 | 693.12 |
| 691 | EM | hand | ARM | Calibration | Field Support | 12.16 | 0 |
| 691 | EM | hand | ARM | Calibration | Subtotal | 0 | 1848.32 |
| 691 | EM | hand | ARM | Site Survey | Supervisor | 17.25 | 1638.75 |
| 691 | EM | hand | ARM | Site Survey | Data Analyst | 17.25 | 983.25 |
| 691 | EM | hand | ARM | Site Survey | Field Support | 17.25 | 0 |
| 691 | EM | hand | ARM | Site Survey | Subtotal | 0 | 2622 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 691 | EM | hand | ARM | Demobilization | Supervisor | 0.5 | 47.5 |
| 691 | EM | hand | ARM | Demobilization | Data Analyst | 0.5 | 28.5 |
| 691 | EM | hand | ARM | Demobilization | Field Support | 0.5 | 0 |
| 691 | EM | hand | ARM | Demobilization | Subtotal | 0 | 76 |
| 691 | EM | hand | ARM | Total | Total | 0 | 4710.48 |
| 622 | dual | cart | BH | Initial Setup | Supervisor | 13.25 | 1258.75 |
| 622 | dual | cart | BH | Initial Setup | Data Analyst | 13.25 | 755.25 |
| 622 | dual | cart | BH | Initial Setup | Field Support | 13.25 | 377.63 |
| 622 | dual | cart | BH | Initial Setup | Subtotal | 0 | 2391.63 |
| 622 | dual | cart | BH | Calibration | Supervisor | 3.33 | 316.35 |
| 622 | dual | cart | BH | Calibration | Data Analyst | 3.33 | 189.81 |
| 622 | dual | cart | BH | Calibration | Field Support | 3.33 | 94.91 |
| 622 | dual | cart | BH | Calibration | Subtotal | 0 | 601.07 |
| 622 | dual | cart | BH | Site Survey | Supervisor | 1.75 | 166.25 |
| 622 | dual | cart | BH | Site Survey | Data Analyst | 1.75 | 99.75 |
| 622 | dual | cart | BH | Site Survey | Field Support | 1.75 | 49.88 |
| 622 | dual | cart | BH | Site Survey | Subtotal | 0 | 315.88 |
| 622 | dual | cart | BH | Demobilization | Supervisor | 1.58 | 150.1 |
| 622 | dual | cart | BH | Demobilization | Data Analyst | 1.58 | 90.06 |
| 622 | dual | cart | BH | Demobilization | Field Support | 1.58 | 45.03 |
| 622 | dual | cart | BH | Demobilization | Subtotal | 0 | 285.19 |
| 622 | dual | cart | BH | Total | Total | 0 | 3593.77 |
| 642 | dual | cart | BH | Initial Setup | Supervisor | 13.25 | 1258.75 |
| 642 | dual | cart | BH | Initial Setup | Data Analyst | 13.25 | 755.25 |
| 642 | dual | cart | BH | Initial Setup | Field Support | 13.25 | 377.63 |
| 642 | dual | cart | BH | Initial Setup | Subtotal | 0 | 2391.63 |
| 642 | dual | cart | BH | Calibration | Supervisor | 4.27 | 405.65 |
| 642 | dual | cart | BH | Calibration | Data Analyst | 4.27 | 243.39 |
| 642 | dual | cart | BH | Calibration | Field Support | 4.27 | 121.7 |
| 642 | dual | cart | BH | Calibration | Subtotal | 0 | 770.74 |
| 642 | dual | cart | BH | Site Survey | Supervisor | 7.72 | 733.4 |
| 642 | dual | cart | BH | Site Survey | Data Analyst | 7.72 | 440.04 |
| 642 | dual | cart | BH | Site Survey | Field Support | 7.72 | 220.02 |
| 642 | dual | cart | BH | Site Survey | Subtotal | 0 | 1393.46 |
| 642 | dual | cart | BH | Demobilization | Supervisor | 1.58 | 150.1 |
| 642 | dual | cart | BH | Demobilization | Data Analyst | 1.58 | 90.06 |
| 642 | dual | cart | BH | Demobilization | Field Support | 1.58 | 45.03 |
| 642 | dual | cart | BH | Demobilization | Subtotal | 0 | 285.19 |
| 642 | dual | cart | BH | Total | Total | 0 | 4841.02 |
| 657 | dual | cart | BH | Initial Setup | Supervisor | 13.25 | 1258.75 |
| 657 | dual | cart | BH | Initial Setup | Data Analyst | 13.25 | 755.25 |
| 657 | dual | cart | BH | Initial Setup | Field Support | 13.25 | 377.63 |
| 657 | dual | cart | BH | Initial Setup | Subtotal | 0 | 2391.63 |
| 657 | dual | cart | BH | Calibration | Supervisor | 6.15 | 584.25 |
| 657 | dual | cart | BH | Calibration | Data Analyst | 6.15 | 350.55 |
| 657 | dual | cart | BH | Calibration | Field Support | 6.15 | 175.28 |
| 657 | dual | cart | BH | Calibration | Subtotal | 0 | 1110.08 |
| 657 | dual | cart | BH | Site Survey | Supervisor | 45.5 | 4322.5 |
| 657 | dual | cart | BH | Site Survey | Data Analyst | 45.5 | 2593.5 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 657 | dual | cart | BH | Site Survey | Field Support | 45.5 | 1296.75 |
| 657 | dual | cart | BH | Site Survey | Subtotal | 0 | 8212.75 |
| 657 | dual | cart | BH | Demobilization | Supervisor | 1.58 | 150.1 |
| 657 | dual | cart | BH | Demobilization | Data Analyst | 1.58 | 90.06 |
| 657 | dual | cart | BH | Demobilization | Field Support | 1.58 | 45.03 |
| 657 | dual | cart | BH | Demobilization | Subtotal | 0 | 285.19 |
| 657 | dual | cart | BH | Total | Total | 0 | 11999.65 |
| 636 | dual | cart | BH | Initial Setup | Supervisor | 13.25 | 1258.75 |
| 636 | dual | cart | BH | Initial Setup | Data Analyst | 13.25 | 755.25 |
| 636 | dual | cart | BH | Initial Setup | Field Support | 13.25 | 377.63 |
| 636 | dual | cart | BH | Initial Setup | Subtotal | 0 | 2391.63 |
| 636 | dual | cart | BH | Calibration | Supervisor | 3.25 | 308.75 |
| 636 | dual | cart | BH | Calibration | Data Analyst | 3.25 | 185.25 |
| 636 | dual | cart | BH | Calibration | Field Support | 3.25 | 92.63 |
| 636 | dual | cart | BH | Calibration | Subtotal | 0 | 586.63 |
| 636 | dual | cart | BH | Site Survey | Supervisor | 8.5 | 807.5 |
| 636 | dual | cart | BH | Site Survey | Data Analyst | 8.5 | 484.5 |
| 636 | dual | cart | BH | Site Survey | Field Support | 8.5 | 242.25 |
| 636 | dual | cart | BH | Site Survey | Subtotal | 0 | 1534.25 |
| 636 | dual | cart | BH | Demobilization | Supervisor | 1.58 | 150.1 |
| 636 | dual | cart | BH | Demobilization | Data Analyst | 1.58 | 90.06 |
| 636 | dual | cart | BH | Demobilization | Field Support | 1.58 | 45.03 |
| 636 | dual | cart | BH | Demobilization | Subtotal | 0 | 285.19 |
| 636 | dual | cart | BH | Total | Total | 0 | 4797.7 |
| 304 | EM | cart | ERDC | Initial Setup | Supervisor | 2.66 | 252.7 |
| 304 | EM | cart | ERDC | Initial Setup | Data Analyst | 2.66 | 151.62 |
| 304 | EM | cart | ERDC | Initial Setup | Field Support | 2.66 | 0 |
| 304 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 404.32 |
| 304 | EM | cart | ERDC | Calibration | Supervisor | 8.42 | 799.9 |
| 304 | EM | cart | ERDC | Calibration | Data Analyst | 8.42 | 479.94 |
| 304 | EM | cart | ERDC | Calibration | Field Support | 8.42 | 239.97 |
| 304 | EM | cart | ERDC | Calibration | Subtotal | 0 | 1519.81 |
| 304 | EM | cart | ERDC | Site Survey | Supervisor | 5.42 | 514.9 |
| 304 | EM | cart | ERDC | Site Survey | Data Analyst | 5.42 | 308.94 |
| 304 | EM | cart | ERDC | Site Survey | Field Support | 5.42 | 154.47 |
| 304 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 978.31 |
| 304 | EM | cart | ERDC | Demobilization | Supervisor | 2.75 | 261.25 |
| 304 | EM | cart | ERDC | Demobilization | Data Analyst | 2.75 | 156.75 |
| 304 | EM | cart | ERDC | Demobilization | Field Support | 2.75 | 78.38 |
| 304 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 496.38 |
| 304 | EM | cart | ERDC | Total | Total | 0 | 3398.82 |
| 305 | EM | cart | ERDC | Initial Setup | Supervisor | 2.66 | 252.7 |
| 305 | EM | cart | ERDC | Initial Setup | Data Analyst | 2.66 | 151.62 |
| 305 | EM | cart | ERDC | Initial Setup | Field Support | 2.66 | 0 |
| 305 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 404.32 |
| 305 | EM | cart | ERDC | Calibration | Supervisor | 17.33 | 1646.35 |
| 305 | EM | cart | ERDC | Calibration | Data Analyst | 17.33 | 987.81 |
| 305 | EM | cart | ERDC | Calibration | Field Support | 17.33 | 493.91 |
| 305 | EM | cart | ERDC | Calibration | Subtotal | 0 | 3128.07 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 305 | EM | cart | ERDC | Site Survey | Supervisor | 140.66 | 13362.7 |
| 305 | EM | cart | ERDC | Site Survey | Data Analyst | 140.66 | 8017.62 |
| 305 | EM | cart | ERDC | Site Survey | Field Support | 140.66 | 4008.81 |
| 305 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 25389.13 |
| 305 | EM | cart | ERDC | Demobilization | Supervisor | 2.75 | 261.25 |
| 305 | EM | cart | ERDC | Demobilization | Data Analyst | 2.75 | 156.75 |
| 305 | EM | cart | ERDC | Demobilization | Field Support | 2.75 | 78.38 |
| 305 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 496.38 |
| 305 | EM | cart | ERDC | Total | Total | 0 | 29417.9 |
| 142 | EM | cart | ERDC | Initial Setup | Supervisor | 4.75 | 451.25 |
| 142 | EM | cart | ERDC | Initial Setup | Data Analyst | 4.75 | 270.75 |
| 142 | EM | cart | ERDC | Initial Setup | Field Support | 4.75 | 270.75 |
| 142 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 992.75 |
| 142 | EM | cart | ERDC | Calibration | Supervisor | 4.25 | 403.75 |
| 142 | EM | cart | ERDC | Calibration | Data Analyst | 4.25 | 242.25 |
| 142 | EM | cart | ERDC | Calibration | Field Support | 4.25 | 242.25 |
| 142 | EM | cart | ERDC | Calibration | Subtotal | 0 | 888.25 |
| 142 | EM | cart | ERDC | Site Survey | Supervisor | 3.83 | 363.85 |
| 142 | EM | cart | ERDC | Site Survey | Data Analyst | 3.83 | 218.31 |
| 142 | EM | cart | ERDC | Site Survey | Field Support | 3.83 | 218.31 |
| 142 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 800.47 |
| 142 | EM | cart | ERDC | Demobilization | Supervisor | 1 | 95 |
| 142 | EM | cart | ERDC | Demobilization | Data Analyst | 1 | 57 |
| 142 | EM | cart | ERDC | Demobilization | Field Support | 1 | 57 |
| 142 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 209 |
| 142 | EM | cart | ERDC | Total | Total | 0 | 2890.47 |
| 141 | EM | cart | ERDC | Initial Setup | Supervisor | 3.25 | 308.75 |
| 141 | EM | cart | ERDC | Initial Setup | Data Analyst | 3.25 | 185.25 |
| 141 | EM | cart | ERDC | Initial Setup | Field Support | 3.25 | 185.25 |
| 141 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 679.25 |
| 141 | EM | cart | ERDC | Calibration | Supervisor | 8.41 | 798.95 |
| 141 | EM | cart | ERDC | Calibration | Data Analyst | 8.41 | 479.37 |
| 141 | EM | cart | ERDC | Calibration | Field Support | 8.41 | 479.37 |
| 141 | EM | cart | ERDC | Calibration | Subtotal | 0 | 1757.59 |
| 141 | EM | cart | ERDC | Site Survey | Supervisor | 12.33 | 1171.35 |
| 141 | EM | cart | ERDC | Site Survey | Data Analyst | 12.33 | 702.81 |
| 141 | EM | cart | ERDC | Site Survey | Field Support | 12.33 | 702.81 |
| 141 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 2576.97 |
| 141 | EM | cart | ERDC | Demobilization | Supervisor | 1 | 95 |
| 141 | EM | cart | ERDC | Demobilization | Data Analyst | 1 | 57 |
| 141 | EM | cart | ERDC | Demobilization | Field Support | 1 | 57 |
| 141 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 209 |
| 141 | EM | cart | ERDC | Total | Total | 0 | 5222.81 |
| 40 | dual | towed | Geocenters | Initial Setup | Supervisor | 1.83 | 173.85 |
| 40 | dual | towed | Geocenters | Initial Setup | Data Analyst | 1.83 | 104.31 |
| 40 | dual | towed | Geocenters | Initial Setup | Field Support | 0 | 0 |
| 40 | dual | towed | Geocenters | Initial Setup | Subtotal | 0 | 278.16 |
| 40 | dual | towed | Geocenters | Calibration | Supervisor | 5.17 | 491.15 |
| 40 | dual | towed | Geocenters | Calibration | Data Analyst | 5.17 | 294.69 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 40 | dual | towed | Geocenters | Calibration | Field Support | 0 | 0 |
| 40 | dual | towed | Geocenters | Calibration | Subtotal | 0 | 785.84 |
| 40 | dual | towed | Geocenters | Site Survey | Supervisor | 11.25 | 1068.75 |
| 40 | dual | towed | Geocenters | Site Survey | Data Analyst | 11.25 | 641.25 |
| 40 | dual | towed | Geocenters | Site Survey | Field Support | 0 | 0 |
| 40 | dual | towed | Geocenters | Site Survey | Subtotal | 0 | 1710 |
| 40 | dual | towed | Geocenters | Demobilization | Supervisor | 2 | 190 |
| 40 | dual | towed | Geocenters | Demobilization | Data Analyst | 2 | 114 |
| 40 | dual | towed | Geocenters | Demobilization | Field Support | 0 | 0 |
| 40 | dual | towed | Geocenters | Demobilization | Subtotal | 0 | 304 |
| 40 | dual | towed | Geocenters | Total | Total | 0 | 3078 |
| 290 | dual | towed | Geocenters | Initial Setup | Supervisor | 6.25 | 593.75 |
| 290 | dual | towed | Geocenters | Initial Setup | Data Analyst | 6.25 | 356.25 |
| 290 | dual | towed | Geocenters | Initial Setup | Field Support | 6.25 | 0 |
| 290 | dual | towed | Geocenters | Initial Setup | Subtotal | 0 | 950 |
| 290 | dual | towed | Geocenters | Calibration | Supervisor | 0.75 | 71.25 |
| 290 | dual | towed | Geocenters | Calibration | Data Analyst | 0.75 | 42.75 |
| 290 | dual | towed | Geocenters | Calibration | Field Support | 0.75 | 0 |
| 290 | dual | towed | Geocenters | Calibration | Subtotal | 0 | 114 |
| 290 | dual | towed | Geocenters | Site Survey | Supervisor | 2.5 | 237.5 |
| 290 | dual | towed | Geocenters | Site Survey | Data Analyst | 2.5 | 142.5 |
| 290 | dual | towed | Geocenters | Site Survey | Field Support | 2.5 | 0 |
| 290 | dual | towed | Geocenters | Site Survey | Subtotal | 0 | 380 |
| 290 | dual | towed | Geocenters | Demobilization | Supervisor | 3.75 | 356.25 |
| 290 | dual | towed | Geocenters | Demobilization | Data Analyst | 3.75 | 213.75 |
| 290 | dual | towed | Geocenters | Demobilization | Field Support | 3.75 | 0 |
| 290 | dual | towed | Geocenters | Demobilization | Subtotal | 0 | 570 |
| 290 | dual | towed | Geocenters | Total | Total | 0 | 2014 |
| 187 | dual | towed | Geocenters | Initial Setup | Supervisor | 1.83 | 173.85 |
| 187 | dual | towed | Geocenters | Initial Setup | Data Analyst | 1.83 | 104.31 |
| 187 | dual | towed | Geocenters | Initial Setup | Field Support | 1.83 | 0 |
| 187 | dual | towed | Geocenters | Initial Setup | Subtotal | 0 | 278.16 |
| 187 | dual | towed | Geocenters | Calibration | Supervisor | 5.17 | 491.15 |
| 187 | dual | towed | Geocenters | Calibration | Data Analyst | 5.17 | 294.69 |
| 187 | dual | towed | Geocenters | Calibration | Field Support | 5.17 | 0 |
| 187 | dual | towed | Geocenters | Calibration | Subtotal | 0 | 785.84 |
| 187 | dual | towed | Geocenters | Site Survey | Supervisor | 17.33 | 1646.35 |
| 187 | dual | towed | Geocenters | Site Survey | Data Analyst | 17.33 | 987.81 |
| 187 | dual | towed | Geocenters | Site Survey | Field Support | 17.33 | 0 |
| 187 | dual | towed | Geocenters | Site Survey | Subtotal | 0 | 2634.16 |
| 187 | dual | towed | Geocenters | Demobilization | Supervisor | 2 | 190 |
| 187 | dual | towed | Geocenters | Demobilization | Data Analyst | 2 | 114 |
| 187 | dual | towed | Geocenters | Demobilization | Field Support | 2 | 0 |
| 187 | dual | towed | Geocenters | Demobilization | Subtotal | 0 | 304 |
| 187 | dual | towed | Geocenters | Total | Total | 0 | 4002.16 |
| 298 | dual | towed | Geocenters | Initial Setup | Supervisor | 6.25 | 593.75 |
| 298 | dual | towed | Geocenters | Initial Setup | Data Analyst | 6.25 | 356.25 |
| 298 | dual | towed | Geocenters | Initial Setup | Field Support | 6.25 | 0 |
| 298 | dual | towed | Geocenters | Initial Setup | Subtotal | 0 | 950 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 298 | dual | towed | Geocenters | Calibration | Supervisor | 0.75 | 71.25 |
| 298 | dual | towed | Geocenters | Calibration | Data Analyst | 0.75 | 42.75 |
| 298 | dual | towed | Geocenters | Calibration | Field Support | 0.75 | 0 |
| 298 | dual | towed | Geocenters | Calibration | Subtotal | 0 | 114 |
| 298 | dual | towed | Geocenters | Site Survey | Supervisor | 13.33 | 1266.35 |
| 298 | dual | towed | Geocenters | Site Survey | Data Analyst | 13.33 | 759.81 |
| 298 | dual | towed | Geocenters | Site Survey | Field Support | 13.33 | 0 |
| 298 | dual | towed | Geocenters | Site Survey | Subtotal | 0 | 2026.16 |
| 298 | dual | towed | Geocenters | Demobilization | Supervisor | 3.75 | 356.25 |
| 298 | dual | towed | Geocenters | Demobilization | Data Analyst | 3.75 | 213.75 |
| 298 | dual | towed | Geocenters | Demobilization | Field Support | 3.75 | 0 |
| 298 | dual | towed | Geocenters | Demobilization | Subtotal | 0 | 570 |
| 298 | dual | towed | Geocenters | Total | Total | 0 | 3660.16 |
| 792 | dual | towed | Geocenters | Initial Setup | Supervisor | 6 | 570 |
| 792 | dual | towed | Geocenters | Initial Setup | Data Analyst | 6 | 0 |
| 792 | dual | towed | Geocenters | Initial Setup | Field Support | 6 | 171 |
| 792 | dual | towed | Geocenters | Initial Setup | Subtotal | 0 | 741 |
| 792 | dual | towed | Geocenters | Calibration | Supervisor | 1.66 | 157.7 |
| 792 | dual | towed | Geocenters | Calibration | Data Analyst | 1.66 | 0 |
| 792 | dual | towed | Geocenters | Calibration | Field Support | 1.66 | 94.62 |
| 792 | dual | towed | Geocenters | Calibration | Subtotal | 0 | 252.32 |
| 792 | dual | towed | Geocenters | Site Survey | Supervisor | 2.42 | 229.9 |
| 792 | dual | towed | Geocenters | Site Survey | Data Analyst | 2.42 | 0 |
| 792 | dual | towed | Geocenters | Site Survey | Field Support | 2.42 | 137.94 |
| 792 | dual | towed | Geocenters | Site Survey | Subtotal | 0 | 367.84 |
| 792 | dual | towed | Geocenters | Demobilization | Supervisor | 2.58 | 245.1 |
| 792 | dual | towed | Geocenters | Demobilization | Data Analyst | 2.58 | 0 |
| 792 | dual | towed | Geocenters | Demobilization | Field Support | 2.58 | 147.06 |
| 792 | dual | towed | Geocenters | Demobilization | Subtotal | 0 | 392.16 |
| 792 | dual | towed | Geocenters | Total | Total | 0 | 1753.32 |
| 802 | dual | towed | Geocenters | Calibration | Data Analyst | 1.66 | 0 |
| 802 | dual | towed | Geocenters | Calibration | Field Support | 1.66 | 94.62 |
| 802 | dual | towed | Geocenters | Calibration | Subtotal | 0 | 252.32 |
| 802 | dual | towed | Geocenters | Site Survey | Supervisor | 14.5 | 1377.5 |
| 802 | dual | towed | Geocenters | Site Survey | Data Analyst | 14.5 | 0 |
| 802 | dual | towed | Geocenters | Site Survey | Field Support | 14.5 | 826.5 |
| 802 | dual | towed | Geocenters | Site Survey | Subtotal | 0 | 2204 |
| 802 | dual | towed | Geocenters | Demobilization | Supervisor | 2.58 | 245.1 |
| 802 | dual | towed | Geocenters | Demobilization | Data Analyst | 2.58 | 0 |
| 802 | dual | towed | Geocenters | Demobilization | Field Support | 2.58 | 147.06 |
| 802 | dual | towed | Geocenters | Demobilization | Subtotal | 0 | 392.16 |
| 802 | dual | towed | Geocenters | Total | Total | 0 | 3589.48 |
| 802 | dual | towed | Geocenters | Initial Setup | Supervisor | 6 | 570 |
| 802 | dual | towed | Geocenters | Initial Setup | Data Analyst | 6 | 0 |
| 802 | dual | towed | Geocenters | Initial Setup | Field Support | 6 | 171 |
| 802 | dual | towed | Geocenters | Initial Setup | Subtotal | 0 | 741 |
| 802 | dual | towed | Geocenters | Calibration | Supervisor | 1.66 | 157.7 |
| 50 | EM | hand | Geophex | Initial Setup | Field Support | 0.33 | 9.41 |
| 50 | EM | hand | Geophex | Initial Setup | Subtotal | 0 | 59.57 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 50 | EM | hand | Geophex | Calibration | Supervisor | 3.5 | 332.5 |
| 50 | EM | hand | Geophex | Calibration | Data Analyst | 3.5 | 199.5 |
| 50 | EM | hand | Geophex | Calibration | Field Support | 3.5 | 99.75 |
| 50 | EM | hand | Geophex | Calibration | Subtotal | 0 | 631.75 |
| 50 | EM | hand | Geophex | Site Survey | Supervisor | 3.65 | 346.75 |
| 50 | EM | hand | Geophex | Site Survey | Data Analyst | 3.65 | 208.05 |
| 50 | EM | hand | Geophex | Site Survey | Field Support | 3.65 | 104.03 |
| 50 | EM | hand | Geophex | Site Survey | Subtotal | 0 | 658.83 |
| 50 | EM | hand | Geophex | Demobilization | Supervisor | 0.16 | 15.2 |
| 50 | EM | hand | Geophex | Demobilization | Data Analyst | 0.16 | 9.12 |
| 50 | EM | hand | Geophex | Demobilization | Field Support | 0.16 | 4.56 |
| 50 | EM | hand | Geophex | Demobilization | Subtotal | 0 | 28.88 |
| 50 | EM | hand | Geophex | Total | Total | 0 | 1379.03 |
| 50 | EM | hand | Geophex | Initial Setup | Supervisor | 0.33 | 31.35 |
| 50 | EM | hand | Geophex | Initial Setup | Data Analyst | 0.33 | 18.81 |
| 680 | EM | hand | Geophex | Initial Setup | Supervisor | 4.83 | 458.85 |
| 680 | EM | hand | Geophex | Initial Setup | Data Analyst | 4.83 | 275.31 |
| 680 | EM | hand | Geophex | Initial Setup | Field Support | 4.83 | 412.97 |
| 680 | EM | hand | Geophex | Initial Setup | Subtotal | 0 | 1147.13 |
| 680 | EM | hand | Geophex | Calibration | Supervisor | 2.5 | 237.5 |
| 680 | EM | hand | Geophex | Calibration | Data Analyst | 2.5 | 142.5 |
| 680 | EM | hand | Geophex | Calibration | Field Support | 2.5 | 0 |
| 680 | EM | hand | Geophex | Calibration | Subtotal | 0 | 380 |
| 680 | EM | hand | Geophex | Site Survey | Supervisor | 4.66 | 442.7 |
| 680 | EM | hand | Geophex | Site Survey | Data Analyst | 4.66 | 265.62 |
| 680 | EM | hand | Geophex | Site Survey | Field Support | 4.66 | 398.43 |
| 680 | EM | hand | Geophex | Site Survey | Subtotal | 0 | 1106.75 |
| 680 | EM | hand | Geophex | Demobilization | Supervisor | 0.83 | 78.85 |
| 680 | EM | hand | Geophex | Demobilization | Data Analyst | 0.83 | 47.31 |
| 680 | EM | hand | Geophex | Demobilization | Field Support | 0.83 | 70.97 |
| 680 | EM | hand | Geophex | Demobilization | Subtotal | 0 | 197.13 |
| 680 | EM | hand | Geophex | Total | Total | 0 | 2831.01 |
| 125 | EM | towed | Geophex | Initial Setup | Supervisor | 4.6 | 437 |
| 125 | EM | towed | Geophex | Initial Setup | Data Analyst | 4.6 | 262.2 |
| 125 | EM | towed | Geophex | Initial Setup | Field Support | 4.6 | 131.1 |
| 125 | EM | towed | Geophex | Initial Setup | Subtotal | 0 | 830.3 |
| 125 | EM | towed | Geophex | Calibration | Supervisor | 6.6 | 627 |
| 125 | EM | towed | Geophex | Calibration | Data Analyst | 6.6 | 376.2 |
| 125 | EM | towed | Geophex | Calibration | Field Support | 6.6 | 188.1 |
| 125 | EM | towed | Geophex | Calibration | Subtotal | 0 | 1191.3 |
| 125 | EM | towed | Geophex | Site Survey | Supervisor | 0.9 | 85.5 |
| 125 | EM | towed | Geophex | Site Survey | Data Analyst | 0.9 | 51.3 |
| 125 | EM | towed | Geophex | Site Survey | Field Support | 0.9 | 25.65 |
| 125 | EM | towed | Geophex | Site Survey | Subtotal | 0 | 162.45 |
| 125 | EM | towed | Geophex | Demobilization | Supervisor | 1.12 | 106.4 |
| 125 | EM | towed | Geophex | Demobilization | Data Analyst | 1.12 | 63.84 |
| 125 | EM | towed | Geophex | Demobilization | Field Support | 1.12 | 0 |
| 125 | EM | towed | Geophex | Demobilization | Subtotal | 0 | 170.24 |
| 125 | EM | towed | Geophex | Total | Total | 0 | 2354.29 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 49 | EM | cart | Geophex | Initial Setup | Supervisor | 3.6 | 342 |
| 49 | EM | cart | Geophex | Initial Setup | Data Analyst | 3.6 | 205.2 |
| 49 | EM | cart | Geophex | Initial Setup | Field Support | 3.6 | 102.6 |
| 49 | EM | cart | Geophex | Initial Setup | Subtotal | 0 | 649.8 |
| 49 | EM | cart | Geophex | Calibration | Supervisor | 6.6 | 627 |
| 49 | EM | cart | Geophex | Calibration | Data Analyst | 6.6 | 376.2 |
| 49 | EM | cart | Geophex | Calibration | Field Support | 6.6 | 188.1 |
| 49 | EM | cart | Geophex | Calibration | Subtotal | 0 | 1191.3 |
| 49 | EM | cart | Geophex | Site Survey | Supervisor | 9.9 | 940.5 |
| 49 | EM | cart | Geophex | Site Survey | Data Analyst | 9.9 | 564.3 |
| 49 | EM | cart | Geophex | Site Survey | Field Support | 9.9 | 282.15 |
| 49 | EM | cart | Geophex | Site Survey | Subtotal | 0 | 1786.95 |
| 49 | EM | cart | Geophex | Demobilization | Supervisor | 1.12 | 106.4 |
| 49 | EM | cart | Geophex | Demobilization | Data Analyst | 1.12 | 63.84 |
| 49 | EM | cart | Geophex | Demobilization | Field Support | 1.12 | 0 |
| 49 | EM | cart | Geophex | Demobilization | Subtotal | 0 | 170.24 |
| 49 | EM | cart | Geophex | Total | Total | 0 | 3798.29 |
| 451 | EM | cart | Geophex | Initial Setup | Supervisor | 3.33 | 632.7 |
| 451 | EM | cart | Geophex | Initial Setup | Data Analyst | 3.33 | 189.81 |
| 451 | EM | cart | Geophex | Initial Setup | Field Support | 3.33 | 474.53 |
| 451 | EM | cart | Geophex | Initial Setup | Subtotal | 0 | 1297.04 |
| 451 | EM | cart | Geophex | Calibration | Supervisor | 3.52 | 668.8 |
| 451 | EM | cart | Geophex | Calibration | Data Analyst | 3.52 | 200.64 |
| 451 | EM | cart | Geophex | Calibration | Field Support | 3.52 | 501.6 |
| 451 | EM | cart | Geophex | Calibration | Subtotal | 0 | 1371.04 |
| 451 | EM | cart | Geophex | Site Survey | Supervisor | 30.53 | 5800.7 |
| 451 | EM | cart | Geophex | Site Survey | Data Analyst | 30.53 | 1740.21 |
| 451 | EM | cart | Geophex | Site Survey | Field Support | 30.53 | 4350.53 |
| 451 | EM | cart | Geophex | Site Survey | Subtotal | 0 | 11891.44 |
| 451 | EM | cart | Geophex | Demobilization | Supervisor | 2 | 380 |
| 451 | EM | cart | Geophex | Demobilization | Data Analyst | 2 | 114 |
| 451 | EM | cart | Geophex | Demobilization | Field Support | 2 | 285 |
| 451 | EM | cart | Geophex | Demobilization | Subtotal | 0 | 779 |
| 451 | EM | cart | Geophex | Total | Total | 0 | 15338.52 |
| 665 | EM | hand | Geophex | Initial Setup | Supervisor | 4.83 | 458.85 |
| 665 | EM | hand | Geophex | Initial Setup | Data Analyst | 4.83 | 275.31 |
| 665 | EM | hand | Geophex | Initial Setup | Field Support | 4.83 | 412.97 |
| 665 | EM | hand | Geophex | Initial Setup | Subtotal | 0 | 1147.13 |
| 665 | EM | hand | Geophex | Calibration | Supervisor | 2.5 | 237.5 |
| 665 | EM | hand | Geophex | Calibration | Data Analyst | 2.5 | 142.5 |
| 665 | EM | hand | Geophex | Calibration | Field Support | 2.5 | 0 |
| 665 | EM | hand | Geophex | Calibration | Subtotal | 0 | 380 |
| 665 | EM | hand | Geophex | Site Survey | Supervisor | 51.08 | 4852.6 |
| 665 | EM | hand | Geophex | Site Survey | Data Analyst | 51.08 | 2911.56 |
| 665 | EM | hand | Geophex | Site Survey | Field Support | 51.08 | 4367.34 |
| 665 | EM | hand | Geophex | Site Survey | Subtotal | 0 | 12131.5 |
| 665 | EM | hand | Geophex | Demobilization | Supervisor | 0.83 | 78.85 |
| 665 | EM | hand | Geophex | Demobilization | Data Analyst | 0.83 | 47.31 |
| 665 | EM | hand | Geophex | Demobilization | Field Support | 0.83 | 70.97 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 665 | EM | hand | Geophex | Demobilization | Subtotal | 0 | 197.13 |
| 665 | EM | hand | Geophex | Total | Total | 0 | 13855.76 |
| 129 | EM | towed | Geophex | Initial Setup | Supervisor | 3.58 | 340.1 |
| 129 | EM | towed | Geophex | Initial Setup | Data Analyst | 3.58 | 204.06 |
| 129 | EM | towed | Geophex | Initial Setup | Field Support | 3.58 | 204.06 |
| 129 | EM | towed | Geophex | Initial Setup | Subtotal | 0 | 748.22 |
| 129 | EM | towed | Geophex | Calibration | Supervisor | 2.93 | 278.35 |
| 129 | EM | towed | Geophex | Calibration | Data Analyst | 0 | 0 |
| 129 | EM | towed | Geophex | Calibration | Field Support | 0 | 0 |
| 129 | EM | towed | Geophex | Calibration | Subtotal | 0 | 278.35 |
| 129 | EM | towed | Geophex | Site Survey | Supervisor | 120.88 | 11483.6 |
| 129 | EM | towed | Geophex | Site Survey | Data Analyst | 120.88 | 6890.16 |
| 129 | EM | towed | Geophex | Site Survey | Field Support | 120.88 | 13780.32 |
| 129 | EM | towed | Geophex | Site Survey | Subtotal | 0 | 32154.08 |
| 129 | EM | towed | Geophex | Demobilization | Supervisor | 1.12 | 106.4 |
| 129 | EM | towed | Geophex | Demobilization | Data Analyst | 1.12 | 63.84 |
| 129 | EM | towed | Geophex | Demobilization | Field Support | 0 | 0 |
| 129 | EM | towed | Geophex | Demobilization | Subtotal | 0 | 170.24 |
| 129 | EM | towed | Geophex | Total | Total | 0 | 33350.89 |
| 449 | EM | cart | Geophex | Initial Setup | Supervisor | 3.58 | 340.1 |
| 449 | EM | cart | Geophex | Initial Setup | Data Analyst | 3.58 | 204.06 |
| 449 | EM | cart | Geophex | Initial Setup | Field Support | 3.58 | 102.03 |
| 449 | EM | cart | Geophex | Initial Setup | Subtotal | 0 | 646.19 |
| 449 | EM | cart | Geophex | Calibration | Supervisor | 3.52 | 334.4 |
| 449 | EM | cart | Geophex | Calibration | Data Analyst | 3.52 | 200.64 |
| 449 | EM | cart | Geophex | Calibration | Field Support | 0 | 0 |
| 449 | EM | cart | Geophex | Calibration | Subtotal | 0 | 535.04 |
| 449 | EM | cart | Geophex | Site Survey | Supervisor | 71.55 | 6797.25 |
| 449 | EM | cart | Geophex | Site Survey | Data Analyst | 71.55 | 4078.35 |
| 449 | EM | cart | Geophex | Site Survey | Field Support | 71.55 | 2039.18 |
| 449 | EM | cart | Geophex | Site Survey | Subtotal | 0 | 12914.78 |
| 449 | EM | cart | Geophex | Demobilization | Supervisor | 1.12 | 106.4 |
| 449 | EM | cart | Geophex | Demobilization | Data Analyst | 1.12 | 63.84 |
| 449 | EM | cart | Geophex | Demobilization | Field Support | 0 | 0 |
| 449 | EM | cart | Geophex | Demobilization | Subtotal | 0 | 170.24 |
| 449 | EM | cart | Geophex | Total | Total | 0 | 14266.25 |
| 694 | EM | cart | Geophex | Initial Setup | Supervisor | 11.25 | 1068.75 |
| 694 | EM | cart | Geophex | Initial Setup | Data Analyst | 11.25 | 641.25 |
| 694 | EM | cart | Geophex | Initial Setup | Field Support | 11.25 | 961.88 |
| 694 | EM | cart | Geophex | Initial Setup | Subtotal | 0 | 2671.88 |
| 694 | EM | cart | Geophex | Calibration | Supervisor | 1.75 | 166.25 |
| 694 | EM | cart | Geophex | Calibration | Data Analyst | 1.75 | 99.75 |
| 694 | EM | cart | Geophex | Calibration | Field Support | 1.75 | 0 |
| 694 | EM | cart | Geophex | Calibration | Subtotal | 0 | 266 |
| 694 | EM | cart | Geophex | Site Survey | Supervisor | 4.25 | 403.75 |
| 694 | EM | cart | Geophex | Site Survey | Data Analyst | 4.25 | 242.25 |
| 694 | EM | cart | Geophex | Site Survey | Field Support | 4.25 | 0 |
| 694 | EM | cart | Geophex | Site Survey | Subtotal | 0 | 646 |
| 694 | EM | cart | Geophex | Demobilization | Supervisor | 0.83 | 78.85 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 694 | EM | cart | Geophex | Demobilization | Data Analyst | 0.83 | 47.31 |
| 694 | EM | cart | Geophex | Demobilization | Field Support | 0.83 | 70.97 |
| 694 | EM | cart | Geophex | Demobilization | Subtotal | 0 | 197.13 |
| 694 | EM | cart | Geophex | Total | Total | 0 | 3781.01 |
| 739 | EM | towed | Geophex | Initial Setup | Supervisor | 13.5 | 1282.5 |
| 739 | EM | towed | Geophex | Initial Setup | Data Analyst | 13.5 | 769.5 |
| 739 | EM | towed | Geophex | Initial Setup | Field Support | 13.5 | 0 |
| 739 | EM | towed | Geophex | Initial Setup | Subtotal | 0 | 2052 |
| 739 | EM | towed | Geophex | Calibration | Supervisor | 1.16 | 110.2 |
| 739 | EM | towed | Geophex | Calibration | Data Analyst | 1.16 | 66.12 |
| 739 | EM | towed | Geophex | Calibration | Field Support | 1.16 | 0 |
| 739 | EM | towed | Geophex | Calibration | Subtotal | 0 | 176.32 |
| 739 | EM | towed | Geophex | Site Survey | Supervisor | 1.16 | 110.2 |
| 739 | EM | towed | Geophex | Site Survey | Data Analyst | 1.16 | 66.12 |
| 739 | EM | towed | Geophex | Site Survey | Field Support | 1.16 | 0 |
| 739 | EM | towed | Geophex | Site Survey | Subtotal | 0 | 176.32 |
| 739 | EM | towed | Geophex | Demobilization | Supervisor | 2.08 | 197.6 |
| 739 | EM | towed | Geophex | Demobilization | Data Analyst | 2.08 | 118.56 |
| 739 | EM | towed | Geophex | Demobilization | Field Support | 2.08 | 0 |
| 739 | EM | towed | Geophex | Demobilization | Subtotal | 0 | 316.16 |
| 739 | EM | towed | Geophex | Total | Total | 0 | 2720.8 |
| 693 | EM | cart | Geophex | Initial Setup | Supervisor | 11.25 | 1068.75 |
| 693 | EM | cart | Geophex | Initial Setup | Data Analyst | 11.25 | 641.25 |
| 693 | EM | cart | Geophex | Initial Setup | Field Support | 11.25 | 961.88 |
| 693 | EM | cart | Geophex | Initial Setup | Subtotal | 0 | 2671.88 |
| 693 | EM | cart | Geophex | Calibration | Supervisor | 1.75 | 166.25 |
| 693 | EM | cart | Geophex | Calibration | Data Analyst | 1.75 | 99.75 |
| 693 | EM | cart | Geophex | Calibration | Field Support | 1.75 | 0 |
| 693 | EM | cart | Geophex | Calibration | Subtotal | 0 | 266 |
| 693 | EM | cart | Geophex | Site Survey | Supervisor | 4.25 | 403.75 |
| 693 | EM | cart | Geophex | Site Survey | Data Analyst | 4.25 | 242.25 |
| 693 | EM | cart | Geophex | Site Survey | Field Support | 4.25 | 0 |
| 693 | EM | cart | Geophex | Site Survey | Subtotal | 0 | 646 |
| 693 | EM | cart | Geophex | Demobilization | Supervisor | 0.83 | 78.85 |
| 693 | EM | cart | Geophex | Demobilization | Data Analyst | 0.83 | 47.31 |
| 693 | EM | cart | Geophex | Demobilization | Field Support | 0.83 | 70.97 |
| 693 | EM | cart | Geophex | Demobilization | Subtotal | 0 | 197.13 |
| 693 | EM | cart | Geophex | Total | Total | 0 | 3781.01 |
| 740 | EM | towed | Geophex | Initial Setup | Supervisor | 13.5 | 1282.5 |
| 740 | EM | towed | Geophex | Initial Setup | Data Analyst | 13.5 | 769.5 |
| 740 | EM | towed | Geophex | Initial Setup | Field Support | 13.5 | 0 |
| 740 | EM | towed | Geophex | Initial Setup | Subtotal | 0 | 2052 |
| 740 | EM | towed | Geophex | Calibration | Supervisor | 1.16 | 110.2 |
| 740 | EM | towed | Geophex | Calibration | Data Analyst | 1.16 | 66.12 |
| 740 | EM | towed | Geophex | Calibration | Field Support | 1.16 | 0 |
| 740 | EM | towed | Geophex | Calibration | Subtotal | 0 | 176.32 |
| 740 | EM | towed | Geophex | Site Survey | Supervisor | 47.5 | 4512.5 |
| 740 | EM | towed | Geophex | Site Survey | Data Analyst | 47.5 | 2707.5 |
| 740 | EM | towed | Geophex | Site Survey | Field Support | 47.5 | 0 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 740 | EM | towed | Geophex | Site Survey | Subtotal | 0 | 7220 |
| 740 | EM | towed | Geophex | Demobilization | Supervisor | 2.08 | 197.6 |
| 740 | EM | towed | Geophex | Demobilization | Data Analyst | 2.08 | 118.56 |
| 740 | EM | towed | Geophex | Demobilization | Field Support | 2.08 | 0 |
| 740 | EM | towed | Geophex | Demobilization | Subtotal | 0 | 316.16 |
| 740 | EM | towed | Geophex | Total | Total | 0 | 9764.48 |
| 184 | EM | hand | G-TEK | Initial Setup | Supervisor | 0 | 0 |
| 184 | EM | hand | G-TEK | Initial Setup | Data Analyst | 0 | 0 |
| 184 | EM | hand | G-TEK | Initial Setup | Field Support | 0 | 0 |
| 184 | EM | hand | G-TEK | Initial Setup | Subtotal | 0 | 0 |
| 184 | EM | hand | G-TEK | Calibration | Supervisor | 2.83 | 268.85 |
| 184 | EM | hand | G-TEK | Calibration | Data Analyst | 2.83 | 161.31 |
| 184 | EM | hand | G-TEK | Calibration | Field Support | 0 | 0 |
| 184 | EM | hand | G-TEK | Calibration | Subtotal | 0 | 430.16 |
| 184 | EM | hand | G-TEK | Site Survey | Supervisor | 0.42 | 39.9 |
| 184 | EM | hand | G-TEK | Site Survey | Data Analyst | 0.42 | 23.94 |
| 184 | EM | hand | G-TEK | Site Survey | Field Support | 0 | 0 |
| 184 | EM | hand | G-TEK | Site Survey | Subtotal | 0 | 63.84 |
| 184 | EM | hand | G-TEK | Demobilization | Supervisor | 2.33 | 221.35 |
| 184 | EM | hand | G-TEK | Demobilization | Data Analyst | 2.33 | 132.81 |
| 184 | EM | hand | G-TEK | Demobilization | Field Support | 0 | 0 |
| 184 | EM | hand | G-TEK | Demobilization | Subtotal | 0 | 354.16 |
| 184 | EM | hand | G-TEK | Total | Total | 0 | 848.16 |
| 183 | EM | sling | G-TEK | Initial Setup | Supervisor | 2.75 | 261.25 |
| 183 | EM | sling | G-TEK | Initial Setup | Data Analyst | 2.75 | 156.75 |
| 183 | EM | sling | G-TEK | Initial Setup | Field Support | 0 | 0 |
| 183 | EM | sling | G-TEK | Initial Setup | Subtotal | 0 | 418 |
| 183 | EM | sling | G-TEK | Calibration | Supervisor | 1.67 | 158.65 |
| 183 | EM | sling | G-TEK | Calibration | Data Analyst | 1.67 | 95.19 |
| 183 | EM | sling | G-TEK | Calibration | Field Support | 0 | 0 |
| 183 | EM | sling | G-TEK | Calibration | Subtotal | 0 | 253.84 |
| 183 | EM | sling | G-TEK | Site Survey | Supervisor | 3.58 | 340.1 |
| 183 | EM | sling | G-TEK | Site Survey | Data Analyst | 3.58 | 204.06 |
| 183 | EM | sling | G-TEK | Site Survey | Field Support | 0 | 0 |
| 183 | EM | sling | G-TEK | Site Survey | Subtotal | 0 | 544.16 |
| 183 | EM | sling | G-TEK | Demobilization | Supervisor | 3.08 | 292.6 |
| 183 | EM | sling | G-TEK | Demobilization | Data Analyst | 3.08 | 175.56 |
| 183 | EM | sling | G-TEK | Demobilization | Field Support | 0 | 0 |
| 183 | EM | sling | G-TEK | Demobilization | Subtotal | 0 | 468.16 |
| 183 | EM | sling | G-TEK | Total | Total | 0 | 1684.16 |
| 545 | EM | sling | G-TEK | Initial Setup | Supervisor | 2.75 | 261.25 |
| 545 | EM | sling | G-TEK | Initial Setup | Data Analyst | 2.75 | 156.75 |
| 545 | EM | sling | G-TEK | Initial Setup | Field Support | 0 | 0 |
| 545 | EM | sling | G-TEK | Initial Setup | Subtotal | 0 | 418 |
| 545 | EM | sling | G-TEK | Calibration | Supervisor | 1.92 | 182.4 |
| 545 | EM | sling | G-TEK | Calibration | Data Analyst | 1.92 | 109.44 |
| 545 | EM | sling | G-TEK | Calibration | Field Support | 0 | 0 |
| 545 | EM | sling | G-TEK | Calibration | Subtotal | 0 | 291.84 |
| 545 | EM | sling | G-TEK | Site Survey | Supervisor | 9.67 | 918.65 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 545 | EM | sling | G-TEK | Site Survey | Data Analyst | 9.67 | 551.19 |
| 545 | EM | sling | G-TEK | Site Survey | Field Support | 0 | 0 |
| 545 | EM | sling | G-TEK | Site Survey | Subtotal | 0 | 1469.84 |
| 545 | EM | sling | G-TEK | Demobilization | Supervisor | 2.33 | 221.35 |
| 545 | EM | sling | G-TEK | Demobilization | Data Analyst | 2.33 | 132.81 |
| 545 | EM | sling | G-TEK | Demobilization | Field Support | 0 | 0 |
| 545 | EM | sling | G-TEK | Demobilization | Subtotal | 0 | 354.16 |
| 545 | EM | sling | G-TEK | Total | Total | 0 | 2533.84 |
| 154 | EM | sling | G-TEK | Initial Setup | Supervisor | 2.75 | 261.25 |
| 154 | EM | sling | G-TEK | Initial Setup | Data Analyst | 2.75 | 156.75 |
| 154 | EM | sling | G-TEK | Initial Setup | Field Support | 0 | 0 |
| 154 | EM | sling | G-TEK | Initial Setup | Subtotal | 0 | 418 |
| 154 | EM | sling | G-TEK | Calibration | Supervisor | 3.5 | 332.5 |
| 154 | EM | sling | G-TEK | Calibration | Data Analyst | 3.5 | 199.5 |
| 154 | EM | sling | G-TEK | Calibration | Field Support | 0 | 0 |
| 154 | EM | sling | G-TEK | Calibration | Subtotal | 0 | 532 |
| 154 | EM | sling | G-TEK | Site Survey | Supervisor | 55.25 | 5248.75 |
| 154 | EM | sling | G-TEK | Site Survey | Data Analyst | 55.25 | 3149.25 |
| 154 | EM | sling | G-TEK | Site Survey | Field Support | 0 | 0 |
| 154 | EM | sling | G-TEK | Site Survey | Subtotal | 0 | 8398 |
| 154 | EM | sling | G-TEK | Demobilization | Supervisor | 3.08 | 292.6 |
| 154 | EM | sling | G-TEK | Demobilization | Data Analyst | 3.08 | 175.56 |
| 154 | EM | sling | G-TEK | Demobilization | Field Support | 0 | 0 |
| 154 | EM | sling | G-TEK | Demobilization | Subtotal | 0 | 468.16 |
| 154 | EM | sling | G-TEK | Total | Total | 0 | 9816.16 |
| 452 | EM | hand | G-TEK | Initial Setup | Supervisor | 2.75 | 261.25 |
| 452 | EM | hand | G-TEK | Initial Setup | Data Analyst | 2.75 | 156.75 |
| 452 | EM | hand | G-TEK | Initial Setup | Field Support | 0 | 0 |
| 452 | EM | hand | G-TEK | Initial Setup | Subtotal | 0 | 418 |
| 452 | EM | hand | G-TEK | Calibration | Supervisor | 4.08 | 387.6 |
| 452 | EM | hand | G-TEK | Calibration | Data Analyst | 4.08 | 232.56 |
| 452 | EM | hand | G-TEK | Calibration | Field Support | 0 | 0 |
| 452 | EM | hand | G-TEK | Calibration | Subtotal | 0 | 620.16 |
| 452 | EM | hand | G-TEK | Site Survey | Supervisor | 10.17 | 966.15 |
| 452 | EM | hand | G-TEK | Site Survey | Data Analyst | 10.17 | 579.69 |
| 452 | EM | hand | G-TEK | Site Survey | Field Support | 0 | 0 |
| 452 | EM | hand | G-TEK | Site Survey | Subtotal | 0 | 1545.84 |
| 452 | EM | hand | G-TEK | Demobilization | Supervisor | 3.08 | 292.6 |
| 452 | EM | hand | G-TEK | Demobilization | Data Analyst | 3.08 | 175.56 |
| 452 | EM | hand | G-TEK | Demobilization | Field Support | 0 | 0 |
| 452 | EM | hand | G-TEK | Demobilization | Subtotal | 0 | 468.16 |
| 452 | EM | hand | G-TEK | Total | Total | 0 | 3052.16 |
| 268 | MAG | sling | G-TEK | Initial Setup | Supervisor | 5.16 | 490.2 |
| 268 | MAG | sling | G-TEK | Initial Setup | Data Analyst | 5.16 | 294.12 |
| 268 | MAG | sling | G-TEK | Initial Setup | Field Support | 5.16 | 147.06 |
| 268 | MAG | sling | G-TEK | Initial Setup | Subtotal | 0 | 931.38 |
| 268 | MAG | sling | G-TEK | Calibration | Supervisor | 0.97 | 92.15 |
| 268 | MAG | sling | G-TEK | Calibration | Data Analyst | 0.97 | 55.29 |
| 268 | MAG | sling | G-TEK | Calibration | Field Support | 0.97 | 27.65 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 268 | MAG | sling | G-TEK | Calibration | Subtotal | 0 | 175.09 |
| 268 | MAG | sling | G-TEK | Site Survey | Supervisor | 1.97 | 187.15 |
| 268 | MAG | sling | G-TEK | Site Survey | Data Analyst | 1.97 | 112.29 |
| 268 | MAG | sling | G-TEK | Site Survey | Field Support | 1.97 | 56.15 |
| 268 | MAG | sling | G-TEK | Site Survey | Subtotal | 0 | 355.59 |
| 268 | MAG | sling | G-TEK | Demobilization | Supervisor | 1.58 | 150.1 |
| 268 | MAG | sling | G-TEK | Demobilization | Data Analyst | 1.58 | 90.06 |
| 268 | MAG | sling | G-TEK | Demobilization | Field Support | 1.58 | 45.03 |
| 268 | MAG | sling | G-TEK | Demobilization | Subtotal | 0 | 285.19 |
| 268 | MAG | sling | G-TEK | Total | Total | 0 | 1747.24 |
| 547 | MAG | sling | G-TEK | Initial Setup | Supervisor | 5.16 | 490.2 |
| 547 | MAG | sling | G-TEK | Initial Setup | Data Analyst | 5.16 | 294.12 |
| 547 | MAG | sling | G-TEK | Initial Setup | Field Support | 5.16 | 147.06 |
| 547 | MAG | sling | G-TEK | Initial Setup | Subtotal | 0 | 931.38 |
| 547 | MAG | sling | G-TEK | Calibration | Supervisor | 1.17 | 111.15 |
| 547 | MAG | sling | G-TEK | Calibration | Data Analyst | 1.17 | 66.69 |
| 547 | MAG | sling | G-TEK | Calibration | Field Support | 1.17 | 33.35 |
| 547 | MAG | sling | G-TEK | Calibration | Subtotal | 0 | 211.19 |
| 547 | MAG | sling | G-TEK | Site Survey | Supervisor | 9.75 | 926.25 |
| 547 | MAG | sling | G-TEK | Site Survey | Data Analyst | 9.75 | 555.75 |
| 547 | MAG | sling | G-TEK | Site Survey | Field Support | 9.75 | 277.88 |
| 547 | MAG | sling | G-TEK | Site Survey | Subtotal | 0 | 1759.88 |
| 547 | MAG | sling | G-TEK | Demobilization | Supervisor | 1.58 | 150.1 |
| 547 | MAG | sling | G-TEK | Demobilization | Data Analyst | 1.58 | 90.06 |
| 547 | MAG | sling | G-TEK | Demobilization | Field Support | 1.58 | 45.03 |
| 547 | MAG | sling | G-TEK | Demobilization | Subtotal | 0 | 285.19 |
| 547 | MAG | sling | G-TEK | Total | Total | 0 | 3187.64 |
| 311 | MAG | sling | G-TEK | Initial Setup | Supervisor | 5.16 | 490.2 |
| 311 | MAG | sling | G-TEK | Initial Setup | Data Analyst | 5.16 | 294.12 |
| 311 | MAG | sling | G-TEK | Initial Setup | Field Support | 5.16 | 147.06 |
| 311 | MAG | sling | G-TEK | Initial Setup | Subtotal | 0 | 931.38 |
| 311 | MAG | sling | G-TEK | Calibration | Supervisor | 4 | 380 |
| 311 | MAG | sling | G-TEK | Calibration | Data Analyst | 4 | 228 |
| 311 | MAG | sling | G-TEK | Calibration | Field Support | 4 | 114 |
| 311 | MAG | sling | G-TEK | Calibration | Subtotal | 0 | 722 |
| 311 | MAG | sling | G-TEK | Site Survey | Supervisor | 57.25 | 5438.75 |
| 311 | MAG | sling | G-TEK | Site Survey | Data Analyst | 57.25 | 3263.25 |
| 311 | MAG | sling | G-TEK | Site Survey | Field Support | 57.25 | 1631.63 |
| 311 | MAG | sling | G-TEK | Site Survey | Subtotal | 0 | 10333.63 |
| 311 | MAG | sling | G-TEK | Demobilization | Supervisor | 1.58 | 150.1 |
| 311 | MAG | sling | G-TEK | Demobilization | Data Analyst | 1.58 | 90.06 |
| 311 | MAG | sling | G-TEK | Demobilization | Field Support | 1.58 | 45.03 |
| 311 | MAG | sling | G-TEK | Demobilization | Subtotal | 0 | 285.19 |
| 311 | MAG | sling | G-TEK | Total | Total | 0 | 12272.2 |
| 454 | MAG | sling | G-TEK | Initial Setup | Supervisor | 5.16 | 490.2 |
| 454 | MAG | sling | G-TEK | Initial Setup | Data Analyst | 5.16 | 294.12 |
| 454 | MAG | sling | G-TEK | Initial Setup | Field Support | 5.16 | 147.06 |
| 454 | MAG | sling | G-TEK | Initial Setup | Subtotal | 0 | 931.38 |
| 454 | MAG | sling | G-TEK | Calibration | Supervisor | 1.33 | 126.35 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 454 | MAG | sling | G-TEK | Calibration | Data Analyst | 1.33 | 75.81 |
| 454 | MAG | sling | G-TEK | Calibration | Field Support | 1.33 | 37.91 |
| 454 | MAG | sling | G-TEK | Calibration | Subtotal | 0 | 240.07 |
| 454 | MAG | sling | G-TEK | Site Survey | Supervisor | 9.5 | 902.5 |
| 454 | MAG | sling | G-TEK | Site Survey | Data Analyst | 9.5 | 541.5 |
| 454 | MAG | sling | G-TEK | Site Survey | Field Support | 9.5 | 270.75 |
| 454 | MAG | sling | G-TEK | Site Survey | Subtotal | 0 | 1714.75 |
| 454 | MAG | sling | G-TEK | Demobilization | Supervisor | 1.58 | 150.1 |
| 454 | MAG | sling | G-TEK | Demobilization | Data Analyst | 1.58 | 90.06 |
| 454 | MAG | sling | G-TEK | Demobilization | Field Support | 1.58 | 45.03 |
| 454 | MAG | sling | G-TEK | Demobilization | Subtotal | 0 | 285.19 |
| 454 | MAG | sling | G-TEK | Total | Total | 0 | 3171.39 |
| 281 | dual | sling | G-TEK | Initial Setup | Supervisor | 5 | 475 |
| 281 | dual | sling | G-TEK | Initial Setup | Data Analyst | 5 | 285 |
| 281 | dual | sling | G-TEK | Initial Setup | Field Support | 5 | 285 |
| 281 | dual | sling | G-TEK | Initial Setup | Subtotal | 0 | 1045 |
| 281 | dual | sling | G-TEK | Calibration | Supervisor | 2.66 | 252.7 |
| 281 | dual | sling | G-TEK | Calibration | Data Analyst | 2.66 | 151.62 |
| 281 | dual | sling | G-TEK | Calibration | Field Support | 2.66 | 151.62 |
| 281 | dual | sling | G-TEK | Calibration | Subtotal | 0 | 555.94 |
| 281 | dual | sling | G-TEK | Site Survey | Supervisor | 3.92 | 372.4 |
| 281 | dual | sling | G-TEK | Site Survey | Data Analyst | 3.92 | 223.44 |
| 281 | dual | sling | G-TEK | Site Survey | Field Support | 3.92 | 223.44 |
| 281 | dual | sling | G-TEK | Site Survey | Subtotal | 0 | 819.28 |
| 281 | dual | sling | G-TEK | Demobilization | Supervisor | 3.5 | 332.5 |
| 281 | dual | sling | G-TEK | Demobilization | Data Analyst | 3.5 | 199.5 |
| 281 | dual | sling | G-TEK | Demobilization | Field Support | 3.5 | 199.5 |
| 281 | dual | sling | G-TEK | Demobilization | Subtotal | 0 | 731.5 |
| 281 | dual | sling | G-TEK | Total | Total | 0 | 3151.72 |
| 380 | dual | sling | G-TEK | Initial Setup | Supervisor | 5 | 475 |
| 380 | dual | sling | G-TEK | Initial Setup | Data Analyst | 5 | 285 |
| 380 | dual | sling | G-TEK | Initial Setup | Field Support | 5 | 427.5 |
| 380 | dual | sling | G-TEK | Initial Setup | Subtotal | 0 | 1187.5 |
| 380 | dual | sling | G-TEK | Calibration | Supervisor | 2.66 | 252.7 |
| 380 | dual | sling | G-TEK | Calibration | Data Analyst | 2.66 | 151.62 |
| 380 | dual | sling | G-TEK | Calibration | Field Support | 2.66 | 227.43 |
| 380 | dual | sling | G-TEK | Calibration | Subtotal | 0 | 631.75 |
| 380 | dual | sling | G-TEK | Site Survey | Supervisor | 5.75 | 546.25 |
| 380 | dual | sling | G-TEK | Site Survey | Data Analyst | 5.75 | 327.75 |
| 380 | dual | sling | G-TEK | Site Survey | Field Support | 5.75 | 327.75 |
| 380 | dual | sling | G-TEK | Site Survey | Subtotal | 0 | 1201.75 |
| 380 | dual | sling | G-TEK | Demobilization | Supervisor | 3.5 | 332.5 |
| 380 | dual | sling | G-TEK | Demobilization | Data Analyst | 3.5 | 199.5 |
| 380 | dual | sling | G-TEK | Demobilization | Field Support | 3.5 | 199.5 |
| 380 | dual | sling | G-TEK | Demobilization | Subtotal | 0 | 731.5 |
| 380 | dual | sling | G-TEK | Total | Total | 0 | 3752.5 |
| 379 | dual | sling | G-TEK | Initial Setup | Supervisor | 5 | 475 |
| 379 | dual | sling | G-TEK | Initial Setup | Data Analyst | 5 | 285 |
| 379 | dual | sling | G-TEK | Initial Setup | Field Support | 5 | 285 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 379 | dual | sling | G-TEK | Initial Setup | Subtotal | 0 | 1045 |
| 379 | dual | sling | G-TEK | Calibration | Supervisor | 2.66 | 252.7 |
| 379 | dual | sling | G-TEK | Calibration | Data Analyst | 2.66 | 151.62 |
| 379 | dual | sling | G-TEK | Calibration | Field Support | 2.66 | 151.62 |
| 379 | dual | sling | G-TEK | Calibration | Subtotal | 0 | 555.94 |
| 379 | dual | sling | G-TEK | Site Survey | Supervisor | 40.83 | 3878.85 |
| 379 | dual | sling | G-TEK | Site Survey | Data Analyst | 40.83 | 2327.31 |
| 379 | dual | sling | G-TEK | Site Survey | Field Support | 40.83 | 2327.31 |
| 379 | dual | sling | G-TEK | Site Survey | Subtotal | 0 | 8533.47 |
| 379 | dual | sling | G-TEK | Demobilization | Supervisor | 3.5 | 332.5 |
| 379 | dual | sling | G-TEK | Demobilization | Data Analyst | 3.5 | 199.5 |
| 379 | dual | sling | G-TEK | Demobilization | Field Support | 3.5 | 199.5 |
| 379 | dual | sling | G-TEK | Demobilization | Subtotal | 0 | 731.5 |
| 379 | dual | sling | G-TEK | Total | Total | 0 | 10865.91 |
| 381 | dual | sling | G-TEK | Initial Setup | Supervisor | 5 | 475 |
