

**SECTION 18**

**WATER RESOURCES**

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## **SECTION 18 WATER RESOURCES**

The water resources baseline information and assessment provides a description of the pre-mine conditions of surface and groundwater flow and water quality within the permit area and adjacent areas. This baseline assessment is developed for the proposed Pinabete Mine Plan permit area (permit area). The proposed permit area will be within portions of the Area 4 North and Area 4 South resource areas of the BHP Navajo Coal Company (BNCC) mining lease, located on the western flank of the San Juan Structural Basin. The coal seams to be mined are associated with the Cretaceous Age Fruitland Formation (Section 17, Geologic Information). The baseline resource assessment for this permit application package establishes the foundation for the determination of probable hydrologic consequences for the proposed surface mine operation (Section 41, Probable Hydrologic Consequences) and for the design of water resources reclamation plans (Section 35, Hydrologic Reclamation Plan) that may be needed to protect surface and groundwater resources.

This baseline evaluation includes a review of reports and data concerning water resources of the region obtained from state and federal agencies, as well as the information developed for BNCC's Navajo Mine and by CONSOL Energy's (formerly Consolidated Coal) Burnham Mine. BNCC implemented a baseline hydrologic monitoring program to obtain additional site-specific information from four ephemeral stream monitoring sites, three surface water impoundment sites, 12 groundwater monitoring wells and piezometers, and 14 vibrating wire piezometers, located within BNCC mining lease Area 4 South and Area 5 that were installed in 1998 and 2007 to supplement the existing information.

### **18.1 Surface Water Resources**

The Pinabete Mine Plan permit area is generally bounded by Pinabete Arroyo along the southwest side of the proposed permit area, by Navajo Mine permit area (Office of Surface Mining Reclamation and Enforcement (OSM) Permit No. NM-0003F) on the north, by the South Fork of Cottonwood Arroyo on the northeast, and the mining lease boundary on the east and west. The Pinabete mining area extends across approximately 8.75 square miles (sq mi) (5,569 acres) of the BNCC mining lease ([Exhibit 18-1-1](#)). Information pertaining to the No Name Arroyo, Brimhall Wash, and selected other regional drainages features are included in this Section to provide additional regional surface water information.

Pinabete Arroyo and the South Fork of the Cottonwood Arroyo are the primary surface water features within the permit area. Portions of the permit area also drain to the mainstem of the Cottonwood Arroyo and to an unnamed tributary to the Chaco River. The mainstem of the Cottonwood Arroyo and the Chaco River are outside of the permit area and will not be directly affected by proposed mining in the permit area. Cottonwood Arroyo, Pinabete Arroyo, and No Name Arroyo flow directly into the Chaco River. Cottonwood Arroyo has a watershed area of 79.8 sq mi. Pinabete Arroyo has a watershed of 60.3 sq mi,

and No Name Arroyo has a watershed of 11.5 sq mi, ([Table 18.1-1](#)). The Chaco River flows north into the San Juan River and drains an area of approximately 4,350 sq mi.

Annual precipitation within the immediate area of the permit area is low, averaging 5.7 inches, and rainfall amounts vary considerably from year to year (Section 12, Climate). The average monthly precipitation varies from 0.1 to 1.2 inches per month, with the most precipitation occurring in July, August, and September (Section 12, Climate). The average annual evaporation rate for this area is about 55 inches per year (Section 12, Climate). Due to the great differential of excess evaporation over precipitation, surface water flow in streams in the permit area occurs only in response to major storm events and base flow is nonexistent.

#### *18.1.1 Perennial and Intermittent Streams*

Although the flow in Pinabete Arroyo and Cottonwood Arroyo is ephemeral, these streams are defined by OSM regulation 30 CFR 701.5 as intermittent because the drainage basin area is greater than 1 sq mi.

Cottonwood Arroyo has a drainage area of about 79.8 sq mi, including approximately 12.4 sq mi of the Chinde Wash that is diverted to the North Fork of the Cottonwood Arroyo by the Amarillo Canal. Slightly less than six percent of the Cottonwood Arroyo watershed lies within the permit area. The South Fork of the Cottonwood flows through the permit area. The drainage area of the South Fork of the Cottonwood upstream of the permit boundary is approximately 18.3 sq mi. An additional 2.7 sq mi are within the permit area, for a total drainage area of approximately 21.1 sq mi ([Table 18.1-1](#) and [Exhibit 18.1-2](#)).

While the Pinabete Arroyo has a total drainage basin of approximately 60.3 sq mi, the size of the drainage basin area upstream of the point where Pinabete Arroyo exits the mine permit boundary is approximately 55.5 sq mi ([Table 18.1-1](#) and [Exhibit 18.1-2](#)). BNCC has assembled baseline information on Pinabete Arroyo, Cottonwood Arroyo, and No Name Arroyo. BNCC has obtained baseline information on flow and water quality of Cottonwood Arroyo at three stations CNS-1, CS-1 and CN-1 as shown on [Exhibit 18.1-2](#) and as described in Chapter 7 of Navajo Mine Permit Application Package (PAP) (OSM Permit No. NM-0003F) (BNCC 2009).

##### 18.1.1.1 Stream Channel Characteristics

The stream channels of Pinabete Arroyo and the South Fork of the Cottonwood Arroyo will not be directly disturbed by proposed mining within the permit area. Culverts will be installed on these streams for the Burnham Road relocation. Construction of the Burnham road and culvert crossings may result in a temporary increase in sediment if storm runoff occurs during construction but, in the long-term, the crossings will be an improvement, due to the anticipated reduction in sediment loads, over the fords that currently exist where the Burnham Road crosses these streams. Stream buffer zones will be demarcated



along these channels to prevent unauthorized disturbance of the designated channel reaches. Stream Buffer Zones are discussed further in Section 40.4.

The South Fork of the Cottonwood Arroyo is a major sand bed ephemeral drainage that passes through the northeastern portion of permit area. [Exhibit 18.1-1](#) shows the watershed area and drainage configuration for Cottonwood Arroyo, including the South Fork of the Cottonwood Arroyo. Cottonwood Arroyo is characterized by a rapid increase in discharge from a dry channel to peak discharge, followed by a recession to low discharge over several hours. These rapidly varying flows can transport large amounts of sediment and cause extensive change channel morphology, particularly noted at surface water station CNS-1. Total sediment and total dissolved solids concentrations are similar to regional values and average 97,989 mg/L and 656 mg/L, respectively.

The configuration of the sand bed channel of the segment of South Fork of the Cottonwood Arroyo, within the permit area, changes in response to the dynamics of sediment transport and deposition during the short duration high intensity flow events that naturally occur in the region. [Exhibit 18.1-3](#) shows channel cross sections from monitoring stations in Cottonwood Arroyo before and after the large flow events that occurred in July and August 1999. The cross-sections, taken in early June 1999 and again in January 2000, show the amount of channel transformation due to large flow events. Only minor changes in channel cross section were observed at stations CS-1 and CN-1 while particularly large changes occurred at station CNS-1. At station CNS-1, the north bank (cut-bank) of the channel moved approximately 60-feet horizontally and channel bottom width increased from about 60 feet to 95 feet between the two survey events in June 1999 and January 2000. In addition to the loss of sediment on the cut-bank, some sediment was temporarily stored as evidenced by the formation of sand bars on the opposite bank and the sediment deposition on the flood plain from out of bank flows.

The main channel segments of Pinabete Arroyo and No Name Arroyo within BNCC's mining lease are similar to the sand bed channel characteristics of the South Fork of the Cottonwood Arroyo. These segments were inventoried in 1998 and 2007 to establish baseline characteristics. The results of the baseline channel inventory for Pinabete Arroyo and No Name Arroyo are included in [Appendix 18.A](#). The purpose of this inventory was to document the channel conditions prior to mining, including bedrock outcrops, and indicators of channel instability such as knick points, channel cut banks, and channel scour or deposition. The channel bed and bank materials, cross sections, and vegetation characteristics were also noted. These properties provide an indication of the capacity of the stream channels to adjust and recover from potential changes in flows that may occur as a result of mining and reclamation.

Exhibits in [Appendix 18.A](#) display the channel profiles for Pinabete and No Name Arroyos and their tributaries within and adjacent to BNCC's mining lease. The channel cross sections for the corresponding

segments of Pinabete Arroyo and No Name Arroyo at the stream monitoring stations are also provided on exhibits in [Appendix 18.A](#).

Pinabete Arroyo is braided in many locations, reflecting the highly variable discharge rates, high bed load, limited vegetation, and high width to depth ratio. Channel depths range from 4 to 10 feet with widths varying from 20 to 80 feet. The main Pinabete Arroyo channel profile is mildly concave with slopes of 0.55% or higher at the upstream segment near the eastern permit boundary and decrease to about 0.33% downstream near the western permit boundary ([Appendix 18.A](#)). Sinuosity is relatively high downstream from Station P-1 for 1,500 feet, upstream and downstream of P-3 for 1,500 feet, and between P-5 and P-6 for 2,500 feet. No knick points, or convex segments, are present in the channel profile in the vicinity of the permit area. The channel maintains a slightly concave graded profile even though there may be continual reworking of sandy channel bed and bank materials. Minor changes in channel geometry and local slope may occur as a result of variation in the properties of channel materials and channel vegetation or in response to changing patterns of floods. Contributing tributaries are incised for as much as 300 feet upstream and exhibit head cuts ranging in height from 2 to 5 feet. Suspended sediment concentrations in storm runoff events are very high with TSS concentrations ranging from 10,200 to 521,000 mg/L in 26 baseline samples collected from Pinabete Arroyo ([Table 18.1-13](#)). For additional information refer to the 1998 and 2007 channel morphology reports in [Appendix 18.A](#).

The main No Name Arroyo channel profile, plotted on exhibits in [Appendix 18.A](#), was developed from 1-foot contour topography generated from aerial surveys conducted in 2008. It exhibits a variable slope with several knick points and convex segments, typical of an unstable channel. The knick point present in the channel profile near inventory location NNA-2 is associated with a 15-foot head cut and a deeply incised channel downstream of this location. Smaller head cuts were also found upstream of this point at locations just below the No Name Impoundment and at several points upstream of the No Name Impoundment. Sediment deposition is occurring at the impoundment where the Burnham Road (BIA Road No. 3005 and Navajo Road N-5082) crosses the No Name Arroyo. This deposition reduces sediment load in water that is released in outflows from the No Name Impoundment. The low sediment concentrations in impoundment outflows has accelerated erosion in the channel bed immediately downstream of the impoundment (Williams and Wolman 1984) and evidently contributes to the head cutting and channel incision observed in the reach further downstream of the impoundment. More detailed information on the channel morphology may be reviewed in the 1998 and 2007 channel morphology reports in [Appendix 18.A](#).

#### 18.1.1.2 Surface Water Flows

Between 1990 and 2000, BNCC performed baseline monitoring of surface water flows and water quality in Cottonwood Arroyo at three stations, CS-1 (South Fork), CN-1 (North Fork), and CNS-1 (main channel). Data collected during the ten years of baseline monitoring were submitted to OSM as part of the quarterly

hydrologic reports and annual hydrologic reports for Navajo Mine (BNCC 2009). From 1990 through 1996, monitoring consisted of single stage sediment samplers in conjunction with crest gauges. From 1997 through 1999, monitoring consisted of automated samplers and ultrasonic water level sensors.

Storm runoff hydrographs for several flow events were generated from the measurements from ultrasonic water level sensors and are provided in Appendix 7-1 of the Navajo Mine PAP (BNCC 2009). These results indicate that for most flow events, runoff volumes (acre/feet) decrease from upstream to downstream. However, the two storm events in early August 1999 were an exception to this, in which runoff volumes increased from upstream to downstream. The loss of water from upstream to downstream is apparently the result of water infiltrating into the sand bed of the progressively widening channel downstream. The two flow events in early August 1999 that show a slight net increase in the total runoff volume from upstream to downstream were preceded by several flow events in late July 1999. These frequent flow and precipitation events would produce high antecedent moisture within the channel bottom, which in turn may limit channel bed infiltration. Also, intense precipitation between the monitoring stations, such as the 2.6 inches of precipitation recorded in August 1999 at MET II, may also account for the increase in flow at the downstream station during these events.

The hydrograph shape for most of the storm runoff events at the Cottonwood stations, particularly in the summer, is characterized by a very sharp rise or spike in the rising limb with a very short duration peak, followed by a gradual falling limb of the hydrograph (BNCC 2009). This hydrograph shape is characteristic of flash flows in ephemeral channels due to high intensity thunderstorms. The shape of the hydrograph and the duration and timing for an individual flow event is similar between stations (Appendix 7-1, Navajo Mine PAP, OSM Permit No. NM-0003F) (BNCC 2009).

Baseline surface water monitoring stations were established on No Name Arroyo and Pinabete Arroyo downstream of BNCC's mining lease in 1998 as shown on [Exhibit 18.1-1](#). Prior to monitoring in year 2007, the lower Pinabete station was moved upstream approximately 6,000 feet from its 1998 location to provide a more suitable location closer to the mine permit boundary. Surface water monitoring stations were also installed on Pinabete Arroyo and No Name upstream of BNCC's mining lease. The monitoring stations were installed on relatively uniform straight channel segments and consisted of two or more single-stage samplers ([Figure 18.1-1](#)) and crest-stage gages ([Figure 18.1-2](#)) installed upstream and downstream of the single stage samplers to measure the slope of the water surface during the peak flow at the monitoring station.

Peak flow estimates (Q) reported in cubic feet per second (cfs) at each of the monitoring station locations ([Table 18.1-2](#)) were developed using Manning's equation as specified below:

$$Q(\text{cfs}) = 1.49 \times \frac{1}{n} \times A \times r^{\frac{2}{3}} \times S^{\frac{1}{2}}$$

The slope of the water surface (S) at each monitoring station location was determined from the measurements at the upstream and downstream crest-stage gages or from the slope of the channel when one of the crest stage gage readings was missing or erroneous. The cross-sectional area (A) and the hydraulic radius (r) corresponding to each measured crest-stage were digitized from the channel cross section at the monitoring station location.

The averages for the cross-sectional area (A) and the hydraulic radius (r) from the two crest stage gage locations at each station were used in Manning's equation to estimate flow except when one of the crest stage gage readings was missing or erroneous. In that case, the single value for A or r was used. The site-specific Manning roughness coefficient (n) was determined for each location during the stream channel inventory using the procedure for small channels as described in Gray (1970). Peak flows determined from crest-stage measurements during the 1997-1998 and 2007-2008 baseline monitoring period at the upstream and downstream sites on Pinabete Arroyo and No Name Arroyo are provided in [Table 18.1-2](#).

Flows in the arroyos draining BNCC's mining lease are flashy and occur in response to short duration, high intensity precipitation events usually during the seasonal thunderstorm months of July through November. The thunderstorms are usually localized and the intense rainfall may not extend throughout the drainage area of the arroyo. Consequently, there may not be much consistency among flows measured upstream or downstream or in adjacent drainages as indicated in [Table 18.1-2](#). Zero flow was recorded between November 1997 and June 1998 on both the Pinabete Arroyo and No Name Arroyo watersheds. Summer monsoonal rains in 1998 resulted in peak storm flows of 22.5 cfs at the upper Pinabete Arroyo site (Upper Pinabete), and 1,717 cfs at the downstream Pinabete Arroyo site (Lower Pinabete). The adjacent, but significantly smaller No Name Arroyo watershed exhibited a peak flow of 1.5 cfs at the upstream site (Upper No Name) in July, while no flow was reported at the No Name Arroyo downstream site (Lower No Name). The maximum peak flow of 2,307 cfs was observed in Pinabete Arroyo at the downstream site (Lower Pinabete) in August 1998, while the maximum peak flow observed in No Name Arroyo was 38.8 cfs at the downstream site (Lower No Name) in October 1998. Peak flow measured during 2007 and 2008 ranged from 0.2 to 7.5 cfs at the Pinabete Arroyo upstream site and from 0.4 to 46.6 cfs at the Pinabete Arroyo downstream site ([Table 18.1-2](#)). These peak flows are lower than the peak flows observed at the Pinabete Arroyo crest-stage gages in 1998. Peak flow measurements during 2007 and 2008 ranged from 0.7 to 19.1 cfs at the upstream No Name Arroyo site. The gages were damaged during a flow event in 2008 and were replaced. The peak flow estimates during 2007 and 2008 for the No Name Arroyo downstream site ranged from immeasurable to 111.1 cfs in 2007 and 2008 ([Table 18.1-2](#)). These peak flows at the lower No Name Arroyo location were higher than measured previously at this location during 1998. The 1998 water year appears to be an average water year, based on the examination of regional flows at two

U.S. Geological Survey (USGS) gages along the San Juan River in Farmington and Shiprock ([Table 18.1-3](#)).

SEDCAD<sup>TM</sup>4 (SEDCAD) modeling was performed on Pinabete Arroyo, No Name Arroyo, and Cottonwood Arroyo to better characterize the flow and sediment regimes. Information used to develop the SEDCAD projections and modeling results are provided in [Appendix 18.B](#). [Table 18.1-4](#) provides a summary of the SEDCAD model results for peak flows and sediment yield for selected storm frequency events for the two surface water monitoring stations on Pinabete Arroyo, the two stations on No Name Arroyo, the South Fork Cottonwood Arroyo, Cottonwood Arroyo at Station CSN-1, and Cottonwood Arroyo at its confluence with the Chaco River.

About 48 percent of the Cottonwood Arroyo watershed is occupied by badlands which accounts for the high discharge and flow intensities observed in this stream. Peak flows from a 10-year, 6-hour (10yr-6hr) event on Cottonwood at Station CSN-1 located near the mining lease boundary are predicted to be about 2,879 cfs ([Table 18.1-4](#)). The Cottonwood Arroyo channel between the mining lease boundary and its mouth with the Chaco River has a uniform gradient. Suspended sediment concentrations are high during storm runoff events and the sandy channel bed and bank materials are reworked by the larger flood events.

The SEDCAD peak flow predictions for the Pinabete Arroyo, No Name Arroyo, and Cottonwood Arroyo are less than the predictions using USGS method for ungaged streams in northwestern New Mexico ([Table 18.1-5](#)). The USGS method was developed in cooperation with the Bureau of Indian Affairs to estimate the magnitude and frequency of peak discharges for ungaged streams within the Navajo Nation in Arizona, Utah, Colorado, and New Mexico (Waltemeyer 2006). Peak discharge estimates in [Table 18.1-5](#) were calculated for Pinabete Arroyo, No Name Arroyo, and Cottonwood Arroyo using the regional equations developed in Waltemeyer (2006)

The SEDCAD predictions are thought to be more reliable, since the modeling incorporated detailed site-specific information on soils (e.g., K-factor and erodible particle size distributions) and cover values that were incorporated into subwatershed characterizations. In addition, the model accounts for the attenuation in flood flows associated with the No Name Impoundment on the No Name Arroyo.

Supplemental information is available from USGS regional sites located on Burnham Wash, a tributary to Brimhall Wash located southeast of the permit area (Site 9367936), the Teec-Ni-Di-Tso Wash, located within the region but further south from the Burnham Wash (Site 9367934), and the Chaco River gage (Site 9367938) ([Exhibit 18.1-1](#)). The first two sites have watersheds of 8.6 sq mi and 7.2 sq mi respectively, very similar in size to the 8.2 sq mi of the No Name Arroyo watershed above the mining lease boundary. The monthly average flow at Teec-Ni-Di-Tso Wash ranged from 0 to 2.2 cfs, with an average maximum

daily flow of 3.6 cfs in January for the 5-year period between 1978 and 1982 ([Table 18.1-6](#)). This 5-year period had 2 years in the 25-50% quartile, 2 years in the 50-75% quartile, and 1 year, 1979, in the top quartile for daily flow ([Table 18.1-3](#)). Average zero daily flow days/month for the period of record ranged from 10 to 27 days, with the most days of flow in January and the fewest days of flow in June. The results for Burnham Wash, located southeast of the permit area on a tributary to Brimhall Wash, were similar ([Table 18.1-7](#)) to those reported for the Teec-Ni-Di-Tso Wash ([Table 18.1-6](#)). The monthly average flow in Burnham Wash ranged from 0.02 to 1.02 cfs, with an average maximum daily flow of 4.8 cfs in January for the 5-year period between 1978 and 1982. Average zero daily flow days/month for the period ranged from 7 to 26 days, with the most days of flow in January and February and the least days of flow in June and July.

Stream flow in the Chaco River is ephemeral upstream of the existing Four Corners Power Plant (FCPP) as indicated by observations and supported by the five years of flow monitoring on the Chaco River at the USGS Site 09367938 near Burnham, New Mexico ([Exhibit 18.1-1](#)). Measurable flows at this station occurred only in response to rainfall or snow melt events. Annual peak storm flows for the 1978 to 1982 (5-year) monitoring period ranged from 950 to 6,740 cfs. The number of flow days per month on the Chaco River is quite variable, with zero flow during many months and flow every day during April 1982 ([Table 18.1-8](#)). Average number of days of zero flow per month ranged from 27.6 days in June to 13.2 days in March ([Table 18.1-8](#)). The flow monitoring results at this station show that streamflow in the Chaco River occurs as discrete flow events that range from less than one day to more than several weeks that are separated by periods of zero flow that can range several days to several months.

Additional perspectives on flow in Pinabete Arroyo can be derived from monitoring performed at the CONSOL Energy's Burnham Mine on Brimhall Wash, located south of permit area ([Exhibit 18.1-1](#)). Part of the Brimhall Wash drainage lies immediately south and adjacent to Pinabete Arroyo. Both streams drain areas with similar landforms, soils, vegetation, and elevations. Brimhall Wash drainage is slightly larger at 85.2 sq mi as compared to Pinabete Arroyo with a 60.3-sq mi watershed. Brimhall Wash was monitored daily over a 3-year period, between October 1, 1977 and May 31, 1980, at two locations: Site M (downstream) and Site N (upstream) (Burnham Mine Permit Application Package on file at the OSM library in Denver, Colorado). Both sites experienced from 0 to 4 flow days/month for most months during the monitoring period, with a maximum of 10 flow days during August 1978 at Site N ([Table 18.1-9](#)). These results show that runoff from summer thunderstorms is localized and that channel conveyance losses can be considerable. For example, while 10 flow days were observed during August 1978 at the Site N, zero flow days were observed during August 1978 at Site M ([Table 18.1-9](#)). Runoff patterns on Pinabete Arroyo are expected to be similar to those observed at Brimhall Wash.

The No Name Impoundment is filled periodically by runoff from storm events. Water was first observed in the No Name Arroyo impoundment in November 1997 and remained in the impoundment until June 1998. A staff gage was installed in the impoundment during the spring of 1998. Staff gage levels were recorded on a monthly basis during year 1998 and as soon as possible after major precipitation events. These results are provided in [Table 18.1-10](#). It appeared that water was lost from this impoundment by both seepage and evaporation. The impoundment was dry from late June until July 26, 1998, when it refilled to the spillway elevation during a storm runoff event. Water remained in the impoundment beyond December 1998. The invert of the spillway on the No Name Impoundment was surveyed in 2008 and was found to be 6 feet above the low point within the impoundment. The survey also showed that the storage capacity of the impoundment at the spillway invert elevation is 19.7 acre feet (ac-ft) and would cover an area of 8 acres. Spillway and elevation-area capacity details for the structure can be reviewed in the baseline SEDCAD runs on “No Name Watershed w/Impoundment”, Structure 8, in [Appendix 18.B](#).

#### 18.1.1.3 Surface Water Quality

The Navajo Nation has adopted the Navajo Nation Surface Water Quality Standards (Navajo Nation Environmental Protection Agency [NNEPA] 2008) which established various surface water use quality standards. These standards apply to all Waters of the Navajo Nation which include, but are not limited to, ephemeral, intermittent, and perennial streams, springs, wetlands, and any natural or man-made depressions or basins that impound water within the border of the Navajo Nation. The standards associate specific uses with specific stream reaches including the Cottonwood Arroyo, Brimhall Wash, and the Chaco River. Specific uses have not been identified for No Name Arroyo and Pinabete Arroyo. It is likely that No Name and Pinabete Arroyos would share the standards with the Chaco River as they are nonperennial tributaries. Designated uses for Cottonwood Arroyo, Brimhall Wash, and the Chaco River include livestock watering (LW), aquatic & wildlife habitat (A&WHbt), fish consumption (FC), and secondary human contact (ScHC) standards (NNEPA 2008). The applicable standards for the designated uses have been identified on [Table 18.1-11](#). The NNEPA has no water quality standard for total dissolved solids (TDS), sulfate, or fluoride but relevant livestock use criteria from Lardy, Stoltenow, and Johnson (2008) have been included in [Table 18.1-11](#) to help assess the suitability of surface water for livestock use. The Navajo Nation surface water quality standard for suspended sediment applies only to surface water that is at or near base flow and does not apply to surface water during or soon after a precipitation event and is therefore not applicable to ephemeral flows (NNEPA 2008).

The USGS monitoring records indicate that sizeable peak flows periodically occur due to high intensity thunderstorm events. The duration of flow resulting from these events is extremely short and typical of ephemeral runoff events. Sampling of such short-duration stream flows with passive single-stage samplers ensures the collection of samples from episodic events. In addition, samplers can be located at several stages within the stream, thereby enabling collection of samples at different flow depths. [Figure 18.1-1](#)



shows the design for the single-stage sediment sampler and [Figure 18.1-2](#) shows the crest stage gage design. The intake on the single-stage samplers points downstream to reduce plugging from debris that might be present in the stream flow. Each sample location along in Pinabete Arroyo and No Name Arroyo had three single-stage sediment samplers at different locations along the channel cross section. Single-stage sediment samplers were also used from 1990 through 1996 at the three Cottonwood Arroyo monitoring stations, CS-1 (South Fork), CN-1 (North Fork), and CNS-1 (main channel). These stations were replaced by automated samplers and ultrasonic water level sensors for the baseline monitoring period from 1997 through 1999.

Analytical results of water samples collected at these monitoring stations are summarized in [Tables 18.1-12](#), [18.1-13](#), and [18.1-14](#) and are discussed below. Flows associated with the water quality samples from the single-stage samplers were inferred from the estimated peak flow for the crest-stage measurements obtained at the same time that the samples were collected.

Samples collected by the automated sampler on the Cottonwood stations CN-1, CS-1, and CNS-1 were analyzed for chemistry and total sediment. For each sample/flow event, only the first sample bottle collected was analyzed for chemistry from each station with the remaining samples analyzed for total sediment. A total of 314 water samples were collected from these stations between 1997-1999, with 255 of these samples analyzed for total sediment and 59 samples analyzed for chemistry. An additional 233 samples were obtained from 1990 to 1997 at these stations from the single stage samplers and from occasional grab samples.

[Table 18.1-12](#) provides a summary of the median concentrations for water quality analysis results from samples collected at each of these Cottonwood baseline monitoring stations. These results show that for all three stations the dominant water type is a sodium sulfate. The median total dissolved solids concentration (TDS) for CN-1 is 780 mg/L with a range of 290-6,220 mg/L. The median TDS concentration for CS-1 is 675 mg/L with a range of 305-9,060 mg/L and for CNS-1 the median TDS concentration is 610 mg/L with a range of 315-15,600 mg/L. These values indicate a slight decrease in TDS concentration from upstream to downstream. More importantly, these values are typical of regional TDS concentrations for surface water quality. Station CN-1 has a slightly higher concentration of sulfate and TDS, which may reflect slightly different soil types in the watershed and possible Navajo Indian Irrigation Project (NIIP) impacts.

Surface water data were collected and analyzed for different parameters during the three years of water monitoring conducted between 1998 and 2008 at stations on Pinabete and No Name Arroyos. Samples were acquired from two sites in Pinabete Arroyo, Upper Pinabete (upstream), and Lower Pinabete (downstream). Samples were collected at the Upper Pinabete site on four dates in 1998, two dates in 2007, and two dates in 2008 ([Table 18.1-13](#)). Samples were collected at the Lower Pinabete site on five dates in



1998, four dates in 2007, and two dates in 2008 ([Table 18.1-13](#)). On some of the sample dates, samples were obtained from more than one of the single-stage sample containers at a sampling location. The surface water in Pinabete Arroyo is a sodium sulfate type ([Figure 18.1-3](#) and [Figure 18.1-4](#)) and had a hardness ranging from 29 to 413 mg/L as calcium carbonate (CaCO<sub>3</sub>), with a median value of hardness of 108 mg/L as CaCO<sub>3</sub>. The conductivity ranged from 396 to 1,940 micro Siemens per centimeter (µS/cm), with a median value of 723 µS/cm. Dissolved aluminum values for all samples ranged from <0.1 to 2.3 mg/L, with a median value of 0.27 mg/L. The chronic aquatic standard for dissolved aluminum is 0.087 mg/L, so virtually all baseline background samples were elevated above that level. Total suspended solids (TSS) values ranged from 10,200 mg/L to 521,000 mg/L, with a median value of 79,200 mg/L. These high sediment loads are consistent with water quality from ephemeral drainages in arid regions. Boron concentrations ranged from 0.06 to 0.9 mg/L. Most of the cadmium results were less than the detection limit of 0.00055 mg/L but four samples detected cadmium at concentrations above the hardness dependent chronic aquatic and wildlife criterion of 0.00026 mg/L. Copper concentrations ranged from 0.006 to 0.026 mg/L, with a median value of 0.009 mg/L and approximately half the samples above the hardness dependent chronic aquatic and wildlife criterion of 0.00956 mg/L. Fluoride concentrations range from <0.20 to 1.19 mg/L. The Upper Pinabete station had dissolved iron concentrations which ranged from <0.05 to 7.00 mg/L while the Lower Pinabete station had values which ranged from <0.02 to 20.3 mg/L. Total iron values ranged from 125 to 1,940 mg/L at the upstream site and ranged from 6 to 1,220 mg/L at the downstream site. The NNEPA has no surface water quality standard associated with iron. For three events, mercury levels were detected at concentrations in excess of the chronic aquatic and wildlife habitat standard of 0.001 µg/L. For all other events, the mercury levels were less than the detection limit, but the method detection limit for mercury of 0.2 µg/L is higher than the chronic aquatic and wildlife habitat standard. Dissolved selenium concentrations range from <0.001 to 0.007 mg/L with some of the concentrations in excess of the chronic aquatic and wildlife habitat standard of 0.002 mg/L.

Samples were acquired from two sites in No Name Arroyo, Upper No Name (upstream) and Lower No Name (downstream), during the 3 years of water monitoring conducted between 1998 and 2008. Samples were collected at the Upper No Name site on two dates in 1998 and on three dates in 2008 ([Table 18.1-14](#)). Samples were collected at the Lower No Name site on three dates in 1998, one date in 2007, and one date in 2008 ([Table 18.1-14](#)). On some of the sample dates, samples were obtained from more than one of the single-stage sample containers at a sampling location. The water at the upstream site (Upper No Name 3) is a sodium-bicarbonate type, while the downstream site (Lower No Name 1) is a sodium sulfate type ([Figure 18.1-4](#) and [Figure 18.1-5](#)). Hardness ranged from 32 to 558 mg/L, with a median value of 106 mg/L. Conductivity ranged from 150 to 1,330 µS/cm, with a median value of 314 µS/cm. The conductivity results are consistent with the TDS concentrations, which ranged from 100 mg/L to 1,030 mg/L, with a median value of 353 mg/L. Dissolved aluminum ranged from 0.15 to 1.65 mg/L. Eight of 13 dissolved aluminum values are elevated above the aquatic and wildlife habitat limit of 0.087 mg/L, but the

detection limit of the other 5 samples exceeded the limit. This is often related to the high concentrations of some analytes that interfere with detection of other analytes at very low concentrations.

Total suspended solids (TSS) values ranged from 367 mg/L to 395,000 mg/L, with a median value of 16,300 mg/L. The two samples collected on August 13, 1998 at the Lower No Name station also show increasing suspended solids with increasing flow as the #2 sampler is set at a higher intake stage. These samples also exhibit considerable variation in major ion concentrations between samples collected at different intake stages during the same runoff event. Dissolved iron concentrations ranged from <0.05 mg/L to 3.31 mg/L on No Name Arroyo, while total iron concentrations ranged from 3 to 6,020 mg/L on sampling at Upper No Name and 1 to 419 mg/L for sampling on Lower No Name. Boron concentrations ranged from <0.05 to 0.5 mg/L, fluoride concentrations ranged from 0.19 to 0.89 mg/L, and dissolved selenium concentrations were less than 0.1 mg/L.

Analysis results of samples from two sites in Brimhall Wash were provided in the Burnham Mine Permit Application Package, on file in the Office of Surface Mining Library in Denver, Colorado. Seventeen samples were collected at the upstream site (Site N), and 19 samples were collected at the downstream site (Site M) between March 14, 1990 and January 8, 1995 ([Table 18.1-15](#)). Both sites exhibit sodium sulfate-type waters ([Figure 18.1-6](#)), with a median hardness of 113 mg/L CaCO<sub>3</sub>. Specific conductance varies substantially, with recorded results ranging from 142 to 27,800 µS/cm. The highest value was recorded following a large storm event on July 23, 1990. Excluding that value, the average specific conductance was 1,277 µS/cm. Total dissolved solids ranged from 10 to 27,500 mg/L, with a median value of 940 mg/L. Three of 36 samples exhibited TDS levels above the relevant livestock use criterion of 3,000 mg/L (Lardy et.al. 2008). Flows at the sites were storm related and sediment laden. Total suspended solids at the two sites ranged from 11,800 to 128,420 mg/L, with a median value of 57,660 mg/L. Total iron values range from 0.27 to 7480 mg/L, with a median value of 202 mg/L. Boron concentrations ranged from 0.02 to 0.36 mg/L and fluoride concentrations ranged from 0.1 to 2.0 mg/L, with a median of 0.9 mg/L. Total selenium was analyzed three times and was always less than the method detection limit at <0.005 mg/L, although the method detection limit for selenium slightly exceeds the aquatic and wildlife habitat standard of 0.002 mg/L. Total mercury was detected in only one of four samples at a concentration of 0.0006 mg/L and was less than the method detection limit of 0.0005 mg/L in the other three samples. Both the detected value and the detection limit for total mercury exceed the chronic aquatic and wildlife habitat limit of 0.001 µg/L. This was also the case with total selenium, which had a detection limit of 0.005 mg/L, while the chronic aquatic and wildlife habitat criterion is 0.002 mg/L. Sulfate concentrations varied substantially, with results ranging from 29 to 18,100 mg/L and a median value of 356 mg/L. Six of 35 values for sulfate exceeded the relevant criterion for livestock use of 1,000 mg/L.

From a general water quality characterization perspective, the samples from the Pinabete Arroyo, No Name Arroyo, and Brimhall Wash monitoring locations ([Table 18.1-13](#), [Table 18.1-14](#), and [Table 18.1-15](#), respectively) appeared to exhibit higher concentrations of major ions and TDS in the first major runoff event of the season as compared to subsequent events. The results from the Upper No Name monitoring station show lower levels of TSS, settleable solids, TDS, and major ion concentrations than were observed at the Lower No Name station or at either of the Pinabete Arroyo monitoring stations. The sodium adsorption ratios were also lower in the samples taken from the No Name Arroyo stations as compared to the Pinabete Arroyo stations.

Changes in TDS and TSS concentrations at upstream and downstream locations on Brimhall Wash were evaluated in the Burnham Mine Permit Application Package on file in the Office of Surface Mining Library in Denver, Colorado ([Table 18.1-16](#) and [Table 18.1-17](#)). These results show median TDS concentrations of 845 mg/L at the upstream site (Site N) and 843 mg/L at the downstream site (Site M). Median TSS concentrations were 20,810 mg/L at the upstream site (Site N) and >20,000 mg/L at the downstream site (Site M). Exceptionally high TSS concentrations were often associated with elevated TDS concentrations.

The USGS monitored stream flow continuously over the period from November 1975 through September 1994 at Station 09367950 on the Chaco River near its mouth as shown on [Exhibit 18.1-1](#). Suspended sediment concentrations were also monitored at this station over the period from October 1976 through September 1982. The stream-flow data show base flows ranging from 0 to 30 cfs during non-storm periods and annual peak storm flows ranging from 1,170 to 6,410 cfs. Discharges from Morgan Lake near the FCPP generate a perennial flow in this lower reach of the Chaco River. Suspended sediment concentrations vary with discharge and typically range from 300 to 5,000 mg/L, except during storm runoff events when concentrations typically range from 50,000 to 150,000 mg/L (USGS 2009).

#### *18.1.2 Lakes, Reservoirs, Other Water Bodies*

There are no lakes or reservoirs within the permit area. However, there are three small impoundments within the permit area, one on a tributary to Cottonwood Arroyo and two on tributaries to Pinabete Arroyo as shown on [Exhibit 18.1-2](#). These are stock watering ponds that catch surface flows from some tributary drainages. These impoundments extend across less than 2 acres each and are often dry. The stock water ponds are not used for irrigation, consumption by humans, or purposes other than livestock watering.

The small pond, on a tributary to Cottonwood Arroyo in Area 4 North on the northwest side of the permit area shown as Pond 4N in [Exhibit 18.1-2](#) has a limited drainage and is usually dry. The small stock impoundment on a tributary to Pinabete Arroyo designated as Stevenson's Well Pond provides a water source for local recharge of the alluvial well located immediately downgradient of the pond. The third pond, located on a tributary to Pinabete Arroyo at the boundary between Area 4 North and Area 4 South, is

designated as the 4N/4S Pond as shown on [Exhibit 18.1-2](#). Water samples were collected at both the 4N/4S Pond and at the Stevenson's Well Site pond. The analytical results from these ponds are summarized in [Table 18.1-18](#). The concentration of dissolved aluminum in one sample at the 4N/4S Pond with a concentration of 0.38 mg/L exceeded the chronic aquatic and wildlife limit of 0.087 mg/L. The cadmium limit is hardness dependent. There is no data on the hardness of these samples, but using the median hardness along Pinabete of 108 mg/L, the dissolved cadmium chronic aquatic limit is 0.00026 mg/L ([Table 18.1-11](#)), which is exceeded by the concentration of 0.00107 mg/L at the 4N/4S Pond, and 0.01397 mg/L at the Stevenson's Well Site pond. Samples collected in 2007 and 2008 from these ponds were also analyzed for pesticides and polychlorinated biphenyls (PCBs). These results show that pesticides and PCB values were below detection limits ([Appendix 18.C](#)).

Other ponds are found within the study area but outside the permit area. The largest of these is the No Name Impoundment located on the No Name Arroyo channel at the intersection of Burnham Road (BIA Road 3005 and Navajo Road N-5082) and No Name Arroyo. This impoundment holds varying amounts of water depending upon the occurrence of storm runoff. Water containment is seasonal according to the monthly monitoring that occurred in 1997 and 1998. The No Name Impoundment contained water from December 1997 past June 11, 1998. When the water level in the impoundment was checked again on July 21, 1998, it was dry and appeared to have been dry from some time. Following storms on July 26, 1998, the impoundment refilled with water, reflecting the fact that storage in the impoundment is dependent on surface water inflow from storm events. Enhanced vegetation growth immediately downstream of the No Name Impoundment strongly suggests that localized groundwater is present due to seepage from the impoundment.

Water quality samples have been collected at No Name Impoundment. Grab samples were obtained monthly in 1998 from the No Name Impoundment when it contained water and was free of ice cover. The analytical results for the water quality samples from the impoundment are summarized in [Table 18.1-18](#). Comparison of the monthly sample results shows higher concentrations of major ions, TDS, and Sodium Adsorption Ration (SAR) in April and May as the impoundment was drying up than in July and August after the impoundment was filled by major storm runoff events on July 26, 1998 and August 21, 1998. Based on these results, the water in the No Name Impoundment appears to be acceptable for livestock watering use even when concentrated by evaporation during storage. Data collected in 2007 and 2008 show PCB values were below detection limits ([Appendix 18.C](#)). There were elevated concentrations of dissolved aluminum above chronic aquatic and wildlife habitat standard. Cadmium chronic aquatic habitat standards are hardness dependent, and the No Name Impoundment had a median hardness of 117.5 mg/L CaCO<sub>3</sub> from 1998 sampling, which results in a standard of 0.00028 mg/L for cadmium. Dissolved cadmium concentrations were 0.00025 mg/L on April 10, 2008 and 0.01397 mg/L on August 12, 2008.

The median hardness of 117.5 generates a chronic aquatic habitat standard of 0.01028 for copper, and the dissolved copper concentrations were 0.0285 mg/L on April 10, 2008 and 0.0088 mg/L August 12, 2008.

#### *18.1.3 Discharges into Surface Water Bodies*

There are no springs, seeps, or man-made discharges into surface water bodies within or adjacent to the permit area.

#### *18.1.4 Surface Water Resources Information Collection and Analysis*

BNCC has obtained baseline information on flow and water quality of Cottonwood Arroyo at three stations CNS-1, CS-1 and CN-1 during the period from 1990 through 1999. BNCC also implemented a baseline hydrologic monitoring program on Pinabete and No Name Arroyos in 2007 and 2008 to supplement monthly data collected in 1998. Water quality and flow information was obtained during this baseline monitoring program from two stream monitoring sites located near the permit boundary on Pinabete Arroyo and from two monitoring stations on No Name Arroyo near the mining lease boundary. Samples were also collected and analyzed for water quality at two impoundments located within the permit area and at the No Name Impoundment located on No Name Arroyo south of the permit area.

A crest-stage gage and single-stage sediment sampler were installed near the upstream and downstream permit boundaries on Pinabete Arroyo and No Name Arroyo. The locations of the crest stage gages and sediment samplers are shown on [Exhibit 18.1-1](#). The designs of the single-stage sediment sampler and crest stage gage are shown in [Figure 18.1-1](#) and [Figure 18.1-2](#), respectively. Surveyed channel profiles and cross sections were established at the crest-stage gage locations. All water samples included field measurements of pH, temperature, and specific conductance. Water quality parameters, consisting of total suspended solids, settleable solids and total dissolved solids, dissolved and total iron and manganese, major cations and anions, 12 trace metals, 3 minor anions, and 2 radium isotopes. The sampling suite and associated data for Pinabete Arroyo and No Name Arroyo samples are summarized on [Table 18.1-12](#) and [Table 18.1-13](#), respectively. Quality assurance and quality control information for the 2007-2008 surface water data is provided in [Appendix 18.D](#).

Channel profiles and cross sections at the crest stage gage locations were surveyed in 2007 and compared to the survey performed in 1998. This comparison provided limited evidence of midterm morphological changes for the project area and provided insights into channel stability.

## **18.2 Groundwater Resources**

The groundwater baseline assessment provides a description of the pre-mine conditions for each water-bearing stratum, including the coal seams and any potentially impacted strata below the lowest coal seam to be mined. The baseline assessment also establishes the foundation for the determination of

probable hydrologic consequences for the surface coal mine operation (Section 41, Probable Hydrologic Consequences) and for the design of water monitoring and mitigation plans that may be needed to ensure that there is no material damage to groundwater resources.

A number of studies of the geology and groundwater hydrology have been conducted by the New Mexico Bureau of Mines and Geology and the USGS in the vicinity of the permit area. BNCC has also conducted extensive drilling and exploration within its mining lease, which, together with data from the nearby Navajo Mine, provide information about the geology and groundwater hydrology of the area to be mined. BNCC has also implemented a groundwater monitoring program (Section 42, Monitoring, Maintenance, Inspections, and Examinations) to obtain site-specific information on groundwater levels, aquifer characteristics, and groundwater quality to supplement the existing information.

#### *18.2.1 Springs, Seeps, and Other Groundwater Discharges*

Direct recharge of overburden is quite low due to the arid climate with average annual precipitation of less than 6 inches and annual evaporation rate of about 55 inches (Section 12, Climate). Recharge rates measured by chloride mass balance methods on undisturbed areas at the nearby Navajo Mine ranged from 0.002 to 0.09 in/yr (Stone 1987). Due to the very low rates of recharge, groundwater discharge rates are also quite low and insufficient to sustain base flow at any streams in the vicinity of the permit area, including the Chaco River.

Site reconnaissance and review of springs identified by the New Mexico Office of the State Engineer (NMOSE) (2010) Navajo Settlement Agreement found no springs within or adjacent to the permit area. Several springs were identified outside the adjacent area as shown on [Exhibit 18.2-1](#). One spring, S-0846 (BIA NO. U-30), was identified about 2.5 miles north of the permit area, immediately west of Navajo Mine Area 3 on Lowe Arroyo. The use of this spring was listed as unknown and the spring was not found during site reconnaissance. Also, the Cottonwood Springs, BIA designations 13R-103 and 13R-104, are identified as spring S-0127 in the NMOSE (2010) Navajo Settlement Agreement. These springs are on upper Cottonwood Arroyo about 4.2 miles northeast of the permit area. Finally, two springs, #52 and #53, were identified in an inventory of wells and springs conducted by Billings and Associates, Inc (BAI) in 1985 for the Navajo Mine. The approximate locations for these springs from the BAI inventory are shown on [Exhibit 18.2-1](#). It is possible that these springs may be the same as the Cottonwood Springs since a number of the springs and wells in the BAI inventory were not mapped accurately.

An intermittent artificial seep was also identified during the site reconnaissance at a location immediately below the surface impoundment on No Name Arroyo. Enhanced vegetation, consisting of dense salt cedar, brush, and grass, occurs for several hundred feet downstream of the No Name impoundment. This seep is the result of the surface impoundment and not a location of groundwater discharge and is not shown on

[Exhibit 18.2-1](#). One location for potential groundwater discharge was identified during the site reconnaissance by enhanced vegetation growth and salt deposits along the on the channel bed and banks at a location on Pinabete Arroyo approximately 1,400 feet upstream of the Burnham Road crossing. These features suggest the presence of a groundwater discharge that is insufficient to sustain flow (Brown 1976). The groundwater source may be from the No. 8 coal seam, which outcrops in the vicinity of this location or it could be from the alluvium, which is known to be partially saturated upstream near the eastern permit boundary at alluvial well PA-1. It is unlikely that these salt deposits are due to evaporation of residual runoff because they occur along the channel bed and bank, not in depressions, and do not extend upstream or downstream of this isolated location.

Groundwater flow directions in the Pinabete alluvium follow the surface water down gradient towards the Chaco River. However, there are no indications of groundwater discharge along the Chaco River in the vicinity of Pinabete Arroyo. The only springs and seeps noted along the Chaco River are far to the north near the FCPP where Stone et.al. (1983) report that several short reaches of the Chaco River flow due to springs issuing from the alluvium. This surface water flow is discussed in Section 18.1.1.

Based on the potentiometric surfaces presented in Section 18.2.4, flow directions in the Fruitland coals are toward the north-northeast. Potentiometric gradients in the Pictured Cliffs Sandstone (PCS) are toward the north. The northerly gradients in these potentiometric surfaces are influenced by the topographic low along the San Juan River valley. There may also be some local influence of topographic lows along the Chaco River tributaries on potentiometric gradients in these units. Potential rates of discharge from these bedrock units are extremely low due to the low recharge rates and low hydraulic conductivity of these units.

#### *18.2.2 Wells*

An inventory of water supply wells located within and adjacent to the permit area was prepared from well information from a several sources. The sources include the water supply wells identified by the NMOSE (2010) Navajo Settlement Agreement, the inventory of wells conducted by BAI in 1985 for the Navajo Mine, wells identified in the “Groundwater Operations Manual and Well Survey for Navajo Mine and Vicinity” that was completed by Metric Corporation (1991), and wells found in review of permits on file at the Navajo Nation Water Resource Management office in Fort Defiance, Arizona.

The study area for the inventory presented in this section extends from Chaco River and its alluvium on the west to about four miles east of BNCC’s mining lease shown in [Exhibit 18.2-1](#). Relevant information on the wells shown in [Exhibit 18.2-1](#) is provided in [Table 18.2-1](#). Wells that were installed for the sole purpose of monitoring are not shown on [Exhibit 18.2-1](#). These monitoring wells, including the monitoring wells that have been abandoned, are depicted on [Exhibit 18.2-2](#). Although the completion zone for some of the wells is not specified in the information sources, it is believed that almost all of the water wells located



within the study area are completed within the alluvium of the Chaco River, Pinabete Arroyo, and Brimhall Wash due to their locations on [Exhibit 18.2-1](#). Only four of the wells in [Table 18.2-1](#) are believed to be completed in bedrock formations. Well 13-AW is a flowing artesian oil and gas well that was converted to stock water use that is sourced from bedrock below the PCS, most likely from the Menefee Formation. The completion zone for well W-606, located in Area 5 of the BNCC mining lease, is not specified. This well was capped and welded shut during the site reconnaissance and the well depth could not be measured. However, based on the depth reported by Metric Corporation (1991), this well may be completed within the PCS. Likewise, Tribal Well 13-7-2, located approximately 300-feet south of the Burnham Chapter House, is a PCS well that was originally installed for water supply for Burnham. It was replaced and abandoned due to poor yield and poor water quality. Finally, Well #90, located along the Chaco River north of Brimhall Wash, was identified as a PCS well in the BAI inventory for Navajo Mine. These water-bearing units are deeper than the PCS but it is possible that the uppermost screen interval in this well could be within the PCS.

The following three water wells were indicated to be within the permit area from one or more of the various sources of available information used for the well inventory:

- Well W-0345 (13R-48) is a dug alluvial well located on Pinabete Arroyo west of the Burnham Road. This well includes a hand pump and tank and is used for stock watering.
- Well #70 is identified in the 1985 BAI inventory for the Navajo Mine as a dug alluvial well. This well could not be found in the site reconnaissance and alluvium does not exist at the location identified by BAI.
- Well W-0343 (13-5-1) is an alluvial well located on a tributary to Pinabete Arroyo adjacent to the Burnham Road. This well is recharged by an adjacent man-made pond (Stevenson Well Pond) and is equipped with a hand pump. This well is also referred to as the Stevenson Well.

Well W-0344 (#93) identified as a Pinabete alluvial well several hundred feet south of the permit area at a location adjacent to the Burnham Road was not found in the site reconnaissance.

### *18.2.3 Aquifers and Other Groundwater Resources*

The hydrogeologic units within and adjacent to the permit area that could potentially be affected by proposed mining and reclamation within permit area include:

- The alluvium of the Chaco River, Cottonwood Arroyo, and Pinabete Arroyo
- The coal seams of the Fruitland Formation
- The Pictured Cliffs Sandstone (PCS), located below the Fruitland Formation No. 2 coal seam

Alluvial fill deposits occur in the valley bottoms of the Cottonwood Arroyo and Pinabete Arroyo, within the permit area, along the Chaco River to the west of the permit area and along portions of No Name



Arroyo southwest of the permit area. However, these deposits are not considered Alluvial Valley Floors (AVF). Refer to Section 19 (Alluvial Valley Floors) for information on the negative determination for AVF within and adjacent to the permit area. Portions of the alluvium of Cottonwood Arroyo and Pinabete Arroyo are saturated and will yield water to wells, as evidenced by the dug wells completed in the alluvium of both the Cottonwood Arroyo and Pinabete Arroyo as indicated in Section 18.2.2 ([Exhibit 18.2-1](#)). The alluvium of the Chaco River also contains groundwater as indicated by the dug wells located adjacent to the Chaco River ([Exhibit 18.2-1](#)). As stated in Section 18.2.1, the groundwater is not sufficient for sustained base flow in any of these drainages.

The alluvium of No Name Arroyo was found to be dry based on alluvial monitoring well GM-23, which was installed in 1976 in association with a proposed coal gasification project and screened only in the alluvium of No Name Arroyo. This well was plugged and abandoned in 1994 by BNCC at the request of the OSM. Two new alluvial monitoring wells, NNA-1 and NNA-2, were installed in 1998 at locations upstream and downstream of the No Name Impoundment as shown in [Exhibit 18.2-2](#). Water level monitoring data from these wells further support the dry character of the alluvium along No Name Arroyo. However, saturated conditions may occasionally occur within the alluvium of No Name Arroyo for a relatively short distance downstream of the No Name Impoundment due to seepage from the impoundment. The No Name Impoundment is discussed in Section 18.1.2.

Groundwater is also found in the coal units of the Fruitland Formation and in the PCS, which underlies the Fruitland Formation in the permit area. The geologic strata within the permit and adjacent area dip gently to the east toward the center of the San Juan Basin at an angle of 1 to 2 degrees. A more thorough description of the regional and localized geology of the permit area is provided in Section 17 (Geologic Information). Based on both regional and site-specific information, the Fruitland Formation and associated coal units, and the PCS are unsaturated or partially saturated near the outcrop of these units on the western side of the permit area but become saturated to the east and down dip of the outcrop.

Based on baseline information obtained from water level elevations measured in the wells and piezometers, the general groundwater flow directions in the Fruitland Formation within Area 3, Area 4 North, Area 4 South, and Area 5 of the BNCC mining lease are vertically downward through the interbedded shale and coal units of the Fruitland Formation and into the PCS and laterally within individual coal seams toward the north-northeast with some localized flow toward the topographic lows along the Cottonwood Arroyo and Pinabete Arroyo. Although the vertical hydraulic conductivities of the interbedded shales in the Fruitland Formation are quite low, recharge rates are lower still. Direct recharge rates measured by chloride mass balance methods on undisturbed areas at the Navajo Mine ranged from 0.002 to 0.09 in/yr (Stone 1987). The highest recharge rate of 0.09 in/yr was for valley terraces while the lowest recharge rate of 0.002 in/yr was for badland areas. Recharge from upland flats averaged 0.03 in/yr. Based on the research by Kearns

and Hendrickx (1998), areal recharge is thought to occur during very large precipitation events and during extended wet periods with increasing soil moisture. Recharge is expected to be higher from saturated alluvium and surface impoundments. Although Stone's research (1986 and 1987) did not include recharge estimates for surface impoundments, it does provide an estimate of an average recharge rate of 0.16 in/yr from depressions within reclaimed mine areas at the Navajo Mine.

Based on BNCC's mining experience at Navajo Mine, the coals, overburden, and interburden in the Fruitland Formation are not expected to yield much water during mining. The saturated sands that occur in the Fruitland Formation are of limited extent and only yield significant water when recharged by water from the NIIP. NIIP influences do not extend into the drainages associated with the permit area, although the North Fork of the Cottonwood Arroyo does receive direct discharges of water from irrigation canals. The direct discharges occur when an over supply of water in the canal is released directly to the stream channel. Direct discharge is highly variable, occurs quickly, and can last up to 12 hours. However, usually there is no flow in Cottonwood Arroyo and it retains the characteristics of an ephemeral stream. The pre-mine groundwater in the Fruitland Formation throughout most of the BNCC mining lease will not support beneficial use because of the very low well yields and poor water quality. As indicated in Section 18.2.2, there are no known water supply wells completed in the Fruitland Formation within or adjacent to the permit area.

The PCS is a well-cemented, low-permeability, marine sand and is the first water-bearing unit below the lowest coal seam to be mined (No. 2 coal seam). Based on the information in Section 17 (Geologic Information), the PCS is approximately 110 to 120 feet thick and follows the structure of the Fruitland Formation, dipping to the east at approximately 2 degrees, although the structure varies locally. The PCS conformably overlies the Lewis Shale, with the contact marked by a zone of interbedded sandstones and mudstones in the lower part of the PCS (Stone et.al. 1983). It outcrops just west of the mine area and east of the Chaco River. Within and adjacent to the permit area, the general groundwater flow in the PCS is toward the north. The PCS is also a natural gas reservoir in the San Juan Basin. Stone et.al. (1983) state that the PCS cannot be considered a major aquifer and it is important only because it is the water-bearing horizon immediately underlying the coals in the Fruitland Formation.

Water yields from monitoring wells completed in the PCS at the BNCC's mining lease are quite low. Two of the PCS wells, KPC2007-2 and KPC2007-3, installed within the BNCC Navajo mining lease south of the permit area were quickly pumped or bailed dry during conventional sampling. The yield from PCS monitoring well KPC98-01, located west of the permit area wells was sufficient to sustain a rate of about 0.4 gallons per minute (gpm) during a constant rate pumping test. The fourth PCS monitoring well KPC2007-01 was installed within the permit area. This well was pumped dry after about 140 minutes

during a constant-rate pumping test at a rate of about 0.95 gpm with most of the pumped water derived from well bore storage.

There are no known water supply wells completed in the PCS within or adjacent to the permit area. As indicated in Section 18.2.2, one water supply well, 13-7-2, was installed in the PCS south of the BNCC mining lease near the Burnham Chapter House as shown in [Exhibit 18.2-1](#). This well was originally completed as a water supply for the Burnham Chapter House but was replaced and abandoned due to the poor yield and poor water quality. Another well, 13-15-1, located south of the permit area and within Area 5 of BNCC's mining lease could also be screened in the PCS as discussed in Section 18.2.2.

#### 18.2.3.1 Groundwater Quantity

Monitoring wells and vibrating wire piezometers (VWPs) were installed in the Fruitland coal seams, in the alluvium of Pinabete Arroyo and No Name Arroyo, and in the PCS in 1998 and in 2007 for baseline hydrogeology characterization of Area 4 South and Area 5 of BNCCs mining lease. The No. 3 coal seam was the target for much of the characterization of the Fruitland Coal because the No 3 coal seam is continuous over most of Area 4 South and Area 5 of the BNCC mining lease. The No. 2 and No 3 coal seams are hydrologically connected and sometimes merge within the mining lease area. Three monitoring wells and three VWPs were installed in the No. 3 coal seam. Four VWPs were also installed within the No. 2 coal seam within Area 4 South and Area 5 of the BNCC mining lease.

The upper coal seams (Nos. 6, 7, and 8) do not exist over the entire lease area but outcrop toward the western limits of the mine lease and are washed out within portions of the drainages, particularly along Pinabete Arroyo. The No. 8 coal seam is typically the thickest coal seam and is believed to exhibit the highest hydraulic conductivity of the coals. All coal seams include splits and partings, although these are most extensive in the No. 8 coal seam as indicated in Section 17 (Geologic Information). The No. 8 coal seam depicted in the cross sections in [Exhibit 18.2-2](#) includes splits and partings. The groundwater monitoring and hydrogeologic characterization program for Area 4 South and Area 5 of BNCC's mining lease also included the installation of one monitoring well and one VWP in the No. 8 coal seam, one VWP in the No. 7 coal seam and one VWP in the No. 6 coal seam.

Four monitoring wells and four VWPs were installed in the PCS within Areas 4 South and 5 of the BNCC mining lease. Well KPC2007-03 was installed to measure water levels within the PCS at the western boundary of the BNCC mining lease. The 2007 drilling program work plan called for installation of a No. 2 coal monitoring well at this location along the western boundary of the BNCC mining lease. However, the No. 2 coal seam was observed to be dry during drilling at this location so the well was completed in the upper part of the PCS to monitor water levels. The PCS well KPC2007-02 was installed to measure water levels and to characterize baseline water quality within the PCS up gradient of Area 4 South. Sampling of

this well found high pH and elevated calcium, which is an indication of well-grout influence. Consequently, this well has been used only for water level monitoring in the baseline program. The PCS well KPC2007-01 was installed to measure water levels and to characterize baseline water quality within the PCS within the permit area. The VWP's were installed to measure potentiometric levels within the PCS and various coal units within the permit area. Completion diagrams for the monitoring wells installed in years 1998 and 2007 as well as VWP's installed in 2007 are provided in [Appendix 18.E](#).

Historical water level data collected during the mid-1970s are also available for six wells that were completed in the PCS within or adjacent to the BNCC mining lease for a previously proposed project. The locations for these PCS monitoring wells are shown on [Exhibit 18.2-2](#). Historical baseline water quality data were also obtained at five of these PCS wells. These PCS monitoring wells and piezometers were plugged and abandoned in 1994. Historic water level monitoring data and pumping test data are also available for the PCS well O-1, located at the Burnham Mine situated southeast of BNCC mining lease as shown on [Exhibit 18.2-2](#). These data, together with data from the adjacent Navajo Mine and other regional sources, supplement the recent baseline groundwater information obtained for Area 4 South and Area 5 of BNCC's mining lease.

#### 18.2.3.1.1 Alluvial Aquifer Information

Baseline monitoring of the alluvium of Cottonwood Arroyo was conducted at four alluvial well monitoring locations shown on [Exhibit 18.2-2](#). Baseline water quality information obtained prior to year 1983 from the monitoring wells GM-17 and QACW-2 (GM-18) are included in Appendix 6-C of the Navajo Mine PAP (BNCC 2009). Well GM-17 is completed in the alluvium of North Fork of the Cottonwood Arroyo. A dug well, GM-18, completed in the alluvium of Cottonwood Arroyo west of the permit area, was converted for use as a monitoring well and is designated as QACW-2 in [Exhibit 18.2-2](#). This well was included in the Navajo Mine quarterly monitoring program (OSM Permit No. NM-0003F) (BNCC 2009). However, the well is usually dry and relatively few samples have been obtained during baseline monitoring. Water quality samples could not be obtained from alluvial monitoring well QACW-1 because it was dry or had insufficient water for sampling during baseline monitoring from 1987 through 1998. The well was subsequently removed by the advance of mining operations in Area 3. BNCC has also performed baseline monitoring of well QACW-2B completed in the alluvium of Cottonwood Arroyo west of the permit area as shown in [Exhibit 18.2-2](#). This well is a dug well that has been used for stock water supply and is not owned by BNCC.

Two alluvial monitoring wells, PA-1 and PA-2, were installed in 1998 within the alluvium of Pinabete Arroyo near dug water wells at the locations shown on [Exhibit 18.2-2](#). Two alluvial monitoring wells, NNA-1 and NNA-2, were also installed in the alluvium of No Name Arroyo at locations upstream and downstream of the No Name Impoundment as shown on [Exhibit 18.2-2](#).

Water levels were measured monthly at each of the alluvial monitoring wells. [Table 18.2-2](#) summarizes the water level readings in each of the Pinabete alluvial monitoring wells during the baseline monitoring program. The water level readings in each of the Cottonwood alluvial monitoring wells during the monitoring period are summarized in [Table 18.2-3](#). The No Name alluvial well NNA-2 has been dry during the entire baseline monitoring program. The No Name alluvial well NNA-1, located down gradient from the No Name Impoundment, has been dry except during the latter half of 1998 when seepage associated high water levels in the impoundment provided a source of water for the alluvium at this well. The data for the Pinabete alluvial wells show a decline in water levels during the spring and early summer of 1998 followed by a rise in water levels due to thunderstorm runoff events in late summer and fall of 1998. In 2007, water levels declined slightly from August through December.

Well completion and aquifer test results for the alluvial monitoring wells are summarized in [Table 18.2-4](#). Well completion diagrams for the Pinabete and No Name alluvial wells are provided in [Appendix 18.E](#). Well completion diagrams could not be found for the Cottonwood alluvial wells. Aquifer test data and interpretation results for the monitoring wells installed in year 1998 are provided in [Appendix 18.F](#). The calculated or measured hydraulic conductivities for the Pinabete Arroyo alluvium of 51.3 feet per day (ft/day) ( $1.8 \times 10^{-2}$  centimeter per second (cm/sec)) and 11.1 ft/day ( $4.1 \times 10^{-3}$  cm/sec) are within the range expected for clean sand and are considerably higher than the bedrock values in the area. Well yields from the alluvium, however, are limited by a very low saturated thickness of about 5 feet or less. Saturated thickness in the No Name alluvial wells was insufficient to permit a pumping test or slug test. The hydraulic conductivity of the No Name alluvium is expected to be considerably lower than the Pinabete Arroyo alluvium due to the high percentage of fine-grained alluvial silts and clays, as evidenced by the well logs.

#### 18.2.3.1.2 Fruitland Formation Information

Groundwater production from the Fruitland coal seams is quite limited. The majority of exploration drill holes through the Fruitland Formation within BNCC mining lease Area 4 South and Area 5 did not yield measurable groundwater during drilling. Measurable water was encountered at a few locations. Specifically, three boreholes located within the northeast portion of Area 4 South produced water at rates estimated at greater than 10 gpm. This groundwater is believed to be associated with the No. 6 and the No. 8 coal seams. Measurable water was also encountered in the No. 8 coal seam during completion of the No. 3 Coal seam well KF-98-03. At this location, groundwater was first encountered in the unconsolidated sand and gravel above the No. 8 coal seam at a depth of about 22 feet. The No. 8 coal seam was encountered in the depth interval from 24 to 38 feet. Water was produced at a rate of about 2 to 3 gpm from the coal and the overlying sand and gravel.

In 2007, well KF2007-01 was completed in the No. 8 coal seam to characterize the groundwater near the permit boundary to the east of the No. 3 coal seam well KF-98-03. Well KF2007-01 is the only coal seam well within BNCC mining lease Area 4 South and Area 5 with sufficient yield to permit the application of a constant rate pumping test to determine hydraulic characteristics of the coal. The water yields from wells KF-98-02, KF-98-03, and KF-98-04, completed in the No. 3 coal seam, are all very low and these wells are quickly pumped or bailed dry during conventional sampling. The locations for the four additional coal monitoring wells are shown on [Exhibit 18.2-2](#), along with the wells previously installed for groundwater monitoring within Area 3 at the Navajo Mine. Completion diagrams and lithologic logs for these additional coal monitoring wells are provided in [Appendix 18.E](#).

Potentiometric elevations measured at the monitoring wells and VWP's completed in the Fruitland coal seams within BNCC mining lease Area 4 North, Area 4 South, and Area 5 are provided in [Table 18.2-5](#). Wide fluctuations in water levels in the No. 3 coal seam wells occurred during the 1998 monitoring period. These fluctuations were the result of well development, aquifer testing, and sampling. A considerable amount of time is required for water levels in these wells to approach equilibrium due to the low hydraulic conductivity of the coal. Quarterly sampling using micro-purge sampling techniques was performed for the sampling program starting in 2007 so that the magnitude of fluctuation resulting from sampling was limited.

Well KF-98-04 was designated to be screened in the first saturated bedrock unit adjacent to the alluvium of Pinabete Arroyo near alluvial well PA-1. The purpose of this well was to help evaluate the relationship between water levels in alluvium and water levels in the bedrock underlying the alluvium. The first saturated bedrock below the alluvium was at a depth of about 63 to 64 feet in the No. 3 coal seam, demonstrating that the saturated alluvium within the Pinabete Arroyo at this location is perched above the underlying unsaturated bedrock. Monitoring well KF-98-04 has remained dry throughout most of the 2007-2008 monitoring period, with only 0.1 foot of saturation recorded on October 4, 2007.

Static water level readings could not be obtained monthly at well KF-98-03 after October 4, 2007 because this well was being periodically purged and bailed as part of a program to remove influence from grout that may have penetrated portions of the sand pack surrounding the screened interval in this well. This well and two of the new PCS wells (KPC2007-02 and KPC2007-03) exhibited low yield and pH levels  $\leq 12$ , indicating that the annular space cement grout may have penetrated the bentonite seal on top of the sand pack surrounding the screened interval in these wells during well completion. The grout penetration is believed to be the result of the low hydraulic heads in the coal combined with the high-pressure head of the grout seal placed in the annular space. The monitoring wells with the largest annular cement interval are also the wells with unusually high pH values that are indicative of grout intrusion. The low yield of the No. 3 coal seam at well KF98-03 has also limited the prospect of grout removal by well purging.

Consequently, in the fall of 2007, acid treatment was used to remediate cement contamination of the monitoring well sand pack materials. Due to the very low yield at these wells, bailing and purging of wells KF-98-03 and KPC2007-02 have continued, reducing the times when static water level measurements could be taken at these wells.

In 1998, a displacement (slug) test was performed at well KF-98-02 and bailed recovery tests were conducted at wells KF-98-03 and KF-98-04 to determine transmissivity and hydraulic conductivity in the No. 3 coal seam. Test results found very low transmissivity values ranging from 0.01 to 0.001 square feet per day ( $\text{ft}^2/\text{day}$ ) and hydraulic conductivity values ranging from 0.002 to 0.00013  $\text{ft}/\text{day}$  ( $3.5 \times 10^{-7}$  to  $4.6 \times 10^{-8}$   $\text{cm}/\text{sec}$ ) as summarized in [Table 18.2-6](#). These values are consistent with the hydraulic conductivity values of 0.001, 0.002, 0.0014, and 0.003  $\text{ft}/\text{day}$  estimated for the No. 2, No. 3, and No. 4-6 coal seam wells, respectively, at the KF84-22 well series located at the Navajo Mine Area 4 North ([Table 18.2-6](#)). Well KF84-22A was not tested at this location but hydraulic conductivity values ranging from 0.004 to 0.06  $\text{ft}/\text{day}$  ( $1.4 \times 10^{-5}$  to  $1.4 \times 10^{-6}$   $\text{cm}/\text{sec}$ ) with a geometric mean of 0.033  $\text{ft}/\text{day}$  ( $1.16 \times 10^{-5}$   $\text{cm}/\text{sec}$ ) were estimated from tests at three No. 8 seam coal wells (SJKF84#3, SJKF84#4, and SJKF84#5) located adjacent to the Navajo Mine. These results are comparable to the hydraulic conductivity value of 0.056  $\text{ft}/\text{day}$  ( $2 \times 10^{-5}$   $\text{cm}/\text{sec}$ ) estimated for the No. 8 coal seam well KF2007-01 as described in [Appendix 18.F](#) and summarized in [Table 18.2-6](#).

In a separate set of tests, the transmissivity and hydraulic conductivity values calculated from the observation well response during a pumping test of the No. 8 coal seam well, G-20, located at the San Juan Mine were 0.017  $\text{ft}^2/\text{day}$  and 0.001  $\text{ft}/\text{day}$  ( $3.5 \times 10^{-7}$   $\text{cm}/\text{sec}$ ), respectively (San Juan Coal Company 2009). These results for the hydraulic conductivity of No. 8 coal at the San Juan Mine are lower than the values from well tests at BNCC's mining lease. However, the observation well response from the pumping test for this well at the San Juan Mine is useful because it provides a reliable estimate for the storage coefficient of  $4.2 \times 10^{-4}$  for the No. 8 coal seam.

Potentiometric elevations in the saturated coal units and the underlying PCS were also measured using VWP's installed at five locations throughout BNCC's mining lease in Area 4 South and Area 5 as shown on [Exhibit 18.2-2](#). VWP construction details are provided in [Appendix 18.E](#). Potentiometric elevations measured at the VWP's completed in the coals are summarized in [Table 18.2-5](#). The December 2007 measurements of potentiometric elevations in the coal wells and VWP's were used to estimate the potentiometric surface for the No. 3 and No. 8 coal seams at the site as presented in [Exhibit 18.2-3](#) and [Exhibit 18.2-4](#), respectively. The potentiometric levels measured on July 6, 1989 at the No. 2 and No. 3 coal seams at the KF84-22 well series located north of the permit area were also used in developing the potentiometric surfaces in these exhibits. The potentiometric gradients in both the No. 2 and No. 3 coal

units indicate groundwater flow components toward the north-northeast in the vicinity of these monitoring wells and piezometers.

Potentiometric gradients in the upper coal seams in the vicinity of the permit area are expected to be generally toward the northeast, similar to the gradients observed in the No. 2 and No. 3 coals, although local gradients may be influenced by the lower elevations along Pinabete Arroyo, No Name Arroyo, and Cottonwood Arroyo. The No. 6, No. 7, and No. 8 coal seams outcrop along the valleys of Pinabete Arroyo, No Name Arroyo, and Cottonwood Arroyo within the mining lease area. Field observations of salt deposits and enhanced vegetation production suggest that local discharge may occur from the No. 8 coal at the coal subcrop beneath the Pinabete alluvium as discussed previously in Section 18.2.1.

Potentiometric elevations in the monitored coal units and in the underlying PCS were plotted for four of the nested VWP locations, to depict vertical gradients and possible seasonal patterns. Plots were not prepared for the VWP2007-4 location for the reason that only one VWP was installed in the PCS at this location because the overlying Fruitland coal units appeared to be dry during piezometer installation. [Figure 18.2-1](#) shows consistent potentiometric elevations over time for the No. 2 coal seam and the PCS at location VWP2007-05. The slightly higher potentiometric elevation in the PCS indicates a slight upward gradient from the PCS to the Fruitland Formation at this location.

A plot of the potentiometric levels in the No. 2 and No. 3 coal seams and the PCS at well VWP2007-03 is provided in [Figure 18.2-2](#). The results show consistent downward gradients from the No. 3 coal seam to the PCS. The wide fluctuation in potentiometric levels in well KPC2007-02 is due to the bailing and purging of this well. [Figure 18.2-3](#) shows the potentiometric levels in the PCS and in the upper and lower coal units at the VWP2007-02 location. The results show high downward gradients from the No. 8 coal seam to the No. 3 coal seam and slight upward gradients from the PCS to the No. 3 coal seam.

A plot of potentiometric elevations in the PCS and in No. 6, No. 3, and No. 2 coal seams at well VWP2007-01 is provided in [Figure 18.2-4](#). The results show consistent downward gradients from the No. 6 coal to the PCS, with the highest vertical gradients between the No. 6 and the No. 3 coal seams. The plot also includes water levels measured in the PCS well KPC2007-01 at the VWP2007-01 location. Measured water elevations in well KPC2007-01 are consistently about 6 feet lower than the potentiometric elevation measured in the PCS at VWP2007-01. The VWP in the PCS at this location is installed at the top of the PCS, while the well screen and filter pack extend through about 75 feet of the PCS. The difference between the two measurements suggests that hydrostatic heads are higher at the top of the PCS at this location and decline with depth. Thus, downward gradients are believed to continue through the PCS at this location.



#### 18.2.3.1.3 Pictured Cliffs Sandstone Information

The PCS underlies the Fruitland Formation and follows the structure of the Fruitland coal seams. The PCS is a marginal water resource due to the low permeabilities, poor water quality, gas production, and low yields (Stone et.al. 1983). The PCS conformably overlies and intertongues with the Lewis Shale. As discussed previously, the PCS appears to be on the order of 110 to 120 feet thick within BNCC's mining lease Areas 4 North, Area 4 South, and Area 5.

Well KPC-98-01 was installed in 1998 west of the permit area near the PCS outcrop at the location shown in [Exhibit 18.2-2](#). In 2007, wells KPC2007-01, KPC2007-02, and KPC2007-3 were completed in the PCS at the locations shown in [Exhibit 18.2-2](#). Completion diagrams and lithologic logs for these PCS wells are provided in [Appendix 18.E](#).

VWPs were installed in the PCS at four of the five VWP locations as shown on [Exhibit 18.2-2](#). A VWP was not installed in the PCS at the VWP2007-03 location because monitoring well KPC2007-02 was installed in the PCS at this location. Construction diagrams and lithologic logs for these VWP installations are provided in [Appendix 18.E](#). Potentiometric elevations measured at the PCS wells and the VWPs installed in the PCS are summarized in [Table 18.2-7](#).

Historical water level data collected during the mid-1970s are also available in a report by Science Application, Inc. (1979) for six wells that were completed in the PCS within or adjacent to Area 4 North, Area 4 South, and Area 5 of BNCC's mining lease ([Table 18.2-8](#)). These abandoned PCS monitoring wells are designated as GM wells with water elevations shown on [Exhibit 18.2-5](#). These PCS monitoring wells and piezometers were plugged and abandoned in 1994. Historic water level monitoring data are also available for the PCS monitoring well O-1 located at the Burnham Mine southeast of BNCC's mining lease as shown in [Exhibit 18.2-2](#).

The December 2007 measurements of potentiometric elevations in the PCS wells and VWPs installed in the PCS were used to estimate the potentiometric surface presented in [Exhibit 18.2-5](#). The potentiometric elevations measured during the 1970s at the abandoned PCS monitoring wells were also used to develop this potentiometric surface for the PCS. The potentiometric gradients in PCS indicate an overall northerly gradient. There is a slight easterly component in the gradients at the southern end of the site due to a structural high in the PCS along the southeast perimeter of Area 5 of BNCC's mining lease. There are also local gradients toward the topographic lows along No Name Arroyo, Pinabete Arroyo, and Cottonwood Arroyo.

An aquifer test was conducted in 1975 at well T4-1 installed in the PCS near the western side of Area 5 of BNCC's mining lease as shown in [Exhibit 18.2-2](#). The drawdown and recovery measurements were

recorded at the pumped well and at observation well GM30A, located 55.8 feet from the pumping well, and at observation well T4-2 located 12.5 feet from the pumping well. The top of the PCS is approximately 146 feet below ground surface at the test location while the static water level was at a depth of 134 feet, demonstrating confined conditions at the test location (Science Application Inc. 1979). The results of this aquifer test are summarized in [Table 18.2-9](#), along with the results of tests performed at the PCS monitoring wells installed as part of this baseline monitoring program. The testing results and interpretations performed for the PCS baseline monitoring wells are provided in [Appendix 18.F](#).

The hydraulic conductivity from the recovery response at well GM-30A from the pumping test at the PCS well T4-1 was 0.0016 ft/day ( $5.6 \times 10^{-7}$  cm/sec). The storage coefficient determined from the observation well response at GM-30A was  $3.4 \times 10^{-5}$ . The highest hydraulic conductivity estimate for the PCS near the permit area was 0.02 ft/day ( $7.0 \times 10^{-6}$  cm/sec) obtained from the test at monitoring well KPC-98-01, located northwest of the mining lease as shown on [Exhibit 18.2-2](#). The PCS is unconfined at this location. The results for this well are consistent with the aquifer test results of 0.032 ft/day ( $1.1 \times 10^{-5}$  cm/sec) from a slug test at Well O-1 completed in the PCS at the Burnham Mine but higher than the range from 0.01 to 0.0001 ft/day ( $3.5 \times 10^{-6}$  to  $3.5 \times 10^{-8}$  cm/sec) obtained from the slug tests at the three other PCS monitoring wells as summarized in [Table 18.2-9](#).

Pumping test results for the PCS monitoring well O-1 in the Burnham Mine permit application package are on file in the library of the OSM in Denver, CO. In this well test, pumping at a relatively high rate of 18.3 gpm could be sustained for only 8.7 minutes when most of the well-bore storage water was removed and the test had to be terminated. Although the results were interpreted in the Burnham Mine permit application package as a pumping test, this approach is not correct due to the predominant influence of well-bore storage. Consequently, the well test results have been reinterpreted as a slug test in this report. Slug test results indicate a hydraulic conductivity of 0.032 ft/day ( $1.1 \times 10^{-5}$  cm/sec).

#### 18.2.3.2 Groundwater Quality

The water quality characteristics of the Cottonwood, Pinabete and No Name alluvium, the Fruitland coal seams, and the underlying PCS have been determined from the baseline groundwater monitoring. The results are presented in the subsequent subsections and show that the groundwater within and adjacent to the permit area is poor and suitable only for marginal livestock use based on the relevant groundwater use criteria listed [Table 18.2-10](#). The use criteria in [Table 18.2-10](#) are not enforceable standards with respect to groundwater and are included only as a reference for the suitability of the groundwater quality for domestic water supply and for livestock use. These use criteria are mostly derived from the Navajo Nation surface water quality criteria (NNEPA 2008) for domestic water supply and for livestock watering use. Lardy, Stoltenow, and Johnson (2008) provide relevant livestock watering criteria for TDS, sulfate and fluoride but do not provide a livestock use criterion for chloride.

#### 18.2.3.2.1 Alluvial Groundwater Quality

Quarterly samples were obtained from the two alluvial monitoring wells installed in Pinabete Arroyo and four alluvial wells within the Cottonwood Arroyo. No samples have been obtained from No Name well NNA-2 because the well was dry throughout the baseline monitoring program in 1998 and in 2007-2008. Saturated conditions occurred during the latter half of 1998 at the No Name alluvial monitoring well NNA-1, located below the No Name Impoundment. Two quarterly samples were obtained from this well during this period. At other times during the baseline monitoring period this well has been dry and no samples were obtained. QACW-2 is usually dry and relatively few samples have been obtained during baseline monitoring. Water quality samples could not be obtained from alluvial monitoring well QACW-1 because it was dry or had insufficient water for sampling during baseline monitoring from 1987 through 1998. The analytical results for the water quality samples from these wells are summarized below.

The baseline water quality monitoring results for the Cottonwood alluvial wells are summarized in [Table 18.2-11](#). These results show the water quality of the alluvium of Cottonwood Arroyo to be a sodium-sulfate type of poor water quality with relatively high but variable TDS concentrations. TDS concentrations at monitoring well QACW-2B, located near the mouth of Cottonwood Arroyo, ranged from 2,590 to 3,615 mg/L. This monitoring well is a stock water well that was converted to a monitoring well and is referred to as well 13-R-28A in [Exhibit 18.2-1](#). Median sulfate concentrations exceed recommended livestock use criteria at all the Cottonwood alluvial wells. Median concentrations of TDS and sulfate in the groundwater within the Cottonwood alluvial wells also exceeds the U.S. Environmental Protection Agency (USEPA) Secondary Drinking water use criteria listed [Table 18.2-10](#). Fluoride concentrations fluctuate in the alluvial groundwater and are often above relevant criteria for livestock and drinking water use.

Water quality analytical results from quarterly monitoring at Pinabete alluvial wells, PA-1 and PA-2, are provided in [Table 18.2-12](#) and [Table 18.2-13](#), respectively. These results show the water quality of the alluvium of Pinabete Arroyo to be a sodium-sulfate type with TDS concentrations ranging from 1,500 to 4,300 mg/L. Water within the alluvium is unsuitable for drinking water use due to TDS, sulfate, fluoride, iron, and manganese concentrations above secondary drinking water standards. The quality of the alluvial groundwater varies although the TDS, sulfate, and fluoride concentrations usually exceed relevant criteria for livestock use.

Water quality analytical results in [Table 18.2-14](#), from sampling of the No Name Arroyo alluvial well NNA-1, show the water to be a sodium-sulfate type similar to Pinabete Arroyo but with much higher sulfate, sodium, and TDS concentrations. Water quality within the alluvium downstream of the No Name Impoundment is unsuitable for either drinking water or livestock water use.

Some information on the baseline water quality in the Chaco River Alluvium is provided by Thorn (1993). These results show considerable variability in the alluvial water quality with TDS concentrations ranging from 742 to 11,900 mg/L, sulfate concentrations from 350 to 6,600 mg/L, and fluoride concentrations ranging from 0.4 to 1.7 mg/L. Additional water quality information for the Chaco River alluvium is included in the well inventory included in Appendix 6.E of the Navajo Mine PAP (OSM Permit No. NM-0003F) (BNCC 2009). The available water quality information from this well inventory show TDS concentrations ranging from 1,950 mg/L to 3,110 mg/L and sulfate concentrations ranging from 1,100 to 1,790 mg/L at wells located west of Areas 2, 3 and 4 at the Navajo Mine.

#### 18.2.3.2.2 Fruitland Formation Groundwater Quality

The No. 3 coal seam well KF-98-04 has been essentially dry throughout the baseline monitoring period, with the exception of about 3 feet of initial saturation following well completion. Although a sample was obtained from this well in March 1998 following well completion, the well could not be purged and the water sample collected immediately following well completion cannot be considered to be representative of baseline conditions.

Water quality analytical results from the baseline sampling of the No. 3 coal seam well KF-98-02 are provided in [Table 18.2-15](#). Results indicate some initial influence from drilling fluids or from the annular grout seal in the first two samples from this well. The reduction in both the pH and calcium concentrations with subsequent sampling suggests the reduction of any influence from drilling fluids or from the annular grout seal in subsequent samples from this well. The pH levels in this well have declined with time and the November 2007 results were within the range from 7 to 9 that is generally expected for the Fruitland coals within the San Juan Basin.

As shown in [Table 18.2-15](#), water quality within the No. 3 coal seam at monitoring well KF-98-02 is unsuitable for drinking water use due to concentrations of TDS, chloride, and boron above the Navajo Nation water quality criteria for drinking water use. The TDS concentrations in water at this monitoring location also exceed the relevant criterion for livestock use. Based on the recent samples from the No. 3 coal seam well KF-98-02, the groundwater in the No. 3 coal seam at this location is a sodium-bicarbonate-chloride type, with TDS of about 3,300 mg/L ([Table 18.2-15](#)). The ion composition results are consistent with the baseline coal water quality monitoring data at the Navajo Mine, which show the coal seams to be of a sodium-bicarbonate-chloride type, although TDS concentrations are higher at the Navajo Mine wells as indicated in [Table 18.2-16](#).

[Table 18.2-16](#) provides median concentrations from baseline monitoring of coal wells at the Navajo Mine. Water quality monitoring data from the coal wells located within or adjacent to the Navajo Mine permit area show very high concentrations of TDS in the coal seam groundwater, with median concentrations at

individual wells ranging from 2,770 mg/L to 13,400 mg/L. The concentrations of TDS, chloride, sodium, and bicarbonate are lower in the No. 3 coal seam monitoring well KF-98-02 in [Table 18.2-15](#) in comparison to the median concentrations observed at the No. 3 coal seam monitoring well KF84-21A in [Table 18.2-16](#). Lower concentrations of these constituents would be expected at well KF-98-02 because it is located up gradient from well KF84-21A and closer to the likely recharge source.

The coal seam water quality results in [Table 18.2-16](#) show that TDS concentrations increase with depth and distance from the outcrop. Furthermore, TDS concentrations as high as 50,000 mg/L have been observed in the Fruitland coal units east and down dip of the Navajo Mine permit area (BNCC 2009). The TDS concentrations ranged from 43,035 to 50,810 mg/L at monitoring wells SJKF84#2 and SJKF84#3 installed in the No. 8 coal down dip of the Navajo Mine (Chapter 6, Navajo Mine Permit Application Package, BNCC 2009). The lower concentrations of TDS occur within close proximity to the coal outcrop, although concentrations of sulfate are higher near the outcrop and sulfate is generally absent down dip due to sulfate reduction.

Water quality analytical results from the baseline sampling of the No. 8 coal seam monitoring well KF2007-01 are provided in [Table 18.2-17](#). There was considerable fluctuation in the pH and in the concentrations of TDS and major ions observed in samples from this well. These fluctuations are not uncommon after completion of wells with very low rates of water production because it is not possible to fully develop the well. Stabilization of water quality parameters is expected to occur over time, similar to what has occurred at well KF-98-02. Water quality within the No. 8 coal at this monitoring location is unsuitable for drinking water due to concentrations of TDS, chloride, fluoride, and sulfate that are above the USEPA secondary drinking water use criteria. The sulfate and TDS concentrations in coal water at this monitoring location often exceed relevant criteria for livestock use.

Baseline monitoring of coal wells located within and adjacent to the permit area indicated that well yields at most locations would not be sufficient to sustain use for livestock water supply. In limited locations where the coals may yield sufficient to occasionally fill a stock tank, the water could provide for marginal livestock use, although the recommended livestock criteria for TDS and sulfate are usually exceeded. The water quality would result in restrictions for use as a supply for young calves or as a long-term supply for cattle. Also, the water in the coal units would not be suitable for drinking water due to elevated TDS, chloride, boron, and sulfate concentrations. Based on the trends observed from sampling of coal wells at the BNCC mining lease, concentrations of TDS, bicarbonate, and chloride appear to increase with depth and distance from the outcrop but sulfate concentrations appear to decrease.

There is also an apparent trend of increasing TDS, chloride, and bicarbonate concentrations and decreasing sulfate concentrations toward the north-northeast in the direction of the potentiometric gradient. This trend

appears in concentrations observed at the No. 8 coal seam well KF84-22A in comparison with the concentrations observed at the No. 8 coal seam well KF84-18B located north-northeast of well KF84-22A. A similar trend is also observed in the comparison of results for the No. 3 coal seam well KF-98-02 with the down gradient No. 3 coal seam well KF84-21A.

Groundwater chemistry changes or evolves along its flow path from the recharge area to the discharge area. Precipitation is low in TDS, is naturally weakly acidic, and contains bicarbonate due to the solution of carbon dioxide in the air. In this portion of the San Juan Basin, the precipitation reaching the ground is immediately neutralized and acquires sodium, sulfate, and other ions. Water that has only a short residence time in the ground is still typically high in TDS concentrations, with sodium, sulfate, and bicarbonate the dominant ions as indicated by both the surface water and alluvial groundwater samples. Calcium is also present due to dissolution of calcium carbonate, but at concentrations that are considerably lower than sodium. Chloride concentrations are typically lower near the recharge areas, although both chloride and TDS can vary with the spatial variation in recharge rates and frequency of leaching of salts from the unsaturated zone.

As groundwater migrates through the saturated zones it is no longer in contact with atmospheric carbon dioxide and its capacity to dissolve carbonates diminishes. The chemistry of the groundwater continues to evolve as other soluble minerals dissolve and cation exchange processes reduce the proportion of calcium and increase the proportion of sodium in solution. Sulfate reduction also occurs when groundwater transitions from oxidizing to reducing conditions, particularly within the coals.

#### 18.2.3.2.3 Pictured Cliffs Sandstone Groundwater Quality

Water quality analytical results from the baseline sampling of PCS well KPC-98-01 are provided in [Table 18.2-18](#). When the initial sample was collected from PCS monitoring well KPC-98-01 in 1998, it showed some influence of drilling fluids based on the low TDS, sulfate, and chloride and higher pH and nitrate observed in the initial well sample as shown in [Table 18.2-18](#). It is suspected that the well was not fully developed due to low permeability and limited saturation. Sampling results starting in 2007 are more consistent and representative of baseline conditions within the PCS at this location. Based on the recent samples, the groundwater in the PCS at this location is a sodium-sulfate-bicarbonate type with TDS above 6,000 mg/L.

The ion composition results in water samples from well KPC-98-01 are consistent with the results from well KPC2007-01 ([Table 18.2-19](#)). TDS concentrations are quite similar at the two PCS wells with concentrations at well KPC2007-01 slightly below 6,000 mg/L and concentrations at well KPC-98-01 slightly above 6,000 mg/L. The groundwater in the PCS at these two locations is unsuitable for either domestic or livestock use due to the high TDS and sulfate concentrations.

Water quality monitoring data for the PCS were also available from samples collected during the mid-1970s from five wells that were completed in the PCS within or adjacent to Area 4 North, Area 4 South, and Area 5 of BNCC's mining lease. The locations for these PCS monitoring wells are shown on [Exhibit 18.2-2](#).

Water quality analytical results of the baseline samples from PCS monitoring well GM-21, located within Area 5, are provided in [Table 18.2-20](#). The water quality results are consistent with the results from wells KPC-98-01 and KPC2007-01. The groundwater is a sodium-sulfate-bicarbonate type with TDS above 6,000 mg/L.

Historic baseline water quality results from PCS monitoring well GM-20 are summarized in [Table 18.2-21](#). This well was located within the center of Area 4 South of BNCC's Navajo mining lease. These results indicate TDS concentrations between 5,000 and 6,000 mg/L, which are comparable with results from the other PCS monitoring wells. The groundwater in the PCS at this location is a sodium-sulfate-chloride-bicarbonate type, with higher chloride concentrations than in the other nearby PCS monitoring wells. The earlier samples from this well also show an elevated groundwater pH. It is quite likely that this well also encountered some influence of grout intrusion that was not removed during well development or grout curing. The elevated pH influence does not appear in the later samples from this well.

Baseline water quality data for PCS monitoring well GM-19 are summarized in [Table 18.2-22](#). This well was located within the proposed permit area. The resulting water type is similar to the water type from PCS monitoring well GM-20, although TDS concentrations are higher, ranging between 7,810 and 9,270 mg/L, with corresponding higher concentrations of sulfate, chloride, sodium, and bicarbonate.

Baseline water quality data for PCS monitoring well GM-30A are provided in [Table 18.2-23](#). This well was located on the west side of Area 5 of BNCC's mining lease. The results indicate a sodium-sulfate-chloride type with TDS concentrations between 6,000 and 7,000 mg/L, and are comparable with the results from PCS monitoring wells within Areas 4 North, Area 4 South, and Area 5 of BNCC's mining lease. The ion balance in the first sample from this well was poor but improved in the second sample. Anion-cation balances greater than  $\pm 0.10$  are often an indicator of poor quantitative results. Sometimes, a lack of ion balance can be explained by the presence of high metals in acidic waters or soluble silica in alkaline waters that may not have been considered in calculating the ion balance. However, in this case, it appears that the lack of balance is the low sulfate concentration reported in the first sample, which appears to be erroneous. All the other major ions were consistent between the two samples.



The water sample results from well GM-28 are not included in this report because the ion balance was poor with 37% and 48% difference in the two samples. This well was located north of the permit area, as shown in [Exhibit 18-2-2](#). Despite the poor ion balance, results for TDS are meaningful. The TDS concentrations in the samples from this well ranged from 4,334 to 6,580 mg/L. These results are consistent with the TDS concentrations observed at other PCS monitoring wells and slightly lower than the TDS concentration observed at well GM-19 located within the permit area.

In summary, groundwater quality data from monitoring wells located within and adjacent to the permit area indicate the groundwater in the PCS has high TDS concentrations, ranging from 5,000 mg/L to over 9,000 mg/L. Sulfate is the dominant anion, although the concentrations of chloride and bicarbonate are also relatively high. Sodium is the dominant cation. Magnesium and calcium concentrations are quite low and are typically less than the potassium concentrations, although potassium was not included in the samples from the GM wells that were collected during the 1970s. Generally, water quality changes are observed in the first few samples obtained from monitoring wells, apparently due to the difficulty in developing these low-yield wells. Thus, samples obtained after the initial two samples are believed to provide a better representation of baseline conditions.

The high concentrations of TDS, sulfate, chloride, and boron in the water from the PCS within and adjacent to the permit area preclude its use for domestic purposes. The PCS is also a poor source for livestock watering due to the very high TDS and sulfate concentrations, and low permeability and low yield, as stated in Section 18.2.3.1.3. The TDS and sulfate concentrations are lower in the water in the alluvium of Pinabete Arroyo, making it a better source for livestock use, although the TDS and sulfate concentrations in the alluvium are often above relevant criteria for livestock use.

#### *18.2.4 Groundwater Resources Information Collection and Analysis*

The baseline groundwater evaluation included a review of reports and data concerning groundwater resources of the region from New Mexico and federal agencies as well as the information provided in the permit application package and the groundwater monitoring reports for BNCC's Navajo Mine and CONSOL Energy's Burnham Mine (monitoring reports on file at the OSM Library in Denver, Colorado). BNCC has also conducted extensive drilling within the permit area which, together with data from the adjacent Navajo Mine and the nearby Burnham Mine, provide information about the geology and groundwater hydrology of the permit area and surrounding areas. BNCC also implemented a groundwater monitoring program in 1998 and in 2007 and 2008 to obtain site-specific information on groundwater levels, aquifer characteristics, and groundwater quality for the previously proposed Navajo Mine Extension Project. The baseline monitoring program and assessment were developed in accordance with the "Work Plan for Baseline Groundwater Hydrology for the Navajo Mine Extension Project" submitted to OSM on



May 23, 2007. The focus of this baseline monitoring program encompassed areas within and adjacent to the permit area.

An inventory of permitted wells and springs was conducted based on information from several sources, including the New Mexico Office of the State Engineer (NMOSE) (2010) Navajo Settlement Agreement, the inventory of wells and springs conducted by Billings and Associates, Inc (BAI) in 1985 for the Navajo Mine, wells identified in the “Groundwater Operations Manual and Well Survey for Navajo Mine and Vicinity” that was completed by Metric Corporation (1991), wells found in review of permits on file at the Navajo Nation Water Resource Management office in Fort Defiance, Arizona and a site reconnaissance for springs, seeps, and wells located within the permit area and adjacent area. Some of the data used in the discussion of baseline conditions were collected by other companies or organizations for other projects. As a result, the particular analytes considered and the associated detection limits may be slightly different from those included in BNCC’s baseline monitoring in years 2007 and 2008. Efforts have been made to address these differences within the discussion of the data or in the tables used to report the results. Quality assurance and quality control information for the 2007-2008 groundwater data is provided in [Appendix 18.G](#).

### **18.3 Hydrologic Model**

Groundwater models are useful to support the interpretation of baseline hydrogeologic information. Furthermore, groundwater models are required for the predictive evaluations needed to prepare a probable hydrologic consequence (PHC) assessment of proposed mining and reclamation activities. Groundwater models used for a PHC assessment can range from simple empirical equations to complex numerical computer simulations of groundwater flow and chemistry.

Site-specific data or data representative of the site conditions are needed to apply groundwater models. Extrapolation of data from adjacent or nearby areas or using typical values for parameters from similar hydrogeologic environments is acceptable when the similarity of the areas is established. Numerical groundwater flow models can help to develop a better understanding of the hydrogeologic system, including the groundwater flow relationships between hydrogeologic units and between surface water and groundwater. Model calibration can also serve to revise the conceptual model of the groundwater system and provide a better assessment of the properties of hydrogeologic units on a regional scale that cannot be obtained solely from local pumping testing results.

The first step in developing a groundwater model is to establish the objectives of the study. Specific objectives of the groundwater model are as follows:

- The first objective is to provide a better understanding of the baseline groundwater flow systems within and adjacent to the proposed mining location.

- The second objective is to provide a better understanding of the likely groundwater changes that may occur during and after mining.

#### *18.3.1 Groundwater Model Development*

A multilayer, numerical, groundwater flow model has been developed to model the groundwater flow systems within and adjacent to the permit area. A detailed presentation of the numerical groundwater flow model is included in Appendix 41.B, in Section 41 (Probable Hydrologic Consequences). This report includes a description of the conceptual model of the groundwater flow system. A conceptual groundwater model is a complex hypothesis of the characteristics and functions of a hydrogeologic system, including recharge and discharge relationships, groundwater flow within and between hydrogeologic units, and the expected properties of these hydrogeologic units. An essential part of both the conceptual and numerical models is a graphical representation of the horizontal and vertical boundaries of the hydrogeologic system (the model domain) and the delineation of the hydrogeologic units within the model domain that are believed to have the primary controlling influence on groundwater flows. Another element of the conceptual model is to define, to the extent possible, the properties of these hydrogeologic units, including the thickness, hydraulic conductivities, and storage characteristics across the model domain. The conceptual model also includes the hydrogeologist's understanding of spatial relationships between and approximate rates of recharge and discharge, including the groundwater inflows and outflows from the model domain.

The delineation of the hydrogeologic units within and adjacent to permit area was based on the extensive geologic and groundwater information obtained from a variety of sources, including the baseline information presented in this baseline Section. Although the coal geology is complex with multiple coal bed splits and pinch outs, there is good correlation and spatial continuity for particular coal zones, or seams, at the Pinabete permit area and adjacent Navajo Mine. These coal seams may feature one coal bed, or they may include splits with multiple coal beds. For these reasons, the conceptual hydrogeologic model and the numerical groundwater model for the permit area and adjacent area handle the individual coal zones, or seams, as separate and distinct hydrogeologic units. The PCS, the first hydrogeologic unit below the Fruitland Formation, has been included in the groundwater flow model. The top of the Lewis Shale, below the PCS, has been included as the base of the model domain. The delineation of these hydrogeologic units within the permit area was created from the extensive geologic and groundwater information developed for the project. Information was also obtained from a variety of sources to help delineate the hydrogeologic units and define groundwater conditions for the portions of the model domain that are beyond the limits of the permit area.

### 18.3.2 Baseline Groundwater Model Results

The multilayer groundwater model was calibrated to obtain a good match with potentiometric surfaces and water levels established from the baseline groundwater studies at the permit area while maintaining consistency with the site-specific recharge estimates from Stone (1986) and the range of hydraulic conductivities associated with each hydrogeologic unit. During model calibration, hydraulic conductivities were applied only for the entire hydrogeologic unit and not spatially within a unit. Without a consistent geologic basis, spatial adjustments in hydrologic conductivities would lead to over-parameterization of the model to match modeled potentiometric levels with observed values. Although some of the differences between the modeled and observed potentiometric levels may be associated with spatial variation in hydrogeologic properties within a hydrogeologic unit, the chosen method for model calibration allows for the overall groundwater flow within each hydrogeologic unit and between units to be represented by the calibrated groundwater model.

Generally, a shale zone such as the Lewis Shale would be considered as an impermeable boundary. However, given the low recharge rates at the permit area, the overall low permeability of the Fruitland Formation shales and coals, and the relatively low permeability of the PCS, the flow conditions at the boundary between the PCS and Lewis Shale were found to be significant for calibrating the groundwater flow model. Providing for downward flow from the PCS into the Lewis Shale was required in order to reach an adequate calibration with recharge rates consistent with the measurements from Stone (1987). Downward flow and downward gradients are also indicated by hydrogeologic studies and tests of the Lewis Shale and the PCS immediately west of the permit area (Science Application, Inc. 1979).

[Table 18.3-1](#) shows the relationship between the modeled recharge rates and the measurements by Stone (1987). Outside of the alluvial valleys, recharge rates were adjusted by slope within the range of estimates from Stone (1987) for badland areas and for upland flats. The modeled potentiometric surface for the PCS, the No. 3 coal seam, and the No. 8 coal seam are provided in [Figure 18.3-1](#), [Figure 18.3-2](#), and [Figure 18.3-3](#), respectively. These results are consistent with the potentiometric surfaces developed from baseline monitoring in Section 18.2.4. However, the modeled potentiometric surfaces extend beyond the limits that could be depicted from well measurements. These potentiometric surfaces and flow patterns are consistent with the conceptual model and all the geologic and hydrogeologic information and the specified boundary conditions.

The results in [Figure 18.3-1](#) show a component of groundwater flow from the PCS to the topographic lows along the west side of the model domain in the valleys of Brimhall Wash, No Name Arroyo, Pinabete Arroyo, and Cottonwood Arroyo. Although portions of the PCS along the western outcrop remain unsaturated, as indicated in [Figure 18.3-1](#), the model estimates potentiometric elevations for these unsaturated zones.

The results for the No. 3 coal seam in [Figure 18.3-2](#) also show a component of groundwater flow to the topographic lows along the west side of the model domain in the valleys of No Name Arroyo, Pinabete Arroyo, and Cottonwood Arroyo. The No. 3 coal seam is not present over a portion of the Brimhall Wash drainage or along the western portion of the model domain. Also, the No 3 coal seam is unsaturated in areas along the western outcrop and remains unsaturated in the modeled potentiometric surface as indicated in [Figure 18.3-2](#). A similar pattern is observed in [Figure 18.3-3](#) for the No. 8 coal seam, although this coal is not present over a large portion of the Brimhall drainage or within a large portion of the No Name Arroyo and Pinabete Arroyo valleys within the permit area. In addition to the flow toward the topographic lows, there is a component of flow down dip to the northeast. Portions of the No. 8 coal seam near the western outcrop are unsaturated, as shown in [Figure 18.3-3](#). Not shown in these figures for individual hydrogeologic units are the overall downward gradients and downward flow between units. In fact, the model predicts perched groundwater conditions in the shallower coals along the western portion of the permit areas as depicted by the north-south section in [Figure 18.3-4](#).

The calibrated numerical model helps confirm the conceptual model. The numerical model is well constrained and consistent with the recharge rates measured by Stone (1987) and with the hydraulic conductivities and heads measured within the various hydrogeologic units in the model domain.

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Table 18.1-1 Watershed Areas for Permit Area and nearby USGS Gages

| Name of watershed / description of location                | Watershed (sq miles)             |  |                  | USGS gage |
|--|----------------------------------|--|------------------|-----------|
|  | Upstream of Coal Permit Boundary | Upstream of exit from Coal Permit Boundary | Entire watershed |           |
| Drainages intersecting permit area upstream and downstream |                                  |  |                  |           |
| South Fork of Cottonwood Arroyo                            | 18.3                             | 20.7                                       | 21.1             | NA        |
| Pinabete Arroyo  | 51.8                             | 55.7                                       | 60.3             | NA        |
| Drainages outside of permit area                           |                                  |  |                  |           |
| No Name Arroyo   |                                  |  | 11.5             | NA        |
| Regional gages   |                                  |  |                  |           |
| Teec-Ni-Di-Tso Wash  | -                                | -  | 7.2              | 9367934   |
| Burnham Wash   | -                                | -  | 8.6              | 9367936   |
| Chaco River  | -                                | -  | 3,640            | 9367938   |
| Chaco River  | -                                | -  | 4,350            | 9367950   |
| San Juan River at Farmington, NM                           | -                                | -  | 7,240            | 9365000   |
| San Juan River at Shiprock, NM                             | -                                | -  | 12,900           | 9368000   |

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Table 18.1-2 Baseline Peak Flow Measurements on Pinabete Arroyo and No Name Arroyo in 1997, 1998, 2007, and 2008

| Monitoring period | Peak Flow Measurement - Q (cfs)           |   |   |   |
|-------------------|---|---|---|---|
|                   | Pinabete Arroyo upstream (upper Pinabete) | Pinabete Arroyo downstream (lower Pinabete) | No Name Arroyo upstream (upper No Name) | No Name Arroyo downstream (lower No Name) |
| Nov. 1997         | 0   | 0   | 0                                       | 0   |
| Dec. 1997         | 0   | 0   | 0                                       | 0   |
| Jan. 1998         | 0   | 0   | 0                                       | 0   |
| Feb. 1998         | 0   | 0   | 0                                       | 0   |
| Mar. 1998         | 0   | 0   | 0                                       | 0   |
| Apr. 1998         | 0   | 0   | 0                                       | 0   |
| May 1998          | 0   | 0   | 0                                       | 0   |
| June 1998         | 0   | 0   | 0                                       | 0   |
| July 1998         | 22.5                                      | 1717  | 1.5                                     | 0   |
| Aug. 1998         | 1079                                      | 2307  | *                                       | *   |
| Sept. 1998        | 0   | 4.9   | 9.5                                     | 74  |
| Oct. 1998         | 1073**                                    | 119**                                       | 17.7**                                  | 38.8**                                    |
| Nov. 1998         | 308                                       | 145   | 3.9                                     | 9.9                                       |
| Dec. 1998         | 0   | 0   | 0                                       | 0   |
| Aug. 2007         | 0.68                                      | -   | -                                       | 111.06                                    |
| Oct. 2007         | 2.04                                      | 16.41                                       | 0.73                                    | 5.66                                      |
| Dec. 2007         | 2.04                                      | 36.32                                       | 0.73                                    | 2.62                                      |
| Feb. 2008         | 4.46                                      | 24.05                                       | 19.14                                   | 10.19                                     |
| July 2008         | 7.53                                      | 46.62                                       | NA                                      | 11.64                                     |
| Aug. 2008         | 0.44                                      | NA  | NA                                      | 0.00                                      |

Q - runoff rate

cfs - cubic feet per second

\* Site could not be accessed on 26 Aug 1998. Measurement taken in September is likely due to the storm on 21 Aug 1998

\*\*October flows determined from measurements taken on 7 Nov. 1998



Table 18.1-3 Comparison of Average Annual Flows at Five Regional USGS Gages for Selected Years Between 1978 and 2010

|   | Teec-Ni-Di-Tso Wash | Burnham Wash | Chaco River | Chaco River | San Juan at Farmington | San Juan at Shiprock | Flow distribution quartile |
|---|---------------------|--------------|-------------|-------------|------------------------|----------------------|----------------------------|
| Area (sq miles)                                       | 7.2                 | 85.2         | 3640        | 4350        | 7,240                  | 12,900               |                            |
| USGS ID   | 9367934             | 9367936      | 9367938     | 9367950     | 9365000                | 9368000              |                            |
| Selected years (flows in cubic feet per second [cfs]) |                     |              |             |             |                        |                      |                            |
| 1978  | 0.072               | 0.657        | 15.2        | 34.6        | 1303                   | 1186                 | 25%-50%                    |
| 1979  | 0.207               | 0.333        | 77.7        | 85.1        | 3574                   | 3706                 | 75%-100%                   |
| 1980  | 0.121               | 0.132        | 10.7        | 25.2        | 2475                   | 2588                 | 50%-75%                    |
| 1981  | 0.029               | 0.058        | 7.35        | 20.8        | 1276                   | 1309                 | 25%-50%                    |
| 1982  | 0.337               | 0.396        | 19.1        | 51.2        | 1967                   | 1940                 | 50%-75%                    |
| 1998  | ND                  | ND           | ND          | ND          | 2036                   | 1760                 | 50%-75%                    |
| 2007  | ND                  | ND           | ND          | ND          | 1782                   | 1838                 | 25%-50%                    |
| 2008  | ND                  | ND           | ND          | ND          | 2597                   | 2574                 | 50%-75%                    |
| 2009  | ND                  | ND           | ND          | ND          | 1298                   | 1247                 | 25%-50%                    |
| 2010  | ND                  | ND           | ND          | ND          | 1111                   | 1031                 | 0%-25%                     |

**Lowest Quartile** 1990, 2010  
**25%-50%** 1978, 1981, 1991, 2007, 2009  
**50-75%** 1980, 1982, 1992, 1994, **1998 (close to average)**, 2008  
**Top Quartile** **1979 (very high)**, 1993, 1995

ND - No data collected; gages not operated after 1983 water year  
 Source: USGS 2009

Table 18.1-4 SEDCAD™ 4 Estimated Peak Discharge and Sediment Yield

| Watershed location         | SEDCAD designation | 2yr-6hr event<br>(0.85 inches) |                          | 10yr-6hr event<br>(1.28 inches) |                          | 25yr-6hr event<br>(1.56 inches) |                          | 100yr-6hr event<br>(2.04 inches) |                          |
|----------------------------|--------------------|--------------------------------|--------------------------|---------------------------------|--------------------------|---------------------------------|--------------------------|----------------------------------|--------------------------|
|                            |                    | Peak discharge<br>(cfs)        | Sediment<br>yield (tons) | Peak dscharge<br>(cfs)          | Sediment<br>yield (tons) | Peak discharge<br>(cfs)         | Sediment<br>yield (tons) | Peak discharge<br>(cfs)          | Sediment<br>yield (tons) |
| South Fork Cottonwood      | Structure 21       | 729                            | 4,561                    | 1,588                           | 11,292                   | 2,220                           | 16,455                   | 3,439                            | 26,631                   |
| Cottonwood at CSN-1        | Structure 36       | 1,258                          | 10,716                   | 2,871                           | 27,297                   | 4,106                           | 40,745                   | 6,428                            | 67,549                   |
| Pinabete upstream          | Structure 6        | 406                            | 2,251                    | 1,124                           | 8,093                    | 1,715                           | 13,703                   | 2,879                            | 25,544                   |
| Pinabete downstream        | Structure 8        | 396                            | 2,147                    | 1,099                           | 7,808                    | 1,678                           | 13,103                   | 2,817                            | 24,239                   |
| No Name upstream           | Structure 2        | 54                             | 69                       | 231                             | 302                      | 297                             | 461                      | 523                              | 868                      |
| No Name downstream         | Structure 5        | 114                            | 290                      | 564                             | 1,544                    | 661                             | 1,781                    | 1,022                            | 3,091                    |
| Cottonwood at Confluence   | Structure 37       | 1,250                          | 10,744                   | 2,839                           | 30,644                   | 4,049                           | 40,586                   | 6,325                            | 67,181                   |
| Unnamed Tributary to Chaco | Structure 1        | 50                             | 158                      | 137                             | 497                      | 205                             | 788                      | 334                              | 1,380                    |

cfs - cubic feet per second

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Table 18.1-5 Peak Discharge Estimates for Watersheds Based on Drainage Area Using Regional Equations

|                   | Discharge area<br>(mi <sup>2</sup> )<br>A | Average basin<br>elevation (ft msl)<br>E | Average basin slope<br>(%)<br>S | Peak discharge (cfs) |       |        |        |        |        |         |
|-------------------|---|--|---------------------------------|----------------------|-------|--------|--------|--------|--------|---------|
|                   |   |  |                                 | Q2                   | Q5    | Q10    | Q25    | Q50    | Q100   | Q500    |
| No Name Arroyo    | 11.5                                      | 5503.77                                  | 1.54                            | 294                  | 1,943 | 3,361  | 6,456  | 9,482  | 13,764 | 27,068  |
| Pinabete Arroyo   | 58.4                                      | 5880                                     | 1.82                            | 568                  | 3,329 | 5,479  | 9,972  | 14,134 | 19,821 | 36,596  |
| Cottonwood Arroyo | 80.4                                      | 5588                                     | 10.6                            | 700                  | 7,786 | 13,591 | 26,257 | 38,900 | 55,889 | 108,738 |

Source: Waltemeyer 2006

mi<sup>2</sup> - square mile

ft msl - feet above mean sea level

cfs - cubic feet per second

Q - runoff rate

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Table 18.1-6 Average Monthly Flow, Maximum Daily Flow, and Number of Zero Flow Days at USGS 09367934, Teec-Ni-Di-Tso Wash near Burnham, New Mexico

| Year                            | Monthly mean discharge (cfs) (calculation period: October 1977 to September 1982) |       |       |       |       |       |       |       |       |       |       |       |
|---------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|                                 | Jan   | Feb   | Mar   | Apr   | May   | Jun   | Jul   | Aug   | Sep   | Oct   | Nov   | Dec   |
| 1977                            | -   | -     | -     | -     | -     | -     | -     | -     | -     | 0.046 | 0.088 | 0     |
| 1978                            | 0   | 0     | 0     | 0.04  | 0.349 | 0     | 0     | 0.035 | 0.297 | 0.084 | 0.271 | 0.604 |
| 1979                            | 1.41  | 0     | 0.008 | 0.004 | 0.019 | 0.024 | 0     | 0.023 | 0.003 | 0.071 | 0.173 | 0     |
| 1980                            | 0.721   | 0.236 | 0     | 0     | 0.048 | 0     | 0     | 0.194 | 0.001 | 0     | 0     | 0     |
| 1981                            | 0   | 0     | 0.115 | 0.077 | 0     | 0.007 | 0.12  | 0.006 | 0.026 | 0.081 | 0.064 | 0     |
| 1982                            | 0   | 1.44  | 0.077 | 0.033 | 0.189 | 0     | 0.047 | 2.18  | 0.002 | -     | -     | -     |
| Mean of monthly discharge (cfs) | 0.43  | 0.34  | 0.04  | 0.03  | 0.12  | 0.01  | 0.03  | 0.49  | 0.07  | 0.06  | 0.12  | 0.12  |
| Avg. max daily flow (cfs)       | 3.6   | 2.2   | 0.58  | 0.24  | 1.2   | 0.13  | 0.36  | 10    | 0.66  | 0.48  | 0.76  | 1.3   |
| Zero flow days                  | 10  | 15    | 25    | 24    | 21    | 27    | 23    | 21    | 20    | 23    | 16    | 25    |

cfs - cubic feet per second

Source: [http://waterdata.usgs.gov/nm/nwis/dvstat/?referred\\_module=sw&site\\_no=09367934&por\\_09367934\\_1=559352.00060.1,1977-10-01,1982-10-14&format=html\\_table&stat\\_cds=mean\\_va&date\\_format=YYYY-MM-DD&rdb\\_compression=file&submitted\\_form=parameter\\_selection\\_list](http://waterdata.usgs.gov/nm/nwis/dvstat/?referred_module=sw&site_no=09367934&por_09367934_1=559352.00060.1,1977-10-01,1982-10-14&format=html_table&stat_cds=mean_va&date_format=YYYY-MM-DD&rdb_compression=file&submitted_form=parameter_selection_list)

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Table 18.1-7 Average Monthly Flow, Maximum Daily Flow, and Number of Zero Flow Days at USGS 09367936, Burnham Wash near Burnham, New Mexico

| Year                      | Monthly mean discharge (cfs) (calculation period: October 1977 to September 1982) |       |       |       |       |       |       |       |       |       |       |       |
|---------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|                           | Jan   | Feb   | Mar   | Apr   | May   | Jun   | Jul   | Aug   | Sep   | Oct   | Nov   | Dec   |
| 1977                      | -   | -     | -     | -     | -     | -     | -     | -     | -     | 0.292 | 0.325 | 0     |
| 1978                      | 0.173   | 0.068 | 0.1   | 0.181 | 5.48  | 0     | 0     | 0.053 | 1.13  | 0.409 | 1.53  | 0.366 |
| 1979                      | 1.54  | 0     | 0.012 | 0.005 | 0.029 | 0.036 | 0     | 0.035 | 0.005 | 0.071 | 0.225 | 0.039 |
| 1980                      | 0.418   | 0.394 | 0.007 | 0.006 | 0.068 | 0     | 0.005 | 0.278 | 0.087 | 0.01  | 0     | 0     |
| 1981                      | 0   | 0     | 0.248 | 0.067 | 0.009 | 0.053 | 0.16  | 0.004 | 0.141 | 0.232 | 0.059 | 0     |
| 1982                      | 0   | 2.81  | 0.117 | 0.061 | 0.194 | 0     | 0     | 1.46  | 0.001 | -     | -     | -     |
| Mean of monthly discharge | 0.43  | 0.65  | 0.1   | 0.06  | 1.2   | 0.02  | 0.03  | 0.37  | 0.27  | 0.2   | 0.43  | 0.08  |
| Avg. max daily flow       | 4.8   | 1.9   | 0.91  | 0.8   | 14    | 0.2   | 0.4   | 5.1   | 3.6   | 2.3   | 2.8   | 1.4   |
| Zero flow days            | 7   | 7     | 14    | 20    | 17    | 26    | 26    | 22    | 18    | 17    | 17    | 25    |

cfs - cubic feet per second

Source: [http://waterdata.usgs.gov/nm/nwis/dvstat/?referred\\_module=sw&site\\_no=09367936&por\\_09367936\\_1=559353,00060,1,1977-10-01,1982-10-14&format=html\\_table&stat\\_cds=mean\\_va&date\\_format=YYYY-MM-DD&rdb\\_compression=file&submitted\\_form=parameter\\_selection\\_list](http://waterdata.usgs.gov/nm/nwis/dvstat/?referred_module=sw&site_no=09367936&por_09367936_1=559353,00060,1,1977-10-01,1982-10-14&format=html_table&stat_cds=mean_va&date_format=YYYY-MM-DD&rdb_compression=file&submitted_form=parameter_selection_list)

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Table 18.1-8 Days with Flow and Average Monthly Zero Flow Days at at USGS 09367938, Chaco River near Burnham, New Mexico

| Month/Year             | Jan  | Feb  | Mar  | Apr  | May  | Jun  | Jul  | Aug  | Sep  | Oct  | Nov  | Dec  |
|------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| 1977                   | -    | -    | -    | -    | -    | -    | -    | -    | -    | 0    | 8    | 0    |
| 1978                   | 1    | 22   | 23   | 0    | 8    | 0    | 0    | 3    | 7    | 8    | 24   | 11   |
| 1979                   | 13   | 15   | 22   | 12   | 14   | 6    | 5    | 10   | 0    | 7    | 6    | 0    |
| 1980                   | 20   | 19   | 0    | 9    | 20   | 0    | 1    | 0    | 9    | 5    | 0    | 0    |
| 1981                   | 0    | 0    | 15   | 2    | 0    | 6    | 17   | 0    | 11   | 3    | 1    | 0    |
| 1982                   | 0    | 0    | 29   | 30   | 13   | 0    | 5    | 29   | 24   |      |      |      |
| Average zero flow days | 24.2 | 17.0 | 13.2 | 19.4 | 20.0 | 27.6 | 25.4 | 22.6 | 19.8 | 26.4 | 22.2 | 28.8 |
| Median zero flow days  | 1    | 15   | 22   | 9    | 13   | 0    | 5    | 3    | 9    | 5    | 6    | 0    |

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Table 18.1-9 Days with Flow and Average Monthly Zero Flow Days at Site N (Upstream) and Site M (Downstream) on Burnham Wash between October 1, 1977 and May 31, 1980

Site N

| Month/Year             | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 1977                   | -   | -   | -   | -   | -   | -   | -   | -   | -   | 0   | 3   | 0   |
| 1978                   | 0   | 0   | 4   | 3   | 8   | 0   | 2   | 10  | 9   | 8   | 5   | 3   |
| 1979                   | 4   | 0   | 0   | 0   | 2   | 2   | 1   | 1   | 0   | 1   | 0   | 0   |
| 1980                   | 2   | 1   | 0   | 0   | 0   | -   | -   | -   | -   | -   | -   | -   |
| Average zero flow days | 28  | 28  | 27  | 28  | 28  | 28  | 28  | 21  | 21  | 26  | 23  | 28  |

Site M

| Month / Year           | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 1977                   | -   | -   | -   | -   | -   | -   | -   | -   | -   | 0   | 0   | 0   |
| 1978                   | 0   | 0   | 0   | 0   | 4   | 0   | 0   | 0   | 3   | 3   | 3   | 0   |
| 1979                   | 3   | 0   | 0   | 0   | 2   | 0   | 3   | 0   | 0   | 2   | 6   | 0   |
| 1980                   | 0   | 5   | 0   | 0   | 0   | -   | -   | -   | -   | -   | -   | -   |
| Average zero flow days | 28  | 24  | 29  | 30  | 20  | 30  | 28  | 28  | 22  | 23  | 20  | 31  |

Source:

Brimhall Watershed Flows from Hydrologic\_Monitoring\_Program\_1978.pdf from CONSOL Energy's Burnham Mine SMCRA Permit (OSM permit number NM-005)

Table 18.1-10 No Name Impoundment Staff Gage Readings from 1998

| Date       | Staff gage reading (ft) |
|------------|-------------------------|
| 11/17/1997 | Thin ice                |
| 5/12/1998  | 2                       |
| 6/11/1998  | 1.04                    |
| 7/21/1998  | dry                     |
| 7/29/1998  | > 5.0                   |
| 8/20/1998  | > 5.0                   |
| 8/26/1998  | > 5.0                   |
| 9/30/1998  | 5                       |
| 10/15/1998 | 4.2                     |
| 11/7/1998  | 3.8                     |
| 12/17/1998 | 3.7                     |



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Table 18.1-11 Baseline Surface Water Quality Analytes with Applicable Water Quality Standards, Methodologies, and Minimum Detection Limits

| Constituent<br>(mg/L, unless specified) | Livestock | Aquatic &<br>Wildlife Habitat<br>(Acute) | Aquatic &<br>Wildlife Habitat<br>(Chronic) | Secondary<br>Human Contact | Fish<br>Consumption |
|---|-----------|--|--|----------------------------|---------------------|
| Aluminum                                |           | 0.75                                     | 0.087                                      |                            |                     |
| Arsenic                                 | 0.2       | 0.34                                     | 0.15                                       | 0.28                       | 0.08                |
| Barium                                  |           |  |  | 98                         |                     |
| Boron                                   | 5         |  |  | 126                        |                     |
| Cadmium <sup>1</sup>                    | 0.05      | 0.00217                                  | 0.00026                                    | 0.47                       | 0.008               |
| Chromium (III+IV)                       | 1         |  |  |                            |                     |
| III*                                    |           | 0.00035                                  | 0.0201                                     | 1400                       | 75                  |
| IV                                      |           | 0.016                                    | 0.011                                      | 2.8                        | 0.15                |
| Copper <sup>1</sup>                     | 0.5       | 0.01445                                  | 0.00956                                    | 9.33                       |                     |
| Fluoride                                | 2*        |  |  |                            |                     |
| Lead <sup>1</sup>                       | 0.1       | 0.07022                                  | 0.00274                                    | 0.015                      |                     |
| Mercury                                 |           | 0.0024                                   | 0.000001                                   | 0.28                       | 0.00015             |
| Nitrate                                 | 132       |  |  | 1493.33                    |                     |
| pH (standard units)                     | 6.5-9.0   | 6.5-9.0                                  | 6.5-9.0                                    | 6.5-9.0                    |                     |
| Radium 226+228                          | 30        |  |  |                            |                     |
| Selenium                                | 0.05      | 0.033                                    | 0.002                                      | 4.67                       | 0.67                |
| Silver <sup>1</sup>                     |           | 0.00367                                  |  | 0.00467                    | 8                   |
| Sulfate                                 | 1000*     |  |  |                            |                     |
| TDS                                     | 3000*     |  |  |                            |                     |
| Zinc <sup>1</sup>                       | 25        | 0.0214                                   | 0.0215                                     | 280                        | 5.1                 |

Note all values are NNEPA 2008 criterion unless otherwise specified

<sup>1</sup> Aquatic & Wildlife Criterion are hardness dependent and calculated for a hardness of 108 mg/L as CaCO<sub>3</sub>, which is the median for Pinabete and Cottonwood Arroyos

\*Lardy, Stoltenow and Johnson 2008

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Table 18.1-12 Median Concentrations at Cottonwood Baseline Monitoring Stations

| Parameter <sup>1</sup>                                 | CN-1    | CS-1    | CNS-1   |
|--|---------|---------|---------|
| Start Date   | 7/18/90 | 7/18/90 | 7/18/90 |
| End Date   | 9/2/99  | 9/5/99  | 8/3/99  |
| Max # of Observations                                  | 96      | 92      | 104     |
| pH (S.U.)  | 7.95    | 8.4     | 8.3     |
| Total Dissolved Solids (mg/l)                          | 780     | 675     | 610     |
| Total Suspended Solids (mg/l)                          | 87500   | 59400   | 65300   |
| Total Settleable Solids (mg/l)                         | 59.45   | 114     | 37.55   |
| Conductivity (µmhos/cm)                                | 1035    | 817     | 760     |
| Arsenic(mg/L)  | <0.0015 | <0.002  | <0.002  |
| Boron (mg/l)   | 0.08    | 0.12    | 0.13    |
| Calcium (mg/l)   | 35      | 23      | 25      |
| Cadmium (mg/L)   | <0.0025 | <0.0025 | <0.0025 |
| Chloride (mg/l)  | 16      | 12.8    | 13      |
| Iron (mg/l)  | 2.03    | 1.66    | 2.37    |
| Total Iron (mg/l)                                      | 174     | 225.5   | 203     |
| Lead   | <0.01   | <0.01   | <0.01   |
| Magnesium (mg/l)                                       | 3.9     | 2.6     | 3.8     |
| Manganese (uncharacterized, presumed dissolved) (mg/l) | <0.1    | <0.1    | <0.1    |
| Total Manganese (mg/l)                                 | 10.15   | 4.2     | 5.128   |
| Nitrate as N (mg/L)                                    | 7       | 7.65    | 8       |
| Potassium (mg/l)                                       | 5.2     | 5.04    | 4.7     |
| Selenium (mg/l)  | <0.0025 | <0.0025 | <0.0025 |
| Sulfate (mg/l)   | 386     | 275     | 257     |
| Sodium (mg/l)  | 205     | 175     | 160     |
| Bicarbonate as CaCO <sub>3</sub> (mg/l)                | 170     | 151     | 141     |
| Carbonate as CaCO <sub>3</sub> (mg/l)                  | 1       | 2.4     | 2.2     |

<sup>1</sup>Medians calculated based on half of the detection limit. Less than symbols (<) associated with half value, for which actual value is not certain

Table 18.1-13 Water quality and flow data on Pinabete Arroyo between July 29, 1998 and July 21, 2008

| Sample ID                        | Sample date | Flow (cfs) | Alkalinity as CaCO3 (mg/L) | Q | Aluminum, D (mg/L) | Q | Arsenic, D (mg/L) | Barium, D (mg/L) | Bicarbonate as CaCO3 (mg/L) | Q | Boron, D (mg/L) | Cation anion balance (CAB) (%) | Q | Cadmium, D (mg/L) | Calcium, D (mg/L) | Q | Carbonate as CaCO3 (mg/L) | Q | Chloride (mg/L) | Q | Chromium, D (mg/L) | Q | Electrical conductivity (EC) (µS/cm) | Copper, D (mg/L) | Q | Fluoride (mg/L) |
|----------------------------------|-------------|------------|----------------------------|---|--------------------|---|-------------------|------------------|-----------------------------|---|-----------------|--------------------------------|---|-------------------|-------------------|---|---------------------------|---|-----------------|---|--------------------|---|--------------------------------------|------------------|---|-----------------|
| Upper Pinabete <sup>1</sup>      | 7/29/1998   | 22.50      | -                          |   | -                  |   | -                 | -                | 207                         |   | 0.06            | -                              |   | -                 | 39                | < | 1                         |   | 9               |   | -                  |   | 930                                  | -                |   | 0.78            |
| Upper Pinabete <sup>1</sup>      | 8/26/1998   | 1079       | -                          |   | -                  |   | -                 | -                | 178                         |   | 0.09            | -                              |   | -                 | 73                | < | 1                         |   | 32              |   | -                  |   | 1640                                 | -                |   | 1.09            |
| Upper Pinabete <sup>1</sup>      | 9/30/1998   | -          | -                          |   | -                  |   | -                 | -                | 269                         |   | 0.09            | -                              |   | -                 | 65                | < | 1                         |   | 24              |   | -                  |   | 1460                                 | -                |   | 1.19            |
| Upper Pinabete <sup>1</sup>      | 11/7/1998   | 308        | -                          |   | -                  |   | -                 | -                | 156                         |   | 0.07            | -                              |   | -                 | 24                | < | 1                         |   | 10              |   | -                  |   | 880                                  | -                |   | 0.90            |
| Upper Pinabete #3                | 10/8/2007   | 2.04       | 116                        |   | 0.28               |   | 0.0084            | 0.0313           | 114                         |   | 0.30            | 0.19                           | < | 0.00005           | 15                | < | 10                        |   | 10              | < | 0.001              |   | 584                                  | 0.0080           | < | 0.2             |
| Upper Pinabete #3                | 12/3/2007   | 2.07       | 119                        | < | 0.10               |   | 0.015             | 0.0388           | 117                         | < | 0.10            | 3.22                           | < | 0.00005           | 22.1              | < | 10                        |   | 10              | < | 0.001              |   | 962                                  | 0.0096           | < | 0.2             |
| Upper Pinabete grab <sup>2</sup> | 2/13/2008   | 4.46       | 53                         |   | 0.42               |   | 0.0204            | 0.0433           | 53                          |   | 0.9             | 4.43                           | < | 0.00005           | 23.6              | < | 10                        |   | 11              |   | 0.002              |   | 1520                                 | 0.0261           | < | 0.2             |
| Upper Pinabete #2                | 8/12/2008   | 0.44       | 123                        | < | 0.10               |   | 0.0009            | 0.0685           | 123                         |   | 0.1             | 5.93                           |   | 0.00014           | 94.2              | < | 10                        | < | 10              | < | 0.001              |   | 1460                                 | 0.0115           | < | 0.2             |
| Upper Pinabete #3                | 8/12/2008   | 0.44       | 228                        | < | 0.10               |   | 0.0022            | 0.1120           | 228                         |   | 0.1             | 5.35                           | < | 0.00005           | 101               | < | 10                        |   | 10              | < | 0.001              |   | 1810                                 | 0.0090           | < | 0.2             |
| Lower Pinabete <sup>1</sup>      | 7/29/1998   | 1717       | -                          |   | -                  |   | -                 | -                | 464                         |   | 0.17            | -                              |   | -                 | 141               | < | 1                         |   | 27              |   | -                  |   | 1940                                 | -                |   | 0.40            |
| Lower Pinabete <sup>1</sup>      | 8/26/1998   | 2307       | -                          |   | -                  |   | -                 | -                | 307                         |   | 0.11            | -                              |   | -                 | 71                | < | 1                         |   | 34              |   | -                  |   | 1530                                 | -                |   | 0.70            |
| Lower Pinabete <sup>1</sup>      | 9/30/1998   | 4.90       | -                          |   | -                  |   | -                 | -                | 132                         | < | 0.05            | -                              |   | -                 | 50                | < | 1                         |   | 6               |   | -                  |   | 410                                  | -                |   | 0.45            |
| Lower Pinabete <sup>1</sup>      | 11/7/1998   | 145        | -                          |   | -                  |   | -                 | -                | 125                         |   | 0.14            | -                              |   | -                 | 19                | < | 1                         |   | 8               |   | -                  |   | 600                                  | -                |   | 0.75            |
| Lower Pinabete #1                | 11/18/1998  | 145        | -                          |   | -                  |   | -                 | -                | 107                         |   | 0.07            | -                              |   | -                 | 20                |   | 3                         |   | 7               |   | -                  |   | 480                                  | -                |   | 0.60            |
| Lower Pinabete #2                | 11/18/1998  | 145        | -                          |   | -                  |   | -                 | -                | 120                         |   | 0.09            | -                              |   | -                 | 20                |   | 3                         |   | 8               |   | -                  |   | 570                                  | -                |   | 0.75            |
| Lower Pinabete grab <sup>2</sup> | 9/18/2007   | -          | 102                        | < | 0.10               |   | 0.0013            | 0.0366           | 102                         | < | 0.10            | 0.07                           | < | 0.00005           | 27.3              | < | 10                        | < | 10              | < | 0.001              |   | 396                                  | 0.0072           |   | 0.2             |
| Lower Pinabete #1                | 9/24/2007   | -          | 134                        |   | 0.21               |   | 0.0133            | 0.2193           | 134                         |   | 0.2             | 1.05                           | < | 0.00005           | 48.9              | < | 10                        |   | 13              | < | 0.001              |   | 866                                  | 0.0109           | < | 0.2             |
| Lower Pinabete #2                | 9/24/2007   | -          | 139                        |   | 0.12               |   | 0.0062            | 0.1359           | 139                         |   | 0.1             | 6.57                           | < | 0.00005           | 39.4              | < | 10                        |   | 11              | < | 0.001              |   | 776                                  | 0.0104           | < | 0.2             |
| Lower Pinabete #1                | 10/8/2007   | 16.41      | 147                        |   | 0.21               |   | 0.0015            | 0.0528           | 147                         |   | 0.30            | 2.11                           | < | 0.00005           | 32.7              | < | 10                        |   | 13              |   | 0.001              |   | 1020                                 | 0.0076           | < | 0.20            |
| Lower Pinabete #2                | 10/8/2007   | 16.41      | 158                        |   | 0.26               |   | 0.0100            | 0.0621           | 156                         |   | 0.30            | 6.01                           | < | 0.00005           | 34.4              | < | 10                        |   | 15              |   | 0.001              |   | 1040                                 | 0.0095           | < | 0.20            |
| Lower Pinabete #1 <sup>4</sup>   | 12/3/2007   | 36.32      | -                          |   | -                  |   | -                 | -                | -                           |   | -               | -                              |   | -                 | -                 |   | -                         |   | -               |   | -                  |   | 708                                  | -                |   | -               |
| Lower Pinabete #2                | 12/3/2007   | 36.32      | 138                        | < | 0.1                |   | 0.0101            | 0.0247           | 138                         | < | 0.10            | 4.03                           | < | 0.00005           | 18.1              | < | 10                        | < | 10              | < | 0.001              |   | 654                                  | 0.0117           | < | 0.20            |
| Lower Pinabete #3 <sup>4</sup>   | 12/3/2007   | 36.30      | -                          |   | -                  |   | -                 | -                | -                           |   | -               | -                              |   | -                 | -                 |   | -                         |   | -               |   | -                  |   | 655                                  | -                |   | -               |
| Lower Pinabete #1                | 2/13/2008   | 24.05      | 145                        |   | 2.30               |   | 0.0094            | 0.0344           | 125                         |   | 0.9             | 5.05                           |   | 0.00005           | 9.5               |   | 20                        | < | 10              |   | 0.003              |   | 502                                  | 0.0171           | < | 0.2             |
| Lower Pinabete #2                | 2/13/2008   | 24.05      | 124                        | < | 0.10               |   | 0.0025            | 0.0421           | 124                         |   | 0.5             | 4.50                           | < | 0.00005           | 72.4              | < | 10                        |   | 13              |   | 0.002              |   | 666                                  | 0.0070           | < | 0.2             |
| Lower Pinabete #1                | 7/21/2008   | 46.62      | 212                        | < | 0.10               | < | 0.005             | 0.076            | 212                         |   | 0.1             | 2.86                           |   | 0.0681            | 48.2              | < | 10                        | < | 10              | < | 0.01               |   | 723                                  | 0.009            | < | 0.2             |
| Lower Pinabete #2                | 7/21/2008   | 46.62      | 200                        | < | 0.10               | < | 0.005             | 0.071            | 200                         | < | 0.1             | 3.39                           |   | 0.0037            | 42.8              | < | 10                        |   | 10              | < | 0.01               |   | 641                                  | 0.006            | < | 0.2             |
| Lower Pinabete #3                | 7/21/2008   | 46.62      | 170                        | < | 0.10               | < | 0.005             | 0.050            | 170                         | < | 0.1             | 4.25                           | < | 0.0005            | 36.5              | < | 10                        | < | 10              | < | 0.01               |   | 584                                  | 0.007            | < | 0.2             |

<sup>1</sup> Sampler designation was only provided if more than one sampler contained water

<sup>2</sup> If water was flowing when the samplers where visited, a grab sample was taken

<sup>3</sup> Very limited sample volume

<sup>4</sup> If water is present in all three samplers, full analysis was completed on one with abbreviated analyses on the other two

Q - Qualifier

D - Dissolved

T - Total

cfs - cubic feet per second

mg/L - milligrams per liter

µS/cm - microsiemens per centimeter

su - standard units

pCi/L - picocuries per liter

Table 18.1-13 (Continued)

| Sample ID                        | Sample date | Hardness (calc) | Q | Hydroxide as CaCO <sub>3</sub> (mg/L) | Q | Iron, D (mg/L) | Iron, T (mg/L) | Q | Lead, D (mg/L) | Magnesium, D (mg/L) | Q | Manganese, D (mg/L) | Manganese, T (mg/L) | Q | Mercury (mg/L) | Q | Nitrate/ Nitrite as N (mg/L) | pH (su) | Q | Phosphorous, T (mg/L) | Potassium, D (mg/L) | Radium 226 (pCi/L) | Radium 228 (pCi/L) | Sodium adsorption ratio (SAR) | Q |
|----------------------------------|-------------|-----------------|---|---------------------------------------|---|----------------|----------------|---|----------------|---------------------|---|---------------------|---------------------|---|----------------|---|------------------------------|---------|---|-----------------------|---------------------|--------------------|--------------------|-------------------------------|---|
| Upper Pinabete <sup>1</sup>      | 7/29/1998   | 110             |   | -                                     |   | 7.00           | 118            |   | -              | 2.9                 |   | 0.357               | 12.80               |   | -              |   | -                            | 8.10    |   | -                     | 5.5                 | -                  | -                  | 6.3                           | < |
| Upper Pinabete <sup>1</sup>      | 8/26/1998   | 209             |   | -                                     |   | 0.15           | 286            |   | -              | 6.8                 |   | 0.007               | 12.90               |   | -              |   | -                            | 7.80    |   | -                     | 5.7                 | -                  | -                  | 8.0                           | < |
| Upper Pinabete <sup>1</sup>      | 9/30/1998   | 186             |   | -                                     |   | 1.17           | 1140           |   | -              | 5.7                 |   | 0.453               | 24.40               |   | -              |   | -                            | 7.60    |   | -                     | 5.3                 | -                  | -                  | 7.7                           | < |
| Upper Pinabete <sup>1</sup>      | 11/7/1998   | 87              |   | -                                     |   | 0.05           | 6              |   | -              | 6.8                 | < | 0.01                | 2.20                |   | -              |   | -                            | 8.20    |   | -                     | 8.6                 | -                  | -                  | 8.0                           | < |
| Upper Pinabete #3                | 10/8/2007   | 41              | < | 10                                    | < | 0.05           | 1150           |   | 0.0002         | 0.9                 | < | 0.005               | 22.80               | < | 0.0002         |   | 0.74                         | 8.24    |   | 3.09                  | 3.5                 | -                  | -                  | -                             |   |
| Upper Pinabete #3                | 12/3/2007   | 62              | < | 10                                    | < | 0.05           | 1220           | < | 0.0001         | 1.7                 | < | 0.005               | 24.1                | < | 0.0002         |   | 2.48                         | 8.11    |   | 0.26                  | 3.7                 | -                  | -                  | -                             |   |
| Upper Pinabete grab <sup>2</sup> | 2/13/2008   | 68              | < | 10                                    |   | 0.26           | 571            |   | 0.0005         | 2.2                 |   | 0.005               | 8.09                |   | 0.0016         |   | 1.65                         | 7.99    |   | 0.89                  | 5.5                 | -                  | -                  | -                             |   |
| Upper Pinabete #2                | 8/12/2008   | 262             | < | 10                                    | < | 0.05           | <sup>(3)</sup> |   | 0.0001         | 6.4                 | < | 0.005               | <sup>(3)</sup>      |   | <sup>(3)</sup> |   | <sup>(3)</sup>               | 7.51    |   | <sup>(3)</sup>        | 7.8                 | -                  | -                  | -                             |   |
| Upper Pinabete #3                | 8/12/2008   | 281             | < | 10                                    | < | 0.05           | 59.0           | < | 0.0001         | 7.0                 | < | 0.005               | 16.1                | < | 0.0002         |   | 0.06                         | 7.48    |   | 0.09                  | 8.0                 | -                  | -                  | -                             |   |
| Lower Pinabete <sup>1</sup>      | 7/29/1998   | 413             |   | -                                     | < | 0.02           | 155            |   | -              | 14.7                |   | 3.76                | 28.40               |   | -              |   | -                            | 7.00    |   | -                     | 10.7                | -                  | -                  | 5.1                           | < |
| Lower Pinabete <sup>1</sup>      | 8/26/1998   | 201             |   | -                                     |   | 1.35           | 305            |   | -              | 6.0                 |   | 0.21                | 21.40               |   | -              |   | -                            | 7.60    |   | -                     | 6.6                 | -                  | -                  | 7.5                           | < |
| Lower Pinabete <sup>1</sup>      | 9/30/1998   | 147             |   | -                                     |   | 1.66           | 216            |   | -              | 5.3                 |   | 0.125               | 4.07                |   | -              |   | -                            | 8.10    |   | -                     | 9.1                 | -                  | -                  | 1.9                           | < |
| Lower Pinabete <sup>1</sup>      | 11/7/1998   | 62              |   | -                                     |   | 20.30          | 1490           |   | -              | 3.4                 |   | 2.11                | 52.00               |   | -              |   | -                            | 8.20    |   | -                     | 5.4                 | -                  | -                  | 6.0                           | < |
| Lower Pinabete #1                | 11/18/1998  | 59              |   | -                                     |   | 0.03           | 472            |   | -              | 2.1                 | < | 0.01                | 7.80                |   | -              |   | -                            | 8.40    |   | -                     | 4.6                 | -                  | -                  | 4.8                           | < |
| Lower Pinabete #2                | 11/18/1998  | 61              |   | -                                     |   | 3.50           | 844            |   | -              | 2.6                 |   | 0.11                | 13.40               |   | -              |   | -                            | 8.30    |   | -                     | 3.8                 | -                  | -                  | 5.8                           | < |
| Lower Pinabete grab <sup>2</sup> | 9/18/2007   | 77              | < | 10                                    |   | 0.05           | 125            |   | 0.0002         | 2.1                 | < | 0.005               | 5.86                | < | 0.0002         |   | 1.73                         | 8.02    |   | 0.12                  | 5.0                 | 1.7 ± 0.6          | 3.0 ± 0.7          | -                             |   |
| Lower Pinabete #1                | 9/24/2007   | 137             | < | 10                                    |   | 0.07           | <sup>(3)</sup> |   | 0.0003         | 3.6                 | < | 0.005               | <sup>(3)</sup>      | < | 0.0002         |   | 1.93                         | 7.64    |   | 0.26                  | 4.8                 | -                  | -                  | -                             |   |
| Lower Pinabete #2                | 9/24/2007   | 111             | < | 10                                    |   | 0.13           | 391            | < | 0.0002         | 3.1                 |   | 0.006               | 20.2                | < | 0.0002         |   | 0.85                         | 7.39    |   | 0.52                  | 5.1                 | -                  | -                  | -                             | < |
| Lower Pinabete #1                | 10/8/2007   | 90              | < | 10                                    |   | 0.12           | 1550           |   | 0.0004         | 2.1                 |   | 0.017               | 38.4                | < | 0.0002         |   | 0.31                         | 8.07    |   | 2.06                  | 5.0                 | -                  | -                  | -                             |   |
| Lower Pinabete #2                | 10/8/2007   | 95              | < | 10                                    |   | 0.13           | 1940           |   | 0.0002         | 2.2                 |   | 0.009               | 55.90               | < | 0.0002         |   | 0.31                         | 8.01    |   | 0.64                  | 5.1                 | -                  | -                  | -                             |   |
| Lower Pinabete #1 <sup>4</sup>   | 12/3/2007   | -               |   | -                                     |   | -              | -              |   | -              | -                   |   | -                   | -                   |   | -              |   | -                            | 8.19    |   | -                     | -                   | -                  | -                  | -                             |   |
| Lower Pinabete #2                | 12/3/2007   | 51              | < | 10                                    | < | 0.05           | 775            | < | 0.0001         | 1.3                 | < | 0.005               | 16.7                | < | 0.0002         |   | 3.40                         | 8.16    |   | 0.17                  | 4.10                | -                  | -                  | -                             |   |
| Lower Pinabete #3 <sup>4</sup>   | 12/3/2007   | -               |   | -                                     |   | -              | -              |   | -              | -                   |   | -                   | -                   |   | -              |   | -                            | 8.21    |   | -                     | -                   | -                  | -                  | -                             |   |
| Lower Pinabete #1                | 2/13/2008   | 29              | < | 10                                    |   | 1.04           | 1120           |   | 0.0011         | 1.2                 |   | 0.012               | 22.5                |   | 0.0024         |   | 0.98                         | 8.56    |   | 0.69                  | 3.0                 | -                  | -                  | -                             |   |
| Lower Pinabete #2                | 2/13/2008   | 248             | < | 10                                    | < | 0.05           | 1260           | < | 0.0001         | 16.4                | < | 0.005               | 25.5                |   | 0.0032         |   | 1.79                         | 8.35    |   | 0.36                  | 4.4                 | -                  | -                  | -                             |   |
| Lower Pinabete #1                | 7/21/2008   | 139             | < | 10                                    |   | 0.30           | 1100           | < | 0.001          | 4.6                 |   | 0.899               | 35.5                |   | 0.0015         |   | 0.04                         | 7.49    |   | 0.89                  | 6.2                 | -                  | -                  | -                             | < |
| Lower Pinabete #2                | 7/21/2008   | 125             | < | 10                                    |   | 0.06           | 574            | < | 0.001          | 4.3                 |   | 0.645               | 19.6                |   | 0.0011         |   | 0.54                         | 7.61    |   | 0.83                  | 6.8                 | -                  | -                  | -                             | < |
| Lower Pinabete #3                | 7/21/2008   | 106             | < | 10                                    |   | 0.12           | 566            |   | 0.003          | 3.6                 |   | 0.506               | 19.0                |   | 0.0010         |   | 0.46                         | 7.66    |   | 0.58                  | 6.2                 | -                  | -                  | -                             | < |

<sup>1</sup> Sampler designation was only provided if more than one sampler contained water  
<sup>2</sup> If water was flowing when the samplers where visited, a grab sample was taken  
<sup>3</sup> Very limited sample volume  
<sup>4</sup> If water is present in all three samplers, full analysis was completed on one with abbreviated analyses on the other two  
Q - Qualifier  
D - Dissolved  
T - Total  
cfs - cubic feet per second  
mg/L - milligrams per liter  
µS/cm - microsiemens per centimeter  
su - standard units  
pCi/L - picocuries per liter

Table 18.1-13 (Continued)

| Sample ID                        | Sample date | Selenium, D (mg/L) | Q | Settleable solids (mL/L) | Q | Silver, D (mg/L) | Sodium, D (mg/L) | Q | Sulfate (mg/L) | Total dissolved solids (TDS) (mg/L) | Total suspended solids (TSS) (mg/L) | Q | Zinc, D (mg/L) |
|----------------------------------|-------------|--------------------|---|--------------------------|---|------------------|------------------|---|----------------|-------------------------------------|-------------------------------------|---|----------------|
| Upper Pinabete <sup>1</sup>      | 7/29/1998   | 0.005              |   | 705                      |   | -                | 151.0            |   | 319            | 610                                 | 109,000                             |   | -              |
| Upper Pinabete <sup>1</sup>      | 8/26/1998   | 0.005              |   | 714                      |   | -                | 265.0            |   | 581            | 1,200                               |                                     |   | -              |
| Upper Pinabete <sup>1</sup>      | 9/30/1998   | 0.005              |   | 800                      |   | -                | 242.0            |   | 360            | 1,060                               | 178,000                             |   | -              |
| Upper Pinabete <sup>1</sup>      | 11/7/1998   | 0.005              |   | 14.4                     |   | -                | 166.0            |   | 313            | 620                                 | 305,000                             |   | -              |
| Upper Pinabete #3                | 10/8/2007   | 0.003              |   | 27.1                     | < | 0.00005          | 115.0            |   | 180            | 660                                 | 64,200                              |   | 0.001          |
| Upper Pinabete #3                | 12/3/2007   | 0.002              |   | 3.9                      | < | 0.00005          | 194.0            |   | 390            | 835                                 | 89,900                              |   | 0.002          |
| Upper Pinabete grab <sup>2</sup> | 2/13/2008   | 0.005              |   | 9.6                      |   | 0.00010          | 309              |   | 740            | 5,300                               | 26,600                              |   | 0.004          |
| Upper Pinabete #2                | 8/12/2008   | 0.002              |   | 904                      | < | 0.00005          | 278.0            |   | 840            | 1,270                               | 521,000                             |   | 0.002          |
| Upper Pinabete #3                | 8/12/2008   | 0.001              |   | 658                      | < | 0.00005          | 284.0            |   | 780            | 1,270                               | 140,000                             |   | 0.001          |
| Lower Pinabete <sup>1</sup>      | 7/29/1998   | 0.005              |   | 850                      |   | -                | 238.0            |   | 684            | 1,410                               | 279,000                             |   | -              |
| Lower Pinabete <sup>1</sup>      | 8/26/1998   | 0.005              |   | 890                      |   | -                | 243.0            |   | 591            | 1,220                               | -                                   |   | -              |
| Lower Pinabete <sup>1</sup>      | 9/30/1998   | 0.005              |   | 4.5                      |   | -                | 52.8             |   | 130            | 350                                 | 24,200                              |   | -              |
| Lower Pinabete <sup>1</sup>      | 11/7/1998   | 0.005              |   | 1.0                      |   | -                | 108.0            |   | 164            | 390                                 | 34,700                              |   | -              |
| Lower Pinabete #1                | 11/18/1998  | 0.005              |   | 9.9                      |   | -                | 85.1             |   | 123            | 370                                 | 28,400                              |   | -              |
| Lower Pinabete #2                | 11/18/1998  | 0.005              |   | 9.5                      |   | -                | 103.0            |   | 169            | 400                                 | 49,200                              |   | -              |
| Lower Pinabete grab <sup>2</sup> | 9/18/2007   | 0.002              |   | 31.4                     |   | 0.00008          | 54.2             |   | 100            | 295                                 | 17,900                              |   | 0.003          |
| Lower Pinabete #1                | 9/24/2007   | 0.002              |   | 400                      | < | 0.00005          | 138.0            |   | 295            | 570                                 | 89,600                              |   | 0.016          |
| Lower Pinabete #2                | 9/24/2007   | 0.001              |   | 184                      | < | 0.00005          | 96.2             |   | 235            | 460                                 | 97,600                              |   | 0.015          |
| Lower Pinabete #1                | 10/8/2007   | 0.007              |   | 727                      | < | 0.00005          | 180.0            |   | 360            | 600                                 | 132,000                             |   | 0.002          |
| Lower Pinabete #2                | 10/8/2007   | 0.007              |   | 766                      | < | 0.00005          | 179.0            |   | 390            | 620                                 | 156,000                             |   | 0.002          |
| Lower Pinabete #1 <sup>4</sup>   | 12/3/2007   | -                  |   | 25.6                     |   | -                | -                |   | -              | 1,130                               | 88,000                              |   | -              |
| Lower Pinabete #2                | 12/3/2007   | 0.003              |   | 16.7                     |   | 0.00006          | 137.0            |   | 190            | 935                                 | 51,800                              |   | 0.006          |
| Lower Pinabete #3 <sup>4</sup>   | 12/3/2007   | -                  |   | 17.9                     |   | -                | -                |   | -              | 1,270                               | 68,000                              |   | -              |
| Lower Pinabete #1                | 2/13/2008   | 0.003              |   | 111.0                    |   | 0.00006          | 140              |   | 165            | 28,400                              | 10,200                              |   | 0.006          |
| Lower Pinabete #2                | 2/13/2008   | 0.003              |   | 174.0                    | < | 0.00005          | 30.2             |   | 170            | 13,600                              | 70,400                              |   | 0.004          |
| Lower Pinabete #1                | 7/21/2008   | 0.01               |   | 290                      | < | 0.0005           | 112.0            |   | 180            | 500                                 | 102,000                             |   | 0.16           |
| Lower Pinabete #2                | 7/21/2008   | 0.01               |   | 190                      | < | 0.0005           | 98.5             |   | 140            | 430                                 | 50,300                              |   | 0.01           |
| Lower Pinabete #3                | 7/21/2008   | 0.01               |   | 190                      | < | 0.0005           | 93.6             |   | 138            | 400                                 | 48,900                              | < | 0.01           |

<sup>1</sup> Sampler designation was only provided if more than one sampler contained water

<sup>2</sup> If water was flowing when the samplers were visited, a grab sample was taken

<sup>3</sup> Very limited sample volume

<sup>4</sup> If water is present in all three samplers, full analysis was completed on one with abbreviated analyses on the other two

Q - Qualifier

D - Dissolved

T - Total

cfs - cubic feet per second

mg/L - milligrams per liter

µS/cm - microsiemens per centimeter

su - standard units

pCi/L - picocuries per liter

Table 18.1-14 Water quality and flow data on No Name Arroyo between July 29, 1998 and August 12, 2008

| Sample ID                       | Sample date | Flow (cfs) | Alkalinity as CaCO3 (mg/L) | Q | Aluminum, D (mg/L) | Q | Arsenic, D (mg/L) | Barium, D (mg/L) | Bicarbonate as CaCO3 (mg/L) | Q | Boron, D (mg/L) | Cation anion balance (CAB) (%) | Q | Cadmium, D (mg/L) | Calcium, D (mg/L) | Q | Carbonate as CaCO3 (mg/L) | Q | Chloride (mg/L) | Q | Chromium, D (mg/L) |
|---------------------------------|-------------|------------|----------------------------|---|--------------------|---|-------------------|------------------|-----------------------------|---|-----------------|--------------------------------|---|-------------------|-------------------|---|---------------------------|---|-----------------|---|--------------------|
| Upper No Name <sup>1</sup>      | 7/29/1998   | 2          | -                          |   | -                  |   | -                 | -                | 132                         |   | <0.05           | -                              |   | -                 | 35                | < | 1                         |   | 8               |   | -                  |
| Upper No Name <sup>1</sup>      | 9/30/1998   | 10         | -                          |   | -                  |   | -                 | -                | 180                         |   | <0.05           | -                              |   | -                 | 42                |   | 3                         |   | 7               |   | -                  |
| Upper No Name #2                | 2/13/2008   | 19         | 106                        |   | 0.52               |   | 0.0027            | 0.0287           | 106                         |   | 0.5             | 4.62                           | < | 0.00005           | 11.5              | < | 10                        |   | 19              |   | 0.002              |
| Upper No Name #3                | 2/13/2008   | 19         | 122                        |   | 1.65               |   | 0.0046            | 0.0468           | 122                         |   | 0.4             | 12.4                           | < | 0.00005           | 16.3              | < | 10                        | < | 10              |   | 0.003              |
| Upper No Name grab <sup>2</sup> | 2/13/2008   | 19.14      | 132                        |   | 0.56               |   | 0.0038            | 0.0361           | 132                         |   | 0.3             | 2.28                           | < | 0.00005           | 17.9              | < | 10                        | < | 10              |   | 0.003              |
| Upper No Name #2                | 7/21/2008   | -          | 128                        | < | 0.10               | < | 0.005             | 0.050            | 128                         | < | 0.1             | 3.08                           |   | 0.0099            | 17.0              | < | 10                        | < | 10              | < | 0.01               |
| Upper No Name #3                | 7/21/2008   | -          | 133                        | < | 0.10               | < | 0.005             | 0.053            | 133                         | < | 0.1             | 4.53                           |   | 0.0011            | 18.5              | < | 10                        | < | 10              | < | 0.01               |
| Upper No Name #1                | 8/12/2008   | -          | 119                        | < | 0.10               |   | 0.0032            | 0.0658           | 119                         | < | 0.1             | 6.90                           |   | 0.00025           | 23.8              | < | 10                        | < | 10              | < | 0.001              |
| Upper No Name #2                | 8/12/2008   | -          | 121                        | < | 0.10               |   | 0.0023            | 0.0606           | 121                         | < | 0.1             | 3.63                           | < | 0.00005           | 22.8              | < | 10                        | < | 10              | < | 0.001              |
| Upper No Name #3                | 8/12/2008   | -          | 110                        |   | 0.15               |   | 0.0019            | 0.0583           | 110                         | < | 0.1             | 4.07                           |   | 0.00062           | 20.3              | < | 10                        | < | 10              | < | 0.001              |
| Lower No Name #1                | 8/13/1998   | -          | -                          |   | -                  |   | -                 | -                | 417                         |   | 0.2             | -                              |   | -                 | 92                | < | 1                         |   | 11              |   | -                  |
| Lower No Name #2                | 8/14/1998   | -          | -                          |   | -                  |   | -                 | -                | 232                         |   | 0.2             | -                              |   | -                 | 121               | < | 1                         |   | 17              |   | -                  |
| Lower No Name <sup>1</sup>      | 9/30/1998   | 74.00      | -                          |   | -                  |   | -                 | -                | 264                         |   | 0.1             | -                              |   | -                 | 77                | < | 1                         |   | 9               |   | -                  |
| Lower No Name #1                | 8/28/2007   | -          | 129                        | < | 0.10               |   | 0.0011            | 0.0474           | 129                         | < | 0.1             | 9.65                           | < | 0.00005           | 45.6              | < | 10                        | < | 10              | < | 0.001              |
| Lower No Name #2                | 8/28/2007   | -          | 158                        | < | 0.10               |   | 0.0011            | 0.0500           | 158                         | < | 0.1             | 14.2                           | < | 0.00005           | 39.5              | < | 10                        | < | 10              | < | 0.001              |
| Lower No Name #1                | 8/12/2008   | -          | 302                        | < | 0.10               |   | 0.0051            | 0.122            | 302                         | < | 0.1             | 3.80                           | < | 0.00005           | 147               | < | 10                        | < | 10              | < | 0.001              |
| Lower No Name #2                | 8/12/2008   | -          | 270                        | < | 0.10               |   | 0.0045            | 0.111            | 270                         |   | 0.2             | 1.19                           |   | 0.00095           | 120               | < | 10                        | < | 10              | < | 0.001              |
| Lower No Name #3                | 8/12/2008   | -          | 320                        | < | 0.10               |   | 0.0058            | 0.138            | 320                         |   | 0.2             | 9.71                           | < | 0.00005           | 186               | < | 10                        | < | 10              | < | 0.001              |

<sup>1</sup> Sampler designation was only provided if more than one sampler contained water

<sup>2</sup> If water was flowing when the samplers where visited, a grab sample was taken

Q - Qualifier

D - Dissolved

T - Total

cfs - cubic feet per second

mg/L - milligrams per liter

µs/cm - microsiemens per centimeter

su - standard units

Table 18.1-14 (Continued)

| Sample ID                       | Sample date | Electrical conductivity (EC) (µs/cm) | Copper, D (mg/L) | Q | Fluoride (mg/L) | Q | Hydroxide as CaCO3 (mg/L) | Q | Iron, D (mg/L) | Iron, T (mg/L) | Q | Lead, D (mg/L) | Magnesium, D (mg/L) | Q | Manganese, D (mg/L) | Manganese, T (mg/L) | Q | Mercury (mg/L) | Q | Nitrate/Nitrite as N (mg/L) | pH (su) | Q |
|---------------------------------|-------------|--------------------------------------|------------------|---|-----------------|---|---------------------------|---|----------------|----------------|---|----------------|---------------------|---|---------------------|---------------------|---|----------------|---|-----------------------------|---------|---|
| Upper No Name <sup>1</sup>      | 7/29/1998   | 150                                  | -                |   | 0.19            |   | -                         |   | 0.58           | 6020           |   | -              | 2.1                 |   | 0.24                | 1.28                |   | -              |   | -                           | 8.10    |   |
| Upper No Name <sup>1</sup>      | 9/30/1998   | 290                                  | -                |   | 0.26            |   | -                         |   | 0.46           | 5              |   | -              | 2.3                 |   | 0.043               | 0.13                |   | -              |   | -                           | 8.40    |   |
| Upper No Name #2                | 2/13/2008   | 197                                  | 0.0067           |   | 0.20            | < | 10                        |   | 0.28           | 66             |   | 0.0002         | 0.9                 | < | 0.005               | 1.27                | < | 0.0002         |   | 0.26                        | 8.16    |   |
| Upper No Name #3                | 2/13/2008   | 217                                  | 0.0124           |   | 0.30            | < | 10                        |   | 0.80           | 88             |   | 0.0006         | 1.4                 |   | 0.008               | 1.96                | < | 0.0002         |   | 0.33                        | 8.16    |   |
| Upper No Name grab <sup>2</sup> | 2/13/2008   | 337                                  | 0.0099           |   | 0.30            | < | 10                        |   | 0.41           | 35             |   | 0.0003         | 1.2                 | < | 0.005               | 0.40                | < | 0.0002         |   | 0.40                        | 8.12    |   |
| Upper No Name #2                | 7/21/2008   | 205                                  | 0.007            |   | 0.3             | < | 10                        |   | 0.10           | 108            | < | 0.001          | 1.1                 |   | 0.090               | 2.55                |   | 0.0003         |   | 0.04                        | 8.07    |   |
| Upper No Name #3                | 7/21/2008   | 215                                  | 0.008            |   | 0.3             | < | 10                        |   | 0.08           | 123            | < | 0.001          | 1.2                 |   | 0.115               | 2.67                |   | 0.0003         | < | 0.02                        | 8.02    |   |
| Upper No Name #1                | 8/12/2008   | 270                                  | 0.0044           | < | 0.2             | < | 10                        | < | 0.05           | 7.07           | < | 0.0001         | 1.5                 |   | 0.040               | 4.36                | < | 0.0002         |   | 0.06                        | 7.83    | < |
| Upper No Name #2                | 8/12/2008   | 286                                  | 0.0044           | < | 0.2             | < | 10                        | < | 0.05           | 3.24           | < | 0.0001         | 1.4                 | < | 0.005               | 1.56                | < | 0.0002         |   | 0.06                        | 7.88    |   |
| Upper No Name #3                | 8/12/2008   | 241                                  | 0.0042           | < | 0.2             | < | 10                        |   | 0.10           | 3.43           |   | 0.0002         | 1.2                 | < | 0.005               | 2.17                | < | 0.0002         |   | 0.03                        | 7.92    |   |
| Lower No Name #1                | 8/13/1998   | 1020                                 | -                |   | 0.64            |   | -                         |   | 0.45           | 5              |   | -              | 10.7                |   | 0.034               | 0.13                |   | -              |   | -                           | 7.60    |   |
| Lower No Name #2                | 8/14/1998   | 1050                                 | -                |   | 0.68            |   | -                         |   | 0.05           | 1              |   | -              | 14.0                | < | 0.005               | 0.02                |   | -              |   | -                           | 8.00    |   |
| Lower No Name <sup>1</sup>      | 9/30/1998   | 730                                  | -                |   | 0.89            |   | -                         |   | 3.31           | 290            |   | -              | 8.8                 |   | 0.8                 | 6.38                |   | -              |   | -                           | 7.70    |   |
| Lower No Name #1                | 8/28/2007   | 612                                  | 0.0072           |   | 0.4             | < | 10                        | < | 0.05           | 258            | < | 0.0001         | 4.5                 |   | 0.007               | 5.79                | < | 0.0002         |   | 2.94                        | 7.91    |   |
| Lower No Name #2                | 8/28/2007   | 498                                  | 0.0056           |   | 0.3             | < | 10                        | < | 0.05           | 419            | < | 0.0001         | 3.9                 |   | 0.010               | 10.3                | < | 0.0002         |   | 2.94                        | 7.90    | < |
| Lower No Name #1                | 8/12/2008   | 1170                                 | 0.0057           | < | 0.2             | < | 10                        |   | 1.59           | 8.1            |   | 0.0092         | 17.7                |   | 0.233               | 13.1                | < | 0.0002         |   | 0.41                        | 7.29    |   |
| Lower No Name #2                | 8/12/2008   | 1000                                 | 0.0063           | < | 0.2             | < | 10                        |   | 0.08           | 16.4           |   | 0.0002         | 14.7                |   | 0.568               | 13.6                | < | 0.0002         |   | 0.06                        | 7.33    |   |
| Lower No Name #3                | 8/12/2008   | 1330                                 | 0.0063           | < | 0.2             | < | 10                        |   | 0.08           | 17.0           |   | 0.0002         | 22.6                |   | 0.206               | 25.5                | < | 0.0002         |   | 0.09                        | 7.17    | < |

<sup>1</sup> Sampler designation was only provided if more than one sampler contained water

<sup>2</sup> If water was flowing when the samplers where visited, a grab sample was taken

Q - Qualifier

D - Dissolved

T - Total

cfs - cubic feet per second

mg/L - milligrams per liter

µs/cm - microsiemens per centimeter

su - standard units

Table 18.1-14 (Continued)

| Sample ID                       | Sample date | Phosphorous, T (mg/L) | Potassium, D (mg/L) | Sodium adsorption ration ( SAR) | Q | Selenium, D (mg/L) | Q | Settleable solids (mL/L) | Q | Silver, D (mg/L) | Sodium, D (mg/L) | Q | Sulfate (mg/L) | Total dissolved solids (TDS) (mg/L) | Total suspended solids (TSS) (mg/L) | Q | Zinc, D (mg/L) |
|---------------------------------|-------------|-----------------------|---------------------|---------------------------------|---|--------------------|---|--------------------------|---|------------------|------------------|---|----------------|-------------------------------------|-------------------------------------|---|----------------|
| Upper No Name <sup>1</sup>      | 7/29/1998   | -                     | 6.0                 | 0.8                             | < | 0.005              |   | 3                        |   | -                | 18.6             |   | 16             | 100                                 | 7,400                               |   | -              |
| Upper No Name <sup>1</sup>      | 9/30/1998   | -                     | 8.2                 | 0.7                             | < | 0.005              |   | 0.1                      |   | -                | 17.3             |   | 7              | 190                                 | 1,520                               |   | -              |
| Upper No Name #2                | 2/13/2008   | 0.26                  | 3.7                 | -                               | < | 0.001              |   | 1.6                      | < | 0.00005          | 27.4             | < | 10             | 320                                 | 2,550                               |   | 0.004          |
| Upper No Name #3                | 2/13/2008   | 0.19                  | 4.8                 | -                               | < | 0.001              |   | 3.7                      |   | 0.00024          | 35.3             | < | 10             | 160                                 | 5,520                               |   | 0.005          |
| Upper No Name grab <sup>2</sup> | 2/13/2008   | 0.29                  | 3.9                 | -                               | < | 0.001              | < | 0.5                      |   | 0.00007          | 44.9             |   | 30             | 490                                 | 367                                 |   | 0.007          |
| Upper No Name #2                | 7/21/2008   | 0.12                  | 3.3                 | 0.7                             | < | 0.01               |   | 8.4                      | < | 0.0005           | 24.5             | < | 10             | 180                                 | 8,100                               |   | 0.03           |
| Upper No Name #3                | 7/21/2008   | 0.09                  | 3.5                 | 0.7                             | < | 0.01               |   | 8.4                      | < | 0.0005           | 25.2             | < | 10             | 135                                 | 6,780                               |   | 0.03           |
| Upper No Name #1                | 8/12/2008   | 0.05                  | 4.5                 | -                               | < | 0.001              |   | 27.9                     | < | 0.00005          | 25.9             | < | 10             | 220                                 | 19,400                              |   | 0.002          |
| Upper No Name #2                | 8/12/2008   | 0.13                  | 4.2                 | -                               | < | 0.001              |   | 18.1                     | < | 0.00005          | 28.8             |   | 16             | 195                                 | 15,900                              |   | 0.001          |
| Upper No Name #3                | 8/12/2008   | 0.79                  | 4.0                 | -                               |   | -                  |   | 12.3                     | < | 0.00005          | 23.5             | < | 10             | 160                                 | 8,170                               |   | 0.001          |
| Lower No Name #1                | 8/13/1998   | -                     | 13.6                | 2.0                             | < | 0.005              |   | 162                      |   | -                | 82.9             |   | 131            | 530                                 | 26,100                              |   | -              |
| Lower No Name #2                | 8/14/1998   | -                     | 29.5                | 2.0                             | < | 0.005              |   | 194                      |   | -                | 95.0             |   | 383            | 840                                 | 78,400                              |   | -              |
| Lower No Name <sup>1</sup>      | 9/30/1998   | -                     | 9.6                 | 1.7                             | < | 0.0                |   | 251.0                    |   | -                | 60.6             |   | 142            | 520                                 | 36,800                              |   | -              |
| Lower No Name #1                | 8/28/2007   | 0.12                  | 7.7                 | -                               |   | 0.001              |   | 121                      | < | 0.00005          | 64.9             |   | 220            | 445                                 | 16,700                              |   | 0.010          |
| Lower No Name #2                | 8/28/2007   | 0.05                  | 10.0                | -                               |   | 0.001              |   | 77.7                     | < | 0.00005          | 44.7             |   | 152            | 385                                 | 31,500                              |   | 0.002          |
| Lower No Name #1                | 8/12/2008   | 0.13                  | 11.3                | -                               |   | 0.001              |   | 571                      | < | 0.00005          | 67.1             |   | 380            | 810                                 | 394,000                             |   | 0.001          |
| Lower No Name #2                | 8/12/2008   | 35.0                  | 10.8                | -                               |   | 0.001              |   | 450                      | < | 0.00005          | 55.1             |   | 265            | 670                                 | 246,000                             |   | 0.004          |
| Lower No Name #3                | 8/12/2008   | 0.05                  | 11.0                | -                               |   | 0.001              |   | 670                      |   | 0.00135          | 75.4             |   | 600            | 1030                                | 395,000                             |   | 0.004          |