| 381 | dual | sling | G-TEK | Initial Setup | Data Analyst | 5 | 285 |
| 381 | dual | sling | G-TEK | Initial Setup | Field Support | 5 | 427.5 |
| 381 | dual | sling | G-TEK | Initial Setup | Subtotal | 0 | 1187.5 |
| 381 | dual | sling | G-TEK | Calibration | Supervisor | 2.66 | 252.7 |
| 381 | dual | sling | G-TEK | Calibration | Data Analyst | 2.66 | 151.62 |
| 381 | dual | sling | G-TEK | Calibration | Field Support | 2.66 | 227.43 |
| 381 | dual | sling | G-TEK | Calibration | Subtotal | 0 | 631.75 |
| 381 | dual | sling | G-TEK | Site Survey | Supervisor | 23.92 | 2272.4 |
| 381 | dual | sling | G-TEK | Site Survey | Data Analyst | 23.92 | 1363.44 |
| 381 | dual | sling | G-TEK | Site Survey | Field Support | 23.92 | 1363.44 |
| 381 | dual | sling | G-TEK | Site Survey | Subtotal | 0 | 4999.28 |
| 381 | dual | sling | G-TEK | Demobilization | Supervisor | 3.5 | 332.5 |
| 381 | dual | sling | G-TEK | Demobilization | Data Analyst | 3.5 | 199.5 |
| 381 | dual | sling | G-TEK | Demobilization | Field Support | 3.5 | 199.5 |
| 381 | dual | sling | G-TEK | Demobilization | Subtotal | 0 | 731.5 |
| 381 | dual | sling | G-TEK | Total | Total | 0 | 7550.03 |
| 237 | MAG | hand | HFA | Initial Setup | Supervisor | 0.25 | 23.75 |
| 237 | MAG | hand | HFA | Initial Setup | Data Analyst | 0.25 | 0 |
| 237 | MAG | hand | HFA | Initial Setup | Field Support | 0.25 | 7.13 |
| 237 | MAG | hand | HFA | Initial Setup | Subtotal | 0 | 30.88 |
| 237 | MAG | hand | HFA | Calibration | Supervisor | 3.33 | 316.35 |
| 237 | MAG | hand | HFA | Calibration | Data Analyst | 3.33 | 0 |
| 237 | MAG | hand | HFA | Calibration | Field Support | 3.33 | 94.91 |
| 237 | MAG | hand | HFA | Calibration | Subtotal | 0 | 411.26 |
| 237 | MAG | hand | HFA | Site Survey | Supervisor | 2.33 | 221.35 |
| 237 | MAG | hand | HFA | Site Survey | Data Analyst | 2.33 | 0 |
| 237 | MAG | hand | HFA | Site Survey | Field Support | 2.33 | 66.41 |
| 237 | MAG | hand | HFA | Site Survey | Subtotal | 0 | 287.76 |
| 237 | MAG | hand | HFA | Demobilization | Supervisor | 0.17 | 16.15 |
| 237 | MAG | hand | HFA | Demobilization | Data Analyst | 0.17 | 0 |
| 237 | MAG | hand | HFA | Demobilization | Field Support | 0.17 | 4.85 |
| 237 | MAG | hand | HFA | Demobilization | Subtotal | 0 | 21 |
| 237 | MAG | hand | HFA | Total | Total | 0 | 750.9 |
| 676 | MAG | hand | HFA | Initial Setup | Supervisor | 0.25 | 23.75 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 676 | MAG | hand | HFA | Initial Setup | Data Analyst | 0.25 | 0 |
| 676 | MAG | hand | HFA | Initial Setup | Field Support | 0.25 | 7.13 |
| 676 | MAG | hand | HFA | Initial Setup | Subtotal | 0 | 30.88 |
| 676 | MAG | hand | HFA | Calibration | Supervisor | 3.33 | 316.35 |
| 676 | MAG | hand | HFA | Calibration | Data Analyst | 3.33 | 0 |
| 676 | MAG | hand | HFA | Calibration | Field Support | 3.33 | 94.91 |
| 676 | MAG | hand | HFA | Calibration | Subtotal | 0 | 411.26 |
| 676 | MAG | hand | HFA | Site Survey | Supervisor | 10.33 | 981.35 |
| 676 | MAG | hand | HFA | Site Survey | Data Analyst | 10.33 | 0 |
| 676 | MAG | hand | HFA | Site Survey | Field Support | 10.33 | 883.22 |
| 676 | MAG | hand | HFA | Site Survey | Subtotal | 0 | 1864.57 |
| 676 | MAG | hand | HFA | Demobilization | Supervisor | 0.17 | 16.15 |
| 676 | MAG | hand | HFA | Demobilization | Data Analyst | 0.17 | 0 |
| 676 | MAG | hand | HFA | Demobilization | Field Support | 0.17 | 14.54 |
| 676 | MAG | hand | HFA | Demobilization | Subtotal | 0 | 30.69 |
| 676 | MAG | hand | HFA | Total | Total | 0 | 2337.4 |
| 231 | MAG | hand | HFA | Initial Setup | Supervisor | 0.25 | 23.75 |
| 231 | MAG | hand | HFA | Initial Setup | Data Analyst | 0.25 | 0 |
| 231 | MAG | hand | HFA | Initial Setup | Field Support | 0.25 | 7.13 |
| 231 | MAG | hand | HFA | Initial Setup | Subtotal | 0 | 30.88 |
| 231 | MAG | hand | HFA | Calibration | Supervisor | 3.33 | 316.35 |
| 231 | MAG | hand | HFA | Calibration | Data Analyst | 3.33 | 0 |
| 231 | MAG | hand | HFA | Calibration | Field Support | 3.33 | 94.91 |
| 231 | MAG | hand | HFA | Calibration | Subtotal | 0 | 411.26 |
| 231 | MAG | hand | HFA | Site Survey | Supervisor | 90.25 | 8573.75 |
| 231 | MAG | hand | HFA | Site Survey | Data Analyst | 90.25 | 0 |
| 231 | MAG | hand | HFA | Site Survey | Field Support | 90.25 | 2572.13 |
| 231 | MAG | hand | HFA | Site Survey | Subtotal | 0 | 11145.88 |
| 231 | MAG | hand | HFA | Demobilization | Supervisor | 13.5 | 1282.5 |
| 231 | MAG | hand | HFA | Demobilization | Data Analyst | 13.5 | 0 |
| 231 | MAG | hand | HFA | Demobilization | Field Support | 13.5 | 1154.25 |
| 231 | MAG | hand | HFA | Demobilization | Subtotal | 0 | 2436.75 |
| 231 | MAG | hand | HFA | Total | Total | 0 | 14024.77 |
| 486 | MAG | hand | HFA | Initial Setup | Supervisor | 0.25 | 23.75 |
| 486 | MAG | hand | HFA | Initial Setup | Data Analyst | 0.25 | 0 |
| 486 | MAG | hand | HFA | Initial Setup | Field Support | 0.25 | 7.13 |
| 486 | MAG | hand | HFA | Initial Setup | Subtotal | 0 | 30.88 |
| 486 | MAG | hand | HFA | Calibration | Supervisor | 3.33 | 316.35 |
| 486 | MAG | hand | HFA | Calibration | Data Analyst | 3.33 | 0 |
| 486 | MAG | hand | HFA | Calibration | Field Support | 3.33 | 94.91 |
| 486 | MAG | hand | HFA | Calibration | Subtotal | 0 | 411.26 |
| 486 | MAG | hand | HFA | Site Survey | Supervisor | 13.92 | 1322.4 |
| 486 | MAG | hand | HFA | Site Survey | Data Analyst | 13.92 | 0 |
| 486 | MAG | hand | HFA | Site Survey | Field Support | 13.92 | 396.72 |
| 486 | MAG | hand | HFA | Site Survey | Subtotal | 0 | 1719.12 |
| 486 | MAG | hand | HFA | Demobilization | Supervisor | 0.17 | 16.15 |
| 486 | MAG | hand | HFA | Demobilization | Data Analyst | 0.17 | 0 |
| 486 | MAG | hand | HFA | Demobilization | Field Support | 0.17 | 14.54 |
| 486 | MAG | hand | HFA | Demobilization | Subtotal | 0 | 30.69 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 486 | MAG | hand | HFA | Total | Total | 0 | 2191.95 |
| 647 | EM | towed | NAEVA | Initial Setup | Supervisor | 1.83 | 173.85 |
| 647 | EM | towed | NAEVA | Initial Setup | Data Analyst | 1.83 | 104.31 |
| 647 | EM | towed | NAEVA | Initial Setup | Field Support | 1.83 | 104.31 |
| 647 | EM | towed | NAEVA | Initial Setup | Subtotal | 0 | 382.47 |
| 647 | EM | towed | NAEVA | Calibration | Supervisor | 4 | 380 |
| 647 | EM | towed | NAEVA | Calibration | Data Analyst | 4 | 228 |
| 647 | EM | towed | NAEVA | Calibration | Field Support | 4 | 228 |
| 647 | EM | towed | NAEVA | Calibration | Subtotal | 0 | 836 |
| 647 | EM | towed | NAEVA | Site Survey | Supervisor | 1.83 | 173.85 |
| 647 | EM | towed | NAEVA | Site Survey | Data Analyst | 1.83 | 104.31 |
| 647 | EM | towed | NAEVA | Site Survey | Field Support | 1.83 | 104.31 |
| 647 | EM | towed | NAEVA | Site Survey | Subtotal | 0 | 382.47 |
| 647 | EM | towed | NAEVA | Demobilization | Supervisor | 1.58 | 150.1 |
| 647 | EM | towed | NAEVA | Demobilization | Data Analyst | 1.58 | 90.06 |
| 647 | EM | towed | NAEVA | Demobilization | Field Support | 1.58 | 0 |
| 647 | EM | towed | NAEVA | Demobilization | Subtotal | 0 | 240.16 |
| 647 | EM | towed | NAEVA | Total | Total | 0 | 1841.1 |
| 396 | EM | 2-man | NAEVA | Initial Setup | Supervisor | 0.75 | 71.25 |
| 396 | EM | 2-man | NAEVA | Initial Setup | Data Analyst | 0.75 | 42.75 |
| 396 | EM | 2-man | NAEVA | Initial Setup | Field Support | 0.75 | 42.75 |
| 396 | EM | 2-man | NAEVA | Initial Setup | Subtotal | 0 | 156.75 |
| 396 | EM | 2-man | NAEVA | Calibration | Supervisor | 3.25 | 308.75 |
| 396 | EM | 2-man | NAEVA | Calibration | Data Analyst | 3.25 | 185.25 |
| 396 | EM | 2-man | NAEVA | Calibration | Field Support | 3.25 | 0 |
| 396 | EM | 2-man | NAEVA | Calibration | Subtotal | 0 | 494 |
| 396 | EM | 2-man | NAEVA | Site Survey | Supervisor | 2.75 | 261.25 |
| 396 | EM | 2-man | NAEVA | Site Survey | Data Analyst | 2.75 | 156.75 |
| 396 | EM | 2-man | NAEVA | Site Survey | Field Support | 2.75 | 0 |
| 396 | EM | 2-man | NAEVA | Site Survey | Subtotal | 0 | 418 |
| 396 | EM | 2-man | NAEVA | Demobilization | Supervisor | 1.58 | 150.1 |
| 396 | EM | 2-man | NAEVA | Demobilization | Data Analyst | 1.58 | 90.06 |
| 396 | EM | 2-man | NAEVA | Demobilization | Field Support | 1.58 | 0 |
| 396 | EM | 2-man | NAEVA | Demobilization | Subtotal | 0 | 240.16 |
| 396 | EM | 2-man | NAEVA | Total | Total | 0 | 1308.91 |
| 397 | EM | towed | NAEVA | Initial Setup | Supervisor | 1.83 | 173.85 |
| 397 | EM | towed | NAEVA | Initial Setup | Data Analyst | 1.83 | 104.31 |
| 397 | EM | towed | NAEVA | Initial Setup | Field Support | 1.83 | 104.31 |
| 397 | EM | towed | NAEVA | Initial Setup | Subtotal | 0 | 382.47 |
| 397 | EM | towed | NAEVA | Calibration | Supervisor | 4.5 | 427.5 |
| 397 | EM | towed | NAEVA | Calibration | Data Analyst | 4.5 | 256.5 |
| 397 | EM | towed | NAEVA | Calibration | Field Support | 4.5 | 256.5 |
| 397 | EM | towed | NAEVA | Calibration | Subtotal | 0 | 940.5 |
| 397 | EM | towed | NAEVA | Site Survey | Supervisor | 5.25 | 498.75 |
| 397 | EM | towed | NAEVA | Site Survey | Data Analyst | 5.25 | 299.25 |
| 397 | EM | towed | NAEVA | Site Survey | Field Support | 5.25 | 299.25 |
| 397 | EM | towed | NAEVA | Site Survey | Subtotal | 0 | 1097.25 |
| 397 | EM | towed | NAEVA | Demobilization | Supervisor | 1.58 | 150.1 |
| 397 | EM | towed | NAEVA | Demobilization | Data Analyst | 1.58 | 90.06 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 397 | EM | towed | NAEVA | Demobilization | Field Support | 1.58 | 0 |
| 397 | EM | towed | NAEVA | Demobilization | Subtotal | 0 | 240.16 |
| 397 | EM | towed | NAEVA | Total | Total | 0 | 2660.38 |
| 597 | EM | 2-man | NAEVA | Initial Setup | Supervisor | 0.75 | 71.25 |
| 597 | EM | 2-man | NAEVA | Initial Setup | Data Analyst | 0.75 | 42.75 |
| 597 | EM | 2-man | NAEVA | Initial Setup | Field Support | 0.75 | 42.75 |
| 597 | EM | 2-man | NAEVA | Initial Setup | Subtotal | 0 | 156.75 |
| 597 | EM | 2-man | NAEVA | Calibration | Supervisor | 4.08 | 387.6 |
| 597 | EM | 2-man | NAEVA | Calibration | Data Analyst | 4.08 | 232.56 |
| 597 | EM | 2-man | NAEVA | Calibration | Field Support | 4.08 | 0 |
| 597 | EM | 2-man | NAEVA | Calibration | Subtotal | 0 | 620.16 |
| 597 | EM | 2-man | NAEVA | Site Survey | Supervisor | 13.5 | 1282.5 |
| 597 | EM | 2-man | NAEVA | Site Survey | Data Analyst | 13.5 | 769.5 |
| 597 | EM | 2-man | NAEVA | Site Survey | Field Support | 13.5 | 769.5 |
| 597 | EM | 2-man | NAEVA | Site Survey | Subtotal | 0 | 2821.5 |
| 597 | EM | 2-man | NAEVA | Demobilization | Supervisor | 1.58 | 150.1 |
| 597 | EM | 2-man | NAEVA | Demobilization | Data Analyst | 1.58 | 90.06 |
| 597 | EM | 2-man | NAEVA | Demobilization | Field Support | 1.58 | 0 |
| 597 | EM | 2-man | NAEVA | Demobilization | Subtotal | 0 | 240.16 |
| 597 | EM | 2-man | NAEVA | Total | Total | 0 | 3838.57 |
| 406 | EM | towed | NAEVA | Initial Setup | Supervisor | 1.83 | 173.85 |
| 406 | EM | towed | NAEVA | Initial Setup | Data Analyst | 1.83 | 104.31 |
| 406 | EM | towed | NAEVA | Initial Setup | Field Support | 1.83 | 104.31 |
| 406 | EM | towed | NAEVA | Initial Setup | Subtotal | 0 | 382.47 |
| 406 | EM | towed | NAEVA | Calibration | Supervisor | 7.25 | 688.75 |
| 406 | EM | towed | NAEVA | Calibration | Data Analyst | 7.25 | 413.25 |
| 406 | EM | towed | NAEVA | Calibration | Field Support | 7.25 | 413.25 |
| 406 | EM | towed | NAEVA | Calibration | Subtotal | 0 | 1515.25 |
| 406 | EM | towed | NAEVA | Site Survey | Supervisor | 41.58 | 3950.1 |
| 406 | EM | towed | NAEVA | Site Survey | Data Analyst | 41.58 | 2370.06 |
| 406 | EM | towed | NAEVA | Site Survey | Field Support | 41.58 | 2370.06 |
| 406 | EM | towed | NAEVA | Site Survey | Subtotal | 0 | 8690.22 |
| 406 | EM | towed | NAEVA | Demobilization | Supervisor | 1.58 | 150.1 |
| 406 | EM | towed | NAEVA | Demobilization | Data Analyst | 1.58 | 90.06 |
| 406 | EM | towed | NAEVA | Demobilization | Field Support | 1.58 | 0 |
| 406 | EM | towed | NAEVA | Demobilization | Subtotal | 0 | 240.16 |
| 406 | EM | towed | NAEVA | Total | Total | 0 | 10828.1 |
| 494 | EM | 2-man | NAEVA | Initial Setup | Supervisor | 0.75 | 71.25 |
| 494 | EM | 2-man | NAEVA | Initial Setup | Data Analyst | 0.75 | 42.75 |
| 494 | EM | 2-man | NAEVA | Initial Setup | Field Support | 0.75 | 42.75 |
| 494 | EM | 2-man | NAEVA | Initial Setup | Subtotal | 0 | 156.75 |
| 494 | EM | 2-man | NAEVA | Calibration | Supervisor | 4.08 | 387.6 |
| 494 | EM | 2-man | NAEVA | Calibration | Data Analyst | 4.08 | 232.56 |
| 494 | EM | 2-man | NAEVA | Calibration | Field Support | 4.08 | 0 |
| 494 | EM | 2-man | NAEVA | Calibration | Subtotal | 0 | 620.16 |
| 494 | EM | 2-man | NAEVA | Site Survey | Supervisor | 22.17 | 2106.15 |
| 494 | EM | 2-man | NAEVA | Site Survey | Data Analyst | 22.17 | 1263.69 |
| 494 | EM | 2-man | NAEVA | Site Survey | Field Support | 22.17 | 0 |
| 494 | EM | 2-man | NAEVA | Site Survey | Subtotal | 0 | 3369.84 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 494 | EM | 2-man | NAEVA | Demobilization | Supervisor | 1.58 | 150.1 |
| 494 | EM | 2-man | NAEVA | Demobilization | Data Analyst | 1.58 | 90.06 |
| 494 | EM | 2-man | NAEVA | Demobilization | Field Support | 1.58 | 0 |
| 494 | EM | 2-man | NAEVA | Demobilization | Subtotal | 0 | 240.16 |
| 494 | EM | 2-man | NAEVA | Total | Total | 0 | 4386.91 |
| 127 | EM | towed | NRL | Initial Setup | Supervisor | 3.33 | 316.35 |
| 127 | EM | towed | NRL | Initial Setup | Data Analyst | 3.33 | 189.81 |
| 127 | EM | towed | NRL | Initial Setup | Field Support | 6.66 | 379.62 |
| 127 | EM | towed | NRL | Initial Setup | Subtotal | 0 | 885.78 |
| 127 | EM | towed | NRL | Calibration | Supervisor | 1.9 | 180.5 |
| 127 | EM | towed | NRL | Calibration | Data Analyst | 1.9 | 108.3 |
| 127 | EM | towed | NRL | Calibration | Field Support | 3.8 | 216.6 |
| 127 | EM | towed | NRL | Calibration | Subtotal | 0 | 505.4 |
| 127 | EM | towed | NRL | Site Survey | Supervisor | 1.62 | 153.9 |
| 127 | EM | towed | NRL | Site Survey | Data Analyst | 1.62 | 92.34 |
| 127 | EM | towed | NRL | Site Survey | Field Support | 3.24 | 184.68 |
| 127 | EM | towed | NRL | Site Survey | Subtotal | 0 | 430.92 |
| 127 | EM | towed | NRL | Demobilization | Supervisor | 1 | 95 |
| 127 | EM | towed | NRL | Demobilization | Data Analyst | 1 | 57 |
| 127 | EM | towed | NRL | Demobilization | Field Support | 2 | 114 |
| 127 | EM | towed | NRL | Demobilization | Subtotal | 0 | 266 |
| 127 | EM | towed | NRL | Total | Total | 0 | 2088.1 |
| 675 | EM | towed | NRL | Initial Setup | Supervisor | 3.58 | 340.1 |
| 675 | EM | towed | NRL | Initial Setup | Data Analyst | 3.58 | 204.06 |
| 675 | EM | towed | NRL | Initial Setup | Field Support | 3.58 | 204.06 |
| 675 | EM | towed | NRL | Initial Setup | Subtotal | 0 | 748.22 |
| 675 | EM | towed | NRL | Calibration | Supervisor | 7.72 | 733.4 |
| 675 | EM | towed | NRL | Calibration | Data Analyst | 7.72 | 440.04 |
| 675 | EM | towed | NRL | Calibration | Field Support | 7.72 | 440.04 |
| 675 | EM | towed | NRL | Calibration | Subtotal | 0 | 1613.48 |
| 675 | EM | towed | NRL | Site Survey | Supervisor | 22.5 | 2137.5 |
| 675 | EM | towed | NRL | Site Survey | Data Analyst | 22.5 | 1282.5 |
| 675 | EM | towed | NRL | Site Survey | Field Support | 22.5 | 1282.5 |
| 675 | EM | towed | NRL | Site Survey | Subtotal | 0 | 4702.5 |
| 675 | EM | towed | NRL | Demobilization | Supervisor | 1 | 95 |
| 675 | EM | towed | NRL | Demobilization | Data Analyst | 1 | 57 |
| 675 | EM | towed | NRL | Demobilization | Field Support | 1 | 57 |
| 675 | EM | towed | NRL | Demobilization | Subtotal | 0 | 209 |
| 675 | EM | towed | NRL | Total | Total | 0 | 7273.2 |
| 671 | MAG | towed | NRL | Initial Setup | Supervisor | 1.5 | 142.5 |
| 671 | MAG | towed | NRL | Initial Setup | Data Analyst | 1.5 | 85.5 |
| 671 | MAG | towed | NRL | Initial Setup | Field Support | 1.5 | 42.75 |
| 671 | MAG | towed | NRL | Initial Setup | Subtotal | 0 | 270.75 |
| 671 | MAG | towed | NRL | Calibration | Supervisor | 1.62 | 153.9 |
| 671 | MAG | towed | NRL | Calibration | Data Analyst | 1.62 | 92.34 |
| 671 | MAG | towed | NRL | Calibration | Field Support | 1.62 | 46.17 |
| 671 | MAG | towed | NRL | Calibration | Subtotal | 0 | 292.41 |
| 671 | MAG | towed | NRL | Site Survey | Supervisor | 2.03 | 192.85 |
| 671 | MAG | towed | NRL | Site Survey | Data Analyst | 2.03 | 115.71 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 671 | MAG | towed | NRL | Site Survey | Field Support | 2.03 | 57.86 |
| 671 | MAG | towed | NRL | Site Survey | Subtotal | 0 | 366.42 |
| 671 | MAG | towed | NRL | Demobilization | Supervisor | 1 | 95 |
| 671 | MAG | towed | NRL | Demobilization | Data Analyst | 1 | 57 |
| 671 | MAG | towed | NRL | Demobilization | Field Support | 1 | 28.5 |
| 671 | MAG | towed | NRL | Demobilization | Subtotal | 0 | 180.5 |
| 671 | MAG | towed | NRL | Total | Total | 0 | 1110.08 |
| 673 | MAG | towed | NRL | Initial Setup | Supervisor | 1.5 | 142.5 |
| 673 | MAG | towed | NRL | Initial Setup | Data Analyst | 1.5 | 85.5 |
| 673 | MAG | towed | NRL | Initial Setup | Field Support | 1.5 | 42.75 |
| 673 | MAG | towed | NRL | Initial Setup | Subtotal | 0 | 270.75 |
| 673 | MAG | towed | NRL | Calibration | Supervisor | 0.75 | 71.25 |
| 673 | MAG | towed | NRL | Calibration | Data Analyst | 0.75 | 42.75 |
| 673 | MAG | towed | NRL | Calibration | Field Support | 0.75 | 21.38 |
| 673 | MAG | towed | NRL | Calibration | Subtotal | 0 | 135.38 |
| 673 | MAG | towed | NRL | Site Survey | Supervisor | 7.23 | 686.85 |
| 673 | MAG | towed | NRL | Site Survey | Data Analyst | 7.23 | 412.11 |
| 673 | MAG | towed | NRL | Site Survey | Field Support | 7.23 | 206.06 |
| 673 | MAG | towed | NRL | Site Survey | Subtotal | 0 | 1305.02 |
| 673 | MAG | towed | NRL | Demobilization | Supervisor | 1 | 95 |
| 673 | MAG | towed | NRL | Demobilization | Data Analyst | 1 | 57 |
| 673 | MAG | towed | NRL | Demobilization | Field Support | 1 | 28.5 |
| 673 | MAG | towed | NRL | Demobilization | Subtotal | 0 | 180.5 |
| 673 | MAG | towed | NRL | Total | Total | 0 | 1891.65 |
| 252 | EM | cart | Parsons | Initial Setup | Supervisor | 1.66 | 157.7 |
| 252 | EM | cart | Parsons | Initial Setup | Data Analyst | 1.66 | 94.62 |
| 252 | EM | cart | Parsons | Initial Setup | Field Support | 1.66 | 47.31 |
| 252 | EM | cart | Parsons | Initial Setup | Subtotal | 0 | 299.63 |
| 252 | EM | cart | Parsons | Calibration | Supervisor | 1.33 | 126.35 |
| 252 | EM | cart | Parsons | Calibration | Data Analyst | 1.33 | 75.81 |
| 252 | EM | cart | Parsons | Calibration | Field Support | 1.33 | 37.91 |
| 252 | EM | cart | Parsons | Calibration | Subtotal | 0 | 240.07 |
| 252 | EM | cart | Parsons | Site Survey | Supervisor | 4 | 380 |
| 252 | EM | cart | Parsons | Site Survey | Data Analyst | 4 | 228 |
| 252 | EM | cart | Parsons | Site Survey | Field Support | 4 | 114 |
| 252 | EM | cart | Parsons | Site Survey | Subtotal | 0 | 722 |
| 252 | EM | cart | Parsons | Demobilization | Supervisor | 0.92 | 87.4 |
| 252 | EM | cart | Parsons | Demobilization | Data Analyst | 0.92 | 52.44 |
| 252 | EM | cart | Parsons | Demobilization | Field Support | 0.92 | 78.66 |
| 252 | EM | cart | Parsons | Demobilization | Subtotal | 0 | 218.5 |
| 252 | EM | cart | Parsons | Total | Total | 0 | 1480.2 |
| 572 | EM | cart | Parsons | Initial Setup | Supervisor | 1.66 | 157.7 |
| 572 | EM | cart | Parsons | Initial Setup | Data Analyst | 1.66 | 94.62 |
| 572 | EM | cart | Parsons | Initial Setup | Field Support | 1.66 | 47.31 |
| 572 | EM | cart | Parsons | Initial Setup | Subtotal | 0 | 299.63 |
| 572 | EM | cart | Parsons | Calibration | Supervisor | 1.58 | 150.1 |
| 572 | EM | cart | Parsons | Calibration | Data Analyst | 1.58 | 90.06 |
| 572 | EM | cart | Parsons | Calibration | Field Support | 1.58 | 45.03 |
| 572 | EM | cart | Parsons | Calibration | Subtotal | 0 | 285.19 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 572 | EM | cart | Parsons | Site Survey | Supervisor | 15 | 1425 |
| 572 | EM | cart | Parsons | Site Survey | Data Analyst | 15 | 855 |
| 572 | EM | cart | Parsons | Site Survey | Field Support | 15 | 427.5 |
| 572 | EM | cart | Parsons | Site Survey | Subtotal | 0 | 2707.5 |
| 572 | EM | cart | Parsons | Demobilization | Supervisor | 0.92 | 87.4 |
| 572 | EM | cart | Parsons | Demobilization | Data Analyst | 0.92 | 52.44 |
| 572 | EM | cart | Parsons | Demobilization | Field Support | 0.92 | 78.66 |
| 572 | EM | cart | Parsons | Demobilization | Subtotal | 0 | 218.5 |
| 572 | EM | cart | Parsons | Total | Total | 0 | 3510.82 |
| 411 | EM | cart | Parsons | Initial Setup | Supervisor | 1.66 | 157.7 |
| 411 | EM | cart | Parsons | Initial Setup | Data Analyst | 1.66 | 94.62 |
| 411 | EM | cart | Parsons | Initial Setup | Field Support | 1.66 | 47.31 |
| 411 | EM | cart | Parsons | Initial Setup | Subtotal | 0 | 299.63 |
| 411 | EM | cart | Parsons | Calibration | Supervisor | 3.16 | 300.2 |
| 411 | EM | cart | Parsons | Calibration | Data Analyst | 3.16 | 180.12 |
| 411 | EM | cart | Parsons | Calibration | Field Support | 3.16 | 270.18 |
| 411 | EM | cart | Parsons | Calibration | Subtotal | 0 | 750.5 |
| 411 | EM | cart | Parsons | Site Survey | Supervisor | 64.08 | 6087.6 |
| 411 | EM | cart | Parsons | Site Survey | Data Analyst | 64.08 | 3652.56 |
| 411 | EM | cart | Parsons | Site Survey | Field Support | 64.08 | 5478.84 |
| 411 | EM | cart | Parsons | Site Survey | Subtotal | 0 | 15219 |
| 411 | EM | cart | Parsons | Demobilization | Supervisor | 0.92 | 87.4 |
| 411 | EM | cart | Parsons | Demobilization | Data Analyst | 0.92 | 52.44 |
| 411 | EM | cart | Parsons | Demobilization | Field Support | 0.92 | 26.22 |
| 411 | EM | cart | Parsons | Demobilization | Subtotal | 0 | 166.06 |
| 411 | EM | cart | Parsons | Total | Total | 0 | 16435.19 |
| 496 | EM | cart | Parsons | Initial Setup | Supervisor | 1.66 | 157.7 |
| 496 | EM | cart | Parsons | Initial Setup | Data Analyst | 1.66 | 94.62 |
| 496 | EM | cart | Parsons | Initial Setup | Field Support | 1.66 | 47.31 |
| 496 | EM | cart | Parsons | Initial Setup | Subtotal | 0 | 299.63 |
| 496 | EM | cart | Parsons | Calibration | Supervisor | 1.92 | 182.4 |
| 496 | EM | cart | Parsons | Calibration | Data Analyst | 1.92 | 109.44 |
| 496 | EM | cart | Parsons | Calibration | Field Support | 1.92 | 164.16 |
| 496 | EM | cart | Parsons | Calibration | Subtotal | 0 | 456 |
| 496 | EM | cart | Parsons | Site Survey | Supervisor | 14.25 | 1353.75 |
| 496 | EM | cart | Parsons | Site Survey | Data Analyst | 14.25 | 812.25 |
| 496 | EM | cart | Parsons | Site Survey | Field Support | 14.25 | 1218.38 |
| 496 | EM | cart | Parsons | Site Survey | Subtotal | 0 | 3384.38 |
| 496 | EM | cart | Parsons | Demobilization | Supervisor | 0.92 | 87.4 |
| 496 | EM | cart | Parsons | Demobilization | Data Analyst | 0.92 | 52.44 |
| 496 | EM | cart | Parsons | Demobilization | Field Support | 0.92 | 78.66 |
| 496 | EM | cart | Parsons | Demobilization | Subtotal | 0 | 218.5 |
| 496 | EM | cart | Parsons | Total | Total | 0 | 4358.51 |
| 257 | MAG | hand | Parsons | Initial Setup | Supervisor | 0.25 | 23.75 |
| 257 | MAG | hand | Parsons | Initial Setup | Data Analyst | 0.25 | 14.25 |
| 257 | MAG | hand | Parsons | Initial Setup | Field Support | 0.25 | 21.38 |
| 257 | MAG | hand | Parsons | Initial Setup | Subtotal | 0 | 59.38 |
| 257 | MAG | hand | Parsons | Calibration | Supervisor | 1.42 | 134.9 |
| 257 | MAG | hand | Parsons | Calibration | Data Analyst | 1.42 | 80.94 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 257 | MAG | hand | Parsons | Calibration | Field Support | 1.42 | 121.41 |
| 257 | MAG | hand | Parsons | Calibration | Subtotal | 0 | 337.25 |
| 257 | MAG | hand | Parsons | Site Survey | Supervisor | 1.5 | 142.5 |
| 257 | MAG | hand | Parsons | Site Survey | Data Analyst | 1.5 | 85.5 |
| 257 | MAG | hand | Parsons | Site Survey | Field Support | 1.5 | 128.25 |
| 257 | MAG | hand | Parsons | Site Survey | Subtotal | 0 | 356.25 |
| 257 | MAG | hand | Parsons | Demobilization | Supervisor | 0.75 | 71.25 |
| 257 | MAG | hand | Parsons | Demobilization | Data Analyst | 0.75 | 42.75 |
| 257 | MAG | hand | Parsons | Demobilization | Field Support | 0.75 | 64.13 |
| 257 | MAG | hand | Parsons | Demobilization | Subtotal | 0 | 178.13 |
| 257 | MAG | hand | Parsons | Total | Total | 0 | 931.01 |
| 573 | MAG | hand | Parsons | Initial Setup | Supervisor | 0.25 | 23.75 |
| 573 | MAG | hand | Parsons | Initial Setup | Data Analyst | 0.25 | 14.25 |
| 573 | MAG | hand | Parsons | Initial Setup | Field Support | 0.25 | 21.38 |
| 573 | MAG | hand | Parsons | Initial Setup | Subtotal | 0 | 59.38 |
| 573 | MAG | hand | Parsons | Calibration | Supervisor | 1.42 | 134.9 |
| 573 | MAG | hand | Parsons | Calibration | Data Analyst | 1.42 | 80.94 |
| 573 | MAG | hand | Parsons | Calibration | Field Support | 1.42 | 121.41 |
| 573 | MAG | hand | Parsons | Calibration | Subtotal | 0 | 337.25 |
| 573 | MAG | hand | Parsons | Site Survey | Supervisor | 6.25 | 593.75 |
| 573 | MAG | hand | Parsons | Site Survey | Data Analyst | 6.25 | 356.25 |
| 573 | MAG | hand | Parsons | Site Survey | Field Support | 6.25 | 890.63 |
| 573 | MAG | hand | Parsons | Site Survey | Subtotal | 0 | 1840.63 |
| 573 | MAG | hand | Parsons | Demobilization | Supervisor | 1.75 | 166.25 |
| 573 | MAG | hand | Parsons | Demobilization | Data Analyst | 1.75 | 99.75 |
| 573 | MAG | hand | Parsons | Demobilization | Field Support | 1.75 | 99.75 |
| 573 | MAG | hand | Parsons | Demobilization | Subtotal | 0 | 365.75 |
| 573 | MAG | hand | Parsons | Total | Total | 0 | 2603.01 |
| 229 | MAG | hand | Parsons | Initial Setup | Supervisor | 0.25 | 23.75 |
| 229 | MAG | hand | Parsons | Initial Setup | Data Analyst | 0.25 | 14.25 |
| 229 | MAG | hand | Parsons | Initial Setup | Field Support | 0.25 | 21.38 |
| 229 | MAG | hand | Parsons | Initial Setup | Subtotal | 0 | 59.38 |
| 229 | MAG | hand | Parsons | Calibration | Supervisor | 1.42 | 134.9 |
| 229 | MAG | hand | Parsons | Calibration | Data Analyst | 1.42 | 80.94 |
| 229 | MAG | hand | Parsons | Calibration | Field Support | 1.42 | 121.41 |
| 229 | MAG | hand | Parsons | Calibration | Subtotal | 0 | 337.25 |
| 229 | MAG | hand | Parsons | Site Survey | Supervisor | 41.25 | 3918.75 |
| 229 | MAG | hand | Parsons | Site Survey | Data Analyst | 41.25 | 2351.25 |
| 229 | MAG | hand | Parsons | Site Survey | Field Support | 41.25 | 5878.13 |
| 229 | MAG | hand | Parsons | Site Survey | Subtotal | 0 | 12148.13 |
| 229 | MAG | hand | Parsons | Demobilization | Supervisor | 1.75 | 166.25 |
| 229 | MAG | hand | Parsons | Demobilization | Data Analyst | 1.75 | 99.75 |
| 229 | MAG | hand | Parsons | Demobilization | Field Support | 1.75 | 99.75 |
| 229 | MAG | hand | Parsons | Demobilization | Subtotal | 0 | 365.75 |
| 229 | MAG | hand | Parsons | Total | Total | 0 | 12910.51 |
| 499 | MAG | hand | Parsons | Initial Setup | Supervisor | 0.25 | 23.75 |
| 499 | MAG | hand | Parsons | Initial Setup | Data Analyst | 0.25 | 14.25 |
| 499 | MAG | hand | Parsons | Initial Setup | Field Support | 0.25 | 21.38 |
| 499 | MAG | hand | Parsons | Initial Setup | Subtotal | 0 | 59.38 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 499 | MAG | hand | Parsons | Calibration | Supervisor | 1.42 | 134.9 |
| 499 | MAG | hand | Parsons | Calibration | Data Analyst | 1.42 | 80.94 |
| 499 | MAG | hand | Parsons | Calibration | Field Support | 1.42 | 121.41 |
| 499 | MAG | hand | Parsons | Calibration | Subtotal | 0 | 337.25 |
| 499 | MAG | hand | Parsons | Site Survey | Supervisor | 9.58 | 910.1 |
| 499 | MAG | hand | Parsons | Site Survey | Data Analyst | 9.58 | 546.06 |
| 499 | MAG | hand | Parsons | Site Survey | Field Support | 9.58 | 1365.15 |
| 499 | MAG | hand | Parsons | Site Survey | Subtotal | 0 | 2821.31 |
| 499 | MAG | hand | Parsons | Demobilization | Supervisor | 1.75 | 166.25 |
| 499 | MAG | hand | Parsons | Demobilization | Data Analyst | 1.75 | 99.75 |
| 499 | MAG | hand | Parsons | Demobilization | Field Support | 1.75 | 99.75 |
| 499 | MAG | hand | Parsons | Demobilization | Subtotal | 0 | 365.75 |
| 499 | MAG | hand | Parsons | Total | Total | 0 | 3583.69 |
| 197 | EM | cart | Shaw | Initial Setup | Supervisor | 2.07 | 196.65 |
| 197 | EM | cart | Shaw | Initial Setup | Data Analyst | 2.07 | 117.99 |
| 197 | EM | cart | Shaw | Initial Setup | Field Support | 2.07 | 59 |
| 197 | EM | cart | Shaw | Initial Setup | Subtotal | 0 | 373.64 |
| 197 | EM | cart | Shaw | Calibration | Supervisor | 1.43 | 135.85 |
| 197 | EM | cart | Shaw | Calibration | Data Analyst | 1.43 | 81.51 |
| 197 | EM | cart | Shaw | Calibration | Field Support | 1.43 | 40.76 |
| 197 | EM | cart | Shaw | Calibration | Subtotal | 0 | 258.12 |
| 197 | EM | cart | Shaw | Site Survey | Supervisor | 2.58 | 245.1 |
| 197 | EM | cart | Shaw | Site Survey | Data Analyst | 2.58 | 147.06 |
| 197 | EM | cart | Shaw | Site Survey | Field Support | 2.58 | 73.53 |
| 197 | EM | cart | Shaw | Site Survey | Subtotal | 0 | 465.69 |
| 197 | EM | cart | Shaw | Demobilization | Supervisor | 2.66 | 252.7 |
| 197 | EM | cart | Shaw | Demobilization | Data Analyst | 2.66 | 151.62 |
| 197 | EM | cart | Shaw | Demobilization | Field Support | 2.66 | 151.62 |
| 197 | EM | cart | Shaw | Demobilization | Subtotal | 0 | 555.94 |
| 197 | EM | cart | Shaw | Total | Total | 0 | 1653.39 |
| 552 | EM | cart | Shaw | Initial Setup | Supervisor | 2.07 | 196.65 |
| 552 | EM | cart | Shaw | Initial Setup | Data Analyst | 2.07 | 117.99 |
| 552 | EM | cart | Shaw | Initial Setup | Field Support | 2.07 | 58.99 |
| 552 | EM | cart | Shaw | Initial Setup | Subtotal | 0 | 373.63 |
| 552 | EM | cart | Shaw | Calibration | Supervisor | 1.52 | 144.4 |
| 552 | EM | cart | Shaw | Calibration | Data Analyst | 1.52 | 86.64 |
| 552 | EM | cart | Shaw | Calibration | Field Support | 1.52 | 43.32 |
| 552 | EM | cart | Shaw | Calibration | Subtotal | 0 | 274.36 |
| 552 | EM | cart | Shaw | Site Survey | Supervisor | 4.92 | 467.4 |
| 552 | EM | cart | Shaw | Site Survey | Data Analyst | 4.92 | 280.44 |
| 552 | EM | cart | Shaw | Site Survey | Field Support | 4.92 | 280.44 |
| 552 | EM | cart | Shaw | Site Survey | Subtotal | 0 | 1028.28 |
| 552 | EM | cart | Shaw | Demobilization | Supervisor | 2.66 | 252.7 |
| 552 | EM | cart | Shaw | Demobilization | Data Analyst | 2.66 | 151.62 |
| 552 | EM | cart | Shaw | Demobilization | Field Support | 2.66 | 151.62 |
| 552 | EM | cart | Shaw | Demobilization | Subtotal | 0 | 555.94 |
| 552 | EM | cart | Shaw | Total | Total | 0 | 2232.21 |
| 201 | EM | cart | Shaw | Initial Setup | Supervisor | 2.07 | 196.65 |
| 201 | EM | cart | Shaw | Initial Setup | Data Analyst | 2.07 | 117.99 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 201 | EM | cart | Shaw | Initial Setup | Field Support | 2.07 | 117.99 |
| 201 | EM | cart | Shaw | Initial Setup | Subtotal | 0 | 432.63 |
| 201 | EM | cart | Shaw | Calibration | Supervisor | 2.01 | 190.95 |
| 201 | EM | cart | Shaw | Calibration | Data Analyst | 2.01 | 114.57 |
| 201 | EM | cart | Shaw | Calibration | Field Support | 2.01 | 114.57 |
| 201 | EM | cart | Shaw | Calibration | Subtotal | 0 | 420.09 |
| 201 | EM | cart | Shaw | Site Survey | Supervisor | 35.5 | 3372.5 |
| 201 | EM | cart | Shaw | Site Survey | Data Analyst | 35.5 | 2023.5 |
| 201 | EM | cart | Shaw | Site Survey | Field Support | 35.5 | 2023.5 |
| 201 | EM | cart | Shaw | Site Survey | Subtotal | 0 | 7419.5 |
| 201 | EM | cart | Shaw | Demobilization | Supervisor | 2.66 | 252.7 |
| 201 | EM | cart | Shaw | Demobilization | Data Analyst | 2.66 | 151.62 |
| 201 | EM | cart | Shaw | Demobilization | Field Support | 2.66 | 151.62 |
| 201 | EM | cart | Shaw | Demobilization | Subtotal | 0 | 555.94 |
| 201 | EM | cart | Shaw | Total | Total | 0 | 8828.16 |
| 461 | EM | cart | Shaw | Initial Setup | Supervisor | 2.07 | 196.65 |
| 461 | EM | cart | Shaw | Initial Setup | Data Analyst | 2.07 | 117.99 |
| 461 | EM | cart | Shaw | Initial Setup | Field Support | 2.07 | 58.99 |
| 461 | EM | cart | Shaw | Initial Setup | Subtotal | 0 | 373.63 |
| 461 | EM | cart | Shaw | Calibration | Supervisor | 1.43 | 135.85 |
| 461 | EM | cart | Shaw | Calibration | Data Analyst | 1.43 | 81.51 |
| 461 | EM | cart | Shaw | Calibration | Field Support | 1.43 | 40.76 |
| 461 | EM | cart | Shaw | Calibration | Subtotal | 0 | 258.12 |
| 461 | EM | cart | Shaw | Site Survey | Supervisor | 6.25 | 593.75 |
| 461 | EM | cart | Shaw | Site Survey | Data Analyst | 6.25 | 356.25 |
| 461 | EM | cart | Shaw | Site Survey | Field Support | 6.25 | 356.25 |
| 461 | EM | cart | Shaw | Site Survey | Subtotal | 0 | 1306.25 |
| 461 | EM | cart | Shaw | Demobilization | Supervisor | 2.66 | 252.7 |
| 461 | EM | cart | Shaw | Demobilization | Data Analyst | 2.66 | 151.62 |
| 461 | EM | cart | Shaw | Demobilization | Field Support | 2.66 | 151.62 |
| 461 | EM | cart | Shaw | Demobilization | Subtotal | 0 | 555.94 |
| 461 | EM | cart | Shaw | Total | Total | 0 | 2493.94 |
| 198 | MAG | cart | Shaw | Initial Setup | Supervisor | 2.07 | 196.65 |
| 198 | MAG | cart | Shaw | Initial Setup | Data Analyst | 2.07 | 117.99 |
| 198 | MAG | cart | Shaw | Initial Setup | Field Support | 2.07 | 59 |
| 198 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 373.64 |
| 198 | MAG | cart | Shaw | Calibration | Supervisor | 2 | 190 |
| 198 | MAG | cart | Shaw | Calibration | Data Analyst | 2 | 114 |
| 198 | MAG | cart | Shaw | Calibration | Field Support | 2 | 57 |
| 198 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 361 |
| 198 | MAG | cart | Shaw | Site Survey | Supervisor | 1.33 | 126.35 |
| 198 | MAG | cart | Shaw | Site Survey | Data Analyst | 1.33 | 75.81 |
| 198 | MAG | cart | Shaw | Site Survey | Field Support | 1.33 | 37.91 |
| 198 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 240.07 |
| 198 | MAG | cart | Shaw | Demobilization | Supervisor | 2.66 | 252.7 |
| 198 | MAG | cart | Shaw | Demobilization | Data Analyst | 2.66 | 151.62 |
| 198 | MAG | cart | Shaw | Demobilization | Field Support | 2.66 | 151.62 |
| 198 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 555.94 |
| 198 | MAG | cart | Shaw | Total | Total | 0 | 1530.65 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 404 | MAG | cart | Shaw | Initial Setup | Supervisor | 1.42 | 134.9 |
| 404 | MAG | cart | Shaw | Initial Setup | Data Analyst | 1.42 | 80.94 |
| 404 | MAG | cart | Shaw | Initial Setup | Field Support | 1.42 | 80.94 |
| 404 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 296.78 |
| 404 | MAG | cart | Shaw | Calibration | Supervisor | 0.08 | 7.6 |
| 404 | MAG | cart | Shaw | Calibration | Data Analyst | 0.08 | 4.56 |
| 404 | MAG | cart | Shaw | Calibration | Field Support | 0.08 | 4.56 |
| 404 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 16.72 |
| 404 | MAG | cart | Shaw | Site Survey | Supervisor | 0.25 | 23.75 |
| 404 | MAG | cart | Shaw | Site Survey | Data Analyst | 0.25 | 14.25 |
| 404 | MAG | cart | Shaw | Site Survey | Field Support | 0.25 | 14.25 |
| 404 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 52.25 |
| 404 | MAG | cart | Shaw | Demobilization | Supervisor | 2.67 | 253.65 |
| 404 | MAG | cart | Shaw | Demobilization | Data Analyst | 2.67 | 152.19 |
| 404 | MAG | cart | Shaw | Demobilization | Field Support | 2.67 | 152.19 |
| 404 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 558.03 |
| 404 | MAG | cart | Shaw | Total | Total | 0 | 923.78 |
| 206 | MAG | cart | Shaw | Demobilization | Supervisor | 2.66 | 252.7 |
| 206 | MAG | cart | Shaw | Demobilization | Data Analyst | 2.66 | 151.62 |
| 206 | MAG | cart | Shaw | Demobilization | Field Support | 2.66 | 151.62 |
| 206 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 555.94 |
| 206 | MAG | cart | Shaw | Total | Total | 0 | 1485.51 |
| 206 | MAG | cart | Shaw | Initial Setup | Supervisor | 2.07 | 196.65 |
| 206 | MAG | cart | Shaw | Initial Setup | Data Analyst | 2.07 | 117.99 |
| 206 | MAG | cart | Shaw | Initial Setup | Field Support | 2.07 | 58.99 |
| 206 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 373.63 |
| 206 | MAG | cart | Shaw | Calibration | Supervisor | 2 | 190 |
| 206 | MAG | cart | Shaw | Calibration | Data Analyst | 2 | 114 |
| 206 | MAG | cart | Shaw | Calibration | Field Support | 2 | 114 |
| 206 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 418 |
| 206 | MAG | cart | Shaw | Site Survey | Supervisor | 0.66 | 62.7 |
| 206 | MAG | cart | Shaw | Site Survey | Data Analyst | 0.66 | 37.62 |
| 206 | MAG | cart | Shaw | Site Survey | Field Support | 0.66 | 37.62 |
| 206 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 137.94 |
| 492 | MAG | cart | Shaw | Initial Setup | Supervisor | 2.07 | 196.65 |
| 492 | MAG | cart | Shaw | Initial Setup | Data Analyst | 2.07 | 117.98 |
| 492 | MAG | cart | Shaw | Initial Setup | Field Support | 2.07 | 58.99 |
| 492 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 373.62 |
| 492 | MAG | cart | Shaw | Calibration | Supervisor | 2.5 | 237.5 |
| 492 | MAG | cart | Shaw | Calibration | Data Analyst | 2.5 | 142.5 |
| 492 | MAG | cart | Shaw | Calibration | Field Support | 2.5 | 142.5 |
| 492 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 522.5 |
| 492 | MAG | cart | Shaw | Site Survey | Supervisor | 14.33 | 1361.35 |
| 492 | MAG | cart | Shaw | Site Survey | Data Analyst | 14.33 | 816.81 |
| 492 | MAG | cart | Shaw | Site Survey | Field Support | 14.33 | 816.81 |
| 492 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 2994.97 |
| 492 | MAG | cart | Shaw | Demobilization | Supervisor | 2.66 | 252.7 |
| 492 | MAG | cart | Shaw | Demobilization | Data Analyst | 2.66 | 151.62 |
| 492 | MAG | cart | Shaw | Demobilization | Field Support | 2.66 | 151.62 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 492 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 555.94 |
| 492 | MAG | cart | Shaw | Total | Total | 0 | 4447.03 |
| 376 | MAG | cart | Shaw | Initial Setup | Supervisor | 2.07 | 196.65 |
| 376 | MAG | cart | Shaw | Initial Setup | Data Analyst | 2.07 | 117.99 |
| 376 | MAG | cart | Shaw | Initial Setup | Field Support | 2.07 | 58.99 |
| 376 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 373.63 |
| 376 | MAG | cart | Shaw | Calibration | Supervisor | 2.08 | 197.6 |
| 376 | MAG | cart | Shaw | Calibration | Data Analyst | 2.08 | 118.56 |
| 376 | MAG | cart | Shaw | Calibration | Field Support | 2.08 | 59.28 |
| 376 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 375.44 |
| 376 | MAG | cart | Shaw | Site Survey | Supervisor | 2.75 | 261.25 |
| 376 | MAG | cart | Shaw | Site Survey | Data Analyst | 2.75 | 156.75 |
| 376 | MAG | cart | Shaw | Site Survey | Field Support | 2.75 | 156.75 |
| 376 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 574.75 |
| 376 | MAG | cart | Shaw | Demobilization | Supervisor | 2.66 | 252.7 |
| 376 | MAG | cart | Shaw | Demobilization | Data Analyst | 2.66 | 151.62 |
| 376 | MAG | cart | Shaw | Demobilization | Field Support | 2.66 | 151.62 |
| 376 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 555.94 |
| 376 | MAG | cart | Shaw | Total | Total | 0 | 1879.76 |
| 157 | EM | cart | TTF | Initial Setup | Supervisor | 4.25 | 403.75 |
| 157 | EM | cart | TTF | Initial Setup | Data Analyst | 4.25 | 242.25 |
| 157 | EM | cart | TTF | Initial Setup | Field Support | 4.25 | 121.13 |
| 157 | EM | cart | TTF | Initial Setup | Subtotal | 0 | 767.13 |
| 157 | EM | cart | TTF | Calibration | Supervisor | 1.72 | 163.4 |
| 157 | EM | cart | TTF | Calibration | Data Analyst | 1.72 | 98.04 |
| 157 | EM | cart | TTF | Calibration | Field Support | 1.72 | 49.02 |
| 157 | EM | cart | TTF | Calibration | Subtotal | 0 | 310.46 |
| 157 | EM | cart | TTF | Site Survey | Supervisor | 1.37 | 130.15 |
| 157 | EM | cart | TTF | Site Survey | Data Analyst | 1.37 | 78.09 |
| 157 | EM | cart | TTF | Site Survey | Field Support | 1.37 | 39.05 |
| 157 | EM | cart | TTF | Site Survey | Subtotal | 0 | 247.29 |
| 157 | EM | cart | TTF | Demobilization | Supervisor | 2.58 | 245.1 |
| 157 | EM | cart | TTF | Demobilization | Data Analyst | 2.58 | 147.06 |
| 157 | EM | cart | TTF | Demobilization | Field Support | 2.58 | 73.53 |
| 157 | EM | cart | TTF | Demobilization | Subtotal | 0 | 465.69 |
| 157 | EM | cart | TTF | Total | Total | 0 | 1790.57 |
| 159 | EM | sling | TTF | Initial Setup | Supervisor | 4.25 | 403.75 |
| 159 | EM | sling | TTF | Initial Setup | Data Analyst | 4.25 | 242.25 |
| 159 | EM | sling | TTF | Initial Setup | Field Support | 4.25 | 121.13 |
| 159 | EM | sling | TTF | Initial Setup | Subtotal | 0 | 767.13 |
| 159 | EM | sling | TTF | Calibration | Supervisor | 7.58 | 720.1 |
| 159 | EM | sling | TTF | Calibration | Data Analyst | 7.58 | 432.06 |
| 159 | EM | sling | TTF | Calibration | Field Support | 0 | 0 |
| 159 | EM | sling | TTF | Calibration | Subtotal | 0 | 1152.16 |
| 159 | EM | sling | TTF | Site Survey | Supervisor | 3.75 | 356.25 |
| 159 | EM | sling | TTF | Site Survey | Data Analyst | 3.75 | 213.75 |
| 159 | EM | sling | TTF | Site Survey | Field Support | 0 | 0 |
| 159 | EM | sling | TTF | Site Survey | Subtotal | 0 | 570 |
| 159 | EM | sling | TTF | Demobilization | Supervisor | 2.58 | 245.1 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 159 | EM | sling | TTF | Demobilization | Data Analyst | 2.58 | 147.06 |
| 159 | EM | sling | TTF | Demobilization | Field Support | 2.58 | 73.53 |
| 159 | EM | sling | TTF | Demobilization | Subtotal | 0 | 465.69 |
| 159 | EM | sling | TTF | Total | Total | 0 | 2954.98 |
| 549 | EM | sling | TTF | Initial Setup | Supervisor | 4.25 | 403.75 |
| 549 | EM | sling | TTF | Initial Setup | Data Analyst | 4.25 | 242.25 |
| 549 | EM | sling | TTF | Initial Setup | Field Support | 4.25 | 121.13 |
| 549 | EM | sling | TTF | Initial Setup | Subtotal | 0 | 767.13 |
| 549 | EM | sling | TTF | Calibration | Supervisor | 1.78 | 169.1 |
| 549 | EM | sling | TTF | Calibration | Data Analyst | 1.78 | 101.46 |
| 549 | EM | sling | TTF | Calibration | Field Support | 1.78 | 50.73 |
| 549 | EM | sling | TTF | Calibration | Subtotal | 0 | 321.29 |
| 549 | EM | sling | TTF | Site Survey | Supervisor | 5.33 | 506.35 |
| 549 | EM | sling | TTF | Site Survey | Data Analyst | 5.33 | 303.81 |
| 549 | EM | sling | TTF | Site Survey | Field Support | 5.33 | 151.91 |
| 549 | EM | sling | TTF | Site Survey | Subtotal | 0 | 962.07 |
| 549 | EM | sling | TTF | Demobilization | Supervisor | 2.58 | 245.1 |
| 549 | EM | sling | TTF | Demobilization | Data Analyst | 2.58 | 147.06 |
| 549 | EM | sling | TTF | Demobilization | Field Support | 2.58 | 73.53 |
| 549 | EM | sling | TTF | Demobilization | Subtotal | 0 | 465.69 |
| 549 | EM | sling | TTF | Total | Total | 0 | 2516.18 |
| 165 | EM | cart | TTF | Initial Setup | Supervisor | 4.25 | 403.75 |
| 165 | EM | cart | TTF | Initial Setup | Data Analyst | 4.25 | 242.25 |
| 165 | EM | cart | TTF | Initial Setup | Field Support | 4.25 | 121.13 |
| 165 | EM | cart | TTF | Initial Setup | Subtotal | 0 | 767.13 |
| 165 | EM | cart | TTF | Calibration | Supervisor | 2.35 | 223.25 |
| 165 | EM | cart | TTF | Calibration | Data Analyst | 2.35 | 133.95 |
| 165 | EM | cart | TTF | Calibration | Field Support | 2.35 | 66.98 |
| 165 | EM | cart | TTF | Calibration | Subtotal | 0 | 424.18 |
| 165 | EM | cart | TTF | Site Survey | Supervisor | 63.78 | 6059.1 |
| 165 | EM | cart | TTF | Site Survey | Data Analyst | 63.78 | 3635.46 |
| 165 | EM | cart | TTF | Site Survey | Field Support | 63.78 | 1817.73 |
| 165 | EM | cart | TTF | Site Survey | Subtotal | 0 | 11512.29 |
| 165 | EM | cart | TTF | Demobilization | Supervisor | 2.58 | 245.1 |
| 165 | EM | cart | TTF | Demobilization | Data Analyst | 2.58 | 147.06 |
| 165 | EM | cart | TTF | Demobilization | Field Support | 2.58 | 73.53 |
| 165 | EM | cart | TTF | Demobilization | Subtotal | 0 | 465.69 |
| 165 | EM | cart | TTF | Total | Total | 0 | 13169.28 |
| 457 | EM | sling | TTF | Initial Setup | Supervisor | 4.25 | 403.75 |
| 457 | EM | sling | TTF | Initial Setup | Data Analyst | 4.25 | 242.25 |
| 457 | EM | sling | TTF | Initial Setup | Field Support | 4.25 | 121.13 |
| 457 | EM | sling | TTF | Initial Setup | Subtotal | 0 | 767.13 |
| 457 | EM | sling | TTF | Calibration | Supervisor | 9.48 | 900.6 |
| 457 | EM | sling | TTF | Calibration | Data Analyst | 9.48 | 540.36 |
| 457 | EM | sling | TTF | Calibration | Field Support | 9.48 | 270.18 |
| 457 | EM | sling | TTF | Calibration | Subtotal | 0 | 1711.14 |
| 457 | EM | sling | TTF | Site Survey | Supervisor | 12.22 | 1160.9 |
| 457 | EM | sling | TTF | Site Survey | Data Analyst | 12.22 | 696.54 |
| 457 | EM | sling | TTF | Site Survey | Field Support | 12.22 | 348.27 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 457 | EM | sling | TTF | Site Survey | Subtotal | 0 | 2205.71 |
| 457 | EM | sling | TTF | Demobilization | Supervisor | 2.58 | 245.1 |
| 457 | EM | sling | TTF | Demobilization | Data Analyst | 2.58 | 147.06 |
| 457 | EM | sling | TTF | Demobilization | Field Support | 2.58 | 73.53 |
| 457 | EM | sling | TTF | Demobilization | Subtotal | 0 | 465.69 |
| 457 | EM | sling | TTF | Total | Total | 0 | 5149.67 |
| 764 | EM | towed | VF WARNER | Initial Setup | Supervisor | 3.75 | 356.25 |
| 764 | EM | towed | VF WARNER | Initial Setup | Data Analyst | 3.75 | 213.75 |
| 764 | EM | towed | VF WARNER | Initial Setup | Field Support | 0 | 0 |
| 764 | EM | towed | VF WARNER | Initial Setup | Subtotal | 0 | 570 |
| 764 | EM | towed | VF WARNER | Calibration | Supervisor | 0.96 | 91.2 |
| 764 | EM | towed | VF WARNER | Calibration | Data Analyst | 0.96 | 54.72 |
| 764 | EM | towed | VF WARNER | Calibration | Field Support | 0 | 0 |
| 764 | EM | towed | VF WARNER | Calibration | Subtotal | 0 | 145.92 |
| 764 | EM | towed | VF WARNER | Site Survey | Supervisor | 0.96 | 91.2 |
| 764 | EM | towed | VF WARNER | Site Survey | Data Analyst | 0.96 | 54.72 |
| 764 | EM | towed | VF WARNER | Site Survey | Field Support | 0 | 0 |
| 764 | EM | towed | VF WARNER | Site Survey | Subtotal | 0 | 145.92 |
| 764 | EM | towed | VF WARNER | Demobilization | Supervisor | 4.25 | 403.75 |
| 764 | EM | towed | VF WARNER | Demobilization | Data Analyst | 4.25 | 242.25 |
| 764 | EM | towed | VF WARNER | Demobilization | Field Support | 0 | 0 |
| 764 | EM | towed | VF WARNER | Demobilization | Subtotal | 0 | 646 |
| 764 | EM | towed | VF WARNER | Total | Total | 0 | 1507.84 |
| 45 | GPR | cart | Witten | Initial Setup | Supervisor | 1.56 | 148.2 |
| 45 | GPR | cart | Witten | Initial Setup | Data Analyst | 1.56 | 88.92 |
| 45 | GPR | cart | Witten | Initial Setup | Field Support | 1.56 | 44.46 |
| 45 | GPR | cart | Witten | Initial Setup | Subtotal | 0 | 281.58 |
| 45 | GPR | cart | Witten | Calibration | Supervisor | 1.96 | 186.2 |
| 45 | GPR | cart | Witten | Calibration | Data Analyst | 1.96 | 111.72 |
| 45 | GPR | cart | Witten | Calibration | Field Support | 1.96 | 55.86 |
| 45 | GPR | cart | Witten | Calibration | Subtotal | 0 | 353.78 |
| 45 | GPR | cart | Witten | Site Survey | Supervisor | 5.43 | 515.85 |
| 45 | GPR | cart | Witten | Site Survey | Data Analyst | 5.43 | 309.51 |
| 45 | GPR | cart | Witten | Site Survey | Field Support | 5.43 | 154.76 |
| 45 | GPR | cart | Witten | Site Survey | Subtotal | 0 | 980.12 |
| 45 | GPR | cart | Witten | Demobilization | Supervisor | 1 | 95 |
| 45 | GPR | cart | Witten | Demobilization | Data Analyst | 1 | 57 |
| 45 | GPR | cart | Witten | Demobilization | Field Support | 1 | 28.5 |
| 45 | GPR | cart | Witten | Demobilization | Subtotal | 0 | 180.5 |
| 45 | GPR | cart | Witten | Total | Total | 0 | 1795.98 |
| 126 | GPR | cart | Witten | Initial Setup | Supervisor | 1.56 | 148.2 |
| 126 | GPR | cart | Witten | Initial Setup | Data Analyst | 1.56 | 88.92 |
| 126 | GPR | cart | Witten | Initial Setup | Field Support | 1.56 | 44.46 |
| 126 | GPR | cart | Witten | Initial Setup | Subtotal | 0 | 281.58 |
| 126 | GPR | cart | Witten | Calibration | Supervisor | 1.96 | 186.2 |
| 126 | GPR | cart | Witten | Calibration | Data Analyst | 1.96 | 111.72 |
| 126 | GPR | cart | Witten | Calibration | Field Support | 1.96 | 55.86 |
| 126 | GPR | cart | Witten | Calibration | Subtotal | 0 | 353.78 |
| 126 | GPR | cart | Witten | Site Survey | Supervisor | 0.72 | 68.4 |

| <i>Aberdeen Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 126 | GPR | cart | Witten | Site Survey | Data Analyst | 0.72 | 41.04 |
| 126 | GPR | cart | Witten | Site Survey | Field Support | 0.72 | 20.52 |
| 126 | GPR | cart | Witten | Site Survey | Subtotal | 0 | 129.96 |
| 126 | GPR | cart | Witten | Demobilization | Supervisor | 1 | 95 |
| 126 | GPR | cart | Witten | Demobilization | Data Analyst | 1 | 57 |
| 126 | GPR | cart | Witten | Demobilization | Field Support | 1 | 28.5 |
| 126 | GPR | cart | Witten | Demobilization | Subtotal | 0 | 180.5 |
| 126 | GPR | cart | Witten | Total | Total | 0 | 945.82 |
| 37 | EM | cart | Zonge | Initial Setup | Supervisor | 4.83 | 458.85 |
| 37 | EM | cart | Zonge | Initial Setup | Data Analyst | 4.83 | 275.31 |
| 37 | EM | cart | Zonge | Initial Setup | Field Support | 4.83 | 137.66 |
| 37 | EM | cart | Zonge | Initial Setup | Subtotal | 0 | 871.82 |
| 37 | EM | cart | Zonge | Calibration | Supervisor | 4.53 | 430.35 |
| 37 | EM | cart | Zonge | Calibration | Data Analyst | 4.53 | 258.21 |
| 37 | EM | cart | Zonge | Calibration | Field Support | 4.53 | 129.1 |
| 37 | EM | cart | Zonge | Calibration | Subtotal | 0 | 817.67 |
| 37 | EM | cart | Zonge | Site Survey | Supervisor | 3.23 | 306.85 |
| 37 | EM | cart | Zonge | Site Survey | Data Analyst | 3.23 | 184.11 |
| 37 | EM | cart | Zonge | Site Survey | Field Support | 3.23 | 92.06 |
| 37 | EM | cart | Zonge | Site Survey | Subtotal | 0 | 583.02 |
| 37 | EM | cart | Zonge | Demobilization | Supervisor | 1.75 | 166.25 |
| 37 | EM | cart | Zonge | Demobilization | Data Analyst | 1.75 | 99.75 |
| 37 | EM | cart | Zonge | Demobilization | Field Support | 0 | 0 |
| 37 | EM | cart | Zonge | Demobilization | Subtotal | 0 | 266 |
| 37 | EM | cart | Zonge | Total | Total | 0 | 2538.51 |
| 38 | EM | cart | Zonge | Initial Setup | Supervisor | 4.83 | 458.85 |
| 38 | EM | cart | Zonge | Initial Setup | Data Analyst | 4.83 | 275.31 |
| 38 | EM | cart | Zonge | Initial Setup | Field Support | 4.83 | 137.66 |
| 38 | EM | cart | Zonge | Initial Setup | Subtotal | 0 | 871.82 |
| 38 | EM | cart | Zonge | Calibration | Supervisor | 5 | 475 |
| 38 | EM | cart | Zonge | Calibration | Data Analyst | 5 | 285 |
| 38 | EM | cart | Zonge | Calibration | Field Support | 5 | 142.5 |
| 38 | EM | cart | Zonge | Calibration | Subtotal | 0 | 902.5 |
| 38 | EM | cart | Zonge | Site Survey | Supervisor | 108.7 | 10326.5 |
| 38 | EM | cart | Zonge | Site Survey | Data Analyst | 108.7 | 6195.9 |
| 38 | EM | cart | Zonge | Site Survey | Field Support | 108.7 | 3872.44 |
| 38 | EM | cart | Zonge | Site Survey | Subtotal | 0 | 20394.84 |
| 38 | EM | cart | Zonge | Demobilization | Supervisor | 1.75 | 166.25 |
| 38 | EM | cart | Zonge | Demobilization | Data Analyst | 1.75 | 99.75 |
| 38 | EM | cart | Zonge | Demobilization | Field Support | 0 | 0 |
| 38 | EM | cart | Zonge | Demobilization | Subtotal | 0 | 266 |
| 38 | EM | cart | Zonge | Total | Total | 0 | 22435.16 |
| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 383 | dual | cart | BH | Initial Setup | Supervisor | 7.83 | 743.85 |
| 383 | dual | cart | BH | Initial Setup | Data Analyst | 7.83 | 446.31 |
| 383 | dual | cart | BH | Initial Setup | Field Support | 7.83 | 0 |
| 383 | dual | cart | BH | Initial Setup | Subtotal | 0 | 1190.16 |
| 383 | dual | cart | BH | Calibration | Supervisor | 4.2 | 399 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 383 | dual | cart | BH | Calibration | Data Analyst | 4.2 | 239.4 |
| 383 | dual | cart | BH | Calibration | Field Support | 4.2 | 0 |
| 383 | dual | cart | BH | Calibration | Subtotal | 0 | 638.4 |
| 383 | dual | cart | BH | Site Survey | Supervisor | 2 | 190 |
| 383 | dual | cart | BH | Site Survey | Data Analyst | 2 | 114 |
| 383 | dual | cart | BH | Site Survey | Field Support | 2 | 0 |
| 383 | dual | cart | BH | Site Survey | Subtotal | 0 | 304 |
| 383 | dual | cart | BH | Demobilization | Supervisor | 1.72 | 163.4 |
| 383 | dual | cart | BH | Demobilization | Data Analyst | 1.72 | 98.04 |
| 383 | dual | cart | BH | Demobilization | Field Support | 1.72 | 0 |
| 383 | dual | cart | BH | Demobilization | Subtotal | 0 | 261.44 |
| 383 | dual | cart | BH | Total | Total | 0 | 2394 |
| 607 | dual | cart | BH | Initial Setup | Supervisor | 7.83 | 743.85 |
| 607 | dual | cart | BH | Initial Setup | Data Analyst | 7.83 | 446.31 |
| 607 | dual | cart | BH | Initial Setup | Field Support | 7.83 | 0 |
| 607 | dual | cart | BH | Initial Setup | Subtotal | 0 | 1190.16 |
| 607 | dual | cart | BH | Calibration | Supervisor | 4.45 | 422.75 |
| 607 | dual | cart | BH | Calibration | Data Analyst | 4.45 | 253.65 |
| 607 | dual | cart | BH | Calibration | Field Support | 4.45 | 0 |
| 607 | dual | cart | BH | Calibration | Subtotal | 0 | 676.4 |
| 607 | dual | cart | BH | Site Survey | Supervisor | 11.28 | 1071.6 |
| 607 | dual | cart | BH | Site Survey | Data Analyst | 11.28 | 642.96 |
| 607 | dual | cart | BH | Site Survey | Field Support | 11.28 | 0 |
| 607 | dual | cart | BH | Site Survey | Subtotal | 0 | 1714.56 |
| 607 | dual | cart | BH | Demobilization | Supervisor | 1.72 | 163.4 |
| 607 | dual | cart | BH | Demobilization | Data Analyst | 1.72 | 98.04 |
| 607 | dual | cart | BH | Demobilization | Field Support | 1.72 | 0 |
| 607 | dual | cart | BH | Demobilization | Subtotal | 0 | 261.44 |
| 607 | dual | cart | BH | Total | Total | 0 | 3842.56 |
| 655 | dual | cart | BH | Initial Setup | Supervisor | 7.83 | 743.85 |
| 655 | dual | cart | BH | Initial Setup | Data Analyst | 7.83 | 446.31 |
| 655 | dual | cart | BH | Initial Setup | Field Support | 7.83 | 0 |
| 655 | dual | cart | BH | Initial Setup | Subtotal | 0 | 1190.16 |
| 655 | dual | cart | BH | Calibration | Supervisor | 5.15 | 489.25 |
| 655 | dual | cart | BH | Calibration | Data Analyst | 5.15 | 293.55 |
| 655 | dual | cart | BH | Calibration | Field Support | 5.15 | 0 |
| 655 | dual | cart | BH | Calibration | Subtotal | 0 | 782.8 |
| 655 | dual | cart | BH | Site Survey | Supervisor | 11.46 | 1088.7 |
| 655 | dual | cart | BH | Site Survey | Data Analyst | 11.46 | 653.22 |
| 655 | dual | cart | BH | Site Survey | Field Support | 11.46 | 0 |
| 655 | dual | cart | BH | Site Survey | Subtotal | 0 | 1741.92 |
| 655 | dual | cart | BH | Demobilization | Supervisor | 1.72 | 163.4 |
| 655 | dual | cart | BH | Demobilization | Data Analyst | 1.72 | 98.04 |
| 655 | dual | cart | BH | Demobilization | Field Support | 1.72 | 0 |
| 655 | dual | cart | BH | Demobilization | Subtotal | 0 | 261.44 |
| 655 | dual | cart | BH | Total | Total | 0 | 3976.32 |
| 651 | dual | towed | BH | Initial Setup | Supervisor | 7.83 | 743.85 |
| 651 | dual | towed | BH | Initial Setup | Data Analyst | 7.83 | 446.31 |
| 651 | dual | towed | BH | Initial Setup | Field Support | 7.83 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 651 | dual | towed | BH | Initial Setup | Subtotal | 0 | 1190.16 |
| 651 | dual | towed | BH | Calibration | Supervisor | 10.92 | 1037.4 |
| 651 | dual | towed | BH | Calibration | Data Analyst | 10.92 | 622.44 |
| 651 | dual | towed | BH | Calibration | Field Support | 10.92 | 0 |
| 651 | dual | towed | BH | Calibration | Subtotal | 0 | 1659.84 |
| 651 | dual | towed | BH | Site Survey | Supervisor | 48.1 | 4569.5 |
| 651 | dual | towed | BH | Site Survey | Data Analyst | 48.1 | 2741.7 |
| 651 | dual | towed | BH | Site Survey | Field Support | 48.1 | 0 |
| 651 | dual | towed | BH | Site Survey | Subtotal | 0 | 7311.2 |
| 651 | dual | towed | BH | Demobilization | Supervisor | 1.72 | 163.4 |
| 651 | dual | towed | BH | Demobilization | Data Analyst | 1.72 | 98.04 |
| 651 | dual | towed | BH | Demobilization | Field Support | 1.72 | 0 |
| 651 | dual | towed | BH | Demobilization | Subtotal | 0 | 261.44 |
| 651 | dual | towed | BH | Total | Total | 0 | 10422.64 |
| 216 | EM | cart | ERDC | Initial Setup | Supervisor | 3.17 | 301.15 |
| 216 | EM | cart | ERDC | Initial Setup | Data Analyst | 3.17 | 180.69 |
| 216 | EM | cart | ERDC | Initial Setup | Field Support | 3.17 | 271.05 |
| 216 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 752.89 |
| 216 | EM | cart | ERDC | Calibration | Supervisor | 9.45 | 897.75 |
| 216 | EM | cart | ERDC | Calibration | Data Analyst | 9.45 | 538.65 |
| 216 | EM | cart | ERDC | Calibration | Field Support | 9.45 | 807.98 |
| 216 | EM | cart | ERDC | Calibration | Subtotal | 0 | 2244.38 |
| 216 | EM | cart | ERDC | Site Survey | Supervisor | 10.5 | 997.5 |
| 216 | EM | cart | ERDC | Site Survey | Data Analyst | 10.5 | 598.5 |
| 216 | EM | cart | ERDC | Site Survey | Field Support | 10.5 | 897.75 |
| 216 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 2493.75 |
| 216 | EM | cart | ERDC | Demobilization | Supervisor | 0.6 | 57 |
| 216 | EM | cart | ERDC | Demobilization | Data Analyst | 0.6 | 34.2 |
| 216 | EM | cart | ERDC | Demobilization | Field Support | 0.6 | 51.3 |
| 216 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 142.5 |
| 216 | EM | cart | ERDC | Total | Total | 0 | 5633.52 |
| 249 | EM | cart | ERDC | Initial Setup | Supervisor | 1.08 | 102.6 |
| 249 | EM | cart | ERDC | Initial Setup | Data Analyst | 1.08 | 61.56 |
| 249 | EM | cart | ERDC | Initial Setup | Field Support | 1.08 | 61.56 |
| 249 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 225.72 |
| 249 | EM | cart | ERDC | Calibration | Supervisor | 17.35 | 1648.25 |
| 249 | EM | cart | ERDC | Calibration | Data Analyst | 17.35 | 988.95 |
| 249 | EM | cart | ERDC | Calibration | Field Support | 17.35 | 988.95 |
| 249 | EM | cart | ERDC | Calibration | Subtotal | 0 | 3626.15 |
| 249 | EM | cart | ERDC | Site Survey | Supervisor | 135.88 | 12908.6 |
| 249 | EM | cart | ERDC | Site Survey | Data Analyst | 135.88 | 7745.16 |
| 249 | EM | cart | ERDC | Site Survey | Field Support | 135.88 | 7745.16 |
| 249 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 28398.92 |
| 249 | EM | cart | ERDC | Demobilization | Supervisor | 2.16 | 205.2 |
| 249 | EM | cart | ERDC | Demobilization | Data Analyst | 2.16 | 122.55 |
| 249 | EM | cart | ERDC | Demobilization | Field Support | 2.16 | 122.55 |
| 249 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 450.3 |
| 249 | EM | cart | ERDC | Total | Total | 0 | 32701.09 |
| 134 | EM | cart | ERDC | Initial Setup | Supervisor | 6.25 | 593.75 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 134 | EM | cart | ERDC | Initial Setup | Data Analyst | 6.25 | 356.25 |
| 134 | EM | cart | ERDC | Initial Setup | Field Support | 6.25 | 534.38 |
| 134 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 1484.38 |
| 134 | EM | cart | ERDC | Calibration | Supervisor | 7.5 | 712.5 |
| 134 | EM | cart | ERDC | Calibration | Data Analyst | 7.5 | 427.5 |
| 134 | EM | cart | ERDC | Calibration | Field Support | 7.5 | 641.25 |
| 134 | EM | cart | ERDC | Calibration | Subtotal | 0 | 1781.25 |
| 134 | EM | cart | ERDC | Site Survey | Supervisor | 3.75 | 356.25 |
| 134 | EM | cart | ERDC | Site Survey | Data Analyst | 3.75 | 213.75 |
| 134 | EM | cart | ERDC | Site Survey | Field Support | 3.75 | 320.63 |
| 134 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 890.63 |
| 134 | EM | cart | ERDC | Demobilization | Supervisor | 0.6 | 57 |
| 134 | EM | cart | ERDC | Demobilization | Data Analyst | 0.6 | 34.2 |
| 134 | EM | cart | ERDC | Demobilization | Field Support | 0.6 | 51.3 |
| 134 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 142.5 |
| 134 | EM | cart | ERDC | Total | Total | 0 | 4298.76 |
| 509 | EM | cart | ERDC | Initial Setup | Supervisor | 6.5 | 617.5 |
| 509 | EM | cart | ERDC | Initial Setup | Data Analyst | 6.5 | 370.5 |
| 509 | EM | cart | ERDC | Initial Setup | Field Support | 6.5 | 555.75 |
| 509 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 1543.75 |
| 509 | EM | cart | ERDC | Calibration | Supervisor | 5.55 | 527.25 |
| 509 | EM | cart | ERDC | Calibration | Data Analyst | 5.55 | 316.35 |
| 509 | EM | cart | ERDC | Calibration | Field Support | 5.55 | 474.53 |
| 509 | EM | cart | ERDC | Calibration | Subtotal | 0 | 1318.13 |
| 509 | EM | cart | ERDC | Site Survey | Supervisor | 10.55 | 1002.25 |
| 509 | EM | cart | ERDC | Site Survey | Data Analyst | 10.55 | 601.35 |
| 509 | EM | cart | ERDC | Site Survey | Field Support | 10.55 | 300.68 |
| 509 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 1904.28 |
| 509 | EM | cart | ERDC | Demobilization | Supervisor | 0.77 | 73.15 |
| 509 | EM | cart | ERDC | Demobilization | Data Analyst | 0.77 | 43.89 |
| 509 | EM | cart | ERDC | Demobilization | Field Support | 0.77 | 21.95 |
| 509 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 138.99 |
| 509 | EM | cart | ERDC | Total | Total | 0 | 4905.15 |
| 136 | EM | cart | ERDC | Initial Setup | Supervisor | 6.5 | 617.5 |
| 136 | EM | cart | ERDC | Initial Setup | Data Analyst | 6.5 | 370.5 |
| 136 | EM | cart | ERDC | Initial Setup | Field Support | 6.5 | 370.5 |
| 136 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 1358.5 |
| 136 | EM | cart | ERDC | Calibration | Supervisor | 5.37 | 510.15 |
| 136 | EM | cart | ERDC | Calibration | Data Analyst | 5.37 | 306.09 |
| 136 | EM | cart | ERDC | Calibration | Field Support | 5.37 | 459.14 |
| 136 | EM | cart | ERDC | Calibration | Subtotal | 0 | 1275.38 |
| 136 | EM | cart | ERDC | Site Survey | Supervisor | 5.55 | 527.25 |
| 136 | EM | cart | ERDC | Site Survey | Data Analyst | 5.55 | 316.35 |
| 136 | EM | cart | ERDC | Site Survey | Field Support | 5.55 | 158.18 |
| 136 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 1001.78 |
| 136 | EM | cart | ERDC | Demobilization | Supervisor | 0.77 | 73.15 |
| 136 | EM | cart | ERDC | Demobilization | Data Analyst | 0.77 | 43.89 |
| 136 | EM | cart | ERDC | Demobilization | Field Support | 0.77 | 21.95 |
| 136 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 138.99 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 136 | EM | cart | ERDC | Total | Total | 0 | 3774.65 |
| 135 | EM | cart | ERDC | Initial Setup | Supervisor | 5.5 | 522.5 |
| 135 | EM | cart | ERDC | Initial Setup | Data Analyst | 5.5 | 313.5 |
| 135 | EM | cart | ERDC | Initial Setup | Field Support | 5.5 | 313.5 |
| 135 | EM | cart | ERDC | Initial Setup | Subtotal | 0 | 1149.5 |
| 135 | EM | cart | ERDC | Calibration | Supervisor | 7.08 | 672.6 |
| 135 | EM | cart | ERDC | Calibration | Data Analyst | 7.08 | 403.56 |
| 135 | EM | cart | ERDC | Calibration | Field Support | 7.08 | 403.56 |
| 135 | EM | cart | ERDC | Calibration | Subtotal | 0 | 1479.72 |
| 135 | EM | cart | ERDC | Site Survey | Supervisor | 92.95 | 8830.25 |
| 135 | EM | cart | ERDC | Site Survey | Data Analyst | 92.95 | 5298.15 |
| 135 | EM | cart | ERDC | Site Survey | Field Support | 92.95 | 5298.15 |
| 135 | EM | cart | ERDC | Site Survey | Subtotal | 0 | 19426.55 |
| 135 | EM | cart | ERDC | Demobilization | Supervisor | 0.76 | 72.2 |
| 135 | EM | cart | ERDC | Demobilization | Data Analyst | 0.76 | 43.32 |
| 135 | EM | cart | ERDC | Demobilization | Field Support | 0.76 | 43.32 |
| 135 | EM | cart | ERDC | Demobilization | Subtotal | 0 | 158.84 |
| 135 | EM | cart | ERDC | Total | Total | 0 | 22214.61 |
| 362 | MAG | sling | ERDC | Initial Setup | Supervisor | 0.42 | 39.9 |
| 362 | MAG | sling | ERDC | Initial Setup | Data Analyst | 0.42 | 23.94 |
| 362 | MAG | sling | ERDC | Initial Setup | Field Support | 0.42 | 11.97 |
| 362 | MAG | sling | ERDC | Initial Setup | Subtotal | 0 | 75.81 |
| 362 | MAG | sling | ERDC | Calibration | Supervisor | 4.25 | 403.75 |
| 362 | MAG | sling | ERDC | Calibration | Data Analyst | 4.25 | 242.25 |
| 362 | MAG | sling | ERDC | Calibration | Field Support | 4.25 | 121.13 |
| 362 | MAG | sling | ERDC | Calibration | Subtotal | 0 | 767.13 |
| 362 | MAG | sling | ERDC | Site Survey | Supervisor | 7.75 | 736.25 |
| 362 | MAG | sling | ERDC | Site Survey | Data Analyst | 7.75 | 441.75 |
| 362 | MAG | sling | ERDC | Site Survey | Field Support | 7.75 | 220.88 |
| 362 | MAG | sling | ERDC | Site Survey | Subtotal | 0 | 1398.88 |
| 362 | MAG | sling | ERDC | Demobilization | Supervisor | 0.25 | 23.75 |
| 362 | MAG | sling | ERDC | Demobilization | Data Analyst | 0.25 | 14.25 |
| 362 | MAG | sling | ERDC | Demobilization | Field Support | 0.25 | 7.13 |
| 362 | MAG | sling | ERDC | Demobilization | Subtotal | 0 | 45.13 |
| 362 | MAG | sling | ERDC | Total | Total | 0 | 2286.95 |
| 544 | MAG | sling | ERDC | Initial Setup | Supervisor | 3.33 | 316.35 |
| 544 | MAG | sling | ERDC | Initial Setup | Data Analyst | 3.33 | 189.81 |
| 544 | MAG | sling | ERDC | Initial Setup | Field Support | 3.33 | 94.91 |
| 544 | MAG | sling | ERDC | Initial Setup | Subtotal | 0 | 601.07 |
| 544 | MAG | sling | ERDC | Calibration | Supervisor | 4.92 | 467.4 |
| 544 | MAG | sling | ERDC | Calibration | Data Analyst | 4.92 | 280.44 |
| 544 | MAG | sling | ERDC | Calibration | Field Support | 4.92 | 140.22 |
| 544 | MAG | sling | ERDC | Calibration | Subtotal | 0 | 888.06 |
| 544 | MAG | sling | ERDC | Site Survey | Supervisor | 4.53 | 430.35 |
| 544 | MAG | sling | ERDC | Site Survey | Data Analyst | 4.53 | 258.21 |
| 544 | MAG | sling | ERDC | Site Survey | Field Support | 4.53 | 129.11 |
| 544 | MAG | sling | ERDC | Site Survey | Subtotal | 0 | 817.67 |
| 544 | MAG | sling | ERDC | Demobilization | Supervisor | 0.25 | 23.75 |
| 544 | MAG | sling | ERDC | Demobilization | Data Analyst | 0.25 | 14.25 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 544 | MAG | sling | ERDC | Demobilization | Field Support | 0.25 | 0 |
| 544 | MAG | sling | ERDC | Demobilization | Subtotal | 0 | 38 |
| 544 | MAG | sling | ERDC | Total | Total | 0 | 2344.8 |
| 571 | MAG | sling | ERDC | Demobilization | Subtotal | 0 | 38 |
| 571 | MAG | sling | ERDC | Total | Total | 0 | 2041.55 |
| 571 | MAG | sling | ERDC | Initial Setup | Supervisor | 3.33 | 316.35 |
| 571 | MAG | sling | ERDC | Initial Setup | Data Analyst | 3.33 | 189.81 |
| 571 | MAG | sling | ERDC | Initial Setup | Field Support | 3.33 | 0 |
| 571 | MAG | sling | ERDC | Initial Setup | Subtotal | 0 | 506.16 |
| 571 | MAG | sling | ERDC | Calibration | Supervisor | 5.22 | 495.9 |
| 571 | MAG | sling | ERDC | Calibration | Data Analyst | 5.22 | 297.54 |
| 571 | MAG | sling | ERDC | Calibration | Field Support | 5.22 | 0 |
| 571 | MAG | sling | ERDC | Calibration | Subtotal | 0 | 793.44 |
| 571 | MAG | sling | ERDC | Site Survey | Supervisor | 3.9 | 370.5 |
| 571 | MAG | sling | ERDC | Site Survey | Data Analyst | 3.9 | 222.3 |
| 571 | MAG | sling | ERDC | Site Survey | Field Support | 3.9 | 111.15 |
| 571 | MAG | sling | ERDC | Site Survey | Subtotal | 0 | 703.95 |
| 571 | MAG | sling | ERDC | Demobilization | Supervisor | 0.25 | 23.75 |
| 571 | MAG | sling | ERDC | Demobilization | Data Analyst | 0.25 | 14.25 |
| 571 | MAG | sling | ERDC | Demobilization | Field Support | 0.25 | 0 |
| 364 | MAG | sling | ERDC | Initial Setup | Supervisor | 3.33 | 316.35 |
| 364 | MAG | sling | ERDC | Initial Setup | Data Analyst | 3.33 | 189.81 |
| 364 | MAG | sling | ERDC | Initial Setup | Field Support | 3.33 | 94.91 |
| 364 | MAG | sling | ERDC | Initial Setup | Subtotal | 0 | 601.07 |
| 364 | MAG | sling | ERDC | Calibration | Supervisor | 3.92 | 372.4 |
| 364 | MAG | sling | ERDC | Calibration | Data Analyst | 3.92 | 223.44 |
| 364 | MAG | sling | ERDC | Calibration | Field Support | 3.92 | 111.72 |
| 364 | MAG | sling | ERDC | Calibration | Subtotal | 0 | 707.56 |
| 364 | MAG | sling | ERDC | Site Survey | Supervisor | 26.68 | 2534.6 |
| 364 | MAG | sling | ERDC | Site Survey | Data Analyst | 26.68 | 1520.76 |
| 364 | MAG | sling | ERDC | Site Survey | Field Support | 26.68 | 760.38 |
| 364 | MAG | sling | ERDC | Site Survey | Subtotal | 0 | 4815.74 |
| 364 | MAG | sling | ERDC | Demobilization | Supervisor | 0.25 | 23.75 |
| 364 | MAG | sling | ERDC | Demobilization | Data Analyst | 0.25 | 14.25 |
| 364 | MAG | sling | ERDC | Demobilization | Field Support | 0.25 | 7.13 |
| 364 | MAG | sling | ERDC | Demobilization | Subtotal | 0 | 45.13 |
| 364 | MAG | sling | ERDC | Total | Total | 0 | 6169.5 |
| 769 | MAG | hand | Forester | Calibration | Supervisor | 1.83 | 173.85 |
| 769 | MAG | hand | Forester | Calibration | Data Analyst | 1.83 | 104.31 |
| 769 | MAG | hand | Forester | Calibration | Field Support | 1.83 | 104.31 |
| 769 | MAG | hand | Forester | Calibration | Subtotal | 0 | 382.47 |
| 769 | MAG | hand | Forester | Site Survey | Supervisor | 2.4 | 228 |
| 769 | MAG | hand | Forester | Site Survey | Data Analyst | 2.4 | 136.8 |
| 769 | MAG | hand | Forester | Site Survey | Field Support | 2.4 | 136.8 |
| 769 | MAG | hand | Forester | Site Survey | Subtotal | 0 | 501.6 |
| 769 | MAG | hand | Forester | Demobilization | Supervisor | 1.08 | 102.6 |
| 769 | MAG | hand | Forester | Demobilization | Data Analyst | 1.08 | 61.56 |
| 769 | MAG | hand | Forester | Demobilization | Field Support | 1.08 | 61.56 |
| 769 | MAG | hand | Forester | Demobilization | Subtotal | 0 | 225.72 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 769 | MAG | hand | Forester | Total | Total | 0 | 1214.29 |
| 769 | MAG | hand | Forester | Initial Setup | Supervisor | 0.5 | 47.5 |
| 769 | MAG | hand | Forester | Initial Setup | Data Analyst | 0.5 | 28.5 |
| 769 | MAG | hand | Forester | Initial Setup | Field Support | 0.5 | 28.5 |
| 769 | MAG | hand | Forester | Initial Setup | Subtotal | 0 | 104.5 |
| 770 | MAG | hand | Forester | Initial Setup | Supervisor | 0.5 | 47.5 |
| 770 | MAG | hand | Forester | Initial Setup | Data Analyst | 0.5 | 28.5 |
| 770 | MAG | hand | Forester | Initial Setup | Field Support | 0.5 | 28.5 |
| 770 | MAG | hand | Forester | Initial Setup | Subtotal | 0 | 104.5 |
| 770 | MAG | hand | Forester | Calibration | Supervisor | 2.03 | 192.85 |
| 770 | MAG | hand | Forester | Calibration | Data Analyst | 2.03 | 115.71 |
| 770 | MAG | hand | Forester | Calibration | Field Support | 2.03 | 115.71 |
| 770 | MAG | hand | Forester | Calibration | Subtotal | 0 | 424.27 |
| 770 | MAG | hand | Forester | Site Survey | Supervisor | 45.55 | 4327.25 |
| 770 | MAG | hand | Forester | Site Survey | Data Analyst | 45.55 | 2596.35 |
| 770 | MAG | hand | Forester | Site Survey | Field Support | 45.55 | 2596.35 |
| 770 | MAG | hand | Forester | Site Survey | Subtotal | 0 | 9519.95 |
| 770 | MAG | hand | Forester | Demobilization | Supervisor | 1.08 | 102.6 |
| 770 | MAG | hand | Forester | Demobilization | Data Analyst | 1.08 | 61.56 |
| 770 | MAG | hand | Forester | Demobilization | Field Support | 1.08 | 61.56 |
| 770 | MAG | hand | Forester | Demobilization | Subtotal | 0 | 225.72 |
| 770 | MAG | hand | Forester | Total | Total | 0 | 10274.44 |
| 293 | dual | towed | Geocenters | Initial Setup | Supervisor | 2.9 | 275.5 |
| 293 | dual | towed | Geocenters | Initial Setup | Data Analyst | 2.9 | 165.3 |
| 293 | dual | towed | Geocenters | Initial Setup | Field Support | 2.9 | 0 |
| 293 | dual | towed | Geocenters | Initial Setup | Subtotal | 0 | 440.8 |
| 293 | dual | towed | Geocenters | Calibration | Supervisor | 0.43 | 40.85 |
| 293 | dual | towed | Geocenters | Calibration | Data Analyst | 0.43 | 24.51 |
| 293 | dual | towed | Geocenters | Calibration | Field Support | 0.43 | 0 |
| 293 | dual | towed | Geocenters | Calibration | Subtotal | 0 | 65.36 |
| 293 | dual | towed | Geocenters | Site Survey | Supervisor | 2.57 | 244.15 |
| 293 | dual | towed | Geocenters | Site Survey | Data Analyst | 2.57 | 146.49 |
| 293 | dual | towed | Geocenters | Site Survey | Field Support | 2.57 | 0 |
| 293 | dual | towed | Geocenters | Site Survey | Subtotal | 0 | 390.64 |
| 293 | dual | towed | Geocenters | Demobilization | Supervisor | 1.88 | 178.6 |
| 293 | dual | towed | Geocenters | Demobilization | Data Analyst | 1.88 | 107.16 |
| 293 | dual | towed | Geocenters | Demobilization | Field Support | 1.88 | 0 |
| 293 | dual | towed | Geocenters | Demobilization | Subtotal | 0 | 285.76 |
| 293 | dual | towed | Geocenters | Total | Total | 0 | 1182.56 |
| 299 | dual | towed | Geocenters | Initial Setup | Supervisor | 2.9 | 275.5 |
| 299 | dual | towed | Geocenters | Initial Setup | Data Analyst | 2.9 | 165.3 |
| 299 | dual | towed | Geocenters | Initial Setup | Field Support | 2.9 | 0 |
| 299 | dual | towed | Geocenters | Initial Setup | Subtotal | 0 | 440.8 |
| 299 | dual | towed | Geocenters | Calibration | Supervisor | 0.43 | 40.85 |
| 299 | dual | towed | Geocenters | Calibration | Data Analyst | 0.43 | 24.51 |
| 299 | dual | towed | Geocenters | Calibration | Field Support | 0.43 | 0 |
| 299 | dual | towed | Geocenters | Calibration | Subtotal | 0 | 65.36 |
| 299 | dual | towed | Geocenters | Site Survey | Supervisor | 15.32 | 1455.4 |
| 299 | dual | towed | Geocenters | Site Survey | Data Analyst | 15.32 | 873.24 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 299 | dual | towed | Geocenters | Site Survey | Field Support | 15.32 | 0 |
| 299 | dual | towed | Geocenters | Site Survey | Subtotal | 0 | 2328.64 |
| 299 | dual | towed | Geocenters | Demobilization | Supervisor | 1.88 | 178.6 |
| 299 | dual | towed | Geocenters | Demobilization | Data Analyst | 1.88 | 107.16 |
| 299 | dual | towed | Geocenters | Demobilization | Field Support | 1.88 | 0 |
| 299 | dual | towed | Geocenters | Demobilization | Subtotal | 0 | 285.76 |
| 299 | dual | towed | Geocenters | Total | Total | 0 | 3120.56 |
| 186 | EM | hand | G-TEK | Initial Setup | Supervisor | 1.67 | 158.65 |
| 186 | EM | hand | G-TEK | Initial Setup | Data Analyst | 1.67 | 95.19 |
| 186 | EM | hand | G-TEK | Initial Setup | Field Support | 1.67 | 0 |
| 186 | EM | hand | G-TEK | Initial Setup | Subtotal | 0 | 253.84 |
| 186 | EM | hand | G-TEK | Calibration | Supervisor | 1.25 | 118.75 |
| 186 | EM | hand | G-TEK | Calibration | Data Analyst | 1.25 | 71.25 |
| 186 | EM | hand | G-TEK | Calibration | Field Support | 1.25 | 0 |
| 186 | EM | hand | G-TEK | Calibration | Subtotal | 0 | 190 |
| 186 | EM | hand | G-TEK | Site Survey | Supervisor | 1.17 | 111.15 |
| 186 | EM | hand | G-TEK | Site Survey | Data Analyst | 1.17 | 66.69 |
| 186 | EM | hand | G-TEK | Site Survey | Field Support | 1.17 | 0 |
| 186 | EM | hand | G-TEK | Site Survey | Subtotal | 0 | 177.84 |
| 186 | EM | hand | G-TEK | Demobilization | Supervisor | 1.28 | 121.6 |
| 186 | EM | hand | G-TEK | Demobilization | Data Analyst | 1.28 | 72.96 |
| 186 | EM | hand | G-TEK | Demobilization | Field Support | 1.28 | 0 |
| 186 | EM | hand | G-TEK | Demobilization | Subtotal | 0 | 194.56 |
| 186 | EM | hand | G-TEK | Total | Total | 0 | 816.24 |
| 144 | EM | hand | G-TEK | Initial Setup | Supervisor | 1.66 | 157.7 |
| 144 | EM | hand | G-TEK | Initial Setup | Data Analyst | 1.66 | 94.62 |
| 144 | EM | hand | G-TEK | Initial Setup | Field Support | 1.66 | 0 |
| 144 | EM | hand | G-TEK | Initial Setup | Subtotal | 0 | 252.32 |
| 144 | EM | hand | G-TEK | Calibration | Supervisor | 3.8 | 361 |
| 144 | EM | hand | G-TEK | Calibration | Data Analyst | 3.8 | 216.6 |
| 144 | EM | hand | G-TEK | Calibration | Field Support | 3.8 | 0 |
| 144 | EM | hand | G-TEK | Calibration | Subtotal | 0 | 577.6 |
| 144 | EM | hand | G-TEK | Site Survey | Supervisor | 11.28 | 1071.6 |
| 144 | EM | hand | G-TEK | Site Survey | Data Analyst | 11.28 | 642.96 |
| 144 | EM | hand | G-TEK | Site Survey | Field Support | 11.28 | 0 |
| 144 | EM | hand | G-TEK | Site Survey | Subtotal | 0 | 1714.56 |
| 144 | EM | hand | G-TEK | Demobilization | Supervisor | 1.28 | 121.6 |
| 144 | EM | hand | G-TEK | Demobilization | Data Analyst | 1.28 | 72.96 |
| 144 | EM | hand | G-TEK | Demobilization | Field Support | 1.28 | 0 |
| 144 | EM | hand | G-TEK | Demobilization | Subtotal | 0 | 194.56 |
| 144 | EM | hand | G-TEK | Total | Total | 0 | 2739.04 |
| 579 | EM | sling | G-TEK | Initial Setup | Supervisor | 1.66 | 157.7 |
| 579 | EM | sling | G-TEK | Initial Setup | Data Analyst | 1.66 | 94.62 |
| 579 | EM | sling | G-TEK | Initial Setup | Field Support | 1.66 | 0 |
| 579 | EM | sling | G-TEK | Initial Setup | Subtotal | 0 | 252.32 |
| 579 | EM | sling | G-TEK | Calibration | Supervisor | 3.7 | 351.5 |
| 579 | EM | sling | G-TEK | Calibration | Data Analyst | 3.7 | 210.9 |
| 579 | EM | sling | G-TEK | Calibration | Field Support | 3.7 | 0 |
| 579 | EM | sling | G-TEK | Calibration | Subtotal | 0 | 562.4 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 579 | EM | sling | G-TEK | Site Survey | Supervisor | 7.38 | 701.1 |
| 579 | EM | sling | G-TEK | Site Survey | Data Analyst | 7.38 | 420.66 |
| 579 | EM | sling | G-TEK | Site Survey | Field Support | 7.38 | 0 |
| 579 | EM | sling | G-TEK | Site Survey | Subtotal | 0 | 1121.76 |
| 579 | EM | sling | G-TEK | Demobilization | Supervisor | 1.28 | 121.6 |
| 579 | EM | sling | G-TEK | Demobilization | Data Analyst | 1.28 | 72.96 |
| 579 | EM | sling | G-TEK | Demobilization | Field Support | 1.28 | 0 |
| 579 | EM | sling | G-TEK | Demobilization | Subtotal | 0 | 194.56 |
| 579 | EM | sling | G-TEK | Total | Total | 0 | 2131.04 |
| 148 | EM | sling | G-TEK | Initial Setup | Supervisor | 1.67 | 158.65 |
| 148 | EM | sling | G-TEK | Initial Setup | Data Analyst | 1.67 | 95.19 |
| 148 | EM | sling | G-TEK | Initial Setup | Field Support | 1.67 | 47.6 |
| 148 | EM | sling | G-TEK | Initial Setup | Subtotal | 0 | 301.44 |
| 148 | EM | sling | G-TEK | Calibration | Supervisor | 3.58 | 340.1 |
| 148 | EM | sling | G-TEK | Calibration | Data Analyst | 3.58 | 204.06 |
| 148 | EM | sling | G-TEK | Calibration | Field Support | 3.58 | 102.03 |
| 148 | EM | sling | G-TEK | Calibration | Subtotal | 0 | 646.19 |
| 148 | EM | sling | G-TEK | Site Survey | Supervisor | 57.82 | 5492.9 |
| 148 | EM | sling | G-TEK | Site Survey | Data Analyst | 57.82 | 3295.74 |
| 148 | EM | sling | G-TEK | Site Survey | Field Support | 57.82 | 1647.87 |
| 148 | EM | sling | G-TEK | Site Survey | Subtotal | 0 | 10436.51 |
| 148 | EM | sling | G-TEK | Demobilization | Supervisor | 1.28 | 121.6 |
| 148 | EM | sling | G-TEK | Demobilization | Data Analyst | 1.28 | 72.96 |
| 148 | EM | sling | G-TEK | Demobilization | Field Support | 1.28 | 36.48 |
| 148 | EM | sling | G-TEK | Demobilization | Subtotal | 0 | 231.04 |
| 148 | EM | sling | G-TEK | Total | Total | 0 | 11615.18 |
| 431 | MAG | sling | G-TEK | Initial Setup | Supervisor | 2.17 | 206.15 |
| 431 | MAG | sling | G-TEK | Initial Setup | Data Analyst | 2.17 | 123.69 |
| 431 | MAG | sling | G-TEK | Initial Setup | Field Support | 2.17 | 61.85 |
| 431 | MAG | sling | G-TEK | Initial Setup | Subtotal | 0 | 391.69 |
| 431 | MAG | sling | G-TEK | Calibration | Supervisor | 0.9 | 85.5 |
| 431 | MAG | sling | G-TEK | Calibration | Data Analyst | 0.9 | 51.3 |
| 431 | MAG | sling | G-TEK | Calibration | Field Support | 0.9 | 25.65 |
| 431 | MAG | sling | G-TEK | Calibration | Subtotal | 0 | 162.45 |
| 431 | MAG | sling | G-TEK | Site Survey | Supervisor | 0.77 | 73.15 |
| 431 | MAG | sling | G-TEK | Site Survey | Data Analyst | 0.77 | 43.89 |
| 431 | MAG | sling | G-TEK | Site Survey | Field Support | 0.77 | 21.95 |
| 431 | MAG | sling | G-TEK | Site Survey | Subtotal | 0 | 138.99 |
| 431 | MAG | sling | G-TEK | Demobilization | Supervisor | 2.67 | 253.65 |
| 431 | MAG | sling | G-TEK | Demobilization | Data Analyst | 2.67 | 152.19 |
| 431 | MAG | sling | G-TEK | Demobilization | Field Support | 2.67 | 0 |
| 431 | MAG | sling | G-TEK | Demobilization | Subtotal | 0 | 405.84 |
| 431 | MAG | sling | G-TEK | Total | Total | 0 | 1098.97 |
| 536 | MAG | sling | G-TEK | Initial Setup | Supervisor | 2.16 | 205.2 |
| 536 | MAG | sling | G-TEK | Initial Setup | Data Analyst | 2.16 | 123.12 |
| 536 | MAG | sling | G-TEK | Initial Setup | Field Support | 2.16 | 0 |
| 536 | MAG | sling | G-TEK | Initial Setup | Subtotal | 0 | 328.32 |
| 536 | MAG | sling | G-TEK | Calibration | Supervisor | 2.78 | 264.1 |
| 536 | MAG | sling | G-TEK | Calibration | Data Analyst | 2.78 | 158.46 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 536 | MAG | sling | G-TEK | Calibration | Field Support | 2.78 | 0 |
| 536 | MAG | sling | G-TEK | Calibration | Subtotal | 0 | 422.56 |
| 536 | MAG | sling | G-TEK | Site Survey | Supervisor | 18.23 | 1731.85 |
| 536 | MAG | sling | G-TEK | Site Survey | Data Analyst | 18.23 | 1039.11 |
| 536 | MAG | sling | G-TEK | Site Survey | Field Support | 18.23 | 0 |
| 536 | MAG | sling | G-TEK | Site Survey | Subtotal | 0 | 2770.96 |
| 536 | MAG | sling | G-TEK | Demobilization | Supervisor | 2.66 | 252.7 |
| 536 | MAG | sling | G-TEK | Demobilization | Data Analyst | 2.66 | 151.62 |
| 536 | MAG | sling | G-TEK | Demobilization | Field Support | 2.66 | 0 |
| 536 | MAG | sling | G-TEK | Demobilization | Subtotal | 0 | 404.32 |
| 536 | MAG | sling | G-TEK | Total | Total | 0 | 3926.16 |
| 581 | MAG | sling | G-TEK | Initial Setup | Supervisor | 2.17 | 206.15 |
| 581 | MAG | sling | G-TEK | Initial Setup | Data Analyst | 2.17 | 123.69 |
| 581 | MAG | sling | G-TEK | Initial Setup | Field Support | 2.17 | 61.85 |
| 581 | MAG | sling | G-TEK | Initial Setup | Subtotal | 0 | 391.69 |
| 581 | MAG | sling | G-TEK | Calibration | Supervisor | 2.35 | 223.25 |
| 581 | MAG | sling | G-TEK | Calibration | Data Analyst | 2.35 | 133.95 |
| 581 | MAG | sling | G-TEK | Calibration | Field Support | 2.35 | 0 |
| 581 | MAG | sling | G-TEK | Calibration | Subtotal | 0 | 357.2 |
| 581 | MAG | sling | G-TEK | Site Survey | Supervisor | 7.85 | 745.75 |
| 581 | MAG | sling | G-TEK | Site Survey | Data Analyst | 7.85 | 447.45 |
| 581 | MAG | sling | G-TEK | Site Survey | Field Support | 7.85 | 0 |
| 581 | MAG | sling | G-TEK | Site Survey | Subtotal | 0 | 1193.2 |
| 581 | MAG | sling | G-TEK | Demobilization | Supervisor | 2.66 | 252.7 |
| 581 | MAG | sling | G-TEK | Demobilization | Data Analyst | 2.66 | 151.62 |
| 581 | MAG | sling | G-TEK | Demobilization | Field Support | 2.66 | 0 |
| 581 | MAG | sling | G-TEK | Demobilization | Subtotal | 0 | 404.32 |
| 581 | MAG | sling | G-TEK | Total | Total | 0 | 2346.41 |
| 147 | MAG | sling | G-TEK | Initial Setup | Supervisor | 2.17 | 206.15 |
| 147 | MAG | sling | G-TEK | Initial Setup | Data Analyst | 2.17 | 123.69 |
| 147 | MAG | sling | G-TEK | Initial Setup | Field Support | 2.17 | 61.85 |
| 147 | MAG | sling | G-TEK | Initial Setup | Subtotal | 0 | 391.69 |
| 147 | MAG | sling | G-TEK | Calibration | Supervisor | 0.9 | 85.5 |
| 147 | MAG | sling | G-TEK | Calibration | Data Analyst | 0.9 | 51.3 |
| 147 | MAG | sling | G-TEK | Calibration | Field Support | 0.9 | 25.65 |
| 147 | MAG | sling | G-TEK | Calibration | Subtotal | 0 | 162.45 |
| 147 | MAG | sling | G-TEK | Site Survey | Supervisor | 32.12 | 3051.4 |
| 147 | MAG | sling | G-TEK | Site Survey | Data Analyst | 32.12 | 1830.84 |
| 147 | MAG | sling | G-TEK | Site Survey | Field Support | 32.12 | 915.42 |
| 147 | MAG | sling | G-TEK | Site Survey | Subtotal | 0 | 5797.66 |
| 147 | MAG | sling | G-TEK | Demobilization | Supervisor | 2.67 | 253.65 |
| 147 | MAG | sling | G-TEK | Demobilization | Data Analyst | 2.67 | 152.19 |
| 147 | MAG | sling | G-TEK | Demobilization | Field Support | 2.67 | 76.1 |
| 147 | MAG | sling | G-TEK | Demobilization | Subtotal | 0 | 481.94 |
| 147 | MAG | sling | G-TEK | Total | Total | 0 | 6833.74 |
| 238 | MAG | hand | HFA | Initial Setup | Supervisor | 1.33 | 126.35 |
| 238 | MAG | hand | HFA | Initial Setup | Data Analyst | 1.33 | 0 |
| 238 | MAG | hand | HFA | Initial Setup | Field Support | 1.33 | 37.91 |
| 238 | MAG | hand | HFA | Initial Setup | Subtotal | 0 | 164.26 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 238 | MAG | hand | HFA | Calibration | Supervisor | 14.08 | 1337.6 |
| 238 | MAG | hand | HFA | Calibration | Data Analyst | 14.08 | 0 |
| 238 | MAG | hand | HFA | Calibration | Field Support | 14.08 | 401.28 |
| 238 | MAG | hand | HFA | Calibration | Subtotal | 0 | 1738.88 |
| 238 | MAG | hand | HFA | Site Survey | Supervisor | 8.58 | 815.1 |
| 238 | MAG | hand | HFA | Site Survey | Data Analyst | 8.58 | 0 |
| 238 | MAG | hand | HFA | Site Survey | Field Support | 8.58 | 244.53 |
| 238 | MAG | hand | HFA | Site Survey | Subtotal | 0 | 1059.63 |
| 238 | MAG | hand | HFA | Demobilization | Supervisor | 4 | 380 |
| 238 | MAG | hand | HFA | Demobilization | Data Analyst | 4 | 0 |
| 238 | MAG | hand | HFA | Demobilization | Field Support | 4 | 114 |
| 238 | MAG | hand | HFA | Demobilization | Subtotal | 0 | 494 |
| 238 | MAG | hand | HFA | Total | Total | 0 | 3456.77 |
| 528 | MAG | hand | HFA | Initial Setup | Supervisor | 1.33 | 126.35 |
| 528 | MAG | hand | HFA | Initial Setup | Data Analyst | 1.33 | 75.81 |
| 528 | MAG | hand | HFA | Initial Setup | Field Support | 0 | 0 |
| 528 | MAG | hand | HFA | Initial Setup | Subtotal | 0 | 202.16 |
| 528 | MAG | hand | HFA | Calibration | Supervisor | 12.08 | 1147.6 |
| 528 | MAG | hand | HFA | Calibration | Data Analyst | 12.08 | 688.56 |
| 528 | MAG | hand | HFA | Calibration | Field Support | 0 | 0 |
| 528 | MAG | hand | HFA | Calibration | Subtotal | 0 | 1836.16 |
| 528 | MAG | hand | HFA | Site Survey | Supervisor | 15.55 | 1477.25 |
| 528 | MAG | hand | HFA | Site Survey | Data Analyst | 15.55 | 886.35 |
| 528 | MAG | hand | HFA | Site Survey | Field Support | 0 | 0 |
| 528 | MAG | hand | HFA | Site Survey | Subtotal | 0 | 2363.6 |
| 528 | MAG | hand | HFA | Demobilization | Supervisor | 4 | 380 |
| 528 | MAG | hand | HFA | Demobilization | Data Analyst | 4 | 228 |
| 528 | MAG | hand | HFA | Demobilization | Field Support | 0 | 0 |
| 528 | MAG | hand | HFA | Demobilization | Subtotal | 0 | 608 |
| 528 | MAG | hand | HFA | Total | Total | 0 | 5009.92 |
| 587 | MAG | hand | HFA | Initial Setup | Supervisor | 1.33 | 126.35 |
| 587 | MAG | hand | HFA | Initial Setup | Data Analyst | 1.33 | 75.81 |
| 587 | MAG | hand | HFA | Initial Setup | Field Support | 1.33 | 0 |
| 587 | MAG | hand | HFA | Initial Setup | Subtotal | 0 | 202.16 |
| 587 | MAG | hand | HFA | Calibration | Supervisor | 12.75 | 1211.25 |
| 587 | MAG | hand | HFA | Calibration | Data Analyst | 12.75 | 726.75 |
| 587 | MAG | hand | HFA | Calibration | Field Support | 12.75 | 0 |
| 587 | MAG | hand | HFA | Calibration | Subtotal | 0 | 1938 |
| 587 | MAG | hand | HFA | Site Survey | Supervisor | 27.83 | 2643.85 |
| 587 | MAG | hand | HFA | Site Survey | Data Analyst | 27.83 | 1586.31 |
| 587 | MAG | hand | HFA | Site Survey | Field Support | 27.83 | 0 |
| 587 | MAG | hand | HFA | Site Survey | Subtotal | 0 | 4230.16 |
| 587 | MAG | hand | HFA | Demobilization | Supervisor | 4 | 380 |
| 587 | MAG | hand | HFA | Demobilization | Data Analyst | 4 | 0 |
| 587 | MAG | hand | HFA | Demobilization | Field Support | 4 | 0 |
| 587 | MAG | hand | HFA | Demobilization | Subtotal | 0 | 380 |
| 587 | MAG | hand | HFA | Total | Total | 0 | 6750.32 |
| 442 | MAG | hand | HFA | Initial Setup | Supervisor | 1.33 | 126.35 |
| 442 | MAG | hand | HFA | Initial Setup | Data Analyst | 1.33 | 75.81 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 442 | MAG | hand | HFA | Initial Setup | Field Support | 1.33 | 0 |
| 442 | MAG | hand | HFA | Initial Setup | Subtotal | 0 | 202.16 |
| 442 | MAG | hand | HFA | Calibration | Supervisor | 12.75 | 1211.25 |
| 442 | MAG | hand | HFA | Calibration | Data Analyst | 12.75 | 726.75 |
| 442 | MAG | hand | HFA | Calibration | Field Support | 12.75 | 0 |
| 442 | MAG | hand | HFA | Calibration | Subtotal | 0 | 1938 |
| 442 | MAG | hand | HFA | Site Survey | Supervisor | 179.32 | 17035.4 |
| 442 | MAG | hand | HFA | Site Survey | Data Analyst | 179.32 | 10221.24 |
| 442 | MAG | hand | HFA | Site Survey | Field Support | 179.32 | 0 |
| 442 | MAG | hand | HFA | Site Survey | Subtotal | 0 | 27256.64 |
| 442 | MAG | hand | HFA | Demobilization | Supervisor | 4 | 380 |
| 442 | MAG | hand | HFA | Demobilization | Data Analyst | 4 | 0 |
| 442 | MAG | hand | HFA | Demobilization | Field Support | 4 | 0 |
| 442 | MAG | hand | HFA | Demobilization | Subtotal | 0 | 380 |
| 442 | MAG | hand | HFA | Total | Total | 0 | 29776.8 |
| 667 | EM | towed | NAEVA | Initial Setup | Supervisor | 1.83 | 173.85 |
| 667 | EM | towed | NAEVA | Initial Setup | Data Analyst | 1.83 | 104.31 |
| 667 | EM | towed | NAEVA | Initial Setup | Field Support | 1.83 | 104.31 |
| 667 | EM | towed | NAEVA | Initial Setup | Subtotal | 0 | 382.47 |
| 667 | EM | towed | NAEVA | Calibration | Supervisor | 4.58 | 435.1 |
| 667 | EM | towed | NAEVA | Calibration | Data Analyst | 4.58 | 261.06 |
| 667 | EM | towed | NAEVA | Calibration | Field Support | 4.58 | 261.06 |
| 667 | EM | towed | NAEVA | Calibration | Subtotal | 0 | 957.22 |
| 667 | EM | towed | NAEVA | Site Survey | Supervisor | 1.58 | 150.1 |
| 667 | EM | towed | NAEVA | Site Survey | Data Analyst | 1.58 | 90.06 |
| 667 | EM | towed | NAEVA | Site Survey | Field Support | 1.58 | 90.06 |
| 667 | EM | towed | NAEVA | Site Survey | Subtotal | 0 | 330.22 |
| 667 | EM | towed | NAEVA | Demobilization | Supervisor | 2.16 | 205.2 |
| 667 | EM | towed | NAEVA | Demobilization | Data Analyst | 2.16 | 123.12 |
| 667 | EM | towed | NAEVA | Demobilization | Field Support | 2.16 | 123.12 |
| 667 | EM | towed | NAEVA | Demobilization | Subtotal | 0 | 451.44 |
| 667 | EM | towed | NAEVA | Total | Total | 0 | 2121.35 |
| 666 | EM | 2-man | NAEVA | Initial Setup | Supervisor | 0.92 | 87.4 |
| 666 | EM | 2-man | NAEVA | Initial Setup | Data Analyst | 0.92 | 52.44 |
| 666 | EM | 2-man | NAEVA | Initial Setup | Field Support | 0.92 | 52.44 |
| 666 | EM | 2-man | NAEVA | Initial Setup | Subtotal | 0 | 192.28 |
| 666 | EM | 2-man | NAEVA | Calibration | Supervisor | 3.5 | 332.5 |
| 666 | EM | 2-man | NAEVA | Calibration | Data Analyst | 3.5 | 199.5 |
| 666 | EM | 2-man | NAEVA | Calibration | Field Support | 3.5 | 199.5 |
| 666 | EM | 2-man | NAEVA | Calibration | Subtotal | 0 | 731.5 |
| 666 | EM | 2-man | NAEVA | Site Survey | Supervisor | 2.42 | 229.9 |
| 666 | EM | 2-man | NAEVA | Site Survey | Data Analyst | 2.42 | 137.94 |
| 666 | EM | 2-man | NAEVA | Site Survey | Field Support | 2.42 | 137.94 |
| 666 | EM | 2-man | NAEVA | Site Survey | Subtotal | 0 | 505.78 |
| 666 | EM | 2-man | NAEVA | Demobilization | Supervisor | 2.16 | 205.2 |
| 666 | EM | 2-man | NAEVA | Demobilization | Data Analyst | 2.16 | 123.12 |
| 666 | EM | 2-man | NAEVA | Demobilization | Field Support | 2.16 | 123.12 |
| 666 | EM | 2-man | NAEVA | Demobilization | Subtotal | 0 | 451.44 |
| 666 | EM | 2-man | NAEVA | Total | Total | 0 | 1881 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 670 | EM | 2-man | NAEVA | Initial Setup | Supervisor | 0.92 | 87.4 |
| 670 | EM | 2-man | NAEVA | Initial Setup | Data Analyst | 0.92 | 52.44 |
| 670 | EM | 2-man | NAEVA | Initial Setup | Field Support | 0.92 | 52.44 |
| 670 | EM | 2-man | NAEVA | Initial Setup | Subtotal | 0 | 192.28 |
| 670 | EM | 2-man | NAEVA | Calibration | Supervisor | 3.83 | 363.85 |
| 670 | EM | 2-man | NAEVA | Calibration | Data Analyst | 3.83 | 218.31 |
| 670 | EM | 2-man | NAEVA | Calibration | Field Support | 3.83 | 218.31 |
| 670 | EM | 2-man | NAEVA | Calibration | Subtotal | 0 | 800.47 |
| 670 | EM | 2-man | NAEVA | Site Survey | Supervisor | 10.92 | 1037.4 |
| 670 | EM | 2-man | NAEVA | Site Survey | Data Analyst | 10.92 | 622.44 |
| 670 | EM | 2-man | NAEVA | Site Survey | Field Support | 10.92 | 622.44 |
| 670 | EM | 2-man | NAEVA | Site Survey | Subtotal | 0 | 2282.28 |
| 670 | EM | 2-man | NAEVA | Demobilization | Supervisor | 2.16 | 205.2 |
| 670 | EM | 2-man | NAEVA | Demobilization | Data Analyst | 2.16 | 123.12 |
| 670 | EM | 2-man | NAEVA | Demobilization | Field Support | 2.16 | 123.12 |
| 670 | EM | 2-man | NAEVA | Demobilization | Subtotal | 0 | 451.44 |
| 670 | EM | 2-man | NAEVA | Total | Total | 0 | 3726.47 |
| 669 | EM | 2-man | NAEVA | Initial Setup | Supervisor | 0.92 | 87.4 |
| 669 | EM | 2-man | NAEVA | Initial Setup | Data Analyst | 0.92 | 52.44 |
| 669 | EM | 2-man | NAEVA | Initial Setup | Field Support | 0.92 | 52.44 |
| 669 | EM | 2-man | NAEVA | Initial Setup | Subtotal | 0 | 192.28 |
| 669 | EM | 2-man | NAEVA | Calibration | Supervisor | 4.16 | 395.2 |
| 669 | EM | 2-man | NAEVA | Calibration | Data Analyst | 4.16 | 237.12 |
| 669 | EM | 2-man | NAEVA | Calibration | Field Support | 4.16 | 237.12 |
| 669 | EM | 2-man | NAEVA | Calibration | Subtotal | 0 | 869.44 |
| 669 | EM | 2-man | NAEVA | Site Survey | Supervisor | 10.66 | 1012.7 |
| 669 | EM | 2-man | NAEVA | Site Survey | Data Analyst | 10.66 | 607.62 |
| 669 | EM | 2-man | NAEVA | Site Survey | Field Support | 10.66 | 607.62 |
| 669 | EM | 2-man | NAEVA | Site Survey | Subtotal | 0 | 2227.94 |
| 669 | EM | 2-man | NAEVA | Demobilization | Supervisor | 2.16 | 205.2 |
| 669 | EM | 2-man | NAEVA | Demobilization | Data Analyst | 2.16 | 123.12 |
| 669 | EM | 2-man | NAEVA | Demobilization | Field Support | 2.16 | 123.12 |
| 669 | EM | 2-man | NAEVA | Demobilization | Subtotal | 0 | 451.44 |
| 669 | EM | 2-man | NAEVA | Total | Total | 0 | 3741.1 |
| 668 | EM | towed | NAEVA | Initial Setup | Supervisor | 1.83 | 173.85 |
| 668 | EM | towed | NAEVA | Initial Setup | Data Analyst | 1.83 | 104.31 |
| 668 | EM | towed | NAEVA | Initial Setup | Field Support | 1.83 | 104.31 |
| 668 | EM | towed | NAEVA | Initial Setup | Subtotal | 0 | 382.47 |
| 668 | EM | towed | NAEVA | Calibration | Supervisor | 6.92 | 657.4 |
| 668 | EM | towed | NAEVA | Calibration | Data Analyst | 6.92 | 394.44 |
| 668 | EM | towed | NAEVA | Calibration | Field Support | 6.92 | 394.44 |
| 668 | EM | towed | NAEVA | Calibration | Subtotal | 0 | 1446.28 |
| 668 | EM | towed | NAEVA | Site Survey | Supervisor | 38.92 | 3697.4 |
| 668 | EM | towed | NAEVA | Site Survey | Data Analyst | 38.92 | 2218.44 |
| 668 | EM | towed | NAEVA | Site Survey | Field Support | 38.92 | 2218.44 |
| 668 | EM | towed | NAEVA | Site Survey | Subtotal | 0 | 8134.28 |
| 668 | EM | towed | NAEVA | Demobilization | Supervisor | 2.16 | 205.2 |
| 668 | EM | towed | NAEVA | Demobilization | Data Analyst | 2.16 | 123.12 |
| 668 | EM | towed | NAEVA | Demobilization | Field Support | 2.16 | 0 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 668 | EM | towed | NAEVA | Demobilization | Subtotal | 0 | 328.32 |
| 668 | EM | towed | NAEVA | Total | Total | 0 | 10291.35 |
| 213 | EM | towed | NRL | Initial Setup | Supervisor | 3 | 285 |
| 213 | EM | towed | NRL | Initial Setup | Data Analyst | 3 | 171 |
| 213 | EM | towed | NRL | Initial Setup | Field Support | 3 | 171 |
| 213 | EM | towed | NRL | Initial Setup | Subtotal | 0 | 627 |
| 213 | EM | towed | NRL | Calibration | Supervisor | 1.93 | 183.35 |
| 213 | EM | towed | NRL | Calibration | Data Analyst | 1.93 | 110.01 |
| 213 | EM | towed | NRL | Calibration | Field Support | 1.93 | 110.01 |
| 213 | EM | towed | NRL | Calibration | Subtotal | 0 | 403.37 |
| 213 | EM | towed | NRL | Site Survey | Supervisor | 3.17 | 301.15 |
| 213 | EM | towed | NRL | Site Survey | Data Analyst | 3.17 | 180.69 |
| 213 | EM | towed | NRL | Site Survey | Field Support | 3.17 | 180.69 |
| 213 | EM | towed | NRL | Site Survey | Subtotal | 0 | 662.53 |
| 213 | EM | towed | NRL | Demobilization | Supervisor | 2.3 | 218.5 |
| 213 | EM | towed | NRL | Demobilization | Data Analyst | 2.3 | 131.1 |
| 213 | EM | towed | NRL | Demobilization | Field Support | 0 | 0 |
| 213 | EM | towed | NRL | Demobilization | Subtotal | 0 | 349.6 |
| 213 | EM | towed | NRL | Total | Total | 0 | 2042.5 |
| 245 | EM | towed | NRL | Initial Setup | Supervisor | 2.5 | 237.5 |
| 245 | EM | towed | NRL | Initial Setup | Data Analyst | 2.5 | 142.5 |
| 245 | EM | towed | NRL | Initial Setup | Field Support | 2.5 | 142.5 |
| 245 | EM | towed | NRL | Initial Setup | Subtotal | 0 | 522.5 |
| 245 | EM | towed | NRL | Calibration | Supervisor | 2.43 | 230.85 |
| 245 | EM | towed | NRL | Calibration | Data Analyst | 2.43 | 138.51 |
| 245 | EM | towed | NRL | Calibration | Field Support | 2.43 | 138.51 |
| 245 | EM | towed | NRL | Calibration | Subtotal | 0 | 507.87 |
| 245 | EM | towed | NRL | Site Survey | Supervisor | 42.77 | 4063.15 |
| 245 | EM | towed | NRL | Site Survey | Data Analyst | 42.77 | 2437.89 |
| 245 | EM | towed | NRL | Site Survey | Field Support | 42.77 | 2437.89 |
| 245 | EM | towed | NRL | Site Survey | Subtotal | 0 | 8938.93 |
| 245 | EM | towed | NRL | Demobilization | Supervisor | 2.3 | 218.5 |
| 245 | EM | towed | NRL | Demobilization | Data Analyst | 2.3 | 131.1 |
| 245 | EM | towed | NRL | Demobilization | Field Support | 2.3 | 131.1 |
| 245 | EM | towed | NRL | Demobilization | Subtotal | 0 | 480.7 |
| 245 | EM | towed | NRL | Total | Total | 0 | 10450 |
| 690 | EM | cart | Parsons | Initial Setup | Supervisor | 1.33 | 126.35 |
| 690 | EM | cart | Parsons | Initial Setup | Data Analyst | 1.33 | 75.81 |
| 690 | EM | cart | Parsons | Initial Setup | Field Support | 1.33 | 0 |
| 690 | EM | cart | Parsons | Initial Setup | Subtotal | 0 | 202.16 |
| 690 | EM | cart | Parsons | Calibration | Supervisor | 1.42 | 134.9 |
| 690 | EM | cart | Parsons | Calibration | Data Analyst | 1.42 | 80.94 |
| 690 | EM | cart | Parsons | Calibration | Field Support | 1.42 | 0 |
| 690 | EM | cart | Parsons | Calibration | Subtotal | 0 | 215.84 |
| 690 | EM | cart | Parsons | Site Survey | Supervisor | 2.58 | 245.1 |
| 690 | EM | cart | Parsons | Site Survey | Data Analyst | 2.58 | 147.06 |
| 690 | EM | cart | Parsons | Site Survey | Field Support | 2.58 | 0 |
| 690 | EM | cart | Parsons | Site Survey | Subtotal | 0 | 392.16 |
| 690 | EM | cart | Parsons | Demobilization | Supervisor | 0.66 | 62.7 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 690 | EM | cart | Parsons | Demobilization | Data Analyst | 0.66 | 37.62 |
| 690 | EM | cart | Parsons | Demobilization | Field Support | 0.66 | 0 |
| 690 | EM | cart | Parsons | Demobilization | Subtotal | 0 | 100.32 |
| 690 | EM | cart | Parsons | Total | Total | 0 | 910.48 |
| 532 | EM | cart | Parsons | Initial Setup | Supervisor | 2 | 190 |
| 532 | EM | cart | Parsons | Initial Setup | Data Analyst | 2 | 114 |
| 532 | EM | cart | Parsons | Initial Setup | Field Support | 2 | 114 |
| 532 | EM | cart | Parsons | Initial Setup | Subtotal | 0 | 418 |
| 532 | EM | cart | Parsons | Calibration | Supervisor | 4.75 | 451.25 |
| 532 | EM | cart | Parsons | Calibration | Data Analyst | 4.75 | 270.75 |
| 532 | EM | cart | Parsons | Calibration | Field Support | 4.75 | 270.75 |
| 532 | EM | cart | Parsons | Calibration | Subtotal | 0 | 992.75 |
| 532 | EM | cart | Parsons | Site Survey | Supervisor | 22.17 | 2106.15 |
| 532 | EM | cart | Parsons | Site Survey | Data Analyst | 22.17 | 1263.69 |
| 532 | EM | cart | Parsons | Site Survey | Field Support | 22.17 | 1263.69 |
| 532 | EM | cart | Parsons | Site Survey | Subtotal | 0 | 4633.53 |
| 532 | EM | cart | Parsons | Demobilization | Supervisor | 2 | 190 |
| 532 | EM | cart | Parsons | Demobilization | Data Analyst | 2 | 114 |
| 532 | EM | cart | Parsons | Demobilization | Field Support | 2 | 114 |
| 532 | EM | cart | Parsons | Demobilization | Subtotal | 0 | 418 |
| 532 | EM | cart | Parsons | Total | Total | 0 | 6462.28 |
| 588 | EM | cart | Parsons | Initial Setup | Supervisor | 1.33 | 126.35 |
| 588 | EM | cart | Parsons | Initial Setup | Data Analyst | 1.33 | 75.81 |
| 588 | EM | cart | Parsons | Initial Setup | Field Support | 1.33 | 0 |
| 588 | EM | cart | Parsons | Initial Setup | Subtotal | 0 | 202.16 |
| 588 | EM | cart | Parsons | Calibration | Supervisor | 3.92 | 372.4 |
| 588 | EM | cart | Parsons | Calibration | Data Analyst | 3.92 | 223.44 |
| 588 | EM | cart | Parsons | Calibration | Field Support | 3.92 | 223.44 |
| 588 | EM | cart | Parsons | Calibration | Subtotal | 0 | 819.28 |
| 588 | EM | cart | Parsons | Site Survey | Supervisor | 22.08 | 2097.6 |
| 588 | EM | cart | Parsons | Site Survey | Data Analyst | 22.08 | 1258.56 |
| 588 | EM | cart | Parsons | Site Survey | Field Support | 22.08 | 1258.56 |
| 588 | EM | cart | Parsons | Site Survey | Subtotal | 0 | 4614.72 |
| 588 | EM | cart | Parsons | Demobilization | Supervisor | 2 | 190 |
| 588 | EM | cart | Parsons | Demobilization | Data Analyst | 2 | 114 |
| 588 | EM | cart | Parsons | Demobilization | Field Support | 2 | 114 |
| 588 | EM | cart | Parsons | Demobilization | Subtotal | 0 | 418 |
| 588 | EM | cart | Parsons | Total | Total | 0 | 6054.16 |
| 425 | EM | cart | Parsons | Initial Setup | Supervisor | 2 | 190 |
| 425 | EM | cart | Parsons | Initial Setup | Data Analyst | 2 | 114 |
| 425 | EM | cart | Parsons | Initial Setup | Field Support | 2 | 114 |
| 425 | EM | cart | Parsons | Initial Setup | Subtotal | 0 | 418 |
| 425 | EM | cart | Parsons | Calibration | Supervisor | 2.42 | 229.9 |
| 425 | EM | cart | Parsons | Calibration | Data Analyst | 2.42 | 137.94 |
| 425 | EM | cart | Parsons | Calibration | Field Support | 2.42 | 137.94 |
| 425 | EM | cart | Parsons | Calibration | Subtotal | 0 | 505.78 |
| 425 | EM | cart | Parsons | Site Survey | Supervisor | 63.17 | 6001.15 |
| 425 | EM | cart | Parsons | Site Survey | Data Analyst | 63.17 | 3600.69 |
| 425 | EM | cart | Parsons | Site Survey | Field Support | 63.17 | 3600.69 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 425 | EM | cart | Parsons | Site Survey | Subtotal | 0 | 13202.53 |
| 425 | EM | cart | Parsons | Demobilization | Supervisor | 2 | 190 |
| 425 | EM | cart | Parsons | Demobilization | Data Analyst | 2 | 114 |
| 425 | EM | cart | Parsons | Demobilization | Field Support | 2 | 114 |
| 425 | EM | cart | Parsons | Demobilization | Subtotal | 0 | 418 |
| 425 | EM | cart | Parsons | Total | Total | 0 | 14544.31 |
| 606 | MAG | hand | Parsons | Initial Setup | Supervisor | 0.5 | 47.5 |
| 606 | MAG | hand | Parsons | Initial Setup | Data Analyst | 0.5 | 28.5 |
| 606 | MAG | hand | Parsons | Initial Setup | Field Support | 0.5 | 57 |
| 606 | MAG | hand | Parsons | Initial Setup | Subtotal | 0 | 133 |
| 606 | MAG | hand | Parsons | Calibration | Supervisor | 0.33 | 31.35 |
| 606 | MAG | hand | Parsons | Calibration | Data Analyst | 0.33 | 18.81 |
| 606 | MAG | hand | Parsons | Calibration | Field Support | 0.33 | 37.62 |
| 606 | MAG | hand | Parsons | Calibration | Subtotal | 0 | 87.78 |
| 606 | MAG | hand | Parsons | Site Survey | Supervisor | 0.75 | 71.25 |
| 606 | MAG | hand | Parsons | Site Survey | Data Analyst | 0.75 | 42.75 |
| 606 | MAG | hand | Parsons | Site Survey | Field Support | 0.75 | 85.5 |
| 606 | MAG | hand | Parsons | Site Survey | Subtotal | 0 | 199.5 |
| 606 | MAG | hand | Parsons | Demobilization | Supervisor | 0.83 | 78.85 |
| 606 | MAG | hand | Parsons | Demobilization | Data Analyst | 0.83 | 47.31 |
| 606 | MAG | hand | Parsons | Demobilization | Field Support | 0.83 | 118.28 |
| 606 | MAG | hand | Parsons | Demobilization | Subtotal | 0 | 244.44 |
| 606 | MAG | hand | Parsons | Total | Total | 0 | 664.72 |
| 601 | MAG | hand | Parsons | Initial Setup | Supervisor | 0.5 | 47.5 |
| 601 | MAG | hand | Parsons | Initial Setup | Data Analyst | 0.5 | 28.5 |
| 601 | MAG | hand | Parsons | Initial Setup | Field Support | 0.5 | 57 |
| 601 | MAG | hand | Parsons | Initial Setup | Subtotal | 0 | 133 |
| 601 | MAG | hand | Parsons | Calibration | Supervisor | 0.33 | 31.35 |
| 601 | MAG | hand | Parsons | Calibration | Data Analyst | 0.33 | 18.81 |
| 601 | MAG | hand | Parsons | Calibration | Field Support | 0.33 | 37.62 |
| 601 | MAG | hand | Parsons | Calibration | Subtotal | 0 | 87.78 |
| 601 | MAG | hand | Parsons | Site Survey | Supervisor | 6.05 | 574.75 |
| 601 | MAG | hand | Parsons | Site Survey | Data Analyst | 6.05 | 344.85 |
| 601 | MAG | hand | Parsons | Site Survey | Field Support | 6.05 | 862.13 |
| 601 | MAG | hand | Parsons | Site Survey | Subtotal | 0 | 1781.73 |
| 601 | MAG | hand | Parsons | Demobilization | Supervisor | 0.83 | 78.85 |
| 601 | MAG | hand | Parsons | Demobilization | Data Analyst | 0.83 | 47.31 |
| 601 | MAG | hand | Parsons | Demobilization | Field Support | 0.83 | 118.28 |
| 601 | MAG | hand | Parsons | Demobilization | Subtotal | 0 | 244.44 |
| 601 | MAG | hand | Parsons | Total | Total | 0 | 2246.95 |
| 602 | MAG | hand | Parsons | Initial Setup | Supervisor | 0.5 | 47.5 |
| 602 | MAG | hand | Parsons | Initial Setup | Data Analyst | 0.5 | 28.5 |
| 602 | MAG | hand | Parsons | Initial Setup | Field Support | 0.5 | 57 |
| 602 | MAG | hand | Parsons | Initial Setup | Subtotal | 0 | 133 |
| 602 | MAG | hand | Parsons | Calibration | Supervisor | 0.33 | 31.35 |
| 602 | MAG | hand | Parsons | Calibration | Data Analyst | 0.33 | 18.81 |
| 602 | MAG | hand | Parsons | Calibration | Field Support | 0.33 | 37.62 |
| 602 | MAG | hand | Parsons | Calibration | Subtotal | 0 | 87.78 |
| 602 | MAG | hand | Parsons | Site Survey | Supervisor | 7.33 | 696.35 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 602 | MAG | hand | Parsons | Site Survey | Data Analyst | 7.33 | 417.81 |
| 602 | MAG | hand | Parsons | Site Survey | Field Support | 7.33 | 1044.53 |
| 602 | MAG | hand | Parsons | Site Survey | Subtotal | 0 | 2158.69 |
| 602 | MAG | hand | Parsons | Demobilization | Supervisor | 0.83 | 78.85 |
| 602 | MAG | hand | Parsons | Demobilization | Data Analyst | 0.83 | 47.31 |
| 602 | MAG | hand | Parsons | Demobilization | Field Support | 0.83 | 118.28 |
| 602 | MAG | hand | Parsons | Demobilization | Subtotal | 0 | 244.44 |
| 602 | MAG | hand | Parsons | Total | Total | 0 | 2623.91 |
| 426 | MAG | hand | Parsons | Initial Setup | Supervisor | 0.5 | 47.5 |
| 426 | MAG | hand | Parsons | Initial Setup | Data Analyst | 0.5 | 28.5 |
| 426 | MAG | hand | Parsons | Initial Setup | Field Support | 0.5 | 57 |
| 426 | MAG | hand | Parsons | Initial Setup | Subtotal | 0 | 133 |
| 426 | MAG | hand | Parsons | Calibration | Supervisor | 0.33 | 31.35 |
| 426 | MAG | hand | Parsons | Calibration | Data Analyst | 0.33 | 18.81 |
| 426 | MAG | hand | Parsons | Calibration | Field Support | 0.33 | 37.62 |
| 426 | MAG | hand | Parsons | Calibration | Subtotal | 0 | 87.78 |
| 426 | MAG | hand | Parsons | Site Survey | Supervisor | 39 | 3705 |
| 426 | MAG | hand | Parsons | Site Survey | Data Analyst | 39 | 2223 |
| 426 | MAG | hand | Parsons | Site Survey | Field Support | 39 | 4446 |
| 426 | MAG | hand | Parsons | Site Survey | Subtotal | 0 | 10374 |
| 426 | MAG | hand | Parsons | Demobilization | Supervisor | 0.83 | 78.85 |
| 426 | MAG | hand | Parsons | Demobilization | Data Analyst | 0.83 | 47.31 |
| 426 | MAG | hand | Parsons | Demobilization | Field Support | 0.83 | 118.28 |
| 426 | MAG | hand | Parsons | Demobilization | Subtotal | 0 | 244.44 |
| 426 | MAG | hand | Parsons | Total | Total | 0 | 10839.22 |
| 199 | EM | cart | Shaw | Initial Setup | Supervisor | 2.41 | 228.95 |
| 199 | EM | cart | Shaw | Initial Setup | Data Analyst | 2.41 | 137.37 |
| 199 | EM | cart | Shaw | Initial Setup | Field Support | 2.41 | 68.69 |
| 199 | EM | cart | Shaw | Initial Setup | Subtotal | 0 | 435.01 |
| 199 | EM | cart | Shaw | Calibration | Supervisor | 6 | 570 |
| 199 | EM | cart | Shaw | Calibration | Data Analyst | 6 | 342 |
| 199 | EM | cart | Shaw | Calibration | Field Support | 6 | 171 |
| 199 | EM | cart | Shaw | Calibration | Subtotal | 0 | 1083 |
| 199 | EM | cart | Shaw | Site Survey | Supervisor | 1.11 | 105.45 |
| 199 | EM | cart | Shaw | Site Survey | Data Analyst | 1.11 | 63.27 |
| 199 | EM | cart | Shaw | Site Survey | Field Support | 1.11 | 31.64 |
| 199 | EM | cart | Shaw | Site Survey | Subtotal | 0 | 200.36 |
| 199 | EM | cart | Shaw | Demobilization | Supervisor | 1.08 | 102.6 |
| 199 | EM | cart | Shaw | Demobilization | Data Analyst | 1.08 | 61.56 |
| 199 | EM | cart | Shaw | Demobilization | Field Support | 1.08 | 30.78 |
| 199 | EM | cart | Shaw | Demobilization | Subtotal | 0 | 194.95 |
| 199 | EM | cart | Shaw | Total | Total | 0 | 1913.32 |
| 211 | EM | cart | Shaw | Initial Setup | Supervisor | 2.42 | 229.9 |
| 211 | EM | cart | Shaw | Initial Setup | Data Analyst | 2.42 | 137.94 |
| 211 | EM | cart | Shaw | Initial Setup | Field Support | 2.42 | 68.97 |
| 211 | EM | cart | Shaw | Initial Setup | Subtotal | 0 | 436.81 |
| 211 | EM | cart | Shaw | Calibration | Supervisor | 2.92 | 277.4 |
| 211 | EM | cart | Shaw | Calibration | Data Analyst | 2.92 | 166.44 |
| 211 | EM | cart | Shaw | Calibration | Field Support | 2.92 | 83.22 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 211 | EM | cart | Shaw | Calibration | Subtotal | 0 | 527.06 |
| 211 | EM | cart | Shaw | Site Survey | Supervisor | 21.47 | 2039.65 |
| 211 | EM | cart | Shaw | Site Survey | Data Analyst | 21.47 | 1223.79 |
| 211 | EM | cart | Shaw | Site Survey | Field Support | 21.47 | 611.9 |
| 211 | EM | cart | Shaw | Site Survey | Subtotal | 0 | 3875.34 |
| 211 | EM | cart | Shaw | Demobilization | Supervisor | 1.08 | 102.6 |
| 211 | EM | cart | Shaw | Demobilization | Data Analyst | 1.08 | 61.56 |
| 211 | EM | cart | Shaw | Demobilization | Field Support | 1.08 | 30.78 |
| 211 | EM | cart | Shaw | Demobilization | Subtotal | 0 | 194.94 |
| 211 | EM | cart | Shaw | Total | Total | 0 | 5034.15 |
| 207 | EM | cart | Shaw | Initial Setup | Supervisor | 2.42 | 229.9 |
| 207 | EM | cart | Shaw | Initial Setup | Data Analyst | 2.42 | 137.94 |
| 207 | EM | cart | Shaw | Initial Setup | Field Support | 2.42 | 68.97 |
| 207 | EM | cart | Shaw | Initial Setup | Subtotal | 0 | 436.81 |
| 207 | EM | cart | Shaw | Calibration | Supervisor | 2.58 | 245.1 |
| 207 | EM | cart | Shaw | Calibration | Data Analyst | 2.58 | 147.06 |
| 207 | EM | cart | Shaw | Calibration | Field Support | 2.58 | 73.53 |
| 207 | EM | cart | Shaw | Calibration | Subtotal | 0 | 465.69 |
| 207 | EM | cart | Shaw | Site Survey | Supervisor | 3.42 | 324.9 |
| 207 | EM | cart | Shaw | Site Survey | Data Analyst | 3.42 | 194.94 |
| 207 | EM | cart | Shaw | Site Survey | Field Support | 3.42 | 97.47 |
| 207 | EM | cart | Shaw | Site Survey | Subtotal | 0 | 617.31 |
| 207 | EM | cart | Shaw | Demobilization | Supervisor | 1.08 | 102.6 |
| 207 | EM | cart | Shaw | Demobilization | Data Analyst | 1.08 | 61.56 |
| 207 | EM | cart | Shaw | Demobilization | Field Support | 1.08 | 30.78 |
| 207 | EM | cart | Shaw | Demobilization | Subtotal | 0 | 194.94 |
| 207 | EM | cart | Shaw | Total | Total | 0 | 1714.75 |
| 354 | EM | cart | Shaw | Initial Setup | Supervisor | 2.42 | 229.9 |
| 354 | EM | cart | Shaw | Initial Setup | Data Analyst | 2.42 | 137.94 |
| 354 | EM | cart | Shaw | Initial Setup | Field Support | 2.42 | 68.97 |
| 354 | EM | cart | Shaw | Initial Setup | Subtotal | 0 | 436.81 |
| 354 | EM | cart | Shaw | Calibration | Supervisor | 2.58 | 245.1 |
| 354 | EM | cart | Shaw | Calibration | Data Analyst | 2.58 | 147.06 |
| 354 | EM | cart | Shaw | Calibration | Field Support | 2.58 | 73.53 |
| 354 | EM | cart | Shaw | Calibration | Subtotal | 0 | 465.69 |
| 354 | EM | cart | Shaw | Site Survey | Supervisor | 29.57 | 2809.15 |
| 354 | EM | cart | Shaw | Site Survey | Data Analyst | 29.57 | 1685.49 |
| 354 | EM | cart | Shaw | Site Survey | Field Support | 29.57 | 842.74 |
| 354 | EM | cart | Shaw | Site Survey | Subtotal | 0 | 5337.38 |
| 354 | EM | cart | Shaw | Demobilization | Supervisor | 1.08 | 102.6 |
| 354 | EM | cart | Shaw | Demobilization | Data Analyst | 1.08 | 61.56 |
| 354 | EM | cart | Shaw | Demobilization | Field Support | 1.08 | 30.78 |
| 354 | EM | cart | Shaw | Demobilization | Subtotal | 0 | 194.94 |
| 354 | EM | cart | Shaw | Total | Total | 0 | 6434.82 |
| 312 | MAG | cart | Shaw | Initial Setup | Supervisor | 3.25 | 308.75 |
| 312 | MAG | cart | Shaw | Initial Setup | Data Analyst | 3.25 | 185.25 |
| 312 | MAG | cart | Shaw | Initial Setup | Field Support | 3.25 | 92.63 |
| 312 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 586.63 |
| 312 | MAG | cart | Shaw | Calibration | Supervisor | 0.16 | 15.2 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 312 | MAG | cart | Shaw | Calibration | Data Analyst | 0.16 | 9.12 |
| 312 | MAG | cart | Shaw | Calibration | Field Support | 0.16 | 4.56 |
| 312 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 28.88 |
| 312 | MAG | cart | Shaw | Site Survey | Supervisor | 2.32 | 220.4 |
| 312 | MAG | cart | Shaw | Site Survey | Data Analyst | 2.32 | 132.24 |
| 312 | MAG | cart | Shaw | Site Survey | Field Support | 2.32 | 66.12 |
| 312 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 418.76 |
| 312 | MAG | cart | Shaw | Demobilization | Supervisor | 0.75 | 71.25 |
| 312 | MAG | cart | Shaw | Demobilization | Data Analyst | 0.75 | 42.75 |
| 312 | MAG | cart | Shaw | Demobilization | Field Support | 0.75 | 21.38 |
| 312 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 135.38 |
| 312 | MAG | cart | Shaw | Total | Total | 0 | 1169.65 |
| 541 | MAG | cart | Shaw | Initial Setup | Supervisor | 3.25 | 308.75 |
| 541 | MAG | cart | Shaw | Initial Setup | Data Analyst | 3.25 | 185.25 |
| 541 | MAG | cart | Shaw | Initial Setup | Field Support | 3.25 | 92.63 |
| 541 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 586.63 |
| 541 | MAG | cart | Shaw | Calibration | Supervisor | 0.16 | 15.2 |
| 541 | MAG | cart | Shaw | Calibration | Data Analyst | 0.16 | 9.12 |
| 541 | MAG | cart | Shaw | Calibration | Field Support | 0.16 | 4.56 |
| 541 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 28.88 |
| 541 | MAG | cart | Shaw | Site Survey | Supervisor | 12.5 | 1187.5 |
| 541 | MAG | cart | Shaw | Site Survey | Data Analyst | 12.5 | 712.5 |
| 541 | MAG | cart | Shaw | Site Survey | Field Support | 12.5 | 356.25 |
| 541 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 2256.25 |
| 541 | MAG | cart | Shaw | Demobilization | Supervisor | 0.75 | 71.25 |
| 541 | MAG | cart | Shaw | Demobilization | Data Analyst | 0.75 | 42.75 |
| 541 | MAG | cart | Shaw | Demobilization | Field Support | 0.75 | 0 |
| 541 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 114 |
| 541 | MAG | cart | Shaw | Total | Total | 0 | 2985.76 |
| 594 | MAG | cart | Shaw | Initial Setup | Supervisor | 3.25 | 308.75 |
| 594 | MAG | cart | Shaw | Initial Setup | Data Analyst | 3.25 | 185.25 |
| 594 | MAG | cart | Shaw | Initial Setup | Field Support | 3.25 | 92.63 |
| 594 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 586.63 |
| 594 | MAG | cart | Shaw | Calibration | Supervisor | 0.17 | 16.15 |
| 594 | MAG | cart | Shaw | Calibration | Data Analyst | 0.17 | 9.69 |
| 594 | MAG | cart | Shaw | Calibration | Field Support | 0.17 | 4.85 |
| 594 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 30.69 |
| 594 | MAG | cart | Shaw | Site Survey | Supervisor | 4.21 | 399.95 |
| 594 | MAG | cart | Shaw | Site Survey | Data Analyst | 4.21 | 239.97 |
| 594 | MAG | cart | Shaw | Site Survey | Field Support | 4.21 | 119.98 |
| 594 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 759.9 |
| 594 | MAG | cart | Shaw | Demobilization | Supervisor | 0.75 | 71.25 |
| 594 | MAG | cart | Shaw | Demobilization | Data Analyst | 0.75 | 42.75 |
| 594 | MAG | cart | Shaw | Demobilization | Field Support | 0.75 | 21 |
| 594 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 135 |
| 594 | MAG | cart | Shaw | Total | Total | 0 | 1512.22 |
| 638 | MAG | cart | Shaw | Initial Setup | Supervisor | 3.25 | 308.75 |
| 638 | MAG | cart | Shaw | Initial Setup | Data Analyst | 3.25 | 185.25 |
| 638 | MAG | cart | Shaw | Initial Setup | Field Support | 3.25 | 92.63 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 638 | MAG | cart | Shaw | Initial Setup | Subtotal | 0 | 586.63 |
| 638 | MAG | cart | Shaw | Calibration | Supervisor | 0.17 | 16.15 |
| 638 | MAG | cart | Shaw | Calibration | Data Analyst | 0.17 | 9.69 |
| 638 | MAG | cart | Shaw | Calibration | Field Support | 0.17 | 4.85 |
| 638 | MAG | cart | Shaw | Calibration | Subtotal | 0 | 30.69 |
| 638 | MAG | cart | Shaw | Site Survey | Supervisor | 20.55 | 1952.25 |
| 638 | MAG | cart | Shaw | Site Survey | Data Analyst | 20.55 | 1171.35 |
| 638 | MAG | cart | Shaw | Site Survey | Field Support | 20.55 | 585.68 |
| 638 | MAG | cart | Shaw | Site Survey | Subtotal | 0 | 3709.28 |
| 638 | MAG | cart | Shaw | Demobilization | Supervisor | 0.75 | 71.25 |
| 638 | MAG | cart | Shaw | Demobilization | Data Analyst | 0.75 | 42.75 |
| 638 | MAG | cart | Shaw | Demobilization | Field Support | 0.75 | 21.38 |
| 638 | MAG | cart | Shaw | Demobilization | Subtotal | 0 | 135.38 |
| 638 | MAG | cart | Shaw | Total | Total | 0 | 4461.98 |
| 168 | EM | cart | TTF | Initial Setup | Supervisor | 1.92 | 182.4 |
| 168 | EM | cart | TTF | Initial Setup | Data Analyst | 1.92 | 328.32 |
| 168 | EM | cart | TTF | Initial Setup | Field Support | 1.92 | 0 |
| 168 | EM | cart | TTF | Initial Setup | Subtotal | 0 | 510.72 |
| 168 | EM | cart | TTF | Calibration | Supervisor | 2.08 | 197.6 |
| 168 | EM | cart | TTF | Calibration | Data Analyst | 2.08 | 355.68 |
| 168 | EM | cart | TTF | Calibration | Field Support | 2.08 | 0 |
| 168 | EM | cart | TTF | Calibration | Subtotal | 0 | 553.28 |
| 168 | EM | cart | TTF | Site Survey | Supervisor | 1.05 | 99.75 |
| 168 | EM | cart | TTF | Site Survey | Data Analyst | 1.05 | 179.55 |
| 168 | EM | cart | TTF | Site Survey | Field Support | 1.05 | 0 |
| 168 | EM | cart | TTF | Site Survey | Subtotal | 0 | 279.3 |
| 168 | EM | cart | TTF | Demobilization | Supervisor | 0.3 | 28.5 |
| 168 | EM | cart | TTF | Demobilization | Data Analyst | 0.3 | 51.3 |
| 168 | EM | cart | TTF | Demobilization | Field Support | 0.3 | 0 |
| 168 | EM | cart | TTF | Demobilization | Subtotal | 0 | 79.8 |
| 168 | EM | cart | TTF | Total | Total | 0 | 1423.1 |
| 171 | EM | cart | TTF | Initial Setup | Supervisor | 1.92 | 182.4 |
| 171 | EM | cart | TTF | Initial Setup | Data Analyst | 1.92 | 109.44 |
| 171 | EM | cart | TTF | Initial Setup | Field Support | 1.92 | 0 |
| 171 | EM | cart | TTF | Initial Setup | Subtotal | 0 | 291.84 |
| 171 | EM | cart | TTF | Calibration | Supervisor | 3.45 | 327.75 |
| 171 | EM | cart | TTF | Calibration | Data Analyst | 3.45 | 196.65 |
| 171 | EM | cart | TTF | Calibration | Field Support | 3.45 | 0 |
| 171 | EM | cart | TTF | Calibration | Subtotal | 0 | 524.4 |
| 171 | EM | cart | TTF | Site Survey | Supervisor | 11.35 | 1078.25 |
| 171 | EM | cart | TTF | Site Survey | Data Analyst | 11.35 | 646.95 |
| 171 | EM | cart | TTF | Site Survey | Field Support | 11.35 | 0 |
| 171 | EM | cart | TTF | Site Survey | Subtotal | 0 | 1725.2 |
| 171 | EM | cart | TTF | Demobilization | Supervisor | 2.33 | 221.35 |
| 171 | EM | cart | TTF | Demobilization | Data Analyst | 2.33 | 132.81 |
| 171 | EM | cart | TTF | Demobilization | Field Support | 2.33 | 0 |
| 171 | EM | cart | TTF | Demobilization | Subtotal | 0 | 354.16 |
| 171 | EM | cart | TTF | Total | Total | 0 | 2895.6 |
| 170 | EM | slings | TTF | Initial Setup | Supervisor | 1.92 | 182.4 |