<sup>1</sup> Sampler designation was only provided if more than one sampler contained water

<sup>2</sup> If water was flowing when the samplers where visited, a grab sample was taken

Q - Qualifier

D - Dissolved

T - Total

cfs - cubic feet per second

mg/L - milligrams per liter

µs/cm - microsiemens per centimeter

su - standard units



Table 18.1-15 Water Quality Data on Brimhall Wash for Site N (Upstream) and Site M (Downstream) Between March 14, 1990 and January 8, 1995

| Sample date | Alkalinity as CaCO3 (mg/L) | Bicarb as CaCO3 (mg/L) | Q | Boron, T (mg/L) | Q | Cation anion balance (CAB) % | Q | Cadmium, T (mg/L) | Calcium, D (mg/L) | Q | Chloride (mg/L) | Electrical conductivity (EC) (µs/cm) | Q | Fluoride (mg/L) | Hardness as CaCO3 (calc) | Q    | Iron, D (mg/L) | Iron, T (mg/L) | Q |
|-------------|----------------------------|------------------------|---|-----------------|---|------------------------------|---|-------------------|-------------------|---|-----------------|--------------------------------------|---|-----------------|--------------------------|------|----------------|----------------|---|
| Site M      |                            |                        |   |                 |   |                              |   |                   |                   |   |                 |                                      |   |                 |                          |      |                |                |   |
| 3/14/1990   |                            | 156                    | < | 5               |   |                              |   |                   | 188               |   | 39.4            | 718                                  |   | 1.2             | 774                      |      | 173            | 234            |   |
| 5/14/1990   |                            | 133                    | < | 5               |   |                              |   |                   | 411               |   | 4.04            | 1280                                 |   | 0.295           | 1040                     |      | 0.11           | 0.65           |   |
| 7/23/1990   |                            | 461                    | < | 5               |   |                              |   |                   | 400               |   | 10.4            | 27800                                |   | 0.656           | 1390                     |      | 1.15           | 10.1           |   |
| 8/24/1990   |                            | 190                    | < | 5               |   |                              |   |                   | 316               |   | 20.3            | 2550                                 |   | 0.398           | 823                      |      | 0.21           | 0.58           |   |
| 9/29/1990   |                            | 89                     | < | 5               |   |                              |   |                   | 480               |   | 4.47            | 222                                  |   | 0.23            | 1203                     |      | 2.39           | 3.69           |   |
| 10/22/1990  |                            | 88.9                   | < | 5               |   |                              | < | 0.005             | 18                |   | 4.6             | 359                                  |   | 0.33            | 53                       |      | 1.76           | 1.8            | < |
| 11/19/1990  |                            | 135                    | < | 5               |   |                              | < | 0.005             | 16.7              |   | 13.4            | 489                                  |   | 0.65            | 53                       |      | 20.9           | 23             | < |
| 1/20/1991   |                            | 530                    | < | 5               |   |                              |   |                   | 550               |   | 82.2            | 7360                                 |   | 0.93            | 1000                     |      | 0.72           | 0.72           |   |
| 6/21/1991   |                            | 1170                   | < | 2.5             |   |                              |   |                   | 28.3              |   | 47.1            | 1540                                 |   | 0.3             | 2650                     |      | 3.66           | 9.71           |   |
| 1/1/1992    |                            | 330                    | < | 2.5             |   |                              |   |                   | 633               |   | 21.1            | 912                                  | < | 0.1             | 1700                     |      | 580            | 582            |   |
| 7/14/1992   | 494                        | 494                    |   |                 | < | 0.84                         |   |                   | 35                |   | 10              | 571                                  |   | 0.6             | 100                      |      | 0.53           | 420            |   |
| 8/31/1992   | 146                        | 146                    |   |                 |   | 4.52                         |   |                   | 13                |   | 10              | 798                                  |   | 1.5             | 37                       |      | 0.94           | 1520           |   |
| 1/1/1993A   | 266                        | 262                    |   |                 | < | 0.47                         |   |                   | 42                |   | 13              | 2180                                 |   | 2               | 126                      | <    | 0.02           | 5.36           |   |
| 1/1/1993B   | 116                        | 116                    |   |                 | < | 3.15                         |   |                   | 60                |   | 13              | 418                                  |   | 0.9             | 146                      |      | 0.16           | 716            |   |
| 3/11/1993   | 140                        | 140                    |   |                 |   | 3.85                         |   |                   | 9                 |   | 11              | 732                                  |   | 0.9             | 31                       |      | 12             | 171            |   |
| 9/6/1993    | 216                        | 216                    |   |                 | < | 2.14                         |   |                   | 28                |   | 8               | 1040                                 |   | 0.9             | 78                       |      | 0.14           | 1210           |   |
| 7/10/1994   | 135                        | 135                    |   |                 | < | 1.59                         |   |                   | 22                |   | 7               |                                      |   | 1.5             | 51                       |      | 0.06           | 163            |   |
| 10/2/1994   | 210                        | 210                    |   |                 |   |                              |   |                   | 53                |   | 21              |                                      |   | 0.4             | 153                      |      | 2.74           | 4.49           |   |
| 1/8/1995    | 172                        | 172                    |   |                 |   |                              |   |                   | 3.5               |   | 4               |                                      |   | 0.6             | 10                       |      | 0.25           | 520            |   |
| Site N      |                            |                        |   |                 |   |                              |   |                   |                   |   |                 |                                      |   |                 |                          |      |                |                |   |
| 5/14/1990   |                            | 277                    | < | 5               |   |                              |   |                   | 26                |   | 13.2            | 1210                                 |   | 1.1             | 80                       |      | 0.18           | 0.8            |   |
| 6/19/1990   |                            | 299                    | < | 5               |   |                              |   |                   | 38.7              |   | 15.3            | 1440                                 |   | 0.848           | 115                      |      | 0.28           | 1.72           |   |
| 8/24/1990   |                            | 518                    | < | 5               |   |                              |   |                   | 238               |   | 4.96            | 1332                                 |   | 0.942           | 599                      |      | 2.1            | 2.6            |   |
| 10/22/1990  |                            | 221                    | < | 5               |   |                              | < | 0.005             | 22.2              |   | 7.2             | 1120                                 |   | 0.89            | 68                       |      | 0.49           | 1.11           | < |
| 1/20/1991   |                            | 588                    | < | 5               |   |                              |   |                   | 354               |   | 360             | 1256                                 | < | 0.2             | 2200                     |      | 25.7           | 398            |   |
| 6/21/1991   |                            | 268                    | < | 2.5             |   |                              |   |                   | 22.2              |   | 7.94            | 676                                  |   | 1.1             | 84                       |      | 1.13           | 2.31           |   |
| 8/20/1991   |                            | 407                    | < | 2.5             |   |                              |   |                   | 43.7              |   | 4.2             |                                      |   | 2200            |                          | 7.26 | 410            |                |   |
| 9/26/1991   |                            | 363                    | < | 2.5             |   |                              |   |                   | 38                | < | 0.5             | 1420                                 |   | 0.77            | 120                      |      | 0.17           | 0.27           |   |
| 1/1/1992    |                            | 290                    | < | 2.5             |   |                              |   |                   | 123               |   | 32.3            | 996                                  |   | 0.2             | 150                      |      | 97.8           | 388            |   |
| 7/14/1992   | 192                        | 192                    |   |                 |   | 1.59                         |   |                   | 26                |   | 24              | 1510                                 |   | 2               | 73                       | <    | 0.02           | 2860           |   |
| 8/31/1992   | 250                        | 250                    |   |                 | < | 5.24                         |   |                   | 49                |   | 46              | 1460                                 |   | 1.7             | 143                      |      | 0.43           | 2080           |   |
| 1/1/1993    | 88                         | 88                     |   |                 |   | 1.26                         |   |                   | 38                |   | 14              | 1050                                 |   | 1.2             | 111                      |      | 0.22           | 255            |   |
| 3/11/1993   | 165                        | 165                    |   |                 | < | 0.42                         |   |                   | 20                |   | 16              | 985                                  |   | 1.1             | 58                       |      | 0.15           | 276            |   |
| 9/29/1993   |                            |                        |   |                 |   |                              |   |                   | 1246              |   | 15              | 142                                  | < | 0.1             | 4370                     |      | 730            | 4510           |   |
| 7/10/1994   | 260                        | 260                    |   |                 | < | 4.49                         |   |                   | 27                |   | 17              |                                      |   | 1.4             | 63                       |      | 0.33           | 3060           |   |
| 10/2/1994   | 950                        | 950                    |   |                 |   |                              |   |                   | 29                |   | 8               |                                      |   | 1.3             | 85                       |      | 0.11           | 7480           |   |
| 1/8/1995    | 182                        | 182                    |   |                 |   |                              |   |                   | 3.5               |   | 10              |                                      |   | 1               | 14                       |      | 0.05           | 1000           |   |

Q - Qualifier  
 BDL - Below Detection Limit  
 D - Dissolved  
 T - Total  
 mg/L - milligrams per liter  
 µs/cm - microsiemens per centimeter  
 su - standard units

Table 18.1-15 (Continued)

| Sample date | Lead, T (mg/L) | Q | Magnesium D (mg/L) | Q | Manganese D (mg/L) | Manganese, T (mg/L) | Q | Mercury, D (mg/L) | Q | Mercury, T (mg/L) | Q | Nitrate nitrogen | Nitrate/Nitrite as N (mg/L) | Q | Nitrite as N (mg/L) | Q | Nitrogen, total Kjeldahl | pH (su) | Potassium, D (mg/L) |
|-------------|----------------|---|--------------------|---|--------------------|---------------------|---|-------------------|---|-------------------|---|------------------|-----------------------------|---|---------------------|---|--------------------------|---------|---------------------|
| Site M      |                |   |                    |   |                    |                     |   |                   |   |                   |   |                  |                             |   |                     |   |                          |         |                     |
| 3/14/1990   |                |   | 74                 |   |                    | 4.45                |   |                   |   |                   |   | 3.08             |                             |   |                     |   |                          | 7.89    | 154                 |
| 5/14/1990   |                |   | 3.28               |   |                    | 0.37                |   |                   |   |                   |   | 0.383            |                             |   |                     |   |                          | 7.49    | 5.08                |
| 7/23/1990   |                |   | 95                 |   |                    | 13.8                |   |                   |   |                   |   | 0.484            |                             |   |                     |   |                          | 7.99    | 19.1                |
| 8/24/1990   |                |   | 8.2                |   |                    | 1.59                |   |                   |   |                   |   | 0.373            |                             |   |                     |   |                          | 8.58    | 5.22                |
| 9/29/1990   |                |   | 1.1                |   |                    | 0.05                |   |                   |   |                   |   | 0.355            |                             |   |                     |   |                          | 7.87    | 3.8                 |
| 10/22/1990  | 0.05           |   | 1.9                |   |                    | 0.02                |   | <                 |   | 0.0005            |   | 0.6              |                             |   |                     |   |                          | 7.96    | 3.29                |
| 11/19/1990  | 0.05           |   | 2.76               |   |                    | 0.16                |   |                   |   | 0.0006            |   | 0.66             |                             |   |                     |   |                          | 8.18    | 15.9                |
| 1/20/1991   |                |   | 73.9               |   |                    | 0.04                |   |                   |   |                   |   | 0.06             |                             |   |                     |   |                          | 7.16    | 8.7                 |
| 6/21/1991   |                |   | 4.25               |   |                    | 0.07                |   |                   |   |                   |   | 0.31             |                             |   |                     |   |                          | 7.29    | 11.3                |
| 1/1/1992    |                |   | 83.5               |   |                    | 5.94                |   |                   |   |                   |   | 1.63             |                             |   |                     |   |                          | 8.13    | 164                 |
| 7/14/1992   |                |   | 3                  |   | 0.38               |                     |   |                   |   |                   |   | 0.05             | 0.13                        |   | 0.08                |   |                          | 7.7     | 4                   |
| 8/31/1992   |                |   | 1                  |   | 0.02               |                     |   |                   |   |                   |   | 0.7              | 0.7                         | < | 0.01                |   |                          | 8.1     | 4                   |
| 1/1/1993A   |                |   | 5                  | < | 0.01               |                     | < | 0.0001            |   |                   |   | 1.36             | 1.36                        | < | 0.01                |   |                          | 8.4     | 1                   |
| 1/1/1993B   |                | < | 1                  | < | 0.01               |                     |   |                   |   |                   |   | 3.54             | 3.59                        |   | 0.05                |   |                          | 7.8     | 1                   |
| 3/11/1993   |                |   | 2                  |   | 7                  |                     |   |                   |   |                   |   | 1.22             | 1.24                        |   | 0.02                |   |                          | 8.3     | 3                   |
| 9/6/1993    |                |   | 2                  |   | 0.01               |                     |   |                   |   |                   |   | 1.92             | 1.98                        |   | 0.06                |   | 9.4                      | 8       | 4                   |
| 7/10/1994   |                | < | 1                  | < | 0.01               |                     |   |                   |   |                   |   | 0.67             | 1.3                         |   | 0.63                |   | 2.4                      | 7.6     | 4                   |
| 10/2/1994   |                |   | 5                  |   | 1.04               |                     |   |                   |   |                   |   | 0.04             | 0.04                        | < | 0.01                | < | 0.1                      | 7.5     | 6                   |
| 1/8/1995    |                |   | 0.3                |   |                    |                     |   |                   |   |                   |   | 7.7              | 7.8                         |   | 0.11                |   | 3.7                      | 8.3     | 1.7                 |
| Site N      |                |   |                    |   |                    |                     |   |                   |   |                   |   |                  |                             |   |                     |   |                          |         |                     |
| 5/14/1990   |                |   | 3.67               |   |                    | 0.17                |   |                   |   |                   |   | 0.651            |                             |   |                     |   |                          | 7.43    | 5.61                |
| 6/19/1990   |                |   | 4.57               |   |                    | 1.4                 |   |                   |   |                   |   | 0.289            |                             |   |                     |   |                          | 7.21    | 4.94                |
| 8/24/1990   |                |   | 1.1                |   |                    | 0.11                |   |                   |   |                   |   | 0.61             |                             |   |                     |   |                          | 7.87    | 5.29                |
| 10/22/1990  | 0.05           |   | 3.03               |   |                    | 0.1                 |   | <                 |   | 0.0005            |   | 0.23             |                             |   |                     |   |                          | 7.51    | 3.88                |
| 1/20/1991   |                |   | 172                |   |                    | 5.05                |   |                   |   |                   |   | 1.83             |                             |   |                     |   |                          | 7.57    | 17.6                |
| 6/21/1991   |                |   | 3.19               |   |                    | 0.39                |   |                   |   |                   | < | 0.05             |                             |   |                     |   |                          | 7.51    | 3.38                |
| 8/20/1991   |                |   | 6.7                |   |                    | 7.21                |   |                   |   |                   |   | 0.39             |                             |   |                     |   |                          | 7.98    | 0.81                |
| 9/26/1991   |                |   | 6.91               |   |                    | 0.83                |   |                   |   |                   | < | 0.05             |                             |   |                     |   |                          | 6.95    | 5                   |
| 1/1/1992    |                |   | 44.5               |   |                    | 2.97                |   |                   |   |                   |   | 0.11             |                             |   |                     |   |                          | 7.98    | 4.72                |
| 7/14/1992   |                |   | 2                  | < | 0.01               |                     |   |                   |   |                   |   | 1.2              | 1.2                         | < | 0.01                |   |                          | 8.2     | 3                   |
| 8/31/1992   |                |   | 5                  |   | 0.08               |                     |   |                   |   |                   |   | 0.25             | 0.31                        |   | 0.06                |   |                          | 8.1     | 5                   |
| 1/1/1993    |                |   | 4                  | < | 0.01               |                     |   |                   |   |                   |   | 2.11             | 2.14                        |   | 0.03                |   |                          | 8.1     | 3                   |
| 3/11/1993   |                |   | 2                  | < | 0.01               |                     |   |                   |   |                   |   | 1.81             | 1.81                        | < | 0.01                |   |                          | 8       | 3                   |
| 9/29/1993   |                |   | 306                |   | 39                 |                     |   |                   |   |                   |   | 13498.4          | 13500                       |   | 1.6                 |   |                          | 0.6     | 90                  |
| 7/10/1994   |                | < | 1                  | < | 0.01               |                     |   |                   |   |                   |   | 0.58             | 0.86                        |   | 0.28                |   | 2.5                      | 7.8     | 4                   |
| 10/2/1994   |                |   | 3                  |   | 0.42               |                     |   |                   |   |                   |   | 0.02             | 0.02                        | < | 0.01                | < | 0.1                      | 8       | 3                   |
| 1/8/1995    |                |   | 1.2                |   |                    |                     |   |                   |   |                   |   | 3.2              | 3.2                         |   |                     |   | 5.7                      | 8.2     | 1.7                 |

Q - Qualifier  
 BDL - Below Detection Limit  
 D - Dissolved  
 T - Total  
 mg/L - milligrams per liter  
 µs/cm - microsiemens per centimeter  
 su - standard units

Table 18.1-15 (Continued)

| Sample date | Sodium adsorption ratio (SAR) | Sodium adsorption ratio (SAR) Calc. | Selenium, D (mg/L) | Q | Selenium, T (mg/L) | Q | Silica | Sodium, D (mg/L) | Sulfate (mg/L) | Q | Total dissolved solids (TDS) (mg/L) | Total suspended solids (TSS) (mg/L) | Q | Vanadium, D (mg/L) | Q | Vanadium, T (mg/L) |      |
|-------------|-------------------------------|-------------------------------------|--------------------|---|--------------------|---|--------|------------------|----------------|---|-------------------------------------|-------------------------------------|---|--------------------|---|--------------------|------|
| Site M      |                               |                                     |                    |   |                    |   |        |                  |                |   |                                     |                                     |   |                    |   |                    |      |
| 3/14/1990   |                               | 18.30                               |                    |   |                    |   | 71     | 1170             | 204            |   | 1980                                |                                     |   |                    |   | <                  | 0.5  |
| 5/14/1990   |                               | 2.71                                |                    |   |                    | < | 1      | 201              | 558            |   | 2500                                |                                     |   |                    |   | <                  | 0.05 |
| 7/23/1990   |                               | 84.04                               |                    |   |                    |   | 10.1   | 7200             | 18100          |   | 24600                               |                                     |   |                    |   | <                  | 0.5  |
| 8/24/1990   |                               | 6.61                                |                    |   |                    |   | 10.4   | 436              | 1091           |   | 1640                                |                                     |   |                    |   | <                  | 0.5  |
| 9/29/1990   |                               | 0.93                                |                    |   |                    |   | 26.2   | 74.2             | 108            |   | 360                                 |                                     |   |                    |   | <                  | 0.5  |
| 10/22/1990  |                               | 5.05                                |                    | < | 0.005              | < | 1      | 84.3             | 85             |   | 392                                 |                                     |   |                    |   | <                  | 0.5  |
| 11/19/1990  |                               | 8.30                                |                    | < | 0.005              |   | 3      | 139              | 166            |   | 404                                 |                                     |   |                    |   | <                  | 0.5  |
| 1/20/1991   |                               | 16.15                               |                    |   |                    |   | 4.6    | 1520             | 3690           |   | 5760                                |                                     |   |                    |   | <                  | 0.1  |
| 6/21/1991   |                               | 14.04                               |                    |   |                    |   | 162    | 303              | 800            |   | 1350                                |                                     |   |                    |   | <                  | 0.5  |
| 1/1/1992    |                               | 2.84                                |                    |   |                    |   | 5050   | 286              | 757            |   | 2110                                |                                     |   |                    |   |                    | 0.4  |
| 7/14/1992   |                               | 8.41                                |                    |   |                    |   | 13.5   | 193              | 29             |   | 480                                 | 61880                               | < | 0.01               |   |                    |      |
| 8/31/1992   |                               | 11.87                               |                    |   |                    |   | 19.8   | 165              | 200            |   | 540                                 | 57660                               | < | 0.01               |   |                    |      |
| 1/1/1993A   |                               | 12.63                               | 0.003              |   |                    |   | 10.9   | 325              | 539            |   | 1062                                |                                     | < | 0.01               |   |                    |      |
| 1/1/1993B   |                               | 5.26                                |                    |   |                    |   | 9.5    | 150              | 356            |   | 652                                 | 14400                               | < | 0.01               |   |                    |      |
| 3/11/1993   | 12.63                         | 12.49                               |                    |   |                    |   | 141    | 159              | 191            |   | 456                                 | 45880                               | < | 0.14               |   |                    |      |
| 9/6/1993    |                               | 10.39                               |                    |   |                    |   | 19.3   | 211              | 328            |   | 726                                 | 46200                               | < | 0.01               |   |                    |      |
| 7/10/1994   | 13.57                         |                                     |                    |   |                    |   | 16.2   |                  | 393            |   | 744                                 |                                     | < | 0.01               |   |                    |      |
| 10/2/1994   |                               |                                     |                    |   |                    |   | 19     |                  | 490            |   | 924                                 |                                     | < | 0.01               |   |                    |      |
| 1/8/1995    |                               |                                     |                    |   |                    |   | 8.4    |                  | 140            |   | 370                                 |                                     |   |                    |   |                    |      |
| Site N      |                               |                                     |                    |   |                    |   |        |                  |                |   |                                     |                                     |   |                    |   |                    |      |
| 5/14/1990   |                               | 9.78                                |                    |   |                    |   | 9.6    | 201              | 167            |   | 555                                 |                                     |   |                    |   | <                  | 0.05 |
| 6/19/1990   |                               | 15.07                               |                    |   |                    |   | 13.3   | 372              | 135            | < | 720                                 |                                     |   |                    |   | <                  | 0.05 |
| 8/24/1990   |                               | 5.34                                |                    |   |                    |   | 9.23   | 300              | 272            |   | 1000                                |                                     |   |                    |   | <                  | 0.5  |
| 10/22/1990  |                               | 11.72                               |                    | < | 0.005              |   | 1.3    | 222              | 298            |   | 956                                 |                                     |   |                    |   | <                  | 0.5  |
| 1/20/1991   |                               | 1.89                                |                    |   |                    |   | 5.3    | 173              | 3010           |   | 4381                                |                                     |   |                    |   |                    | 0.38 |
| 6/21/1991   |                               | 43.51                               |                    |   |                    |   | 10.6   | 828              | 147            |   | 640                                 |                                     |   |                    |   | <                  | 0.5  |
| 8/20/1991   |                               | 21.40                               |                    |   |                    |   | 38.2   | 575              | 1460           |   | 1010                                |                                     |   |                    |   |                    | 1.87 |
| 9/26/1991   |                               | 13.95                               |                    |   |                    |   | 12.6   | 356              | 422            |   | 968                                 |                                     |   |                    |   | <                  | 0.5  |
| 1/1/1992    |                               | 3.54                                |                    |   |                    |   | 16     | 180              | 1380           |   | 2150                                |                                     |   |                    |   |                    | 0.26 |
| 7/14/1992   |                               | 14.81                               |                    |   |                    |   | 22.8   | 291              | 447            |   | 820                                 | 115800                              | < | 0.01               |   |                    |      |
| 8/31/1992   |                               | 9.94                                |                    |   |                    |   | 18.7   | 273              | 494            |   | 1020                                | 128420                              | < | 0.01               |   |                    |      |
| 1/1/1993    |                               | 11.75                               |                    |   |                    |   | 14     | 285              | 587            |   | 960                                 | 11800                               | < | 0.01               |   |                    |      |
| 3/11/1993   | 12.23                         | 12.10                               |                    |   |                    |   | 17.9   | 212              | 329            |   | 648                                 | 110120                              | < | 0.01               |   |                    |      |
| 9/29/1993   |                               | 2.96                                |                    |   |                    |   | 311    | 450              |                |   | 2107                                |                                     | < | 0.01               |   |                    |      |
| 7/10/1994   | 15.91                         |                                     |                    |   |                    |   | 23.3   |                  | 461            |   | 1050                                |                                     | < | 0.01               |   |                    |      |
| 10/2/1994   |                               |                                     |                    |   |                    |   | 16.1   |                  | 140            |   | 520                                 |                                     | < | 0.01               |   |                    |      |
| 1/8/1995    |                               |                                     |                    |   |                    |   | 13     |                  | 220            |   | 440                                 |                                     |   |                    |   |                    |      |

Q - Qualifier  
 BDL - Below Detection Limit  
 D - Dissolved  
 T - Total  
 mg/L - milligrams per liter  
 µs/cm - microsiemens per centimeter  
 su - standard units

Pinabete Permit Application Package

Table 18.1-16 Comparison of Total Dissolved Solids and Total Suspended Solids at Site M (Downstream) on Brimhall Wash Between February 1979 and September 1982

| Date     | Grab sample | Single-stage sampler | No reference | Total solids (mg/L) | Total dissolved solids (mg/L) | Total suspended solids (mg/L) |
|----------|-------------|----------------------|--------------|---------------------|-------------------------------|-------------------------------|
| 07/01/79 |             |                      | X            | 78,820              | 11,520                        | 67,300                        |
| 02/01/79 |             |                      | X            | 39,327              | 37,489                        | 1,838                         |
| 04/16/81 | X           |                      |              | 78100               | 3400                          | 74700                         |
| 06/04/81 | X           |                      |              | 4,220               | 2,070                         | 2,150                         |
| 07/01/81 | X           |                      |              | 93,010              | 11,500                        | 81,510                        |
| 07/08/81 | X           |                      |              | 68,750              | 2,450                         | 66,300                        |
| 08/13/81 | X           |                      |              | 14,480              | 510                           | 13,970                        |
| 08/31/81 | X           |                      |              | 92,890              | 8,580                         | 84,310                        |
| 09/09/81 |             | X                    |              | 146,230             | 1,470                         | 144,760                       |
| 09/24/81 |             | X                    |              | 135,054             | 1,962                         | 133,092                       |
| 10/05/81 |             | X                    |              | 624                 | 520                           | 104                           |
| 10/05/81 |             | X                    |              | 47,140              | 860                           | 46,280                        |
| 11/30/81 |             | X                    |              | 22,700              | 420                           | 22,280                        |
| 02/16/82 | X           |                      |              | 10,354              | 254                           | 10,100                        |
| 02/25/82 | X           |                      |              | 21,461              | 451                           | 21,010                        |
| 03/03/82 | X           |                      |              | 18,107              | 537                           | 17,570                        |
| 03/17/82 | X           |                      |              | 68,133              | 693                           | 67,440                        |
| 03/29/82 | X           |                      |              | 4,192               | 720                           | 3,472                         |
| 05/03/82 | X           |                      |              | 5,548               | 579                           | 4,969                         |
| 05/05/82 | X           |                      |              | 4,320               | 210                           | 4,110                         |
| 07/19/82 | X           |                      |              | 6,038               | 877                           | 5,161                         |
| 07/26/82 | X           |                      |              | 20,370              | 370                           | > 20,000                      |
| 07/28/82 |             | X                    |              | 20,620              | 620                           | > 20,000                      |
| 07/28/82 | X           |                      |              | 21,000              | 1,100                         | > 20,000                      |
| 08/03/82 | X           |                      |              | 20,749              | 749                           | > 20,000                      |
| 08/12/82 |             |                      | X            | 20,848              | 843                           | > 20,000                      |
| 08/17/82 |             |                      | X            | 5,910               | 1,000                         | 4,910                         |
| 08/23/82 | X           |                      |              | 19183               | 863                           | 18,320                        |
| 08/25/82 | X           |                      |              | 20841               | 841                           | > 20,000                      |
| 09/10/82 |             |                      | X            | 20873               | 873                           | > 20,000                      |
| 09/13/82 |             |                      | X            | 20,570              | 570                           | > 20,000                      |
| Average  |             |                      |              | 37,112              | 3,061                         | > 34,053                      |
| Median   |             |                      |              | 20,841              | 843                           | > 20,000                      |

mg/L - milligrams per liter

*Pinabete Permit Application Package*

Table 18.1-17 Comparison of Total Dissolved Solids and Total Suspended Solids on at Site N (Upstream) on Brimhall Wash between February 1979 and September 1982

| Date     | Grab sample | Single-stage sampler | No reference | Total solids (mg/L) | Total dissolved solids (mg/L) | Total suspended solids (mg/L) |
|----------|-------------|----------------------|--------------|---------------------|-------------------------------|-------------------------------|
| 07/01/79 |             |                      | X            | 64,497              | 24,373                        | 40,124                        |
| 04/16/81 | X           |                      |              | 71,790              | 90                            | 71,700                        |
| 06/04/81 |             | X                    |              | QNS                 |                               |                               |
| 07/01/81 | X           |                      |              | 55,730              | 10,280                        | 45,450                        |
| 07/08/81 | X           |                      |              | 69,550              | 4,220                         | 65,330                        |
| 07/10/81 |             | X                    |              | 126,720             | 1,844                         | 124,876                       |
| 08/12/81 |             | X                    |              | 149,080             | 2,110                         | 146,970                       |
| 08/31/81 | X           |                      |              | 35,470              | 9,050                         | 26,420                        |
| 09/09/81 | X           |                      |              | 172,938             | 1,910                         | 171,028                       |
| 09/24/81 | X           |                      |              | 24,568              | 2,404                         | 22,164                        |
| 10/05/81 | X           |                      |              |                     | QNS                           | 77,780                        |
| 11/30/81 | X           |                      |              | 89,850              | 690                           | 89,160                        |
| 02/16/82 | X           |                      |              | 7,430               | 220                           | 7,210                         |
| 02/25/82 | X           |                      |              | 31,310              | 380                           | 30,930                        |
| 03/03/82 | X           |                      |              | 21,210              | 400                           | 20,810                        |
| 03/17/82 | X           |                      |              | 20,341              | 391                           | 19,950                        |
| 03/29/82 | X           |                      |              | 4,046               | 600                           | 3,446                         |
| 05/03/82 | X           |                      |              | 4,729               | 389                           | 4,340                         |
| 05/05/82 | X           |                      |              | 4,413               | 420                           | 3,993                         |
| 07/28/82 |             | X                    |              | 21,062              | 1,062                         | > 20,000                      |
| 08/03/82 | X           |                      |              | 20,890              | 890                           | > 20,000                      |
| 08/12/82 |             | X                    |              | 20,820              | 820                           | > 20,000                      |
| 08/17/82 | X           | X                    |              | 5,169               | 449                           | 4,720                         |
| 08/23/82 | X           |                      |              | 19,900              | 900                           | 19,000                        |
| 09/10/82 |             | X                    |              | 20,800              | 800                           | > 20,000                      |
| 09/13/82 |             | X                    |              | 20,870              | 870                           | > 20,000                      |
| Average  |             |                      |              | 45,133              | 2,732                         | > 49,770                      |
| Median   |             |                      |              | 21,136              | 845                           | 20,810                        |

mg/L - milligrams per liter  
 QNS - Quantity not sufficient

Table 18.1-18 Surface Water Quality for Other Bodies of Water Within and Adjacent to the NMEP Permit Area

| Sample ID   | Sample date | Alkalinity as CaCO3 (mg/L) | Aluminum, D (mg/L) | Aluminum, T (mg/L) | Arsenic, D (mg/L) | Arsenic, T (mg/L) | Barium, D (mg/L) | Barium, T (mg/L) | Bicarbonate as CaCO3 (mg/L) | Boron, D (mg/L) | Cation anion balance (CAB) (%) | Cadmium, D (mg/L) | Calcium, D (mg/L) | Carbonate as CaCO3 (mg/L) | Chloride (mg/L) | Chromium, D (mg/L) | Cobalt, D (mg/L) |
|---|-------------|----------------------------|--------------------|--------------------|-------------------|-------------------|------------------|------------------|-----------------------------|-----------------|--------------------------------|-------------------|-------------------|---------------------------|-----------------|--------------------|------------------|
| Ponds within Pinabete watershed                                   |             |                            |                    |                    |                   |                   |                  |                  |                             |                 |                                |                   |                   |                           |                 |                    |                  |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | 4/10/08     | -                          | -                  | 19.9               | -                 | 0.0008            | -                | 0.175            | -                           | 0.2             | -                              | < 0.00005         | -                 | -                         | -               | 0.006              | 0.00029          |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | 5/12/08     | -                          | -                  | 181                | -                 | 0.0051            | -                | 0.905            | -                           | 0.4             | -                              | < 0.00005         | -                 | -                         | -               | 0.008              | 0.00257          |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | 7/21/08     | 248                        | 0.38               | -                  | < 0.005           | -                 | 0.124            | -                | 248                         | 0.2             | 3.92                           | 0.0054            | 54.2              | < 10                      | 11              | < 0.01             | -                |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | 8/12/08     | -                          | -                  | 3.64               | -                 | 0.0020            | -                | 0.2250           | -                           | 0.2             | -                              | 0.00107           | -                 | -                         | -               | < 0.001            | 0.00080          |
| Stevenson's Well Site Pond (aka Well Site Pond)                   | 7/21/08     | 312                        | < 0.10             | -                  | < 0.005           | -                 | 0.208            | -                | 312                         | 0.2             | 2.29                           | 0.0083            | 44.6              | < 10                      | 19              | < 0.01             | -                |
| Stevenson's Well Site Pond (aka Well Site Pond)                   | 8/12/08     | -                          | -                  | 1.83               | -                 | < 0.0025          | -                | 0.1550           | -                           | < 0.1           | -                              | 0.01397           | -                 | -                         | -               | < 0.001            | 0.00030          |
| Ponds within No Name watershed                                    |             |                            |                    |                    |                   |                   |                  |                  |                             |                 |                                |                   |                   |                           |                 |                    |                  |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 4/30/98     | -                          | -                  | -                  | -                 | -                 | -                | -                | 129                         | 0.10            | -                              | -                 | 17                | 1                         | 17              | -                  | -                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 5/15/98     | -                          | -                  | -                  | -                 | -                 | -                | -                | 162                         | 0.12            | -                              | -                 | 15                | < 1                       | 19              | -                  | -                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 7/29/98     | -                          | -                  | -                  | -                 | -                 | -                | -                | 109                         | < 0.05          | -                              | -                 | 24                | < 1                       | 4               | -                  | -                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 8/20/98     | -                          | -                  | -                  | -                 | -                 | -                | -                | 170                         | 0.06            | -                              | -                 | 42                | < 1                       | 7               | -                  | -                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 8/26/98     | -                          | -                  | -                  | -                 | -                 | -                | -                | 135                         | < 0.05          | -                              | -                 | 41                | < 1                       | 6               | -                  | -                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 9/30/98     | -                          | -                  | -                  | -                 | -                 | -                | -                | 195                         | 0.07            | -                              | -                 | 46                | < 1                       | 6               | -                  | -                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 11/7/98     | -                          | -                  | -                  | -                 | -                 | -                | -                | 204                         | 0.08            | -                              | -                 | 43                | < 1                       | 6               | -                  | -                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 12/1/98     | -                          | -                  | -                  | -                 | -                 | -                | -                | 165                         | 0.08            | -                              | -                 | 45                | < 1                       | 67              | -                  | -                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 4/10/08     | -                          | -                  | 32.4               | -                 | 0.0013            | -                | 0.356            | -                           | 0.3             | -                              | 0.00025           | -                 | -                         | -               | 0.004              | 0.00151          |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 8/12/08     | -                          | -                  | 1.67               | -                 | < 0.0025          | -                | 0.1130           | -                           | < 0.10          | -                              | 0.00010           | -                 | -                         | -               | < 0.001            | 0.00018          |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 4/1/09      | 189                        | 0.13               | 16.60              | 0.002             | 0.0028            | 0.124            | 0.2520           | 185                         | 0.20            | 0.07                           | < 0.00005         | 26                | < 10                      | 18              | 0.006              | 0.00052          |

D - Dissolved  
T - Total  
mg/L - milligrams per liter  
µs/cm - microsiemens per centimeter  
su - standard units

Table 18.1-18 (Continued)

| Sample ID   | Electrical conductivity (EC) (µs/cm) | Copper, D (mg/L) | Fluoride (mg/L) | Hardness (calc) | Hydroxide as CaCO3 (mg/L) | Iron, D (mg/L) | Iron, T (mg/L) | Lead, D (mg/L) | Magnesium, D (mg/L) | Manganese, D (mg/L) | Manganese, T (mg/L) | Mercury, T (mg/L) | Nitrate/Nitrite as N (mg/L) | pH (su) | Phosphorous, T (mg/L) | Potassium, D (mg/L) | Sodium adsorption ratio (SAR) |
|---|--------------------------------------|------------------|-----------------|-----------------|---------------------------|----------------|----------------|----------------|---------------------|---------------------|---------------------|-------------------|-----------------------------|---------|-----------------------|---------------------|-------------------------------|
| Ponds within Pinabete watershed                                   |                                      |                  |                 |                 |                           |                |                |                |                     |                     |                     |                   |                             |         |                       |                     |                               |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | -                                    | 0.0064           | -               | -               | -                         | -              | -              | < 0.0001       | -                   | -                   | -                   | < 0.0002          | -                           | -       | -                     | -                   | -                             |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | -                                    | 0.0356           | -               | -               | -                         | -              | -              | 0.0002         | -                   | -                   | -                   | 0.0008            | -                           | -       | -                     | -                   | -                             |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | 673                                  | 0.016            | 0.9             | 162             | < 10                      | 0.39           | 19             | 0.007          | 6.4                 | 0.377               | 0.910               | 0.0002            | < 0.02                      | 7.62    | 0.18                  | 12.1                | -                             |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | -                                    | 0.0068           | -               | -               | -                         | -              | -              | 0.0016         | -                   | -                   | -                   | < 0.0002          | -                           | -       | -                     | -                   | -                             |
| Stevenson's Well Site Pond (aka Well Site Pond)                   | 608                                  | 0.014            | 1.2             | -               | < 10                      | 0.05           | 383            | < 0.001        | < 0.5               | 0.357               | 9.26                | 0.0008            | 0.03                        | 7.80    | < 0.05                | 7.5                 | 0.7                           |
| Stevenson's Well Site Pond (aka Well Site Pond)                   | -                                    | 0.0068           | -               | -               | -                         | -              | -              | 0.0016         | -                   | -                   | -                   | < 0.0002          | -                           | -       | -                     | -                   | -                             |
| Ponds within No Name watershed                                    |                                      |                  |                 |                 |                           |                |                |                |                     |                     |                     |                   |                             |         |                       |                     |                               |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 430                                  | -                | 0.70            | 55              | -                         | 1.07           | -              | -              | 3.9                 | 0.315               | -                   | -                 | -                           | 8.60    | -                     | 11.1                | 3.4                           |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 470                                  | -                | 0.85            | 46              | -                         | 0.39           | -              | -              | 3.6                 | 0.026               | -                   | -                 | -                           | 8.90    | -                     | 8.9                 | 4.4                           |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 250                                  | -                | 0.51            | 40              | -                         | 0.15           | -              | -              | 2.3                 | 0.056               | -                   | -                 | -                           | 7.70    | -                     | 8.3                 | 1.3                           |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 370                                  | -                | 0.44            | 43              | -                         | <0.02          | -              | -              | 3.5                 | 0.152               | -                   | -                 | -                           | 7.80    | -                     | 8.2                 | 1.2                           |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 320                                  | -                | 0.44            | 42              | -                         | 0.59           | -              | -              | 3.1                 | 0.062               | -                   | -                 | -                           | 7.50    | -                     | 8.2                 | 1.1                           |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 410                                  | -                | 0.57            | 49              | -                         | 0.98           | -              | -              | 4.3                 | 0.112               | -                   | -                 | -                           | 8.10    | -                     | 9.3                 | 1.0                           |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 440                                  | -                | 0.47            | 54              | -                         | 0.27           | -              | -              | 5.1                 | 0.020               | -                   | -                 | -                           | 8.20    | -                     | 9.9                 | 2.0                           |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 370                                  | -                | 0.40            | 37              | -                         | 0.37           | -              | -              | 4.2                 | 0.020               | -                   | -                 | -                           | 8.10    | -                     | 6.5                 | 1.3                           |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                                    | 0.0285           | -               | -               | -                         | -              | -              | 0.0055         | -                   | -                   | -                   | < 0.0002          | -                           | -       | -                     | -                   | -                             |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                                    | 0.0088           | -               | -               | -                         | -              | -              | 0.0006         | -                   | -                   | -                   | < 0.0002          | -                           | -       | -                     | -                   | -                             |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | 788                                  | 0.0151           | 1.2             | 83              | < 10                      | 0.08           | 11.6           | < 0.0001       | 4.8                 | 0.040               | 0.232               | < 0.0002          | < 0.020                     | 8.23    | 0.07                  | 7.5                 | 6.4                           |

D - Dissolved  
T - Total  
mg/L - milligrams per liter  
µs/cm - microsiemens per centimeter  
su - standard units

Table 18.1-18 (Continued)

| Sample ID   | Selenium, D (mg/L) | Selenium, T (mg/L) | Settleable solids (mL/L) | Silver, D (mg/L) | Sodium, D (mg/L) | Sulfate (mg/L) | Total dissolved solids (mg/L) | Total suspended solids (mg/L) | Vanadium, D (mg/L) | Zinc, D (mg/L) |
|---|--------------------|--------------------|--------------------------|------------------|------------------|----------------|-------------------------------|-------------------------------|--------------------|----------------|
| Ponds within Pinabete watershed                                   |                    |                    |                          |                  |                  |                |                               |                               |                    |                |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | -                  | < 0.001            | -                        | -                | -                | -              | -                             | -                             | 0.0032             | < 0.001        |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | -                  | 0.001              | -                        | -                | -                | -              | -                             | -                             | 0.0077             | 0.008          |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | < 0.01             | -                  | 5.2                      | < 0.0005         | 90.0             | 122            | 415                           | 727                           | -                  | 0.02           |
| 4N/4S Pond (aka Mid Pinabete Pond or Pond East of Lower Pinabete) | -                  | < 0.001            | -                        | -                | -                | -              | -                             | -                             | 0.0038             | 0.010          |
| Stevenson's Well Site Pond (aka Well Site Pond)                   | < 0.01             | -                  | 37.9                     | < 0.0005         | 86.4             | 39             | 380                           | 9200                          | -                  | 0.02           |
| Stevenson's Well Site Pond (aka Well Site Pond)                   | -                  | 0.002              | -                        | -                | -                | -              | -                             | -                             | 0.0064             | 0.006          |
| Ponds within No Name watershed                                    |                    |                    |                          |                  |                  |                |                               |                               |                    |                |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.005            | < 0.1                    | -                | 59.3             | 52             | 340                           | 140                           | -                  | -              |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.005            | 0.1                      | -                | 72.4             | 52             | 310                           | 123                           | 0.0048             | 0.037          |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.005            | < 0.1                    | -                | 25.8             | 25             | 140                           | 51                            | 0.007              | < 0.003        |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.005            | < 0.1                    | -                | 30.2             | 33             | 270                           | 183                           | -                  | -              |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.005            | < 0.1                    | -                | 26.2             | 30             | 260                           | -                             | -                  | -              |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.005            | < 0.1                    | -                | 27.7             | 29             | 290                           | 32                            | -                  | -              |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.005            | < 0.1                    | -                | 39.1             | 40             | 270                           | 22                            | -                  | -              |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.005            | < 0.2                    | -                | 33.6             | < 5            | 220                           | 19                            | -                  | -              |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.001            | -                        | -                | -                | -              | -                             | -                             | 0.0048             | 0.037          |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | -                  | < 0.001            | -                        | -                | -                | -              | -                             | -                             | 0.0070             | 0.003          |
| No Name Impoundment (aka Mid No Name or Pond Along No Name)       | < 0.001            | < 0.001            | < 0.5                    | < 0.00005        | 133              | 190            | 710                           | 162                           | 0.0024             | 0.002          |

D - Dissolved  
T - Total  
mg/L - milligrams per liter  
µs/cm - microsiemens per centimeter  
su - standard units



Pinabete Permit Application Package

Table 18.2-1. Water Supply Wells in Study Area

| Site Name                           | Type | Owner                                   | Completion               | Construction   | Status      | Primary Use                    | Water Quality Data                      | Depth to Water | Total Depth (ft) |
|-------------------------------------|------|---|--------------------------|--|-------------|--------------------------------|---|----------------|------------------|
| 45 (#34)                            | Well | Navajo                                  | Pinabete/ Chaco Alluvium | NA   |             | Unknown                        | see Myers and Villaneuva (1986) well 45 | 8              | 8                |
| #46                                 | Well | Navajo                                  | Alluvium                 | Dug Well   |             | Unknown                        | see BAI #46                             | 7.3            | 9                |
| #90                                 | Well | Navajo                                  | PCS                      | NA   |             | Stock, Domestic                | NA                                      |                | 131              |
| 13-15-4 (#60)                       | Well | Unknown                                 | Chaco Alluvium           | Concrete collar; wooden lid, bucket operated                                 | Unpermitted | Unknown                        | NA                                      | 8              | 11               |
| 13-7-2                              | Well | Unknown                                 | PCS                      | 7" steel casing w/ windmill on 8'x8' concrete pad                            | Abandoned   | Unknown                        | NA                                      |                | 198.8            |
| 13-7-4                              | Well | Navajo Trust                            | Unknown                  | Hand dug w/ hand pump  | Permitted   | Unknown                        | NA                                      |                | Unknown          |
| 13-AW (13T-513, #58)                | Well | Unknown                                 | Alluvium - Artesian      | NA   | Unpermitted | OG well converted to Livestock | see BAI #58                             | 11             | 530              |
| GM-22 (13R-38)                      | Well | Unknown                                 | Pinabete Alluvium        | Dug well w/concrete pad & windmill   | Permitted   | Monitoring/ Livestock          | NA                                      | 11             | 47               |
| GM-32 (13-15-7)                     | Well | Unknown. Likely the same well as W-0202 | Chaco Alluvium           | Block & Concrete dug well, formerly hand pump operated; 10'x10' concrete pad | Unpermitted | Monitoring/ Livestock          | NA                                      | 8              | 9                |
| GM-35                               | Well | Unknown                                 | Unknown                  | Dug well w/concrete pad operated by portable hand pump                       | Unpermitted | Unknown                        | NA                                      |                | 8.7              |
| GM-36 (13-7-5)                      | Well | Unknown                                 | Unknown                  | Dug well w concrete well head; bucket operated                               | Unpermitted | Livestock & Monitoring         | NA                                      |                | 10.4             |
| W-0148                              | Well | Navajo Trust                            | Unknown                  | NA   |             | Stock Water                    | NA                                      |                | Unknown          |
| W-0202                              | Well | Navajo Trust                            | Chaco Alluvium           | NA   |             | Stock Water                    | NA                                      |                | 7                |
| W-0203 (13-15-5)                    | Well | Navajo Trust                            | Chaco Alluvium           | NA   | Unpermitted | Stock Water                    | NA                                      |                | 8                |
| W-0204 (13-15-6)                    | Well | Navajo Trust                            | Chaco Alluvium           | Dug well; 8'x8' concrete pad; sides eroding into well                        | Unpermitted | Stock Water                    | NA                                      |                | 14               |
| W-0314                              | Well | Navajo Trust                            | Unknown                  | NA   |             | Stock Water                    | NA                                      |                | Unknown          |
| W-0342                              | Well | Navajo Trust                            | Unknown                  | NA   |             | Stock Water                    | NA                                      |                | Unknown          |
| W-0343 (13-5-1, Stevenson, 13-15-2) | Well | Navajo Trust                            | Alluvium                 | 5" steel casing; well cap welded shut  | Permitted   | Stock Water                    | NA                                      |                | Unknown          |
| W-0344 (#93)                        | Well | Navajo Trust                            | Pinabete Alluvium        | NA   |             | Stock Water                    | see BAI #93                             | 7              | 9                |
| W-0345 (13R-48, 13-15-3)            | Well | Navajo Trust                            | Pinabete Alluvium        | Dug well; concrete well head; wooden cover                                   | Permitted   | Stock Water                    | NA                                      | 7              | 10               |

Table 18.2-1-1

Pinabete Permit Application Package

Table 18.2-1. (Continued)

| Site Name                               | Type | Owner        | Completion             | Construction   | Status      | Primary Use              | Water Quality Data                      | Depth to Water | Total Depth (ft) |
|---|------|--------------|------------------------|--|-------------|--------------------------|---|----------------|------------------|
| W-0346 (13R-37, 13-8-4)                 | Well | Navajo Trust | Pinabete Alluvium      | Dug well w/ concrete pad over well; hand pump operable | Unpermitted | Stock Water, Use Unknown | NA                                      | 6              | 8                |
| W-0348 (13-8-1)                         | Well | Navajo Trust | Pinabete Alluvium      | Open well; concrete well head                          | Unpermitted | Stock Water              | NA                                      | 9              | 13               |
| W-0519 (13R-31 #17, G4, 13-14-7)        | Well | Navajo Trust | Chaco Alluvium         | NA   | Unpermitted | Stock Water              | see Thorn (1993) well G4                | 16             | 16               |
| W-520                                   | Well | Unknown      | Unknown                | NA   |             | Stock Water              | NA                                      |                | Unknown          |
| W-0537                                  | Well | Navajo Trust | Unknown                |  |             | Stock Water              | NA                                      |                | Unknown          |
| W-0540                                  | Well | Navajo Trust | Unknown                |  |             | Stock Water              | NA                                      |                | Unknown          |
| W-0545                                  | Well | Navajo Trust | Unknown                |  |             | Stock Water              | NA                                      |                | Unknown          |
| G-3 (#36)                               | Well | Unknown      | Unknown                | NA   |             | Stock Water              | see Thorn (1993) well G3                |                | Unknown          |
| W-0606 (13-15-1)                        | Well | Navajo Trust | Unknown but likely PCS | 5" steel casing w/ 8' x 8' concrete pad; Windmill      | Unpermitted | Stock Water              | NA                                      |                | Unknown          |
| W-0607                                  | Well | Unknown      | Alluvial               | Windmill   |             | Stock Water              | NA                                      | 18             | 25               |
| W-0618 (46,13R-28, #35)                 | Well | Navajo Trust | Cottonwood Alluvium    | NA   |             | Stock Water              | see Myers and Villaneuva (1986) well 46 | 5              | 16               |
| W-0624                                  | Well | Navajo Trust | Unknown                |  |             | Stock Water              | NA                                      |                | Unknown          |
| W-0644 (13R-28A, QACW-2B, CWAP-1, #126) | Well | Navajo Trust | Cottonwood Alluvium    | Hand dug w/ hand pump                                  |             | Stock Water              | see BAI #126                            | Unknown        | 11               |
| W-0645 (13R-29, #61, 13-14-6)           | Well | Navajo Trust | Chaco Alluvium         | NA   | Permitted   | Stock Water              | see BAI #61                             | 12             | 16               |
| W-0686                                  | Well | Navajo Trust | Unknown                | Windmill   |             | Stock Water              | NA                                      |                | Unknown          |
| W-0691 (13-15-8)                        | Well | Navajo Trust | Chaco Alluvium         | Dug well, 5'x5' concrete pad; equipped w/hand pump     | Unpermitted | Stock Water              | NA                                      |                | Unknown          |

PCS - Pictured Cliffs Sandstone

# - BAI - Numbering System from Historic Addendum 12-D-A prepared by Billings and Associates, Inc. 1985

Source of Navajo Trust information - New Mexico Office of the State Engineer. 2010. Notice of Navajo Nation Expedited Inter Se Proceeding. Hydrographic Survey, Appendix M. Acquired from the Internet August 17, 2011 from

<http://www.ose.state.nm.us/water-info/NavajoSettlement/Notice2010/AppendixM.pdf>

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Table 18.2-2 Water Levels in Pinabete Alluvial Monitoring Wells

| Well Name                          | PA-1             |                    | PA-2             |                    |
|------------------------------------|------------------|--------------------|------------------|--------------------|
| Measuring point elevation (ft msl) | 5352.9           |                    | 5431.43          |                    |
| Date                               | Water level (ft) | Elevation (ft msl) | Water level (ft) | Elevation (ft msl) |
| 3/26/1998                          | -                | -                  | 7.61             | 5423.82            |
| 3/29/1998                          | 11.35            | 5341.55            | 7.69             | 5423.74            |
| 4/30/1998                          | 11.42            | 5341.48            | -                | -                  |
| 5/12/1998                          | 11.46            | 5341.44            | 7.94             | 5423.49            |
| 6/11/1998                          | 11.63            | 5341.27            | 8.16             | 5423.27            |
| 7/21/1998                          | 12.04            | 5340.86            | 8.38             | 5423.05            |
| 8/20/1998                          | 11.87            | 5341.03            | 8.24             | 5423.19            |
| 9/30/1998                          | 11.7             | 5341.20            | 8.09             | 5423.34            |
| 11/8/1998                          | 11.4             | 5341.50            | 7.88             | 5423.55            |
| 12/17/1998                         | 11.18            | 5341.72            | 7.63             | 5423.8             |
| 8/22/2007                          | 11.85            | 5341.05            | 8.78             | 5422.65            |
| 9/4/2007                           | 11.95            | 5340.95            | 8.76             | 5422.67            |
| 10/4/2007                          | 12.1             | 5340.80            | NA               | -                  |
| 11/5/2007                          | 12.14            | 5340.76            | -                | -                  |
| 11/15/2007                         | -                | -                  | 8.76             | 5422.67            |
| 12/3/2007                          | 12.09            | 5340.81            | -                | -                  |
| 12/5/2007                          | -                | -                  | 8.7              | 5422.73            |
| 1/17/2008                          | 12.0             | 5340.90            | 8.6              | 5422.83            |
| 2/19/2008                          | -                | -                  | 8.6              | 5422.83            |
| 2/21/2008                          | 11.7             | 5341.20            | -                | -                  |
| 3/20/2008                          | 11.6             | 5341.30            | 8.3              | 5423.18            |
| 4/24/2008                          | 11.5             | 5341.40            | 5.5              | 5425.93            |
| 5/27/2008                          | 11.0             | 5341.90            | 5.0              | 5426.43            |
| 6/24/2008                          | 12.0             | 5340.90            | 8.2              | 5423.23            |
| 7/24/2008                          | 12.2             | 5340.70            | 9.0              | 5422.43            |
| 8/19/2008                          | -                | -                  | 9.2              | 5422.23            |
| 8/20/2008                          | 11.2             | 5341.70            | -                | -                  |
| 9/30/2008                          | 11.0             | 5341.90            | 9.0              | 5422.4             |

ft msl - feet above mean sea level

(-) no measurement taken

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Table 18.2-3 Water Levels in Cottonwood Alluvial Monitoring Wells

| Well Name                          | QACW-1           |                    | QACW-2           |                    | QACW-2B          |                    | GM-17            |                    |
|------------------------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|
| Measuring point elevation (ft msl) | 5300.79          |                    | 5201.64          |                    | 5245             |                    | -                |                    |
| Date                               | Water level (ft) | Elevation (ft msl) | Water level (ft) | Elevation (ft msl) | Water level (ft) | Elevation (ft msl) | Water level (ft) | Elevation (ft msl) |
| 11/16/1974                         | -                | -                  | 9.90             | -                  | -                | -                  | -                | -                  |
| 6/27/1975                          | -                | -                  | 10.70            | -                  | -                | -                  | -                | -                  |
| 8/6/1975                           | -                | -                  | 9.80             | -                  | -                | -                  | -                | -                  |
| 10/14/1975                         | -                | -                  | -                | -                  | -                | -                  | 12.91            | -                  |
| 5/18/1976                          | -                | -                  | -                | -                  | -                | -                  | 12.81            | -                  |
| 9/24/1980                          | -                | -                  | -                | -                  | -                | -                  | 10.88            | -                  |
| 9/17/1981                          | -                | -                  | -                | -                  | -                | -                  | 15.65            | -                  |
| 12/15/1981                         | -                | -                  | -                | -                  | -                | -                  | 16.10            | -                  |
| 6/25/1982                          | -                | -                  | -                | -                  | -                | -                  | 18.15            | -                  |
| 9/29/1982                          | -                | -                  | -                | -                  | -                | -                  | 17.30            | -                  |
| 9/16/1985                          | -                | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 12/16/1985                         | no reading       | -                  | -                | -                  | -                | -                  | -                | -                  |
| 3/7/1986                           | 19.11            | -                  | -                | -                  | -                | -                  | -                | -                  |
| 3/18/1986                          | -                | -                  | 13.80            | -                  | -                | -                  | -                | -                  |
| 6/18/1986                          | no water         | -                  | no water         | -                  | 9.10             | -                  | -                | -                  |
| 9/15/1986                          | 20.90            | -                  | -                | -                  | -                | -                  | -                | -                  |
| 12/9/1986                          | 20.50            | -                  | 13.60            | -                  | 8.90             | -                  | -                | -                  |
| 3/30/1987                          | Dry              | -                  | Dry              | -                  | 8.11             | -                  | -                | -                  |
| 6/17/1987                          | Dry              | -                  | -                | -                  | -                | -                  | -                | -                  |
| 6/18/1987                          | -                | -                  | Dry              | -                  | 9.20             | -                  | -                | -                  |
| 9/15/1987                          | -                | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 9/16/1987                          | 21.90            | -                  | -                | -                  | 9.58             | 5235.42            | -                | -                  |
| 3/24/1988                          | -                | -                  | 13.83            | 5187.81            | -                | -                  | -                | -                  |
| 6/30/1988                          | Dry              | -                  | 14.42            | 5187.22            | 9.25             | 5235.75            | -                | -                  |
| 9/21/1988                          | Dry              | -                  | -                | -                  | -                | -                  | -                | -                  |
| 9/22/1988                          | -                | -                  | 14.00            | 5187.64            | -                | -                  | -                | -                  |
| 12/22/1988                         | Dry              | -                  | 14.25            | 5187.39            | 9.25             | 5235.75            | -                | -                  |
| 3/22/1989                          | Dry              | -                  | -                | -                  | -                | -                  | -                | -                  |
| 3/23/1989                          | -                | -                  | 14.25            | 5187.39            | 9.17             | 5235.83            | -                | -                  |
| 6/27/1989                          | Dry              | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 12/19/1989                         | Dry              | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 4/18/1990                          | Dry              | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 6/20/1990                          | Dry              | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 6/21/1990                          | -                | -                  | -                | -                  | 9.33             | 5235.67            | -                | -                  |
| 9/19/1990                          | -                | -                  | -                | -                  | 9.08             | 5235.92            | -                | -                  |
| 9/21/1990                          | 21.25            | 5279.54            | 14.25            | 5187.39            | -                | -                  | -                | -                  |
| 12/12/1990                         | 21.25            | 5279.54            | 14.42            | 5187.22            | 8.50             | 5236.5             | -                | -                  |
| 12/13/1990                         | -                | -                  | -                | -                  | 8.50             | 5236.5             | -                | -                  |
| 3/14/1991                          | 21.25            | 5279.54            | 14.42            | 5187.22            | 8.42             | 5236.58            | -                | -                  |
| 3/31/1991                          | -                | -                  | -                | -                  | 8.42             | 5236.58            | -                | -                  |
| 6/11/1991                          | -                | -                  | -                | -                  | 8.75             | 5236.25            | -                | -                  |
| 6/12/1991                          | 21.33            | 5279.46            | 14.08            | 5187.56            | 8.75             | 5236.25            | -                | -                  |
| 9/12/1991                          | 21.33            | 5279.39            | 9.25             | 5192.34            | 9.25             | 5235.75            | -                | -                  |
| 12/9/1991                          | 21.42            | 5279.29            | 19.50            | 5182.14            | -                | -                  | -                | -                  |
| 12/11/1991                         | -                | -                  | -                | -                  | 8.92             | 5236.08            | -                | -                  |
| 3/10/1992                          | 21.42            | 5279.37            | 14.42            | 5187.22            | -                | -                  | -                | -                  |
| 3/11/1992                          | -                | -                  | -                | -                  | 8.58             | 5236.42            | -                | -                  |
| 6/9/1992                           | 21.50            | 5279.29            | 19.50            | 5187.06            | 8.83             | 5236.17            | -                | -                  |
| 9/21/1992                          | 21.71            | 5279.08            | 21.71            | 5179.93            | 14.46            | 5230.54            | -                | -                  |
| 9/22/1992                          | -                | -                  | -                | -                  | 8.79             | 5236.21            | -                | -                  |
| 12/16/1992                         | 21.50            | -                  | 14.63            | -                  | -                | -                  | -                | -                  |
| 3/10/1993                          | 21.54            | -                  | 14.58            | -                  | -                | -                  | -                | -                  |
| 6/8/1993                           | 21.42            | -                  | 17.58            | -                  | -                | -                  | -                | -                  |
| 9/8/1993                           | 21.33            | 5279.39            | 15.00            | 5180.24            | 15.00            | 5230               | -                | -                  |
| 12/13/1993                         | 21.25            | -                  | 15.00            | -                  | -                | -                  | -                | -                  |
| 6/14/1994                          | 21.25            | -                  | 15.00            | -                  | -                | -                  | -                | -                  |
| 9/7/1994                           | 21.25            | 5279.49            | 15.00            | 5180.34            | 15.00            | 5230               | -                | -                  |
| 12/13/1994                         | 21.25            | -                  | 15.00            | -                  | -                | -                  | -                | -                  |
| 3/28/1995                          | 20.33            | -                  | 14.79            | -                  | -                | -                  | -                | -                  |
| 6/6/1995                           | 20.42            | 5280.28            | 15.00            | -                  | 9.15             | 5235.85            | -                | -                  |
| 9/26/1995                          | 21.40            | 5279.39            | 15.00            | 5186.64            | 9.83             | 5235.17            | -                | -                  |
| 12/12/1995                         | Dry              | 5280.79            | Dry              | Dry                | -                | -                  | -                | -                  |
| 12/13/1995                         | -                | -                  | -                | -                  | 9.72             | 5235.28            | -                | -                  |
| 3/12/1996                          | Dry              | Dry                | Dry              | Dry                | 9.70             | 5235.3             | -                | -                  |
| 6/25/1996                          | Dry              | Dry                | Dry              | Dry                | 10.01            | 5234.99            | -                | -                  |
| 9/30/1996                          | Dry              | Dry                | Dry              | Dry                | 10.05            | 5234.95            | -                | -                  |

Table 18.2-3 (Continued)

| Well Name                          | QACW-1           |                    | QACW-2           |                    | QACW-2B          |                    | GM-17            |                    |
|------------------------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|
| Measuring point elevation (ft msl) | 5300.79          |                    | 5201.64          |                    | 5245             |                    | -                |                    |
| Date                               | Water level (ft) | Elevation (ft msl) | Water level (ft) | Elevation (ft msl) | Water level (ft) | Elevation (ft msl) | Water level (ft) | Elevation (ft msl) |
| 12/17/1996                         | Dry              | Dry                | Dry              | Dry                | 9.50             | 5235.5             | -                | -                  |
| 3/27/1997                          | Dry              | Dry                | Dry              | Dry                | 9.29             | 5235.71            | -                | -                  |
| 6/27/1997                          | Dry              | Dry                | Dry              | Dry                | 9.61             | 5235.39            | -                | -                  |
| 9/19/1997                          | Dry              | Dry                | Dry              | Dry                | 9.75             | 5235.25            | -                | -                  |
| 12/11/1997                         | Dry              | Dry                | dry              | dry                | 9.60             | 5235.4             | -                | -                  |
| 3/5/1998                           | -                | -                  | Dry              | Dry                | 8.36             | 5236.64            | -                | -                  |
| 6/23/1998                          | 20.80            | 5279.99            | 17.10            | 5184.54            | 10.08            | 5234.92            | -                | -                  |
| 9/9/1998                           | dry              | Dry                | 17.10            | 5184.54            | 10.01            | 5234.99            | -                | -                  |
| 12/8/1998                          | dry              | dry                | Dry              | dry                | 9.45             | 5235.55            | -                | -                  |
| 12/21/2005                         | -                | -                  | dry              | -                  | -                | -                  | -                | -                  |
| 9/27/2007                          | -                | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 12/19/2007                         | -                | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 3/26/2008                          | -                | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 6/30/2008                          | -                | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 9/23/2008                          | -                | -                  | Dry              | -                  | -                | -                  | -                | -                  |
| 12/17/2008                         | -                | -                  | Dry              | -                  | -                | -                  | -                | -                  |

ft msl - feet above mean sea level  
 (-) no measurement taken

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Table 18.2-4 Alluvial Monitoring Well Summary and Aquifer Test Results

| Well    | Location (ft) |           | ID (in)  | Elevation (ft) | Well depth (ft) | Test type                | Transmissivity (ft <sup>2</sup> /day) | Hydraulic conductivity |          | Saturated thickness |
|---------|---------------|-----------|----------|----------------|-----------------|--------------------------|---------------------------------------|------------------------|----------|---------------------|
|         | Northing      | Easting   |          |                |                 |                          |                                       | (ft/day)               | (cm/sec) |                     |
| GM-17   | 2013500       | 309800    | 4        | NA             | 20.3            | NA                       | NA                                    | NA                     | NA       | NA                  |
| QACW-2  | 2009420.7     | 287032.58 | NA       | 5201.64        | NA              | NA                       | NA                                    | NA                     | NA       | NA                  |
| QACW-1  | 2010700       | 304050    | 2        | 5300.79        | 21.45           | NA                       | NA                                    | NA                     | NA       | NA                  |
| QACW-2B | 2008000       | 295200    | dug well | 5245           | 11              | NA                       | NA                                    | NA                     | NA       | NA                  |
| PA-1    | 1990260.3     | 300409.2  | 2.1      | 5351.2         | 15.2            | 2.0 gpm<br>pumping test  | 230.7                                 | 51.3                   | 1.8E-02  | 4.5                 |
| PA-2    | 1980956.9     | 306702.8  | 2.1      | 5429.6         | 9.6             | 0.75 gpm<br>pumping test | 53.6                                  | 10.7                   | 3.8E-03  | 5                   |
| NNA-1   | 1976857.2     | 296773.3  | 2.1      | 5430.5         | 24.8            | NA                       | NA                                    | NA                     | NA       | 0 to 11.5           |
| NNA-2   | 1975404.9     | 299547.6  | 2.1      | 5454.7         | 22.1            | NA                       | NA                                    | NA                     | NA       | 0                   |

ft<sup>2</sup>/day - square feet per day  
 cm/sec - centimeter per second  
 NA - information not available  
 ID - inner diameter

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Table 18.2-5. Potentiometric Elevations in Coal Monitoring Wells and Piezometers

| Well/VWP Name | KF-98-02                          | KF-98-03 | KF-98-04 | KF2007-01 | VWP 2007-01<br>(yellow) | VWP 2007-01<br>(green) | VWP 2007-01<br>S6 (white) | VWP 2007-02<br>(yellow) | VWP 2007-02<br>(white) | VWP 2007-02<br>(blue) | VWP 2007-02<br>(green) | VWP 2007-03<br>(yellow) | VWP 2007-03<br>(red) | VWP 2007-05<br>S2 (blue) |
|---------------|-----------------------------------|----------|----------|-----------|-------------------------|------------------------|---------------------------|-------------------------|------------------------|-----------------------|------------------------|-------------------------|----------------------|--------------------------|
| Coal Unit     | S3                                | S3       | S3       | S8        | S2a/S2b                 | S3                     | S6                        | S2                      | S3                     | S7                    | S8                     | S3                      | S2                   | S2                       |
| Date          | Potentiometric Elevation (ft msl) |          |          |           |                         |                        |                           |                         |                        |                       |                        |                         |                      |                          |
| 4/30/1998     | 5325.75                           | 5294.77  | 5289.62  | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 5/12/1998     | 5331.00                           | 5294.95  | 5289.59  | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 6/11/1998     | 5340.83                           | 5292.87  | 5289.03  | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 7/21/1998     | 5349.56                           | 5293.74  | 5289.07  | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 11/8/1998     |                                   | 5293.78  | 5288.83  | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 12/17/1998    | 5315.64                           | 5292.75  | 5288.85  | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 8/22/2007     | -                                 | 5292.21  | -        | 5392.33   | 5275.44                 | 5278.48                | 5331.54                   | 5292.06                 | 5288.98                | 5372.05               | 5394.32                | 5366.22                 | 5360.25              | -                        |
| 9/4/2007      | 5352.12                           | 5292.37  | -        | 5392.60   | 5273.72                 | 5278.78                | 5331.85                   | 5291.73                 | 5288.58                | 5371.69               | 5394.47                | 5367.05                 | 5357.72              | -                        |
| 10/4/2007     | 5354.47                           | -        | 5288.48  | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 10/9/2007     | -                                 | -        | -        | 5392.81   | 5273.44                 | 5278.79                | 5330.39                   | 5291.30                 | 5287.63                | 5371.25               | 5393.71                | 5367.63                 | 5357.26              | -                        |
| 11/5/2007     | 5356.16                           | -        | -        | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | 5367.88                 | 5357.23              | 5410.91                  |
| 11/15/2007    | -                                 | -        | -        | 5392.86   | 5273.37                 | 5278.69                | 5329.97                   | 5290.94                 | 5288.21                | 5370.93               | 5393.77                | -                       | -                    | -                        |
| 12/3/2007     | -                                 | -        | -        | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | 5367.74                 | 5357.60              | -                        |
| 12/5/2007     | 5323.44                           | 5291.94  | -        | 5392.01   | -                       | 5278.56                | 5329.88                   | 5291.09                 | 5287.85                | 5370.81               | 5393.67                | -                       | -                    | 5410.61                  |
| 1/17/2008     | 5329.14                           | 5292.73  | -        | 5393.06   | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 1/31/2008     | -                                 | -        | -        | -         | 5273.42                 | 5278.79                | 5329.84                   | 5291.91                 | 5288.15                | 5370.74               | 5393.81                | 5368.04                 | 5357.83              | 5410.71                  |
| 2/19/2008     | 5332.94                           | 5291.73  | -        | 5393.36   | 5273.05                 | 5278.62                | 5330.05                   | 5289.57                 | 5287.20                | 5370.63               | 5393.56                | 5368.70                 | 5357.74              | -                        |
| 3/20/2008     | 5328.04                           | 5292.13  | -        | 5392.96   | 5273.15                 | 5278.39                | 5330.09                   | 5289.18                 | 5286.96                | 5370.63               | 5393.71                | 5366.44                 | 5385.30              | -                        |
| 4/24/2008     | 5331.34                           | 5292.83  | -        | 5393.26   | 5273.23                 | 5278.30                | 5330.11                   | 5289.12                 | 5286.86                | 5370.60               | 5393.67                | 5366.52                 | 5385.50              | 5410.22                  |
| 5/27/2008     | -                                 | -        | -        | 5393.06   | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |
| 5/28/2008     | 5332.54                           | -        | -        | -         | 5273.42                 | 5286.86                | 5330.11                   | 5289.70                 | 5286.86                | 5370.54               | 5390.11                | 5365.97                 | 5385.40              | 5410.27                  |
| 6/24/2008     | 5299.04                           | 5291.73  | -        | 5393.06   | 5273.47                 | 5278.62                | 5330.15                   | 5287.02                 | 5287.02                | 5370.59               | 5390.11                | 5365.97                 | 5385.40              | 5410.33                  |
| 7/24/2008     | 5303.84                           | 5293.43  | -        | 5365.96   | 5273.30                 | 5278.76                | 5330.17                   | 5289.63                 | 5286.89                | 5370.51               | 5390.05                | 5366.05                 | 5385.50              | 5410.33                  |
| 8/19/2008     | 5305.84                           | -        | -        | 5392.96   | 5273.42                 | 5278.56                | 5330.17                   | 5286.99                 | 5287.51                | 5370.45               | 5393.48                | 5366.19                 | 5358.26              | 5410.33                  |
| 8/20/2008     | -                                 | 5293.03  | -        | -         | -                       | -                      | -                         | -                       | -                      | -                     | -                      | -                       | -                    | -                        |

Table 18.2-5-1

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Table 18.2-5. (Continued)

| Well/VWP Name | KF-98-02                          | KF-98-03 | KF-98-04 | KF2007-01 | VWP 2007-01<br>(yellow) | VWP 2007-01<br>(green) | VWP 2007-01<br>S6 (white) | VWP 2007-02<br>(yellow) | VWP 2007-02<br>(white) | VWP 2007-02<br>(blue) | VWP 2007-02<br>(green) | VWP 2007-03<br>(yellow) | VWP 2007-03<br>(red) | VWP 2007-05<br>S2 (blue) |
|---------------|-----------------------------------|----------|----------|-----------|-------------------------|------------------------|---------------------------|-------------------------|------------------------|-----------------------|------------------------|-------------------------|----------------------|--------------------------|
| Coal Unit     | S3                                | S3       | S3       | S8        | S2a/S2b                 | S3                     | S6                        | S2                      | S3                     | S7                    | S8                     | S3                      | S2                   | S2                       |
| Date          | Potentiometric Elevation (ft msl) |          |          |           |                         |                        |                           |                         |                        |                       |                        |                         |                      |                          |
| 9/30/2008     | 5300.24                           | 5292.73  | -        | 5392.76   | 5273.45                 | 5278.53                | 5330.42                   | 5287.63                 | 5287.42                | 5370.51               | 5393.36                | 5366.14                 | 5358.11              | 5410.39                  |

ft msl - feet above mean sea level  
VWP - vibrating wire piezometer  
(-) no measurement taken



Table 18.2-6 Coal Monitoring Well Summary and Aquifer Test Results

| Well       | Location (ft) <sup>1</sup> |            | Coal seam | Elevation (ft) | Well depth (ft) | Test type                       | Transmissivity (ft <sup>2</sup> /day) | Hydraulic conductivity |          | Saturated thickness |
|------------|----------------------------|------------|-----------|----------------|-----------------|---------------------------------|---------------------------------------|------------------------|----------|---------------------|
|            | Northing                   | Easting    |           |                |                 |                                 |                                       | (ft/day)               | (cm/sec) |                     |
| Kf-98-02   | 1974601.45                 | 2526796.60 | #3        | 5505.89        | 216.5           | Displacement Test               | 0.0010                                | 0.0001                 | 4.6E-08  | 7.5                 |
| Kf-98-03   | 1984332.35                 | 2527508.40 | #3        | 5423.45        | 133.9           | Bailed Recovery Test            | 0.010                                 | 0.002                  | 7.1E-07  | 5                   |
| Kf-98-04   | 1990225.42                 | 2523277.83 | #3        | 5351.80        | 64.8            | Bailed Recovery Test            | 0.010                                 | 0.001                  | 3.5E-07  | 10                  |
| Kf84-22D   | 2009478.18                 | 2530679.02 | #3        | 5124.20        | 220             | MCWhorter Recovery              | 0.01                                  | 0.002                  | 7.1E-07  | 5.0                 |
| Kf2007-01  | 1995163.61                 | 2525504.37 | #8        | 5557.2         | 118             | Papadopulos-Cooper Pumping Test | 1.398                                 | 0.056                  | 2.0E-05  | 25                  |
| SJKF84#3   | 2088296.86                 | 2558656.03 | #8        | 4990.18        | 120             | MCWhorter Recovery              | 0.71                                  | 0.04                   | 1.4E-05  | 18.0                |
| SJKF84#4   | 2085218.97                 | 2557197.37 | #8        | 5046.67        | 71              | MCWhorter Recovery              | 1.03                                  | 0.06                   | 2.1E-05  | 18.0                |
| SJKF84#5   | 2084335.75                 | 2554186.41 | #8        | 5092.00        | 180             | MCWhorter Recovery              | 0.07                                  | 0.004                  | 1.4E-06  | 18.0                |
| KF84-20(d) | 2017120.64                 | 304307.65  | #7        | 5213.92        | 190             | MCWhorter Recovery              | 0.01                                  | 0.002                  | 7.1E-07  | 5.0                 |
| Kf84-21C   | 2009797.60                 | 2526457.46 | #7        | 5219.66        | 75              | MCWhorter Recovery              | 0.04                                  | 0.008                  | 2.8E-06  | 5.0                 |
| Kf84-22B   | 2009478.18                 | 2530679.02 | #7        | 5204.10        | 140             | MCWhorter Recovery              | 0.02                                  | 0.003                  | 1.1E-06  | 5.0                 |
| Kf84-22C   | 2009478.18                 | 2530679.02 | #4-6      | 5142.50        | 202             | MCWhorter Recovery              | 0.01                                  | 0.0014                 | 4.9E-07  | 7.0                 |
| Kf84-20A   | 2017903.13                 | 2526824.67 | #2        | 5163.78        | 240             | MCWhorter Recovery              | 0.009                                 | 0.001                  | 3.5E-07  | 10.0                |
| Kf84-22E   | 2009478.18                 | 2530679.02 | #2        | 5107.80        | 237             | MCWhorter Recovery              | 0.01                                  | 0.001                  | 3.5E-07  | 10.0                |

ft<sup>2</sup>/day - square feet per day

cm/sec - centimeter per second

<sup>1</sup> Coordinate system - State Plane New Mexico West, NAD 1983

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Table 18.2-7 Water Depths and Potentiometric Elevations in the Pictured Cliffs Sandstone

| Measuring point elevation (ft msl) | Well or Piezometer Name |                    |                  |                    |                  |                    |                  |                    |                              |                              |                               |                               |
|------------------------------------|-------------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------------------|------------------------------|-------------------------------|-------------------------------|
|                                    | KPC-98-01               |                    | KPC2007-01       |                    | KPC2007-02       |                    | KPC2007-03       |                    | VWP 2007-01 Kpc (blue)       | VWP 2007-02 Kpc (red)        | VWP 2007-04 Kpc               | VWP 2007-05 Kpc (red)         |
|                                    | 5366.46                 |                    | 5355.71          |                    | 5515.06          |                    | 5470.23          |                    |                              |                              |                               |                               |
| Date                               | Water depth (ft)        | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Potentiometric elev (ft msl) | Potentiometric elev (ft msl) | Potentiometric Elev. (ft msl) | Potentiometric Elev. (ft msl) |
| 3/29/1998                          | 91.31*                  | 5275.15            | -                | -                  | -                | -                  | -                | -                  | -                            | -                            | -                             | -                             |
| 4/30/1998                          | 86.62                   | 5279.84            | -                | -                  | -                | -                  | -                | -                  | -                            | -                            | -                             | -                             |
| 5/12/1998                          | 84.84                   | 5281.62            | -                | -                  | -                | -                  | -                | -                  | -                            | -                            | -                             | -                             |
| 6/11/1998                          | 106.37                  | 5260.09            | -                | -                  | -                | -                  | -                | -                  | -                            | -                            | -                             | -                             |
| 7/21/1998                          | 97.27                   | 5269.19            | -                | -                  | -                | -                  | -                | -                  | -                            | -                            | -                             | -                             |
| 11/8/1998                          | 80.30                   | 5286.16            | -                | -                  | -                | -                  | -                | -                  | -                            | -                            | -                             | -                             |
| 12/17/1998                         | 89.81                   | 5276.65            | -                | -                  | -                | -                  | -                | -                  | -                            | -                            | -                             | -                             |
| 8/22/2007                          | -                       | -                  | 93.61            | 5262.10            | 217.55           | 5297.51            | -                | -                  | 5270.44                      | -                            | -                             | -                             |
| 8/23/2007                          | 75.09                   | 5291.37            | -                | -                  | -                | -                  | 128.66           | 5341.57            | -                            | 5298.44                      | -                             | -                             |
| 9/4/2007                           | 79.35                   | 5287.11            | 93.68            | 5262.03            | 169.11           | 5345.95            | 128.03           | 5342.20            | 5268.35                      | 5297.90                      | -                             | -                             |
| 10/4/2007                          | 77.56                   | 5288.90            | 93.65            | 5262.06            | -                | -                  | -                | -                  | -                            | 5297.37                      | -                             | -                             |
| 10/9/2007                          | -                       | -                  | -                | -                  | -                | -                  | -                | -                  | 5267.89                      | -                            | -                             | -                             |
| 11/5/2007                          | 76.51                   | 5289.95            | 93.78            | 5261.93            | 183.30           | 5331.76            | 130.67           | 5339.56            | -                            | -                            | 5393.83                       | 5411.60                       |
| 11/15/2007                         | -                       | -                  | -                | -                  | -                | -                  | -                | -                  | 5268.14                      | -                            | -                             | -                             |
| 12/5/2007                          | 78.15                   | 5288.31            | 93.71            | 5262.00            | 163.16           | 5351.90            | 133.71           | 5336.52            | 5268.26                      | 5296.81                      | 5397.48                       | 5411.26                       |
| 1/31/2008                          | -                       | -                  | -                | -                  | -                | -                  | -                | -                  | 5268.09                      | 5297.32                      | 5393.68                       | 5411.54                       |
| 2/19/2008                          | -                       | -                  | -                | -                  | -                | -                  | -                | -                  | 5268.91                      | -                            | -                             | -                             |
| 2/21/2008                          | -                       | -                  | -                | -                  | -                | -                  | -                | -                  | -                            | 5296.42                      | -                             | -                             |
| 3/20/2008                          | 89.80                   | 5276.66            | 96.80            | 5258.91            | 158.80           | 5356.26            | 128.30           | 5341.93            | 5268.95                      | 5296.48                      | 5401.50                       | 5410.79                       |
| 4/24/2008                          | 85.00                   | 5281.46            | 94.10            | 5261.61            | 156.40           | 5358.66            | 123.50           | 5346.73            | 5268.78                      | 5296.42                      | 5401.82                       | 5410.76                       |
| 5/27/2008                          | 81.50                   | 5284.96            | 98.50            | 5257.21            | 155.90           | 5359.16            | 126.50           | 5343.73            | -                            | -                            | -                             | -                             |
| 5/28/2008                          | -                       | -                  | -                | -                  | -                | -                  | -                | -                  | 5269.01                      | 5296.28                      | 5402.20                       | 5410.82                       |
| 6/24/2008                          | 79.90                   | 5286.56            | 94.10            | 5261.61            | 157.10           | 5357.96            | 127.10           | 5343.13            | 5269.04                      | 5296.48                      | 5402.40                       | 5410.88                       |
| 7/24/2008                          | 79.20                   | 5287.26            | 94.00            | 5261.71            | 156.30           | 5358.76            | 126.70           | 5343.53            | 5268.76                      | 5296.39                      | 5402.86                       | 5410.85                       |

Table 18.2-7-1

Table 18.2-7 (Continued)

| Measuring point elevation (ft msl) | Well or Piezometer Name |                    |                  |                    |                  |                    |                  |                    |                              |                              |                               |                               |
|------------------------------------|-------------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------------------|------------------------------|-------------------------------|-------------------------------|
|                                    | KPC-98-01               |                    | KPC2007-01       |                    | KPC2007-02       |                    | KPC2007-03       |                    | VWP 2007-01 Kpc (blue)       | VWP 2007-02 Kpc (red)        | VWP 2007-04 Kpc               | VWP 2007-05 Kpc (red)         |
|                                    | 5366.46                 |                    | 5355.71          |                    | 5515.06          |                    | 5470.23          |                    |                              |                              |                               |                               |
| Date                               | Water depth (ft)        | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Potentiometric elev (ft msl) | Potentiometric elev (ft msl) | Potentiometric Elev. (ft msl) | Potentiometric Elev. (ft msl) |
| 8/19/2008                          | -                       | -                  | -                | -                  | 157.80           | 5357.26            | -                | -                  | 5268.83                      | 5296.14                      | 5402.95                       | 5410.85                       |
| 8/20/2008                          | 78.40                   | 5288.06            | 94.10            | 5261.61            | -                | -                  | 126.70           | 5343.53            | -                            | -                            | -                             | -                             |
| 9/30/2008                          | 77.70                   | 5288.76            | 94.40            | 5261.31            | 155.20           | 5359.86            | 126.80           | 5343.43            | 5268.66                      | 5296.25                      | 5403.30                       | 5410.94                       |

ft msl - feet above mean sea level  
 \*1 day after well development  
 (-) no measurement taken

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Table 18.2-8 Water Depths in the Pictured Cliffs Sandstone Monitoring Wells from 1970s and 1980s

| Well name                 | GM-19            |                    | GM-20            |                    | GM-21            |                    | GM-28            |                    | GM-29            |                    | GM-30A           |                    |
|---------------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|------------------|--------------------|
|                           | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) | Water depth (ft) | Elevation (ft msl) |
| Measuring point elevation | NA               | 5385.0             | NA               | 5470.0             | NA               | 5610.0             | NA               | 5320.0             | NA               | 5380.0             | NA               | 5520.0             |
| 11/16/1974                | -                | -                  | -                | -                  | -                | -                  | -                | -                  | -                | -                  | 132.6            | 5387.4             |
| 3/27/1975                 | -                | -                  | -                | -                  | -                | -                  | -                | -                  | -                | -                  | 132.7            | 5387.3             |
| 11/19/1975                | -                | -                  | -                | -                  | -                | -                  | -                | -                  | -                | -                  | 132.7            | 5387.3             |
| 12/9/1975                 | -                | -                  | -                | -                  | -                | -                  | -                | -                  | -                | -                  | 133.2            | 5386.8             |
| 9/26/1983                 | -                | -                  | -                | -                  | -                | -                  | 52.7             | 5267.4             | -                | -                  | -                | -                  |
| 9/27/1983                 | 119.6            | 5265.5             | 137.5            | 5332.6             | 1892.0           | 5428.1             | -                | -                  | -                | -                  | 135.0            | 5385.0             |
| 4/17/1984                 | -                | -                  | -                | -                  | -                | -                  | 81.0             | 5239.0             | -                | -                  | -                | -                  |
| 7/7/1989                  | 119.7            | 5265.3             | -                | -                  | -                | -                  | 54.6             | 5265.4             | 74.4             | 5305.6             | -                | -                  |
| 7/26/1989                 | -                | -                  | 137.1            | 5332.9             | 181.7            | 5428.4             | -                | -                  | -                | -                  | 133.2            | 5386.8             |

ft msl - feet above mean sea level

NA - information not available

(-) no measurement taken

Table 18.2-9 Pictured Cliffs Sandstone Monitoring Well Summary and Aquifer Test Results

| Well                      | Location (ft) <sup>1</sup> |         | Elevation (ft) | Well Depth (ft) | Test type            | Transmissivity (ft <sup>2</sup> /day) | Hydraulic conductivity |          | Saturated thickness (ft) | Storage coefficient |
|---------------------------|----------------------------|---------|----------------|-----------------|----------------------|---------------------------------------|------------------------|----------|--------------------------|---------------------|
|                           | Northing                   | Easting |                |                 |                      |                                       | (ft/day)               | (cm/sec) |                          |                     |
| KPC-98-01                 | 1993802                    | 290787  | 5366.46        | 125.7           | 0.4 gpm pumping test | 0.79                                  | 0.020                  | 7.1E-06  | 39                       | NA                  |
| KPC2007-01                | 1995103                    | 302596  | 5355.71        | 208.84          | NA                   | 0.576                                 | 0.0074                 | 2.6E-06  | 78                       | NA                  |
| KPC2007-02                | 1975119                    | 303891  | 5515.06        | 320.98          | NA                   | NA                                    | 0.0001                 | 3.5E-08  | NA                       | NA                  |
| KPC2007-03                | 1982885                    | 295091  | 5470.23        | 138.4           | NA                   | NA                                    | 0.0040                 | 1.4E-06  | NA                       | NA                  |
| Pumping test well T4-1    | 1976250                    | 289850  | 5520           | 228             | 0.15 gpm pumping     | 0.1203                                | 0.0014                 | 4.9E-07  | 84                       | 0.00032             |
| Recovery test well GM-30A | 1975811                    | 290347  | NA             | 191.6           | NA                   | 0.1337                                | 0.0016                 | 5.6E-07  | 84                       | 0.00034             |
| O-1                       |                            |         |                |                 | Cooper slug test     | 2.7300                                | 0.0321                 | 1.1E-05  | 85                       | NA                  |
| (18.3 gpm for 8.7 min)    | 1958366                    | 320663  | 5520           | 414             | Horslev slug test    | 3.7500                                | 0.0441                 | 1.6E-05  | 85                       | NA                  |

<sup>1</sup> Coordinates State Plane New Mexico West NAD 1983

ft<sup>2</sup>/day - square feet per day

cm/sec - centimeter per second

gpm - gallon per minute

NA - information not available or not determined

Table 18.2-10. Relevant Groundwater Quality Use Criteria

| Parameter (units)                   | Livestock Watering Criteria <sup>1</sup> | Domestic Water Supply Criteria for Surface Water by 2007 Navajo Nation Standards | EPA Secondary Drinking Water Standards <sup>2</sup> |
|-------------------------------------|--|--|---|
| Arsenic (mg/L)                      | 0.2                                      | 0.01   |   |
| Barium (mg/L)                       |  | 1  |   |
| Boron (mg/L)                        | 5  | 0.63   |   |
| Cadmium (mg/L)                      | 0.05                                     | 0.005  |   |
| Chloride (mg/L)                     |  |  | 250   |
| Chromium (mg/L)                     | 1  | 0.1  |   |
| Copper (mg/L)                       | 0.5(D)                                   | 1.3  | 1   |
| Fluoride (mg/L)                     | 2*                                       | 4  | 2   |
| Total iron (mg/L)                   | -  |  | 0.3   |
| Lead (mg/L)                         | 0.1                                      | 0.015  |   |
| Total manganese (mg/L)              | -  |  | 0.05  |
| Mercury (mg/L)                      | 0.01                                     | 0.002  |   |
| Nitrate (mg/L-N)                    | 0.132                                    | 10   |   |
| pH (su)                             | 6.5-9.0                                  | 5.0-9.0  | 6.5-8.5   |
| Potassium (mg/L)                    |  |  |   |
| Radium-226 (pCi/L)                  | 30**                                     | 5**  |   |
| Radium-228 (pCi/L)                  | 30**                                     | 5**  |   |
| Selenium (mg/L)                     | 0.05                                     | 0.05   |   |
| Silver (mg/L)                       |  | 0.035  | 0.1   |
| Sulfate (mg/L)                      | 1000*                                    |  | 250   |
| Total dissolved solids (TDS) (mg/L) | 3000*                                    |  | 500   |
| Uranium (mg/L)                      |  | 0.03   |   |
| Zinc (mg/L)                         | 25                                       | 2.1  | 5   |

<sup>1</sup> Based on Navajo Nation Environmental Protection Agency Water Quality Program, 2008, Navajo Nation Surface Water Quality Standards 2007, passed by Navajo Nation Resources Committee on May 13, 2008 and on other criteria for livestock use as noted

<sup>2</sup> <http://water.epa.gov/drink/contaminants/secondarystandards.cfm>

\* Although there are no Navajo Nation livestock watering criteria for TDS, sulfate and fluoride, TDS concentrations above 3,000 may adversely affect growing/young livestock and waters with sulfate concentrations above 1,000 mg/l and fluoride concentrations above 2 mg/l are not recommended for livestock use (Lardy, G., C.

\*\* 30 pCi/L criteria for Ra-226 + Ra-228

mg/L - milligram per liter

µS/cm - microsiemens per centimeter

su - standard units

pCi/L - picocuries per liter

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Table 18.2-11 Baseline Water Quality at Cottonwood Arroyo Alluvial Wells

| Parameter                              |        | Cottonwood Alluvial Well |             |             |
|--|--------|--------------------------|-------------|-------------|
|  |        | QACW-2                   | QACW-2B     | GM-17       |
| Baseline Monitoring Period             |        | 1974 - 1998              | 1986 - 1999 | 1975 - 1982 |
| pH (SU) <sup>1</sup>                   | n      | 9                        | 33          | 7           |
|  | median | 7.9                      | 7.8         | 6.9         |
| TDS -180° (mg/L)                       | n      | 14                       | 32          | 11          |
|  | median | 2,305                    | 3,015       | 15,210      |
| Bicarbonate (as HCO <sub>3</sub> mg/L) | n      | 9                        | 32          | 2           |
|  | median | 310                      | 375.2       | 767         |
| Carbonate (as CaCO <sub>3</sub> mg/L)  | n      | 2                        | 15          | 0           |
|  | median | 24                       | 0.5         | NA          |
| Chloride (mg/L)                        | n      | 14                       | 33          | 11          |
|  | median | 28.2                     | 138         | 113         |
| Sulfate (mg/L)                         | n      | 14                       | 32          | 11          |
|  | median | 1,227                    | 1,605       | 9,308       |
| Calcium (mg/L)                         | n      | 9                        | 33          | 8           |
|  | median | 113                      | 154         | 375         |
| Magnesium (mg/L)                       | n      | 11                       | 33          | 10          |
|  | median | 16.2                     | 22.7        | 145.0       |
| Potassium (mg/L)                       | n      | 5                        | 32          | 6           |
|  | median | 2.0                      | 6.5         | 25.5        |
| Sodium (mg/L)                          | n      | 9                        | 33          | 8           |
|  | median | 451                      | 778         | 4,510       |
| Fluoride (mg/L)                        | n      | 14                       | 33          | 11          |
|  | median | 2.35                     | 1.38        | 0.30        |
| Nitrate as N (mg/L)                    | n      | 7                        | 7           | 11          |
|  | median | 0.18                     | 0.09        | 1.03        |
| Boron (mg/L)                           | n      | 13                       | 32          | 11          |
|  | median | 0.11                     | 0.13        | 0.28        |
| Iron, total (mg/L)                     | n      | 4                        | 16          | 9           |
|  | median | 0.03                     | 1.04        | 0.62        |
| Iron, diss.(mg/L)                      | n      | 14                       | 33          | 11          |
|  | median | 0.18                     | 0.10        | 0.09        |
| Manganese, total (mg/L)                | n      | 3                        | 16          | 8           |
|  | median | 0.02                     | 0.37        | 1.765       |
| Manganese, diss. (mg/L)                | n      | 14                       | 33          | 11          |
|  | median | 0.10                     | 0.11        | 1.02        |
| Selenium. (mg/L)                       | n      | 9                        | 33          | 11          |
|  | median | 0.0030                   | 0.0025      | 0.0004      |

<sup>1</sup>Lab pH included in summary only when no field pH data are available for the well  
QACW-2 includes 1974 through 1979 samples from GM-18

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Table 18.2-12 Water Quality at Pinabete Arroyo Alluvial Well PA-1

| Parameter (units)                            | 3/29/1998     | 5/15/1998 | 8/20/1998 | 11/8/1998 | 6/15/2004 | 11/5/2007 | 2/21/2008 | 5/27/2008 | 8/20/2008 | 11/21/2008 |
|--|---------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|
| Total Alkalinity as CaCO <sub>3</sub> (mg/L) | 300           | 297       | 282       | 301       | 302       | 304       | 314       | 310       | 224       | 344        |
| Arsenic (mg/L)                               | <0.005        | <0.005    | <0.005    | <0.005    | -         | 0.0008    | <0.0005   | 0.0007    | <0.0005   | 0.0008     |
| Barium (mg/L)                                | 0.05          | 0.03      | 0.9       | 0.03      | -         | 0.0161    | 0.0144    | 0.0262    | 0.0164    | 0.0174     |
| Bicarbonate as HCO <sub>3</sub> (mg/L)       | 365           | 362       | 344       | 367       | 368       | 371       | 383       | 378.2     | 273       | 420        |
| Boron (mg/L)                                 | 0.17          | 0.2       | 0.2       | 0.22      | -         | 0.787     | 0.2       | 0.2       | 0.2       | 0.2        |
| Ion balance (%)                              | 6.77          | 0.89      | 3.88      | 2.38      | -         | 5.99      | 1.06      | 1.78      | 0.85      | 1.64       |
| Cadmium (mg/L)                               | <0.001        | <0.001    | <0.001    | <0.001    | -         | <0.00005  | <0.00005  | <0.00005  | <0.00005  | <0.00005   |
| Calcium (mg/L)                               | 85.4          | 68.5      | 103       | 90.6      | 102       | 110       | 116       | 137       | 139       | 101        |
| Carbonate (mg/L)                             | <1            | <1        | <1        | <1        | <10       | <10       | <10       | <10       | <10       | <10        |
| Chloride (mg/L)                              | 25            | 22        | 29        | 16        | 14        | 14        | 17        | 36        | 25        | 18         |
| Chromium (mg/L)                              | 0.03* (total) | <0.01     | <0.01     | <0.01     | -         | 0.005     | 0.004     | 0.004     | <0.001    | <0.001     |
| Electrical conductivity (EC) (uS/cm)         | 2540          | 2410      | 2310      | 2150      | 2480      | 2380      | 2380      | 2680      | 3050      | 2520       |
| Copper (mg/L)                                | <0.01         | <0.01     | <0.01     | <0.01     | -         | 0.0106    | 0.0151    | 0.0101    | 0.0094    | 0.0079     |
| Fluoride (mg/L)                              | 2.49          | 2.36      | 2.39      | 2.53      | -         | 2.2       | 2.2       | 2.1       | 2.2       | 3          |
| Hydroxide (mg/L)                             | <1            | <1        | <1        | <1        | <10       | <10       | <10       | <10       | <10       | <10        |
| Iron (mg/L)                                  | 0.99          | 0.06      | <0.02     | <0.02     | -         | <0.05     | <0.05     | <0.05     | <0.05     | <0.05      |
| Total iron (mg/L)                            | 41.9          | 3.07      | 4.43      | 0.25      | -         | 16.7      | 17.5      | 53.2      | 1.39      | 3.88       |
| Lead (mg/L)                                  | <0.005        | <0.005    | <0.005    | <0.005    | -         | <0.0001   | <0.0001   | 0.0002    | 0.0002    | 0.0003     |
| Magnesium (mg/L)                             | 15.4          | 13.4      | 16.5      | 13.8      | 15.8      | 16.3      | 17.9      | 22.3      | 22.3      | 16.4       |
| Manganese, D (mg/L)                          | 0.138         | 0.005     | 0.017     | <0.01     | -         | 0.118     | 0.057     | 0.488     | 0.218     | 0.087      |
| Manganese, T (mg/L)                          | 1.31          | 0.843     | 0.37      | 0.03      | -         | 0.487     | 0.302     | 3.56      | 0.350     | 0.142      |
| Mercury (mg/L)                               | <0.001        | <0.001    | <0.001    | <0.001    | -         | <0.0002   | <0.0002   | 0.0002    | <0.0002   | <0.0002    |



Table 18.2-12 (Continued)

| Parameter (units)                   | 3/29/1998 | 5/15/1998 | 8/20/1998 | 11/8/1998 | 6/15/2004 | 11/5/2007 | 2/21/2008   | 5/27/2008 | 8/20/2008   | 11/21/2008  |
|-------------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-------------|-----------|-------------|-------------|
| Nitrate (mg/L-N)                    | 0.66      | 0.72      | <0.05     | NM        | -         | 0.05      | 0.03        | 0.04      | 0.10        | 0.05        |
| pH (su)                             | 7.6       | 7.5       | 7.5       | 7.7       | 7.67      | 7.61      | 7.54        | 7.53      | 7.48        | 7.78        |
| Potassium (mg/L)                    | 9.8       | 1.8       | 1.7       | 2.9       | 1.4       | 1.4       | 1.3         | 2.7       | 1.7         | 1.7         |
| Radium-226 (pCi/L)                  | <1.69     | 5.78      | NM        | 0.91      | -         | 2.9 ± 0.9 | 0.42 ± 0.34 | 1.3 ± 0.4 | 0.6 ± 0.42  | 0.10 ± 0.22 |
| Radium-228 (pCi/L)                  | <1.9      | 5.77      | NM        | 11.74     | -         | 1.5 ± 0.7 | 0.60 ± 0.40 | 1.1 ± 0.6 | 0.53 ± 0.49 | 0.48 ± 0.38 |
| Selenium (mg/L)                     | 0.005     | 0.005     | <0.005    | <0.005    | 0.014     | 0.006     | 0.004       | 0.006     | 0.003       | 0.006       |
| Silver (mg/L)                       | <0.01     | <0.01     | <0.01     | <0.01     | -         | <0.00005  | <0.00005    | 0.00006   | <0.00005    | <0.00005    |
| Sodium (mg/L)                       | 375       | 458       | 374       | 377       | 464       | 418       | 457         | 511       | 503         | 445         |
| Sulfate (mg/L)                      | 893       | 833       | 875       | 805       | 920       | 1040      | 1060        | 1140      | 1280        | 980         |
| Total dissolved solids (TDS) (mg/L) | 1610      | 1640      | 1730      | 1500      | 1660      | 1680      | 4310        | 1950      | 2030        | 1750        |
| Uranium (mg/L)                      | -         | -         | -         | -         | -         | 0.01010   | 0.01080     | 0.01350   | 0.01620     | 0.01230     |
| Zinc (mg/L)                         | 0.053     | 0.037     | <0.025    | 0.043     | -         | 0.007     | 0.002       | 0.002     | 0.002       | 0.007       |

(-) s no analysis performed  
 mg/L - milligram per liter  
 µS/cm - microsiemens per centimeter  
 su - standard units  
 pCi/L - picocuries per liter

Table 18.2-13 Water Quality at Pinabete Arroyo Alluvial Well PA-2

| Parameter (units)                            | 3/30/1998     | 5/15/1998 | 8/20/1998 | 11/11/1998 | 6/15/2004 | 11/15/2007 | 2/21/2008 | 5/27/2008 | 8/19/2008 | 11/20/2008 |
|--|---------------|-----------|-----------|------------|-----------|------------|-----------|-----------|-----------|------------|
| Total alkalinity as CaCO <sub>3</sub> (mg/L) | 293           | 281       | 315       | 327        | 286       | 410        | 308       | 328       | 405       | 430        |
| Arsenic (mg/L)                               | <0.005        | <0.005    | <0.005    | <0.005     | -         | 0.0012     | 0.0007    | 0.0018    | 0.0008    | 0.0027     |
| Barium (mg/L)                                | 0.04          | 0.02      | <0.2      | 0.02       | -         | 0.0107     | 0.0129    | 0.0195    | 0.0143    | 0.0119     |
| Bicarbonate as HCO <sub>3</sub> (mg/L)       | 357           | 342       | 384       | 398        | 349       | 451        | 376       | 400       | 494       | 525        |
| Boron (mg/L)                                 | 0.19          | 0.2       | 0.22      | 0.31       | -         | 0.2        | 2.1       | 0.2       | 0.3       | 0.2        |
| Ion balance (%)                              | 4.27          | 2.64      | 1.65      | 3.2        | -         | 16         | 6.5       | 5.57      | 0.61      | 8.18       |
| Cadmium (mg/L)                               | <0.001        | <0.001    | <0.001    | <0.001     | -         | <0.00005   | <0.00005  | <0.00005  | <0.00005  | <0.00005   |
| Calcium (mg/L)                               | 56.8          | 61        | 101       | 95         | 87.5      | 95         | 96.0      | 96.8      | 90.8      | 92.3       |
| Carbonate (mg/L)                             | <1            | <1        | <1        | <1         | <10       | 24         | <10       | <10       | <10       | <10        |
| Chloride (mg/L)                              | 22            | 65        | 51        | 35         | 22        | 38         | 30        | 32        | 42        | 45         |
| Chromium (mg/L)                              | 0.03* (total) | <0.01     | <0.01     | <0.01      | -         | 0.006      | 0.004     | 0.003     | <0.001    | 0.009      |
| Electrical conductivity (EC) (uS/cm)         | 4390          | 4510      | 4530      | 4520       | 4040      | 4600       | 4410      | 4110      | 5010      | 4860       |
| Copper (mg/L)                                | <0.01         | <0.01     | <0.01     | <0.01      | -         | 0.0508     | 0.0116    | 0.0225    | 0.0226    | 0.0220     |
| Fluoride (mg/L)                              | 2.47          | 2.81      | 3.06      | 2.91       | -         | 2.8        | 2.4       | 2.5       | 3.1       | 3.3        |
| Hydroxide (mg/L)                             | <1            | <1        | <1        | <1         | <10       | <10        | <10       | <10       | <10       | <10        |
| Iron (mg/L)                                  | 0.11          | <0.02     | <0.02     | 0.04       | -         | <0.05      | <0.05     | <0.05     | <0.05     | <0.05      |
| Total iron (mg/L)                            | 63.9          | 2.88      | 6.55      | 0.13       | -         | 1.86       | 5.61      | 3.03      | 1.86      | 3.19       |
| Lead (mg/L)                                  | <0.005        | <0.005    | <0.005    | <0.005     | -         | <0.0001    | <0.0001   | 0.0001    | 0.0002    | 0.0001     |
| Magnesium (mg/L)                             | 12            | 11        | 16        | 15         | 13.2      | 0.0277     | 15.5      | 16.7      | 15.5      | 16.7       |
| Manganese (mg/L)                             | 1.33          | 0.456     | 0.22      | 0.11       | -         | 0.0277     | 0.090     | 0.141     | 0.128     | 0.135      |
| Total manganese (mg/L)                       | 3.71          | 0.525     | 0.88      | 0.24       | -         | 0.552      | 1.27      | 0.599     | 0.551     | 0.748      |
| Mercury (mg/L)                               | <0.001        | <0.001    | <0.001    | <0.001     | -         | <0.0002    | <0.0002   | 0.0002    | <0.0002   | <0.0002    |

Table 18.2-13 (Continued)

| Parameter (units)                   | 3/30/1998 | 5/15/1998 | 8/20/1998 | 11/11/1998 | 6/15/2004 | 11/15/2007  | 2/21/2008   | 5/27/2008   | 8/19/2008   | 11/20/2008  |
|-------------------------------------|-----------|-----------|-----------|------------|-----------|-------------|-------------|-------------|-------------|-------------|
| Nitrate (mg/L-N)                    | 0.27      | 0.32      | <0.05     | NM         | -         | 0.06        | 0.08        | 0.08        | 0.11        | 0.05        |
| pH (su)                             | 7.9       | 7.4       | 7.3       | 7.5        | 7.62      | 7.19        | 7.41        | 7.5         | 7.21        | 7.31        |
| Potassium (mg/L)                    | 5         | 2         | 3         | 5.4        | 1.8       | 2.1         | 2.0         | 2.4         | 3.3         | 3.2         |
| Radium-226 (pCi/L)                  | <1.69     | 27.9      | -         | 0.48       | -         | 0.67 ± 0.43 | 0.40 ± 0.39 | 0.45 ± 0.34 | 0.60 ± 0.40 | 2.5 ± 0.7   |
| Radium-228 (pCi/L)                  | <1.9      | 1.74      | -         | 9.02       | -         | 0.62 ± 0.48 | 1.4 ± 0.6   | 0.19 ± 0.56 | 1.2 ± 0.5   | 0.55 ± 0.37 |
| Selenium (mg/L)                     | 0.0007    | 0.006     | <0.005    | <0.005     | 0.012     | 0.012       | 0.009       | 0.014       | 0.010       | 0.018       |
| Silver (mg/L)                       | <0.01     | <0.01     | <0.01     | <0.01      | -         | <0.00005    | <0.00005    | 0.00009     | <0.00005    | <0.00005    |
| Sodium (mg/L)                       | 781       | 981       | 872       | 891        | 839       | 809         | 850         | 907         | 966         | 1000        |
| Sulfate (mg/L)                      | 1670      | 1760      | 1690      | 1940       | 1550      | 2200        | 2100        | 2150        | 1950        | 2400        |
| Total Dissolved Solids (TDS) (mg/L) | 2990      | 3150      | 3600      | 3420       | 2780      | 3500        | 3070        | 3030        | 3540        | 3580        |
| Uranium (mg/L)                      | -         | -         | -         | -          | -         | 0.01230     | 0.01120     | 0.01350     | 0.01160     | 0.01170     |
| Zinc (mg/L)                         | 0.051     | 0.025     | <0.025    | 0.18       | -         | 0.003       | 0.008       | 0.009       | 0.004       | 0.008       |

(-) no analysis performed  
 mg/L - milligram per liter  
 μS/cm - microsiemens per centimeter  
 su - standard units  
 pCi/L - picocuries per liter

*Pinabete Permit Application Package*

Table 18.2-14 Water Quality at No Name Arroyo Alluvial Well NNA-1

| Parameter (units)                    | 8/20/1998 | 11/11/1998 |
|--------------------------------------|-----------|------------|
| Arsenic (mg/L)                       | <0.005    | <0.005     |
| Barium (mg/L)                        | 0.9       | 0.02       |
| Boron (mg/L)                         | 2.4       | 0.84       |
| Cadmium (mg/L)                       | <0.001    | <0.001     |
| Chromium (mg/L)                      | <0.01     | <0.01      |
| Copper (mg/L)                        | <0.01     | <0.01      |
| Iron (mg/L)                          | <0.02     | 0.04       |
| Lead (mg/L)                          | <0.005    | <0.005     |
| Manganese (mg/L)                     | 0.084     | 0.45       |
| Mercury (mg/L)                       | <0.001    | <0.001     |
| Selenium (mg/L)                      | 0.008     | 0.043      |
| Silver (mg/L)                        | <0.01     | <0.01      |
| Zinc (mg/L)                          | <0.025    | 0.21       |
| Total Iron (mg/L)                    | 1.56      | 0.17       |
| Total manganese (mg/L)               | 0.13      | 0.66       |
| pH (su)                              | 7.6       | 7.6        |
| Electrical conductivity (EC) (uS/cm) | 13100     | 20700      |
| Total dissolved solids (TDS) (mg/L)  | 12600     | 13400      |
| Fluoride (mg/L)                      | 1.93      | 0.97       |
| Bicarbonate (HCO <sub>3</sub> mg/L)  | 639       | 719        |
| Carbonate (CO <sub>3</sub> mg/L)     | <1        | <1         |
| Chloride (mg/L)                      | 180       | 127        |
| Sulfate (mg/L)                       | 7150      | 10100      |
| Calcium (mg/L)                       | 333       | 293        |
| Magnesium (mg/L)                     | 249       | 205        |
| Potassium (mg/L)                     | 15        | 28.3       |
| Sodium (mg/L)                        | 2640      | 3220       |
| Hydroxide (mg/L)                     | <1        | NA         |
| Total Alkalinity (mg/L)              | 524       | 589        |
| Nitrate (mg/L-N)                     | 5.26      | NA         |
| Ion balance (%)                      | 3.9       | 13.45      |
| Radium-226 (pCi/L)                   | NA        | 1.37       |
| Radium-228 (pCi/L)                   | NA        | 2.81       |

\*secondary standard

\*\* Ra-226 + Ra-228

Table 18.2-15 Water Quality at No. 3 Coal Seam Well KF-98-02

(Samples collected on 3/29/1998 and on 11/8/1998 eliminated due to pH&gt;11)

| Parameter (units)                    | 8/23/2007    | 11/5/2007   | 2/19/2008   | 5/28/2008   | 8/19/2008   | 11/20/2008  |
|--------------------------------------|--------------|-------------|-------------|-------------|-------------|-------------|
| Total alkalinity (mg/L)              | 1530         | 1040        | 1320        | 1390        | 1620        | 1580        |
| Arsenic (mg/L)                       | 0.0055       | 0.0057      | 0.0058      | 0.0045      | 0.0028      | 0.0051      |
| Barium (mg/L)                        | 0.1399       | 0.0925      | 0.1230      | 0.175       | 0.3380      | 0.1420      |
| Bicarbonate (HCO <sub>3</sub> mg/L)  | 1037         | 1269        | 1464        | 1696        | 1928        | 1560        |
| Boron (mg/L)                         | 0.3          | 1.47        | 0.4         | 0.3         | 0.4         | 0.5         |
| Ion balance (%)                      | 3.04         | 8.77        | 0.51        | 1.21        | 4.89        | 2.63        |
| Cadmium (mg/L)                       | <0.00005     | <0.00005    | <0.00005    | <0.00005    | <0.00005    | <0.00005    |
| Calcium (mg/L)                       | 1.6          | 16.2        | 5.5         | 9.1         | 6.7         | 4.6         |
| Carbonate (CO <sub>3</sub> mg/L)     | 408          | <10         | 72          | <10         | 24          | 12          |
| Chloride (mg/L)                      | 930          | 650         | 920         | 950         | 1210        | 1280        |
| Chromium (mg/L)                      | 0.029        | 0.02        | 0.033       | 0.017       | 0.002       | 0.069       |
| Electrical conductivity (EC) (uS/cm) | 5510         | 3790        | 4910        | 5440        | 7050        | 7090        |
| Copper (mg/L)                        | 0.0192       | 0.0124      | 0.0222      | 0.053       | 0.0305      | 0.0263      |
| Fluoride (mg/L)                      | 1.8          | 1.4         | 1.7         | 0.2         | 1.8         | 1.6         |
| Hydroxide (mg/L)                     | <10          | <10         | <10         | <10         | <10         | <10         |
| Iron (mg/L)                          | <0.05        | <0.05       | <0.05       | 0.05        | 0.08        | 0.07        |
| Total iron (mg/L)                    | 0.14         | 0.891       | 0.53        | 0.52        | 0.42        | 1.01        |
| Lead (mg/L)                          | 0.0003       | 0.0003      | 0.0003      | 0.0002      | 0.0005      | 0.0001      |
| Magnesium (mg/L)                     | 0.6          | <0.5        | 0.8         | 1.0         | 2.7         | 2.4         |
| Total manganese (mg/L)               | 0.007        | 0.016       | 0.020       | 0.019       | 0.039       | 0.017       |
| Manganese (mg/L)                     | <0.005       | <0.005      | 0.025       | 0.011       | 0.044       | 0.045       |
| Mercury (mg/L) <sup>1</sup>          | <0.0002      | <0.0002     | <0.0002     | 0.0003      | <0.0002     | <0.0002     |
| Nitrate (mg/L-N)                     | <0.02        | 0.06        | <0.02       | 0.03        | 0.03        | 0.02        |
| pH (su)                              | 9.55         | 7.53        | 8.11        | 7.89        | 7.79        | 8.01        |
| Potassium (mg/L)                     | 12.1         | 8.5         | 11.5        | 12.1        | 13.3        | 13.0        |
| Radium-226 (pCi/L)                   | 0.13 ± 0.28  | 0.31 ± 0.32 | 0.77 ± 0.58 | 0.82 ± 0.72 | 0.50 ± 0.36 | 0.18 ± 0.28 |
| Radium-228 (pCi/L)                   | -0.02 ± 0.46 | 0.34 ± 0.50 | 0.64 ± 0.70 | 0.74 ± 0.75 | 0.83 ± 0.49 | 0.51 ± 0.43 |
| Selenium (mg/L) <sup>2</sup>         | 0.008        | 0.008       | 0.008       | 0.006       | 0.005       | 0.009       |
| Silver (mg/L)                        | <0.00005     | <0.00005    | <0.00005    | 0.00033     | <0.00005    | 0.00016     |
| Sodium (mg/L)                        | 1250         | 786         | 1170        | 1170        | 1310        | 1510        |
| Sulfate (mg/L)                       | 64           | 136         | 118         | 96          | 120         | 36          |
| Total dissolved solids (TDS) (mg/L)  | 3180         | 2220        | 3050        | 3080        | 4040        | 4100        |
| Uranium (mg/L)                       | -            | 0.00424     | 0.00595     | 0.00546     | 0.00532     | 0.00540     |
| Zinc (mg/L)                          | <0.001       | 0.006       | 0.001       | <0.001      | 0.008       | 0.010       |

Table 18.2-15 (Continued)

(Samples collected on 3/29/1998 and on 11/8/1998 eliminated due to pH>11)

| Parameter (units) | 8/23/2007 | 11/5/2007 | 2/19/2008 | 5/28/2008 | 8/19/2008 | 11/20/2008 |
|-------------------|-----------|-----------|-----------|-----------|-----------|------------|
|-------------------|-----------|-----------|-----------|-----------|-----------|------------|

\*secondary standard

\*\* Ra-226 + Ra-228

(-) no analysis performed

mg/L - milligram per liter

µS/cm - microsiemens per centimeter

su - standard units

pCi/L - picocuries per liter

Pinabete Permit Application Package

Table 18.2-16. Baseline Water Quality in the Fruitland Coals at Navajo Mine

| Well             | Well Depth (feet) | Baseline Monitoring Period | pH (SU) |        | TDS -180° (mg/L) |        | Bicarbonate as HCO <sub>3</sub> (mg/L) |        | Carbonate as CO <sub>3</sub> (mg/L) |        | Chloride (mg/L) |        | Sulfate (mg/L) |        | Calcium (mg/L) |        | Magnesium (mg/L) |        | Potassium (mg/L) |        |
|------------------|-------------------|----------------------------|---------|--------|------------------|--------|--|--------|-------------------------------------|--------|-----------------|--------|----------------|--------|----------------|--------|------------------|--------|------------------|--------|
|                  |                   |                            | n       | median | n                | median | n                                      | median | n                                   | median | n               | median | n              | median | n              | median | n                | median | n                | median |
| KF84-21a (No 2)  | 118               | 1984-2001                  | 30      | 7.9    | 30               | 8375   | 30                                     | 1197   | 17                                  | <1     | 30              | 4445   | 30             | 63     | 30             | 13.3   | 30               | 14.9   | 30               | 13.3   |
| KF84-21c (No 7)  | 75                | 1984                       | 1       | 8.08   | 1                | 8505   | 1                                      | 919    | 1                                   | 68.4   | 1               | 3980   | 1              | 184    | 1              | 14.6   | 1                | 14.9   | 1                | 15.0   |
| KF84-22a (No 8)  | 125               | 1984-2001                  | 22      | 8.0    | 22               | 4650   | 22                                     | 1170   | 12                                  | <1     | 22              | 290    | 22             | 2140   | 22             | 15.3   | 22               | 3.5    | 22               | 6.8    |
| KF84-22b (No 7)  | 140               | 1984-2001                  | 26      | 7.4    | 26               | 6115   | 25                                     | 854    | 15                                  | <1     | 25              | 3220   | 26             | <10    | 26             | 45.0   | 26               | 13.4   | 26               | 11.9   |
| KF84-22d (No 3)  | 220               | 1984                       | 1       | 7.94   | 1                | 8610   | 1                                      | 830    | 1                                   | 46.8   | 1               | 3420   | 1              | <10    | 1              | 27.4   | 1                | 18.7   | 1                | 15.8   |
| KF84-22e (No 2)  | 237               | 1984                       | 2       | 7.98   | 2                | 8155   | 2                                      | 814    | 2                                   | 52.8   | 2               | 4185   | 2              | 24.5   | 2              | 35.6   | 2                | 17.5   | 2                | 16.3   |
| KF84-20A (No 3)  | 190               | 1984-2001                  | 26      | 7.93   | 26               | 7260   | 26                                     | 1090   | 23                                  | <1     | 26              | 3715   | 26             | <10    | 26             | 18.4   | 26               | 11.0   | 26               | 11.9   |
| KF84-20C (No 7)  | 240               | 1984-2001                  | 23      | 7.9    | 23               | 2770   | 23                                     | 1562   | 21                                  | <1     | 23              | 715    | 23             | 7      | 23             | 9.6    | 23               | 2.8    | 23               | 5.9    |
| KF84-18b (No 8)  | 133               | 1984-2001                  | 25      | 7.1    | 25               | 9300   | 25                                     | 1030   | 13                                  | <1     | 25              | 4900   | 25             | <10    | 25             | 114.0  | 27               | 24.3   | 25               | 15.0   |
| KF84-18a (No. 6) | 181               | 1984-2001                  | 26      | 7.47   | 26               | 13400  | 26                                     | 450    | 14                                  | <1     | 26              | 7900   | 26             | 5.5    | 26             | 157.0  | 26               | 50.6   | 26               | 22.5   |

| Well             | Well Depth (feet) | Baseline Monitoring Period | Sodium (mg/L) |        | Fluoride (mg/L) |        | Nitrate as N (mg/L) |        | Boron (mg/L) |        | Iron, total (mg/L) |        | Iron, diss. (mg/L) |        | Manganese, total (mg/L) |        | Manganese, diss. (mg/L) |        | Selenium, diss. (mg/L) |        |
|------------------|-------------------|----------------------------|---------------|--------|-----------------|--------|---------------------|--------|--------------|--------|--------------------|--------|--------------------|--------|-------------------------|--------|-------------------------|--------|------------------------|--------|
|                  |                   |                            | n             | median | n               | median | n                   | median | n            | median | n                  | median | n                  | median | n                       | median | n                       | median | n                      | median |
| KF84-21a (No 2)  | 118               | 1984-2001                  | 30            | 3080   | 30              | 1.56   | 5                   | 0.1    | 30           | 0.61   | 21                 | 0.100  | 30                 | 0.100  | 21                      | 0.020  | 30                      | 0.0255 | 29                     | <0.005 |
| KF84-21c (No 7)  | 75                | 1984                       | 1             | 2858   | 1               | 1.79   | 1                   | 394    | 1            | 0.63   | 1                  | -      | 1                  | 0.015  | 1                       | -      | 1                       | 0.3800 | 1                      | <0.001 |
| KF84-22a (No 8)  | 125               | 1984-2001                  | 22            | 1600   | 22              | 2.19   | 3                   | 0.53   | 22           | 0.27   | 19                 | 0.420  | 22                 | 0.080  | 19                      | 0.020  | 22                      | 0.0143 | 22                     | <0.005 |
| KF84-22b (No 7)  | 140               | 1984-2001                  | 26            | 2210   | 25              | 0.89   | 1                   | 0.08   | 25           | 0.39   | 23                 | 1.130  | 26                 | 0.195  | 23                      | 0.300  | 26                      | 0.300  | 26                     | <0.005 |
| KF84-22d (No 3)  | 220               | 1984                       | 1             | 2866   | 1               | 1.28   | 1                   | -      | 1            | 0.5    | 1                  | -      | 1                  | 0.006  | 1                       | -      | 1                       | 0.016  | 1                      | <0.001 |
| KF84-22e (No 2)  | 237               | 1984                       | 2             | 2803   | 2               | 1.23   | 2                   | -      | 2            | 0.51   | 2                  | -      | 2                  | 0.005  | 2                       | -      | 2                       | 0.140  | 2                      | <0.001 |
| KF84-20A (No 3)  | 190               | 1984-2001                  | 26            | 2690   | 26              | 1.39   | 2                   | 0.115  | 26           | 0.55   | 17                 | 2.730  | 26                 | 0.235  | 17                      | 0.180  | 26                      | 0.100  | 26                     | <0.005 |
| KF84-20C (No 7)  | 240               | 1984-2001                  | 23            | 1040   | 23              | 1.74   | 2                   | 0.18   | 21           | 0.42   | 16                 | 0.640  | 23                 | 0.180  | 16                      | 0.075  | 23                      | 0.082  | 23                     | <0.005 |
| KF84-18b (No 8)  | 133               | 1984-2001                  | 25            | 3380   | 25              | 0.44   | 3                   | 0.1    | 25           | 0.73   | 17                 | 11.900 | 25                 | <0.5   | 16                      | 0.380  | 25                      | 0.380  | 25                     | <0.005 |
| KF84-18a (No. 6) | 181               | 1984-2001                  | 26            | 4640   | 26              | 0.66   | 2                   | 0.1    | 26           | 0.72   | 17                 | 3.80   | 26                 | 0.25   | 17                      | 1.33   | 26                      | 1.32   | 19                     | <0.005 |

Median calculation based on all but rejected sample results including field splits and non detected results

Rejected samples include: samples with no sampling or analysis date, samples with pH>11, samples that are clearly inconsistent with results of other damples

For less than detection limit, 1/2 the detection limit used for summary unless the median is a detection limit that is lower than any detected result

uncaracterized metals results included as dissolved metals in statistical summray

Pinabete Permit Application Package

Table 18.2-17 Water Quality at No. 8 Coal Seam Well KF2007-01

| Parameter (units)                    | 8/16/2007 | 11/15/2007 | 5/27/2008 | 8/19/2008 | 11/20/2008 |
|--------------------------------------|-----------|------------|-----------|-----------|------------|
| Total alkalinity (mg/L)              | 1800      | 1670       | 1478      | 1646      | 1670       |
| Arsenic (mg/L)                       | 0.0014    | 0.003      | 0.002     | 0.0017    | 0.0028     |
| Barium (mg/L)                        | 0.0297    | 0.0351     | 0.0344    | 0.0280    | 0.0293     |
| Bicarbonate (HCO <sub>3</sub> mg/L)  | 2098      | 1074       | 1190      | 1490      | 1550       |
| Boron (mg/L)                         | 0.2       | 0.329      | 0.3       | 0.4       | 0.4        |
| Ion balance (%)                      | 7.1       | 4.6        | 8.19      | 6.21      | 1.92       |
| Cadmium (mg/L)                       | <0.00005  | <0.00005   | <0.00005  | <0.00005  | <0.00005   |
| Calcium (mg/L)                       | 4.2       | 2.2        | 2.7       | 3.9       | 3.2        |
| Carbonate (CO <sub>3</sub> mg/L)     | 29        | 284        | 288       | 156       | 120        |
| Chloride (mg/L)                      | 278       | 364        | 362       | 338       | 320        |
| Chromium (mg/L)                      | 0.012     | 0.032      | 0.024     | 0.003     | 0.067      |
| Electrical conductivity (EC) (uS/cm) | 8240      | 7380       | 6330      | 5560      | 5170       |
| Copper (mg/L)                        | 0.0362    | 0.1180     | 0.0737    | 0.0349    | 0.0232     |
| Fluoride (mg/L)                      | 3.1       | 2.6        | 2.6       | 2.7       | 3.3        |
| Hydroxide (mg/L)                     | <10.      | <10        | <10       | <10       | <10        |
| Iron (mg/L)                          | <0.05     | <0.05      | <0.05     | <0.05     | <0.05      |
| Total iron (mg/L)                    | <0.05     | 0.0847     | 0.33      | 1.20      | 0.29       |
| Lead (mg/L)                          | <0.0001   | 0.0003     | <0.0001   | 0.0004    | 0.0322     |
| Magnesium (mg/L)                     | 1.6       | 1.4        | 1.6       | 1.8       | 1.5        |



Pinabete Permit Application Package

Table 18.2-17 (Continued)

| Parameter (units)                   | 8/16/2007   | 11/15/2007  | 5/27/2008   | 8/19/2008   | 11/20/2008  |
|-------------------------------------|-------------|-------------|-------------|-------------|-------------|
| Manganese (mg/L)                    | 0.008       | <0.005      | 0.007       | 0.013       | 0.008       |
| Total manganese (mg/L)              | 0.011       | 0.0168      | 0.023       | 0.052       | 0.017       |
| Mercury (mg/L)                      | <0.0002     | <0.0002     | 0.0004      | <0.0002     | <0.0002     |
| Nitrate (mg/L-N)                    | <0.02       | <0.02       | 0.29        | 0.43        | 0.25        |
| pH (su)                             | 8.12        | 9.56        | 9.09        | 8.64        | 8.75        |
| Potassium (mg/L)                    | 9           | 46.9        | 28.9        | 17.9        | 16.4        |
| Radium-226 (pCi/L)                  | 0.11 ± 0.27 | 0.51 ± 0.35 | 0.33 ± 0.42 | 0.50 ± 0.39 | 0.30 ± 0.30 |
| Radium-228 (pCi/L)                  | 0.32 ± 0.48 | 0.89 ± 0.46 | 0.58 ± 0.50 | 0.76 ± 0.53 | 0.55 ± 0.35 |
| Selenium (mg/L)                     | 0.006       | 0.004       | 0.005       | 0.004       | 0.005       |
| Silver (mg/L)                       | <0.00005    | <0.00005    | 0.00006     | 0.00007     | <0.00005    |
| Sodium (mg/L)                       | 995         | 1780        | 1430        | 1160        | 1180        |
| Sulfate (mg/L)                      | 315         | 2050        | 1380        | 740         | 620         |
| Total dissolved solids (TDS) (mg/L) | 2750        | 5160        | 4130        | 3460        | 3250        |
| Uranium (mg/L)                      | 0.00060     | 0.00059     | 0.00044     | 0.00058     | 0.00037     |
| Zinc (mg/L)                         | 0.002       | 0.003       | 0.002       | 0.014       | 0.010       |

\*secondary standard

\*\* Ra-226 + Ra-228

mg/L - milligram per liter

µS/cm - microsiemens per centimeter

su - standard units

pCi/L - picocuries per liter

Pinabete Permit Application Package

Table 18.2-18 Water Quality at Pictured Cliffs Sandstone Monitoring Well KPC-98-01

| Parameter (units)                            | 3/29/1998      | 11/8/1998 | 8/23/2007 | 11/5/2007 | 2/21/2008 | 5/27/2008 | 8/20/2008 | 11/21/2008 |
|--|----------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|
| Total Alkalinity as CaCO <sub>3</sub> (mg/L) | 131            | 581       | 750       | 930       | 900       | 870       | 740       | 850        |
| Arsenic (mg/L)                               | <0.005         | <0.005    | 0.0042    | 0.00193   | 0.0019    | 0.002     | 0.0017    | 0.0035     |
| Barium (mg/L)                                | 0.02           | 0.02      | 0.0138    | 0.0101    | 0.0123    | 0.0236    | 0.0132    | 0.0126     |
| Bicarbonate as HCO <sub>3</sub> (mg/L)       | 132            | 709       | 891       | 1135      | 1098      | 1061      | 903       | 1037       |
| Boron (mg/L)                                 | 0.12           | 0.61      | 0.6       | 1.11      | 0.7       | 0.7       | 0.6       | 0.7        |
| Ion balance (%)                              | 2.13           | 3.71      | 4.6       | 8.3       | 2.17      | 0.49      | 6.89      | 1.61       |
| Cadmium (mg/L)                               | <0.001         | <0.001    | <0.00005  | <0.00005  | <0.00005  | <0.00005  | <0.00005  | <0.00005   |
| Calcium (mg/L)                               | 26.5           | 33.1      | 28        | 25.2      | 26.8      | 30.8      | 28.4      | 28.6       |
| Carbonate as CO <sub>3</sub> (mg/L)          | 14             | <1        | 12        | <10       | <10       | <10       | <10       | <10        |
| Chloride (mg/L)                              | 39             | 177       | 310       | 212       | 234       | 244       | 220       | 236        |
| Chromium (mg/L)                              | <0.01* (total) | <0.01     | 0.018     | 0.124     | 0.012     | 0.004     | 0.001     | 0.021      |
| Electrical conductivity (EC) (uS/cm)         | 1380           | 6550      | 5510      | 8250      | 8250      | 8250      | 8730      | 8700       |
| Copper (mg/L)                                | <0.01          | <0.01     | 0.0396    | 0.026     | 0.0571    | 0.43      | 0.0468    | 0.0807     |
| Fluoride (mg/L)                              | 2.29           | 1.13      | 1.3       | 1.4       | 1.4       | 1.3       | 1.5       | 1.5        |
| Hydroxide (mg/L)                             | -              | -         | <10       | <10       | <10       | <10       | <10       | <10        |
| Iron (mg/L)                                  | 0.46           | 1.51      | 0.68      | <0.05     | <0.05     | <0.05     | <0.05     | <0.05      |
| Total iron (mg/L)                            | 2.51           | 1.74      | 0.68      | 29.5      | 7.60      | 2.71      | 0.16      | 0.51       |
| Lead (mg/L)                                  | <0.005         | 0.005     | 0.0001    | <0.0001   | 0.0003    | 0.0003    | 0.0002    | 0.0001     |
| Magnesium (mg/L)                             | 2.7            | 5.7       | 8.2       | 6.8       | 7.7       | 8         | 7.4       | 7.7        |
| Manganese (mg/L)                             | 0.013          | 0.08      | 0.063     | 0.0673    | 0.058     | 0.051     | 0.037     | 0.039      |
| Total manganese (mg/L)                       | 0.038          | 0.1       | 0.073     | 0.111     | 0.183     | 0.082     | 0.044     | 0.045      |

Pinabete Permit Application Package

Table 18.2-18 (Continued)

| Parameter (units)                   | 3/29/1998 | 11/8/1998 | 8/23/2007   | 11/5/2007 | 2/21/2008 | 5/27/2008 | 8/20/2008   | 11/21/2008  |
|-------------------------------------|-----------|-----------|-------------|-----------|-----------|-----------|-------------|-------------|
| Mercury (mg/L)                      | <0.001    | <0.001    | <0.0002     | <0.0002   | <0.0002   | <0.0002   | <0.0002     | <0.0002     |
| Nitrate (mg/L-N)                    | 1.54      | -         | <0.02       | 2.29      | 1.94      | 4.46      | 2.68        | 1.92        |
| pH (su)                             | 9.1       | 8         | 7.78        | 7.76      | 7.70      | 7.79      | 7.73        | 7.87        |
| Potassium (mg/L)                    | 8.2       | 17.3      | 9.2         | 7.1       | 8.6       | 10        | 8.5         | 8.1         |
| Radium-226 (pCi/L)                  | <1.69     | 3.92      | 0.92 ± 0.49 | 1.0 ± 0.5 | 1.2 ± 0.5 | 1.5 ± 0.5 | 0.76 ± 0.44 | 0.61 ± 0.36 |
| Radium-228 (pCi/L)                  | <1.9      | 5.42      | 1.2 ± 0.5   | 1.6 ± 0.6 | 1.1 ± 0.4 | 1.2 ± 0.5 | 1.2 ± 0.5   | 1.3 ± 0.4   |
| Selenium (mg/L)                     | <0.005    | <0.005    | 0.005       | 0.00346   | 0.006     | 0.005     | 0.005       | 0.011       |
| Silver (mg/L)                       | <0.01     | <0.01     | <0.00005    | 0.00006   | <0.00005  | 0.00007   | <0.00005    | <0.00005    |
| Sodium (mg/L)                       | 202       | 1490      | 2150        | 1790      | 1930      | 2270      | 1690        | 1980        |
| Sulfate (mg/L)                      | 350       | 2680      | 3900        | 3350      | 3300      | 3800      | 3300        | 3400        |
| Total dissolved solids (TDS) (mg/L) | 800       | 4830      | 6640        | 6060      | 6050      | 5900      | 5820        | 6360        |
| Uranium (mg/L)                      | -         | -         | 0.01901     | 0.01230   | 0.01220   | 0.00952   | 0.01000     | 0.01010     |
| Zinc (mg/L)                         | 0.093     | 0.365     | 0.002       | 0.201     | 0.018     | 0.022     | 0.019       | 0.027       |

(-) analysis not performed for parameter

mg/L - milligram per liter

µS/cm - microsiemens per centimeter

su - standard units

Table 18.2-19 Water Quality at Pictured Cliffs Sandstone Monitoring Well KPC2007-01

| Parameter (units)                    | 8/16/2007   | 11/15/2007  | 2/19/2008   | 5/28/2008   | 8/20/2008   | 11/20/2008  |
|--------------------------------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Total alkalinity (mg/L)              | 1480        | 1870        | 1900        | 1280        | 1600        | 1440        |
| Arsenic (mg/L)                       | 0.006       | 0.0058      | 0.0052      | 0.0234      | 0.0025      | 0.0051      |
| Barium (mg/L)                        | 0.0342      | 0.0096      | 0.0214      | 0.0341      | 0.0191      | 0.0173      |
| Bicarbonate (HCO <sub>3</sub> mg/L)  | 1732        | 866         | 415         | 1488        | 756         | 1293        |
| Boron (mg/L)                         | 0.3         | 0.429       | 0.5         | 0.6         | 0.4         | 0.5         |
| Ion balance (%)                      | 9           | 10.4        | 11.1        | 6.13        | 17.9        | 7.82        |
| Cadmium (mg/L)                       | <0.00005    | <0.00005    | <0.00005    | <0.00005    | <0.00005    | <0.00005    |
| Calcium (mg/L)                       | 13.4        | 3.6         | 2.4         | 18.6        | 3           | 11.6        |
| Carbonate (mg/L)                     | 60          | 1160        | 1560        | 60          | 980         | 380         |
| Chloride (mg/L)                      | 320         | 304         | 292         | 374         | 365         | 580         |
| Chromium (mg/L)                      | 0.005       | 0.025       | 0.040       | 0.008       | 0.002       | 0.063       |
| Electrical conductivity (EC) (uS/cm) | 8240        | 8260        | 8070        | 7950        | 8560        | 9250        |
| Copper (mg/L)                        | 0.0934      | 0.104       | 0.0785      | 0.2470      | 0.0369      | 0.0412      |
| Fluoride (mg/L)                      | 1.7         | 1.5         | 1.5         | 1.8         | 1.6         | 1.6         |
| Hydroxide (mg/L)                     | <10         | <10         | <10         | <10         | <10         | <10         |
| Iron (mg/L)                          | <0.05       | <0.05       | <0.05       | 0.13        | <0.05       | <0.05       |
| Total iron (mg/L)                    | 1.11        | 0.0892      | 0.93        | 533         | 0.17        | 1.57        |
| Lead (mg/L)                          | <0.0001     | <0.0001     | <0.0001     | 0.0004      | 0.0002      | 0.0002      |
| Magnesium(mg/L)                      | 7.3         | 0.0056      | 4.2         | 9.4         | 4.4         | 7.1         |
| Manganese (mg/L)                     | 0.034       | 0.0244      | <0.005      | 0.022       | <0.005      | 0.0785      |
| Total manganese (mg/L)               | 0.055       | 0.024       | 0.022       | 9.73        | 0.006       | 0.137       |
| Mercury (mg/L)                       | <0.0002     | <0.0002     | <0.0002     | 0.001       | <0.0002     | <0.0002     |
| Nitrate (mg/L-N)                     | <0.02       | <0.02       | 0.03        | 0.05        | 0.65        | 0.07        |
| pH (su)                              | 8.19        | 9.82        | 10.3        | 8.35        | 9.85        | 9.14        |
| Potassium (mg/L)                     | 18.1        | 76.9        | 73.3        | 14.3        | 35.2        | 16.2        |
| Radium-226 (pCi/L)                   | 0.18 ± 0.28 | 0.61 ± 0.39 | 0.01 ± 0.28 | 2.0 ± 0.7   | 0.33 ± 0.32 | 0.10 ± 0.22 |
| Radium-228 (pCi/L)                   | 0.86 ± 0.57 | 0.19 ± 0.44 | 0.37 ± 0.57 | 0.42 ± 0.45 | 0.50 ± 0.47 | 0.37 ± 0.43 |
| Selenium (mg/L)                      | 0.008       | 0.003       | 0.004       | 0.006       | 0.004       | 0.008       |
| Silver (mg/L)                        | <0.00005    | <0.00005    | <0.00005    | <0.00005    | <0.00005    | 0.0001      |
| Sodium (mg/L)                        | 1720        | 2020        | 1920        | 1840        | 1600        | 2020        |
| Sulfate (mg/L)                       | 2750        | 2500        | 2000        | 2900        | 2350        | 2800        |
| Total dissolved solids (TDS) (mg/L)  | 5820        | 5820        | 5650        | 6790        | 5640        | 6280        |
| Uranium (mg/L)                       | 0.00187     | 0.00149     | 0.00065     | 0.00472     | 0.00080     | 0.00089     |

Table 18.2-19 (Continued)

| Parameter (units) | 8/16/2007 | 11/15/2007 | 2/19/2008 | 5/28/2008 | 8/20/2008 | 11/20/2008 |
|-------------------|-----------|------------|-----------|-----------|-----------|------------|
| Zinc (mg/L)       | 0.006     | 0.004      | 0.001     | 0.012     | 0.003     | 0.008      |

\*secondary standard

\*\* Ra-226 + Ra-228

mg/L - milligram per liter

μS/cm - microsiemens per centimeter

su - standard units

pCi/L - picocuries per liter

Table 18.2-20 Water Quality at Pictured Cliffs Sandstone Monitoring Well GM-21

| Parameter (units)                    | 11/16/1974 | 8/4/1976 | 8/22/1977 | 9/10/1979 |
|--------------------------------------|------------|----------|-----------|-----------|
| Arsenic (mg/L)                       | <0.5       | <0.01    | <0.01     | <.0001    |
| Barium (mg/L)                        | -          | <0.1     | <0.5      | 0.05      |
| Boron (mg/L)                         | 0.88       | 0.7      | 1.0       | 1.10      |
| Cadmium (mg/L)                       | 0.081      | <0.001   | <0.01     | <.01      |
| Chromium (mg/L)                      | -          | 0.005    | <0.01     | 0.03      |
| Copper (mg/L)                        | 0.025      | <0.001   | 0.01      | <0.01     |
| Iron (mg/L)                          | 0.2        | 0.198    | <0.05     | 0.04      |
| Lead (mg/L)                          | <0.05      | 0.001    | <0.05     | 0.26      |
| Manganese (mg/L)                     | 0.05       | <0.039   | 0.07      | 0.03      |
| Mercury (mg/L)                       | <0.0005    | <0.0004  | <0.001    | -         |
| Selenium (mg/L)                      | <0.05      | <0.01    | <0.01     | 0.001     |
| Silver (mg/L)                        | -          | <0.001   | <0.05     | <0.1      |
| Zinc (mg/L)                          | 0.447      | 0.045    | 0.06      | 0.62      |
| Total iron (mg/L)                    | -          | -        | -         | 0.41      |
| Total manganese (mg/L)               | -          | -        | -         | 0.11      |
| pH (su)                              | 7.9        | 7.2      | 7.3       | 7         |
| Electrical conductivity (EC) (uS/cm) | -          | -        | -         | -         |
| Total dissolved solids (TDS) (mg/L)  | 6923       | 6624     | 6370      | 6140      |

Table 18.2-20 (Continued)

| Parameter (units)       | 11/16/1974 | 8/4/1976 | 8/22/1977 | 9/10/1979 |
|-------------------------|------------|----------|-----------|-----------|
| Fluoride (mg/L)         | 0.4        | 0.2      | -         | -         |
| Bicarbonate (mg/L)      | 585        | -        | -         | -         |
| Carbonate (mg/L)        | -          | -        | -         | -         |
| Chloride (mg/L)         | 780        | 646      | 150       | 118       |
| Sulfate (mg/L)          | 3600       | 2502     | 2625      | 3740      |
| Calcium (mg/L)          | 423        | 155      | 414       | -         |
| Magnesium (mg/L)        | 65         | 148      | 62        | -         |
| Potassium (mg/L)        | -          | -        | -         | -         |
| Sodium (mg/L)           | 1470       | 920      | 1440      | -         |
| Hydroxide (mg/L)        | -          | -        | -         | -         |
| Total alkalinity (mg/L) | -          | -        | -         | -         |
| Nitrate (mg/L-N)        | -          | -        | 0.4       | -         |
| Ion balance (%)         | 8.2        | -        | -         | -         |
| Radium-226 (pCi/L)      | -          | -        | -         | 0.11      |
| Radium-228 (pCi/L)      | -          | -        | -         | -         |

(-) analysis not performed for parameter

mg/L - milligram per liter

μS/cm - microsiemens per centimeter

su - standard units

pCi/L - picocuries per liter

Pinabete Permit Application Package

Table 18.2-21 Water Quality at Pictured Cliffs Sandstone Monitoring Well GM-20

(Sample collected on 11/16/1974 eliminated due to pH>11)

| Parameter (units)                       | 6/27/1975 | 5/18/1976 | 10/6/1976 | 8/22/1977 | 12/20/1977 | 9/10/1979 |
|---|-----------|-----------|-----------|-----------|------------|-----------|
| Arsenic (mg/L)                          | -         | 0.01      | 0.03      | <0.01     | <0.01      | <0.001    |
| Barium (mg/L)                           | -         | 0.24      | <0.1      | <0.5      | <0.1       | 0.1       |
| Boron (mg/L)                            | -         | 0.88      | 0.2       | 0.9       | 1.2        | 2.24      |
| Cadmium (mg/L)                          | -         | 0.001     | <0.001    | <0.01     | 0.001      | <0.1      |
| Chromium (mg/L)                         | -         | 0.013     | 0.019     | <0.01     | 0.012      | 0.01      |
| Copper (mg/L)                           | -         | 0.016     | 0.006     | 0.01      | 0.008      | 0.03      |
| Iron (mg/L)                             | -         | 0.64      | 0.066     | <0.05     | 0.35       | 0.01      |
| Lead (mg/L)                             | -         | 0.035     | 0.034     | <0.05     | <0.001     | 0.10      |
| Manganese (mg/L)                        | -         | 0.026     | 0.008     | <0.001    | 0.16       | 0.29      |
| Mercury (mg/L)                          | -         | <0.0004   | <0.0004   | <0.001    | <0.0004    | -         |
| Selenium (mg/L) <sup>1</sup>            | -         | <0.01     | <0.01     | <0.01     | <0.01      | 0.001     |
| Silver (mg/L)                           | -         | <0.001    | <0.001    | <0.05     | <0.01      | <.01      |
| Zinc (mg/L)                             | -         | 0.08      | <0.001    | <0.05     | 0.04       | 1.06      |
| Total iron (mg/L)                       | -         | -         | -         | -         | -          | 0.03      |
| Total manganese (mg/L)                  | -         | -         | -         | -         | -          | 0.29      |
| pH (su)                                 | 10.8      | 9.3       | 8.6       | 8.7       | 7.3        | 7         |
| Electrical conductivity (EC)<br>(uS/cm) | 8755      | -         | -         | -         | -          | -         |
| Total dissolved solids (TDS)<br>(mg/L)  | -         | 5711      | 5822      | 5880      | 5050       | 5260      |



Pinabete Permit Application Package

Table 18.2-21 (Continued)

(Sample collected on 11/16/1974 eliminated due to pH>11)

| Parameter (units)                         | 6/27/1975 | 5/18/1976 | 10/6/1976 | 8/22/1977 | 12/20/1977 | 9/10/1979 |
|---|-----------|-----------|-----------|-----------|------------|-----------|
| Fluoride (mg/L)                           | -         | -         | -         | -         | -          | -         |
| Bicarbonate as HCO <sub>3</sub><br>(mg/L) | 290       | 475       | -         | 462       | 269        | -         |
| Carbonate as CO <sub>3</sub> (mg/L)       | 272       | 105       | -         | -         | -          | -         |
| Chloride (mg/L)                           | -         | 2118      | 1280      | 1430      | 757        | 803       |
| Sulfate (mg/L)                            | -         | 1725      | 1830      | 2050      | 2380       | 2250      |
| Calcium (mg/L)                            | -         | 10.6      | 8.5       | 11        | 9.3        | -         |
| Magnesium (mg/L)                          | -         | 4.32      | 4.56      | 7         | 19         | -         |
| Potassium (mg/L)                          | -         | -         | -         | -         | -          | -         |
| Sodium (mg/L)                             | -         | 2000      | 1690      | 2020      | 1600       | -         |
| Hydroxide (mg/L)                          | -         | -         | -         | -         | -          | -         |
| Total alkalinity (mg/L)                   | -         | -         | -         | -         | -          | -         |
| Nitrate (mg/L-N)                          | -         | -         | 0.08      | 0.6       | 0.2        | -         |
| Ion balance (%)                           | -         | 9.8       | -         | 0.9       | 2.5        | -         |

(-) analysis not performed for parameter

mg/L - milligram per liter

μS/cm - microsiemens per centimeter

su - standard units

Pinabete Permit Application Package

Table 18.2-22 Water Quality at Pictured Cliffs Sandstone Monitoring Well GM-19

| Parameter (units)                       | 11/16/1974 | 8/5/1976 | 8/8/1977 | 9/10/1979 |
|---|------------|----------|----------|-----------|
| Arsenic (mg/L)                          | <0.5       | <0.001   | <0.05    | 0.33      |
| Barium (mg/L)                           | -          | <0.1     | <0.5     | 0.08      |
| Boron (mg/L)                            | 1.03       | 0.3      | 1.0      | 0.88      |
| Cadmium (mg/L)                          | 0.016      | <0.001   | <0.01    | <.01      |
| Chromium (mg/L)                         | -          | 0.001    | <0.01    | <.01      |
| Copper (mg/L)                           | 0.015      | 0.001    | 0.02     | 0.02      |
| Iron (mg/L)                             | 0.4        | 0.005    | <0.05    | 0.01      |
| Lead (mg/L)                             | <0.05      | 0.001    | <0.05    | 0.1       |
| Manganese (mg/L)                        | 0.245      | 0.088    | 0.06     | 0.11      |
| Mercury (mg/L)                          | <0.0005    | <0.0004  | <0.001   | -         |
| Selenium (mg/L)                         | <0.05      | <0.01    | <0.01    | 0.002     |
| Silver (mg/L)                           | -          | <0.001   | <0.05    | <.01      |
| Zinc (mg/L)                             | 0.240      | 0.031    | 0.07     | 0.42      |
| Total iron (mg/L)                       | -          | -        | -        | 0.01      |
| Total manganese (mg/L)                  | -          | -        | -        | 0.12      |
| pH (su)                                 | 8.1        | 7.83     | 7.9      | 7.5       |
| Electrical conductivity (EC)<br>(uS/cm) | -          | -        | -        | -         |

Pinabete Permit Application Package

Table 18.2-22 (Continued)

| Parameter (units)                      | 11/16/1974 | 8/5/1976 | 8/8/1977 | 9/10/1979 |
|--|------------|----------|----------|-----------|
| Total dissolved solids (TDS) (mg/L)    | 9172       | 8437     | 7810     | 9270      |
| Fluoride (mg/L)                        | 1.7        | 0.76     | 0.9      | 1.49      |
| Bicarbonate as HCO <sub>3</sub> (mg/L) | 1000       | -        | -        | -         |
| Carbonate as CO <sub>3</sub> (mg/L)    | -          | -        | -        | -         |
| Chloride (mg/L)                        | 1020       | 534.8    | 668      | 1077      |
| Sulfate (mg/L)                         | 4050       | 3685     | 4000     | 4535      |
| Calcium (mg/L)                         | 43         | 13.2     | 200      | -         |
| Magnesium (mg/L)                       | 19         | 3.83     | 38       | -         |
| Potassium (mg/L)                       | -          | -        | -        | -         |
| Sodium (mg/L)                          | 3040       | 1610     | 2200     | -         |
| Hydroxide (mg/L)                       | -          | -        | -        | -         |
| Total alkalinity (mg/L)                | -          | -        | -        | -         |
| Nitrate (mg/L-N)                       | -          | -        | 1.2      | -         |
| Ion balance (%)                        | 2.4        | -        | -        | -         |

(-) analysis not performed for parameter

mg/L - milligram per liter

μS/cm - microsiemens per centimeter

su - standard units

Table 18.2-23 Water Quality at Pictured Cliffs Sandstone Monitoring Well GM-30A

| Parameter (units)                       | 5/19/1976 | 8/22/1977 | 9/10/1979 |
|---|-----------|-----------|-----------|
| Arsenic (mg/L)                          | <0.01     | <0.01     | 0.0019    |
| Barium (mg/L)                           | 0.4       | <0.5      | 0.03      |
| Boron (mg/L)                            | 0.46      | 0.6       | 0.96      |
| Cadmium (mg/L)                          | <0.001    | <0.01     | <.01      |
| Chromium (mg/L)                         | 0.010     | <0.01     | 0.01      |
| Copper (mg/L)                           | 0.007     | 0.01      | <.01      |
| Iron (mg/L)                             | 0.49      | <0.05     | 0.01      |
| Lead (mg/L)                             | 0.20      | <0.05     | 0.13      |
| Manganese (mg/L)                        | 0.07      | 0.04      | <.01      |
| Mercury (mg/L) <sup>1</sup>             | <0.0004   | <0.001    | -         |
| Selenium (mg/L) <sup>2</sup>            | <0.01     | <0.01     | 0.002     |
| Silver (mg/L)                           | <0.001    | <0.05     | <.01      |
| Zinc (mg/L)                             | 0.09      | <0.05     | 0.16      |
| Total iron (mg/L)                       | -         | -         | 0.02      |
| Total manganese (mg/L)                  | -         | -         | 0.05      |
| pH (su)                                 | 7.6       | 7.5       | 7.5       |
| Electrical conductivity (EC)<br>(uS/cm) | -         | -         | -         |

Table 18.2-23 (Continued)

| Parameter (units)                   | 5/19/1976 | 8/22/1977 | 9/10/1979 |
|-------------------------------------|-----------|-----------|-----------|
| Total dissolved solids (TDS) (mg/L) | 6573      | 6930      | 7070      |
| Fluoride (mg/L)                     | -         | -         | -         |
| Bicarbonate (mg/L)                  | 171       | 210       | -         |
| Carbonate (mg/L)                    | -         | -         | -         |
| Chloride (mg/L)                     | 1215      | 1120      | 1203      |
| Sulfate (mg/L)                      | 422       | 3100      | 3105      |
| Calcium (mg/L)                      | 30.8      | 102       | -         |
| Magnesium (mg/L)                    | 17.7      | 22        | -         |
| Potassium (mg/L)                    | -         | -         | -         |
| Sodium (mg/L)                       | 2070      | 2110      | -         |
| Hydroxide (mg/L)                    | -         | -         | -         |
| Total alkalinity (mg/L)             | -         | -         | -         |
| Nitrate (mg/L-N)                    | 0.51      | 0.4       | -         |
| Ion balance (%)                     | 34        | 4.5       | -         |

(-) analysis not performed for parameter

mg/L - milligram per liter

μS/cm - microsiemens per centimeter

su - standard units

Table 18.3-1 Measured and Modeled Recharge Rates

| Surface characterization | Recharge range <sup>1</sup><br>(in/yr) | Mean recharge <sup>1</sup> (in/yr) | Modeled recharge<br>(in/yr) |
|--------------------------|--|------------------------------------|-----------------------------|
| Badlands                 | 0.002 to 0.01                          | 0.006                              |                             |
| Slopes > 5%              |  |                                    | 0.002                       |
| Slopes: 2 to 5%          |  |                                    | 0.01                        |
| Upland flat              | .02 to 0.05                            | 0.03                               |                             |
| Upland flat (slope<1%)   |  |                                    | 0.03                        |
| Upland (slope 1 to 2%)   |  |                                    | 0.02                        |
| Alluvial valley          | 0.09                                   | 0.09                               | 0.09                        |

<sup>1</sup>From Stone 1987

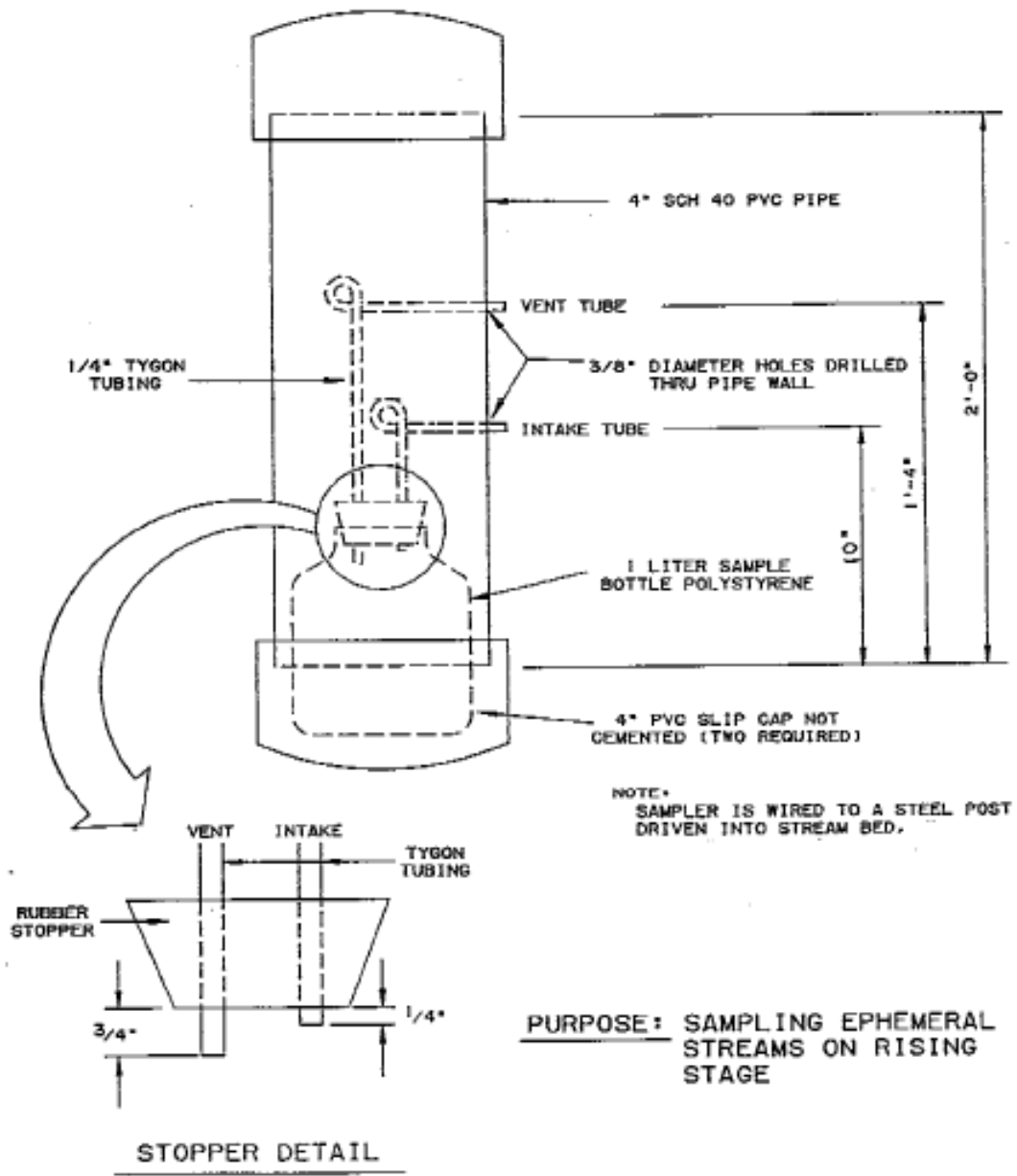


Figure 18.1-1 Schematic of Single-Stage Sediment Sampler

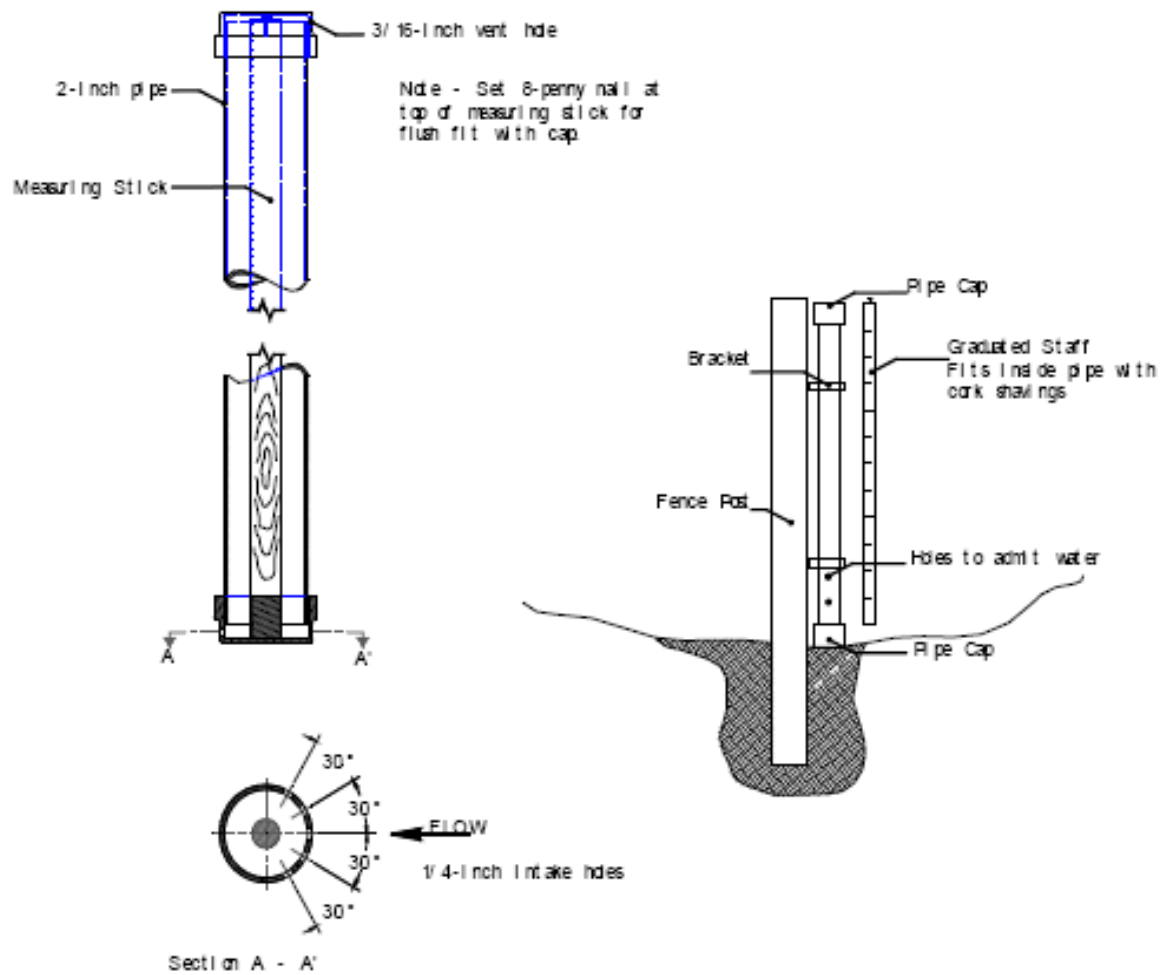
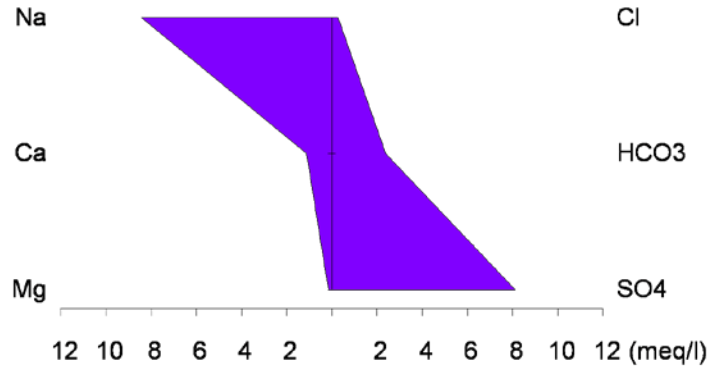


Figure 18.1-2 Schematic of Crest Stage Gage



Upper Pinabete 3, 12/3/2007



Lower Pinabete 2, 12/3/2007

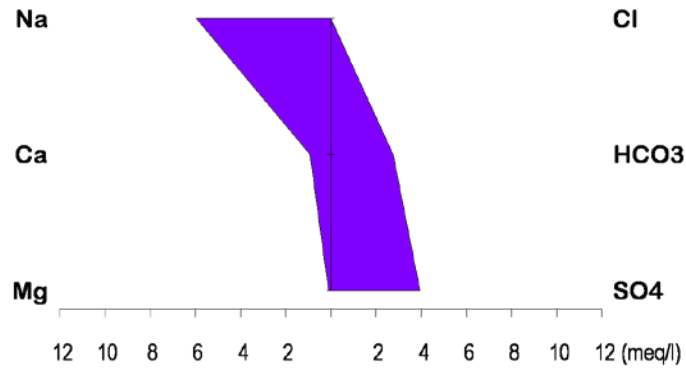


Figure 18.1-3 Pinabete Arroyo Stiff Diagrams

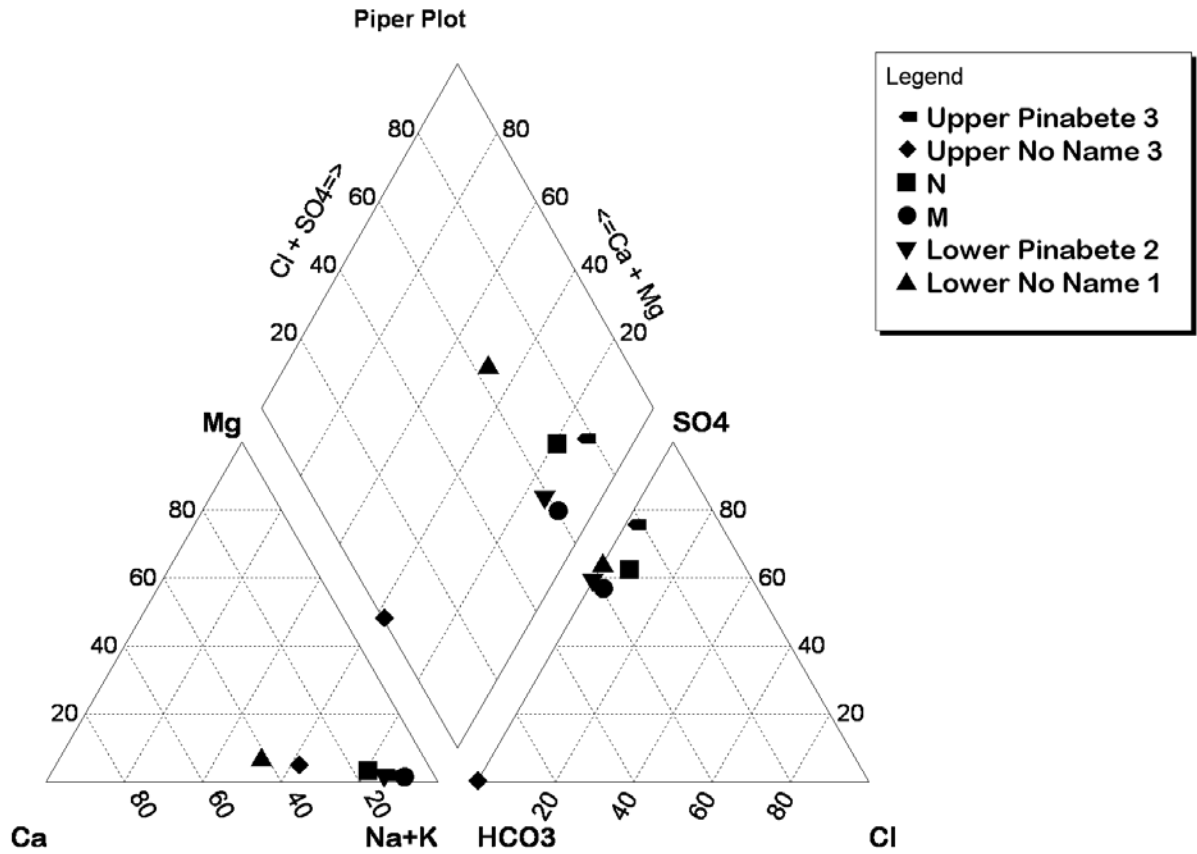
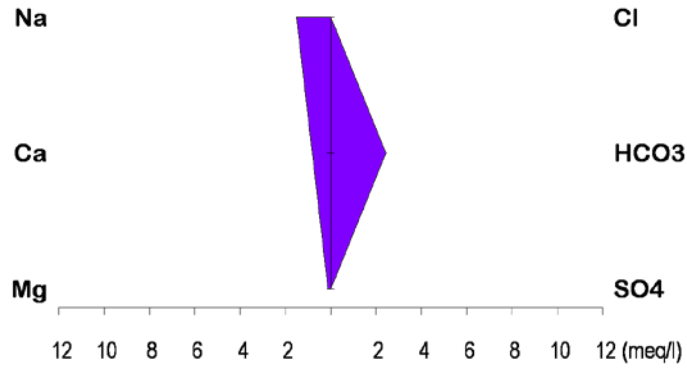


Figure 18.1-4 Piper Plot Diagram for Surface Water Samples from Pinabete Arroyo, No Name Arroyo, and Brimhall Wash

Upper No Name 3, 2/13/2008



Lower No Name 1, 8/28/2007

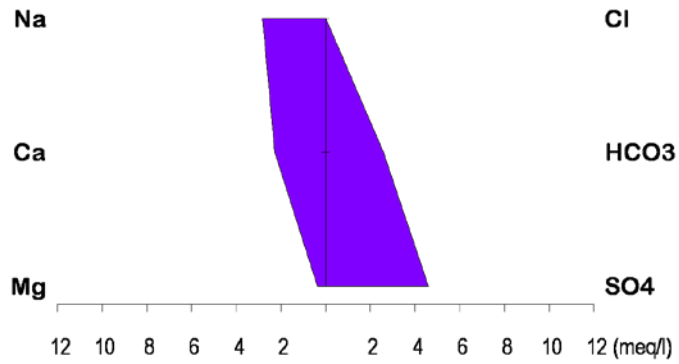
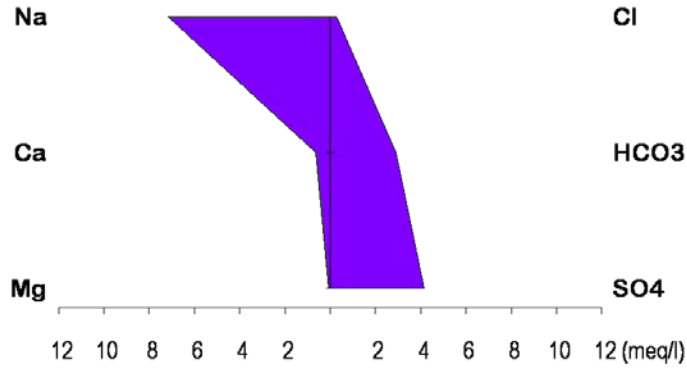


Figure 18.1-5 No Name Arroyo Stiff Diagrams

**M, 8/31/1992**



**N, 8/31/1992**

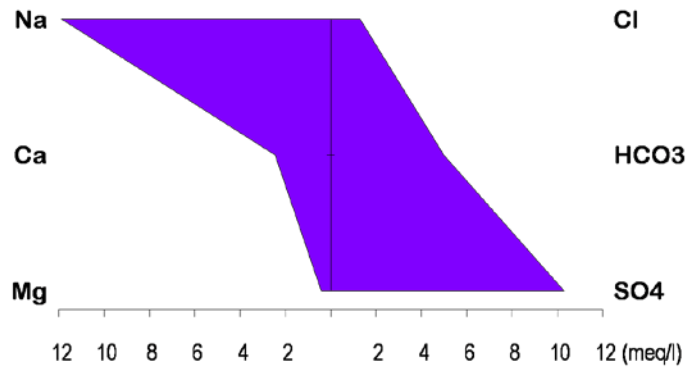


Figure 18.1-6 Brimhall Wash Stiff Diagrams – Upstream (Site N) and Downstream (Site M).

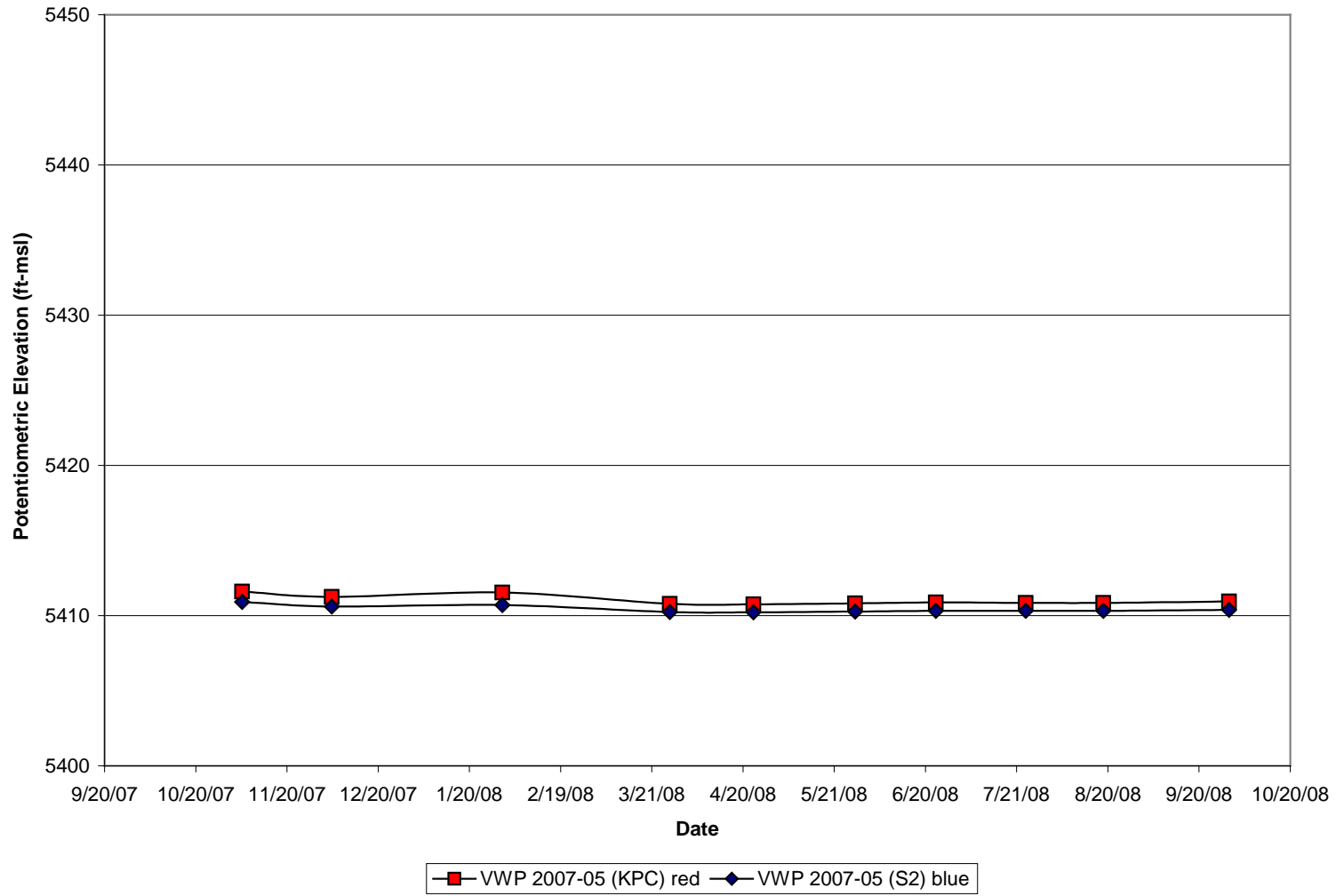


Figure 18.2-1 Baseline Potentiometric Elevations at Location VWP2007-05

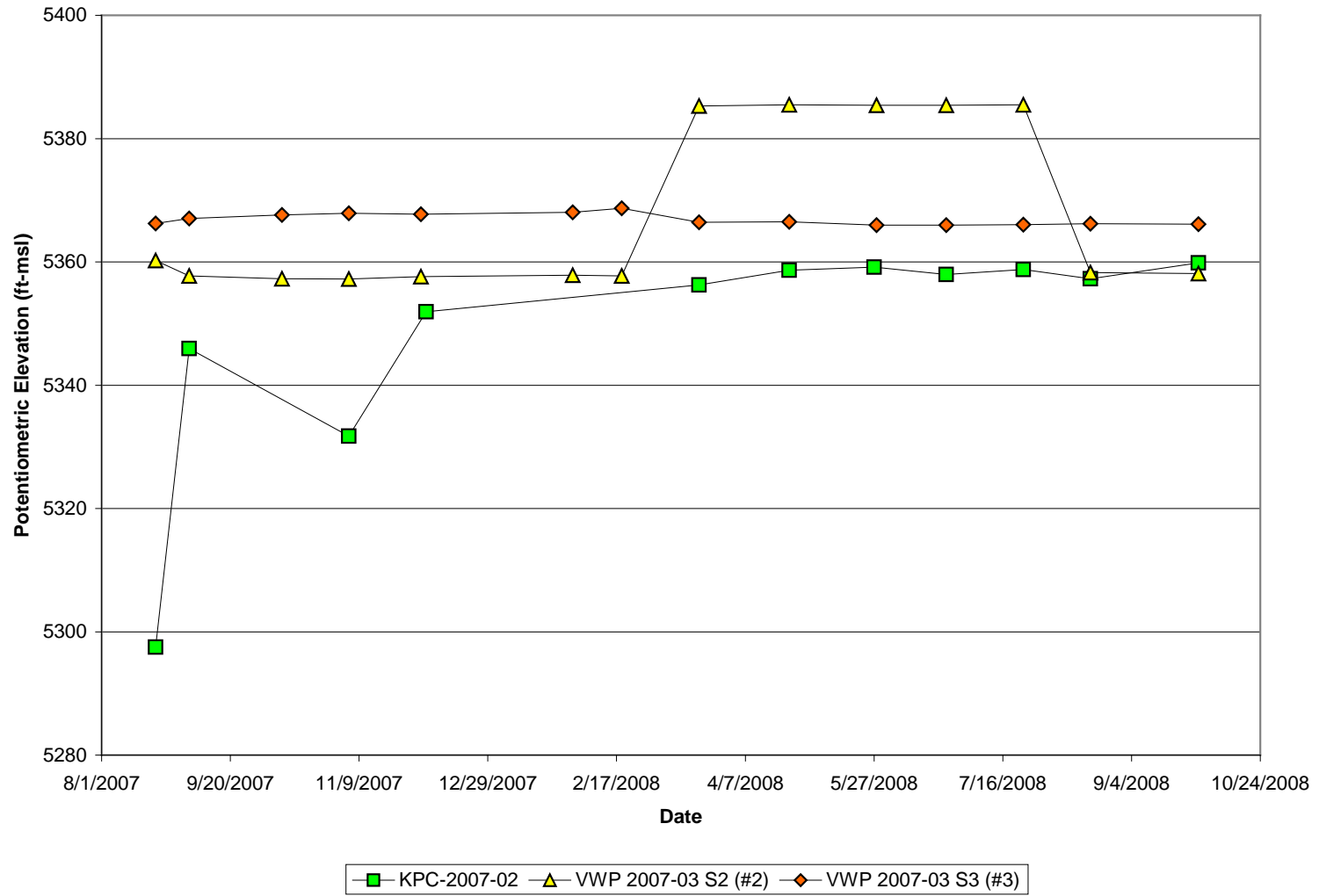


Figure 18.2-2 Baseline Potentiometric Elevations at Location VWP2007-03

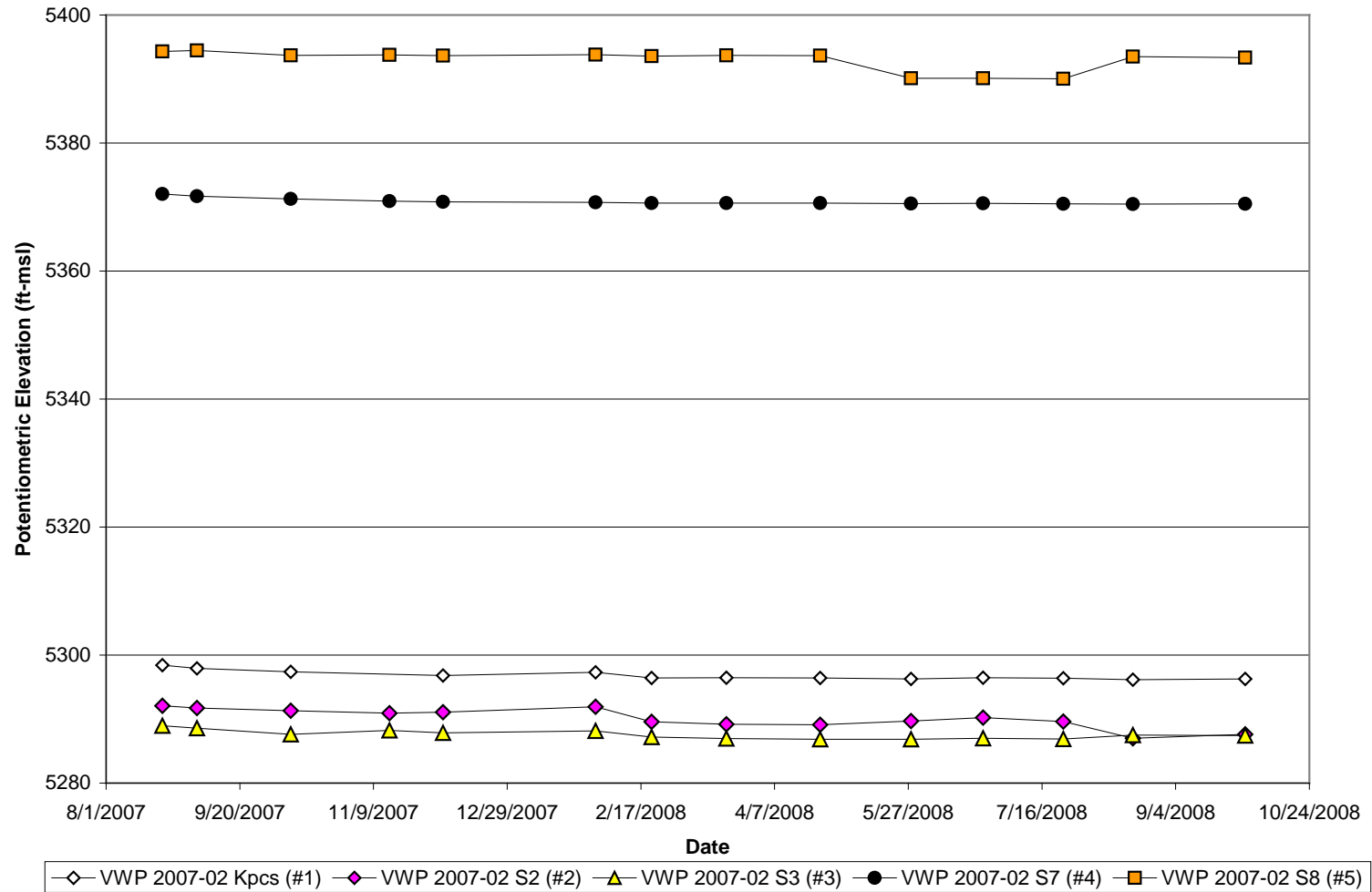


Figure 18.2-3 Baseline Potentiometric Elevations at Location VWP2007-02

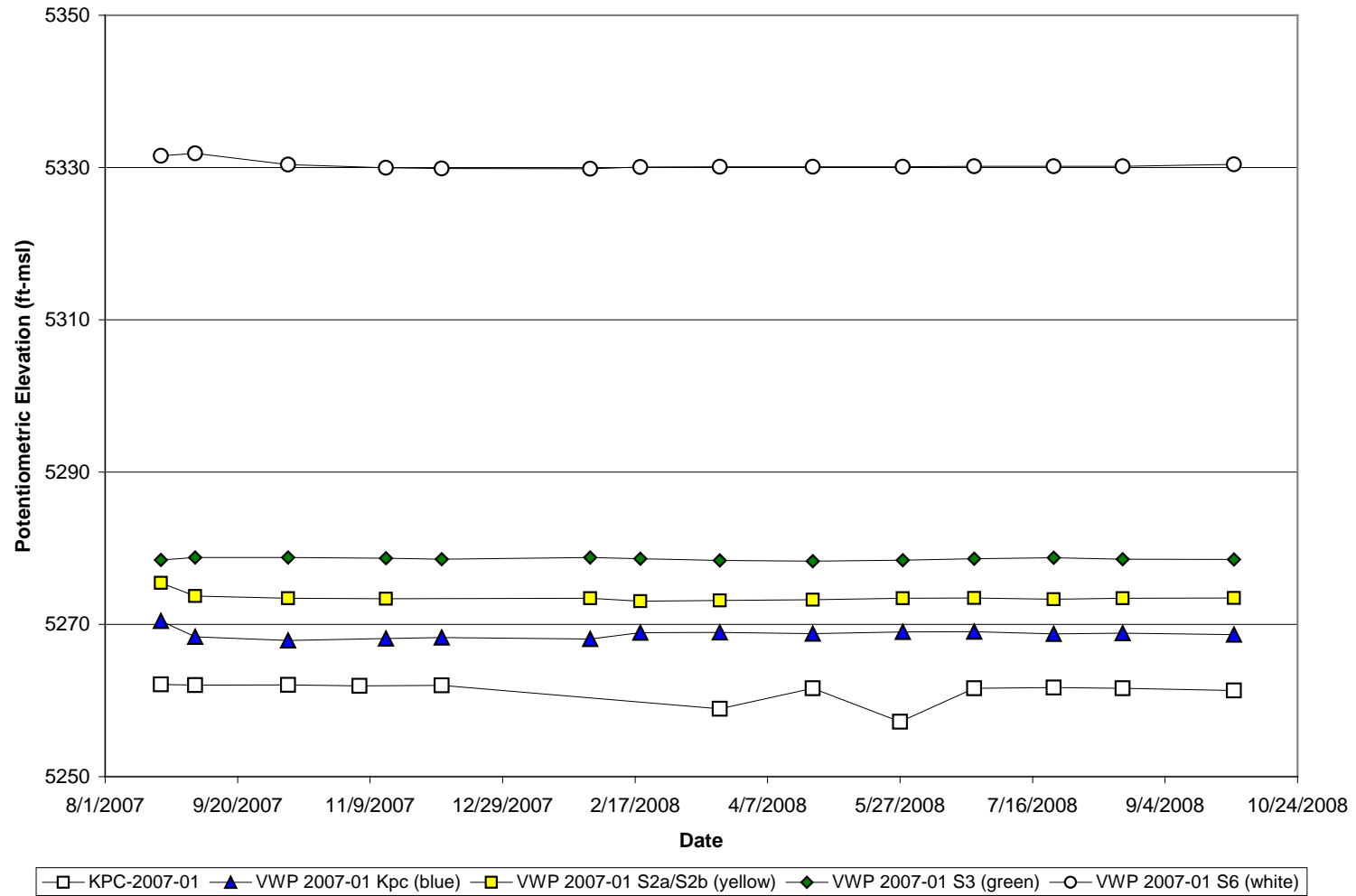


Figure 18.2-4 Baseline Potentiometric Elevations at Location VWP2007-01



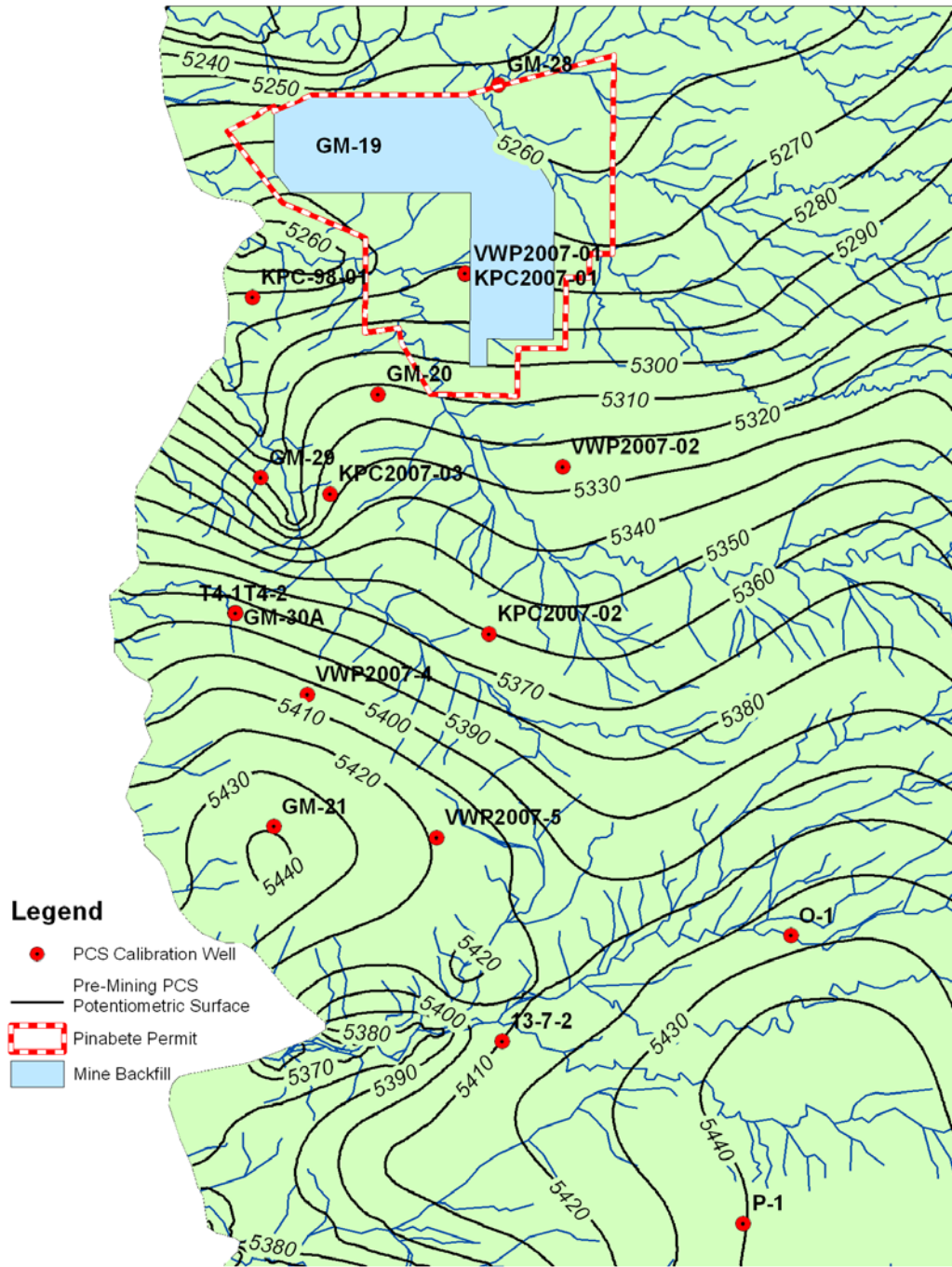


Figure 18.3-1 Modeled Baseline Potentiometric Surface for the Pictured Cliffs Sandstone

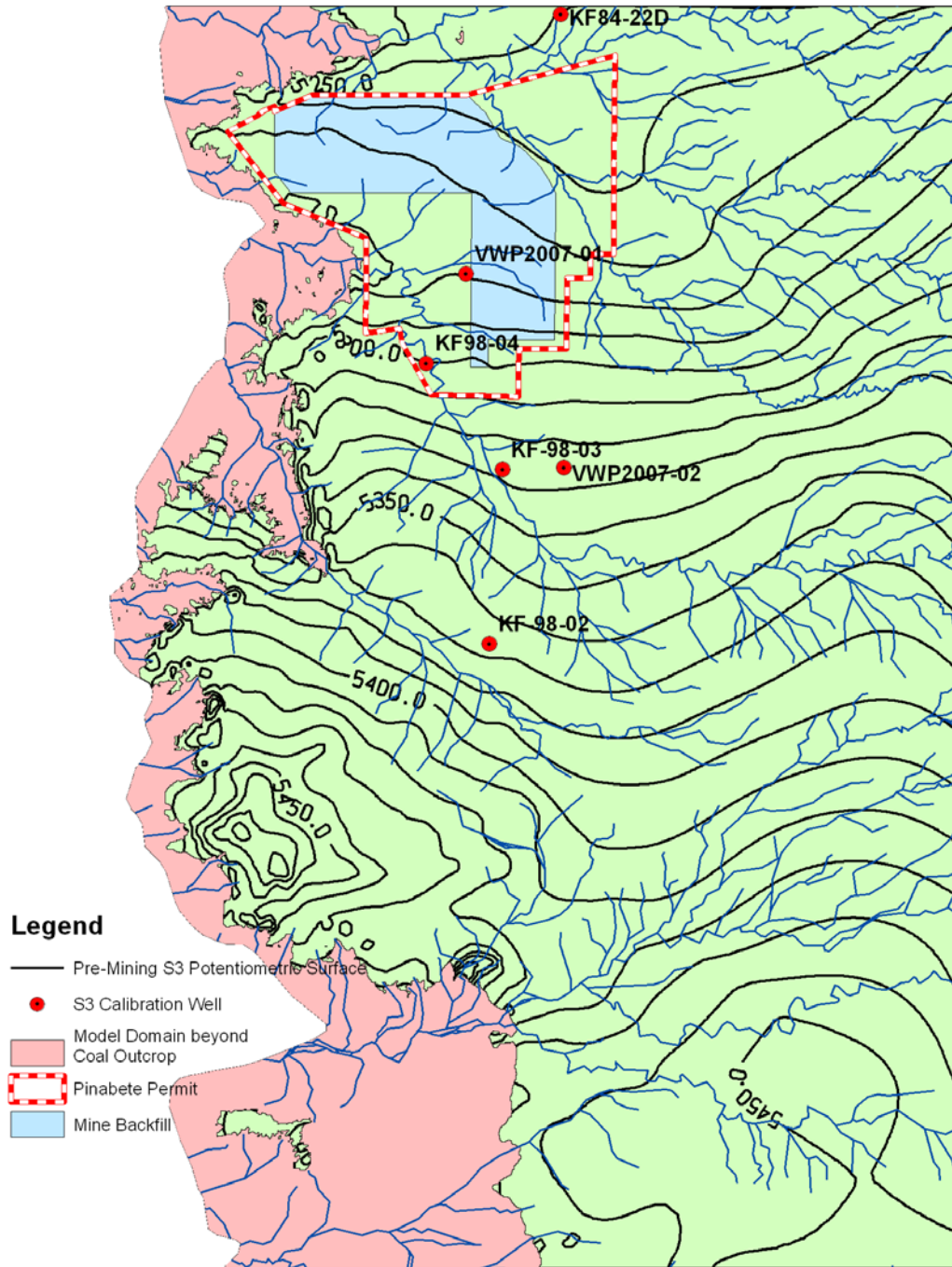


Figure 18.3-2 Modeled Baseline Potentiometric Surface for the No. 3 Coal Seam

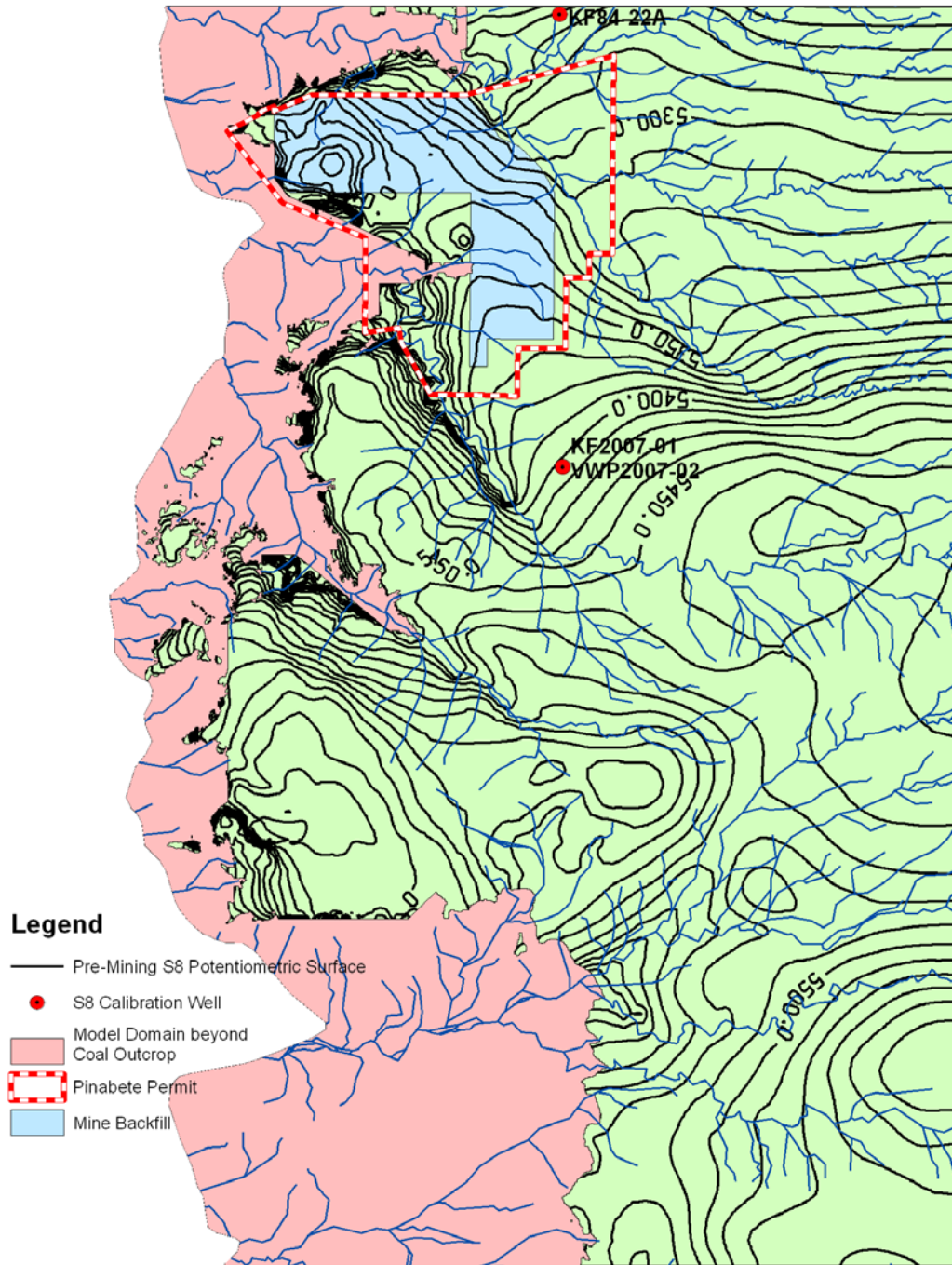


Figure 18.3-3 Modeled Baseline Potentiometric Surface for the No. 8 Coal Seam



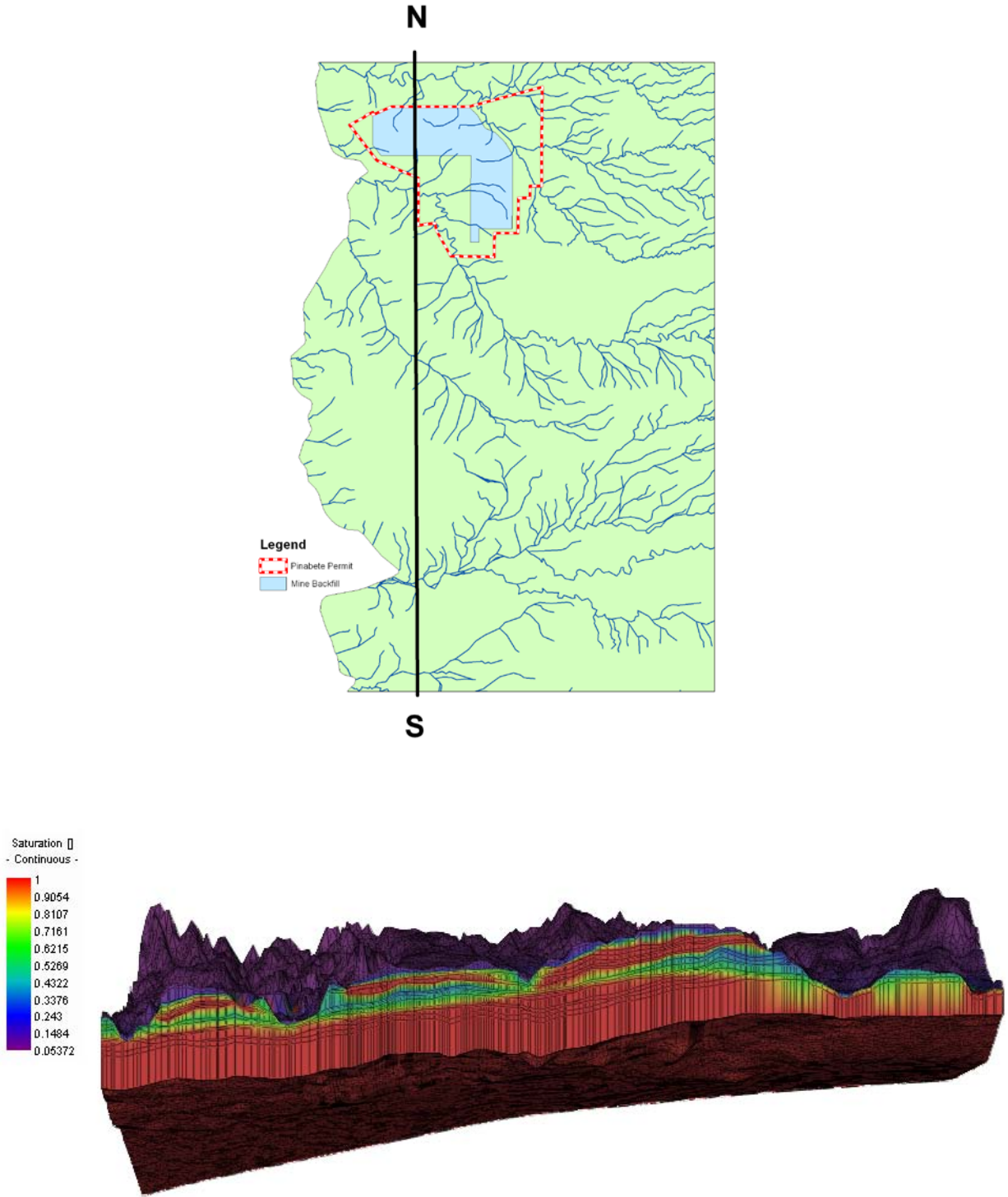
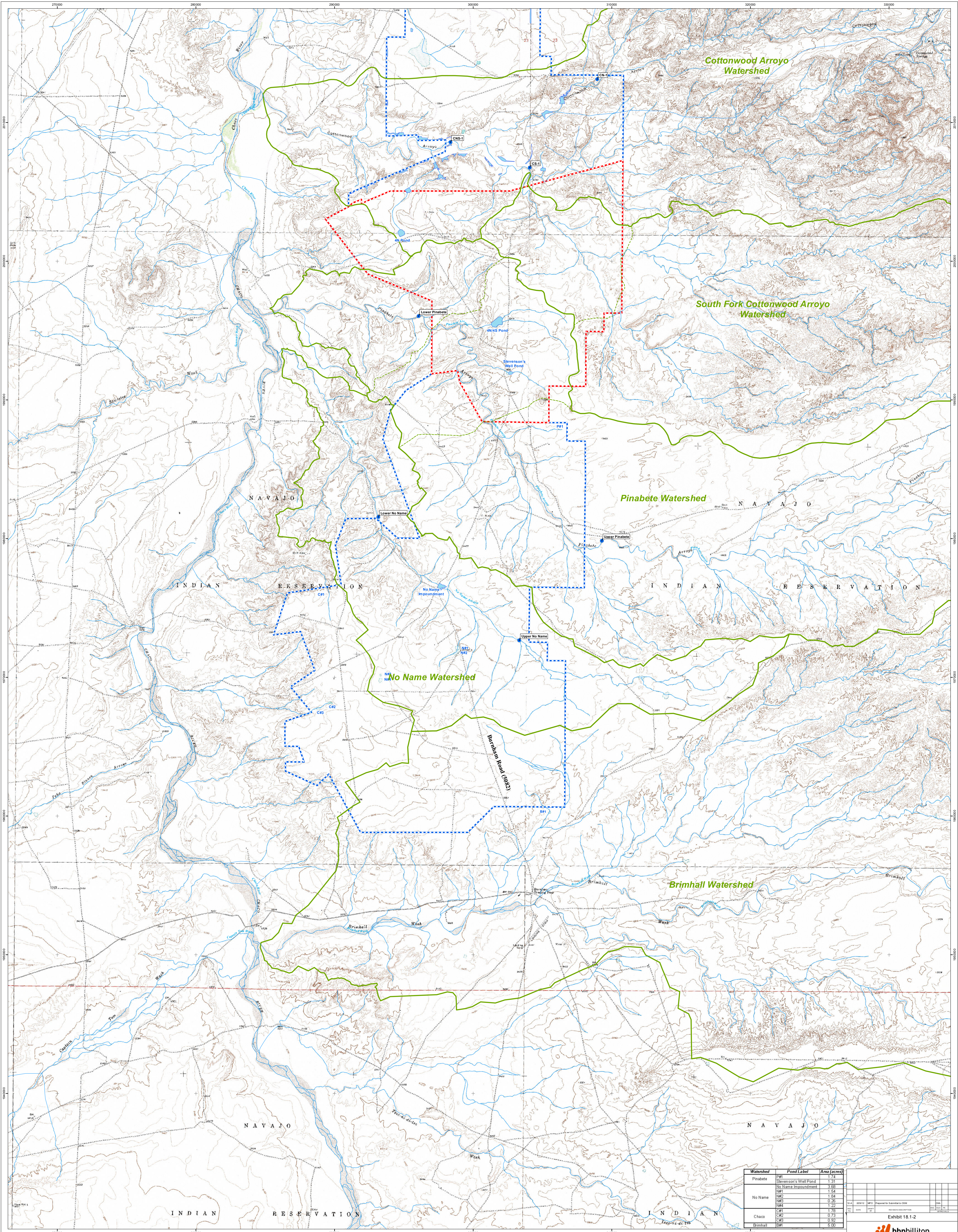


Figure 18.3-4 Modeled Baseline Saturation for a North-South Section at Pinabete Permit Area









| Watershed | Pond Label            | Area (acres) |
|-----------|-----------------------|--------------|
| Pinabete  | SWP                   | 1.74         |
|           | Stevenson's Well Pond | 1.31         |
|           | No Name Impoundment   | 1.58         |
| No Name   | CWS1                  | 1.54         |
|           | CWS2                  | 1.84         |
|           | CWS3                  | 0.26         |
|           | CWS4                  | 1.22         |
| Chaco     | CWS1                  | 1.78         |
|           | CWS2                  | 0.73         |
|           | CWS3                  | 0.92         |
| Brimhall  | SWP                   | 5.00         |

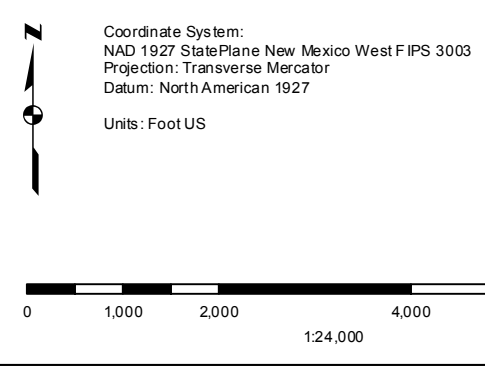
| DATE    | BY  | DESCRIPTION                   |
|---------|-----|-------------------------------|
| 2011/12 | MDP | Prepared for Submittal to OSM |
| 2011    | MDP | Revised                       |

Exhibit 18.1-2



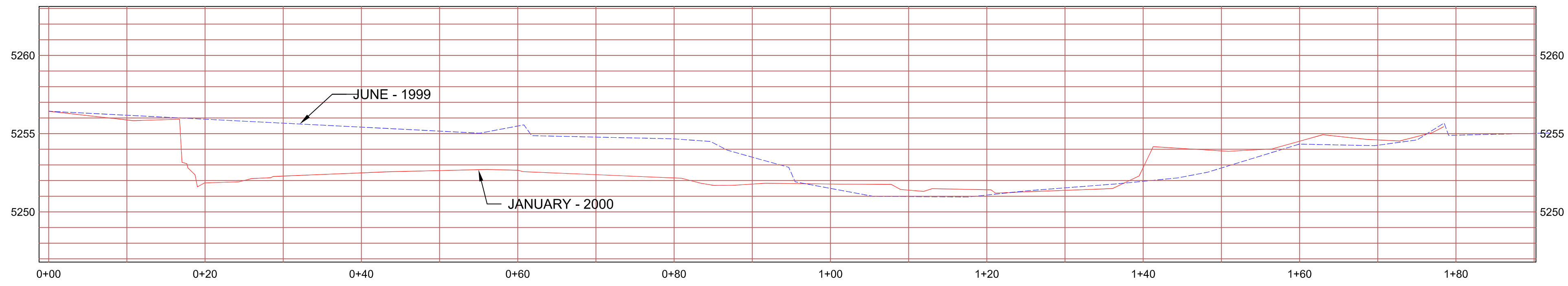
**BHP NAVAJO COAL COMPANY**  
Surface Water Features and Stream Monitoring Stations

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APPROVED BY: CWA DATE: 12/12

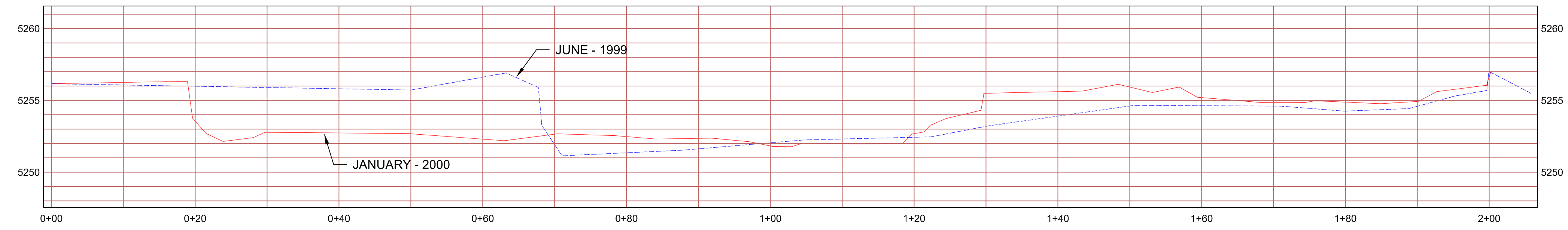


- Legend
- Ponds
  - BNCC Surface Water Monitoring Station
  - Streams
  - Watershed Boundaries
  - Subwatershed Boundaries
  - Pinabete SMCR Permit Area
  - Mining Lease Area

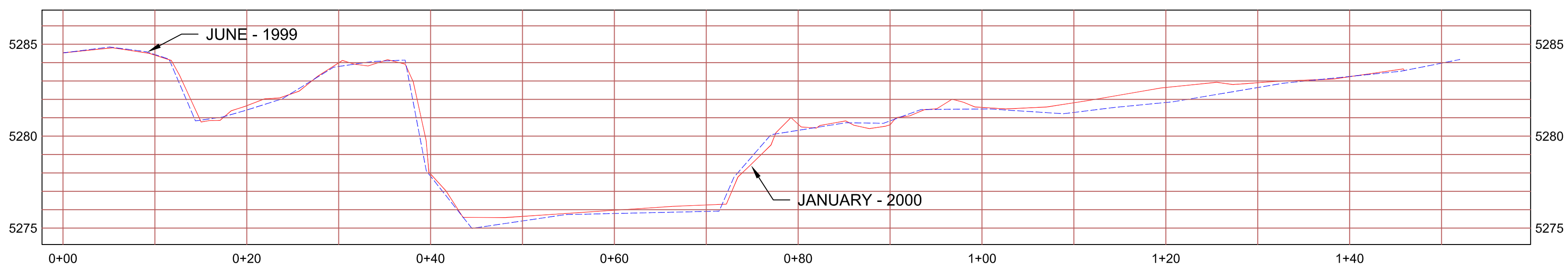




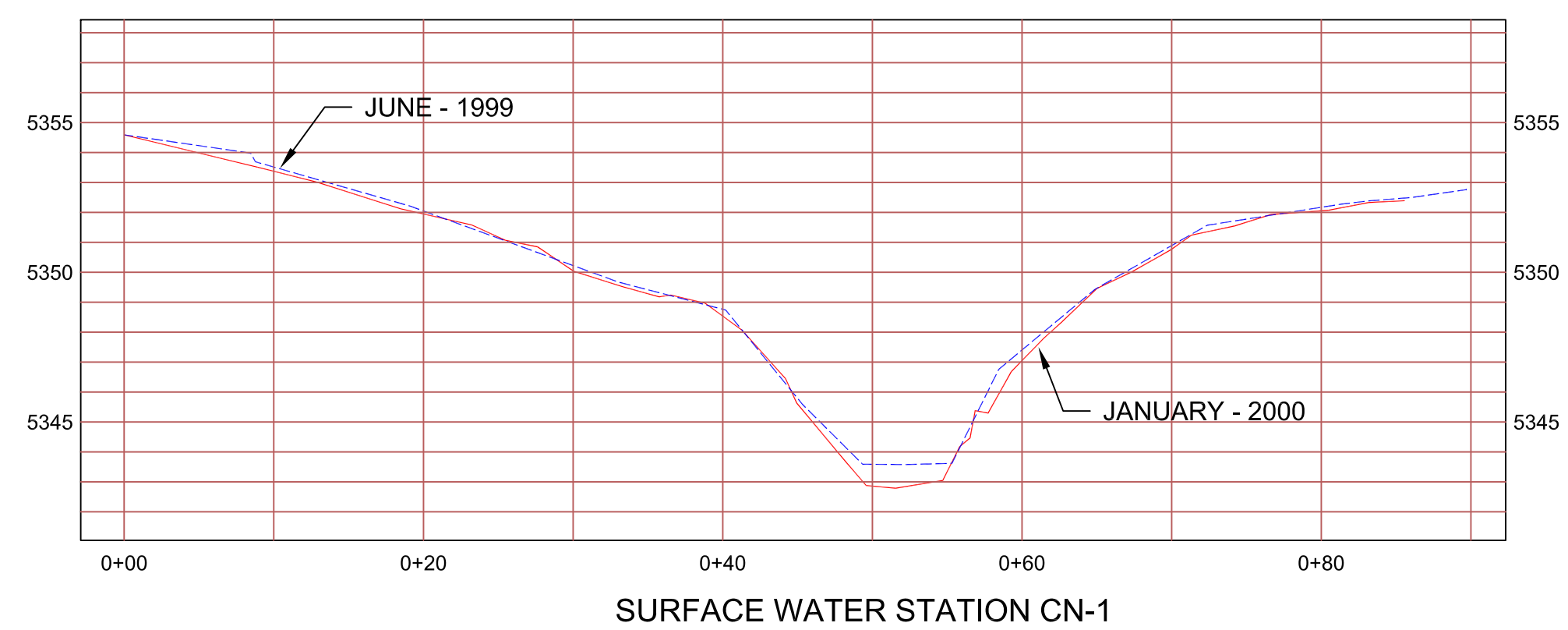
SURFACE WATER STATION CNS-1 SECTION 2 AND 2A  
68 FT DOWNSTREAM FROM SECTION 3 AND 3A



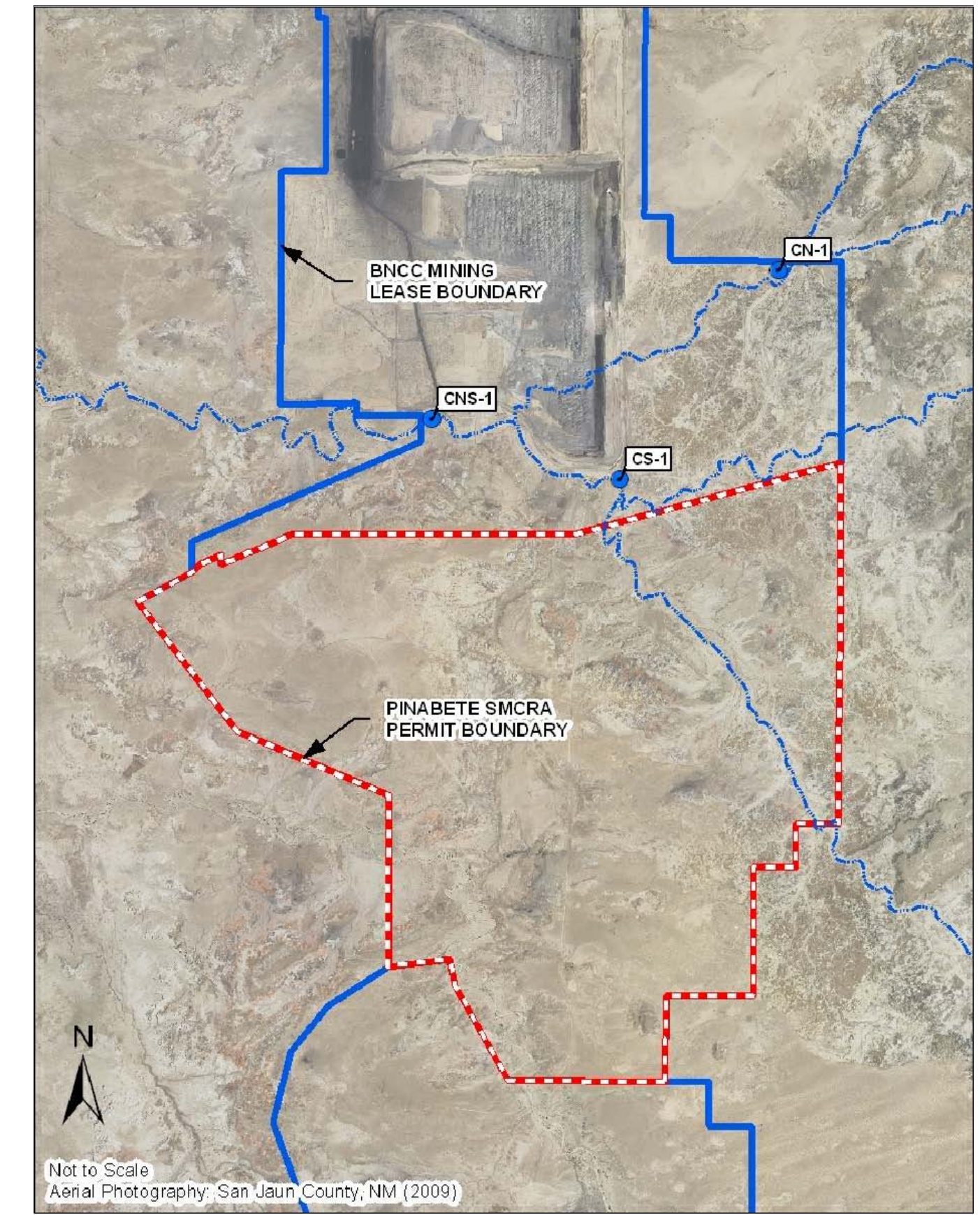
SURFACE WATER STATION CNS-1 SECTION 3 AND 3A  
68 FT UPSTREAM FROM SECTION 2 AND 2A



SURFACE WATER STATION CS-1



SURFACE WATER STATION CN-1



BHP NAVAJO COAL CO.  
PINABETE PERMIT AREA  
PO BOX 1717 FRUITLAND, NEW MEXICO, 87416

ACCOUNT: \_\_\_\_\_  
DATE: 10 FEB 2012  
DESIGNED BY: \_\_\_\_\_  
DRAWN BY: \_\_\_\_\_  
CHECKED BY: CNA  
APPROVED BY: CNA

SURFACE WATER MONITORING  
STATIONS CN-1, CS-1, CNS-1  
JUNE 1999 AND JANUARY 2000  
SURFACES

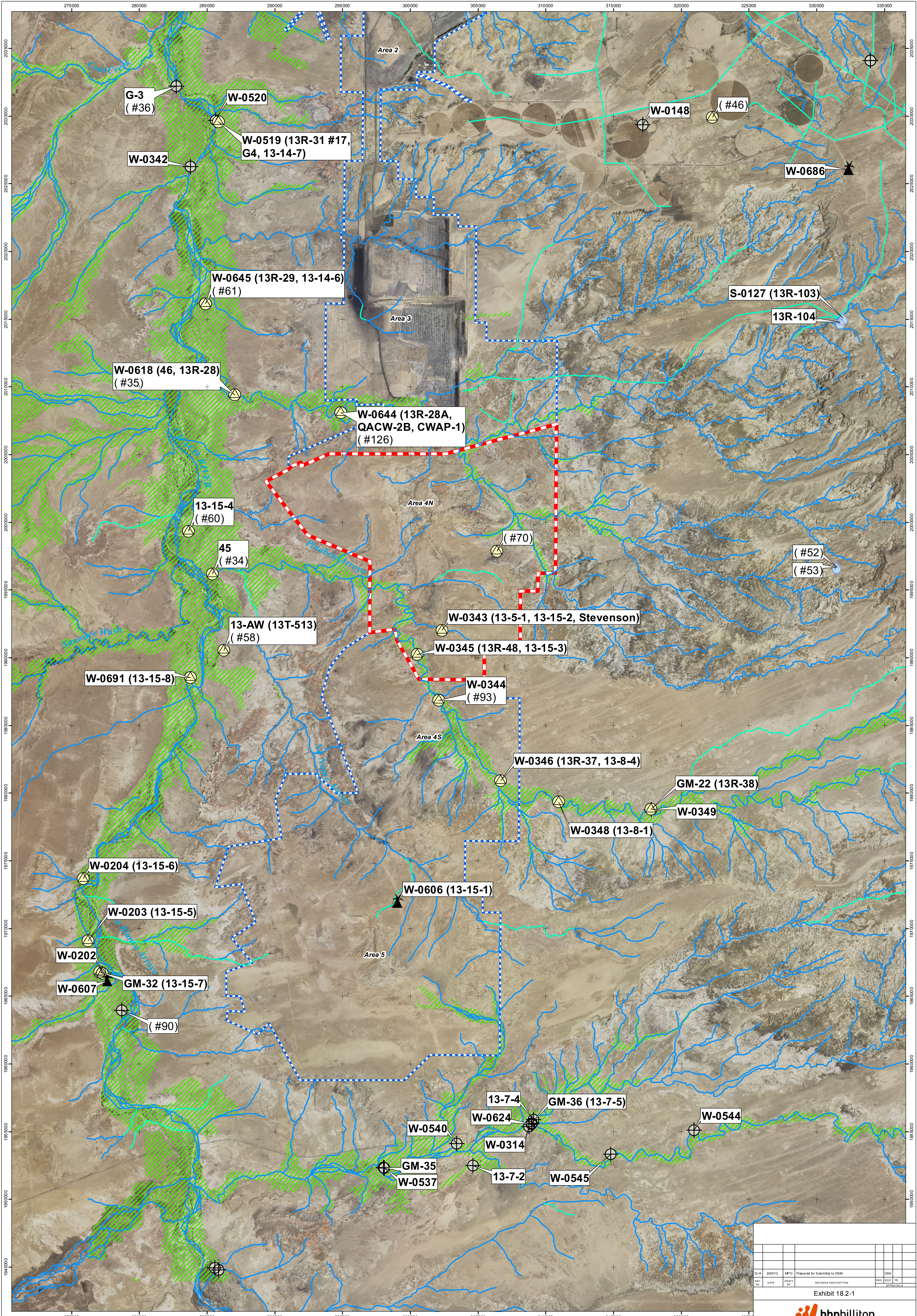
EXHIBIT 18.1-3  
CROSS-SECTIONS  
COTTONWOOD ARROYO

DRAWING  
SHEET  
0

| REV | DATE        | DESCRIPTION                 |
|-----|-------------|-----------------------------|
| 1   | 10 FEB 2012 | ISSUED FOR SUBMITTAL TO OSM |

| PROJECT MANAGER: | REG. NO.: |
|------------------|-----------|
| _____            | _____     |
| ENGR. #/RECORD:  | REG. NO.: |
| _____            | _____     |
| SURV. #/RECORD:  | REG. NO.: |
| _____            | _____     |





Data Sources:  
 Aerial Photography (Geo-Juan County) 2009  
 Navajo Nation Hydrographic Survey (2010)  
 http://www.usgs.gov/mission-areas/water-resources/data-repository/nhdplus/0213.html  
 USGS Geology Maps: MF-536, MF-1076, MF-1077, MF-1080, MF-1052, MF-1063, MF-1078

Coordinate System:  
 NAD 1983 State Plane New Mexico West FIPS 3003  
 Projection: Transverse Mercator  
 Datum: North American 1983  
 Units: Foot US

|  |                             |  |  |
|--|-----------------------------|--|--|
| <p>Water Supply Wells &amp; Springs<sup>1</sup></p> <p>(#BAI Number)</p> <p>Spring &amp; Seep</p> <p>Alluvial Well</p> | <p>Well</p> <p>Windmill</p> | <p>Legend</p> <p>Natural Stream</p> <p>Artificial Path/Ditch</p> <p>Alluvium<sup>2</sup></p> | <p>Pinabete SMCRA Permit Area</p> <p>Mining Lease Area</p> |
|--|-----------------------------|--|--|

|      |         |          |                              |         |      |
|------|---------|----------|------------------------------|---------|------|
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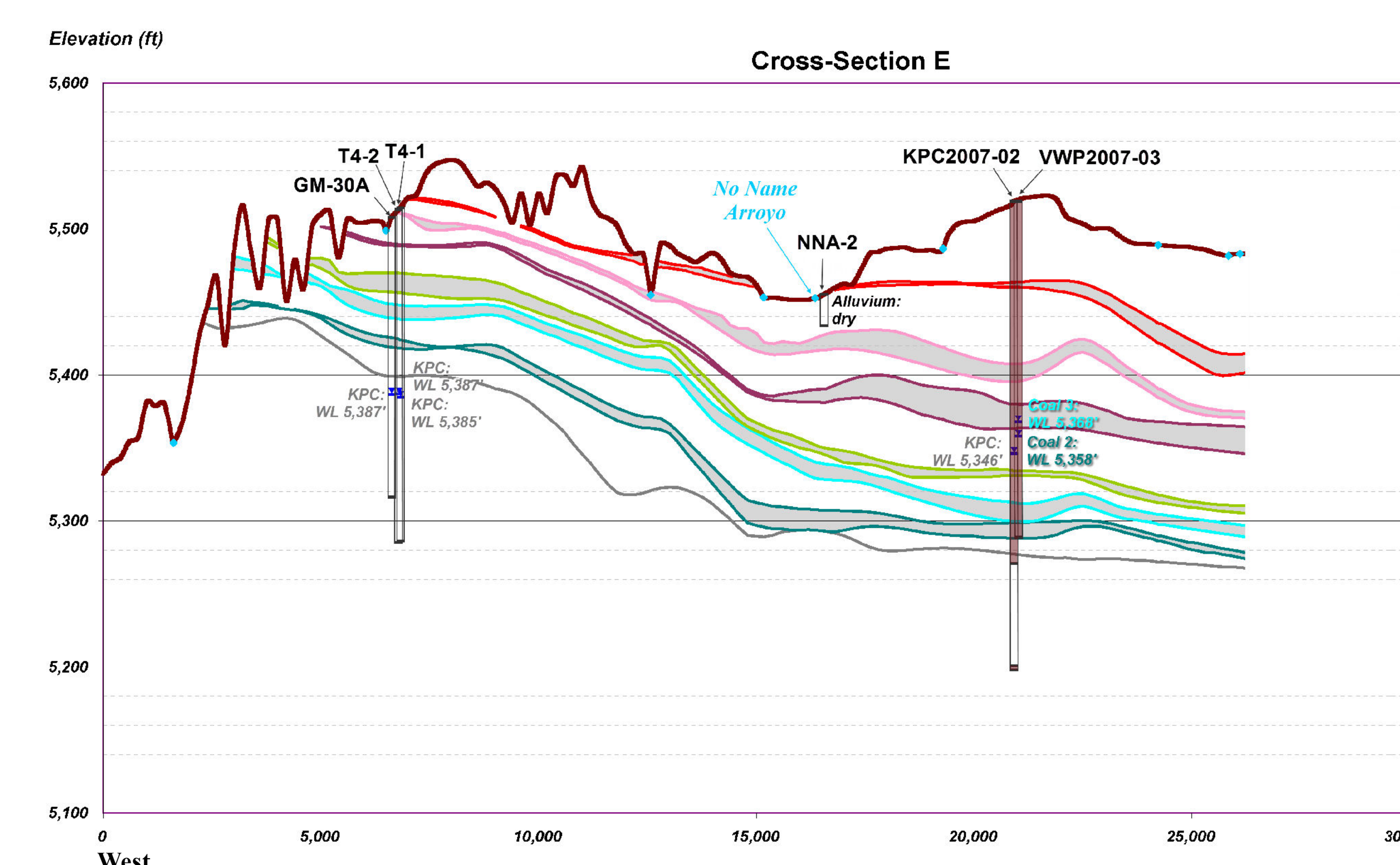
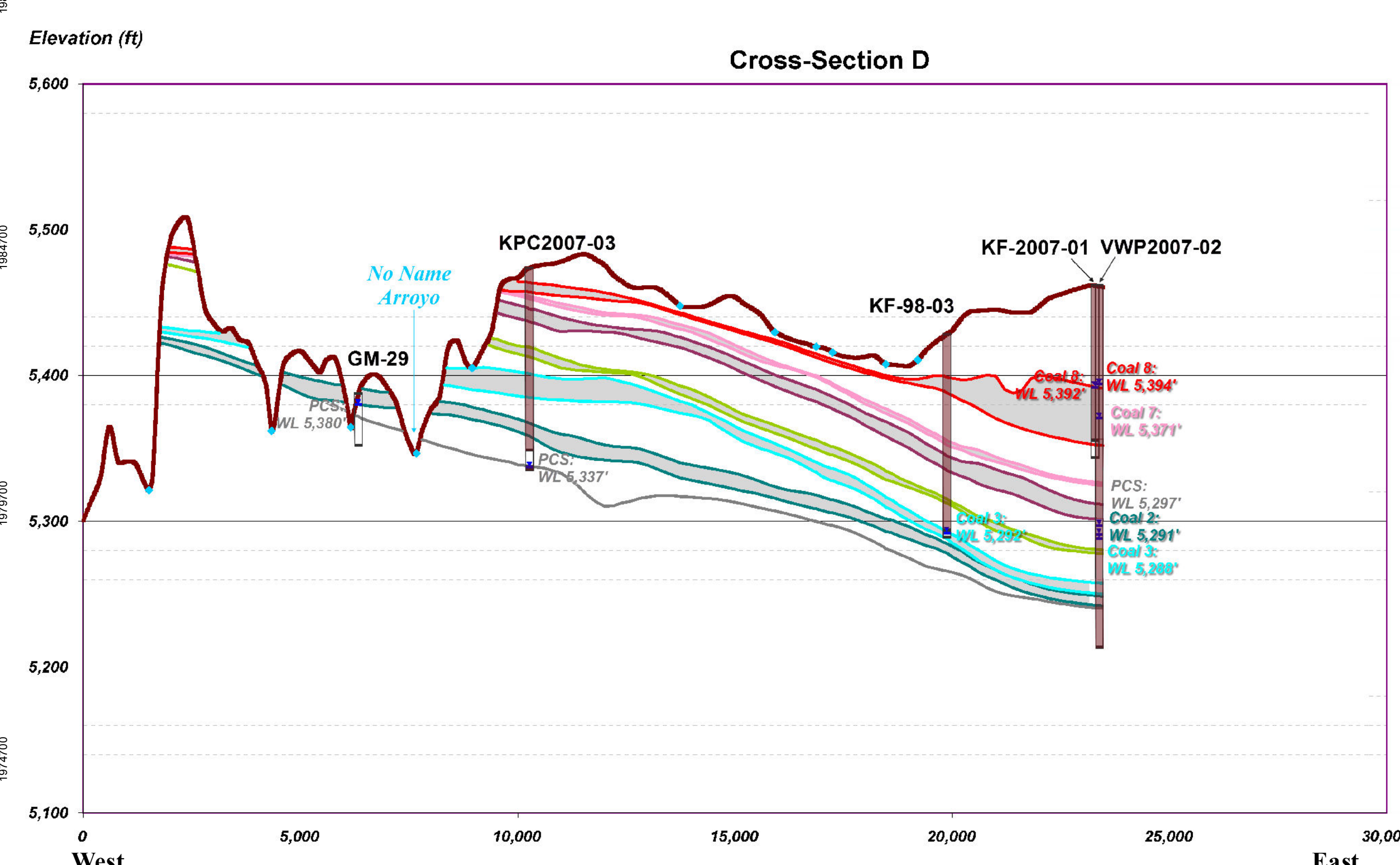
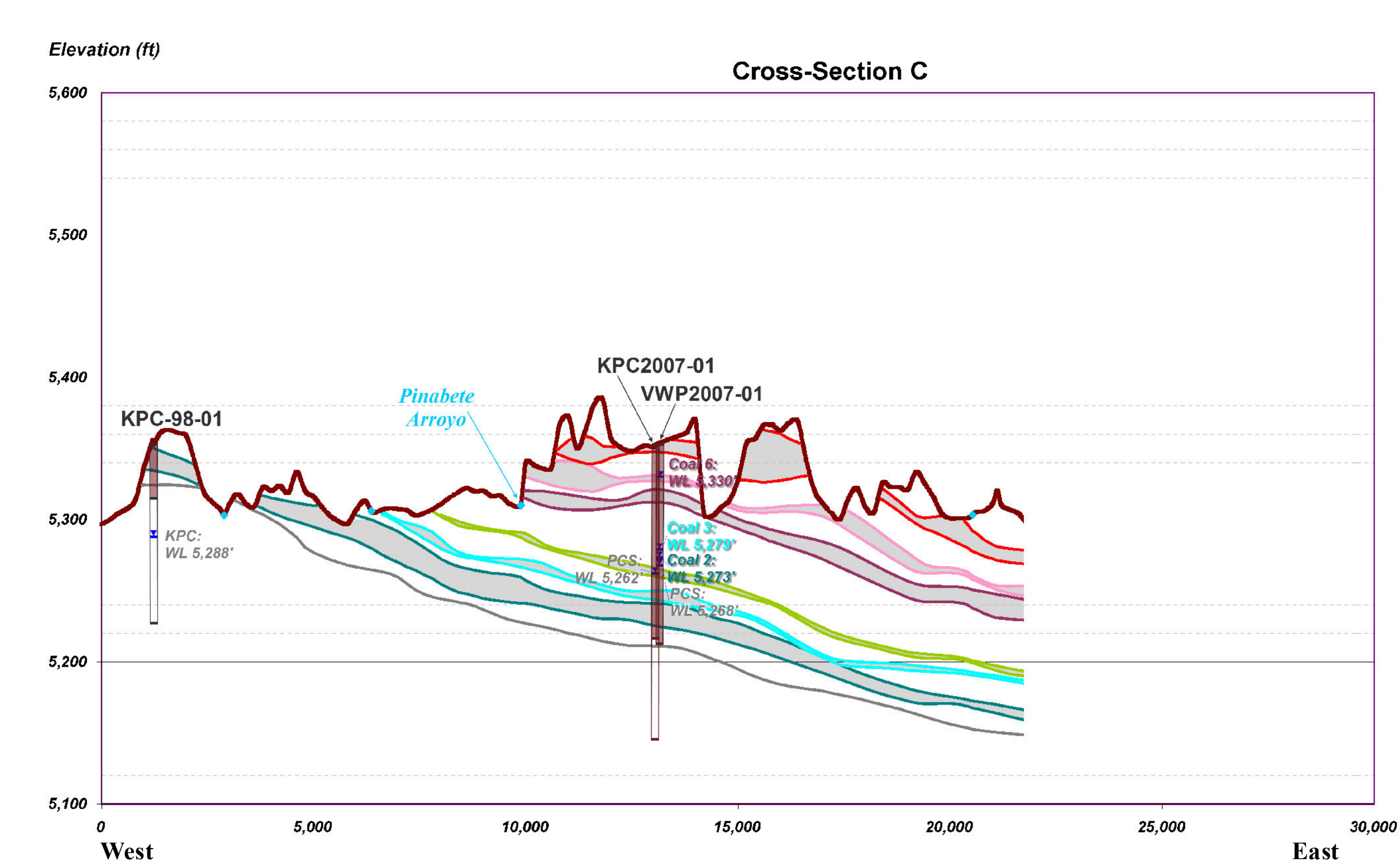
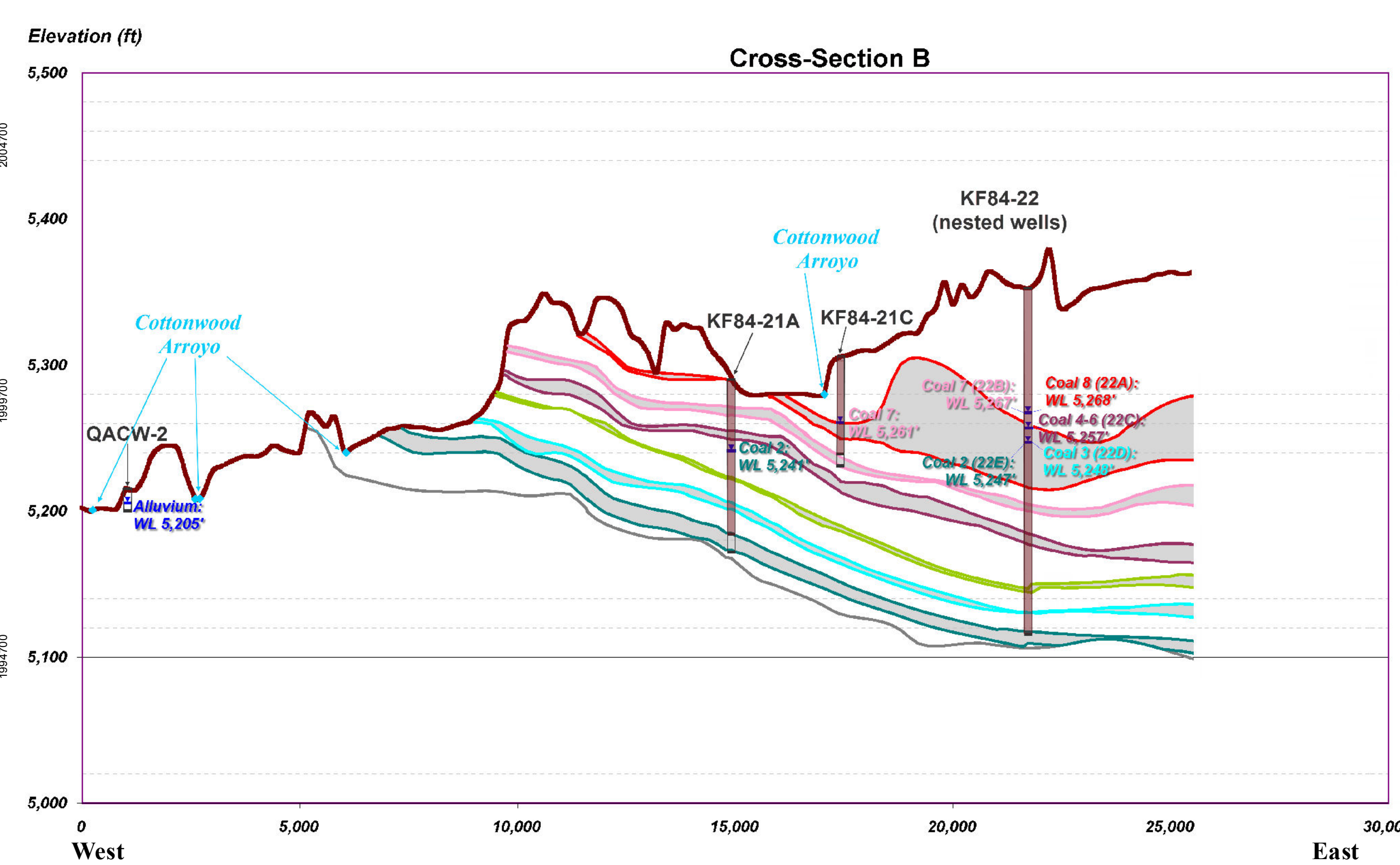
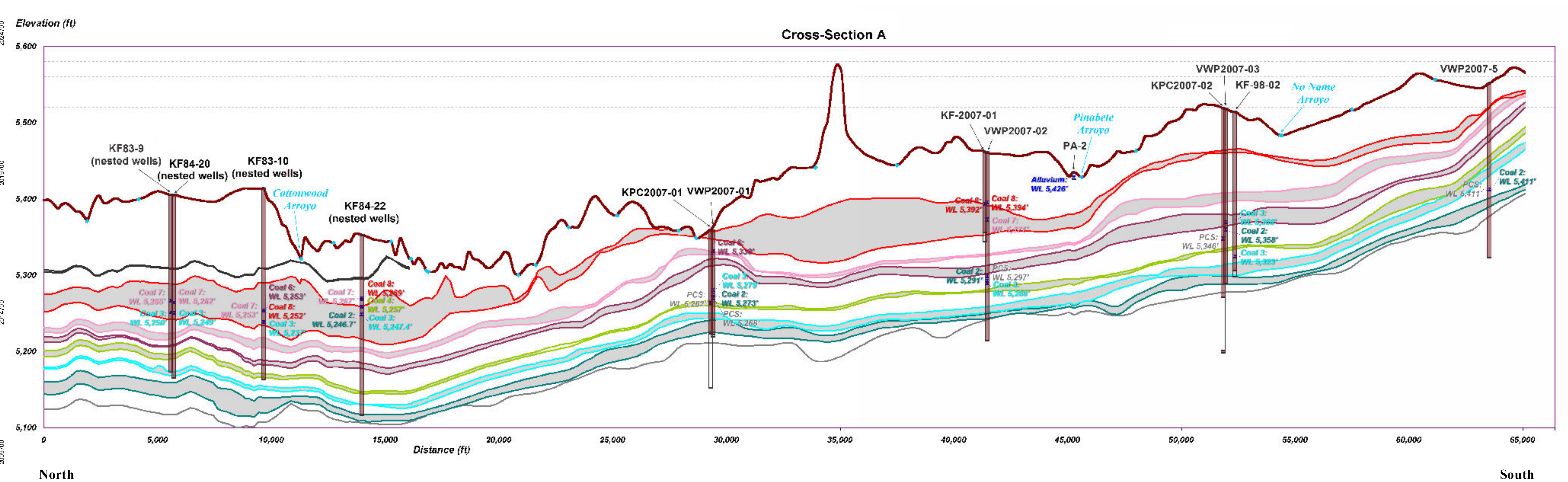
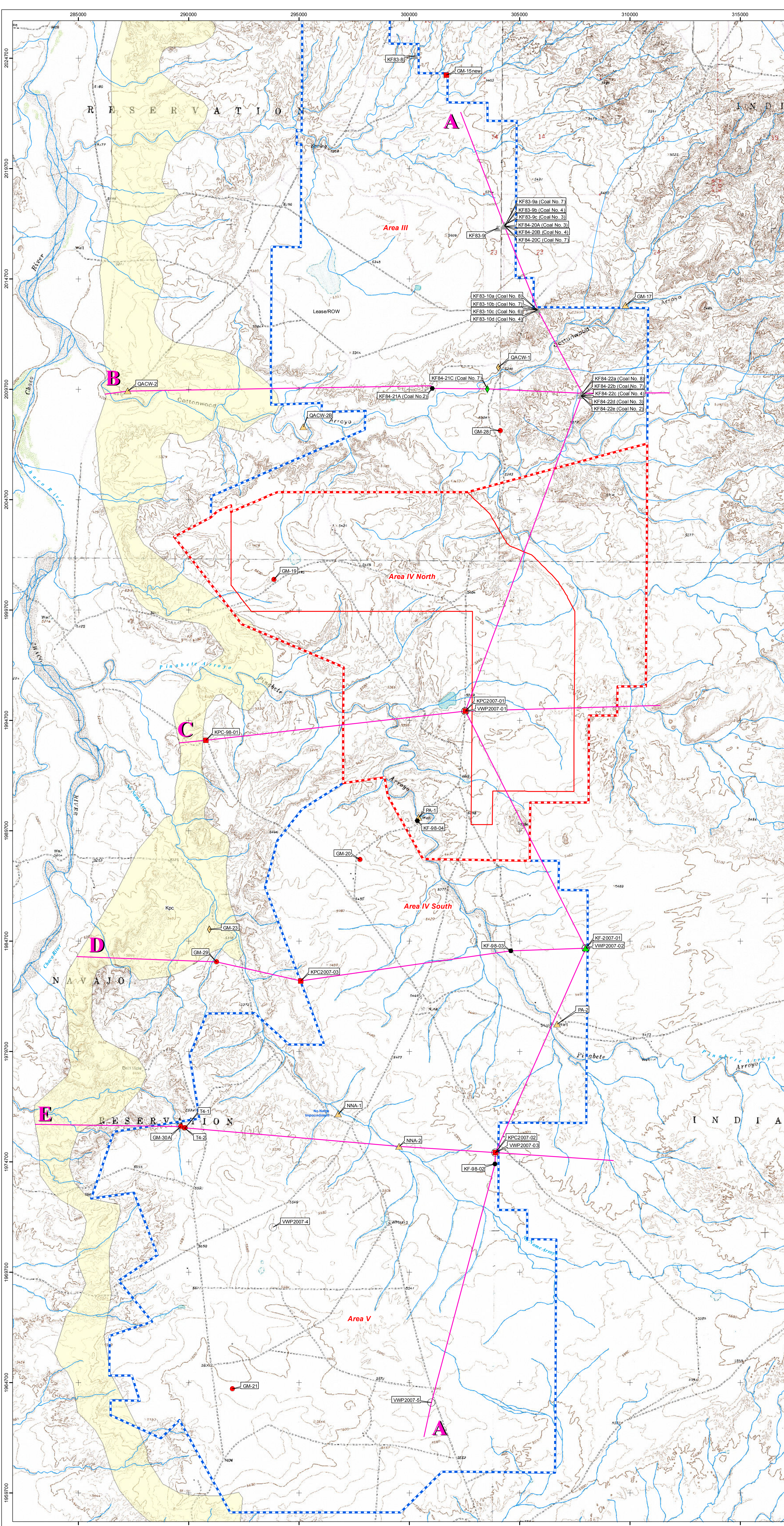
Exhibit 18.2-1

**bhpbilliton**  
 resourcing the future

**BHP NAVAJO COAL COMPANY**  
 Inventory of Water Supply Wells and Springs

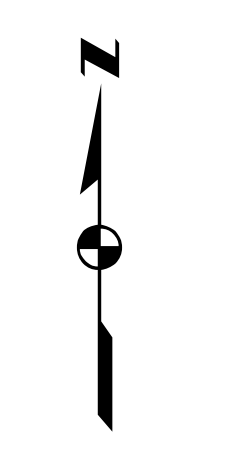
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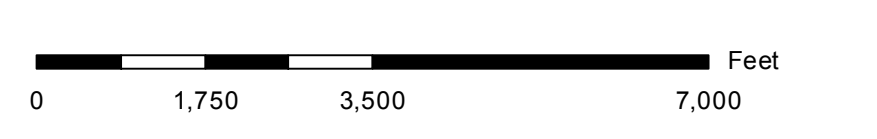
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- ◆ Abandoned Alluvial Monitoring Well
- ◆ Existing Alluvial Monitoring Well
- ◆ Well, Coal No. 2, Existing
- No 3, Coal Monitoring Well
- Well, Coal No. 4, Existing
- No 6, Coal Monitoring Well
- No 7, Coal Monitoring Well
- ▲ No 8, Coal Monitoring Well
- ▲ Fruitland Well or Nested Wells
- Abandoned PCS Monitoring Well
- Existing PCS Monitoring Well
- Nested Vibrating Wire Piezometer
- ▭ Pinabete SMCRA Permit Area
- ▭ Mining Lease Area
- ▭ Proposed Mine Block
- Streams
- Pictured Cliffs Formation (Kpc)

- Cross-Sections
- Pictured Cliffs Top
- S2 Coal
- S3 Coal
- S4 Coal
- S6 Coal
- S7 Coal
- S8 Coal
- S9 Coal
- Topo (2000)
- Wells
- Water Levels
- Streams



Projection Information:  
 State Plane New Mexico West  
 North American Datum 1927  
 FIPS 3003  
 feet

1:24,000



|      |    |          |             |
|------|----|----------|-------------|
| DATE | BY | REVISION | DESCRIPTION |
|      |    |          |             |

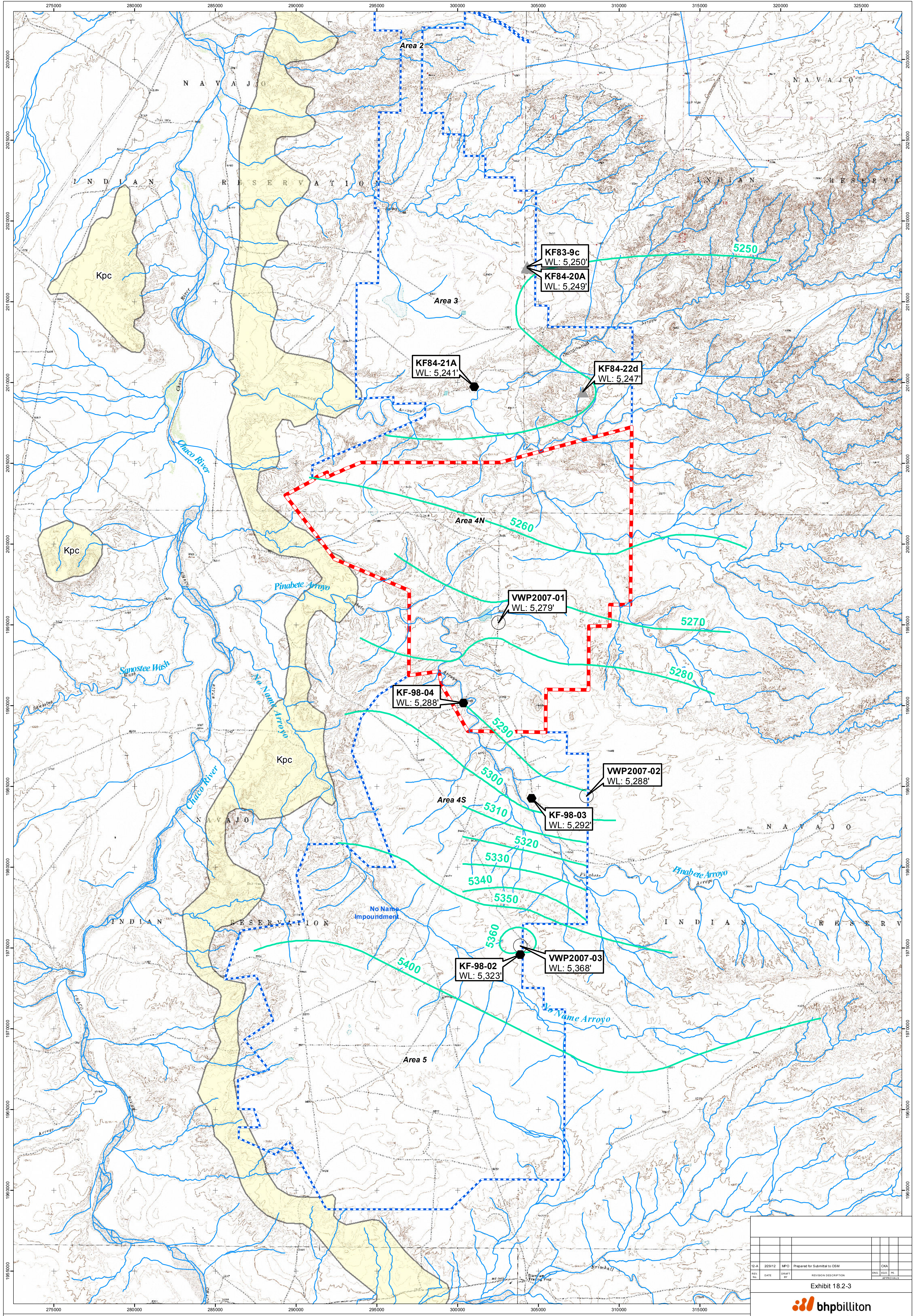
Exhibit 18.2-2

**bhpbilliton**  
 resourcing the future

**BHP NAVAJO COAL COMPANY**  
 Hydrogeologic Cross-Sections,  
 Monitoring Wells, & Piezometers

|                  |              |                    |
|------------------|--------------|--------------------|
| PREPARED BY: MD  | DRAWN BY: MD | PAPER SIZE: ARCH D |
| APPROVED BY: CKA | DATE: 3/9/12 |                    |






Coordinate System:  
 NAD 1983 State Plane New Mexico West FIPS 3003  
 Projection: Transverse Mercator  
 Datum: North American 1983  
 Units: Foot US

- Legend**
- No. 3. Coal Monitoring Well
  - ▲ Fruitland Nested Wells
  - Nested Vibrating Wire Piezometer
  - Coal Seam No. 3 Potentiometric Contours
  - Streams
  - Pictured Cliffs Formation (Kpc)
  - Pinabete SMCR Permit Area
  - Mining Lease Area

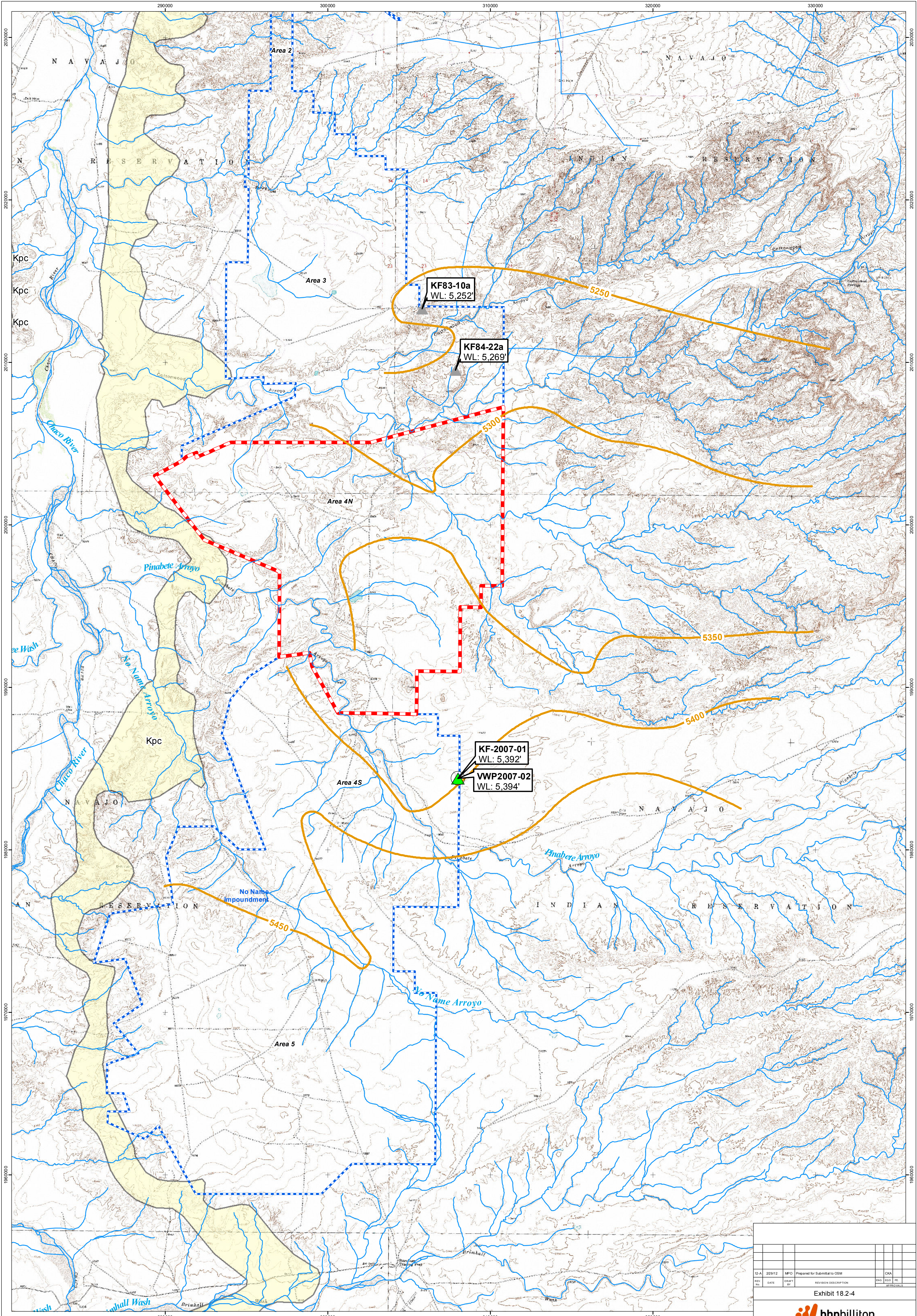
|      |         |          |                                |      |
|------|---------|----------|--------------------------------|------|
| 12-A | 2/29/12 | MPD      | Prepared for Submission to OSM | CKA  |
| REV  | DATE    | DRAWN BY | REVISION DESCRIPTION           | DATE |
|      |         |          |                                |      |

Exhibit 18.2-3

  
 resourcing the future  
**BHP NAVAJO COAL COMPANY**  
 No. 3 Coal Seam Potentiometric Surface

|                  |               |                    |
|------------------|---------------|--------------------|
| PREPARED BY: MD  | DRAWN BY: MPO | PAPER SIZE: ARCH D |
| APPROVED BY: CKA | DATE: 2/12/12 |                    |






Coordinate System:  
 NAD 1983 StatePlane New Mexico West FIPS 3003  
 Projection: Transverse Mercator  
 Datum: North American 1983  
 Units: Feet US

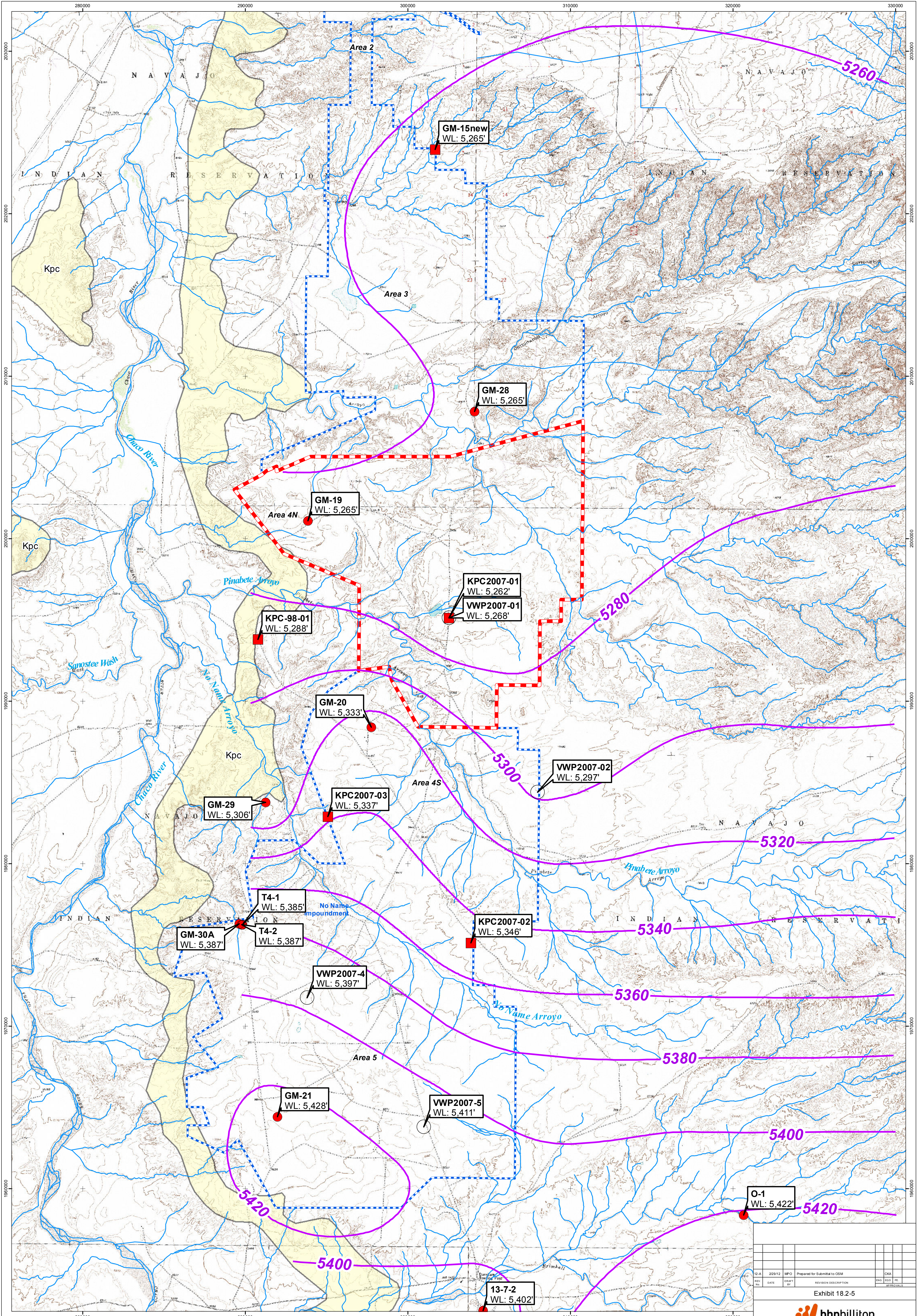
- Legend**
- Well Type, Completion, Status**
- ▲ No. 8. Coal Monitoring Well
  - ▲ Fruitland Nested Well
  - Nested Vibrating Wire Piezometer
  - Coal No. 8 Potentiometric Contours
- Other Features**
- Streams
  - Pictured Cliffs Formation (Kpc)
  - Pinabete SMCRA Permit Area
  - Mining Lease Area

|                |         |          |                                |      |
|----------------|---------|----------|--------------------------------|------|
| 12-A           | 2/29/12 | MPO      | Prepared for Submission to OSM | CKA  |
| REV            | DATE    | DRAWN BY | REVISION DESCRIPTION           | DATE |
| Exhibit 18.2-4 |         |          |                                |      |

  
 resourcing the future  
**BHP NAVAJO COAL COMPANY**  
 No. 8 Coal Seam Potentiometric Surface


|                  |               |                    |
|------------------|---------------|--------------------|
| PREPARED BY: MD  | DRAWN BY: MPO | PAPER SIZE: ARCH D |
| APPROVED BY: CKA | DATE: 2/21/12 |                    |





Coordinate System:  
 NAD 1983 State Plane New Mexico West FIPS 3003  
 Projection: Transverse Mercator  
 Datum: North American 1927  
 Units: Foot US

- Legend**
- Abandoned PCS Monitoring Well
  - Existing PCS Monitoring Well
  - Nested Vibrating Wire Piezometer
  - PCS Potentiometric Contour
  - Streams
  - Pictured Cliffs Formation (Kpc)
  - ▭ Pinabete SM CRA Permit Area
  - ▭ Mining Lease Area

|  |               |                    |                               |         |
|--|---------------|--------------------|-------------------------------|---------|
| 12-A   | 22912         | MPO                | Prepared for Submittal to OSM | CKA     |
| REV  | DATE          | DRAWN BY           | REVISION DESCRIPTION          | CHKD BY |
|  |               |                    |                               |         |
| Exhibit 18.2-5   |               |                    |                               |         |
| <br><b>bhpbilliton</b><br>resourcing the future |               |                    |                               |         |
| <b>BHP NAVAJO COAL COMPANY</b><br>Pictured Cliffs Sandstone (PCS)<br>Potentiometric Elevations                                       |               |                    |                               |         |
| PREPARED BY: MD  | DRAWN BY: MPO | PAPER SIZE: ARCH D |                               |         |
| APPROVED BY: CKA   | DATE: 2/21/12 |                    |                               |         |



## **Appendix 18.A**

Baseline Channel Inventories of Pinabete Arroyo and No Name Arroyo  
from 1998 and 2007 (Edited 2012)

**Appendix 18.A**

**BASELINE CHANNEL INVENTORIES OF PINABETE ARROYO AND NO NAME ARROYO  
FROM 1998 AND 2007 (EDITED 2012)**

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**BASELINE CHANNEL INVENTORIES OF PINABETE ARROYO AND NO NAME ARROYO  
FROM 1998 AND 2007 (EDITED 2012)**

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**BASELINE CHANNEL INVENTORIES OF PINABETE ARROYO AND NO NAME ARROYO  
FROM 1998 AND 2007 (EDITED 2012)**

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**Appendix 18.A**

**BASELINE CHANNEL INVENTORIES OF PINABETE ARROYO AND NO NAME ARROYO  
FROM 1998 AND 2007 (EDITED 2012)**

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## INTRODUCTION

Appendix 18.A includes two channel reconnaissance memos from 1998 and 2007 (edited 2012) on Pinabete and No Name Arroyos, and five exhibits with cross-section and profile information. [Exhibit 18.A-1](#) is the 1998 survey of Pinabete Arroyo with cross-sections at the upstream and downstream monitoring locations and a channel profile which was drawn between the six channel characterization sites' elevation data. The cross-sections shown on [Exhibit 18.A-2](#) documented the 2007 return to the channel characterization sites on Pinabete and re-survey of cross-sections. Two of the Pinabete Arroyo channel characterization sites, Upper Pinabete Station- B (MID) and P-6B (MID), were also resurveyed in 2008 and are presented on [Exhibit 18.A-2](#). [Exhibit 18.A-3](#) is the 1998 survey of No Name Arroyo with cross-sections at the upstream and downstream monitoring locations and a channel profile which was drawn from one mile upstream of the uppermost site, NN-7, to the confluence with the Chaco River, using elevations acquired at the seven channel characterization sites. [Exhibit 18.A-4](#) is a channel profile of lower No Name between channel characterization site NN-3 and the confluence of No Name with the Chaco River developed from aerial survey with ground truth performed to depict topography with and near the channel at a 1-foot contour interval. [Exhibit 18.A-5](#) shows cross-sections developed during the 2007 channel reconnaissance on the No Name stations.

The 1998 channel reconnaissance survey established six stations on Pinabete and seven stations on No Name to assess channel geomorphology conditions. As noted in the section titled "Channel Inventory and Evaluation for No Name Arroyo and Pinabete Arroyo 1998, Edited 2012", the survey consisted of walking one thousand-foot segments of the channel in the vicinity of the stations to generally characterize the channel. The extent of scouring and deposition along the stream, the occurrence of bedrock outcrops, bank stability and vegetative stabilization features were documented. A channel cross section was then chosen which most closely characterized the channel reach. Measurements of channel bottom width, top width and channel depth were made at the cross section using a surveyor's tape and staff gage. The upper and lower sites of each channel became established surface water monitoring locations.

The 2007 Channel Inventory and Evaluation for No Name Arroyo and Pinabete Arroyo were performed to acquire more recent geomorphologic data on Pinabete and No Name Arroyos to reflect pre-mine conditions. The evaluation included a channel stability assessment, a sinuosity evaluation, conceptual classification of bed and bank soils and the subsequent Manning's n values, and a drainage density appraisal. The survey generally returned to the 1998 stations, but many of the original survey posts were not found. A GPS unit was utilized to develop the cross-section information. A new site was established on the lower end of Pinabete (P-6) to better reflect conditions near the northwest lease boundary.

The 1998 profiles and cross sections for Pinabete and No Name ([Exhibit 18.A-1](#) and [Exhibit 18.A-3](#), respectively) include three cross sections at the uppermost and lower most channel geomorphology

stations. The locations of the crest stage gages and single stage sampler were also documented, as these stations became the surface monitoring locations.

The 2007 cross sections for the Pinabete and No Name are presented in [Exhibit 18.A-2](#) and [Exhibit 18.A-5](#), respectively. When cross sectional information for 1998 was available at the station, it was plotted on the cross section. The 1998 data appeared to be between 0.5 and 6 feet lower in elevation than the 2007 data. Rather than interpreting this as an expression of significant aggradation during the 1998-2007 time interval, best characterized as a drought, it is thought that any gross elevation differences are better described as a shift in the original datum. Substantially better channel information was acquired in 2008, when BHP Navajo Coal Company (BNCC) had the lower 4.3 miles of No Name flown for mapping at a 1-foot contour interval. The topographic map showing a 500-foot average coverage on either side of the channel is displayed on [Exhibit 18.A-4](#). A channel profile was developed from this survey which clearly identifies knickpoints at eight locations as the arroyo passes through badland topography. The largest change is seen at 18,450 feet upstream of the confluence, with a 10-foot drop in elevation. A comparison was made between the cross sections surveyed in 2007 and the ones generated by the 1-foot contour map at the Lower No Name monitoring station and NN-3, and the 2008 elevations averaged 3.5 feet higher than the cross-section information developed in 2007. Again, these differences may be the result of differences in the datum used for the surveys. The general shape of the cross sections is very similar, leading us to believe that the surveys were at approximately the same location. However, the difficulty in comparing channel surveys between the two time periods is the result of obtaining consistent information from different groups of surveyors and establishing accurate datum and permanent channel survey monuments in remote locations.

**CHANNEL INVENTORY AND EVALUATION FOR  
NO NAME ARROYO AND PINABETE ARROYO  
1998, EDITED 2012**

**Introduction**

A stream channel inventory and evaluation was conducted to describe the pre-mining conditions for the main channels of Pinabete Arroyo and No Name Arroyo in 1998. The purpose of this work was to document the channel conditions prior to mining, including the presence of bedrock outcrops, and indicators of channel instabilities such as knickpoints, channel cutbanks, and channel scour or deposition. The composition of the channel bed and bank materials, cross section dimensions, and vegetation type and density were also noted. These characteristics provide indications of the capacity of the stream channels to adjust and recover from potential changes due to mining and reclamation. This inventory also included surveys of channel cross sections and slopes and estimation of Manning roughness coefficients at surface water monitoring locations.

**Methods**

A stream channel inventory describes the spatial variability in a stream's characteristics at a specific point in time. Prior to the field visit, main channel profiles were plotted from topographic maps featuring 10-foot contour intervals. Locations of convex segments in the channel profile, channel knickpoints, monitoring station locations, and surface water impoundments were identified on the map. Channel inventory locations were selected to include these channel features. Inventory locations were spaced about every mile through the permit area and at a farther spacing downstream of the permit area. There is no defined channel on No Name Arroyo upstream of the permit area and the inventory did not extend beyond the upstream monitoring station on Pinabete Arroyo.

During the field inventory, a 1,000-foot segment of the channel was walked at each location to roughly characterize the channel. Features including the vegetation conditions on the channel bottom and banks, the occurrence of steep bank slopes and evidence of bank failure, extent of scouring and deposition along the stream, and the occurrence of bedrock outcrops were documented. A channel cross section was then chosen which most closely characterized the channel reach. Measurements of channel bottom width, top width and channel depth were made at the cross section using a surveyor's tape and staff gage. The composition of the channel bottom and bank were field classified in accordance with the Unified Soil Classification (USC) system. Photographs were taken to document channel conditions at each channel inventory location.

At each of the monitoring station locations, channel cross sections, crest stage gages, and single stage sediment samplers were surveyed and estimates of Manning's roughness coefficients were determined

using the procedure for small channels as described in Gray (1970). Using this procedure the value of Manning's roughness coefficient,  $n$ , is estimated from table values for component conditions which affect hydraulic roughness and resistance to flow. These conditions include channel materials, channel vegetation, surface irregularities, variations in channel shape, obstructions, and channel meandering.

The survey of channel cross-sections at the stream monitoring stations was completed on June 2, 1998, before the start of the thunderstorm runoff season, and again on November 30, 1998, at the end of the season. The surveyed sections for both dates are provided in [Exhibit 18.A-1](#) and [Exhibit 18.A-3](#). The channel profiles did not change significantly between the two survey dates but the channel cross sections at the Pinabete Arroyo stations changed due to floods redistributing sediment deposits within the channel. The change in channel cross sections at the No Name Arroyo stations were much less than at the Pinabete station locations.

### **Pinabete Arroyo Inventory**

The main Pinabete Arroyo channel profile shown in [Exhibit 18.A-1](#) exhibits a slightly concave channel profile with channel slopes of 0.55 % or higher at the upstream segment near the eastern permit boundary and decrease to about 0.43 % downstream at the western permit boundary. No knickpoints, or convex segments, are present in the channel profile in the vicinity of the Navajo Mine Extension permit area. Road crossings and monitoring station locations within or near Pinabete Arroyo are also shown on [Exhibit 18.A-1](#). No surface water impoundments are located within the main channel of Pinabete Arroyo within the permit area.

The inventory of channel conditions was conducted at six cross section locations along the main stem of Pinabete Arroyo within or near the permit area. The inventory is presented below. The location descriptions begin with the upstream location and proceed downstream at distances measured along the channel. The cross section locations are shown on [Exhibit 18.A-2](#).

#### *Location P1*

This location is at the upstream monitoring station of Pinabete Arroyo. The channel at this location is incised with a trapezoidal shape featuring a bottom width of 24.5 feet, a top width of 42.5 feet, and a depth of 3 feet. Channel bottom materials are sands (SP) with pebbles and stones. Channel banks consist of medium sand (SP) with semi-consolidated sands and gravels that form steep near vertical banks. Bedrock outcrops occur in the channel banks upstream of location P1. Sandstone slabs and fragments have sloughed into the channel from the erosion of the embankments on meander bends as shown in Figure 18.A-1. No vegetation is found on the channel bottom and sparse shrubs grass and tamarisk occur on the channel banks and sand bars as shown in Figure 18.A-2. The channel appears to be in a state of dynamic equilibrium along this reach. The erosion of the channel banks on meander bends is compensated by sand deposition

on the inside of the meanders. The channel slope at this location is about 0.56% and the valley slope about 0.8%.

The value of Manning's roughness coefficient,  $n$ , was estimated to be 0.032 using the procedure for small channels described in Gray (1970). The estimated contribution to roughness from component conditions includes:

|                                |       |
|--------------------------------|-------|
| Channel materials,             | 0.022 |
| Channel vegetation, negligible | 0.000 |
| Surface irregularities,        | 0.005 |
| Variations in channel section, | 0.005 |
| Obstructions, and meandering,  | 0.000 |



Figure 18.A-1 Pinabete Arroyo upstream of location P1, looking upstream





Figure 18.A-2 Pinabete Arroyo location P1, looking downstream

*Location P2*

This location is approximately 7,700 feet down the channel from location P1. The channel at this location is trapezoidal but wider and shallower than P1 with a bottom width of 40 feet, a top width of 58 feet, and a depth of about 2.1 feet. The channel bottom is comprised of fine sand (SP) with sparse coal and rock fragments. The channel banks consist of sand with negligible fines (SW). Salt deposits occur on bed and bank materials due to evaporation of ground water seepage as shown in Figure 18.A-3. The rate of seepage is insufficient to cause surface flow. The No. 8 coal seam outcrop occurs near this cross section location as shown in Figure 18.A-4 and may be the source of seepage. No vegetation occurs on the channel bottom. Dense shrubs and forbs occur on the channel banks and overbanks. The channel slope at this location is about 0.51% and the valley slope about 0.6%.



Figure 18.A-3 Pinabete Arroyo location P2, looking upstream



Figure 18.A-4 Coal outcrop on channel bank at Pinabete Arroyo location P2

*Location P3*

This location is approximately 5,530 feet down channel from location P2. This location is on a meander bend immediately upstream of the Burnham Road crossing as shown in Figure 18.A-5. The channel at this location is approximately trapezoidal with a 48-foot wide sand bar and the inside of the meander bend. The



bottom width is 24 feet and top width, excluding the sand bar, is 40 feet. The channel is about 2.8 feet deep. The channel bottom and sand bar are comprised of sand with gravel (SW), with a greater gravel fraction on the sand bar. The channel banks are comprised of sand with a higher fine fraction (SP) and are cohesive enough to form steep banks in places. The channel banks are sparsely vegetated and the sand bar and channel bottom are devoid of vegetation as shown in Figure 18.A-5. Shrubs occur on the overbanks. The channel slope at this location is about 0.51% and the valley slope about 0.7%



Figure 18.A-5 Pinabete Arroyo location P3, looking upstream

*Location P4*

This location is at the road crossing to the dug alluvial well and monitoring well PA-1 and is approximately 5,750 feet down the channel from location P3. The channel at this location exhibits considerable meandering with bedrock outcrops common on the outside of meander bends. The channel at this location is approximately trapezoidal with a bottom width of 54 feet and top width of 65 feet. The channel is about 2.0 feet deep. The channel bed and banks are comprised of medium to coarse sand (SW), with a higher gravel fraction on the sand bars located on the inside of meander bends. The channel banks and overbanks are vegetated with grasses and shrubs while channel bottom is devoid of vegetation as shown in Figure 18.A-6. The channel slope at this location is about 0.51% and the valley slope about 0.9%



Figure 18.A-6 Pinabete Arroyo location P4, looking upstream

*Location P5*

This location is approximately 6,600 feet down the channel from location P4. The channel at this location exhibits considerable meandering with steep cutbanks on the outside of meander bends. The channel at this location is slightly narrower than at location P4 with a bottom width of 33 feet. The channel is about 3.0 feet deep. The channel bends and banks on the inside of meander beds are comprised of medium sand (SW) with pebbles. The channel banks on the outside of meander bends are comprised of cohesive sand with fines (SP). The channel banks and overbanks are vegetated with grasses and shrubs while channel bottom is devoid of vegetation as shown in Figure 18.A-7. The channel slope at this location is about 0.51% and the valley slope about 1.2%.



Figure 18.A-7 Pinabete Arroyo location P5, looking downstream

*Location P6*

Location P6 is approximately 16,600 feet downstream of location P5. This location is downstream of the western permit boundary and includes stage crest gages and single stage samplers for the Lower Pinabete Arroyo surface water monitoring station. The channel is approximately trapezoidal in shape with a top width of approximately 115 feet, a bottom width of about 70 to 80 feet, and a channel depth of 4 feet. Channel cross sections associated with the crest stage gages are included on [Exhibit 18.A-1](#). Bottom sediments consist of sand with sparse gravel and rock fragments (SW). Channel banks are sand (SW). A sandstone outcrop occurs on the south bank of the location as shown in Figure 18.A-8. There is no vegetation on the channel bottom and the channel banks are steep with sparse shrub cover. The overbanks have a variable cover of grasses and shrubs. The channel slope at this location is about 0.33 % and the valley slope is about 0.6%.

Manning roughness coefficient for the channel is estimated to be 0.032 using the procedure for small channels described in Gray (1970). The estimated contribution to roughness from component conditions includes:

|                                |       |
|--------------------------------|-------|
| Channel materials,             | 0.022 |
| Channel vegetation, negligible | 0.000 |
| Surface irregularities,        | 0.005 |
| Variations in channel section, | 0.005 |
| Obstructions, and meandering,  | 0.000 |





Figure 18-A.8 Pinabete Arroyo location P6, looking upstream

### **No Name Arroyo Inventory**

An inventory of channel conditions was conducted at nine locations along the main stem of No Name Arroyo within the permit area. The inventory location descriptions begin with the No Name Arroyo downstream monitoring station location (NN-1) and proceed up the channel to the No Name Arroyo upstream monitoring station location (NN-7) ([Exhibit 18.A-3](#)). The No Name surface water impoundment is located on the channel just upstream of location NN-4 at the Burnham road crossing as shown on [Exhibit 18.A-3](#). The water quality monitoring station locations within No Name Arroyo are also shown on [Exhibit 18.A-3](#). The main No Name Arroyo channel profile is shown in [Exhibit 18.A-3](#). Knickpoints are present in the channel profile near inventory locations NN-2 and NN-4 as shown on [Exhibit 18.A-3](#). A small knickpoint also occurs at the bedrock outcrop below location NN-1, although this does not show up on the longitudinal profile.

### *Location NN-1*

This location is at the No Name Arroyo downstream monitoring station which is downstream of the western permit boundary. The channel is incised and is approximately trapezoidal in shape with a bottom width of 12 to 15 feet, a top width of 35 to 50 feet and a depth of about 8 feet. Bottom materials are medium to coarse sand with rock fragments (SW). Bank materials are comprised of cohesive silt (MH). No vegetation is found on the channel bottom although the channel is at times partially filled with tumbleweeds as shown in Figure 18-A.9. Shrubs, grass and forbs occur on the channel overbank while the

channel banks are steep and support sparse vegetation. Sandstone bedrock outcrops in the channel just below the monitoring station as shown in Figure 18.A-9. The channel slope at this location is about 1.4% and the valley slope about 1.4%. Manning roughness coefficient for the channel is estimated to be about 0.037 using the procedure for small channels described in Gray (1970). The estimated contribution to roughness from component conditions includes:

|                                |       |
|--------------------------------|-------|
| Channel materials,             | 0.022 |
| Channel vegetation, low        | 0.000 |
| Surface irregularities,        | 0.010 |
| Variations in channel section, | 0.005 |
| Obstructions, and meandering,  | 0.000 |



Figure 18.A-9 No Name Arroyo location NN-1, looking upstream

*Location NN-2*

This location is immediately above a 15-foot head cut on No Name Arroyo approximately 3,000 feet upstream of the location NN-1. The channel upstream of the head cut is approximately parabolic in shape

with a bottom width of about feet, a top width 15 feet, and a depth of about 1 to 1.5 feet. Channel bed and bank materials are comprised cohesive silts (MH) with dense shrubs and grass as shown in Figure 18-A.10. A relatively broad, well-vegetated floodplain occurs on either side of the channel. Downstream of the head cut, the channel is deeply incised with near vertical banks that slough readily as seen in Figure 18-A.11. Bank materials are cohesive silts (MH). The channel bottom and banks are devoid of vegetation and the channel is partially filled with tumbleweeds as shown in Figure 18.A-11. The channel slope at this location is about 0.71% and the valley slope about 1.3%.



Figure 18.A-10 No Name Arroyo location NN-2, looking upstream





Figure 18.A-11 Headcut below No Name Arroyo Location NN-2, looking downstream

*Location NN-3*

This location is approximately 3,100 feet upstream of the No Name Arroyo location NN-2. The channel is approximately trapezoidal in shape with a bottom width of 5 feet, a top width of approximately 20 feet, and a depth of about 5 feet. The channel bed is composed of medium sand with fine gravel and rock fragments (SP). The channel banks are composed of cohesive silty sand (SM). No vegetation is found on channel bottom but shrubs and grasses are abundant on the channel banks and overbanks as shown in Figure 18-A.12. The channel was partially filled with tumbleweeds as shown in Figure 18.A-12. The channel slope and valley slope at this location are both approximately 0.72%.



Figure 18.A-12 No Name Arroyo location NN-3, looking upstream

*Location NN-4*

This location is immediately below the No Name impoundment approximately 3,350 feet upstream of the No Name Arroyo location NN-3. A channel section was not measured at this location because of the significant variation in channel conditions. The spillway overflow from the impoundment crosses the Burnham road on the south side and flows down a bedrock lined channel to the valley floor below the impoundment as shown in Figure 18-A.13. A very dense growth of shrubs and tamarisk is present in the valley below the impoundment with channel headcuts occurring at a number of places within the valley floor as shown in Figure 18.A-14. The valley floor soils consist of silt and very fine sand (MH). The valley slope just below the No Name impoundment is about 1.0%.





Figure 18.A-13 Spillway channel below No Name Impoundment, location NN-4, looking upstream



Figure 18.A-14 No Name Arroyo location NN-4, looking upstream

*Location NN-5*

This location is upstream of the No Name Impoundment and approximately 3,300 feet upstream of location NN-4. The channel is incised 2 to 3 feet and is irregular in shape with several channels terminating in headcuts upstream of NN-5. Channel top widths vary from several feet to approximately 20 feet on the main channel below location NN-5. No distinct channel occurs in the valley bottom for a distance of about 1,000 feet upstream of the headcuts. Channel bed and bank materials consist of cohesive silt and fine sand



(MH). No vegetation is found on the near vertical banks where they occur but dense shrubs and grasses are abundant on the overbank but less dense on the channel bottom. The dimensions of the channel section were not measured at this location because of the widely varying sections. Tumbleweeds were found at numerous places within the channel as shown in Figure 18.A-15. The valley and channel slope at this location are about 0.78%.



Figure 18.A-15 No Name Arroyo location NN-5, looking downstream

*Location NN-6*

This location is approximately 5,060 feet upstream of the location NN-5. The channel is incised about 2 feet and is irregular in shape as shown in Figure 18-A.16. Small channel headcuts and soil pipes were common around location NN-6. The channel above and below this location occurs intermittently within the valley bottom and is typically associated with channel incision with headcuts and soil pipes. Channel bed and bank materials consist of cohesive silts (MH). Vegetation in these areas is sparse due to the presence of limiting soil conditions. The density of vegetation is greatest in minor depressions where water and windblown soils accumulate but channel erosion or scouring does not occur. A channel section was not measured at this location because of the widely varying sections. Tumbleweeds were found at



numerous places within the channel as shown in Figure 18.A-16. The channel and valley slope at this location is about 0.82%.



Figure 18.A-16 No Name location NN-6, looking upstream

*Location NN-7*

This location is at the upstream monitoring station on No Name Arroyo located just west of the eastern lease boundary approximately 400 feet upstream of location NN-6. The surface water monitoring station includes one stage crest gage and one single stage sampler. The channel is approximately parabolic in shape with a top width of less than 6 feet and a depth of less than 1 foot and but varies along the channel. The channel does not extend upstream of this location and occurs intermittently downstream. Channel rills are found within the broad flat valley of No Name Arroyo both upstream and downstream of the eastern lease boundary. Channel cross-sections associated with the stage crest gage and sediment sampler are included on [Exhibit 18.A-3](#). Channel bed sediments at this location are fine sands (SM). Channel banks are comprised of cohesive silty sand (ML). Vegetation occurs on the channel bank and overbank but is very sparse on the channel bed as shown in Figure 18.A-17. The channel and valley slope at this location are about 0.82%. The Manning roughness coefficient for the channel is estimated to be about 0.055 using the procedure for small channels described in Gray (1970). The estimated contribution to roughness from component conditions includes:

|                              |       |
|------------------------------|-------|
| Channel materials,           | 0.020 |
| Channel vegetation, moderate | 0.010 |



|                                |       |
|--------------------------------|-------|
| Surface irregularities,        | 0.010 |
| Variations in channel section, | 0.015 |
| Obstructions, and meandering,  | 0.000 |



Figure 18.A-17 No Name Arroyo location NN-7, looking downstream

**References**

Gray, D.M. 1970. Handbook on the Principles of Hydrology. Water Information Center, Inc.



**CHANNEL INVENTORY AND EVALUATION FOR  
NO NAME ARROYO AND PINABETE ARROYO  
2007, EDITED 2012**

**Introduction**

From August 27 to August 29, 2007, two URS teams independently conducted a baseline channel inventory survey and a drainage density survey on the Pinabete and No Name Arroyos within Area IV South and Area V. The Pinabete Arroyo is the main drainage path for Area IV South, bisecting the lease by flowing from the southeast corner to the northwest corner. The No Name Arroyo is the main drainage path for Area V, and flows from east to west along its northern boundary, just south of Area IV South. The Pinabete Arroyo is proposed to be diverted into the No Name Arroyo during the mining operation of Area IV South. [Exhibit 18.A-6](#) is a map of the study area.

The baseline channel inventory was performed by the team of Bud Brock and Samrat Mohanty as part of the effort to obtain hydrologic information necessary for evaluation of Probable Hydrologic Consequences (PHC) of the previously proposed mining operations in Area IV South. The drainage density survey was completed by the team of Briana Gunn and Bill Sabatka to estimate input parameters for the development of the Approximate Original Contours (AOC) for Area IV South.

**Baseline Channel Inventory**

The specific objectives of the Baseline Channel Inventory effort are:

- Perform reconnaissance of Pinabete Arroyo and No Name Arroyo, including their major tributaries and associated floodplains to describe pre-mining conditions.
- Evaluate channel stability for both the major arroyos.
- Estimate channel characteristics, such as sinuosity and Manning's n values, for use in later modeling efforts.
- Perform limited conceptual classification of bed and bank soils.

**Field Reconnaissance Methodology**

The URS team performed reconnaissance of the Pinabete Arroyo between the Upper Pinabete Monitoring Station, P-1, and Lower Pinabete Monitoring Station, P-6, and of the No Name Arroyo between Upper No Name Monitoring Station, NN-7, and Lower No Name Monitoring Station, NN-1, as well as their major tributaries and floodplains.

Key channel features identified included road crossings, culverts, dams, tributary junctions, bedrock outcrops, head cuts, bend points, and locations of convex segments within the channel flow path. The conditions of the channels along each course were described, including vegetative conditions in the channel



and on the overbanks, the occurrence of steep bank slopes, evidence of bank failure, extent of scouring and deposition along the stream, and the classification of stream bed sediments. Photographs of the channel conditions were taken as part of the channel baseline survey for future reference during the Surface Water PHC project. A representative sample of the photos is presented in the text.

Limited soil classifications were performed on the channel bed and bank soils. Physical characteristics such as gradation, texture, moisture, plasticity, and density were noted for soils at selected locations. Locations were chosen based on their proximity to the monitoring stations, survey cross-sections, and any location with a perceived change in soil type.

*Observations on No Name Arroyo*

The No Name Arroyo is a fairly “young” arroyo, currently undergoing significant evolution. Overall, the No Name Arroyo is fairly straight for the reach located within the BNCC mining lease and flows in a general northwesterly direction. There are numerous small bends and turns in the channel, but they are minor and have little effect on the overall direction of the stream. The exception is the last major bend in the channel, approximately 900 feet upstream of NN-2. At this location, the channel takes a bend of approximately 30-degrees to the north. From here the channel continues on a north-by-northwesterly direction until the confluence point with Chaco River.

The stream characteristics for No Name Arroyo can be divided into two distinct sections, upstream (east) of Burnham Road and downstream (west) of Burnham Road. For the majority of the stream reach upstream of the Burnham Road, there is a narrow, shallow, and discontinuous low flow channel with the capacity to convey runoff from the frequent storm events (1 to 5 year storm events). The low flow channel varies from 1 to 4 feet in dept and 2 to 10 feet in width. Bends in the channel are up to, and in a few locations exceed, 90-degrees. Flows resultant from the larger storm events overtop the low flow channel and are conveyed in a wide “U” shaped shallow concentrated flow area. The shallow concentrated flow area ranges from approximately 50 to 100 feet wide, with some locations approaching 200 feet. The soil has minimal alluvial deposits consisting primarily of a clayey loam. Vegetation in the shallow concentrated flow area consists of low to medium grass with scattered low to medium brush for an effective ground cover of 60% to 80%. The Manning’s n value for the channel is estimated to be 0.04. The two areas where the channel does not conform to these general statements are described below.





Figure 18.A-18 No Name Arroyo low flow channel upstream of Burnham Road

The area from NN-7 to approximately 500 feet downstream, the channel is incised at a depth of 2 to 4 feet and a width of 10 to 20 feet and has significant braiding. With the exception of the rare major storm events, flow is confined to the channel. The vegetation in the channel is consistent with the downstream section; however, the effective ground cover is approximately 50% in the channel resulting in an estimated Manning's  $n$  value of 0.035.



Figure 18.A-19 No Name Arroyo shallow concentrated flow area upstream of Burnham Road



Immediately upstream of Burnham Road is the other location where the No Name Arroyo characteristics deviate from the typical channel section described above. Burnham Road acts as a retention structure creating a ponding area on the upstream side of the road. No crossing culverts were found. The gradient of the road slopes downward from north to south with a small dip in the road just south of the effective ponding area before the gradient of the road starts in an upward slope. This dip in the road acts as an overflow location for the ponding area and corresponds to a sandstone outcrop that limits the erosion of the roadway. The ponding area has an effective ponding depth of approximately 4 to 6 feet before flow will inundate the overflow location. It is assumed this ponding area was intentionally created to serve as a cattle watering pond. The bottom of ponding area is covered with clayey soil. There is little to no vegetation in the bottom of the ponding area; however, heavy brush is present on the upstream half of the pond overbanks. This heavy brush extends into and up the channel feeding the pond for approximately 500 feet creating an effective ground cover of almost 100% resulting in an estimated Manning's n value for this part of the channel of 0.15.



Figure 18.A-20 No Name Arroyo upstream of NN-7





Figure 18.A-21 No Name Arroyo ponding area upstream of Burnham Road looking upstream

Vegetation in the overbank area is fairly consistent along the stream reach and is composed primarily of low grass with interspersed low brush covering approximately 5% to 30% of the ground. The soil in the overbank area is fairly consistent with that in the channel, with the exception of the presence of more gravel. There are few medium to large size rocks in the channel or overbank area. The Manning's  $n$  value is estimated to be approximately 0.035 for the overbank area.

The overbank areas consist of a gently sloping floodplain area leading to widely spaced rolling hills. The hills range up to approximately 100 feet high and are composed primarily of fractured sandstone gravel intermixed with loose soils. Tributaries in the area are typically shallow concentrated or sheet flow with only a few of the tributaries having incising at the main channel with a head cut depth of 1 to 3 feet. Upstream of the tributary head cut, the flow regime consists of shallow concentrated and sheet flow.

For the majority of the stream reach downstream of Burnham Road, the channel is well defined with incised depths up to 15 feet, steep to vertical side slopes, and bends ranging from 10 to 45-degrees. The soils in the channel banks are collapsible clayey silt. There is a significant amount of fractured sandstone in the bottom of the channel that has washed into the arroyo from the outcroppings to the north or from discrete outcroppings in the channel banks. There are a few scattered locations where fractured sandstone outcroppings are present in the channel banks, almost always on the north side. Sandstone outcroppings were noted in the channel bottom at two locations, approximately 200 feet upstream of NN-2 and approximately 1,500 feet downstream of NN-4. Vegetation in the overbank area is fairly consistent along the stream reach and is composed primarily of low grass with interspersed low brush covering



approximately 5% to 30% of the ground surface. The soil in the overbank area is fairly consistent with that in the channel, with the exception of the presence of more gravel. There are few medium to large size rocks in the channel and overbank areas. The Manning's n value is estimated to be approximately 0.035 for this overbank area. Vegetation and Manning's n values in the channel varies from upstream to downstream and are discussed per section below.



Figure 18.A-22 No Name Arroyo sandstone outcropping upstream of NN-2

Immediately downstream of Burnham Road, the channel is difficult to discern due to the thick vegetation consisting of dense salt cedar, brush, and grass constituting an effective ground cover of approximately 100%. Approximately 500 feet downstream of Burnham Road, the channel flairs out and becomes visible. The channel cross section in this area displays a benched condition. From the channel bank, it drops approximately 8 to 15 feet where it hits a small bench, roughly 5 feet wide. It then drops another 2 to 5 feet to the low flow portion of the channel, which is generally 2 to 5 feet wide. Overall, the channel width varies from approximately 15 to 40 feet wide. This general channel configuration continues downstream for approximately 500 feet to near the location of NN-4. The channel is fairly straight in the area with bends not exceeding 10 to 20 degrees. Due to the thick vegetation, the Manning's n for this portion of the channel is estimated to be 0.15.

From NN-4 to downstream approximately 1,000 feet, the channel is 10 to 12 feet deep and 10 to 20 feet wide. Vegetation in the channel is very thick constituting a ground cover of approximately 80%. Bends are more pronounced and frequent but do not exceed approximately 45 degrees. Due to the thick vegetation, the Manning's n value for this portion of the channel is estimated to be 0.10.





Figure 18.A-23 No Name Arroyo at approximately NN-4

From approximately 1,000 feet downstream of NN-4 to approximately 500 feet downstream of NN-3, the channel is 8 to 10 feet deep and 10 to 20 feet wide. Vegetation in the channel still consists of salt cedar, brush, and low to medium grasses, but the density has decreased to an effective ground cover of approximately 50%. Bends are still fairly frequent but do not exceed approximately 45 degrees. The Manning's n value for this portion of the channel is estimated to be 0.05.

At approximately 500 feet downstream of NN-3, the channel dissipates over the course of approximately 200 feet as it exits a tight meander. The flow regime reverts to shallow concentrated and overland flow for a stretch of approximately 2,000 feet. Where a defined channel exists for this stretch of the arroyo, it is heavily braided, no more than 3 feet deep, and in excess of 30 feet wide. There are stretches where a definitive channel is not present and runoff reverts to sheet flow conditions. Vegetation in the channel and overland flow area is thicker than the downstream channel reaches, consisting of low to medium grasses and weeds, brush, and some salt cedar constituting a ground cover of approximately 50%. The Manning's n value for this portion of the channel is estimated to be 0.04. The overland flow terminates at a major head cut in the channel located approximately 1,000 feet upstream of NN-2. The head cut is approximately 30 feet wide and 12 feet deep. Downstream of the head cut, there is a definable channel as described in the following paragraph.

From the head cut to NN-2, braiding is frequent and the side slopes are vertical. The channel is approximately 8 to 12 feet deep and approximately 10 to 30 feet wide. The top edge of the channel banks tend to be sharp, indicating the channel is relatively new. Bends are fairly minor and range from less than



10 degrees to a maximum of 45 degrees. Vegetation in the channel consists primarily of low grass with some salt cedar and low brush constituting a ground cover of approximately 30%. The Manning's n value for this portion of the channel is estimated to be 0.03.



Figure 18.A-24 No Name Arroyo headcut approximately 1,000 feet upstream of NN-2



Figure 18.A-25 No Name Arroyo from NN-2 to NN-1

From NN-2 to NN-1, the channel banks are vertical or nearly vertical in most locations. In the locations where the channel banks are not vertical, they range to a side slope of approximately 3h:1v. The top edge



of the channel banks have been rounded over by erosion, indicating the incision has been in place for a few years. There is little to no braiding in the channel. Channel depths, widths, vegetative cover, Manning's n value, and bends are consistent with the preceding section.

The overbank areas consist of a gently sloping floodplain area with a varied width from 50 to 200 feet leading to a fairly dense clustering of steep hills. The hills are generally up to approximately 100 feet high and are composed primarily of fractured sandstone overlain by loose soils. The majority of the hills have at least one side consisting of a vertical face of fractured sandstone. Tributaries in the area are typically incised at the main channel and upstream for up to 200 feet with a head cut depth of 2 to 5 feet. Upstream of the tributary head cut, the flow regime consists of shallow concentrated and sheet flow.

*Observations on Pinabete Arroyo*

The Pinabete Arroyo is a well defined and established channel. The overall trend of the channel is fairly straight through the BNCC mining lease area flowing in a general north by northwesterly direction. Right before the channel exits the mining lease area, there are a series of bends that result in an almost 90 degree change in the overall direction of the channel leaving it flowing in a west-by-northwesterly direction until its confluence with the Chaco River.

The stream characteristics for the Pinabete Arroyo are fairly consistent through the study area. The slope of the channel upstream of the BNCC mining lease boundary is 0.65% and downstream of the lease boundary is 0.31%. Typically, the channel is 4 to 10 feet deep and 20 to 80 feet wide with side slopes in the range of 4h:1v to 10h:1v. At the bend points, the side slopes on the outside of the bend transition to vertical. Vegetation in the channel is almost solely confined to the channel banks and consists of low grass, some small brush, and the occasional salt cedar clump. The soil in the channel is primarily silty sand with very little to no clay content. There are a couple of locations where bedrock is exposed in the channel. These are at Burnham Road and approximately half way between P-1 and P-2. Otherwise, the channel is basically devoid of rock of any size, with the exception of the sandstone outcroppings at the bend points. The estimated Manning's n value for the channel is 0.022.

Although the general trend of the arroyo is fairly straight, the sinuosity of the channel is relatively high. There are numerous bend points with angles greater than 90 degrees, with a large percent of the bends approaching 180 degrees. Typically, between the major bend points the channel is fairly straight or has a gentle meander. There are a few locations on the stream reach where the sinuosity is very high, as one bend ties directly into the next and the bends approach or are in excess of 90 degrees. These areas are from P-1 downstream for 1,500 feet, upstream and downstream of P-3 for approximately 1,500 feet, and a 2,500 stretch of the channel centered approximately half way between P-5 and P-6.





Figure 18.A-26 Pinabete Arroyo typical channel



Figure 18.A-27 Pinabete Arroyo exposed bedrock between P-1 and P-2





Figure 18.A-28 Pinabete Arroyo typical bend point upstream of Burnham Road

Tributaries to the Pinabete Arroyo are typically incised near the confluence point to the main channel. The incising extends up the tributary for no more than approximately 300 feet where it terminates in a small head cut of 2 to 5 feet deep. The overbank area can be divided into two sections, upstream (east) and downstream (west) of Burnham Road. As with the No Name Arroyo, the overbank area upstream of Burnham Road consists primarily of gently rolling hills up to approximately 100 feet high composed primarily of fractured sandstone gravel intermixed with loose soils. The soil in the overbank area is fairly consistent with that in the channel, with the exception of the presence of more gravel. Vegetation is composed primarily of low grass with interspersed low brush covering approximately 5% to 30% of the ground. There are few medium to large size rocks in overbank area. The Manning's n value is estimated to be approximately 0.035 for the overbank area.





Figure 18.A-28 Pinabete Arroyo typical bend point upstream of Burnham Road

Downstream of Burnham Road, the overbank area is also similar to that of the No Name Arroyo. Typically, a gently sloping floodplain area up to 200 feet wide leads to steep hills up to approximately 100 feet high. The hills generally have at least one vertical face of exposed sandstone with the other sides composed of fractured sandstone and soil. The soil in the overbank area is fairly consistent with that in the channel, with the exception of the presence of more gravel. Vegetation is composed primarily of low grass with interspersed low brush covering approximately 5% to 50% of the ground. There are numerous medium to large size rocks in overbank area consisting of sandstone that has eroded off the nearby hills. The Manning's  $n$  value is estimated to be approximately 0.05 for this overbank area.

#### **Drainage Density Survey**

This 3-day effort included field reconnaissance of the Pinabete and No Name Arroyos and their major tributaries, developing drainage density data by measuring tributary lengths and areas, measurement of A-channel lengths, and head to ridge lengths.

Several drainage areas for the Pinabete and No Name Arroyos were identified prior to field survey where drainage parameters could be estimated. These locations were selected based on identified hydrologic features and soil types, as well as recommendations from environmental staff of BNCC. Pinabete Drainage Basins 18 and 21, and No Name Basin 1 were selected for reconnaissance. Drainage basin designations are based on a SedCAD model developed by BNCC, and are shown on [Exhibit 18.A-6](#).





Figure 18.A-29 Pinabete Arroyo near confluence of main tributary channel from Drainage Basin 18

#### Day - 1

The URS team performed an overall reconnaissance of the area was performed by driving through the project area from north to south over the watersheds of both the arroyos. The first basin explored was Drainage Basin 18. This drainage basin is located immediately downstream of Burnham Road and drains to the Pinabete Arroyo directly downstream of cross section P-3. A GPS receiver was used to mark the drainage features of the tributary channels within Drainage Basin 18.

The tributary channels within Drainage Basin 18 are fairly flat and narrow, rectangular in shape, have a bottom width varying from less than 1 foot to over 10 feet, and side slopes from 1h:1v to 3h:1v. The main tributary channel within Drainage Basin 18 extends approximately 5,000 feet to the southwest from the confluence with the Pinabete Arroyo. The total length of all the tributary channels within the Drainage Basin 18 is 18,400 feet. The contributing drainage area is estimated to be 322 acres. The estimated drainage density is 60 feet per acre (ft/acre).





Figure 18.A-30 Main tributary channel from Drainage Basin 18 near confluence with Pinabete Arroyo



Figure 18.A-31 Top segment of Drainage Basin 18 main tributary channel





Figure 18.A-32 Top ridge within Drainage Basin 18 - note increased gravel content

During the field investigation, the team observed that there were very few channels that could be classified as type A or B, with the majority of the channels consistent with type C. For this reason, only a few A-channel lengths were measured within Drainage Basin 18. However, due to the flatness of the area and the small changes in grade between channels, none of the measured head to crest lengths were considered representative of the project area.

The soil within the tributaries is alluvial deposits with very few bedrock outcrops. The channel contains small to large fractured sandstone fragments along the channel bottom, extending into the channel side slopes. The channel bank is unstable, resulting in sustained erosion except for the areas with high rock concentrations.

#### Day - 2

During the second day, Drainage Basin 22 and the north end of Drainage Basin 21 were identified to have distinct ridges and valleys containing concave to convex channels where A-channel lengths could be evaluated, and the overall terrain contained a greater amount of elevation change.

In these areas, the tributary channel lengths were measured and coordinates were recorded along the tributary alignments to estimate elevation change and A-channel lengths. Within these areas a soil type that was slightly different than that within Drainage Basin 18 was identified. The soil type has less alluvial



sands and a greater volume of gravel. These areas have a more stable channel configuration, which is narrower with a reduced amount of riling. The estimated average A-channel length and head to ridge length are approximately 30 feet and 150 feet, respectively; with one outlying head to ridge length of approximately 650 feet.



Figure 18.A-33 Center of tributary channel 18R1 in Drainage Basin 18





Figure 18.A-34 Channel 18 on south bank of Pinabete Arroyo



Figure 18.A-35 Bedrock outcrop within main tributary channel of Drainage Basin 18 after rainfall event



Towards the end of the second day, the southern portion of Pinabete Drainage Basin 21 and No Name Drainage Basin 1 were examined. Both these areas have fairly flat topography with no measurable ridges and valleys, and were therefore not further evaluated.

An attempt was made to identify additional contributing drainage areas in the Pinabete watershed that would be representative of the surface generated by the Natural Regrade model. During this process, Drainage Basin 28 was identified. This basin is approximately 1 mile downstream of Drainage Basin 18.

Day - 3

On the third day, measurements of the lengths of the tributaries within Drainage Basin 28 were conducted. The tributaries within this basin have slopes varying from 2 to 20 percent, which is steeper than tributaries measured in the preceding basins. The tributaries are narrower in comparison to those within Drainage Basin 18. The tributary channels generally have a trapezoidal shape, a bottom width varying from 0.5 to 4 feet, and 1h:1v to 2h:1v side slopes. The main tributary channel extends approximately 1,080 feet to the confluence with the Pinabete Arroyo. The total length of all tributaries within Drainage Basin 28 is 2,350 feet. The contributing drainage area is approximately 16.8 acres. The estimated drainage density is 140 ft/acre.



Figure 18.A-36 Typical upstream channel segment in Drainage Basin 28





Figure 18.A-37 Typical A-channel in Drainage Basin 28



Figure 18.A-38 Typical A-channel in Drainage Basin 18



The majority of the tributaries were found to contain an A-channel reach with a measurable head to ridge length. Measurements were taken along the tributary channels. The estimated average A-channel length and head to ridge length are approximately 20 and 100 feet, respectively.

The soil type within Drainage Basin 28 is similar to Drainage Basin 22 with a lower amount of alluvial deposits and a large amount of gravel. For the majority of the tributaries, gravel is present at the transition between the concave to convex areas. Overall, this basin appears to be more stable than Drainage Basin 18.

GPS data were recorded at the estimated upstream and downstream elevation of the Pinabete Arroyo in the NMEP to be used as input in the Natural Regrade model. The upstream and downstream elevations are estimated to be 5,440 feet and 5,310 feet (Mean Sea Level), respectively.

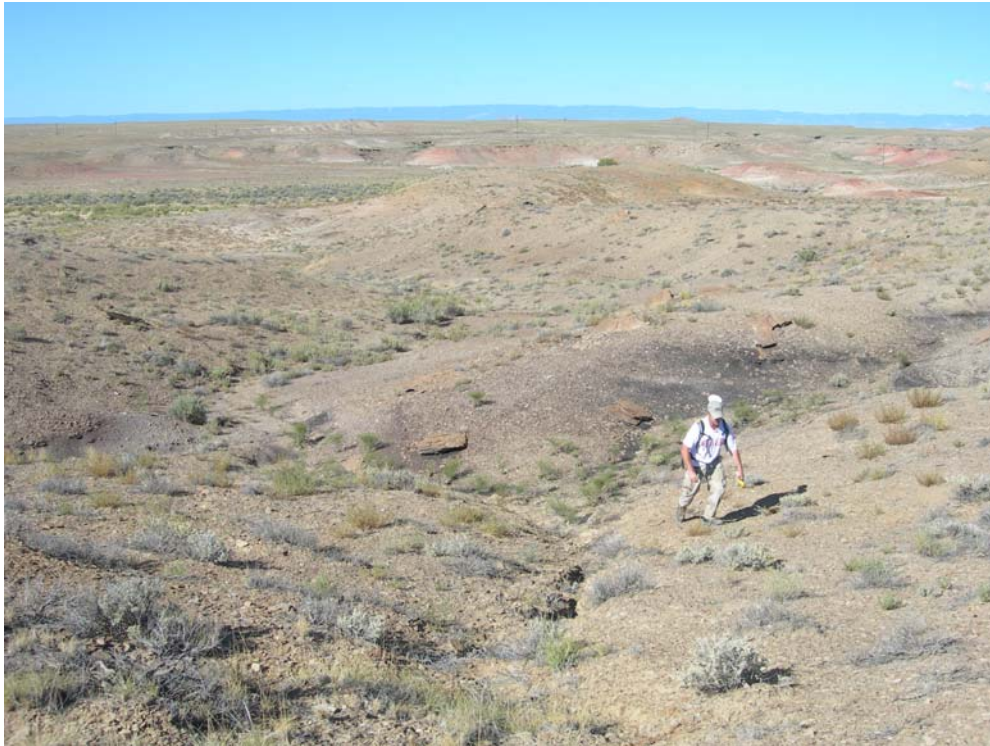


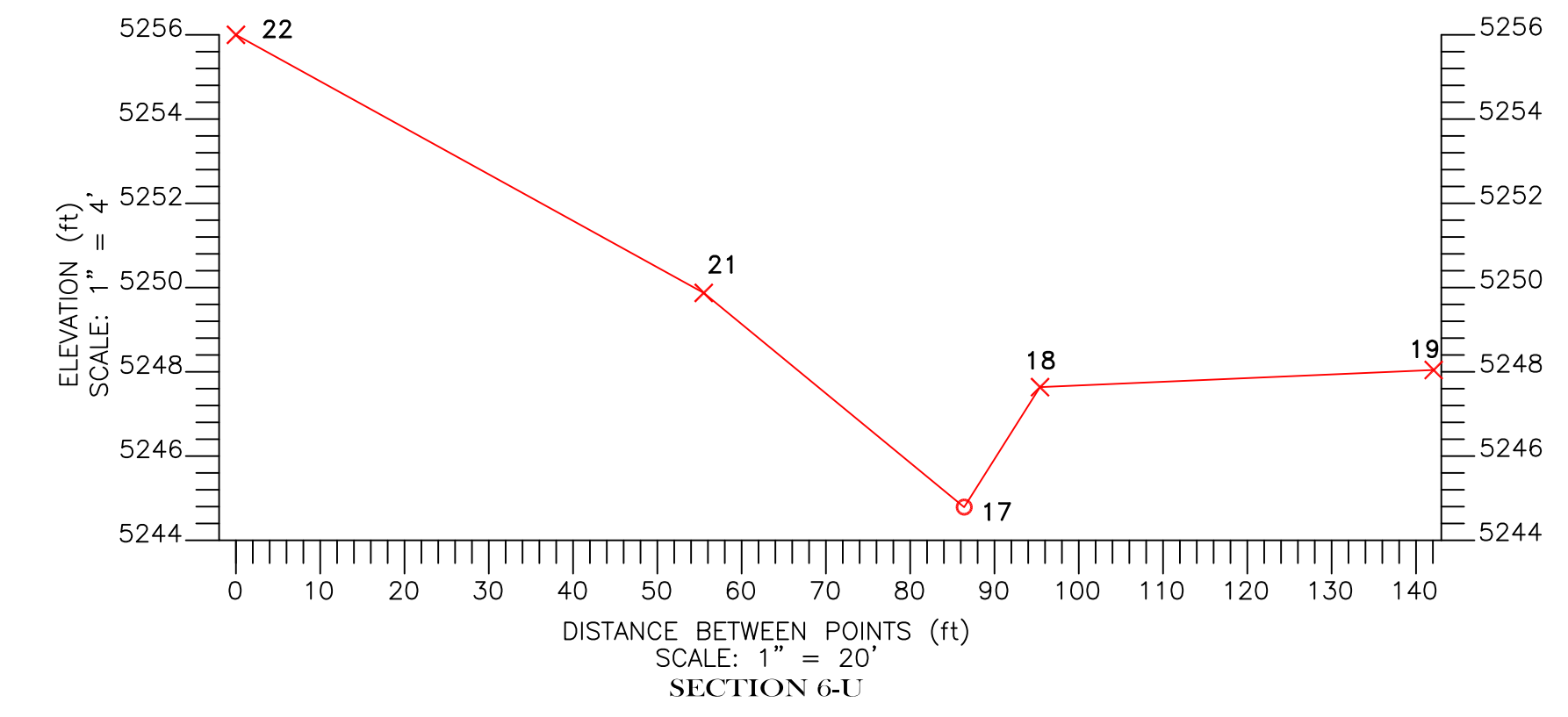
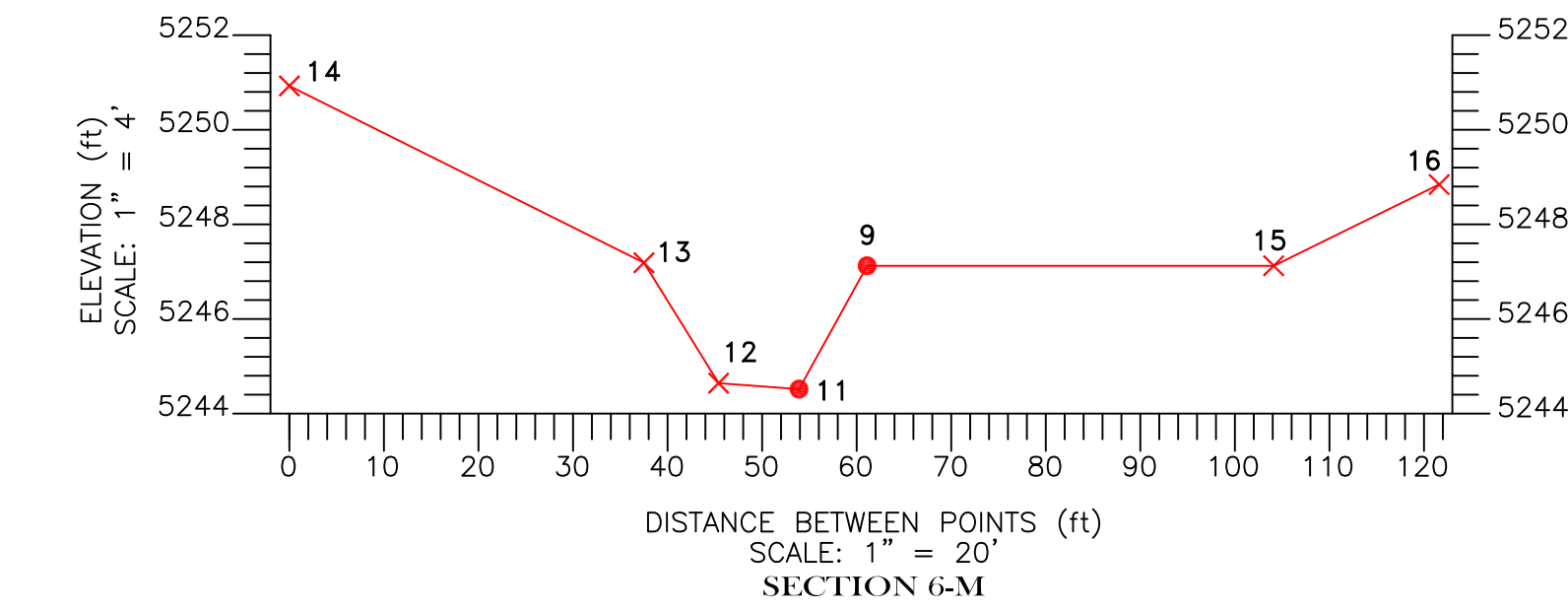
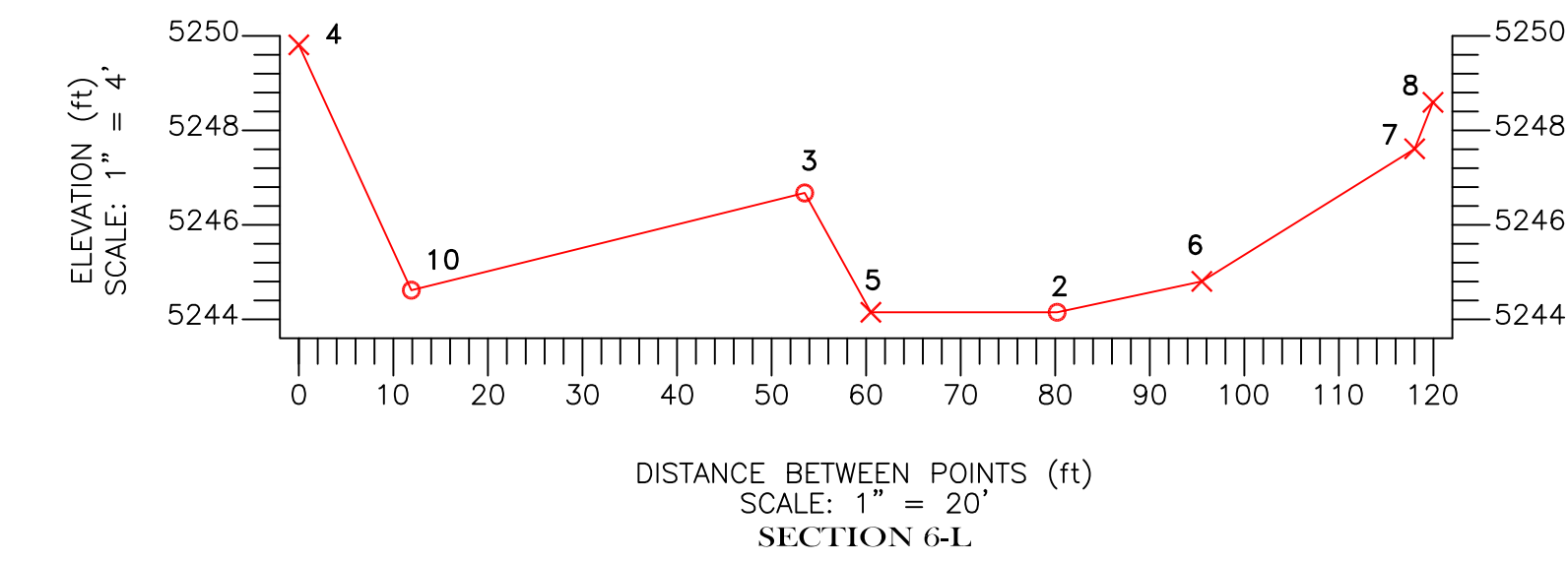
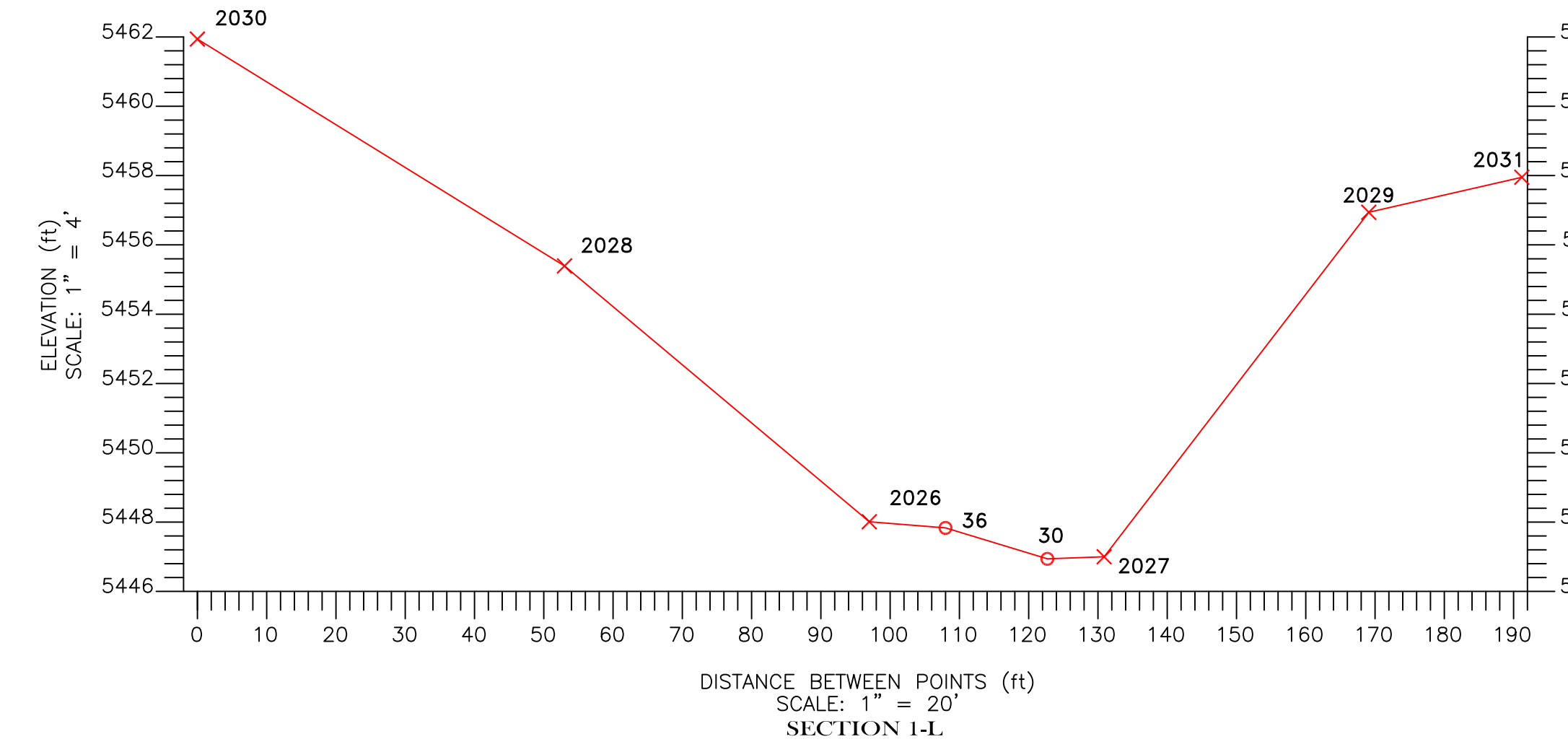
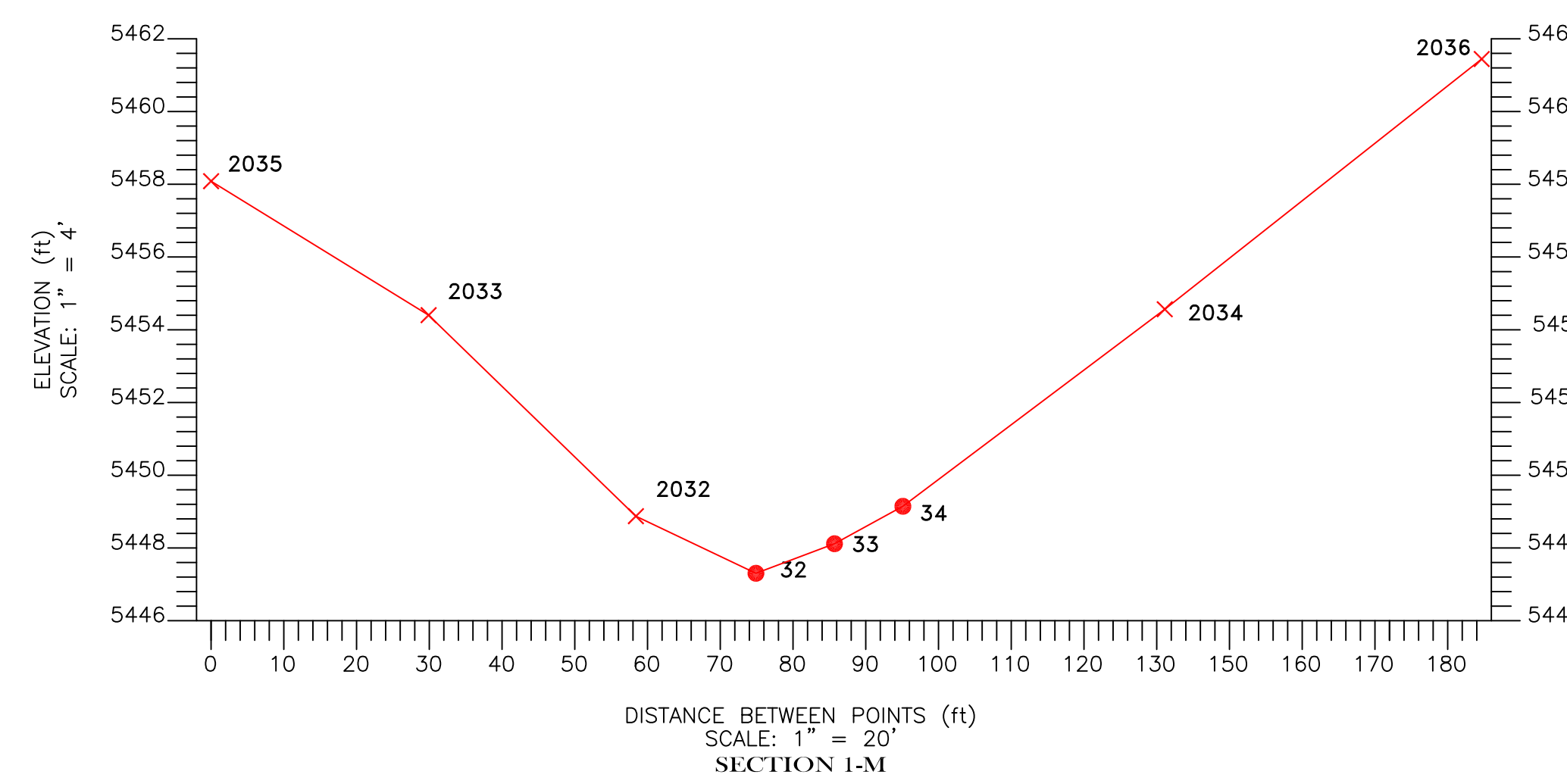
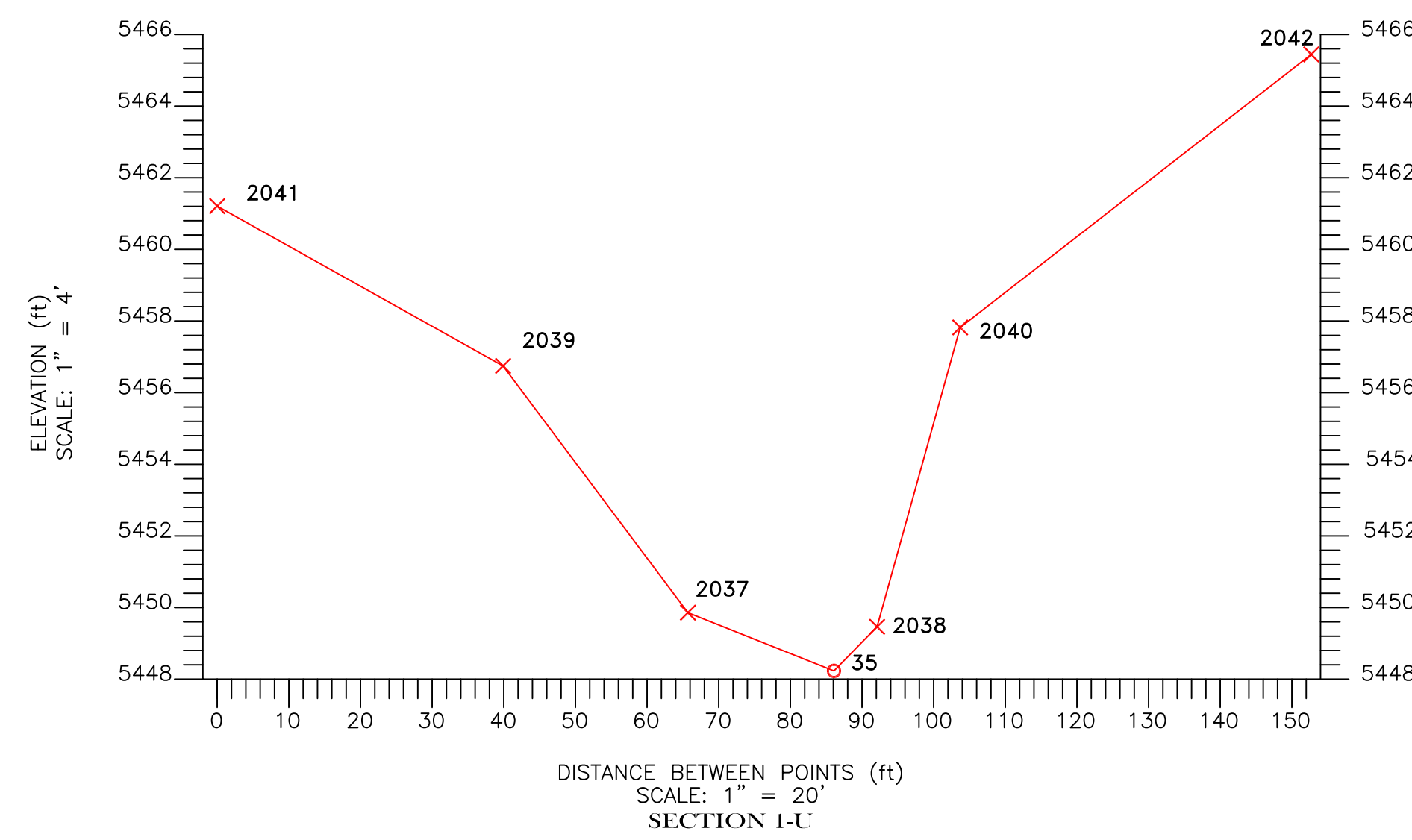
Figure 18.A-39 Typical geomorphologic formations within Drainage Basin 28