| <i>Yuma Proving Ground Demonstrations</i> | | | | | | | |
|---|---------------|-----------------|---------------|----------------|------------------|--------------|-------------|
| Report | Sensor | Platform | Vendor | Task | Personnel | Hours | Cost |
| 170 | EM | sling | TTF | Initial Setup | Data Analyst | 1.92 | 109.44 |
| 170 | EM | sling | TTF | Initial Setup | Field Support | 1.92 | 0 |
| 170 | EM | sling | TTF | Initial Setup | Subtotal | 0 | 291.84 |
| 170 | EM | sling | TTF | Calibration | Supervisor | 3.73 | 354.35 |
| 170 | EM | sling | TTF | Calibration | Data Analyst | 3.73 | 212.61 |
| 170 | EM | sling | TTF | Calibration | Field Support | 3.73 | 0 |
| 170 | EM | sling | TTF | Calibration | Subtotal | 0 | 566.96 |
| 170 | EM | sling | TTF | Site Survey | Supervisor | 8.97 | 852.15 |
| 170 | EM | sling | TTF | Site Survey | Data Analyst | 8.97 | 511.29 |
| 170 | EM | sling | TTF | Site Survey | Field Support | 8.97 | 0 |
| 170 | EM | sling | TTF | Site Survey | Subtotal | 0 | 1363.44 |
| 170 | EM | sling | TTF | Demobilization | Supervisor | 1.66 | 157.7 |
| 170 | EM | sling | TTF | Demobilization | Data Analyst | 1.66 | 94.62 |
| 170 | EM | sling | TTF | Demobilization | Field Support | 1.66 | 0 |
| 170 | EM | sling | TTF | Demobilization | Subtotal | 0 | 252.32 |
| 170 | EM | sling | TTF | Total | Total | 0 | 2474.56 |
| 169 | EM | cart | TTF | Initial Setup | Supervisor | 1.92 | 182.4 |
| 169 | EM | cart | TTF | Initial Setup | Data Analyst | 1.92 | 328.32 |
| 169 | EM | cart | TTF | Initial Setup | Field Support | 1.92 | 0 |
| 169 | EM | cart | TTF | Initial Setup | Subtotal | 0 | 510.72 |
| 169 | EM | cart | TTF | Calibration | Supervisor | 2.7 | 256.5 |
| 169 | EM | cart | TTF | Calibration | Data Analyst | 2.7 | 461.7 |
| 169 | EM | cart | TTF | Calibration | Field Support | 2.7 | 0 |
| 169 | EM | cart | TTF | Calibration | Subtotal | 0 | 718.2 |
| 169 | EM | cart | TTF | Site Survey | Supervisor | 32.17 | 3056.15 |
| 169 | EM | cart | TTF | Site Survey | Data Analyst | 32.17 | 5501.07 |
| 169 | EM | cart | TTF | Site Survey | Field Support | 32.17 | 0 |
| 169 | EM | cart | TTF | Site Survey | Subtotal | 0 | 8557.22 |
| 169 | EM | cart | TTF | Demobilization | Supervisor | 0.67 | 63.65 |
| 169 | EM | cart | TTF | Demobilization | Data Analyst | 0.67 | 114.57 |
| 169 | EM | cart | TTF | Demobilization | Field Support | 0.67 | 0 |
| 169 | EM | cart | TTF | Demobilization | Subtotal | 0 | 178.22 |
| 169 | EM | cart | TTF | Total | Total | 0 | 9964.36 |