Figure 18.A-40 Southern boundary of the permit area looking north

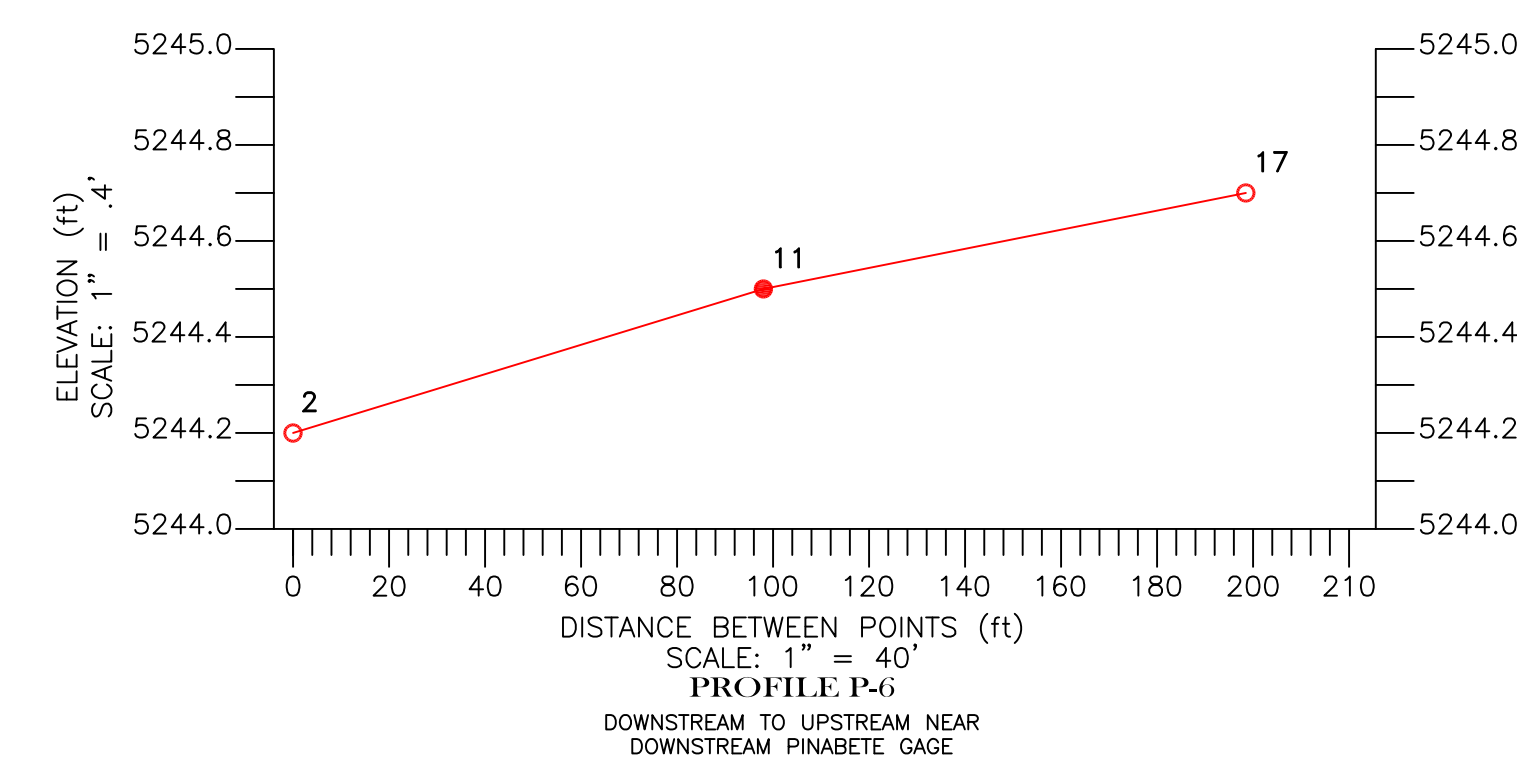
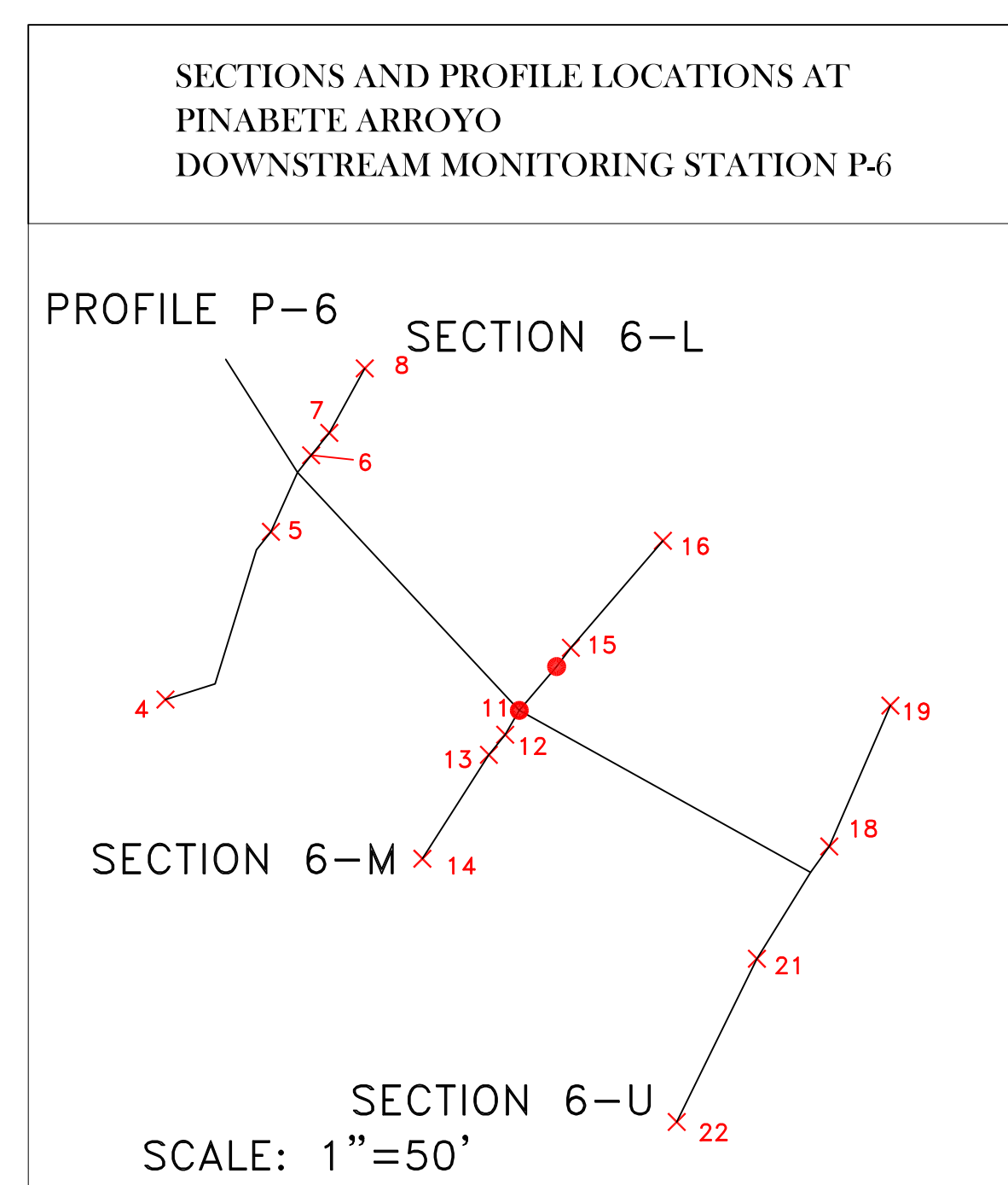
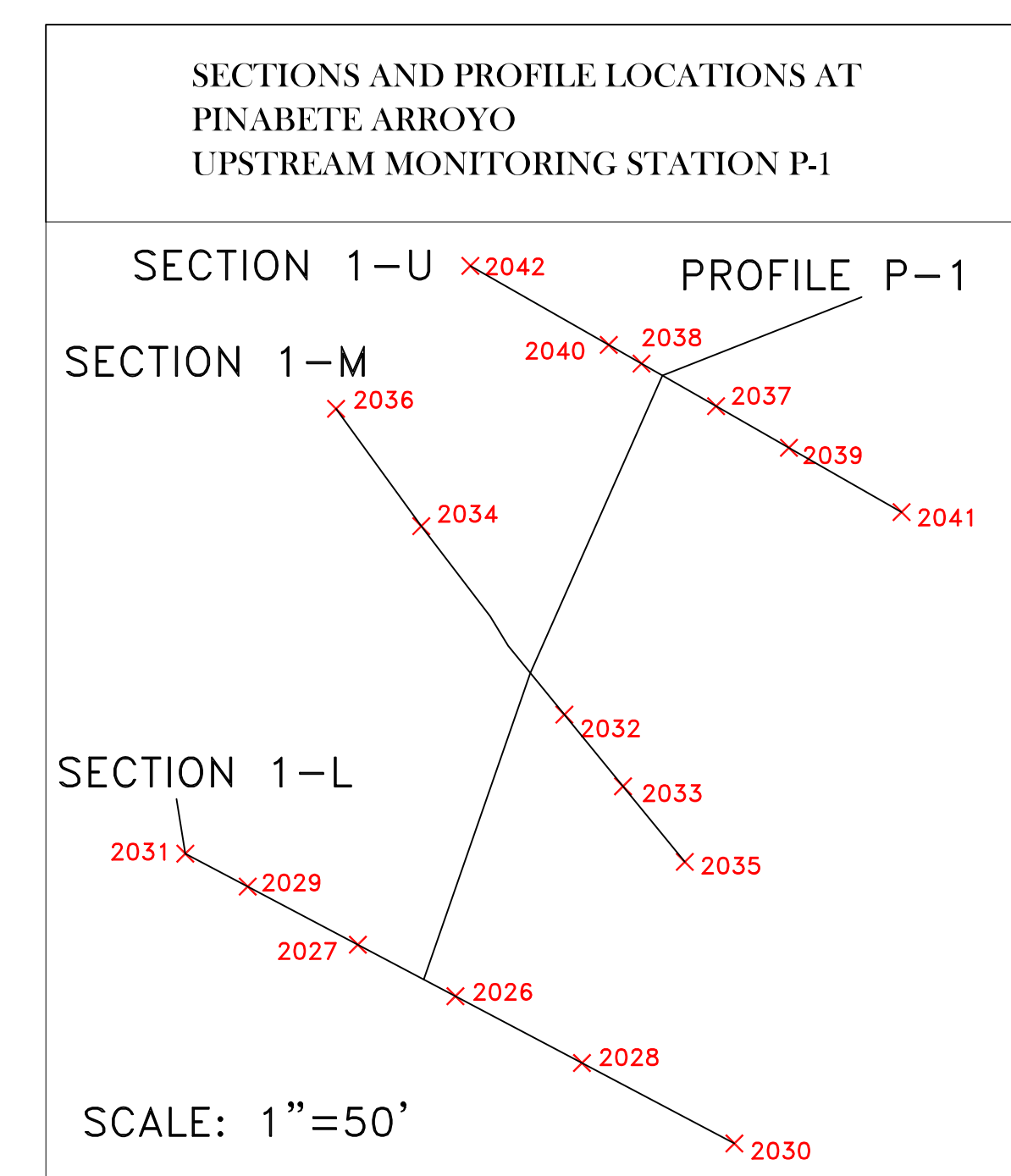
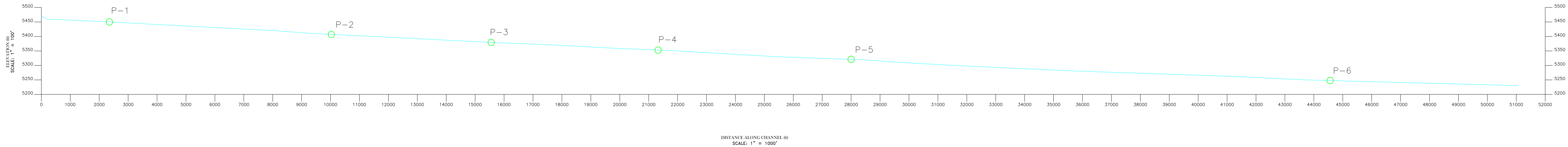




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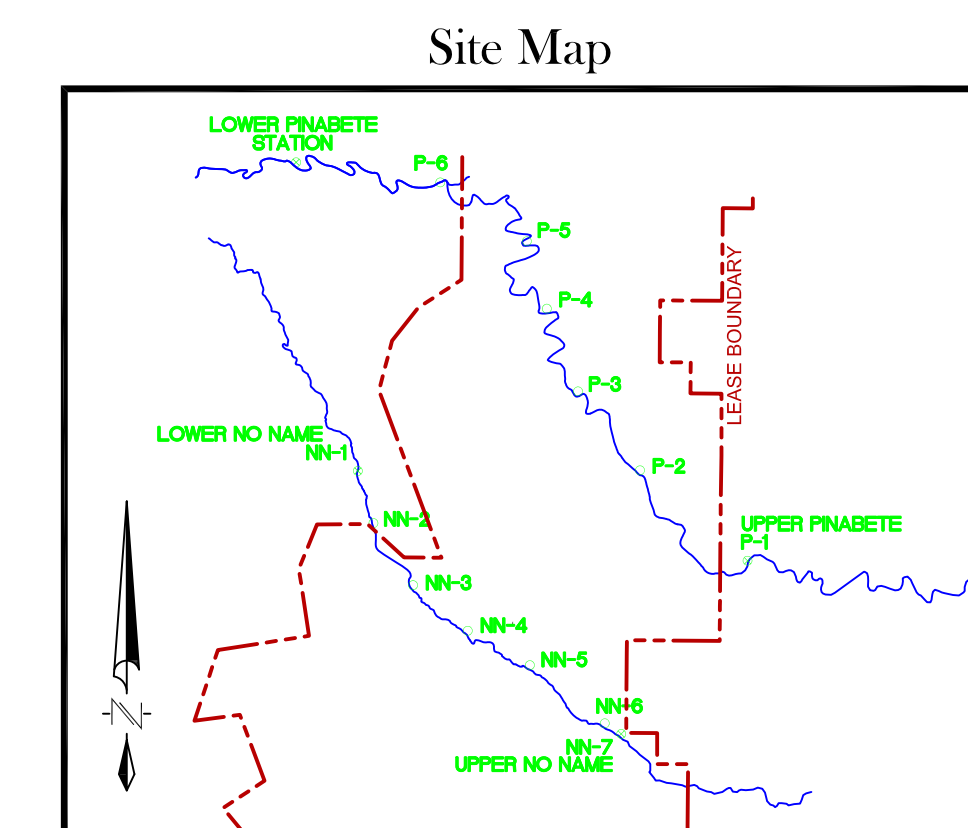
DOWNSTREAM

Longitudinal Profile for Pinabete Arroyo



LEGEND

- P-7 CHANNEL INVENTORY LOCATION
- x SURVEY POINT
- CREST STAGE GAGE
- SINGLE STAGE SAMPLER



|     |         |     |                               |         |
|-----|---------|-----|-------------------------------|---------|
| NO. | DATE    | BY  | DESCRIPTION                   | APP. BY |
| 1   | 3/16/12 | MPD | Submitted to OSM for Approval | IKGA    |
| 2   |         |     |                               |         |
| 3   |         |     |                               |         |
| 4   |         |     |                               |         |

EXHIBIT 18.A-1  
BHP NAVAJO COAL COMPANY

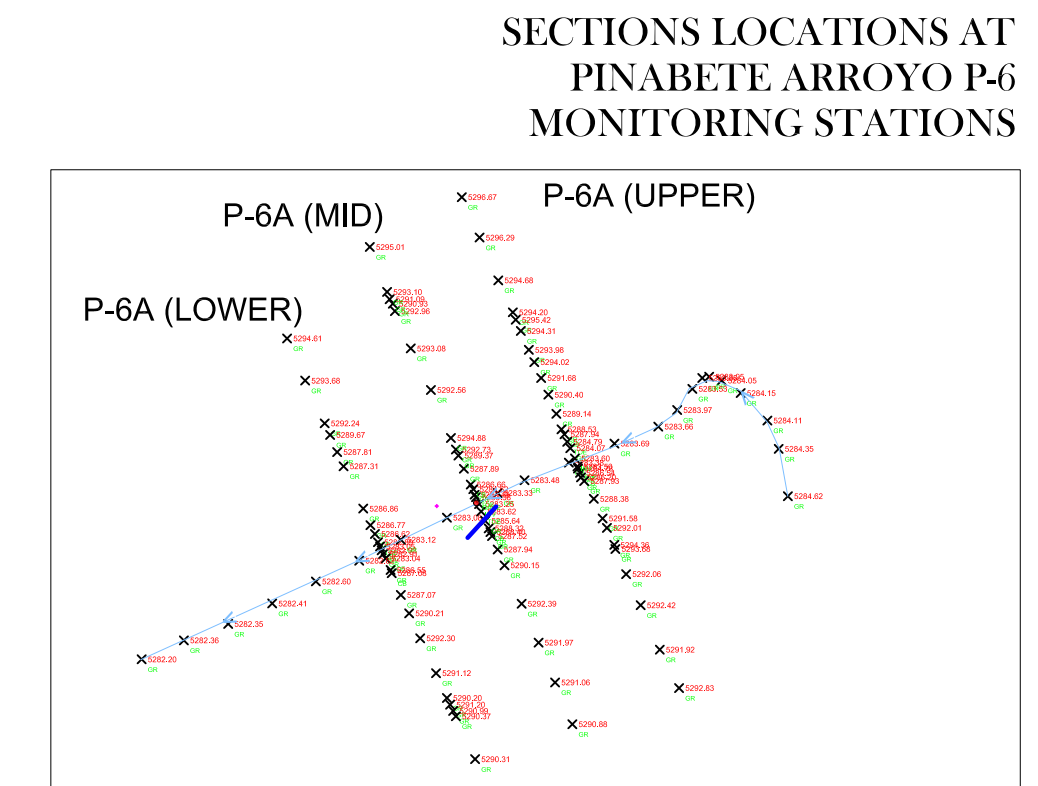
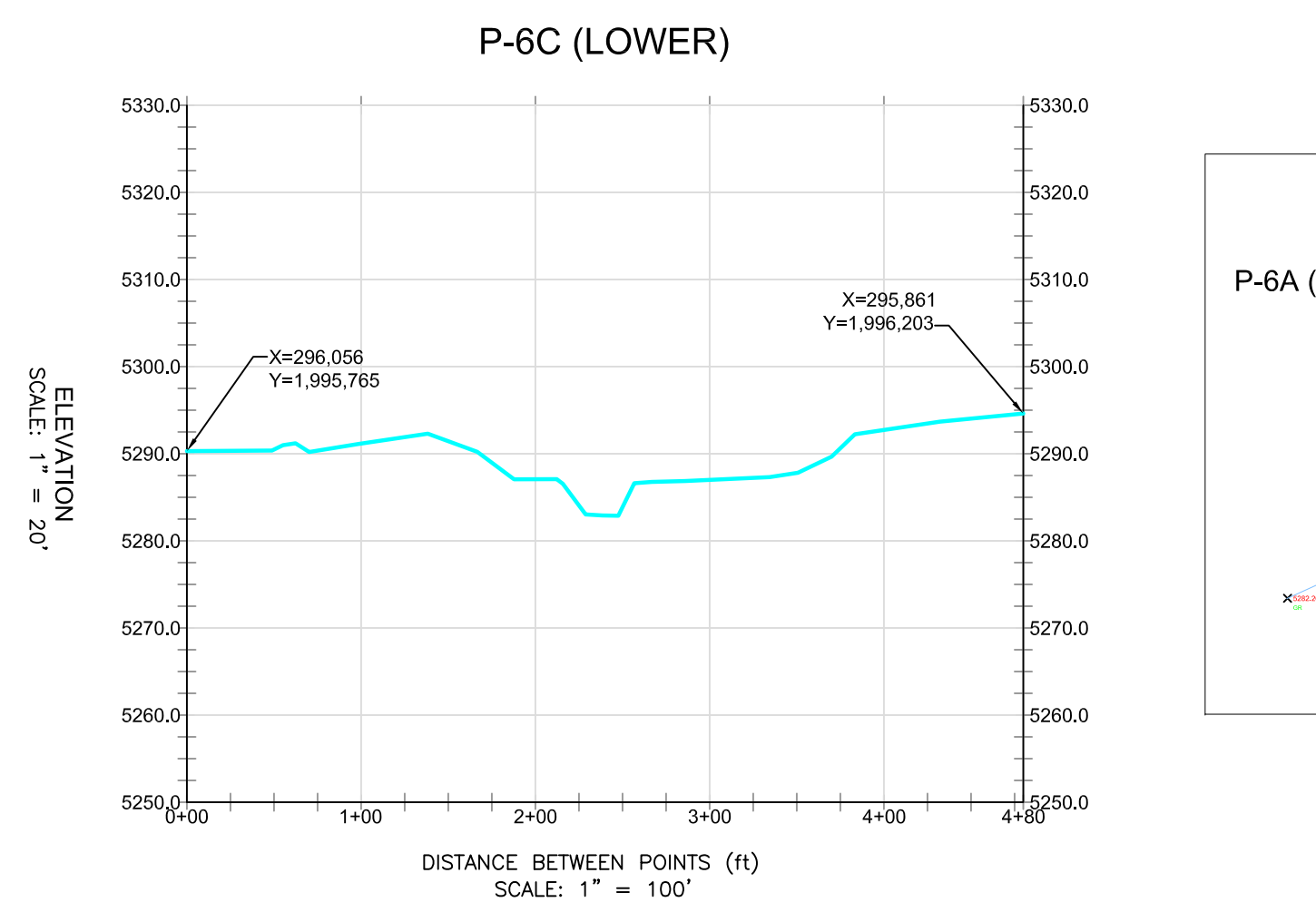
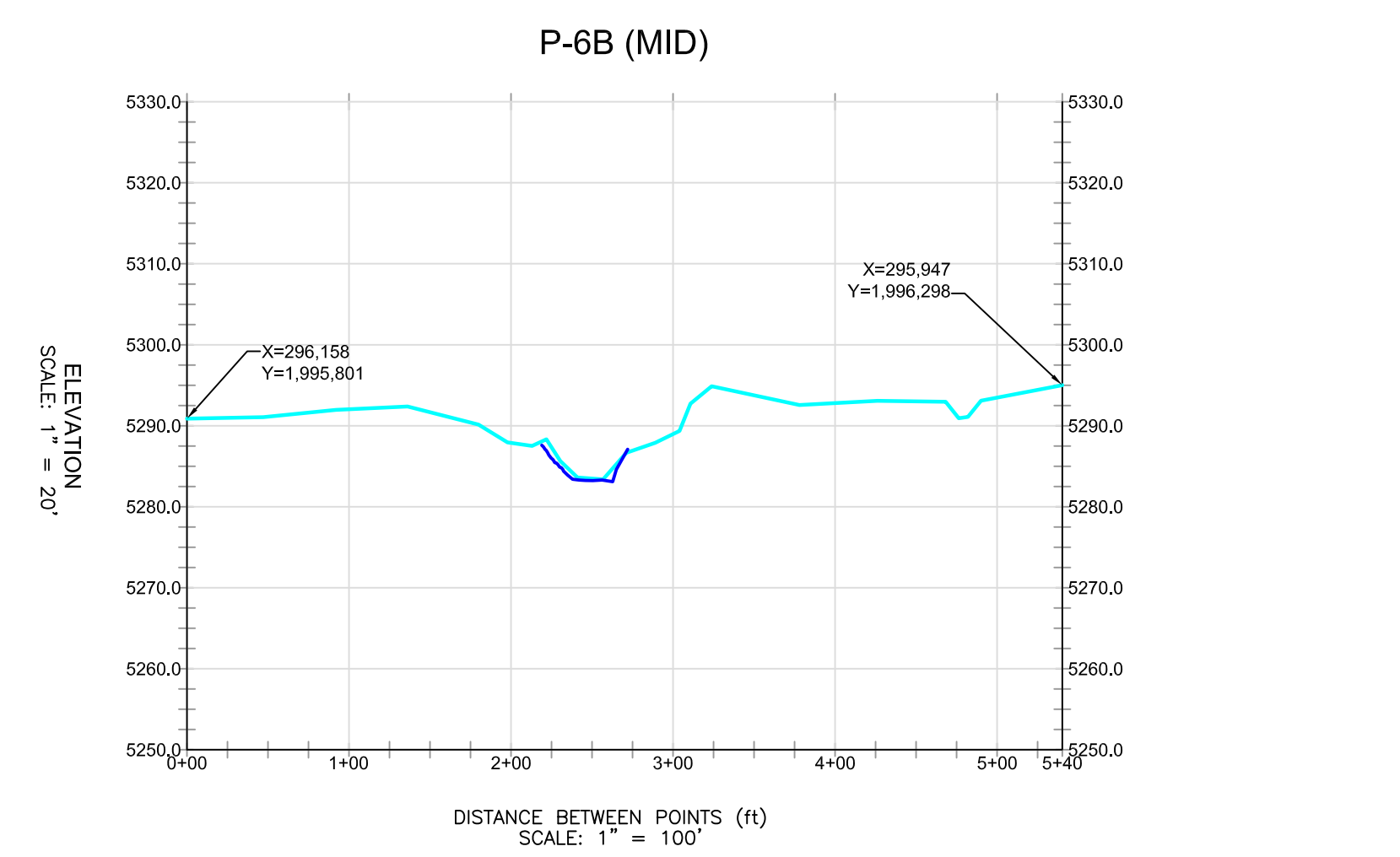
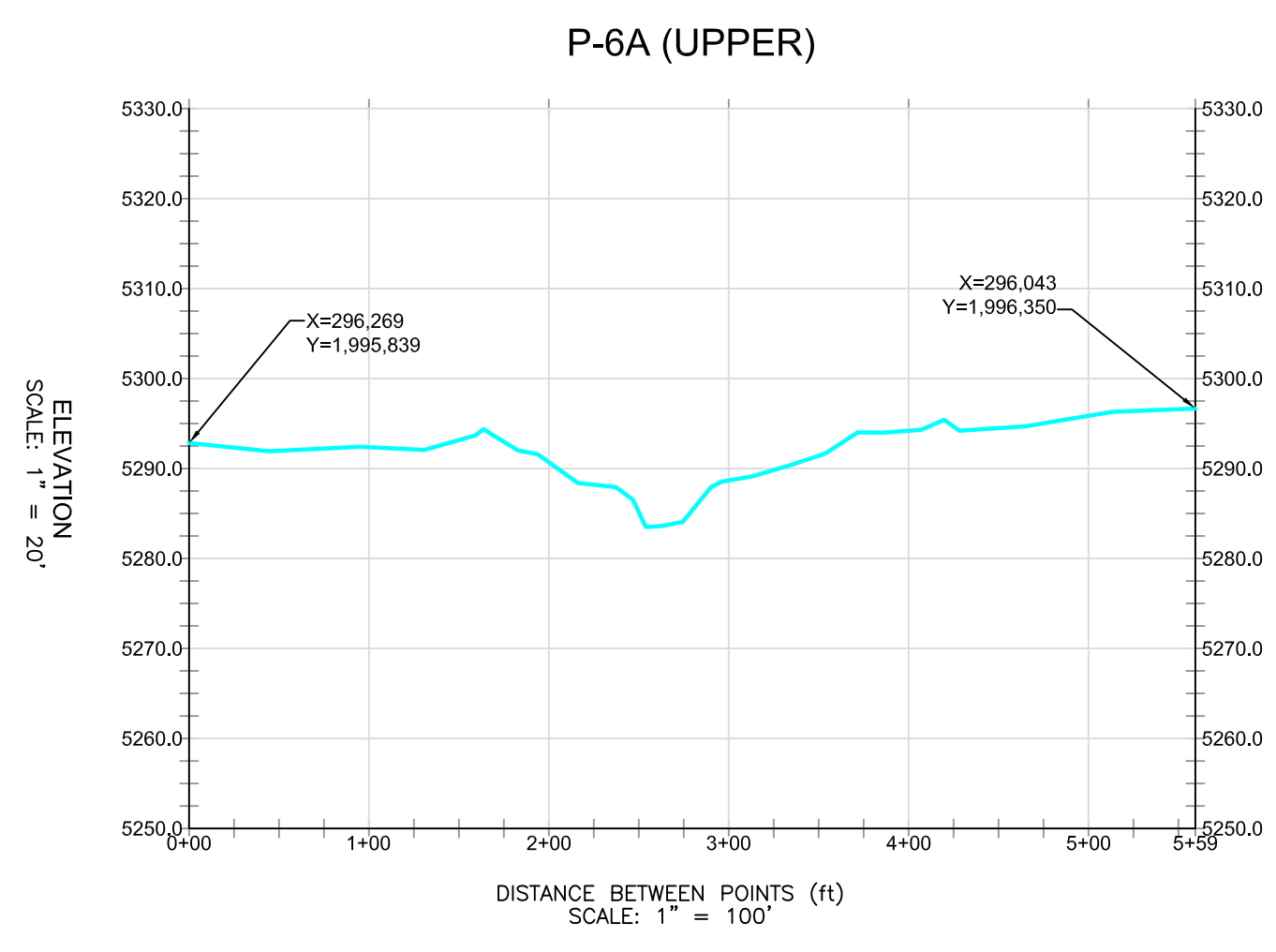
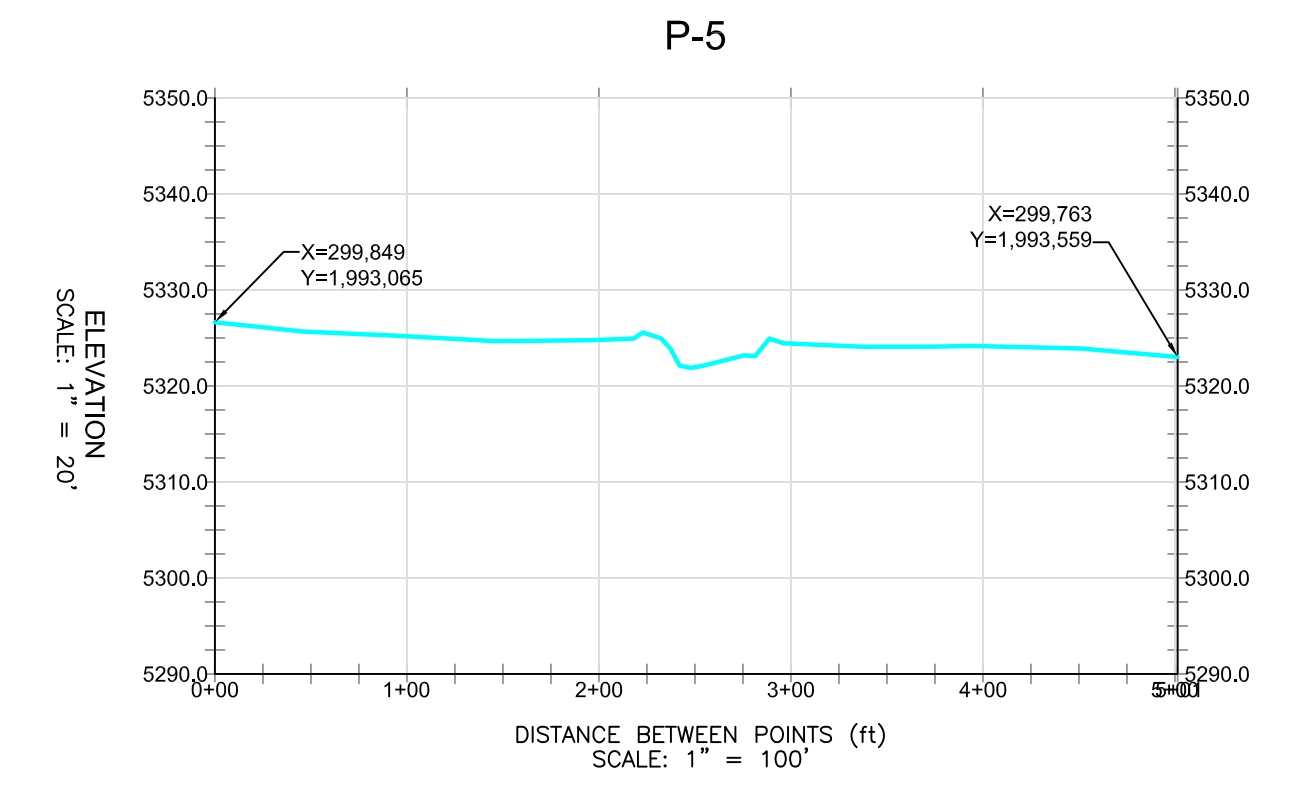
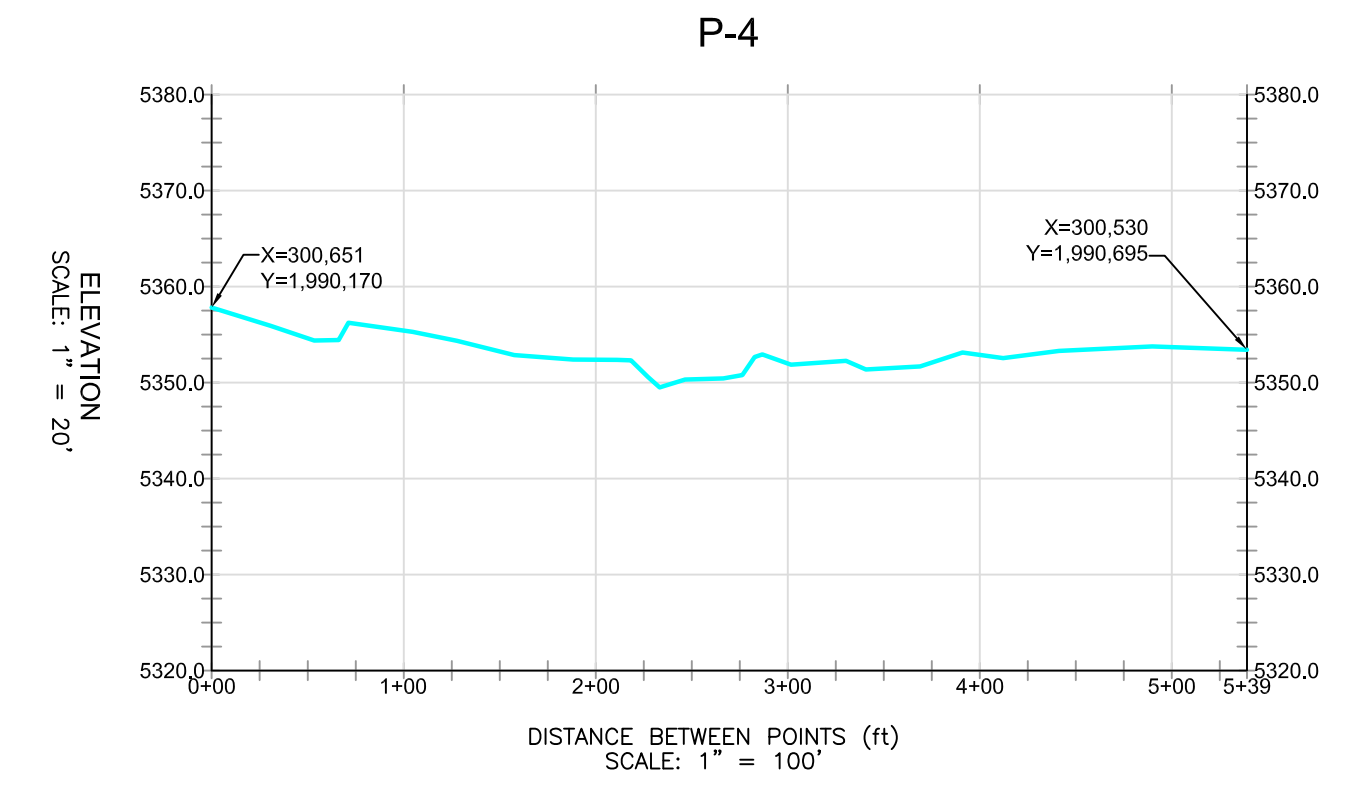
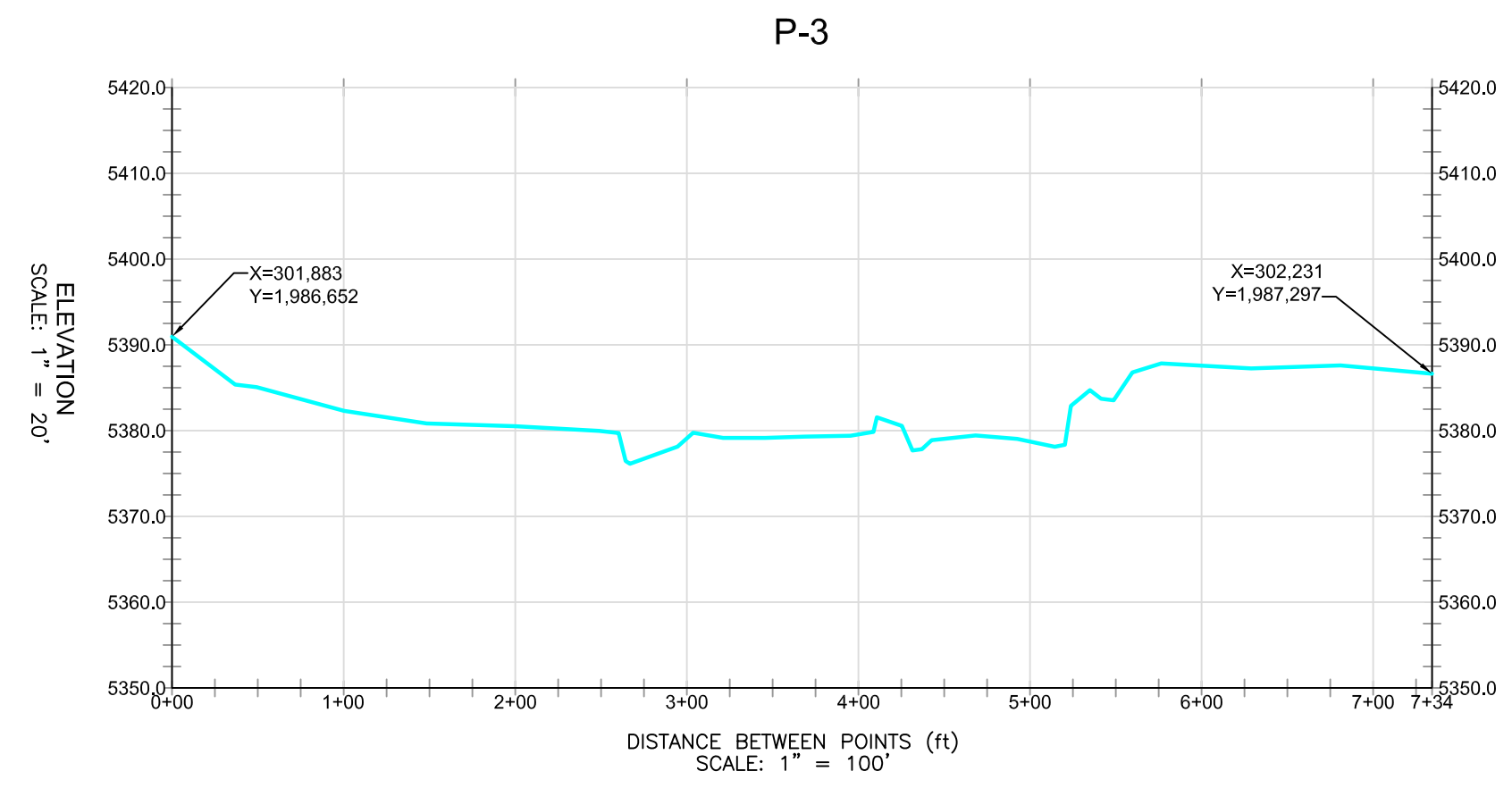
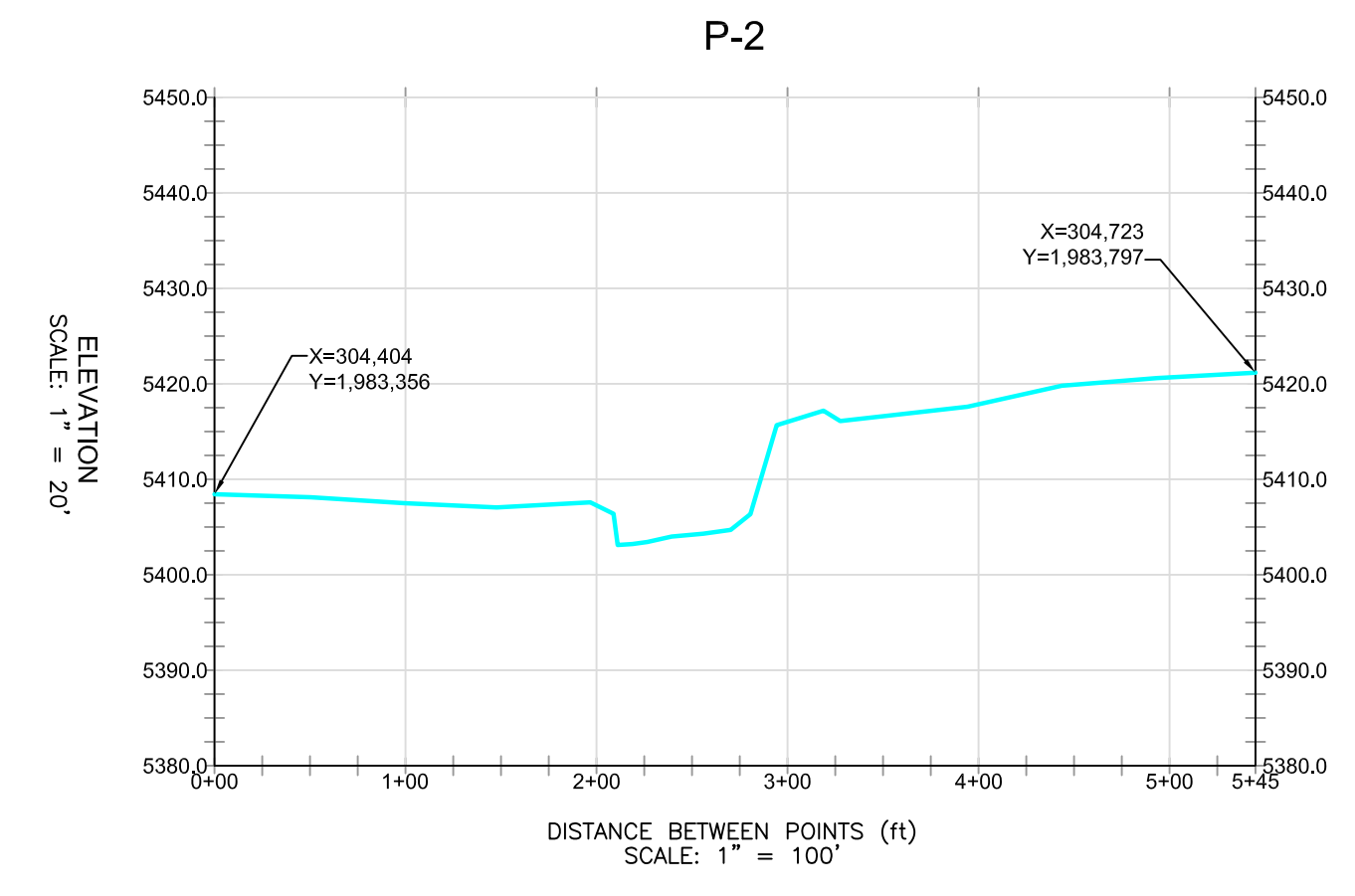
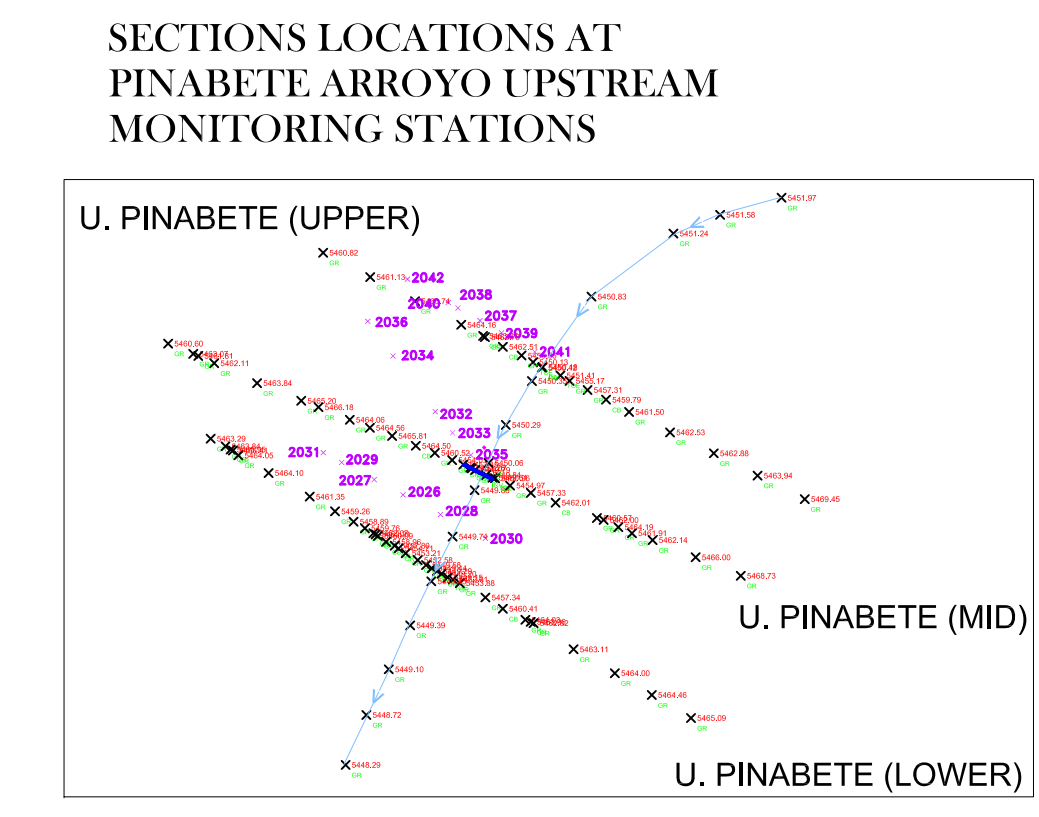
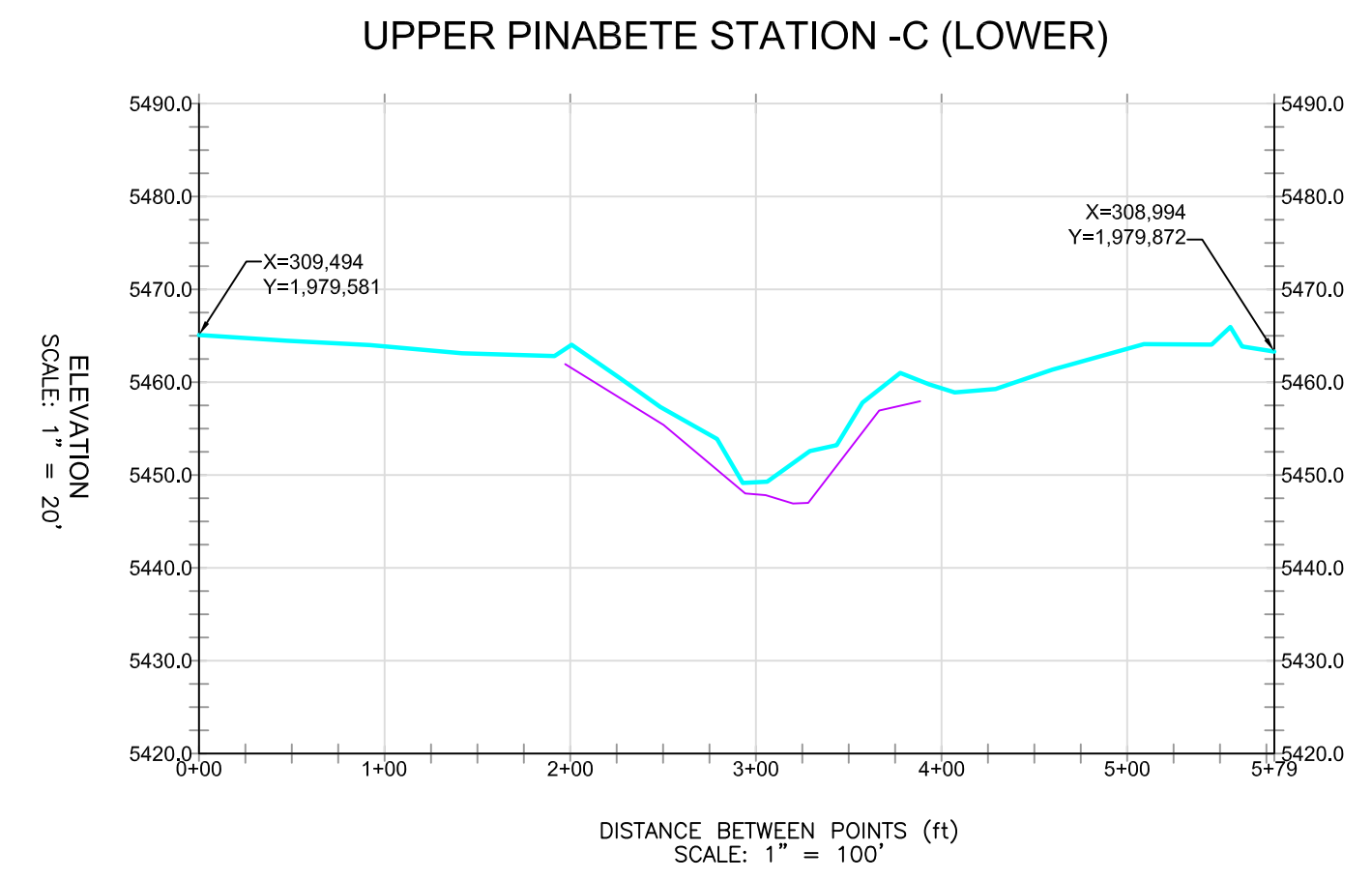
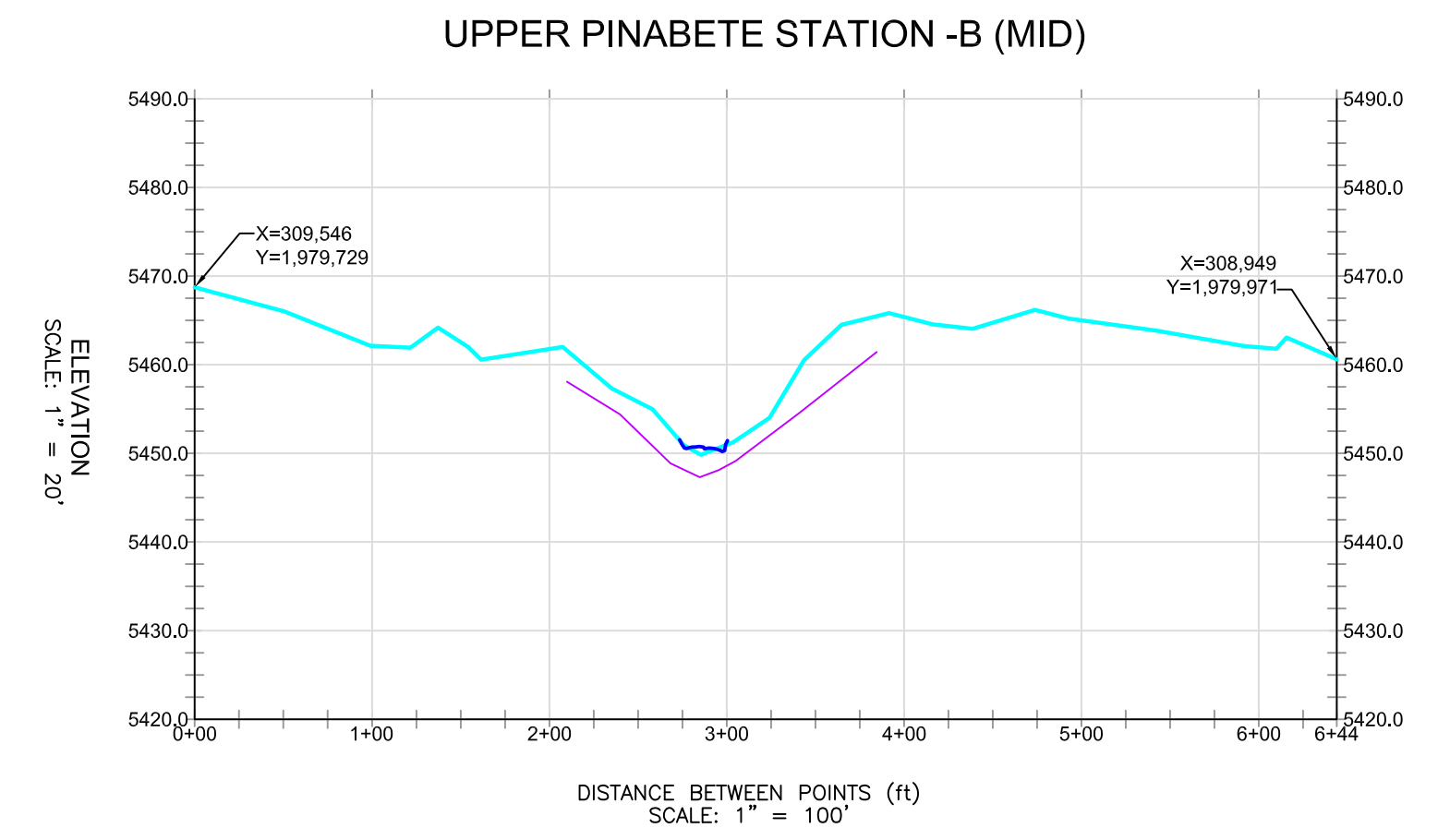
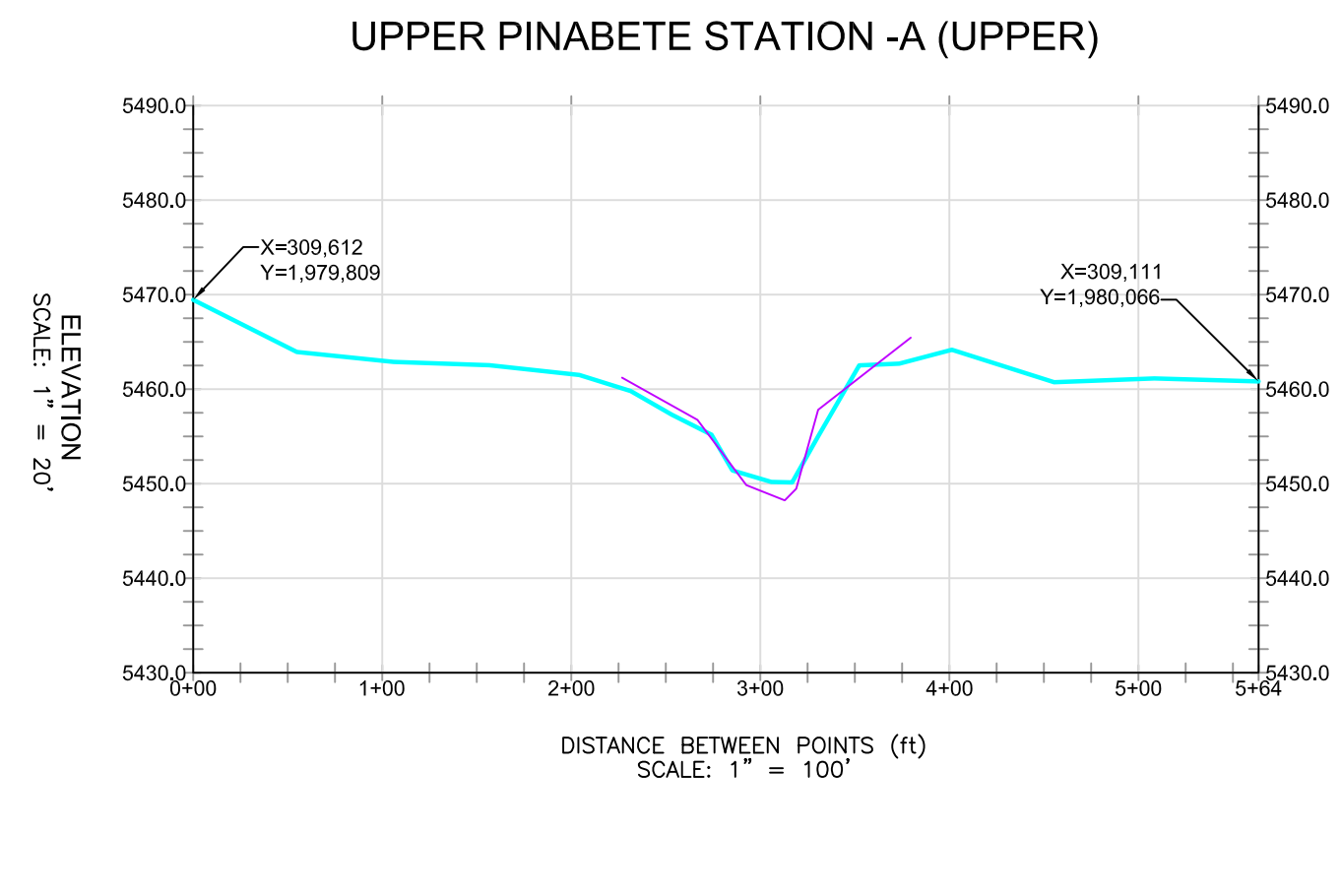
**bhpbilliton**

P.O. BOX 1117  
FRUITLAND, NEW MEXICO 87416  
PHONE: 505/698-4200  
FAX: 505/698-4229

PINABETE PERMIT  
PINABETE ARROYO MONITORING STATION  
INFORMATION AND CHANNEL  
CHARACTERIZATION 1998

PREPARED BY: APO    DRAWN BY: JLS    SCALE: AS SHOWN  
APPROVED BY:    DATE: Mar 16, 2012



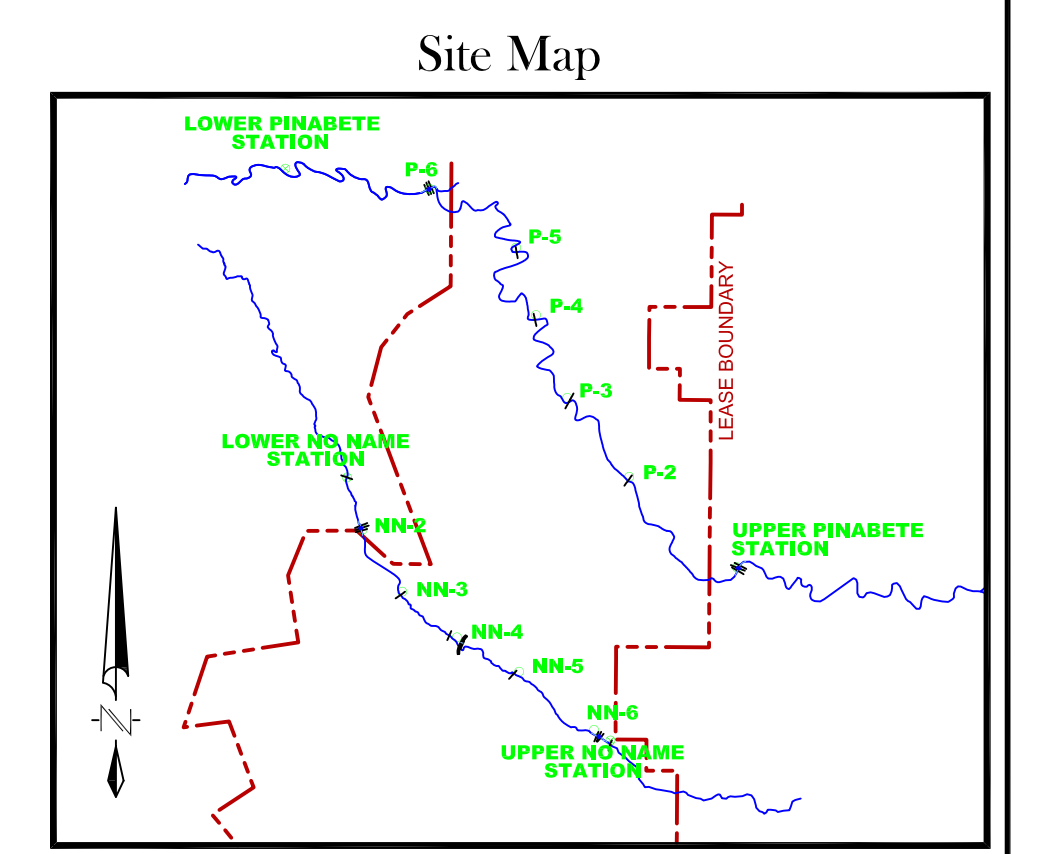


**LEGEND**

- 2008 SURVEYED SECTION
- 2007 SURVEYED SECTION
- 1998 SURVEYED SECTION

**NOTES**

- COORDINATE DATUM IS NEW MEXICO STATE PLANE NAD 27
- FEET WEST ZONE
- CROSS SECTIONS LOOKING DOWNSTREAM



|          |      |          |                      |          |      |      |          |
|----------|------|----------|----------------------|----------|------|------|----------|
| REV. No. | DATE | DRAWN BY | REVISION DESCRIPTION | PREP. BY | E.D. | P.E. | APPROVED |
|          |      |          |                      |          |      |      |          |

**NORWEST**  
ACCIDENT INVESTIGATION

**EXHIBIT 18.A-2**  
**BHP NAVAJO COAL COMPANY**

**bhpbilliton**

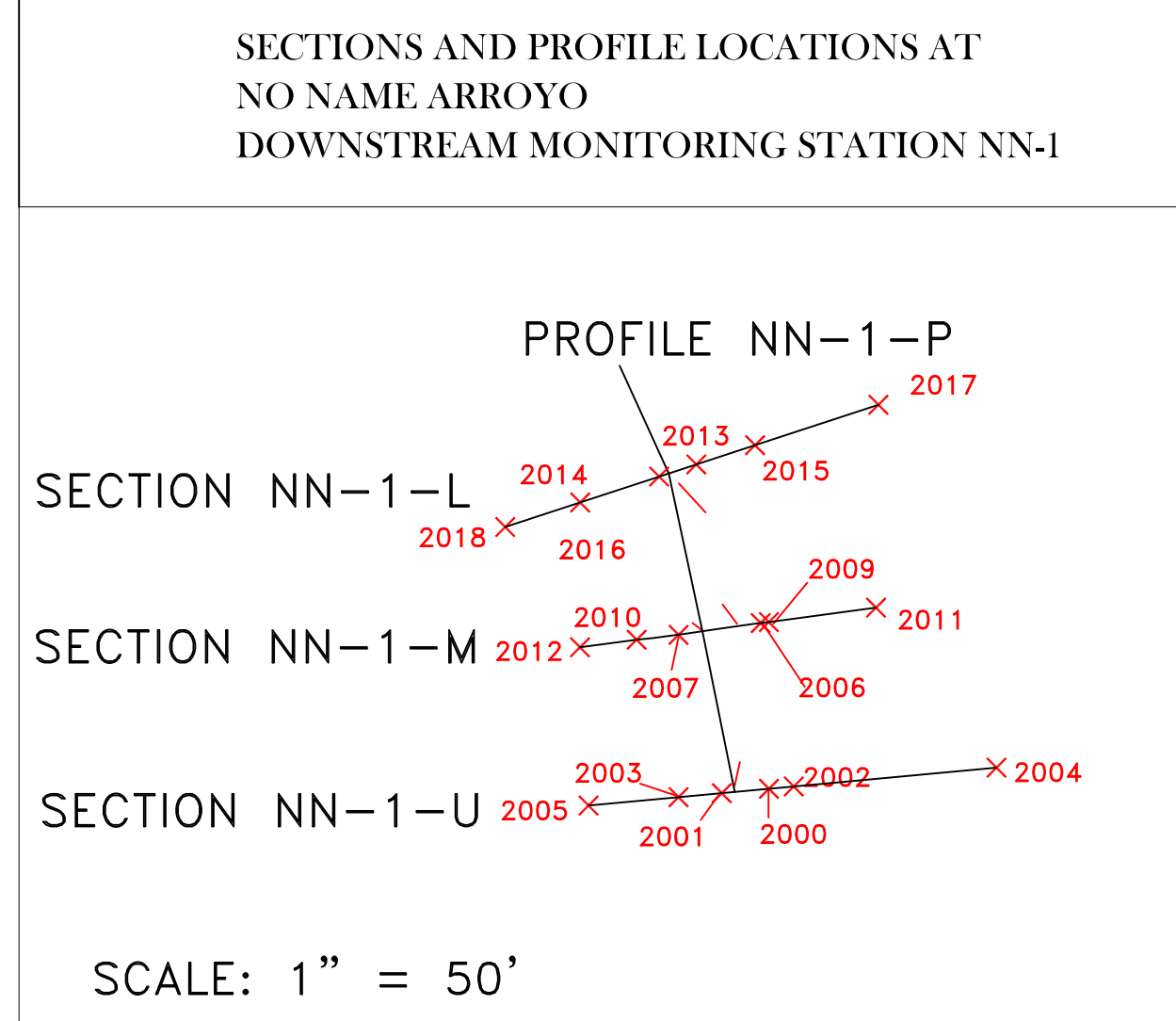
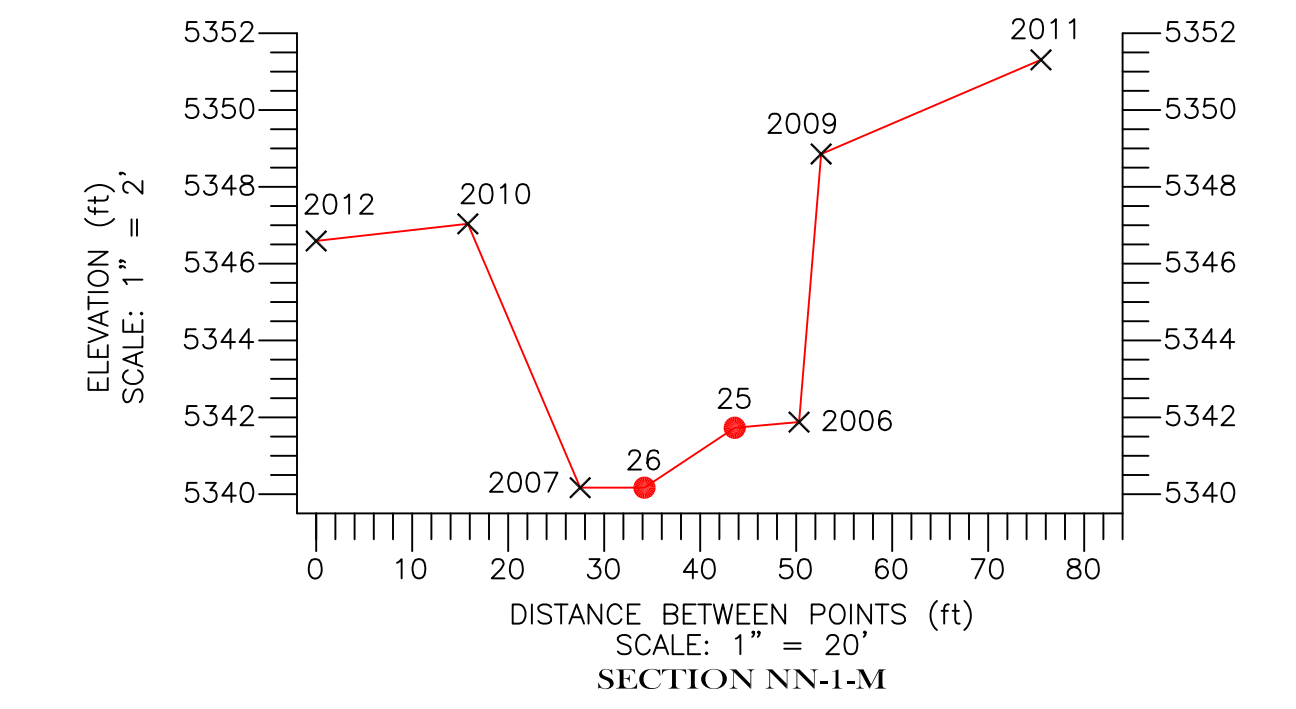
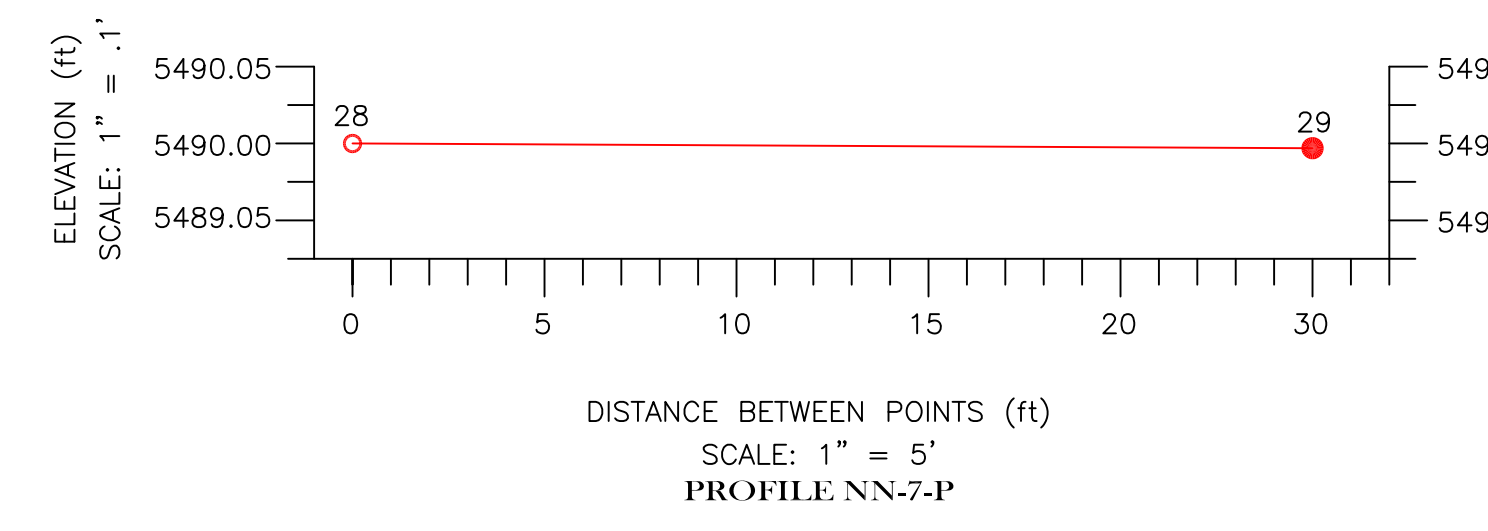
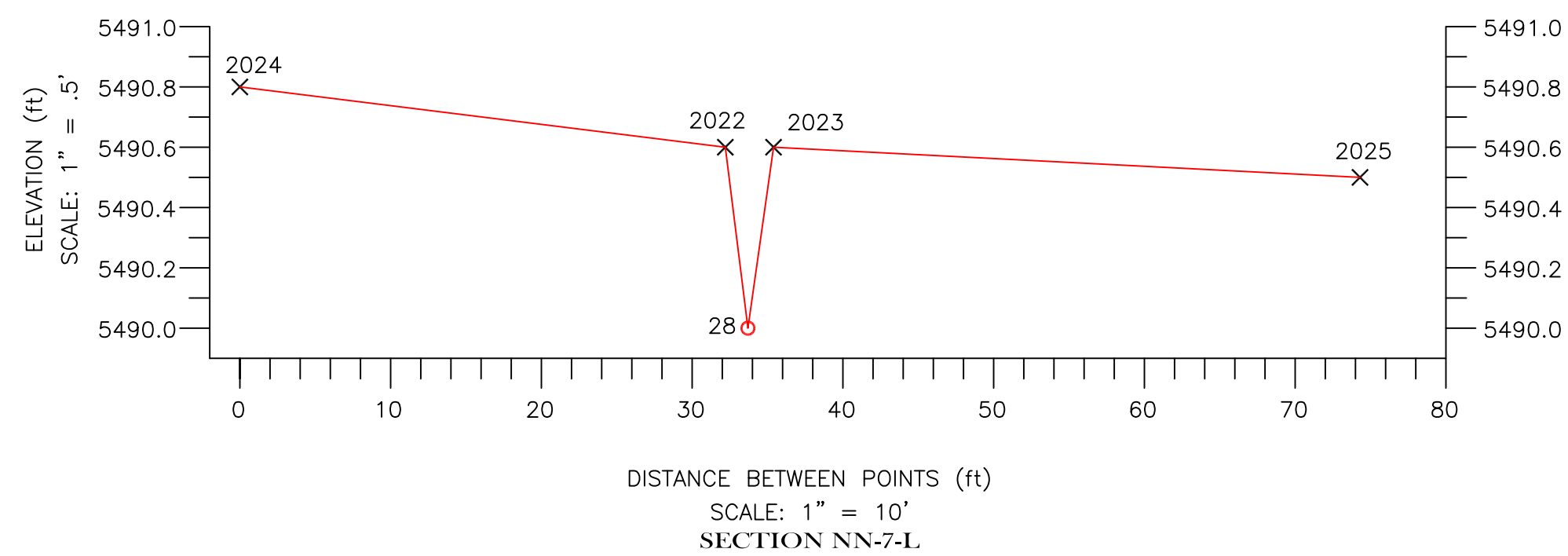
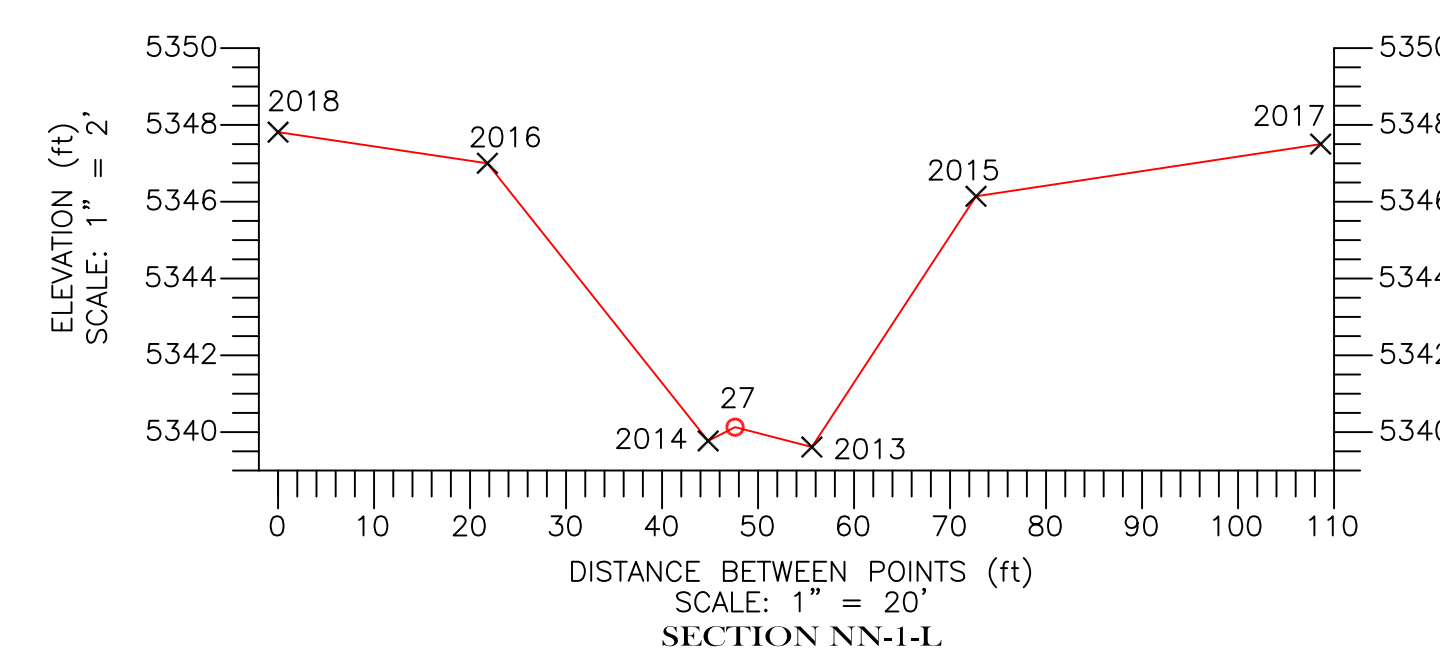
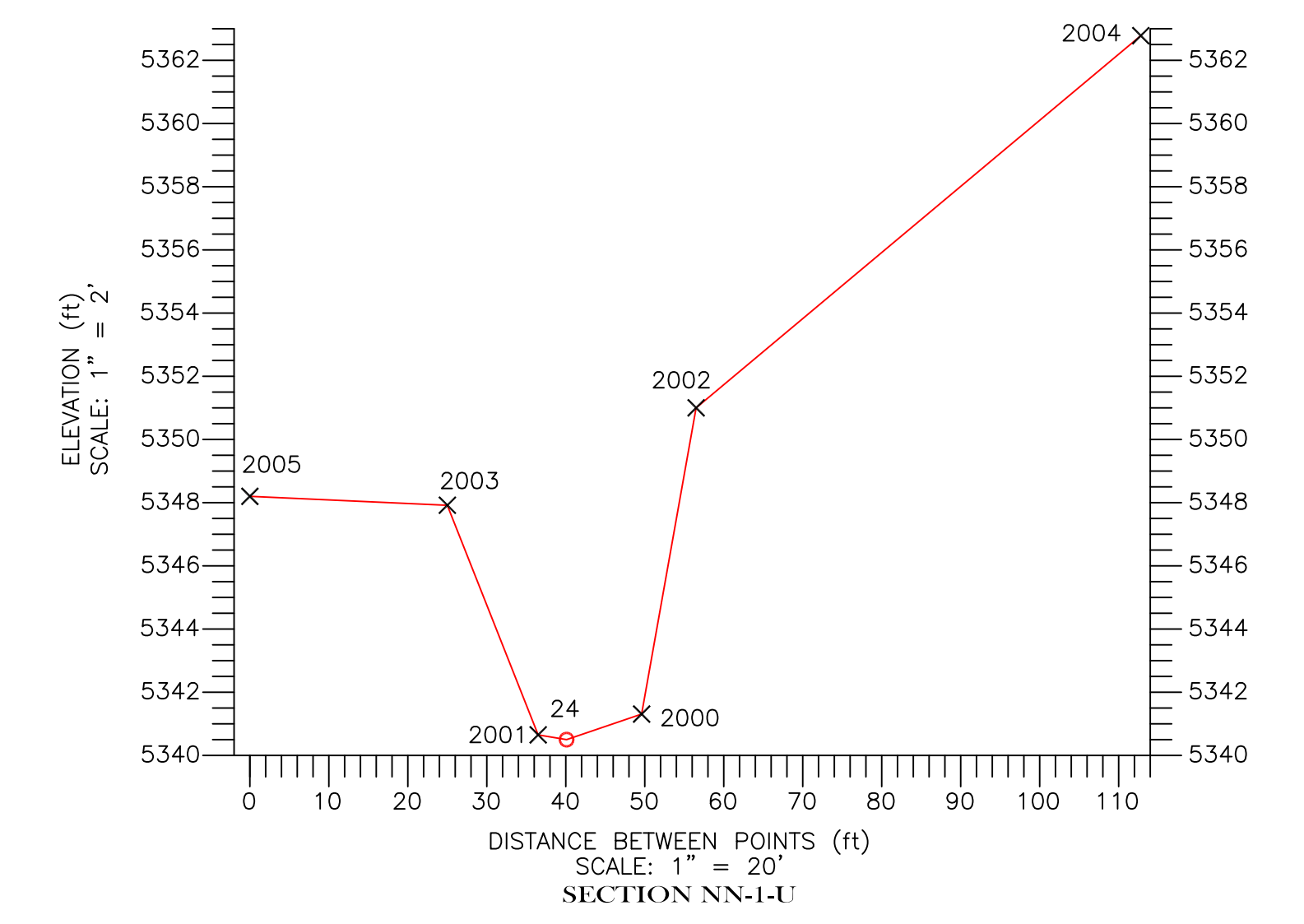
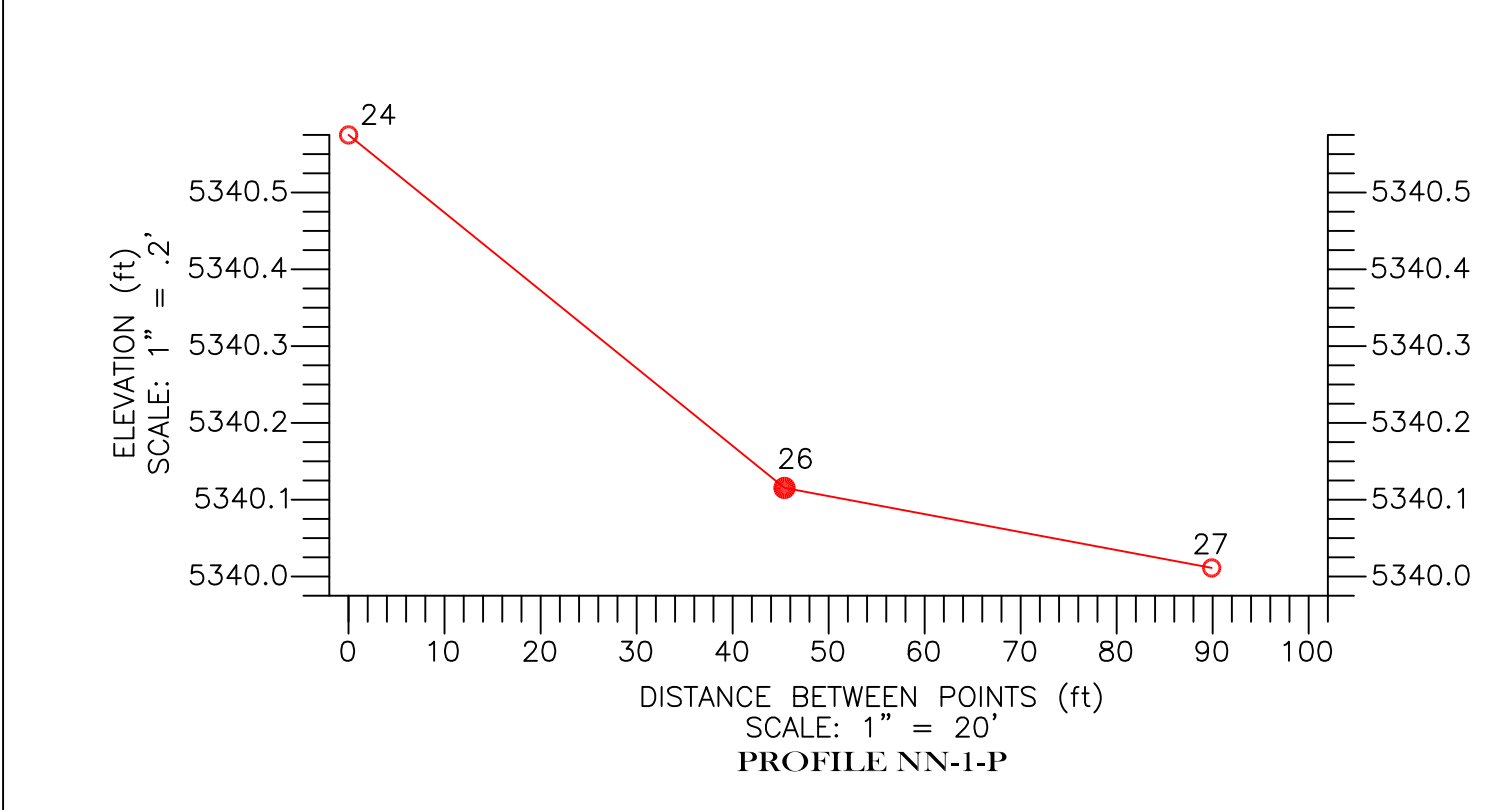
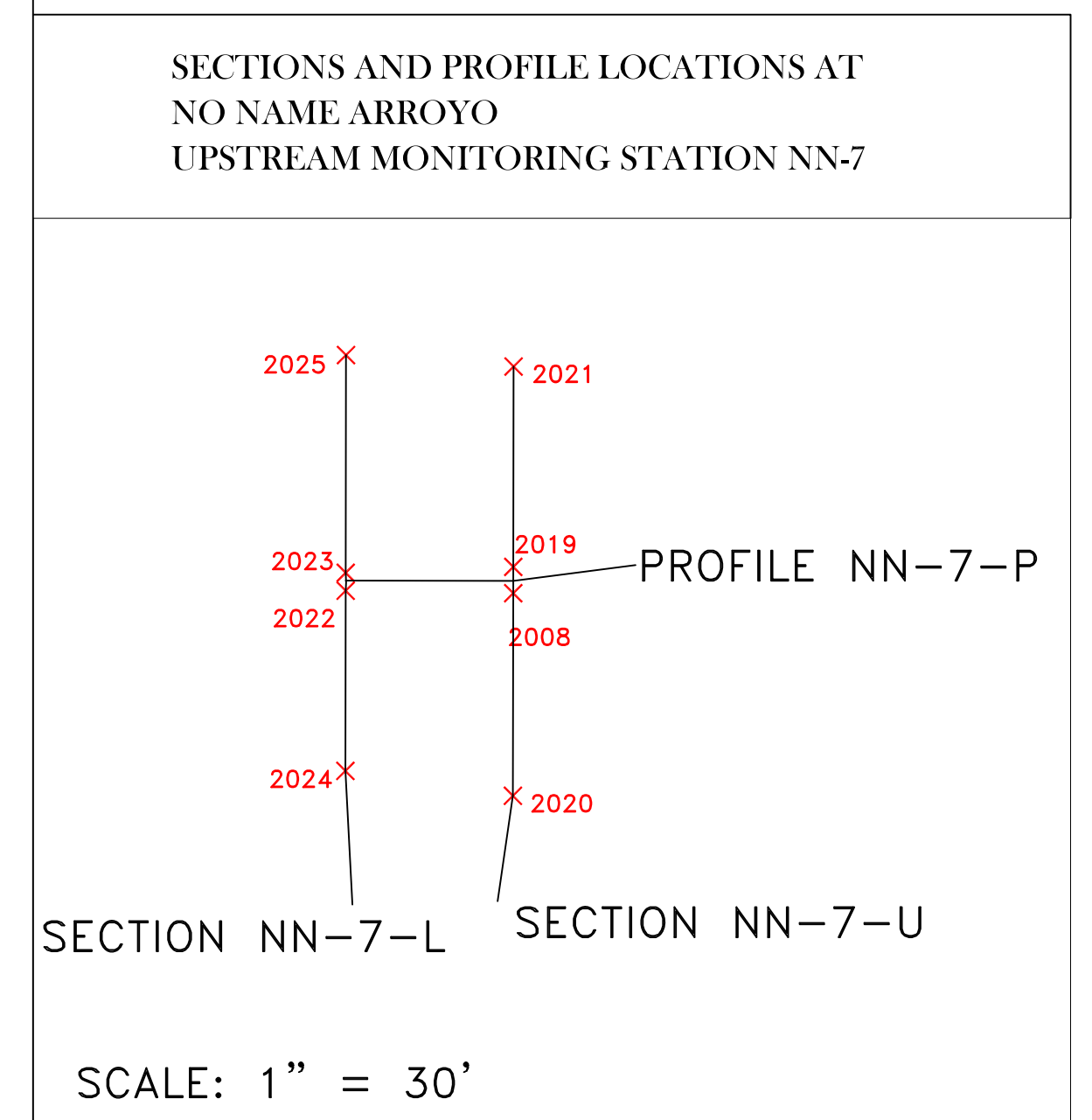
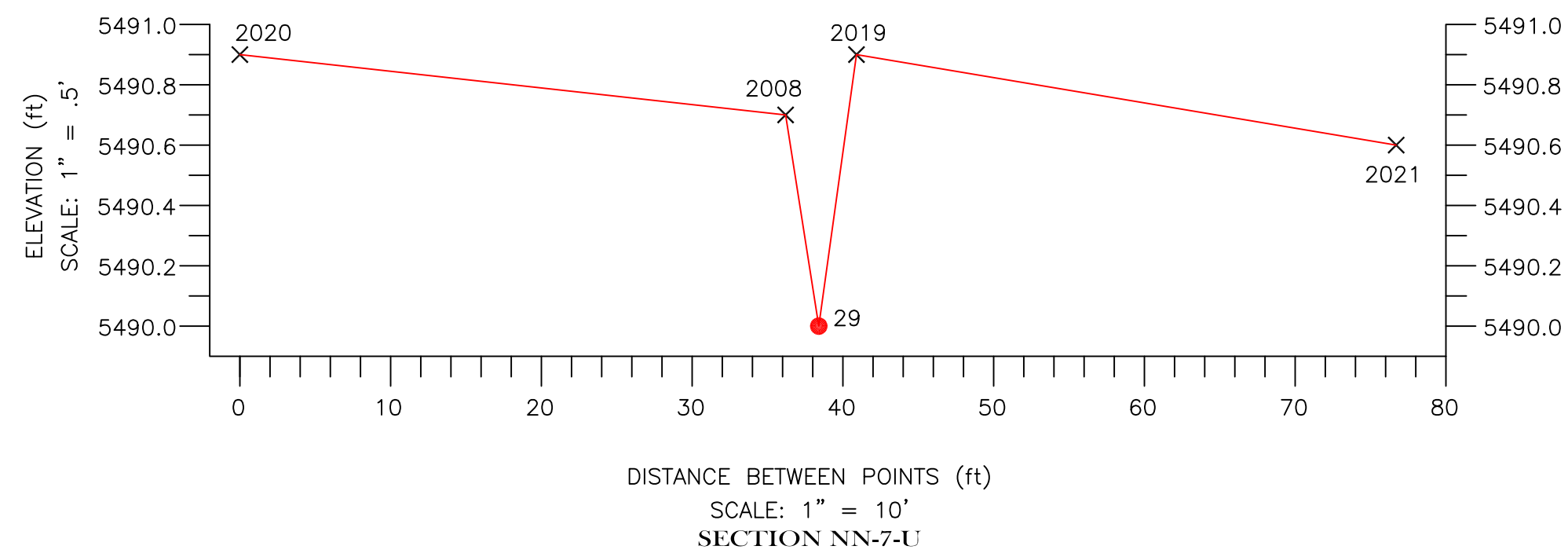
P.O. BOX 1717  
FRUITLAND, NEW MEXICO 87416

PHONE: (505) 698-4200  
FAX: (505) 698-4229

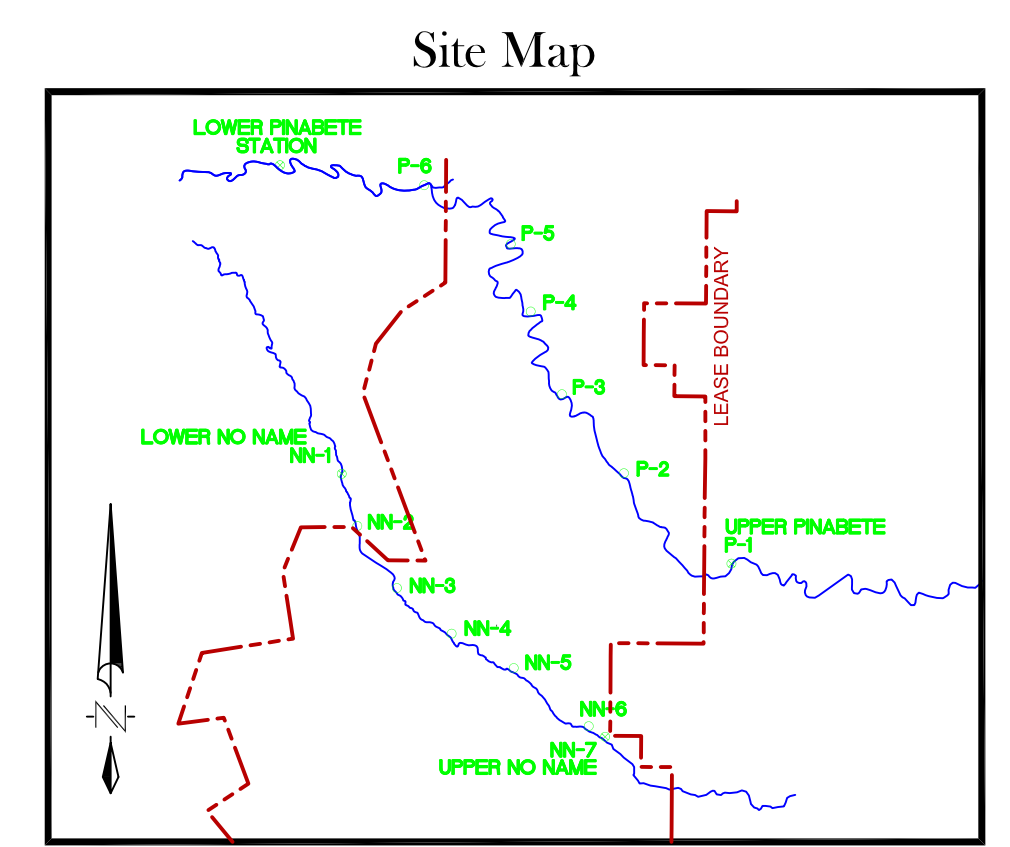
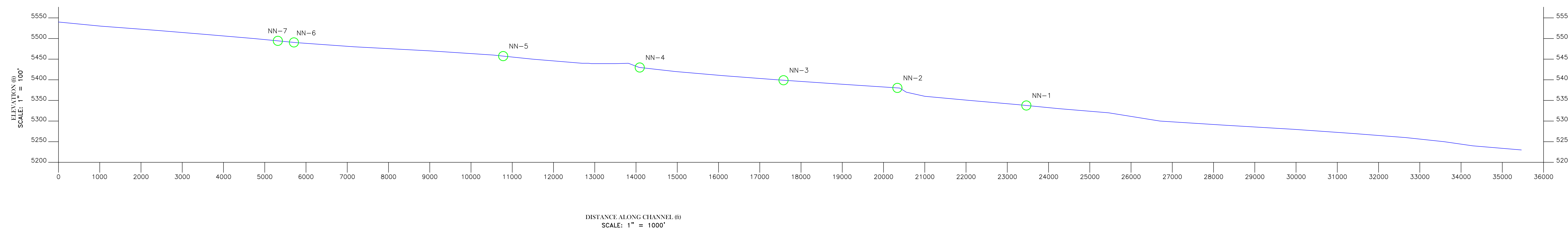
**PINABETE PERMIT**  
**PINABETE ARROYO**  
**CROSS SECTIONS**

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| APPROVED BY |     | DATE     | Mar 16, 2012 |        |          |





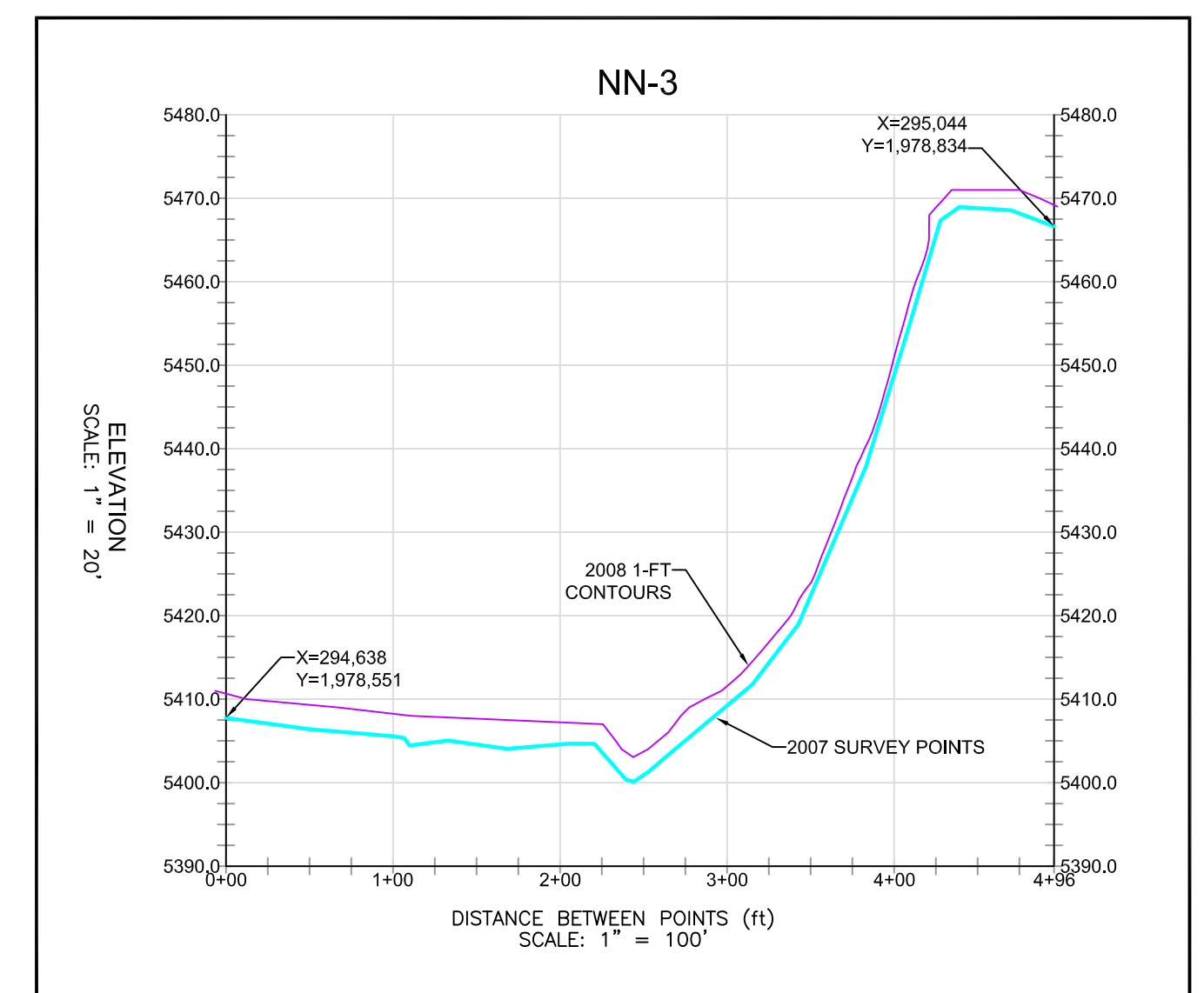
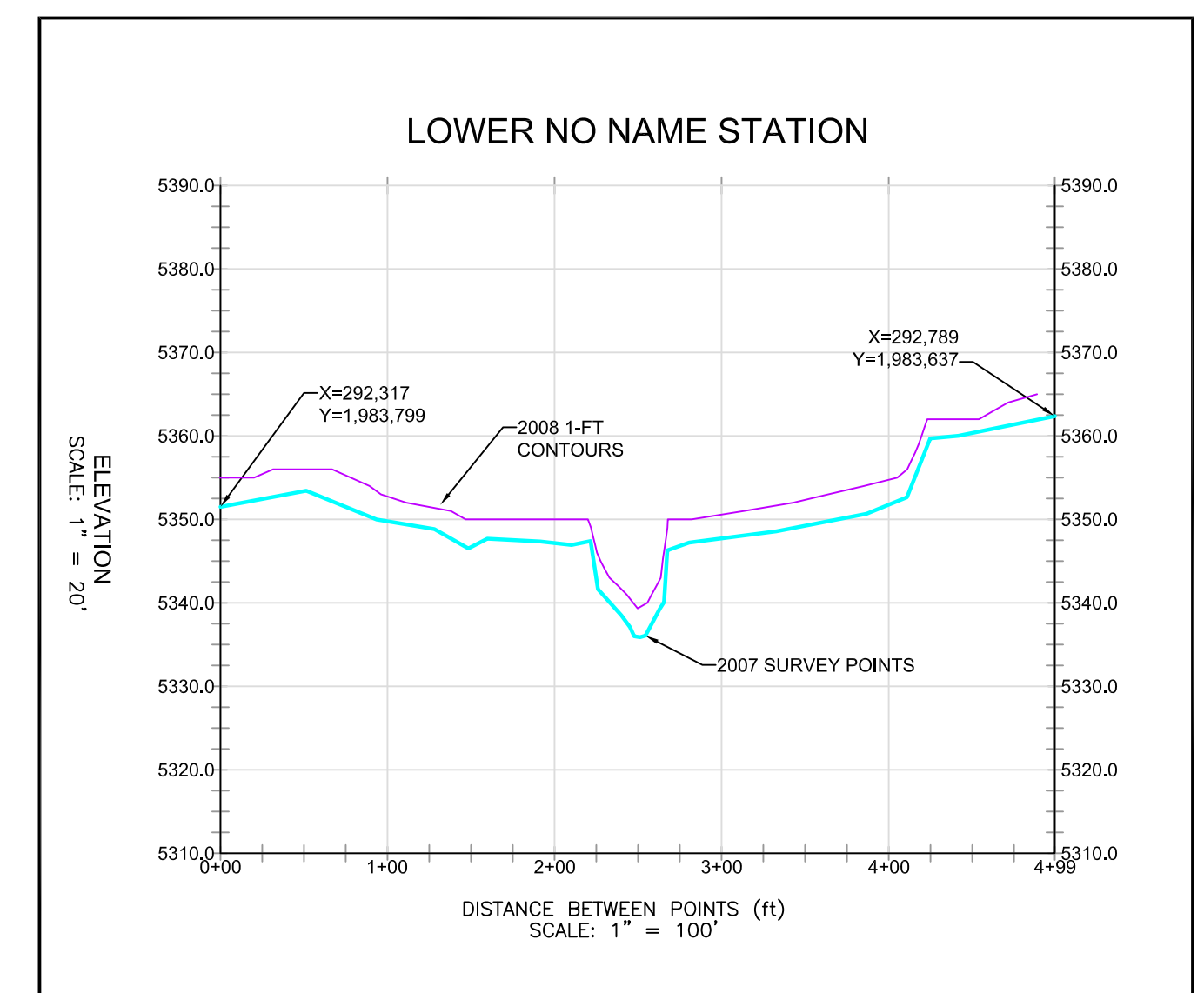
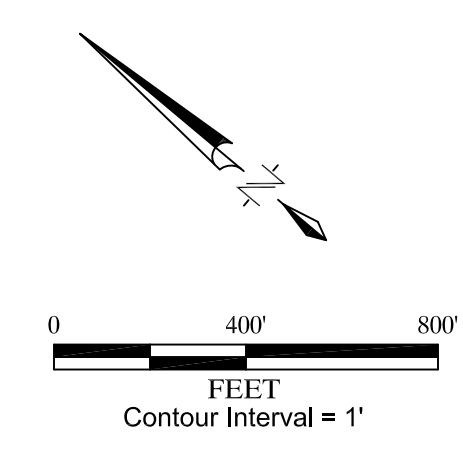
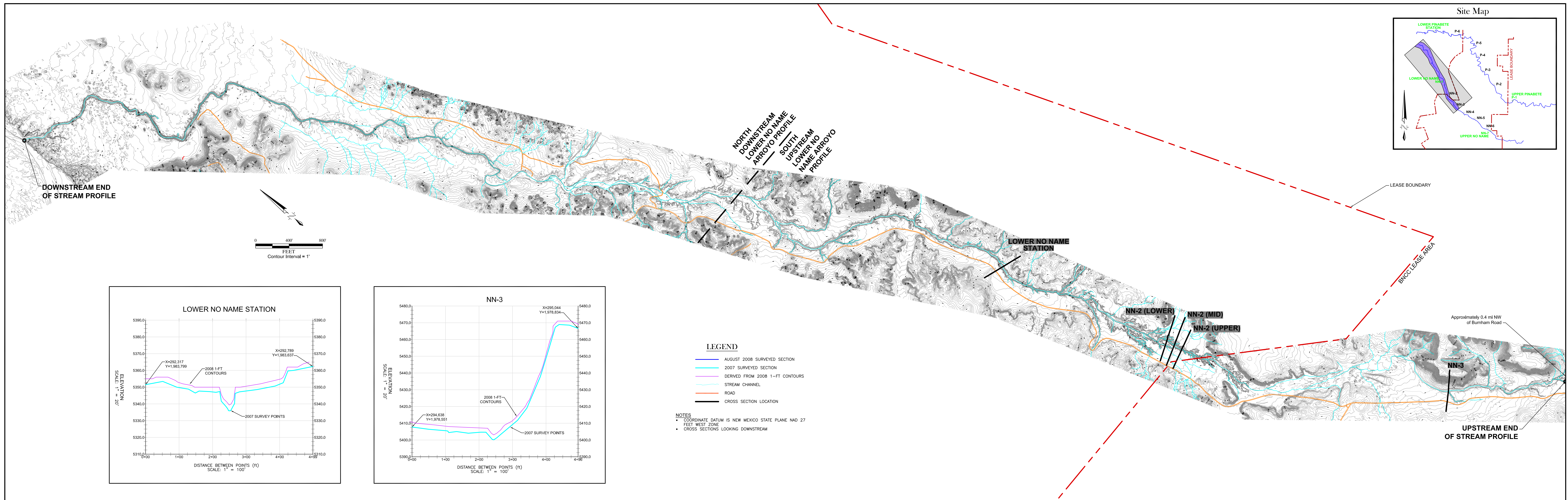
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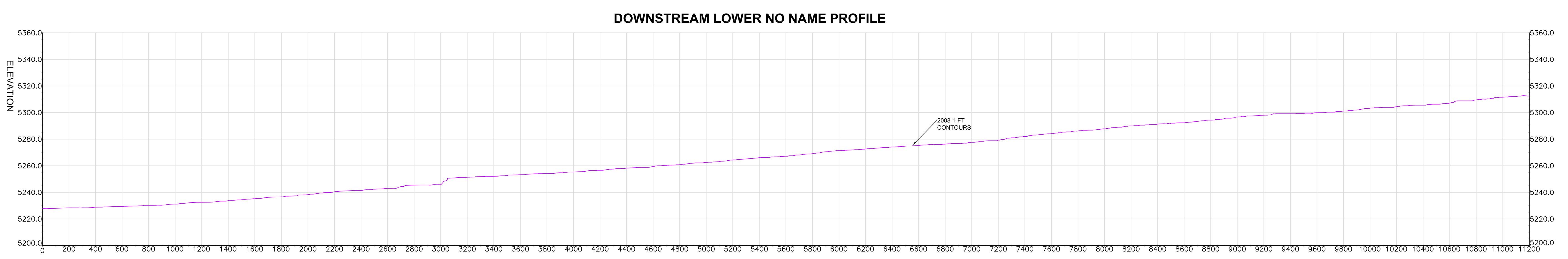
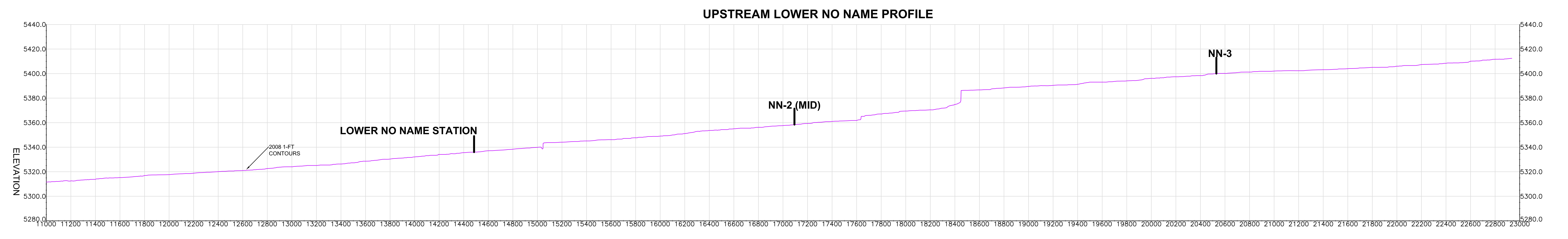
- LEGEND**
- NN-7 CHANNEL INVENTORY LOCATION
  - × SURVEY POINT
  - CREST STAGE GAGE
  - SINGLE STAGE SAMPLER

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| 12-A   | 3/16/12 | MPO      | Submitted to OSM for Approval | CKA      |             |
| REV. NO.   | DATE    | DRWN. BY | REVISION DESCRIPTION          | PREP. BY | APPROVED BY |
|  |         |          |                               |          |             |
| <b>NORWEST</b>   |         |          |                               |          |             |
| <b>EXHIBIT 18.A-3</b>  |         |          |                               |          |             |
| <b>BHP NAVAJO COAL COMPANY</b>   |         |          |                               |          |             |
| <b>bhpbilliton</b>   |         |          |                               |          |             |
| P.O. BOX 1717 FRUITLAND, NEW MEXICO 87416 PHONE: (505) 698-4200 FAX: (505) 698-4229    |         |          |                               |          |             |
| <b>PINABETE PERMIT</b>   |         |          |                               |          |             |
| <b>NO NAME ARROYO MONITORING STATION INFORMATION AND CHANNEL CHARACTERIZATION 1998</b> |         |          |                               |          |             |
| PREPARED BY  | APO     | DRAWN BY | JLS                           | SCALE:   | AS SHOWN    |
| APPROVED BY  |         | DATE     | Mar 16, 2012                  |          |             |





- LEGEND**
- AUGUST 2008 SURVEYED SECTION
  - 2007 SURVEYED SECTION
  - DERIVED FROM 2008 1-FT CONTOURS
  - STREAM CHANNEL
  - ROAD
  - CROSS SECTION LOCATION
- NOTES**
- COORDINATE DATUM IS NEW MEXICO STATE PLANE NAD 27
  - FEET WEST ZONE
  - CROSS SECTIONS LOOKING DOWNSTREAM



|      |         |     |                               |       |      |    |
|------|---------|-----|-------------------------------|-------|------|----|
| NO.  | DATE    | BY  | DESCRIPTION                   | CHK.  | DATE | BY |
| 12-A | 3/16/12 | MPO | Submitted to OSM for Approval | OKA   |      |    |
| REV  | DATE    | BY  | DESCRIPTION                   | PREP. | DATE | BY |
|      |         |     |                               |       |      |    |

**NORWEST**

**EXHIBIT 18.A-4**  
**BHP NAVAJO COAL COMPANY**

**bhpbilliton**

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FRUITLAND, NEW MEXICO 87416

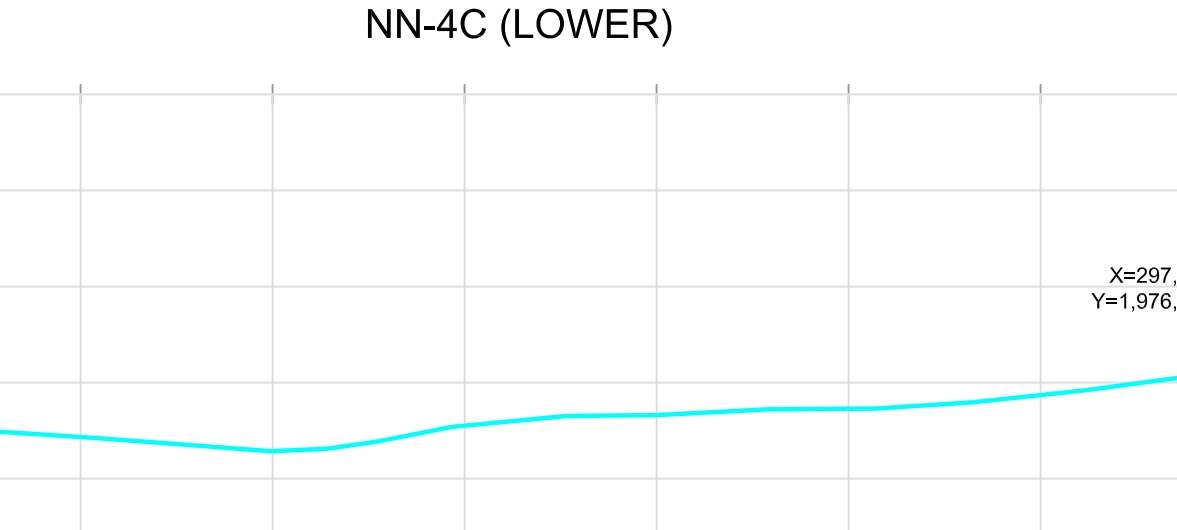
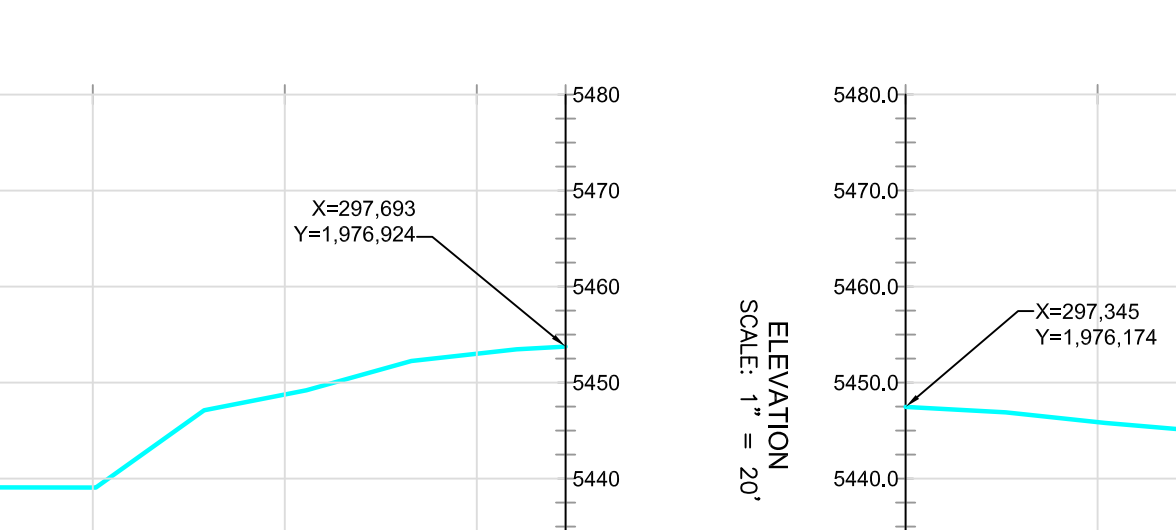
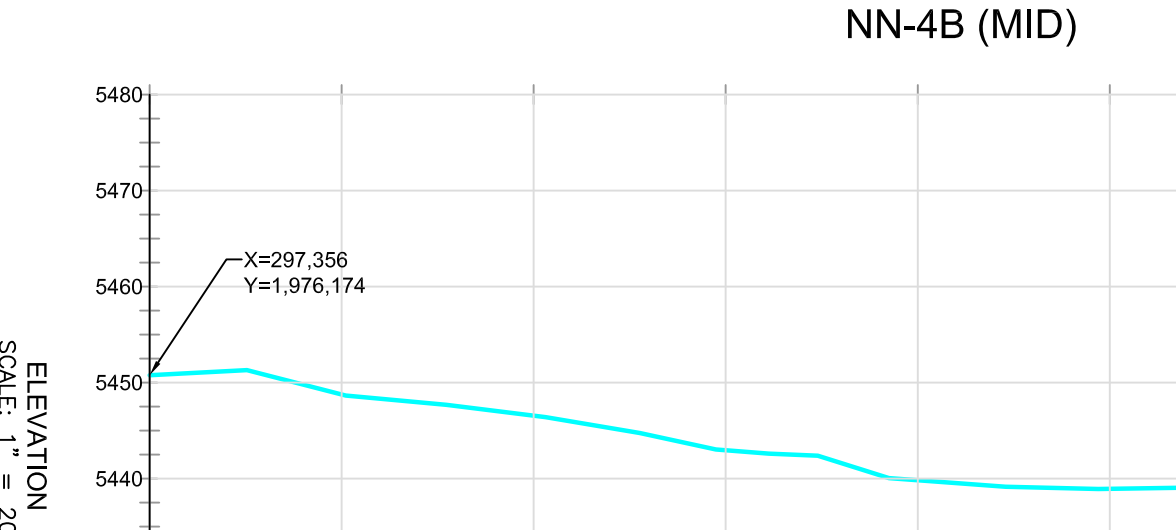
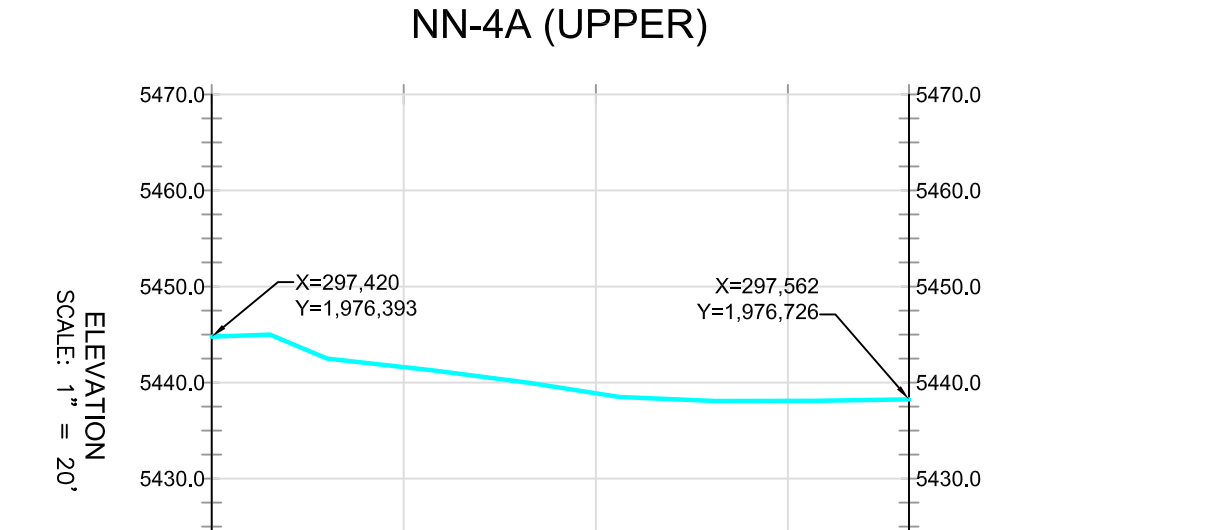
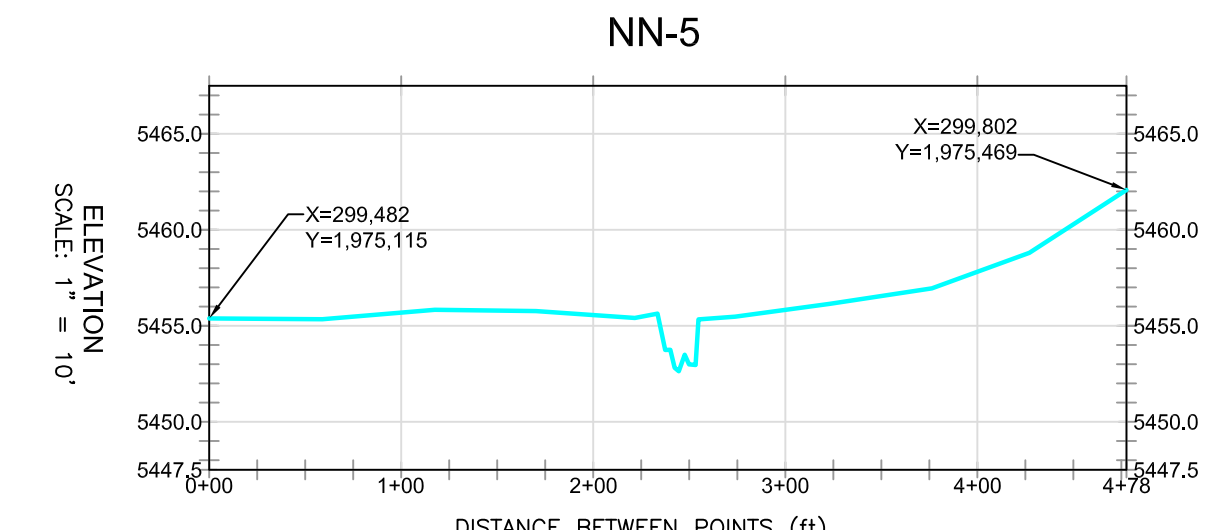
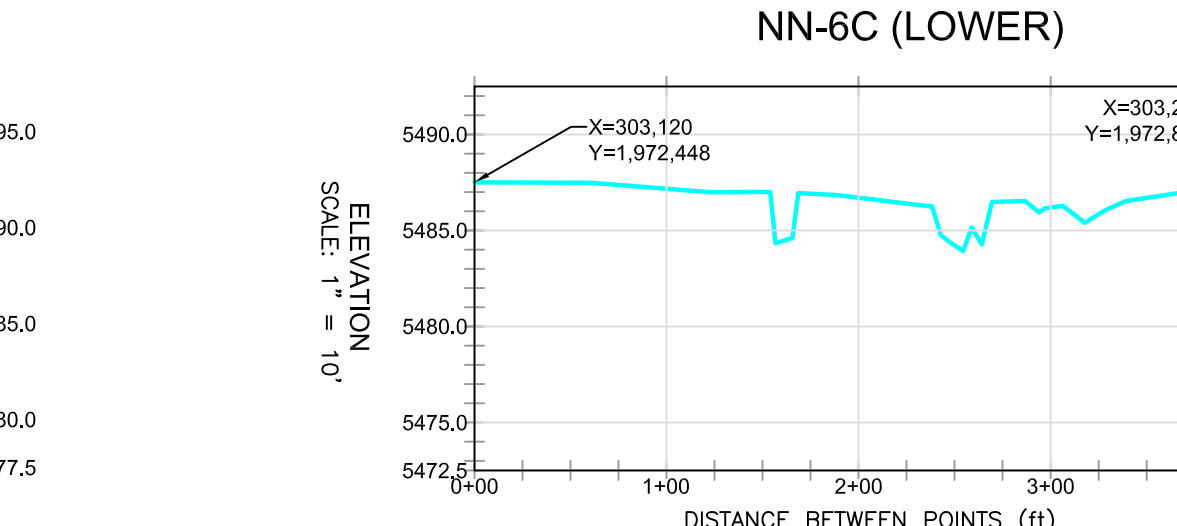
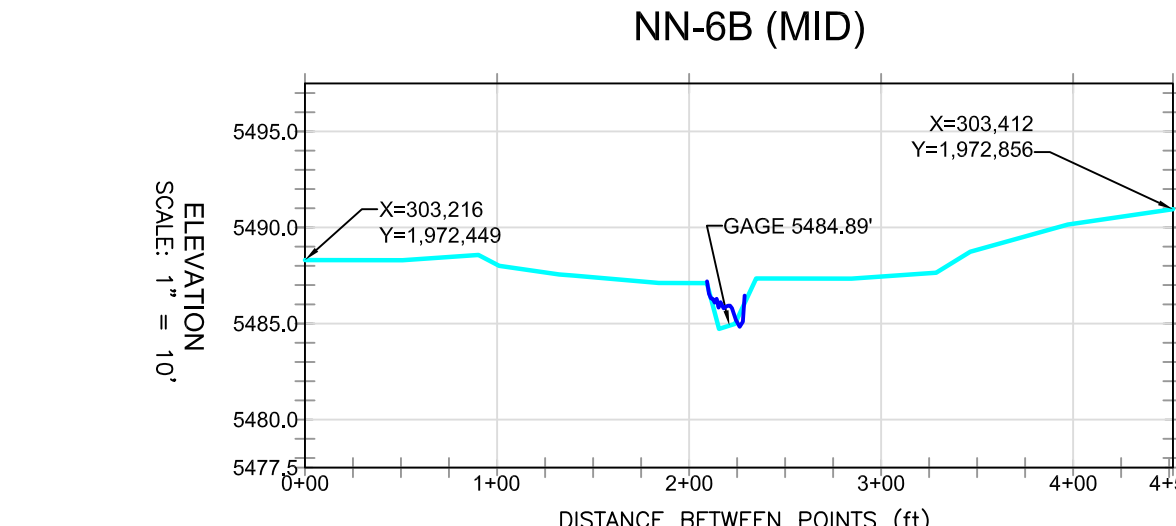
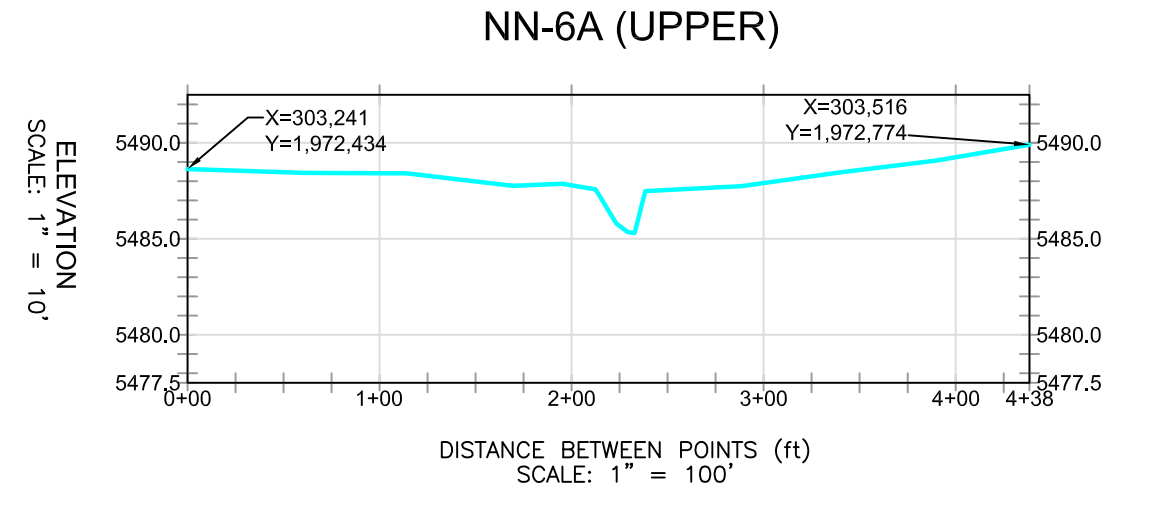
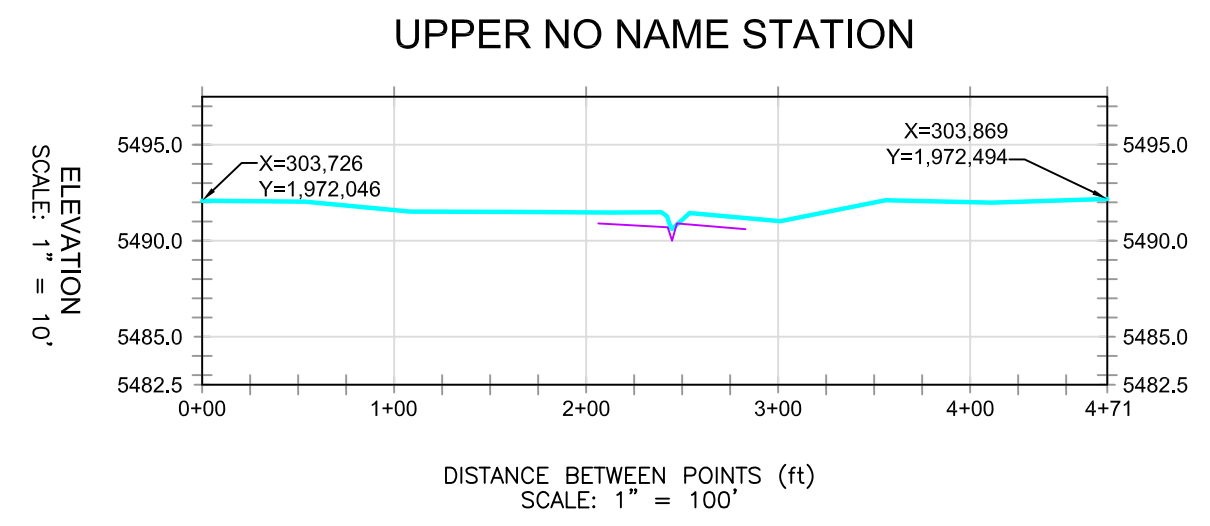
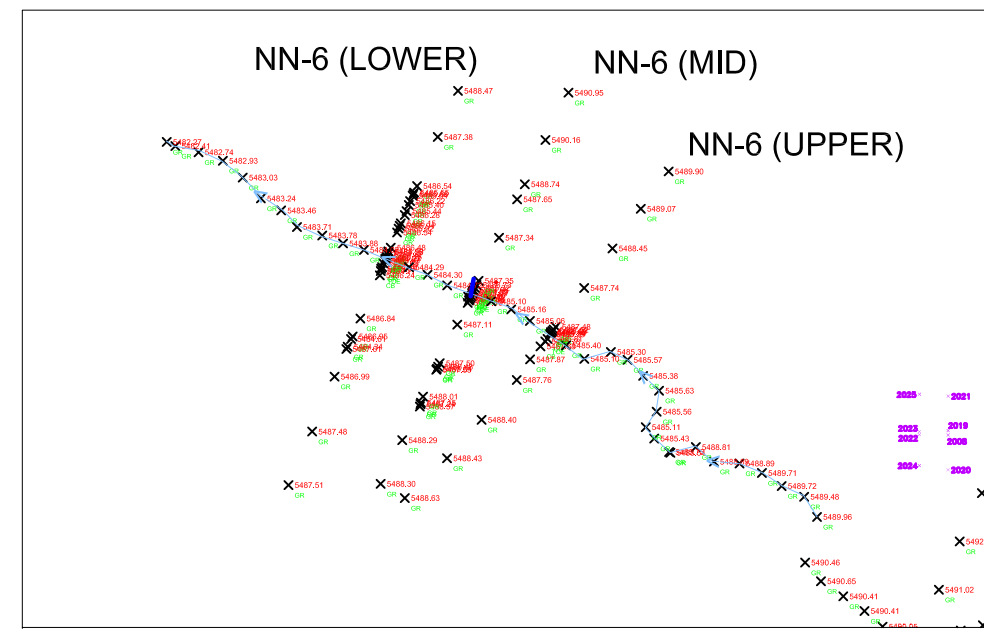
PHONE: (505) 698-4300  
FAX: (505) 698-4229

**PINABETE PERMIT**  
**LOWER NO NAME ARROYO**

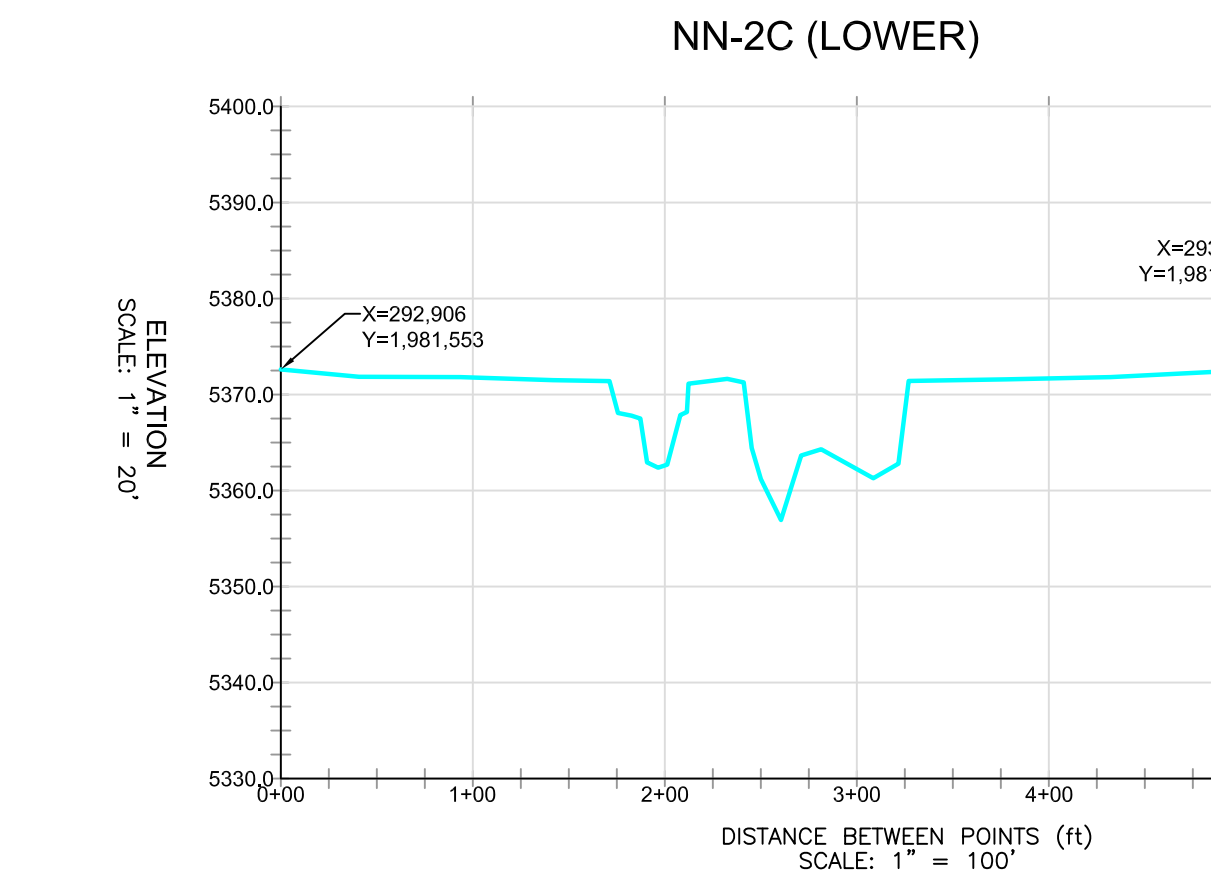
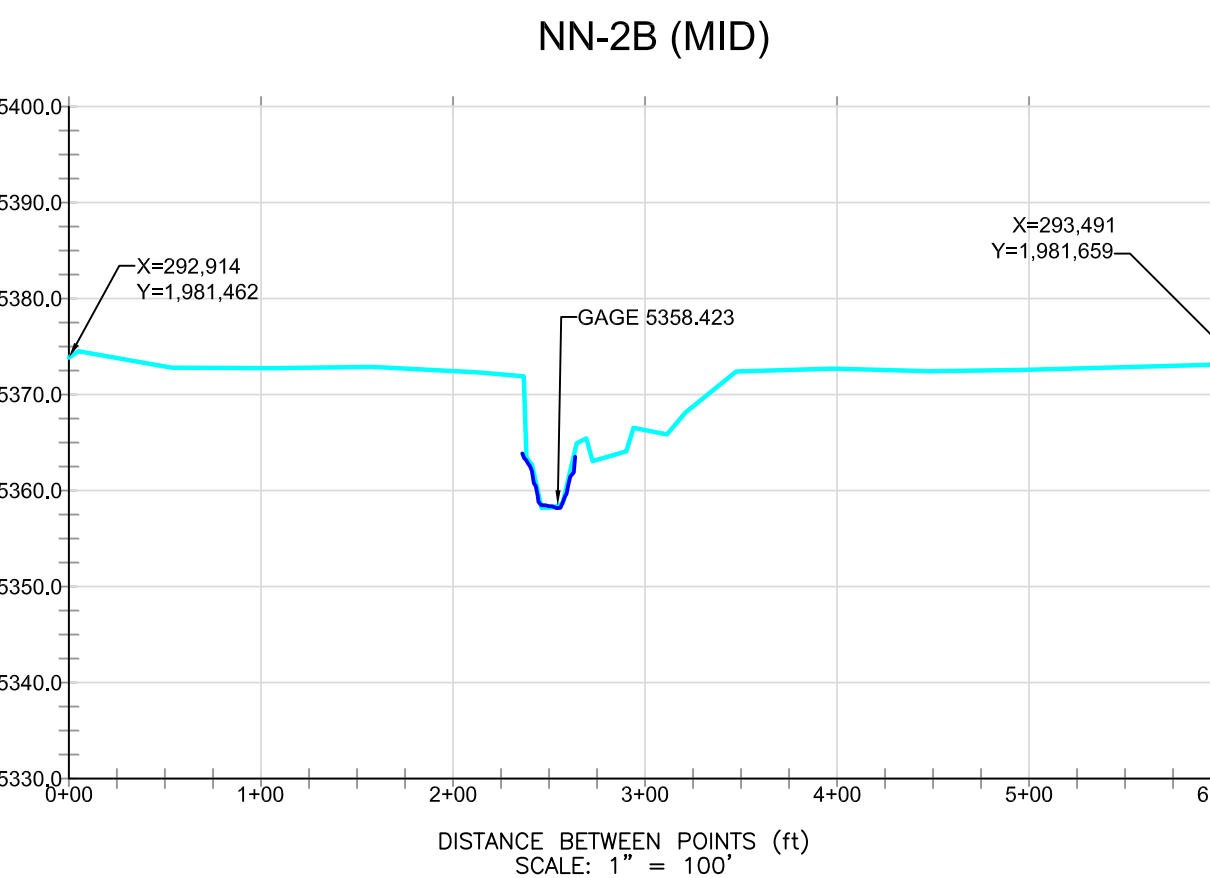
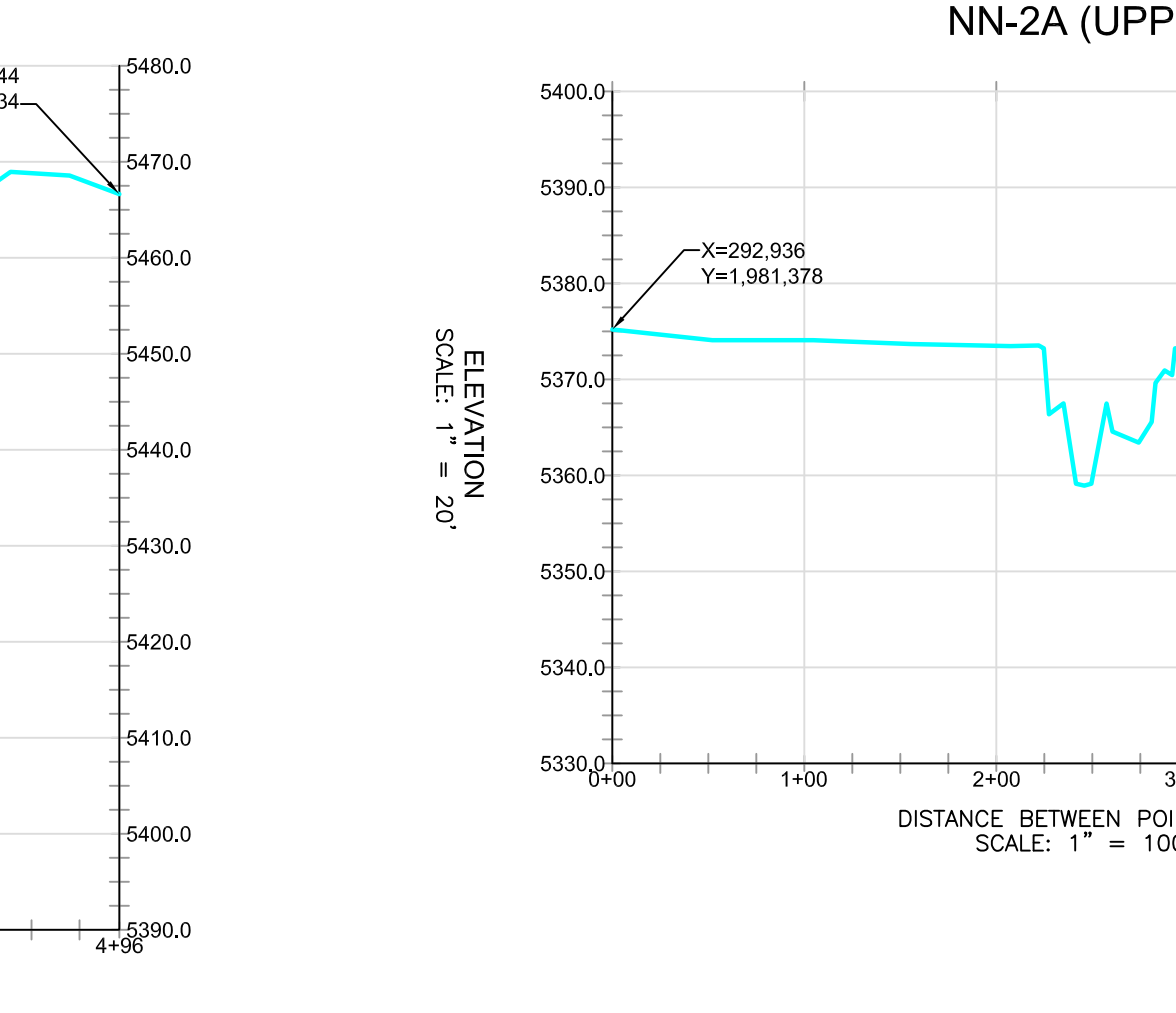
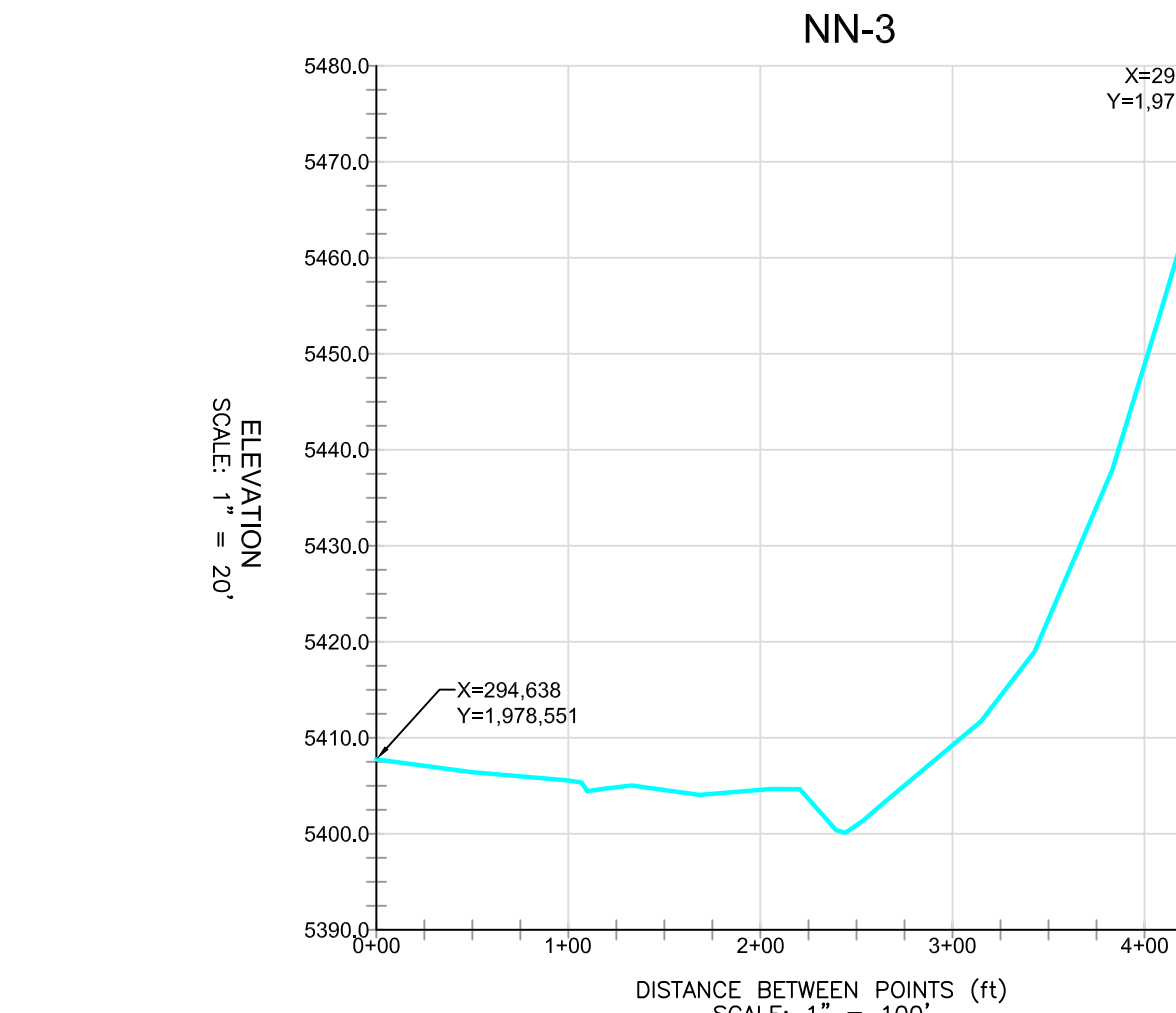
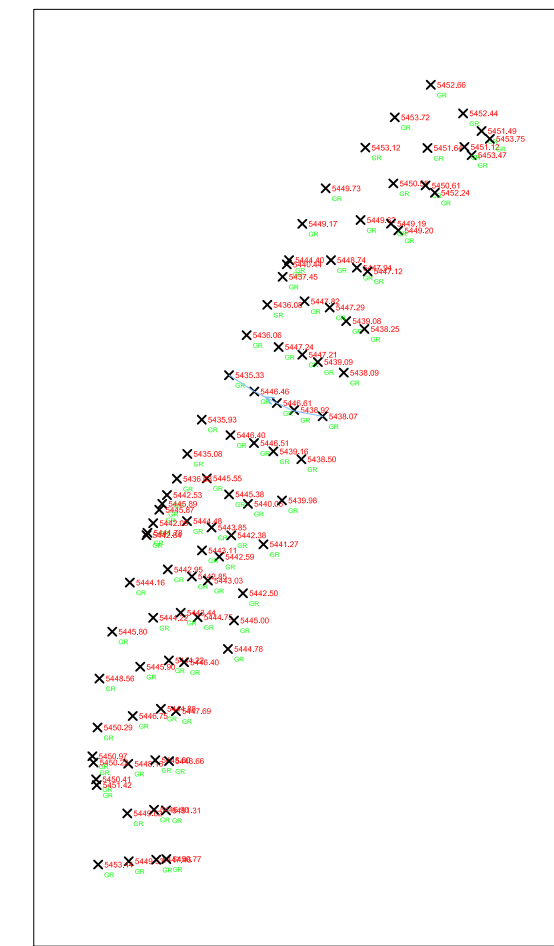
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| APPROVED BY |     | DATE     | Mar 16, 2012 |        |            |



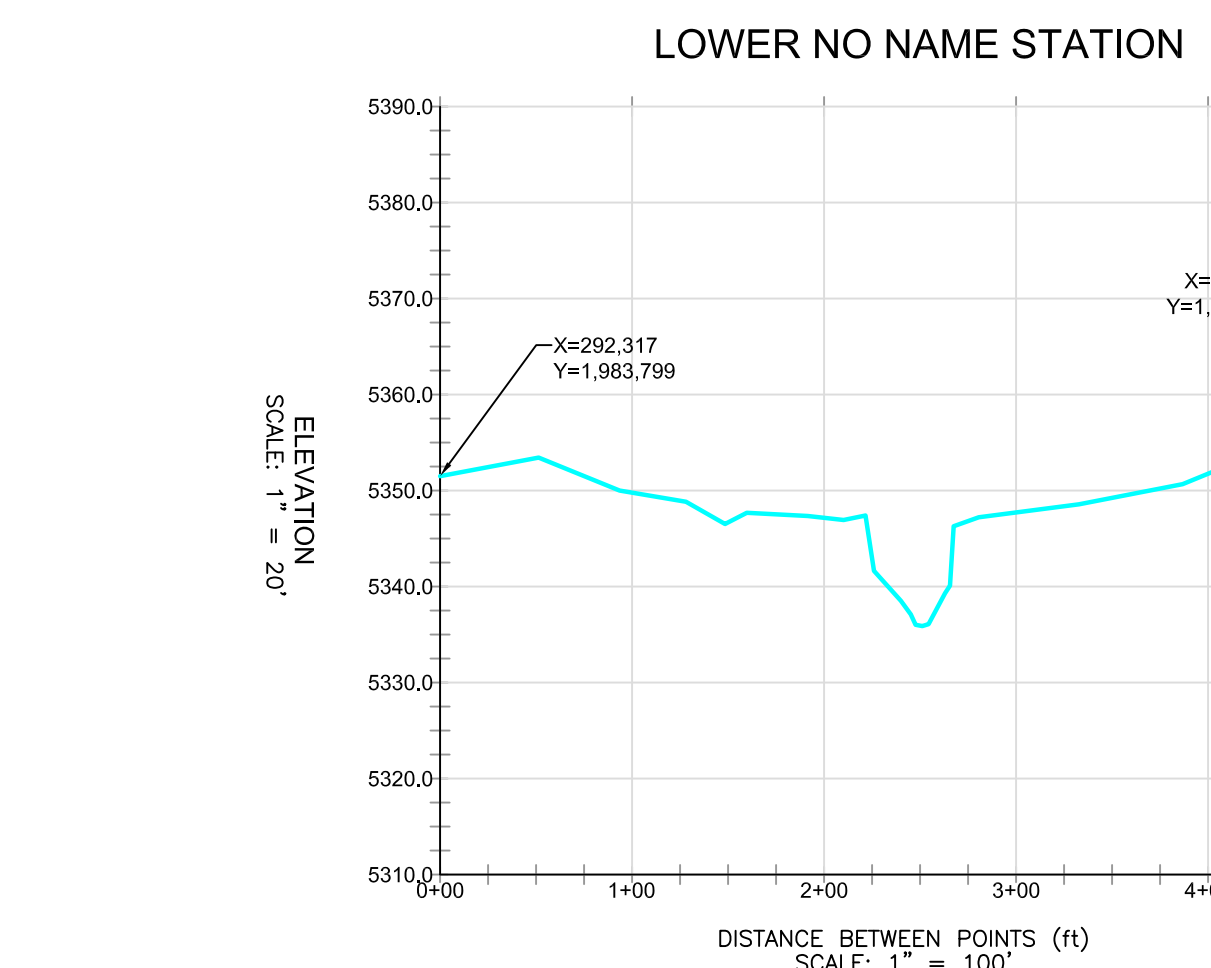
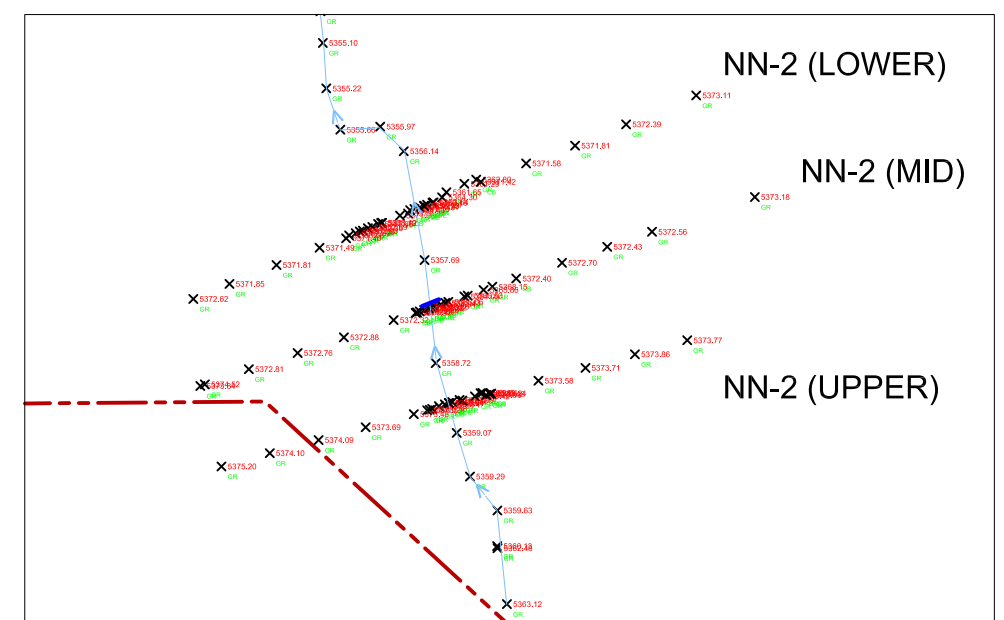
SECTIONS LOCATIONS AT  
NO NAME ARROYO NN-6  
MONITORING STATIONS



SECTIONS LOCATIONS AT  
NO NAME ARROYO NN-4  
MONITORING STATIONS



SECTIONS LOCATIONS AT  
NO NAME ARROYO NN-2  
MONITORING STATIONS

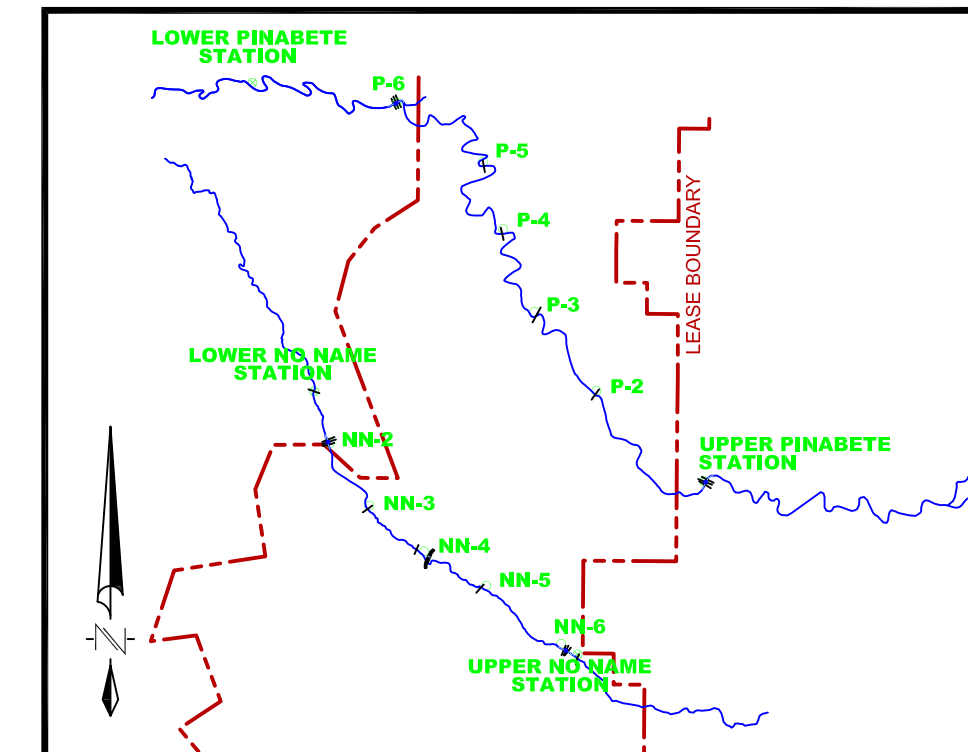


LEGEND

- 2008 SURVEYED SECTION
- 2007 SURVEYED SECTION
- 1998 SURVEYED SECTION

- NOTES
- COORDINATE DATUM IS NEW MEXICO STATE PLANE NAD 27
  - FEET WEST ZONE
  - CROSS SECTIONS LOOKING DOWNSTREAM

Site Map



|          |         |          |                               |          |            |             |
|----------|---------|----------|-------------------------------|----------|------------|-------------|
| REV. No. | DATE    | DRAWN BY | REVISION DESCRIPTION          | PREP. BY | CHECKED BY | APPROVED BY |
| 12-A     | 3/16/12 | MPD      | Submitted to OSM for Approval |          |            |             |

EXHIBIT 18.A-5  
BHP NAVAJO COAL COMPANY

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FRUITLAND, NEW MEXICO 87416

PHONE: (505) 698-4200  
FAX: (505) 698-4229

PINABETE PERMIT  
NO NAME ARROYO CROSS SECTIONS

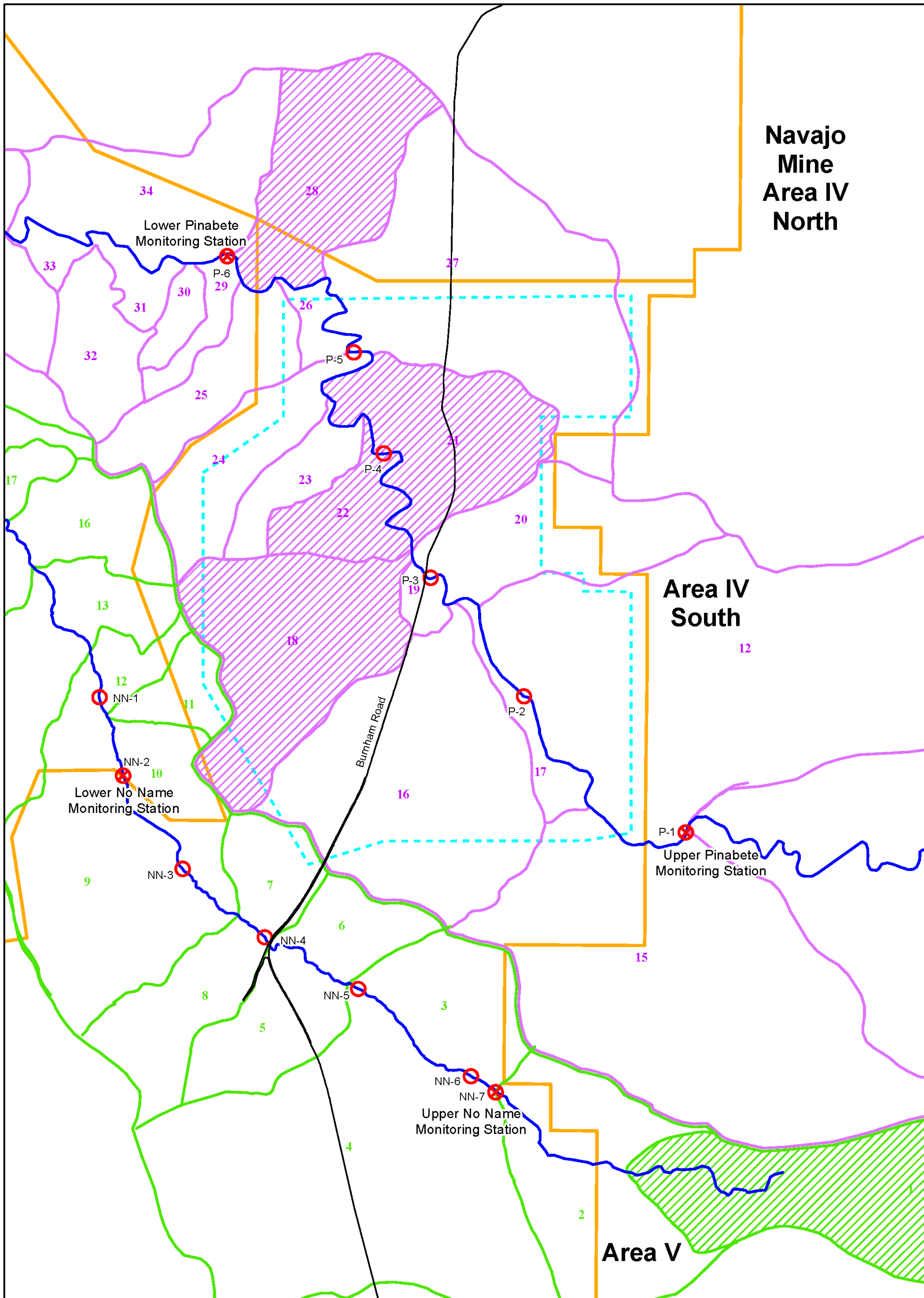
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| PREPARED BY | APO | DRAWN BY | JLS          | SCALE: | AS SHOWN |
| APPROVED BY |     | DATE     | Mar 16, 2012 |        |          |



# Navajo Mine Area IV North

# Area IV South

# Area V



**Legend**

|                       |                      |
|-----------------------|----------------------|
| No Name Basins        | Burnham Road         |
| Pinabete Basins       | AOC Surveyed Basins  |
| Stream Lines          | NavExt_LeaseBoundary |
| Survey Cross Sections | NavExt_MineBlock     |

Exhibit 18.A-6  
Field Reconnaissance Map

N  
0 1,500 3,000 Feet



## **Appendix 18.B**

SEDCAD™4 Modeling of Baseline Flood Flows and Sediment Yields



**APPENDIX 18.B**

**SEDCAD™4 MODELING OF BASELINE FLOOD FLOWS AND SEDIMENT YIELDS**

**TABLE OF CONTENTS**

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|                | <b>Runoff Modeling.....</b>   | <b>2</b>               |
|                | Subwatershed Designation and Slopes .....                                 | 2                      |
|                | Time of Concentration.....  | 2                      |
|                | Rainfall Duration, Frequency, and Distribution .....                      | 3                      |
|                | Curve Number .....  | 3                      |
|                | Hydrologic Response Class .....   | 3                      |
|                | <b>Sedimentology Evaluation .....</b>                                     | <b>3</b>               |
|                | Erodible Particle Size Distributions.....                                 | 4                      |
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|                | <b>Results .....</b>  | <b>6</b>               |
|                | Personnel .....   | 6                      |
|                | References .....  | 7                      |



**APPENDIX 18.B**

**SEDCAD™4 MODELING OF BASELINE FLOOD FLOWS AND SEDIMENT YIELDS**

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|-------------------------------|---|
| <a href="#"><u>18.B-1</u></a> | SEDCAD™ Model Input Factors Based on Erodible Particle Size Distribution Texture Class      |
| <a href="#"><u>18.B-2</u></a> | Pinabete Arroyo SEDCAD™ Model Erodible Particle Size Distribution Input                     |
| <a href="#"><u>18.B-3</u></a> | No Name Arroyo SEDCAD™ Model Erodible Particle Size Distribution Input                      |
| <a href="#"><u>18.B-4</u></a> | Cottonwood Arroyo Unnamed Tributary SEDCAD™ Model Erodible Particle Size Distribution Input |



**APPENDIX 18.B**

**SEDCAD™4 MODELING OF BASELINE FLOOD FLOWS AND SEDIMENT YIELDS**

**LIST OF EXHIBITS**

**EXHIBIT**

**NUMBER**

**EXHIBIT TITLE**

---

[18.B-1](#)

SEDCAD™4 Subwatersheds



**APPENDIX 18.B**

**SEDCAD™4 MODELING OF BASELINE FLOOD FLOWS AND SEDIMENT YIELDS**

**LIST OF ATTACHMENTS**

**ATTACHMENT**

**NUMBER            ATTACHMENT TITLE**

---

|                               |  |
|-------------------------------|--|
| <a href="#"><u>18.B-1</u></a> | Pinabete Arroyo Baseline Hydrology and Sedimentology SEDCAD™ Model Output                    |
| <a href="#"><u>18.B-2</u></a> | No Name Arroyo Baseline Hydrology and Sedimentology SEDCAD™ Model Output with Impoundment    |
| <a href="#"><u>18.B-3</u></a> | No Name Arroyo Baseline Hydrology and Sedimentology SEDCAD™ Model Output without Impoundment |
| <a href="#"><u>18.B-4</u></a> | Cottonwood Arroyo Baseline Hydrology and Sedimentology SEDCAD™ Model Output                  |
| <a href="#"><u>18.B-5</u></a> | Chaco River Unnamed Tributary Baseline Hydrology and Sedimentology SEDCAD™ Model Output      |
| <a href="#"><u>18.B-6</u></a> | Eroded and Parent Soil Particle Size Distribution Analysis February 2008 (edited March 2012) |
| <a href="#"><u>18.B-7</u></a> | Baseline K-factor Laboratory Determination January 2008                                      |



#### **SEDCAD™4 MODELING OF BASELINE FLOOD FLOWS AND SEDIMENT YIELDS**

The SEDCAD™4 (SEDCAD) hydrology model has been used to determine flood flows and sediment yields for the pre-mine baseline watersheds of Pinabete Arroyo, No Name Arroyo, and Cottonwood Arroyos. Application of the SEDCAD program involves subdividing the drainage area into subwatersheds. Designation of subwatersheds with relatively uniform soil and vegetation characteristics helps in the estimation of model parameters required by SEDCAD. Information is required for physical structures located along the channel that may affect flow and sediment routing within the stream channels. SEDCAD null structures are also established at appropriate locations along the channel network where flow and sedimentology predictions are needed.

The SEDCAD input parameters and output results for the 6-hour rainfall event at the 2-year, 10-year, 25-year, 50-year, and 100-year frequencies and the 10-year 24-hour (10yr-24hr) precipitation event for Pinabete Arroyo is provided as [Attachment 18.B-1](#) to this appendix. There are two models for pre-mine conditions on No Name Arroyo. The Burnham Road crosses No Name Arroyo in Area 4 South. The road embankment created the No Name Impoundment. As discussed in Section 18 (Water Resources), this impoundment has been used as a livestock pond. As part of this baseline evaluation, two SEDCAD models were developed for No Name Arroyo, one with the impoundment is provided as [Attachment 18.B-2](#) and one without the impoundment is provided as [Attachment 18.B-3](#). These attachments include the SEDCAD results for the 6-hour rainfall event at the 2-year, 10-year, 25-year, 50-year, and 100-year frequencies and the 10yr-24hr precipitation event. The No Name Arroyo model with the impoundment reflects current existing baseline conditions. The SEDCAD input parameters and output results are provided in [Attachment 18.B-4](#) to this appendix for Cottonwood Arroyo and in [Attachment 18.B-5](#) to this appendix for the Unnamed Tributary to Chaco River. The results for the 6-hour rainfall event at the 2-year, 10-year, 25-year, and 100-year frequencies are provided in these Appendices.

Soil erosion by water for a specific watershed is usually calculated using the well known empirical Revised Universal Soil Loss Equation (RUSLE) (Renard et al. 1997) and is given by the following expression:

$$A = RKLSCP$$

*A* is the average soil loss per unit area, expressed in units selected for *K* and the time period specified by *R*. Normal English units are tons/acre/year.

*R* is the rainfall/runoff factor, which is the number of rainfall units for rainfall energy and runoff, plus the factor for runoff from snowmelt.

*K* is the soil erodibility factor, which is the rate of soil loss per unit of *R* for a given soil on a slope of 9% with slope length of 72.6 feet (22.1 meters).



*L* is the slope length factor, which is the ratio of soil loss from a defined slope length relative to that from a slope length of 72.6 feet (22.1 meters).

*S* is the slope steepness factor, which is the ratio of soil loss from a slope with a given steepness relative to that from a 9% slope.

*C* is the cover and management factor, which is the ratio of soil loss from an area with a known cover and management. And,

*P* is the supporting conservation practice factor.

SEDCAD requires these types of inputs be developed for each watershed being analyzed. To follow is a discussion on how the necessary parameter inputs were developed and calculated for the Pinabete Mine Plan.

### **Runoff Modeling**

#### *Subwatershed Designation and Slopes*

The SEDCAD subwatershed designations and drainage configuration for the watersheds of interest are shown on [Exhibit 18.B-1](#). The subwatershed information was developed using Carlson Civil Suite 2008, AutoCAD®, and ArcGIS® software. The base mapping used to develop these subwatersheds is a combination of 10-foot contoured aerial flight and digital elevation model (DEM) data. The DEM images were based on digital raster graphics, representing U.S. Geologic Survey (USGS) 7.5 minute topographic quadrangle maps (NMRGIS 2009 and USGS 2009). All DEM analysis was performed utilizing the Spatial Analyst extension for ArcGIS® on DEM images projected to the North American Datum of 1927- State Plane New Mexico West coordinate system and in standard units (feet) of measure.

A more detailed analysis was prepared for subwatersheds within the lease boundary because they will be influenced by mining and reclamation activities. The 11.5-square mile (sq mi) No Name Arroyo was divided into 19 subwatersheds. The 60.3-sq mi Pinabete Arroyo watershed was divided into 52 subwatersheds as shown on [Exhibit 18.B-1](#). The 79.8-sq mi drainage of Cottonwood Arroyo was divided into 113 subwatersheds ([Exhibit 18.B-1](#)). Subwatershed parameters required by the SEDCAD program were determined as described below. The unnamed tributary to the Chaco River having a watershed area of only 0.45 sq mi was divided into one subwatershed ([Exhibit 18.B-1](#)).

#### *Time of Concentration*

The time of concentration for each subwatershed was calculated by the SEDCAD program from the length and slope of the longest flow path that was input from the topographic map using AutoCAD® software.



#### *Rainfall Duration, Frequency, and Distribution*

For evaluation purposes, peak flows were estimated for the 6-hour rainfall event at the 2-year, 10-year, 25-year, 50-year, and 100-year frequencies and the 10yr-24hr storm event. Storm precipitation values provided in Section 18 (Water Resources) for the various return periods were obtained from the National Oceanic and Atmospheric Administration (NOAA) online frequency estimates (Bonnin et al. 2006) for the location of Area 4 South from Atlas 14, New Mexico to represent precipitation conditions within the Cottonwood Arroyo, No Name Arroyo and Pinabete Arroyo watersheds. A Soil Conservation Service (SCS) Type II-70 rainfall distribution was applied to all storms, which is consistent with the rainfall distribution used by Navajo Mine.

#### *Curve Number*

Hydrologic group for the various soil types within each watershed was obtained from the Soil Survey of San Juan County, Eastern Part (Keetch 1980) for lands outside the BNCC lease area and from the baseline soils study (Section 14, Soil) for lands inside the BNCC lease area. These soil surveys classified soil types into four hydrologic group ratings: A, B, C, and D. Runoff curve numbers were developed from the “SEDCAD<sup>TM</sup>4 User Manual” and software (Warner et al. 1998) and from SCS Engineering Division Technical Release Urban Hydrology for Small Watersheds, Table 2-2d, page 2-8, "Runoff curve numbers for arid and semiarid rangelands" (USDA 1986), for each hydrologic soil group assuming a land use/condition between “Herbaceous” and “Desert Shrub” each with a poor cover condition. From this information, runoff curve numbers were derived for each of the four surface texture types. The curve numbers derived for each texture type are summarized in [Table 18.B-1](#). The runoff curve number for a subwatershed was calculated as a weighted average based on the overall surface texture proportions determined for that watershed.

#### *Hydrologic Response Class*

A medium hydrologic response class was applied to all subwatersheds. The hydrologic response class determines the shape of the unit hydrograph used in the SEDCAD model. The medium class is typical of agricultural and semiarid rangeland conditions and was determined to be representative of site conditions.

#### **Sedimentology Evaluation**

The SEDCAD sedimentology analysis relies on a rainfall factor, erodible particle size data, a soil’s erodibility factor, the watershed’s topography and the resulting distance of overland flow, cover values and cultural practices at the site. Data for all of these parameters are entered for each subwatershed within the model.



### *Erodible Particle Size Distributions*

BHP Navajo Coal Company (BNCC) obtained information about soils within and adjacent to the Pinabete Mine Plan permit area (permit area) as part of the rigorous baseline soils investigation. This information came from site-specific studies (Section 14, Soil) and regional soil survey data (Keetch 1980). Soil mapping units were categorized into four surface textures to provide a basis for developing values for sedimentology parameters used in the SEDCAD model. These surface texture classes included: fine, fine loamy, coarse loamy, and sandy. ArcGIS® software was used to overlay the pre-mine subwatersheds with the baseline soils information to produce a database file that contained the areas corresponding to each soil type within each subwatershed. Textures were linked to the soil types, and an evaluation of the percentage of each texture within each watershed was calculated as a function of area. This surface texture distribution was used to calculate the remaining factors needed for SEDCAD modeling.

Erodible particle size distributions (EPSD) were developed for each of the four surface texture classes in a study conducted by Dr. Richard Warner of the Biosystems and Agricultural Engineering Department at the University of Kentucky ([Attachment 18.B-6](#)). The SEDCAD modeling software has a maximum of 20 ESPD per watershed model. For some watershed models, there were more subwatersheds than the number of ESPDs allowed by SEDCAD. In these cases, average or representative EPSDs were used. This data was entered into the model, and the specific particle size distribution referenced for each structure. These particle size distributions are specific to each watershed model and are uniquely numbered. Due to formatting difficulties with the SEDCAD output, BNCC has reproduced the particle size distributions for the major model runs in supplemental tables to completely document the assumptions incorporated by the sedimentology analysis. Twenty particle size distributions were utilized to represent Pinabete Arroyo subwatershed conditions as summarized on [Table 18.B-2](#). The 15 particle size distributions for No Name Arroyo are summarized on [Table 18.B-3](#). The five 5 particle size distributions for tributaries to Cottonwood Arroyo are summarized on [Table 18.B-4](#).

### *Erodibility Factor (K)*

The RUSLE K-factor is a measure of a soil's resistance to erosive powers of rainfall energy and runoff. Practically, soil erodibility is an integration of the impacts of rainfall and runoff on soil loss for a given soil. Experimentally, soil loss erodibility is the soil loss per unit rainfall index on a standard erosion plot. K-factor can be obtained through three different sources: published data, the Wischmeier nomograph developed from data collected on 55 different Midwestern USA agricultural soils, or the analytical approximation of the Wischmeier nomograph (Renard et al. 1997). Inter-Mountain Labs (IML) determined the K-factor for the four soil texture types using the analytical approximation of the Wischmeier nomograph, which is given by the following relationship:



$$K = \frac{2.1 \times 10^{-4} (12 - OM) M^{1.14} + 3.25 (S_1 - 2) + 2.5 (P_1 - 3)}{100}$$

$K$  is the soil erodibility factor in tons per acre per unit rainfall index (ton/ac/unit rainfall)

Unit rainfall index is in hundreds of feet · tons-force · inches per hour (100s ft tonsf in/hr)

$OM$  is the percentage organic matter,

$P_1$  is the permeability index (1 to 4),

$S_1$  is the soil structure index (1 to 6)

$M$  is a parameter that depends on the parent particle size distribution and is given by the following and is valid for values of  $\%MS + \%VFS$  less than 70:

$$M = (\%MS + \%VFS)(100 - \%CL)$$

$\%CL$  is percentage clay (size < 0.002 mm in diameter),

$\%MS$  is percentage silt (0.002 – 0.05 mm) and

$\%VFS$  is percentage very fine sand (0.05 – 0.1 mm).

The percentages clay, silt, and very fine sand are obtained directly from the parent particle size distribution, using American Society for Testing and Materials (ASTM) D422 – “Standard Test Method for Particle-Size Analysis of Soils” (ASTM 2000). The percentage of organic matter ( $OM$ ) was determined using the Wakley-Black (WB) method (Nelson and Sommers 1982). IML also determined  $OM$  using the loss on ignition (LOI) described by Nelson and Sommers (1996). The results of these analyses are provided in [Attachment 18.B-7](#). The K-factors for each texture type are summarized in [Table 18.B-1](#). The K-factor for a subwatershed was then calculated as a weighted average based on overall the surface texture distribution determined for that watershed.

#### *Cover Factor (C)*

Representative vegetative cover and surface cover information was derived for each of the EPSD texture classes from baseline vegetation surveys (Section 15, Vegetation). This information was integrated with the EPSD texture class information using ArcGIS® to generate canopy cover and surface cover values for each of the four soil textures. Between 104 and 131 transects were used to determine the mean percent total vegetative cover (canopy cover) and mean percent surface cover for each of the four EPSD texture classes. The canopy cover and surface cover derived for each texture type are summarized in [Table 18.B-1](#). The canopy cover versus surface cover tables for rangeland contained within SEDCAD were expanded through linear interpolation to provide cover factors for subwatersheds based on the surface texture distribution. The average cover values were calculated for subwatersheds as a weighted average based on area. These values were used to determine the cover factor through interpolation in [Table 18.B-1](#).



**Results**

The results of the hydrology and sedimentology models for each of the watersheds are provided as attachments. Each attachment contains the summary output from SEDCAD including: storm information, structure networking, structure routing details, EPSD for each structure, subwatershed hydrology details, subwatershed sedimentology details, subwatershed time of concentration details, subwatershed Muskingum routing details. The subwatershed structure networking is shown on [Exhibit 18.B-1](#). The attachments also contain structure summaries for the following storm events: 10-year 24-hour (10yr-24hr), 2yr-6hr, 10yr-6hr, 25yr-6hr, 50yr-6hr, and 100yr-6hr.

The Pinabete Arroyo summary is presented in [Attachment 18.B-1](#). The No Name Arroyo summary without the impoundment is presented in [Attachment 18.B-3](#). The summary for No Name Arroyo with the impoundment, the current baseline condition, is presented in [Attachment 18.B-2](#). The Cottonwood Arroyo results are presented in [Attachment 18.B-4](#). The summary for Chaco River unnamed tributary is presented in [Attachment 18.B-5](#).

Peak flows and sediment yields calculated from the aforementioned SEDCAD models for the 6-hour rainfall events on 2-year, 10-year, 25-year and 100-year frequencies are reported in Section 18.1 (Surface Water Resources) for each of the surface water monitoring stations on Pinabete and No Name Arroyos, for the South Fork of Cottonwood Arroyo, Cottonwood Arroyo at monitoring station CNS-1, Cottonwood Arroyo at the confluence and the unnamed tributaries to Chaco just downstream of the permit boundary.

*Personnel*

Persons or organizations responsible for data collection, analysis, and preparation of this appendix:

|                         |                           |
|-------------------------|---------------------------|
| Kent Applegate          | Dr. Richard Warner        |
| Daphne Place            | University of Kentucky    |
| Leonard Raymond         |                           |
| Matt Owens              | Norwest Corporation       |
| BHP Navajo Coal Company | Denver, CO                |
|                         | Inter-Mountain Labs, Inc. |
|                         | Sheridan, WY              |



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Table 18.B-1 SEDCAD™ Model Input Factors Based on Erodible Particle Size Distribution Texture Class

| EPSD texture | K-factor | Run-off      |              |               |
|--------------|----------|--------------|--------------|---------------|
|              |          | curve number | Canopy cover | Surface cover |
| Fine         | 0.20     | 93.0         | 4.7          | 30.8          |
| Fine loamy   | 0.27     | 92.4         | 9.2          | 18.1          |
| Coarse loamy | 0.10     | 81.9         | 14.5         | 7.9           |
| Sandy        | 0.20     | 65.6         | 13.9         | 1.6           |



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Table 18.B-2 Pinabete Arroyo SEDCAD™ Model Erodible Particle Size Distribution Input

| EPSD Designation<br>Diameter (mm) | P1      | P2      | P3      | P4      | P5      | P6      | P7      | P8      | P9      | P10     |
|-----------------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 0.450                             | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 |
| 0.250                             | 85.529  | 83.954  | 83.494  | 79.684  | 74.336  | 71.800  | 68.824  | 73.040  | 66.130  | 59.234  |
| 0.150                             | 72.267  | 70.070  | 68.714  | 64.718  | 55.514  | 53.158  | 47.671  | 50.320  | 47.750  | 40.272  |
| 0.075                             | 58.134  | 56.187  | 54.477  | 51.673  | 42.977  | 40.816  | 35.579  | 35.798  | 36.084  | 33.795  |
| 0.01585                           | 49.962  | 48.376  | 46.844  | 44.689  | 37.721  | 35.600  | 31.445  | 31.104  | 31.122  | 31.492  |
| 0.01000                           | 38.953  | 37.808  | 36.471  | 35.083  | 30.403  | 28.065  | 25.380  | 24.310  | 23.407  | 28.022  |
| 0.005012                          | 9.675   | 9.683   | 9.177   | 10.018  | 9.205   | 9.529   | 8.929   | 6.708   | 10.343  | 13.538  |
| 0.001995                          | 6.279   | 6.204   | 5.875   | 6.237   | 5.303   | 5.591   | 4.938   | 3.770   | 6.209   | 7.108   |
| 0.001000                          | 6.010   | 5.917   | 5.567   | 5.908   | 4.905   | 5.155   | 4.462   | 3.276   | 5.698   | 6.676   |
| 0.000398                          | 4.942   | 4.914   | 4.659   | 5.035   | 4.387   | 4.686   | 4.216   | 3.184   | 5.329   | 6.156   |

Note: Values reported as percent of sample passing through sieve with corresponding diameter  
EPSD- erodible particle size distribution



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Table 18.B-2 (Continued)

| EPSD Designation<br>Diameter (mm) | P11     | P12     | P13     | P14     | P15     | P16     | P17     | P18     | P19     | P20     |
|-----------------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 0.450                             | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 |
| 0.250                             | 71.599  | 65.531  | 66.688  | 69.479  | 71.446  | 76.546  | 69.115  | 68.866  | 61.049  | 69.805  |
| 0.150                             | 57.036  | 45.088  | 46.416  | 50.980  | 55.482  | 60.175  | 48.743  | 45.562  | 42.198  | 50.039  |
| 0.075                             | 47.507  | 34.380  | 34.657  | 38.320  | 44.594  | 46.743  | 36.650  | 33.437  | 33.563  | 36.737  |
| 0.01585                           | 42.049  | 30.640  | 30.363  | 32.920  | 39.040  | 40.133  | 32.221  | 30.098  | 30.211  | 31.517  |
| 0.01000                           | 34.448  | 25.007  | 23.816  | 24.755  | 31.086  | 30.717  | 25.703  | 25.355  | 24.943  | 23.611  |
| 0.005012                          | 12.666  | 10.180  | 9.557   | 9.532   | 11.375  | 9.459   | 9.189   | 8.126   | 12.221  | 8.675   |
| 0.001995                          | 7.405   | 5.608   | 5.458   | 5.794   | 6.757   | 5.929   | 5.194   | 4.149   | 6.769   | 5.233   |
| 0.001000                          | 7.069   | 5.126   | 4.956   | 5.304   | 6.368   | 5.532   | 4.723   | 3.674   | 6.286   | 4.726   |
| 0.000398                          | 6.144   | 4.829   | 4.693   | 4.918   | 5.635   | 4.866   | 4.420   | 3.561   | 5.868   | 4.456   |

Note: Values reported as percent of sample passing through sieve with corresponding diameter  
EPSD- erodible particle size distribution



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Table 18.B-3 No Name Arroyo SEDCAD™ Model Erodible Particle Size Distribution Input

| EPSD Designation<br>Diameter (mm) | N1      | N2      | N3      | N4      | N5      | N6      | N7      | N8      | N9      | N10     |
|-----------------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 0.450                             | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 |
| 0.250                             | 67.238  | 70.939  | 74.655  | 74.155  | 77.281  | 75.578  | 77.393  | 77.993  | 77.038  | 78.922  |
| 0.150                             | 49.361  | 52.171  | 54.870  | 54.074  | 57.254  | 54.286  | 57.877  | 59.294  | 57.936  | 60.447  |
| 0.075                             | 37.563  | 37.728  | 38.718  | 39.358  | 43.405  | 40.591  | 43.197  | 45.545  | 44.741  | 46.776  |
| 0.01585                           | 32.342  | 31.597  | 32.157  | 33.572  | 37.974  | 35.722  | 37.191  | 39.656  | 39.265  | 40.830  |
| 0.01000                           | 24.314  | 22.169  | 22.246  | 25.073  | 30.556  | 29.049  | 28.724  | 31.575  | 31.827  | 32.779  |
| 0.005012                          | 10.387  | 8.316   | 6.741   | 7.496   | 7.842   | 7.567   | 7.539   | 8.344   | 8.573   | 8.418   |
| 0.001995                          | 6.291   | 5.386   | 4.536   | 4.624   | 4.493   | 4.182   | 4.580   | 4.932   | 4.921   | 4.949   |
| 0.001000                          | 5.795   | 4.854   | 4.004   | 4.140   | 4.097   | 3.764   | 4.153   | 4.551   | 4.545   | 4.587   |
| 0.000398                          | 5.371   | 4.575   | 3.806   | 3.867   | 3.665   | 3.448   | 3.748   | 4.009   | 4.014   | 3.998   |

Note: Values reported as percent of sample passing through sieve with corresponding diameter  
EPSD- erodible particle size distribution



Table 18.B-3 (Continued)

| EPSD Designation<br>Diameter (mm) | N11     | N12     | N13     | N14     | N15     |
|-----------------------------------|---------|---------|---------|---------|---------|
| 0.450                             | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 |
| 0.250                             | 76.892  | 78.922  | 76.672  | 68.115  | 77.333  |
| 0.150                             | 57.043  | 60.447  | 56.704  | 49.351  | 57.313  |
| 0.075                             | 43.798  | 46.776  | 42.929  | 37.400  | 44.056  |
| 0.01585                           | 38.581  | 40.830  | 37.514  | 32.436  | 38.895  |
| 0.01000                           | 31.549  | 32.779  | 30.059  | 24.922  | 32.007  |
| 0.005012                          | 8.280   | 8.418   | 7.941   | 9.925   | 8.186   |
| 0.001995                          | 4.655   | 4.949   | 4.571   | 5.882   | 4.556   |
| 0.001000                          | 4.275   | 4.587   | 4.167   | 5.396   | 4.184   |
| 0.000398                          | 3.798   | 3.998   | 3.743   | 5.013   | 3.706   |

Note: Values reported as percent of sample passing through sieve with corresponding diameter  
EPSD- erodible particle size distribution



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Table 18.B-4 Cottonwood Arroyo Unnamed Tributary SEDCAD™ Model Erodible Particle Size Distribution Input

| EPSD Designation<br>Diameter (mm) | CW1     | CW2     | CW3     | CW4     | CW5     |
|-----------------------------------|---------|---------|---------|---------|---------|
| 0.450                             | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 |
| 0.250                             | 71.002  | 79.759  | 73.724  | 79.290  | 83.334  |
| 0.150                             | 52.517  | 62.156  | 54.007  | 60.839  | 68.417  |
| 0.075                             | 40.991  | 48.658  | 41.754  | 47.304  | 53.993  |
| 0.01585                           | 36.096  | 42.458  | 36.968  | 41.409  | 46.327  |
| 0.01000                           | 29.101  | 34.107  | 30.394  | 33.504  | 35.855  |
| 0.005012                          | 10.110  | 8.789   | 9.084   | 8.485   | 9.027   |
| 0.001995                          | 5.803   | 5.220   | 5.060   | 4.944   | 5.817   |
| 0.001000                          | 5.384   | 4.878   | 4.663   | 4.594   | 5.499   |
| 0.000398                          | 4.868   | 4.198   | 4.196   | 3.982   | 4.619   |

Note: Values reported as percent of sample passing through sieve with corresponding diameter  
EPSD- erodible particle size distribution

## **Attachment 18.B-1**

Pinabete Arroyo Baseline Hydrology and Sedimentology SEDCAD™ Model Output



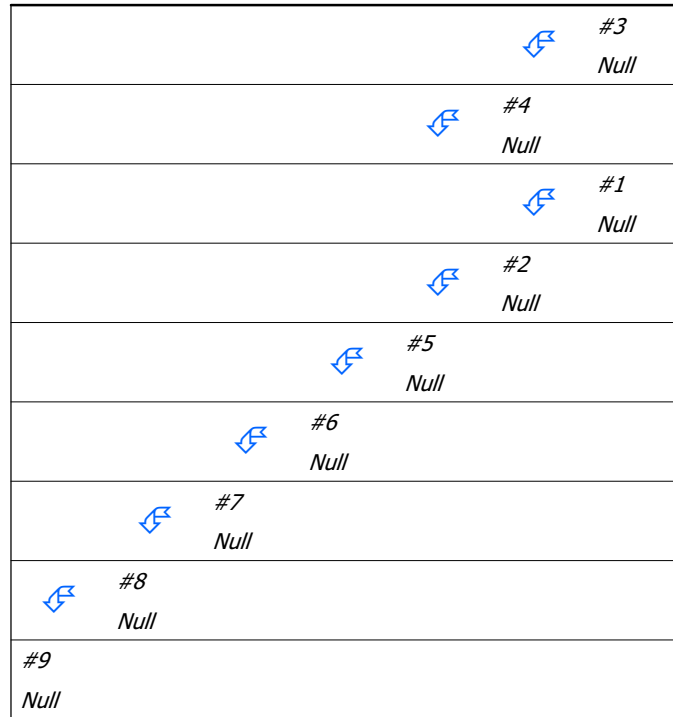
***General Information***

***Storm Information:***

|                 |               |
|-----------------|---------------|
| Storm Type:     | Type II-70    |
| Design Storm:   | 10 yr - 24 hr |
| Rainfall Depth: | 1.700 inches  |

### Structure Networking:

| Type | Stru # | (flows into) | Stru # | Musk. K (hrs) | Musk. X | Description     |
|------|--------|--------------|--------|---------------|---------|-----------------|
| Null | #1     | ==>          | #2     | 1.674         | 0.331   |                 |
| Null | #2     | ==>          | #5     | 4.188         | 0.295   |                 |
| Null | #3     | ==>          | #4     | 1.961         | 0.319   |                 |
| Null | #4     | ==>          | #5     | 3.103         | 0.304   |                 |
| Null | #5     | ==>          | #6     | 1.300         | 0.273   |                 |
| Null | #6     | ==>          | #7     | 0.995         | 0.281   | EAST LEASE BNDY |
| Null | #7     | ==>          | #8     | 2.793         | 0.277   |                 |
| Null | #8     | ==>          | #9     | 2.630         | 0.259   | WEST LEASE BNDY |
| Null | #9     | ==>          | End    | 0.000         | 0.000   |                 |



### Structure Routing Details:

| Stru #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 8. Large gullies, diversions, and low flowing streams | 1.24      | 250.00           | 20,136.00         | 3.34           | 1.674        |
| <b>#1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.674</b> |
| #2        | 8. Large gullies, diversions, and low flowing streams | 0.67      | 245.00           | 36,791.00         | 2.44           | 4.188        |
| <b>#2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>4.188</b> |



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| Stru #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #3        | 8. Large gullies, diversions, and low flowing streams | 0.99      | 210.00           | 21,118.00         | 2.99           | 1.961        |
| <b>#3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.961</b> |
| #4        | 8. Large gullies, diversions, and low flowing streams | 0.77      | 227.00           | 29,388.00         | 2.63           | 3.103        |
| <b>#4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.103</b> |
| #5        | 8. Large gullies, diversions, and low flowing streams | 0.47      | 45.00            | 9,601.00          | 2.05           | 1.300        |
| <b>#5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.300</b> |
| #6        | 8. Large gullies, diversions, and low flowing streams | 0.54      | 42.00            | 7,845.00          | 2.19           | 0.995        |
| <b>#6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.995</b> |
| #7        | 8. Large gullies, diversions, and low flowing streams | 0.49      | 105.00           | 21,218.00         | 2.11           | 2.793        |
| <b>#7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.793</b> |
| #8        | 8. Large gullies, diversions, and low flowing streams | 0.37      | 64.00            | 17,238.00         | 1.82           | 2.630        |
| <b>#8</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.630</b> |

## ***Particle Size Distribution(s) at Each Structure***

### ***Structure #3:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 99.259%  |
| 0.0750    | 91.911%  |
| 0.0159    | 88.676%  |
| 0.0100    | 74.957%  |
| 0.0050    | 29.096%  |
| 0.0020    | 16.176%  |
| 0.0010    | 14.669%  |
| 0.0004    | 13.838%  |

### ***Structure #4:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 97.132%  |
| 0.0159    | 92.310%  |
| 0.0100    | 80.309%  |
| 0.0050    | 32.210%  |
| 0.0020    | 18.271%  |
| 0.0010    | 16.676%  |
| 0.0004    | 15.488%  |

### ***Structure #1:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 99.764%  |
| 0.0159    | 92.546%  |



| Size (mm) | In/Out  |
|-----------|---------|
| 0.0100    | 78.308% |
| 0.0050    | 26.859% |
| 0.0020    | 15.680% |
| 0.0010    | 14.425% |
| 0.0004    | 13.154% |

## ***Structure #2:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 100.000% |
| 0.0159    | 96.270%  |
| 0.0100    | 86.845%  |
| 0.0050    | 31.346%  |
| 0.0020    | 18.868%  |
| 0.0010    | 17.610%  |
| 0.0004    | 15.515%  |

## ***Structure #5:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 98.899%  |
| 0.0159    | 97.137%  |
| 0.0100    | 86.893%  |
| 0.0050    | 30.817%  |
| 0.0020    | 18.355%  |
| 0.0010    | 17.054%  |
| 0.0004    | 15.188%  |

## ***Structure #6 (EAST LEASE BNDY):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 100.000% |
| 0.0159    | 100.000% |
| 0.0100    | 98.333%  |

| Size (mm) | In/Out  |
|-----------|---------|
| 0.0050    | 35.089% |
| 0.0020    | 20.966% |
| 0.0010    | 19.497% |
| 0.0004    | 17.329% |

## ***Structure #7:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 100.000% |
| 0.0159    | 99.658%  |
| 0.0100    | 99.268%  |
| 0.0050    | 36.673%  |
| 0.0020    | 21.873%  |
| 0.0010    | 20.339%  |
| 0.0004    | 18.093%  |

## ***Structure #8 (WEST LEASE BNDY):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 99.583%  |
| 0.0750    | 97.493%  |
| 0.0159    | 96.053%  |
| 0.0100    | 93.300%  |
| 0.0050    | 41.006%  |
| 0.0020    | 24.427%  |
| 0.0010    | 22.693%  |
| 0.0004    | 20.240%  |

## ***Structure #9:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 97.786%  |
| 0.0159    | 95.993%  |
| 0.0100    | 93.435%  |
| 0.0050    | 41.510%  |



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| Size (mm) | In/Out  |
|-----------|---------|
| 0.0020    | 24.717% |
| 0.0010    | 22.955% |
| 0.0004    | 20.486% |

***Structure Detail:***

*Structure #3 (Null)*

*Structure #4 (Null)*

*Structure #1 (Null)*

*Structure #2 (Null)*

*Structure #5 (Null)*

*Structure #6 (Null)*

*EAST LEASE BNDY*

*Structure #7 (Null)*

*Structure #8 (Null)*

*WEST LEASE BNDY*

*Structure #9 (Null)*



### ***Subwatershed Hydrology Detail:***

| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #3     | 1        | 791.300           | 1.145              | 1.181        | 0.350  | 80.800       | M   | 137.26               | 21.870                |
|        | 2        | 1,079.100         | 0.915              | 0.596        | 0.351  | 80.800       | M   | 223.54               | 29.835                |
|        | 3        | 450.300           | 0.571              | 0.319        | 0.355  | 81.300       | M   | 138.88               | 12.992                |
|        | 4        | 742.600           | 0.625              | 0.000        | 0.000  | 78.500       | M   | 162.13               | 16.799                |
|        | 5        | 915.400           | 1.119              | 0.000        | 0.000  | 78.800       | M   | 131.60               | 21.280                |
|        | <b>Σ</b> | <b>3,978.700</b>  |                    |              |        |              |     | <b>440.83</b>        | <b>102.777</b>        |
| #4     | 1        | 546.400           | 0.726              | 1.710        | 0.319  | 81.700       | M   | 147.20               | 16.285                |
|        | 2        | 441.200           | 0.503              | 1.429        | 0.318  | 86.000       | M   | 224.45               | 18.445                |
|        | 3        | 889.400           | 0.815              | 0.998        | 0.318  | 82.100       | M   | 228.19               | 27.379                |
|        | 4        | 1,339.100         | 0.919              | 0.000        | 0.000  | 84.000       | M   | 373.16               | 47.965                |
|        | <b>Σ</b> | <b>7,194.800</b>  |                    |              |        |              |     | <b>603.73</b>        | <b>212.850</b>        |
| #1     | 1        | 1,242.300         | 1.349              | 1.345        | 0.354  | 80.800       | M   | 188.55               | 34.327                |
|        | 2        | 1,662.000         | 1.465              | 0.849        | 0.360  | 80.300       | M   | 224.08               | 44.015                |
|        | 3        | 1,434.000         | 1.573              | 1.241        | 0.357  | 81.100       | M   | 197.43               | 40.634                |
|        | 4        | 842.700           | 1.102              | 0.977        | 0.364  | 81.000       | M   | 153.76               | 23.683                |
|        | 5        | 676.100           | 1.067              | 1.113        | 0.365  | 81.600       | M   | 134.22               | 19.974                |
|        | 6        | 1,223.200         | 0.778              | 0.596        | 0.352  | 81.800       | M   | 315.94               | 36.750                |
|        | 7        | 743.100           | 0.745              | 0.530        | 0.354  | 83.600       | M   | 233.83               | 25.797                |
|        | 8        | 654.500           | 0.801              | 0.000        | 0.000  | 92.200       | M   | 397.48               | 42.811                |
|        | <b>Σ</b> | <b>8,477.900</b>  |                    |              |        |              |     | <b>932.74</b>        | <b>267.991</b>        |
| #2     | 1        | 609.500           | 0.668              | 1.219        | 0.340  | 85.700       | M   | 249.70               | 24.903                |
|        | 2        | 537.100           | 0.610              | 1.436        | 0.329  | 91.600       | M   | 374.99               | 33.711                |
|        | 3        | 455.000           | 0.546              | 1.288        | 0.324  | 82.000       | M   | 154.39               | 13.898                |
|        | 4        | 627.000           | 0.634              | 0.852        | 0.324  | 87.900       | M   | 320.25               | 30.151                |
|        | 5        | 653.100           | 0.452              | 0.453        | 0.315  | 91.200       | M   | 527.57               | 39.848                |
|        | 6        | 957.200           | 0.984              | 0.000        | 0.000  | 89.600       | M   | 407.82               | 52.057                |
|        | <b>Σ</b> | <b>12,316.800</b> |                    |              |        |              |     | <b>1,096.38</b>      | <b>462.559</b>        |
| #5     | 1        | 763.100           | 0.682              | 3.507        | 0.293  | 84.100       | M   | 267.48               | 27.555                |
|        | 2        | 983.300           | 1.117              | 2.231        | 0.289  | 89.200       | M   | 367.53               | 51.945                |
|        | 3        | 1,022.000         | 0.996              | 1.587        | 0.291  | 92.000       | M   | 521.33               | 65.927                |
|        | 4        | 688.700           | 1.908              | 1.255        | 0.291  | 80.800       | M   | 78.28                | 19.028                |
|        | 5        | 754.300           | 2.307              | 1.084        | 0.287  | 86.200       | M   | 119.98               | 31.953                |
|        | 6        | 628.400           | 0.538              | 0.595        | 0.301  | 93.000       | M   | 524.05               | 43.517                |
|        | 7        | 654.500           | 0.560              | 0.000        | 0.000  | 91.500       | M   | 478.48               | 40.785                |
|        | <b>Σ</b> | <b>25,005.900</b> |                    |              |        |              |     | <b>1,684.50</b>      | <b>956.120</b>        |
| #6     | 1        | 901.400           | 1.151              | 1.896        | 0.315  | 81.100       | M   | 160.40               | 25.547                |
|        | 2        | 1,011.200         | 1.871              | 0.166        | 0.287  | 83.500       | M   | 151.23               | 34.801                |

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| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
|        | 3        | 1,166.700         | 1.126              | 0.000        | 0.000  | 92.800       | M   | 575.99               | 79.576                |
|        | <b>Σ</b> | <b>28,085.200</b> |                    |              |        |              |     | <b>1,694.12</b>      | <b>1,096.044</b>      |
| #7     | 1        | 963.500           | 0.819              | 0.665        | 0.285  | 82.900       | M   | 265.26               | 31.644                |
|        | 2        | 1,513.200         | 2.587              | 0.000        | 0.000  | 75.000       | M   | 69.93                | 24.541                |
|        | 3        | 194.900           | 0.596              | 0.000        | 0.000  | 72.600       | M   | 21.05                | 2.452                 |
|        | <b>Σ</b> | <b>30,756.800</b> |                    |              |        |              |     | <b>1,698.39</b>      | <b>1,154.681</b>      |
| #8     | 1        | 386.400           | 0.538              | 2.912        | 0.280  | 93.000       | M   | 322.23               | 26.759                |
|        | 2        | 569.700           | 0.734              | 2.659        | 0.279  | 92.400       | M   | 373.20               | 37.816                |
|        | 3        | 647.700           | 0.853              | 2.311        | 0.280  | 87.600       | M   | 260.78               | 30.470                |
|        | 4        | 754.800           | 1.690              | 2.328        | 0.277  | 76.200       | M   | 57.58                | 13.788                |
|        | 5        | 532.600           | 0.740              | 1.423        | 0.277  | 79.500       | M   | 113.85               | 13.178                |
|        | 6        | 309.700           | 0.436              | 1.168        | 0.285  | 85.600       | M   | 166.21               | 12.570                |
|        | 7        | 158.300           | 0.448              | 0.938        | 0.279  | 83.800       | M   | 71.65                | 5.586                 |
|        | 8        | 304.300           | 0.648              | 0.566        | 0.296  | 80.600       | M   | 80.17                | 8.278                 |
|        | 9        | 211.900           | 0.480              | 0.921        | 0.320  | 83.000       | M   | 85.52                | 7.027                 |
|        | 10       | 711.200           | 0.890              | 0.436        | 0.300  | 83.300       | M   | 190.68               | 24.108                |
|        | 11       | 168.200           | 0.283              | 0.000        | 0.000  | 83.300       | M   | 92.56                | 5.727                 |
|        | <b>Σ</b> | <b>35,511.600</b> |                    |              |        |              |     | <b>1,701.48</b>      | <b>1,339.988</b>      |
| #9     | 1        | 466.200           | 0.574              | 2.401        | 0.265  | 89.000       | M   | 277.79               | 24.314                |
|        | 2        | 427.200           | 0.633              | 2.204        | 0.256  | 84.900       | M   | 169.55               | 16.405                |
|        | 3        | 361.200           | 0.686              | 1.864        | 0.256  | 84.900       | M   | 135.39               | 13.872                |
|        | 4        | 573.300           | 0.655              | 0.983        | 0.255  | 85.800       | M   | 240.22               | 23.605                |
|        | 5        | 473.100           | 0.668              | 0.000        | 0.000  | 84.600       | M   | 176.01               | 17.771                |
|        | <b>Σ</b> | <b>37,812.600</b> |                    |              |        |              |     | <b>1,693.81</b>      | <b>1,435.955</b>      |

## Subwatershed Sedimentology Detail:

| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #3     | 1        | 0.150  | 100.00 | 9.10  | 0.3050 | 1.0000 | 18   | 517.9           | 28,671                     | 8.11                        | 4.88        |
|        | 2        | 0.181  | 100.00 | 10.10 | 0.3050 | 1.0000 | 13   | 1,178.3         | 48,541                     | 17.28                       | 10.19       |
|        | 3        | 0.151  | 200.00 | 5.50  | 0.3050 | 1.0000 | 18   | 316.4           | 31,264                     | 13.05                       | 7.40        |
|        | 4        | 0.183  | 130.00 | 7.60  | 0.3160 | 1.0000 | 12   | 550.1           | 42,933                     | 16.42                       | 9.09        |
|        | 5        | 0.185  | 100.00 | 8.30  | 0.2760 | 1.0000 | 6    | 481.0           | 28,197                     | 6.04                        | 3.53        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>2,338.6</b>  | <b>27,282</b>              | <b>6.12</b>                 | <b>3.73</b> |
| #4     | 1        | 0.173  | 130.00 | 7.00  | 0.2850 | 1.0000 | 7    | 403.2           | 30,444                     | 11.52                       | 6.82        |
|        | 2        | 0.148  | 100.00 | 12.00 | 0.2220 | 1.0000 | 5    | 682.7           | 44,554                     | 17.59                       | 10.60       |
|        | 3        | 0.185  | 75.00  | 13.60 | 0.2740 | 1.0000 | 17   | 1,316.9         | 58,425                     | 20.84                       | 12.39       |



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| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 4        | 0.213  | 100.00 | 10.60 | 0.2330 | 1.0000 | 6    | 1,973.6         | 49,931                     | 15.56                       | 9.28        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>4,860.9</b>  | <b>43,257</b>              | <b>7.92</b>                 | <b>3.05</b> |
| #1     | 1        | 0.220  | 280.00 | 2.20  | 0.2960 | 1.0000 | 13   | 354.5           | 12,409                     | 3.41                        | 2.08        |
|        | 2        | 0.202  | 240.00 | 3.30  | 0.2960 | 1.0000 | 13   | 568.5           | 15,494                     | 3.87                        | 2.36        |
|        | 3        | 0.206  | 280.00 | 2.60  | 0.2960 | 1.0000 | 13   | 434.9           | 12,696                     | 3.05                        | 1.90        |
|        | 4        | 0.188  | 200.00 | 5.10  | 0.2960 | 1.0000 | 13   | 527.8           | 27,112                     | 8.72                        | 5.22        |
|        | 5        | 0.124  | 240.00 | 3.60  | 0.3130 | 1.0000 | 18   | 192.8           | 11,797                     | 3.62                        | 2.17        |
|        | 6        | 0.178  | 130.00 | 7.90  | 0.2850 | 1.0000 | 7    | 1,127.3         | 38,034                     | 13.98                       | 8.19        |
|        | 7        | 0.191  | 100.00 | 9.20  | 0.2540 | 1.0000 | 6    | 825.2           | 39,345                     | 13.70                       | 8.09        |
|        | 8        | 0.199  | 75.00  | 15.10 | 0.1510 | 1.0000 | 2    | 1,562.1         | 42,372                     | 11.59                       | 7.24        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>4,565.8</b>  | <b>34,225</b>              | <b>6.95</b>                 | <b>2.52</b> |
| #2     | 1        | 0.188  | 130.00 | 7.30  | 0.2120 | 1.0000 | 5    | 578.5           | 28,165                     | 9.86                        | 5.93        |
|        | 2        | 0.199  | 75.00  | 12.60 | 0.1510 | 1.0000 | 2    | 1,048.1         | 36,015                     | 11.47                       | 7.19        |
|        | 3        | 0.200  | 100.00 | 8.60  | 0.2020 | 1.0000 | 11   | 346.9           | 31,127                     | 9.19                        | 5.37        |
|        | 4        | 0.193  | 75.00  | 12.30 | 0.1730 | 1.0000 | 4    | 970.3           | 38,511                     | 12.11                       | 7.35        |
|        | 5        | 0.187  | 75.00  | 14.00 | 0.1590 | 1.0000 | 3    | 1,581.0         | 46,771                     | 17.49                       | 10.75       |
|        | 6        | 0.198  | 75.00  | 13.70 | 0.1680 | 1.0000 | 4    | 1,730.8         | 38,951                     | 9.35                        | 5.80        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>7,497.7</b>  | <b>34,701</b>              | <b>4.87</b>                 | <b>1.66</b> |
| #5     | 1        | 0.213  | 130.00 | 6.30  | 0.2330 | 1.0000 | 6    | 688.3           | 29,563                     | 10.84                       | 6.67        |
|        | 2        | 0.209  | 130.00 | 7.10  | 0.1680 | 1.0000 | 4    | 930.8           | 20,627                     | 4.23                        | 2.68        |
|        | 3        | 0.191  | 100.00 | 8.40  | 0.1500 | 1.0000 | 2    | 1,120.2         | 19,452                     | 4.36                        | 2.78        |
|        | 4        | 0.235  | 200.00 | 4.90  | 0.2870 | 1.0000 | 9    | 373.4           | 22,778                     | 4.39                        | 2.78        |
|        | 5        | 0.220  | 240.00 | 3.70  | 0.1900 | 1.0000 | 16   | 260.3           | 9,212                      | 0.56                        | 0.37        |
|        | 6        | 0.200  | 130.00 | 7.30  | 0.1410 | 1.0000 | 1    | 847.6           | 22,769                     | 7.65                        | 4.77        |
|        | 7        | 0.204  | 200.00 | 4.70  | 0.1560 | 1.0000 | 2    | 714.9           | 20,930                     | 6.93                        | 4.24        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>16,003.7</b> | <b>27,738</b>              | <b>3.87</b>                 | <b>1.72</b> |
| #6     | 1        | 0.228  | 280.00 | 2.70  | 0.2870 | 1.0000 | 9    | 331.5           | 15,627                     | 4.99                        | 3.03        |
|        | 2        | 0.226  | 280.00 | 2.40  | 0.2330 | 1.0000 | 6    | 276.0           | 9,268                      | 1.14                        | 0.72        |
|        | 3        | 0.200  | 200.00 | 4.20  | 0.1460 | 1.0000 | 1    | 952.6           | 13,808                     | 2.56                        | 1.63        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>15,104.2</b> | <b>23,367</b>              | <b>1.56</b>                 | <b>0.68</b> |
| #7     | 1        | 0.197  | 280.00 | 2.70  | 0.2330 | 1.0000 | 5    | 347.3           | 13,550                     | 3.91                        | 2.32        |
|        | 2        | 0.204  | 420.00 | 1.80  | 0.3270 | 1.0000 | 19   | 163.4           | 7,759                      | 0.31                        | 0.20        |
|        | 3        | 0.171  | 280.00 | 2.40  | 0.3380 | 1.0000 | 10   | 22.7            | 13,087                     | 3.58                        | 1.86        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>14,905.2</b> | <b>22,598</b>              | <b>1.37</b>                 | <b>0.58</b> |
| #8     | 1        | 0.200  | 280.00 | 2.70  | 0.1410 | 1.0000 | 1    | 216.6           | 9,168                      | 3.08                        | 1.99        |
|        | 2        | 0.204  | 280.00 | 2.30  | 0.1550 | 1.0000 | 3    | 277.0           | 8,371                      | 2.60                        | 1.67        |
|        | 3        | 0.173  | 280.00 | 3.00  | 0.2220 | 1.0000 | 6    | 310.3           | 11,965                     | 4.25                        | 2.65        |
|        | 4        | 0.204  | 280.00 | 3.00  | 0.3180 | 1.0000 | 19   | 144.3           | 12,459                     | 1.51                        | 0.93        |
|        | 5        | 0.187  | 200.00 | 5.90  | 0.2960 | 1.0000 | 12   | 366.8           | 34,625                     | 12.51                       | 7.31        |

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| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 6        | 0.167  | 200.00 | 4.20  | 0.2740 | 1.0000 | 8    | 264.4           | 25,618                     | 12.49                       | 7.48        |
|        | 7        | 0.215  | 100.00 | 9.40  | 0.2650 | 1.0000 | 20   | 219.1           | 48,298                     | 23.28                       | 13.69       |
|        | 8        | 0.201  | 100.00 | 8.10  | 0.2960 | 1.0000 | 13   | 240.3           | 36,721                     | 15.14                       | 8.70        |
|        | 9        | 0.208  | 280.00 | 2.70  | 0.2120 | 1.0000 | 15   | 76.1            | 13,686                     | 5.07                        | 2.94        |
|        | 10       | 0.225  | 200.00 | 4.50  | 0.2540 | 1.0000 | 14   | 548.6           | 27,795                     | 10.17                       | 6.07        |
|        | 11       | 0.198  | 100.00 | 9.20  | 0.2450 | 1.0000 | 6    | 210.9           | 47,825                     | 22.37                       | 12.48       |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>14,698.1</b> | <b>47,845</b>              | <b>4.55</b>                 | <b>0.79</b> |
| #9     | 1        | 0.206  | 130.00 | 7.80  | 0.1800 | 1.0000 | 16   | 600.7           | 28,616                     | 11.28                       | 7.10        |
|        | 2        | 0.189  | 100.00 | 11.10 | 0.2450 | 1.0000 | 6    | 692.7           | 49,867                     | 19.18                       | 11.75       |
|        | 3        | 0.177  | 100.00 | 8.30  | 0.2330 | 1.0000 | 6    | 310.5           | 26,790                     | 9.96                        | 6.07        |
|        | 4        | 0.161  | 100.00 | 10.00 | 0.2220 | 1.0000 | 5    | 664.6           | 33,921                     | 12.01                       | 7.25        |
|        | 5        | 0.175  | 200.00 | 5.90  | 0.2450 | 1.0000 | 6    | 428.6           | 29,984                     | 11.21                       | 6.57        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>15,678.9</b> | <b>32,341</b>              | <b>3.04</b>                 | <b>0.79</b> |

## Subwatershed Time of Concentration Details:

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.99      | 22.00            | 736.00            | 1.720          | 0.118        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.63      | 66.00            | 10,511.00         | 2.370          | 1.231        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.349</b> |
| #1        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.02      | 8.00             | 785.00            | 1.000          | 0.218        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.48      | 242.00           | 16,353.00         | 3.640          | 1.247        |
| <b>#1</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.465</b> |
| #1        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 0.88      | 10.00            | 1,136.10          | 0.930          | 0.339        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.31      | 200.00           | 15,244.00         | 3.430          | 1.234        |
| <b>#1</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.573</b> |
| #1        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.85      | 10.00            | 542.00            | 1.350          | 0.111        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 220.00           | 13,595.00         | 3.810          | 0.991        |
| <b>#1</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.102</b> |
| #1        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 1.23      | 10.00            | 812.00            | 1.100          | 0.205        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.41      | 156.00           | 11,049.00         | 3.560          | 0.862        |
| <b>#1</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.067</b> |
| #1        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 3.12      | 22.00            | 706.00            | 1.760          | 0.111        |



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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.85      | 346.00           | 12,152.00         | 5.060          | 0.667        |
| <b>#1</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.778</b> |
| #1        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 4.66      | 43.00            | 922.01            | 2.150          | 0.119        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.67      | 295.00           | 11,057.38         | 4.900          | 0.626        |
| <b>#1</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.745</b> |
| #1        | 8        | 5. Nearly bare and untilled, and alluvial valley fans | 7.46      | 65.00            | 871.00            | 2.730          | 0.088        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.61      | 324.00           | 12,433.00         | 4.840          | 0.713        |
| <b>#1</b> | <b>8</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.801</b> |
| #2        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 6.24      | 30.00            | 481.00            | 2.490          | 0.053        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.34      | 406.00           | 12,141.00         | 5.480          | 0.615        |
| <b>#2</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.668</b> |
| #2        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.16      | 30.00            | 950.00            | 1.770          | 0.149        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.22      | 432.00           | 10,229.00         | 6.160          | 0.461        |
| <b>#2</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.610</b> |
| #2        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.65      | 10.00            | 378.00            | 1.620          | 0.064        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.72      | 234.00           | 8,592.00          | 4.950          | 0.482        |
| <b>#2</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.546</b> |
| #2        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.07      | 25.00            | 815.00            | 1.750          | 0.129        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.32      | 330.00           | 9,931.00          | 5.460          | 0.505        |
| <b>#2</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.634</b> |
| #2        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 7.45      | 45.00            | 604.00            | 2.720          | 0.061        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.78      | 310.00           | 8,210.00          | 5.820          | 0.391        |
| <b>#2</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.452</b> |
| #2        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 9.10      | 80.00            | 879.00            | 3.010          | 0.081        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.32      | 344.00           | 14,831.00         | 4.560          | 0.903        |
| <b>#2</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.984</b> |
| #3        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.29      | 15.00            | 1,163.00          | 1.130          | 0.285        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.37      | 338.00           | 14,280.00         | 4.610          | 0.860        |
| <b>#3</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.145</b> |
| #3        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.04      | 33.00            | 1,087.00          | 1.740          | 0.173        |

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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.06      | 238.00           | 11,527.00         | 4.310          | 0.742        |
| <b>#3</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.915</b> |
| #3        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 5.02      | 45.00            | 897.00            | 2.230          | 0.111        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.09      | 270.00           | 8,741.00          | 5.270          | 0.460        |
| <b>#3</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.571</b> |
| #3        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 7.41      | 28.00            | 378.00            | 2.720          | 0.038        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.43      | 402.00           | 11,736.00         | 5.550          | 0.587        |
| <b>#3</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.625</b> |
| #3        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 30.00            | 885.00            | 1.840          | 0.133        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.58      | 442.00           | 17,121.00         | 4.820          | 0.986        |
| <b>#3</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.119</b> |
| #4        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.59      | 62.00            | 1,729.00          | 1.890          | 0.254        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.09      | 154.00           | 7,372.00          | 4.330          | 0.472        |
| <b>#4</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.726</b> |
| #4        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 6.83      | 25.00            | 366.00            | 2.610          | 0.038        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.36      | 182.00           | 7,708.00          | 4.600          | 0.465        |
| <b>#4</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.503</b> |
| #4        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 19.03     | 47.00            | 247.00            | 4.360          | 0.015        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 268.00           | 12,586.00         | 4.370          | 0.800        |
| <b>#4</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.815</b> |
| #4        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 14.08     | 50.00            | 355.00            | 3.750          | 0.026        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.46      | 372.00           | 15,119.00         | 4.700          | 0.893        |
| <b>#4</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.919</b> |
| #5        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 12.55     | 65.00            | 518.00            | 3.540          | 0.040        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.92      | 184.00           | 9,592.00          | 4.150          | 0.642        |
| <b>#5</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.682</b> |
| #5        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.10      | 30.00            | 588.00            | 2.250          | 0.072        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.77      | 266.00           | 15,016.00         | 3.990          | 1.045        |
| <b>#5</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.117</b> |
| #5        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.90      | 20.00            | 1,050.00          | 1.380          | 0.211        |



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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.19      | 274.00           | 12,532.00         | 4.430          | 0.785        |
| <b>#5</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.996</b> |
| #5        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.78      | 32.00            | 1,152.00          | 1.660          | 0.192        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.99      | 182.00           | 18,415.00         | 2.980          | 1.716        |
| <b>#5</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.908</b> |
| #5        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 2.52      | 23.00            | 911.00            | 1.580          | 0.160        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.07      | 256.00           | 23,965.00         | 3.100          | 2.147        |
| <b>#5</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.307</b> |
| #5        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 6.36      | 25.00            | 393.00            | 2.520          | 0.043        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.39      | 198.00           | 8,272.00          | 4.640          | 0.495        |
| <b>#5</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.538</b> |
| #5        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 9.66      | 28.00            | 290.00            | 3.100          | 0.025        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.12      | 179.00           | 8,427.00          | 4.370          | 0.535        |
| <b>#5</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.560</b> |
| #6        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 31.83     | 120.00           | 377.00            | 5.640          | 0.018        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.38      | 198.00           | 14,361.00         | 3.520          | 1.133        |
| <b>#6</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.151</b> |
| #6        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 4.25      | 40.00            | 941.00            | 2.060          | 0.126        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.96      | 176.00           | 18,407.00         | 2.930          | 1.745        |
| <b>#6</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.871</b> |
| #6        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.35      | 25.00            | 575.00            | 2.080          | 0.076        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.57      | 224.00           | 14,223.00         | 3.760          | 1.050        |
| <b>#6</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.126</b> |
| #7        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.51      | 10.00            | 399.00            | 1.580          | 0.070        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.11      | 95.00            | 8,524.00          | 3.160          | 0.749        |
| <b>#7</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.819</b> |
| #7        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.14      | 14.00            | 655.00            | 1.460          | 0.124        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.07      | 56.00            | 5,255.00          | 3.090          | 0.472        |
| <b>#7</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.596</b> |
| #8        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.97      | 5.00             | 254.00            | 1.400          | 0.050        |

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| Stru #    | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.64      | 111.00           | 6,755.00          | 3.840          | 0.488        |
| <b>#8</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.538</b> |
| #8        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 2.49      | 8.00             | 321.00            | 1.570          | 0.056        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.16      | 91.00            | 7,866.00          | 3.220          | 0.678        |
| <b>#8</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.734</b> |
| #8        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 3.58      | 25.00            | 698.00            | 1.890          | 0.102        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.12      | 96.00            | 8,579.00          | 3.170          | 0.751        |
| <b>#8</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.853</b> |
| #8        | 4         | 5. Nearly bare and untilled, and alluvial valley fans | 0.85      | 10.00            | 1,181.00          | 0.920          | 0.356        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 0.90      | 123.00           | 13,645.00         | 2.840          | 1.334        |
| <b>#8</b> | <b>4</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.690</b> |
| #8        | 5         | 5. Nearly bare and untilled, and alluvial valley fans | 6.53      | 39.00            | 597.00            | 2.550          | 0.065        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.42      | 123.00           | 8,678.00          | 3.570          | 0.675        |
| <b>#8</b> | <b>5</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.740</b> |
| #8        | 6         | 5. Nearly bare and untilled, and alluvial valley fans | 1.45      | 5.00             | 344.00            | 1.200          | 0.079        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 2.21      | 127.00           | 5,746.00          | 4.460          | 0.357        |
| <b>#8</b> | <b>6</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.436</b> |
| #8        | 7         | 5. Nearly bare and untilled, and alluvial valley fans | 2.98      | 12.00            | 403.00            | 1.720          | 0.065        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.97      | 114.00           | 5,796.00          | 4.200          | 0.383        |
| <b>#8</b> | <b>7</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.448</b> |
| #8        | 8         | 5. Nearly bare and untilled, and alluvial valley fans | 20.11     | 105.00           | 522.00            | 4.480          | 0.032        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.77      | 157.00           | 8,849.00          | 3.990          | 0.616        |
| <b>#8</b> | <b>8</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.648</b> |
| #8        | 9         | 5. Nearly bare and untilled, and alluvial valley fans | 43.35     | 75.00            | 173.00            | 6.580          | 0.007        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.57      | 100.00           | 6,387.00          | 3.750          | 0.473        |
| <b>#8</b> | <b>9</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.480</b> |
| #8        | 10        | 5. Nearly bare and untilled, and alluvial valley fans | 1.85      | 40.00            | 2,159.00          | 1.360          | 0.440        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.53      | 92.00            | 6,011.00          | 3.710          | 0.450        |
| <b>#8</b> | <b>10</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.890</b> |
| #8        | 11        | 5. Nearly bare and untilled, and alluvial valley fans | 4.84      | 24.00            | 496.00            | 2.190          | 0.062        |



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| Stru #    | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |           | 8. Large gullies, diversions, and low flowing streams | 2.79      | 111.00           | 3,980.20          | 5.000          | 0.221        |
| <b>#8</b> | <b>11</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.283</b> |
| #9        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 7.42      | 25.00            | 337.00            | 2.720          | 0.034        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.50      | 107.00           | 7,136.00          | 3.670          | 0.540        |
| <b>#9</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.574</b> |
| #9        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 11.19     | 15.00            | 134.00            | 3.340          | 0.011        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.96      | 184.00           | 9,391.00          | 4.190          | 0.622        |
| <b>#9</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.633</b> |
| #9        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 3.14      | 25.00            | 796.00            | 1.770          | 0.124        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.68      | 132.00           | 7,862.00          | 3.880          | 0.562        |
| <b>#9</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.686</b> |
| #9        | 4         | 5. Nearly bare and untilled, and alluvial valley fans | 12.82     | 35.00            | 273.00            | 3.580          | 0.021        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.93      | 183.00           | 9,495.00          | 4.160          | 0.634        |
| <b>#9</b> | <b>4</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.655</b> |
| #9        | 5         | 5. Nearly bare and untilled, and alluvial valley fans | 2.66      | 15.00            | 564.00            | 1.630          | 0.096        |
|           |           | 8. Large gullies, diversions, and low flowing streams | 1.68      | 135.00           | 8,020.00          | 3.890          | 0.572        |
| <b>#9</b> | <b>5</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.668</b> |

## ***Subwatershed Muskingum Routing Details:***

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.89      | 378.00           | 19,958.00         | 4.120          | 1.345        |
| <b>#1</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.345</b> |
| #1        | 2        | 8. Large gullies, diversions, and low flowing streams | 2.11      | 282.00           | 13,337.00         | 4.360          | 0.849        |
| <b>#1</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.849</b> |
| #1        | 3        | 8. Large gullies, diversions, and low flowing streams | 2.02      | 384.00           | 19,036.00         | 4.260          | 1.241        |
| <b>#1</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.241</b> |
| #1        | 4        | 8. Large gullies, diversions, and low flowing streams | 2.28      | 364.00           | 15,948.82         | 4.530          | 0.977        |
| <b>#1</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.977</b> |
| #1        | 5        | 8. Large gullies, diversions, and low flowing streams | 2.33      | 428.00           | 18,360.00         | 4.580          | 1.113        |
| <b>#1</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.113</b> |

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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.82      | 158.00           | 8,675.00          | 4.040          | 0.596        |
| <b>#1</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.596</b> |
| #1        | 7        | 8. Large gullies, diversions, and low flowing streams | 1.89      | 149.00           | 7,868.00          | 4.120          | 0.530        |
| <b>#1</b> | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.530</b> |
| #2        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.44      | 228.00           | 15,800.00         | 3.600          | 1.219        |
| <b>#2</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.219</b> |
| #2        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.19      | 202.00           | 16,912.00         | 3.270          | 1.436        |
| <b>#2</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.436</b> |
| #2        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.10      | 160.00           | 14,568.00         | 3.140          | 1.288        |
| <b>#2</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.288</b> |
| #2        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.09      | 104.00           | 9,576.00          | 3.120          | 0.852        |
| <b>#2</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.852</b> |
| #2        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.93      | 44.00            | 4,715.00          | 2.890          | 0.453        |
| <b>#2</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.453</b> |
| #3        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.75      | 294.00           | 16,845.00         | 3.960          | 1.181        |
| <b>#3</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.181</b> |
| #3        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.79      | 154.00           | 8,609.00          | 4.010          | 0.596        |
| <b>#3</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.596</b> |
| #3        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.93      | 92.00            | 4,778.00          | 4.160          | 0.319        |
| <b>#3</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.319</b> |
| #4        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.01      | 186.00           | 18,477.00         | 3.000          | 1.710        |
| <b>#4</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.710</b> |
| #4        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.98      | 150.00           | 15,281.00         | 2.970          | 1.429        |
| <b>#4</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.429</b> |
| #4        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.98      | 104.00           | 10,645.00         | 2.960          | 0.998        |
| <b>#4</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.998</b> |
| #5        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.64      | 195.00           | 30,309.00         | 2.400          | 3.507        |
| <b>#5</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.507</b> |
| #5        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.60      | 113.00           | 18,717.00         | 2.330          | 2.231        |
| <b>#5</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.231</b> |
| #5        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.63      | 85.00            | 13,541.00         | 2.370          | 1.587        |
| <b>#5</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.587</b> |
| #5        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.63      | 67.00            | 10,710.00         | 2.370          | 1.255        |



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| Stru #    | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#5</b> | <b>4</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.255</b> |
| #5        | 5         | 8. Large gullies, diversions, and low flowing streams | 0.59      | 53.00            | 8,978.00          | 2.300          | 1.084        |
| <b>#5</b> | <b>5</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.084</b> |
| #5        | 6         | 8. Large gullies, diversions, and low flowing streams | 0.74      | 41.00            | 5,528.00          | 2.580          | 0.595        |
| <b>#5</b> | <b>6</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.595</b> |
| #6        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.94      | 186.00           | 19,797.00         | 2.900          | 1.896        |
| <b>#6</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.896</b> |
| #6        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.58      | 8.00             | 1,372.00          | 2.290          | 0.166        |
| <b>#6</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.166</b> |
| #7        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.57      | 31.00            | 5,417.00          | 2.260          | 0.665        |
| <b>#7</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.665</b> |
| #8        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.53      | 120.00           | 22,753.13         | 2.170          | 2.912        |
| <b>#8</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.912</b> |
| #8        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.51      | 106.00           | 20,587.00         | 2.150          | 2.659        |
| <b>#8</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.659</b> |
| #8        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.53      | 95.00            | 18,060.00         | 2.170          | 2.311        |
| <b>#8</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.311</b> |
| #8        | 4         | 8. Large gullies, diversions, and low flowing streams | 0.50      | 88.00            | 17,689.00         | 2.110          | 2.328        |
| <b>#8</b> | <b>4</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.328</b> |
| #8        | 5         | 8. Large gullies, diversions, and low flowing streams | 0.50      | 54.00            | 10,815.00         | 2.110          | 1.423        |
| <b>#8</b> | <b>5</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.423</b> |
| #8        | 6         | 8. Large gullies, diversions, and low flowing streams | 0.57      | 54.00            | 9,503.00          | 2.260          | 1.168        |
| <b>#8</b> | <b>6</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.168</b> |
| #8        | 7         | 8. Large gullies, diversions, and low flowing streams | 0.51      | 37.00            | 7,229.00          | 2.140          | 0.938        |
| <b>#8</b> | <b>7</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.938</b> |
| #8        | 8         | 8. Large gullies, diversions, and low flowing streams | 0.68      | 34.00            | 5,017.00          | 2.460          | 0.566        |
| <b>#8</b> | <b>8</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.566</b> |
| #8        | 9         | 8. Large gullies, diversions, and low flowing streams | 1.01      | 101.00           | 9,985.00          | 3.010          | 0.921        |
| <b>#8</b> | <b>9</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.921</b> |
| #8        | 10        | 8. Large gullies, diversions, and low flowing streams | 0.72      | 29.00            | 4,009.00          | 2.550          | 0.436        |
| <b>#8</b> | <b>10</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.436</b> |
| #9        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.41      | 68.00            | 16,597.51         | 1.920          | 2.401        |
| <b>#9</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.401</b> |

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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #9        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 51.00            | 14,207.00         | 1.790          | 2.204        |
| <b>#9</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.204</b> |
| #9        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 43.00            | 12,015.00         | 1.790          | 1.864        |
| <b>#9</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.864</b> |
| #9        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.35      | 22.00            | 6,269.00          | 1.770          | 0.983        |
| <b>#9</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.983</b> |



# SEDCAD 4 for Windows - 10-Year 24-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #3 | 3,978.700                                 | 3,978.700                             | 440.83                     | 102.78                               | 2,338.6            | 27,282                              | 6.12                                  | 3.73           |
| #4 | 3,216.100                                 | 7,194.800                             | 603.73                     | 212.85                               | 4,860.9            | 43,257                              | 7.92                                  | 3.05           |
| #1 | 8,477.900                                 | 8,477.900                             | 932.74                     | 267.99                               | 4,565.8            | 34,225                              | 6.95                                  | 2.52           |
| #2 | 3,838.900                                 | 12,316.800                            | 1,096.38                   | 462.56                               | 7,497.7            | 34,701                              | 4.87                                  | 1.66           |
| #5 | 5,494.300                                 | 25,005.900                            | 1,684.50                   | 956.12                               | 16,003.7           | 27,738                              | 3.87                                  | 1.72           |
| #6 | 3,079.300                                 | 28,085.200                            | 1,694.12                   | 1,096.04                             | 15,104.2           | 23,367                              | 1.56                                  | 0.68           |
| #7 | 2,671.600                                 | 30,756.800                            | 1,698.39                   | 1,154.68                             | 14,905.2           | 22,598                              | 1.37                                  | 0.58           |
| #8 | 4,754.800                                 | 35,511.600                            | 1,701.48                   | 1,339.99                             | 14,698.1           | 47,845                              | 4.55                                  | 0.79           |
| #9 | 2,301.000                                 | 37,812.600                            | 1,693.81                   | 1,435.96                             | 15,678.9           | 32,341                              | 3.04                                  | 0.79           |

# SEDCAD 4 for Windows - 2-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #3 | 3,978.700                                 | 3,978.700                             | 54.16                      | 11.47                                | 213.2              | 19,166                              | 1.80                                  | 1.28           |
| #4 | 3,216.100                                 | 7,194.800                             | 98.76                      | 29.58                                | 588.8              | 31,016                              | 3.41                                  | 1.60           |
| #1 | 8,477.900                                 | 8,477.900                             | 154.53                     | 42.61                                | 702.9              | 27,435                              | 3.84                                  | 1.69           |
| #2 | 3,838.900                                 | 12,316.800                            | 330.94                     | 91.74                                | 1,663.8            | 30,443                              | 3.50                                  | 1.52           |
| #5 | 5,494.300                                 | 25,005.900                            | 410.43                     | 194.41                               | 2,430.5            | 16,075                              | 1.29                                  | 0.74           |
| #6 | 3,079.300                                 | 28,085.200                            | 406.03                     | 228.76                               | 2,250.6            | 13,061                              | 0.63                                  | 0.35           |
| #7 | 2,671.600                                 | 30,756.800                            | 402.61                     | 234.65                               | 2,227.6            | 14,438                              | 0.62                                  | 0.30           |
| #8 | 4,754.800                                 | 35,511.600                            | 395.69                     | 274.47                               | 2,146.9            | 38,785                              | 2.40                                  | 0.36           |
| #9 | 2,301.000                                 | 37,812.600                            | 391.10                     | 294.15                               | 2,361.0            | 24,665                              | 1.71                                  | 0.41           |



# SEDCAD 4 for Windows - 10-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #3 | 3,978.700                                 | 3,978.700                             | 265.53                     | 49.06                                | 1,165.5            | 23,780                              | 4.29                                  | 3.13           |
| #4 | 3,216.100                                 | 7,194.800                             | 377.17                     | 107.10                               | 2,542.2            | 37,709                              | 5.84                                  | 2.68           |
| #1 | 8,477.900                                 | 8,477.900                             | 592.57                     | 139.16                               | 2,551.3            | 31,257                              | 5.38                                  | 2.30           |
| #2 | 3,838.900                                 | 12,316.800                            | 789.79                     | 255.55                               | 4,558.0            | 31,911                              | 4.07                                  | 1.66           |
| #5 | 5,494.300                                 | 25,005.900                            | 1,134.22                   | 531.95                               | 8,678.6            | 22,705                              | 2.22                                  | 1.17           |
| #6 | 3,079.300                                 | 28,085.200                            | 1,124.25                   | 614.41                               | 8,093.3            | 18,945                              | 1.13                                  | 0.58           |
| #7 | 2,671.600                                 | 30,756.800                            | 1,117.71                   | 641.23                               | 7,966.0            | 18,866                              | 1.03                                  | 0.50           |
| #8 | 4,754.800                                 | 35,511.600                            | 1,099.20                   | 745.76                               | 7,808.1            | 43,083                              | 3.70                                  | 0.66           |
| #9 | 2,301.000                                 | 37,812.600                            | 1,085.26                   | 799.67                               | 8,366.3            | 28,502                              | 2.47                                  | 0.66           |

# SEDCAD 4 for Windows - 25-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #3 | 3,978.700                                 | 3,978.700                             | 466.46                     | 83.38                                | 2,147.3            | 25,470                              | 5.50                                  | 4.05           |
| #4 | 3,216.100                                 | 7,194.800                             | 639.40                     | 175.00                               | 4,501.6            | 40,588                              | 7.18                                  | 3.31           |
| #1 | 8,477.900                                 | 8,477.900                             | 985.54                     | 222.07                               | 4,256.2            | 32,523                              | 6.32                                  | 2.72           |
| #2 | 3,838.900                                 | 12,316.800                            | 1,143.70                   | 389.57                               | 6,994.1            | 32,748                              | 4.40                                  | 1.76           |
| #5 | 5,494.300                                 | 25,005.900                            | 1,730.17                   | 806.73                               | 14,677.0           | 25,793                              | 3.17                                  | 1.63           |
| #6 | 3,079.300                                 | 28,085.200                            | 1,714.72                   | 926.63                               | 13,702.7           | 21,689                              | 1.39                                  | 0.70           |
| #7 | 2,671.600                                 | 30,756.800                            | 1,705.83                   | 973.65                               | 13,442.9           | 20,981                              | 1.23                                  | 0.59           |
| #8 | 4,754.800                                 | 35,511.600                            | 1,677.53                   | 1,130.54                             | 13,103.4           | 44,100                              | 4.07                                  | 0.78           |
| #9 | 2,301.000                                 | 37,812.600                            | 1,655.79                   | 1,211.78                             | 13,932.0           | 29,937                              | 2.73                                  | 0.77           |



# SEDCAD 4 for Windows - 50-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #3 | 3,978.700                                 | 3,978.700                             | 658.49                     | 115.93                               | 3,130.7            | 26,537                              | 6.27                                  | 4.65           |
| #4 | 3,216.100                                 | 7,194.800                             | 888.09                     | 238.37                               | 6,403.9            | 42,242                              | 8.00                                  | 3.70           |
| #1 | 8,477.900                                 | 8,477.900                             | 1,354.95                   | 298.86                               | 5,899.3            | 33,228                              | 7.05                                  | 3.06           |
| #2 | 3,838.900                                 | 12,316.800                            | 1,488.15                   | 511.26                               | 9,343.7            | 33,523                              | 4.68                                  | 1.86           |
| #5 | 5,494.300                                 | 25,005.900                            | 2,272.37                   | 1,055.73                             | 20,386.0           | 27,512                              | 4.04                                  | 2.07           |
| #6 | 3,079.300                                 | 28,085.200                            | 2,252.50                   | 1,208.91                             | 19,063.8           | 23,337                              | 1.56                                  | 0.77           |
| #7 | 2,671.600                                 | 30,756.800                            | 2,241.50                   | 1,275.49                             | 18,665.9           | 22,547                              | 1.37                                  | 0.65           |
| #8 | 4,754.800                                 | 35,511.600                            | 2,203.65                   | 1,479.73                             | 18,151.3           | 44,954                              | 4.31                                  | 0.86           |
| #9 | 2,301.000                                 | 37,812.600                            | 2,174.95                   | 1,585.49                             | 19,233.8           | 30,979                              | 2.92                                  | 0.84           |

# SEDCAD 4 for Windows - 100-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #3 | 3,978.700                                 | 3,978.700                             | 890.75                     | 154.95                               | 4,359.5            | 27,516                              | 6.97                                  | 5.19           |
| #4 | 3,216.100                                 | 7,194.800                             | 1,185.76                   | 313.49                               | 8,748.1            | 43,827                              | 8.76                                  | 4.06           |
| #1 | 8,477.900                                 | 8,477.900                             | 1,795.71                   | 389.46                               | 7,899.2            | 33,914                              | 7.74                                  | 3.38           |
| #2 | 3,838.900                                 | 12,316.800                            | 1,954.05                   | 652.91                               | 12,353.8           | 34,587                              | 5.03                                  | 2.01           |
| #5 | 5,494.300                                 | 25,005.900                            | 2,905.07                   | 1,345.19                             | 27,274.7           | 28,823                              | 4.66                                  | 2.39           |
| #6 | 3,079.300                                 | 28,085.200                            | 2,879.25                   | 1,536.56                             | 25,543.8           | 24,483                              | 1.88                                  | 0.93           |
| #7 | 2,671.600                                 | 30,756.800                            | 2,865.67                   | 1,626.91                             | 24,968.3           | 23,757                              | 1.49                                  | 0.70           |
| #8 | 4,754.800                                 | 35,511.600                            | 2,816.87                   | 1,886.12                             | 24,239.3           | 45,637                              | 4.52                                  | 0.93           |
| #9 | 2,301.000                                 | 37,812.600                            | 2,780.20                   | 2,020.17                             | 25,625.9           | 31,941                              | 3.08                                  | 0.90           |



## **Attachment 18.B-2**

No Name Arroyo Baseline Hydrology and Sedimentology SEDCAD™ Model Output with Impoundment

***General Information***

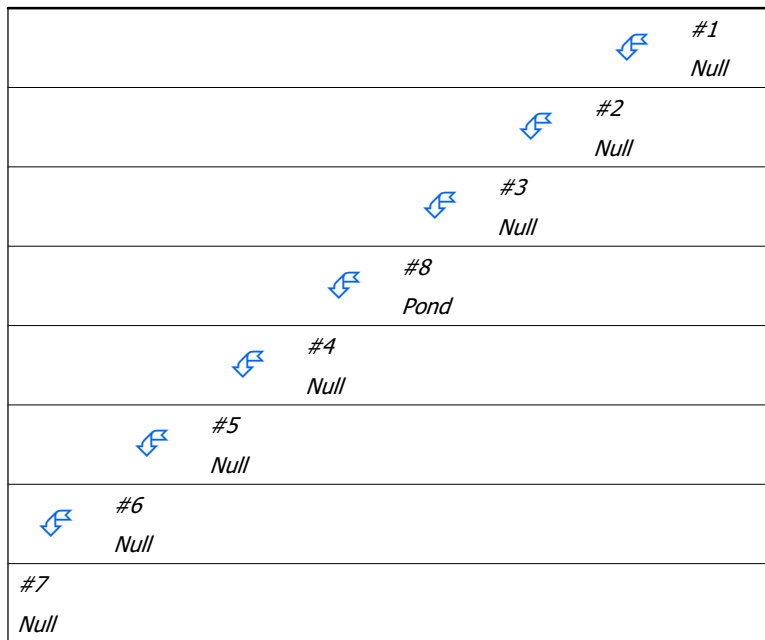
***Storm Information:***

|                 |                 |
|-----------------|-----------------|
| Storm Type:     | NRCS TYPE II-70 |
| Design Storm:   | 10 yr - 24 hr   |
| Rainfall Depth: | 1.700 inches    |



### Structure Networking:

| Type | Stru # | (flows into) | Stru # | Musk. K (hrs) | Musk. X | Description               |
|------|--------|--------------|--------|---------------|---------|---------------------------|
| Null | #1     | ==>          | #2     | 0.814         | 0.291   | SWS01                     |
| Null | #2     | ==>          | #3     | 0.656         | 0.345   | SWS02                     |
| Null | #3     | ==>          | #8     | 0.000         | 0.000   | SWS03, 04, 05             |
| Null | #4     | ==>          | #5     | 0.096         | 0.358   | SWS06, 07                 |
| Null | #5     | ==>          | #6     | 0.681         | 0.307   | SWS08                     |
| Null | #6     | ==>          | #7     | 1.027         | 0.307   | SWS09, 10, 11, 12, 13, 14 |
| Null | #7     | ==>          | End    | 0.000         | 0.000   | SWS15, 16, 17, 18, 19     |
| Pond | #8     | ==>          | #4     | 0.604         | 0.309   | S03 Impoundment Area      |



### Structure Routing Details:

| Stru #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 8. Large gullies, diversions, and low flowing streams | 0.62      | 43.00            | 6,923.00          | 2.36           | 0.814        |
| <b>#1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.814</b> |
| #2        | 8. Large gullies, diversions, and low flowing streams | 1.59      | 142.00           | 8,936.00          | 3.78           | 0.656        |
| <b>#2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.656</b> |
| #4        | 8. Large gullies, diversions, and low flowing streams | 2.03      | 30.00            | 1,480.00          | 4.27           | 0.096        |
| <b>#4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.096</b> |

# SEDCAD 4 for Windows

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| Stru #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #5        | 8. Large gullies, diversions, and low flowing streams | 0.82      | 54.00            | 6,623.00          | 2.70           | 0.681        |
| <b>#5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #6        | 8. Large gullies, diversions, and low flowing streams | 0.82      | 82.00            | 10,027.00         | 2.71           | 1.027        |
| <b>#6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.027</b> |



## ***Particle Size Distribution(s) at Each Structure***

### ***Structure #1 (SWS01):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 100.000% |
| 0.0159    | 87.633%  |
| 0.0100    | 65.880%  |
| 0.0050    | 28.144%  |
| 0.0020    | 17.046%  |
| 0.0010    | 15.702%  |
| 0.0004    | 14.553%  |

### ***Structure #2 (SWS02):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 100.000% |
| 0.0159    | 94.592%  |
| 0.0100    | 70.816%  |
| 0.0050    | 28.706%  |
| 0.0020    | 17.854%  |
| 0.0010    | 16.303%  |
| 0.0004    | 15.212%  |

### ***Structure #3 (SWS03, 04, 05):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 97.877%  |
| 0.0159    | 92.230%  |

| Size (mm) | In/Out  |
|-----------|---------|
| 0.0100    | 76.761% |
| 0.0050    | 25.622% |
| 0.0020    | 16.083% |
| 0.0010    | 14.500% |
| 0.0004    | 13.543% |

**Structure #8 (S03 Impoundment Area):**

| Size (mm) | In       | Out      |
|-----------|----------|----------|
| 0.4250    | 100.000% | 100.000% |
| 0.2500    | 100.000% | 100.000% |
| 0.1500    | 100.000% | 100.000% |
| 0.0750    | 97.877%  | 100.000% |
| 0.0159    | 92.230%  | 100.000% |
| 0.0100    | 76.761%  | 100.000% |
| 0.0050    | 25.622%  | 34.158%  |
| 0.0020    | 16.083%  | 21.441%  |
| 0.0010    | 14.500%  | 19.331%  |
| 0.0004    | 13.543%  | 18.055%  |

**Structure #4 (SWS06, 07):**

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 90.443%  |
| 0.0159    | 84.645%  |
| 0.0100    | 75.204%  |
| 0.0050    | 28.223%  |
| 0.0020    | 17.306%  |
| 0.0010    | 15.616%  |
| 0.0004    | 14.459%  |

**Structure #5 (SWS08):**

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 99.774%  |
| 0.0750    | 92.709%  |
| 0.0159    | 85.990%  |
| 0.0100    | 75.443%  |



| Size (mm) | In/Out  |
|-----------|---------|
| 0.0050    | 27.397% |
| 0.0020    | 16.752% |
| 0.0010    | 15.142% |
| 0.0004    | 13.966% |

***Structure #6 (SWS09, 10, 11, 12, 13, 14):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 99.349%  |
| 0.0750    | 90.724%  |
| 0.0159    | 85.928%  |
| 0.0100    | 79.191%  |
| 0.0050    | 25.810%  |
| 0.0020    | 15.481%  |
| 0.0010    | 14.068%  |
| 0.0004    | 12.817%  |

***Structure #7:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 97.978%  |
| 0.0750    | 93.104%  |
| 0.0159    | 88.810%  |
| 0.0100    | 79.800%  |
| 0.0050    | 25.172%  |
| 0.0020    | 14.985%  |
| 0.0010    | 13.630%  |
| 0.0004    | 12.388%  |

### Structure Detail:

Structure #1 (Null)

SWS01

Structure #2 (Null)

SWS02

Structure #3 (Null)

SWS03, 04, 05

Structure #8 (Pond)

S03 Impoundment Area

Pond Inputs:

|                    |             |
|--------------------|-------------|
| Initial Pool Elev: | 5,441.01 ft |
| Initial Pool:      | 0.00 ac-ft  |
| *Sediment Storage: | 0.00 ac-ft  |
| Dead Space:        | 5.00 %      |

*\*No sediment capacity defined*

Pond Results:

|                         |             |
|-------------------------|-------------|
| Peak Elevation:         | 5,448.48 ft |
| H'graph Detention Time: | 1.10 hrs    |
| Pond Model:             | CSTRS       |
| Dewater Time:           | 1.31 days   |
| Trap Efficiency:        | 24.99 %     |

*Dewatering time is calculated from peak stage to lowest spillway*

#### Elevation-Capacity-Discharge Table

| Elevation | Area (ac) | Capacity (ac-ft) | Discharge (cfs) | Dewater Time (hrs)  |
|-----------|-----------|------------------|-----------------|---------------------|
| 5,441.00  | 0.000     | 0.000            | 0.000           | Top of Sed. Storage |
| 5,441.01  | 0.011     | 0.000            | 0.000           |                     |
| 5,442.00  | 1.075     | 0.394            | 0.001           |                     |
| 5,443.00  | 2.094     | 1.950            | 0.001           |                     |
| 5,444.00  | 2.823     | 4.399            | 0.001           |                     |
| 5,445.00  | 4.127     | 7.854            | 0.001           |                     |
| 5,446.00  | 5.827     | 12.807           | 0.001           |                     |
| 5,447.00  | 7.996     | 19.691           | 55.000          | 26.25               |



| Elevation | Area<br>(ac) | Capacity<br>(ac-ft) | Discharge<br>(cfs) | Dewater<br>Time<br>(hrs) |
|-----------|--------------|---------------------|--------------------|--------------------------|
| 5,448.00  | 10.478       | 28.900              | 300.000            | 3.95                     |
| 5,448.48  | 12.103       | 34.593              | 571.922            | 1.35 Peak Stage          |
| 5,449.00  | 13.565       | 40.888              | 872.600            |                          |
| 5,450.00  | 16.428       | 55.862              | 1,000.000          |                          |

### Detailed Discharge Table

| Elevation<br>(ft) | User-<br>input discharge<br>(cfs) | Combined<br>Total<br>Discharge<br>(cfs) |
|-------------------|-----------------------------------|---|
| 5,441.00          | 0.000                             | 0.000                                   |
| 5,441.01          | 0.000                             | 0.000                                   |
| 5,442.00          | 0.001                             | 0.001                                   |
| 5,443.00          | 0.001                             | 0.001                                   |
| 5,444.00          | 0.001                             | 0.001                                   |
| 5,445.00          | 0.001                             | 0.001                                   |
| 5,446.00          | 0.001                             | 0.001                                   |
| 5,447.00          | 55.000                            | 55.000                                  |
| 5,448.00          | 300.000                           | 300.000                                 |
| 5,449.00          | 872.600                           | 872.600                                 |
| 5,450.00          | 1,000.000                         | 1,000.000                               |

Structure #4 (Null)

*SWS06, 07*

Structure #5 (Null)

*SWS08*

Structure #6 (Null)

*SWS09, 10, 11, 12, 13, 14*

Structure #7 (Null)

*SWS15, 16, 17, 18, 19*

***Subwatershed Hydrology Detail:***

| Stru #    | SWS #    | SWS Area (ac)    | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|-----------|----------|------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #1        | 1        | 999.370          | 1.261              | 0.000        | 0.000  | 81.700       | M   | 162.56               | 29.766                |
|           | <b>Σ</b> | <b>999.370</b>   |                    |              |        |              |     | <b>162.56</b>        | <b>29.766</b>         |
| #2        | 1        | 856.430          | 1.610              | 0.000        | 0.000  | 85.700       | M   | 167.83               | 34.941                |
|           | <b>Σ</b> | <b>1,855.800</b> |                    |              |        |              |     | <b>280.33</b>        | <b>64.707</b>         |
| #3        | 1        | 925.920          | 1.675              | 0.409        | 0.297  | 88.800       | M   | 230.14               | 47.520                |
|           | 2        | 1,019.220        | 1.106              | 0.193        | 0.261  | 87.000       | M   | 299.75               | 45.846                |
|           | 3        | 428.940          | 0.766              | 0.000        | 0.000  | 87.400       | M   | 169.66               | 19.891                |
|           | <b>Σ</b> | <b>4,229.880</b> |                    |              |        |              |     | <b>611.92</b>        | <b>177.964</b>        |
| <b>#8</b> | <b>Σ</b> | <b>4,229.880</b> |                    |              |        |              |     | <b>611.92</b>        | <b>177.964</b>        |
| #4        | 1        | 551.860          | 0.790              | 0.364        | 0.292  | 86.200       | M   | 192.60               | 23.387                |
|           | 2        | 516.780          | 0.565              | 0.000        | 0.000  | 88.400       | M   | 271.74               | 25.785                |
|           | <b>Σ</b> | <b>5,298.520</b> |                    |              |        |              |     | <b>620.07</b>        | <b>214.321</b>        |
| #5        | 1        | 233.280          | 0.469              | 0.000        | 0.000  | 87.900       | M   | 131.66               | 11.232                |
|           | <b>Σ</b> | <b>5,531.800</b> |                    |              |        |              |     | <b>624.80</b>        | <b>225.554</b>        |
| #6        | 1        | 126.980          | 0.164              | 0.545        | 0.308  | 86.900       | M   | 101.83               | 5.787                 |
|           | 2        | 235.630          | 0.327              | 0.427        | 0.341  | 86.700       | M   | 144.93               | 10.409                |
|           | 3        | 258.380          | 0.416              | 0.365        | 0.294  | 88.300       | M   | 161.17               | 12.840                |
|           | 4        | 180.930          | 0.449              | 0.176        | 0.301  | 86.700       | M   | 94.53                | 7.968                 |
|           | 5        | 189.850          | 0.326              | 0.146        | 0.330  | 86.800       | M   | 117.89               | 8.448                 |
|           | 6        | 172.360          | 0.753              | 0.000        | 0.000  | 88.300       | M   | 74.40                | 8.537                 |
|           | <b>Σ</b> | <b>6,695.930</b> |                    |              |        |              |     | <b>642.03</b>        | <b>279.543</b>        |
| #7        | 1        | 91.450           | 0.220              | 0.854        | 0.310  | 86.800       | M   | 65.92                | 4.081                 |
|           | 2        | 286.490          | 0.566              | 0.642        | 0.312  | 87.100       | M   | 134.68               | 12.994                |
|           | 3        | 75.280           | 0.179              | 0.610        | 0.308  | 86.800       | M   | 58.49                | 3.393                 |
|           | 4        | 128.700          | 0.157              | 0.270        | 0.325  | 86.800       | M   | 102.47               | 5.822                 |
|           | 5        | 67.060           | 0.333              | 0.000        | 0.000  | 82.000       | M   | 27.39                | 2.057                 |
|           | <b>Σ</b> | <b>7,344.910</b> |                    |              |        |              |     | <b>652.74</b>        | <b>307.890</b>        |

***Subwatershed Sedimentology Detail:***



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| Stru #    | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|-----------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #1        | 1        | 0.233  | 280.00 | 2.40  | 0.2650 | 1.0000 | 1    | 308.7           | 12,523                     | 3.66                        | 2.22        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>308.7</b>    | <b>12,523</b>              | <b>3.66</b>                 | <b>2.22</b> |
| #2        | 1        | 0.245  | 420.00 | 1.40  | 0.2450 | 1.0000 | 2    | 236.1           | 7,888                      | 2.53                        | 1.60        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>494.6</b>    | <b>8,847</b>               | <b>2.26</b>                 | <b>1.44</b> |
| #3        | 1        | 0.235  | 280.00 | 2.20  | 0.2330 | 1.0000 | 3    | 399.8           | 9,626                      | 3.28                        | 2.12        |
|           | 2        | 0.204  | 280.00 | 2.30  | 0.2330 | 1.0000 | 4    | 410.4           | 10,604                     | 3.76                        | 2.33        |
|           | 3        | 0.158  | 240.00 | 3.80  | 0.2110 | 1.0000 | 5    | 198.1           | 12,102                     | 4.07                        | 2.45        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>1,239.2</b>  | <b>8,405</b>               | <b>1.82</b>                 | <b>1.10</b> |
| <b>#8</b> | <b>Σ</b> |        |        |       |        |        |      | <b>1,239.2</b>  | <b>8,405</b>               | <b>1.82</b>                 | <b>1.10</b> |
| #4        | 1        | 0.150  | 200.00 | 6.00  | 0.2320 | 1.0000 | 6    | 433.9           | 22,402                     | 7.69                        | 4.65        |
|           | 2        | 0.183  | 100.00 | 9.10  | 0.1990 | 1.0000 | 7    | 662.4           | 31,375                     | 12.99                       | 7.74        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>1,675.7</b>  | <b>26,789</b>              | <b>6.05</b>                 | <b>1.29</b> |
| #5        | 1        | 0.170  | 100.00 | 10.10 | 0.1890 | 1.0000 | 8    | 294.8           | 32,531                     | 12.94                       | 7.60        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>1,875.5</b>  | <b>27,699</b>              | <b>6.19</b>                 | <b>1.36</b> |
| #6        | 1        | 0.160  | 100.00 | 11.50 | 0.1990 | 1.0000 | 9    | 207.4           | 44,285                     | 21.06                       | 12.35       |
|           | 2        | 0.145  | 100.00 | 12.00 | 0.2110 | 1.0000 | 15   | 360.7           | 43,171                     | 18.39                       | 10.71       |
|           | 3        | 0.171  | 100.00 | 8.20  | 0.1850 | 1.0000 | 10   | 246.1           | 23,504                     | 9.41                        | 5.60        |
|           | 4        | 0.150  | 75.00  | 12.10 | 0.2110 | 1.0000 | 11   | 215.6           | 33,725                     | 13.34                       | 7.79        |
|           | 5        | 0.143  | 75.00  | 13.30 | 0.2110 | 1.0000 | 15   | 271.8           | 40,504                     | 17.28                       | 9.97        |
|           | 6        | 0.164  | 75.00  | 13.90 | 0.1850 | 1.0000 | 12   | 225.3           | 31,654                     | 9.95                        | 6.04        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>2,775.0</b>  | <b>27,766</b>              | <b>5.64</b>                 | <b>1.48</b> |
| #7        | 1        | 0.143  | 100.00 | 10.40 | 0.2110 | 1.0000 | 15   | 110.9           | 33,271                     | 15.18                       | 9.02        |
|           | 2        | 0.162  | 75.00  | 15.20 | 0.2220 | 1.0000 | 13   | 527.1           | 48,820                     | 18.88                       | 11.36       |
|           | 3        | 0.143  | 75.00  | 20.10 | 0.2110 | 1.0000 | 15   | 180.8           | 64,982                     | 30.56                       | 18.04       |
|           | 4        | 0.143  | 100.00 | 8.10  | 0.2110 | 1.0000 | 15   | 113.6           | 24,801                     | 11.77                       | 6.76        |
|           | 5        | 0.215  | 100.00 | 8.20  | 0.2760 | 1.0000 | 14   | 61.3            | 39,773                     | 19.09                       | 10.40       |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>3,362.1</b>  | <b>34,942</b>              | <b>6.86</b>                 | <b>1.57</b> |

## Subwatershed Time of Concentration Details:

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.30      | 9.00             | 692.00            | 1.140          | 0.168        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.35      | 186.00           | 13,736.00         | 3.490          | 1.093        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.261</b> |
| #2        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.06      | 11.00            | 1,041.00          | 1.020          | 0.283        |

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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.41      | 37.00            | 9,125.00          | 1.910          | 1.327        |
| <b>#2</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.610</b> |
| #3        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 0.13      | 1.00             | 743.49            | 0.360          | 0.573        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.79      | 84.00            | 10,596.69         | 2.670          | 1.102        |
| <b>#3</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.675</b> |
| #3        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.79      | 40.00            | 1,056.00          | 1.940          | 0.151        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.20      | 135.00           | 11,282.00         | 3.280          | 0.955        |
| <b>#3</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.106</b> |
| #3        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.48      | 14.00            | 945.00            | 1.210          | 0.216        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.68      | 129.00           | 7,691.00          | 3.880          | 0.550        |
| <b>#3</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.766</b> |
| #4        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 0.96      | 7.00             | 731.00            | 0.970          | 0.209        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.94      | 169.00           | 8,725.00          | 4.170          | 0.581        |
| <b>#4</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.790</b> |
| #4        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 4.40      | 43.00            | 978.00            | 2.090          | 0.129        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.35      | 170.00           | 7,224.00          | 4.600          | 0.436        |
| <b>#4</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.565</b> |
| #5        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.11      | 22.00            | 1,044.00          | 1.450          | 0.200        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.14      | 162.00           | 5,158.00          | 5.310          | 0.269        |
| <b>#5</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.469</b> |
| #6        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.94      | 12.00            | 243.00            | 2.220          | 0.030        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.62      | 144.00           | 3,117.00          | 6.440          | 0.134        |
| <b>#6</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.164</b> |
| #6        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 4.52      | 46.00            | 1,017.00          | 2.120          | 0.133        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.40      | 132.00           | 3,879.00          | 5.530          | 0.194        |
| <b>#6</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.327</b> |
| #6        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.83      | 23.00            | 813.00            | 1.680          | 0.134        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.68      | 134.00           | 4,999.00          | 4.910          | 0.282        |
| <b>#6</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.416</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 4.43      | 28.00            | 632.00            | 2.100          | 0.083        |



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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.77      | 182.00           | 6,575.00          | 4.990          | 0.366        |
| <b>#6</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.449</b> |
| #6        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 6.63      | 41.00            | 618.00            | 2.570          | 0.066        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.36      | 102.00           | 4,321.00          | 4.600          | 0.260        |
| <b>#6</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.326</b> |
| #6        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 0.41      | 4.00             | 979.00            | 0.630          | 0.431        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.88      | 170.00           | 5,907.00          | 5.080          | 0.322        |
| <b>#6</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.753</b> |
| #7        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 18.35     | 60.00            | 327.00            | 4.280          | 0.021        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.36      | 133.00           | 3,954.00          | 5.500          | 0.199        |
| <b>#7</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.220</b> |
| #7        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.42      | 20.00            | 826.00            | 1.550          | 0.148        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.59      | 188.00           | 7,257.00          | 4.820          | 0.418        |
| <b>#7</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.566</b> |
| #7        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 10.34     | 74.00            | 716.00            | 3.210          | 0.061        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.74      | 132.00           | 2,785.00          | 6.530          | 0.118        |
| <b>#7</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.179</b> |
| #7        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 17.05     | 37.00            | 217.00            | 4.120          | 0.014        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.52      | 102.00           | 2,899.00          | 5.620          | 0.143        |
| <b>#7</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.157</b> |
| #7        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 0.95      | 2.00             | 211.00            | 0.970          | 0.060        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.06      | 32.00            | 3,028.00          | 3.080          | 0.273        |
| <b>#7</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.333</b> |

## ***Subwatershed Muskingum Routing Details:***

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #3        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.68      | 25.00            | 3,656.00          | 2.480          | 0.409        |
| <b>#3</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.409</b> |
| #3        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.39      | 5.00             | 1,298.00          | 1.860          | 0.193        |
| <b>#3</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.193</b> |

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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #4        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.64      | 20.00            | 3,139.00          | 2.390          | 0.364        |
| <b>#4</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.364</b> |
| #6        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.82      | 44.00            | 5,337.00          | 2.720          | 0.545        |
| <b>#6</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.545</b> |
| #6        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.47      | 82.00            | 5,593.07          | 3.630          | 0.427        |
| <b>#6</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.427</b> |
| #6        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.66      | 21.00            | 3,199.00          | 2.430          | 0.365        |
| <b>#6</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.365</b> |
| #6        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.74      | 12.00            | 1,631.00          | 2.570          | 0.176        |
| <b>#6</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.176</b> |
| #6        | 6        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#6</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.86      | 73.00            | 8,524.00          | 2.770          | 0.854        |
| <b>#7</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.854</b> |
| #7        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.89      | 58.00            | 6,527.00          | 2.820          | 0.642        |
| <b>#7</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.642</b> |
| #7        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.83      | 50.00            | 5,997.00          | 2.730          | 0.610        |
| <b>#7</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.610</b> |
| #7        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.11      | 34.00            | 3,071.00          | 3.150          | 0.270        |
| <b>#7</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.270</b> |
| #7        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |



# SEDCAD 4 for Windows - 10-Year 24-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 162.56                     | 29.77                                | 308.7              | 12,523                              | 3.66                                  | 2.22           |
| #2 | 856.430                                   | 1,855.800                             | 280.33                     | 64.71                                | 494.6              | 8,847                               | 2.26                                  | 1.44           |
| #3 | 2,374.080                                 | 4,229.880                             | 611.92                     | 177.96                               | 1,239.2            | 8,405                               | 1.82                                  | 1.10           |
| #8 | In  |                                       | 611.92                     | 177.96                               | 1,239.2            | 8,405                               | 1.82                                  | 1.10           |
|    | Out                                       | 0.000                                 | 571.92                     | 165.15                               | 929.5              | 6,960                               | 0.41                                  | 0.24           |
| #4 | 1,068.640                                 | 5,298.520                             | 620.07                     | 214.32                               | 1,675.7            | 26,789                              | 6.05                                  | 1.29           |
| #5 | 233.280                                   | 5,531.800                             | 624.80                     | 225.55                               | 1,875.5            | 27,699                              | 6.19                                  | 1.36           |
| #6 | 1,164.130                                 | 6,695.930                             | 642.03                     | 279.54                               | 2,775.0            | 27,766                              | 5.64                                  | 1.48           |
| #7 | 648.980                                   | 7,344.910                             | 652.74                     | 307.89                               | 3,362.1            | 34,942                              | 6.86                                  | 1.57           |

# SEDCAD 4 for Windows - 2-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|          | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----------|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1       | 999.370                                   | 999.370                               | 24.54                      | 4.06                                 | 35.1               | 8,569                               | 1.37                                  | 1.01           |
| #2       | 856.430                                   | 1,855.800                             | 54.18                      | 10.99                                | 68.8               | 5,906                               | 0.91                                  | 0.70           |
| #3       | 2,374.080                                 | 4,229.880                             | 162.83                     | 37.32                                | 242.2              | 6,598                               | 1.12                                  | 0.81           |
| #8<br>In | 0.000                                     | 4,229.880                             | 162.83                     | 37.32                                | 242.2              | 6,598                               | 1.12                                  | 0.81           |
| Out      |   |                                       | 93.21                      | 24.51                                | 115.9              | 5,833                               | 0.21                                  | 0.12           |
| #4       | 1,068.640                                 | 5,298.520                             | 101.16                     | 35.56                                | 234.9              | 19,908                              | 4.55                                  | 1.10           |
| #5       | 233.280                                   | 5,531.800                             | 113.85                     | 38.19                                | 290.0              | 21,442                              | 5.04                                  | 1.31           |
| #6       | 1,164.130                                 | 6,695.930                             | 163.52                     | 50.34                                | 537.0              | 23,458                              | 5.41                                  | 1.80           |
| #7       | 648.980                                   | 7,344.910                             | 173.96                     | 56.37                                | 664.8              | 28,570                              | 6.13                                  | 1.85           |



# SEDCAD 4 for Windows - 10-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 102.78                     | 14.94                                | 162.3              | 10,997                              | 2.81                                  | 2.03           |
| #2 | 856.430                                   | 1,855.800                             | 184.74                     | 34.40                                | 271.1              | 7,706                               | 1.69                                  | 1.26           |
| #3 | 2,374.080                                 | 4,229.880                             | 431.44                     | 100.54                               | 736.4              | 7,513                               | 1.50                                  | 1.07           |
| #8 | In  |                                       | 431.44                     | 100.54                               | 736.4              | 7,513                               | 1.50                                  | 1.07           |
|    | Out                                       | 0.000                                 | 382.13                     | 87.73                                | 532.0              | 6,367                               | 0.36                                  | 0.25           |
| #4 | 1,068.640                                 | 5,298.520                             | 411.91                     | 116.15                               | 958.8              | 23,926                              | 5.10                                  | 1.29           |
| #5 | 233.280                                   | 5,531.800                             | 415.11                     | 122.72                               | 1,080.4            | 24,656                              | 5.14                                  | 1.34           |
| #6 | 1,164.130                                 | 6,695.930                             | 436.61                     | 153.94                               | 1,634.7            | 24,988                              | 4.84                                  | 1.50           |
| #7 | 648.980                                   | 7,344.910                             | 459.56                     | 170.04                               | 2,019.5            | 31,828                              | 6.13                                  | 1.67           |

# SEDCAD 4 for Windows - 25-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 172.71                     | 24.46                                | 286.1              | 11,847                              | 3.37                                  | 2.44           |
| #2 | 856.430                                   | 1,855.800                             | 297.02                     | 53.97                                | 461.0              | 8,420                               | 2.09                                  | 1.56           |
| #3 | 2,374.080                                 | 4,229.880                             | 643.53                     | 150.86                               | 1,161.2            | 7,904                               | 1.65                                  | 1.18           |
| #8 | In  |                                       | 643.53                     | 150.86                               | 1,161.2            | 7,904                               | 1.65                                  | 1.18           |
|    | Out                                       | 0.000                                 | 603.72                     | 138.05                               | 901.9              | 6,632                               | 0.39                                  | 0.29           |
| #4 | 1,068.640                                 | 5,298.520                             | 655.72                     | 179.99                               | 1,593.4            | 25,101                              | 5.51                                  | 1.42           |
| #5 | 233.280                                   | 5,531.800                             | 660.92                     | 189.61                               | 1,781.2            | 25,958                              | 5.63                                  | 1.49           |
| #6 | 1,164.130                                 | 6,695.930                             | 679.87                     | 235.67                               | 2,626.8            | 26,001                              | 5.16                                  | 1.62           |
| #7 | 648.980                                   | 7,344.910                             | 684.67                     | 259.74                               | 3,161.3            | 32,691                              | 6.12                                  | 1.67           |



# SEDCAD 4 for Windows - 50-Year 6-Hour Storm Summary

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## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 238.50                     | 33.34                                | 407.6              | 12,383                              | 3.74                                  | 2.70           |
| #2 | 856.430                                   | 1,855.800                             | 400.79                     | 71.89                                | 644.6              | 8,870                               | 2.36                                  | 1.75           |
| #3 | 2,374.080                                 | 4,229.880                             | 833.00                     | 195.96                               | 1,557.5            | 8,153                               | 1.78                                  | 1.27           |
| #8 | In  |                                       | 833.00                     | 195.96                               | 1,557.5            | 8,153                               | 1.78                                  | 1.27           |
|    | Out                                       | 0.000                                 | 794.10                     | 183.15                               | 1,247.6            | 6,840                               | 0.58                                  | 0.43           |
| #4 | 1,068.640                                 | 5,298.520                             | 863.16                     | 237.10                               | 2,179.5            | 25,893                              | 5.80                                  | 1.50           |
| #5 | 233.280                                   | 5,531.800                             | 870.11                     | 249.40                               | 2,427.5            | 26,767                              | 5.95                                  | 1.58           |
| #6 | 1,164.130                                 | 6,695.930                             | 894.70                     | 308.63                               | 3,552.4            | 26,816                              | 5.48                                  | 1.72           |
| #7 | 648.980                                   | 7,344.910                             | 894.21                     | 339.81                               | 4,251.4            | 33,481                              | 6.45                                  | 1.76           |

# SEDCAD 4 for Windows - 100-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |      |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|------|
| #1 | 999.370                                   | 999.370                               | 317.38                     | 43.86                                | 557.8              | 12,883                              | 4.07                                  | 2.94           |      |
| #2 | 856.430                                   | 1,855.800                             | 522.95                     | 92.86                                | 868.3              | 9,277                               | 2.60                                  | 1.92           |      |
| #3 | 2,374.080                                 | 4,229.880                             | 1,050.99                   | 247.96                               | 2,028.7            | 8,385                               | 1.92                                  | 1.37           |      |
| #8 | In<br>Out                                 | 0.000                                 | 4,229.880                  | 1,050.99                             | 247.96             | 2,028.7                             | 8,385                                 | 1.92           | 1.37 |
|    |   |                                       |                            | 934.11                               | 235.15             | 1,646.4                             | 7,047                                 | 0.73           | 0.53 |
| #4 | 1,068.640                                 | 5,298.520                             | 1,010.93                   | 302.85                               | 2,775.0            | 26,217                              | 5.95                                  | 1.52           |      |
| #5 | 233.280                                   | 5,531.800                             | 1,021.67                   | 318.22                               | 3,091.3            | 27,184                              | 6.14                                  | 1.60           |      |
| #6 | 1,164.130                                 | 6,695.930                             | 1,068.25                   | 392.52                               | 4,543.6            | 27,354                              | 5.75                                  | 1.78           |      |
| #7 | 648.980                                   | 7,344.910                             | 1,114.89                   | 431.90                               | 5,564.1            | 34,562                              | 7.33                                  | 1.99           |      |



## **Attachment 18.B-3**

No Name Arroyo Baseline Hydrology and Sedimentology SEDCAD™ Model Output without  
Impoundment

***General Information***

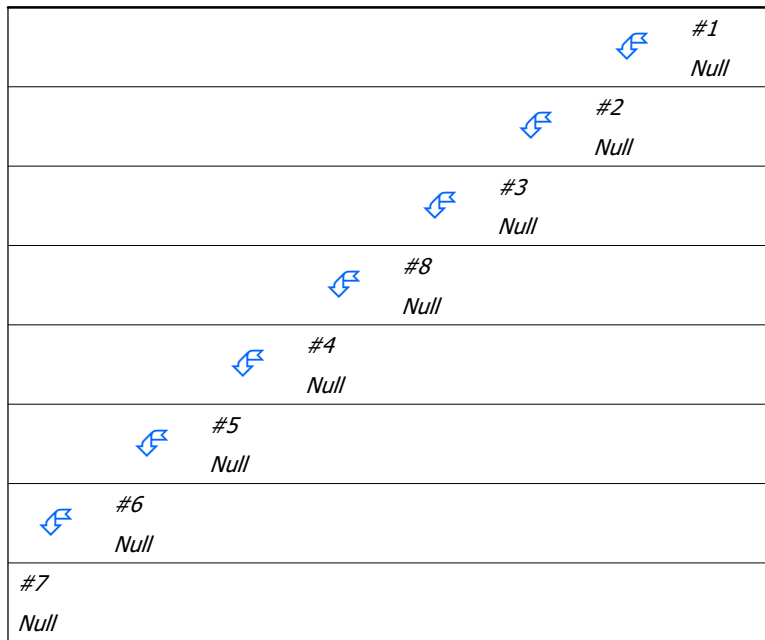
***Storm Information:***

|                 |                 |
|-----------------|-----------------|
| Storm Type:     | NRCS TYPE II-70 |
| Design Storm:   | 10 yr - 24 hr   |
| Rainfall Depth: | 1.700 inches    |



### Structure Networking:

| Type | Stru # | (flows into) | Stru # | Musk. K (hrs) | Musk. X | Description               |
|------|--------|--------------|--------|---------------|---------|---------------------------|
| Null | #1     | ==>          | #2     | 0.814         | 0.291   | SWS01                     |
| Null | #2     | ==>          | #3     | 0.656         | 0.345   | SWS02                     |
| Null | #3     | ==>          | #8     | 0.000         | 0.000   | SWS03, 04, 05             |
| Null | #4     | ==>          | #5     | 0.096         | 0.358   | SWS06, 07                 |
| Null | #5     | ==>          | #6     | 0.681         | 0.307   | SWS08                     |
| Null | #6     | ==>          | #7     | 1.027         | 0.307   | SWS09, 10, 11, 12, 13, 14 |
| Null | #7     | ==>          | End    | 0.000         | 0.000   | SWS15, 16, 17, 18, 19     |
| Null | #8     | ==>          | #4     | 0.604         | 0.309   | S03 Impoundment Area      |



### Structure Routing Details:

| Stru #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 8. Large gullies, diversions, and low flowing streams | 0.62      | 43.00            | 6,923.00          | 2.36           | 0.814        |
| <b>#1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.814</b> |
| #2        | 8. Large gullies, diversions, and low flowing streams | 1.59      | 142.00           | 8,936.00          | 3.78           | 0.656        |
| <b>#2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.656</b> |
| #4        | 8. Large gullies, diversions, and low flowing streams | 2.03      | 30.00            | 1,480.00          | 4.27           | 0.096        |
| <b>#4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.096</b> |

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| Stru #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #5        | 8. Large gullies, diversions, and low flowing streams | 0.82      | 54.00            | 6,623.00          | 2.70           | 0.681        |
| <b>#5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #6        | 8. Large gullies, diversions, and low flowing streams | 0.82      | 82.00            | 10,027.00         | 2.71           | 1.027        |
| <b>#6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.027</b> |



## ***Particle Size Distribution(s) at Each Structure***

### ***Structure #1 (SWS01):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 100.000% |
| 0.0159    | 87.633%  |
| 0.0100    | 65.880%  |
| 0.0050    | 28.144%  |
| 0.0020    | 17.046%  |
| 0.0010    | 15.702%  |
| 0.0004    | 14.553%  |

### ***Structure #2 (SWS02):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 100.000% |
| 0.0159    | 94.592%  |
| 0.0100    | 70.816%  |
| 0.0050    | 28.706%  |
| 0.0020    | 17.854%  |
| 0.0010    | 16.303%  |
| 0.0004    | 15.212%  |

### ***Structure #3 (SWS03, 04, 05):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 97.877%  |
| 0.0159    | 92.230%  |

| Size (mm) | In/Out  |
|-----------|---------|
| 0.0100    | 76.761% |
| 0.0050    | 25.622% |
| 0.0020    | 16.083% |
| 0.0010    | 14.500% |
| 0.0004    | 13.543% |

***Structure #8 (S03 Impoundment Area):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 97.877%  |
| 0.0159    | 92.230%  |
| 0.0100    | 76.761%  |
| 0.0050    | 25.622%  |
| 0.0020    | 16.083%  |
| 0.0010    | 14.500%  |
| 0.0004    | 13.543%  |

***Structure #4 (SWS06, 07):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 100.000% |
| 0.0750    | 91.615%  |
| 0.0159    | 86.011%  |
| 0.0100    | 76.336%  |
| 0.0050    | 23.361%  |
| 0.0020    | 14.325%  |
| 0.0010    | 12.926%  |
| 0.0004    | 11.968%  |

***Structure #5 (SWS08):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 99.810%  |
| 0.0750    | 93.331%  |
| 0.0159    | 86.940%  |
| 0.0100    | 76.363%  |



| Size (mm) | In/Out  |
|-----------|---------|
| 0.0050    | 23.079% |
| 0.0020    | 14.112% |
| 0.0010    | 12.756% |
| 0.0004    | 11.765% |

## ***Structure #6 (SWS09, 10, 11, 12, 13, 14):***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 99.151%  |
| 0.0750    | 90.981%  |
| 0.0159    | 86.749%  |
| 0.0100    | 78.947%  |
| 0.0050    | 22.775%  |
| 0.0020    | 13.661%  |
| 0.0010    | 12.414%  |
| 0.0004    | 11.310%  |

## ***Structure #7:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 98.085%  |
| 0.0750    | 93.580%  |
| 0.0159    | 89.264%  |
| 0.0100    | 79.577%  |
| 0.0050    | 22.691%  |
| 0.0020    | 13.507%  |
| 0.0010    | 12.286%  |
| 0.0004    | 11.166%  |

***Structure Detail:***

*Structure #1 (Null)*

*SWS01*

*Structure #2 (Null)*

*SWS02*

*Structure #3 (Null)*

*SWS03, 04, 05*

*Structure #8 (Null)*

*S03 Impoundment Area*

*Structure #4 (Null)*

*SWS06, 07*

*Structure #5 (Null)*

*SWS08*

*Structure #6 (Null)*

*SWS09, 10, 11, 12, 13, 14*

*Structure #7 (Null)*

*SWS15, 16, 17, 18, 19*



***Subwatershed Hydrology Detail:***

| Stru #    | SWS #    | SWS Area (ac)    | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|-----------|----------|------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #1        | 1        | 999.370          | 1.261              | 0.000        | 0.000  | 81.700       | M   | 162.56               | 29.766                |
|           | <b>Σ</b> | <b>999.370</b>   |                    |              |        |              |     | <b>162.56</b>        | <b>29.766</b>         |
| #2        | 1        | 856.430          | 1.610              | 0.000        | 0.000  | 85.700       | M   | 167.83               | 34.941                |
|           | <b>Σ</b> | <b>1,855.800</b> |                    |              |        |              |     | <b>280.33</b>        | <b>64.707</b>         |
| #3        | 1        | 925.920          | 1.675              | 0.409        | 0.297  | 88.800       | M   | 230.14               | 47.520                |
|           | 2        | 1,019.220        | 1.106              | 0.193        | 0.261  | 87.000       | M   | 299.75               | 45.846                |
|           | 3        | 428.940          | 0.766              | 0.000        | 0.000  | 87.400       | M   | 169.66               | 19.891                |
|           | <b>Σ</b> | <b>4,229.880</b> |                    |              |        |              |     | <b>611.92</b>        | <b>177.964</b>        |
| <b>#8</b> | <b>Σ</b> | <b>4,229.880</b> |                    |              |        |              |     | <b>611.92</b>        | <b>177.964</b>        |
| #4        | 1        | 551.860          | 0.790              | 0.364        | 0.292  | 86.200       | M   | 192.60               | 23.387                |
|           | 2        | 516.780          | 0.565              | 0.000        | 0.000  | 88.400       | M   | 271.74               | 25.785                |
|           | <b>Σ</b> | <b>5,298.520</b> |                    |              |        |              |     | <b>681.43</b>        | <b>227.135</b>        |
| #5        | 1        | 233.280          | 0.469              | 0.000        | 0.000  | 87.900       | M   | 131.66               | 11.232                |
|           | <b>Σ</b> | <b>5,531.800</b> |                    |              |        |              |     | <b>693.15</b>        | <b>238.368</b>        |
| #6        | 1        | 126.980          | 0.164              | 0.545        | 0.308  | 86.900       | M   | 101.83               | 5.787                 |
|           | 2        | 235.630          | 0.327              | 0.427        | 0.341  | 86.700       | M   | 144.93               | 10.409                |
|           | 3        | 258.380          | 0.416              | 0.365        | 0.294  | 88.300       | M   | 161.17               | 12.840                |
|           | 4        | 180.930          | 0.449              | 0.176        | 0.301  | 86.700       | M   | 94.53                | 7.968                 |
|           | 5        | 189.850          | 0.326              | 0.146        | 0.330  | 86.800       | M   | 117.89               | 8.448                 |
|           | 6        | 172.360          | 0.753              | 0.000        | 0.000  | 88.300       | M   | 74.40                | 8.537                 |
|           | <b>Σ</b> | <b>6,695.930</b> |                    |              |        |              |     | <b>729.05</b>        | <b>292.357</b>        |
| #7        | 1        | 91.450           | 0.220              | 0.854        | 0.310  | 86.800       | M   | 65.92                | 4.081                 |
|           | 2        | 286.490          | 0.566              | 0.642        | 0.312  | 87.100       | M   | 134.68               | 12.994                |
|           | 3        | 75.280           | 0.179              | 0.610        | 0.308  | 86.800       | M   | 58.49                | 3.393                 |
|           | 4        | 128.700          | 0.157              | 0.270        | 0.325  | 86.800       | M   | 102.47               | 5.822                 |
|           | 5        | 67.060           | 0.333              | 0.000        | 0.000  | 82.000       | M   | 27.39                | 2.057                 |
|           | <b>Σ</b> | <b>7,344.910</b> |                    |              |        |              |     | <b>737.87</b>        | <b>320.705</b>        |

***Subwatershed Sedimentology Detail:***

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| Stru #    | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|-----------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #1        | 1        | 0.233  | 280.00 | 2.40  | 0.2650 | 1.0000 | 1    | 308.7           | 12,523                     | 3.66                        | 2.22        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>308.7</b>    | <b>12,523</b>              | <b>3.66</b>                 | <b>2.22</b> |
| #2        | 1        | 0.245  | 420.00 | 1.40  | 0.2450 | 1.0000 | 2    | 236.1           | 7,888                      | 2.53                        | 1.60        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>494.6</b>    | <b>8,847</b>               | <b>2.26</b>                 | <b>1.44</b> |
| #3        | 1        | 0.235  | 280.00 | 2.20  | 0.2330 | 1.0000 | 3    | 399.8           | 9,626                      | 3.28                        | 2.12        |
|           | 2        | 0.204  | 280.00 | 2.30  | 0.2330 | 1.0000 | 4    | 410.4           | 10,604                     | 3.76                        | 2.33        |
|           | 3        | 0.158  | 240.00 | 3.80  | 0.2110 | 1.0000 | 5    | 198.1           | 12,102                     | 4.07                        | 2.45        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>1,239.2</b>  | <b>8,405</b>               | <b>1.82</b>                 | <b>1.10</b> |
| <b>#8</b> | <b>Σ</b> |        |        |       |        |        |      | <b>1,239.2</b>  | <b>8,405</b>               | <b>1.82</b>                 | <b>1.10</b> |
| #4        | 1        | 0.150  | 200.00 | 6.00  | 0.2320 | 1.0000 | 6    | 433.9           | 22,402                     | 7.69                        | 4.65        |
|           | 2        | 0.183  | 100.00 | 9.10  | 0.1990 | 1.0000 | 7    | 662.4           | 31,375                     | 12.99                       | 7.74        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>2,024.4</b>  | <b>27,253</b>              | <b>6.05</b>                 | <b>1.45</b> |
| #5        | 1        | 0.170  | 100.00 | 10.10 | 0.1890 | 1.0000 | 8    | 294.8           | 32,531                     | 12.94                       | 7.60        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>2,226.3</b>  | <b>28,294</b>              | <b>6.25</b>                 | <b>1.51</b> |
| #6        | 1        | 0.160  | 100.00 | 11.50 | 0.1990 | 1.0000 | 9    | 207.4           | 44,285                     | 21.06                       | 12.35       |
|           | 2        | 0.145  | 100.00 | 12.00 | 0.2110 | 1.0000 | 15   | 360.7           | 43,171                     | 18.39                       | 10.71       |
|           | 3        | 0.171  | 100.00 | 8.20  | 0.1850 | 1.0000 | 10   | 246.1           | 23,504                     | 9.41                        | 5.60        |
|           | 4        | 0.150  | 75.00  | 12.10 | 0.2110 | 1.0000 | 11   | 215.6           | 33,725                     | 13.34                       | 7.79        |
|           | 5        | 0.143  | 75.00  | 13.30 | 0.2110 | 1.0000 | 15   | 271.8           | 40,504                     | 17.28                       | 9.97        |
|           | 6        | 0.164  | 75.00  | 13.90 | 0.1850 | 1.0000 | 12   | 225.3           | 31,654                     | 9.95                        | 6.04        |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>3,144.8</b>  | <b>28,310</b>              | <b>5.83</b>                 | <b>1.62</b> |
| #7        | 1        | 0.143  | 100.00 | 10.40 | 0.2110 | 1.0000 | 15   | 110.9           | 33,271                     | 15.18                       | 9.02        |
|           | 2        | 0.162  | 75.00  | 15.20 | 0.2220 | 1.0000 | 13   | 527.1           | 48,820                     | 18.88                       | 11.36       |
|           | 3        | 0.143  | 75.00  | 20.10 | 0.2110 | 1.0000 | 15   | 180.8           | 64,982                     | 30.56                       | 18.04       |
|           | 4        | 0.143  | 100.00 | 8.10  | 0.2110 | 1.0000 | 15   | 113.6           | 24,801                     | 11.77                       | 6.76        |
|           | 5        | 0.215  | 100.00 | 8.20  | 0.2760 | 1.0000 | 14   | 61.3            | 39,773                     | 19.09                       | 10.40       |
|           | <b>Σ</b> |        |        |       |        |        |      | <b>3,729.9</b>  | <b>35,233</b>              | <b>7.02</b>                 | <b>1.69</b> |

## Subwatershed Time of Concentration Details:

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.30      | 9.00             | 692.00            | 1.140          | 0.168        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.35      | 186.00           | 13,736.00         | 3.490          | 1.093        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.261</b> |
| #2        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.06      | 11.00            | 1,041.00          | 1.020          | 0.283        |



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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.41      | 37.00            | 9,125.00          | 1.910          | 1.327        |
| <b>#2</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.610</b> |
| #3        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 0.13      | 1.00             | 743.49            | 0.360          | 0.573        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.79      | 84.00            | 10,596.69         | 2.670          | 1.102        |
| <b>#3</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.675</b> |
| #3        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.79      | 40.00            | 1,056.00          | 1.940          | 0.151        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.20      | 135.00           | 11,282.00         | 3.280          | 0.955        |
| <b>#3</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.106</b> |
| #3        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.48      | 14.00            | 945.00            | 1.210          | 0.216        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.68      | 129.00           | 7,691.00          | 3.880          | 0.550        |
| <b>#3</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.766</b> |
| #4        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 0.96      | 7.00             | 731.00            | 0.970          | 0.209        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.94      | 169.00           | 8,725.00          | 4.170          | 0.581        |
| <b>#4</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.790</b> |
| #4        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 4.40      | 43.00            | 978.00            | 2.090          | 0.129        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.35      | 170.00           | 7,224.00          | 4.600          | 0.436        |
| <b>#4</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.565</b> |
| #5        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.11      | 22.00            | 1,044.00          | 1.450          | 0.200        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.14      | 162.00           | 5,158.00          | 5.310          | 0.269        |
| <b>#5</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.469</b> |
| #6        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.94      | 12.00            | 243.00            | 2.220          | 0.030        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.62      | 144.00           | 3,117.00          | 6.440          | 0.134        |
| <b>#6</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.164</b> |
| #6        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 4.52      | 46.00            | 1,017.00          | 2.120          | 0.133        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.40      | 132.00           | 3,879.00          | 5.530          | 0.194        |
| <b>#6</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.327</b> |
| #6        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.83      | 23.00            | 813.00            | 1.680          | 0.134        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.68      | 134.00           | 4,999.00          | 4.910          | 0.282        |
| <b>#6</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.416</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 4.43      | 28.00            | 632.00            | 2.100          | 0.083        |

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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.77      | 182.00           | 6,575.00          | 4.990          | 0.366        |
| <b>#6</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.449</b> |
| #6        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 6.63      | 41.00            | 618.00            | 2.570          | 0.066        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.36      | 102.00           | 4,321.00          | 4.600          | 0.260        |
| <b>#6</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.326</b> |
| #6        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 0.41      | 4.00             | 979.00            | 0.630          | 0.431        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.88      | 170.00           | 5,907.00          | 5.080          | 0.322        |
| <b>#6</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.753</b> |
| #7        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 18.35     | 60.00            | 327.00            | 4.280          | 0.021        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.36      | 133.00           | 3,954.00          | 5.500          | 0.199        |
| <b>#7</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.220</b> |
| #7        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.42      | 20.00            | 826.00            | 1.550          | 0.148        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.59      | 188.00           | 7,257.00          | 4.820          | 0.418        |
| <b>#7</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.566</b> |
| #7        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 10.34     | 74.00            | 716.00            | 3.210          | 0.061        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.74      | 132.00           | 2,785.00          | 6.530          | 0.118        |
| <b>#7</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.179</b> |
| #7        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 17.05     | 37.00            | 217.00            | 4.120          | 0.014        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.52      | 102.00           | 2,899.00          | 5.620          | 0.143        |
| <b>#7</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.157</b> |
| #7        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 0.95      | 2.00             | 211.00            | 0.970          | 0.060        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.06      | 32.00            | 3,028.00          | 3.080          | 0.273        |
| <b>#7</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.333</b> |

## ***Subwatershed Muskingum Routing Details:***

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #3        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.68      | 25.00            | 3,656.00          | 2.480          | 0.409        |
| <b>#3</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.409</b> |
| #3        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.39      | 5.00             | 1,298.00          | 1.860          | 0.193        |
| <b>#3</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.193</b> |



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| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #4        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.64      | 20.00            | 3,139.00          | 2.390          | 0.364        |
| <b>#4</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.364</b> |
| #6        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.82      | 44.00            | 5,337.00          | 2.720          | 0.545        |
| <b>#6</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.545</b> |
| #6        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.47      | 82.00            | 5,593.07          | 3.630          | 0.427        |
| <b>#6</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.427</b> |
| #6        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.66      | 21.00            | 3,199.00          | 2.430          | 0.365        |
| <b>#6</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.365</b> |
| #6        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.74      | 12.00            | 1,631.00          | 2.570          | 0.176        |
| <b>#6</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.176</b> |
| #6        | 6        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#6</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.86      | 73.00            | 8,524.00          | 2.770          | 0.854        |
| <b>#7</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.854</b> |
| #7        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.89      | 58.00            | 6,527.00          | 2.820          | 0.642        |
| <b>#7</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.642</b> |
| #7        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.83      | 50.00            | 5,997.00          | 2.730          | 0.610        |
| <b>#7</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.610</b> |
| #7        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.11      | 34.00            | 3,071.00          | 3.150          | 0.270        |
| <b>#7</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.270</b> |
| #7        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |

# SEDCAD 4 for Windows - 10-Year 24-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 162.56                     | 29.77                                | 308.7              | 12,523                              | 3.66                                  | 2.22           |
| #2 | 856.430                                   | 1,855.800                             | 280.33                     | 64.71                                | 494.6              | 8,847                               | 2.26                                  | 1.44           |
| #3 | 2,374.080                                 | 4,229.880                             | 611.92                     | 177.96                               | 1,239.2            | 8,405                               | 1.82                                  | 1.10           |
| #8 | 0.000                                     | 4,229.880                             | 611.92                     | 177.96                               | 1,239.2            | 8,405                               | 1.82                                  | 1.10           |
| #4 | 1,068.640                                 | 5,298.520                             | 681.43                     | 227.14                               | 2,024.4            | 27,253                              | 6.05                                  | 1.45           |
| #5 | 233.280                                   | 5,531.800                             | 693.15                     | 238.37                               | 2,226.3            | 28,294                              | 6.25                                  | 1.51           |
| #6 | 1,164.130                                 | 6,695.930                             | 729.05                     | 292.36                               | 3,144.8            | 28,310                              | 5.83                                  | 1.62           |
| #7 | 648.980                                   | 7,344.910                             | 737.87                     | 320.70                               | 3,729.9            | 35,233                              | 7.02                                  | 1.69           |



# SEDCAD 4 for Windows - 2-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 24.54                      | 4.06                                 | 35.1               | 8,569                               | 1.37                                  | 1.01           |
| #2 | 856.430                                   | 1,855.800                             | 54.18                      | 10.99                                | 68.8               | 5,906                               | 0.91                                  | 0.70           |
| #3 | 2,374.080                                 | 4,229.880                             | 162.83                     | 37.32                                | 242.2              | 6,598                               | 1.12                                  | 0.81           |
| #8 | 0.000                                     | 4,229.880                             | 162.83                     | 37.32                                | 242.2              | 6,598                               | 1.12                                  | 0.81           |
| #4 | 1,068.640                                 | 5,298.520                             | 184.02                     | 48.38                                | 413.6              | 22,630                              | 4.06                                  | 1.12           |
| #5 | 233.280                                   | 5,531.800                             | 187.35                     | 51.00                                | 457.2              | 23,063                              | 4.00                                  | 1.14           |
| #6 | 1,164.130                                 | 6,695.930                             | 198.53                     | 63.15                                | 649.4              | 22,914                              | 3.78                                  | 1.24           |
| #7 | 648.980                                   | 7,344.910                             | 201.76                     | 69.18                                | 767.4              | 28,608                              | 4.36                                  | 1.24           |

# SEDCAD 4 for Windows - 10-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 102.78                     | 14.94                                | 162.3              | 10,997                              | 2.81                                  | 2.03           |
| #2 | 856.430                                   | 1,855.800                             | 184.74                     | 34.40                                | 271.1              | 7,706                               | 1.69                                  | 1.26           |
| #3 | 2,374.080                                 | 4,229.880                             | 431.44                     | 100.54                               | 736.4              | 7,513                               | 1.50                                  | 1.07           |
| #8 | 0.000                                     | 4,229.880                             | 431.44                     | 100.54                               | 736.4              | 7,513                               | 1.50                                  | 1.07           |
| #4 | 1,068.640                                 | 5,298.520                             | 482.25                     | 128.96                               | 1,216.8            | 24,685                              | 5.00                                  | 1.40           |
| #5 | 233.280                                   | 5,531.800                             | 489.89                     | 135.53                               | 1,339.9            | 25,479                              | 5.10                                  | 1.45           |
| #6 | 1,164.130                                 | 6,695.930                             | 516.87                     | 166.75                               | 1,900.8            | 25,548                              | 4.74                                  | 1.54           |
| #7 | 648.980                                   | 7,344.910                             | 523.87                     | 182.85                               | 2,253.7            | 31,814                              | 5.63                                  | 1.59           |



# SEDCAD 4 for Windows - 25-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 172.71                     | 24.46                                | 286.1              | 11,847                              | 3.37                                  | 2.44           |
| #2 | 856.430                                   | 1,855.800                             | 297.02                     | 53.97                                | 461.0              | 8,420                               | 2.09                                  | 1.56           |
| #3 | 2,374.080                                 | 4,229.880                             | 643.53                     | 150.86                               | 1,161.2            | 7,904                               | 1.65                                  | 1.18           |
| #8 | 0.000                                     | 4,229.880                             | 643.53                     | 150.86                               | 1,161.2            | 7,904                               | 1.65                                  | 1.18           |
| #4 | 1,068.640                                 | 5,298.520                             | 716.55                     | 192.81                               | 1,900.8            | 25,592                              | 5.50                                  | 1.55           |
| #5 | 233.280                                   | 5,531.800                             | 727.98                     | 202.42                               | 2,090.1            | 26,518                              | 5.66                                  | 1.61           |
| #6 | 1,164.130                                 | 6,695.930                             | 766.65                     | 248.48                               | 2,957.5            | 26,507                              | 5.28                                  | 1.73           |
| #7 | 648.980                                   | 7,344.910                             | 776.05                     | 272.55                               | 3,508.0            | 33,080                              | 6.35                                  | 1.80           |

# SEDCAD 4 for Windows - 50-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 238.50                     | 33.34                                | 407.6              | 12,383                              | 3.74                                  | 2.70           |
| #2 | 856.430                                   | 1,855.800                             | 400.79                     | 71.89                                | 644.6              | 8,870                               | 2.36                                  | 1.75           |
| #3 | 2,374.080                                 | 4,229.880                             | 833.00                     | 195.96                               | 1,557.5            | 8,153                               | 1.78                                  | 1.27           |
| #8 | 0.000                                     | 4,229.880                             | 833.00                     | 195.96                               | 1,557.5            | 8,153                               | 1.78                                  | 1.27           |
| #4 | 1,068.640                                 | 5,298.520                             | 925.53                     | 249.91                               | 2,536.1            | 26,223                              | 5.88                                  | 1.66           |
| #5 | 233.280                                   | 5,531.800                             | 941.08                     | 262.21                               | 2,787.4            | 27,237                              | 6.08                                  | 1.74           |
| #6 | 1,164.130                                 | 6,695.930                             | 988.90                     | 321.44                               | 3,935.3            | 27,254                              | 5.69                                  | 1.87           |
| #7 | 648.980                                   | 7,344.910                             | 1,000.26                   | 352.63                               | 4,668.1            | 33,908                              | 6.85                                  | 1.95           |



# SEDCAD 4 for Windows - 100-Year 6-Hour Storm Summary

Civil Software Design, LLC

## ***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 999.370                                   | 999.370                               | 317.38                     | 43.86                                | 557.8              | 12,883                              | 4.07                                  | 2.94           |
| #2 | 856.430                                   | 1,855.800                             | 522.95                     | 92.86                                | 868.3              | 9,277                               | 2.60                                  | 1.92           |
| #3 | 2,374.080                                 | 4,229.880                             | 1,050.99                   | 247.96                               | 2,028.7            | 8,385                               | 1.92                                  | 1.37           |
| #8 | 0.000                                     | 4,229.880                             | 1,050.99                   | 247.96                               | 2,028.7            | 8,385                               | 1.92                                  | 1.37           |
| #4 | 1,068.640                                 | 5,298.520                             | 1,165.55                   | 315.66                               | 3,287.9            | 26,769                              | 6.25                                  | 1.78           |
| #5 | 233.280                                   | 5,531.800                             | 1,185.81                   | 331.03                               | 3,612.0            | 27,859                              | 6.49                                  | 1.86           |
| #6 | 1,164.130                                 | 6,695.930                             | 1,244.10                   | 405.34                               | 5,090.3            | 27,832                              | 6.08                                  | 2.00           |
| #7 | 648.980                                   | 7,344.910                             | 1,257.44                   | 444.71                               | 6,038.5            | 34,529                              | 7.32                                  | 2.10           |

## **Attachment 18.B-4**

Cottonwood Arroyo Baseline Hydrology and Sedimentology SEDCAD™ Model Output



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# **Cottonwood Arroyo Pre-mine Hydrology and Sedimentology**

***The drainage subdivisions used to model the hydrology is shown  
on Exhibit 18.B.***

***Revised February 2012***

Art O'Hayre

***General Information***

***Storm Information:***

|                 |              |
|-----------------|--------------|
| Storm Type:     | Type II-70   |
| Design Storm:   | 10 yr - 6 hr |
| Rainfall Depth: | 1.280 inches |

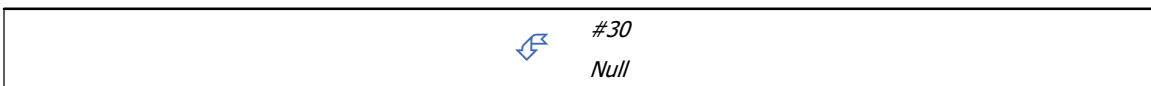
***Particle Size Distribution:***























| Size (mm) | PostMine-LoamySand | PreMine-LoamySand | PreMine-Badlands | LoamySand Postmining |
|-----------|--------------------|-------------------|------------------|----------------------|
| 2.0000    | 100.000%           | 100.000%          | 100.000%         | 0.000%               |
| 0.1000    | 26.500%            | 30.000%           | 83.500%          | 0.000%               |
| 0.0500    | 14.000%            | 17.000%           | 77.000%          | 0.000%               |
| 0.0020    | 11.000%            | 11.000%           | 56.000%          | 0.000%               |
| 0.0010    | 0.000%             | 0.000%            | 0.000%           | 0.000%               |
















### *Structure Networking:*

| Type | Stru # | (flows into) | Stru # | Musk. K (hrs) | Musk. X | Description                   |
|------|--------|--------------|--------|---------------|---------|-------------------------------|
| Null | #1     | ==>          | #2     | 0.961         | 0.307   |                               |
| Null | #2     | ==>          | #3     | 0.068         | 0.331   |                               |
| Null | #3     | ==>          | #4     | 0.000         | 0.000   |                               |
| Null | #4     | ==>          | #9     | 0.718         | 0.281   |                               |
| Null | #5     | ==>          | #6     | 1.205         | 0.328   |                               |
| Null | #6     | ==>          | #7     | 0.189         | 0.304   |                               |
| Null | #7     | ==>          | #8     | 0.000         | 0.000   |                               |
| Null | #8     | ==>          | #10    | 0.989         | 0.300   |                               |
| Null | #9     | ==>          | #11    | 0.000         | 0.000   |                               |
| Null | #10    | ==>          | #11    | 0.000         | 0.000   |                               |
| Null | #11    | ==>          | #21    | 0.495         | 0.453   |                               |
| Null | #12    | ==>          | #13    | 0.076         | 0.330   |                               |
| Null | #13    | ==>          | #14    | 3.790         | 0.314   |                               |
| Null | #14    | ==>          | #16    | 1.198         | 0.286   |                               |
| Null | #15    | ==>          | #16    | 1.198         | 0.286   |                               |
| Null | #16    | ==>          | #20    | 0.911         | 0.280   |                               |
| Null | #17    | ==>          | #19    | 0.000         | 0.000   |                               |
| Null | #18    | ==>          | #19    | 0.000         | 0.000   |                               |
| Null | #19    | ==>          | #20    | 0.915         | 0.252   |                               |
| Null | #20    | ==>          | #22    | 0.000         | 0.000   |                               |
| Null | #21    | ==>          | #22    | 0.000         | 0.000   |                               |
| Null | #22    | ==>          | #23    | 0.811         | 0.247   |                               |
| Null | #23    | ==>          | #35    | 0.000         | 0.000   |                               |
| Null | #24    | ==>          | #25    | 0.964         | 0.340   |                               |
| Null | #25    | ==>          | #27    | 1.454         | 0.333   |                               |
| Null | #26    | ==>          | #27    | 1.454         | 0.333   |                               |
| Null | #27    | ==>          | #29    | 0.800         | 0.323   |                               |
| Null | #28    | ==>          | #29    | 0.800         | 0.323   |                               |
| Null | #29    | ==>          | #32    | 0.479         | 0.298   |                               |
| Null | #30    | ==>          | #32    | 0.479         | 0.298   |                               |
| Null | #31    | ==>          | #33    | 0.000         | 0.000   |                               |
| Null | #32    | ==>          | #33    | 0.000         | 0.000   |                               |
| Null | #33    | ==>          | #34    | 1.372         | 0.293   | Inlet to North Fork Diversion |
| Null | #34    | ==>          | #35    | 0.000         | 0.000   |                               |
| Null | #35    | ==>          | #36    | 0.735         | 0.251   |                               |
| Null | #36    | ==>          | #37    | 3.388         | 0.246   |                               |
| Null | #37    | ==>          | End    | 0.000         | 0.000   |                               |



|   |   |             |   |
|---|---|-------------|---|
|   |    | #28<br>Null |   |
|   |   |             |      |
|   |   |             |    |
|   |   |             |      |
|   |   |             |      |
|   |    | #29<br>Null |   |
|   |    | #32<br>Null |   |
|   |    | #31<br>Null |   |
|   |    | #33<br>Null |   |
|  |   | #34<br>Null |   |
|   |   |             |    |
|   |   |             |  |
|   |   |             |  |
|   |   |             |    |
|   |  | #10<br>Null |   |
|   |   |             |  |
|   |   |             |  |
|   |   |             |  |
|   |   |             |    |
|   |   |             |    |
|   |  | #11<br>Null |   |
|   |  | #21<br>Null |   |



|             |   |   |
|-------------|---|---|
|             |    | #18<br>Null   |
|             |    | #17<br>Null   |
|             |    | #19<br>Null   |
|             |    | #15<br>Null   |
|             |   |  #12<br>Null |
|             |   |  #13<br>Null   |
|             |    | #14<br>Null   |
|             |    | #16<br>Null   |
|             |    | #20<br>Null   |
|             |    | #22<br>Null   |
|             |    | #23<br>Null   |
|             |  | #35<br>Null   |
|             |  | #36<br>Null   |
| #37<br>Null |   |   |

### Structure Routing Details:

| Stru #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 8. Large gullies, diversions, and low flowing streams | 0.81      | 76.00            | 9,347.00          | 2.70           | 0.961        |
| <b>#1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.961</b> |
| #2        | 8. Large gullies, diversions, and low flowing streams | 1.23      | 10.00            | 814.00            | 3.32           | 0.068        |
| <b>#2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.068</b> |
| #3        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.00           | 0.000        |
| <b>#3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #4        | 8. Large gullies, diversions, and low flowing streams | 0.53      | 30.00            | 5,637.00          | 2.18           | 0.718        |
| <b>#4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.718</b> |

| Stru #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|---|-----------|------------------|-------------------|----------------|--------------|
| #5         | 8. Large gullies, diversions, and low flowing streams | 1.17      | 165.00           | 14,065.00         | 3.24           | 1.205        |
| <b>#5</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.205</b> |
| #6         | 8. Large gullies, diversions, and low flowing streams | 0.78      | 14.00            | 1,799.25          | 2.64           | 0.189        |
| <b>#6</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.189</b> |
| #8         | 8. Large gullies, diversions, and low flowing streams | 0.72      | 65.00            | 9,046.00          | 2.54           | 0.989        |
| <b>#8</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.989</b> |
| #11        | 8. Large gullies, diversions, and low flowing streams | 30.00     | 8,801.00         | 29,336.66         | 16.43          | 0.495        |
| <b>#11</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.495</b> |
| #12        | 8. Large gullies, diversions, and low flowing streams | 1.21      | 11.00            | 906.00            | 3.30           | 0.076        |
| <b>#12</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.076</b> |
| #13        | 8. Large gullies, diversions, and low flowing streams | 0.92      | 363.00           | 39,301.00         | 2.88           | 3.790        |
| <b>#13</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.790</b> |
| #14        | 8. Large gullies, diversions, and low flowing streams | 0.58      | 57.00            | 9,834.00          | 2.28           | 1.198        |
| <b>#14</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.198</b> |
| #15        | 8. Large gullies, diversions, and low flowing streams | 0.58      | 57.00            | 9,834.00          | 2.28           | 1.198        |
| <b>#15</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.198</b> |
| #16        | 8. Large gullies, diversions, and low flowing streams | 0.52      | 37.00            | 7,084.00          | 2.16           | 0.911        |
| <b>#16</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.911</b> |
| #19        | 8. Large gullies, diversions, and low flowing streams | 0.33      | 19.00            | 5,699.00          | 1.73           | 0.915        |
| <b>#19</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.915</b> |
| #22        | 8. Large gullies, diversions, and low flowing streams | 0.31      | 15.00            | 4,852.00          | 1.66           | 0.811        |
| <b>#22</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.811</b> |
| #24        | 8. Large gullies, diversions, and low flowing streams | 1.46      | 184.00           | 12,568.00         | 3.62           | 0.964        |
| <b>#24</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.964</b> |
| #25        | 8. Large gullies, diversions, and low flowing streams | 1.28      | 228.00           | 17,755.00         | 3.39           | 1.454        |
| <b>#25</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.454</b> |
| #26        | 8. Large gullies, diversions, and low flowing streams | 1.28      | 228.00           | 17,755.62         | 3.39           | 1.454        |
| <b>#26</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.454</b> |
| #27        | 8. Large gullies, diversions, and low flowing streams | 1.07      | 96.00            | 8,938.00          | 3.10           | 0.800        |
| <b>#27</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.800</b> |
| #28        | 8. Large gullies, diversions, and low flowing streams | 1.07      | 96.00            | 8,938.00          | 3.10           | 0.800        |
| <b>#28</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.800</b> |
| #29        | 8. Large gullies, diversions, and low flowing streams | 0.70      | 30.00            | 4,313.00          | 2.50           | 0.479        |



| Stru #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#29</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.479</b> |
| #30        | 8. Large gullies, diversions, and low flowing streams | 0.70      | 30.00            | 4,313.00          | 2.50           | 0.479        |
| <b>#30</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.479</b> |
| #33        | 8. Large gullies, diversions, and low flowing streams | 0.65      | 77.00            | 11,910.00         | 2.41           | 1.372        |
| <b>#33</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.372</b> |
| #35        | 8. Large gullies, diversions, and low flowing streams | 0.33      | 15.00            | 4,554.00          | 1.72           | 0.735        |
| <b>#35</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.735</b> |
| #36        | 8. Large gullies, diversions, and low flowing streams | 0.30      | 60.00            | 20,005.00         | 1.64           | 3.388        |
| <b>#36</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.388</b> |

### ***Structure Summary:***

|     | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|-----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #30 | 476.400                                   | 476.400                               | 15.70                      | 2.21                                 | 15.3               | 7,167                               | 2.78                                  | 1.97           |
| #28 | 1,217.900                                 | 1,217.900                             | 382.70                     | 43.31                                | 2,332.2            | 55,472                              | 0.03                                  | 0.02           |
| #26 | 2,486.400                                 | 2,486.400                             | 68.99                      | 19.67                                | 120.6              | 6,040                               | 1.43                                  | 1.06           |
| #24 | 8,061.800                                 | 8,061.800                             | 94.96                      | 55.80                                | 195.1              | 4,045                               | 0.42                                  | 0.27           |
| #25 | 1,015.700                                 | 9,077.500                             | 129.82                     | 70.58                                | 314.3              | 15,722                              | 4.37                                  | 0.91           |
| #27 | 1,783.700                                 | 13,347.600                            | 257.18                     | 116.43                               | 1,049.3            | 28,391                              | 12.11                                 | 2.82           |
| #29 | 966.000                                   | 15,531.500                            | 568.72                     | 193.37                               | 5,788.0            | 69,501                              | 6.28                                  | 1.96           |
| #32 | 293.700                                   | 16,301.600                            | 577.68                     | 208.81                               | 6,156.3            | 61,380                              | 1.79                                  | 0.63           |
| #31 | 957.100                                   | 957.100                               | 385.29                     | 40.58                                | 1,766.9            | 40,461                              | 0.55                                  | 0.43           |
| #33 | 0.000                                     | 17,258.700                            | 689.75                     | 249.39                               | 7,923.2            | 52,770                              | 1.36                                  | 0.59           |
| #34 | 932.500                                   | 18,191.200                            | 700.01                     | 280.79                               | 7,357.0            | 43,693                              | 0.08                                  | 0.03           |
| #5  | 2,023.000                                 | 2,023.000                             | 569.83                     | 57.97                                | 1,713.8            | 40,068                              | 2.73                                  | 1.47           |
| #6  | 1,743.200                                 | 3,766.200                             | 653.56                     | 112.46                               | 3,143.8            | 35,092                              | 0.20                                  | 0.12           |
| #7  | 2,395.300                                 | 6,161.500                             | 1,113.99                   | 216.70                               | 8,725.2            | 44,676                              | 0.00                                  | 0.00           |
| #8  | 0.000                                     | 6,161.500                             | 1,113.99                   | 216.70                               | 8,725.2            | 44,676                              | 0.00                                  | 0.00           |
| #10 | 1,053.200                                 | 7,214.700                             | 1,133.41                   | 254.36                               | 8,518.5            | 40,724                              | 0.09                                  | 0.05           |
| #1  | 2,411.100                                 | 2,411.100                             | 392.20                     | 53.71                                | 1,765.4            | 36,630                              | 4.79                                  | 3.12           |
| #2  | 1,497.000                                 | 3,908.100                             | 470.12                     | 113.29                               | 2,441.9            | 23,797                              | 0.18                                  | 0.12           |
| #3  | 862.700                                   | 4,770.800                             | 595.07                     | 141.33                               | 2,727.8            | 18,782                              | 0.05                                  | 0.04           |
| #4  | 0.000                                     | 4,770.800                             | 595.07                     | 141.33                               | 2,727.8            | 18,782                              | 0.05                                  | 0.04           |
| #9  | 425.500                                   | 5,196.300                             | 607.92                     | 156.87                               | 2,731.1            | 16,538                              | 0.00                                  | 0.00           |
| #11 | 0.000                                     | 12,411.000                            | 1,534.59                   | 411.23                               | 11,249.6           | 33,725                              | 0.05                                  | 0.03           |
| #21 | 1,080.800                                 | 13,491.800                            | 1,588.44                   | 441.92                               | 11,292.1           | 32,718                              | 0.02                                  | 0.01           |
| #18 | 848.500                                   | 848.500                               | 183.01                     | 26.77                                | 311.1              | 14,117                              | 0.05                                  | 0.03           |
| #17 | 182.200                                   | 182.200                               | 129.55                     | 8.20                                 | 119.5              | 15,200                              | 0.69                                  | 0.49           |
| #19 | 0.000                                     | 1,030.700                             | 301.05                     | 34.98                                | 430.6              | 13,250                              | 0.20                                  | 0.14           |
| #15 | 1,992.700                                 | 1,992.700                             | 432.94                     | 58.72                                | 2,203.9            | 44,481                              | 1.26                                  | 0.77           |
| #12 | 3,494.500                                 | 3,494.500                             | 233.63                     | 38.33                                | 558.4              | 16,053                              | 6.71                                  | 4.46           |
| #13 | 2,720.700                                 | 6,215.200                             | 410.93                     | 68.61                                | 1,149.1            | 17,747                              | 8.09                                  | 5.58           |
| #14 | 5,096.800                                 | 11,312.000                            | 521.22                     | 201.24                               | 4,552.2            | 78,723                              | 1.23                                  | 0.25           |
| #16 | 876.500                                   | 14,181.200                            | 881.07                     | 298.76                               | 8,200.5            | 55,106                              | 1.30                                  | 0.47           |
| #20 | 681.900                                   | 15,893.800                            | 909.02                     | 362.94                               | 8,814.8            | 42,311                              | 0.37                                  | 0.15           |
| #22 | 0.000                                     | 29,385.600                            | 2,359.66                   | 804.86                               | 20,106.9           | 33,948                              | 0.14                                  | 0.08           |
| #23 | 752.900                                   | 30,138.500                            | 2,337.19                   | 824.67                               | 19,890.7           | 32,983                              | 0.00                                  | 0.00           |
| #35 | 0.000                                     | 48,329.700                            | 2,883.99                   | 1,105.46                             | 27,247.8           | 30,808                              | 0.01                                  | 0.01           |
| #36 | 730.590                                   | 49,060.290                            | 2,870.74                   | 1,119.67                             | 27,292.6           | 36,689                              | 0.01                                  | 0.01           |
| #37 | 2,208.500                                 | 51,268.790                            | 2,839.00                   | 1,165.01                             | 27,242.5           | 31,579                              | 0.24                                  | 0.13           |



## ***Particle Size Distribution(s) at Each Structure***

### ***Structure #30:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 61.212%  |
| 0.0020    | 39.608%  |
| 0.0010    | 0.000%   |

### ***Structure #28:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.873%  |
| 0.0010    | 0.000%   |

### ***Structure #26:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 84.182%  |
| 0.0020    | 54.471%  |
| 0.0010    | 0.000%   |

### ***Structure #24:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 93.900%  |
| 0.0020    | 78.509%  |
| 0.0010    | 0.000%   |

**Structure #25:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 80.595%  |
| 0.0500    | 68.505%  |
| 0.0020    | 61.192%  |
| 0.0010    | 0.000%   |

**Structure #27:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 75.314%  |
| 0.0500    | 52.685%  |
| 0.0020    | 39.141%  |
| 0.0010    | 0.000%   |

**Structure #29:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 95.562%  |
| 0.0500    | 91.459%  |
| 0.0020    | 85.259%  |
| 0.0010    | 0.000%   |

**Structure #32:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.317%  |
| 0.0020    | 92.618%  |
| 0.0010    | 0.000%   |

**Structure #31:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 96.135%  |
| 0.0010    | 0.000%   |



**Structure #33 (Inlet to North Fork Diversion):**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.470%  |
| 0.0020    | 93.402%  |
| 0.0010    | 0.000%   |

**Structure #34:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.500%  |
| 0.0010    | 0.000%   |

**Structure #5:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 93.455%  |
| 0.0020    | 88.980%  |
| 0.0010    | 0.000%   |

**Structure #6:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.356%  |
| 0.0010    | 0.000%   |

**Structure #7:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #8:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #10:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.796%  |
| 0.0020    | 99.658%  |
| 0.0010    | 0.000%   |

**Structure #1:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 95.498%  |
| 0.0500    | 85.914%  |
| 0.0020    | 80.819%  |
| 0.0010    | 0.000%   |

**Structure #2:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 97.866%  |
| 0.0010    | 0.000%   |

**Structure #3:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.192%  |
| 0.0010    | 0.000%   |



**Structure #4:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.192%  |
| 0.0010    | 0.000%   |

**Structure #9:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #11:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.845%  |
| 0.0020    | 99.741%  |
| 0.0010    | 0.000%   |

**Structure #21:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.791%  |
| 0.0010    | 0.000%   |

**Structure #18:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.022%  |
| 0.0010    | 0.000%   |

**Structure #17:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 87.184%  |
| 0.0010    | 0.000%   |

**Structure #19:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 95.736%  |
| 0.0010    | 0.000%   |

**Structure #15:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 98.087%  |
| 0.0020    | 94.423%  |
| 0.0010    | 0.000%   |

**Structure #12:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 83.026%  |
| 0.0500    | 56.746%  |
| 0.0020    | 36.718%  |
| 0.0010    | 0.000%   |

**Structure #13:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 80.507%  |
| 0.0500    | 51.093%  |
| 0.0020    | 33.060%  |
| 0.0010    | 0.000%   |



**Structure #14:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 95.609%  |
| 0.0010    | 0.000%   |

**Structure #16:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.498%  |
| 0.0020    | 93.958%  |
| 0.0010    | 0.000%   |

**Structure #20:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 97.546%  |
| 0.0010    | 0.000%   |

**Structure #22:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.807%  |
| 0.0010    | 0.000%   |

**Structure #23:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #35:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.865%  |
| 0.0010    | 0.000%   |

**Structure #36:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.890%  |
| 0.0010    | 0.000%   |

**Structure #37:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.235%  |
| 0.0020    | 98.796%  |
| 0.0010    | 0.000%   |



**Structure Detail:**

Structure #30 (Null)

Structure #28 (Null)

Structure #26 (Null)

Structure #24 (Null)

Structure #25 (Null)

Structure #27 (Null)

Structure #29 (Null)

Structure #32 (Null)

Structure #31 (Null)

Structure #33 (Null)

*Inlet to North Fork Diversion*

Structure #34 (Null)

Structure #5 (Null)

Structure #6 (Null)

Structure #7 (Null)

Structure #8 (Null)

Structure #10 (Null)

Structure #1 (Null)

Structure #2 (Null)

Structure #3 (Null)

Structure #4 (Null)

Structure #9 (Null)

Structure #11 (Null)

Structure #21 (Null)

Structure #18 (Null)

Structure #17 (Null)

Structure #19 (Null)

Structure #15 (Null)

Structure #12 (Null)

Structure #13 (Null)

Structure #14 (Null)

Structure #16 (Null)

Structure #20 (Null)

Structure #22 (Null)

Structure #23 (Null)

Structure #35 (Null)

Structure #36 (Null)

Structure #37 (Null)



### *Subwatershed Hydrology Detail:*

| Stru #     | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|------------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #30        | 1        | 476.400           | 1.131              | 0.000        | 0.000  | 73.100       | M   | 15.70                | 2.214                 |
|            | <b>Σ</b> | <b>476.400</b>    |                    |              |        |              |     | <b>15.70</b>         | <b>2.214</b>          |
| #28        | 1        | 772.300           | 0.657              | 0.523        | 0.334  | 90.400       | M   | 348.71               | 27.461                |
|            | 2        | 445.600           | 0.587              | 0.000        | 0.000  | 90.400       | M   | 217.35               | 15.851                |
|            | <b>Σ</b> | <b>1,217.900</b>  |                    |              |        |              |     | <b>382.70</b>        | <b>43.312</b>         |
| #26        | 1        | 447.600           | 2.192              | 0.000        | 0.000  | 74.200       | M   | 10.72                | 2.498                 |
|            | 2        | 2,038.800         | 3.000              | 0.000        | 0.000  | 77.000       | M   | 59.31                | 17.168                |
|            | <b>Σ</b> | <b>2,486.400</b>  |                    |              |        |              |     | <b>68.99</b>         | <b>19.666</b>         |
| #24        | 1        | 2,607.500         | 5.367              | 2.377        | 0.305  | 75.200       | M   | 35.68                | 16.987                |
|            | 2        | 2,331.900         | 4.813              | 2.431        | 0.304  | 74.700       | M   | 32.19                | 14.077                |
|            | 3        | 1,758.500         | 2.231              | 1.788        | 0.297  | 76.200       | M   | 57.92                | 13.255                |
|            | 4        | 1,363.900         | 2.618              | 0.000        | 0.000  | 77.000       | M   | 44.42                | 11.485                |
|            | <b>Σ</b> | <b>8,061.800</b>  |                    |              |        |              |     | <b>94.96</b>         | <b>55.804</b>         |
| #25        | 1        | 515.200           | 0.990              | 0.342        | 0.357  | 78.200       | M   | 44.10                | 5.083                 |
|            | 2        | 130.500           | 0.787              | 0.342        | 0.357  | 78.100       | M   | 13.16                | 1.271                 |
|            | 3        | 370.000           | 0.516              | 0.000        | 0.000  | 85.700       | M   | 125.08               | 8.421                 |
|            | <b>Σ</b> | <b>9,077.500</b>  |                    |              |        |              |     | <b>129.82</b>        | <b>70.579</b>         |
| #27        | 1        | 354.400           | 0.612              | 1.233        | 0.337  | 83.100       | M   | 81.00                | 6.173                 |
|            | 2        | 305.200           | 0.529              | 1.054        | 0.328  | 84.000       | M   | 85.27                | 5.846                 |
|            | 3        | 289.800           | 0.692              | 0.551        | 0.328  | 75.500       | M   | 21.73                | 1.976                 |
|            | 4        | 253.000           | 0.361              | 0.551        | 0.328  | 79.400       | M   | 53.79                | 2.908                 |
|            | 5        | 581.300           | 0.980              | 0.000        | 0.000  | 82.300       | M   | 84.68                | 9.284                 |
|            | <b>Σ</b> | <b>13,347.600</b> |                    |              |        |              |     | <b>257.18</b>        | <b>116.433</b>        |
| #29        | 1        | 508.800           | 0.409              | 0.416        | 0.312  | 89.500       | M   | 285.47               | 16.691                |
|            | 2        | 233.200           | 0.521              | 0.291        | 0.312  | 91.600       | M   | 136.95               | 9.256                 |
|            | 3        | 224.000           | 0.467              | 0.000        | 0.000  | 90.000       | M   | 121.81               | 7.678                 |
|            | <b>Σ</b> | <b>15,531.500</b> |                    |              |        |              |     | <b>568.72</b>        | <b>193.370</b>        |
| #32        | 1        | 293.700           | 0.576              | 0.000        | 0.000  | 93.000       | M   | 183.24               | 13.227                |
|            | <b>Σ</b> | <b>16,301.600</b> |                    |              |        |              |     | <b>577.68</b>        | <b>208.811</b>        |
| #31        | 1        | 431.100           | 0.588              | 0.450        | 0.336  | 91.500       | M   | 232.24               | 16.956                |
|            | 2        | 325.800           | 0.432              | 0.149        | 0.327  | 93.000       | M   | 240.11               | 14.690                |
|            | 3        | 200.200           | 0.373              | 0.000        | 0.000  | 92.900       | M   | 157.01               | 8.931                 |
|            | <b>Σ</b> | <b>957.100</b>    |                    |              |        |              |     | <b>385.29</b>        | <b>40.576</b>         |
| <b>#33</b> | <b>Σ</b> | <b>17,258.700</b> |                    |              |        |              |     | <b>689.75</b>        | <b>249.387</b>        |

| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS  | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|------|----------------------|-----------------------|
| #34    | 1        | 91.700            | 0.244              | 0.965        | 0.300  | 92.300       | M    | 80.75                | 3.907                 |
|        | 2        | 105.200           | 0.256              | 0.965        | 0.300  | 93.000       | M    | 96.06                | 4.763                 |
|        | 3        | 735.600           | 0.885              | 0.000        | 0.000  | 88.900       | M    | 231.14               | 22.735                |
|        | <b>Σ</b> | <b>18,191.200</b> |                    |              |        |              |      | <b>700.01</b>        | <b>280.792</b>        |
| #5     | 1        | 503.600           | 0.618              | 0.000        | 0.000  | 87.600       | M    | 181.32               | 13.768                |
|        | 2        | 406.500           | 0.388              | 0.501        | 0.350  | 84.800       | M    | 150.41               | 8.450                 |
|        | 3        | 439.600           | 0.342              | 0.681        | 0.347  | 87.800       | M    | 231.97               | 12.313                |
|        | 4        | 162.600           | 0.280              | 0.681        | 0.347  | 86.000       | M    | 79.58                | 3.825                 |
|        | 5        | 294.100           | 0.375              | 1.021        | 0.348  | 92.000       | M    | 213.88               | 12.088                |
|        | 6        | 216.600           | 0.272              | 1.018        | 0.348  | 90.100       | M    | 154.07               | 7.526                 |
|        | <b>Σ</b> | <b>2,023.000</b>  |                    |              |        |              |      | <b>569.83</b>        | <b>57.970</b>         |
| #6     | 1        | 149.100           | 0.331              | 0.000        | 0.000  | 92.600       | M    | 120.20               | 6.499                 |
|        | 2        | 245.000           | 0.529              | 0.192        | 0.328  | 88.100       | M    | 103.04               | 7.033                 |
|        | 3        | 276.200           | 0.450              | 0.461        | 0.319  | 89.500       | M    | 146.70               | 9.035                 |
|        | 4        | 158.400           | 0.380              | 1.385        | 0.185  | 93.000       | M    | 124.15               | 7.126                 |
|        | 5        | 206.200           | 0.402              | 0.796        | 0.320  | 89.400       | M    | 115.74               | 6.701                 |
|        | 6        | 414.000           | 0.430              | 1.066        | 0.323  | 87.200       | M    | 181.89               | 10.921                |
|        | 7        | 294.300           | 0.535              | 1.066        | 0.323  | 86.400       | M    | 104.00               | 7.171                 |
|        | <b>Σ</b> | <b>3,766.200</b>  |                    |              |        |              |      | <b>653.56</b>        | <b>112.457</b>        |
| #7     | 1        | 731.700           | 1.274              | 0.000        | 0.000  | 93.000       | M    | 255.12               | 32.900                |
|        | 2        | 445.800           | 1.043              | 0.000        | 0.000  | 93.000       | M    | 182.08               | 20.038                |
|        | 3        | 270.800           | 0.804              | 0.000        | 0.000  | 93.000       | M    | 134.47               | 12.176                |
|        | 4        | 78.900            | 0.267              | 1.035        | 0.328  | 93.000       | M    | 71.04                | 3.568                 |
|        | 5        | 154.900           | 0.310              | 1.071        | 0.326  | 93.000       | M    | 132.26               | 6.996                 |
|        | 6        | 101.400           | 0.288              | 1.164        | 0.328  | 92.900       | M    | 88.35                | 4.536                 |
|        | 7        | 117.700           | 0.298              | 1.344        | 0.329  | 92.200       | M    | 95.91                | 4.942                 |
|        | 8        | 494.100           | 0.518              | 1.344        | 0.329  | 91.300       | M    | 283.54               | 19.084                |
|        | <b>Σ</b> | <b>6,161.500</b>  |                    |              |        |              |      | <b>1,113.99</b>      | <b>216.697</b>        |
| #8     | 1        | 0.000             | 0.000              | 0.000        | 0.000  | 1.000        | 0.00 | 0.000                |                       |
|        | <b>Σ</b> | <b>6,161.500</b>  |                    |              |        |              |      | <b>1,113.99</b>      | <b>216.697</b>        |
| #10    | 1        | 355.500           | 1.286              | 0.000        | 0.000  | 93.000       | M    | 123.01               | 15.981                |
|        | 2        | 307.100           | 1.282              | 0.668        | 0.305  | 83.200       | M    | 39.93                | 5.401                 |
|        | 3        | 147.300           | 1.245              | 0.517        | 0.303  | 90.600       | M    | 41.73                | 5.327                 |
|        | 4        | 126.400           | 0.585              | 0.517        | 0.303  | 93.000       | M    | 78.09                | 5.694                 |
|        | 5        | 116.900           | 1.179              | 0.621        | 0.305  | 93.000       | M    | 43.37                | 5.257                 |
|        | <b>Σ</b> | <b>7,214.700</b>  |                    |              |        |              |      | <b>1,133.41</b>      | <b>254.357</b>        |
| #1     | 1        | 557.400           | 0.941              | 0.000        | 0.000  | 83.600       | M    | 97.16                | 10.228                |
|        | 2        | 169.600           | 1.616              | 0.677        | 0.333  | 93.000       | M    | 48.64                | 7.624                 |
|        | 3        | 636.400           | 1.842              | 0.729        | 0.333  | 81.000       | M    | 47.29                | 8.792                 |
|        | 4        | 223.400           | 0.846              | 1.005        | 0.336  | 84.100       | M    | 44.68                | 4.320                 |



| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS   | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|-------|----------------------|-----------------------|
|        | 5        | 77.700            | 0.330              | 1.392        | 0.341  | 81.400       | M     | 22.18                | 1.129                 |
|        | 6        | 746.600           | 0.678              | 1.392        | 0.341  | 88.200       | M     | 267.03               | 21.621                |
|        | <b>Σ</b> | <b>2,411.100</b>  |                    |              |        |              |       | <b>392.20</b>        | <b>53.715</b>         |
| #2     | 1        | 257.000           | 0.423              | 0.000        | 0.000  | 93.000       | M     | 191.46               | 11.596                |
|        | 2        | 180.500           | 0.562              | 0.478        | 0.281  | 91.800       | M     | 102.88               | 7.288                 |
|        | 3        | 200.700           | 0.687              | 0.574        | 0.283  | 93.000       | M     | 111.40               | 9.029                 |
|        | 4        | 438.600           | 0.811              | 0.574        | 0.283  | 93.000       | M     | 216.42               | 19.727                |
|        | 5        | 420.200           | 1.247              | 0.801        | 0.293  | 88.000       | M     | 92.44                | 11.930                |
|        | <b>Σ</b> | <b>3,908.100</b>  |                    |              |        |              |       | <b>470.12</b>        | <b>113.285</b>        |
| #3     | 1        | 172.600           | 0.443              | 0.000        | 0.000  | 93.000       | M     | 125.54               | 7.770                 |
|        | 2        | 311.200           | 0.890              | 0.000        | 0.000  | 88.900       | M     | 97.37                | 9.620                 |
|        | 3        | 378.900           | 0.632              | 0.209        | 0.314  | 87.900       | M     | 138.33               | 10.658                |
|        | <b>Σ</b> | <b>4,770.800</b>  |                    |              |        |              |       | <b>595.07</b>        | <b>141.332</b>        |
| #4     | <b>Σ</b> | <b>4,770.800</b>  |                    |              |        |              |       | <b>595.07</b>        | <b>141.332</b>        |
| #9     | 1        | 425.500           | 0.830              | 0.000        | 0.000  | 90.700       | M     | 166.84               | 15.542                |
|        | <b>Σ</b> | <b>5,196.300</b>  |                    |              |        |              |       | <b>607.92</b>        | <b>156.874</b>        |
| #11    | <b>Σ</b> | <b>12,411.000</b> |                    |              |        |              |       | <b>1,534.59</b>      | <b>411.231</b>        |
| #21    | 1        | 272.800           | 0.819              | 0.000        | 0.000  | 86.900       | M     | 74.74                | 6.974                 |
|        | 2        | 230.500           | 0.388              | 0.694        | 0.266  | 89.200       | M     | 129.51               | 7.335                 |
|        | 3        | 181.100           | 0.289              | 0.877        | 0.256  | 91.300       | M     | 138.97               | 7.007                 |
|        | 4        | 396.400           | 0.939              | 0.877        | 0.256  | 86.100       | M     | 90.27                | 9.371                 |
|        | <b>Σ</b> | <b>13,491.800</b> |                    |              |        |              |       | <b>1,588.44</b>      | <b>441.918</b>        |
| #18    | 1        | 301.700           | 0.652              | 0.000        | 0.000  | 93.000       | M     | 173.54               | 13.585                |
|        | 2        | 546.800           | 0.768              | 0.561        | 0.320  | 86.300       | M     | 148.05               | 13.189                |
|        | <b>Σ</b> | <b>848.500</b>    |                    |              |        |              |       | <b>183.01</b>        | <b>26.774</b>         |
| #17    | 1        | 182.200           | 0.462              | 0.000        | 0.000  | 93.000       | M     | 129.55               | 8.202                 |
|        | <b>Σ</b> | <b>182.200</b>    |                    |              |        |              |       | <b>129.55</b>        | <b>8.202</b>          |
| #19    | <b>Σ</b> | <b>1,030.700</b>  |                    |              |        |              |       | <b>301.05</b>        | <b>34.976</b>         |
| #15    | 1        | 437.400           | 0.803              | 0.000        | 0.000  | 91.300       | M     | 185.92               | 16.863                |
|        | 2        | 549.000           | 0.637              | 0.654        | 0.327  | 91.300       | M     | 275.19               | 21.177                |
|        | 3        | 1,006.300         | 1.023              | 0.768        | 0.331  | 84.700       | M     | 185.11               | 20.683                |
|        | <b>Σ</b> | <b>1,992.700</b>  |                    |              |        |              |       | <b>432.94</b>        | <b>58.723</b>         |
| #12    | 1        | 517.800           | 0.791              | 0.000        | 0.000  | 81.900       | M     | 85.06                | 7.915                 |
|        | 2        | 229.000           | 0.571              | 0.043        | 0.418  | 80.100       | M     | 38.64                | 2.855                 |
|        | 3        | 592.700           | 0.706              | 0.044        | 0.417  | 81.500       | M     | 101.30               | 8.668                 |
|        | 4        | 1,806.900         | 1.542              | 0.487        | 0.362  | 76.700       | M     | 86.99                | 14.604                |
|        | 5        | 348.100           | 0.618              | 0.487        | 0.362  | 80.000       | 54.66 | 4.285                |                       |

| Stru #   | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|----------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| <b>Σ</b> |          | <b>3,494.500</b>  |                    |              |        |              |     | <b>233.63</b>        | <b>38.327</b>         |
| #13      | 1        | 411.600           | 0.725              | 0.000        | 0.000  | 79.700       | M   | 55.06                | 4.891                 |
|          | 2        | 636.400           | 0.774              | 0.322        | 0.336  | 80.700       | M   | 91.95                | 8.503                 |
|          | 3        | 319.000           | 0.575              | 0.685        | 0.318  | 85.500       | M   | 98.20                | 7.115                 |
|          | 4        | 231.700           | 0.314              | 0.923        | 0.328  | 80.400       | M   | 60.73                | 3.000                 |
|          | 5        | 1,122.000         | 1.308              | 0.923        | 0.328  | 74.700       | M   | 44.53                | 6.775                 |
| <b>Σ</b> |          | <b>6,215.200</b>  |                    |              |        |              |     | <b>410.93</b>        | <b>68.612</b>         |
| #14      | 1        | 405.900           | 0.384              | 0.000        | 0.000  | 90.800       | M   | 263.85               | 14.961                |
|          | 2        | 411.100           | 0.452              | 0.707        | 0.308  | 90.700       | M   | 242.63               | 15.020                |
|          | 3        | 787.400           | 0.658              | 0.975        | 0.307  | 91.400       | M   | 389.56               | 30.676                |
|          | 4        | 144.200           | 0.341              | 1.716        | 0.310  | 86.200       | M   | 65.46                | 3.461                 |
|          | 5        | 343.800           | 0.289              | 1.970        | 0.312  | 86.500       | M   | 173.76               | 8.480                 |
|          | 6        | 392.800           | 0.806              | 2.107        | 0.316  | 81.900       | M   | 63.61                | 6.004                 |
|          | 7        | 528.200           | 0.518              | 2.544        | 0.316  | 87.200       | M   | 206.25               | 13.918                |
|          | 8        | 890.900           | 1.253              | 2.544        | 0.316  | 83.500       | M   | 122.07               | 16.175                |
|          | 9        | 741.400           | 1.076              | 3.047        | 0.316  | 84.800       | M   | 132.42               | 15.394                |
|          | 10       | 451.100           | 0.916              | 3.354        | 0.316  | 83.900       | M   | 83.00                | 8.542                 |
| <b>Σ</b> |          | <b>11,312.000</b> |                    |              |        |              |     | <b>521.22</b>        | <b>201.243</b>        |
| #16      | 1        | 329.600           | 0.641              | 0.000        | 0.000  | 93.000       | M   | 191.76               | 14.834                |
|          | 2        | 348.400           | 0.542              | 0.509        | 0.286  | 92.500       | M   | 216.12               | 14.980                |
|          | 3        | 198.500           | 0.266              | 0.943        | 0.279  | 93.000       | M   | 178.92               | 8.977                 |
| <b>Σ</b> |          | <b>14,181.200</b> |                    |              |        |              |     | <b>881.07</b>        | <b>298.756</b>        |
| #20      | 1        | 296.300           | 0.667              | 0.000        | 0.000  | 91.700       | M   | 149.26               | 11.862                |
|          | 2        | 385.600           | 0.713              | 0.476        | 0.440  | 93.000       | M   | 208.57               | 17.345                |
| <b>Σ</b> |          | <b>15,893.800</b> |                    |              |        |              |     | <b>909.02</b>        | <b>362.939</b>        |
| #22      | <b>Σ</b> | <b>29,385.600</b> |                    |              |        |              |     | <b>2,359.66</b>      | <b>804.857</b>        |
| #23      | 1        | 442.400           | 0.960              | 0.000        | 0.000  | 85.300       | M   | 91.16                | 9.657                 |
|          | 2        | 310.500           | 0.538              | 0.559        | 0.291  | 89.500       | M   | 147.54               | 10.156                |
| <b>Σ</b> |          | <b>30,138.500</b> |                    |              |        |              |     | <b>2,337.19</b>      | <b>824.670</b>        |
| #35      | <b>Σ</b> | <b>48,329.700</b> |                    |              |        |              |     | <b>2,883.99</b>      | <b>1,105.461</b>      |
| #36      | 1        | 298.200           | 0.987              | 0.000        | 0.000  | 85.000       | M   | 58.26                | 6.317                 |
|          | 2        | 196.800           | 0.441              | 0.000        | 0.000  | 87.900       | M   | 91.10                | 5.542                 |
|          | 3        | 235.590           | 0.885              | 0.166        | 0.372  | 78.300       | M   | 22.32                | 2.354                 |
| <b>Σ</b> |          | <b>49,060.290</b> |                    |              |        |              |     | <b>2,870.74</b>      | <b>1,119.675</b>      |
| #37      | 1        | 744.000           | 1.756              | 0.000        | 0.000  | 84.800       | M   | 88.80                | 15.442                |
|          | 2        | 296.000           | 0.439              | 1.780        | 0.243  | 87.800       | M   | 136.09               | 8.260                 |
|          | 3        | 237.700           | 0.333              | 1.649        | 0.246  | 85.500       | M   | 102.26               | 5.321                 |
|          | 4        | 561.400           | 1.502              | 1.780        | 0.243  | 84.100       | M   | 70.78                | 10.848                |



| Stru #   | SWS # | SWS Area (ac) | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |                  |
|----------|-------|---------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|------------------|
|          | 5     | 369.400       | 0.817              | 2.236        | 0.284  | 81.600       | M   | 57.12                | 5.464                 |                  |
| <b>Σ</b> |       |               |                    |              |        |              |     | <b>51,268.790</b>    | <b>2,839.00</b>       | <b>1,165.010</b> |