APPENDIX E. LOCATION ERROR HISTOGRAMS

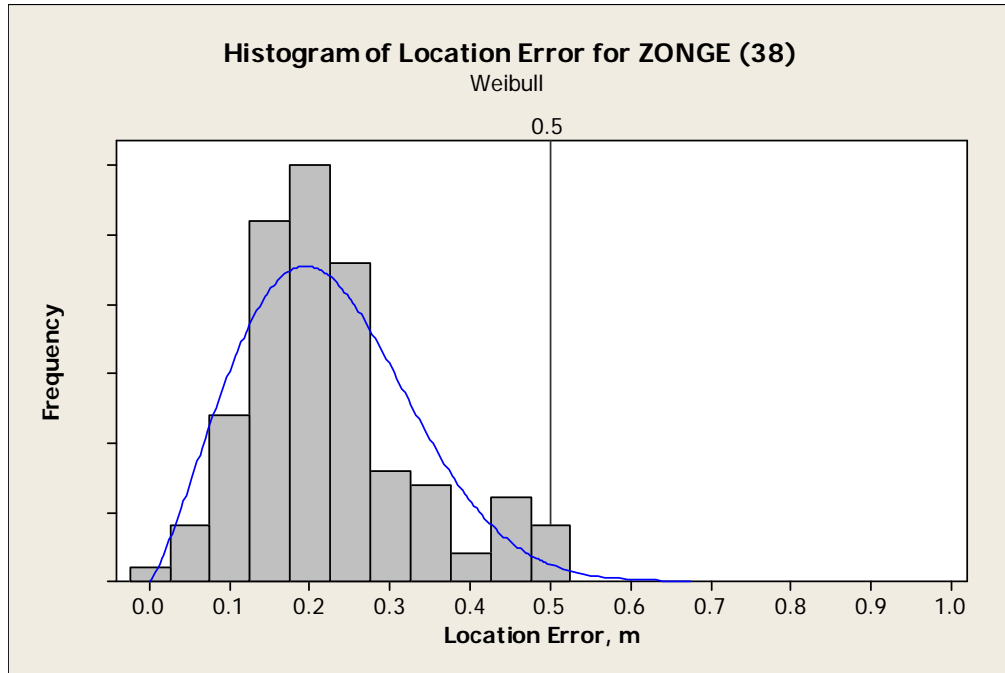


Figure E-1. Location Error Histogram for Zonge, SR #38.