***Subwatershed Sedimentology Detail:***

| Stru #   | SWS # | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|----------|-------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #30      | 1     | 0.095  | 200.00 | 3.80  | 0.3720 | 1.0000 | 2    | 15.3            | 7,167                      | 2.78                        | 1.97        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>15.3</b>     | <b>7,167</b>               | <b>2.78</b>                 | <b>1.97</b> |
| #28      | 1     | 0.187  | 100.00 | 10.10 | 0.3750 | 1.0000 | 3    | 1,831.9         | 67,442                     | 0.00                        | 0.00        |
|          | 2     | 0.196  | 100.00 | 10.20 | 0.3930 | 1.0000 | 3    | 1,151.2         | 74,204                     | 0.07                        | 0.05        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>2,332.2</b>  | <b>55,472</b>              | <b>0.03</b>                 | <b>0.02</b> |
| #26      | 1     | 0.155  | 400.00 | 1.40  | 0.3480 | 1.0000 | 2    | 10.2            | 4,082                      | 1.09                        | 0.81        |
|          | 2     | 0.155  | 300.00 | 2.40  | 0.3340 | 1.0000 | 2    | 110.4           | 6,393                      | 1.49                        | 1.10        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>120.6</b>    | <b>6,040</b>               | <b>1.43</b>                 | <b>1.06</b> |
| #24      | 1     | 0.128  | 300.00 | 2.30  | 0.3360 | 1.0000 | 2    | 66.0            | 3,840                      | 0.35                        | 0.26        |
|          | 2     | 0.136  | 300.00 | 2.70  | 0.3440 | 1.0000 | 2    | 70.5            | 4,930                      | 0.50                        | 0.37        |
|          | 3     | 0.107  | 300.00 | 2.30  | 0.3330 | 1.0000 | 2    | 62.4            | 4,664                      | 1.37                        | 1.02        |
|          | 4     | 0.163  | 400.00 | 1.60  | 0.3210 | 1.0000 | 2    | 57.9            | 5,031                      | 1.35                        | 0.99        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>195.1</b>    | <b>4,045</b>               | <b>0.42</b>                 | <b>0.27</b> |
| #25      | 1     | 0.125  | 400.00 | 1.90  | 0.3440 | 1.0000 | 2    | 34.8            | 7,104                      | 3.32                        | 2.35        |
|          | 2     | 0.124  | 300.00 | 2.60  | 0.3280 | 1.0000 | 2    | 9.3             | 7,737                      | 3.85                        | 2.68        |
|          | 3     | 0.122  | 175.00 | 4.90  | 0.2660 | 1.0000 | 2    | 138.2           | 17,512                     | 10.27                       | 7.04        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>314.3</b>    | <b>15,722</b>              | <b>4.37</b>                 | <b>0.91</b> |
| #27      | 1     | 0.127  | 175.00 | 5.90  | 0.3160 | 1.0000 | 2    | 134.4           | 22,614                     | 12.66                       | 8.90        |
|          | 2     | 0.122  | 150.00 | 7.50  | 0.2920 | 1.0000 | 2    | 138.7           | 24,759                     | 14.29                       | 9.99        |
|          | 3     | 0.070  | 125.00 | 8.40  | 0.3270 | 1.0000 | 2    | 23.7            | 12,704                     | 6.26                        | 4.32        |
|          | 4     | 0.097  | 125.00 | 9.60  | 0.3170 | 1.0000 | 2    | 80.5            | 30,075                     | 17.67                       | 11.85       |
|          | 5     | 0.126  | 125.00 | 8.90  | 0.3290 | 1.0000 | 2    | 239.4           | 26,689                     | 13.37                       | 9.42        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>1,049.3</b>  | <b>28,391</b>              | <b>12.11</b>                | <b>2.82</b> |
| #29      | 1     | 0.190  | 125.00 | 9.80  | 0.3930 | 1.0000 | 3    | 1,365.3         | 83,318                     | 3.07                        | 2.16        |
|          | 2     | 0.203  | 125.00 | 8.90  | 0.3940 | 1.0000 | 3    | 603.0           | 66,304                     | 1.59                        | 1.12        |
|          | 3     | 0.193  | 125.00 | 8.40  | 0.3940 | 1.0000 | 3    | 441.4           | 59,660                     | 1.55                        | 1.08        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>5,788.0</b>  | <b>69,501</b>              | <b>6.28</b>                 | <b>1.96</b> |
| #32      | 1     | 0.210  | 150.00 | 7.70  | 0.3990 | 1.0000 | 3    | 811.1           | 62,434                     | 1.37                        | 0.97        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>6,156.3</b>  | <b>61,380</b>              | <b>1.79</b>                 | <b>0.63</b> |

| Stru #     | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|------------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #31        | 1        | 0.204  | 125.00 | 8.70  | 0.3620 | 1.0000 | 3    | 1,013.7         | 60,814                     | 0.53                        | 0.37        |
|            | 2        | 0.210  | 150.00 | 7.30  | 0.3990 | 1.0000 | 3    | 950.2           | 65,819                     | 3.41                        | 2.41        |
|            | 3        | 0.210  | 175.00 | 4.50  | 0.3980 | 1.0000 | 3    | 385.8           | 44,601                     | 2.82                        | 1.98        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>1,766.9</b>  | <b>40,461</b>              | <b>0.55</b>                 | <b>0.43</b> |
| <b>#33</b> | <b>Σ</b> |        |        |       |        |        |      | <b>7,923.2</b>  | <b>52,770</b>              | <b>1.36</b>                 | <b>0.59</b> |
| #34        | 1        | 0.189  | 175.00 | 4.60  | 0.2250 | 1.0000 | 3    | 86.5            | 22,344                     | 1.96                        | 1.42        |
|            | 2        | 0.206  | 175.00 | 5.10  | 0.3620 | 1.0000 | 3    | 206.3           | 43,231                     | 3.80                        | 2.76        |
|            | 3        | 0.176  | 175.00 | 4.20  | 0.2510 | 1.0000 | 3    | 400.7           | 18,159                     | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>7,357.0</b>  | <b>43,693</b>              | <b>0.08</b>                 | <b>0.03</b> |
| #5         | 1        | 0.149  | 75.00  | 12.50 | 0.3230 | 1.0000 | 3    | 670.0           | 50,428                     | 0.00                        | 0.00        |
|            | 2        | 0.133  | 75.00  | 15.80 | 0.3190 | 1.0000 | 2    | 545.2           | 67,505                     | 40.75                       | 28.02       |
|            | 3        | 0.103  | 100.00 | 11.00 | 0.2030 | 1.0000 | 3    | 312.6           | 26,590                     | 1.17                        | 0.81        |
|            | 4        | 0.093  | 75.00  | 13.80 | 0.2130 | 1.0000 | 2    | 96.3            | 26,589                     | 16.60                       | 11.46       |
|            | 5        | 0.123  | 100.00 | 11.00 | 0.1370 | 1.0000 | 3    | 238.9           | 20,258                     | 1.18                        | 0.84        |
|            | 6        | 0.149  | 75.00  | 14.70 | 0.1990 | 1.0000 | 3    | 330.1           | 44,599                     | 3.21                        | 2.28        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>1,713.8</b>  | <b>40,068</b>              | <b>2.73</b>                 | <b>1.47</b> |
| #6         | 1        | 0.208  | 175.00 | 4.30  | 0.3980 | 1.0000 | 3    | 263.3           | 41,902                     | 2.95                        | 2.07        |
|            | 2        | 0.183  | 175.00 | 5.40  | 0.3910 | 1.0000 | 3    | 271.1           | 40,223                     | 0.00                        | 0.00        |
|            | 3        | 0.188  | 150.00 | 7.60  | 0.3900 | 1.0000 | 3    | 500.1           | 56,955                     | 1.53                        | 1.07        |
|            | 4        | 0.210  | 150.00 | 6.30  | 0.3990 | 1.0000 | 3    | 380.9           | 52,378                     | 3.26                        | 2.41        |
|            | 5        | 0.185  | 125.00 | 8.10  | 0.3860 | 1.0000 | 3    | 351.4           | 53,638                     | 2.03                        | 1.44        |
|            | 6        | 0.104  | 100.00 | 11.30 | 0.2240 | 1.0000 | 3    | 295.4           | 27,989                     | 0.49                        | 0.34        |
|            | 7        | 0.164  | 100.00 | 11.20 | 0.3740 | 1.0000 | 3    | 444.3           | 63,189                     | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>3,143.8</b>  | <b>35,092</b>              | <b>0.20</b>                 | <b>0.12</b> |
| #7         | 1        | 0.208  | 150.00 | 7.80  | 0.3780 | 1.0000 | 3    | 1,546.4         | 47,076                     | 0.00                        | 0.00        |
|            | 2        | 0.209  | 100.00 | 10.20 | 0.3940 | 1.0000 | 3    | 1,272.4         | 63,450                     | 0.00                        | 0.00        |
|            | 3        | 0.210  | 150.00 | 6.70  | 0.3990 | 1.0000 | 3    | 570.4           | 47,474                     | 0.00                        | 0.00        |
|            | 4        | 0.210  | 100.00 | 11.50 | 0.3990 | 1.0000 | 3    | 343.1           | 94,143                     | 8.06                        | 5.87        |
|            | 5        | 0.210  | 150.00 | 7.10  | 0.3990 | 1.0000 | 3    | 436.9           | 62,203                     | 4.78                        | 3.45        |
|            | 6        | 0.209  | 150.00 | 7.90  | 0.3990 | 1.0000 | 3    | 301.6           | 65,955                     | 5.34                        | 3.87        |
|            | 7        | 0.206  | 75.00  | 15.50 | 0.3990 | 1.0000 | 3    | 593.0           | 116,344                    | 8.81                        | 6.42        |
|            | 8        | 0.202  | 75.00  | 14.50 | 0.3980 | 1.0000 | 3    | 2,089.2         | 107,811                    | 2.44                        | 1.76        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>8,725.2</b>  | <b>44,676</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #8         | 1        | 0.000  | 0.00   | 0.00  | 0.0000 | 1.0000 | 0    | 0.0             | 1                          | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>8,725.2</b>  | <b>44,676</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #10        | 1        | 0.190  | 300.00 | 2.70  | 0.1930 | 1.0000 | 3    | 125.7           | 8,003                      | 0.00                        | 0.00        |
|            | 2        | 0.153  | 200.00 | 3.50  | 0.3610 | 1.0000 | 2    | 61.7            | 11,607                     | 5.45                        | 3.93        |
|            | 3        | 0.189  | 200.00 | 3.70  | 0.3190 | 1.0000 | 3    | 72.2            | 13,712                     | 0.00                        | 0.00        |
|            | 4        | 0.190  | 300.00 | 2.10  | 0.1940 | 1.0000 | 3    | 43.8            | 7,943                      | 0.16                        | 0.11        |



| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 5        | 0.201  | 300.00 | 2.00  | 0.3030 | 1.0000 | 3    | 47.8            | 9,191                      | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>8,518.5</b>  | <b>40,724</b>              | <b>0.09</b>                 | <b>0.05</b> |
| #1     | 1        | 0.157  | 150.00 | 6.80  | 0.3830 | 1.0000 | 2    | 313.9           | 31,708                     | 16.32                       | 11.49       |
|        | 2        | 0.210  | 150.00 | 6.60  | 0.3990 | 1.0000 | 3    | 244.8           | 32,032                     | 0.00                        | 0.00        |
|        | 3        | 0.149  | 200.00 | 3.90  | 0.3870 | 1.0000 | 2    | 102.9           | 11,753                     | 4.57                        | 3.34        |
|        | 4        | 0.169  | 175.00 | 4.70  | 0.3950 | 1.0000 | 2    | 105.8           | 25,092                     | 13.31                       | 9.47        |
|        | 5        | 0.157  | 100.00 | 10.10 | 0.3940 | 1.0000 | 2    | 57.7            | 53,203                     | 32.06                       | 22.27       |
|        | 6        | 0.175  | 75.00  | 12.60 | 0.2840 | 1.0000 | 3    | 1,117.8         | 52,264                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>1,765.4</b>  | <b>36,630</b>              | <b>4.79</b>                 | <b>3.12</b> |
| #2     | 1        | 0.190  | 150.00 | 7.90  | 0.1930 | 1.0000 | 3    | 346.0           | 30,942                     | 1.66                        | 1.16        |
|        | 2        | 0.184  | 175.00 | 4.80  | 0.2010 | 1.0000 | 3    | 127.8           | 18,066                     | 0.30                        | 0.21        |
|        | 3        | 0.202  | 200.00 | 3.90  | 0.3220 | 1.0000 | 3    | 190.3           | 21,517                     | 0.00                        | 0.00        |
|        | 4        | 0.203  | 150.00 | 7.40  | 0.3220 | 1.0000 | 3    | 837.0           | 42,735                     | 0.00                        | 0.00        |
|        | 5        | 0.181  | 175.00 | 5.10  | 0.3710 | 1.0000 | 3    | 305.1           | 25,752                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>2,441.9</b>  | <b>23,797</b>              | <b>0.18</b>                 | <b>0.12</b> |
| #3     | 1        | 0.190  | 175.00 | 5.20  | 0.1930 | 1.0000 | 3    | 158.4           | 21,221                     | 1.05                        | 0.74        |
|        | 2        | 0.177  | 175.00 | 4.20  | 0.2560 | 1.0000 | 3    | 156.5           | 16,762                     | 0.00                        | 0.00        |
|        | 3        | 0.166  | 175.00 | 4.30  | 0.2290 | 1.0000 | 3    | 173.0           | 16,953                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>2,727.8</b>  | <b>18,782</b>              | <b>0.05</b>                 | <b>0.04</b> |
| #4     | <b>Σ</b> |        |        |       |        |        |      | <b>2,727.8</b>  | <b>18,782</b>              | <b>0.05</b>                 | <b>0.04</b> |
| #9     | 1        | 0.189  | 175.00 | 4.44  | 0.1970 | 1.0000 | 3    | 239.5           | 15,887                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>2,731.1</b>  | <b>16,538</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #11    | <b>Σ</b> |        |        |       |        |        |      | <b>11,249.6</b> | <b>33,725</b>              | <b>0.05</b>                 | <b>0.03</b> |
| #21    | 1        | 0.177  | 175.00 | 4.44  | 0.2560 | 1.0000 | 3    | 118.7           | 17,681                     | 0.00                        | 0.00        |
|        | 2        | 0.184  | 175.00 | 5.81  | 0.2210 | 1.0000 | 3    | 192.2           | 27,033                     | 1.09                        | 0.77        |
|        | 3        | 0.185  | 300.00 | 2.70  | 0.2180 | 1.0000 | 3    | 93.1            | 13,510                     | 0.99                        | 0.72        |
|        | 4        | 0.175  | 300.00 | 2.66  | 0.2690 | 1.0000 | 3    | 99.3            | 10,803                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>11,292.1</b> | <b>32,718</b>              | <b>0.02</b>                 | <b>0.01</b> |
| #18    | 1        | 0.193  | 300.00 | 2.80  | 0.2200 | 1.0000 | 3    | 166.4           | 12,680                     | 0.08                        | 0.06        |
|        | 2        | 0.173  | 175.00 | 4.70  | 0.3880 | 1.0000 | 3    | 388.7           | 30,310                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>311.1</b>    | <b>14,117</b>              | <b>0.05</b>                 | <b>0.03</b> |
| #17    | 1        | 0.196  | 300.00 | 2.60  | 0.2600 | 1.0000 | 3    | 119.5           | 15,200                     | 0.69                        | 0.49        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>119.5</b>    | <b>15,200</b>              | <b>0.69</b>                 | <b>0.49</b> |
| #19    | <b>Σ</b> |        |        |       |        |        |      | <b>430.6</b>    | <b>13,250</b>              | <b>0.20</b>                 | <b>0.14</b> |
| #15    | 1        | 0.201  | 125.00 | 8.20  | 0.3960 | 1.0000 | 3    | 875.5           | 52,729                     | 0.00                        | 0.00        |
|        | 2        | 0.161  | 100.00 | 11.40 | 0.3060 | 1.0000 | 3    | 1,156.8         | 55,407                     | 0.00                        | 0.00        |
|        | 3        | 0.118  | 100.00 | 10.20 | 0.2850 | 1.0000 | 2    | 533.7           | 26,236                     | 13.40                       | 9.61        |

| Stru #   | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|----------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| <b>Σ</b> |          |        |        |       |        |        |      | <b>2,203.9</b>  | <b>44,481</b>              | <b>1.26</b>                 | <b>0.77</b> |
| #12      | 1        | 0.124  | 150.00 | 6.30  | 0.3070 | 1.0000 | 2    | 148.5           | 19,741                     | 10.37                       | 7.20        |
|          | 2        | 0.132  | 200.00 | 3.60  | 0.3500 | 1.0000 | 2    | 36.4            | 13,817                     | 7.60                        | 5.13        |
|          | 3        | 0.136  | 175.00 | 5.00  | 0.3330 | 1.0000 | 2    | 177.8           | 21,738                     | 11.65                       | 8.02        |
|          | 4        | 0.188  | 200.00 | 3.40  | 0.3570 | 1.0000 | 2    | 197.1           | 13,622                     | 5.15                        | 3.73        |
|          | 5        | 0.228  | 175.00 | 4.10  | 0.3640 | 1.0000 | 2    | 128.9           | 31,777                     | 17.19                       | 11.85       |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>558.4</b>    | <b>16,053</b>              | <b>6.71</b>                 | <b>4.46</b> |
| #13      | 1        | 0.128  | 150.00 | 6.90  | 0.3390 | 1.0000 | 2    | 110.5           | 23,979                     | 12.49                       | 8.59        |
|          | 2        | 0.130  | 175.00 | 5.70  | 0.3300 | 1.0000 | 2    | 178.6           | 21,951                     | 11.41                       | 7.97        |
|          | 3        | 0.191  | 175.00 | 6.00  | 0.2890 | 1.0000 | 2    | 226.5           | 33,049                     | 19.05                       | 13.35       |
|          | 4        | 0.122  | 175.00 | 5.10  | 0.3460 | 1.0000 | 2    | 69.8            | 24,833                     | 14.95                       | 10.22       |
|          | 5        | 0.137  | 175.00 | 4.20  | 0.3530 | 1.0000 | 2    | 88.6            | 13,184                     | 5.06                        | 3.67        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>1,149.1</b>  | <b>17,747</b>              | <b>8.09</b>                 | <b>5.58</b> |
| #14      | 1        | 0.196  | 100.00 | 10.20 | 0.3980 | 1.0000 | 3    | 1,259.0         | 86,487                     | 4.31                        | 3.00        |
|          | 2        | 0.193  | 150.00 | 6.70  | 0.4020 | 1.0000 | 3    | 826.2           | 56,062                     | 1.89                        | 1.34        |
|          | 3        | 0.169  | 75.00  | 13.80 | 0.3240 | 1.0000 | 3    | 2,082.9         | 67,952                     | 0.00                        | 0.00        |
|          | 4        | 0.114  | 100.00 | 11.00 | 0.2980 | 1.0000 | 3    | 122.8           | 36,090                     | 1.27                        | 0.91        |
|          | 5        | 0.078  | 100.00 | 10.10 | 0.1830 | 1.0000 | 3    | 130.6           | 15,659                     | 0.79                        | 0.57        |
|          | 6        | 0.084  | 150.00 | 7.10  | 0.2700 | 1.0000 | 2    | 72.2            | 12,296                     | 6.43                        | 4.61        |
|          | 7        | 0.087  | 100.00 | 10.00 | 0.1840 | 1.0000 | 3    | 203.3           | 14,793                     | 0.00                        | 0.00        |
|          | 8        | 0.126  | 150.00 | 6.70  | 0.2740 | 1.0000 | 2    | 261.0           | 16,178                     | 7.68                        | 5.60        |
|          | 9        | 0.117  | 150.00 | 7.30  | 0.2600 | 1.0000 | 2    | 254.1           | 16,557                     | 8.36                        | 6.10        |
|          | 10       | 0.115  | 125.00 | 8.50  | 0.2610 | 1.0000 | 2    | 152.1           | 17,901                     | 9.30                        | 6.77        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>4,552.2</b>  | <b>78,723</b>              | <b>1.23</b>                 | <b>0.25</b> |
| #16      | 1        | 0.200  | 200.00 | 3.30  | 0.3000 | 1.0000 | 3    | 269.1           | 18,736                     | 0.16                        | 0.12        |
|          | 2        | 0.204  | 150.00 | 6.00  | 0.3630 | 1.0000 | 3    | 664.4           | 45,187                     | 1.15                        | 0.82        |
|          | 3        | 0.210  | 150.00 | 6.10  | 0.3990 | 1.0000 | 3    | 514.2           | 56,689                     | 4.87                        | 3.55        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>8,200.5</b>  | <b>55,106</b>              | <b>1.30</b>                 | <b>0.47</b> |
| #20      | 1        | 0.186  | 175.00 | 4.80  | 0.2130 | 1.0000 | 3    | 221.4           | 19,337                     | 0.00                        | 0.00        |
|          | 2        | 0.194  | 200.00 | 3.80  | 0.2330 | 1.0000 | 3    | 264.4           | 15,676                     | 0.00                        | 0.00        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>8,814.8</b>  | <b>42,311</b>              | <b>0.37</b>                 | <b>0.15</b> |
| #22      | <b>Σ</b> |        |        |       |        |        |      | <b>20,106.9</b> | <b>33,948</b>              | <b>0.14</b>                 | <b>0.08</b> |
| #23      | 1        | 0.172  | 175.00 | 4.20  | 0.2810 | 1.0000 | 3    | 161.2           | 17,281                     | 0.00                        | 0.00        |
|          | 2        | 0.185  | 150.00 | 6.00  | 0.2160 | 1.0000 | 3    | 232.8           | 23,728                     | 0.14                        | 0.10        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>19,890.7</b> | <b>32,983</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #35      | <b>Σ</b> |        |        |       |        |        |      | <b>27,247.8</b> | <b>30,808</b>              | <b>0.01</b>                 | <b>0.01</b> |
| #36      | 1        | 0.190  | 175.00 | 5.94  | 0.2830 | 1.0000 | 3    | 152.8           | 24,939                     | 0.00                        | 0.00        |
|          | 2        | 0.180  | 125.00 | 9.92  | 0.2410 | 1.0000 | 3    | 230.0           | 43,767                     | 0.83                        | 0.57        |



| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 3        | 0.151  | 300.00 | 2.63  | 0.3890 | 1.0000 | 2    | 25.9            | 11,526                     | 5.58                        | 3.90        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>27,292.6</b> | <b>36,689</b>              | <b>0.01</b>                 | <b>0.01</b> |
| #37    | 1        | 0.196  | 200.00 | 3.80  | 0.3980 | 1.0000 | 2    | 265.1           | 17,384                     | 7.49                        | 5.41        |
|        | 2        | 0.193  | 175.00 | 5.40  | 0.4020 | 1.0000 | 3    | 375.9           | 45,440                     | 0.86                        | 0.62        |
|        | 3        | 0.173  | 150.00 | 7.11  | 0.2770 | 1.0000 | 3    | 185.8           | 35,144                     | 1.19                        | 0.86        |
|        | 4        | 0.171  | 150.00 | 6.52  | 0.2990 | 1.0000 | 2    | 221.9           | 20,384                     | 9.20                        | 6.74        |
|        | 5        | 0.078  | 400.00 | 1.20  | 0.1830 | 1.0000 | 2    | 9.4             | 1,760                      | 0.91                        | 0.66        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>27,242.5</b> | <b>31,579</b>              | <b>0.24</b>                 | <b>0.13</b> |

### Subwatershed Time of Concentration Details:

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.65      | 50.00            | 1,369.00          | 1.910          | 0.199        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.57      | 157.00           | 10,030.00         | 3.750          | 0.742        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.941</b> |
| #1        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 6.63      | 70.00            | 1,056.00          | 2.570          | 0.114        |
|           |          | 5. Nearly bare and untilled, and alluvial valley fans | 1.98      | 150.00           | 7,573.00          | 1.400          | 1.502        |
| <b>#1</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.616</b> |
| #1        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.65      | 117.00           | 7,070.00          | 1.280          | 1.534        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.43      | 126.00           | 5,188.00          | 4.670          | 0.308        |
| <b>#1</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.842</b> |
| #1        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 5.77      | 260.00           | 4,506.00          | 2.400          | 0.521        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.84      | 168.00           | 5,924.00          | 5.050          | 0.325        |
| <b>#1</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.846</b> |
| #1        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 19.93     | 180.00           | 903.00            | 4.460          | 0.056        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.30      | 178.00           | 5,393.00          | 5.450          | 0.274        |
| <b>#1</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.330</b> |
| #1        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 13.43     | 105.00           | 782.00            | 3.660          | 0.059        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.62      | 283.00           | 10,822.00         | 4.850          | 0.619        |
| <b>#1</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.678</b> |
| #2        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 6.84      | 70.00            | 1,024.00          | 2.610          | 0.108        |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 70.00            | 4,325.00          | 3.810          | 0.315        |
| <b>#2</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.423</b> |
| #2        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.56      | 45.00            | 810.00            | 2.350          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.86      | 40.00            | 4,663.00          | 2.770          | 0.467        |
| <b>#2</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.562</b> |
| #2        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 5.89      | 50.00            | 849.00            | 2.420          | 0.097        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.17      | 80.00            | 6,862.00          | 3.230          | 0.590        |
| <b>#2</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.687</b> |
| #2        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 12.63     | 95.00            | 752.00            | 3.550          | 0.058        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.40      | 135.00           | 9,630.00          | 3.550          | 0.753        |
| <b>#2</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.811</b> |
| #2        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 11.02     | 70.00            | 635.00            | 3.320          | 0.053        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.46      | 40.00            | 8,732.00          | 2.030          | 1.194        |
| <b>#2</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.247</b> |
| #3        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 10.00            | 805.00            | 1.110          | 0.201        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.33      | 40.00            | 3,017.00          | 3.450          | 0.242        |
| <b>#3</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.443</b> |
| #3        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 0.68      | 10.00            | 1,478.00          | 0.820          | 0.500        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.78      | 100.00           | 5,622.00          | 4.000          | 0.390        |
| <b>#3</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.890</b> |
| #3        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.66      | 70.00            | 1,501.00          | 2.150          | 0.193        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.17      | 60.00            | 5,126.00          | 3.240          | 0.439        |
| <b>#3</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.632</b> |
| #5        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 19.06     | 285.00           | 1,495.00          | 4.360          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.64      | 242.00           | 9,174.00          | 4.870          | 0.523        |
| <b>#5</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.618</b> |
| #5        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 14.27     | 105.00           | 736.00            | 3.770          | 0.054        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.08      | 297.00           | 7,279.00          | 6.050          | 0.334        |
| <b>#5</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.388</b> |
| #5        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 8.27      | 35.00            | 423.00            | 2.870          | 0.040        |



| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.44      | 208.00           | 6,049.00          | 5.560          | 0.302        |
| <b>#5</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.342</b> |
| #5        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 14.58     | 85.00            | 583.00            | 3.810          | 0.042        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.53      | 248.00           | 5,473.00          | 6.380          | 0.238        |
| <b>#5</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.280</b> |
| #5        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 5.07      | 70.00            | 1,382.00          | 2.250          | 0.170        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.89      | 170.00           | 4,375.00          | 5.910          | 0.205        |
| <b>#5</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.375</b> |
| #5        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 12.48     | 90.00            | 721.00            | 3.530          | 0.056        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 5.16      | 274.00           | 5,308.02          | 6.810          | 0.216        |
| <b>#5</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.272</b> |
| #6        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 5.36      | 75.00            | 1,399.00          | 2.310          | 0.168        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.41      | 66.00            | 2,742.00          | 4.650          | 0.163        |
| <b>#6</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.331</b> |
| #6        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 80.00            | 2,359.00          | 1.840          | 0.356        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.63      | 80.00            | 3,039.00          | 4.860          | 0.173        |
| <b>#6</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.529</b> |
| #6        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.60      | 34.00            | 739.00            | 2.140          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.33      | 136.00           | 5,845.00          | 4.570          | 0.355        |
| <b>#6</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.450</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 6.06      | 85.00            | 1,402.00          | 2.460          | 0.158        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.52      | 96.00            | 3,810.00          | 4.760          | 0.222        |
| <b>#6</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.380</b> |
| #6        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 7.24      | 70.00            | 967.00            | 2.690          | 0.099        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.34      | 117.00           | 5,003.00          | 4.580          | 0.303        |
| <b>#6</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.402</b> |
| #6        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 31.83     | 183.00           | 575.00            | 5.640          | 0.028        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.38      | 270.00           | 7,990.00          | 5.510          | 0.402        |
| <b>#6</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.430</b> |
| #6        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 23.08     | 325.00           | 1,408.00          | 4.800          | 0.081        |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.88      | 240.00           | 8,327.00          | 5.090          | 0.454        |
| <b>#6</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.535</b> |
| #7        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.42     | 90.00            | 788.00            | 3.370          | 0.064        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.46      | 230.00           | 15,769.00         | 3.620          | 1.210        |
| <b>#7</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.274</b> |
| #7        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 10.97     | 60.00            | 547.00            | 3.310          | 0.045        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.61      | 220.00           | 13,660.00         | 3.800          | 0.998        |
| <b>#7</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.043</b> |
| #7        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 6.40      | 60.00            | 938.00            | 2.520          | 0.103        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.72      | 171.00           | 9,931.00          | 3.930          | 0.701        |
| <b>#7</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.804</b> |
| #7        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 19.23     | 80.00            | 416.00            | 4.380          | 0.026        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.45      | 100.00           | 4,083.00          | 4.690          | 0.241        |
| <b>#7</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.267</b> |
| #7        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 6.09      | 67.00            | 1,101.00          | 2.460          | 0.124        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.51      | 80.00            | 3,184.00          | 4.750          | 0.186        |
| <b>#7</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.310</b> |
| #7        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 5.93      | 63.00            | 1,062.00          | 2.430          | 0.121        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.74      | 82.00            | 2,993.00          | 4.960          | 0.167        |
| <b>#7</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.288</b> |
| #7        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 7.97      | 65.00            | 816.00            | 2.820          | 0.080        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.48      | 153.00           | 4,400.00          | 5.590          | 0.218        |
| <b>#7</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.298</b> |
| #7        | 8        | 5. Nearly bare and untilled, and alluvial valley fans | 6.60      | 50.00            | 758.00            | 2.560          | 0.082        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.66      | 473.00           | 10,157.00         | 6.470          | 0.436        |
| <b>#7</b> | <b>8</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.518</b> |
| #9        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.35      | 90.00            | 2,687.00          | 1.830          | 0.407        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.58      | 20.00            | 3,463.00          | 2.270          | 0.423        |
| <b>#9</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.830</b> |
| #10       | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 41.00            | 3,317.00          | 1.110          | 0.830        |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.70      | 29.00            | 4,125.00          | 2.510          | 0.456        |
| <b>#10</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.286</b> |
| #10        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.25      | 125.00           | 5,554.00          | 1.500          | 1.028        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 85.00            | 3,997.00          | 4.370          | 0.254        |
| <b>#10</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.282</b> |
| #10        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.39      | 68.00            | 4,904.00          | 1.170          | 1.164        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.73      | 90.00            | 1,904.00          | 6.520          | 0.081        |
| <b>#10</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.245</b> |
| #10        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.76      | 51.00            | 1,357.00          | 1.930          | 0.195        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.65      | 22.00            | 3,385.00          | 2.410          | 0.390        |
| <b>#10</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.585</b> |
| #10        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 1.63      | 88.00            | 5,391.16          | 1.270          | 1.179        |
| <b>#10</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.179</b> |
| #12        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.50      | 75.00            | 1,667.00          | 2.120          | 0.218        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.85      | 155.00           | 8,400.00          | 4.070          | 0.573        |
| <b>#12</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.791</b> |
| #12        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.99      | 50.00            | 1,674.03          | 1.720          | 0.270        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.67      | 70.00            | 4,201.17          | 3.870          | 0.301        |
| <b>#12</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.571</b> |
| #12        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.04      | 57.00            | 1,411.00          | 2.000          | 0.195        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.55      | 107.00           | 6,884.00          | 3.740          | 0.511        |
| <b>#12</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.706</b> |
| #12        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.23      | 84.00            | 3,771.04          | 1.490          | 0.703        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 186.00           | 11,515.60         | 3.810          | 0.839        |
| <b>#12</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.542</b> |
| #12        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.68      | 53.00            | 1,442.00          | 1.910          | 0.209        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.95      | 120.00           | 6,155.00          | 4.180          | 0.409        |
| <b>#12</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.618</b> |
| #13        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.62      | 62.00            | 1,342.00          | 2.140          | 0.174        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.91      | 157.00           | 8,225.00          | 4.140          | 0.551        |
| <b>#13</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.725</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #13        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.91      | 50.00            | 1,717.00          | 1.700          | 0.280        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.28      | 183.00           | 8,039.00          | 4.520          | 0.494        |
| <b>#13</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.774</b> |
| #13        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 6.18      | 95.00            | 1,537.00          | 2.480          | 0.172        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 135.00           | 6,347.00          | 4.370          | 0.403        |
| <b>#13</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.575</b> |
| #13        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.17      | 10.00            | 315.00            | 1.780          | 0.049        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.30      | 100.00           | 4,344.00          | 4.550          | 0.265        |
| <b>#13</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.314</b> |
| #13        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.10      | 70.00            | 2,255.00          | 1.760          | 0.355        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.23      | 140.00           | 11,392.00         | 3.320          | 0.953        |
| <b>#13</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.308</b> |
| #14        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 10.59     | 63.00            | 595.00            | 3.250          | 0.050        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.60      | 151.00           | 5,808.00          | 4.830          | 0.334        |
| <b>#14</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.384</b> |
| #14        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.28      | 67.00            | 920.00            | 2.690          | 0.095        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.17      | 123.00           | 5,670.00          | 4.410          | 0.357        |
| <b>#14</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.452</b> |
| #14        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 21.46     | 150.00           | 699.00            | 4.630          | 0.041        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.10      | 364.00           | 11,728.00         | 5.280          | 0.617        |
| <b>#14</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.658</b> |
| #14        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 35.00            | 1,032.00          | 1.840          | 0.155        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.97      | 103.00           | 3,470.00          | 5.160          | 0.186        |
| <b>#14</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.341</b> |
| #14        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 28.15     | 125.00           | 444.00            | 5.300          | 0.023        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.18      | 246.00           | 5,886.00          | 6.130          | 0.266        |
| <b>#14</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.289</b> |
| #14        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 3.18      | 40.00            | 1,257.00          | 1.780          | 0.196        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.29      | 228.00           | 9,963.00          | 4.530          | 0.610        |
| <b>#14</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.806</b> |



| Stru #     | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #14        | 7         | 5. Nearly bare and untilled, and alluvial valley fans | 16.72     | 100.00           | 598.00            | 4.080          | 0.040        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.81      | 243.00           | 8,649.00          | 5.020          | 0.478        |
| <b>#14</b> | <b>7</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.518</b> |
| #14        | 8         | 5. Nearly bare and untilled, and alluvial valley fans | 1.70      | 47.00            | 2,765.00          | 1.300          | 0.590        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.44      | 274.00           | 11,208.00         | 4.690          | 0.663        |
| <b>#14</b> | <b>8</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.253</b> |
| #14        | 9         | 5. Nearly bare and untilled, and alluvial valley fans | 2.87      | 105.00           | 3,657.00          | 1.690          | 0.601        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.43      | 194.00           | 7,991.00          | 4.670          | 0.475        |
| <b>#14</b> | <b>9</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.076</b> |
| #14        | 10        | 5. Nearly bare and untilled, and alluvial valley fans | 2.75      | 80.00            | 2,907.00          | 1.650          | 0.489        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.41      | 172.00           | 7,149.00          | 4.650          | 0.427        |
| <b>#14</b> | <b>10</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.916</b> |
| #15        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 12.80     | 54.00            | 422.00            | 3.570          | 0.032        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.68      | 181.00           | 10,781.00         | 3.880          | 0.771        |
| <b>#15</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.803</b> |
| #15        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 44.22     | 260.00           | 588.00            | 6.640          | 0.024        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.45      | 254.00           | 10,354.00         | 4.690          | 0.613        |
| <b>#15</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.637</b> |
| #15        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 10.04     | 85.00            | 847.00            | 3.160          | 0.074        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.34      | 366.00           | 15,663.00         | 4.580          | 0.949        |
| <b>#15</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.023</b> |
| #16        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 4.17      | 15.00            | 360.00            | 2.040          | 0.049        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.42      | 108.00           | 7,618.00          | 3.570          | 0.592        |
| <b>#16</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.641</b> |
| #16        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 8.70      | 62.00            | 713.00            | 2.940          | 0.067        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.99      | 144.00           | 7,241.00          | 4.230          | 0.475        |
| <b>#16</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.542</b> |
| #16        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 6.88      | 32.00            | 465.00            | 2.620          | 0.049        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.29      | 81.00            | 3,543.00          | 4.530          | 0.217        |
| <b>#16</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.266</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #17        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 9.37      | 65.00            | 694.00            | 3.060          | 0.062        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.19      | 56.00            | 4,712.00          | 3.270          | 0.400        |
| <b>#17</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.462</b> |
| #18        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 9.00      | 60.00            | 667.00            | 2.990          | 0.061        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.97      | 61.00            | 6,287.00          | 2.950          | 0.591        |
| <b>#18</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.652</b> |
| #18        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.47      | 33.00            | 1,336.00          | 1.570          | 0.236        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.01      | 164.00           | 8,154.00          | 4.250          | 0.532        |
| <b>#18</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.768</b> |
| #20        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.87     | 45.00            | 379.00            | 3.440          | 0.030        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.75      | 45.00            | 5,969.00          | 2.600          | 0.637        |
| <b>#20</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.667</b> |
| #20        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.40      | 45.00            | 833.00            | 2.320          | 0.099        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.30      | 98.00            | 7,547.00          | 3.410          | 0.614        |
| <b>#20</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.713</b> |
| #21        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.09      | 60.00            | 1,467.00          | 2.020          | 0.201        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.93      | 60.00            | 6,433.00          | 2.890          | 0.618        |
| <b>#21</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.819</b> |
| #21        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.50      | 50.00            | 1,430.00          | 1.860          | 0.213        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.15      | 60.00            | 2,785.00          | 4.400          | 0.175        |
| <b>#21</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.388</b> |
| #21        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.70      | 15.00            | 881.00            | 1.300          | 0.188        |
|            |          | 9. Small streams flowing bankfull                     | 1.49      | 60.00            | 4,014.00          | 11.000         | 0.101        |
| <b>#21</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.289</b> |
| #21        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.21      | 40.00            | 1,811.02          | 1.480          | 0.339        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.84      | 50.00            | 5,949.54          | 2.750          | 0.600        |
| <b>#21</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.939</b> |
| #23        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.44      | 65.00            | 2,660.01          | 1.560          | 0.473        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.33      | 10.00            | 3,017.50          | 1.720          | 0.487        |
| <b>#23</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.960</b> |
| #23        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.49      | 60.00            | 1,718.01          | 1.860          | 0.256        |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.66      | 65.00            | 3,926.06          | 3.860          | 0.282        |
| <b>#23</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.538</b> |
| #24        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.71      | 430.00           | 25,118.00         | 1.300          | 5.367        |
| <b>#24</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>5.367</b> |
| #24        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.84      | 430.00           | 23,393.00         | 1.350          | 4.813        |
| <b>#24</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>4.813</b> |
| #24        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.82      | 155.00           | 8,498.00          | 1.350          | 1.748        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.84      | 40.00            | 4,771.00          | 2.740          | 0.483        |
| <b>#24</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.231</b> |
| #24        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 50.00            | 4,042.00          | 1.110          | 1.011        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.49      | 60.00            | 12,150.00         | 2.100          | 1.607        |
| <b>#24</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.618</b> |
| #25        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 0.51      | 10.00            | 1,950.00          | 0.710          | 0.762        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.81      | 60.00            | 3,322.00          | 4.030          | 0.228        |
| <b>#25</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.990</b> |
| #25        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.11      | 25.00            | 2,254.00          | 1.050          | 0.596        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.36      | 75.00            | 3,178.00          | 4.600          | 0.191        |
| <b>#25</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.787</b> |
| #25        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 3.23      | 30.00            | 929.00            | 1.790          | 0.144        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.45      | 154.00           | 6,297.00          | 4.690          | 0.372        |
| <b>#25</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.516</b> |
| #26        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.20      | 103.00           | 8,602.00          | 1.090          | 2.192        |
| <b>#26</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.192</b> |
| #26        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.23      | 120.00           | 9,780.00          | 1.100          | 2.469        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.18      | 184.00           | 8,454.00          | 4.420          | 0.531        |
| <b>#26</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>3.000</b> |
| #27        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.32      | 50.00            | 1,158.02          | 2.070          | 0.155        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.53      | 198.00           | 7,838.16          | 4.760          | 0.457        |
| <b>#27</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.612</b> |
| #27        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.26      | 30.00            | 570.00            | 2.290          | 0.069        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.15      | 278.00           | 8,822.00          | 5.320          | 0.460        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#27</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.529</b> |
| #27        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 16.33     | 80.00            | 490.00            | 4.040          | 0.033        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.15      | 225.00           | 10,443.00         | 4.400          | 0.659        |
| <b>#27</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.692</b> |
| #27        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 12.43     | 65.00            | 523.00            | 3.520          | 0.041        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.49      | 225.00           | 6,454.00          | 5.600          | 0.320        |
| <b>#27</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.361</b> |
| #27        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 9.40      | 25.00            | 266.00            | 3.060          | 0.024        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.32      | 364.00           | 15,700.00         | 4.560          | 0.956        |
| <b>#27</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.980</b> |
| #28        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 5.25      | 40.00            | 762.00            | 2.290          | 0.092        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.96      | 310.00           | 10,479.34         | 5.150          | 0.565        |
| <b>#28</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.657</b> |
| #28        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 25.86     | 105.00           | 406.00            | 5.080          | 0.022        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.96      | 310.00           | 10,479.34         | 5.150          | 0.565        |
| <b>#28</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.587</b> |
| #29        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.58     | 30.00            | 259.00            | 3.400          | 0.021        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.61      | 288.00           | 7,976.00          | 5.700          | 0.388        |
| <b>#29</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.409</b> |
| #29        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 8.06      | 40.00            | 496.00            | 2.830          | 0.048        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.90      | 252.00           | 8,693.55          | 5.100          | 0.473        |
| <b>#29</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.521</b> |
| #29        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 7.25      | 25.00            | 345.00            | 2.690          | 0.035        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.26      | 158.00           | 7,001.00          | 4.500          | 0.432        |
| <b>#29</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.467</b> |
| #30        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.93      | 35.00            | 710.00            | 2.220          | 0.088        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.67      | 243.00           | 14,540.00         | 3.870          | 1.043        |
| <b>#30</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.131</b> |
| #31        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.91      | 15.00            | 515.00            | 1.700          | 0.084        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.74      | 247.00           | 9,006.00          | 4.960          | 0.504        |
| <b>#31</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.588</b> |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #31        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.46      | 25.00            | 335.00            | 2.730          | 0.034        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.18      | 138.00           | 6,335.00          | 4.420          | 0.398        |
| <b>#31</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.432</b> |
| #31        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 3.84      | 20.00            | 521.00            | 1.950          | 0.074        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.24      | 108.00           | 4,826.00          | 4.480          | 0.299        |
| <b>#31</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.373</b> |
| #32        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.48      | 22.00            | 632.00            | 1.860          | 0.094        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.56      | 101.00           | 6,494.00          | 3.740          | 0.482        |
| <b>#32</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.576</b> |
| #34        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.21      | 25.00            | 779.00            | 1.790          | 0.120        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.80      | 63.00            | 2,251.00          | 5.010          | 0.124        |
| <b>#34</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.244</b> |
| #34        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.75      | 40.00            | 696.00            | 2.390          | 0.080        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 23.00     | 2,100.00         | 9,130.43          | 14.380         | 0.176        |
| <b>#34</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.256</b> |
| #34        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.67      | 40.00            | 1,500.00          | 1.630          | 0.255        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.28      | 98.00            | 7,675.00          | 3.380          | 0.630        |
| <b>#34</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.885</b> |
| #36        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.21      | 105.00           | 3,274.00          | 1.790          | 0.508        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.21      | 5.00             | 2,367.00          | 1.370          | 0.479        |
| <b>#36</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.987</b> |
| #36        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.50      | 140.00           | 2,547.00          | 2.340          | 0.302        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.58      | 30.00            | 1,897.00          | 3.770          | 0.139        |
| <b>#36</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.441</b> |
| #36        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.03      | 80.00            | 3,938.62          | 1.420          | 0.770        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.52      | 50.00            | 1,981.86          | 4.760          | 0.115        |
| <b>#36</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.885</b> |
| #37        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.68      | 129.00           | 2,754.05          | 2.160          | 0.354        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.16      | 10.00            | 6,108.73          | 1.210          | 1.402        |
| <b>#37</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.756</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #37        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.32      | 90.00            | 1,229.00          | 2.700          | 0.126        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 70.00            | 4,309.01          | 3.820          | 0.313        |
| <b>#37</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.439</b> |
| #37        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 8.10      | 100.00           | 1,234.00          | 2.840          | 0.120        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.66      | 100.00           | 3,763.21          | 4.890          | 0.213        |
| <b>#37</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.333</b> |
| #37        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 5.09      | 90.00            | 1,768.03          | 2.250          | 0.218        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.36      | 30.00            | 8,326.39          | 1.800          | 1.284        |
| <b>#37</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.502</b> |
| #37        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 0.81      | 20.00            | 2,466.09          | 0.900          | 0.761        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.06      | 50.00            | 1,231.01          | 6.040          | 0.056        |
| <b>#37</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.817</b> |

### ***Subwatershed Muskingum Routing Details:***

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.29      | 107.00           | 8,294.00          | 3.400          | 0.677        |
| <b>#1</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.677</b> |
| #1        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.27      | 113.00           | 8,880.00          | 3.380          | 0.729        |
| <b>#1</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.729</b> |
| #1        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.35      | 171.00           | 12,634.00         | 3.490          | 1.005        |
| <b>#1</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.005</b> |
| #1        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.49      | 274.00           | 18,349.00         | 3.660          | 1.392        |
| <b>#1</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.392</b> |
| #1        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.49      | 274.00           | 18,349.00         | 3.660          | 1.392        |
| <b>#1</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.392</b> |
| #2        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.53      | 20.00            | 3,756.00          | 2.180          | 0.478        |
| <b>#2</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.478</b> |
| #2        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.55      | 25.00            | 4,570.00          | 2.210          | 0.574        |
| <b>#2</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.574</b> |
| #2        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.55      | 25.00            | 4,570.00          | 2.210          | 0.574        |
| <b>#2</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.574</b> |



| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #2        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.65      | 45.00            | 6,955.00          | 2.410          | 0.801        |
| <b>#2</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.801</b> |
| #3        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.92      | 20.00            | 2,168.00          | 2.880          | 0.209        |
| <b>#3</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.209</b> |
| #5        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#5</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #5        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.75      | 125.00           | 7,149.00          | 3.960          | 0.501        |
| <b>#5</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.501</b> |
| #5        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.65      | 155.00           | 9,418.00          | 3.840          | 0.681        |
| <b>#5</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #5        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.65      | 155.00           | 9,418.00          | 3.840          | 0.681        |
| <b>#5</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #5        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.67      | 239.00           | 14,273.00         | 3.880          | 1.021        |
| <b>#5</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.021</b> |
| #5        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.68      | 239.00           | 14,223.00         | 3.880          | 1.018        |
| <b>#5</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.018</b> |
| #6        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.16      | 26.00            | 2,241.00          | 3.230          | 0.192        |
| <b>#6</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.192</b> |
| #6        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.00      | 50.00            | 4,987.00          | 3.000          | 0.461        |
| <b>#6</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.461</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.00      | 50.00            | 4,987.00          | 1.000          | 1.385        |
| <b>#6</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.385</b> |
| #6        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.02      | 89.00            | 8,685.00          | 3.030          | 0.796        |
| <b>#6</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.796</b> |
| #6        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.06      | 126.00           | 11,860.00         | 3.090          | 1.066        |
| <b>#6</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.066</b> |
| #6        | 7        | 8. Large gullies, diversions, and low flowing streams | 1.06      | 126.00           | 11,860.00         | 3.090          | 1.066        |
| <b>#6</b> | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.066</b> |
| #7        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.16      | 140.00           | 12,037.00         | 3.230          | 1.035        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#7</b>  | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.035</b> |
| #7         | 5        | 8. Large gullies, diversions, and low flowing streams | 1.14      | 140.00           | 12,307.69         | 3.190          | 1.071        |
| <b>#7</b>  | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.071</b> |
| #7         | 6        | 8. Large gullies, diversions, and low flowing streams | 1.17      | 158.00           | 13,546.00         | 3.230          | 1.164        |
| <b>#7</b>  | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.164</b> |
| #7         | 7        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 187.00           | 15,784.00         | 3.260          | 1.344        |
| <b>#7</b>  | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.344</b> |
| #7         | 8        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 187.00           | 15,784.00         | 3.260          | 1.344        |
| <b>#7</b>  | <b>8</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.344</b> |
| #10        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.76      | 37.00            | 4,861.00          | 2.610          | 0.517        |
| <b>#10</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.517</b> |
| #10        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.76      | 37.00            | 4,861.00          | 2.610          | 0.517        |
| <b>#10</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.517</b> |
| #10        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.79      | 47.00            | 5,956.00          | 2.660          | 0.621        |
| <b>#10</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.621</b> |
| #12        | 2        | 8. Large gullies, diversions, and low flowing streams | 8.24      | 111.00           | 1,347.00          | 8.610          | 0.043        |
| <b>#12</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.043</b> |
| #12        | 3        | 8. Large gullies, diversions, and low flowing streams | 8.01      | 109.00           | 1,360.00          | 8.490          | 0.044        |
| <b>#12</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.044</b> |
| #12        | 4        | 8. Large gullies, diversions, and low flowing streams | 2.24      | 176.00           | 7,866.00          | 4.480          | 0.487        |
| <b>#12</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.487</b> |
| #12        | 5        | 8. Large gullies, diversions, and low flowing streams | 2.24      | 176.00           | 7,866.00          | 4.480          | 0.487        |
| <b>#12</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.487</b> |
| #13        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.34      | 54.00            | 4,025.00          | 3.470          | 0.322        |
| <b>#13</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.322</b> |
| #13        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.98      | 72.00            | 7,333.00          | 2.970          | 0.685        |
| <b>#13</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.685</b> |
| #13        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 127.00           | 10,806.00         | 3.250          | 0.923        |
| <b>#13</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.923</b> |
| #13        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 127.00           | 10,806.00         | 3.250          | 0.923        |
| <b>#13</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.923</b> |
| #14        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#14</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |



| Stru #     | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #14        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.83      | 58.00            | 6,957.00          | 2.730          | 0.707        |
| <b>#14</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.707</b> |
| #14        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.81      | 77.00            | 9,480.00          | 2.700          | 0.975        |
| <b>#14</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.975</b> |
| #14        | 4         | 8. Large gullies, diversions, and low flowing streams | 0.86      | 147.00           | 17,117.00         | 2.770          | 1.716        |
| <b>#14</b> | <b>4</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.716</b> |
| #14        | 5         | 8. Large gullies, diversions, and low flowing streams | 0.88      | 175.00           | 19,934.00         | 2.810          | 1.970        |
| <b>#14</b> | <b>5</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.970</b> |
| #14        | 6         | 8. Large gullies, diversions, and low flowing streams | 0.95      | 211.00           | 22,155.00         | 2.920          | 2.107        |
| <b>#14</b> | <b>6</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.107</b> |
| #14        | 7         | 8. Large gullies, diversions, and low flowing streams | 0.96      | 257.00           | 26,835.00         | 2.930          | 2.544        |
| <b>#14</b> | <b>7</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.544</b> |
| #14        | 8         | 8. Large gullies, diversions, and low flowing streams | 0.96      | 257.00           | 26,835.00         | 2.930          | 2.544        |
| <b>#14</b> | <b>8</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.544</b> |
| #14        | 9         | 8. Large gullies, diversions, and low flowing streams | 0.95      | 307.00           | 32,146.59         | 2.930          | 3.047        |
| <b>#14</b> | <b>9</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.047</b> |
| #14        | 10        | 8. Large gullies, diversions, and low flowing streams | 0.96      | 339.00           | 35,382.00         | 2.930          | 3.354        |
| <b>#14</b> | <b>10</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.354</b> |
| #15        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#15</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #15        | 2         | 8. Large gullies, diversions, and low flowing streams | 1.14      | 86.00            | 7,535.00          | 3.200          | 0.654        |
| <b>#15</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.654</b> |
| #15        | 3         | 8. Large gullies, diversions, and low flowing streams | 1.25      | 115.00           | 9,236.00          | 3.340          | 0.768        |
| <b>#15</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.768</b> |
| #16        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.58      | 24.00            | 4,161.00          | 2.270          | 0.509        |
| <b>#16</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.509</b> |
| #16        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.51      | 37.00            | 7,269.00          | 2.140          | 0.943        |
| <b>#16</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.943</b> |
| #17        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#17</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #18        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#18</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #18        | 2         | 8. Large gullies, diversions, and low flowing streams | 1.02      | 62.00            | 6,103.00          | 3.020          | 0.561        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#18</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.561</b> |
| #20        | 2        | 8. Large gullies, diversions, and low flowing streams | 17.00     | 3,605.00         | 21,205.88         | 12.360         | 0.476        |
| <b>#20</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.476</b> |
| #21        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#21</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #21        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.41      | 20.00            | 4,824.00          | 1.930          | 0.694        |
| <b>#21</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.694</b> |
| #21        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 20.00            | 5,626.00          | 1.780          | 0.877        |
| <b>#21</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.877</b> |
| #21        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 20.00            | 5,626.00          | 1.780          | 0.877        |
| <b>#21</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.877</b> |
| #23        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#23</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #23        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.63      | 30.00            | 4,771.75          | 2.370          | 0.559        |
| <b>#23</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.559</b> |
| #24        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.79      | 180.00           | 22,769.00         | 2.660          | 2.377        |
| <b>#24</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.377</b> |
| #24        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.78      | 180.00           | 23,111.00         | 2.640          | 2.431        |
| <b>#24</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.431</b> |
| #24        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#24</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #25        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.99      | 104.00           | 5,220.00          | 4.230          | 0.342        |
| <b>#25</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.342</b> |
| #25        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.99      | 104.00           | 5,220.00          | 4.230          | 0.342        |
| <b>#25</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.342</b> |
| #25        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#25</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #27        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.38      | 216.00           | 15,629.00         | 3.520          | 1.233        |
| <b>#27</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.233</b> |
| #27        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.17      | 144.00           | 12,301.00         | 3.240          | 1.054        |
| <b>#27</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.054</b> |
| #27        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 76.00            | 6,454.00          | 3.250          | 0.551        |
| <b>#27</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.551</b> |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #27        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 76.00            | 6,454.00          | 3.250          | 0.551        |
| <b>#27</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.551</b> |
| #28        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.30      | 84.00            | 6,445.17          | 3.420          | 0.523        |
| <b>#28</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.523</b> |
| #29        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.88      | 37.00            | 4,210.00          | 2.810          | 0.416        |
| <b>#29</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.416</b> |
| #29        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.88      | 26.00            | 2,949.00          | 2.810          | 0.291        |
| <b>#29</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.291</b> |
| #31        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.35      | 76.00            | 5,639.00          | 3.480          | 0.450        |
| <b>#31</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.450</b> |
| #31        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.15      | 20.00            | 1,734.00          | 3.220          | 0.149        |
| <b>#31</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.149</b> |
| #34        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.73      | 65.00            | 8,900.00          | 2.560          | 0.965        |
| <b>#34</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.965</b> |
| #34        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.73      | 65.00            | 8,900.00          | 2.560          | 0.965        |
| <b>#34</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.965</b> |
| #36        | 3        | 8. Large gullies, diversions, and low flowing streams | 2.71      | 80.00            | 2,957.00          | 4.930          | 0.166        |
| <b>#36</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.166</b> |
| #37        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.29      | 30.00            | 10,319.91         | 1.610          | 1.780        |
| <b>#37</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.780</b> |
| #37        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.31      | 30.00            | 9,800.71          | 1.650          | 1.649        |
| <b>#37</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.649</b> |
| #37        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.29      | 30.00            | 10,319.91         | 1.610          | 1.780        |
| <b>#37</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.780</b> |
| #37        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.56      | 100.00           | 17,956.54         | 2.230          | 2.236        |
| <b>#37</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.236</b> |

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# **Cottonwood Arroyo Pre-mine Hydrology and Sedimentology**

***The drainage subdivisions used to model the hydrology is shown  
on Exhibit 18.B***

***Revised Febuary 2012***

Art O'Hayre



***General Information***

***Storm Information:***

|                 |              |
|-----------------|--------------|
| Storm Type:     | Type II-70   |
| Design Storm:   | 2 yr - 6 hr  |
| Rainfall Depth: | 0.850 inches |

***Particle Size Distribution:***

| Size (mm) | PostMine-LoamySand | PreMine-LoamySand | PreMine-Badlands | LoamySand Postmining |
|-----------|--------------------|-------------------|------------------|----------------------|
| 2.0000    | 100.000%           | 100.000%          | 100.000%         | 0.000%               |
| 0.1000    | 26.500%            | 30.000%           | 83.500%          | 0.000%               |
| 0.0500    | 14.000%            | 17.000%           | 77.000%          | 0.000%               |
| 0.0020    | 11.000%            | 11.000%           | 56.000%          | 0.000%               |
| 0.0010    | 0.000%             | 0.000%            | 0.000%           | 0.000%               |

### *Structure Summary:*

|     | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|-----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #30 | 476.400                                   | 476.400                               | 0.42                       | 0.11                                 | 0.4                | 2,965                               | 1.82                                  | 1.55           |
| #28 | 1,217.900                                 | 1,217.900                             | 168.77                     | 19.36                                | 939.7              | 51,228                              | 0.00                                  | 0.00           |
| #26 | 2,486.400                                 | 2,486.400                             | 8.59                       | 2.86                                 | 13.1               | 4,375                               | 0.55                                  | 0.42           |
| #24 | 8,061.800                                 | 8,061.800                             | 11.17                      | 6.64                                 | 17.5               | 2,885                               | 0.18                                  | 0.12           |
| #25 | 1,015.700                                 | 9,077.500                             | 43.84                      | 10.83                                | 64.9               | 15,537                              | 6.38                                  | 1.81           |
| #27 | 1,783.700                                 | 13,347.600                            | 76.77                      | 20.93                                | 211.6              | 23,433                              | 10.13                                 | 3.20           |
| #29 | 966.000                                   | 15,531.500                            | 221.98                     | 55.19                                | 2,116.8            | 64,602                              | 2.94                                  | 1.26           |
| #32 | 293.700                                   | 16,301.600                            | 225.12                     | 61.87                                | 2,217.3            | 56,165                              | 0.00                                  | 0.00           |
| #31 | 957.100                                   | 957.100                               | 186.43                     | 19.66                                | 773.0              | 37,599                              | 0.40                                  | 0.30           |
| #33 | 0.000                                     | 17,258.700                            | 306.26                     | 81.53                                | 2,990.3            | 46,265                              | 0.13                                  | 0.07           |
| #34 | 932.500                                   | 18,191.200                            | 312.79                     | 95.29                                | 2,757.0            | 37,581                              | 0.05                                  | 0.03           |
| #5  | 2,023.000                                 | 2,023.000                             | 229.14                     | 23.65                                | 597.2              | 35,964                              | 1.23                                  | 0.63           |
| #6  | 1,743.200                                 | 3,766.200                             | 265.00                     | 46.82                                | 1,150.6            | 31,888                              | 0.18                                  | 0.10           |
| #7  | 2,395.300                                 | 6,161.500                             | 489.93                     | 97.92                                | 3,549.5            | 40,575                              | 0.00                                  | 0.00           |
| #8  | 0.000                                     | 6,161.500                             | 489.93                     | 97.92                                | 3,549.5            | 40,575                              | 0.00                                  | 0.00           |
| #10 | 1,053.200                                 | 7,214.700                             | 502.27                     | 115.36                               | 3,451.8            | 36,547                              | 0.05                                  | 0.03           |
| #1  | 2,411.100                                 | 2,411.100                             | 145.59                     | 19.69                                | 601.9              | 34,411                              | 2.97                                  | 1.92           |
| #2  | 1,497.000                                 | 3,908.100                             | 219.24                     | 47.99                                | 977.7              | 22,730                              | 0.13                                  | 0.09           |
| #3  | 862.700                                   | 4,770.800                             | 274.62                     | 60.13                                | 1,092.3            | 18,273                              | 0.04                                  | 0.03           |
| #4  | 0.000                                     | 4,770.800                             | 274.62                     | 60.13                                | 1,092.3            | 18,273                              | 0.04                                  | 0.03           |
| #9  | 425.500                                   | 5,196.300                             | 278.73                     | 67.17                                | 1,092.8            | 15,772                              | 0.00                                  | 0.00           |
| #11 | 0.000                                     | 12,411.000                            | 706.54                     | 182.52                               | 4,544.5            | 30,480                              | 0.02                                  | 0.01           |
| #21 | 1,080.800                                 | 13,491.800                            | 728.86                     | 194.95                               | 4,561.0            | 29,762                              | 0.00                                  | 0.00           |
| #18 | 848.500                                   | 848.500                               | 87.84                      | 11.61                                | 118.2              | 12,305                              | 0.00                                  | 0.00           |
| #17 | 182.200                                   | 182.200                               | 65.14                      | 4.08                                 | 55.0               | 14,274                              | 0.37                                  | 0.26           |
| #19 | 0.000                                     | 1,030.700                             | 148.60                     | 15.69                                | 173.2              | 11,407                              | 0.09                                  | 0.07           |
| #15 | 1,992.700                                 | 1,992.700                             | 180.77                     | 24.60                                | 857.0              | 40,282                              | 0.20                                  | 0.12           |
| #12 | 3,494.500                                 | 3,494.500                             | 54.37                      | 8.31                                 | 106.0              | 14,291                              | 5.52                                  | 3.61           |
| #13 | 2,720.700                                 | 6,215.200                             | 99.03                      | 15.37                                | 232.3              | 16,747                              | 7.21                                  | 4.76           |
| #14 | 5,096.800                                 | 11,312.000                            | 214.75                     | 67.68                                | 1,686.3            | 69,407                              | 0.58                                  | 0.15           |
| #16 | 876.500                                   | 14,181.200                            | 384.91                     | 111.41                               | 3,202.2            | 48,003                              | 0.53                                  | 0.23           |
| #20 | 681.900                                   | 15,893.800                            | 399.88                     | 141.32                               | 3,473.7            | 36,837                              | 0.00                                  | 0.00           |
| #22 | 0.000                                     | 29,385.600                            | 1,034.13                   | 336.26                               | 8,034.7            | 30,529                              | 0.00                                  | 0.00           |
| #23 | 752.900                                   | 30,138.500                            | 1,025.65                   | 343.99                               | 7,929.8            | 29,707                              | 0.00                                  | 0.00           |
| #35 | 0.000                                     | 48,329.700                            | 1,260.70                   | 439.29                               | 10,686.8           | 27,942                              | 0.01                                  | 0.01           |
| #36 | 730.590                                   | 49,060.290                            | 1,258.12                   | 444.11                               | 10,716.3           | 34,997                              | 0.00                                  | 0.00           |
| #37 | 2,208.500                                 | 51,268.790                            | 1,249.70                   | 459.47                               | 10,744.2           | 29,250                              | 0.14                                  | 0.08           |



## ***Particle Size Distribution(s) at Each Structure***

### ***Structure #30:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 48.542%  |
| 0.0500    | 27.507%  |
| 0.0020    | 17.799%  |
| 0.0010    | 0.000%   |

### ***Structure #28:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

### ***Structure #26:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 98.959%  |
| 0.0020    | 67.283%  |
| 0.0010    | 0.000%   |

### ***Structure #24:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 82.732%  |
| 0.0010    | 0.000%   |

**Structure #25:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 75.475%  |
| 0.0500    | 54.531%  |
| 0.0020    | 41.368%  |
| 0.0010    | 0.000%   |

**Structure #27:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 83.117%  |
| 0.0500    | 53.429%  |
| 0.0020    | 36.645%  |
| 0.0010    | 0.000%   |

**Structure #29:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 98.330%  |
| 0.0500    | 95.362%  |
| 0.0020    | 92.997%  |
| 0.0010    | 0.000%   |

**Structure #32:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #31:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 96.996%  |
| 0.0010    | 0.000%   |



**Structure #33 (Inlet to North Fork Diversion):**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.224%  |
| 0.0010    | 0.000%   |

**Structure #34:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.610%  |
| 0.0010    | 0.000%   |

**Structure #5:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 97.321%  |
| 0.0020    | 93.713%  |
| 0.0010    | 0.000%   |

**Structure #6:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.412%  |
| 0.0010    | 0.000%   |

**Structure #7:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #8:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #10:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.871%  |
| 0.0020    | 99.779%  |
| 0.0010    | 0.000%   |

**Structure #1:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 98.279%  |
| 0.0500    | 91.147%  |
| 0.0020    | 86.784%  |
| 0.0010    | 0.000%   |

**Structure #2:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.374%  |
| 0.0010    | 0.000%   |

**Structure #3:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.425%  |
| 0.0010    | 0.000%   |



**Structure #4:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.425%  |
| 0.0010    | 0.000%   |

**Structure #9:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #11:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.832%  |
| 0.0010    | 0.000%   |

**Structure #21:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #18:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #17:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 92.667%  |
| 0.0010    | 0.000%   |

**Structure #19:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 97.672%  |
| 0.0010    | 0.000%   |

**Structure #15:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.619%  |
| 0.0010    | 0.000%   |

**Structure #12:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 91.000%  |
| 0.0500    | 61.522%  |
| 0.0020    | 39.808%  |
| 0.0010    | 0.000%   |

**Structure #13:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 88.147%  |
| 0.0500    | 54.905%  |
| 0.0020    | 35.527%  |
| 0.0010    | 0.000%   |



**Structure #14:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 97.648%  |
| 0.0010    | 0.000%   |

**Structure #16:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 96.875%  |
| 0.0010    | 0.000%   |

**Structure #20:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #22:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #23:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #35:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.899%  |
| 0.0010    | 0.000%   |

**Structure #36:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #37:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.526%  |
| 0.0020    | 99.244%  |
| 0.0010    | 0.000%   |



### *Subwatershed Hydrology Detail:*

| Stru #     | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|------------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #30        | 1        | 476.400           | 1.131              | 0.000        | 0.000  | 73.100       | M   | 0.42                 | 0.108                 |
|            | <b>Σ</b> | <b>476.400</b>    |                    |              |        |              |     | <b>0.42</b>          | <b>0.108</b>          |
| #28        | 1        | 772.300           | 0.657              | 0.523        | 0.334  | 90.400       | M   | 154.33               | 12.273                |
|            | 2        | 445.600           | 0.587              | 0.000        | 0.000  | 90.400       | M   | 96.41                | 7.084                 |
|            | <b>Σ</b> | <b>1,217.900</b>  |                    |              |        |              |     | <b>168.77</b>        | <b>19.357</b>         |
| #26        | 1        | 447.600           | 2.192              | 0.000        | 0.000  | 74.200       | M   | 0.63                 | 0.195                 |
|            | 2        | 2,038.800         | 3.000              | 0.000        | 0.000  | 77.000       | M   | 7.95                 | 2.663                 |
|            | <b>Σ</b> | <b>2,486.400</b>  |                    |              |        |              |     | <b>8.59</b>          | <b>2.858</b>          |
| #24        | 1        | 2,607.500         | 5.367              | 2.377        | 0.305  | 75.200       | M   | 3.53                 | 1.798                 |
|            | 2        | 2,331.900         | 4.813              | 2.431        | 0.304  | 74.700       | M   | 2.75                 | 1.295                 |
|            | 3        | 1,758.500         | 2.231              | 1.788        | 0.297  | 76.200       | M   | 6.20                 | 1.768                 |
|            | 4        | 1,363.900         | 2.618              | 0.000        | 0.000  | 77.000       | M   | 5.82                 | 1.781                 |
|            | <b>Σ</b> | <b>8,061.800</b>  |                    |              |        |              |     | <b>11.17</b>         | <b>6.642</b>          |
| #25        | 1        | 515.200           | 0.990              | 0.342        | 0.357  | 78.200       | M   | 6.68                 | 0.949                 |
|            | 2        | 130.500           | 0.787              | 0.342        | 0.357  | 78.100       | M   | 1.94                 | 0.234                 |
|            | 3        | 370.000           | 0.516              | 0.000        | 0.000  | 85.700       | M   | 43.63                | 3.000                 |
|            | <b>Σ</b> | <b>9,077.500</b>  |                    |              |        |              |     | <b>43.84</b>         | <b>10.825</b>         |
| #27        | 1        | 354.400           | 0.612              | 1.233        | 0.337  | 83.100       | M   | 22.90                | 1.867                 |
|            | 2        | 305.200           | 0.529              | 1.054        | 0.328  | 84.000       | M   | 26.16                | 1.879                 |
|            | 3        | 289.800           | 0.692              | 0.551        | 0.328  | 75.500       | M   | 1.46                 | 0.226                 |
|            | 4        | 253.000           | 0.361              | 0.551        | 0.328  | 79.400       | M   | 10.21                | 0.631                 |
|            | 5        | 581.300           | 0.980              | 0.000        | 0.000  | 82.300       | M   | 22.25                | 2.645                 |
|            | <b>Σ</b> | <b>13,347.600</b> |                    |              |        |              |     | <b>76.77</b>         | <b>20.932</b>         |
| #29        | 1        | 508.800           | 0.409              | 0.416        | 0.312  | 89.500       | M   | 123.40               | 7.174                 |
|            | 2        | 233.200           | 0.521              | 0.291        | 0.312  | 91.600       | M   | 64.31                | 4.349                 |
|            | 3        | 224.000           | 0.467              | 0.000        | 0.000  | 90.000       | M   | 53.48                | 3.373                 |
|            | <b>Σ</b> | <b>15,531.500</b> |                    |              |        |              |     | <b>221.98</b>        | <b>55.186</b>         |
| #32        | 1        | 293.700           | 0.576              | 0.000        | 0.000  | 93.000       | M   | 91.29                | 6.575                 |
|            | <b>Σ</b> | <b>16,301.600</b> |                    |              |        |              |     | <b>225.12</b>        | <b>61.868</b>         |
| #31        | 1        | 431.100           | 0.588              | 0.450        | 0.336  | 91.500       | M   | 108.09               | 7.934                 |
|            | 2        | 325.800           | 0.432              | 0.149        | 0.327  | 93.000       | M   | 121.15               | 7.302                 |
|            | 3        | 200.200           | 0.373              | 0.000        | 0.000  | 92.900       | M   | 79.56                | 4.422                 |
|            | <b>Σ</b> | <b>957.100</b>    |                    |              |        |              |     | <b>186.43</b>        | <b>19.658</b>         |
| <b>#33</b> | <b>Σ</b> | <b>17,258.700</b> |                    |              |        |              |     | <b>306.26</b>        | <b>81.526</b>         |

| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS  | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|------|----------------------|-----------------------|
| #34    | 1        | 91.700            | 0.244              | 0.965        | 0.300  | 92.300       | M    | 40.53                | 1.889                 |
|        | 2        | 105.200           | 0.256              | 0.965        | 0.300  | 93.000       | M    | 49.60                | 2.367                 |
|        | 3        | 735.600           | 0.885              | 0.000        | 0.000  | 88.900       | M    | 95.10                | 9.513                 |
|        | <b>Σ</b> | <b>18,191.200</b> |                    |              |        |              |      | <b>312.79</b>        | <b>95.295</b>         |
| #5     | 1        | 503.600           | 0.618              | 0.000        | 0.000  | 87.600       | M    | 70.38                | 5.418                 |
|        | 2        | 406.500           | 0.388              | 0.501        | 0.350  | 84.800       | M    | 50.23                | 2.856                 |
|        | 3        | 439.600           | 0.342              | 0.681        | 0.347  | 87.800       | M    | 93.95                | 4.893                 |
|        | 4        | 162.600           | 0.280              | 0.681        | 0.347  | 86.000       | M    | 29.90                | 1.385                 |
|        | 5        | 294.100           | 0.375              | 1.021        | 0.348  | 92.000       | M    | 104.07               | 5.773                 |
|        | 6        | 216.600           | 0.272              | 1.018        | 0.348  | 90.100       | M    | 70.08                | 3.321                 |
|        | <b>Σ</b> | <b>2,023.000</b>  |                    |              |        |              |      | <b>229.14</b>        | <b>23.646</b>         |
| #6     | 1        | 149.100           | 0.331              | 0.000        | 0.000  | 92.600       | M    | 60.49                | 3.180                 |
|        | 2        | 245.000           | 0.529              | 0.192        | 0.328  | 88.100       | M    | 41.26                | 2.835                 |
|        | 3        | 276.200           | 0.450              | 0.461        | 0.319  | 89.500       | M    | 63.13                | 3.884                 |
|        | 4        | 158.400           | 0.380              | 1.385        | 0.185  | 93.000       | M    | 63.13                | 3.542                 |
|        | 5        | 206.200           | 0.402              | 0.796        | 0.320  | 89.400       | M    | 49.86                | 2.867                 |
|        | 6        | 414.000           | 0.430              | 1.066        | 0.323  | 87.200       | M    | 70.28                | 4.213                 |
|        | 7        | 294.300           | 0.535              | 1.066        | 0.323  | 86.400       | M    | 37.89                | 2.654                 |
|        | <b>Σ</b> | <b>3,766.200</b>  |                    |              |        |              |      | <b>265.00</b>        | <b>46.822</b>         |
| #7     | 1        | 731.700           | 1.274              | 0.000        | 0.000  | 93.000       | M    | 125.32               | 16.354                |
|        | 2        | 445.800           | 1.043              | 0.000        | 0.000  | 93.000       | M    | 89.59                | 9.961                 |
|        | 3        | 270.800           | 0.804              | 0.000        | 0.000  | 93.000       | M    | 66.41                | 6.053                 |
|        | 4        | 78.900            | 0.267              | 1.035        | 0.328  | 93.000       | M    | 36.64                | 1.774                 |
|        | 5        | 154.900           | 0.310              | 1.071        | 0.326  | 93.000       | M    | 67.89                | 3.478                 |
|        | 6        | 101.400           | 0.288              | 1.164        | 0.328  | 92.900       | M    | 45.26                | 2.246                 |
|        | 7        | 117.700           | 0.298              | 1.344        | 0.329  | 92.200       | M    | 47.63                | 2.379                 |
|        | 8        | 494.100           | 0.518              | 1.344        | 0.329  | 91.300       | M    | 131.34               | 8.857                 |
|        | <b>Σ</b> | <b>6,161.500</b>  |                    |              |        |              |      | <b>489.93</b>        | <b>97.922</b>         |
| #8     | 1        | 0.000             | 0.000              | 0.000        | 0.000  | 1.000        | 0.00 | 0.000                |                       |
|        | <b>Σ</b> | <b>6,161.500</b>  |                    |              |        |              |      | <b>489.93</b>        | <b>97.922</b>         |
| #10    | 1        | 355.500           | 1.286              | 0.000        | 0.000  | 93.000       | M    | 60.42                | 7.944                 |
|        | 2        | 307.100           | 1.282              | 0.668        | 0.305  | 83.200       | M    | 11.38                | 1.645                 |
|        | 3        | 147.300           | 1.245              | 0.517        | 0.303  | 90.600       | M    | 18.52                | 2.401                 |
|        | 4        | 126.400           | 0.585              | 0.517        | 0.303  | 93.000       | M    | 38.88                | 2.830                 |
|        | 5        | 116.900           | 1.179              | 0.621        | 0.305  | 93.000       | M    | 21.32                | 2.613                 |
|        | <b>Σ</b> | <b>7,214.700</b>  |                    |              |        |              |      | <b>502.27</b>        | <b>115.355</b>        |
| #1     | 1        | 557.400           | 0.941              | 0.000        | 0.000  | 83.600       | M    | 28.55                | 3.202                 |
|        | 2        | 169.600           | 1.616              | 0.677        | 0.333  | 93.000       | M    | 23.89                | 3.790                 |
|        | 3        | 636.400           | 1.842              | 0.729        | 0.333  | 81.000       | M    | 11.02                | 2.246                 |
|        | 4        | 223.400           | 0.846              | 1.005        | 0.336  | 84.100       | M    | 13.64                | 1.398                 |



| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS   | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|-------|----------------------|-----------------------|
|        | 5        | 77.700            | 0.330              | 1.392        | 0.341  | 81.400       | M     | 5.49                 | 0.299                 |
|        | 6        | 746.600           | 0.678              | 1.392        | 0.341  | 88.200       | M     | 106.62               | 8.758                 |
|        | <b>Σ</b> | <b>2,411.100</b>  |                    |              |        |              |       | <b>145.59</b>        | <b>19.692</b>         |
| #2     | 1        | 257.000           | 0.423              | 0.000        | 0.000  | 93.000       | M     | 96.72                | 5.764                 |
|        | 2        | 180.500           | 0.562              | 0.478        | 0.281  | 91.800       | M     | 48.62                | 3.452                 |
|        | 3        | 200.700           | 0.687              | 0.574        | 0.283  | 93.000       | M     | 55.21                | 4.488                 |
|        | 4        | 438.600           | 0.811              | 0.574        | 0.283  | 93.000       | M     | 106.86               | 9.806                 |
|        | 5        | 420.200           | 1.247              | 0.801        | 0.293  | 88.000       | M     | 36.13                | 4.787                 |
|        | <b>Σ</b> | <b>3,908.100</b>  |                    |              |        |              |       | <b>219.24</b>        | <b>47.989</b>         |
| #3     | 1        | 172.600           | 0.443              | 0.000        | 0.000  | 93.000       | M     | 63.26                | 3.862                 |
|        | 2        | 311.200           | 0.890              | 0.000        | 0.000  | 88.900       | M     | 40.06                | 4.025                 |
|        | 3        | 378.900           | 0.632              | 0.209        | 0.314  | 87.900       | M     | 54.50                | 4.256                 |
|        | <b>Σ</b> | <b>4,770.800</b>  |                    |              |        |              |       | <b>274.62</b>        | <b>60.132</b>         |
| #4     | <b>Σ</b> | <b>4,770.800</b>  |                    |              |        |              |       | <b>274.62</b>        | <b>60.132</b>         |
| #9     | 1        | 425.500           | 0.830              | 0.000        | 0.000  | 90.700       | M     | 74.57                | 7.035                 |
|        | <b>Σ</b> | <b>5,196.300</b>  |                    |              |        |              |       | <b>278.73</b>        | <b>67.167</b>         |
| #11    | <b>Σ</b> | <b>12,411.000</b> |                    |              |        |              |       | <b>706.54</b>        | <b>182.522</b>        |
| #21    | 1        | 272.800           | 0.819              | 0.000        | 0.000  | 86.900       | M     | 27.62                | 2.650                 |
|        | 2        | 230.500           | 0.388              | 0.694        | 0.266  | 89.200       | M     | 55.42                | 3.111                 |
|        | 3        | 181.100           | 0.289              | 0.877        | 0.256  | 91.300       | M     | 66.39                | 3.252                 |
|        | 4        | 396.400           | 0.939              | 0.877        | 0.256  | 86.100       | M     | 31.67                | 3.413                 |
|        | <b>Σ</b> | <b>13,491.800</b> |                    |              |        |              |       | <b>728.86</b>        | <b>194.947</b>        |
| #18    | 1        | 301.700           | 0.652              | 0.000        | 0.000  | 93.000       | M     | 86.12                | 6.753                 |
|        | 2        | 546.800           | 0.768              | 0.561        | 0.320  | 86.300       | M     | 52.82                | 4.856                 |
|        | <b>Σ</b> | <b>848.500</b>    |                    |              |        |              |       | <b>87.84</b>         | <b>11.608</b>         |
| #17    | 1        | 182.200           | 0.462              | 0.000        | 0.000  | 93.000       | M     | 65.14                | 4.077                 |
|        | <b>Σ</b> | <b>182.200</b>    |                    |              |        |              |       | <b>65.14</b>         | <b>4.077</b>          |
| #19    | <b>Σ</b> | <b>1,030.700</b>  |                    |              |        |              |       | <b>148.60</b>        | <b>15.685</b>         |
| #15    | 1        | 437.400           | 0.803              | 0.000        | 0.000  | 91.300       | M     | 85.27                | 7.826                 |
|        | 2        | 549.000           | 0.637              | 0.654        | 0.327  | 91.300       | M     | 126.59               | 9.828                 |
|        | 3        | 1,006.300         | 1.023              | 0.768        | 0.331  | 84.700       | M     | 59.01                | 6.949                 |
|        | <b>Σ</b> | <b>1,992.700</b>  |                    |              |        |              |       | <b>180.77</b>        | <b>24.603</b>         |
| #12    | 1        | 517.800           | 0.791              | 0.000        | 0.000  | 81.900       | M     | 21.49                | 2.184                 |
|        | 2        | 229.000           | 0.571              | 0.043        | 0.418  | 80.100       | M     | 7.95                 | 0.669                 |
|        | 3        | 592.700           | 0.706              | 0.044        | 0.417  | 81.500       | M     | 24.57                | 2.314                 |
|        | 4        | 1,806.900         | 1.542              | 0.487        | 0.362  | 76.700       | M     | 9.77                 | 2.147                 |
|        | 5        | 348.100           | 0.618              | 0.487        | 0.362  | 80.000       | 11.07 | 0.993                |                       |

| Stru #   | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|----------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| <b>Σ</b> |          | <b>3,494.500</b>  |                    |              |        |              |     | <b>54.37</b>         | <b>8.307</b>          |
| #13      | 1        | 411.600           | 0.725              | 0.000        | 0.000  | 79.700       | M   | 10.68                | 1.098                 |
|          | 2        | 636.400           | 0.774              | 0.322        | 0.336  | 80.700       | M   | 20.37                | 2.112                 |
|          | 3        | 319.000           | 0.575              | 0.685        | 0.318  | 85.500       | M   | 33.59                | 2.506                 |
|          | 4        | 231.700           | 0.314              | 0.923        | 0.328  | 80.400       | M   | 13.44                | 0.724                 |
|          | 5        | 1,122.000         | 1.308              | 0.923        | 0.328  | 74.700       | M   | 2.63                 | 0.623                 |
| <b>Σ</b> |          | <b>6,215.200</b>  |                    |              |        |              |     | <b>99.03</b>         | <b>15.370</b>         |
| #14      | 1        | 405.900           | 0.384              | 0.000        | 0.000  | 90.800       | M   | 121.19               | 6.801                 |
|          | 2        | 411.100           | 0.452              | 0.707        | 0.308  | 90.700       | M   | 109.89               | 6.798                 |
|          | 3        | 787.400           | 0.658              | 0.975        | 0.307  | 91.400       | M   | 179.88               | 14.295                |
|          | 4        | 144.200           | 0.341              | 1.716        | 0.310  | 86.200       | M   | 24.38                | 1.267                 |
|          | 5        | 343.800           | 0.289              | 1.970        | 0.312  | 86.500       | M   | 66.96                | 3.155                 |
|          | 6        | 392.800           | 0.806              | 2.107        | 0.316  | 81.900       | M   | 16.07                | 1.657                 |
|          | 7        | 528.200           | 0.518              | 2.544        | 0.316  | 87.200       | M   | 78.91                | 5.369                 |
|          | 8        | 890.900           | 1.253              | 2.544        | 0.316  | 83.500       | M   | 35.63                | 5.030                 |
|          | 9        | 741.400           | 1.076              | 3.047        | 0.316  | 84.800       | M   | 42.51                | 5.204                 |
|          | 10       | 451.100           | 0.916              | 3.354        | 0.316  | 83.900       | M   | 24.97                | 2.728                 |
| <b>Σ</b> |          | <b>11,312.000</b> |                    |              |        |              |     | <b>214.75</b>        | <b>67.675</b>         |
| #16      | 1        | 329.600           | 0.641              | 0.000        | 0.000  | 93.000       | M   | 95.21                | 7.374                 |
|          | 2        | 348.400           | 0.542              | 0.509        | 0.286  | 92.500       | M   | 105.55               | 7.299                 |
|          | 3        | 198.500           | 0.266              | 0.943        | 0.279  | 93.000       | M   | 92.31                | 4.462                 |
| <b>Σ</b> |          | <b>14,181.200</b> |                    |              |        |              |     | <b>384.91</b>        | <b>111.413</b>        |
| #20      | 1        | 296.300           | 0.667              | 0.000        | 0.000  | 91.700       | M   | 69.85                | 5.596                 |
|          | 2        | 385.600           | 0.713              | 0.476        | 0.440  | 93.000       | M   | 103.27               | 8.622                 |
| <b>Σ</b> |          | <b>15,893.800</b> |                    |              |        |              |     | <b>399.88</b>        | <b>141.317</b>        |
| #22      | <b>Σ</b> | <b>29,385.600</b> |                    |              |        |              |     | <b>1,034.13</b>      | <b>336.264</b>        |
| #23      | 1        | 442.400           | 0.960              | 0.000        | 0.000  | 85.300       | M   | 30.32                | 3.363                 |
|          | 2        | 310.500           | 0.538              | 0.559        | 0.291  | 89.500       | M   | 63.07                | 4.365                 |
| <b>Σ</b> |          | <b>30,138.500</b> |                    |              |        |              |     | <b>1,025.65</b>      | <b>343.992</b>        |
| #35      | <b>Σ</b> | <b>48,329.700</b> |                    |              |        |              |     | <b>1,260.70</b>      | <b>439.287</b>        |
| #36      | 1        | 298.200           | 0.987              | 0.000        | 0.000  | 85.000       | M   | 18.97                | 2.161                 |
|          | 2        | 196.800           | 0.441              | 0.000        | 0.000  | 87.900       | M   | 36.43                | 2.213                 |
|          | 3        | 235.590           | 0.885              | 0.166        | 0.372  | 78.300       | M   | 3.44                 | 0.446                 |
| <b>Σ</b> |          | <b>49,060.290</b> |                    |              |        |              |     | <b>1,258.12</b>      | <b>444.107</b>        |
| #37      | 1        | 744.000           | 1.756              | 0.000        | 0.000  | 84.800       | M   | 28.64                | 5.220                 |
|          | 2        | 296.000           | 0.439              | 1.780        | 0.243  | 87.800       | M   | 54.17                | 3.282                 |
|          | 3        | 237.700           | 0.333              | 1.649        | 0.246  | 85.500       | M   | 36.50                | 1.874                 |
|          | 4        | 561.400           | 1.502              | 1.780        | 0.243  | 84.100       | M   | 21.68                | 3.510                 |



| Stru #   | SWS # | SWS Area (ac) | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |                |
|----------|-------|---------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|----------------|
|          | 5     | 369.400       | 0.817              | 2.236        | 0.284  | 81.600       | M   | 14.00                | 1.471                 |                |
| <b>Σ</b> |       |               |                    |              |        |              |     | <b>51,268.790</b>    | <b>1,249.70</b>       | <b>459.465</b> |

***Subwatershed Sedimentology Detail:***

| Stru #   | SWS # | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|----------|-------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #30      | 1     | 0.095  | 200.00 | 3.80  | 0.3720 | 1.0000 | 2    | 0.4             | 2,965                      | 1.82                        | 1.55        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>0.4</b>      | <b>2,965</b>               | <b>1.82</b>                 | <b>1.55</b> |
| #28      | 1     | 0.187  | 100.00 | 10.10 | 0.3750 | 1.0000 | 3    | 739.2           | 61,682                     | 0.00                        | 0.00        |
|          | 2     | 0.196  | 100.00 | 10.20 | 0.3930 | 1.0000 | 3    | 465.2           | 68,043                     | 0.00                        | 0.00        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>939.7</b>    | <b>51,228</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #26      | 1     | 0.155  | 400.00 | 1.40  | 0.3480 | 1.0000 | 2    | 0.5             | 2,388                      | 0.74                        | 0.59        |
|          | 2     | 0.155  | 300.00 | 2.40  | 0.3340 | 1.0000 | 2    | 12.6            | 4,534                      | 0.54                        | 0.41        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>13.1</b>     | <b>4,375</b>               | <b>0.55</b>                 | <b>0.42</b> |
| #24      | 1     | 0.128  | 300.00 | 2.30  | 0.3360 | 1.0000 | 2    | 5.1             | 2,784                      | 0.20                        | 0.15        |
|          | 2     | 0.136  | 300.00 | 2.70  | 0.3440 | 1.0000 | 2    | 4.7             | 3,502                      | 0.38                        | 0.29        |
|          | 3     | 0.107  | 300.00 | 2.30  | 0.3330 | 1.0000 | 2    | 5.8             | 3,108                      | 0.51                        | 0.39        |
|          | 4     | 0.163  | 400.00 | 1.60  | 0.3210 | 1.0000 | 2    | 6.5             | 3,508                      | 0.46                        | 0.36        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>17.5</b>     | <b>2,885</b>               | <b>0.18</b>                 | <b>0.12</b> |
| #25      | 1     | 0.125  | 400.00 | 1.90  | 0.3440 | 1.0000 | 2    | 4.7             | 5,072                      | 1.86                        | 1.34        |
|          | 2     | 0.124  | 300.00 | 2.60  | 0.3280 | 1.0000 | 2    | 1.2             | 5,507                      | 2.23                        | 1.57        |
|          | 3     | 0.122  | 175.00 | 4.90  | 0.2660 | 1.0000 | 2    | 43.0            | 15,659                     | 8.76                        | 5.86        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>64.9</b>     | <b>15,537</b>              | <b>6.38</b>                 | <b>1.81</b> |
| #27      | 1     | 0.127  | 175.00 | 5.90  | 0.3160 | 1.0000 | 2    | 33.9            | 19,102                     | 9.87                        | 6.86        |
|          | 2     | 0.122  | 150.00 | 7.50  | 0.2920 | 1.0000 | 2    | 37.9            | 21,382                     | 11.60                       | 7.99        |
|          | 3     | 0.070  | 125.00 | 8.40  | 0.3270 | 1.0000 | 2    | 1.5             | 6,752                      | 2.44                        | 1.82        |
|          | 4     | 0.097  | 125.00 | 9.60  | 0.3170 | 1.0000 | 2    | 13.5            | 23,951                     | 12.80                       | 8.34        |
|          | 5     | 0.126  | 125.00 | 8.90  | 0.3290 | 1.0000 | 2    | 56.1            | 22,130                     | 9.81                        | 6.86        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>211.6</b>    | <b>23,433</b>              | <b>10.13</b>                | <b>3.20</b> |
| #29      | 1     | 0.190  | 125.00 | 9.80  | 0.3930 | 1.0000 | 3    | 532.0           | 77,172                     | 0.75                        | 0.52        |
|          | 2     | 0.203  | 125.00 | 8.90  | 0.3940 | 1.0000 | 3    | 258.7           | 61,430                     | 0.00                        | 0.00        |
|          | 3     | 0.193  | 125.00 | 8.40  | 0.3940 | 1.0000 | 3    | 175.6           | 54,954                     | 0.00                        | 0.00        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>2,116.8</b>  | <b>64,602</b>              | <b>2.94</b>                 | <b>1.26</b> |
| #32      | 1     | 0.210  | 150.00 | 7.70  | 0.3990 | 1.0000 | 3    | 371.2           | 58,211                     | 0.00                        | 0.00        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>2,217.3</b>  | <b>56,165</b>              | <b>0.00</b>                 | <b>0.00</b> |

| Stru #     | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|------------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #31        | 1        | 0.204  | 125.00 | 8.70  | 0.3620 | 1.0000 | 3    | 431.7           | 55,950                     | 0.00                        | 0.00        |
|            | 2        | 0.210  | 150.00 | 7.30  | 0.3990 | 1.0000 | 3    | 438.0           | 62,096                     | 2.06                        | 1.43        |
|            | 3        | 0.210  | 175.00 | 4.50  | 0.3980 | 1.0000 | 3    | 177.9           | 42,351                     | 1.96                        | 1.35        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>773.0</b>    | <b>37,599</b>              | <b>0.40</b>                 | <b>0.30</b> |
| <b>#33</b> | <b>Σ</b> |        |        |       |        |        |      | <b>2,990.3</b>  | <b>46,265</b>              | <b>0.13</b>                 | <b>0.07</b> |
| #34        | 1        | 0.189  | 175.00 | 4.60  | 0.2250 | 1.0000 | 3    | 39.1            | 21,215                     | 1.55                        | 1.10        |
|            | 2        | 0.206  | 175.00 | 5.10  | 0.3620 | 1.0000 | 3    | 96.3            | 41,216                     | 3.06                        | 2.19        |
|            | 3        | 0.176  | 175.00 | 4.20  | 0.2510 | 1.0000 | 3    | 149.6           | 16,385                     | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>2,757.0</b>  | <b>37,581</b>              | <b>0.05</b>                 | <b>0.03</b> |
| #5         | 1        | 0.149  | 75.00  | 12.50 | 0.3230 | 1.0000 | 3    | 233.9           | 45,624                     | 0.00                        | 0.00        |
|            | 2        | 0.133  | 75.00  | 15.80 | 0.3190 | 1.0000 | 2    | 160.7           | 60,621                     | 35.07                       | 23.47       |
|            | 3        | 0.103  | 100.00 | 11.00 | 0.2030 | 1.0000 | 3    | 112.4           | 24,558                     | 0.41                        | 0.28        |
|            | 4        | 0.093  | 75.00  | 13.80 | 0.2130 | 1.0000 | 2    | 31.5            | 24,650                     | 15.01                       | 10.10       |
|            | 5        | 0.123  | 100.00 | 11.00 | 0.1370 | 1.0000 | 3    | 105.5           | 18,986                     | 0.74                        | 0.52        |
|            | 6        | 0.149  | 75.00  | 14.70 | 0.1990 | 1.0000 | 3    | 134.3           | 42,024                     | 2.19                        | 1.53        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>597.2</b>    | <b>35,964</b>              | <b>1.23</b>                 | <b>0.63</b> |
| #6         | 1        | 0.208  | 175.00 | 4.30  | 0.3980 | 1.0000 | 3    | 120.1           | 39,925                     | 2.16                        | 1.49        |
|            | 2        | 0.183  | 175.00 | 5.40  | 0.3910 | 1.0000 | 3    | 97.6            | 36,476                     | 0.00                        | 0.00        |
|            | 3        | 0.188  | 150.00 | 7.60  | 0.3900 | 1.0000 | 3    | 194.4           | 52,428                     | 0.00                        | 0.00        |
|            | 4        | 0.210  | 150.00 | 6.30  | 0.3990 | 1.0000 | 3    | 176.3           | 49,309                     | 2.24                        | 1.64        |
|            | 5        | 0.185  | 125.00 | 8.10  | 0.3860 | 1.0000 | 3    | 136.3           | 49,341                     | 0.54                        | 0.38        |
|            | 6        | 0.104  | 100.00 | 11.30 | 0.2240 | 1.0000 | 3    | 101.7           | 25,411                     | 0.00                        | 0.00        |
|            | 7        | 0.164  | 100.00 | 11.20 | 0.3740 | 1.0000 | 3    | 144.7           | 56,415                     | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>1,150.6</b>  | <b>31,888</b>              | <b>0.18</b>                 | <b>0.10</b> |
| #7         | 1        | 0.208  | 150.00 | 7.80  | 0.3780 | 1.0000 | 3    | 702.2           | 43,218                     | 0.00                        | 0.00        |
|            | 2        | 0.209  | 100.00 | 10.20 | 0.3940 | 1.0000 | 3    | 578.3           | 58,417                     | 0.00                        | 0.00        |
|            | 3        | 0.210  | 150.00 | 6.70  | 0.3990 | 1.0000 | 3    | 259.8           | 43,870                     | 0.00                        | 0.00        |
|            | 4        | 0.210  | 100.00 | 11.50 | 0.3990 | 1.0000 | 3    | 160.1           | 89,864                     | 6.44                        | 4.62        |
|            | 5        | 0.210  | 150.00 | 7.10  | 0.3990 | 1.0000 | 3    | 203.3           | 58,980                     | 3.65                        | 2.61        |
|            | 6        | 0.209  | 150.00 | 7.90  | 0.3990 | 1.0000 | 3    | 139.9           | 62,665                     | 4.16                        | 2.98        |
|            | 7        | 0.206  | 75.00  | 15.50 | 0.3990 | 1.0000 | 3    | 266.1           | 110,381                    | 6.55                        | 4.71        |
|            | 8        | 0.202  | 75.00  | 14.50 | 0.3980 | 1.0000 | 3    | 883.3           | 99,436                     | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>3,549.5</b>  | <b>40,575</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #8         | 1        | 0.000  | 0.00   | 0.00  | 0.0000 | 1.0000 | 0    | 0.0             | 1                          | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>3,549.5</b>  | <b>40,575</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #10        | 1        | 0.190  | 300.00 | 2.70  | 0.1930 | 1.0000 | 3    | 57.1            | 7,337                      | 0.00                        | 0.00        |
|            | 2        | 0.153  | 200.00 | 3.50  | 0.3610 | 1.0000 | 2    | 15.7            | 9,695                      | 3.99                        | 2.88        |
|            | 3        | 0.189  | 200.00 | 3.70  | 0.3190 | 1.0000 | 3    | 29.3            | 12,402                     | 0.00                        | 0.00        |
|            | 4        | 0.190  | 300.00 | 2.10  | 0.1940 | 1.0000 | 3    | 20.0            | 7,361                      | 0.00                        | 0.00        |

| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 5        | 0.201  | 300.00 | 2.00  | 0.3030 | 1.0000 | 3    | 21.7            | 8,433                      | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>3,451.8</b>  | <b>36,547</b>              | <b>0.05</b>                 | <b>0.03</b> |
| #1     | 1        | 0.157  | 150.00 | 6.80  | 0.3830 | 1.0000 | 2    | 82.5            | 26,888                     | 12.53                       | 8.75        |
|        | 2        | 0.210  | 150.00 | 6.60  | 0.3990 | 1.0000 | 3    | 111.1           | 29,342                     | 0.00                        | 0.00        |
|        | 3        | 0.149  | 200.00 | 3.90  | 0.3870 | 1.0000 | 2    | 21.2            | 9,384                      | 2.84                        | 2.10        |
|        | 4        | 0.169  | 175.00 | 4.70  | 0.3950 | 1.0000 | 2    | 28.9            | 21,381                     | 10.40                       | 7.35        |
|        | 5        | 0.157  | 100.00 | 10.10 | 0.3940 | 1.0000 | 2    | 12.5            | 44,935                     | 25.37                       | 17.19       |
|        | 6        | 0.175  | 75.00  | 12.60 | 0.2840 | 1.0000 | 3    | 403.0           | 47,055                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>601.9</b>    | <b>34,411</b>              | <b>2.97</b>                 | <b>1.92</b> |
| #2     | 1        | 0.190  | 150.00 | 7.90  | 0.1930 | 1.0000 | 3    | 159.6           | 29,198                     | 1.03                        | 0.71        |
|        | 2        | 0.184  | 175.00 | 4.80  | 0.2010 | 1.0000 | 3    | 55.3            | 16,688                     | 0.00                        | 0.00        |
|        | 3        | 0.202  | 200.00 | 3.90  | 0.3220 | 1.0000 | 3    | 86.9            | 19,896                     | 0.00                        | 0.00        |
|        | 4        | 0.203  | 150.00 | 7.40  | 0.3220 | 1.0000 | 3    | 381.1           | 39,430                     | 0.00                        | 0.00        |
|        | 5        | 0.181  | 175.00 | 5.10  | 0.3710 | 1.0000 | 3    | 108.1           | 22,816                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>977.7</b>    | <b>22,730</b>              | <b>0.13</b>                 | <b>0.09</b> |
| #3     | 1        | 0.190  | 175.00 | 5.20  | 0.1930 | 1.0000 | 3    | 72.9            | 19,971                     | 0.61                        | 0.42        |
|        | 2        | 0.177  | 175.00 | 4.20  | 0.2560 | 1.0000 | 3    | 58.4            | 15,122                     | 0.00                        | 0.00        |
|        | 3        | 0.166  | 175.00 | 4.30  | 0.2290 | 1.0000 | 3    | 61.4            | 15,297                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>1,092.3</b>  | <b>18,273</b>              | <b>0.04</b>                 | <b>0.03</b> |
| #4     | <b>Σ</b> |        |        |       |        |        |      | <b>1,092.3</b>  | <b>18,273</b>              | <b>0.04</b>                 | <b>0.03</b> |
| #9     | 1        | 0.189  | 175.00 | 4.44  | 0.1970 | 1.0000 | 3    | 97.9            | 14,473                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>1,092.8</b>  | <b>15,772</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #11    | <b>Σ</b> |        |        |       |        |        |      | <b>4,544.5</b>  | <b>30,480</b>              | <b>0.02</b>                 | <b>0.01</b> |
| #21    | 1        | 0.177  | 175.00 | 4.44  | 0.2560 | 1.0000 | 3    | 39.5            | 15,701                     | 0.00                        | 0.00        |
|        | 2        | 0.184  | 175.00 | 5.81  | 0.2210 | 1.0000 | 3    | 73.9            | 24,858                     | 0.33                        | 0.23        |
|        | 3        | 0.185  | 300.00 | 2.70  | 0.2180 | 1.0000 | 3    | 40.0            | 12,731                     | 0.71                        | 0.50        |
|        | 4        | 0.175  | 300.00 | 2.66  | 0.2690 | 1.0000 | 3    | 31.4            | 9,428                      | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>4,561.0</b>  | <b>29,762</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #18    | 1        | 0.193  | 300.00 | 2.80  | 0.2200 | 1.0000 | 3    | 76.0            | 11,763                     | 0.00                        | 0.00        |
|        | 2        | 0.173  | 175.00 | 4.70  | 0.3880 | 1.0000 | 3    | 124.7           | 26,650                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>118.2</b>    | <b>12,305</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #17    | 1        | 0.196  | 300.00 | 2.60  | 0.2600 | 1.0000 | 3    | 55.0            | 14,274                     | 0.37                        | 0.26        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>55.0</b>     | <b>14,274</b>              | <b>0.37</b>                 | <b>0.26</b> |
| #19    | <b>Σ</b> |        |        |       |        |        |      | <b>173.2</b>    | <b>11,407</b>              | <b>0.09</b>                 | <b>0.07</b> |
| #15    | 1        | 0.201  | 125.00 | 8.20  | 0.3960 | 1.0000 | 3    | 368.1           | 48,226                     | 0.00                        | 0.00        |
|        | 2        | 0.161  | 100.00 | 11.40 | 0.3060 | 1.0000 | 3    | 487.2           | 50,739                     | 0.00                        | 0.00        |
|        | 3        | 0.118  | 100.00 | 10.20 | 0.2850 | 1.0000 | 2    | 152.8           | 22,483                     | 10.48                       | 7.48        |



| Stru #   | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|----------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| <b>Σ</b> |          |        |        |       |        |        |      | <b>857.0</b>    | <b>40,282</b>              | <b>0.20</b>                 | <b>0.12</b> |
| #12      | 1        | 0.124  | 150.00 | 6.30  | 0.3070 | 1.0000 | 2    | 33.4            | 16,317                     | 7.66                        | 5.26        |
|          | 2        | 0.132  | 200.00 | 3.60  | 0.3500 | 1.0000 | 2    | 6.7             | 11,058                     | 5.41                        | 3.57        |
|          | 3        | 0.136  | 175.00 | 5.00  | 0.3330 | 1.0000 | 2    | 38.4            | 17,881                     | 8.59                        | 5.82        |
|          | 4        | 0.188  | 200.00 | 3.40  | 0.3570 | 1.0000 | 2    | 19.8            | 8,880                      | 2.17                        | 1.65        |
|          | 5        | 0.228  | 175.00 | 4.10  | 0.3640 | 1.0000 | 2    | 23.2            | 25,014                     | 11.93                       | 8.15        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>106.0</b>    | <b>14,291</b>              | <b>5.52</b>                 | <b>3.61</b> |
| #13      | 1        | 0.128  | 150.00 | 6.90  | 0.3390 | 1.0000 | 2    | 19.1            | 18,713                     | 8.41                        | 5.72        |
|          | 2        | 0.130  | 175.00 | 5.70  | 0.3300 | 1.0000 | 2    | 35.2            | 17,524                     | 7.99                        | 5.56        |
|          | 3        | 0.191  | 175.00 | 6.00  | 0.2890 | 1.0000 | 2    | 69.3            | 29,144                     | 15.93                       | 11.00       |
|          | 4        | 0.122  | 175.00 | 5.10  | 0.3460 | 1.0000 | 2    | 13.5            | 20,608                     | 11.54                       | 7.65        |
|          | 5        | 0.137  | 175.00 | 4.20  | 0.3530 | 1.0000 | 2    | 4.8             | 7,061                      | 2.12                        | 1.69        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>232.3</b>    | <b>16,747</b>              | <b>7.21</b>                 | <b>4.76</b> |
| #14      | 1        | 0.196  | 100.00 | 10.20 | 0.3980 | 1.0000 | 3    | 523.7           | 80,672                     | 2.17                        | 1.48        |
|          | 2        | 0.193  | 150.00 | 6.70  | 0.4020 | 1.0000 | 3    | 340.2           | 51,669                     | 0.39                        | 0.28        |
|          | 3        | 0.169  | 75.00  | 13.80 | 0.3240 | 1.0000 | 3    | 881.1           | 62,374                     | 0.00                        | 0.00        |
|          | 4        | 0.114  | 100.00 | 11.00 | 0.2980 | 1.0000 | 3    | 40.3            | 32,851                     | 0.11                        | 0.08        |
|          | 5        | 0.078  | 100.00 | 10.10 | 0.1830 | 1.0000 | 3    | 44.0            | 14,425                     | 0.35                        | 0.25        |
|          | 6        | 0.084  | 150.00 | 7.10  | 0.2700 | 1.0000 | 2    | 16.3            | 10,073                     | 4.71                        | 3.36        |
|          | 7        | 0.087  | 100.00 | 10.00 | 0.1840 | 1.0000 | 3    | 69.6            | 13,279                     | 0.00                        | 0.00        |
|          | 8        | 0.126  | 150.00 | 6.70  | 0.2740 | 1.0000 | 2    | 68.1            | 13,578                     | 5.70                        | 4.16        |
|          | 9        | 0.117  | 150.00 | 7.30  | 0.2600 | 1.0000 | 2    | 73.3            | 14,162                     | 6.51                        | 4.74        |
|          | 10       | 0.115  | 125.00 | 8.50  | 0.2610 | 1.0000 | 2    | 41.0            | 15,152                     | 7.17                        | 5.20        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>1,686.3</b>  | <b>69,407</b>              | <b>0.58</b>                 | <b>0.15</b> |
| #16      | 1        | 0.200  | 200.00 | 3.30  | 0.3000 | 1.0000 | 3    | 122.9           | 17,391                     | 0.00                        | 0.00        |
|          | 2        | 0.204  | 150.00 | 6.00  | 0.3630 | 1.0000 | 3    | 297.4           | 41,912                     | 0.09                        | 0.06        |
|          | 3        | 0.210  | 150.00 | 6.10  | 0.3990 | 1.0000 | 3    | 240.0           | 54,115                     | 3.89                        | 2.79        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>3,202.2</b>  | <b>48,003</b>              | <b>0.53</b>                 | <b>0.23</b> |
| #20      | 1        | 0.186  | 175.00 | 4.80  | 0.2130 | 1.0000 | 3    | 95.0            | 17,756                     | 0.00                        | 0.00        |
|          | 2        | 0.194  | 200.00 | 3.80  | 0.2330 | 1.0000 | 3    | 120.6           | 14,509                     | 0.00                        | 0.00        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>3,473.7</b>  | <b>36,837</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #22      | <b>Σ</b> |        |        |       |        |        |      | <b>8,034.7</b>  | <b>30,529</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #23      | 1        | 0.172  | 175.00 | 4.20  | 0.2810 | 1.0000 | 3    | 48.2            | 14,969                     | 0.00                        | 0.00        |
|          | 2        | 0.185  | 150.00 | 6.00  | 0.2160 | 1.0000 | 3    | 90.2            | 21,665                     | 0.00                        | 0.00        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>7,929.8</b>  | <b>29,707</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #35      | <b>Σ</b> |        |        |       |        |        |      | <b>10,686.8</b> | <b>27,942</b>              | <b>0.01</b>                 | <b>0.01</b> |
| #36      | 1        | 0.190  | 175.00 | 5.94  | 0.2830 | 1.0000 | 3    | 44.7            | 21,503                     | 0.00                        | 0.00        |
|          | 2        | 0.180  | 125.00 | 9.92  | 0.2410 | 1.0000 | 3    | 82.3            | 40,194                     | 0.00                        | 0.00        |

| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 3        | 0.151  | 300.00 | 2.63  | 0.3890 | 1.0000 | 2    | 3.6             | 8,290                      | 3.23                        | 2.29        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>10,716.3</b> | <b>34,997</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #37    | 1        | 0.196  | 200.00 | 3.80  | 0.3980 | 1.0000 | 2    | 76.7            | 14,865                     | 5.59                        | 4.04        |
|        | 2        | 0.193  | 175.00 | 5.40  | 0.4020 | 1.0000 | 3    | 133.8           | 41,249                     | 0.00                        | 0.00        |
|        | 3        | 0.173  | 150.00 | 7.11  | 0.2770 | 1.0000 | 3    | 58.2            | 31,798                     | 0.00                        | 0.00        |
|        | 4        | 0.171  | 150.00 | 6.52  | 0.2990 | 1.0000 | 2    | 60.8            | 17,257                     | 6.83                        | 5.01        |
|        | 5        | 0.078  | 400.00 | 1.20  | 0.1830 | 1.0000 | 2    | 2.1             | 1,430                      | 0.66                        | 0.47        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>10,744.2</b> | <b>29,250</b>              | <b>0.14</b>                 | <b>0.08</b> |

### Subwatershed Time of Concentration Details:

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.65      | 50.00            | 1,369.00          | 1.910          | 0.199        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.57      | 157.00           | 10,030.00         | 3.750          | 0.742        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.941</b> |
| #1        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 6.63      | 70.00            | 1,056.00          | 2.570          | 0.114        |
|           |          | 5. Nearly bare and untilled, and alluvial valley fans | 1.98      | 150.00           | 7,573.00          | 1.400          | 1.502        |
| <b>#1</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.616</b> |
| #1        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.65      | 117.00           | 7,070.00          | 1.280          | 1.534        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.43      | 126.00           | 5,188.00          | 4.670          | 0.308        |
| <b>#1</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.842</b> |
| #1        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 5.77      | 260.00           | 4,506.00          | 2.400          | 0.521        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.84      | 168.00           | 5,924.00          | 5.050          | 0.325        |
| <b>#1</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.846</b> |
| #1        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 19.93     | 180.00           | 903.00            | 4.460          | 0.056        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.30      | 178.00           | 5,393.00          | 5.450          | 0.274        |
| <b>#1</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.330</b> |
| #1        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 13.43     | 105.00           | 782.00            | 3.660          | 0.059        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.62      | 283.00           | 10,822.00         | 4.850          | 0.619        |
| <b>#1</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.678</b> |
| #2        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 6.84      | 70.00            | 1,024.00          | 2.610          | 0.108        |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 70.00            | 4,325.00          | 3.810          | 0.315        |
| <b>#2</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.423</b> |
| #2        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.56      | 45.00            | 810.00            | 2.350          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.86      | 40.00            | 4,663.00          | 2.770          | 0.467        |
| <b>#2</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.562</b> |
| #2        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 5.89      | 50.00            | 849.00            | 2.420          | 0.097        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.17      | 80.00            | 6,862.00          | 3.230          | 0.590        |
| <b>#2</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.687</b> |
| #2        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 12.63     | 95.00            | 752.00            | 3.550          | 0.058        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.40      | 135.00           | 9,630.00          | 3.550          | 0.753        |
| <b>#2</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.811</b> |
| #2        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 11.02     | 70.00            | 635.00            | 3.320          | 0.053        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.46      | 40.00            | 8,732.00          | 2.030          | 1.194        |
| <b>#2</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.247</b> |
| #3        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 10.00            | 805.00            | 1.110          | 0.201        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.33      | 40.00            | 3,017.00          | 3.450          | 0.242        |
| <b>#3</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.443</b> |
| #3        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 0.68      | 10.00            | 1,478.00          | 0.820          | 0.500        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.78      | 100.00           | 5,622.00          | 4.000          | 0.390        |
| <b>#3</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.890</b> |
| #3        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.66      | 70.00            | 1,501.00          | 2.150          | 0.193        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.17      | 60.00            | 5,126.00          | 3.240          | 0.439        |
| <b>#3</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.632</b> |
| #5        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 19.06     | 285.00           | 1,495.00          | 4.360          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.64      | 242.00           | 9,174.00          | 4.870          | 0.523        |
| <b>#5</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.618</b> |
| #5        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 14.27     | 105.00           | 736.00            | 3.770          | 0.054        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.08      | 297.00           | 7,279.00          | 6.050          | 0.334        |
| <b>#5</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.388</b> |
| #5        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 8.27      | 35.00            | 423.00            | 2.870          | 0.040        |



| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.44      | 208.00           | 6,049.00          | 5.560          | 0.302        |
| <b>#5</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.342</b> |
| #5        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 14.58     | 85.00            | 583.00            | 3.810          | 0.042        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.53      | 248.00           | 5,473.00          | 6.380          | 0.238        |
| <b>#5</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.280</b> |
| #5        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 5.07      | 70.00            | 1,382.00          | 2.250          | 0.170        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.89      | 170.00           | 4,375.00          | 5.910          | 0.205        |
| <b>#5</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.375</b> |
| #5        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 12.48     | 90.00            | 721.00            | 3.530          | 0.056        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 5.16      | 274.00           | 5,308.02          | 6.810          | 0.216        |
| <b>#5</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.272</b> |
| #6        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 5.36      | 75.00            | 1,399.00          | 2.310          | 0.168        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.41      | 66.00            | 2,742.00          | 4.650          | 0.163        |
| <b>#6</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.331</b> |
| #6        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 80.00            | 2,359.00          | 1.840          | 0.356        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.63      | 80.00            | 3,039.00          | 4.860          | 0.173        |
| <b>#6</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.529</b> |
| #6        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.60      | 34.00            | 739.00            | 2.140          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.33      | 136.00           | 5,845.00          | 4.570          | 0.355        |
| <b>#6</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.450</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 6.06      | 85.00            | 1,402.00          | 2.460          | 0.158        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.52      | 96.00            | 3,810.00          | 4.760          | 0.222        |
| <b>#6</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.380</b> |
| #6        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 7.24      | 70.00            | 967.00            | 2.690          | 0.099        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.34      | 117.00           | 5,003.00          | 4.580          | 0.303        |
| <b>#6</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.402</b> |
| #6        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 31.83     | 183.00           | 575.00            | 5.640          | 0.028        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.38      | 270.00           | 7,990.00          | 5.510          | 0.402        |
| <b>#6</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.430</b> |
| #6        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 23.08     | 325.00           | 1,408.00          | 4.800          | 0.081        |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.88      | 240.00           | 8,327.00          | 5.090          | 0.454        |
| <b>#6</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.535</b> |
| #7        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.42     | 90.00            | 788.00            | 3.370          | 0.064        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.46      | 230.00           | 15,769.00         | 3.620          | 1.210        |
| <b>#7</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.274</b> |
| #7        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 10.97     | 60.00            | 547.00            | 3.310          | 0.045        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.61      | 220.00           | 13,660.00         | 3.800          | 0.998        |
| <b>#7</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.043</b> |
| #7        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 6.40      | 60.00            | 938.00            | 2.520          | 0.103        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.72      | 171.00           | 9,931.00          | 3.930          | 0.701        |
| <b>#7</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.804</b> |
| #7        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 19.23     | 80.00            | 416.00            | 4.380          | 0.026        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.45      | 100.00           | 4,083.00          | 4.690          | 0.241        |
| <b>#7</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.267</b> |
| #7        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 6.09      | 67.00            | 1,101.00          | 2.460          | 0.124        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.51      | 80.00            | 3,184.00          | 4.750          | 0.186        |
| <b>#7</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.310</b> |
| #7        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 5.93      | 63.00            | 1,062.00          | 2.430          | 0.121        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.74      | 82.00            | 2,993.00          | 4.960          | 0.167        |
| <b>#7</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.288</b> |
| #7        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 7.97      | 65.00            | 816.00            | 2.820          | 0.080        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.48      | 153.00           | 4,400.00          | 5.590          | 0.218        |
| <b>#7</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.298</b> |
| #7        | 8        | 5. Nearly bare and untilled, and alluvial valley fans | 6.60      | 50.00            | 758.00            | 2.560          | 0.082        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.66      | 473.00           | 10,157.00         | 6.470          | 0.436        |
| <b>#7</b> | <b>8</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.518</b> |
| #9        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.35      | 90.00            | 2,687.00          | 1.830          | 0.407        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.58      | 20.00            | 3,463.00          | 2.270          | 0.423        |
| <b>#9</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.830</b> |
| #10       | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 41.00            | 3,317.00          | 1.110          | 0.830        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.70      | 29.00            | 4,125.00          | 2.510          | 0.456        |
| <b>#10</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.286</b> |
| #10        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.25      | 125.00           | 5,554.00          | 1.500          | 1.028        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 85.00            | 3,997.00          | 4.370          | 0.254        |
| <b>#10</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.282</b> |
| #10        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.39      | 68.00            | 4,904.00          | 1.170          | 1.164        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.73      | 90.00            | 1,904.00          | 6.520          | 0.081        |
| <b>#10</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.245</b> |
| #10        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.76      | 51.00            | 1,357.00          | 1.930          | 0.195        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.65      | 22.00            | 3,385.00          | 2.410          | 0.390        |
| <b>#10</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.585</b> |
| #10        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 1.63      | 88.00            | 5,391.16          | 1.270          | 1.179        |
| <b>#10</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.179</b> |
| #12        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.50      | 75.00            | 1,667.00          | 2.120          | 0.218        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.85      | 155.00           | 8,400.00          | 4.070          | 0.573        |
| <b>#12</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.791</b> |
| #12        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.99      | 50.00            | 1,674.03          | 1.720          | 0.270        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.67      | 70.00            | 4,201.17          | 3.870          | 0.301        |
| <b>#12</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.571</b> |
| #12        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.04      | 57.00            | 1,411.00          | 2.000          | 0.195        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.55      | 107.00           | 6,884.00          | 3.740          | 0.511        |
| <b>#12</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.706</b> |
| #12        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.23      | 84.00            | 3,771.04          | 1.490          | 0.703        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 186.00           | 11,515.60         | 3.810          | 0.839        |
| <b>#12</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.542</b> |
| #12        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.68      | 53.00            | 1,442.00          | 1.910          | 0.209        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.95      | 120.00           | 6,155.00          | 4.180          | 0.409        |
| <b>#12</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.618</b> |
| #13        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.62      | 62.00            | 1,342.00          | 2.140          | 0.174        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.91      | 157.00           | 8,225.00          | 4.140          | 0.551        |
| <b>#13</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.725</b> |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #13        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.91      | 50.00            | 1,717.00          | 1.700          | 0.280        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.28      | 183.00           | 8,039.00          | 4.520          | 0.494        |
| <b>#13</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.774</b> |
| #13        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 6.18      | 95.00            | 1,537.00          | 2.480          | 0.172        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 135.00           | 6,347.00          | 4.370          | 0.403        |
| <b>#13</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.575</b> |
| #13        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.17      | 10.00            | 315.00            | 1.780          | 0.049        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.30      | 100.00           | 4,344.00          | 4.550          | 0.265        |
| <b>#13</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.314</b> |
| #13        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.10      | 70.00            | 2,255.00          | 1.760          | 0.355        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.23      | 140.00           | 11,392.00         | 3.320          | 0.953        |
| <b>#13</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.308</b> |
| #14        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 10.59     | 63.00            | 595.00            | 3.250          | 0.050        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.60      | 151.00           | 5,808.00          | 4.830          | 0.334        |
| <b>#14</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.384</b> |
| #14        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.28      | 67.00            | 920.00            | 2.690          | 0.095        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.17      | 123.00           | 5,670.00          | 4.410          | 0.357        |
| <b>#14</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.452</b> |
| #14        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 21.46     | 150.00           | 699.00            | 4.630          | 0.041        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.10      | 364.00           | 11,728.00         | 5.280          | 0.617        |
| <b>#14</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.658</b> |
| #14        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 35.00            | 1,032.00          | 1.840          | 0.155        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.97      | 103.00           | 3,470.00          | 5.160          | 0.186        |
| <b>#14</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.341</b> |
| #14        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 28.15     | 125.00           | 444.00            | 5.300          | 0.023        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.18      | 246.00           | 5,886.00          | 6.130          | 0.266        |
| <b>#14</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.289</b> |
| #14        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 3.18      | 40.00            | 1,257.00          | 1.780          | 0.196        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.29      | 228.00           | 9,963.00          | 4.530          | 0.610        |
| <b>#14</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.806</b> |

| Stru #     | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #14        | 7         | 5. Nearly bare and untilled, and alluvial valley fans | 16.72     | 100.00           | 598.00            | 4.080          | 0.040        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.81      | 243.00           | 8,649.00          | 5.020          | 0.478        |
| <b>#14</b> | <b>7</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.518</b> |
| #14        | 8         | 5. Nearly bare and untilled, and alluvial valley fans | 1.70      | 47.00            | 2,765.00          | 1.300          | 0.590        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.44      | 274.00           | 11,208.00         | 4.690          | 0.663        |
| <b>#14</b> | <b>8</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.253</b> |
| #14        | 9         | 5. Nearly bare and untilled, and alluvial valley fans | 2.87      | 105.00           | 3,657.00          | 1.690          | 0.601        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.43      | 194.00           | 7,991.00          | 4.670          | 0.475        |
| <b>#14</b> | <b>9</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.076</b> |
| #14        | 10        | 5. Nearly bare and untilled, and alluvial valley fans | 2.75      | 80.00            | 2,907.00          | 1.650          | 0.489        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.41      | 172.00           | 7,149.00          | 4.650          | 0.427        |
| <b>#14</b> | <b>10</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.916</b> |
| #15        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 12.80     | 54.00            | 422.00            | 3.570          | 0.032        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.68      | 181.00           | 10,781.00         | 3.880          | 0.771        |
| <b>#15</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.803</b> |
| #15        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 44.22     | 260.00           | 588.00            | 6.640          | 0.024        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.45      | 254.00           | 10,354.00         | 4.690          | 0.613        |
| <b>#15</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.637</b> |
| #15        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 10.04     | 85.00            | 847.00            | 3.160          | 0.074        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.34      | 366.00           | 15,663.00         | 4.580          | 0.949        |
| <b>#15</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.023</b> |
| #16        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 4.17      | 15.00            | 360.00            | 2.040          | 0.049        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.42      | 108.00           | 7,618.00          | 3.570          | 0.592        |
| <b>#16</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.641</b> |
| #16        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 8.70      | 62.00            | 713.00            | 2.940          | 0.067        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.99      | 144.00           | 7,241.00          | 4.230          | 0.475        |
| <b>#16</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.542</b> |
| #16        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 6.88      | 32.00            | 465.00            | 2.620          | 0.049        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.29      | 81.00            | 3,543.00          | 4.530          | 0.217        |
| <b>#16</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.266</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #17        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 9.37      | 65.00            | 694.00            | 3.060          | 0.062        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.19      | 56.00            | 4,712.00          | 3.270          | 0.400        |
| <b>#17</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.462</b> |
| #18        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 9.00      | 60.00            | 667.00            | 2.990          | 0.061        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.97      | 61.00            | 6,287.00          | 2.950          | 0.591        |
| <b>#18</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.652</b> |
| #18        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.47      | 33.00            | 1,336.00          | 1.570          | 0.236        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.01      | 164.00           | 8,154.00          | 4.250          | 0.532        |
| <b>#18</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.768</b> |
| #20        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.87     | 45.00            | 379.00            | 3.440          | 0.030        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.75      | 45.00            | 5,969.00          | 2.600          | 0.637        |
| <b>#20</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.667</b> |
| #20        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.40      | 45.00            | 833.00            | 2.320          | 0.099        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.30      | 98.00            | 7,547.00          | 3.410          | 0.614        |
| <b>#20</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.713</b> |
| #21        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.09      | 60.00            | 1,467.00          | 2.020          | 0.201        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.93      | 60.00            | 6,433.00          | 2.890          | 0.618        |
| <b>#21</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.819</b> |
| #21        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.50      | 50.00            | 1,430.00          | 1.860          | 0.213        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.15      | 60.00            | 2,785.00          | 4.400          | 0.175        |
| <b>#21</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.388</b> |
| #21        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.70      | 15.00            | 881.00            | 1.300          | 0.188        |
|            |          | 9. Small streams flowing bankfull                     | 1.49      | 60.00            | 4,014.00          | 11.000         | 0.101        |
| <b>#21</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.289</b> |
| #21        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.21      | 40.00            | 1,811.02          | 1.480          | 0.339        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.84      | 50.00            | 5,949.54          | 2.750          | 0.600        |
| <b>#21</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.939</b> |
| #23        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.44      | 65.00            | 2,660.01          | 1.560          | 0.473        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.33      | 10.00            | 3,017.50          | 1.720          | 0.487        |
| <b>#23</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.960</b> |
| #23        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.49      | 60.00            | 1,718.01          | 1.860          | 0.256        |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.66      | 65.00            | 3,926.06          | 3.860          | 0.282        |
| <b>#23</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.538</b> |
| #24        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.71      | 430.00           | 25,118.00         | 1.300          | 5.367        |
| <b>#24</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>5.367</b> |
| #24        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.84      | 430.00           | 23,393.00         | 1.350          | 4.813        |
| <b>#24</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>4.813</b> |
| #24        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.82      | 155.00           | 8,498.00          | 1.350          | 1.748        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.84      | 40.00            | 4,771.00          | 2.740          | 0.483        |
| <b>#24</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.231</b> |
| #24        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 50.00            | 4,042.00          | 1.110          | 1.011        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.49      | 60.00            | 12,150.00         | 2.100          | 1.607        |
| <b>#24</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.618</b> |
| #25        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 0.51      | 10.00            | 1,950.00          | 0.710          | 0.762        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.81      | 60.00            | 3,322.00          | 4.030          | 0.228        |
| <b>#25</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.990</b> |
| #25        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.11      | 25.00            | 2,254.00          | 1.050          | 0.596        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.36      | 75.00            | 3,178.00          | 4.600          | 0.191        |
| <b>#25</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.787</b> |
| #25        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 3.23      | 30.00            | 929.00            | 1.790          | 0.144        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.45      | 154.00           | 6,297.00          | 4.690          | 0.372        |
| <b>#25</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.516</b> |
| #26        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.20      | 103.00           | 8,602.00          | 1.090          | 2.192        |
| <b>#26</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.192</b> |
| #26        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.23      | 120.00           | 9,780.00          | 1.100          | 2.469        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.18      | 184.00           | 8,454.00          | 4.420          | 0.531        |
| <b>#26</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>3.000</b> |
| #27        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.32      | 50.00            | 1,158.02          | 2.070          | 0.155        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.53      | 198.00           | 7,838.16          | 4.760          | 0.457        |
| <b>#27</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.612</b> |
| #27        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.26      | 30.00            | 570.00            | 2.290          | 0.069        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.15      | 278.00           | 8,822.00          | 5.320          | 0.460        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#27</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.529</b> |
| #27        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 16.33     | 80.00            | 490.00            | 4.040          | 0.033        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.15      | 225.00           | 10,443.00         | 4.400          | 0.659        |
| <b>#27</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.692</b> |
| #27        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 12.43     | 65.00            | 523.00            | 3.520          | 0.041        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.49      | 225.00           | 6,454.00          | 5.600          | 0.320        |
| <b>#27</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.361</b> |
| #27        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 9.40      | 25.00            | 266.00            | 3.060          | 0.024        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.32      | 364.00           | 15,700.00         | 4.560          | 0.956        |
| <b>#27</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.980</b> |
| #28        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 5.25      | 40.00            | 762.00            | 2.290          | 0.092        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.96      | 310.00           | 10,479.34         | 5.150          | 0.565        |
| <b>#28</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.657</b> |
| #28        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 25.86     | 105.00           | 406.00            | 5.080          | 0.022        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.96      | 310.00           | 10,479.34         | 5.150          | 0.565        |
| <b>#28</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.587</b> |
| #29        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.58     | 30.00            | 259.00            | 3.400          | 0.021        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.61      | 288.00           | 7,976.00          | 5.700          | 0.388        |
| <b>#29</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.409</b> |
| #29        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 8.06      | 40.00            | 496.00            | 2.830          | 0.048        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.90      | 252.00           | 8,693.55          | 5.100          | 0.473        |
| <b>#29</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.521</b> |
| #29        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 7.25      | 25.00            | 345.00            | 2.690          | 0.035        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.26      | 158.00           | 7,001.00          | 4.500          | 0.432        |
| <b>#29</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.467</b> |
| #30        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.93      | 35.00            | 710.00            | 2.220          | 0.088        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.67      | 243.00           | 14,540.00         | 3.870          | 1.043        |
| <b>#30</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.131</b> |
| #31        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.91      | 15.00            | 515.00            | 1.700          | 0.084        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.74      | 247.00           | 9,006.00          | 4.960          | 0.504        |
| <b>#31</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.588</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #31        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.46      | 25.00            | 335.00            | 2.730          | 0.034        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.18      | 138.00           | 6,335.00          | 4.420          | 0.398        |
| <b>#31</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.432</b> |
| #31        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 3.84      | 20.00            | 521.00            | 1.950          | 0.074        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.24      | 108.00           | 4,826.00          | 4.480          | 0.299        |
| <b>#31</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.373</b> |
| #32        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.48      | 22.00            | 632.00            | 1.860          | 0.094        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.56      | 101.00           | 6,494.00          | 3.740          | 0.482        |
| <b>#32</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.576</b> |
| #34        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.21      | 25.00            | 779.00            | 1.790          | 0.120        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.80      | 63.00            | 2,251.00          | 5.010          | 0.124        |
| <b>#34</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.244</b> |
| #34        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.75      | 40.00            | 696.00            | 2.390          | 0.080        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 23.00     | 2,100.00         | 9,130.43          | 14.380         | 0.176        |
| <b>#34</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.256</b> |
| #34        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.67      | 40.00            | 1,500.00          | 1.630          | 0.255        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.28      | 98.00            | 7,675.00          | 3.380          | 0.630        |
| <b>#34</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.885</b> |
| #36        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.21      | 105.00           | 3,274.00          | 1.790          | 0.508        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.21      | 5.00             | 2,367.00          | 1.370          | 0.479        |
| <b>#36</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.987</b> |
| #36        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.50      | 140.00           | 2,547.00          | 2.340          | 0.302        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.58      | 30.00            | 1,897.00          | 3.770          | 0.139        |
| <b>#36</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.441</b> |
| #36        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.03      | 80.00            | 3,938.62          | 1.420          | 0.770        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.52      | 50.00            | 1,981.86          | 4.760          | 0.115        |
| <b>#36</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.885</b> |
| #37        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.68      | 129.00           | 2,754.05          | 2.160          | 0.354        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.16      | 10.00            | 6,108.73          | 1.210          | 1.402        |
| <b>#37</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.756</b> |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #37        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.32      | 90.00            | 1,229.00          | 2.700          | 0.126        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 70.00            | 4,309.01          | 3.820          | 0.313        |
| <b>#37</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.439</b> |
| #37        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 8.10      | 100.00           | 1,234.00          | 2.840          | 0.120        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.66      | 100.00           | 3,763.21          | 4.890          | 0.213        |
| <b>#37</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.333</b> |
| #37        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 5.09      | 90.00            | 1,768.03          | 2.250          | 0.218        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.36      | 30.00            | 8,326.39          | 1.800          | 1.284        |
| <b>#37</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.502</b> |
| #37        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 0.81      | 20.00            | 2,466.09          | 0.900          | 0.761        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.06      | 50.00            | 1,231.01          | 6.040          | 0.056        |
| <b>#37</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.817</b> |

### ***Subwatershed Muskingum Routing Details:***

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.29      | 107.00           | 8,294.00          | 3.400          | 0.677        |
| <b>#1</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.677</b> |
| #1        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.27      | 113.00           | 8,880.00          | 3.380          | 0.729        |
| <b>#1</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.729</b> |
| #1        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.35      | 171.00           | 12,634.00         | 3.490          | 1.005        |
| <b>#1</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.005</b> |
| #1        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.49      | 274.00           | 18,349.00         | 3.660          | 1.392        |
| <b>#1</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.392</b> |
| #1        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.49      | 274.00           | 18,349.00         | 3.660          | 1.392        |
| <b>#1</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.392</b> |
| #2        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.53      | 20.00            | 3,756.00          | 2.180          | 0.478        |
| <b>#2</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.478</b> |
| #2        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.55      | 25.00            | 4,570.00          | 2.210          | 0.574        |
| <b>#2</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.574</b> |
| #2        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.55      | 25.00            | 4,570.00          | 2.210          | 0.574        |
| <b>#2</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.574</b> |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #2        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.65      | 45.00            | 6,955.00          | 2.410          | 0.801        |
| <b>#2</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.801</b> |
| #3        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.92      | 20.00            | 2,168.00          | 2.880          | 0.209        |
| <b>#3</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.209</b> |
| #5        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#5</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #5        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.75      | 125.00           | 7,149.00          | 3.960          | 0.501        |
| <b>#5</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.501</b> |
| #5        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.65      | 155.00           | 9,418.00          | 3.840          | 0.681        |
| <b>#5</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #5        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.65      | 155.00           | 9,418.00          | 3.840          | 0.681        |
| <b>#5</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #5        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.67      | 239.00           | 14,273.00         | 3.880          | 1.021        |
| <b>#5</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.021</b> |
| #5        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.68      | 239.00           | 14,223.00         | 3.880          | 1.018        |
| <b>#5</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.018</b> |
| #6        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.16      | 26.00            | 2,241.00          | 3.230          | 0.192        |
| <b>#6</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.192</b> |
| #6        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.00      | 50.00            | 4,987.00          | 3.000          | 0.461        |
| <b>#6</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.461</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.00      | 50.00            | 4,987.00          | 1.000          | 1.385        |
| <b>#6</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.385</b> |
| #6        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.02      | 89.00            | 8,685.00          | 3.030          | 0.796        |
| <b>#6</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.796</b> |
| #6        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.06      | 126.00           | 11,860.00         | 3.090          | 1.066        |
| <b>#6</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.066</b> |
| #6        | 7        | 8. Large gullies, diversions, and low flowing streams | 1.06      | 126.00           | 11,860.00         | 3.090          | 1.066        |
| <b>#6</b> | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.066</b> |
| #7        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.16      | 140.00           | 12,037.00         | 3.230          | 1.035        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#7</b>  | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.035</b> |
| #7         | 5        | 8. Large gullies, diversions, and low flowing streams | 1.14      | 140.00           | 12,307.69         | 3.190          | 1.071        |
| <b>#7</b>  | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.071</b> |
| #7         | 6        | 8. Large gullies, diversions, and low flowing streams | 1.17      | 158.00           | 13,546.00         | 3.230          | 1.164        |
| <b>#7</b>  | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.164</b> |
| #7         | 7        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 187.00           | 15,784.00         | 3.260          | 1.344        |
| <b>#7</b>  | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.344</b> |
| #7         | 8        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 187.00           | 15,784.00         | 3.260          | 1.344        |
| <b>#7</b>  | <b>8</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.344</b> |
| #10        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.76      | 37.00            | 4,861.00          | 2.610          | 0.517        |
| <b>#10</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.517</b> |
| #10        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.76      | 37.00            | 4,861.00          | 2.610          | 0.517        |
| <b>#10</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.517</b> |
| #10        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.79      | 47.00            | 5,956.00          | 2.660          | 0.621        |
| <b>#10</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.621</b> |
| #12        | 2        | 8. Large gullies, diversions, and low flowing streams | 8.24      | 111.00           | 1,347.00          | 8.610          | 0.043        |
| <b>#12</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.043</b> |
| #12        | 3        | 8. Large gullies, diversions, and low flowing streams | 8.01      | 109.00           | 1,360.00          | 8.490          | 0.044        |
| <b>#12</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.044</b> |
| #12        | 4        | 8. Large gullies, diversions, and low flowing streams | 2.24      | 176.00           | 7,866.00          | 4.480          | 0.487        |
| <b>#12</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.487</b> |
| #12        | 5        | 8. Large gullies, diversions, and low flowing streams | 2.24      | 176.00           | 7,866.00          | 4.480          | 0.487        |
| <b>#12</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.487</b> |
| #13        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.34      | 54.00            | 4,025.00          | 3.470          | 0.322        |
| <b>#13</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.322</b> |
| #13        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.98      | 72.00            | 7,333.00          | 2.970          | 0.685        |
| <b>#13</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.685</b> |
| #13        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 127.00           | 10,806.00         | 3.250          | 0.923        |
| <b>#13</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.923</b> |
| #13        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 127.00           | 10,806.00         | 3.250          | 0.923        |
| <b>#13</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.923</b> |
| #14        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#14</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |



| Stru #     | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #14        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.83      | 58.00            | 6,957.00          | 2.730          | 0.707        |
| <b>#14</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.707</b> |
| #14        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.81      | 77.00            | 9,480.00          | 2.700          | 0.975        |
| <b>#14</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.975</b> |
| #14        | 4         | 8. Large gullies, diversions, and low flowing streams | 0.86      | 147.00           | 17,117.00         | 2.770          | 1.716        |
| <b>#14</b> | <b>4</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.716</b> |
| #14        | 5         | 8. Large gullies, diversions, and low flowing streams | 0.88      | 175.00           | 19,934.00         | 2.810          | 1.970        |
| <b>#14</b> | <b>5</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.970</b> |
| #14        | 6         | 8. Large gullies, diversions, and low flowing streams | 0.95      | 211.00           | 22,155.00         | 2.920          | 2.107        |
| <b>#14</b> | <b>6</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.107</b> |
| #14        | 7         | 8. Large gullies, diversions, and low flowing streams | 0.96      | 257.00           | 26,835.00         | 2.930          | 2.544        |
| <b>#14</b> | <b>7</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.544</b> |
| #14        | 8         | 8. Large gullies, diversions, and low flowing streams | 0.96      | 257.00           | 26,835.00         | 2.930          | 2.544        |
| <b>#14</b> | <b>8</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.544</b> |
| #14        | 9         | 8. Large gullies, diversions, and low flowing streams | 0.95      | 307.00           | 32,146.59         | 2.930          | 3.047        |
| <b>#14</b> | <b>9</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.047</b> |
| #14        | 10        | 8. Large gullies, diversions, and low flowing streams | 0.96      | 339.00           | 35,382.00         | 2.930          | 3.354        |
| <b>#14</b> | <b>10</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.354</b> |
| #15        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#15</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #15        | 2         | 8. Large gullies, diversions, and low flowing streams | 1.14      | 86.00            | 7,535.00          | 3.200          | 0.654        |
| <b>#15</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.654</b> |
| #15        | 3         | 8. Large gullies, diversions, and low flowing streams | 1.25      | 115.00           | 9,236.00          | 3.340          | 0.768        |
| <b>#15</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.768</b> |
| #16        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.58      | 24.00            | 4,161.00          | 2.270          | 0.509        |
| <b>#16</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.509</b> |
| #16        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.51      | 37.00            | 7,269.00          | 2.140          | 0.943        |
| <b>#16</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.943</b> |
| #17        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#17</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #18        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#18</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #18        | 2         | 8. Large gullies, diversions, and low flowing streams | 1.02      | 62.00            | 6,103.00          | 3.020          | 0.561        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#18</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.561</b> |
| #20        | 2        | 8. Large gullies, diversions, and low flowing streams | 17.00     | 3,605.00         | 21,205.88         | 12.360         | 0.476        |
| <b>#20</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.476</b> |
| #21        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#21</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #21        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.41      | 20.00            | 4,824.00          | 1.930          | 0.694        |
| <b>#21</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.694</b> |
| #21        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 20.00            | 5,626.00          | 1.780          | 0.877        |
| <b>#21</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.877</b> |
| #21        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 20.00            | 5,626.00          | 1.780          | 0.877        |
| <b>#21</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.877</b> |
| #23        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#23</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #23        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.63      | 30.00            | 4,771.75          | 2.370          | 0.559        |
| <b>#23</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.559</b> |
| #24        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.79      | 180.00           | 22,769.00         | 2.660          | 2.377        |
| <b>#24</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.377</b> |
| #24        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.78      | 180.00           | 23,111.00         | 2.640          | 2.431        |
| <b>#24</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.431</b> |
| #24        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#24</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #25        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.99      | 104.00           | 5,220.00          | 4.230          | 0.342        |
| <b>#25</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.342</b> |
| #25        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.99      | 104.00           | 5,220.00          | 4.230          | 0.342        |
| <b>#25</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.342</b> |
| #25        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#25</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #27        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.38      | 216.00           | 15,629.00         | 3.520          | 1.233        |
| <b>#27</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.233</b> |
| #27        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.17      | 144.00           | 12,301.00         | 3.240          | 1.054        |
| <b>#27</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.054</b> |
| #27        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 76.00            | 6,454.00          | 3.250          | 0.551        |
| <b>#27</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.551</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #27        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 76.00            | 6,454.00          | 3.250          | 0.551        |
| <b>#27</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.551</b> |
| #28        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.30      | 84.00            | 6,445.17          | 3.420          | 0.523        |
| <b>#28</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.523</b> |
| #29        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.88      | 37.00            | 4,210.00          | 2.810          | 0.416        |
| <b>#29</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.416</b> |
| #29        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.88      | 26.00            | 2,949.00          | 2.810          | 0.291        |
| <b>#29</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.291</b> |
| #31        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.35      | 76.00            | 5,639.00          | 3.480          | 0.450        |
| <b>#31</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.450</b> |
| #31        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.15      | 20.00            | 1,734.00          | 3.220          | 0.149        |
| <b>#31</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.149</b> |
| #34        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.73      | 65.00            | 8,900.00          | 2.560          | 0.965        |
| <b>#34</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.965</b> |
| #34        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.73      | 65.00            | 8,900.00          | 2.560          | 0.965        |
| <b>#34</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.965</b> |
| #36        | 3        | 8. Large gullies, diversions, and low flowing streams | 2.71      | 80.00            | 2,957.00          | 4.930          | 0.166        |
| <b>#36</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.166</b> |
| #37        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.29      | 30.00            | 10,319.91         | 1.610          | 1.780        |
| <b>#37</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.780</b> |
| #37        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.31      | 30.00            | 9,800.71          | 1.650          | 1.649        |
| <b>#37</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.649</b> |
| #37        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.29      | 30.00            | 10,319.91         | 1.610          | 1.780        |
| <b>#37</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.780</b> |
| #37        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.56      | 100.00           | 17,956.54         | 2.230          | 2.236        |
| <b>#37</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.236</b> |



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# **Cottonwood Arroyo Pre-mine Hydrology and Sedimentology**

***The drainage subdivisions used to model the hydrology is shown  
on Exhibit 18.B.***

***Revised February 2012***

Art O'Hayre

***General Information***

***Storm Information:***

|                 |              |
|-----------------|--------------|
| Storm Type:     | Type II-70   |
| Design Storm:   | 25 yr - 6 hr |
| Rainfall Depth: | 1.560 inches |

***Particle Size Distribution:***

| Size (mm) | PostMine-LoamySand | PreMine-LoamySand | PreMine-Badlands | LoamySand Postmining |
|-----------|--------------------|-------------------|------------------|----------------------|
| 2.0000    | 100.000%           | 100.000%          | 100.000%         | 0.000%               |
| 0.1000    | 26.500%            | 30.000%           | 83.500%          | 0.000%               |
| 0.0500    | 14.000%            | 17.000%           | 77.000%          | 0.000%               |
| 0.0020    | 11.000%            | 11.000%           | 56.000%          | 0.000%               |
| 0.0010    | 0.000%             | 0.000%            | 0.000%           | 0.000%               |

### ***Structure Summary:***

|     | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|-----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #30 | 476.400                                   | 476.400                               | 36.53                      | 4.76                                 | 37.8               | 8,241                               | 3.58                                  | 2.53           |
| #28 | 1,217.900                                 | 1,217.900                             | 540.05                     | 60.99                                | 3,425.4            | 57,102                              | 0.35                                  | 0.25           |
| #26 | 2,486.400                                 | 2,486.400                             | 132.85                     | 36.83                                | 246.5              | 6,616                               | 1.86                                  | 1.38           |
| #24 | 8,061.800                                 | 8,061.800                             | 184.75                     | 107.97                               | 413.0              | 4,459                               | 0.52                                  | 0.33           |
| #25 | 1,015.700                                 | 9,077.500                             | 200.88                     | 132.08                               | 560.2              | 15,558                              | 3.88                                  | 0.78           |
| #27 | 1,783.700                                 | 13,347.600                            | 411.67                     | 211.75                               | 1,872.8            | 29,782                              | 12.72                                 | 2.77           |
| #29 | 966.000                                   | 15,531.500                            | 846.18                     | 320.24                               | 8,834.4            | 71,508                              | 7.80                                  | 2.18           |
| #32 | 293.700                                   | 16,301.600                            | 861.61                     | 342.94                               | 9,448.4            | 63,077                              | 3.77                                  | 1.20           |
| #31 | 957.100                                   | 957.100                               | 527.85                     | 55.53                                | 2,515.1            | 41,599                              | 0.63                                  | 0.49           |
| #33 | 0.000                                     | 17,258.700                            | 979.82                     | 398.47                               | 11,963.5           | 54,725                              | 2.76                                  | 1.10           |
| #34 | 932.500                                   | 18,191.200                            | 992.63                     | 443.02                               | 11,159.6           | 45,924                              | 0.09                                  | 0.03           |
| #5  | 2,023.000                                 | 2,023.000                             | 837.11                     | 84.35                                | 2,651.8            | 41,867                              | 3.61                                  | 1.97           |
| #6  | 1,743.200                                 | 3,766.200                             | 956.02                     | 162.51                               | 4,790.3            | 36,533                              | 0.21                                  | 0.12           |
| #7  | 2,395.300                                 | 6,161.500                             | 1,580.25                   | 304.55                               | 12,734.9           | 46,225                              | 0.00                                  | 0.00           |
| #8  | 0.000                                     | 6,161.500                             | 1,580.25                   | 304.55                               | 12,734.9           | 46,225                              | 0.00                                  | 0.00           |
| #10 | 1,053.200                                 | 7,214.700                             | 1,604.48                   | 357.12                               | 12,452.2           | 42,273                              | 0.11                                  | 0.07           |
| #1  | 2,411.100                                 | 2,411.100                             | 588.72                     | 81.15                                | 2,757.0            | 37,715                              | 5.52                                  | 3.62           |
| #2  | 1,497.000                                 | 3,908.100                             | 655.37                     | 163.33                               | 3,619.6            | 24,206                              | 0.19                                  | 0.13           |
| #3  | 862.700                                   | 4,770.800                             | 829.77                     | 203.32                               | 4,035.6            | 18,997                              | 0.06                                  | 0.04           |
| #4  | 0.000                                     | 4,770.800                             | 829.77                     | 203.32                               | 4,035.6            | 18,997                              | 0.06                                  | 0.04           |
| #9  | 425.500                                   | 5,196.300                             | 849.71                     | 225.11                               | 4,042.0            | 16,916                              | 0.00                                  | 0.00           |
| #11 | 0.000                                     | 12,411.000                            | 2,175.32                   | 582.22                               | 16,494.3           | 34,910                              | 0.07                                  | 0.04           |
| #21 | 1,080.800                                 | 13,491.800                            | 2,220.17                   | 626.96                               | 16,455.3           | 33,282                              | 0.03                                  | 0.02           |
| #18 | 848.500                                   | 848.500                               | 268.00                     | 38.22                                | 496.6              | 15,750                              | 0.12                                  | 0.07           |
| #17 | 182.200                                   | 182.200                               | 174.08                     | 11.12                                | 167.2              | 15,582                              | 0.82                                  | 0.58           |
| #19 | 0.000                                     | 1,030.700                             | 409.10                     | 49.34                                | 663.8              | 14,808                              | 0.28                                  | 0.18           |
| #15 | 1,992.700                                 | 1,992.700                             | 627.55                     | 84.79                                | 3,281.0            | 46,290                              | 1.92                                  | 1.17           |
| #12 | 3,494.500                                 | 3,494.500                             | 397.28                     | 66.53                                | 1,024.9            | 16,872                              | 7.34                                  | 4.90           |
| #13 | 2,720.700                                 | 6,215.200                             | 697.21                     | 118.62                               | 2,079.9            | 18,344                              | 8.61                                  | 6.01           |
| #14 | 5,096.800                                 | 11,312.000                            | 857.46                     | 314.10                               | 7,172.5            | 83,385                              | 1.80                                  | 0.36           |
| #16 | 876.500                                   | 14,181.200                            | 1,254.01                   | 451.62                               | 12,480.7           | 57,021                              | 1.79                                  | 0.63           |
| #20 | 681.900                                   | 15,893.800                            | 1,290.99                   | 540.86                               | 13,372.2           | 43,852                              | 0.63                                  | 0.26           |
| #22 | 0.000                                     | 29,385.600                            | 3,356.18                   | 1,167.82                             | 29,827.5           | 35,065                              | 0.24                                  | 0.13           |
| #23 | 752.900                                   | 30,138.500                            | 3,323.41                   | 1,197.06                             | 29,527.9           | 34,065                              | 0.00                                  | 0.00           |
| #35 | 0.000                                     | 48,329.700                            | 4,127.57                   | 1,640.09                             | 40,687.5           | 31,691                              | 0.02                                  | 0.01           |
| #36 | 730.590                                   | 49,060.290                            | 4,106.02                   | 1,662.08                             | 40,745.8           | 37,462                              | 0.02                                  | 0.01           |
| #37 | 2,208.500                                 | 51,268.790                            | 4,049.05                   | 1,731.98                             | 40,586.1           | 32,624                              | 0.29                                  | 0.15           |



## ***Particle Size Distribution(s) at Each Structure***

### ***Structure #30:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 95.919%  |
| 0.0500    | 54.354%  |
| 0.0020    | 35.170%  |
| 0.0010    | 0.000%   |

### ***Structure #28:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.281%  |
| 0.0010    | 0.000%   |

### ***Structure #26:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 77.468%  |
| 0.0020    | 50.127%  |
| 0.0010    | 0.000%   |

### ***Structure #24:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 92.408%  |
| 0.0020    | 76.427%  |
| 0.0010    | 0.000%   |

**Structure #25:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 81.685%  |
| 0.0500    | 71.766%  |
| 0.0020    | 65.129%  |
| 0.0010    | 0.000%   |

**Structure #27:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 74.075%  |
| 0.0500    | 52.339%  |
| 0.0020    | 39.457%  |
| 0.0010    | 0.000%   |

**Structure #29:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 94.549%  |
| 0.0500    | 89.941%  |
| 0.0020    | 81.885%  |
| 0.0010    | 0.000%   |

**Structure #32:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 96.353%  |
| 0.0020    | 87.711%  |
| 0.0010    | 0.000%   |

**Structure #31:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 95.759%  |
| 0.0010    | 0.000%   |

**Structure #33 (Inlet to North Fork Diversion):**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 97.119%  |
| 0.0020    | 89.403%  |
| 0.0010    | 0.000%   |

**Structure #34:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.472%  |
| 0.0010    | 0.000%   |

**Structure #5:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 99.651%  |
| 0.0500    | 91.884%  |
| 0.0020    | 85.871%  |
| 0.0010    | 0.000%   |

**Structure #6:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.363%  |
| 0.0010    | 0.000%   |

**Structure #7:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |



**Structure #8:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #10:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.741%  |
| 0.0020    | 99.580%  |
| 0.0010    | 0.000%   |

**Structure #1:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 94.414%  |
| 0.0500    | 84.026%  |
| 0.0020    | 78.767%  |
| 0.0010    | 0.000%   |

**Structure #2:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 97.739%  |
| 0.0010    | 0.000%   |

**Structure #3:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.130%  |
| 0.0010    | 0.000%   |

**Structure #4:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.130%  |
| 0.0010    | 0.000%   |

**Structure #9:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #11:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.805%  |
| 0.0020    | 99.683%  |
| 0.0010    | 0.000%   |

**Structure #21:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.759%  |
| 0.0010    | 0.000%   |

**Structure #18:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 97.922%  |
| 0.0010    | 0.000%   |

**Structure #17:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 85.172%  |
| 0.0010    | 0.000%   |

**Structure #19:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 94.709%  |
| 0.0010    | 0.000%   |

**Structure #15:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 96.507%  |
| 0.0020    | 92.676%  |
| 0.0010    | 0.000%   |

**Structure #12:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 80.910%  |
| 0.0500    | 54.212%  |
| 0.0020    | 35.079%  |
| 0.0010    | 0.000%   |

**Structure #13:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 78.331%  |
| 0.0500    | 49.080%  |
| 0.0020    | 31.758%  |
| 0.0010    | 0.000%   |



**Structure #14:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 93.915%  |
| 0.0010    | 0.000%   |

**Structure #16:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.094%  |
| 0.0020    | 92.311%  |
| 0.0010    | 0.000%   |

**Structure #20:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 95.936%  |
| 0.0010    | 0.000%   |

**Structure #22:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.045%  |
| 0.0010    | 0.000%   |

**Structure #23:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #35:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.855%  |
| 0.0010    | 0.000%   |

**Structure #36:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.838%  |
| 0.0010    | 0.000%   |

**Structure #37:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.126%  |
| 0.0020    | 98.596%  |
| 0.0010    | 0.000%   |

### *Subwatershed Hydrology Detail:*

| Stru #     | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|------------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #30        | 1        | 476.400           | 1.131              | 0.000        | 0.000  | 73.100       | M   | 36.53                | 4.764                 |
|            | <b>Σ</b> | <b>476.400</b>    |                    |              |        |              |     | <b>36.53</b>         | <b>4.764</b>          |
| #28        | 1        | 772.300           | 0.657              | 0.523        | 0.334  | 90.400       | M   | 491.68               | 38.669                |
|            | 2        | 445.600           | 0.587              | 0.000        | 0.000  | 90.400       | M   | 305.95               | 22.321                |
|            | <b>Σ</b> | <b>1,217.900</b>  |                    |              |        |              |     | <b>540.05</b>        | <b>60.991</b>         |
| #26        | 1        | 447.600           | 2.192              | 0.000        | 0.000  | 74.200       | M   | 23.11                | 5.111                 |
|            | 2        | 2,038.800         | 3.000              | 0.000        | 0.000  | 77.000       | M   | 112.68               | 31.721                |
|            | <b>Σ</b> | <b>2,486.400</b>  |                    |              |        |              |     | <b>132.85</b>        | <b>36.832</b>         |
| #24        | 1        | 2,607.500         | 5.367              | 2.377        | 0.305  | 75.200       | M   | 71.74                | 33.393                |
|            | 2        | 2,331.900         | 4.813              | 2.431        | 0.304  | 74.700       | M   | 66.31                | 28.216                |
|            | 3        | 1,758.500         | 2.231              | 1.788        | 0.297  | 76.200       | M   | 113.95               | 25.140                |
|            | 4        | 1,363.900         | 2.618              | 0.000        | 0.000  | 77.000       | M   | 84.58                | 21.220                |
|            | <b>Σ</b> | <b>8,061.800</b>  |                    |              |        |              |     | <b>184.75</b>        | <b>107.969</b>        |
| #25        | 1        | 515.200           | 0.990              | 0.342        | 0.357  | 78.200       | M   | 81.39                | 9.063                 |
|            | 2        | 130.500           | 0.787              | 0.342        | 0.357  | 78.100       | M   | 24.40                | 2.273                 |
|            | 3        | 370.000           | 0.516              | 0.000        | 0.000  | 85.700       | M   | 190.15               | 12.775                |
|            | <b>Σ</b> | <b>9,077.500</b>  |                    |              |        |              |     | <b>200.88</b>        | <b>132.080</b>        |
| #27        | 1        | 354.400           | 0.612              | 1.233        | 0.337  | 83.100       | M   | 129.85               | 9.820                 |
|            | 2        | 305.200           | 0.529              | 1.054        | 0.328  | 84.000       | M   | 133.52               | 9.142                 |
|            | 3        | 289.800           | 0.692              | 0.551        | 0.328  | 75.500       | M   | 44.45                | 3.841                 |
|            | 4        | 253.000           | 0.361              | 0.551        | 0.328  | 79.400       | M   | 93.60                | 5.022                 |
|            | 5        | 581.300           | 0.980              | 0.000        | 0.000  | 82.300       | M   | 139.19               | 15.009                |
|            | <b>Σ</b> | <b>13,347.600</b> |                    |              |        |              |     | <b>411.67</b>        | <b>211.747</b>        |
| #29        | 1        | 508.800           | 0.409              | 0.416        | 0.312  | 89.500       | M   | 404.67               | 23.823                |
|            | 2        | 233.200           | 0.521              | 0.291        | 0.312  | 91.600       | M   | 188.69               | 12.806                |
|            | 3        | 224.000           | 0.467              | 0.000        | 0.000  | 90.000       | M   | 171.82               | 10.877                |
|            | <b>Σ</b> | <b>15,531.500</b> |                    |              |        |              |     | <b>846.18</b>        | <b>320.244</b>        |
| #32        | 1        | 293.700           | 0.576              | 0.000        | 0.000  | 93.000       | M   | 247.25               | 17.930                |
|            | <b>Σ</b> | <b>16,301.600</b> |                    |              |        |              |     | <b>861.61</b>        | <b>342.938</b>        |
| #31        | 1        | 431.100           | 0.588              | 0.450        | 0.336  | 91.500       | M   | 321.18               | 23.493                |
|            | 2        | 325.800           | 0.432              | 0.149        | 0.327  | 93.000       | M   | 322.14               | 19.913                |
|            | 3        | 200.200           | 0.373              | 0.000        | 0.000  | 92.900       | M   | 210.22               | 12.124                |
|            | <b>Σ</b> | <b>957.100</b>    |                    |              |        |              |     | <b>527.85</b>        | <b>55.530</b>         |
| <b>#33</b> | <b>Σ</b> | <b>17,258.700</b> |                    |              |        |              |     | <b>979.82</b>        | <b>398.468</b>        |



| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS  | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|------|----------------------|-----------------------|
| #34    | 1        | 91.700            | 0.244              | 0.965        | 0.300  | 92.300       | M    | 108.45               | 5.351                 |
|        | 2        | 105.200           | 0.256              | 0.965        | 0.300  | 93.000       | M    | 127.71               | 6.456                 |
|        | 3        | 735.600           | 0.885              | 0.000        | 0.000  | 88.900       | M    | 335.17               | 32.747                |
|        | <b>Σ</b> | <b>18,191.200</b> |                    |              |        |              |      | <b>992.63</b>        | <b>443.022</b>        |
| #5     | 1        | 503.600           | 0.618              | 0.000        | 0.000  | 87.600       | M    | 268.07               | 20.239                |
|        | 2        | 406.500           | 0.388              | 0.501        | 0.350  | 84.800       | M    | 230.58               | 13.021                |
|        | 3        | 439.600           | 0.342              | 0.681        | 0.347  | 87.800       | M    | 336.99               | 18.042                |
|        | 4        | 162.600           | 0.280              | 0.681        | 0.347  | 86.000       | M    | 118.70               | 5.772                 |
|        | 5        | 294.100           | 0.375              | 1.021        | 0.348  | 92.000       | M    | 290.40               | 16.627                |
|        | 6        | 216.600           | 0.272              | 1.018        | 0.348  | 90.100       | M    | 214.22               | 10.646                |
|        | <b>Σ</b> | <b>2,023.000</b>  |                    |              |        |              |      | <b>837.11</b>        | <b>84.347</b>         |
| #6     | 1        | 149.100           | 0.331              | 0.000        | 0.000  | 92.600       | M    | 161.30               | 8.862                 |
|        | 2        | 245.000           | 0.529              | 0.192        | 0.328  | 88.100       | M    | 150.59               | 10.257                |
|        | 3        | 276.200           | 0.450              | 0.461        | 0.319  | 89.500       | M    | 208.50               | 12.896                |
|        | 4        | 158.400           | 0.380              | 1.385        | 0.185  | 93.000       | M    | 166.02               | 9.660                 |
|        | 5        | 206.200           | 0.402              | 0.796        | 0.320  | 89.400       | M    | 164.26               | 9.578                 |
|        | 6        | 414.000           | 0.430              | 1.066        | 0.323  | 87.200       | M    | 269.04               | 16.158                |
|        | 7        | 294.300           | 0.535              | 1.066        | 0.323  | 86.400       | M    | 156.53               | 10.750                |
|        | <b>Σ</b> | <b>3,766.200</b>  |                    |              |        |              |      | <b>956.02</b>        | <b>162.509</b>        |
| #7     | 1        | 731.700           | 1.274              | 0.000        | 0.000  | 93.000       | M    | 346.80               | 44.600                |
|        | 2        | 445.800           | 1.043              | 0.000        | 0.000  | 93.000       | M    | 247.27               | 27.164                |
|        | 3        | 270.800           | 0.804              | 0.000        | 0.000  | 93.000       | M    | 182.24               | 16.506                |
|        | 4        | 78.900            | 0.267              | 1.035        | 0.328  | 93.000       | M    | 94.49                | 4.837                 |
|        | 5        | 154.900           | 0.310              | 1.071        | 0.326  | 93.000       | M    | 176.25               | 9.484                 |
|        | 6        | 101.400           | 0.288              | 1.164        | 0.328  | 92.900       | M    | 117.81               | 6.157                 |
|        | 7        | 117.700           | 0.298              | 1.344        | 0.329  | 92.200       | M    | 129.29               | 6.777                 |
|        | 8        | 494.100           | 0.518              | 1.344        | 0.329  | 91.300       | M    | 392.49               | 26.519                |
|        | <b>Σ</b> | <b>6,161.500</b>  |                    |              |        |              |      | <b>1,580.25</b>      | <b>304.553</b>        |
| #8     | 1        | 0.000             | 0.000              | 0.000        | 0.000  | 1.000        | 0.00 | 0.000                |                       |
|        | <b>Σ</b> | <b>6,161.500</b>  |                    |              |        |              |      | <b>1,580.25</b>      | <b>304.553</b>        |
| #10    | 1        | 355.500           | 1.286              | 0.000        | 0.000  | 93.000       | M    | 167.23               | 21.664                |
|        | 2        | 307.100           | 1.282              | 0.668        | 0.305  | 83.200       | M    | 64.37                | 8.575                 |
|        | 3        | 147.300           | 1.245              | 0.517        | 0.303  | 90.600       | M    | 58.93                | 7.480                 |
|        | 4        | 126.400           | 0.585              | 0.517        | 0.303  | 93.000       | M    | 105.39               | 7.719                 |
|        | 5        | 116.900           | 1.179              | 0.621        | 0.305  | 93.000       | M    | 58.93                | 7.126                 |
|        | <b>Σ</b> | <b>7,214.700</b>  |                    |              |        |              |      | <b>1,604.48</b>      | <b>357.116</b>        |
| #1     | 1        | 557.400           | 0.941              | 0.000        | 0.000  | 83.600       | M    | 155.00               | 16.115                |
|        | 2        | 169.600           | 1.616              | 0.677        | 0.333  | 93.000       | M    | 66.17                | 10.336                |
|        | 3        | 636.400           | 1.842              | 0.729        | 0.333  | 81.000       | M    | 80.29                | 14.616                |
|        | 4        | 223.400           | 0.846              | 1.005        | 0.336  | 84.100       | M    | 70.44                | 6.742                 |

| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS   | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|-------|----------------------|-----------------------|
|        | 5        | 77.700            | 0.330              | 1.392        | 0.341  | 81.400       | M     | 36.23                | 1.860                 |
|        | 6        | 746.600           | 0.678              | 1.392        | 0.341  | 88.200       | M     | 391.01               | 31.484                |
|        | <b>Σ</b> | <b>2,411.100</b>  |                    |              |        |              |       | <b>588.72</b>        | <b>81.153</b>         |
| #2     | 1        | 257.000           | 0.423              | 0.000        | 0.000  | 93.000       | M     | 256.73               | 15.720                |
|        | 2        | 180.500           | 0.562              | 0.478        | 0.281  | 91.800       | M     | 141.48               | 10.054                |
|        | 3        | 200.700           | 0.687              | 0.574        | 0.283  | 93.000       | M     | 150.71               | 12.240                |
|        | 4        | 438.600           | 0.811              | 0.574        | 0.283  | 93.000       | M     | 293.34               | 26.741                |
|        | 5        | 420.200           | 1.247              | 0.801        | 0.293  | 88.000       | M     | 135.94               | 17.427                |
|        | <b>Σ</b> | <b>3,908.100</b>  |                    |              |        |              |       | <b>655.37</b>        | <b>163.335</b>        |
| #3     | 1        | 172.600           | 0.443              | 0.000        | 0.000  | 93.000       | M     | 168.52               | 10.532                |
|        | 2        | 311.200           | 0.890              | 0.000        | 0.000  | 88.900       | M     | 141.19               | 13.857                |
|        | 3        | 378.900           | 0.632              | 0.209        | 0.314  | 87.900       | M     | 203.46               | 15.593                |
|        | <b>Σ</b> | <b>4,770.800</b>  |                    |              |        |              |       | <b>829.77</b>        | <b>203.316</b>        |
| #4     | <b>Σ</b> | <b>4,770.800</b>  |                    |              |        |              |       | <b>829.77</b>        | <b>203.316</b>        |
| #9     | 1        | 425.500           | 0.830              | 0.000        | 0.000  | 90.700       | M     | 234.68               | 21.789                |
|        | <b>Σ</b> | <b>5,196.300</b>  |                    |              |        |              |       | <b>849.71</b>        | <b>225.105</b>        |
| #11    | <b>Σ</b> | <b>12,411.000</b> |                    |              |        |              |       | <b>2,175.32</b>      | <b>582.221</b>        |
| #21    | 1        | 272.800           | 0.819              | 0.000        | 0.000  | 86.900       | M     | 111.80               | 10.369                |
|        | 2        | 230.500           | 0.388              | 0.694        | 0.266  | 89.200       | M     | 184.23               | 10.517                |
|        | 3        | 181.100           | 0.289              | 0.877        | 0.256  | 91.300       | M     | 189.85               | 9.736                 |
|        | 4        | 396.400           | 0.939              | 0.877        | 0.256  | 86.100       | M     | 136.92               | 14.118                |
|        | <b>Σ</b> | <b>13,491.800</b> |                    |              |        |              |       | <b>2,220.17</b>      | <b>626.962</b>        |
| #18    | 1        | 301.700           | 0.652              | 0.000        | 0.000  | 93.000       | M     | 234.61               | 18.415                |
|        | 2        | 546.800           | 0.768              | 0.561        | 0.320  | 86.300       | M     | 223.53               | 19.804                |
|        | <b>Σ</b> | <b>848.500</b>    |                    |              |        |              |       | <b>268.00</b>        | <b>38.220</b>         |
| #17    | 1        | 182.200           | 0.462              | 0.000        | 0.000  | 93.000       | M     | 174.08               | 11.118                |
|        | <b>Σ</b> | <b>182.200</b>    |                    |              |        |              |       | <b>174.08</b>        | <b>11.118</b>         |
| #19    | <b>Σ</b> | <b>1,030.700</b>  |                    |              |        |              |       | <b>409.10</b>        | <b>49.338</b>         |
| #15    | 1        | 437.400           | 0.803              | 0.000        | 0.000  | 91.300       | M     | 258.94               | 23.432                |
|        | 2        | 549.000           | 0.637              | 0.654        | 0.327  | 91.300       | M     | 382.26               | 29.427                |
|        | 3        | 1,006.300         | 1.023              | 0.768        | 0.331  | 84.700       | M     | 288.75               | 31.930                |
|        | <b>Σ</b> | <b>1,992.700</b>  |                    |              |        |              |       | <b>627.55</b>        | <b>84.789</b>         |
| #12    | 1        | 517.800           | 0.791              | 0.000        | 0.000  | 81.900       | M     | 140.91               | 12.902                |
|        | 2        | 229.000           | 0.571              | 0.043        | 0.418  | 80.100       | M     | 66.83                | 4.847                 |
|        | 3        | 592.700           | 0.706              | 0.044        | 0.417  | 81.500       | M     | 169.25               | 14.252                |
|        | 4        | 1,806.900         | 1.542              | 0.487        | 0.362  | 76.700       | M     | 168.42               | 27.242                |
|        | 5        | 348.100           | 0.618              | 0.487        | 0.362  | 80.000       | 94.98 | 7.291                |                       |

| Stru #   | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|----------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| <b>Σ</b> |          | <b>3,494.500</b>  |                    |              |        |              |     | <b>397.28</b>        | <b>66.533</b>         |
| #13      | 1        | 411.600           | 0.725              | 0.000        | 0.000  | 79.700       | M   | 96.79                | 8.384                 |
|          | 2        | 636.400           | 0.774              | 0.322        | 0.336  | 80.700       | M   | 157.14               | 14.233                |
|          | 3        | 319.000           | 0.575              | 0.685        | 0.318  | 85.500       | M   | 149.91               | 10.830                |
|          | 4        | 231.700           | 0.314              | 0.923        | 0.328  | 80.400       | M   | 101.73               | 5.057                 |
|          | 5        | 1,122.000         | 1.308              | 0.923        | 0.328  | 74.700       | M   | 94.33                | 13.581                |
| <b>Σ</b> |          | <b>6,215.200</b>  |                    |              |        |              |     | <b>697.21</b>        | <b>118.618</b>        |
| #14      | 1        | 405.900           | 0.384              | 0.000        | 0.000  | 90.800       | M   | 365.33               | 20.943                |
|          | 2        | 411.100           | 0.452              | 0.707        | 0.308  | 90.700       | M   | 338.08               | 21.056                |
|          | 3        | 787.400           | 0.658              | 0.975        | 0.307  | 91.400       | M   | 540.50               | 42.565                |
|          | 4        | 144.200           | 0.341              | 1.716        | 0.310  | 86.200       | M   | 98.01                | 5.205                 |
|          | 5        | 343.800           | 0.289              | 1.970        | 0.312  | 86.500       | M   | 257.38               | 12.690                |
|          | 6        | 392.800           | 0.806              | 2.107        | 0.316  | 81.900       | M   | 105.39               | 9.788                 |
|          | 7        | 528.200           | 0.518              | 2.544        | 0.316  | 87.200       | M   | 306.31               | 20.592                |
|          | 8        | 890.900           | 1.253              | 2.544        | 0.316  | 83.500       | M   | 195.49               | 25.534                |
|          | 9        | 741.400           | 1.076              | 3.047        | 0.316  | 84.800       | M   | 206.21               | 23.723                |
|          | 10       | 451.100           | 0.916              | 3.354        | 0.316  | 83.900       | M   | 131.53               | 13.383                |
| <b>Σ</b> |          | <b>11,312.000</b> |                    |              |        |              |     | <b>857.46</b>        | <b>314.097</b>        |
| #16      | 1        | 329.600           | 0.641              | 0.000        | 0.000  | 93.000       | M   | 259.17               | 20.109                |
|          | 2        | 348.400           | 0.542              | 0.509        | 0.286  | 92.500       | M   | 293.69               | 20.454                |
|          | 3        | 198.500           | 0.266              | 0.943        | 0.279  | 93.000       | M   | 237.98               | 12.169                |
| <b>Σ</b> |          | <b>14,181.200</b> |                    |              |        |              |     | <b>1,254.01</b>      | <b>451.619</b>        |
| #20      | 1        | 296.300           | 0.667              | 0.000        | 0.000  | 91.700       | M   | 206.13               | 16.387                |
|          | 2        | 385.600           | 0.713              | 0.476        | 0.440  | 93.000       | M   | 282.30               | 23.513                |
| <b>Σ</b> |          | <b>15,893.800</b> |                    |              |        |              |     | <b>1,290.99</b>      | <b>540.857</b>        |
| #22      | <b>Σ</b> | <b>29,385.600</b> |                    |              |        |              |     | <b>3,356.18</b>      | <b>1,167.818</b>      |
| #23      | 1        | 442.400           | 0.960              | 0.000        | 0.000  | 85.300       | M   | 140.43               | 14.750                |
|          | 2        | 310.500           | 0.538              | 0.559        | 0.291  | 89.500       | M   | 210.50               | 14.496                |
| <b>Σ</b> |          | <b>30,138.500</b> |                    |              |        |              |     | <b>3,323.41</b>      | <b>1,197.064</b>      |
| #35      | <b>Σ</b> | <b>48,329.700</b> |                    |              |        |              |     | <b>4,127.57</b>      | <b>1,640.087</b>      |
| #36      | 1        | 298.200           | 0.987              | 0.000        | 0.000  | 85.000       | M   | 90.30                | 9.700                 |
|          | 2        | 196.800           | 0.441              | 0.000        | 0.000  | 87.900       | M   | 133.11               | 8.109                 |
|          | 3        | 235.590           | 0.885              | 0.166        | 0.372  | 78.300       | M   | 41.09                | 4.186                 |
| <b>Σ</b> |          | <b>49,060.290</b> |                    |              |        |              |     | <b>4,106.02</b>      | <b>1,662.082</b>      |
| #37      | 1        | 744.000           | 1.756              | 0.000        | 0.000  | 84.800       | M   | 138.50               | 23.796                |
|          | 2        | 296.000           | 0.439              | 1.780        | 0.243  | 87.800       | M   | 199.18               | 12.104                |
|          | 3        | 237.700           | 0.333              | 1.649        | 0.246  | 85.500       | M   | 154.65               | 8.100                 |
|          | 4        | 561.400           | 1.502              | 1.780        | 0.243  | 84.100       | M   | 111.96               | 16.932                |



| Stru #   | SWS # | SWS Area (ac) | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |                  |
|----------|-------|---------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|------------------|
|          | 5     | 369.400       | 0.817              | 2.236        | 0.284  | 81.600       | M   | 95.38                | 8.964                 |                  |
| <b>Σ</b> |       |               |                    |              |        |              |     | <b>51,268.790</b>    | <b>4,049.05</b>       | <b>1,731.978</b> |