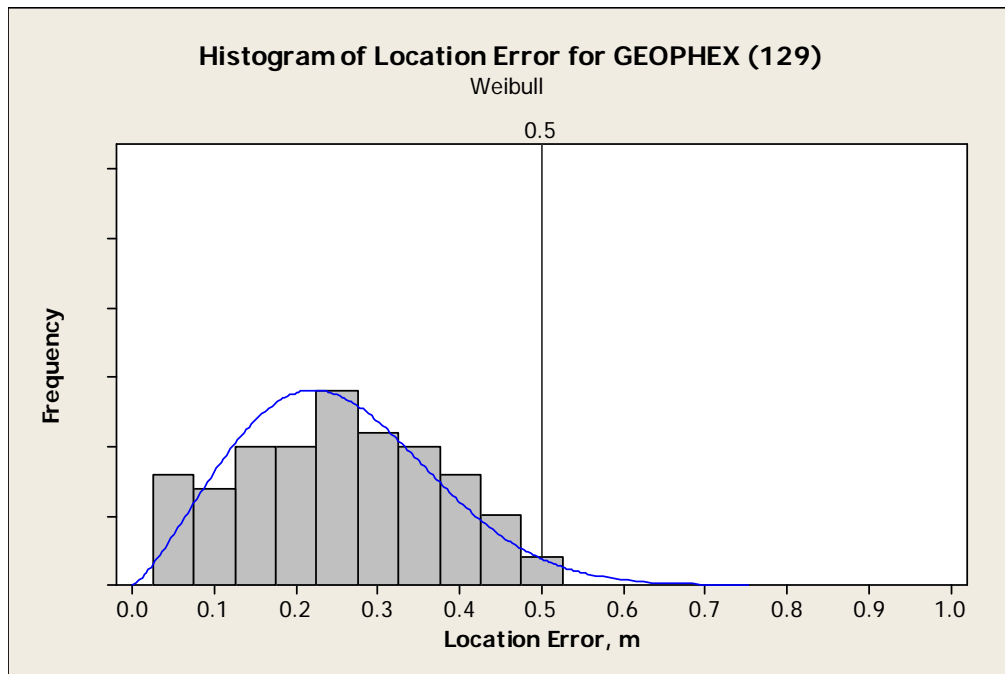


Figure E-2. Location Error Histogram for Geophex, SR #129.

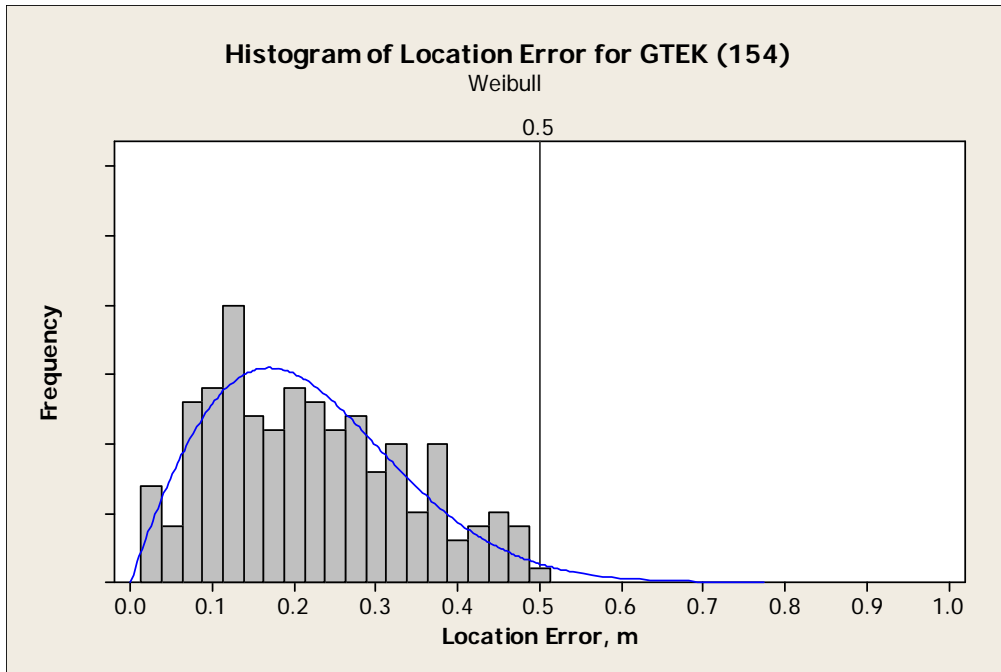


Figure E-3. Location Error Histogram for G-TEK, SR #154.

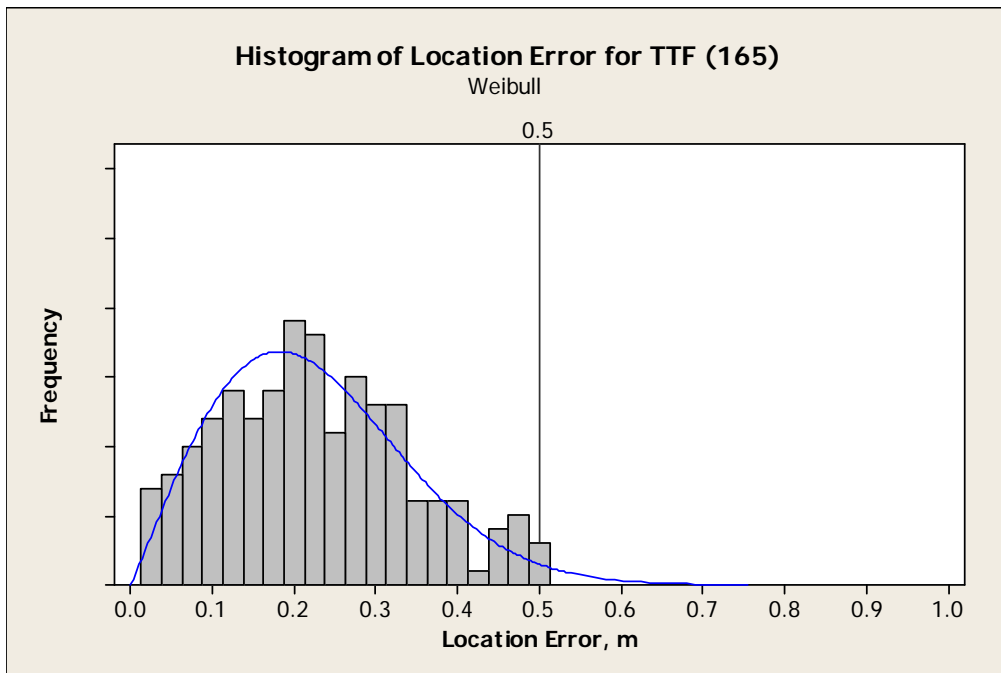


Figure E-4. Location Error Histogram for TTF, SR 165.

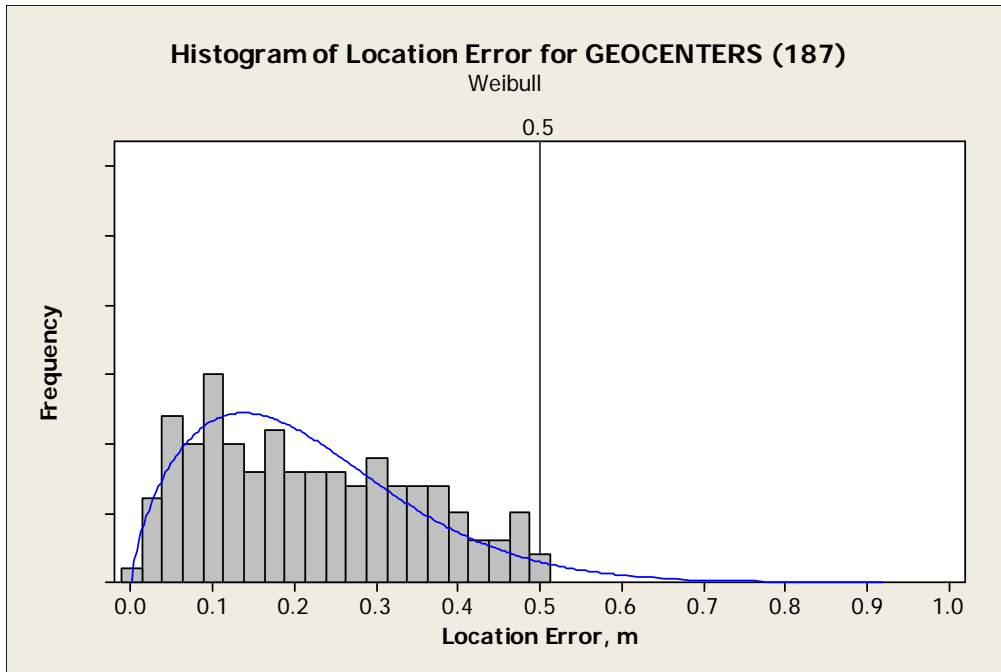


Figure E-5. Location Error Histogram for Geocenters, SR #187.

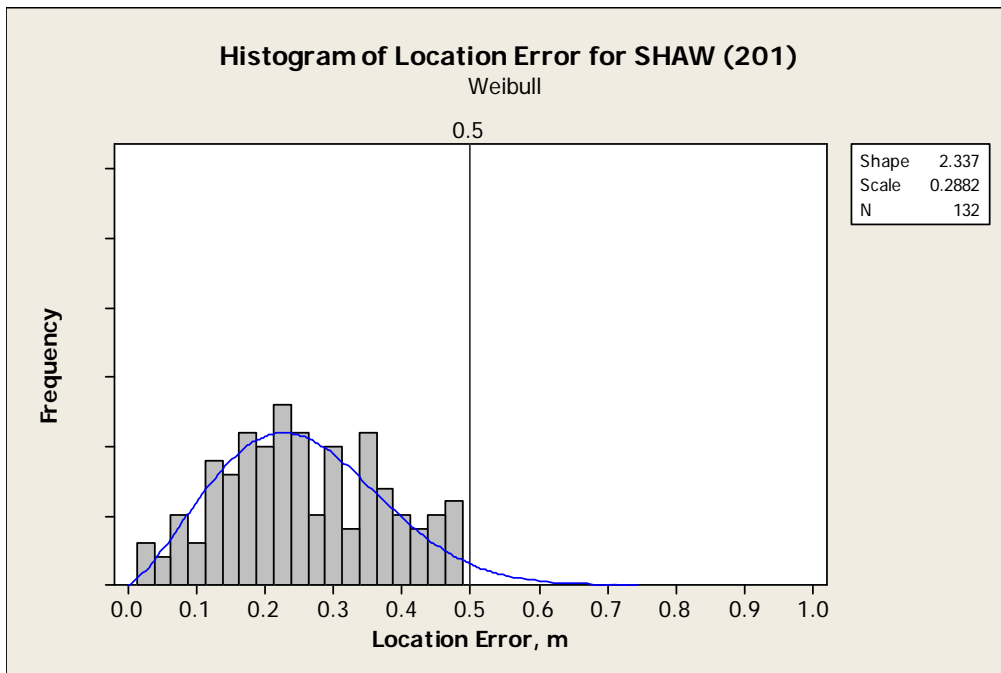


Figure E-6. Location Error Histogram for Shaw, SR #201.

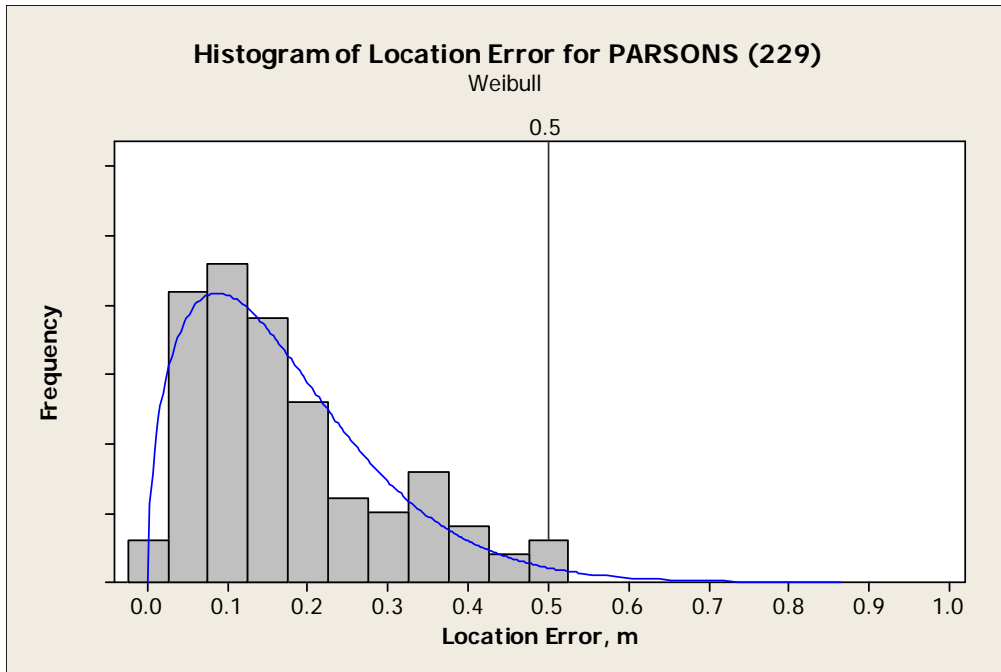


Figure E-7. Location Error Histogram for Parsons, SR #229.

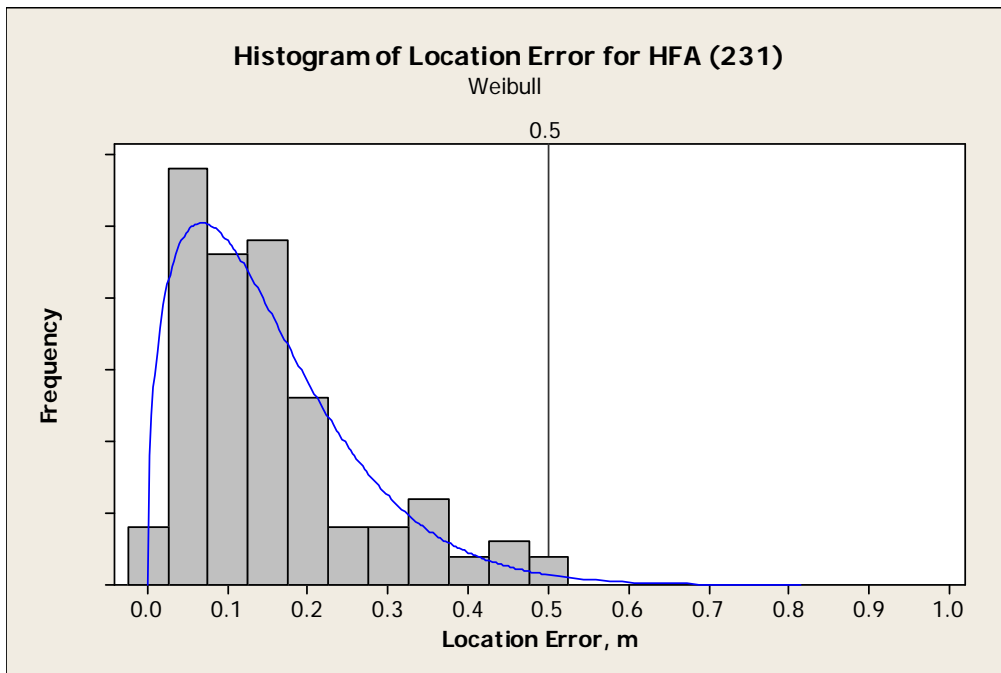


Figure E-8. Location Error Histogram for HFA, SR #231.

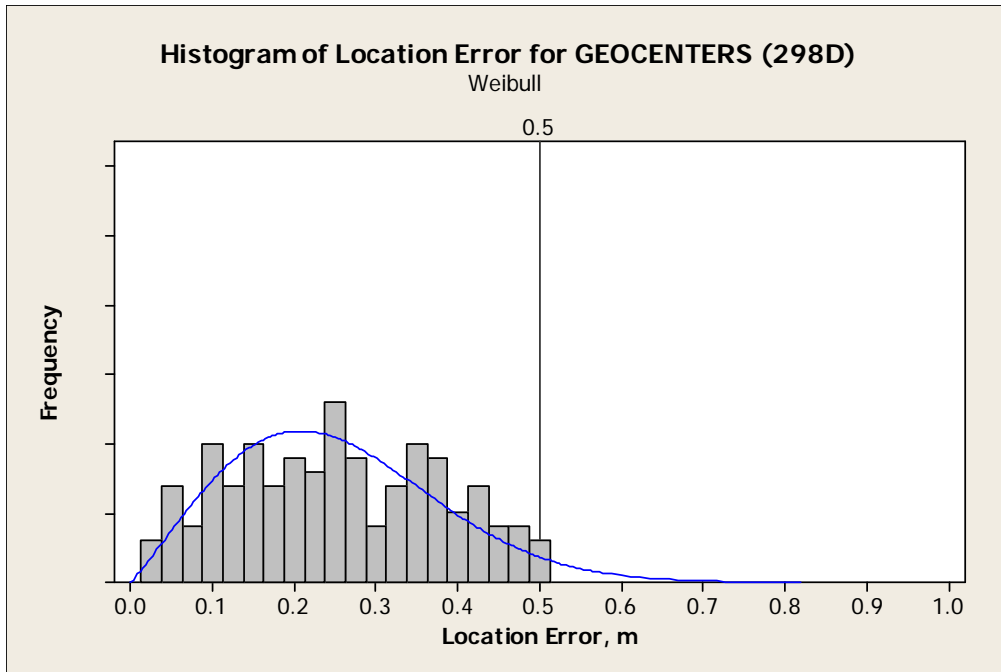


Figure E-9. Location Error Histogram for Geocenters, SR #298.

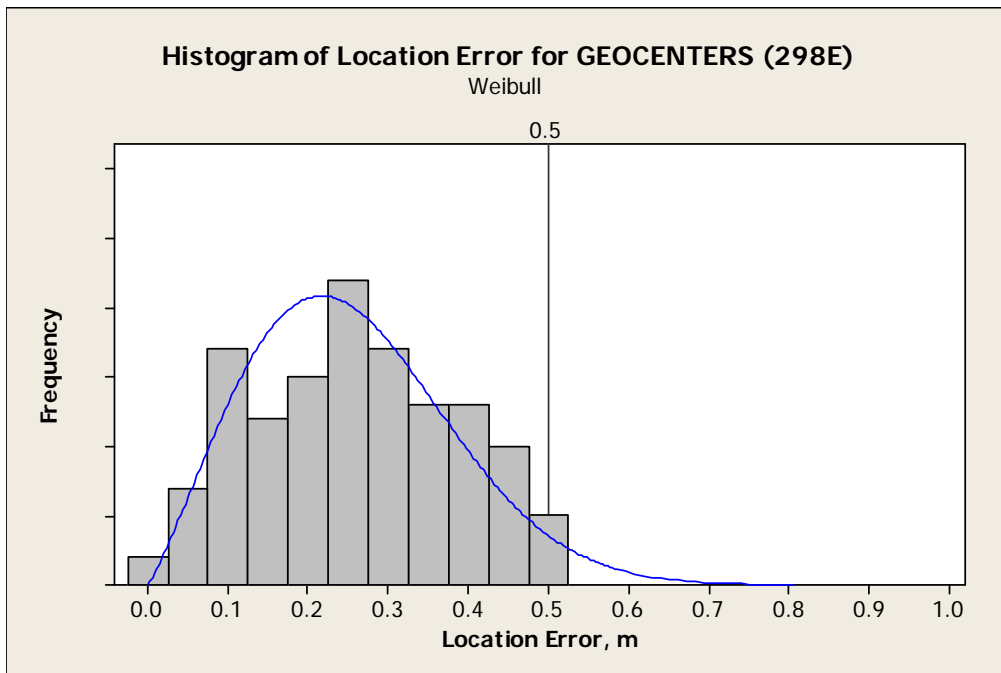


Figure E-10. Location Error Histogram for Geocenters, SR #298.

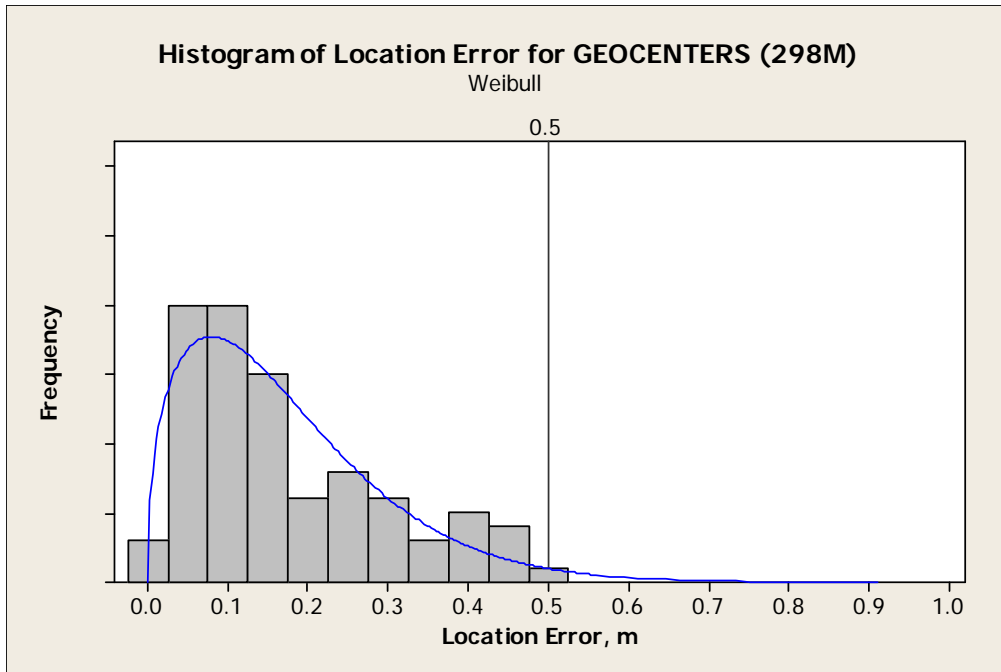


Figure E-11. Location Error Histogram for Geocenters, SR #298.

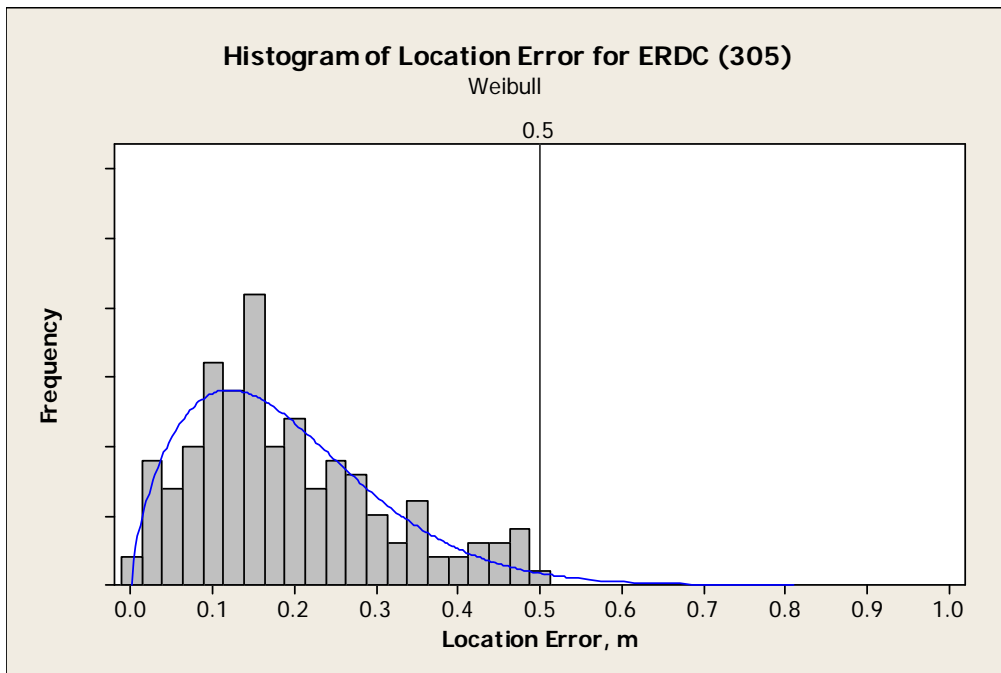


Figure E-12. Location Error Histogram for ERDC, SR #305.

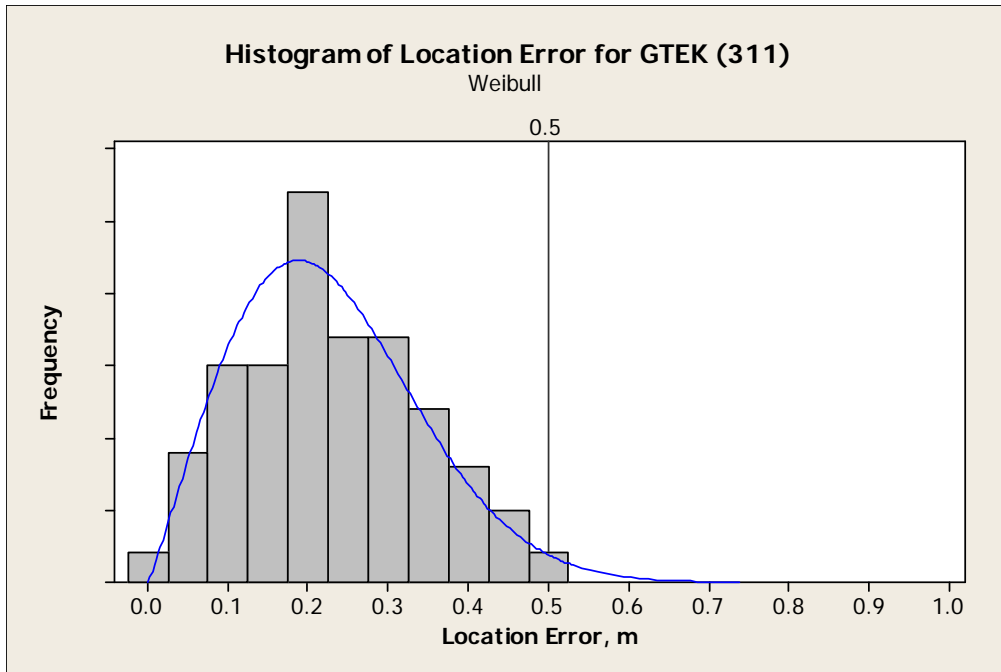


Figure E-13. Location Error Histogram for G-TEK SR #311.

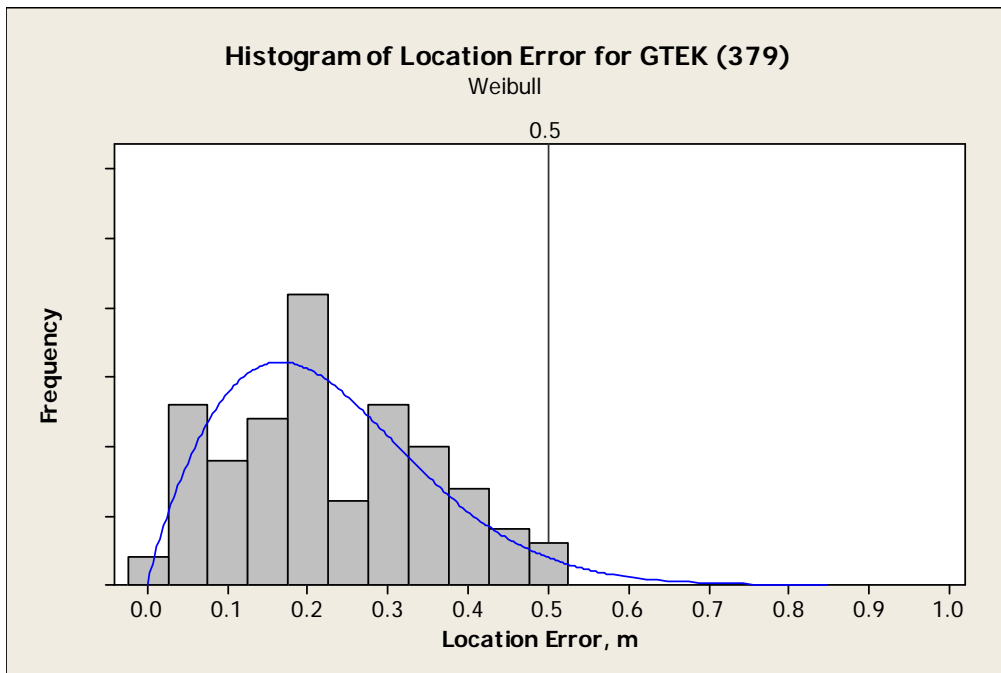


Figure E-14. Location Error Histogram for G-TEK, SR #379.

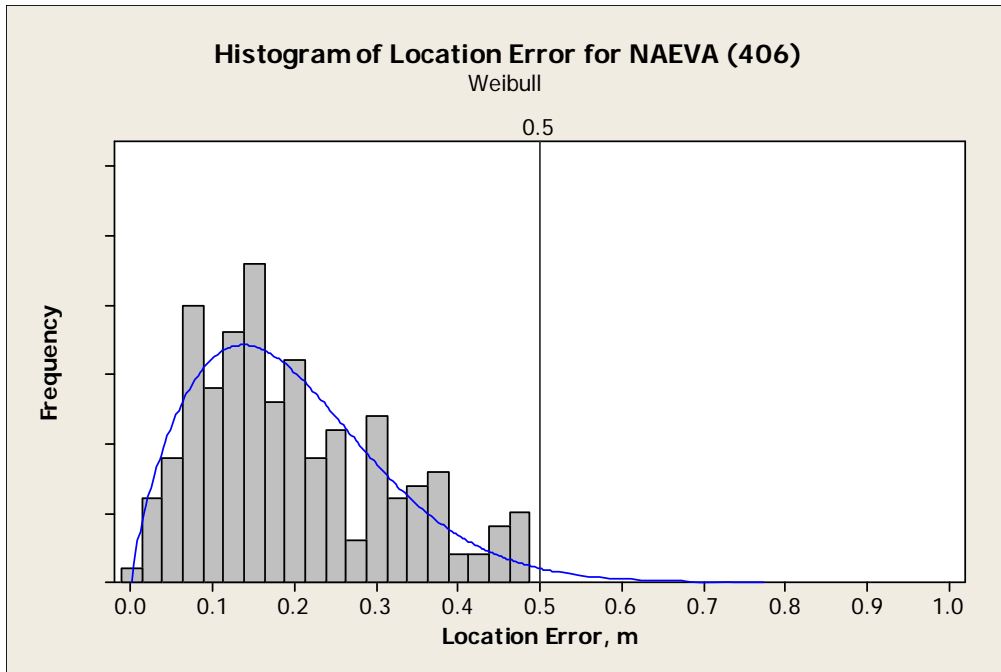


Figure E-15. Location Error Histogram for NAEVA, SR #406.

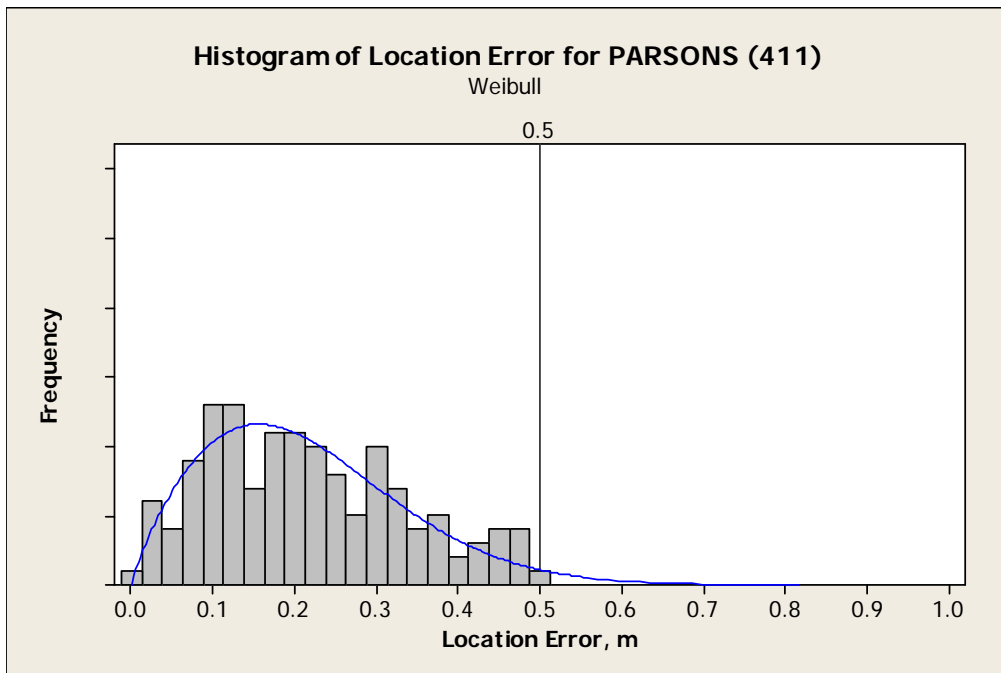


Figure E-16. Location Error Histogram for Parsons, SR #411.

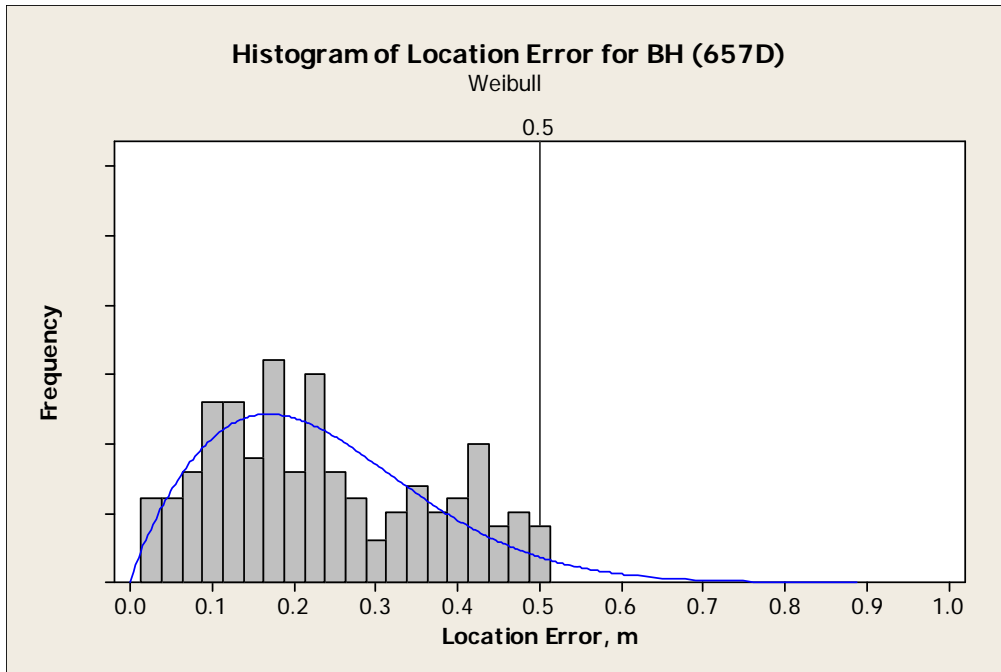


Figure E-17. Location Error Histogram for BH, SR #657.

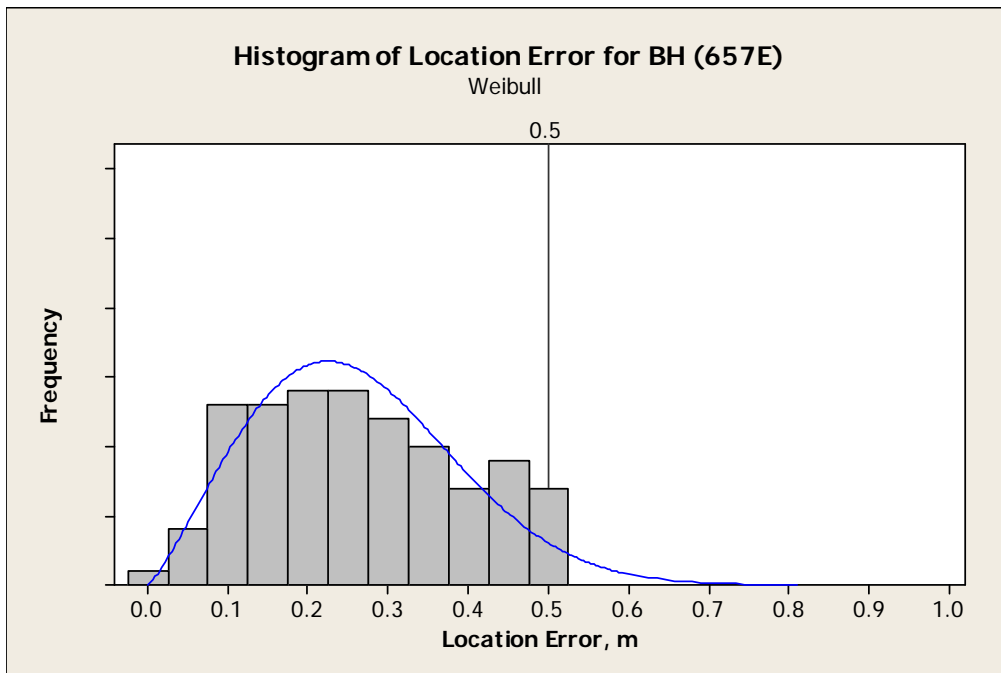


Figure E-18. Location Error Histogram for BH, SR #657.

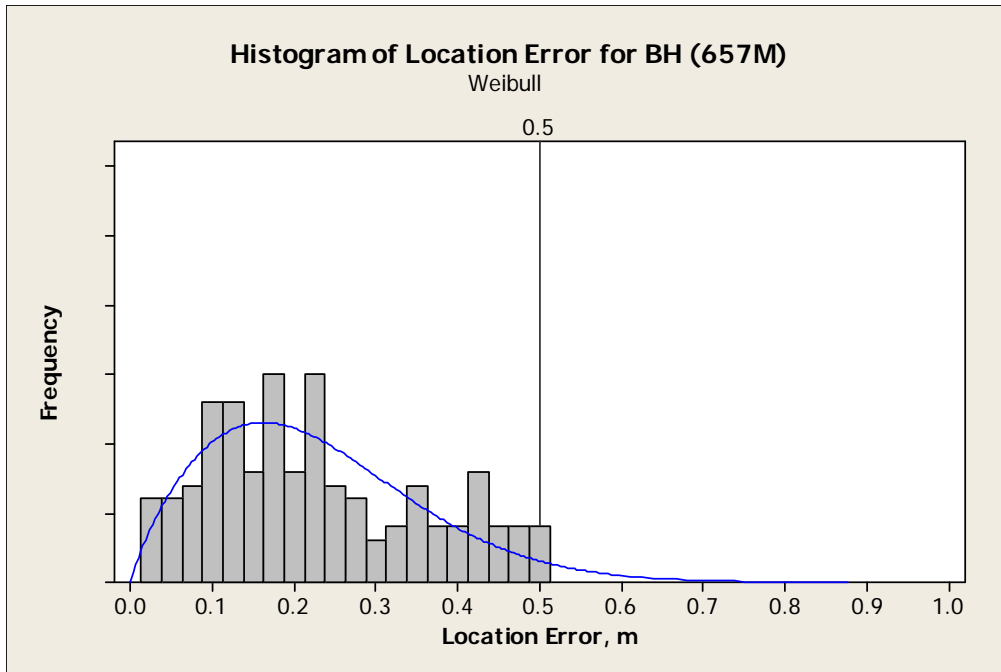


Figure E-19. Location Error Histogram for BH, SR #657.

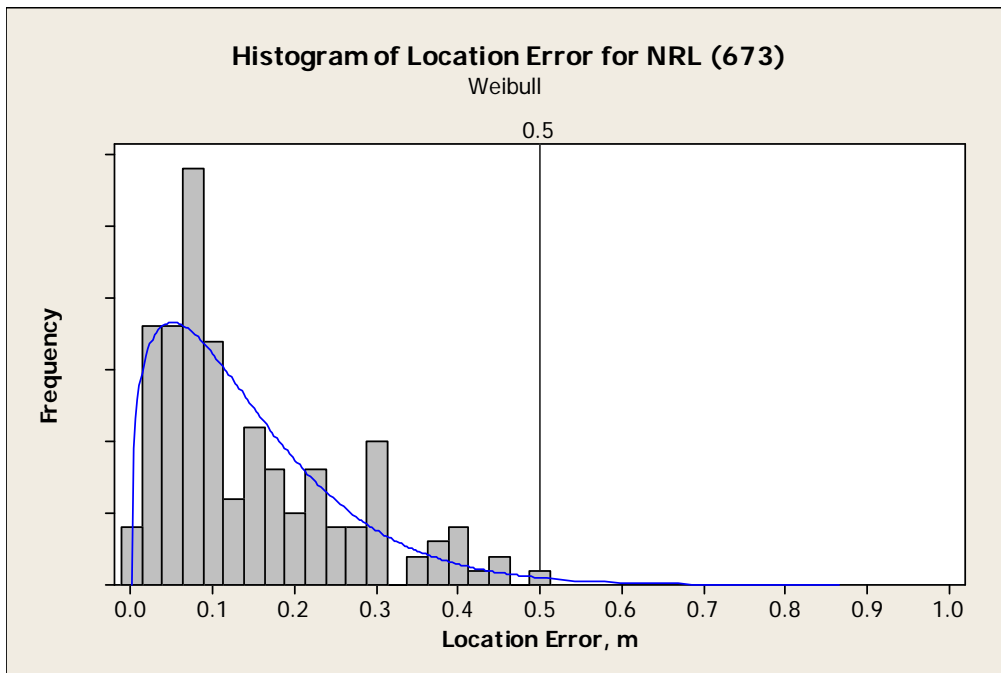


Figure E-20. Location Error Histogram for NRL, SR #673.

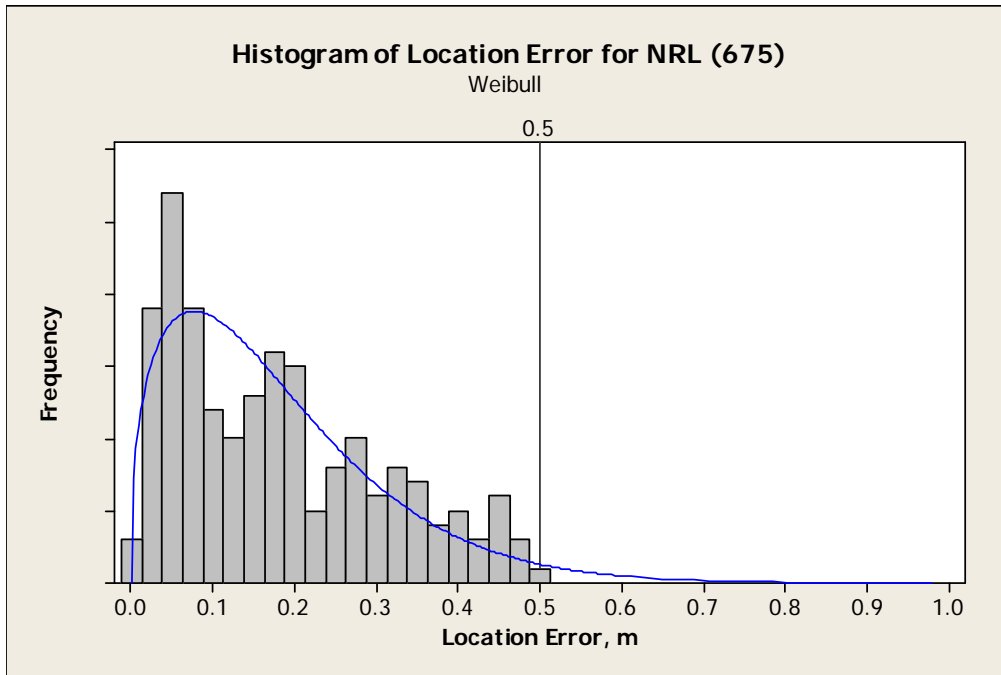


Figure E-21. Location Error Histogram for NRL, SR #675.

APPENDIX F. ESTIMATED CUMULATIVE PROBABILITY OF LOCATION ERROR

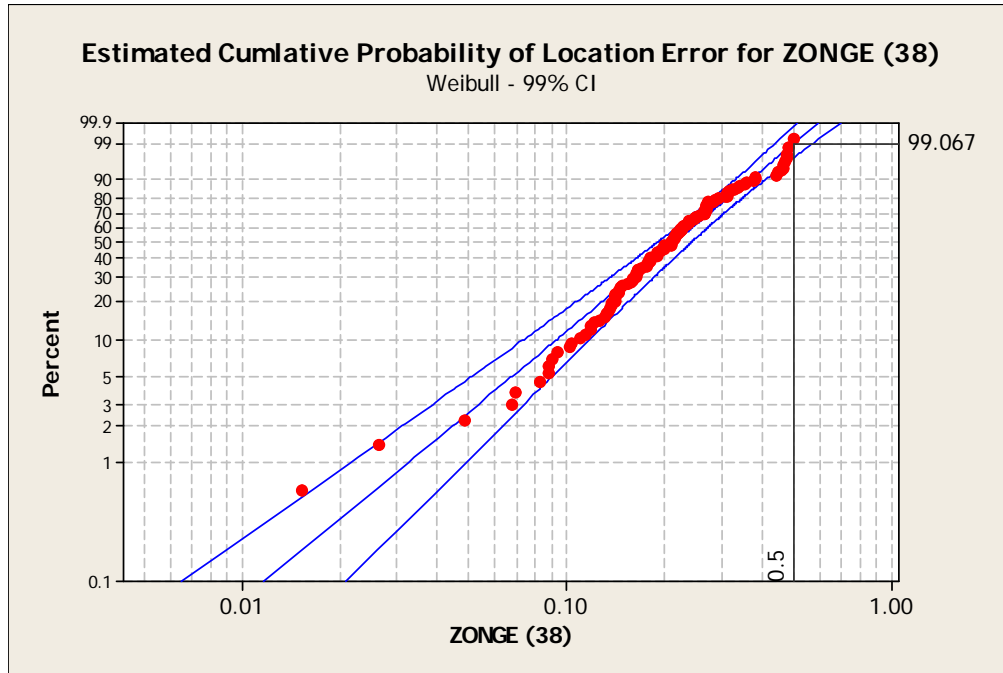


Figure F-1. Estimated Cumulative Probability of Location Error, Zonge, SR #38.

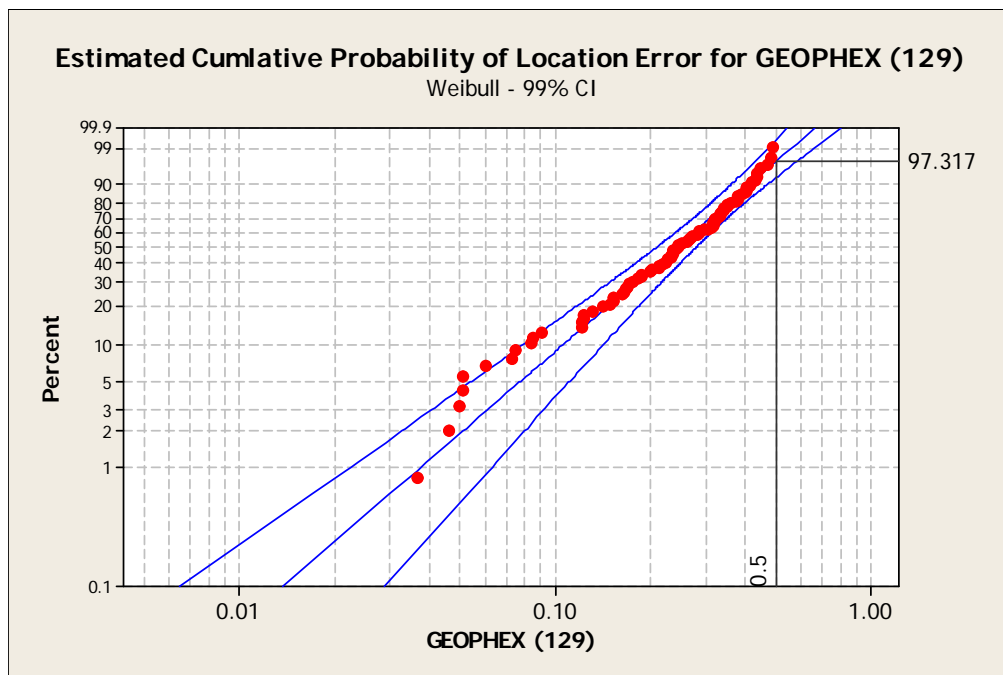


Figure F-2. Estimated Cumulative Probability of Location Error, Geophex, SR #129.

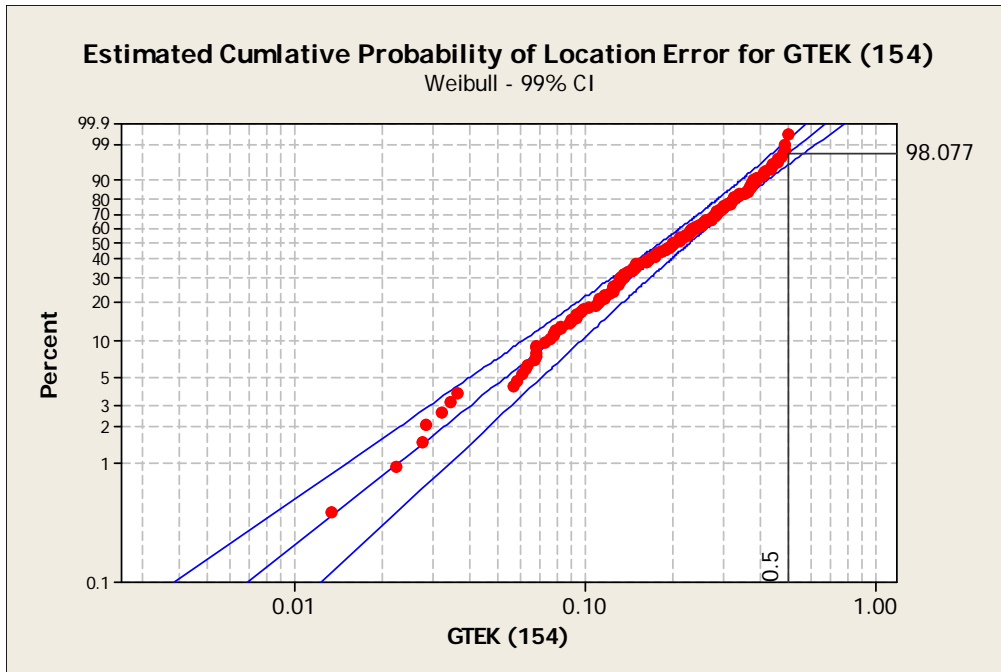


Figure F-3. Estimated Cumulative Probability of Location Error, G-TEK, SR #154.

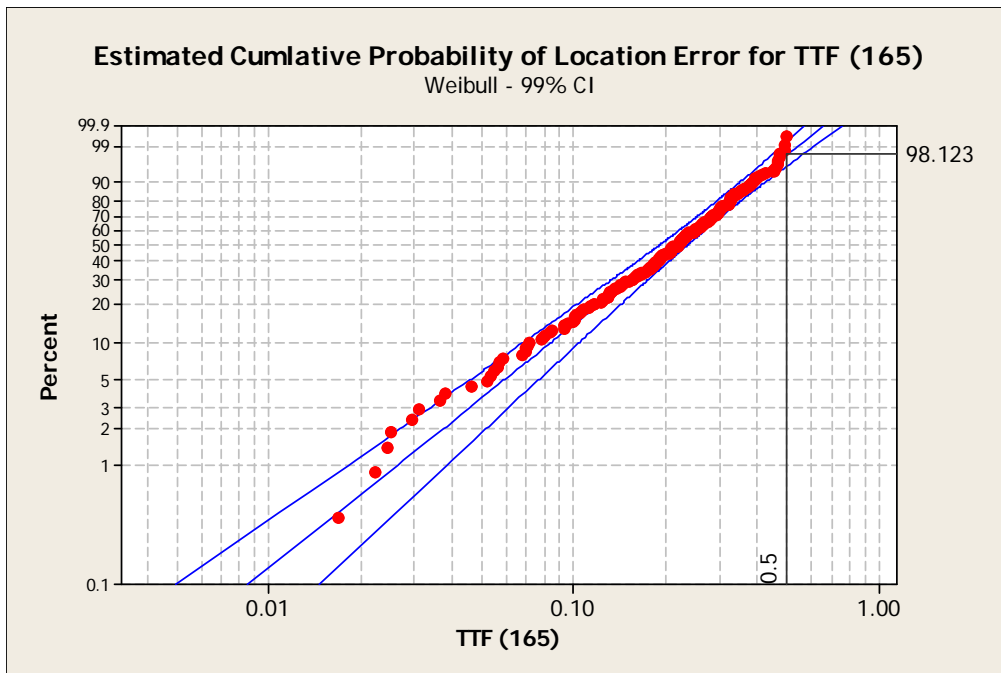


Figure F-4. Estimated Cumulative Probability of Location Error, TTF, SR #165.

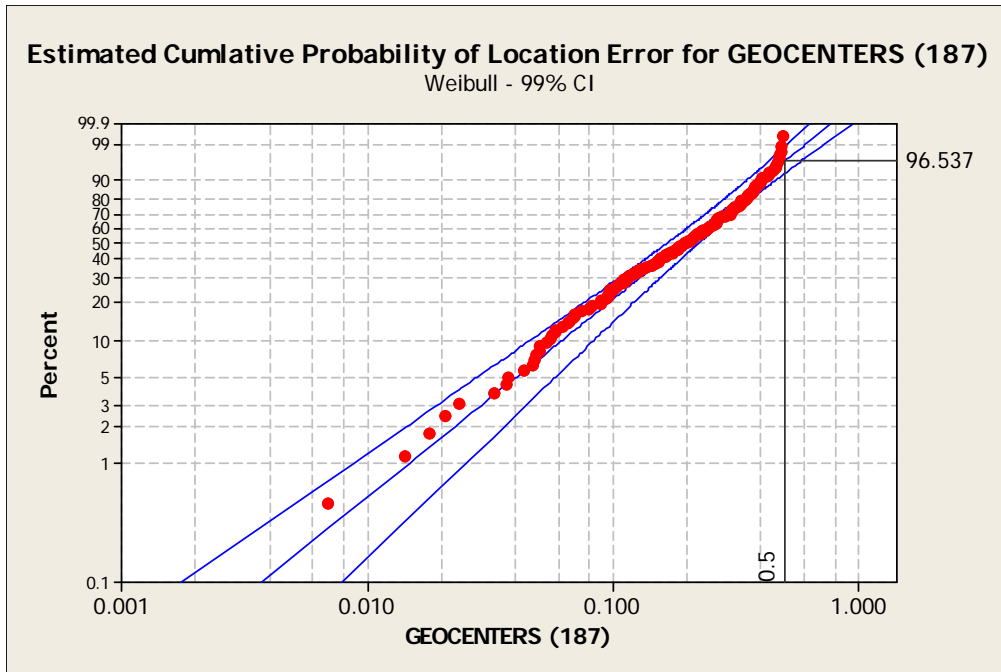


Figure F-5. Estimated Cumulative Probability of Location Error, Geocenters, SR #187.

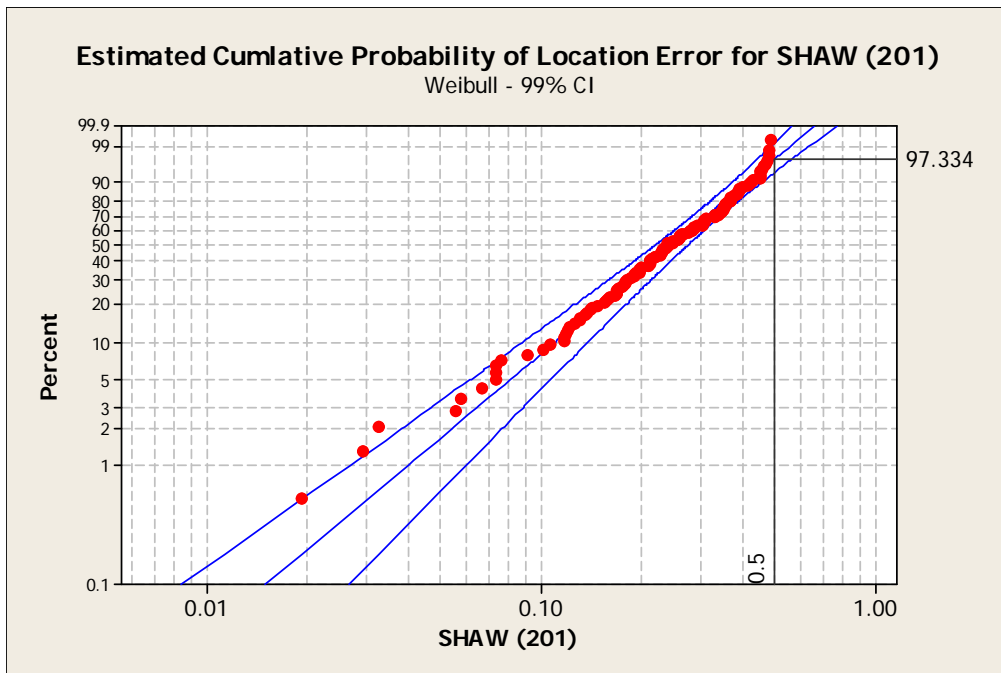


Figure F-6. Estimated Cumulative Probability of Location Error, Shaw, SR #201.

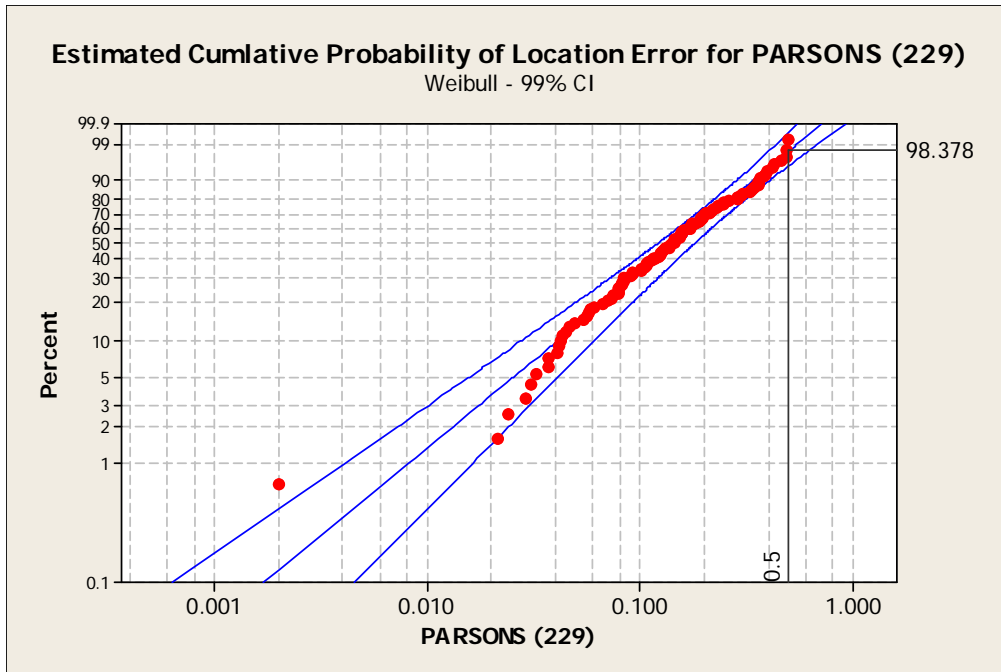


Figure F-7. Estimated Cumulative Probability of Location Error, Parsons, SR #229.

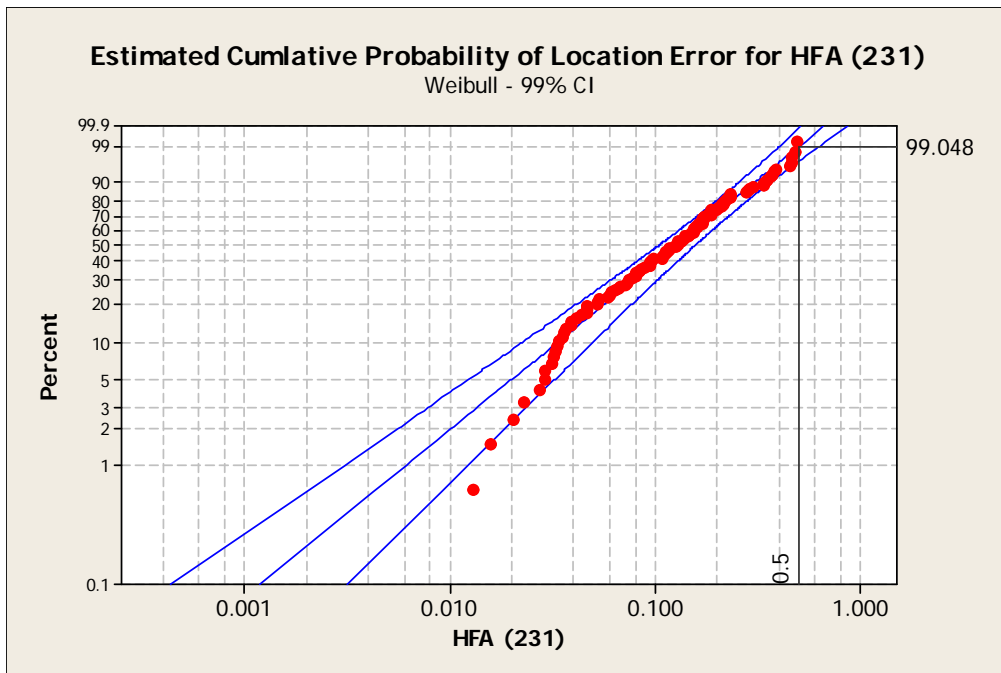


Figure F-8. Estimated Cumulative Probability of Location Error, HFA, SR #231.

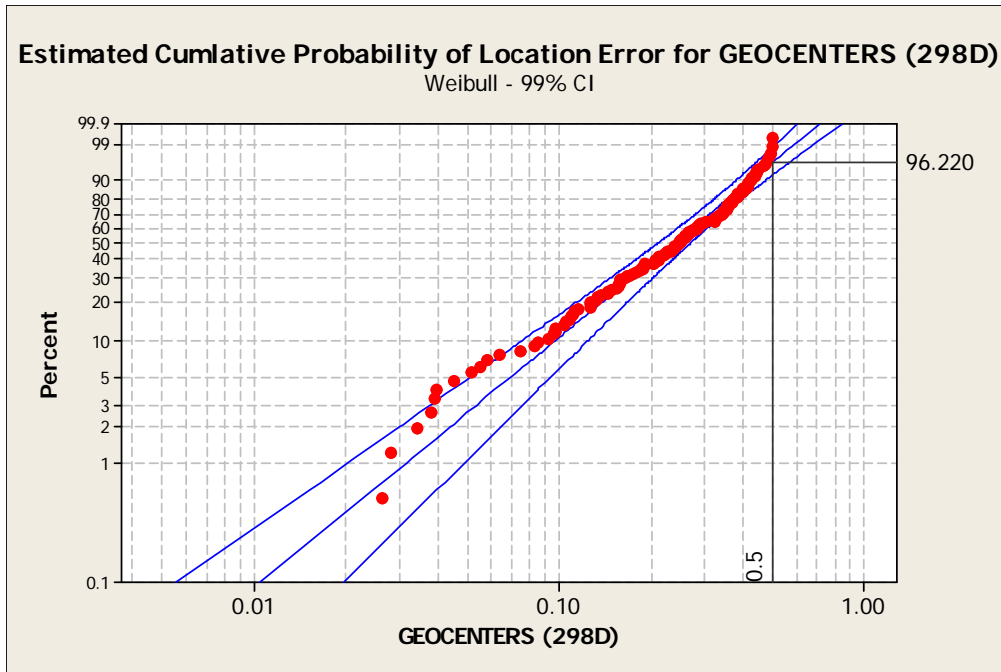


Figure F-9. Estimated Cumulative Probability of Location Error, Geocenters, SR #298.

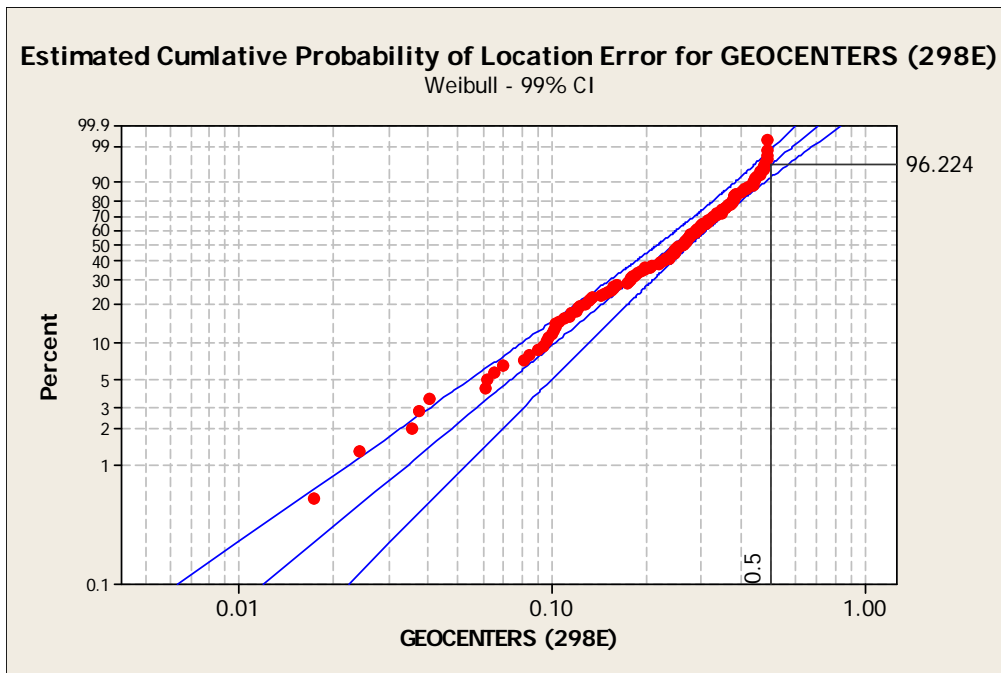


Figure F-10. Estimated Cumulative Probability of Location Error, Geocenters, SR #298.

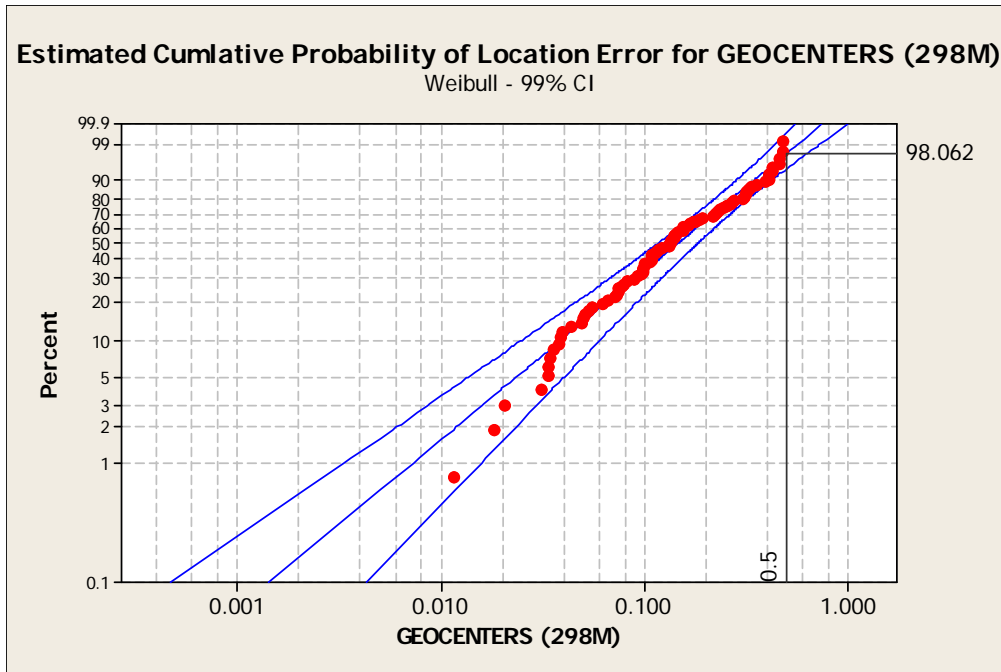


Figure F-11. Estimated Cumulative Probability of Location Error, Geocenters, SR #298.

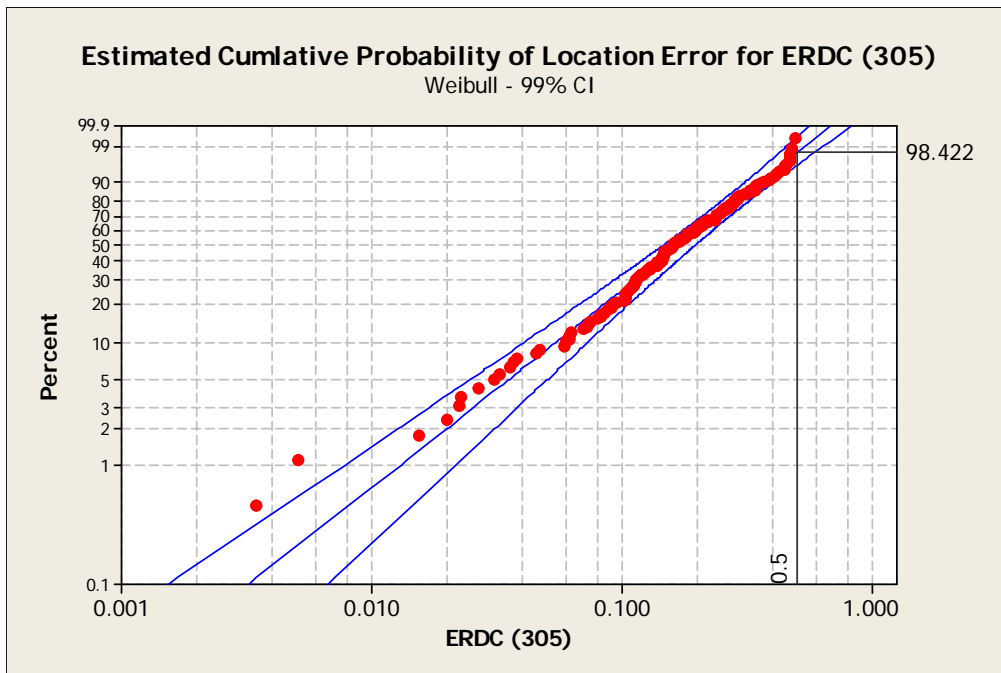


Figure F-12. Estimated Cumulative Probability of Location Error, ERDC, SR #305.

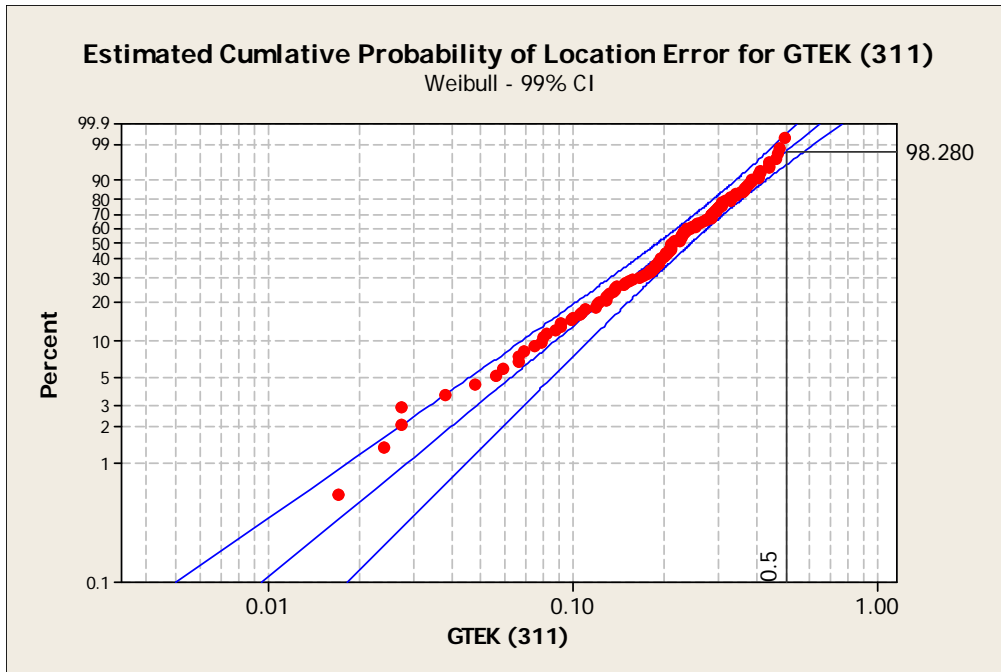


Figure F-13. Estimated Cumulative Probability of Location Error, G-TEK, SR #311.

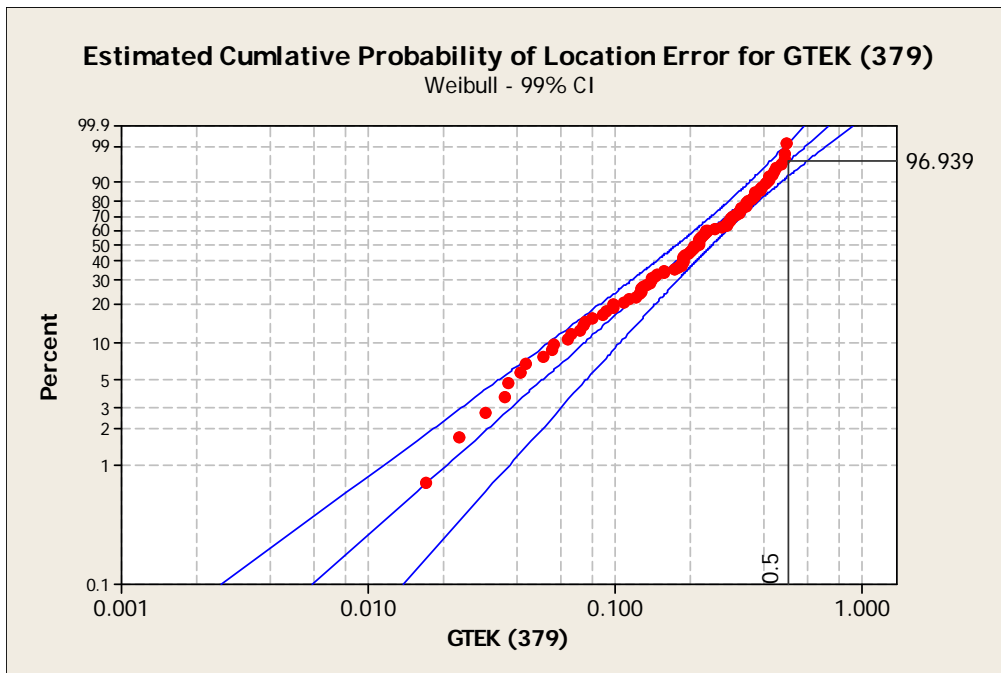


Figure F-14. Estimated Cumulative Probability of Location Error, G-TEK, SR #379.

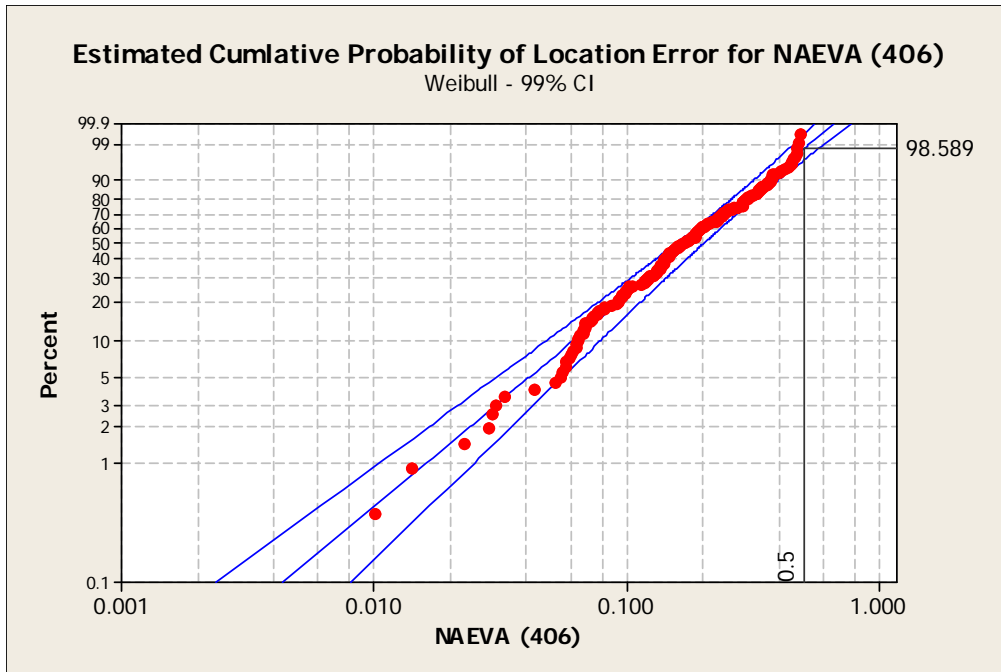


Figure F-15. Estimated Cumulative Probability of Location Error, NAEVA SR #406.

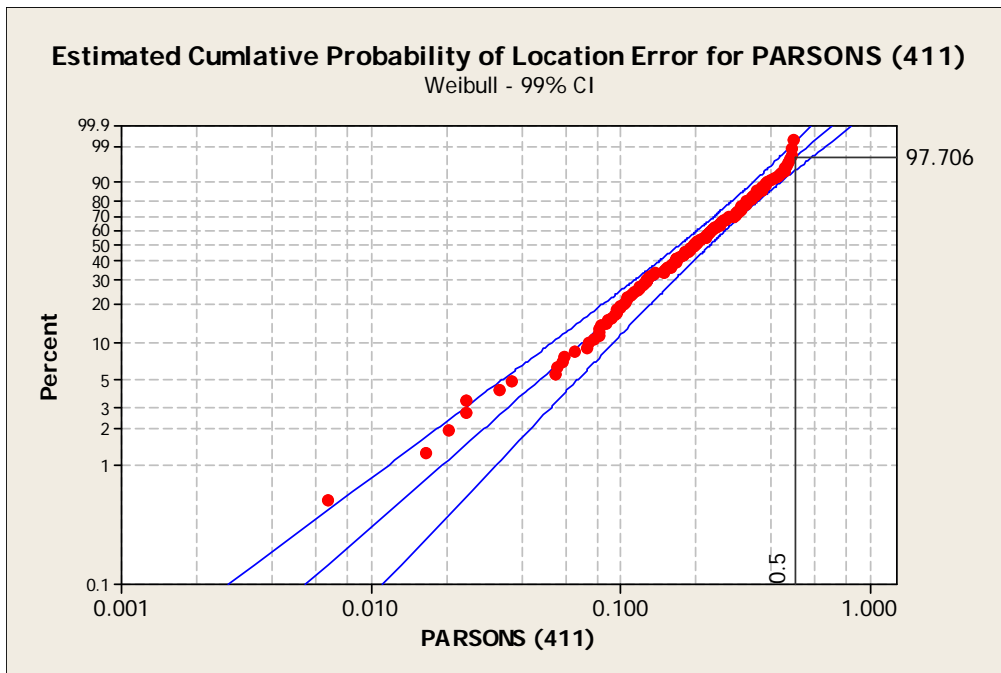


Figure F-16. Estimated Cumulative Probability of Location Error, Parsons, SR #411.

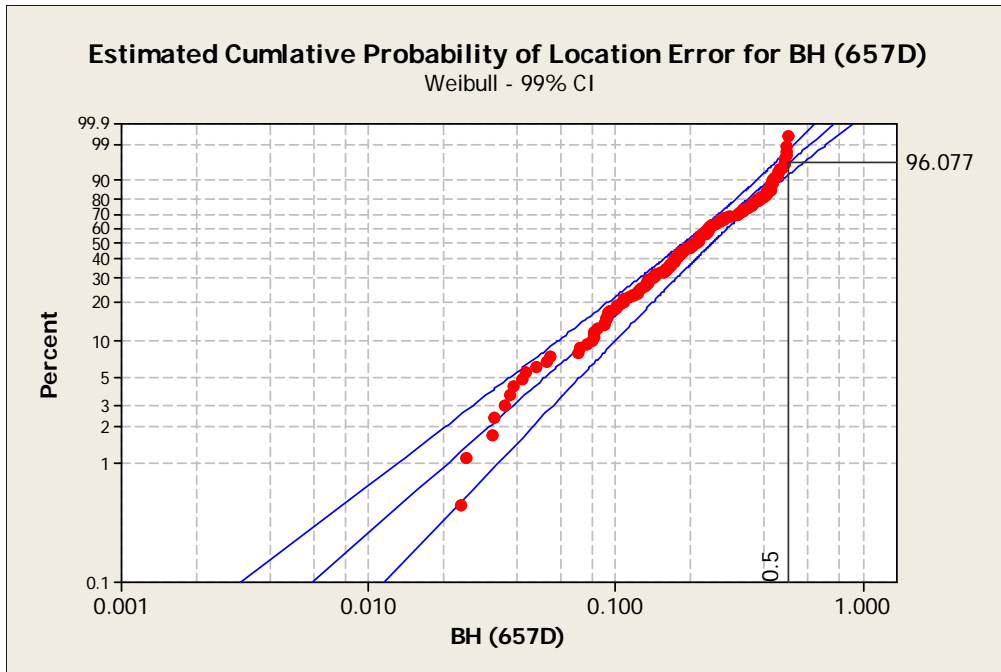


Figure F-17. Estimated Cumulative Probability of Location Error, BH, SR #657.