***Subwatershed Sedimentology Detail:***

| Stru #   | SWS # | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|----------|-------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #30      | 1     | 0.095  | 200.00 | 3.80  | 0.3720 | 1.0000 | 2    | 37.8            | 8,241                      | 3.58                        | 2.53        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>37.8</b>     | <b>8,241</b>               | <b>3.58</b>                 | <b>2.53</b> |
| #28      | 1     | 0.187  | 100.00 | 10.10 | 0.3750 | 1.0000 | 3    | 2,689.8         | 70,014                     | 0.00                        | 0.00        |
|          | 2     | 0.196  | 100.00 | 10.20 | 0.3930 | 1.0000 | 3    | 1,688.7         | 76,821                     | 0.95                        | 0.67        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>3,425.4</b>  | <b>57,102</b>              | <b>0.35</b>                 | <b>0.25</b> |
| #26      | 1     | 0.155  | 400.00 | 1.40  | 0.3480 | 1.0000 | 2    | 23.5            | 4,623                      | 1.48                        | 1.08        |
|          | 2     | 0.155  | 300.00 | 2.40  | 0.3340 | 1.0000 | 2    | 223.0           | 7,027                      | 1.94                        | 1.43        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>246.5</b>    | <b>6,616</b>               | <b>1.86</b>                 | <b>1.38</b> |
| #24      | 1     | 0.128  | 300.00 | 2.30  | 0.3360 | 1.0000 | 2    | 142.6           | 4,234                      | 0.49                        | 0.37        |
|          | 2     | 0.136  | 300.00 | 2.70  | 0.3440 | 1.0000 | 2    | 156.0           | 5,467                      | 0.69                        | 0.51        |
|          | 3     | 0.107  | 300.00 | 2.30  | 0.3330 | 1.0000 | 2    | 130.5           | 5,163                      | 1.74                        | 1.28        |
|          | 4     | 0.163  | 400.00 | 1.60  | 0.3210 | 1.0000 | 2    | 117.0           | 5,534                      | 1.71                        | 1.25        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>413.0</b>    | <b>4,459</b>               | <b>0.52</b>                 | <b>0.33</b> |
| #25      | 1     | 0.125  | 400.00 | 1.90  | 0.3440 | 1.0000 | 2    | 67.8            | 7,753                      | 3.82                        | 2.71        |
|          | 2     | 0.124  | 300.00 | 2.60  | 0.3280 | 1.0000 | 2    | 18.3            | 8,435                      | 4.40                        | 3.07        |
|          | 3     | 0.122  | 175.00 | 4.90  | 0.2660 | 1.0000 | 2    | 220.7           | 18,283                     | 10.89                       | 7.52        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>560.2</b>    | <b>15,558</b>              | <b>3.88</b>                 | <b>0.78</b> |
| #27      | 1     | 0.127  | 175.00 | 5.90  | 0.3160 | 1.0000 | 2    | 227.1           | 23,856                     | 13.64                       | 9.65        |
|          | 2     | 0.122  | 150.00 | 7.50  | 0.2920 | 1.0000 | 2    | 229.0           | 25,945                     | 15.24                       | 10.73       |
|          | 3     | 0.070  | 125.00 | 8.40  | 0.3270 | 1.0000 | 2    | 51.3            | 14,063                     | 7.33                        | 5.09        |
|          | 4     | 0.097  | 125.00 | 9.60  | 0.3170 | 1.0000 | 2    | 149.1           | 31,802                     | 19.09                       | 12.97       |
|          | 5     | 0.126  | 125.00 | 8.90  | 0.3290 | 1.0000 | 2    | 413.8           | 28,401                     | 14.71                       | 10.41       |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>1,872.8</b>  | <b>29,782</b>              | <b>12.72</b>                | <b>2.77</b> |
| #29      | 1     | 0.190  | 125.00 | 9.80  | 0.3930 | 1.0000 | 3    | 2,025.8         | 86,051                     | 4.01                        | 2.83        |
|          | 2     | 0.203  | 125.00 | 8.90  | 0.3940 | 1.0000 | 3    | 865.3           | 68,289                     | 2.28                        | 1.62        |
|          | 3     | 0.193  | 125.00 | 8.40  | 0.3940 | 1.0000 | 3    | 650.4           | 61,594                     | 2.23                        | 1.56        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>8,834.4</b>  | <b>71,508</b>              | <b>7.80</b>                 | <b>2.18</b> |
| #32      | 1     | 0.210  | 150.00 | 7.70  | 0.3990 | 1.0000 | 3    | 1,137.5         | 64,212                     | 1.95                        | 1.39        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>9,448.4</b>  | <b>63,077</b>              | <b>3.77</b>                 | <b>1.20</b> |

| Stru #     | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|------------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #31        | 1        | 0.204  | 125.00 | 8.70  | 0.3620 | 1.0000 | 3    | 1,459.0         | 62,828                     | 1.19                        | 0.85        |
|            | 2        | 0.210  | 150.00 | 7.30  | 0.3990 | 1.0000 | 3    | 1,328.3         | 67,409                     | 3.95                        | 2.81        |
|            | 3        | 0.210  | 175.00 | 4.50  | 0.3980 | 1.0000 | 3    | 539.2           | 45,502                     | 3.16                        | 2.24        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>2,515.1</b>  | <b>41,599</b>              | <b>0.63</b>                 | <b>0.49</b> |
| <b>#33</b> | <b>Σ</b> |        |        |       |        |        |      | <b>11,963.5</b> | <b>54,725</b>              | <b>2.76</b>                 | <b>1.10</b> |
| #34        | 1        | 0.189  | 175.00 | 4.60  | 0.2250 | 1.0000 | 3    | 121.7           | 22,791                     | 2.13                        | 1.55        |
|            | 2        | 0.206  | 175.00 | 5.10  | 0.3620 | 1.0000 | 3    | 286.9           | 44,058                     | 4.10                        | 3.00        |
|            | 3        | 0.176  | 175.00 | 4.20  | 0.2510 | 1.0000 | 3    | 605.3           | 18,983                     | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>11,159.6</b> | <b>45,924</b>              | <b>0.09</b>                 | <b>0.03</b> |
| #5         | 1        | 0.149  | 75.00  | 12.50 | 0.3230 | 1.0000 | 3    | 1,034.7         | 52,699                     | 0.00                        | 0.00        |
|            | 2        | 0.133  | 75.00  | 15.80 | 0.3190 | 1.0000 | 2    | 882.3           | 70,193                     | 42.92                       | 29.78       |
|            | 3        | 0.103  | 100.00 | 11.00 | 0.2030 | 1.0000 | 3    | 477.2           | 27,418                     | 1.49                        | 1.04        |
|            | 4        | 0.093  | 75.00  | 13.80 | 0.2130 | 1.0000 | 2    | 151.7           | 27,429                     | 17.29                       | 12.07       |
|            | 5        | 0.123  | 100.00 | 11.00 | 0.1370 | 1.0000 | 3    | 338.9           | 20,783                     | 1.35                        | 0.97        |
|            | 6        | 0.149  | 75.00  | 14.70 | 0.1990 | 1.0000 | 3    | 482.1           | 45,729                     | 3.62                        | 2.59        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>2,651.8</b>  | <b>41,867</b>              | <b>3.61</b>                 | <b>1.97</b> |
| #6         | 1        | 0.208  | 175.00 | 4.30  | 0.3980 | 1.0000 | 3    | 369.3           | 42,677                     | 3.27                        | 2.31        |
|            | 2        | 0.183  | 175.00 | 5.40  | 0.3910 | 1.0000 | 3    | 414.2           | 41,856                     | 0.48                        | 0.34        |
|            | 3        | 0.188  | 150.00 | 7.60  | 0.3900 | 1.0000 | 3    | 743.1           | 58,940                     | 2.20                        | 1.55        |
|            | 4        | 0.210  | 150.00 | 6.30  | 0.3990 | 1.0000 | 3    | 531.4           | 53,736                     | 3.69                        | 2.72        |
|            | 5        | 0.185  | 125.00 | 8.10  | 0.3860 | 1.0000 | 3    | 522.2           | 55,347                     | 2.64                        | 1.88        |
|            | 6        | 0.104  | 100.00 | 11.30 | 0.2240 | 1.0000 | 3    | 458.0           | 29,084                     | 0.88                        | 0.62        |
|            | 7        | 0.164  | 100.00 | 11.20 | 0.3740 | 1.0000 | 3    | 700.8           | 65,996                     | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>4,790.3</b>  | <b>36,533</b>              | <b>0.21</b>                 | <b>0.12</b> |
| #7         | 1        | 0.208  | 150.00 | 7.80  | 0.3780 | 1.0000 | 3    | 2,177.7         | 48,781                     | 0.00                        | 0.00        |
|            | 2        | 0.209  | 100.00 | 10.20 | 0.3940 | 1.0000 | 3    | 1,790.8         | 65,658                     | 0.00                        | 0.00        |
|            | 3        | 0.210  | 150.00 | 6.70  | 0.3990 | 1.0000 | 3    | 801.8           | 49,036                     | 0.00                        | 0.00        |
|            | 4        | 0.210  | 100.00 | 11.50 | 0.3990 | 1.0000 | 3    | 477.3           | 96,068                     | 8.73                        | 6.38        |
|            | 5        | 0.210  | 150.00 | 7.10  | 0.3990 | 1.0000 | 3    | 608.5           | 63,520                     | 5.23                        | 3.80        |
|            | 6        | 0.209  | 150.00 | 7.90  | 0.3990 | 1.0000 | 3    | 420.5           | 67,295                     | 5.82                        | 4.25        |
|            | 7        | 0.206  | 75.00  | 15.50 | 0.3990 | 1.0000 | 3    | 836.5           | 118,836                    | 9.71                        | 7.12        |
|            | 8        | 0.202  | 75.00  | 14.50 | 0.3980 | 1.0000 | 3    | 3,013.5         | 111,222                    | 3.59                        | 2.60        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>12,734.9</b> | <b>46,225</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #8         | 1        | 0.000  | 0.00   | 0.00  | 0.0000 | 1.0000 | 0    | 0.0             | 1                          | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>12,734.9</b> | <b>46,225</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #10        | 1        | 0.190  | 300.00 | 2.70  | 0.1930 | 1.0000 | 3    | 177.0           | 8,298                      | 0.00                        | 0.00        |
|            | 2        | 0.153  | 200.00 | 3.50  | 0.3610 | 1.0000 | 2    | 104.5           | 12,354                     | 6.02                        | 4.35        |
|            | 3        | 0.189  | 200.00 | 3.70  | 0.3190 | 1.0000 | 3    | 105.9           | 14,296                     | 0.00                        | 0.00        |
|            | 4        | 0.190  | 300.00 | 2.10  | 0.1940 | 1.0000 | 3    | 61.5            | 8,188                      | 0.23                        | 0.17        |

| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 5        | 0.201  | 300.00 | 2.00  | 0.3030 | 1.0000 | 3    | 67.2            | 9,536                      | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>12,452.2</b> | <b>42,273</b>              | <b>0.11</b>                 | <b>0.07</b> |
| #1     | 1        | 0.157  | 150.00 | 6.80  | 0.3830 | 1.0000 | 2    | 525.9           | 33,536                     | 17.76                       | 12.57       |
|        | 2        | 0.210  | 150.00 | 6.60  | 0.3990 | 1.0000 | 3    | 344.9           | 33,236                     | 0.00                        | 0.00        |
|        | 3        | 0.149  | 200.00 | 3.90  | 0.3870 | 1.0000 | 2    | 184.0           | 12,655                     | 5.25                        | 3.82        |
|        | 4        | 0.169  | 175.00 | 4.70  | 0.3950 | 1.0000 | 2    | 175.1           | 26,524                     | 14.42                       | 10.30       |
|        | 5        | 0.157  | 100.00 | 10.10 | 0.3940 | 1.0000 | 2    | 100.5           | 55,458                     | 33.92                       | 23.86       |
|        | 6        | 0.175  | 75.00  | 12.60 | 0.2840 | 1.0000 | 3    | 1,708.1         | 54,643                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>2,757.0</b>  | <b>37,715</b>              | <b>5.52</b>                 | <b>3.62</b> |
| #2     | 1        | 0.190  | 150.00 | 7.90  | 0.1930 | 1.0000 | 3    | 483.6           | 31,655                     | 1.91                        | 1.35        |
|        | 2        | 0.184  | 175.00 | 4.80  | 0.2010 | 1.0000 | 3    | 182.9           | 18,684                     | 0.49                        | 0.35        |
|        | 3        | 0.202  | 200.00 | 3.90  | 0.3220 | 1.0000 | 3    | 267.3           | 22,234                     | 0.20                        | 0.14        |
|        | 4        | 0.203  | 150.00 | 7.40  | 0.3220 | 1.0000 | 3    | 1,176.7         | 44,218                     | 0.00                        | 0.00        |
|        | 5        | 0.181  | 175.00 | 5.10  | 0.3710 | 1.0000 | 3    | 468.2           | 26,988                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>3,619.6</b>  | <b>24,206</b>              | <b>0.19</b>                 | <b>0.13</b> |
| #3     | 1        | 0.190  | 175.00 | 5.20  | 0.1930 | 1.0000 | 3    | 221.4           | 21,734                     | 1.23                        | 0.87        |
|        | 2        | 0.177  | 175.00 | 4.20  | 0.2560 | 1.0000 | 3    | 236.3           | 17,524                     | 0.00                        | 0.00        |
|        | 3        | 0.166  | 175.00 | 4.30  | 0.2290 | 1.0000 | 3    | 265.7           | 17,717                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>4,035.6</b>  | <b>18,997</b>              | <b>0.06</b>                 | <b>0.04</b> |
| #4     | <b>Σ</b> |        |        |       |        |        |      | <b>4,035.6</b>  | <b>18,997</b>              | <b>0.06</b>                 | <b>0.04</b> |
| #9     | 1        | 0.189  | 175.00 | 4.44  | 0.1970 | 1.0000 | 3    | 350.3           | 16,517                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>4,042.0</b>  | <b>16,916</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #11    | <b>Σ</b> |        |        |       |        |        |      | <b>16,494.3</b> | <b>34,910</b>              | <b>0.07</b>                 | <b>0.04</b> |
| #21    | 1        | 0.177  | 175.00 | 4.44  | 0.2560 | 1.0000 | 3    | 185.7           | 18,511                     | 0.00                        | 0.00        |
|        | 2        | 0.184  | 175.00 | 5.81  | 0.2210 | 1.0000 | 3    | 286.5           | 27,896                     | 1.39                        | 0.99        |
|        | 3        | 0.185  | 300.00 | 2.70  | 0.2180 | 1.0000 | 3    | 133.3           | 13,847                     | 1.11                        | 0.80        |
|        | 4        | 0.175  | 300.00 | 2.66  | 0.2690 | 1.0000 | 3    | 157.7           | 11,371                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>16,455.3</b> | <b>33,282</b>              | <b>0.03</b>                 | <b>0.02</b> |
| #18    | 1        | 0.193  | 300.00 | 2.80  | 0.2200 | 1.0000 | 3    | 233.6           | 13,072                     | 0.20                        | 0.15        |
|        | 2        | 0.173  | 175.00 | 4.70  | 0.3880 | 1.0000 | 3    | 614.7           | 31,763                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>496.6</b>    | <b>15,750</b>              | <b>0.12</b>                 | <b>0.07</b> |
| #17    | 1        | 0.196  | 300.00 | 2.60  | 0.2600 | 1.0000 | 3    | 167.2           | 15,582                     | 0.82                        | 0.58        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>167.2</b>    | <b>15,582</b>              | <b>0.82</b>                 | <b>0.58</b> |
| #19    | <b>Σ</b> |        |        |       |        |        |      | <b>663.8</b>    | <b>14,808</b>              | <b>0.28</b>                 | <b>0.18</b> |
| #15    | 1        | 0.201  | 125.00 | 8.20  | 0.3960 | 1.0000 | 3    | 1,267.2         | 54,687                     | 0.00                        | 0.00        |
|        | 2        | 0.161  | 100.00 | 11.40 | 0.3060 | 1.0000 | 3    | 1,671.9         | 57,370                     | 0.43                        | 0.31        |
|        | 3        | 0.118  | 100.00 | 10.20 | 0.2850 | 1.0000 | 2    | 873.0           | 27,740                     | 14.56                       | 10.46       |



| Stru #   | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|----------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| <b>Σ</b> |          |        |        |       |        |        |      | <b>3,281.0</b>  | <b>46,290</b>              | <b>1.92</b>                 | <b>1.17</b> |
| #12      | 1        | 0.124  | 150.00 | 6.30  | 0.3070 | 1.0000 | 2    | 259.1           | 20,985                     | 11.35                       | 7.93        |
|          | 2        | 0.132  | 200.00 | 3.60  | 0.3500 | 1.0000 | 2    | 66.5            | 14,727                     | 8.34                        | 5.68        |
|          | 3        | 0.136  | 175.00 | 5.00  | 0.3330 | 1.0000 | 2    | 313.0           | 23,102                     | 12.74                       | 8.84        |
|          | 4        | 0.188  | 200.00 | 3.40  | 0.3570 | 1.0000 | 2    | 404.6           | 15,016                     | 6.20                        | 4.48        |
|          | 5        | 0.228  | 175.00 | 4.10  | 0.3640 | 1.0000 | 2    | 236.6           | 33,971                     | 18.96                       | 13.17       |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>1,024.9</b>  | <b>16,872</b>              | <b>7.34</b>                 | <b>4.90</b> |
| #13      | 1        | 0.128  | 150.00 | 6.90  | 0.3390 | 1.0000 | 2    | 205.0           | 25,757                     | 13.91                       | 9.63        |
|          | 2        | 0.130  | 175.00 | 5.70  | 0.3300 | 1.0000 | 2    | 321.8           | 23,501                     | 12.64                       | 8.87        |
|          | 3        | 0.191  | 175.00 | 6.00  | 0.2890 | 1.0000 | 2    | 363.2           | 34,639                     | 20.30                       | 14.29       |
|          | 4        | 0.122  | 175.00 | 5.10  | 0.3460 | 1.0000 | 2    | 124.9           | 26,092                     | 15.97                       | 11.02       |
|          | 5        | 0.137  | 175.00 | 4.20  | 0.3530 | 1.0000 | 2    | 199.0           | 14,832                     | 6.29                        | 4.55        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>2,079.9</b>  | <b>18,344</b>              | <b>8.61</b>                 | <b>6.01</b> |
| #14      | 1        | 0.196  | 100.00 | 10.20 | 0.3980 | 1.0000 | 3    | 1,823.8         | 88,626                     | 5.13                        | 3.60        |
|          | 2        | 0.193  | 150.00 | 6.70  | 0.4020 | 1.0000 | 3    | 1,202.1         | 57,829                     | 2.49                        | 1.77        |
|          | 3        | 0.169  | 75.00  | 13.80 | 0.3240 | 1.0000 | 3    | 3,005.9         | 70,417                     | 0.28                        | 0.20        |
|          | 4        | 0.114  | 100.00 | 11.00 | 0.2980 | 1.0000 | 3    | 193.5           | 37,483                     | 1.77                        | 1.28        |
|          | 5        | 0.078  | 100.00 | 10.10 | 0.1830 | 1.0000 | 3    | 203.9           | 16,212                     | 0.99                        | 0.72        |
|          | 6        | 0.084  | 150.00 | 7.10  | 0.2700 | 1.0000 | 2    | 126.0           | 13,104                     | 7.06                        | 5.08        |
|          | 7        | 0.087  | 100.00 | 10.00 | 0.1840 | 1.0000 | 3    | 315.9           | 15,469                     | 0.14                        | 0.10        |
|          | 8        | 0.126  | 150.00 | 6.70  | 0.2740 | 1.0000 | 2    | 438.7           | 17,197                     | 8.46                        | 6.18        |
|          | 9        | 0.117  | 150.00 | 7.30  | 0.2600 | 1.0000 | 2    | 414.9           | 17,508                     | 9.09                        | 6.64        |
|          | 10       | 0.115  | 125.00 | 8.50  | 0.2610 | 1.0000 | 2    | 253.2           | 18,957                     | 10.12                       | 7.38        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>7,172.5</b>  | <b>83,385</b>              | <b>1.80</b>                 | <b>0.36</b> |
| #16      | 1        | 0.200  | 200.00 | 3.30  | 0.3000 | 1.0000 | 3    | 377.7           | 19,309                     | 0.34                        | 0.24        |
|          | 2        | 0.204  | 150.00 | 6.00  | 0.3630 | 1.0000 | 3    | 939.3           | 46,550                     | 1.59                        | 1.14        |
|          | 3        | 0.210  | 150.00 | 6.10  | 0.3990 | 1.0000 | 3    | 715.4           | 57,910                     | 5.27                        | 3.86        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>12,480.7</b> | <b>57,021</b>              | <b>1.79</b>                 | <b>0.63</b> |
| #20      | 1        | 0.186  | 175.00 | 4.80  | 0.2130 | 1.0000 | 3    | 318.0           | 20,003                     | 0.08                        | 0.06        |
|          | 2        | 0.194  | 200.00 | 3.80  | 0.2330 | 1.0000 | 3    | 371.5           | 16,201                     | 0.07                        | 0.05        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>13,372.2</b> | <b>43,852</b>              | <b>0.63</b>                 | <b>0.26</b> |
| #22      | <b>Σ</b> |        |        |       |        |        |      | <b>29,827.5</b> | <b>35,065</b>              | <b>0.24</b>                 | <b>0.13</b> |
| #23      | 1        | 0.172  | 175.00 | 4.20  | 0.2810 | 1.0000 | 3    | 260.3           | 18,176                     | 0.00                        | 0.00        |
|          | 2        | 0.185  | 150.00 | 6.00  | 0.2160 | 1.0000 | 3    | 346.7           | 24,651                     | 0.44                        | 0.31        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>29,527.9</b> | <b>34,065</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #35      | <b>Σ</b> |        |        |       |        |        |      | <b>40,687.5</b> | <b>31,691</b>              | <b>0.02</b>                 | <b>0.01</b> |
| #36      | 1        | 0.190  | 175.00 | 5.94  | 0.2830 | 1.0000 | 3    | 248.3           | 26,262                     | 0.00                        | 0.00        |
|          | 2        | 0.180  | 125.00 | 9.92  | 0.2410 | 1.0000 | 3    | 352.0           | 45,436                     | 1.42                        | 0.98        |

| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 3        | 0.151  | 300.00 | 2.63  | 0.3890 | 1.0000 | 2    | 50.2            | 12,518                     | 6.37                        | 4.47        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>40,745.8</b> | <b>37,462</b>              | <b>0.02</b>                 | <b>0.01</b> |
| #37    | 1        | 0.196  | 200.00 | 3.80  | 0.3980 | 1.0000 | 2    | 433.2           | 18,411                     | 8.26                        | 5.97        |
|        | 2        | 0.193  | 175.00 | 5.40  | 0.4020 | 1.0000 | 3    | 576.2           | 47,282                     | 1.47                        | 1.07        |
|        | 3        | 0.173  | 150.00 | 7.11  | 0.2770 | 1.0000 | 3    | 296.4           | 36,579                     | 1.69                        | 1.23        |
|        | 4        | 0.171  | 150.00 | 6.52  | 0.2990 | 1.0000 | 2    | 368.1           | 21,649                     | 10.16                       | 7.45        |
|        | 5        | 0.078  | 400.00 | 1.20  | 0.1830 | 1.0000 | 2    | 16.6            | 1,881                      | 1.01                        | 0.73        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>40,586.1</b> | <b>32,624</b>              | <b>0.29</b>                 | <b>0.15</b> |

### Subwatershed Time of Concentration Details:

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.65      | 50.00            | 1,369.00          | 1.910          | 0.199        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.57      | 157.00           | 10,030.00         | 3.750          | 0.742        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.941</b> |
| #1        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 6.63      | 70.00            | 1,056.00          | 2.570          | 0.114        |
|           |          | 5. Nearly bare and untilled, and alluvial valley fans | 1.98      | 150.00           | 7,573.00          | 1.400          | 1.502        |
| <b>#1</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.616</b> |
| #1        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.65      | 117.00           | 7,070.00          | 1.280          | 1.534        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.43      | 126.00           | 5,188.00          | 4.670          | 0.308        |
| <b>#1</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.842</b> |
| #1        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 5.77      | 260.00           | 4,506.00          | 2.400          | 0.521        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.84      | 168.00           | 5,924.00          | 5.050          | 0.325        |
| <b>#1</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.846</b> |
| #1        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 19.93     | 180.00           | 903.00            | 4.460          | 0.056        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.30      | 178.00           | 5,393.00          | 5.450          | 0.274        |
| <b>#1</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.330</b> |
| #1        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 13.43     | 105.00           | 782.00            | 3.660          | 0.059        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.62      | 283.00           | 10,822.00         | 4.850          | 0.619        |
| <b>#1</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.678</b> |
| #2        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 6.84      | 70.00            | 1,024.00          | 2.610          | 0.108        |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 70.00            | 4,325.00          | 3.810          | 0.315        |
| <b>#2</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.423</b> |
| #2        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.56      | 45.00            | 810.00            | 2.350          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.86      | 40.00            | 4,663.00          | 2.770          | 0.467        |
| <b>#2</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.562</b> |
| #2        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 5.89      | 50.00            | 849.00            | 2.420          | 0.097        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.17      | 80.00            | 6,862.00          | 3.230          | 0.590        |
| <b>#2</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.687</b> |
| #2        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 12.63     | 95.00            | 752.00            | 3.550          | 0.058        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.40      | 135.00           | 9,630.00          | 3.550          | 0.753        |
| <b>#2</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.811</b> |
| #2        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 11.02     | 70.00            | 635.00            | 3.320          | 0.053        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.46      | 40.00            | 8,732.00          | 2.030          | 1.194        |
| <b>#2</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.247</b> |
| #3        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 10.00            | 805.00            | 1.110          | 0.201        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.33      | 40.00            | 3,017.00          | 3.450          | 0.242        |
| <b>#3</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.443</b> |
| #3        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 0.68      | 10.00            | 1,478.00          | 0.820          | 0.500        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.78      | 100.00           | 5,622.00          | 4.000          | 0.390        |
| <b>#3</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.890</b> |
| #3        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.66      | 70.00            | 1,501.00          | 2.150          | 0.193        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.17      | 60.00            | 5,126.00          | 3.240          | 0.439        |
| <b>#3</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.632</b> |
| #5        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 19.06     | 285.00           | 1,495.00          | 4.360          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.64      | 242.00           | 9,174.00          | 4.870          | 0.523        |
| <b>#5</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.618</b> |
| #5        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 14.27     | 105.00           | 736.00            | 3.770          | 0.054        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.08      | 297.00           | 7,279.00          | 6.050          | 0.334        |
| <b>#5</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.388</b> |
| #5        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 8.27      | 35.00            | 423.00            | 2.870          | 0.040        |



| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.44      | 208.00           | 6,049.00          | 5.560          | 0.302        |
| <b>#5</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.342</b> |
| #5        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 14.58     | 85.00            | 583.00            | 3.810          | 0.042        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.53      | 248.00           | 5,473.00          | 6.380          | 0.238        |
| <b>#5</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.280</b> |
| #5        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 5.07      | 70.00            | 1,382.00          | 2.250          | 0.170        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.89      | 170.00           | 4,375.00          | 5.910          | 0.205        |
| <b>#5</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.375</b> |
| #5        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 12.48     | 90.00            | 721.00            | 3.530          | 0.056        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 5.16      | 274.00           | 5,308.02          | 6.810          | 0.216        |
| <b>#5</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.272</b> |
| #6        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 5.36      | 75.00            | 1,399.00          | 2.310          | 0.168        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.41      | 66.00            | 2,742.00          | 4.650          | 0.163        |
| <b>#6</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.331</b> |
| #6        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 80.00            | 2,359.00          | 1.840          | 0.356        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.63      | 80.00            | 3,039.00          | 4.860          | 0.173        |
| <b>#6</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.529</b> |
| #6        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.60      | 34.00            | 739.00            | 2.140          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.33      | 136.00           | 5,845.00          | 4.570          | 0.355        |
| <b>#6</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.450</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 6.06      | 85.00            | 1,402.00          | 2.460          | 0.158        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.52      | 96.00            | 3,810.00          | 4.760          | 0.222        |
| <b>#6</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.380</b> |
| #6        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 7.24      | 70.00            | 967.00            | 2.690          | 0.099        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.34      | 117.00           | 5,003.00          | 4.580          | 0.303        |
| <b>#6</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.402</b> |
| #6        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 31.83     | 183.00           | 575.00            | 5.640          | 0.028        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.38      | 270.00           | 7,990.00          | 5.510          | 0.402        |
| <b>#6</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.430</b> |
| #6        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 23.08     | 325.00           | 1,408.00          | 4.800          | 0.081        |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.88      | 240.00           | 8,327.00          | 5.090          | 0.454        |
| <b>#6</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.535</b> |
| #7        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.42     | 90.00            | 788.00            | 3.370          | 0.064        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.46      | 230.00           | 15,769.00         | 3.620          | 1.210        |
| <b>#7</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.274</b> |
| #7        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 10.97     | 60.00            | 547.00            | 3.310          | 0.045        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.61      | 220.00           | 13,660.00         | 3.800          | 0.998        |
| <b>#7</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.043</b> |
| #7        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 6.40      | 60.00            | 938.00            | 2.520          | 0.103        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.72      | 171.00           | 9,931.00          | 3.930          | 0.701        |
| <b>#7</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.804</b> |
| #7        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 19.23     | 80.00            | 416.00            | 4.380          | 0.026        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.45      | 100.00           | 4,083.00          | 4.690          | 0.241        |
| <b>#7</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.267</b> |
| #7        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 6.09      | 67.00            | 1,101.00          | 2.460          | 0.124        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.51      | 80.00            | 3,184.00          | 4.750          | 0.186        |
| <b>#7</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.310</b> |
| #7        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 5.93      | 63.00            | 1,062.00          | 2.430          | 0.121        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.74      | 82.00            | 2,993.00          | 4.960          | 0.167        |
| <b>#7</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.288</b> |
| #7        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 7.97      | 65.00            | 816.00            | 2.820          | 0.080        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.48      | 153.00           | 4,400.00          | 5.590          | 0.218        |
| <b>#7</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.298</b> |
| #7        | 8        | 5. Nearly bare and untilled, and alluvial valley fans | 6.60      | 50.00            | 758.00            | 2.560          | 0.082        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.66      | 473.00           | 10,157.00         | 6.470          | 0.436        |
| <b>#7</b> | <b>8</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.518</b> |
| #9        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.35      | 90.00            | 2,687.00          | 1.830          | 0.407        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.58      | 20.00            | 3,463.00          | 2.270          | 0.423        |
| <b>#9</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.830</b> |
| #10       | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 41.00            | 3,317.00          | 1.110          | 0.830        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.70      | 29.00            | 4,125.00          | 2.510          | 0.456        |
| <b>#10</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.286</b> |
| #10        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.25      | 125.00           | 5,554.00          | 1.500          | 1.028        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 85.00            | 3,997.00          | 4.370          | 0.254        |
| <b>#10</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.282</b> |
| #10        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.39      | 68.00            | 4,904.00          | 1.170          | 1.164        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.73      | 90.00            | 1,904.00          | 6.520          | 0.081        |
| <b>#10</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.245</b> |
| #10        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.76      | 51.00            | 1,357.00          | 1.930          | 0.195        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.65      | 22.00            | 3,385.00          | 2.410          | 0.390        |
| <b>#10</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.585</b> |
| #10        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 1.63      | 88.00            | 5,391.16          | 1.270          | 1.179        |
| <b>#10</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.179</b> |
| #12        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.50      | 75.00            | 1,667.00          | 2.120          | 0.218        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.85      | 155.00           | 8,400.00          | 4.070          | 0.573        |
| <b>#12</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.791</b> |
| #12        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.99      | 50.00            | 1,674.03          | 1.720          | 0.270        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.67      | 70.00            | 4,201.17          | 3.870          | 0.301        |
| <b>#12</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.571</b> |
| #12        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.04      | 57.00            | 1,411.00          | 2.000          | 0.195        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.55      | 107.00           | 6,884.00          | 3.740          | 0.511        |
| <b>#12</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.706</b> |
| #12        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.23      | 84.00            | 3,771.04          | 1.490          | 0.703        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 186.00           | 11,515.60         | 3.810          | 0.839        |
| <b>#12</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.542</b> |
| #12        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.68      | 53.00            | 1,442.00          | 1.910          | 0.209        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.95      | 120.00           | 6,155.00          | 4.180          | 0.409        |
| <b>#12</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.618</b> |
| #13        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.62      | 62.00            | 1,342.00          | 2.140          | 0.174        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.91      | 157.00           | 8,225.00          | 4.140          | 0.551        |
| <b>#13</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.725</b> |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #13        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.91      | 50.00            | 1,717.00          | 1.700          | 0.280        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.28      | 183.00           | 8,039.00          | 4.520          | 0.494        |
| <b>#13</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.774</b> |
| #13        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 6.18      | 95.00            | 1,537.00          | 2.480          | 0.172        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 135.00           | 6,347.00          | 4.370          | 0.403        |
| <b>#13</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.575</b> |
| #13        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.17      | 10.00            | 315.00            | 1.780          | 0.049        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.30      | 100.00           | 4,344.00          | 4.550          | 0.265        |
| <b>#13</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.314</b> |
| #13        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.10      | 70.00            | 2,255.00          | 1.760          | 0.355        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.23      | 140.00           | 11,392.00         | 3.320          | 0.953        |
| <b>#13</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.308</b> |
| #14        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 10.59     | 63.00            | 595.00            | 3.250          | 0.050        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.60      | 151.00           | 5,808.00          | 4.830          | 0.334        |
| <b>#14</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.384</b> |
| #14        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.28      | 67.00            | 920.00            | 2.690          | 0.095        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.17      | 123.00           | 5,670.00          | 4.410          | 0.357        |
| <b>#14</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.452</b> |
| #14        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 21.46     | 150.00           | 699.00            | 4.630          | 0.041        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.10      | 364.00           | 11,728.00         | 5.280          | 0.617        |
| <b>#14</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.658</b> |
| #14        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 35.00            | 1,032.00          | 1.840          | 0.155        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.97      | 103.00           | 3,470.00          | 5.160          | 0.186        |
| <b>#14</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.341</b> |
| #14        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 28.15     | 125.00           | 444.00            | 5.300          | 0.023        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.18      | 246.00           | 5,886.00          | 6.130          | 0.266        |
| <b>#14</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.289</b> |
| #14        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 3.18      | 40.00            | 1,257.00          | 1.780          | 0.196        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.29      | 228.00           | 9,963.00          | 4.530          | 0.610        |
| <b>#14</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.806</b> |

| Stru #     | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #14        | 7         | 5. Nearly bare and untilled, and alluvial valley fans | 16.72     | 100.00           | 598.00            | 4.080          | 0.040        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.81      | 243.00           | 8,649.00          | 5.020          | 0.478        |
| <b>#14</b> | <b>7</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.518</b> |
| #14        | 8         | 5. Nearly bare and untilled, and alluvial valley fans | 1.70      | 47.00            | 2,765.00          | 1.300          | 0.590        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.44      | 274.00           | 11,208.00         | 4.690          | 0.663        |
| <b>#14</b> | <b>8</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.253</b> |
| #14        | 9         | 5. Nearly bare and untilled, and alluvial valley fans | 2.87      | 105.00           | 3,657.00          | 1.690          | 0.601        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.43      | 194.00           | 7,991.00          | 4.670          | 0.475        |
| <b>#14</b> | <b>9</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.076</b> |
| #14        | 10        | 5. Nearly bare and untilled, and alluvial valley fans | 2.75      | 80.00            | 2,907.00          | 1.650          | 0.489        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.41      | 172.00           | 7,149.00          | 4.650          | 0.427        |
| <b>#14</b> | <b>10</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.916</b> |
| #15        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 12.80     | 54.00            | 422.00            | 3.570          | 0.032        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.68      | 181.00           | 10,781.00         | 3.880          | 0.771        |
| <b>#15</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.803</b> |
| #15        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 44.22     | 260.00           | 588.00            | 6.640          | 0.024        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.45      | 254.00           | 10,354.00         | 4.690          | 0.613        |
| <b>#15</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.637</b> |
| #15        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 10.04     | 85.00            | 847.00            | 3.160          | 0.074        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.34      | 366.00           | 15,663.00         | 4.580          | 0.949        |
| <b>#15</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.023</b> |
| #16        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 4.17      | 15.00            | 360.00            | 2.040          | 0.049        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.42      | 108.00           | 7,618.00          | 3.570          | 0.592        |
| <b>#16</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.641</b> |
| #16        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 8.70      | 62.00            | 713.00            | 2.940          | 0.067        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.99      | 144.00           | 7,241.00          | 4.230          | 0.475        |
| <b>#16</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.542</b> |
| #16        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 6.88      | 32.00            | 465.00            | 2.620          | 0.049        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.29      | 81.00            | 3,543.00          | 4.530          | 0.217        |
| <b>#16</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.266</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #17        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 9.37      | 65.00            | 694.00            | 3.060          | 0.062        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.19      | 56.00            | 4,712.00          | 3.270          | 0.400        |
| <b>#17</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.462</b> |
| #18        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 9.00      | 60.00            | 667.00            | 2.990          | 0.061        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.97      | 61.00            | 6,287.00          | 2.950          | 0.591        |
| <b>#18</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.652</b> |
| #18        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.47      | 33.00            | 1,336.00          | 1.570          | 0.236        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.01      | 164.00           | 8,154.00          | 4.250          | 0.532        |
| <b>#18</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.768</b> |
| #20        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.87     | 45.00            | 379.00            | 3.440          | 0.030        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.75      | 45.00            | 5,969.00          | 2.600          | 0.637        |
| <b>#20</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.667</b> |
| #20        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.40      | 45.00            | 833.00            | 2.320          | 0.099        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.30      | 98.00            | 7,547.00          | 3.410          | 0.614        |
| <b>#20</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.713</b> |
| #21        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.09      | 60.00            | 1,467.00          | 2.020          | 0.201        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.93      | 60.00            | 6,433.00          | 2.890          | 0.618        |
| <b>#21</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.819</b> |
| #21        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.50      | 50.00            | 1,430.00          | 1.860          | 0.213        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.15      | 60.00            | 2,785.00          | 4.400          | 0.175        |
| <b>#21</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.388</b> |
| #21        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.70      | 15.00            | 881.00            | 1.300          | 0.188        |
|            |          | 9. Small streams flowing bankfull                     | 1.49      | 60.00            | 4,014.00          | 11.000         | 0.101        |
| <b>#21</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.289</b> |
| #21        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.21      | 40.00            | 1,811.02          | 1.480          | 0.339        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.84      | 50.00            | 5,949.54          | 2.750          | 0.600        |
| <b>#21</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.939</b> |
| #23        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.44      | 65.00            | 2,660.01          | 1.560          | 0.473        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.33      | 10.00            | 3,017.50          | 1.720          | 0.487        |
| <b>#23</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.960</b> |
| #23        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.49      | 60.00            | 1,718.01          | 1.860          | 0.256        |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.66      | 65.00            | 3,926.06          | 3.860          | 0.282        |
| <b>#23</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.538</b> |
| #24        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.71      | 430.00           | 25,118.00         | 1.300          | 5.367        |
| <b>#24</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>5.367</b> |
| #24        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.84      | 430.00           | 23,393.00         | 1.350          | 4.813        |
| <b>#24</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>4.813</b> |
| #24        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.82      | 155.00           | 8,498.00          | 1.350          | 1.748        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.84      | 40.00            | 4,771.00          | 2.740          | 0.483        |
| <b>#24</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.231</b> |
| #24        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 50.00            | 4,042.00          | 1.110          | 1.011        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.49      | 60.00            | 12,150.00         | 2.100          | 1.607        |
| <b>#24</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.618</b> |
| #25        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 0.51      | 10.00            | 1,950.00          | 0.710          | 0.762        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.81      | 60.00            | 3,322.00          | 4.030          | 0.228        |
| <b>#25</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.990</b> |
| #25        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.11      | 25.00            | 2,254.00          | 1.050          | 0.596        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.36      | 75.00            | 3,178.00          | 4.600          | 0.191        |
| <b>#25</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.787</b> |
| #25        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 3.23      | 30.00            | 929.00            | 1.790          | 0.144        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.45      | 154.00           | 6,297.00          | 4.690          | 0.372        |
| <b>#25</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.516</b> |
| #26        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.20      | 103.00           | 8,602.00          | 1.090          | 2.192        |
| <b>#26</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.192</b> |
| #26        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.23      | 120.00           | 9,780.00          | 1.100          | 2.469        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.18      | 184.00           | 8,454.00          | 4.420          | 0.531        |
| <b>#26</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>3.000</b> |
| #27        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.32      | 50.00            | 1,158.02          | 2.070          | 0.155        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.53      | 198.00           | 7,838.16          | 4.760          | 0.457        |
| <b>#27</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.612</b> |
| #27        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.26      | 30.00            | 570.00            | 2.290          | 0.069        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.15      | 278.00           | 8,822.00          | 5.320          | 0.460        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#27</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.529</b> |
| #27        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 16.33     | 80.00            | 490.00            | 4.040          | 0.033        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.15      | 225.00           | 10,443.00         | 4.400          | 0.659        |
| <b>#27</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.692</b> |
| #27        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 12.43     | 65.00            | 523.00            | 3.520          | 0.041        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.49      | 225.00           | 6,454.00          | 5.600          | 0.320        |
| <b>#27</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.361</b> |
| #27        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 9.40      | 25.00            | 266.00            | 3.060          | 0.024        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.32      | 364.00           | 15,700.00         | 4.560          | 0.956        |
| <b>#27</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.980</b> |
| #28        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 5.25      | 40.00            | 762.00            | 2.290          | 0.092        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.96      | 310.00           | 10,479.34         | 5.150          | 0.565        |
| <b>#28</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.657</b> |
| #28        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 25.86     | 105.00           | 406.00            | 5.080          | 0.022        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.96      | 310.00           | 10,479.34         | 5.150          | 0.565        |
| <b>#28</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.587</b> |
| #29        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.58     | 30.00            | 259.00            | 3.400          | 0.021        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.61      | 288.00           | 7,976.00          | 5.700          | 0.388        |
| <b>#29</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.409</b> |
| #29        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 8.06      | 40.00            | 496.00            | 2.830          | 0.048        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.90      | 252.00           | 8,693.55          | 5.100          | 0.473        |
| <b>#29</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.521</b> |
| #29        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 7.25      | 25.00            | 345.00            | 2.690          | 0.035        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.26      | 158.00           | 7,001.00          | 4.500          | 0.432        |
| <b>#29</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.467</b> |
| #30        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.93      | 35.00            | 710.00            | 2.220          | 0.088        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.67      | 243.00           | 14,540.00         | 3.870          | 1.043        |
| <b>#30</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.131</b> |
| #31        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.91      | 15.00            | 515.00            | 1.700          | 0.084        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.74      | 247.00           | 9,006.00          | 4.960          | 0.504        |
| <b>#31</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.588</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #31        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.46      | 25.00            | 335.00            | 2.730          | 0.034        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.18      | 138.00           | 6,335.00          | 4.420          | 0.398        |
| <b>#31</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.432</b> |
| #31        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 3.84      | 20.00            | 521.00            | 1.950          | 0.074        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.24      | 108.00           | 4,826.00          | 4.480          | 0.299        |
| <b>#31</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.373</b> |
| #32        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.48      | 22.00            | 632.00            | 1.860          | 0.094        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.56      | 101.00           | 6,494.00          | 3.740          | 0.482        |
| <b>#32</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.576</b> |
| #34        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.21      | 25.00            | 779.00            | 1.790          | 0.120        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.80      | 63.00            | 2,251.00          | 5.010          | 0.124        |
| <b>#34</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.244</b> |
| #34        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.75      | 40.00            | 696.00            | 2.390          | 0.080        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 23.00     | 2,100.00         | 9,130.43          | 14.380         | 0.176        |
| <b>#34</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.256</b> |
| #34        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.67      | 40.00            | 1,500.00          | 1.630          | 0.255        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.28      | 98.00            | 7,675.00          | 3.380          | 0.630        |
| <b>#34</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.885</b> |
| #36        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.21      | 105.00           | 3,274.00          | 1.790          | 0.508        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.21      | 5.00             | 2,367.00          | 1.370          | 0.479        |
| <b>#36</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.987</b> |
| #36        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.50      | 140.00           | 2,547.00          | 2.340          | 0.302        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.58      | 30.00            | 1,897.00          | 3.770          | 0.139        |
| <b>#36</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.441</b> |
| #36        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.03      | 80.00            | 3,938.62          | 1.420          | 0.770        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.52      | 50.00            | 1,981.86          | 4.760          | 0.115        |
| <b>#36</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.885</b> |
| #37        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.68      | 129.00           | 2,754.05          | 2.160          | 0.354        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.16      | 10.00            | 6,108.73          | 1.210          | 1.402        |
| <b>#37</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.756</b> |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #37        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.32      | 90.00            | 1,229.00          | 2.700          | 0.126        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 70.00            | 4,309.01          | 3.820          | 0.313        |
| <b>#37</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.439</b> |
| #37        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 8.10      | 100.00           | 1,234.00          | 2.840          | 0.120        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.66      | 100.00           | 3,763.21          | 4.890          | 0.213        |
| <b>#37</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.333</b> |
| #37        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 5.09      | 90.00            | 1,768.03          | 2.250          | 0.218        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.36      | 30.00            | 8,326.39          | 1.800          | 1.284        |
| <b>#37</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.502</b> |
| #37        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 0.81      | 20.00            | 2,466.09          | 0.900          | 0.761        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.06      | 50.00            | 1,231.01          | 6.040          | 0.056        |
| <b>#37</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.817</b> |

### ***Subwatershed Muskingum Routing Details:***

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.29      | 107.00           | 8,294.00          | 3.400          | 0.677        |
| <b>#1</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.677</b> |
| #1        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.27      | 113.00           | 8,880.00          | 3.380          | 0.729        |
| <b>#1</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.729</b> |
| #1        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.35      | 171.00           | 12,634.00         | 3.490          | 1.005        |
| <b>#1</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.005</b> |
| #1        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.49      | 274.00           | 18,349.00         | 3.660          | 1.392        |
| <b>#1</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.392</b> |
| #1        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.49      | 274.00           | 18,349.00         | 3.660          | 1.392        |
| <b>#1</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.392</b> |
| #2        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.53      | 20.00            | 3,756.00          | 2.180          | 0.478        |
| <b>#2</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.478</b> |
| #2        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.55      | 25.00            | 4,570.00          | 2.210          | 0.574        |
| <b>#2</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.574</b> |
| #2        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.55      | 25.00            | 4,570.00          | 2.210          | 0.574        |
| <b>#2</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.574</b> |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #2        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.65      | 45.00            | 6,955.00          | 2.410          | 0.801        |
| <b>#2</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.801</b> |
| #3        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.92      | 20.00            | 2,168.00          | 2.880          | 0.209        |
| <b>#3</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.209</b> |
| #5        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#5</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #5        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.75      | 125.00           | 7,149.00          | 3.960          | 0.501        |
| <b>#5</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.501</b> |
| #5        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.65      | 155.00           | 9,418.00          | 3.840          | 0.681        |
| <b>#5</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #5        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.65      | 155.00           | 9,418.00          | 3.840          | 0.681        |
| <b>#5</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #5        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.67      | 239.00           | 14,273.00         | 3.880          | 1.021        |
| <b>#5</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.021</b> |
| #5        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.68      | 239.00           | 14,223.00         | 3.880          | 1.018        |
| <b>#5</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.018</b> |
| #6        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.16      | 26.00            | 2,241.00          | 3.230          | 0.192        |
| <b>#6</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.192</b> |
| #6        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.00      | 50.00            | 4,987.00          | 3.000          | 0.461        |
| <b>#6</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.461</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.00      | 50.00            | 4,987.00          | 1.000          | 1.385        |
| <b>#6</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.385</b> |
| #6        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.02      | 89.00            | 8,685.00          | 3.030          | 0.796        |
| <b>#6</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.796</b> |
| #6        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.06      | 126.00           | 11,860.00         | 3.090          | 1.066        |
| <b>#6</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.066</b> |
| #6        | 7        | 8. Large gullies, diversions, and low flowing streams | 1.06      | 126.00           | 11,860.00         | 3.090          | 1.066        |
| <b>#6</b> | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.066</b> |
| #7        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.16      | 140.00           | 12,037.00         | 3.230          | 1.035        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#7</b>  | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.035</b> |
| #7         | 5        | 8. Large gullies, diversions, and low flowing streams | 1.14      | 140.00           | 12,307.69         | 3.190          | 1.071        |
| <b>#7</b>  | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.071</b> |
| #7         | 6        | 8. Large gullies, diversions, and low flowing streams | 1.17      | 158.00           | 13,546.00         | 3.230          | 1.164        |
| <b>#7</b>  | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.164</b> |
| #7         | 7        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 187.00           | 15,784.00         | 3.260          | 1.344        |
| <b>#7</b>  | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.344</b> |
| #7         | 8        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 187.00           | 15,784.00         | 3.260          | 1.344        |
| <b>#7</b>  | <b>8</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.344</b> |
| #10        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.76      | 37.00            | 4,861.00          | 2.610          | 0.517        |
| <b>#10</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.517</b> |
| #10        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.76      | 37.00            | 4,861.00          | 2.610          | 0.517        |
| <b>#10</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.517</b> |
| #10        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.79      | 47.00            | 5,956.00          | 2.660          | 0.621        |
| <b>#10</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.621</b> |
| #12        | 2        | 8. Large gullies, diversions, and low flowing streams | 8.24      | 111.00           | 1,347.00          | 8.610          | 0.043        |
| <b>#12</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.043</b> |
| #12        | 3        | 8. Large gullies, diversions, and low flowing streams | 8.01      | 109.00           | 1,360.00          | 8.490          | 0.044        |
| <b>#12</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.044</b> |
| #12        | 4        | 8. Large gullies, diversions, and low flowing streams | 2.24      | 176.00           | 7,866.00          | 4.480          | 0.487        |
| <b>#12</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.487</b> |
| #12        | 5        | 8. Large gullies, diversions, and low flowing streams | 2.24      | 176.00           | 7,866.00          | 4.480          | 0.487        |
| <b>#12</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.487</b> |
| #13        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.34      | 54.00            | 4,025.00          | 3.470          | 0.322        |
| <b>#13</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.322</b> |
| #13        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.98      | 72.00            | 7,333.00          | 2.970          | 0.685        |
| <b>#13</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.685</b> |
| #13        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 127.00           | 10,806.00         | 3.250          | 0.923        |
| <b>#13</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.923</b> |
| #13        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 127.00           | 10,806.00         | 3.250          | 0.923        |
| <b>#13</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.923</b> |
| #14        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#14</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |



| Stru #     | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #14        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.83      | 58.00            | 6,957.00          | 2.730          | 0.707        |
| <b>#14</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.707</b> |
| #14        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.81      | 77.00            | 9,480.00          | 2.700          | 0.975        |
| <b>#14</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.975</b> |
| #14        | 4         | 8. Large gullies, diversions, and low flowing streams | 0.86      | 147.00           | 17,117.00         | 2.770          | 1.716        |
| <b>#14</b> | <b>4</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.716</b> |
| #14        | 5         | 8. Large gullies, diversions, and low flowing streams | 0.88      | 175.00           | 19,934.00         | 2.810          | 1.970        |
| <b>#14</b> | <b>5</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.970</b> |
| #14        | 6         | 8. Large gullies, diversions, and low flowing streams | 0.95      | 211.00           | 22,155.00         | 2.920          | 2.107        |
| <b>#14</b> | <b>6</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.107</b> |
| #14        | 7         | 8. Large gullies, diversions, and low flowing streams | 0.96      | 257.00           | 26,835.00         | 2.930          | 2.544        |
| <b>#14</b> | <b>7</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.544</b> |
| #14        | 8         | 8. Large gullies, diversions, and low flowing streams | 0.96      | 257.00           | 26,835.00         | 2.930          | 2.544        |
| <b>#14</b> | <b>8</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.544</b> |
| #14        | 9         | 8. Large gullies, diversions, and low flowing streams | 0.95      | 307.00           | 32,146.59         | 2.930          | 3.047        |
| <b>#14</b> | <b>9</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.047</b> |
| #14        | 10        | 8. Large gullies, diversions, and low flowing streams | 0.96      | 339.00           | 35,382.00         | 2.930          | 3.354        |
| <b>#14</b> | <b>10</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.354</b> |
| #15        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#15</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #15        | 2         | 8. Large gullies, diversions, and low flowing streams | 1.14      | 86.00            | 7,535.00          | 3.200          | 0.654        |
| <b>#15</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.654</b> |
| #15        | 3         | 8. Large gullies, diversions, and low flowing streams | 1.25      | 115.00           | 9,236.00          | 3.340          | 0.768        |
| <b>#15</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.768</b> |
| #16        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.58      | 24.00            | 4,161.00          | 2.270          | 0.509        |
| <b>#16</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.509</b> |
| #16        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.51      | 37.00            | 7,269.00          | 2.140          | 0.943        |
| <b>#16</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.943</b> |
| #17        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#17</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #18        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#18</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #18        | 2         | 8. Large gullies, diversions, and low flowing streams | 1.02      | 62.00            | 6,103.00          | 3.020          | 0.561        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#18</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.561</b> |
| #20        | 2        | 8. Large gullies, diversions, and low flowing streams | 17.00     | 3,605.00         | 21,205.88         | 12.360         | 0.476        |
| <b>#20</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.476</b> |
| #21        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#21</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #21        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.41      | 20.00            | 4,824.00          | 1.930          | 0.694        |
| <b>#21</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.694</b> |
| #21        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 20.00            | 5,626.00          | 1.780          | 0.877        |
| <b>#21</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.877</b> |
| #21        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 20.00            | 5,626.00          | 1.780          | 0.877        |
| <b>#21</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.877</b> |
| #23        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#23</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #23        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.63      | 30.00            | 4,771.75          | 2.370          | 0.559        |
| <b>#23</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.559</b> |
| #24        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.79      | 180.00           | 22,769.00         | 2.660          | 2.377        |
| <b>#24</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.377</b> |
| #24        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.78      | 180.00           | 23,111.00         | 2.640          | 2.431        |
| <b>#24</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.431</b> |
| #24        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#24</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #25        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.99      | 104.00           | 5,220.00          | 4.230          | 0.342        |
| <b>#25</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.342</b> |
| #25        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.99      | 104.00           | 5,220.00          | 4.230          | 0.342        |
| <b>#25</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.342</b> |
| #25        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#25</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #27        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.38      | 216.00           | 15,629.00         | 3.520          | 1.233        |
| <b>#27</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.233</b> |
| #27        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.17      | 144.00           | 12,301.00         | 3.240          | 1.054        |
| <b>#27</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.054</b> |
| #27        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 76.00            | 6,454.00          | 3.250          | 0.551        |
| <b>#27</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.551</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #27        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 76.00            | 6,454.00          | 3.250          | 0.551        |
| <b>#27</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.551</b> |
| #28        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.30      | 84.00            | 6,445.17          | 3.420          | 0.523        |
| <b>#28</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.523</b> |
| #29        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.88      | 37.00            | 4,210.00          | 2.810          | 0.416        |
| <b>#29</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.416</b> |
| #29        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.88      | 26.00            | 2,949.00          | 2.810          | 0.291        |
| <b>#29</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.291</b> |
| #31        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.35      | 76.00            | 5,639.00          | 3.480          | 0.450        |
| <b>#31</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.450</b> |
| #31        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.15      | 20.00            | 1,734.00          | 3.220          | 0.149        |
| <b>#31</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.149</b> |
| #34        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.73      | 65.00            | 8,900.00          | 2.560          | 0.965        |
| <b>#34</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.965</b> |
| #34        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.73      | 65.00            | 8,900.00          | 2.560          | 0.965        |
| <b>#34</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.965</b> |
| #36        | 3        | 8. Large gullies, diversions, and low flowing streams | 2.71      | 80.00            | 2,957.00          | 4.930          | 0.166        |
| <b>#36</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.166</b> |
| #37        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.29      | 30.00            | 10,319.91         | 1.610          | 1.780        |
| <b>#37</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.780</b> |
| #37        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.31      | 30.00            | 9,800.71          | 1.650          | 1.649        |
| <b>#37</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.649</b> |
| #37        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.29      | 30.00            | 10,319.91         | 1.610          | 1.780        |
| <b>#37</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.780</b> |
| #37        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.56      | 100.00           | 17,956.54         | 2.230          | 2.236        |
| <b>#37</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.236</b> |



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# **Cottonwood Arroyo Pre-mine Hydrology and Sedimentology**

***The drainage subdivisions used to model the hydrology is shown  
on Exhibit 18.B.***

***Revised February 2012***

Art O'Hayre

***General Information***

***Storm Information:***

|                 |               |
|-----------------|---------------|
| Storm Type:     | Type II-70    |
| Design Storm:   | 100 yr - 6 hr |
| Rainfall Depth: | 2.040 inches  |

***Particle Size Distribution:***

| Size (mm) | PostMine-LoamySand | PreMine-LoamySand | PreMine-Badlands | LoamySand Postmining |
|-----------|--------------------|-------------------|------------------|----------------------|
| 2.0000    | 100.000%           | 100.000%          | 100.000%         | 0.000%               |
| 0.1000    | 26.500%            | 30.000%           | 83.500%          | 0.000%               |
| 0.0500    | 14.000%            | 17.000%           | 77.000%          | 0.000%               |
| 0.0020    | 11.000%            | 11.000%           | 56.000%          | 0.000%               |
| 0.0010    | 0.000%             | 0.000%            | 0.000%           | 0.000%               |

### ***Structure Summary:***

|     | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|-----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #30 | 476.400                                   | 476.400                               | 86.92                      | 10.78                                | 97.1               | 9,320                               | 4.41                                  | 3.12           |
| #28 | 1,217.900                                 | 1,217.900                             | 832.25                     | 93.54                                | 5,541.5            | 59,612                              | 0.74                                  | 0.53           |
| #26 | 2,486.400                                 | 2,486.400                             | 275.55                     | 74.66                                | 548.8              | 7,278                               | 2.35                                  | 1.74           |
| #24 | 8,061.800                                 | 8,061.800                             | 386.57                     | 224.86                               | 949.6              | 4,970                               | 0.73                                  | 0.46           |
| #25 | 1,015.700                                 | 9,077.500                             | 393.25                     | 268.09                               | 1,185.4            | 15,996                              | 3.69                                  | 0.75           |
| #27 | 1,783.700                                 | 13,347.600                            | 724.52                     | 419.60                               | 3,780.3            | 31,465                              | 13.44                                 | 2.82           |
| #29 | 966.000                                   | 15,531.500                            | 1,383.20                   | 586.28                               | 15,023.3           | 74,082                              | 9.73                                  | 2.44           |
| #32 | 293.700                                   | 16,301.600                            | 1,413.07                   | 623.43                               | 16,148.1           | 65,499                              | 6.14                                  | 1.76           |
| #31 | 957.100                                   | 957.100                               | 785.51                     | 82.54                                | 3,927.1            | 43,239                              | 0.95                                  | 0.75           |
| #33 | 0.000                                     | 17,258.700                            | 1,524.15                   | 705.97                               | 20,075.2           | 57,140                              | 4.55                                  | 1.65           |
| #34 | 932.500                                   | 18,191.200                            | 1,541.21                   | 774.90                               | 18,828.3           | 47,805                              | 0.35                                  | 0.13           |
| #5  | 2,023.000                                 | 2,023.000                             | 1,349.47                   | 134.18                               | 4,549.4            | 44,265                              | 4.91                                  | 2.73           |
| #6  | 1,743.200                                 | 3,766.200                             | 1,527.16                   | 256.62                               | 8,062.5            | 38,199                              | 0.25                                  | 0.15           |
| #7  | 2,395.300                                 | 6,161.500                             | 2,444.68                   | 466.74                               | 20,462.9           | 48,159                              | 0.00                                  | 0.00           |
| #8  | 0.000                                     | 6,161.500                             | 2,444.68                   | 466.74                               | 20,462.9           | 48,159                              | 0.00                                  | 0.00           |
| #10 | 1,053.200                                 | 7,214.700                             | 2,478.16                   | 546.78                               | 20,048.7           | 44,185                              | 0.15                                  | 0.09           |
| #1  | 2,411.100                                 | 2,411.100                             | 969.41                     | 134.57                               | 4,774.2            | 39,132                              | 6.43                                  | 4.23           |
| #2  | 1,497.000                                 | 3,908.100                             | 1,059.91                   | 257.90                               | 6,149.0            | 25,315                              | 0.21                                  | 0.14           |
| #3  | 862.700                                   | 4,770.800                             | 1,261.81                   | 320.10                               | 6,643.4            | 19,781                              | 0.07                                  | 0.05           |
| #4  | 0.000                                     | 4,770.800                             | 1,261.81                   | 320.10                               | 6,643.4            | 19,781                              | 0.07                                  | 0.05           |
| #9  | 425.500                                   | 5,196.300                             | 1,293.61                   | 353.35                               | 6,647.8            | 18,054                              | 0.00                                  | 0.00           |
| #11 | 0.000                                     | 12,411.000                            | 3,374.35                   | 900.14                               | 26,696.5           | 36,391                              | 0.09                                  | 0.05           |
| #21 | 1,080.800                                 | 13,491.800                            | 3,438.75                   | 971.45                               | 26,631.1           | 34,667                              | 0.04                                  | 0.02           |
| #18 | 848.500                                   | 848.500                               | 434.05                     | 59.62                                | 885.6              | 17,901                              | 0.19                                  | 0.12           |
| #17 | 182.200                                   | 182.200                               | 254.12                     | 16.35                                | 256.5              | 16,193                              | 1.00                                  | 0.71           |
| #19 | 0.000                                     | 1,030.700                             | 603.09                     | 75.97                                | 1,142.2            | 16,875                              | 0.37                                  | 0.24           |
| #15 | 1,992.700                                 | 1,992.700                             | 996.33                     | 133.89                               | 5,389.3            | 48,450                              | 2.83                                  | 1.71           |
| #12 | 3,494.500                                 | 3,494.500                             | 739.31                     | 126.25                               | 2,083.8            | 17,988                              | 8.18                                  | 5.49           |
| #13 | 2,720.700                                 | 6,215.200                             | 1,297.09                   | 224.49                               | 4,182.2            | 19,433                              | 9.44                                  | 6.62           |
| #14 | 5,096.800                                 | 11,312.000                            | 1,550.26                   | 540.08                               | 12,534.2           | 88,446                              | 3.03                                  | 0.57           |
| #16 | 876.500                                   | 14,181.200                            | 1,948.63                   | 751.77                               | 21,034.7           | 61,015                              | 2.67                                  | 0.89           |
| #20 | 681.900                                   | 15,893.800                            | 2,001.09                   | 886.93                               | 22,465.7           | 46,594                              | 1.11                                  | 0.44           |
| #22 | 0.000                                     | 29,385.600                            | 5,214.55                   | 1,858.38                             | 49,096.9           | 36,590                              | 0.42                                  | 0.22           |
| #23 | 752.900                                   | 30,138.500                            | 5,165.20                   | 1,905.61                             | 48,634.1           | 35,589                              | 0.04                                  | 0.02           |
| #35 | 0.000                                     | 48,329.700                            | 6,464.76                   | 2,680.51                             | 67,462.3           | 33,006                              | 0.09                                  | 0.05           |
| #36 | 730.590                                   | 49,060.290                            | 6,428.18                   | 2,717.89                             | 67,548.5           | 38,350                              | 0.03                                  | 0.01           |
| #37 | 2,208.500                                 | 51,268.790                            | 6,324.95                   | 2,836.00                             | 67,180.5           | 37,669                              | 0.39                                  | 0.18           |



***Particle Size Distribution(s) at Each Structure***

***Structure #30:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 85.557%  |
| 0.0500    | 48.482%  |
| 0.0020    | 31.371%  |
| 0.0010    | 0.000%   |

***Structure #28:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 96.519%  |
| 0.0010    | 0.000%   |

***Structure #26:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 70.975%  |
| 0.0020    | 45.925%  |
| 0.0010    | 0.000%   |

***Structure #24:***

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 91.071%  |
| 0.0020    | 70.221%  |
| 0.0010    | 0.000%   |

**Structure #25:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 83.836%  |
| 0.0500    | 74.932%  |
| 0.0020    | 66.501%  |
| 0.0010    | 0.000%   |

**Structure #27:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 73.416%  |
| 0.0500    | 52.287%  |
| 0.0020    | 39.482%  |
| 0.0010    | 0.000%   |

**Structure #29:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 93.366%  |
| 0.0500    | 88.050%  |
| 0.0020    | 77.980%  |
| 0.0010    | 0.000%   |

**Structure #32:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 98.135%  |
| 0.0500    | 93.024%  |
| 0.0020    | 82.321%  |
| 0.0010    | 0.000%   |

**Structure #31:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 93.833%  |
| 0.0010    | 0.000%   |

**Structure #33 (Inlet to North Fork Diversion):**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 98.500%  |
| 0.0500    | 94.389%  |
| 0.0020    | 84.573%  |
| 0.0010    | 0.000%   |

**Structure #34:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 97.937%  |
| 0.0010    | 0.000%   |

**Structure #5:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 97.755%  |
| 0.0500    | 89.765%  |
| 0.0020    | 81.592%  |
| 0.0010    | 0.000%   |

**Structure #6:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 98.129%  |
| 0.0010    | 0.000%   |

**Structure #7:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |



**Structure #8:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #10:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.672%  |
| 0.0020    | 99.485%  |
| 0.0010    | 0.000%   |

**Structure #1:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 92.714%  |
| 0.0500    | 81.846%  |
| 0.0020    | 76.465%  |
| 0.0010    | 0.000%   |

**Structure #2:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 97.665%  |
| 0.0010    | 0.000%   |

**Structure #3:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.062%  |
| 0.0010    | 0.000%   |

**Structure #4:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.062%  |
| 0.0010    | 0.000%   |

**Structure #9:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 100.000% |
| 0.0010    | 0.000%   |

**Structure #11:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.753%  |
| 0.0020    | 99.613%  |
| 0.0010    | 0.000%   |

**Structure #21:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.702%  |
| 0.0010    | 0.000%   |

**Structure #18:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 96.995%  |
| 0.0010    | 0.000%   |

**Structure #17:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 82.629%  |
| 0.0010    | 0.000%   |

**Structure #19:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 93.769%  |
| 0.0010    | 0.000%   |

**Structure #15:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 94.463%  |
| 0.0020    | 90.477%  |
| 0.0010    | 0.000%   |

**Structure #12:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 78.989%  |
| 0.0500    | 51.223%  |
| 0.0020    | 33.145%  |
| 0.0010    | 0.000%   |

**Structure #13:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 75.897%  |
| 0.0500    | 46.580%  |
| 0.0020    | 30.140%  |
| 0.0010    | 0.000%   |



**Structure #14:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 99.621%  |
| 0.0020    | 90.811%  |
| 0.0010    | 0.000%   |

**Structure #16:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 98.395%  |
| 0.0020    | 89.680%  |
| 0.0010    | 0.000%   |

**Structure #20:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 93.292%  |
| 0.0010    | 0.000%   |

**Structure #22:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 96.769%  |
| 0.0010    | 0.000%   |

**Structure #23:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.713%  |
| 0.0010    | 0.000%   |

**Structure #35:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.217%  |
| 0.0010    | 0.000%   |

**Structure #36:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 100.000% |
| 0.0500    | 100.000% |
| 0.0020    | 99.777%  |
| 0.0010    | 0.000%   |

**Structure #37:**

| Size (mm) | In/Out   |
|-----------|----------|
| 2.0000    | 100.000% |
| 0.1000    | 99.797%  |
| 0.0500    | 98.990%  |
| 0.0020    | 98.362%  |
| 0.0010    | 0.000%   |

### ***Subwatershed Hydrology Detail:***

| Stru #     | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|------------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #30        | 1        | 476.400           | 1.131              | 0.000        | 0.000  | 73.100       | M   | 86.92                | 10.783                |
|            | <b>Σ</b> | <b>476.400</b>    |                    |              |        |              |     | <b>86.92</b>         | <b>10.783</b>         |
| #28        | 1        | 772.300           | 0.657              | 0.523        | 0.334  | 90.400       | M   | 752.74               | 59.308                |
|            | 2        | 445.600           | 0.587              | 0.000        | 0.000  | 90.400       | M   | 467.33               | 34.234                |
|            | <b>Σ</b> | <b>1,217.900</b>  |                    |              |        |              |     | <b>832.25</b>        | <b>93.542</b>         |
| #26        | 1        | 447.600           | 2.192              | 0.000        | 0.000  | 74.200       | M   | 52.15                | 11.131                |
|            | 2        | 2,038.800         | 3.000              | 0.000        | 0.000  | 77.000       | M   | 230.69               | 63.525                |
|            | <b>Σ</b> | <b>2,486.400</b>  |                    |              |        |              |     | <b>275.55</b>        | <b>74.655</b>         |
| #24        | 1        | 2,607.500         | 5.367              | 2.377        | 0.305  | 75.200       | M   | 153.86               | 70.433                |
|            | 2        | 2,331.900         | 4.813              | 2.431        | 0.304  | 74.700       | M   | 144.95               | 60.455                |
|            | 3        | 1,758.500         | 2.231              | 1.788        | 0.297  | 76.200       | M   | 240.04               | 51.476                |
|            | 4        | 1,363.900         | 2.618              | 0.000        | 0.000  | 77.000       | M   | 173.49               | 42.495                |
|            | <b>Σ</b> | <b>8,061.800</b>  |                    |              |        |              |     | <b>386.57</b>        | <b>224.858</b>        |
| #25        | 1        | 515.200           | 0.990              | 0.342        | 0.357  | 78.200       | M   | 161.95               | 17.593                |
|            | 2        | 130.500           | 0.787              | 0.342        | 0.357  | 78.100       | M   | 48.57                | 4.423                 |
|            | 3        | 370.000           | 0.516              | 0.000        | 0.000  | 85.700       | M   | 316.29               | 21.215                |
|            | <b>Σ</b> | <b>9,077.500</b>  |                    |              |        |              |     | <b>393.25</b>        | <b>268.089</b>        |
| #27        | 1        | 354.400           | 0.612              | 1.233        | 0.337  | 83.100       | M   | 227.69               | 17.118                |
|            | 2        | 305.200           | 0.529              | 1.054        | 0.328  | 84.000       | M   | 229.89               | 15.662                |
|            | 3        | 289.800           | 0.692              | 0.551        | 0.328  | 75.500       | M   | 96.22                | 8.028                 |
|            | 4        | 253.000           | 0.361              | 0.551        | 0.328  | 79.400       | M   | 174.11               | 9.470                 |
|            | 5        | 581.300           | 0.980              | 0.000        | 0.000  | 82.300       | M   | 249.37               | 26.582                |
|            | <b>Σ</b> | <b>13,347.600</b> |                    |              |        |              |     | <b>724.52</b>        | <b>419.604</b>        |
| #29        | 1        | 508.800           | 0.409              | 0.416        | 0.312  | 89.500       | M   | 621.45               | 37.080                |
|            | 2        | 233.200           | 0.521              | 0.291        | 0.312  | 91.600       | M   | 281.23               | 19.263                |
|            | 3        | 224.000           | 0.467              | 0.000        | 0.000  | 90.000       | M   | 262.75               | 16.791                |
|            | <b>Σ</b> | <b>15,531.500</b> |                    |              |        |              |     | <b>1,383.20</b>      | <b>586.280</b>        |
| #32        | 1        | 293.700           | 0.576              | 0.000        | 0.000  | 93.000       | M   | 361.60               | 26.368                |
|            | <b>Σ</b> | <b>16,301.600</b> |                    |              |        |              |     | <b>1,413.07</b>      | <b>623.431</b>        |
| #31        | 1        | 431.100           | 0.588              | 0.450        | 0.336  | 91.500       | M   | 480.90               | 35.394                |
|            | 2        | 325.800           | 0.432              | 0.149        | 0.327  | 93.000       | M   | 469.94               | 29.285                |
|            | 3        | 200.200           | 0.373              | 0.000        | 0.000  | 92.900       | M   | 306.19               | 17.858                |
|            | <b>Σ</b> | <b>957.100</b>    |                    |              |        |              |     | <b>785.51</b>        | <b>82.537</b>         |
| <b>#33</b> | <b>Σ</b> | <b>17,258.700</b> |                    |              |        |              |     | <b>1,524.15</b>      | <b>705.968</b>        |



| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS  | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|------|----------------------|-----------------------|
| #34    | 1        | 91.700            | 0.244              | 0.965        | 0.300  | 92.300       | M    | 157.04               | 7.958                 |
|        | 2        | 105.200           | 0.256              | 0.965        | 0.300  | 93.000       | M    | 182.91               | 9.495                 |
|        | 3        | 735.600           | 0.885              | 0.000        | 0.000  | 88.900       | M    | 529.41               | 51.478                |
|        | <b>Σ</b> | <b>18,191.200</b> |                    |              |        |              |      | <b>1,541.21</b>      | <b>774.899</b>        |
| #5     | 1        | 503.600           | 0.618              | 0.000        | 0.000  | 87.600       | M    | 431.41               | 32.518                |
|        | 2        | 406.500           | 0.388              | 0.501        | 0.350  | 84.800       | M    | 387.10               | 21.979                |
|        | 3        | 439.600           | 0.342              | 0.681        | 0.347  | 87.800       | M    | 530.42               | 28.890                |
|        | 4        | 162.600           | 0.280              | 0.681        | 0.347  | 86.000       | M    | 192.17               | 9.534                 |
|        | 5        | 294.100           | 0.375              | 1.021        | 0.348  | 92.000       | M    | 427.35               | 24.849                |
|        | 6        | 216.600           | 0.272              | 1.018        | 0.348  | 90.100       | M    | 322.06               | 16.408                |
|        | <b>Σ</b> | <b>2,023.000</b>  |                    |              |        |              |      | <b>1,349.47</b>      | <b>134.179</b>        |
| #6     | 1        | 149.100           | 0.331              | 0.000        | 0.000  | 92.600       | M    | 234.00               | 13.116                |
|        | 2        | 245.000           | 0.529              | 0.192        | 0.328  | 88.100       | M    | 239.24               | 16.340                |
|        | 3        | 276.200           | 0.450              | 0.461        | 0.319  | 89.500       | M    | 321.32               | 20.072                |
|        | 4        | 158.400           | 0.380              | 1.385        | 0.185  | 93.000       | M    | 241.78               | 14.207                |
|        | 5        | 206.200           | 0.402              | 0.796        | 0.320  | 89.400       | M    | 252.54               | 14.933                |
|        | 6        | 414.000           | 0.430              | 1.066        | 0.323  | 87.200       | M    | 431.96               | 26.139                |
|        | 7        | 294.300           | 0.535              | 1.066        | 0.323  | 86.400       | M    | 256.99               | 17.634                |
|        | <b>Σ</b> | <b>3,766.200</b>  |                    |              |        |              |      | <b>1,527.16</b>      | <b>256.621</b>        |
| #7     | 1        | 731.700           | 1.274              | 0.000        | 0.000  | 93.000       | M    | 510.48               | 65.589                |
|        | 2        | 445.800           | 1.043              | 0.000        | 0.000  | 93.000       | M    | 363.36               | 39.948                |
|        | 3        | 270.800           | 0.804              | 0.000        | 0.000  | 93.000       | M    | 267.12               | 24.274                |
|        | 4        | 78.900            | 0.267              | 1.035        | 0.328  | 93.000       | M    | 135.40               | 7.113                 |
|        | 5        | 154.900           | 0.310              | 1.071        | 0.326  | 93.000       | M    | 253.21               | 13.947                |
|        | 6        | 101.400           | 0.288              | 1.164        | 0.328  | 92.900       | M    | 169.28               | 9.070                 |
|        | 7        | 117.700           | 0.298              | 1.344        | 0.329  | 92.200       | M    | 188.00               | 10.096                |
|        | 8        | 494.100           | 0.518              | 1.344        | 0.329  | 91.300       | M    | 588.05               | 40.082                |
|        | <b>Σ</b> | <b>6,161.500</b>  |                    |              |        |              |      | <b>2,444.68</b>      | <b>466.740</b>        |
| #8     | 1        | 0.000             | 0.000              | 0.000        | 0.000  | 1.000        | 0.00 | 0.000                |                       |
|        | <b>Σ</b> | <b>6,161.500</b>  |                    |              |        |              |      | <b>2,444.68</b>      | <b>466.740</b>        |
| #10    | 1        | 355.500           | 1.286              | 0.000        | 0.000  | 93.000       | M    | 246.17               | 31.859                |
|        | 2        | 307.100           | 1.282              | 0.668        | 0.305  | 83.200       | M    | 113.34               | 14.918                |
|        | 3        | 147.300           | 1.245              | 0.517        | 0.303  | 90.600       | M    | 90.51                | 11.434                |
|        | 4        | 126.400           | 0.585              | 0.517        | 0.303  | 93.000       | M    | 154.15               | 11.351                |
|        | 5        | 116.900           | 1.179              | 0.621        | 0.305  | 93.000       | M    | 86.70                | 10.480                |
|        | <b>Σ</b> | <b>7,214.700</b>  |                    |              |        |              |      | <b>2,478.16</b>      | <b>546.782</b>        |
| #1     | 1        | 557.400           | 0.941              | 0.000        | 0.000  | 83.600       | M    | 269.99               | 27.820                |
|        | 2        | 169.600           | 1.616              | 0.677        | 0.333  | 93.000       | M    | 97.53                | 15.200                |
|        | 3        | 636.400           | 1.842              | 0.729        | 0.333  | 81.000       | M    | 148.68               | 26.594                |
|        | 4        | 223.400           | 0.846              | 1.005        | 0.336  | 84.100       | M    | 121.50               | 11.530                |

| Stru # | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS    | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|-------------------|--------------------|--------------|--------|--------------|--------|----------------------|-----------------------|
|        | 5        | 77.700            | 0.330              | 1.392        | 0.341  | 81.400       | M      | 64.44                | 3.356                 |
|        | 6        | 746.600           | 0.678              | 1.392        | 0.341  | 88.200       | M      | 623.33               | 50.074                |
|        | <b>Σ</b> | <b>2,411.100</b>  |                    |              |        |              |        | <b>969.41</b>        | <b>134.574</b>        |
| #2     | 1        | 257.000           | 0.423              | 0.000        | 0.000  | 93.000       | M      | 374.44               | 23.118                |
|        | 2        | 180.500           | 0.562              | 0.478        | 0.281  | 91.800       | M      | 210.48               | 15.074                |
|        | 3        | 200.700           | 0.687              | 0.574        | 0.283  | 93.000       | M      | 220.68               | 18.000                |
|        | 4        | 438.600           | 0.811              | 0.574        | 0.283  | 93.000       | M      | 429.99               | 39.326                |
|        | 5        | 420.200           | 1.247              | 0.801        | 0.293  | 88.000       | M      | 218.78               | 27.811                |
|        | <b>Σ</b> | <b>3,908.100</b>  |                    |              |        |              |        | <b>1,059.91</b>      | <b>257.902</b>        |
| #3     | 1        | 172.600           | 0.443              | 0.000        | 0.000  | 93.000       | M      | 245.91               | 15.489                |
|        | 2        | 311.200           | 0.890              | 0.000        | 0.000  | 88.900       | M      | 223.03               | 21.783                |
|        | 3        | 378.900           | 0.632              | 0.209        | 0.314  | 87.900       | M      | 325.75               | 24.926                |
|        | <b>Σ</b> | <b>4,770.800</b>  |                    |              |        |              |        | <b>1,261.81</b>      | <b>320.099</b>        |
| #4     | <b>Σ</b> | <b>4,770.800</b>  |                    |              |        |              |        | <b>1,261.81</b>      | <b>320.099</b>        |
| #9     | 1        | 425.500           | 0.830              | 0.000        | 0.000  | 90.700       | M      | 358.63               | 33.255                |
|        | <b>Σ</b> | <b>5,196.300</b>  |                    |              |        |              |        | <b>1,293.61</b>      | <b>353.354</b>        |
| #11    | <b>Σ</b> | <b>12,411.000</b> |                    |              |        |              |        | <b>3,374.35</b>      | <b>900.137</b>        |
| #21    | 1        | 272.800           | 0.819              | 0.000        | 0.000  | 86.900       | M      | 183.13               | 16.861                |
|        | 2        | 230.500           | 0.388              | 0.694        | 0.266  | 89.200       | M      | 283.84               | 16.451                |
|        | 3        | 181.100           | 0.289              | 0.877        | 0.256  | 91.300       | M      | 280.07               | 14.716                |
|        | 4        | 396.400           | 0.939              | 0.877        | 0.256  | 86.100       | M      | 227.82               | 23.280                |
|        | <b>Σ</b> | <b>13,491.800</b> |                    |              |        |              |        | <b>3,438.75</b>      | <b>971.445</b>        |
| #18    | 1        | 301.700           | 0.652              | 0.000        | 0.000  | 93.000       | M      | 343.42               | 27.082                |
|        | 2        | 546.800           | 0.768              | 0.561        | 0.320  | 86.300       | M      | 370.15               | 32.542                |
|        | <b>Σ</b> | <b>848.500</b>    |                    |              |        |              |        | <b>434.05</b>        | <b>59.624</b>         |
| #17    | 1        | 182.200           | 0.462              | 0.000        | 0.000  | 93.000       | M      | 254.12               | 16.351                |
|        | <b>Σ</b> | <b>182.200</b>    |                    |              |        |              |        | <b>254.12</b>        | <b>16.351</b>         |
| #19    | <b>Σ</b> | <b>1,030.700</b>  |                    |              |        |              |        | <b>603.09</b>        | <b>75.975</b>         |
| #15    | 1        | 437.400           | 0.803              | 0.000        | 0.000  | 91.300       | M      | 391.26               | 35.417                |
|        | 2        | 549.000           | 0.637              | 0.654        | 0.327  | 91.300       | M      | 575.39               | 44.478                |
|        | 3        | 1,006.300         | 1.023              | 0.768        | 0.331  | 84.700       | M      | 492.78               | 53.997                |
|        | <b>Σ</b> | <b>1,992.700</b>  |                    |              |        |              |        | <b>996.33</b>        | <b>133.892</b>        |
| #12    | 1        | 517.800           | 0.791              | 0.000        | 0.000  | 81.900       | M      | 253.96               | 23.036                |
|        | 2        | 229.000           | 0.571              | 0.043        | 0.418  | 80.100       | M      | 124.82               | 8.994                 |
|        | 3        | 592.700           | 0.706              | 0.044        | 0.417  | 81.500       | M      | 307.18               | 25.658                |
|        | 4        | 1,806.900         | 1.542              | 0.487        | 0.362  | 76.700       | M      | 350.97               | 55.002                |
|        | 5        | 348.100           | 0.618              | 0.487        | 0.362  | 80.000       | 178.31 | 13.561               |                       |

| Stru #   | SWS #    | SWS Area (ac)     | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|----------|----------|-------------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| <b>Σ</b> |          | <b>3,494.500</b>  |                    |              |        |              |     | <b>739.31</b>        | <b>126.252</b>        |
| #13      | 1        | 411.600           | 0.725              | 0.000        | 0.000  | 79.700       | M   | 183.88               | 15.700                |
|          | 2        | 636.400           | 0.774              | 0.322        | 0.336  | 80.700       | M   | 291.36               | 26.065                |
|          | 3        | 319.000           | 0.575              | 0.685        | 0.318  | 85.500       | M   | 251.02               | 18.050                |
|          | 4        | 231.700           | 0.314              | 0.923        | 0.328  | 80.400       | M   | 183.82               | 9.322                 |
|          | 5        | 1,122.000         | 1.308              | 0.923        | 0.328  | 74.700       | M   | 210.47               | 29.098                |
| <b>Σ</b> |          | <b>6,215.200</b>  |                    |              |        |              |     | <b>1,297.09</b>      | <b>224.487</b>        |
| #14      | 1        | 405.900           | 0.384              | 0.000        | 0.000  | 90.800       | M   | 546.94               | 31.913                |
|          | 2        | 411.100           | 0.452              | 0.707        | 0.308  | 90.700       | M   | 510.03               | 32.137                |
|          | 3        | 787.400           | 0.658              | 0.975        | 0.307  | 91.400       | M   | 812.59               | 64.232                |
|          | 4        | 144.200           | 0.341              | 1.716        | 0.310  | 86.200       | M   | 159.03               | 8.568                 |
|          | 5        | 343.800           | 0.289              | 1.970        | 0.312  | 86.500       | M   | 413.08               | 20.780                |
|          | 6        | 392.800           | 0.806              | 2.107        | 0.316  | 81.900       | M   | 190.01               | 17.476                |
|          | 7        | 528.200           | 0.518              | 2.544        | 0.316  | 87.200       | M   | 494.68               | 33.311                |
|          | 8        | 890.900           | 1.253              | 2.544        | 0.316  | 83.500       | M   | 341.95               | 44.165                |
|          | 9        | 741.400           | 1.076              | 3.047        | 0.316  | 84.800       | M   | 351.34               | 40.044                |
|          | 10       | 451.100           | 0.916              | 3.354        | 0.316  | 83.900       | M   | 227.77               | 22.972                |
| <b>Σ</b> |          | <b>11,312.000</b> |                    |              |        |              |     | <b>1,550.26</b>      | <b>540.085</b>        |
| #16      | 1        | 329.600           | 0.641              | 0.000        | 0.000  | 93.000       | M   | 379.34               | 29.573                |
|          | 2        | 348.400           | 0.542              | 0.509        | 0.286  | 92.500       | M   | 432.31               | 30.323                |
|          | 3        | 198.500           | 0.266              | 0.943        | 0.279  | 93.000       | M   | 340.98               | 17.895                |
| <b>Σ</b> |          | <b>14,181.200</b> |                    |              |        |              |     | <b>1,948.63</b>      | <b>751.769</b>        |
| #20      | 1        | 296.300           | 0.667              | 0.000        | 0.000  | 91.700       | M   | 308.29               | 24.609                |
|          | 2        | 385.600           | 0.713              | 0.476        | 0.440  | 93.000       | M   | 413.48               | 34.579                |
| <b>Σ</b> |          | <b>15,893.800</b> |                    |              |        |              |     | <b>2,001.09</b>      | <b>886.931</b>        |
| #22      | <b>Σ</b> | <b>29,385.600</b> |                    |              |        |              |     | <b>5,214.55</b>      | <b>1,858.376</b>      |
| #23      | 1        | 442.400           | 0.960              | 0.000        | 0.000  | 85.300       | M   | 236.99               | 24.672                |
|          | 2        | 310.500           | 0.538              | 0.559        | 0.291  | 89.500       | M   | 326.13               | 22.562                |
| <b>Σ</b> |          | <b>30,138.500</b> |                    |              |        |              |     | <b>5,165.20</b>      | <b>1,905.611</b>      |
| #35      | <b>Σ</b> | <b>48,329.700</b> |                    |              |        |              |     | <b>6,464.76</b>      | <b>2,680.510</b>      |
| #36      | 1        | 298.200           | 0.987              | 0.000        | 0.000  | 85.000       | M   | 153.24               | 16.314                |
|          | 2        | 196.800           | 0.441              | 0.000        | 0.000  | 87.900       | M   | 211.08               | 12.962                |
|          | 3        | 235.590           | 0.885              | 0.166        | 0.372  | 78.300       | M   | 81.43                | 8.105                 |
| <b>Σ</b> |          | <b>49,060.290</b> |                    |              |        |              |     | <b>6,428.18</b>      | <b>2,717.891</b>      |
| #37      | 1        | 744.000           | 1.756              | 0.000        | 0.000  | 84.800       | M   | 236.22               | 40.167                |
|          | 2        | 296.000           | 0.439              | 1.780        | 0.243  | 87.800       | M   | 316.41               | 19.381                |
|          | 3        | 237.700           | 0.333              | 1.649        | 0.246  | 85.500       | M   | 254.20               | 13.499                |
|          | 4        | 561.400           | 1.502              | 1.780        | 0.243  | 84.100       | M   | 193.60               | 28.954                |



| Stru #   | SWS # | SWS Area (ac) | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |                  |
|----------|-------|---------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|------------------|
|          | 5     | 369.400       | 0.817              | 2.236        | 0.284  | 81.600       | M   | 173.21               | 16.105                |                  |
| <b>Σ</b> |       |               |                    |              |        |              |     | <b>51,268.790</b>    | <b>6,324.95</b>       | <b>2,835.999</b> |

***Subwatershed Sedimentology Detail:***

| Stru #   | SWS # | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|----------|-------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #30      | 1     | 0.095  | 200.00 | 3.80  | 0.3720 | 1.0000 | 2    | 97.1            | 9,320                      | 4.41                        | 3.12        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>97.1</b>     | <b>9,320</b>               | <b>4.41</b>                 | <b>3.12</b> |
| #28      | 1     | 0.187  | 100.00 | 10.10 | 0.3750 | 1.0000 | 3    | 4,338.2         | 73,262                     | 0.83                        | 0.60        |
|          | 2     | 0.196  | 100.00 | 10.20 | 0.3930 | 1.0000 | 3    | 2,720.2         | 80,011                     | 2.01                        | 1.43        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>5,541.5</b>  | <b>59,612</b>              | <b>0.74</b>                 | <b>0.53</b> |
| #26      | 1     | 0.155  | 400.00 | 1.40  | 0.3480 | 1.0000 | 2    | 57.3            | 5,194                      | 1.90                        | 1.38        |
|          | 2     | 0.155  | 300.00 | 2.40  | 0.3340 | 1.0000 | 2    | 491.5           | 7,755                      | 2.47                        | 1.81        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>548.8</b>    | <b>7,278</b>               | <b>2.35</b>                 | <b>1.74</b> |
| #24      | 1     | 0.128  | 300.00 | 2.30  | 0.3360 | 1.0000 | 2    | 331.9           | 4,689                      | 0.69                        | 0.52        |
|          | 2     | 0.136  | 300.00 | 2.70  | 0.3440 | 1.0000 | 2    | 370.4           | 6,080                      | 1.07                        | 0.79        |
|          | 3     | 0.107  | 300.00 | 2.30  | 0.3330 | 1.0000 | 2    | 295.9           | 5,731                      | 2.16                        | 1.59        |
|          | 4     | 0.163  | 400.00 | 1.60  | 0.3210 | 1.0000 | 2    | 258.2           | 6,111                      | 2.13                        | 1.55        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>949.6</b>    | <b>4,970</b>               | <b>0.73</b>                 | <b>0.46</b> |
| #25      | 1     | 0.125  | 400.00 | 1.90  | 0.3440 | 1.0000 | 2    | 144.5           | 8,472                      | 4.38                        | 3.12        |
|          | 2     | 0.124  | 300.00 | 2.60  | 0.3280 | 1.0000 | 2    | 39.0            | 9,182                      | 4.99                        | 3.51        |
|          | 3     | 0.122  | 175.00 | 4.90  | 0.2660 | 1.0000 | 2    | 389.9           | 19,291                     | 11.68                       | 8.13        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>1,185.4</b>  | <b>15,996</b>              | <b>3.69</b>                 | <b>0.75</b> |
| #27      | 1     | 0.127  | 175.00 | 5.90  | 0.3160 | 1.0000 | 2    | 424.5           | 25,447                     | 14.88                       | 10.58       |
|          | 2     | 0.122  | 150.00 | 7.50  | 0.2920 | 1.0000 | 2    | 419.7           | 27,541                     | 16.50                       | 11.70       |
|          | 3     | 0.070  | 125.00 | 8.40  | 0.3270 | 1.0000 | 2    | 119.4           | 15,575                     | 8.52                        | 5.95        |
|          | 4     | 0.097  | 125.00 | 9.60  | 0.3170 | 1.0000 | 2    | 301.0           | 33,444                     | 20.45                       | 14.14       |
|          | 5     | 0.126  | 125.00 | 8.90  | 0.3290 | 1.0000 | 2    | 789.9           | 30,401                     | 16.28                       | 11.59       |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>3,780.3</b>  | <b>31,465</b>              | <b>13.44</b>                | <b>2.82</b> |
| #29      | 1     | 0.190  | 125.00 | 9.80  | 0.3930 | 1.0000 | 3    | 3,300.2         | 89,222                     | 5.11                        | 3.64        |
|          | 2     | 0.203  | 125.00 | 8.90  | 0.3940 | 1.0000 | 3    | 1,359.9         | 71,018                     | 3.10                        | 2.22        |
|          | 3     | 0.193  | 125.00 | 8.40  | 0.3940 | 1.0000 | 3    | 1,052.2         | 63,883                     | 3.03                        | 2.14        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>15,023.3</b> | <b>74,082</b>              | <b>9.73</b>                 | <b>2.44</b> |
| #32      | 1     | 0.210  | 150.00 | 7.70  | 0.3990 | 1.0000 | 3    | 1,746.7         | 66,745                     | 2.70                        | 1.93        |
| <b>Σ</b> |       |        |        |       |        |        |      | <b>16,148.1</b> | <b>65,499</b>              | <b>6.14</b>                 | <b>1.76</b> |

| Stru #     | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|------------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| #31        | 1        | 0.204  | 125.00 | 8.70  | 0.3620 | 1.0000 | 3    | 2,300.9         | 65,305                     | 1.98                        | 1.42        |
|            | 2        | 0.210  | 150.00 | 7.30  | 0.3990 | 1.0000 | 3    | 2,036.7         | 70,003                     | 4.74                        | 3.39        |
|            | 3        | 0.210  | 175.00 | 4.50  | 0.3980 | 1.0000 | 3    | 826.7           | 47,117                     | 3.68                        | 2.62        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>3,927.1</b>  | <b>43,239</b>              | <b>0.95</b>                 | <b>0.75</b> |
| <b>#33</b> | <b>Σ</b> |        |        |       |        |        |      | <b>20,075.2</b> | <b>57,140</b>              | <b>4.55</b>                 | <b>1.65</b> |
| #34        | 1        | 0.189  | 175.00 | 4.60  | 0.2250 | 1.0000 | 3    | 187.0           | 23,363                     | 2.32                        | 1.70        |
|            | 2        | 0.206  | 175.00 | 5.10  | 0.3620 | 1.0000 | 3    | 435.3           | 45,146                     | 4.46                        | 3.28        |
|            | 3        | 0.176  | 175.00 | 4.20  | 0.2510 | 1.0000 | 3    | 1,007.3         | 20,005                     | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>18,828.3</b> | <b>47,805</b>              | <b>0.35</b>                 | <b>0.13</b> |
| #5         | 1        | 0.149  | 75.00  | 12.50 | 0.3230 | 1.0000 | 3    | 1,761.5         | 55,417                     | 0.26                        | 0.18        |
|            | 2        | 0.133  | 75.00  | 15.80 | 0.3190 | 1.0000 | 2    | 1,581.0         | 73,701                     | 45.73                       | 32.04       |
|            | 3        | 0.103  | 100.00 | 11.00 | 0.2030 | 1.0000 | 3    | 800.7           | 28,422                     | 1.85                        | 1.32        |
|            | 4        | 0.093  | 75.00  | 13.80 | 0.2130 | 1.0000 | 2    | 263.1           | 28,361                     | 18.06                       | 12.80       |
|            | 5        | 0.123  | 100.00 | 11.00 | 0.1370 | 1.0000 | 3    | 527.0           | 21,481                     | 1.58                        | 1.14        |
|            | 6        | 0.149  | 75.00  | 14.70 | 0.1990 | 1.0000 | 3    | 771.8           | 47,043                     | 4.10                        | 2.97        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>4,549.4</b>  | <b>44,265</b>              | <b>4.91</b>                 | <b>2.73</b> |
| #6         | 1        | 0.208  | 175.00 | 4.30  | 0.3980 | 1.0000 | 3    | 566.5           | 43,809                     | 3.67                        | 2.62        |
|            | 2        | 0.183  | 175.00 | 5.40  | 0.3910 | 1.0000 | 3    | 696.7           | 43,787                     | 1.15                        | 0.81        |
|            | 3        | 0.188  | 150.00 | 7.60  | 0.3900 | 1.0000 | 3    | 1,212.9         | 61,278                     | 2.99                        | 2.13        |
|            | 4        | 0.210  | 150.00 | 6.30  | 0.3990 | 1.0000 | 3    | 814.1           | 55,762                     | 4.31                        | 3.20        |
|            | 5        | 0.185  | 125.00 | 8.10  | 0.3860 | 1.0000 | 3    | 852.0           | 57,331                     | 3.34                        | 2.40        |
|            | 6        | 0.104  | 100.00 | 11.30 | 0.2240 | 1.0000 | 3    | 781.6           | 30,493                     | 1.34                        | 0.95        |
|            | 7        | 0.164  | 100.00 | 11.20 | 0.3740 | 1.0000 | 3    | 1,220.4         | 69,527                     | 1.18                        | 0.84        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>8,062.5</b>  | <b>38,199</b>              | <b>0.25</b>                 | <b>0.15</b> |
| #7         | 1        | 0.208  | 150.00 | 7.80  | 0.3780 | 1.0000 | 3    | 3,355.9         | 50,966                     | 0.00                        | 0.00        |
|            | 2        | 0.209  | 100.00 | 10.20 | 0.3940 | 1.0000 | 3    | 2,757.2         | 68,474                     | 0.00                        | 0.00        |
|            | 3        | 0.210  | 150.00 | 6.70  | 0.3990 | 1.0000 | 3    | 1,232.8         | 51,046                     | 0.00                        | 0.00        |
|            | 4        | 0.210  | 100.00 | 11.50 | 0.3990 | 1.0000 | 3    | 724.5           | 98,573                     | 9.53                        | 7.00        |
|            | 5        | 0.210  | 150.00 | 7.10  | 0.3990 | 1.0000 | 3    | 925.0           | 65,247                     | 5.79                        | 4.23        |
|            | 6        | 0.209  | 150.00 | 7.90  | 0.3990 | 1.0000 | 3    | 640.0           | 69,035                     | 6.39                        | 4.69        |
|            | 7        | 0.206  | 75.00  | 15.50 | 0.3990 | 1.0000 | 3    | 1,289.7         | 122,298                    | 10.82                       | 7.97        |
|            | 8        | 0.202  | 75.00  | 14.50 | 0.3980 | 1.0000 | 3    | 4,762.8         | 115,519                    | 4.96                        | 3.61        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>20,462.9</b> | <b>48,159</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #8         | 1        | 0.000  | 0.00   | 0.00  | 0.0000 | 1.0000 | 0    | 0.0             | 1                          | 0.00                        | 0.00        |
|            | <b>Σ</b> |        |        |       |        |        |      | <b>20,462.9</b> | <b>48,159</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #10        | 1        | 0.190  | 300.00 | 2.70  | 0.1930 | 1.0000 | 3    | 272.9           | 8,677                      | 0.00                        | 0.00        |
|            | 2        | 0.153  | 200.00 | 3.50  | 0.3610 | 1.0000 | 2    | 195.6           | 13,269                     | 6.72                        | 4.86        |
|            | 3        | 0.189  | 200.00 | 3.70  | 0.3190 | 1.0000 | 3    | 170.7           | 15,060                     | 0.00                        | 0.00        |
|            | 4        | 0.190  | 300.00 | 2.10  | 0.1940 | 1.0000 | 3    | 94.4            | 8,517                      | 0.33                        | 0.24        |

| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 5        | 0.201  | 300.00 | 2.00  | 0.3030 | 1.0000 | 3    | 103.6           | 9,977                      | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>20,048.7</b> | <b>44,185</b>              | <b>0.15</b>                 | <b>0.09</b> |
| #1     | 1        | 0.157  | 150.00 | 6.80  | 0.3830 | 1.0000 | 2    | 974.2           | 35,729                     | 19.48                       | 13.87       |
|        | 2        | 0.210  | 150.00 | 6.60  | 0.3990 | 1.0000 | 3    | 531.9           | 34,819                     | 0.00                        | 0.00        |
|        | 3        | 0.149  | 200.00 | 3.90  | 0.3870 | 1.0000 | 2    | 363.4           | 13,724                     | 6.05                        | 4.41        |
|        | 4        | 0.169  | 175.00 | 4.70  | 0.3950 | 1.0000 | 2    | 321.0           | 28,267                     | 15.78                       | 11.32       |
|        | 5        | 0.157  | 100.00 | 10.10 | 0.3940 | 1.0000 | 2    | 193.1           | 58,434                     | 36.30                       | 25.77       |
|        | 6        | 0.175  | 75.00  | 12.60 | 0.2840 | 1.0000 | 3    | 2,876.0         | 57,530                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>4,774.2</b>  | <b>39,132</b>              | <b>6.43</b>                 | <b>4.23</b> |
| #2     | 1        | 0.190  | 150.00 | 7.90  | 0.1930 | 1.0000 | 3    | 741.4           | 32,869                     | 2.28                        | 1.62        |
|        | 2        | 0.184  | 175.00 | 4.80  | 0.2010 | 1.0000 | 3    | 286.7           | 19,447                     | 0.71                        | 0.51        |
|        | 3        | 0.202  | 200.00 | 3.90  | 0.3220 | 1.0000 | 3    | 410.8           | 23,164                     | 0.46                        | 0.33        |
|        | 4        | 0.203  | 150.00 | 7.40  | 0.3220 | 1.0000 | 3    | 1,809.1         | 46,104                     | 0.00                        | 0.00        |
|        | 5        | 0.181  | 175.00 | 5.10  | 0.3710 | 1.0000 | 3    | 794.1           | 28,621                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>6,149.0</b>  | <b>25,315</b>              | <b>0.21</b>                 | <b>0.14</b> |
| #3     | 1        | 0.190  | 175.00 | 5.20  | 0.1930 | 1.0000 | 3    | 339.6           | 22,578                     | 1.48                        | 1.05        |
|        | 2        | 0.177  | 175.00 | 4.20  | 0.2560 | 1.0000 | 3    | 393.3           | 18,469                     | 0.00                        | 0.00        |
|        | 3        | 0.166  | 175.00 | 4.30  | 0.2290 | 1.0000 | 3    | 449.8           | 18,658                     | 0.06                        | 0.04        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>6,643.4</b>  | <b>19,781</b>              | <b>0.07</b>                 | <b>0.05</b> |
| #4     | <b>Σ</b> |        |        |       |        |        |      | <b>6,643.4</b>  | <b>19,781</b>              | <b>0.07</b>                 | <b>0.05</b> |
| #9     | 1        | 0.189  | 175.00 | 4.44  | 0.1970 | 1.0000 | 3    | 562.9           | 17,305                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>6,647.8</b>  | <b>18,054</b>              | <b>0.00</b>                 | <b>0.00</b> |
| #11    | <b>Σ</b> |        |        |       |        |        |      | <b>26,696.5</b> | <b>36,391</b>              | <b>0.09</b>                 | <b>0.05</b> |
| #21    | 1        | 0.177  | 175.00 | 4.44  | 0.2560 | 1.0000 | 3    | 321.5           | 19,609                     | 0.00                        | 0.00        |
|        | 2        | 0.184  | 175.00 | 5.81  | 0.2210 | 1.0000 | 3    | 468.9           | 28,898                     | 1.75                        | 1.25        |
|        | 3        | 0.185  | 300.00 | 2.70  | 0.2180 | 1.0000 | 3    | 208.9           | 14,256                     | 1.25                        | 0.91        |
|        | 4        | 0.175  | 300.00 | 2.66  | 0.2690 | 1.0000 | 3    | 277.5           | 12,099                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>26,631.1</b> | <b>34,667</b>              | <b>0.04</b>                 | <b>0.02</b> |
| #18    | 1        | 0.193  | 300.00 | 2.80  | 0.2200 | 1.0000 | 3    | 358.9           | 13,605                     | 0.36                        | 0.26        |
|        | 2        | 0.173  | 175.00 | 4.70  | 0.3880 | 1.0000 | 3    | 1,076.7         | 33,688                     | 0.00                        | 0.00        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>885.6</b>    | <b>17,901</b>              | <b>0.19</b>                 | <b>0.12</b> |
| #17    | 1        | 0.196  | 300.00 | 2.60  | 0.2600 | 1.0000 | 3    | 256.5           | 16,193                     | 1.00                        | 0.71        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>256.5</b>    | <b>16,193</b>              | <b>1.00</b>                 | <b>0.71</b> |
| #19    | <b>Σ</b> |        |        |       |        |        |      | <b>1,142.2</b>  | <b>16,875</b>              | <b>0.37</b>                 | <b>0.24</b> |
| #15    | 1        | 0.201  | 125.00 | 8.20  | 0.3960 | 1.0000 | 3    | 2,012.4         | 57,137                     | 0.00                        | 0.00        |
|        | 2        | 0.161  | 100.00 | 11.40 | 0.3060 | 1.0000 | 3    | 2,649.4         | 59,791                     | 1.19                        | 0.85        |
|        | 3        | 0.118  | 100.00 | 10.20 | 0.2850 | 1.0000 | 2    | 1,580.5         | 29,583                     | 15.98                       | 11.51       |



| Stru #   | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|----------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
| <b>Σ</b> |          |        |        |       |        |        |      | <b>5,389.3</b>  | <b>48,450</b>              | <b>2.83</b>                 | <b>1.71</b> |
| #12      | 1        | 0.124  | 150.00 | 6.30  | 0.3070 | 1.0000 | 2    | 498.5           | 22,410                     | 12.48                       | 8.80        |
|          | 2        | 0.132  | 200.00 | 3.60  | 0.3500 | 1.0000 | 2    | 133.4           | 15,703                     | 9.13                        | 6.31        |
|          | 3        | 0.136  | 175.00 | 5.00  | 0.3330 | 1.0000 | 2    | 607.5           | 24,640                     | 13.97                       | 9.79        |
|          | 4        | 0.188  | 200.00 | 3.40  | 0.3570 | 1.0000 | 2    | 904.7           | 16,633                     | 7.42                        | 5.37        |
|          | 5        | 0.228  | 175.00 | 4.10  | 0.3640 | 1.0000 | 2    | 476.5           | 36,486                     | 20.95                       | 14.66       |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>2,083.8</b>  | <b>17,988</b>              | <b>8.18</b>                 | <b>5.49</b> |
| #13      | 1        | 0.128  | 150.00 | 6.90  | 0.3390 | 1.0000 | 2    | 417.2           | 27,706                     | 15.46                       | 10.81       |
|          | 2        | 0.130  | 175.00 | 5.70  | 0.3300 | 1.0000 | 2    | 638.1           | 25,298                     | 14.04                       | 9.91        |
|          | 3        | 0.191  | 175.00 | 6.00  | 0.2890 | 1.0000 | 2    | 645.3           | 36,645                     | 21.88                       | 15.51       |
|          | 4        | 0.122  | 175.00 | 5.10  | 0.3460 | 1.0000 | 2    | 245.0           | 27,365                     | 17.00                       | 11.90       |
|          | 5        | 0.137  | 175.00 | 4.20  | 0.3530 | 1.0000 | 2    | 478.0           | 16,624                     | 7.66                        | 5.54        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>4,182.2</b>  | <b>19,433</b>              | <b>9.44</b>                 | <b>6.62</b> |
| #14      | 1        | 0.196  | 100.00 | 10.20 | 0.3980 | 1.0000 | 3    | 2,894.3         | 91,132                     | 6.10                        | 4.33        |
|          | 2        | 0.193  | 150.00 | 6.70  | 0.4020 | 1.0000 | 3    | 1,917.7         | 59,949                     | 3.20                        | 2.29        |
|          | 3        | 0.169  | 75.00  | 13.80 | 0.3240 | 1.0000 | 3    | 4,755.6         | 73,521                     | 1.21                        | 0.87        |
|          | 4        | 0.114  | 100.00 | 11.00 | 0.2980 | 1.0000 | 3    | 335.5           | 39,158                     | 2.35                        | 1.70        |
|          | 5        | 0.078  | 100.00 | 10.10 | 0.1830 | 1.0000 | 3    | 350.3           | 16,865                     | 1.22                        | 0.89        |
|          | 6        | 0.084  | 150.00 | 7.10  | 0.2700 | 1.0000 | 2    | 242.5           | 14,080                     | 7.82                        | 5.64        |
|          | 7        | 0.087  | 100.00 | 10.00 | 0.1840 | 1.0000 | 3    | 540.9           | 16,298                     | 0.40                        | 0.29        |
|          | 8        | 0.126  | 150.00 | 6.70  | 0.2740 | 1.0000 | 2    | 815.5           | 18,458                     | 9.42                        | 6.89        |
|          | 9        | 0.117  | 150.00 | 7.30  | 0.2600 | 1.0000 | 2    | 749.6           | 18,705                     | 10.00                       | 7.32        |
|          | 10       | 0.115  | 125.00 | 8.50  | 0.2610 | 1.0000 | 2    | 466.0           | 20,278                     | 11.14                       | 8.14        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>12,534.2</b> | <b>88,446</b>              | <b>3.03</b>                 | <b>0.57</b> |
| #16      | 1        | 0.200  | 200.00 | 3.30  | 0.3000 | 1.0000 | 3    | 580.2           | 20,094                     | 0.57                        | 0.41        |
|          | 2        | 0.204  | 150.00 | 6.00  | 0.3630 | 1.0000 | 3    | 1,454.1         | 48,328                     | 2.14                        | 1.53        |
|          | 3        | 0.210  | 150.00 | 6.10  | 0.3990 | 1.0000 | 3    | 1,085.9         | 59,491                     | 5.76                        | 4.23        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>21,034.7</b> | <b>61,015</b>              | <b>2.67</b>                 | <b>0.89</b> |
| #20      | 1        | 0.186  | 175.00 | 4.80  | 0.2130 | 1.0000 | 3    | 500.2           | 20,831                     | 0.34                        | 0.24        |
|          | 2        | 0.194  | 200.00 | 3.80  | 0.2330 | 1.0000 | 3    | 570.9           | 16,880                     | 0.26                        | 0.18        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>22,465.7</b> | <b>46,594</b>              | <b>1.11</b>                 | <b>0.44</b> |
| #22      | <b>Σ</b> |        |        |       |        |        |      | <b>49,096.9</b> | <b>36,590</b>              | <b>0.42</b>                 | <b>0.22</b> |
| #23      | 1        | 0.172  | 175.00 | 4.20  | 0.2810 | 1.0000 | 3    | 465.5           | 19,330                     | 0.00                        | 0.00        |
|          | 2        | 0.185  | 150.00 | 6.00  | 0.2160 | 1.0000 | 3    | 567.6           | 25,763                     | 0.79                        | 0.56        |
| <b>Σ</b> |          |        |        |       |        |        |      | <b>48,634.1</b> | <b>35,589</b>              | <b>0.04</b>                 | <b>0.02</b> |
| #35      | <b>Σ</b> |        |        |       |        |        |      | <b>67,462.3</b> | <b>33,006</b>              | <b>0.09</b>                 | <b>0.05</b> |
| #36      | 1        | 0.190  | 175.00 | 5.94  | 0.2830 | 1.0000 | 3    | 446.6           | 27,939                     | 0.00                        | 0.00        |
|          | 2        | 0.180  | 125.00 | 9.92  | 0.2410 | 1.0000 | 3    | 592.7           | 47,347                     | 2.10                        | 1.47        |

| Stru # | SWS #    | Soil K | L (ft) | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l) |
|--------|----------|--------|--------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|-------------|
|        | 3        | 0.151  | 300.00 | 2.63  | 0.3890 | 1.0000 | 2    | 106.7           | 13,665                     | 7.26                        | 5.12        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>67,548.5</b> | <b>38,350</b>              | <b>0.03</b>                 | <b>0.01</b> |
| #37    | 1        | 0.196  | 200.00 | 3.80  | 0.3980 | 1.0000 | 2    | 783.3           | 19,671                     | 9.21                        | 6.67        |
|        | 2        | 0.193  | 175.00 | 5.40  | 0.4020 | 1.0000 | 3    | 971.9           | 49,434                     | 2.19                        | 1.61        |
|        | 3        | 0.173  | 150.00 | 7.11  | 0.2770 | 1.0000 | 3    | 521.1           | 38,313                     | 2.27                        | 1.66        |
|        | 4        | 0.171  | 150.00 | 6.52  | 0.2990 | 1.0000 | 2    | 675.5           | 23,203                     | 11.33                       | 8.31        |
|        | 5        | 0.078  | 400.00 | 1.20  | 0.1830 | 1.0000 | 2    | 32.1            | 2,023                      | 1.12                        | 0.81        |
|        | <b>Σ</b> |        |        |       |        |        |      | <b>67,180.5</b> | <b>37,669</b>              | <b>0.39</b>                 | <b>0.18</b> |

### Subwatershed Time of Concentration Details:

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.65      | 50.00            | 1,369.00          | 1.910          | 0.199        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.57      | 157.00           | 10,030.00         | 3.750          | 0.742        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.941</b> |
| #1        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 6.63      | 70.00            | 1,056.00          | 2.570          | 0.114        |
|           |          | 5. Nearly bare and untilled, and alluvial valley fans | 1.98      | 150.00           | 7,573.00          | 1.400          | 1.502        |
| <b>#1</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.616</b> |
| #1        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.65      | 117.00           | 7,070.00          | 1.280          | 1.534        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.43      | 126.00           | 5,188.00          | 4.670          | 0.308        |
| <b>#1</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.842</b> |
| #1        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 5.77      | 260.00           | 4,506.00          | 2.400          | 0.521        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.84      | 168.00           | 5,924.00          | 5.050          | 0.325        |
| <b>#1</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.846</b> |
| #1        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 19.93     | 180.00           | 903.00            | 4.460          | 0.056        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.30      | 178.00           | 5,393.00          | 5.450          | 0.274        |
| <b>#1</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.330</b> |
| #1        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 13.43     | 105.00           | 782.00            | 3.660          | 0.059        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.62      | 283.00           | 10,822.00         | 4.850          | 0.619        |
| <b>#1</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.678</b> |
| #2        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 6.84      | 70.00            | 1,024.00          | 2.610          | 0.108        |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 70.00            | 4,325.00          | 3.810          | 0.315        |
| <b>#2</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.423</b> |
| #2        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.56      | 45.00            | 810.00            | 2.350          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.86      | 40.00            | 4,663.00          | 2.770          | 0.467        |
| <b>#2</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.562</b> |
| #2        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 5.89      | 50.00            | 849.00            | 2.420          | 0.097        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.17      | 80.00            | 6,862.00          | 3.230          | 0.590        |
| <b>#2</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.687</b> |
| #2        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 12.63     | 95.00            | 752.00            | 3.550          | 0.058        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.40      | 135.00           | 9,630.00          | 3.550          | 0.753        |
| <b>#2</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.811</b> |
| #2        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 11.02     | 70.00            | 635.00            | 3.320          | 0.053        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.46      | 40.00            | 8,732.00          | 2.030          | 1.194        |
| <b>#2</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.247</b> |
| #3        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 10.00            | 805.00            | 1.110          | 0.201        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.33      | 40.00            | 3,017.00          | 3.450          | 0.242        |
| <b>#3</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.443</b> |
| #3        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 0.68      | 10.00            | 1,478.00          | 0.820          | 0.500        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.78      | 100.00           | 5,622.00          | 4.000          | 0.390        |
| <b>#3</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.890</b> |
| #3        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.66      | 70.00            | 1,501.00          | 2.150          | 0.193        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.17      | 60.00            | 5,126.00          | 3.240          | 0.439        |
| <b>#3</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.632</b> |
| #5        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 19.06     | 285.00           | 1,495.00          | 4.360          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.64      | 242.00           | 9,174.00          | 4.870          | 0.523        |
| <b>#5</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.618</b> |
| #5        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 14.27     | 105.00           | 736.00            | 3.770          | 0.054        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.08      | 297.00           | 7,279.00          | 6.050          | 0.334        |
| <b>#5</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.388</b> |
| #5        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 8.27      | 35.00            | 423.00            | 2.870          | 0.040        |



| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.44      | 208.00           | 6,049.00          | 5.560          | 0.302        |
| <b>#5</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.342</b> |
| #5        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 14.58     | 85.00            | 583.00            | 3.810          | 0.042        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.53      | 248.00           | 5,473.00          | 6.380          | 0.238        |
| <b>#5</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.280</b> |
| #5        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 5.07      | 70.00            | 1,382.00          | 2.250          | 0.170        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.89      | 170.00           | 4,375.00          | 5.910          | 0.205        |
| <b>#5</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.375</b> |
| #5        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 12.48     | 90.00            | 721.00            | 3.530          | 0.056        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 5.16      | 274.00           | 5,308.02          | 6.810          | 0.216        |
| <b>#5</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.272</b> |
| #6        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 5.36      | 75.00            | 1,399.00          | 2.310          | 0.168        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.41      | 66.00            | 2,742.00          | 4.650          | 0.163        |
| <b>#6</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.331</b> |
| #6        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 80.00            | 2,359.00          | 1.840          | 0.356        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.63      | 80.00            | 3,039.00          | 4.860          | 0.173        |
| <b>#6</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.529</b> |
| #6        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.60      | 34.00            | 739.00            | 2.140          | 0.095        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.33      | 136.00           | 5,845.00          | 4.570          | 0.355        |
| <b>#6</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.450</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 6.06      | 85.00            | 1,402.00          | 2.460          | 0.158        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.52      | 96.00            | 3,810.00          | 4.760          | 0.222        |
| <b>#6</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.380</b> |
| #6        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 7.24      | 70.00            | 967.00            | 2.690          | 0.099        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.34      | 117.00           | 5,003.00          | 4.580          | 0.303        |
| <b>#6</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.402</b> |
| #6        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 31.83     | 183.00           | 575.00            | 5.640          | 0.028        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.38      | 270.00           | 7,990.00          | 5.510          | 0.402        |
| <b>#6</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.430</b> |
| #6        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 23.08     | 325.00           | 1,408.00          | 4.800          | 0.081        |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.88      | 240.00           | 8,327.00          | 5.090          | 0.454        |
| <b>#6</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.535</b> |
| #7        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.42     | 90.00            | 788.00            | 3.370          | 0.064        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.46      | 230.00           | 15,769.00         | 3.620          | 1.210        |
| <b>#7</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.274</b> |
| #7        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 10.97     | 60.00            | 547.00            | 3.310          | 0.045        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.61      | 220.00           | 13,660.00         | 3.800          | 0.998        |
| <b>#7</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.043</b> |
| #7        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 6.40      | 60.00            | 938.00            | 2.520          | 0.103        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 1.72      | 171.00           | 9,931.00          | 3.930          | 0.701        |
| <b>#7</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.804</b> |
| #7        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 19.23     | 80.00            | 416.00            | 4.380          | 0.026        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.45      | 100.00           | 4,083.00          | 4.690          | 0.241        |
| <b>#7</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.267</b> |
| #7        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 6.09      | 67.00            | 1,101.00          | 2.460          | 0.124        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.51      | 80.00            | 3,184.00          | 4.750          | 0.186        |
| <b>#7</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.310</b> |
| #7        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 5.93      | 63.00            | 1,062.00          | 2.430          | 0.121        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 2.74      | 82.00            | 2,993.00          | 4.960          | 0.167        |
| <b>#7</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.288</b> |
| #7        | 7        | 5. Nearly bare and untilled, and alluvial valley fans | 7.97      | 65.00            | 816.00            | 2.820          | 0.080        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 3.48      | 153.00           | 4,400.00          | 5.590          | 0.218        |
| <b>#7</b> | <b>7</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.298</b> |
| #7        | 8        | 5. Nearly bare and untilled, and alluvial valley fans | 6.60      | 50.00            | 758.00            | 2.560          | 0.082        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 4.66      | 473.00           | 10,157.00         | 6.470          | 0.436        |
| <b>#7</b> | <b>8</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.518</b> |
| #9        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.35      | 90.00            | 2,687.00          | 1.830          | 0.407        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 0.58      | 20.00            | 3,463.00          | 2.270          | 0.423        |
| <b>#9</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.830</b> |
| #10       | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 41.00            | 3,317.00          | 1.110          | 0.830        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.70      | 29.00            | 4,125.00          | 2.510          | 0.456        |
| <b>#10</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.286</b> |
| #10        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.25      | 125.00           | 5,554.00          | 1.500          | 1.028        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 85.00            | 3,997.00          | 4.370          | 0.254        |
| <b>#10</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.282</b> |
| #10        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.39      | 68.00            | 4,904.00          | 1.170          | 1.164        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.73      | 90.00            | 1,904.00          | 6.520          | 0.081        |
| <b>#10</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.245</b> |
| #10        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.76      | 51.00            | 1,357.00          | 1.930          | 0.195        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.65      | 22.00            | 3,385.00          | 2.410          | 0.390        |
| <b>#10</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.585</b> |
| #10        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 1.63      | 88.00            | 5,391.16          | 1.270          | 1.179        |
| <b>#10</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.179</b> |
| #12        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.50      | 75.00            | 1,667.00          | 2.120          | 0.218        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.85      | 155.00           | 8,400.00          | 4.070          | 0.573        |
| <b>#12</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.791</b> |
| #12        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.99      | 50.00            | 1,674.03          | 1.720          | 0.270        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.67      | 70.00            | 4,201.17          | 3.870          | 0.301        |
| <b>#12</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.571</b> |
| #12        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 4.04      | 57.00            | 1,411.00          | 2.000          | 0.195        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.55      | 107.00           | 6,884.00          | 3.740          | 0.511        |
| <b>#12</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.706</b> |
| #12        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.23      | 84.00            | 3,771.04          | 1.490          | 0.703        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 186.00           | 11,515.60         | 3.810          | 0.839        |
| <b>#12</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.542</b> |
| #12        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.68      | 53.00            | 1,442.00          | 1.910          | 0.209        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.95      | 120.00           | 6,155.00          | 4.180          | 0.409        |
| <b>#12</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.618</b> |
| #13        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.62      | 62.00            | 1,342.00          | 2.140          | 0.174        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.91      | 157.00           | 8,225.00          | 4.140          | 0.551        |
| <b>#13</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.725</b> |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #13        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.91      | 50.00            | 1,717.00          | 1.700          | 0.280        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.28      | 183.00           | 8,039.00          | 4.520          | 0.494        |
| <b>#13</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.774</b> |
| #13        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 6.18      | 95.00            | 1,537.00          | 2.480          | 0.172        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.13      | 135.00           | 6,347.00          | 4.370          | 0.403        |
| <b>#13</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.575</b> |
| #13        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.17      | 10.00            | 315.00            | 1.780          | 0.049        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.30      | 100.00           | 4,344.00          | 4.550          | 0.265        |
| <b>#13</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.314</b> |
| #13        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 3.10      | 70.00            | 2,255.00          | 1.760          | 0.355        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.23      | 140.00           | 11,392.00         | 3.320          | 0.953        |
| <b>#13</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.308</b> |
| #14        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 10.59     | 63.00            | 595.00            | 3.250          | 0.050        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.60      | 151.00           | 5,808.00          | 4.830          | 0.334        |
| <b>#14</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.384</b> |
| #14        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.28      | 67.00            | 920.00            | 2.690          | 0.095        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.17      | 123.00           | 5,670.00          | 4.410          | 0.357        |
| <b>#14</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.452</b> |
| #14        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 21.46     | 150.00           | 699.00            | 4.630          | 0.041        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.10      | 364.00           | 11,728.00         | 5.280          | 0.617        |
| <b>#14</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.658</b> |
| #14        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 3.39      | 35.00            | 1,032.00          | 1.840          | 0.155        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.97      | 103.00           | 3,470.00          | 5.160          | 0.186        |
| <b>#14</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.341</b> |
| #14        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 28.15     | 125.00           | 444.00            | 5.300          | 0.023        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.18      | 246.00           | 5,886.00          | 6.130          | 0.266        |
| <b>#14</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.289</b> |
| #14        | 6        | 5. Nearly bare and untilled, and alluvial valley fans | 3.18      | 40.00            | 1,257.00          | 1.780          | 0.196        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.29      | 228.00           | 9,963.00          | 4.530          | 0.610        |
| <b>#14</b> | <b>6</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.806</b> |

| Stru #     | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #14        | 7         | 5. Nearly bare and untilled, and alluvial valley fans | 16.72     | 100.00           | 598.00            | 4.080          | 0.040        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.81      | 243.00           | 8,649.00          | 5.020          | 0.478        |
| <b>#14</b> | <b>7</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.518</b> |
| #14        | 8         | 5. Nearly bare and untilled, and alluvial valley fans | 1.70      | 47.00            | 2,765.00          | 1.300          | 0.590        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.44      | 274.00           | 11,208.00         | 4.690          | 0.663        |
| <b>#14</b> | <b>8</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.253</b> |
| #14        | 9         | 5. Nearly bare and untilled, and alluvial valley fans | 2.87      | 105.00           | 3,657.00          | 1.690          | 0.601        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.43      | 194.00           | 7,991.00          | 4.670          | 0.475        |
| <b>#14</b> | <b>9</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.076</b> |
| #14        | 10        | 5. Nearly bare and untilled, and alluvial valley fans | 2.75      | 80.00            | 2,907.00          | 1.650          | 0.489        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.41      | 172.00           | 7,149.00          | 4.650          | 0.427        |
| <b>#14</b> | <b>10</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.916</b> |
| #15        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 12.80     | 54.00            | 422.00            | 3.570          | 0.032        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.68      | 181.00           | 10,781.00         | 3.880          | 0.771        |
| <b>#15</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.803</b> |
| #15        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 44.22     | 260.00           | 588.00            | 6.640          | 0.024        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.45      | 254.00           | 10,354.00         | 4.690          | 0.613        |
| <b>#15</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.637</b> |
| #15        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 10.04     | 85.00            | 847.00            | 3.160          | 0.074        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.34      | 366.00           | 15,663.00         | 4.580          | 0.949        |
| <b>#15</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.023</b> |
| #16        | 1         | 5. Nearly bare and untilled, and alluvial valley fans | 4.17      | 15.00            | 360.00            | 2.040          | 0.049        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.42      | 108.00           | 7,618.00          | 3.570          | 0.592        |
| <b>#16</b> | <b>1</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.641</b> |
| #16        | 2         | 5. Nearly bare and untilled, and alluvial valley fans | 8.70      | 62.00            | 713.00            | 2.940          | 0.067        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 1.99      | 144.00           | 7,241.00          | 4.230          | 0.475        |
| <b>#16</b> | <b>2</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.542</b> |
| #16        | 3         | 5. Nearly bare and untilled, and alluvial valley fans | 6.88      | 32.00            | 465.00            | 2.620          | 0.049        |
|            |           | 8. Large gullies, diversions, and low flowing streams | 2.29      | 81.00            | 3,543.00          | 4.530          | 0.217        |
| <b>#16</b> | <b>3</b>  | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.266</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #17        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 9.37      | 65.00            | 694.00            | 3.060          | 0.062        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.19      | 56.00            | 4,712.00          | 3.270          | 0.400        |
| <b>#17</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.462</b> |
| #18        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 9.00      | 60.00            | 667.00            | 2.990          | 0.061        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.97      | 61.00            | 6,287.00          | 2.950          | 0.591        |
| <b>#18</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.652</b> |
| #18        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 2.47      | 33.00            | 1,336.00          | 1.570          | 0.236        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.01      | 164.00           | 8,154.00          | 4.250          | 0.532        |
| <b>#18</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.768</b> |
| #20        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.87     | 45.00            | 379.00            | 3.440          | 0.030        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.75      | 45.00            | 5,969.00          | 2.600          | 0.637        |
| <b>#20</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.667</b> |
| #20        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.40      | 45.00            | 833.00            | 2.320          | 0.099        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.30      | 98.00            | 7,547.00          | 3.410          | 0.614        |
| <b>#20</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.713</b> |
| #21        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.09      | 60.00            | 1,467.00          | 2.020          | 0.201        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.93      | 60.00            | 6,433.00          | 2.890          | 0.618        |
| <b>#21</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.819</b> |
| #21        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.50      | 50.00            | 1,430.00          | 1.860          | 0.213        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.15      | 60.00            | 2,785.00          | 4.400          | 0.175        |
| <b>#21</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.388</b> |
| #21        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.70      | 15.00            | 881.00            | 1.300          | 0.188        |
|            |          | 9. Small streams flowing bankfull                     | 1.49      | 60.00            | 4,014.00          | 11.000         | 0.101        |
| <b>#21</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.289</b> |
| #21        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 2.21      | 40.00            | 1,811.02          | 1.480          | 0.339        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.84      | 50.00            | 5,949.54          | 2.750          | 0.600        |
| <b>#21</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.939</b> |
| #23        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.44      | 65.00            | 2,660.01          | 1.560          | 0.473        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.33      | 10.00            | 3,017.50          | 1.720          | 0.487        |
| <b>#23</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.960</b> |
| #23        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 3.49      | 60.00            | 1,718.01          | 1.860          | 0.256        |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.66      | 65.00            | 3,926.06          | 3.860          | 0.282        |
| <b>#23</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.538</b> |
| #24        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.71      | 430.00           | 25,118.00         | 1.300          | 5.367        |
| <b>#24</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>5.367</b> |
| #24        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.84      | 430.00           | 23,393.00         | 1.350          | 4.813        |
| <b>#24</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>4.813</b> |
| #24        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 1.82      | 155.00           | 8,498.00          | 1.350          | 1.748        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.84      | 40.00            | 4,771.00          | 2.740          | 0.483        |
| <b>#24</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.231</b> |
| #24        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.24      | 50.00            | 4,042.00          | 1.110          | 1.011        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.49      | 60.00            | 12,150.00         | 2.100          | 1.607        |
| <b>#24</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.618</b> |
| #25        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 0.51      | 10.00            | 1,950.00          | 0.710          | 0.762        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.81      | 60.00            | 3,322.00          | 4.030          | 0.228        |
| <b>#25</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.990</b> |
| #25        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.11      | 25.00            | 2,254.00          | 1.050          | 0.596        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.36      | 75.00            | 3,178.00          | 4.600          | 0.191        |
| <b>#25</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.787</b> |
| #25        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 3.23      | 30.00            | 929.00            | 1.790          | 0.144        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.45      | 154.00           | 6,297.00          | 4.690          | 0.372        |
| <b>#25</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.516</b> |
| #26        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 1.20      | 103.00           | 8,602.00          | 1.090          | 2.192        |
| <b>#26</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>2.192</b> |
| #26        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 1.23      | 120.00           | 9,780.00          | 1.100          | 2.469        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.18      | 184.00           | 8,454.00          | 4.420          | 0.531        |
| <b>#26</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>3.000</b> |
| #27        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.32      | 50.00            | 1,158.02          | 2.070          | 0.155        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.53      | 198.00           | 7,838.16          | 4.760          | 0.457        |
| <b>#27</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.612</b> |
| #27        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.26      | 30.00            | 570.00            | 2.290          | 0.069        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.15      | 278.00           | 8,822.00          | 5.320          | 0.460        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#27</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.529</b> |
| #27        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 16.33     | 80.00            | 490.00            | 4.040          | 0.033        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.15      | 225.00           | 10,443.00         | 4.400          | 0.659        |
| <b>#27</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.692</b> |
| #27        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 12.43     | 65.00            | 523.00            | 3.520          | 0.041        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.49      | 225.00           | 6,454.00          | 5.600          | 0.320        |
| <b>#27</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.361</b> |
| #27        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 9.40      | 25.00            | 266.00            | 3.060          | 0.024        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.32      | 364.00           | 15,700.00         | 4.560          | 0.956        |
| <b>#27</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.980</b> |
| #28        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 5.25      | 40.00            | 762.00            | 2.290          | 0.092        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.96      | 310.00           | 10,479.34         | 5.150          | 0.565        |
| <b>#28</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.657</b> |
| #28        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 25.86     | 105.00           | 406.00            | 5.080          | 0.022        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.96      | 310.00           | 10,479.34         | 5.150          | 0.565        |
| <b>#28</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.587</b> |
| #29        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 11.58     | 30.00            | 259.00            | 3.400          | 0.021        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 3.61      | 288.00           | 7,976.00          | 5.700          | 0.388        |
| <b>#29</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.409</b> |
| #29        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 8.06      | 40.00            | 496.00            | 2.830          | 0.048        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.90      | 252.00           | 8,693.55          | 5.100          | 0.473        |
| <b>#29</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.521</b> |
| #29        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 7.25      | 25.00            | 345.00            | 2.690          | 0.035        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.26      | 158.00           | 7,001.00          | 4.500          | 0.432        |
| <b>#29</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.467</b> |
| #30        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.93      | 35.00            | 710.00            | 2.220          | 0.088        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.67      | 243.00           | 14,540.00         | 3.870          | 1.043        |
| <b>#30</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.131</b> |
| #31        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 2.91      | 15.00            | 515.00            | 1.700          | 0.084        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.74      | 247.00           | 9,006.00          | 4.960          | 0.504        |
| <b>#31</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.588</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #31        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.46      | 25.00            | 335.00            | 2.730          | 0.034        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.18      | 138.00           | 6,335.00          | 4.420          | 0.398        |
| <b>#31</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.432</b> |
| #31        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 3.84      | 20.00            | 521.00            | 1.950          | 0.074        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.24      | 108.00           | 4,826.00          | 4.480          | 0.299        |
| <b>#31</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.373</b> |
| #32        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.48      | 22.00            | 632.00            | 1.860          | 0.094        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.56      | 101.00           | 6,494.00          | 3.740          | 0.482        |
| <b>#32</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.576</b> |
| #34        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.21      | 25.00            | 779.00            | 1.790          | 0.120        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.80      | 63.00            | 2,251.00          | 5.010          | 0.124        |
| <b>#34</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.244</b> |
| #34        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.75      | 40.00            | 696.00            | 2.390          | 0.080        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 23.00     | 2,100.00         | 9,130.43          | 14.380         | 0.176        |
| <b>#34</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.256</b> |
| #34        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.67      | 40.00            | 1,500.00          | 1.630          | 0.255        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.28      | 98.00            | 7,675.00          | 3.380          | 0.630        |
| <b>#34</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.885</b> |
| #36        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 3.21      | 105.00           | 3,274.00          | 1.790          | 0.508        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.21      | 5.00             | 2,367.00          | 1.370          | 0.479        |
| <b>#36</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.987</b> |
| #36        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 5.50      | 140.00           | 2,547.00          | 2.340          | 0.302        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.58      | 30.00            | 1,897.00          | 3.770          | 0.139        |
| <b>#36</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.441</b> |
| #36        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 2.03      | 80.00            | 3,938.62          | 1.420          | 0.770        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.52      | 50.00            | 1,981.86          | 4.760          | 0.115        |
| <b>#36</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.885</b> |
| #37        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.68      | 129.00           | 2,754.05          | 2.160          | 0.354        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.16      | 10.00            | 6,108.73          | 1.210          | 1.402        |
| <b>#37</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.756</b> |



| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #37        | 2        | 5. Nearly bare and untilled, and alluvial valley fans | 7.32      | 90.00            | 1,229.00          | 2.700          | 0.126        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 1.62      | 70.00            | 4,309.01          | 3.820          | 0.313        |
| <b>#37</b> | <b>2</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.439</b> |
| #37        | 3        | 5. Nearly bare and untilled, and alluvial valley fans | 8.10      | 100.00           | 1,234.00          | 2.840          | 0.120        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 2.66      | 100.00           | 3,763.21          | 4.890          | 0.213        |
| <b>#37</b> | <b>3</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.333</b> |
| #37        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 5.09      | 90.00            | 1,768.03          | 2.250          | 0.218        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 0.36      | 30.00            | 8,326.39          | 1.800          | 1.284        |
| <b>#37</b> | <b>4</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>1.502</b> |
| #37        | 5        | 5. Nearly bare and untilled, and alluvial valley fans | 0.81      | 20.00            | 2,466.09          | 0.900          | 0.761        |
|            |          | 8. Large gullies, diversions, and low flowing streams | 4.06      | 50.00            | 1,231.01          | 6.040          | 0.056        |
| <b>#37</b> | <b>5</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.817</b> |

### ***Subwatershed Muskingum Routing Details:***

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.29      | 107.00           | 8,294.00          | 3.400          | 0.677        |
| <b>#1</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.677</b> |
| #1        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.27      | 113.00           | 8,880.00          | 3.380          | 0.729        |
| <b>#1</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.729</b> |
| #1        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.35      | 171.00           | 12,634.00         | 3.490          | 1.005        |
| <b>#1</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.005</b> |
| #1        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.49      | 274.00           | 18,349.00         | 3.660          | 1.392        |
| <b>#1</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.392</b> |
| #1        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.49      | 274.00           | 18,349.00         | 3.660          | 1.392        |
| <b>#1</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.392</b> |
| #2        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.53      | 20.00            | 3,756.00          | 2.180          | 0.478        |
| <b>#2</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.478</b> |
| #2        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.55      | 25.00            | 4,570.00          | 2.210          | 0.574        |
| <b>#2</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.574</b> |
| #2        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.55      | 25.00            | 4,570.00          | 2.210          | 0.574        |
| <b>#2</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.574</b> |

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #2        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.65      | 45.00            | 6,955.00          | 2.410          | 0.801        |
| <b>#2</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.801</b> |
| #3        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.92      | 20.00            | 2,168.00          | 2.880          | 0.209        |
| <b>#3</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.209</b> |
| #5        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#5</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #5        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.75      | 125.00           | 7,149.00          | 3.960          | 0.501        |
| <b>#5</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.501</b> |
| #5        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.65      | 155.00           | 9,418.00          | 3.840          | 0.681        |
| <b>#5</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #5        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.65      | 155.00           | 9,418.00          | 3.840          | 0.681        |
| <b>#5</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.681</b> |
| #5        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.67      | 239.00           | 14,273.00         | 3.880          | 1.021        |
| <b>#5</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.021</b> |
| #5        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.68      | 239.00           | 14,223.00         | 3.880          | 1.018        |
| <b>#5</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.018</b> |
| #6        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.16      | 26.00            | 2,241.00          | 3.230          | 0.192        |
| <b>#6</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.192</b> |
| #6        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.00      | 50.00            | 4,987.00          | 3.000          | 0.461        |
| <b>#6</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.461</b> |
| #6        | 4        | 5. Nearly bare and untilled, and alluvial valley fans | 1.00      | 50.00            | 4,987.00          | 1.000          | 1.385        |
| <b>#6</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.385</b> |
| #6        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.02      | 89.00            | 8,685.00          | 3.030          | 0.796        |
| <b>#6</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.796</b> |
| #6        | 6        | 8. Large gullies, diversions, and low flowing streams | 1.06      | 126.00           | 11,860.00         | 3.090          | 1.066        |
| <b>#6</b> | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.066</b> |
| #6        | 7        | 8. Large gullies, diversions, and low flowing streams | 1.06      | 126.00           | 11,860.00         | 3.090          | 1.066        |
| <b>#6</b> | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.066</b> |
| #7        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#7</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #7        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.16      | 140.00           | 12,037.00         | 3.230          | 1.035        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#7</b>  | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.035</b> |
| #7         | 5        | 8. Large gullies, diversions, and low flowing streams | 1.14      | 140.00           | 12,307.69         | 3.190          | 1.071        |
| <b>#7</b>  | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.071</b> |
| #7         | 6        | 8. Large gullies, diversions, and low flowing streams | 1.17      | 158.00           | 13,546.00         | 3.230          | 1.164        |
| <b>#7</b>  | <b>6</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.164</b> |
| #7         | 7        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 187.00           | 15,784.00         | 3.260          | 1.344        |
| <b>#7</b>  | <b>7</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.344</b> |
| #7         | 8        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 187.00           | 15,784.00         | 3.260          | 1.344        |
| <b>#7</b>  | <b>8</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.344</b> |
| #10        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.76      | 37.00            | 4,861.00          | 2.610          | 0.517        |
| <b>#10</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.517</b> |
| #10        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.76      | 37.00            | 4,861.00          | 2.610          | 0.517        |
| <b>#10</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.517</b> |
| #10        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.79      | 47.00            | 5,956.00          | 2.660          | 0.621        |
| <b>#10</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.621</b> |
| #12        | 2        | 8. Large gullies, diversions, and low flowing streams | 8.24      | 111.00           | 1,347.00          | 8.610          | 0.043        |
| <b>#12</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.043</b> |
| #12        | 3        | 8. Large gullies, diversions, and low flowing streams | 8.01      | 109.00           | 1,360.00          | 8.490          | 0.044        |
| <b>#12</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.044</b> |
| #12        | 4        | 8. Large gullies, diversions, and low flowing streams | 2.24      | 176.00           | 7,866.00          | 4.480          | 0.487        |
| <b>#12</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.487</b> |
| #12        | 5        | 8. Large gullies, diversions, and low flowing streams | 2.24      | 176.00           | 7,866.00          | 4.480          | 0.487        |
| <b>#12</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.487</b> |
| #13        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.34      | 54.00            | 4,025.00          | 3.470          | 0.322        |
| <b>#13</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.322</b> |
| #13        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.98      | 72.00            | 7,333.00          | 2.970          | 0.685        |
| <b>#13</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.685</b> |
| #13        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 127.00           | 10,806.00         | 3.250          | 0.923        |
| <b>#13</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.923</b> |
| #13        | 5        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 127.00           | 10,806.00         | 3.250          | 0.923        |
| <b>#13</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.923</b> |
| #14        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#14</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |



| Stru #     | SWS #     | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|-----------|---|-----------|------------------|-------------------|----------------|--------------|
| #14        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.83      | 58.00            | 6,957.00          | 2.730          | 0.707        |
| <b>#14</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.707</b> |
| #14        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.81      | 77.00            | 9,480.00          | 2.700          | 0.975        |
| <b>#14</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.975</b> |
| #14        | 4         | 8. Large gullies, diversions, and low flowing streams | 0.86      | 147.00           | 17,117.00         | 2.770          | 1.716        |
| <b>#14</b> | <b>4</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.716</b> |
| #14        | 5         | 8. Large gullies, diversions, and low flowing streams | 0.88      | 175.00           | 19,934.00         | 2.810          | 1.970        |
| <b>#14</b> | <b>5</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.970</b> |
| #14        | 6         | 8. Large gullies, diversions, and low flowing streams | 0.95      | 211.00           | 22,155.00         | 2.920          | 2.107        |
| <b>#14</b> | <b>6</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.107</b> |
| #14        | 7         | 8. Large gullies, diversions, and low flowing streams | 0.96      | 257.00           | 26,835.00         | 2.930          | 2.544        |
| <b>#14</b> | <b>7</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.544</b> |
| #14        | 8         | 8. Large gullies, diversions, and low flowing streams | 0.96      | 257.00           | 26,835.00         | 2.930          | 2.544        |
| <b>#14</b> | <b>8</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.544</b> |
| #14        | 9         | 8. Large gullies, diversions, and low flowing streams | 0.95      | 307.00           | 32,146.59         | 2.930          | 3.047        |
| <b>#14</b> | <b>9</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.047</b> |
| #14        | 10        | 8. Large gullies, diversions, and low flowing streams | 0.96      | 339.00           | 35,382.00         | 2.930          | 3.354        |
| <b>#14</b> | <b>10</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>3.354</b> |
| #15        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#15</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #15        | 2         | 8. Large gullies, diversions, and low flowing streams | 1.14      | 86.00            | 7,535.00          | 3.200          | 0.654        |
| <b>#15</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.654</b> |
| #15        | 3         | 8. Large gullies, diversions, and low flowing streams | 1.25      | 115.00           | 9,236.00          | 3.340          | 0.768        |
| <b>#15</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.768</b> |
| #16        | 2         | 8. Large gullies, diversions, and low flowing streams | 0.58      | 24.00            | 4,161.00          | 2.270          | 0.509        |
| <b>#16</b> | <b>2</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.509</b> |
| #16        | 3         | 8. Large gullies, diversions, and low flowing streams | 0.51      | 37.00            | 7,269.00          | 2.140          | 0.943        |
| <b>#16</b> | <b>3</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.943</b> |
| #17        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#17</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #18        | 1         | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#18</b> | <b>1</b>  | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #18        | 2         | 8. Large gullies, diversions, and low flowing streams | 1.02      | 62.00            | 6,103.00          | 3.020          | 0.561        |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| <b>#18</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.561</b> |
| #20        | 2        | 8. Large gullies, diversions, and low flowing streams | 17.00     | 3,605.00         | 21,205.88         | 12.360         | 0.476        |
| <b>#20</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.476</b> |
| #21        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#21</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #21        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.41      | 20.00            | 4,824.00          | 1.930          | 0.694        |
| <b>#21</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.694</b> |
| #21        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 20.00            | 5,626.00          | 1.780          | 0.877        |
| <b>#21</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.877</b> |
| #21        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.36      | 20.00            | 5,626.00          | 1.780          | 0.877        |
| <b>#21</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.877</b> |
| #23        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#23</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #23        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.63      | 30.00            | 4,771.75          | 2.370          | 0.559        |
| <b>#23</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.559</b> |
| #24        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.79      | 180.00           | 22,769.00         | 2.660          | 2.377        |
| <b>#24</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.377</b> |
| #24        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.78      | 180.00           | 23,111.00         | 2.640          | 2.431        |
| <b>#24</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.431</b> |
| #24        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#24</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #25        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.99      | 104.00           | 5,220.00          | 4.230          | 0.342        |
| <b>#25</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.342</b> |
| #25        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.99      | 104.00           | 5,220.00          | 4.230          | 0.342        |
| <b>#25</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.342</b> |
| #25        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.00      | 0.00             | 0.00              | 0.000          | 0.000        |
| <b>#25</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.000</b> |
| #27        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.38      | 216.00           | 15,629.00         | 3.520          | 1.233        |
| <b>#27</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.233</b> |
| #27        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.17      | 144.00           | 12,301.00         | 3.240          | 1.054        |
| <b>#27</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.054</b> |
| #27        | 3        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 76.00            | 6,454.00          | 3.250          | 0.551        |
| <b>#27</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.551</b> |

| Stru #     | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|------------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #27        | 4        | 8. Large gullies, diversions, and low flowing streams | 1.18      | 76.00            | 6,454.00          | 3.250          | 0.551        |
| <b>#27</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.551</b> |
| #28        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.30      | 84.00            | 6,445.17          | 3.420          | 0.523        |
| <b>#28</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.523</b> |
| #29        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.88      | 37.00            | 4,210.00          | 2.810          | 0.416        |
| <b>#29</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.416</b> |
| #29        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.88      | 26.00            | 2,949.00          | 2.810          | 0.291        |
| <b>#29</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.291</b> |
| #31        | 1        | 8. Large gullies, diversions, and low flowing streams | 1.35      | 76.00            | 5,639.00          | 3.480          | 0.450        |
| <b>#31</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.450</b> |
| #31        | 2        | 8. Large gullies, diversions, and low flowing streams | 1.15      | 20.00            | 1,734.00          | 3.220          | 0.149        |
| <b>#31</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.149</b> |
| #34        | 1        | 8. Large gullies, diversions, and low flowing streams | 0.73      | 65.00            | 8,900.00          | 2.560          | 0.965        |
| <b>#34</b> | <b>1</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.965</b> |
| #34        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.73      | 65.00            | 8,900.00          | 2.560          | 0.965        |
| <b>#34</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.965</b> |
| #36        | 3        | 8. Large gullies, diversions, and low flowing streams | 2.71      | 80.00            | 2,957.00          | 4.930          | 0.166        |
| <b>#36</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.166</b> |
| #37        | 2        | 8. Large gullies, diversions, and low flowing streams | 0.29      | 30.00            | 10,319.91         | 1.610          | 1.780        |
| <b>#37</b> | <b>2</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.780</b> |
| #37        | 3        | 8. Large gullies, diversions, and low flowing streams | 0.31      | 30.00            | 9,800.71          | 1.650          | 1.649        |
| <b>#37</b> | <b>3</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.649</b> |
| #37        | 4        | 8. Large gullies, diversions, and low flowing streams | 0.29      | 30.00            | 10,319.91         | 1.610          | 1.780        |
| <b>#37</b> | <b>4</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>1.780</b> |
| #37        | 5        | 8. Large gullies, diversions, and low flowing streams | 0.56      | 100.00           | 17,956.54         | 2.230          | 2.236        |
| <b>#37</b> | <b>5</b> | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>2.236</b> |



## **Attachment 18.B-5**

Chaco River Unnamed Tributary Baseline Hydrology and Sedimentology SEDCAD™ Model Output

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**UNNAMED TRIBUTARY TO CHACO PRE-**  
**MINE HYDROLOGY AND**  
**SEDIMENTOLOGY**

*PRE-MINE*

BHP Billiton

***General Information***

***Storm Information:***

|                 |              |
|-----------------|--------------|
| Storm Type:     | Type II-70   |
| Design Storm:   | 2 yr - 6 hr  |
| Rainfall Depth: | 0.850 inches |

***Particle Size Distribution:***

| Size (mm) | CW1      | CW2      | CW3      | CW4      | CW5      |
|-----------|----------|----------|----------|----------|----------|
| 0.4250    | 100.000% | 100.000% | 100.000% | 100.000% | 100.000% |
| 0.2500    | 71.002%  | 79.759%  | 73.724%  | 79.290%  | 83.334%  |
| 0.1500    | 52.517%  | 62.156%  | 54.007%  | 60.839%  | 68.417%  |
| 0.0750    | 40.991%  | 48.658%  | 41.754%  | 47.304%  | 53.993%  |
| 0.0159    | 36.096%  | 42.458%  | 36.968%  | 41.409%  | 46.327%  |
| 0.0100    | 29.101%  | 34.107%  | 30.394%  | 33.504%  | 35.855%  |
| 0.0050    | 10.110%  | 8.789%   | 9.084%   | 8.485%   | 9.027%   |
| 0.0020    | 5.803%   | 5.220%   | 5.060%   | 4.944%   | 5.817%   |
| 0.0010    | 5.384%   | 4.878%   | 4.663%   | 4.594%   | 5.499%   |
| 0.0004    | 4.868%   | 4.198%   | 4.196%   | 3.982%   | 4.619%   |



**Structure Networking:**

| Type | Stru # | (flows into) | Stru # | Musk. K (hrs) | Musk. X | Description                           |
|------|--------|--------------|--------|---------------|---------|---------------------------------------|
| Null | #1     | ==>          | End    | 0.000         | 0.000   | Unnamed Tributary to Chaco CHA S1 SW1 |

|      |
|------|
| #1   |
| Null |

***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 287.200                                   | 287.200                               | 49.89                      | 2.27                                 | 157.5              | 77,436                              | 31.75                                 | 20.44          |

## *Particle Size Distribution(s) at Each Structure*

### *Structure #1:*

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 90.136%  |
| 0.0750    | 69.686%  |
| 0.0159    | 61.698%  |
| 0.0100    | 50.726%  |
| 0.0050    | 15.161%  |
| 0.0020    | 8.445%   |
| 0.0010    | 7.782%   |
| 0.0004    | 7.003%   |



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***Structure Detail:***

***Structure #1 (Null)***

*Unnamed Tributary to Chaco CHA S1 SW1*

**Subwatershed Hydrology Detail:**

| Stru # | SWS #    | SWS Area (ac)  | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|----------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #1     | 1        | 287.200        | 0.270              | 0.000        | 0.000  | 85.500       | M   | 49.89                | 2.267                 |
|        | <b>Σ</b> | <b>287.200</b> |                    |              |        |              |     | <b>49.89</b>         | <b>2.267</b>          |

**Subwatershed Sedimentology Detail:**

| Stru # | SWS #    | Soil K | L (ft)   | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l)  |
|--------|----------|--------|----------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|--------------|
| #1     | 1        | 0.151  | 1,000.00 | 7.30  | 0.2450 | 1.0000 | 3    | 157.5           | 77,436                     | 31.75                       | 20.44        |
|        | <b>Σ</b> |        |          |       |        |        |      | <b>157.5</b>    | <b>77,436</b>              | <b>31.75</b>                | <b>20.44</b> |

**Subwatershed Time of Concentration Details:**

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.80      | 80.64            | 1,680.00          | 2.190          | 0.213        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 7.30      | 122.64           | 1,680.00          | 8.100          | 0.057        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.270</b> |

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**UNNAMED TRIBUTARY TO CHACO PRE-**  
**MINE HYDROLOGY AND**  
**SEDIMENTOLOGY**

*PRE-MINE - 10-yr, 6-hr Storm*

BHP Billiton



***General Information***

***Storm Information:***

|                 |              |
|-----------------|--------------|
| Storm Type:     | Type II-70   |
| Design Storm:   | 10 yr - 6 hr |
| Rainfall Depth: | 1.280 inches |

***Particle Size Distribution:***

| Size (mm) | CW1      | CW2      | CW3      | CW4      | CW5      |
|-----------|----------|----------|----------|----------|----------|
| 0.4250    | 100.000% | 100.000% | 100.000% | 100.000% | 100.000% |
| 0.2500    | 71.002%  | 79.759%  | 73.724%  | 79.290%  | 83.334%  |
| 0.1500    | 52.517%  | 62.156%  | 54.007%  | 60.839%  | 68.417%  |
| 0.0750    | 40.991%  | 48.658%  | 41.754%  | 47.304%  | 53.993%  |
| 0.0159    | 36.096%  | 42.458%  | 36.968%  | 41.409%  | 46.327%  |
| 0.0100    | 29.101%  | 34.107%  | 30.394%  | 33.504%  | 35.855%  |
| 0.0050    | 10.110%  | 8.789%   | 9.084%   | 8.485%   | 9.027%   |
| 0.0020    | 5.803%   | 5.220%   | 5.060%   | 4.944%   | 5.817%   |
| 0.0010    | 5.384%   | 4.878%   | 4.663%   | 4.594%   | 5.499%   |
| 0.0004    | 4.868%   | 4.198%   | 4.196%   | 3.982%   | 4.619%   |

***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 287.200                                   | 287.200                               | 136.65                     | 6.43                                 | 496.7              | 81,953                              | 36.29                                 | 24.48          |

## *Particle Size Distribution(s) at Each Structure*

### *Structure #1:*

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 82.463%  |
| 0.0750    | 63.754%  |
| 0.0159    | 56.446%  |
| 0.0100    | 46.409%  |
| 0.0050    | 13.870%  |
| 0.0020    | 7.726%   |
| 0.0010    | 7.120%   |
| 0.0004    | 6.407%   |



**Subwatershed Hydrology Detail:**

| Stru # | SWS #    | SWS Area (ac)  | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|----------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #1     | 1        | 287.200        | 0.270              | 0.000        | 0.000  | 85.500       | M   | 136.65               | 6.435                 |
|        | <b>Σ</b> | <b>287.200</b> |                    |              |        |              |     | <b>136.65</b>        | <b>6.435</b>          |

**Subwatershed Sedimentology Detail:**

| Stru # | SWS #    | Soil K | L (ft)   | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l)  |
|--------|----------|--------|----------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|--------------|
| #1     | 1        | 0.151  | 1,000.00 | 7.30  | 0.2450 | 1.0000 | 3    | 496.7           | 81,953                     | 36.29                       | 24.48        |
|        | <b>Σ</b> |        |          |       |        |        |      | <b>496.7</b>    | <b>81,953</b>              | <b>36.29</b>                | <b>24.48</b> |

**Subwatershed Time of Concentration Details:**

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.80      | 80.64            | 1,680.00          | 2.190          | 0.213        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 7.30      | 122.64           | 1,680.00          | 8.100          | 0.057        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.270</b> |

---

**UNNAMED TRIBUTARY TO CHACO PRE-**  
**MINE HYDROLOGY AND**  
**SEDIMENTOLOGY**

*PRE-MINE 25-yr, 6-hour PRECIPITATION*

BHP Billiton

***General Information***

***Storm Information:***

|                 |              |
|-----------------|--------------|
| Storm Type:     | Type II-70   |
| Design Storm:   | 25 yr - 6 hr |
| Rainfall Depth: | 1.560 inches |

***Particle Size Distribution:***

| Size (mm) | CW1      | CW2      | CW3      | CW4      | CW5      |
|-----------|----------|----------|----------|----------|----------|
| 0.4250    | 100.000% | 100.000% | 100.000% | 100.000% | 100.000% |
| 0.2500    | 71.002%  | 79.759%  | 73.724%  | 79.290%  | 83.334%  |
| 0.1500    | 52.517%  | 62.156%  | 54.007%  | 60.839%  | 68.417%  |
| 0.0750    | 40.991%  | 48.658%  | 41.754%  | 47.304%  | 53.993%  |
| 0.0159    | 36.096%  | 42.458%  | 36.968%  | 41.409%  | 46.327%  |
| 0.0100    | 29.101%  | 34.107%  | 30.394%  | 33.504%  | 35.855%  |
| 0.0050    | 10.110%  | 8.789%   | 9.084%   | 8.485%   | 9.027%   |
| 0.0020    | 5.803%   | 5.220%   | 5.060%   | 4.944%   | 5.817%   |
| 0.0010    | 5.384%   | 4.878%   | 4.663%   | 4.594%   | 5.499%   |
| 0.0004    | 4.868%   | 4.198%   | 4.196%   | 3.982%   | 4.619%   |



***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 287.200                                   | 287.200                               | 204.62                     | 9.79                                 | 787.9              | 84,130                              | 38.23                                 | 26.15          |

## *Particle Size Distribution(s) at Each Structure*

### *Structure #1:*

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 79.764%  |
| 0.0750    | 61.668%  |
| 0.0159    | 54.599%  |
| 0.0100    | 44.890%  |
| 0.0050    | 13.416%  |
| 0.0020    | 7.473%   |
| 0.0010    | 6.887%   |
| 0.0004    | 6.197%   |

**Subwatershed Hydrology Detail:**

| Stru # | SWS #    | SWS Area (ac)  | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|--------|----------|----------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #1     | 1        | 287.200        | 0.270              | 0.000        | 0.000  | 85.500       | M   | 204.62               | 9.794                 |
|        | <b>Σ</b> | <b>287.200</b> |                    |              |        |              |     | <b>204.62</b>        | <b>9.794</b>          |

**Subwatershed Sedimentology Detail:**

| Stru # | SWS #    | Soil K | L (ft)   | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l)  |
|--------|----------|--------|----------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|--------------|
| #1     | 1        | 0.151  | 1,000.00 | 7.30  | 0.2450 | 1.0000 | 3    | 787.9           | 84,130                     | 38.23                       | 26.15        |
|        | <b>Σ</b> |        |          |       |        |        |      | <b>787.9</b>    | <b>84,130</b>              | <b>38.23</b>                | <b>26.15</b> |

**Subwatershed Time of Concentration Details:**

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.80      | 80.64            | 1,680.00          | 2.190          | 0.213        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 7.30      | 122.64           | 1,680.00          | 8.100          | 0.057        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.270</b> |



**UNNAMED TRIBUTARY TO CHACO PRE-**  
**MINE HYDROLOGY AND**  
**SEDIMENTOLOGY**

*PRE-MINE 100-yr, 6-hour PRECIPITATION*

BHP Billiton

## *General Information*

### *Storm Information:*

|                 |               |
|-----------------|---------------|
| Storm Type:     | Type II-70    |
| Design Storm:   | 100 yr - 6 hr |
| Rainfall Depth: | 2.040 inches  |

### *Particle Size Distribution:*

| Size (mm) | CW1      | CW2      | CW3      | CW4      | CW5      |
|-----------|----------|----------|----------|----------|----------|
| 0.4250    | 100.000% | 100.000% | 100.000% | 100.000% | 100.000% |
| 0.2500    | 71.002%  | 79.759%  | 73.724%  | 79.290%  | 83.334%  |
| 0.1500    | 52.517%  | 62.156%  | 54.007%  | 60.839%  | 68.417%  |
| 0.0750    | 40.991%  | 48.658%  | 41.754%  | 47.304%  | 53.993%  |
| 0.0159    | 36.096%  | 42.458%  | 36.968%  | 41.409%  | 46.327%  |
| 0.0100    | 29.101%  | 34.107%  | 30.394%  | 33.504%  | 35.855%  |
| 0.0050    | 10.110%  | 8.789%   | 9.084%   | 8.485%   | 9.027%   |
| 0.0020    | 5.803%   | 5.220%   | 5.060%   | 4.944%   | 5.817%   |
| 0.0010    | 5.384%   | 4.878%   | 4.663%   | 4.594%   | 5.499%   |
| 0.0004    | 4.868%   | 4.198%   | 4.196%   | 3.982%   | 4.619%   |

***Structure Summary:***

|    | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | 287.200                                   | 287.200                               | 334.11                     | 16.32                                | 1,380.2            | 86,982                              | 40.63                                 | 28.22          |



***Particle Size Distribution(s) at Each Structure***

***Structure #1:***

| Size (mm) | In/Out   |
|-----------|----------|
| 0.4250    | 100.000% |
| 0.2500    | 100.000% |
| 0.1500    | 76.713%  |
| 0.0750    | 59.308%  |
| 0.0159    | 52.510%  |
| 0.0100    | 43.172%  |
| 0.0050    | 12.903%  |
| 0.0020    | 7.187%   |
| 0.0010    | 6.623%   |
| 0.0004    | 5.960%   |

***Subwatershed Hydrology Detail:***

| Stru #   | SWS # | SWS Area (ac)  | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|----------|-------|----------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #1       | 1     | 287.200        | 0.270              | 0.000        | 0.000  | 85.500       | M   | 334.11               | 16.324                |
| <b>Σ</b> |       | <b>287.200</b> |                    |              |        |              |     | <b>334.11</b>        | <b>16.324</b>         |

***Subwatershed Sedimentology Detail:***

| Stru #   | SWS # | Soil K | L (ft)   | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l)  |
|----------|-------|--------|----------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|--------------|
| #1       | 1     | 0.151  | 1,000.00 | 7.30  | 0.2450 | 1.0000 | 3    | 1,380.2         | 86,982                     | 40.63                       | 28.22        |
| <b>Σ</b> |       |        |          |       |        |        |      | <b>1,380.2</b>  | <b>86,982</b>              | <b>40.63</b>                | <b>28.22</b> |

***Subwatershed Time of Concentration Details:***

| Stru #    | SWS #    | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|-----------|----------|---|-----------|------------------|-------------------|----------------|--------------|
| #1        | 1        | 5. Nearly bare and untilled, and alluvial valley fans | 4.80      | 80.64            | 1,680.00          | 2.190          | 0.213        |
|           |          | 8. Large gullies, diversions, and low flowing streams | 7.30      | 122.64           | 1,680.00          | 8.100          | 0.057        |
| <b>#1</b> | <b>1</b> | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.270</b> |

## **Attachment 18.B-6**

Eroded and Parent Soil Particle Size Distribution Analysis February 2008 (edited March 2012)



# **ERODED AND PARENT SOIL PARTICLE SIZE DISTRIBUTION ANALYSIS**

***BHP NAVAJO COAL COMPANY***

FEBRUARY 2008

**PREPARED FOR:**

BHP Navajo Coal Company

**PREPARED BY:**

**UNIVERSITY OF KENTUCKY  
BIOSYSTEMS AND AGRICULTURAL ENGINEERING DEPARTMENT  
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**EDITED BY:**

BHP Navajo Coal Company  
(March 2012 *for formatting*)

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## **1. INTRODUCTION**

The Parent Soil and Eroded Particle Size Distribution (EPSD) analysis conducted on four different composite sediment samples from the BHP Billiton Navajo Extension Project area was complete and the results are presented herein. The analysis was completed using the composite samples that were forwarded to the University of Kentucky.