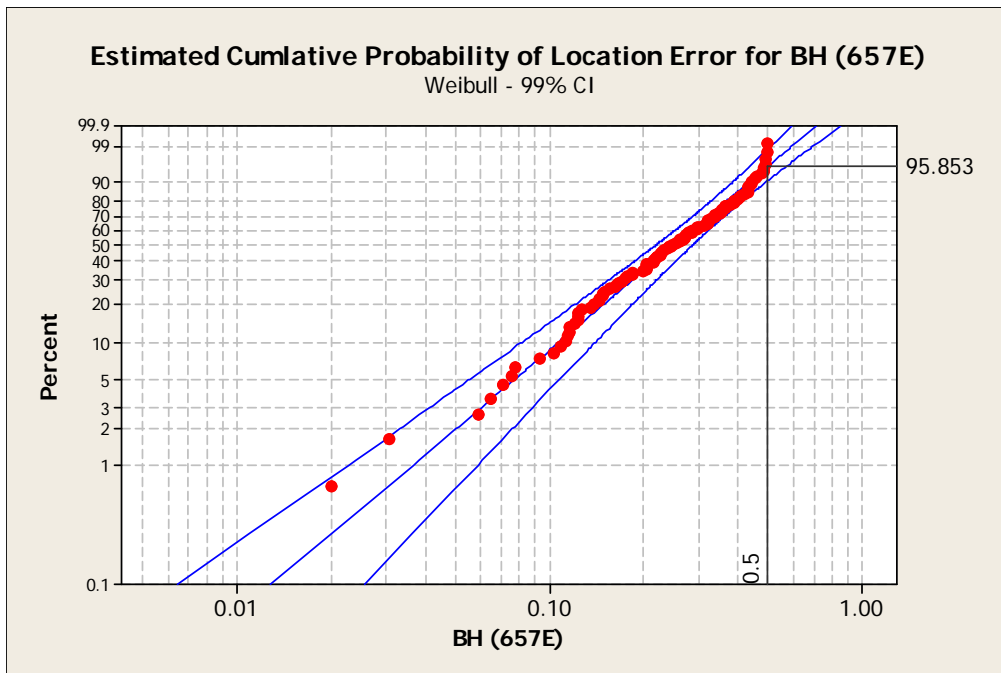


Figure F-18. Estimated Cumulative Probability of Location Error, BH, SR #657.

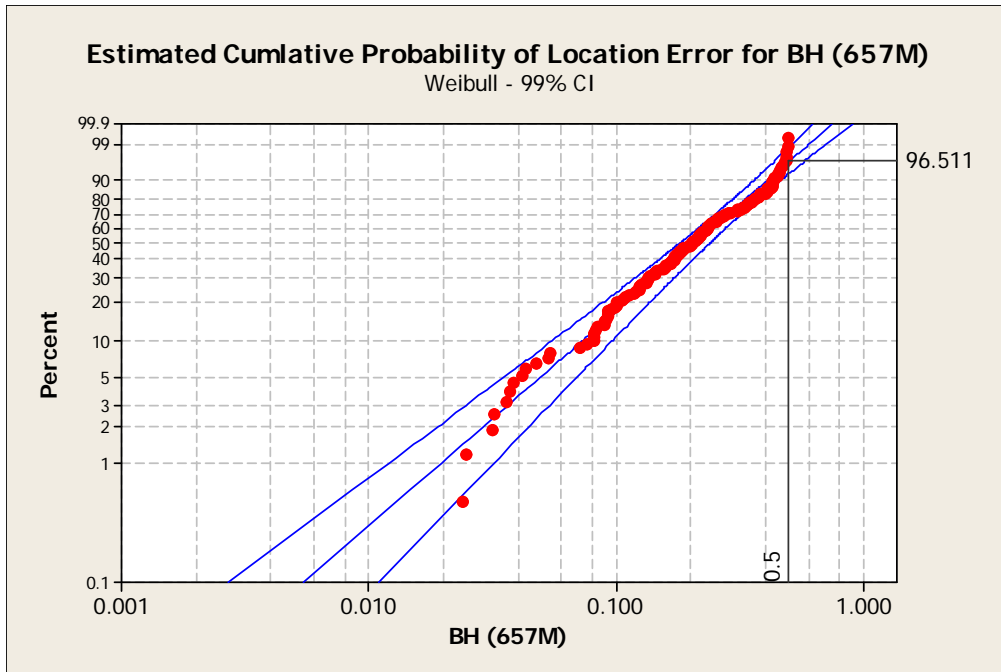


Figure F-19. Estimated Cumulative Probability of Location Error, BH, SR #657.

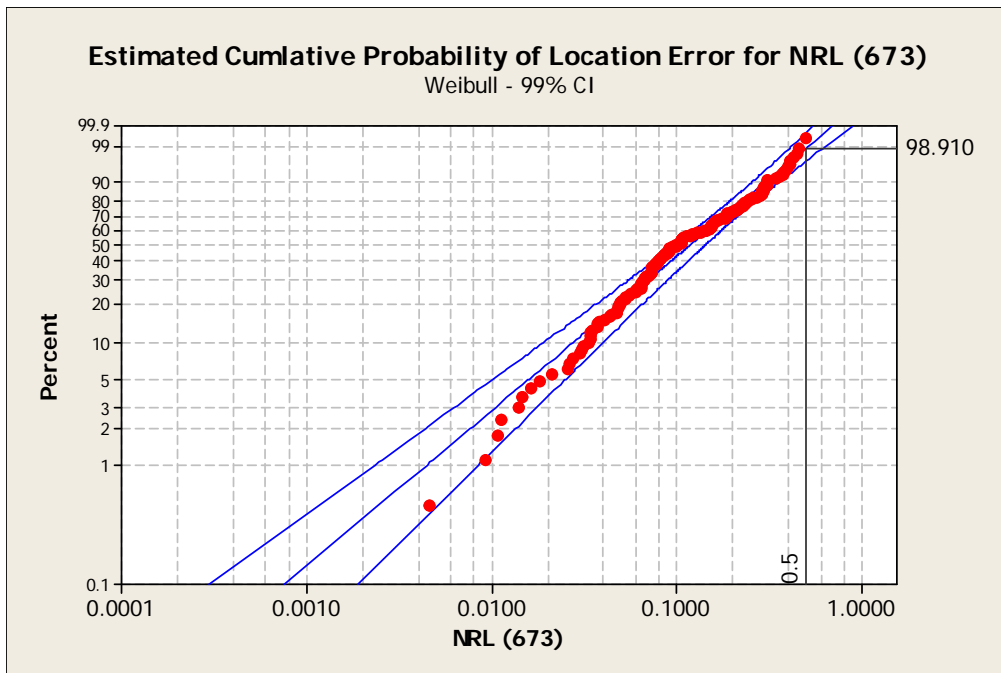


Figure F-20. Estimated Cumulative Probability of Location Error, NRL, SR #673.

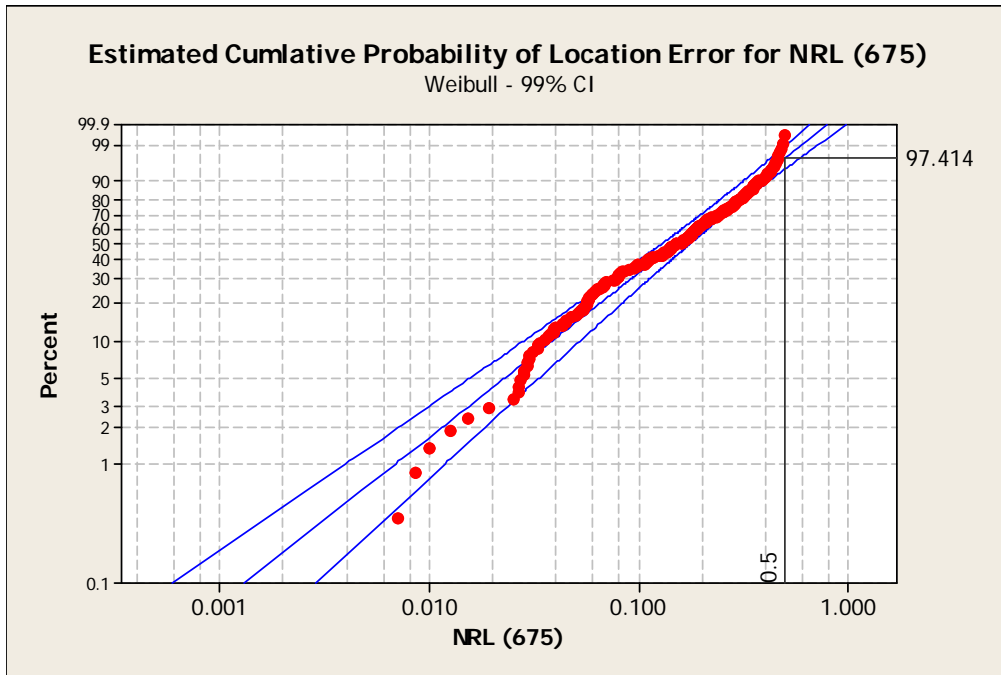


Figure F-21. Estimated Cumulative Probability of Location Error, NRL, SR #675.

APPENDIX G. P_d RESULTS PER ORDNANCE TYPE

Note: The GT has been limited to 11D depth. Challenge area and/or overlapping items have been excluded. Results have been rounded to the nearest 0.05 increment of P_d.

| 105H Ordnance | | | |
|--|--------------|-----------------------|--------------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| 105H Ordnance | | | |
| APG | | YPG | |
| System | Pdres | System | Pdres |
| EM61/Cart(411) | 0.95 | EM63/Cart(249) | 1.00 |
| EM61/Cart(201) | 0.95 | MTADS/Towed(245) | 1.00 |
| EM61/Cart(165) | 0.95 | EM61G822A/Towed(651M) | 1.00 |
| MTADS/Towed(675) | 0.95 | TM4/Sling(147) | 1.00 |
| SAM/Sling(379) | 0.95 | EM61G822A/Towed(651D) | 1.00 |
| STOLS/Towed(298E) | 0.85 | EM61/Towed(668) | 0.95 |
| TM5/Sling(154) | 0.85 | EM61/Cart(425) | 0.95 |
| EM61G822A/Cart(657M) | 0.85 | GEM3/Cart(135) | 0.95 |
| MTADS/Towed(673) | 0.85 | STOLS/Towed(299E) | 0.95 |
| EM61G822A/Cart(657D) | 0.85 | TM5/Sling(148) | 0.95 |
| STOLS/Towed(187) | 0.85 | SCH/Hand(426) | 0.95 |
| STOLS/Towed(298D) | 0.85 | STOLS/Towed(299D) | 0.95 |
| EM61/Towed(406) | 0.80 | EM61/Cart(169) | 0.90 |
| SCH/Hand(229) | 0.80 | EM61G822A/Towed(651E) | 0.85 |
| STOLS/Towed(298M) | 0.80 | STOLS/Towed(299M) | 0.85 |
| TM4/Sling(311) | 0.75 | TM4/Sling(364) | 0.85 |
| EM61G822A/Cart(657E) | 0.65 | SCH/Hand(442) | 0.70 |
| EM63/Cart(305) | 0.65 | EM61/Cart(354) | 0.50 |
| EMFAST4D/Cart(38) | 0.65 | MAG858/Cart(638) | 0.10 |
| SCH/Hand(231) | 0.60 | | |
| GEM3/Towed(129) | 0.45 | | |
| MAG858/Cart(492) | 0.45 | | |

Figure G-1. 105H Ordnance.

| 105mmP Ordnance | | | |
|--|--------------|-----------------------|--------------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| 105mmP Ordnance | | | |
| APG | | YPG | |
| System | Pdres | System | Pdres |
| MTADS/Towed(675) | 1.00 | EM61/Towed(668) | 1.00 |
| TM5/Sling(154) | 1.00 | EM61/Cart(169) | 1.00 |
| MTADS/Towed(673) | 1.00 | EM63/Cart(249) | 1.00 |
| EM61/Towed(406) | 0.90 | MTADS/Towed(245) | 1.00 |
| EM61/Cart(411) | 0.90 | STOLS/Towed(299E) | 1.00 |
| EM61/Cart(165) | 0.90 | EM61G822A/Towed(651M) | 1.00 |
| STOLS/Towed(298M) | 0.90 | STOLS/Towed(299M) | 1.00 |
| EM61/Cart(201) | 0.85 | EM61G822A/Towed(651D) | 1.00 |
| EM61G822A/Cart(657E) | 0.85 | STOLS/Towed(299D) | 1.00 |
| EM63/Cart(305) | 0.85 | TM5/Sling(148) | 0.95 |
| EMFAST4D/Cart(38) | 0.85 | EM61/Cart(425) | 0.90 |
| GEM3/Towed(129) | 0.85 | GEM3/Cart(135) | 0.85 |
| STOLS/Towed(298E) | 0.85 | TM4/Sling(364) | 0.85 |
| EM61G822A/Cart(657M) | 0.85 | TM4/Sling(147) | 0.85 |
| SCH/Hand(231) | 0.85 | SCH/Hand(426) | 0.75 |
| SCH/Hand(229) | 0.85 | EM61G822A/Towed(651E) | 0.70 |
| TM4/Sling(311) | 0.85 | SCH/Hand(442) | 0.70 |
| EM61G822A/Cart(657D) | 0.85 | EM61/Cart(354) | 0.40 |
| STOLS/Towed(187) | 0.85 | MAG858/Cart(638) | 0.05 |
| STOLS/Towed(298D) | 0.85 | | |
| SAM/Sling(379) | 0.65 | | |
| MAG858/Cart(492) | 0.35 | | |

Figure G-2. 105mmP Ordnance.

| 155mmP Ordnance | | | |
|---|-------|-----------------------|-------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| System | Pdres | System | Pdres |
| MTADS/Towed(673) | 1.00 | EM61G822A/Towed(651D) | 1.00 |
| EM61/Cart(165) | 0.95 | EM61/Towed(668) | 0.95 |
| STOLS/Towed(187) | 0.95 | EM63/Cart(249) | 0.95 |
| MTADS/Towed(675) | 0.90 | MTADS/Towed(245) | 0.95 |
| EM61/Towed(406) | 0.85 | TM5/Sling(148) | 0.95 |
| TM5/Sling(154) | 0.85 | EM61G822A/Towed(651M) | 0.95 |
| TM4/Sling(311) | 0.85 | EM61/Cart(425) | 0.90 |
| EM61/Cart(411) | 0.80 | EM61/Cart(169) | 0.90 |
| EM61/Cart(201) | 0.80 | STOLS/Towed(299E) | 0.90 |
| EM61G822A/Cart(657M) | 0.80 | STOLS/Towed(299M) | 0.90 |
| STOLS/Towed(298M) | 0.80 | TM4/Sling(147) | 0.90 |
| EM61G822A/Cart(657D) | 0.80 | STOLS/Towed(299D) | 0.90 |
| SCH/Hand(229) | 0.70 | SCH/Hand(426) | 0.80 |
| SCH/Hand(231) | 0.65 | EM61G822A/Towed(651E) | 0.75 |
| EM63/Cart(305) | 0.60 | GEM3/Cart(135) | 0.75 |
| STOLS/Towed(298E) | 0.60 | SCH/Hand(442) | 0.70 |
| SAM/Sling(379) | 0.60 | TM4/Sling(364) | 0.70 |
| STOLS/Towed(298D) | 0.60 | EM61/Cart(354) | 0.40 |
| EM61G822A/Cart(657E) | 0.55 | MAG858/Cart(638) | 0.05 |
| EMFAST4D/Cart(38) | 0.55 | | |
| GEM3/Towed(129) | 0.50 | | |
| MAG858/Cart(492) | 0.40 | | |

Figure G-3. 155mmP Ordnance.

| 2.75 inch Rocket Ordnance | | | |
|---|-------|-----------------------|-------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| System | Pdres | System | Pdres |
| STOLS/Towed(187) | 0.95 | STOLS/Towed(299E) | 0.95 |
| MTADS/Towed(675) | 0.90 | STOLS/Towed(299D) | 0.95 |
| MTADS/Towed(673) | 0.90 | EM61/Cart(169) | 0.90 |
| SCH/Hand(231) | 0.90 | EM63/Cart(249) | 0.90 |
| SCH/Hand(229) | 0.90 | MTADS/Towed(245) | 0.90 |
| EM61/Cart(411) | 0.85 | TM5/Sling(148) | 0.90 |
| EM63/Cart(305) | 0.85 | TM4/Sling(147) | 0.90 |
| EMFAST4D/Cart(38) | 0.85 | GEM3/Cart(135) | 0.80 |
| TM5/Sling(154) | 0.85 | SCH/Hand(426) | 0.80 |
| EM61G822A/Cart(657M) | 0.85 | STOLS/Towed(299M) | 0.80 |
| STOLS/Towed(298M) | 0.85 | EM61G822A/Towed(651D) | 0.80 |
| EM61G822A/Cart(657D) | 0.85 | EM61G822A/Towed(651M) | 0.75 |
| EM61/Cart(165) | 0.75 | EM61/Towed(668) | 0.70 |
| TM4/Sling(311) | 0.75 | EM61/Cart(425) | 0.70 |
| SAM/Sling(379) | 0.75 | SCH/Hand(442) | 0.70 |
| EM61/Towed(406) | 0.65 | TM4/Sling(364) | 0.55 |
| EM61/Cart(201) | 0.65 | EM61G822A/Towed(651E) | 0.50 |
| STOLS/Towed(298E) | 0.60 | EM61/Cart(354) | 0.25 |
| STOLS/Towed(298D) | 0.60 | MAG858/Cart(638) | 0.10 |
| EM61G822A/Cart(657E) | 0.55 | | |
| GEM3/Towed(129) | 0.55 | | |
| MAG858/Cart(492) | 0.25 | | |

Figure G-4. 2.75 inch Rocket Ordnance.

| 20mmP Ordnance | | | |
|---|-------|-----------------------|-------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| System | Pdres | System | Pdres |
| EM61/Towed(406) | 0.70 | EM61/Towed(668) | 0.90 |
| EM61/Cart(165) | 0.70 | MTADS/Towed(245) | 0.90 |
| MTADS/Towed(675) | 0.70 | EM61/Cart(169) | 0.85 |
| TM5/Sling(154) | 0.50 | TM5/Sling(148) | 0.85 |
| MTADS/Towed(673) | 0.40 | EM61G822A/Towed(651D) | 0.80 |
| SCH/Hand(231) | 0.40 | EM63/Cart(249) | 0.75 |
| SCH/Hand(229) | 0.35 | EM61G822A/Towed(651M) | 0.70 |
| EM61/Cart(201) | 0.30 | EM61/Cart(425) | 0.50 |
| EM63/Cart(305) | 0.30 | TM4/Sling(147) | 0.45 |
| EMFAST4D/Cart(38) | 0.25 | STOLS/Towed(299E) | 0.40 |
| GEM3/Towed(129) | 0.25 | STOLS/Towed(299D) | 0.40 |
| STOLS/Towed(298E) | 0.25 | EM61G822A/Towed(651E) | 0.35 |
| TM4/Sling(311) | 0.25 | SCH/Hand(442) | 0.30 |
| STOLS/Towed(298D) | 0.25 | SCH/Hand(426) | 0.30 |
| EM61/Cart(411) | 0.20 | EM61/Cart(354) | 0.10 |
| EM61G822A/Cart(657M) | 0.20 | GEM3/Cart(135) | 0.05 |
| EM61G822A/Cart(657D) | 0.20 | MAG858/Cart(638) | 0.05 |
| EM61G822A/Cart(657E) | 0.15 | STOLS/Towed(299M) | 0.00 |
| STOLS/Towed(187) | 0.15 | TM4/Sling(364) | 0.00 |
| MAG858/Cart(492) | 0.10 | | |
| STOLS/Towed(298M) | 0.00 | | |
| SAM/Sling(379) | 0.00 | | |

Figure G-5. 20mmP Ordnance.

| 40mmG Ordnance | | | |
|---|-------|-----------------------|-------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| System | Pdres | System | Pdres |
| TM5/Sling(154) | 0.90 | EM61/Towed(668) | 0.95 |
| EM61/Cart(165) | 0.80 | EM61/Cart(169) | 0.95 |
| EM61/Towed(406) | 0.75 | EM63/Cart(249) | 0.95 |
| EM63/Cart(305) | 0.70 | MTADS/Towed(245) | 0.95 |
| MTADS/Towed(675) | 0.70 | TM5/Sling(148) | 0.95 |
| EM61/Cart(201) | 0.55 | STOLS/Towed(299E) | 0.85 |
| STOLS/Towed(187) | 0.55 | STOLS/Towed(299D) | 0.85 |
| EM61/Cart(411) | 0.50 | EM61/Cart(425) | 0.65 |
| STOLS/Towed(298E) | 0.40 | EM61G822A/Towed(651E) | 0.55 |
| STOLS/Towed(298D) | 0.40 | EM61G822A/Towed(651D) | 0.40 |
| EM61G822A/Cart(657E) | 0.35 | GEM3/Cart(135) | 0.35 |
| EM61G822A/Cart(657D) | 0.35 | EM61/Cart(354) | 0.25 |
| EMFAST4D/Cart(38) | 0.20 | EM61G822A/Towed(651M) | 0.00 |
| GEM3/Towed(129) | 0.20 | MAG858/Cart(638) | 0.00 |
| SAM/Sling(379) | 0.05 | SCH/Hand(442) | 0.00 |
| EM61G822A/Cart(657M) | 0.00 | SCH/Hand(426) | 0.00 |
| MAG858/Cart(492) | 0.00 | STOLS/Towed(299M) | 0.00 |
| MTADS/Towed(673) | 0.00 | TM4/Sling(364) | 0.00 |
| SCH/Hand(231) | 0.00 | TM4/Sling(147) | 0.00 |
| SCH/Hand(229) | 0.00 | | |
| STOLS/Towed(298M) | 0.00 | | |
| TM4/Sling(311) | 0.00 | | |

Figure G-6. 40mmG Ordnance.

| 40mmP Ordnance | | | |
|---|-------|-----------------------|-------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| System | Pdres | System | Pdres |
| EM61/Towed(406) | 0.90 | MTADS/Towed(245) | 1.00 |
| TM5/Sling(154) | 0.90 | TM5/Sling(148) | 1.00 |
| MTADS/Towed(673) | 0.90 | EM61/Towed(668) | 0.90 |
| TM4/Sling(311) | 0.90 | EM61/Cart(169) | 0.90 |
| EM61G822A/Cart(657D) | 0.90 | EM63/Cart(249) | 0.90 |
| SAM/Sling(379) | 0.90 | STOLS/Towed(299E) | 0.90 |
| EM61/Cart(201) | 0.80 | STOLS/Towed(299D) | 0.90 |
| EM61/Cart(165) | 0.80 | EM61G822A/Towed(651E) | 0.85 |
| EM61G822A/Cart(657E) | 0.80 | EM61G822A/Towed(651M) | 0.85 |
| EM61G822A/Cart(657M) | 0.80 | EM61G822A/Towed(651D) | 0.85 |
| SCH/Hand(229) | 0.80 | EM61/Cart(425) | 0.75 |
| STOLS/Towed(187) | 0.80 | SCH/Hand(426) | 0.75 |
| EM61/Cart(411) | 0.65 | GEM3/Cart(135) | 0.60 |
| EM63/Cart(305) | 0.65 | SCH/Hand(442) | 0.60 |
| EMFAST4D/Cart(38) | 0.65 | TM4/Sling(147) | 0.60 |
| GEM3/Towed(129) | 0.65 | TM4/Sling(364) | 0.35 |
| MTADS/Towed(675) | 0.65 | EM61/Cart(354) | 0.25 |
| STOLS/Towed(298E) | 0.65 | STOLS/Towed(299M) | 0.15 |
| SCH/Hand(231) | 0.65 | MAG858/Cart(638) | 0.10 |
| STOLS/Towed(298D) | 0.65 | | |
| STOLS/Towed(298M) | 0.55 | | |
| MAG858/Cart(492) | 0.45 | | |

Figure G-7. 40mmP Ordnance.

| 57mmP Ordnance | | | |
|---|-------|-----------------------|-------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| TotalInformation | 57mmP | TotalInformation | 57mmP |
| TM5/Sling(154) | 1.00 | MTADS/Towed(245) | 1.00 |
| EM61/Towed(406) | 0.85 | EM61G822A/Towed(651M) | 1.00 |
| EM61/Cart(201) | 0.85 | EM61G822A/Towed(651D) | 1.00 |
| EM61/Cart(165) | 0.85 | EM61/Towed(668) | 0.95 |
| EM63/Cart(305) | 0.85 | EM61/Cart(425) | 0.95 |
| MTADS/Towed(675) | 0.85 | EM61/Cart(169) | 0.95 |
| STOLS/Towed(298E) | 0.85 | EM63/Cart(249) | 0.95 |
| MTADS/Towed(673) | 0.85 | STOLS/Towed(299E) | 0.95 |
| STOLS/Towed(187) | 0.85 | TM5/Sling(148) | 0.95 |
| STOLS/Towed(298D) | 0.85 | STOLS/Towed(299D) | 0.95 |
| EM61/Cart(411) | 0.75 | GEM3/Cart(135) | 0.85 |
| EMFAST4D/Cart(38) | 0.75 | TM4/Sling(147) | 0.85 |
| EM61G822A/Cart(657M) | 0.70 | SCH/Hand(442) | 0.80 |
| SCH/Hand(229) | 0.70 | SCH/Hand(426) | 0.75 |
| TM4/Sling(311) | 0.70 | TM4/Sling(364) | 0.75 |
| EM61G822A/Cart(657D) | 0.70 | EM61G822A/Towed(651E) | 0.65 |
| SAM/Sling(379) | 0.70 | STOLS/Towed(299M) | 0.45 |
| SCH/Hand(231) | 0.60 | EM61/Cart(354) | 0.40 |
| EM61G822A/Cart(657E) | 0.45 | MAG858/Cart(638) | 0.05 |
| GEM3/Towed(129) | 0.45 | | |
| STOLS/Towed(298M) | 0.45 | | |
| MAG858/Cart(492) | 0.10 | | |

Figure G-8. 57mmP Ordnance.

| 60mmM Ordnance | | | |
|---|-------|-----------------------|-------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| TotalInformation | 60mmM | TotalInformation | 60mmM |
| MTADS/Towed(675) | 0.85 | MTADS/Towed(245) | 0.95 |
| EM61/Towed(406) | 0.80 | TM5/Sling(148) | 0.95 |
| EM61/Cart(165) | 0.80 | EM61/Cart(169) | 0.90 |
| EM63/Cart(305) | 0.80 | EM63/Cart(249) | 0.90 |
| STOLS/Towed(298D) | 0.80 | STOLS/Towed(299E) | 0.90 |
| EM61/Cart(201) | 0.75 | STOLS/Towed(299D) | 0.90 |
| MTADS/Towed(673) | 0.75 | EM61/Towed(668) | 0.85 |
| TM4/Sling(311) | 0.75 | EM61G822A/Towed(651M) | 0.85 |
| EM61G822A/Cart(657D) | 0.75 | EM61G822A/Towed(651D) | 0.85 |
| EM61/Cart(411) | 0.65 | SCH/Hand(426) | 0.75 |
| EMFAST4D/Cart(38) | 0.65 | TM4/Sling(147) | 0.75 |
| STOLS/Towed(298E) | 0.65 | EM61/Cart(425) | 0.70 |
| TM5/Sling(154) | 0.65 | EM61G822A/Towed(651E) | 0.60 |
| EM61G822A/Cart(657M) | 0.65 | GEM3/Cart(135) | 0.60 |
| STOLS/Towed(187) | 0.65 | STOLS/Towed(299M) | 0.55 |
| EM61G822A/Cart(657E) | 0.60 | SCH/Hand(442) | 0.45 |
| SCH/Hand(231) | 0.60 | TM4/Sling(364) | 0.45 |
| STOLS/Towed(298M) | 0.60 | EM61/Cart(354) | 0.20 |
| SCH/Hand(229) | 0.55 | MAG858/Cart(638) | 0.20 |
| GEM3/Towed(129) | 0.45 | | |
| SAM/Sling(379) | 0.40 | | |
| MAG858/Cart(492) | 0.20 | | |

Figure G-9. 60mmM Ordnance.

| 81mmM Ordnance | | | |
|---|-------|-----------------------|-------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| TotalInformation | 81mmM | TotalInformation | 81mmM |
| MTADS/Towed(673) | 0.95 | EM61/Cart(169) | 0.95 |
| EM61/Towed(406) | 0.90 | EM61/Towed(668) | 0.90 |
| EM61/Cart(165) | 0.90 | EM63/Cart(249) | 0.90 |
| MTADS/Towed(675) | 0.90 | MTADS/Towed(245) | 0.90 |
| TM5/Sling(154) | 0.90 | STOLS/Towed(299E) | 0.90 |
| EM61G822A/Cart(657D) | 0.90 | TM5/Sling(148) | 0.90 |
| STOLS/Towed(187) | 0.90 | EM61G822A/Towed(651M) | 0.90 |
| EM61/Cart(201) | 0.85 | EM61G822A/Towed(651D) | 0.90 |
| EM63/Cart(305) | 0.85 | STOLS/Towed(299D) | 0.90 |
| EM61G822A/Cart(657M) | 0.85 | EM61/Cart(425) | 0.85 |
| STOLS/Towed(298D) | 0.85 | SCH/Hand(426) | 0.85 |
| STOLS/Towed(298E) | 0.80 | TM4/Sling(147) | 0.85 |
| SCH/Hand(231) | 0.80 | GEM3/Cart(135) | 0.80 |
| TM4/Sling(311) | 0.80 | STOLS/Towed(299M) | 0.75 |
| EM61/Cart(411) | 0.70 | EM61G822A/Towed(651E) | 0.70 |
| STOLS/Towed(298M) | 0.70 | SCH/Hand(442) | 0.65 |
| EMFAST4D/Cart(38) | 0.65 | TM4/Sling(364) | 0.65 |
| SAM/Sling(379) | 0.65 | EM61/Cart(354) | 0.40 |
| GEM3/Towed(129) | 0.55 | MAG858/Cart(638) | 0.15 |
| EM61G822A/Cart(657E) | 0.50 | | |
| SCH/Hand(229) | 0.50 | | |
| MAG858/Cart(492) | 0.20 | | |

Figure G-10. 81mmM Ordnance.

| BDU28 Ordnance | | | |
|--|--------------|-------------------------|--------------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| TotalInformation | BDU28 | TotalInformation | BDU28 |
| EM61/Cart(411) | 0.90 | EM61/Towed(668) | 0.95 |
| EM61/Cart(201) | 0.90 | EM61/Cart(169) | 0.95 |
| EM61/Cart(165) | 0.90 | MTADS/Towed(245) | 0.95 |
| MTADS/Towed(675) | 0.90 | STOLS/Towed(299E) | 0.95 |
| TM5/Sling(154) | 0.90 | TM5/Sling(148) | 0.95 |
| SCH/Hand(229) | 0.90 | EM61G822A/Towed(651M) | 0.95 |
| EM61/Towed(406) | 0.85 | EM61G822A/Towed(651D) | 0.95 |
| EM63/Cart(305) | 0.85 | STOLS/Towed(299D) | 0.95 |
| MTADS/Towed(673) | 0.85 | EM63/Cart(249) | 0.90 |
| SCH/Hand(231) | 0.85 | SCH/Hand(426) | 0.90 |
| STOLS/Towed(187) | 0.85 | EM61/Cart(425) | 0.85 |
| EM61G822A/Cart(657M) | 0.75 | TM4/Sling(147) | 0.85 |
| EM61G822A/Cart(657D) | 0.75 | GEM3/Cart(135) | 0.60 |
| STOLS/Towed(298D) | 0.75 | SCH/Hand(442) | 0.60 |
| EMFAST4D/Cart(38) | 0.70 | TM4/Sling(364) | 0.60 |
| TM4/Sling(311) | 0.70 | EM61G822A/Towed(651E) | 0.55 |
| STOLS/Towed(298E) | 0.60 | STOLS/Towed(299M) | 0.50 |
| EM61G822A/Cart(657E) | 0.55 | EM61/Cart(354) | 0.40 |
| STOLS/Towed(298M) | 0.55 | MAG858/Cart(638) | 0.15 |
| SAM/Sling(379) | 0.55 | | |
| GEM3/Towed(129) | 0.45 | | |
| MAG858/Cart(492) | 0.10 | | |

Figure G-11. BDU28 Ordnance.

| BLU26 Ordnance | | | |
|--|--------------|-------------------------|--------------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| TotalInformation | BLU26 | TotalInformation | BLU26 |
| EM61/Towed(406) | 1.00 | EM61/Towed(668) | 0.95 |
| EM61/Cart(411) | 1.00 | EM61/Cart(425) | 0.95 |
| EM61/Cart(165) | 1.00 | EM63/Cart(249) | 0.95 |
| EM63/Cart(305) | 1.00 | MTADS/Towed(245) | 0.95 |
| EMFAST4D/Cart(38) | 1.00 | STOLS/Towed(299E) | 0.95 |
| MTADS/Towed(675) | 1.00 | TM5/Sling(148) | 0.95 |
| TM5/Sling(154) | 1.00 | STOLS/Towed(299D) | 0.95 |
| STOLS/Towed(187) | 1.00 | EM61/Cart(169) | 0.90 |
| MTADS/Towed(673) | 0.90 | EM61G822A/Towed(651D) | 0.85 |
| EM61/Cart(201) | 0.85 | EM61G822A/Towed(651M) | 0.75 |
| STOLS/Towed(298E) | 0.85 | EM61G822A/Towed(651E) | 0.70 |
| EM61G822A/Cart(657M) | 0.85 | GEM3/Cart(135) | 0.65 |
| EM61G822A/Cart(657D) | 0.85 | TM4/Sling(147) | 0.65 |
| STOLS/Towed(298D) | 0.85 | SCH/Hand(442) | 0.45 |
| TM4/Sling(311) | 0.75 | SCH/Hand(426) | 0.40 |
| GEM3/Towed(129) | 0.65 | EM61/Cart(354) | 0.30 |
| SCH/Hand(231) | 0.65 | TM4/Sling(364) | 0.25 |
| SAM/Sling(379) | 0.50 | MAG858/Cart(638) | 0.05 |
| EM61G822A/Cart(657E) | 0.40 | STOLS/Towed(299M) | 0.05 |
| SCH/Hand(229) | 0.40 | | |
| STOLS/Towed(298M) | 0.25 | | |
| MAG858/Cart(492) | 0.15 | | |

Figure G-12. BDU26 Ordnance.

| M42 Ordnance | | | |
|--|------------|-------------------------|------------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| TotalInformation | M42 | TotalInformation | M42 |
| EM61/Towed(406) | 1.00 | MTADS/Towed(245) | 1.00 |
| EM63/Cart(305) | 1.00 | EM61/Cart(169) | 0.95 |
| TM5/Sling(154) | 1.00 | EM63/Cart(249) | 0.95 |
| EM61/Cart(165) | 0.90 | TM5/Sling(148) | 0.95 |
| EMFAST4D/Cart(38) | 0.90 | EM61/Towed(668) | 0.90 |
| EM61/Cart(411) | 0.85 | STOLS/Towed(299E) | 0.85 |
| MTADS/Towed(675) | 0.85 | STOLS/Towed(299D) | 0.85 |
| MTADS/Towed(673) | 0.85 | EM61G822A/Towed(651D) | 0.75 |
| SCH/Hand(231) | 0.85 | TM4/Sling(147) | 0.70 |
| SCH/Hand(229) | 0.85 | EM61/Cart(425) | 0.65 |
| EM61G822A/Cart(657D) | 0.85 | EM61G822A/Towed(651M) | 0.65 |
| STOLS/Towed(298D) | 0.85 | EM61G822A/Towed(651E) | 0.55 |
| STOLS/Towed(298E) | 0.75 | SCH/Hand(442) | 0.45 |
| EM61G822A/Cart(657M) | 0.75 | SCH/Hand(426) | 0.45 |
| TM4/Sling(311) | 0.65 | GEM3/Cart(135) | 0.40 |
| SAM/Sling(379) | 0.60 | TM4/Sling(364) | 0.35 |
| STOLS/Towed(298M) | 0.50 | STOLS/Towed(299M) | 0.20 |
| STOLS/Towed(187) | 0.50 | EM61/Cart(354) | 0.10 |
| EM61/Cart(201) | 0.40 | MAG858/Cart(638) | 0.05 |
| GEM3/Towed(129) | 0.35 | | |
| EM61G822A/Cart(657E) | 0.15 | | |
| MAG858/Cart(492) | 0.10 | | |

Figure G-13. M42 Ordnance.

| M75 Ordnance | | | |
|--|------------|-------------------------|------------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| TotalInformation | M75 | TotalInformation | M75 |
| EM61/Towed(406) | 0.00 | TM5/Sling(148) | 1.00 |
| EM61/Cart(411) | 0.00 | EM61/Towed(668) | 0.95 |
| EM61/Cart(201) | 0.00 | EM63/Cart(249) | 0.95 |
| EM61/Cart(165) | 0.00 | EM61/Cart(425) | 0.90 |
| EM61G822A/Cart(657E) | 0.00 | EM61/Cart(169) | 0.90 |
| EM63/Cart(305) | 0.00 | MTADS/Towed(245) | 0.90 |
| EMFAST4D/Cart(38) | 0.00 | STOLS/Towed(299E) | 0.90 |
| GEM3/Towed(129) | 0.00 | STOLS/Towed(299D) | 0.90 |
| MTADS/Towed(675) | 0.00 | EM61G822A/Towed(651M) | 0.85 |
| STOLS/Towed(298E) | 0.00 | EM61G822A/Towed(651D) | 0.85 |
| TM5/Sling(154) | 0.00 | GEM3/Cart(135) | 0.80 |
| EM61G822A/Cart(657M) | 0.00 | SCH/Hand(442) | 0.75 |
| MAG858/Cart(492) | 0.00 | SCH/Hand(426) | 0.75 |
| MTADS/Towed(673) | 0.00 | TM4/Sling(147) | 0.70 |
| SCH/Hand(231) | 0.00 | EM61G822A/Towed(651E) | 0.55 |
| SCH/Hand(229) | 0.00 | EM61/Cart(354) | 0.40 |
| STOLS/Towed(298M) | 0.00 | TM4/Sling(364) | 0.35 |
| TM4/Sling(311) | 0.00 | STOLS/Towed(299M) | 0.25 |
| EM61G822A/Cart(657D) | 0.00 | MAG858/Cart(638) | 0.00 |
| SAM/Sling(379) | 0.00 | | |
| STOLS/Towed(187) | 0.00 | | |
| STOLS/Towed(298D) | 0.00 | | |

Figure G-14. M75 Ordnance. No M75 ordnance were employed at APG.

| MK118 Ordnance | | | |
|--|--------------|-------------------------|--------------|
| Ground Truth Limited to 11 Diameters, No Challenge Area, No Overlap | | | |
| APG | | YPG | |
| TotalInformation | MK118 | TotalInformation | MK118 |
| EM61/Cart(165) | 0.60 | EM61/Towed(668) | 1.00 |
| MTADS/Towed(675) | 0.60 | EM61/Cart(169) | 1.00 |
| EM61/Towed(406) | 0.40 | MTADS/Towed(245) | 1.00 |
| EM61/Cart(201) | 0.40 | TM5/Sling(148) | 1.00 |
| STOLS/Towed(298E) | 0.40 | EM63/Cart(249) | 0.85 |
| TM5/Sling(154) | 0.40 | STOLS/Towed(299E) | 0.85 |
| STOLS/Towed(187) | 0.40 | STOLS/Towed(299D) | 0.85 |
| EM61/Cart(411) | 0.20 | EM61/Cart(425) | 0.70 |
| EM61G822A/Cart(657E) | 0.20 | EM61G822A/Towed(651D) | 0.45 |
| EM63/Cart(305) | 0.20 | EM61G822A/Towed(651E) | 0.35 |
| EMFAST4D/Cart(38) | 0.20 | GEM3/Cart(135) | 0.20 |
| STOLS/Towed(298D) | 0.20 | EM61/Cart(354) | 0.15 |
| GEM3/Towed(129) | 0.00 | EM61G822A/Towed(651M) | 0.00 |
| EM61G822A/Cart(657M) | 0.00 | MAG858/Cart(638) | 0.00 |
| MAG858/Cart(492) | 0.00 | SCH/Hand(442) | 0.00 |
| MTADS/Towed(673) | 0.00 | SCH/Hand(426) | 0.00 |
| SCH/Hand(231) | 0.00 | STOLS/Towed(299M) | 0.00 |
| SCH/Hand(229) | 0.00 | TM4/Sling(364) | 0.00 |
| STOLS/Towed(298M) | 0.00 | TM4/Sling(147) | 0.00 |
| TM4/Sling(311) | 0.00 | | |
| EM61G822A/Cart(657D) | 0.00 | | |
| SAM/Sling(379) | 0.00 | | |

Figure G-15. MK118 Ordnance.

APPENDIX H. REFERENCES

1. Standardized UXO Technology Demonstration Site Handbook, DTC Project No. 8-CO-160-000-473, Report No. ATC-8349, March 2002.
2. Aberdeen Proving Ground Soil Survey Report, October 1998.
3. Data Summary, UXO Standardized Test Site: APG Soils Description, May 2002.
4. Yuma Proving Ground Soil Survey Report, May 2003.
5. Survey of Munition Response Technologies, ESTCP, ITRC and SERDP, June 2006.
6. The Army Environmental Quality Technology Program A(1.6.a) UXO Screening, Detection, and Discrimination EQT-ORD, Office of the Assistant Secretary of the Army (ALT, I&E), April 2002.

APPENDIX I. ABBREVIATIONS

| | | |
|-------|---|--|
| AC | = | alternating current |
| APG | = | Aberdeen Proving Ground |
| ASCII | = | American Standard Code for Information Interchange |
| ATC | = | U.S. Army Aberdeen Test Center |
| DMM | = | discarded military munitions |
| EM | = | electromagnetic |
| EMI | = | electromagnetic induction |
| EMIS | = | Electromagnetic Induction Spectroscopy |
| ESTCP | = | Environmental Security Technology Certification Program |
| EQT | = | Army Environmental Quality Technology Program |
| ERDC | = | U.S. Army Corps of Engineers Engineering Research and Development Center |
| EZ | = | easy |
| GPO | = | geophysical prove-out |
| GPR | = | ground-penetrating radar |
| GPS | = | Global Positioning System |
| GT | = | Ground Truth |
| IDA | = | Institute for Defense Analysis |
| JPG | = | Jefferson Proving Ground |
| MAG | = | magnetometer |
| MEC | = | munitions and explosives of concern |
| MTADS | = | multi-sensor towed array detection system |
| NRL | = | Naval Research Laboratory |
| POC | = | point of contact |
| QA | = | quality assurance |
| QC | = | quality control |
| ROC | = | receiver-operating characteristic |
| RTK | = | real time kinematic |
| RTS | = | Robotic Total Station |
| SERDP | = | Strategic Environmental Research and Development Program |
| SOTA | = | state-of-the-art |
| TTFW | = | Tetro Tech Foster Wheeler |
| USAEC | = | U.S. Army Environmental Command |
| UXO | = | unexploded ordnance |
| YPG | = | U.S. Army Yuma Proving Ground |