The report contains analysis for:

1. Eroded particle size analysis (rainfall simulator, wet sieve and particle size analyzer) based on 3 replicates per sediment sample.
2. Standard soil particle analysis (Mechanical sieving washing material finer than 0.106 mm. Disperse particles finer than 0.075 mm then use particle size analyzer) based on three replicates per sediment sample.
3. Organic material.
4. Calculation of K-factor.

## **2. SEDIMENT CHARACTERIZATION**

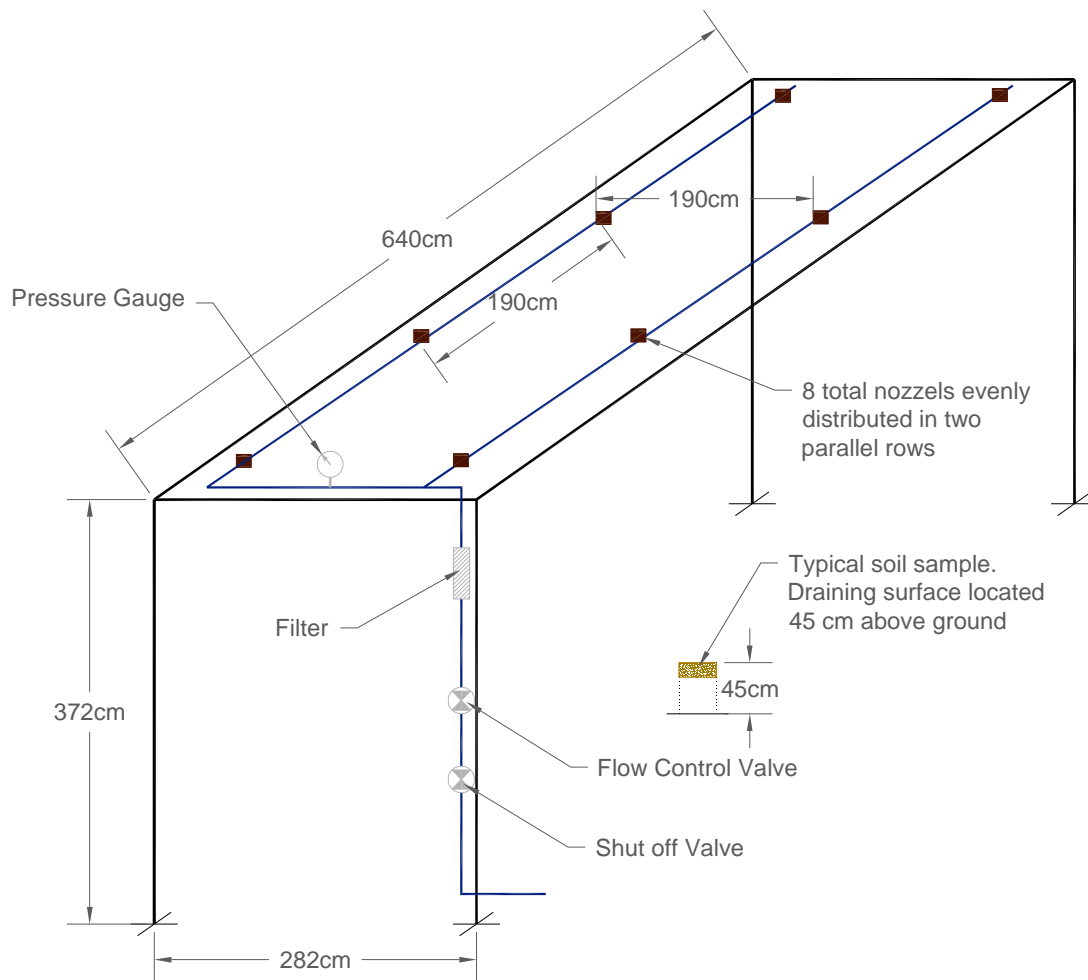
Soil samples, representing specific land uses and spatial distributions, were collected from designated locations around the Navajo Extension Project site. Each group of sample locations were selected to obtain a composite sample that is a reasonable representation of the sediment characteristics found in that particular watershed or area of interest. The particular sampling locations, used to make up the composite samples, were chosen by BHP consultants.



### **3. METHODOLOGY**

The rainfall simulator developed at the University of Kentucky for erosion studies was utilized to generate the rainfall necessary to obtain the EPSD data from the soil samples. The simulator is approximately 6m by 3m and rainfall nozzles were located 3m above the soil samples to develop the proper rainfall distribution, drop size and raindrop velocity (see Figure 1). Nozzles were operated at 7 psi. The calibration consisted of a trade off between rainfall intensity and on/off pulse time while maintaining approximately a 7 psi pressure at the nozzles. Based on these calibrations a 2 seconds on, 3 seconds off pulse was utilized generating approximately a 2 in/hr (50 mm/hr) rainfall rate. The ~2 inch/hr rate (50 mm/hr) was based on the rainfall intensity for a 10-year 24-hour (Type II-70 rainfall distribution) design storm. The experiments were conducted for 1 hour to generate runoff that produced a large enough quantity of sediment to conduct analysis. The soil samples used for the rainfall simulator were located in rectangular containers (see Figure A3) with a surface area of approximately 0.53 ft<sup>2</sup> (6 ¾ in. wide by 11 ¼ in. long). Each container has a 9% slope inclination. Sediment-laden runoff was directed to a series of sieve trays that were located in an 18.75 L bucket and wet sieving was conducted. Rainfall was precluded from entering the buckets through protection afforded by plexiglass covers (see Figures A1 to A3 on Appendix A). The sediment that passed the 200 sieve was processed through the X-Ray particle size analyzer. No dispersion agent was used.

**Figure 1:** Schematic of the Rainfall Simulator used to obtain the EPSD of the soil samples.



### **3.1 Procedure**

#### **3.1.1 Eroded Particle Size Distribution**

The three replicates of each soil sample are rained on for approximately one hour or until enough runoff containing sufficient sediment particles has been collected. The runoff is then sieved using a mechanical/pneumatic wet sieving device to obtain the portion of the particle distribution that is retained in the set of sieves #60 (0.250 mm), #100 (0.150 mm), #140 (0.106 mm) and #200 (0.075 mm). The wet sieve test procedure used in this case is an alternative from the standard test found in ASTM D1140 (American Standard for Testing Materials). The portion of the EPSD retained above 0.075 mm is then obtained by weighting the dried soil retained in each of the sieves. Once the wet sieving is complete, the finer portion of the sediments in the runoff is dried to retrieve the particles finer than 0.075 mm and an X-Ray particle size analyzer is used to obtain the remainder spectrum of the EPSD curve.

The particle size analyzer used for this analysis is a SEDIGRAPH 5100 from MICROMERITICS owned by the University of Kentucky (see Figure 2). This particle size analyzer uses the sedimentation technique, which measures the gravity-induced settling rates of different size particles in a liquid of known properties.

The SediGraph 5100 uses a narrow, horizontally collimated beam of X-rays to directly measure the relative mass concentration of particles in the liquid medium. This is accomplished by first measuring the intensity of a reference X-ray beam which is projected through the clear liquid medium prior to the introduction of the sample. A homogeneously dispersed mixture of solid sample and liquid is next circulated through the cell. The solid particles absorb (and scatter) some of the X-ray energy, which again is measured, this time to establish a value for full scale attenuation. Agitation of the mixture is ceased and the dispersion is allowed to settle while X-ray intensity is monitored. During the sedimentation process, the largest particles are first to fall below the measuring level, and each mass measurement represents the cumulative mass fraction of the remaining fine particles. Gradually, finer and finer particles settle out, ultimately clearing the measuring zone of suspended particles and allowing the X-ray beam to again pass through the cell unattenuated. The particle size analyzer determines particle size from velocity measurements by applying Stokes law under the known conditions of liquid density and viscosity and particle density. Settling velocity is determined at each relative mass measurement from knowledge of the distance the X-ray beam is from the top of the sample cell and the time at which the mass measurement was taken. From the velocity equals distance divided by time relationship, it can determine the maximum velocity of all particles remaining above the measurement zone, these velocities being associated with the finer particles. A sequence of closely-spaced measurements provides a distribution of mass fraction remaining in suspension versus velocity or size class or, as more commonly termed, cumulative mass percent finer. Finally, the SediGraph 5100 can measure particles from 300 to 0.10  $\mu\text{m}$  equivalent spherical diameter.



The Sedigraph 5100 was maintained/tuned and calibrated by University of Kentucky personnel prior to the present ESPD analysis. The equipment was last calibrated on the 19<sup>th</sup> of April, 2007 following Micromeritics guidelines.



**Figure 2:** SediGraph 5100 Particle Size Analyzer

### **3.1.2 Parent Particle Size Distribution (PPSD)**

The soil material is first air dried. The portion of dry soil passing sieve # 10 was then grinded to break up all clumps. A sample of approximately 500 g is obtained by quartering. The sample is then introduced to a rack of 7 different sieves with openings of decreasing size from top to bottom (a pan is placed below the stack to collect the finer portion). The rack of sieves is shaken using a mechanical powered shaker (see Figure A4 on Appendix A) for at least 10 minutes. The sieves used to obtain the spectrum of the PPSD above 0.075 mm were 8 in. (203 mm) in diameter and with openings of 2.000 mm, 0.595 mm, 0.425 mm, 0.250 mm, 0.150 mm, 0.106 mm and 0.075 mm (corresponding to sieves # 10, 30, 40, 60, 100, 140 and 200, respectively). After the sample is shaken, the mass of soil retained on sieves # 10, 30, 40, 60 and 100 are determined. The material collected in sieves # 140 and # 200 was washed through the sieves to remove all the remaining fines. In this case, portions retained on those two sieves are collected separately and oven-dried before the retained mass is measured.

The soil particles that passed through sieve #200 are first chemically dispersed using sodium hexametaphosphate dispersant and then analyzed using the X-Ray particle size analyzer.

### 3.1.3 Erodibility Factor K

Soil erosion by water for a specific watershed is usually calculated using the well known empirical Revised Universal Soil Loss Equation (Renard *et al.*) and is given by the following expression:

$$A = RKLSCP$$

*A* is the average soil loss per unit area, expressed in units selected for *K* and the time period specified by *R*. Normal English units are tons/acre/year.

*R* is the rainfall/runoff factor, which is the number of rainfall units for rainfall energy and runoff, plus the factor for runoff from snowmelt.

*K* is the soil erodibility factor, which is the rate of soil loss per unit of *R* for a given soil on a slope of 9% with slope length of 72.6 ft (22.1 m).

*L* is the slope length factor, which is the ratio of soil loss from a defined slope length relative to that from a slope length of 72.6 ft (22.1 m).

*S* is the slope steepness factor, which is the ratio of soil loss from a slope with a given steepness relative to that from a 9% slope.

*C* is the cover and management factor, which is the ratio of soil loss from an area with a known cover and management. And,

*P* is the supporting conservation practice factor.

The RUSLE K-Factor is a measure of a soil's resistance to erosive powers of rainfall energy and runoff. Practically, soil erodibility is an integration of the impacts of rainfall and runoff on soil loss for a given soil. Experimentally, soil loss erodibility is the soil loss per unit rainfall index on a standard erosion plot.

The K-factor can be obtained through 3 different sources. Through published data, Wischmeier nomograph developed from data collected on 55 different Midwestern USA agricultural soils or using the analytical approximation of the Wischmeier nomograph, which is given by the following relationship:

$$K = \frac{2.1 \times 10^{-4} (12 - OM) M^{1.14} + 3.25(S_1 - 2) + 2.5(P_1 - 3)}{100}$$

where *K* is the soil erodibility factor in tons per acre per unit rainfall index (tons · acre · hr/hundreds · acre · ft · tonsf · in.), *OM* is the percentage organic matter, *P<sub>1</sub>* is the permeability index (1 to 4), *S<sub>1</sub>* is the soil structure index (1 to 6) and *M* is a parameter that depends on the parent particle size distribution and is given by:

$$M = (\%MS + \%VFS)(100 - \%CL)$$

where %*CL* is percentage clay (size < 0.002 mm in diameter), %*MS* is percentage silt (0.002 – 0.05 mm) and %*VFS* is percentage very fine sand (0.05 – 0.1 mm). The above equation is valid for values of %*MS* + %*VFS* less than 70.

It is important to note that the Wischmeier nomograph works well for soils that have similar characteristics of those found in the Midwestern area of the United States; however it did not yield good results for Hawaiian soils, for example.

The percentage clay, silt and very fine sand are obtained directly from the parent particle size distribution (see 2.1.2). The percentage in organic matter *OM* is determined by firing the soil sample (around 25 grams) at a temperature of 550 °C for a period of 1 hour in a furnace. The loss by weight of the sample during this ignition is calculated as the organic matter. Results are reported as percent organic matter by weight in the soil.

The Wischmeier nomograph only considers soils with *OM* less or equal than 4%; thus the calculations were made by adjusting the *OM* to a maximum of 4%. Note that this reduction in the *OM* translates into a more conservative condition.

Since no information regarding permeability and structure of the sediment samples tested is available, only the first approximation of the K factor using the Wischmeier nomograph will be provided.



## **4. RESULTS**

### **4.1 Sample NMA: “Sandy”**



Average total sediment mass yielded during rainfall simulator test: 28.32 g

Average mass of EPSD coarser than 0.250 mm: 14.02 g

#### **4.1.1 Parent Soil Description**

- a) Texture: sand with few fine gravels.
- b) Color: brown.
- c) Fine fraction (< 0.075 mm): 3.255%
- d) USDA Textural Classification: SAND

#### **4.1.2 K – Factor Calculation**

Organic Material: 0.854%

Percent Silt + Very Fine Sand (0.002 – 0.1 mm): 5.475%

Percent Sand (0.1 – 2 mm): 93.370 %

First Approximation: **K = 0.06**

### 4.1.3 Parent Particle Size Distribution

**Table 1:** Parent Particle Size Distribution for Sample NMA

| Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) |
|---------------|---------------------------|---------------|---------------------------|---------------|---------------------------|
| 2             | 99.496                    | 0.01059       | 0.833                     | 0.001059      | 0.577                     |
| 0.6           | 91.745                    | 0.01          | 0.828                     | 0.001         | 0.567                     |
| 0.425         | 82.640                    | 0.009441      | 0.823                     | 0.000944      | 0.556                     |
| 0.25          | 46.119                    | 0.008913      | 0.821                     | 0.000891      | 0.544                     |
| 0.15          | 12.976                    | 0.008414      | 0.819                     | 0.000841      | 0.531                     |
| 0.106         | 6.126                     | 0.007943      | 0.816                     | 0.000794      | 0.520                     |
| 0.075         | 3.255                     | 0.007499      | 0.815                     | 0.00075       | 0.506                     |
| 0.07079       | 2.957                     | 0.007079      | 0.815                     | 0.000708      | 0.493                     |
| 0.06683       | 2.860                     | 0.006683      | 0.813                     | 0.000668      | 0.483                     |
| 0.0631        | 2.745                     | 0.00631       | 0.810                     | 0.000631      | 0.473                     |
| 0.05957       | 2.616                     | 0.005957      | 0.809                     | 0.000596      | 0.460                     |
| 0.05623       | 2.474                     | 0.005623      | 0.806                     | 0.000562      | 0.450                     |
| 0.05309       | 2.324                     | 0.005309      | 0.801                     | 0.000531      | 0.439                     |
| 0.05012       | 2.170                     | 0.005012      | 0.796                     | 0.000501      | 0.426                     |
| 0.04732       | 2.018                     | 0.004732      | 0.788                     | 0.000473      | 0.412                     |
| 0.04467       | 1.870                     | 0.004467      | 0.779                     | 0.000447      | 0.400                     |
| 0.04217       | 1.731                     | 0.004217      | 0.771                     | 0.000422      | 0.386                     |
| 0.03981       | 1.603                     | 0.003981      | 0.759                     | 0.000398      | 0.374                     |
| 0.03758       | 1.490                     | 0.003758      | 0.747                     | 0.000376      | 0.362                     |
| 0.03548       | 1.390                     | 0.003548      | 0.736                     | 0.000355      | 0.351                     |
| 0.0335        | 1.306                     | 0.00335       | 0.721                     | 0.000335      | 0.341                     |
| 0.03162       | 1.237                     | 0.003162      | 0.708                     | 0.000316      | 0.334                     |
| 0.02985       | 1.177                     | 0.002985      | 0.697                     | 0.000299      | 0.325                     |
| 0.02818       | 1.130                     | 0.002818      | 0.684                     | 0.000282      | 0.318                     |
| 0.02661       | 1.092                     | 0.002661      | 0.676                     | 0.000266      | 0.310                     |
| 0.02512       | 1.060                     | 0.002512      | 0.668                     | 0.000251      | 0.301                     |
| 0.02371       | 1.032                     | 0.002371      | 0.664                     |               |                           |
| 0.02239       | 1.008                     | 0.002239      | 0.659                     |               |                           |
| 0.02113       | 0.986                     | 0.002113      | 0.656                     |               |                           |
| 0.01995       | 0.966                     | 0.001995      | 0.651                     |               |                           |
| 0.01884       | 0.945                     | 0.001884      | 0.648                     |               |                           |
| 0.01778       | 0.927                     | 0.001778      | 0.641                     |               |                           |
| 0.01679       | 0.911                     | 0.001679      | 0.636                     |               |                           |
| 0.01585       | 0.897                     | 0.001585      | 0.628                     |               |                           |
| 0.01496       | 0.884                     | 0.001496      | 0.623                     |               |                           |
| 0.01413       | 0.873                     | 0.001413      | 0.615                     |               |                           |
| 0.01334       | 0.862                     | 0.001334      | 0.606                     |               |                           |
| 0.01259       | 0.852                     | 0.001259      | 0.600                     |               |                           |
| 0.01189       | 0.846                     | 0.001189      | 0.592                     |               |                           |
| 0.01122       | 0.838                     | 0.001122      | 0.586                     |               |                           |

Figure 3: Parent Particle Size Distributions Chart for Sample NMA

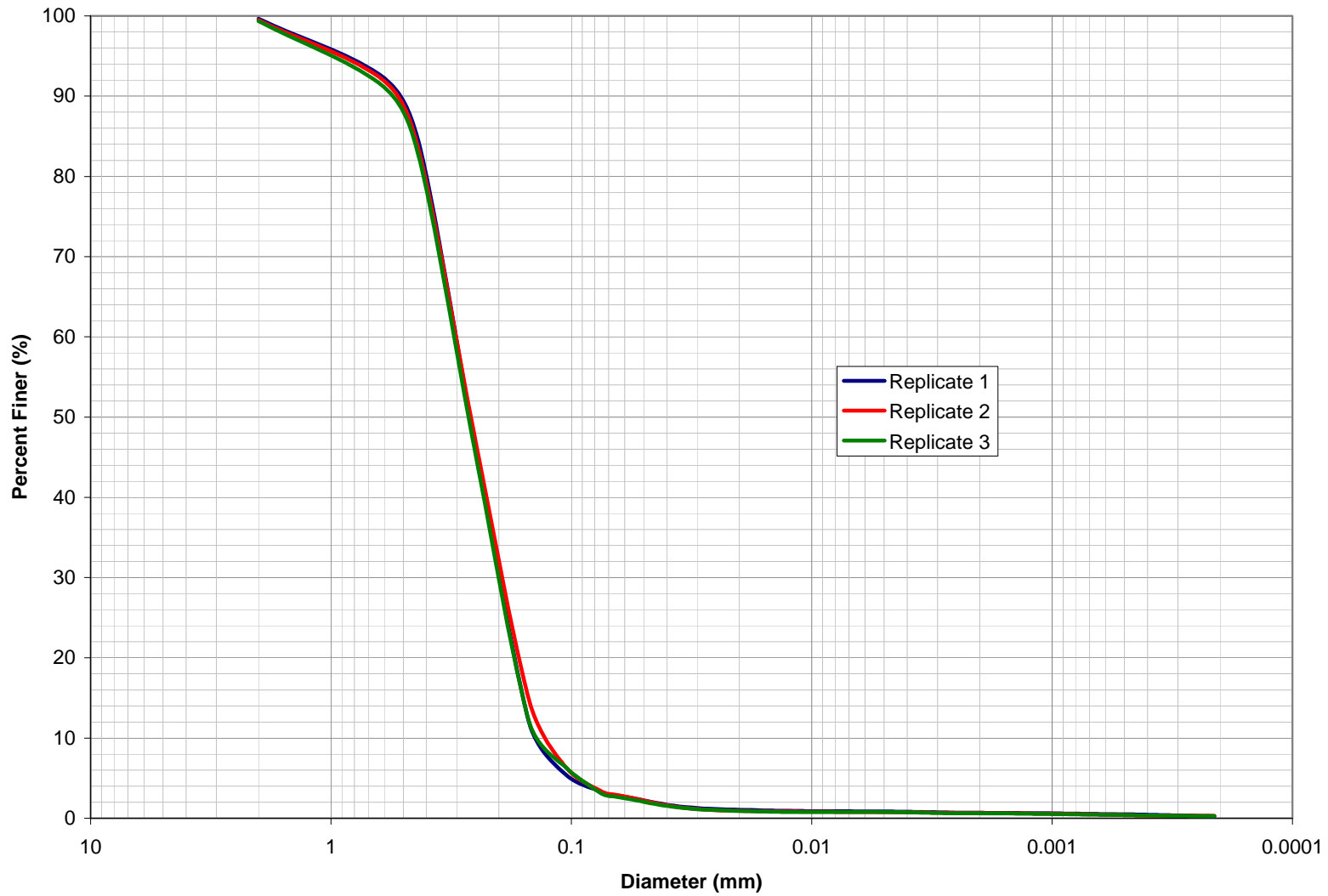
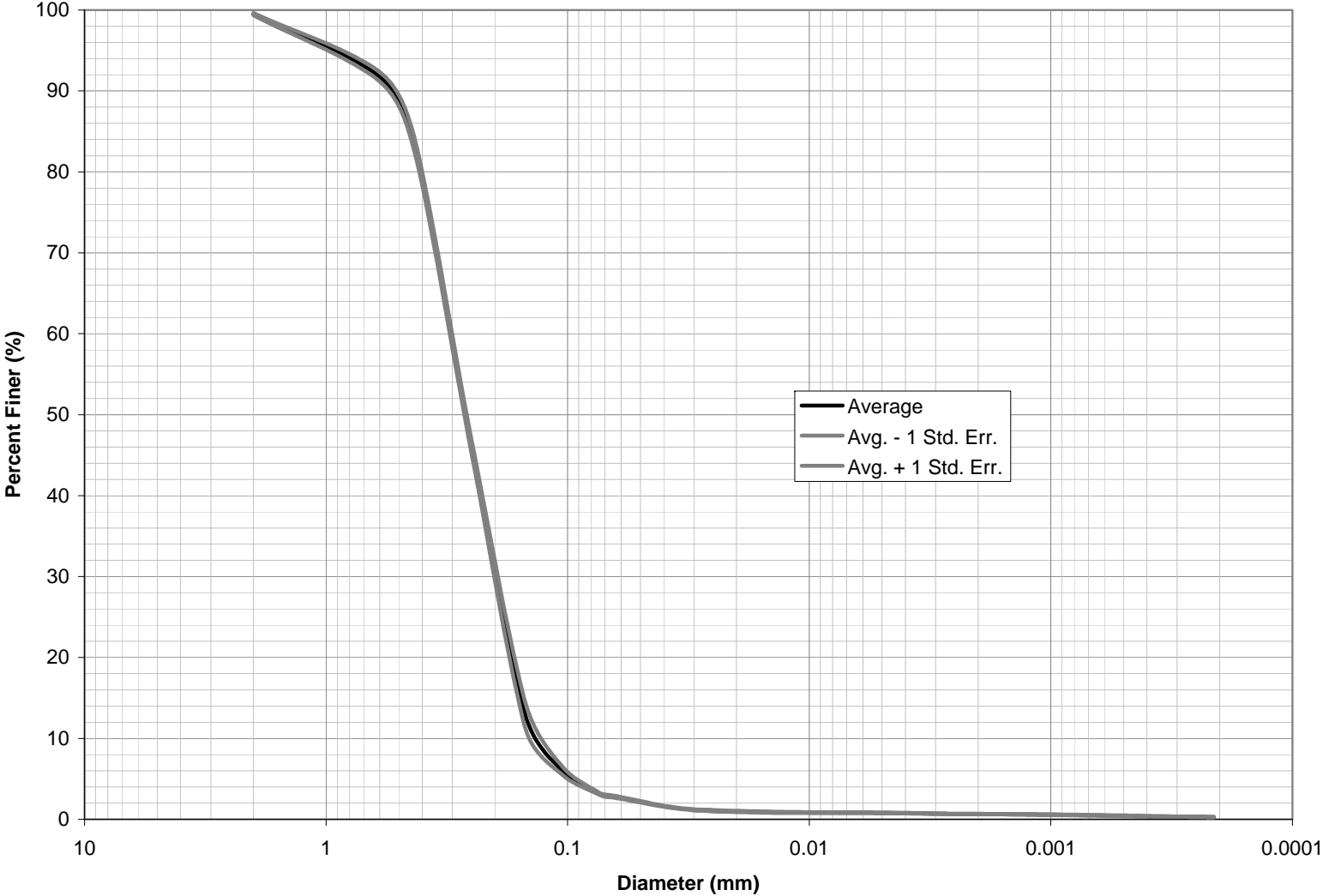




Figure 4: Average Parent Particle Size Distribution Chart for Sample NMA



#### 4.1.4 Eroded Particle Size Distribution

**Table 2:** Eroded Particle Size Distribution for Sample NMA

| Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) |
|---------------|---------------------------|---------------|---------------------------|---------------|---------------------------|
| 0.25          | 50.527                    | 0.008913      | 26.486                    | 0.000891      | 8.559                     |
| 0.15          | 33.896                    | 0.008414      | 25.897                    | 0.000841      | 8.543                     |
| 0.106         | 31.867                    | 0.007943      | 25.254                    | 0.000794      | 8.527                     |
| 0.075         | 31.272                    | 0.007499      | 24.514                    | 0.00075       | 8.504                     |
| 0.07079       | 31.272                    | 0.007079      | 23.679                    | 0.000708      | 8.480                     |
| 0.06683       | 31.272                    | 0.006683      | 22.783                    | 0.000668      | 8.448                     |
| 0.0631        | 31.272                    | 0.00631       | 21.768                    | 0.000631      | 8.409                     |
| 0.05957       | 31.272                    | 0.005957      | 20.684                    | 0.000596      | 8.369                     |
| 0.05623       | 31.272                    | 0.005623      | 19.540                    | 0.000562      | 8.322                     |
| 0.05309       | 31.272                    | 0.005309      | 18.344                    | 0.000531      | 8.283                     |
| 0.05012       | 31.272                    | 0.005012      | 17.120                    | 0.000501      | 8.235                     |
| 0.04732       | 31.272                    | 0.004732      | 15.916                    | 0.000473      | 8.188                     |
| 0.04467       | 31.272                    | 0.004467      | 14.786                    | 0.000447      | 8.141                     |
| 0.04217       | 31.272                    | 0.004217      | 13.728                    | 0.000422      | 8.094                     |
| 0.03981       | 31.272                    | 0.003981      | 12.790                    | 0.000398      | 7.929                     |
| 0.03758       | 31.272                    | 0.003758      | 11.976                    | 0.000376      | 7.714                     |
| 0.03548       | 31.272                    | 0.003548      | 11.319                    | 0.000355      | 7.483                     |
| 0.0335        | 31.188                    | 0.00335       | 10.810                    | 0.000335      | 7.218                     |
| 0.03162       | 31.104                    | 0.003162      | 10.392                    | 0.000316      | 6.945                     |
| 0.02985       | 30.997                    | 0.002985      | 10.082                    | 0.000299      | 6.664                     |
| 0.02818       | 30.905                    | 0.002818      | 9.848                     | 0.000282      | 6.349                     |
| 0.02661       | 30.814                    | 0.002661      | 9.653                     | 0.000266      | 6.035                     |
| 0.02512       | 30.714                    | 0.002512      | 9.496                     | 0.000251      | 5.712                     |
| 0.02371       | 30.630                    | 0.002371      | 9.371                     | 0.000237      | 5.381                     |
| 0.02239       | 30.529                    | 0.002239      | 9.254                     | 0.000224      | 5.033                     |
| 0.02113       | 30.446                    | 0.002113      | 9.163                     | 0.000211      | 4.661                     |
| 0.01995       | 30.362                    | 0.001995      | 9.064                     |               |                           |
| 0.01884       | 30.261                    | 0.001884      | 8.997                     |               |                           |
| 0.01778       | 30.178                    | 0.001778      | 8.931                     |               |                           |
| 0.01679       | 30.077                    | 0.001679      | 8.890                     |               |                           |
| 0.01585       | 29.929                    | 0.001585      | 8.841                     |               |                           |
| 0.01496       | 29.757                    | 0.001496      | 8.816                     |               |                           |
| 0.01413       | 29.543                    | 0.001413      | 8.775                     |               |                           |
| 0.01334       | 29.297                    | 0.001334      | 8.758                     |               |                           |
| 0.01259       | 29.026                    | 0.001259      | 8.733                     |               |                           |
| 0.01189       | 28.713                    | 0.001189      | 8.716                     |               |                           |
| 0.01122       | 28.354                    | 0.001122      | 8.683                     |               |                           |
| 0.01059       | 27.939                    | 0.001059      | 8.666                     |               |                           |
| 0.01          | 27.491                    | 0.001         | 8.625                     |               |                           |
| 0.009441      | 27.005                    | 0.000944      | 8.583                     |               |                           |

Figure 5: Eroded Particle Size Distributions Chart for Sample NMA

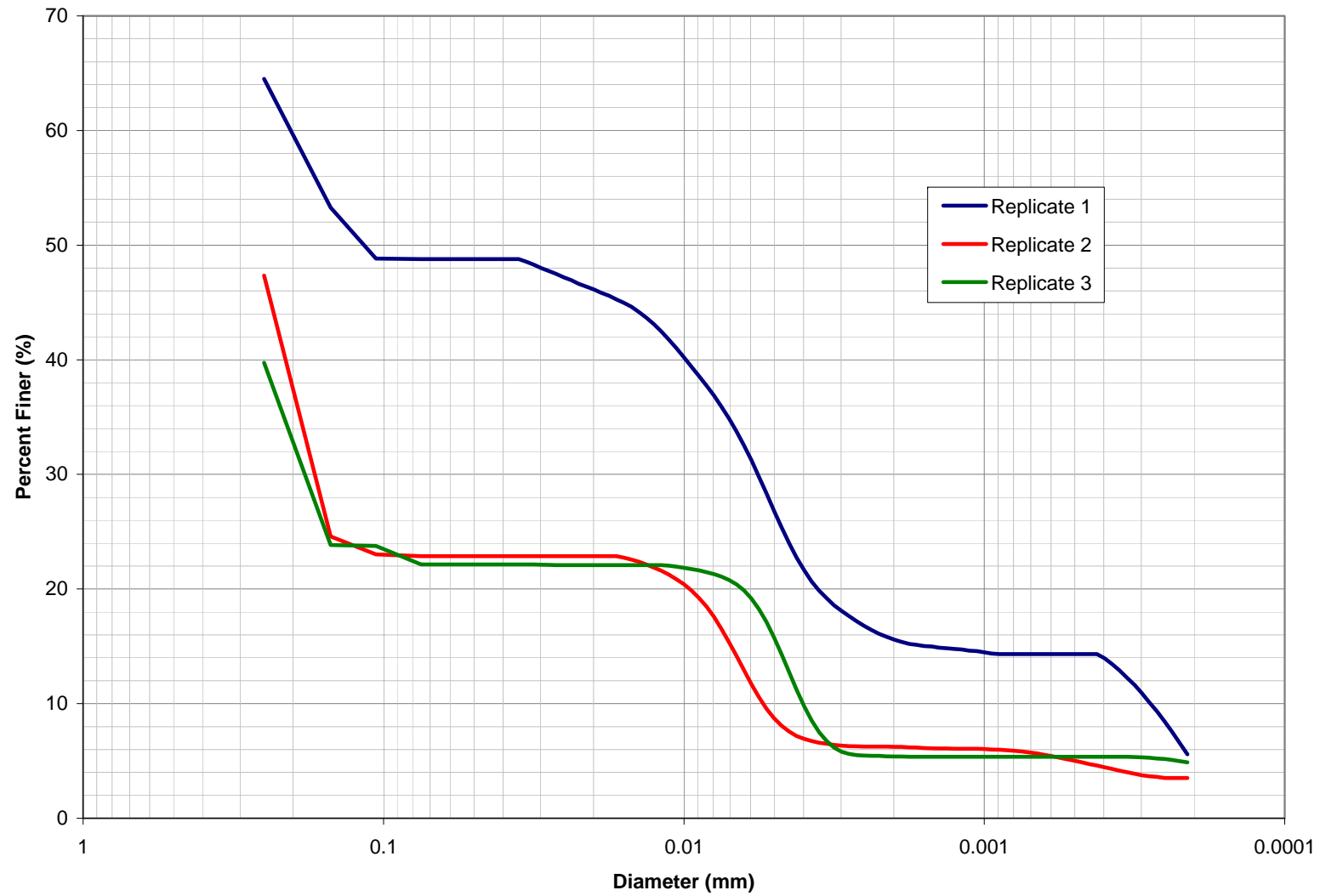




Figure 6: Average Eroded Particle Size Distribution Chart for Sample NMA

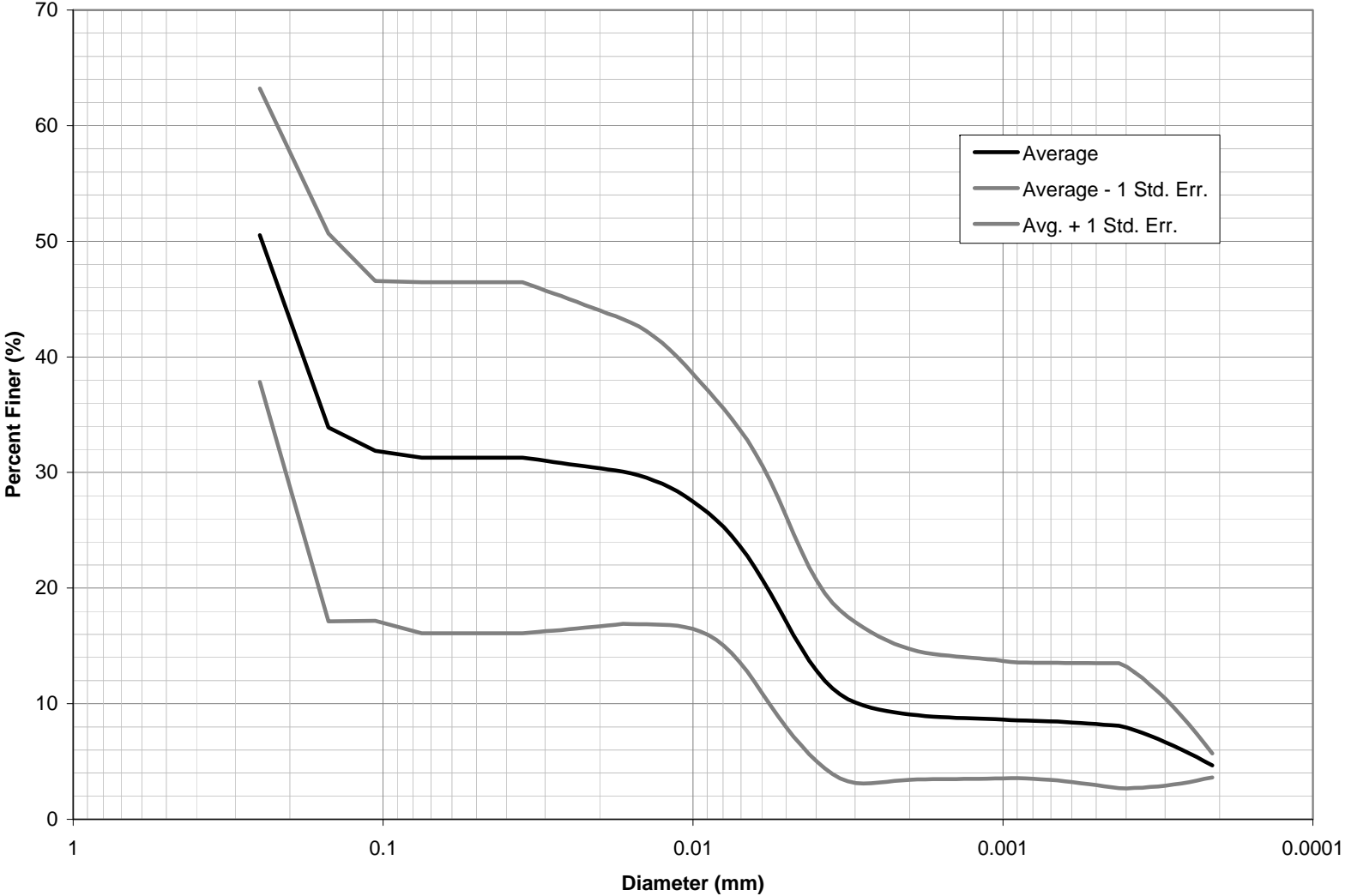
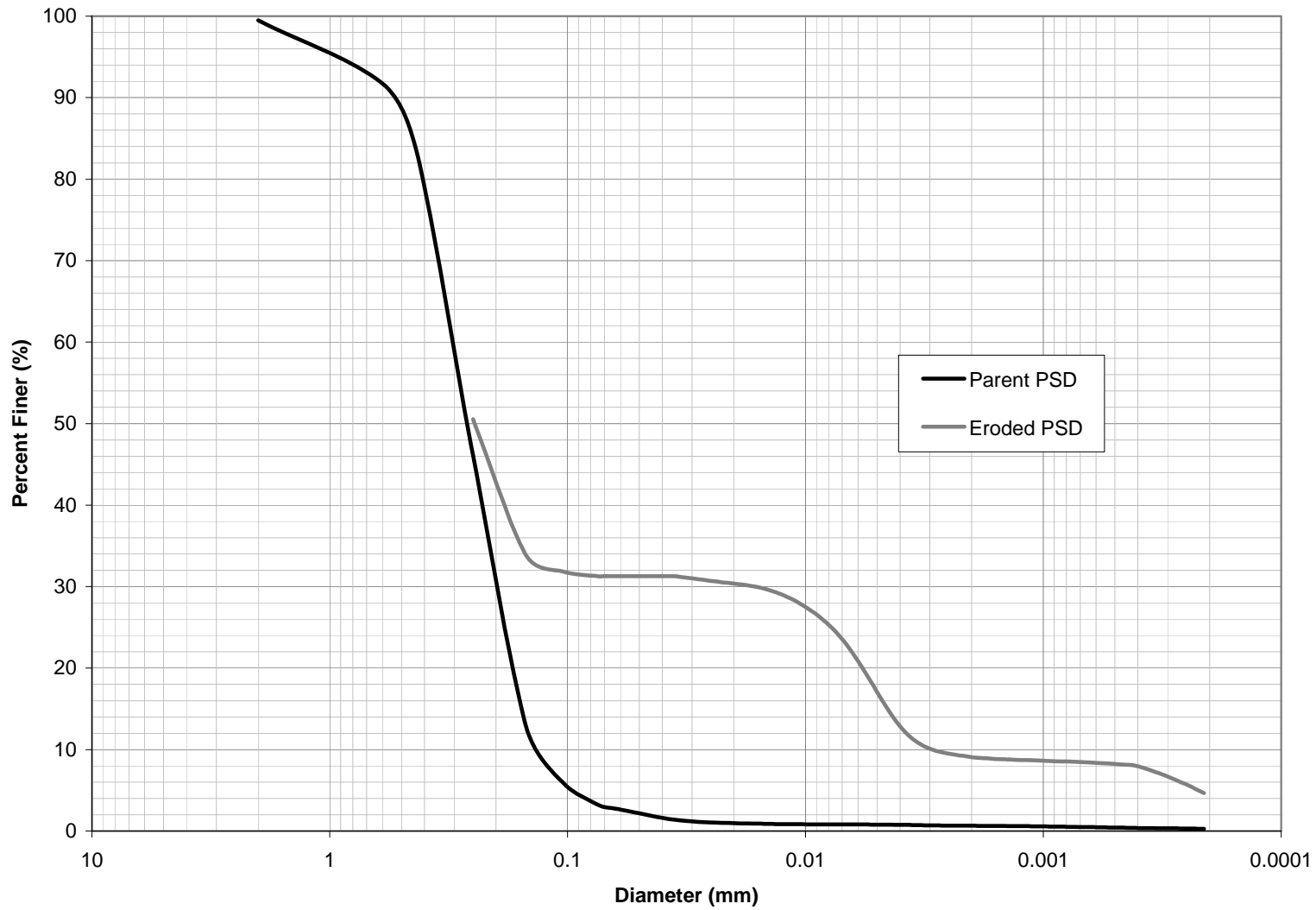


Figure 7: Combined Particle Size Distributions Chart for Sample NMA



## **4.2 Sample NMB: “Fine”**



Average total sediment mass yielded during rainfall simulator test: 30.31g

Average mass of EPSD coarser than 0.250 mm: 4.36g

### **4.2.1 Description**

- a) Texture: fine sand with silts and fine gravels.
- b) Color: grey.
- c) Fine fraction (< 0.075%): 15.937%
- d) USDA Textural Classification: LOAMY SAND

### **4.2.2 K – Factor Calculation**

Organic Material: 6.445%

Percent Silt + Very Fine Sand (0.002 – 0.1 mm): 15.100%

Percent Sand (0.1 – 2 mm): 75.114%

First Approximation: **K = 0.08**



### 4.2.3 Parent Particle Size Distribution

**Table 3: Parent Particle Size Distribution for Sample NMB**

| Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) |
|---------------|---------------------------|---------------|---------------------------|---------------|---------------------------|
| 2             | 93.744                    | 0.01059       | 7.207                     | 0.001059      | 1.228                     |
| 0.6           | 73.095                    | 0.01          | 7.088                     | 0.001         | 1.174                     |
| 0.425         | 63.904                    | 0.009441      | 6.986                     | 0.000944      | 1.126                     |
| 0.25          | 43.103                    | 0.008913      | 6.895                     | 0.000891      | 1.083                     |
| 0.15          | 21.889                    | 0.008414      | 6.815                     | 0.000841      | 1.057                     |
| 0.106         | 18.629                    | 0.007943      | 6.740                     | 0.000794      | 1.030                     |
| 0.075         | 15.937                    | 0.007499      | 6.665                     | 0.00075       | 1.014                     |
| 0.07079       | 15.565                    | 0.007079      | 6.595                     | 0.000708      | 0.997                     |
| 0.06683       | 15.420                    | 0.006683      | 6.525                     | 0.000668      | 0.987                     |
| 0.0631        | 15.233                    | 0.00631       | 6.449                     | 0.000631      | 0.976                     |
| 0.05957       | 15.013                    | 0.005957      | 6.363                     | 0.000596      | 0.965                     |
| 0.05623       | 14.751                    | 0.005623      | 6.277                     | 0.000562      | 0.944                     |
| 0.05309       | 14.456                    | 0.005309      | 6.191                     | 0.000531      | 0.922                     |
| 0.05012       | 14.128                    | 0.005012      | 6.094                     | 0.000501      | 0.896                     |
| 0.04732       | 13.784                    | 0.004732      | 5.997                     | 0.000473      | 0.869                     |
| 0.04467       | 13.414                    | 0.004467      | 5.890                     | 0.000447      | 0.843                     |
| 0.04217       | 13.033                    | 0.004217      | 5.783                     | 0.000422      | 0.811                     |
| 0.03981       | 12.657                    | 0.003981      | 5.664                     | 0.000398      | 0.784                     |
| 0.03758       | 12.281                    | 0.003758      | 5.557                     | 0.000376      | 0.768                     |
| 0.03548       | 11.910                    | 0.003548      | 5.429                     | 0.000355      | 0.752                     |
| 0.0335        | 11.551                    | 0.00335       | 5.305                     | 0.000335      | 0.735                     |
| 0.03162       | 11.213                    | 0.003162      | 5.177                     | 0.000316      | 0.724                     |
| 0.02985       | 10.885                    | 0.002985      | 5.037                     | 0.000299      | 0.707                     |
| 0.02818       | 10.584                    | 0.002818      | 4.882                     | 0.000282      | 0.696                     |
| 0.02661       | 10.294                    | 0.002661      | 4.710                     | 0.000266      | 0.685                     |
| 0.02512       | 10.021                    | 0.002512      | 4.528                     | 0.000251      | 0.674                     |
| 0.02371       | 9.769                     | 0.002371      | 4.319                     |               |                           |
| 0.02239       | 9.532                     | 0.002239      | 4.083                     |               |                           |
| 0.02113       | 9.301                     | 0.002113      | 3.821                     |               |                           |
| 0.01995       | 9.091                     | 0.001995      | 3.531                     |               |                           |
| 0.01884       | 8.887                     | 0.001884      | 3.230                     |               |                           |
| 0.01778       | 8.683                     | 0.001778      | 2.925                     |               |                           |
| 0.01679       | 8.500                     | 0.001679      | 2.614                     |               |                           |
| 0.01585       | 8.318                     | 0.001585      | 2.330                     |               |                           |
| 0.01496       | 8.135                     | 0.001496      | 2.072                     |               |                           |
| 0.01413       | 7.964                     | 0.001413      | 1.846                     |               |                           |
| 0.01334       | 7.797                     | 0.001334      | 1.664                     |               |                           |
| 0.01259       | 7.631                     | 0.001259      | 1.513                     |               |                           |
| 0.01189       | 7.475                     | 0.001189      | 1.400                     |               |                           |
| 0.01122       | 7.336                     | 0.001122      | 1.304                     |               |                           |

Figure 8: Parent Particle Size Distributions Chart for Sample NMB

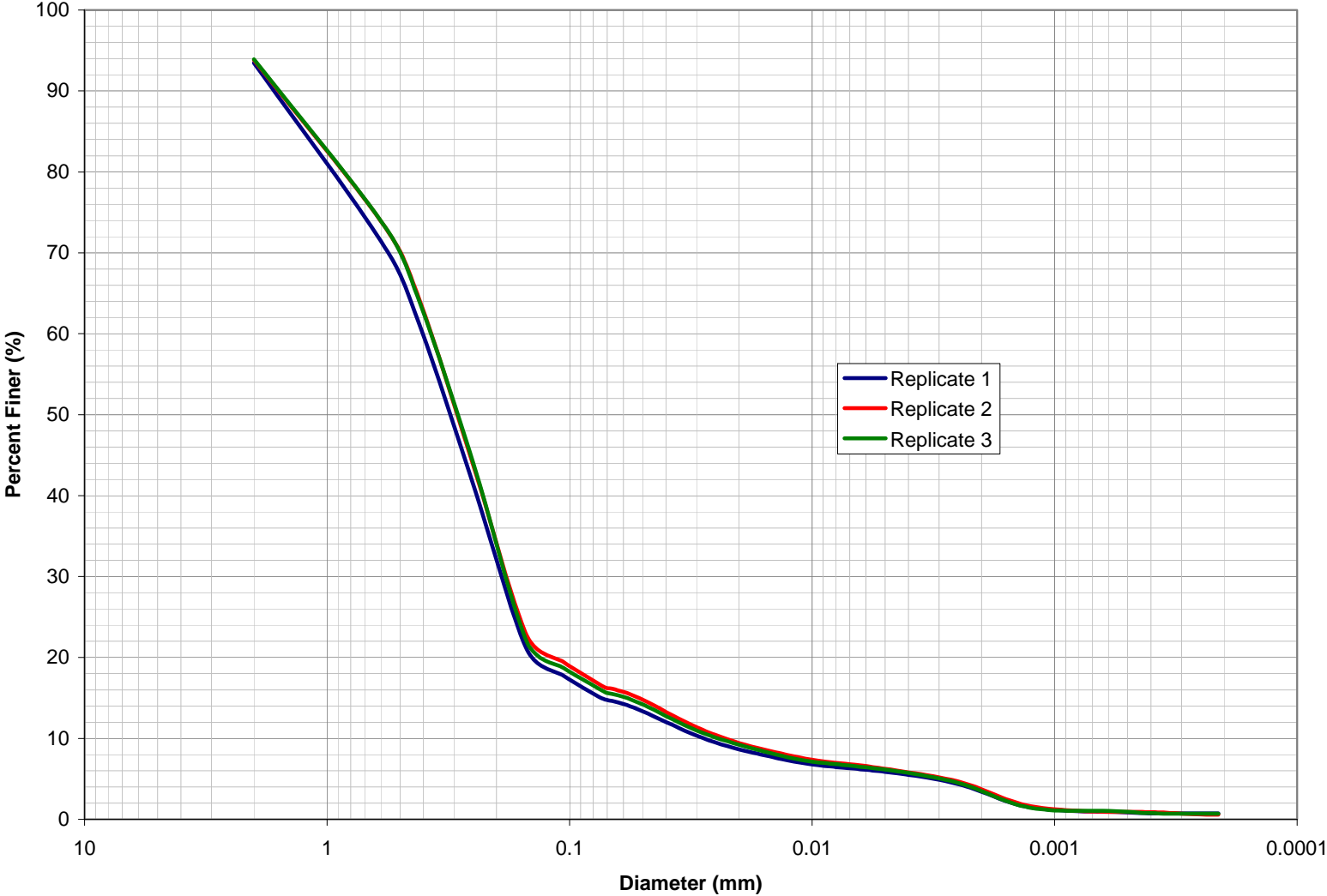
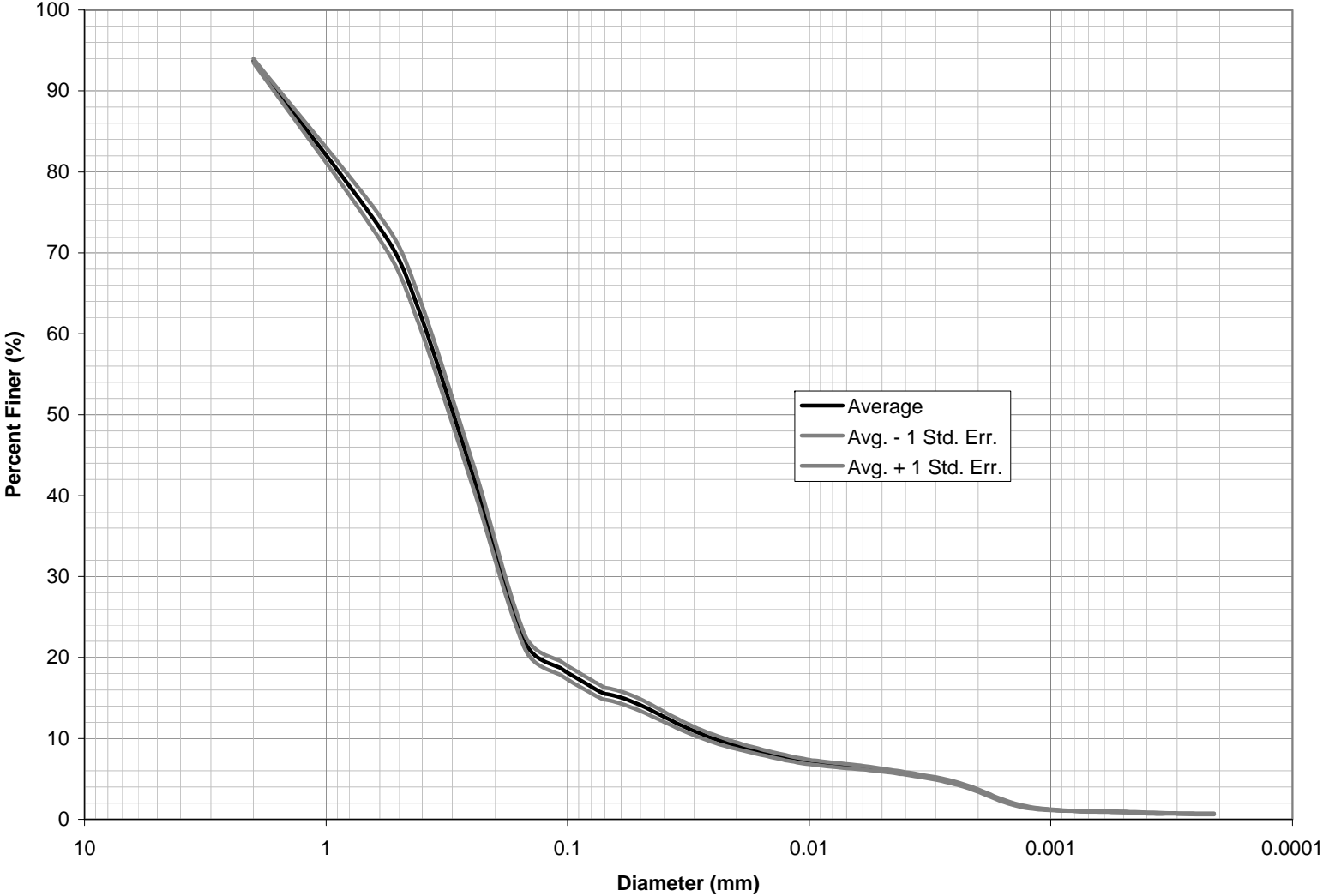


Figure 9: Average Parent Particle Size Distribution Chart for Sample NMB





#### 4.2.4 Eroded Particle Size Distribution

**Table 4:** Eroded Particle Size Distribution for Sample NMB

| Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) |
|---------------|---------------------------|---------------|---------------------------|---------------|---------------------------|
| 0.25          | 85.662                    | 0.008913      | 34.035                    | 0.000891      | 5.951                     |
| 0.15          | 72.479                    | 0.008414      | 31.104                    | 0.000841      | 5.894                     |
| 0.106         | 65.122                    | 0.007943      | 28.034                    | 0.000794      | 5.856                     |
| 0.075         | 58.342                    | 0.007499      | 24.920                    | 0.00075       | 5.779                     |
| 0.07079       | 58.110                    | 0.007079      | 21.841                    | 0.000708      | 5.723                     |
| 0.06683       | 58.052                    | 0.006683      | 18.973                    | 0.000668      | 5.667                     |
| 0.0631        | 57.974                    | 0.00631       | 16.376                    | 0.000631      | 5.592                     |
| 0.05957       | 57.897                    | 0.005957      | 14.130                    | 0.000596      | 5.516                     |
| 0.05623       | 57.820                    | 0.005623      | 12.273                    | 0.000562      | 5.441                     |
| 0.05309       | 57.722                    | 0.005309      | 10.807                    | 0.000531      | 5.366                     |
| 0.05012       | 57.605                    | 0.005012      | 9.694                     | 0.000501      | 5.291                     |
| 0.04732       | 57.468                    | 0.004732      | 8.875                     | 0.000473      | 5.197                     |
| 0.04467       | 57.312                    | 0.004467      | 8.271                     | 0.000447      | 5.122                     |
| 0.04217       | 57.096                    | 0.004217      | 7.843                     | 0.000422      | 5.047                     |
| 0.03981       | 56.862                    | 0.003981      | 7.494                     | 0.000398      | 4.953                     |
| 0.03758       | 56.627                    | 0.003758      | 7.224                     | 0.000376      | 4.840                     |
| 0.03548       | 56.372                    | 0.003548      | 7.030                     | 0.000355      | 4.745                     |
| 0.0335        | 56.078                    | 0.00335       | 6.857                     | 0.000335      | 4.651                     |
| 0.03162       | 55.786                    | 0.003162      | 6.722                     | 0.000316      | 4.556                     |
| 0.02985       | 55.532                    | 0.002985      | 6.586                     | 0.000299      | 4.441                     |
| 0.02818       | 55.259                    | 0.002818      | 6.528                     | 0.000282      | 4.286                     |
| 0.02661       | 54.967                    | 0.002661      | 6.469                     | 0.000266      | 4.149                     |
| 0.02512       | 54.659                    | 0.002512      | 6.411                     | 0.000251      | 4.011                     |
| 0.02371       | 54.311                    | 0.002371      | 6.392                     | 0.000237      | 3.910                     |
| 0.02239       | 53.924                    | 0.002239      | 6.374                     | 0.000224      | 3.810                     |
| 0.02113       | 53.461                    | 0.002113      | 6.335                     | 0.000211      | 3.729                     |
| 0.01995       | 52.939                    | 0.001995      | 6.297                     |               |                           |
| 0.01884       | 52.360                    | 0.001884      | 6.258                     |               |                           |
| 0.01778       | 51.704                    | 0.001778      | 6.220                     |               |                           |
| 0.01679       | 50.969                    | 0.001679      | 6.162                     |               |                           |
| 0.01585       | 50.138                    | 0.001585      | 6.125                     |               |                           |
| 0.01496       | 49.288                    | 0.001496      | 6.087                     |               |                           |
| 0.01413       | 48.303                    | 0.001413      | 6.049                     |               |                           |
| 0.01334       | 47.224                    | 0.001334      | 6.030                     |               |                           |
| 0.01259       | 46.007                    | 0.001259      | 6.030                     |               |                           |
| 0.01189       | 44.656                    | 0.001189      | 6.030                     |               |                           |
| 0.01122       | 43.054                    | 0.001122      | 6.030                     |               |                           |
| 0.01059       | 41.199                    | 0.001059      | 6.030                     |               |                           |
| 0.01          | 39.091                    | 0.001         | 6.030                     |               |                           |
| 0.009441      | 36.710                    | 0.000944      | 5.991                     |               |                           |

Figure 10: Eroded Particle Size Distributions Chart for Sample NMB

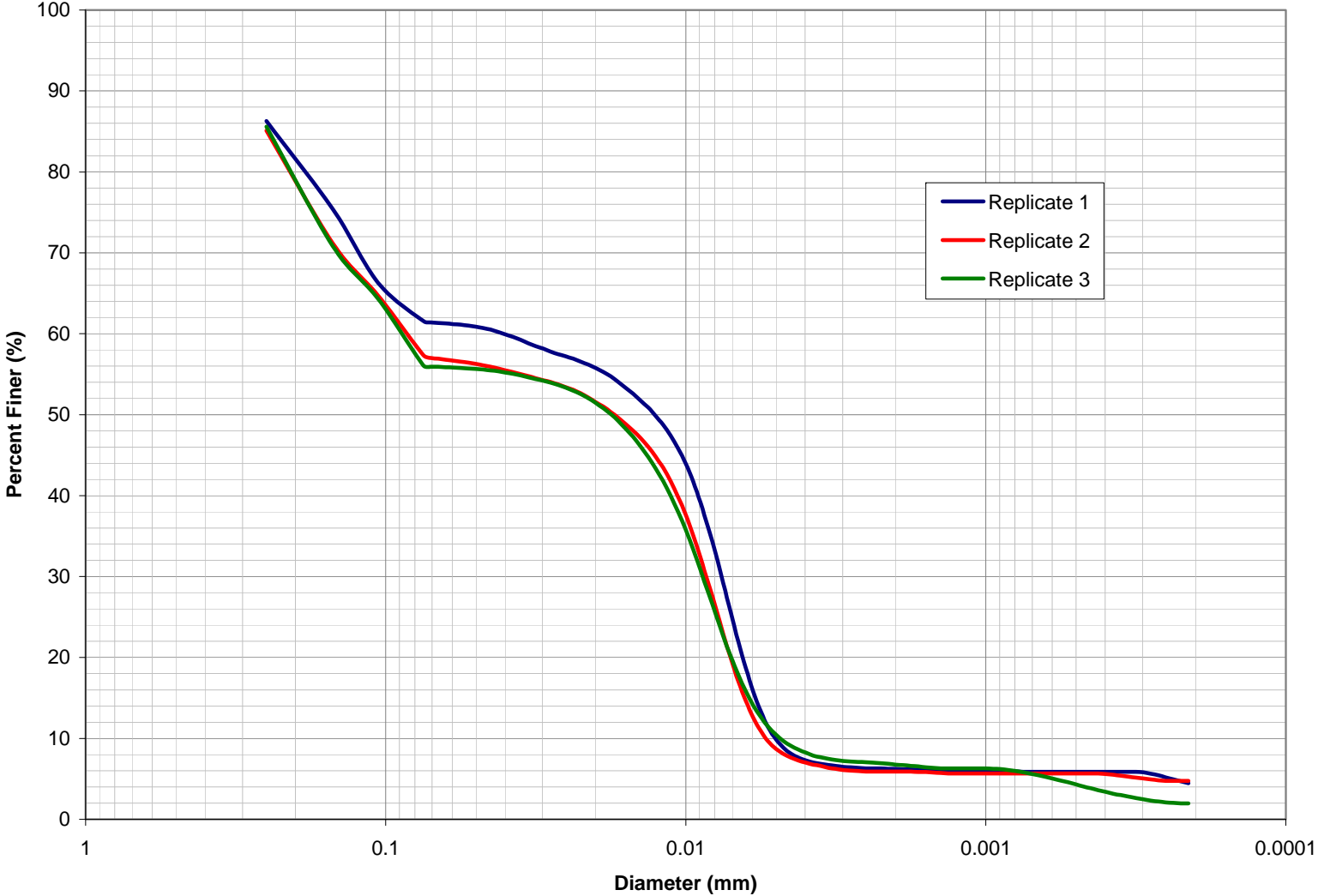


Figure 11: Average Eroded Particle Size Distribution Chart for Sample NMB

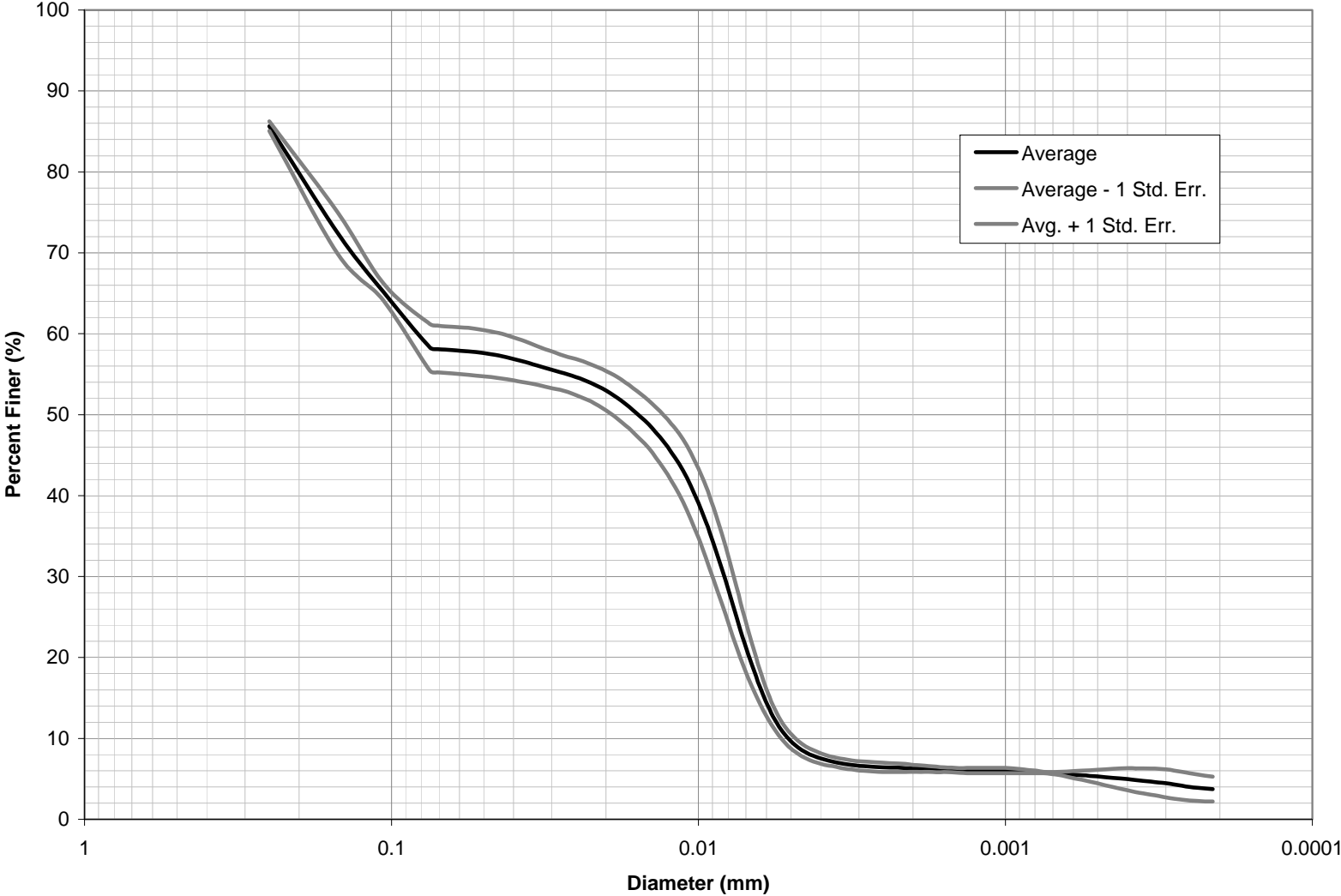
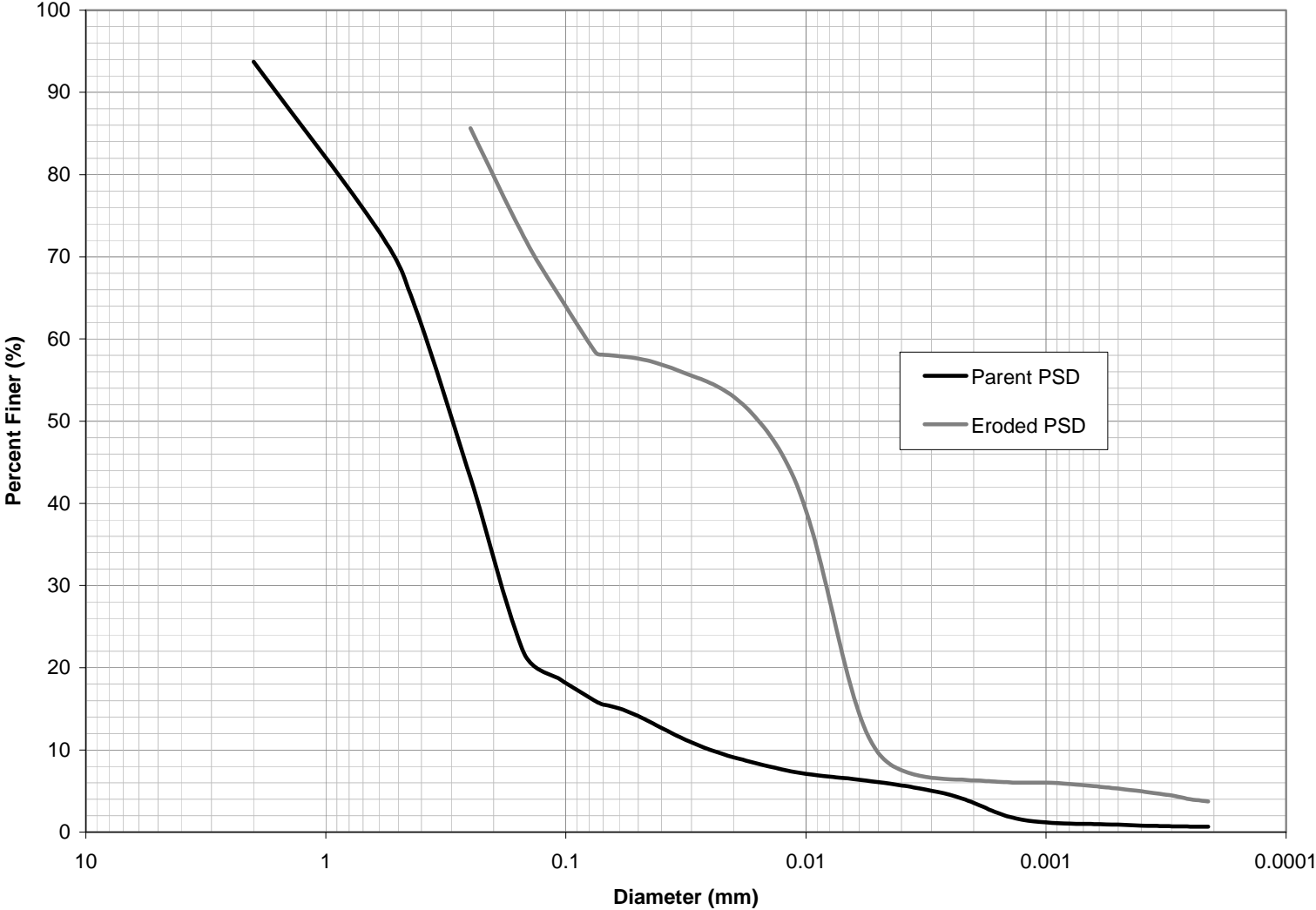




Figure 12: Combined Particle Size Distributions Chart for Sample NMB



### **4.3 Sample NMC: “Fine Loamy”**



Average total sediment mass yielded during rainfall simulator test: 29.547g  
Average mass of EPSD coarser than 0.250 mm: 6.71g

#### **4.3.1 Description**

- a) Texture: fine sand with fine gravels.
- b) Color: light grey.
- c) Fine fraction (< 0.075%): 15.196%
- d) USDA Textural Classification: LOAMY SAND

#### **4.3.2 K – Factor Calculation**

Organic Material: 2.860%  
Percent Silt + Very Fine Sand (0.002 – 0.1 mm): 15.90%  
Percent Sand (0.1 – 2 mm): 74.84%

First Approximation: **K = 0.08**

### 4.3.3 Parent Particle Size Distribution

**Table 5:** Parent Particle Size Distribution for Sample NMC

| Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) |
|---------------|---------------------------|---------------|---------------------------|---------------|---------------------------|
| 2             | 94.392                    | 0.01059       | 5.854                     | 0.001059      | 2.668                     |
| 0.6           | 76.394                    | 0.01          | 5.765                     | 0.001         | 2.594                     |
| 0.425         | 67.811                    | 0.009441      | 5.687                     | 0.000944      | 2.526                     |
| 0.25          | 49.075                    | 0.008913      | 5.609                     | 0.000891      | 2.448                     |
| 0.15          | 25.542                    | 0.008414      | 5.531                     | 0.000841      | 2.380                     |
| 0.106         | 19.553                    | 0.007943      | 5.469                     | 0.000794      | 2.307                     |
| 0.075         | 15.196                    | 0.007499      | 5.401                     | 0.00075       | 2.234                     |
| 0.07079       | 14.591                    | 0.007079      | 5.350                     | 0.000708      | 2.161                     |
| 0.06683       | 14.372                    | 0.006683      | 5.283                     | 0.000668      | 2.083                     |
| 0.0631        | 14.108                    | 0.00631       | 5.221                     | 0.000631      | 2.010                     |
| 0.05957       | 13.801                    | 0.005957      | 5.164                     | 0.000596      | 1.932                     |
| 0.05623       | 13.448                    | 0.005623      | 5.097                     | 0.000562      | 1.854                     |
| 0.05309       | 13.059                    | 0.005309      | 5.030                     | 0.000531      | 1.781                     |
| 0.05012       | 12.628                    | 0.005012      | 4.962                     | 0.000501      | 1.713                     |
| 0.04732       | 12.192                    | 0.004732      | 4.884                     | 0.000473      | 1.645                     |
| 0.04467       | 11.729                    | 0.004467      | 4.795                     | 0.000447      | 1.583                     |
| 0.04217       | 11.277                    | 0.004217      | 4.707                     | 0.000422      | 1.521                     |
| 0.03981       | 10.825                    | 0.003981      | 4.613                     | 0.000398      | 1.470                     |
| 0.03758       | 10.393                    | 0.003758      | 4.514                     | 0.000376      | 1.423                     |
| 0.03548       | 9.976                     | 0.003548      | 4.410                     | 0.000355      | 1.371                     |
| 0.0335        | 9.592                     | 0.00335       | 4.311                     | 0.000335      | 1.330                     |
| 0.03162       | 9.238                     | 0.003162      | 4.212                     | 0.000316      | 1.289                     |
| 0.02985       | 8.910                     | 0.002985      | 4.119                     | 0.000299      | 1.253                     |
| 0.02818       | 8.618                     | 0.002818      | 4.025                     | 0.000282      | 1.232                     |
| 0.02661       | 8.338                     | 0.002661      | 3.947                     | 0.000266      | 1.212                     |
| 0.02512       | 8.094                     | 0.002512      | 3.864                     | 0.000251      | 1.212                     |
| 0.02371       | 7.859                     | 0.002371      | 3.796                     |               |                           |
| 0.02239       | 7.646                     | 0.002239      | 3.722                     |               |                           |
| 0.02113       | 7.443                     | 0.002113      | 3.649                     |               |                           |
| 0.01995       | 7.257                     | 0.001995      | 3.571                     |               |                           |
| 0.01884       | 7.086                     | 0.001884      | 3.487                     |               |                           |
| 0.01778       | 6.915                     | 0.001778      | 3.404                     |               |                           |
| 0.01679       | 6.765                     | 0.001679      | 3.320                     |               |                           |
| 0.01585       | 6.619                     | 0.001585      | 3.232                     |               |                           |
| 0.01496       | 6.485                     | 0.001496      | 3.143                     |               |                           |
| 0.01413       | 6.361                     | 0.001413      | 3.060                     |               |                           |
| 0.01334       | 6.253                     | 0.001334      | 2.976                     |               |                           |
| 0.01259       | 6.144                     | 0.001259      | 2.893                     |               |                           |
| 0.01189       | 6.040                     | 0.001189      | 2.814                     |               |                           |
| 0.01122       | 5.942                     | 0.001122      | 2.741                     |               |                           |



Figure 13: Parent Particle Size Distributions Chart for Sample NMC

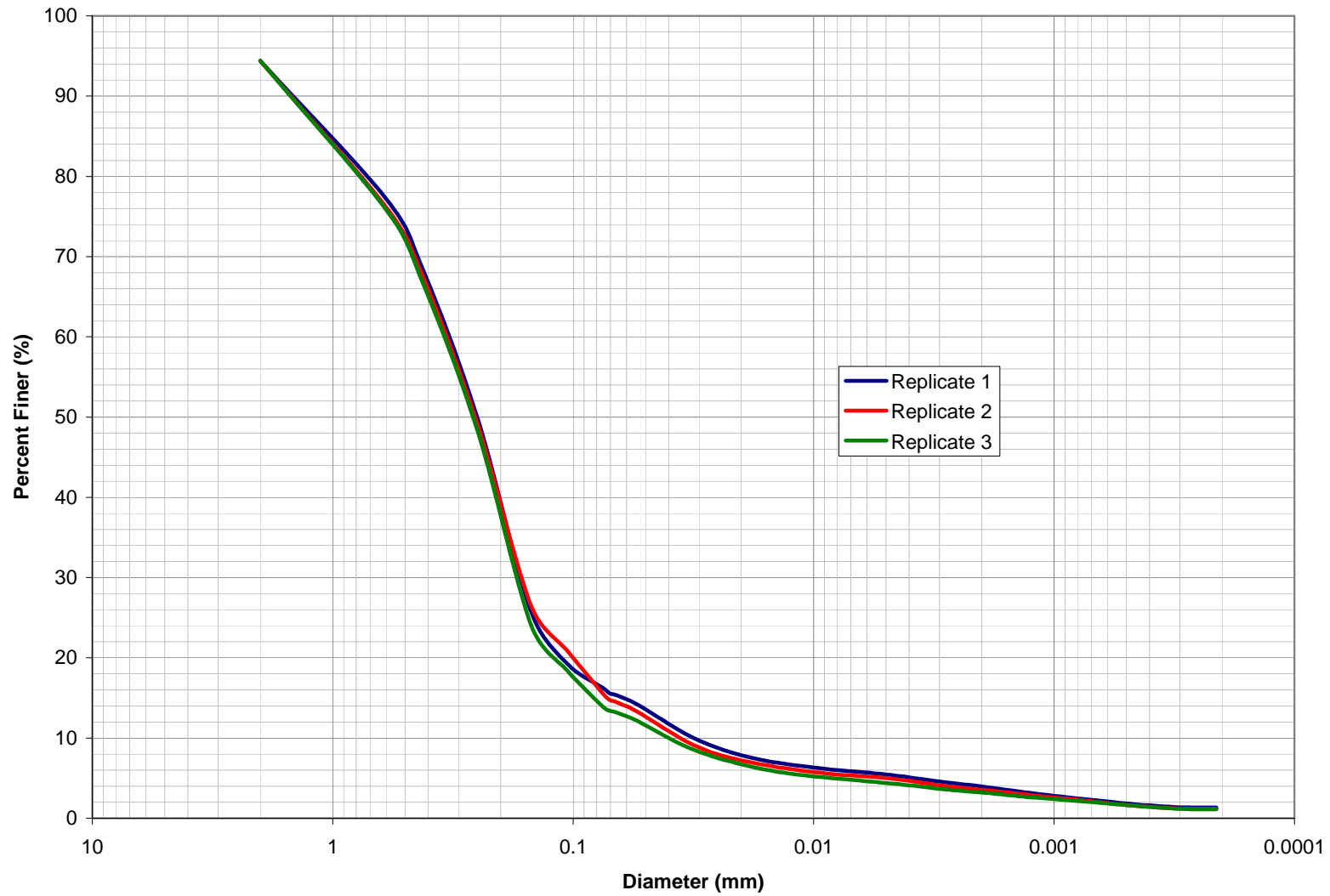
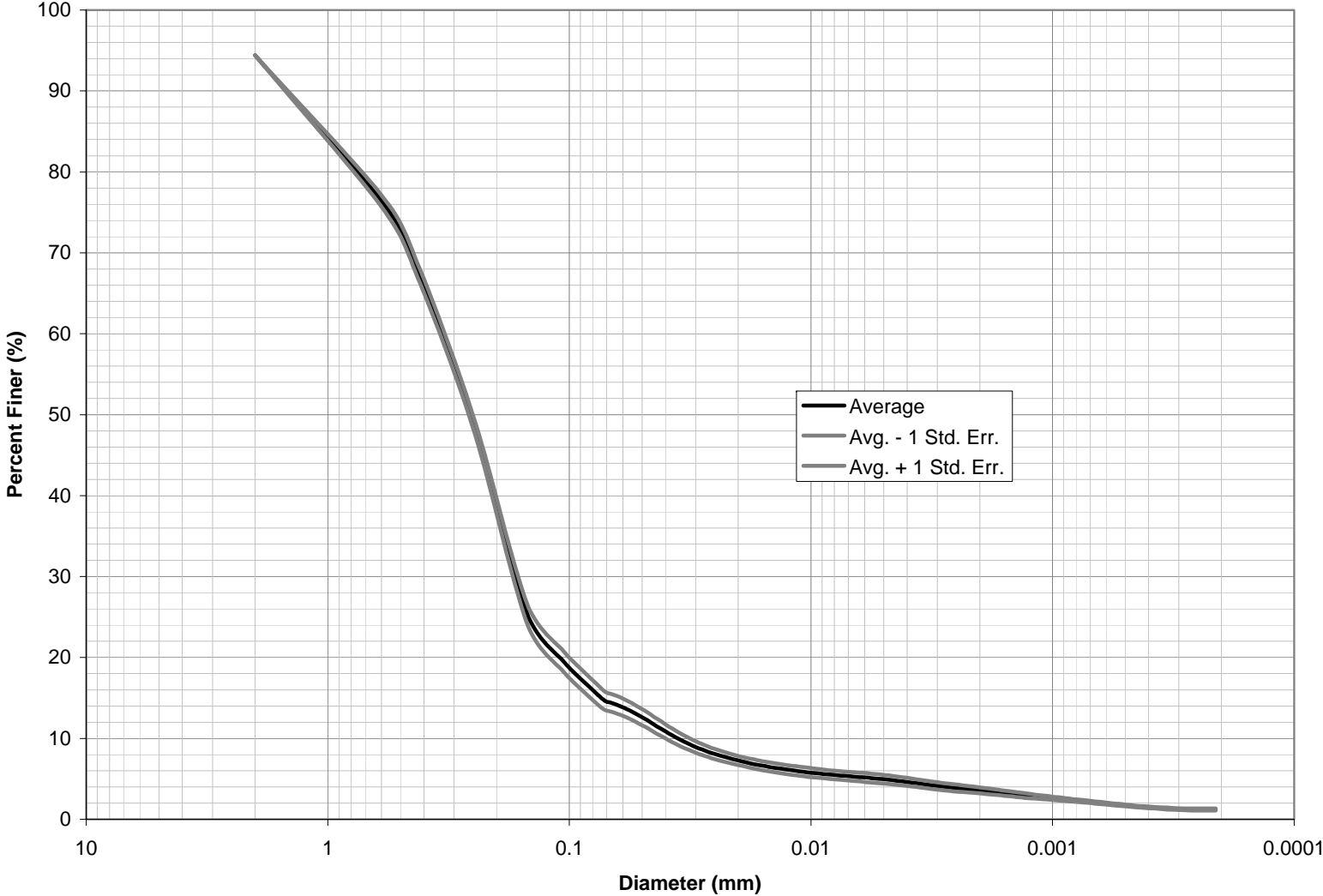


Figure 14: Average Parent Particle Size Distribution Chart for Sample NMC



### 4.3.4 Eroded Particle Size Distribution

**Table 6:** Eroded Particle Size Distribution for Sample NMC

| Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) |
|---------------|---------------------------|---------------|---------------------------|---------------|---------------------------|
| 0.25          | 77.102                    | 0.008913      | 14.836                    | 0.000891      | 3.480                     |
| 0.15          | 57.325                    | 0.008414      | 12.958                    | 0.000841      | 3.480                     |
| 0.106         | 46.724                    | 0.007943      | 11.237                    | 0.000794      | 3.480                     |
| 0.075         | 38.620                    | 0.007499      | 9.749                     | 0.00075       | 3.480                     |
| 0.07079       | 38.515                    | 0.007079      | 8.498                     | 0.000708      | 3.480                     |
| 0.06683       | 38.450                    | 0.006683      | 7.520                     | 0.000668      | 3.480                     |
| 0.0631        | 38.384                    | 0.00631       | 6.737                     | 0.000631      | 3.480                     |
| 0.05957       | 38.306                    | 0.005957      | 6.151                     | 0.000596      | 3.480                     |
| 0.05623       | 38.175                    | 0.005623      | 5.708                     | 0.000562      | 3.480                     |
| 0.05309       | 38.031                    | 0.005309      | 5.382                     | 0.000531      | 3.480                     |
| 0.05012       | 37.887                    | 0.005012      | 5.122                     | 0.000501      | 3.480                     |
| 0.04732       | 37.704                    | 0.004732      | 4.926                     | 0.000473      | 3.480                     |
| 0.04467       | 37.495                    | 0.004467      | 4.744                     | 0.000447      | 3.467                     |
| 0.04217       | 37.313                    | 0.004217      | 4.601                     | 0.000422      | 3.454                     |
| 0.03981       | 37.104                    | 0.003981      | 4.484                     | 0.000398      | 3.401                     |
| 0.03758       | 36.870                    | 0.003758      | 4.380                     | 0.000376      | 3.336                     |
| 0.03548       | 36.675                    | 0.003548      | 4.275                     | 0.000355      | 3.245                     |
| 0.0335        | 36.429                    | 0.00335       | 4.210                     | 0.000335      | 3.166                     |
| 0.03162       | 36.181                    | 0.003162      | 4.158                     | 0.000316      | 3.089                     |
| 0.02985       | 35.922                    | 0.002985      | 4.119                     | 0.000299      | 3.011                     |
| 0.02818       | 35.662                    | 0.002818      | 4.119                     | 0.000282      | 2.908                     |
| 0.02661       | 35.376                    | 0.002661      | 4.106                     | 0.000266      | 2.793                     |
| 0.02512       | 35.051                    | 0.002512      | 4.106                     | 0.000251      | 2.666                     |
| 0.02371       | 34.700                    | 0.002371      | 4.106                     | 0.000237      | 2.527                     |
| 0.02239       | 34.322                    | 0.002239      | 4.093                     | 0.000224      | 2.350                     |
| 0.02113       | 33.905                    | 0.002113      | 4.093                     | 0.000211      | 2.148                     |
| 0.01995       | 33.437                    | 0.001995      | 4.067                     |               |                           |
| 0.01884       | 32.916                    | 0.001884      | 4.028                     |               |                           |
| 0.01778       | 32.332                    | 0.001778      | 3.963                     |               |                           |
| 0.01679       | 31.642                    | 0.001679      | 3.885                     |               |                           |
| 0.01585       | 30.862                    | 0.001585      | 3.807                     |               |                           |
| 0.01496       | 29.965                    | 0.001496      | 3.716                     |               |                           |
| 0.01413       | 28.911                    | 0.001413      | 3.638                     |               |                           |
| 0.01334       | 27.701                    | 0.001334      | 3.559                     |               |                           |
| 0.01259       | 26.281                    | 0.001259      | 3.507                     |               |                           |
| 0.01189       | 24.679                    | 0.001189      | 3.493                     |               |                           |
| 0.01122       | 22.907                    | 0.001122      | 3.480                     |               |                           |
| 0.01059       | 20.965                    | 0.001059      | 3.480                     |               |                           |
| 0.01          | 18.931                    | 0.001         | 3.480                     |               |                           |
| 0.009441      | 16.871                    | 0.000944      | 3.480                     |               |                           |



Figure 15: Eroded Particle Size Distributions Chart for Sample NMC

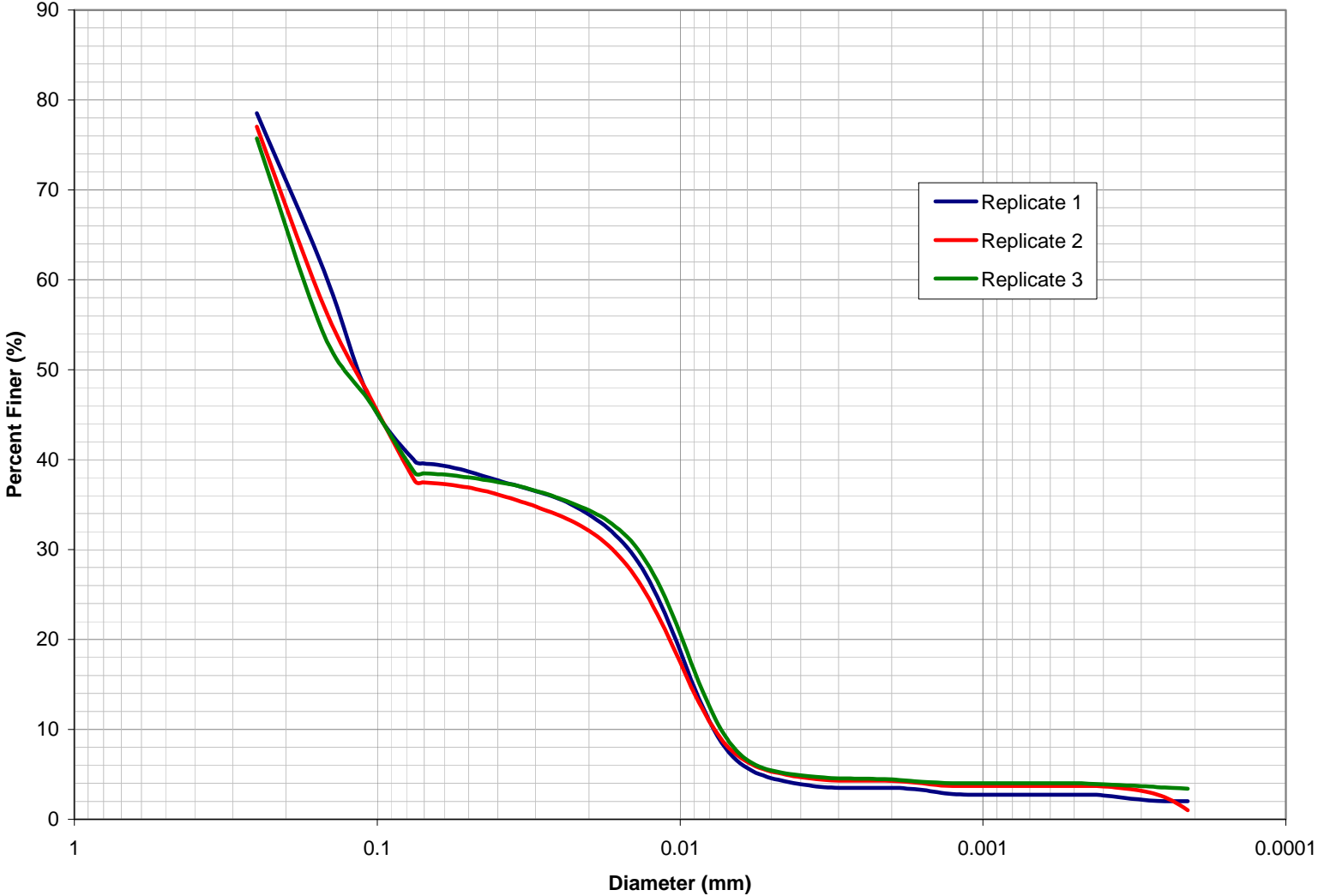


Figure 16: Average Eroded Particle Size Distribution Chart for Sample NMC

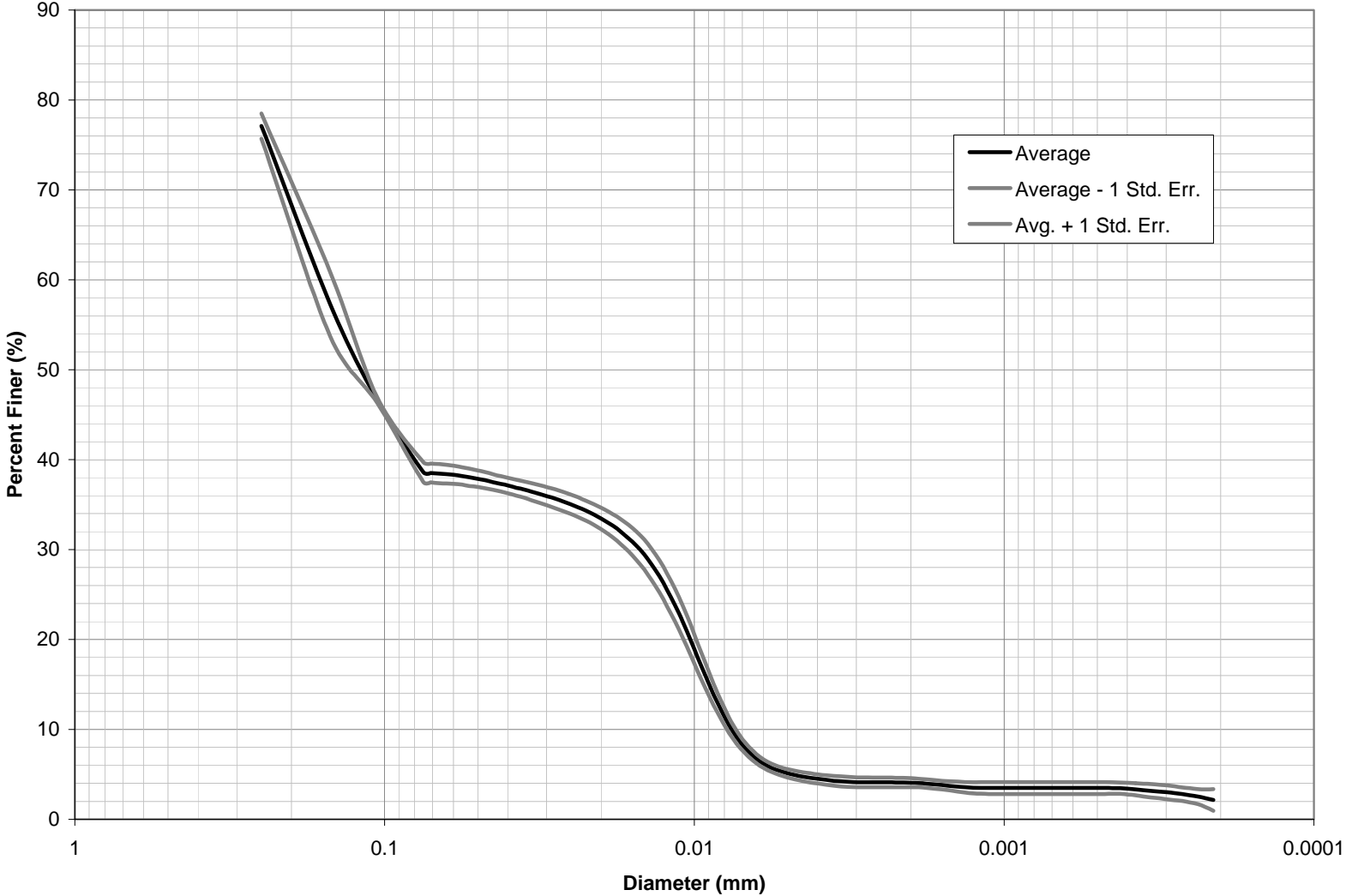
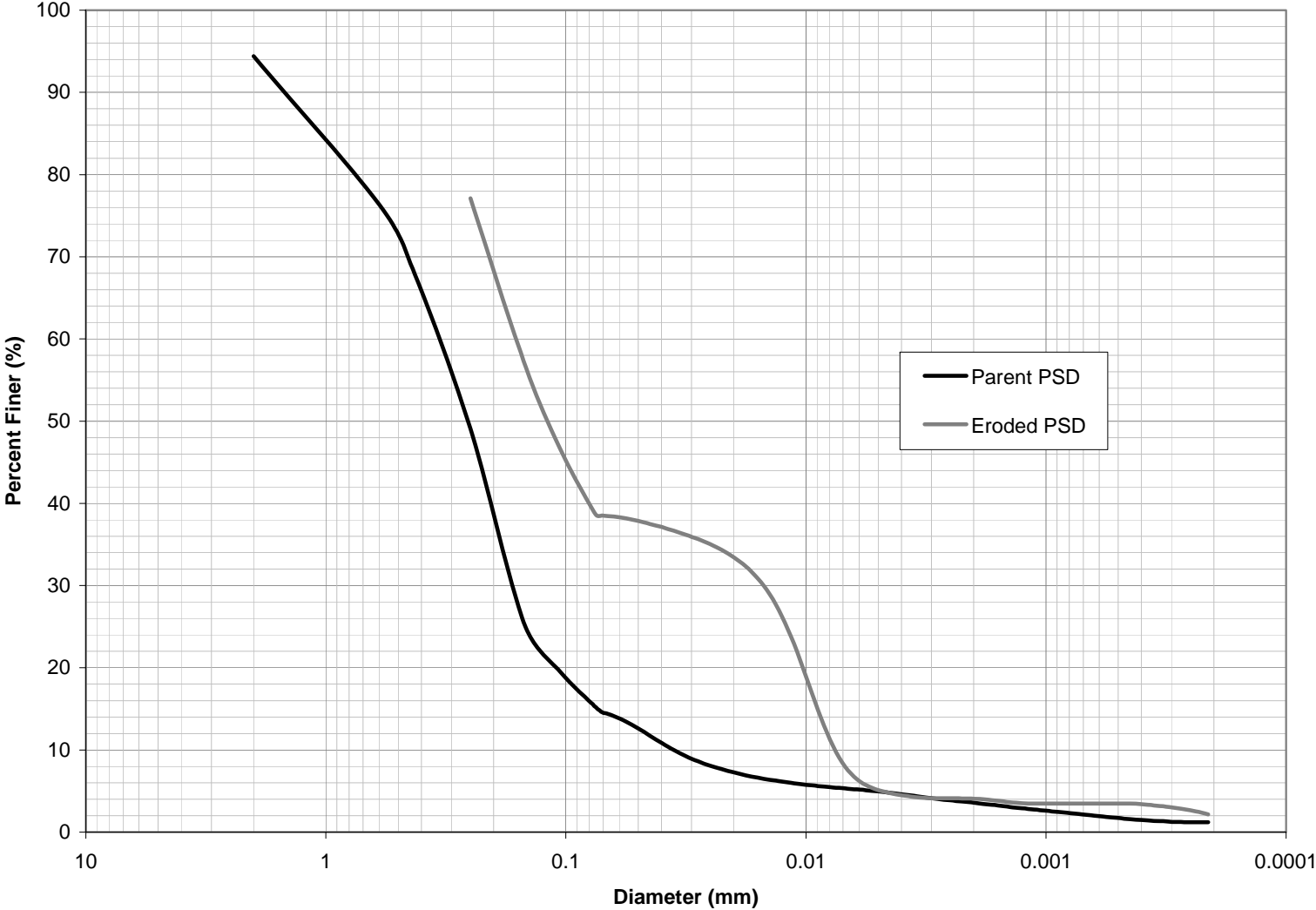


Figure 17: Combined Particle Size Distributions Chart for Sample NMC





#### **4.4 Sample NMD: “Coarse Loamy”**



Average total sediment mass yielded during rainfall simulator test: 54.46g

Average mass of EPSD coarser than 0.250 mm: 14.38g

##### **4.4.1 Description**

- a) Texture: fine sand with silts and fine gravels.
- b) Color: light brown.
- c) Fine fraction (< 0.075%): 12.687%
- d) USDA Textural Classification: SAND

##### **4.4.2 K – Factor Calculation**

Organic Material: 1.812%

Percent Silt + Very Fine Sand (0.002 – 0.1 mm): 15.0%

Percent Sand (0.1 – 2 mm): 79.86%

First Approximation: **K = 0.07**

### 4.4.3 Parent Particle Size Distribution

**Table 7:** Parent Particle Size Distribution for Sample NMD

| Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) |
|---------------|---------------------------|---------------|---------------------------|---------------|---------------------------|
| 2             | 97.568                    | 0.01059       | 4.091                     | 0.001059      | 1.999                     |
| 0.6           | 89.006                    | 0.01          | 4.043                     | 0.001         | 1.947                     |
| 0.425         | 82.521                    | 0.009441      | 3.991                     | 0.000944      | 1.886                     |
| 0.25          | 57.564                    | 0.008913      | 3.948                     | 0.000891      | 1.838                     |
| 0.15          | 23.865                    | 0.008414      | 3.913                     | 0.000841      | 1.781                     |
| 0.106         | 17.704                    | 0.007943      | 3.878                     | 0.000794      | 1.720                     |
| 0.075         | 12.687                    | 0.007499      | 3.847                     | 0.00075       | 1.668                     |
| 0.07079       | 11.997                    | 0.007079      | 3.816                     | 0.000708      | 1.607                     |
| 0.06683       | 11.753                    | 0.006683      | 3.790                     | 0.000668      | 1.546                     |
| 0.0631        | 11.456                    | 0.00631       | 3.759                     | 0.000631      | 1.481                     |
| 0.05957       | 11.120                    | 0.005957      | 3.729                     | 0.000596      | 1.416                     |
| 0.05623       | 10.727                    | 0.005623      | 3.690                     | 0.000562      | 1.355                     |
| 0.05309       | 10.308                    | 0.005309      | 3.646                     | 0.000531      | 1.290                     |
| 0.05012       | 9.863                     | 0.005012      | 3.598                     | 0.000501      | 1.225                     |
| 0.04732       | 9.401                     | 0.004732      | 3.546                     | 0.000473      | 1.169                     |
| 0.04467       | 8.935                     | 0.004467      | 3.481                     | 0.000447      | 1.121                     |
| 0.04217       | 8.469                     | 0.004217      | 3.411                     | 0.000422      | 1.074                     |
| 0.03981       | 8.033                     | 0.003981      | 3.342                     | 0.000398      | 1.035                     |
| 0.03758       | 7.620                     | 0.003758      | 3.263                     | 0.000376      | 0.996                     |
| 0.03548       | 7.237                     | 0.003548      | 3.190                     | 0.000355      | 0.970                     |
| 0.0335        | 6.889                     | 0.00335       | 3.107                     | 0.000335      | 0.943                     |
| 0.03162       | 6.580                     | 0.003162      | 3.037                     | 0.000316      | 0.912                     |
| 0.02985       | 6.306                     | 0.002985      | 2.967                     | 0.000299      | 0.881                     |
| 0.02818       | 6.067                     | 0.002818      | 2.906                     | 0.000282      | 0.837                     |
| 0.02661       | 5.854                     | 0.002661      | 2.854                     | 0.000266      | 0.788                     |
| 0.02512       | 5.667                     | 0.002512      | 2.810                     | 0.000251      | 0.730                     |
| 0.02371       | 5.493                     | 0.002371      | 2.771                     |               |                           |
| 0.02239       | 5.336                     | 0.002239      | 2.731                     |               |                           |
| 0.02113       | 5.192                     | 0.002113      | 2.697                     |               |                           |
| 0.01995       | 5.062                     | 0.001995      | 2.662                     |               |                           |
| 0.01884       | 4.944                     | 0.001884      | 2.622                     |               |                           |
| 0.01778       | 4.826                     | 0.001778      | 2.570                     |               |                           |
| 0.01679       | 4.726                     | 0.001679      | 2.518                     |               |                           |
| 0.01585       | 4.626                     | 0.001585      | 2.452                     |               |                           |
| 0.01496       | 4.534                     | 0.001496      | 2.391                     |               |                           |
| 0.01413       | 4.447                     | 0.001413      | 2.322                     |               |                           |
| 0.01334       | 4.369                     | 0.001334      | 2.248                     |               |                           |
| 0.01259       | 4.295                     | 0.001259      | 2.183                     |               |                           |
| 0.01189       | 4.221                     | 0.001189      | 2.122                     |               |                           |
| 0.01122       | 4.156                     | 0.001122      | 2.061                     |               |                           |

Figure 18: Parent Particle Size Distributions Chart for Sample NMD

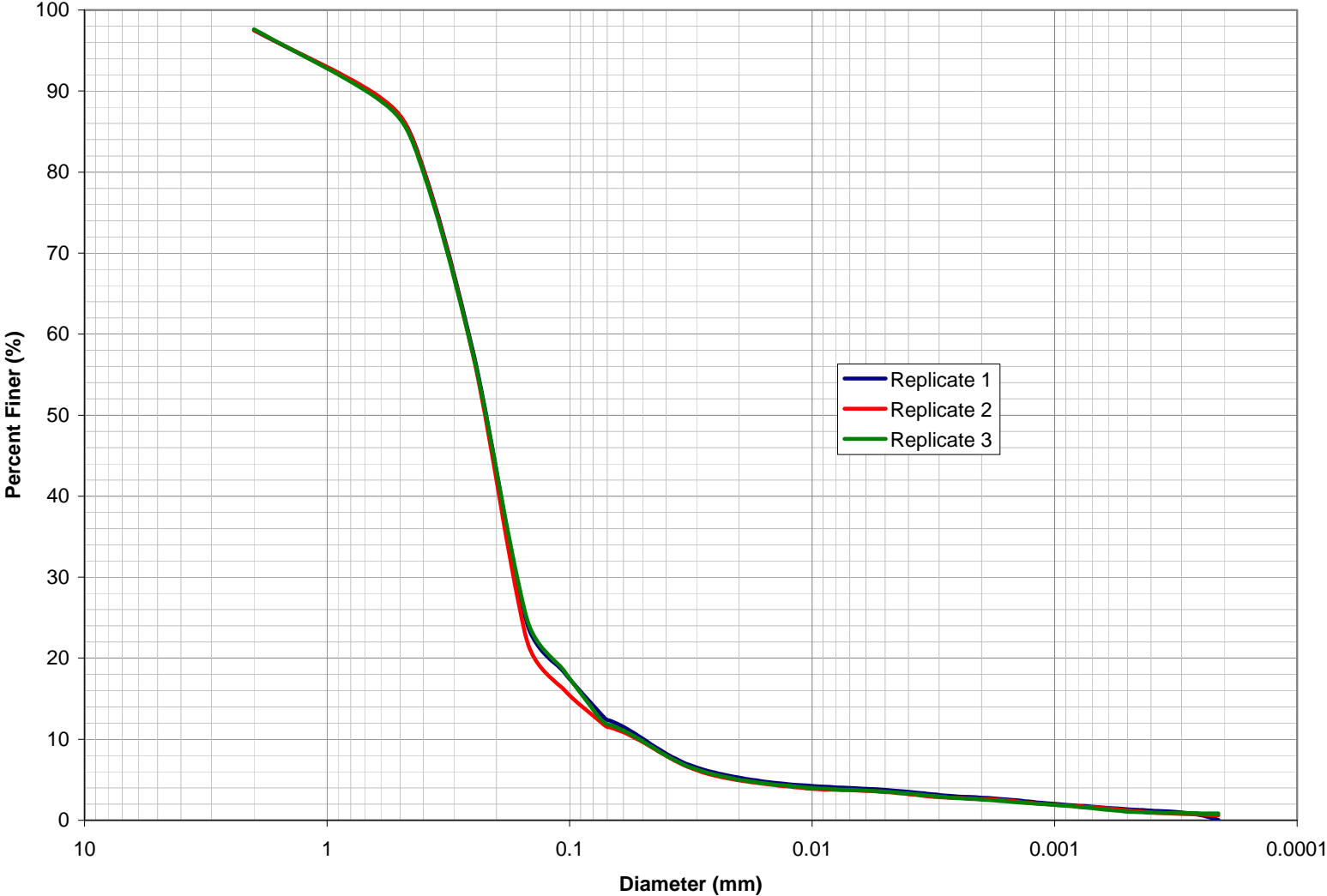
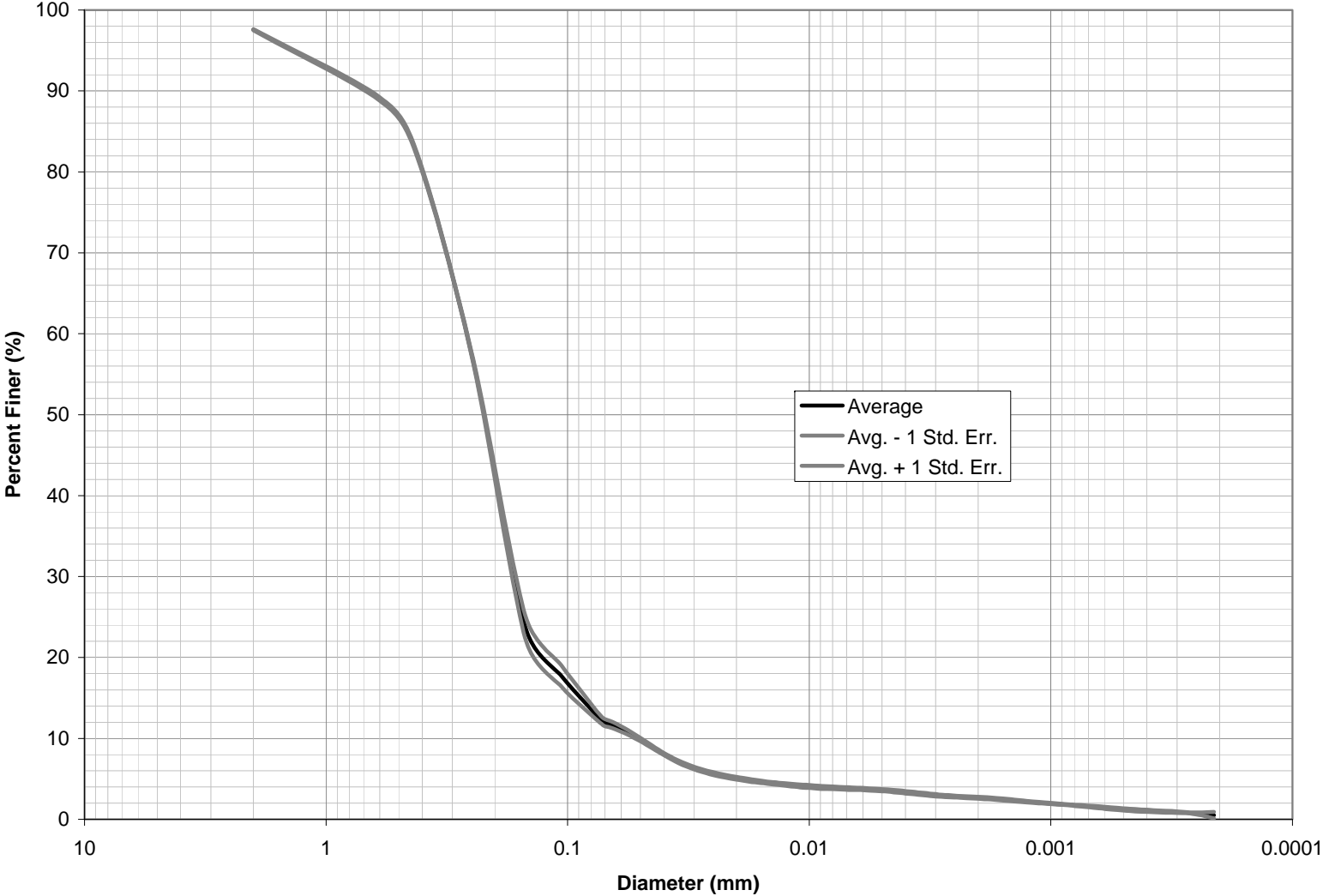


Figure 19: Average Parent Particle Size Distribution Chart for Sample NMD





#### 4.4.4 Eroded Particle Size Distribution

**Table 8:** Eroded Particle Size Distribution for Sample NMD

| Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) | Diameter (mm) | Average Percent Finer (%) |
|---------------|---------------------------|---------------|---------------------------|---------------|---------------------------|
| 0.25          | 70.762                    | 0.008913      | 24.412                    | 0.000891      | 2.690                     |
| 0.15          | 45.246                    | 0.008414      | 23.111                    | 0.000841      | 2.690                     |
| 0.106         | 37.534                    | 0.007943      | 21.599                    | 0.000794      | 2.690                     |
| 0.075         | 32.679                    | 0.007499      | 19.885                    | 0.00075       | 2.690                     |
| 0.07079       | 32.669                    | 0.007079      | 17.989                    | 0.000708      | 2.690                     |
| 0.06683       | 32.659                    | 0.006683      | 15.969                    | 0.000668      | 2.690                     |
| 0.0631        | 32.640                    | 0.00631       | 13.910                    | 0.000631      | 2.690                     |
| 0.05957       | 32.621                    | 0.005957      | 11.902                    | 0.000596      | 2.690                     |
| 0.05623       | 32.582                    | 0.005623      | 10.027                    | 0.000562      | 2.690                     |
| 0.05309       | 32.534                    | 0.005309      | 8.362                     | 0.000531      | 2.690                     |
| 0.05012       | 32.467                    | 0.005012      | 6.956                     | 0.000501      | 2.690                     |
| 0.04732       | 32.390                    | 0.004732      | 5.810                     | 0.000473      | 2.690                     |
| 0.04467       | 32.289                    | 0.004467      | 4.963                     | 0.000447      | 2.690                     |
| 0.04217       | 32.166                    | 0.004217      | 4.323                     | 0.000422      | 2.690                     |
| 0.03981       | 32.052                    | 0.003981      | 3.907                     | 0.000398      | 2.690                     |
| 0.03758       | 31.928                    | 0.003758      | 3.631                     | 0.000376      | 2.681                     |
| 0.03548       | 31.818                    | 0.003548      | 3.453                     | 0.000355      | 2.662                     |
| 0.0335        | 31.694                    | 0.00335       | 3.345                     | 0.000335      | 2.643                     |
| 0.03162       | 31.608                    | 0.003162      | 3.288                     | 0.000316      | 2.624                     |
| 0.02985       | 31.508                    | 0.002985      | 3.246                     | 0.000299      | 2.562                     |
| 0.02818       | 31.421                    | 0.002818      | 3.212                     | 0.000282      | 2.477                     |
| 0.02661       | 31.325                    | 0.002661      | 3.203                     | 0.000266      | 2.392                     |
| 0.02512       | 31.215                    | 0.002512      | 3.193                     | 0.000251      | 2.283                     |
| 0.02371       | 31.100                    | 0.002371      | 3.183                     | 0.000237      | 2.169                     |
| 0.02239       | 30.980                    | 0.002239      | 3.174                     | 0.000224      | 2.042                     |
| 0.02113       | 30.837                    | 0.002113      | 3.164                     | 0.000211      | 1.928                     |
| 0.01995       | 30.684                    | 0.001995      | 3.145                     |               |                           |
| 0.01884       | 30.532                    | 0.001884      | 3.126                     |               |                           |
| 0.01778       | 30.365                    | 0.001778      | 3.097                     |               |                           |
| 0.01679       | 30.165                    | 0.001679      | 3.058                     |               |                           |
| 0.01585       | 29.955                    | 0.001585      | 3.020                     |               |                           |
| 0.01496       | 29.727                    | 0.001496      | 2.963                     |               |                           |
| 0.01413       | 29.455                    | 0.001413      | 2.897                     |               |                           |
| 0.01334       | 29.141                    | 0.001334      | 2.831                     |               |                           |
| 0.01259       | 28.765                    | 0.001259      | 2.775                     |               |                           |
| 0.01189       | 28.318                    | 0.001189      | 2.728                     |               |                           |
| 0.01122       | 27.808                    | 0.001122      | 2.704                     |               |                           |
| 0.01059       | 27.171                    | 0.001059      | 2.690                     |               |                           |
| 0.01          | 26.409                    | 0.001         | 2.690                     |               |                           |
| 0.009441      | 25.501                    | 0.000944      | 2.690                     |               |                           |

Figure 20: Eroded Particle Size Distributions Chart for Sample NMD

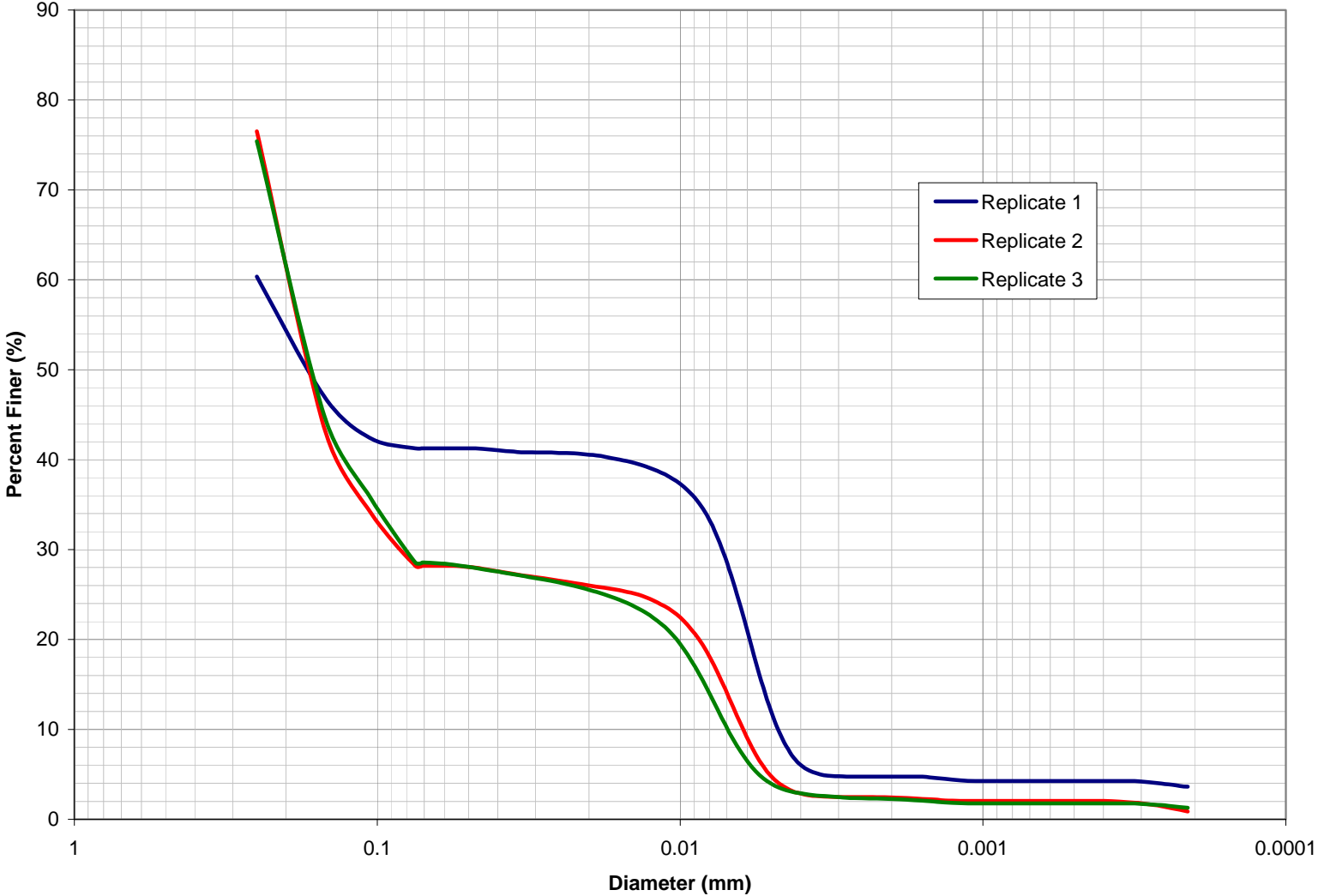


Figure 21: Average Eroded Particle Size Distribution Chart for Sample NMD

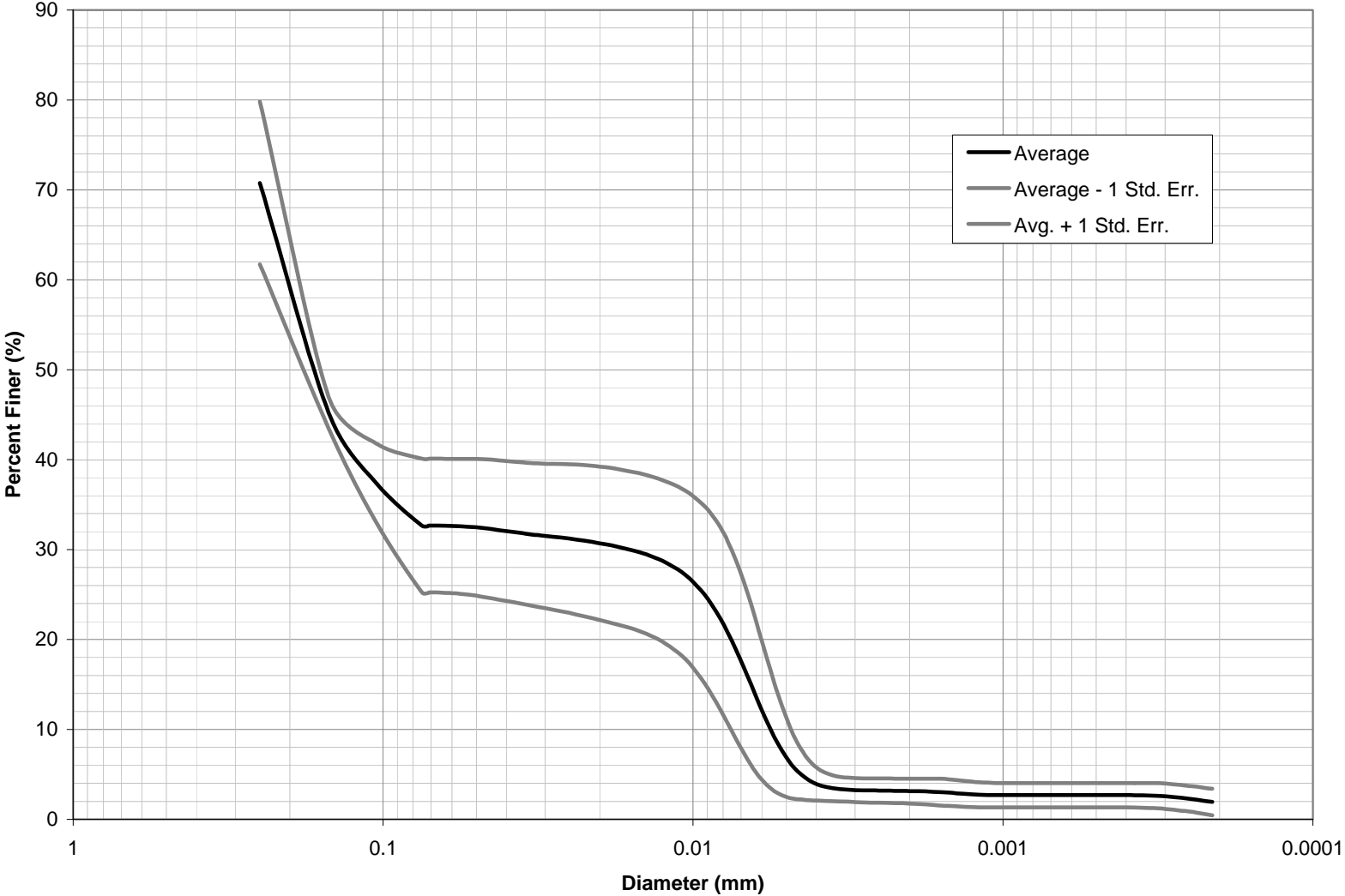
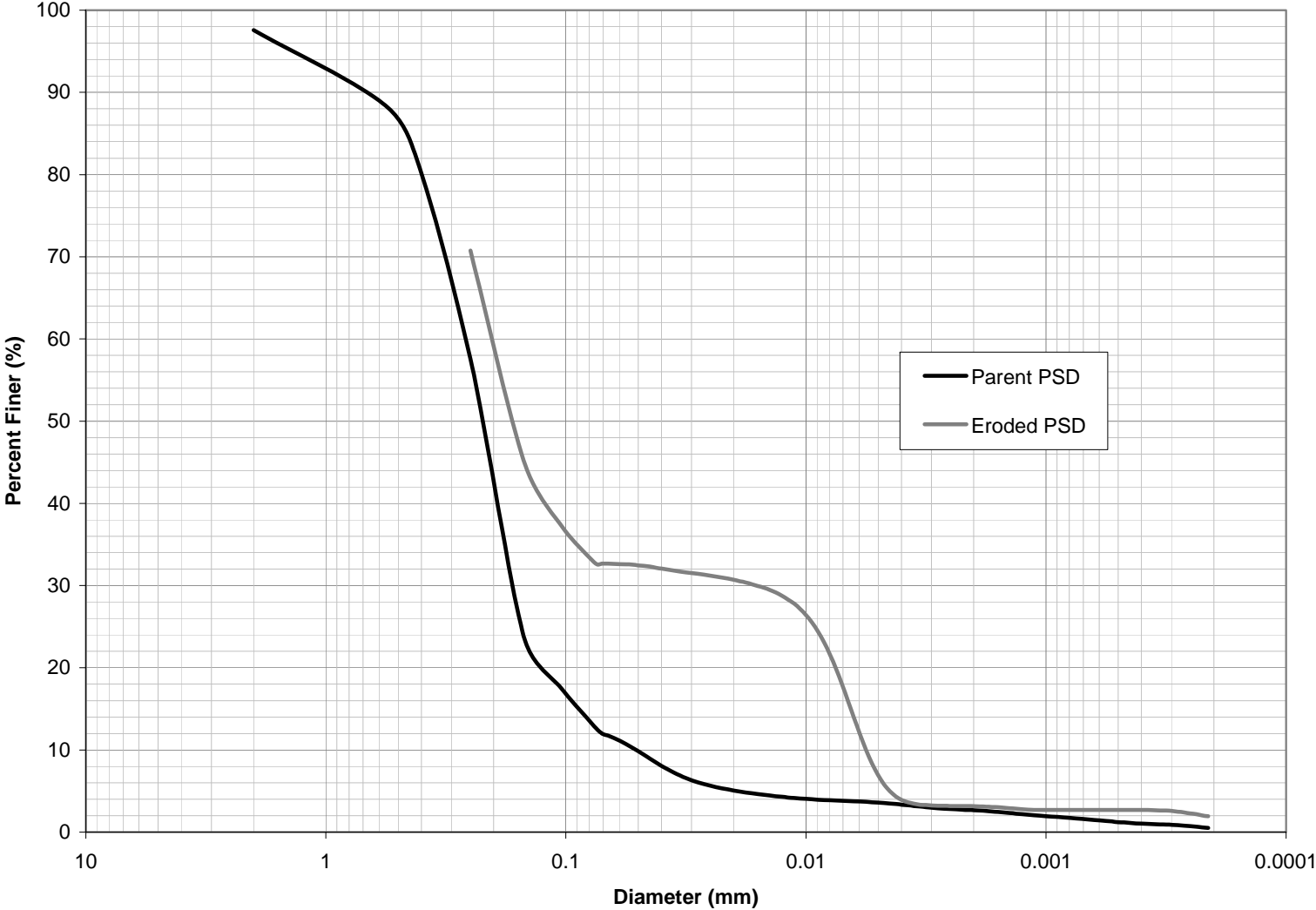


Figure 22: Combined Particle Size Distributions Chart for Sample NMD





## **5. REFERENCES**

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3. Renard, K.G., Foster, G.R., Weesies, G.A., McCool, D.K., and D.C. Yoder, coordinators. 1996. USDA-ARS. Agriculture Handbook No. 703: Predicting soil erosion by water - a guide to conservation planning with the revised universal soil loss equation (RUSLE). Soil and Water Conservation Society office, Ankeny, IA.
4. USDA National Soil Erosion Research Laboratory. 1995. USDA - Water Erosion Prediction Project (WEPP) User Summary. NSERL Report N0.11, July 1995.

## **APPENDIX A: PHOTOS TAKEN DURING EPSD TESTING**

Figure 23: Rainfall Simulator – General View



Figure 24: Rainfall Simulator – Soil Samples



Figure 25: Rainfall Simulator – Soil Samples (details)





Figure 26: Wet Sieve Test



Figure 27: Dry Sieve Test



## **Attachment 18.B-7**

Baseline K-factor Laboratory Determination January 2008



**Soil Analysis Report**  
**BHP Billiton**  
300 W Arrington, Suite 200  
Farmington, NM 87401

Project ID: NMEP Erodibility  
Date Received: 1/10/2008

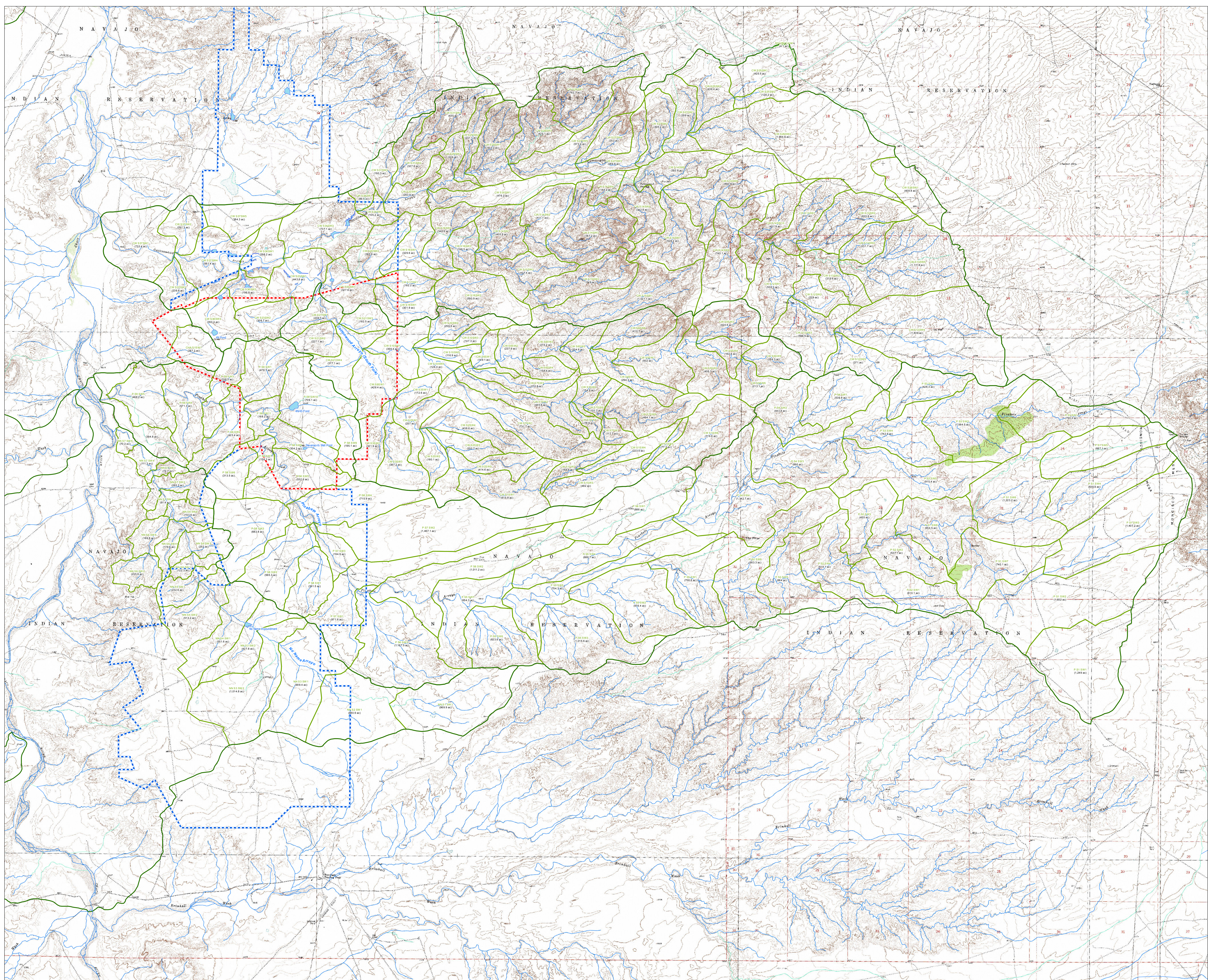
Report ID: S0801141001  
Date Reported: 1/30/2008  
Work Order: S0801141

| Lab ID       | Sample ID    | Organic | Sand | Silt | Clay | Very | Texture         | K-factor               | Structure | Permeability | M      | Description                 |
|--------------|--------------|---------|------|------|------|------|-----------------|------------------------|-----------|--------------|--------|-----------------------------|
|              |              | Matter  |      |      |      | Fine |                 | (t.ac.h/100acft.tf.in) |           |              |        |                             |
|              |              | %       | %    | %    | %    | %    |                 |                        | s         | p            |        |                             |
| S0801141-001 | Fine         | 4.7     | 39.0 | 31.0 | 30.0 | 9.3  | Clay Loam       | 0.19                   | 3         | 4            | 2821.0 | OM - Walkley/Black          |
| S0801141-002 | Fine Loamy   | 1.1     | 53.0 | 26.0 | 21.0 | 12.6 | Sandy Clay Loam | 0.27                   | 3         | 4            | 3049.4 | OM - Walkley/Black          |
| S0801141-003 | Sandy        | 0.1     | 85.0 | 7.0  | 8.0  | 8.1  | Loamy Sand      | 0.10                   | 3         | 2            | 1389.2 | OM - Walkley/Black          |
| S0801141-004 | Coarse Loamy | 0.5     | 70.0 | 16.0 | 14.0 | 15.5 | Sandy Loam      | 0.21                   | 3         | 2            | 2709.0 | OM - Walkley/Black          |
| S0801141-001 | Fine         | 4.5     | 39.0 | 31.0 | 30.0 | 9.3  | Clay Loam       | 0.19                   | 3         | 4            | 2821.0 | OM - Walkley/Black w/o coal |
| S0801141-002 | Fine Loamy   | 1.0     | 53.0 | 26.0 | 21.0 | 12.6 | Sandy Clay Loam | 0.27                   | 3         | 4            | 3049.4 | OM - Walkley/Black          |
| S0801141-003 | Sandy        | 0.1     | 85.0 | 7.0  | 8.0  | 8.1  | Loamy Sand      | 0.10                   | 3         | 2            | 1389.2 | OM - Walkley/Black          |
| S0801141-004 | Coarse Loamy | 0.5     | 70.0 | 16.0 | 14.0 | 15.5 | Sandy Loam      | 0.21                   | 3         | 2            | 2709.0 | OM - Walkley/Black          |
| S0801141-001 | Fine         | 4.7     | 39.0 | 31.0 | 30.0 | 9.3  | Clay Loam       | 0.19                   | 3         | 4            | 2821.0 | OM - LOI                    |
| S0801141-002 | Fine Loamy   | 1.8     | 53.0 | 26.0 | 21.0 | 12.6 | Sandy Clay Loam | 0.26                   | 3         | 4            | 3049.4 | OM - LOI                    |
| S0801141-003 | Sandy        | 0.6     | 85.0 | 7.0  | 8.0  | 8.1  | Loamy Sand      | 0.10                   | 3         | 2            | 1389.2 | OM - LOI                    |
| S0801141-004 | Coarse Loamy | 1.2     | 70.0 | 16.0 | 14.0 | 15.5 | Sandy Loam      | 0.19                   | 3         | 2            | 2709.0 | OM - LOI                    |
| S0801141-001 | Fine         | 3.4     | 39.0 | 31.0 | 30.0 | 9.3  | Clay Loam       | 0.21                   | 3         | 4            | 2821.0 | OM - LOI w/o coal           |
| S0801141-002 | Fine Loamy   | 1.6     | 53.0 | 26.0 | 21.0 | 12.6 | Sandy Clay Loam | 0.26                   | 3         | 4            | 3049.4 | OM - LOI                    |
| S0801141-003 | Sandy        | 0.5     | 85.0 | 7.0  | 8.0  | 8.1  | Loamy Sand      | 0.10                   | 3         | 2            | 1389.2 | OM - LOI                    |
| S0801141-004 | Coarse Loamy | 0.9     | 70.0 | 16.0 | 14.0 | 15.5 | Sandy Loam      | 0.20                   | 3         | 2            | 2709.0 | OM - LOI                    |

These Results apply only to the samples tested.

Reviewed by: \_\_\_\_\_  
Chris Johnston, Soil Scientist



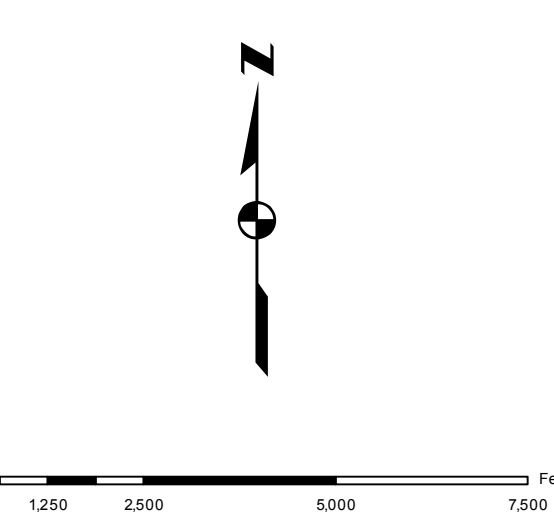


**Legend**

- SEDCAD Subwatersheds
- Watershed Boundaries
- Ponds
- Artificial Canal/Ditch
- Natural Stream
- SMCRA Permit Boundary
- BNCC Lease and ROWs
- BNCC Resource Areas

**Data Sources:**  
National Hydrography Dataset

Coordinate System:  
NAD 1983 State Plane New Mexico West FIPS 5003  
Projection: Transverse Mercator  
Datum: North American 1983  
Units: Feet US



|      |        |     |                               |      |
|------|--------|-----|-------------------------------|------|
| 12-A | 3/2/14 | MPO | Prepared for Submittal to OSM | OKA  |
| Rev  | Date   | By  | Description                   | Appr |

Exhibit 18-B-1

**bhpbilliton**  
resourcing the future

**BHP NAVAJO COAL COMPANY**  
Pinabete Permit Area  
SEDCAD Subwatersheds

|                  |               |                    |
|------------------|---------------|--------------------|
| PREPARED BY: MD  | DRAWN BY: MPO | PAPER SIZE: ARCH E |
| APPROVED BY: OKA | DATE: 3/2/12  |                    |



## **Appendix 18.C**

Laboratory Reports for Pesticide and PCB Analyses of Pond Waters

Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: BHP  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
04/22/08 14:33

**Mid Penabete  
T800496-02 (Water)**

| Analyte | Result | Reporting Limit | Units | Dilution | Batch | Prepared | Analyzed | Method | Notes |
|---------|--------|-----------------|-------|----------|-------|----------|----------|--------|-------|
|---------|--------|-----------------|-------|----------|-------|----------|----------|--------|-------|

**SunStar Laboratories, Inc.**

**Organochlorine Pesticides by EPA Method 8081A**

|                     |    |      |      |   |         |          |          |           |  |
|---------------------|----|------|------|---|---------|----------|----------|-----------|--|
| alpha-BHC           | ND | 1.00 | ug/l | 1 | 8041610 | 04/16/08 | 04/17/08 | EPA 8081A |  |
| gamma-BHC (Lindane) | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| beta-BHC            | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| delta-BHC           | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Heptachlor          | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Aldrin              | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Heptachlor epoxide  | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| gamma-Chlordane     | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| alpha-Chlordane     | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Endosulfan I        | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| 4,4'-DDE            | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Dieldrin            | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Endrin              | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| 4,4'-DDD            | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Endosulfan II       | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| 4,4'-DDT            | ND | 2.00 | "    | " | "       | "        | "        | "         |  |
| Endrin aldehyde     | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Endosulfan sulfate  | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Methoxychlor        | ND | 5.00 | "    | " | "       | "        | "        | "         |  |
| Endrin ketone       | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Toxaphene           | ND | 20.0 | "    | " | "       | "        | "        | "         |  |

Surrogate: Tetrachloro-meta-xylene

73.3 %

35-140

"

"

"

"

**Polychlorinated Biphenyls by EPA Method 8082**

|          |    |      |      |   |         |          |          |          |  |
|----------|----|------|------|---|---------|----------|----------|----------|--|
| PCB-1016 | ND | 2.00 | ug/l | 1 | 8041611 | 04/16/08 | 04/17/08 | EPA 8082 |  |
| PCB-1221 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1232 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1242 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1248 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1254 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1260 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |

Surrogate: Tetrachloro-meta-xylene

68.4 %

35-140

"

"

"

"

SunStar Laboratories, Inc.

The results in this report apply to the samples analyzed in accordance with the chain of custody document. This analytical report must be reproduced in its entirety.

*Albert T. Vargas*

Albert Vargas, Senior Project Coordinator



PHONE (575) 393-2326 • 101 E. MARLAND • HOBBS, NM 88240

ANALYTICAL RESULTS FOR  
 GREEN ANALYTICAL LABORATORIES, INC.  
 ATTN: DEBBIE ZUFELT  
 75 SUTTLE STREET  
 DURANGO, CO 81303  
 FAX TO: (970) 247-4227

Receiving Date: 08/14/08  
 Reporting Date: 09/03/08  
 Project Number: 808-067-02  
 Project Name: BHP BILLITON NMEP  
 Project Location: NOT GIVEN  
 Lab Number: H15736-1  
 Sample ID: POND EAST OF L. PINABETE

Analysis Date: 08/21/08  
 Sampling Date: 08/12/08  
 Sample Type: SURFACE WATER  
 Sample Condition: COOL & INTACT  
 Sample Received By: ML  
 Analyzed By: CK

| AROCLORS (PCB's)<br>(mg/L) | Sample<br>Result | Method<br>Blank | True Value |       | %IA  |
|----------------------------|------------------|-----------------|------------|-------|------|
|                            |                  |                 | QC         | QC    |      |
|                            | H15736-1         |                 |            |       |      |
| PCB 1016                   | <0.020           | <0.020          | 0.115      | 0.100 | 115  |
| PCB 1221                   | <0.020           | <0.020          | NR         | NR    | NR   |
| PCB 1232                   | <0.020           | <0.020          | NR         | NR    | NR   |
| PCB 1242                   | <0.020           | <0.020          | 0.082      | 0.100 | 82.1 |
| PCB 1248                   | <0.020           | <0.020          | NR         | NR    | NR   |
| PCB 1254                   | <0.020           | <0.020          | 0.079      | 0.100 | 79.4 |
| PCB 1260                   | <0.020           | <0.020          | 0.093      | 0.100 | 92.5 |

% Recovery

|                  |      |
|------------------|------|
| Nitrobenzene-d5  | 17.1 |
| 2-Fluorobiphenyl | 22.3 |
| Terphenyl-d14    | 0.0* |

METHOD: SW-846 3510, 8270

\*Note: Surrogate outside historical limits due to matrix interference.

  
 \_\_\_\_\_  
 Lab Director

09/03/08  
 \_\_\_\_\_  
 Date

PLEASE NOTE: Liability and Damages. Cardinal's liability and client's exclusive remedy for any claim arising, whether based in contract or tort, shall be limited to the amount paid by client for analyses. All claims, including those for negligence and any other cause whatsoever shall be deemed waived unless made in writing and received by Cardinal within thirty (30) days after completion of the applicable service. In no event shall Cardinal be liable for incidental or consequential damages, including, without limitation, business interruptions, loss of use, or loss of profits incurred by client, its subsidiaries, affiliates or successors arising out of or related to the performance of services hereunder by Cardinal, regardless of whether such claim is based upon any of the above-stated reasons or otherwise. Results relate only to the samples identified above. This report shall not be reproduced except in full with written approval of Cardinal Laboratories.



Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: GA  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
05/20/08 14:45

**Pond East of Lower Pinabete  
T800629-01 (Water)**

| Analyte | Result | Reporting Limit | Units | Dilution | Batch | Prepared | Analyzed | Method | Notes |
|---------|--------|-----------------|-------|----------|-------|----------|----------|--------|-------|
|---------|--------|-----------------|-------|----------|-------|----------|----------|--------|-------|

**SunStar Laboratories, Inc.**

**Organochlorine Pesticides by EPA Method 8081A**

|                     |    |      |      |   |         |          |          |           |  |
|---------------------|----|------|------|---|---------|----------|----------|-----------|--|
| alpha-BHC           | ND | 1.00 | ug/l | 1 | 8051408 | 05/14/08 | 05/15/08 | EPA 8081A |  |
| gamma-BHC (Lindane) | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| beta-BHC            | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| delta-BHC           | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Heptachlor          | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Aldrin              | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Heptachlor epoxide  | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| gamma-Chlordane     | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| alpha-Chlordane     | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Endosulfan I        | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| 4,4'-DDE            | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Dieldrin            | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Endrin              | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| 4,4'-DDD            | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Endosulfan II       | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| 4,4'-DDT            | ND | 2.00 | "    | " | "       | "        | "        | "         |  |
| Endrin aldehyde     | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Endosulfan sulfate  | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Methoxychlor        | ND | 5.00 | "    | " | "       | "        | "        | "         |  |
| Endrin ketone       | ND | 1.00 | "    | " | "       | "        | "        | "         |  |
| Toxaphene           | ND | 20.0 | "    | " | "       | "        | "        | "         |  |

Surrogate: Tetrachloro-meta-xylene

101 % 35-140

**Polychlorinated Biphenyls by EPA Method 8082**

|          |    |      |      |   |         |          |          |          |  |
|----------|----|------|------|---|---------|----------|----------|----------|--|
| PCB-1016 | ND | 2.00 | ug/l | 1 | 8051407 | 05/14/08 | 05/15/08 | EPA 8082 |  |
| PCB-1221 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1232 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1242 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1248 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1254 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |
| PCB-1260 | ND | 2.00 | "    | " | "       | "        | "        | "        |  |

Surrogate: Tetrachloro-meta-xylene

84.7 % 35-140

SunStar Laboratories, Inc.

The results in this report apply to the samples analyzed in accordance with the chain of custody document. This analytical report must be reproduced in its entirety.

*Albert Vargas*

Albert Vargas, Senior Project Coordinator



# ARDINAL LABORATORIES

PHONE (575) 393-2326 • 101 E. MARLAND • HOBBS, NM 88240

ANALYTICAL RESULTS FOR  
GREEN ANALYTICAL LABORATORIES, INC.  
ATTN: DEBBIE ZUFELT  
75 SUTTLE STREET  
DURANGO, CO 81303  
FAX TO: (970) 247-4227

Receiving Date: 08/14/08  
Reporting Date: 09/03/08  
Project Number: 808-067-02  
Project Name: BHP BILLITON NMEP  
Project Location: NOT GIVEN  
Sample ID: POND EAST OF L. PINABETE  
Lab Number: H15736-1

Extraction Date: 08/19/08  
Analysis Date: 09/02/08  
Sampling Date: 08/12/08  
Sample Type: SURFACE WATER  
Sample Condition: COOL & INTACT  
Sample Received By: ML  
Analyzed By: CK

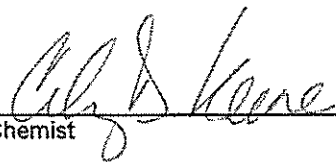
| PESTICIDES<br>(mg/L) | Sample Result<br>H15736-1 | Method<br>Blank | True Value |      |       |
|----------------------|---------------------------|-----------------|------------|------|-------|
|                      |                           |                 | QC         | %IA  | QC    |
| 4,4'-DDE             | <0.020                    | <0.002          | 0.050      | 99.1 | 0.050 |
| 4,4'-DDD             | <0.050                    | <0.005          | 0.044      | 88.3 | 0.050 |
| 4,4'-DDT             | <0.100                    | <0.010          | 0.062      | 124  | 0.050 |
| Chlordane            | <0.200                    | <0.020          | 0.091      | 91.1 | 0.100 |


% Recovery

|                  |       |
|------------------|-------|
| Nitrobenzene-d5  | 6.60* |
| 2-Fluorobiphenyl | 5.15* |
| Terphenyl-d14    | 0.0*  |

METHODS: EPA SW-846 8270

\*Note: Surrogate recovery outside historical limits due to matrix interference and sample dilution.

  
\_\_\_\_\_  
Chemist

  
\_\_\_\_\_  
Date

Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: BHP  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
04/22/08 14:33

Mid No Name  
T800496-01 (Water)

| Analyte | Result | Reporting Limit | Units | Dilution | Batch | Prepared | Analyzed | Method | Notes |
|---------|--------|-----------------|-------|----------|-------|----------|----------|--------|-------|
|---------|--------|-----------------|-------|----------|-------|----------|----------|--------|-------|

SunStar Laboratories, Inc.

Organochlorine Pesticides by EPA Method 8081A

| Analyte             | Result | Reporting Limit | Units | Dilution | Batch   | Prepared | Analyzed | Method    | Notes |
|---------------------|--------|-----------------|-------|----------|---------|----------|----------|-----------|-------|
| alpha-BHC           | ND     | 1.00            | ug/l  | 1        | 8041610 | 04/16/08 | 04/17/08 | EPA 8081A |       |
| gamma-BHC (Lindane) | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| beta-BHC            | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| delta-BHC           | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Heptachlor          | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Aldrin              | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Heptachlor epoxide  | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| gamma-Chlordane     | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| alpha-Chlordane     | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Endosulfan I        | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| 4,4'-DDE            | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Dieldrin            | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Endrin              | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| 4,4'-DDD            | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Endosulfan II       | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| 4,4'-DDT            | ND     | 2.00            | "     | "        | "       | "        | "        | "         |       |
| Endrin aldehyde     | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Endosulfan sulfate  | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Methoxychlor        | ND     | 5.00            | "     | "        | "       | "        | "        | "         |       |
| Endrin ketone       | ND     | 1.00            | "     | "        | "       | "        | "        | "         |       |
| Toxaphene           | ND     | 20.0            | "     | "        | "       | "        | "        | "         |       |

Surrogate: Tetrachloro-meta-xylene

70.6 %

35-140

"

"

"

"

Polychlorinated Biphenyls by EPA Method 8082

| Analyte  | Result | Reporting Limit | Units | Dilution | Batch   | Prepared | Analyzed | Method   | Notes |
|----------|--------|-----------------|-------|----------|---------|----------|----------|----------|-------|
| PCB-1016 | ND     | 2.00            | ug/l  | 1        | 8041611 | 04/16/08 | 04/17/08 | EPA 8082 |       |
| PCB-1221 | ND     | 2.00            | "     | "        | "       | "        | "        | "        |       |
| PCB-1232 | ND     | 2.00            | "     | "        | "       | "        | "        | "        |       |
| PCB-1242 | ND     | 2.00            | "     | "        | "       | "        | "        | "        |       |
| PCB-1248 | ND     | 2.00            | "     | "        | "       | "        | "        | "        |       |
| PCB-1254 | ND     | 2.00            | "     | "        | "       | "        | "        | "        |       |
| PCB-1260 | ND     | 2.00            | "     | "        | "       | "        | "        | "        |       |

Surrogate: Tetrachloro-meta-xylene

68.0 %

35-140

"

"

"

"

SunStar Laboratories, Inc.



Albert Vargas, Senior Project Coordinator

The results in this report apply to the samples analyzed in accordance with the chain of custody document. This analytical report must be reproduced in its entirety.



# ARDINAL LABORATORIES

PHONE (575) 393-2326 • 101 E. MARLAND • HOBBS, NM 88240

ANALYTICAL RESULTS FOR  
GREEN ANALYTICAL LABORATORIES, INC.  
ATTN: DEBBIE ZUFELT  
75 SUTTLE STREET  
DURANGO, CO 81303  
FAX TO: (970) 247-4227

Receiving Date: 08/14/08  
Reporting Date: 09/03/08  
Project Number: 808-067-06  
Project Name: BHP BILLITON NMEP  
Project Location: NOT GIVEN  
Lab Number: H15736-2  
Sample ID: POND ALONG NO NAME

Analysis Date: 08/21/08  
Sampling Date: 08/12/08  
Sample Type: SURFACE WATER  
Sample Condition: COOL & INTACT  
Sample Received By: ML  
Analyzed By: CK

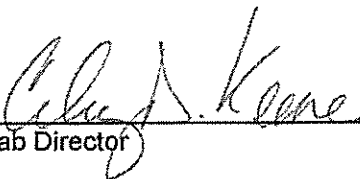
| AROCLORS (PCB's)<br>(mg/L) | Sample<br>Result | Method<br>Blank | QC    | True Value<br>QC | %IA  |
|----------------------------|------------------|-----------------|-------|------------------|------|
|                            | H15736-2         |                 |       |                  |      |
| PCB 1016                   | <0.020           | <0.020          | 0.115 | 0.100            | 115  |
| PCB 1221                   | <0.020           | <0.020          | NR    | NR               | NR   |
| PCB 1232                   | <0.020           | <0.020          | NR    | NR               | NR   |
| PCB 1242                   | <0.020           | <0.020          | 0.082 | 0.100            | 82.1 |
| PCB 1248                   | <0.020           | <0.020          | NR    | NR               | NR   |
| PCB 1254                   | <0.020           | <0.020          | 0.079 | 0.100            | 79.4 |
| PCB 1260                   | <0.020           | <0.020          | 0.093 | 0.100            | 92.5 |


% Recovery

|                  |      |
|------------------|------|
| Nitrobenzene-d5  | 49.2 |
| 2-Fluorobiphenyl | 99.9 |
| Terphenyl-d14    | 0.0* |

METHOD: SW-846 3510, 8270

\*Note: Surrogate outside historical limits due to matrix interference.

  
\_\_\_\_\_  
Lab Director

  
\_\_\_\_\_  
Date





PHONE (575) 393-2326 • 101 E. MARLAND • HOBBS, NM 88240

ANALYTICAL RESULTS FOR  
 GREEN ANALYTICAL LABORATORIES, INC.  
 ATTN: DEBBIE ZUFELT  
 75 SUTTLE STREET  
 DURANGO, CO 81303  
 FAX TO: (970) 247-4227

Receiving Date: 08/14/08  
 Reporting Date: 09/03/08  
 Project Number: 808-067-12  
 Project Name: BHP BILLITON NMEP  
 Project Location: NOT GIVEN  
 Lab Number: H15736-3  
 Sample ID: WELL SITE POND

Analysis Date: 08/21/08  
 Sampling Date: 08/12/08  
 Sample Type: SURFACE WATER  
 Sample Condition: COOL & INTACT  
 Sample Received By: ML  
 Analyzed By: CK

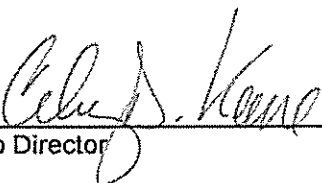
| AROCLORS (PCB's)<br>(mg/L) | Sample<br>Result<br>H15736-3 | Method<br>Blank | QC    | True Value<br>QC | %IA  |
|----------------------------|------------------------------|-----------------|-------|------------------|------|
| PCB 1016                   | <0.020                       | <0.020          | 0.115 | 0.100            | 115  |
| PCB 1221                   | <0.020                       | <0.020          | NR    | NR               | NR   |
| PCB 1232                   | <0.020                       | <0.020          | NR    | NR               | NR   |
| PCB 1242                   | <0.020                       | <0.020          | 0.082 | 0.100            | 82.1 |
| PCB 1248                   | <0.020                       | <0.020          | NR    | NR               | NR   |
| PCB 1254                   | <0.020                       | <0.020          | 0.079 | 0.100            | 79.4 |
| PCB 1260                   | <0.020                       | <0.020          | 0.093 | 0.100            | 92.5 |

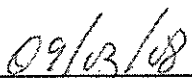
% Recovery

|                  |      |
|------------------|------|
| Nitrobenzene-d5  | 62.2 |
| 2-Fluorobiphenyl | 95.2 |
| Terphenyl-d14    | 0.0* |

METHOD: SW-846 3510, 8270

\*Note: Surrogate outside historical limits due to matrix interference.

  
 Lab Director

  
 Date



PHONE (575) 393-2326 • 101 E. MARLAND • HOBBS, NM 88240

ANALYTICAL RESULTS FOR  
GREEN ANALYTICAL LABORATORIES, INC.  
ATTN: DEBBIE ZUFELT  
75 SUTTLE STREET  
DURANGO, CO 81303  
FAX TO: (970) 247-4227

Receiving Date: 08/14/08  
Reporting Date: 09/03/08  
Project Number: 808-067-12  
Project Name: BHP BILLITON NMEP  
Project Location: NOT GIVEN  
Sample ID: WELL SITE POND  
Lab Number: H15736-3

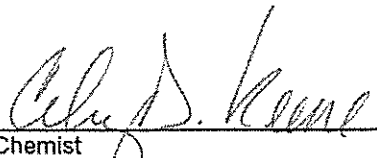
Extraction Date: 08/19/08  
Analysis Date: 09/02/08  
Sampling Date: 08/12/08  
Sample Type: SURFACE WATER  
Sample Condition: COOL & INTACT  
Sample Received By: ML  
Analyzed By: CK


| PESTICIDES<br>(mg/L) | Sample Result | Method | True Value |      |       |
|----------------------|---------------|--------|------------|------|-------|
|                      | H15736-3      | Blank  | QC         | %IA  | QC    |
| 4,4'-DDE             | <0.020        | <0.002 | 0.050      | 99.1 | 0.050 |
| 4,4'-DDD             | <0.050        | <0.005 | 0.044      | 88.3 | 0.050 |
| 4,4'-DDT             | <0.100        | <0.010 | 0.062      | 124  | 0.050 |
| Chlordane            | <0.200        | <0.020 | 0.091      | 91.1 | 0.100 |

| % Recovery       |      |
|------------------|------|
| Nitrobenzene-d5  | 13.8 |
| 2-Fluorobiphenyl | 13.0 |
| Terphenyl-d14    | 0.0* |

METHODS: EPA SW-846 8270

\*Note: Surrogate recovery outside historical limits due to matrix interference and sample dilution.

  
\_\_\_\_\_  
Chemist

  
\_\_\_\_\_  
Date

Laboratory QA/QC Reports

Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: BHP  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
04/22/08 14:33

**Organochlorine Pesticides by EPA Method 8081A - Quality Control**  
**SunStar Laboratories, Inc.**

| Analyte | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|

**Batch 8041610 - EPA 3510C GCMS/ECD**

**Blank (8041610-BLK1)**

Prepared: 04/16/08 Analyzed: 04/17/08

| Analyte                                   | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | ND     |                 | ug/l  | 1.00        |               | 75.3 | 35-140      |     |           |       |
| alpha-BHC                                 | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| gamma-BHC (Lindane)                       | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| beta-BHC                                  | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| delta-BHC                                 | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Heptachlor                                | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Aldrin                                    | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Heptachlor epoxide                        | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| gamma-Chlordane                           | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| alpha-Chlordane                           | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Endosulfan I                              | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| 4,4'-DDE                                  | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Dieldrin                                  | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Endrin                                    | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| 4,4'-DDD                                  | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Endosulfan II                             | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| 4,4'-DDT                                  | ND     | 2.00            | "     |             |               |      |             |     |           |       |
| Endrin aldehyde                           | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Endosulfan sulfate                        | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Methoxychlor                              | ND     | 5.00            | "     |             |               |      |             |     |           |       |
| Endrin ketone                             | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Toxaphene                                 | ND     | 20.0            | "     |             |               |      |             |     |           |       |

**LCS (8041610-BS1)**

Prepared: 04/16/08 Analyzed: 04/17/08

| Analyte                                   | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.827  |                 | ug/l  | 1.00        |               | 82.7 | 35-140      |     |           |       |
| gamma-BHC (Lindane)                       | 1.53   | 1.00            | "     | 2.00        |               | 76.6 | 40-120      |     |           |       |
| Heptachlor                                | 1.67   | 1.00            | "     | 2.00        |               | 83.3 | 40-120      |     |           |       |
| Aldrin                                    | 1.59   | 1.00            | "     | 2.00        |               | 79.3 | 40-120      |     |           |       |
| Dieldrin                                  | 1.98   | 1.00            | "     | 2.00        |               | 99.0 | 40-120      |     |           |       |
| Endrin                                    | 2.10   | 1.00            | "     | 2.00        |               | 105  | 40-120      |     |           |       |
| 4,4'-DDT                                  | 2.01   | 2.00            | "     | 2.00        |               | 101  | 40-120      |     |           |       |

SunStar Laboratories, Inc.

Albert Vargas, Senior Project Coordinator

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Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: BHP  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
04/22/08 14:33

**Organochlorine Pesticides by EPA Method 8081A - Quality Control**  
**SunStar Laboratories, Inc.**

| Analyte | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|

**Batch 8041610 - EPA 3510C GCMS/ECD**

**LCS Dup (8041610-BSD1)**

Prepared: 04/16/08 Analyzed: 04/17/08

|   |       |      |      |      |  |      |        |      |    |  |
|---|-------|------|------|------|--|------|--------|------|----|--|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.903 |      | ug/l | 1.00 |  | 90.3 | 35-140 |      |    |  |
| gamma-BHC (Lindane)                       | 1.63  | 1.00 | "    | 2.00 |  | 81.4 | 40-120 | 6.11 | 20 |  |
| Heptachlor                                | 1.71  | 1.00 | "    | 2.00 |  | 85.7 | 40-120 | 2.85 | 20 |  |
| Aldrin                                    | 1.64  | 1.00 | "    | 2.00 |  | 82.2 | 40-120 | 3.60 | 20 |  |
| Dieldrin                                  | 2.01  | 1.00 | "    | 2.00 |  | 101  | 40-120 | 1.72 | 20 |  |
| Endrin                                    | 2.19  | 1.00 | "    | 2.00 |  | 110  | 40-120 | 4.12 | 20 |  |
| 4,4'-DDT                                  | 2.03  | 2.00 | "    | 2.00 |  | 102  | 40-120 | 1.03 | 20 |  |

SunStar Laboratories, Inc.



Albert Vargas, Senior Project Coordinator

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ANALYTICAL RESULTS FOR  
GREEN ANALYTICAL LABORATORIES, INC.  
ATTN: DEBBIE ZUFELT  
75 SUTTLE STREET  
DURANGO, CO 81303  
FAX TO: (970) 247-4227

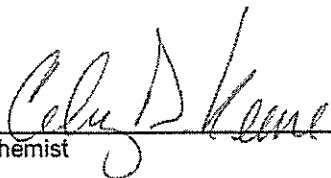
Receiving Date: 08/14/08  
Reporting Date: 09/03/08  
Project Number: 808-067-06  
Project Name: BHP BILLITON NMEP  
Project Location: NOT GIVEN  
Sample ID: POND ALONG NO NAME  
Lab Number: H15736-2


Extraction Date: 08/19/08  
Analysis Date: 09/02/08  
Sampling Date: 08/12/08  
Sample Type: SURFACE WATER  
Sample Condition: COOL & INTACT  
Sample Received By: ML  
Analyzed By: CK

| PESTICIDES<br>(mg/L) | Sample Result<br>H15736-2 | Method |       | True Value |       |
|----------------------|---------------------------|--------|-------|------------|-------|
|                      |                           | Blank  | QC    | %IA        | QC    |
| 4,4'-DDE             | <0.020                    | <0.002 | 0.050 | 99.1       | 0.050 |
| 4,4'-DDD             | <0.050                    | <0.005 | 0.044 | 88.3       | 0.050 |
| 4,4'-DDT             | <0.100                    | <0.010 | 0.062 | 124        | 0.050 |
| Chlordane            | <0.200                    | <0.020 | 0.091 | 91.1       | 0.100 |

| % Recovery       |      |
|------------------|------|
| Nitrobenzene-d5  | 18.8 |
| 2-Fluorobiphenyl | 18.1 |
| Terphenyl-d14    | 31.0 |

METHODS: EPA SW-846 8270

  
\_\_\_\_\_  
Chemist

  
\_\_\_\_\_  
Date

Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: BHP  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
04/22/08 14:33

**Polychlorinated Biphenyls by EPA Method 8082 - Quality Control  
SunStar Laboratories, Inc.**

| Analyte | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|

**Batch 8041611 - EPA 3510C GCMS/ECD**

**Blank (8041611-BLK1)**

Prepared: 04/16/08 Analyzed: 04/17/08

|   |       |      |      |      |  |      |        |  |  |  |
|---|-------|------|------|------|--|------|--------|--|--|--|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.650 |      | ug/l | 1.00 |  | 65.0 | 35-140 |  |  |  |
| PCB-1016                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1221                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1232                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1242                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1248                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1254                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1260                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |

**LCS (8041611-BS1)**

Prepared: 04/16/08 Analyzed: 04/17/08

|   |       |      |      |      |  |      |        |  |  |  |
|---|-------|------|------|------|--|------|--------|--|--|--|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.766 |      | ug/l | 1.00 |  | 76.6 | 40-130 |  |  |  |
| PCB-1016                                  | 7.55  | 2.00 | "    | 10.0 |  | 75.5 | 40-130 |  |  |  |
| PCB-1260                                  | 10.8  | 2.00 | "    | 10.0 |  | 108  | 40-130 |  |  |  |

**LCS Dup (8041611-BSD1)**

Prepared: 04/16/08 Analyzed: 04/17/08

|   |       |      |      |      |  |      |        |      |    |  |
|---|-------|------|------|------|--|------|--------|------|----|--|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.670 |      | ug/l | 1.00 |  | 67.0 | 40-130 |      |    |  |
| PCB-1016                                  | 6.83  | 2.00 | "    | 10.0 |  | 68.3 | 40-130 | 9.96 | 30 |  |
| PCB-1260                                  | 9.06  | 2.00 | "    | 10.0 |  | 90.6 | 40-130 | 17.2 | 30 |  |

SunStar Laboratories, Inc.

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Albert Vargas, Senior Project Coordinator

Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: BHP  
Project Number: [none]  
Project Manager: Debbie Zufelt

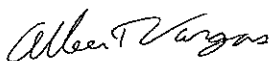
Reported:  
04/22/08 14:33

### Notes and Definitions

DET Analyte DETECTED  
ND Analyte NOT DETECTED at or above the reporting limit  
NR Not Reported  
dry Sample results reported on a dry weight basis  
RPD Relative Percent Difference

---

SunStar Laboratories, Inc.



Albert Vargas, Senior Project Coordinator

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Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: GA  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
05/20/08 14:45

**Organochlorine Pesticides by EPA Method 8081A - Quality Control**  
**SunStar Laboratories, Inc.**

| Analyte | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|

**Batch 8051408 - EPA 3510C GCMS/ECD**

**Blank (8051408-BLK1)**

Prepared: 05/14/08 Analyzed: 05/15/08

| Analyte                                   | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | ND     |                 | ug/l  | 1.00        |               | 90.6 | 35-140      |     |           |       |
| alpha-BHC                                 | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| gamma-BHC (Lindane)                       | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| beta-BHC                                  | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| delta-BHC                                 | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Heptachlor                                | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Aldrin                                    | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Heptachlor epoxide                        | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| gamma-Chlordane                           | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| alpha-Chlordane                           | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Endosulfan I                              | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| 4,4'-DDE                                  | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Dieldrin                                  | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Endrin                                    | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| 4,4'-DDD                                  | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Endosulfan II                             | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| 4,4'-DDT                                  | ND     | 2.00            | "     |             |               |      |             |     |           |       |
| Endrin aldehyde                           | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Endosulfan sulfate                        | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Methoxychlor                              | ND     | 5.00            | "     |             |               |      |             |     |           |       |
| Endrin ketone                             | ND     | 1.00            | "     |             |               |      |             |     |           |       |
| Toxaphene                                 | ND     | 20.0            | "     |             |               |      |             |     |           |       |

**LCS (8051408-BS1)**

Prepared: 05/14/08 Analyzed: 05/15/08

| Analyte                                   | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.935  |                 | ug/l  | 1.00        |               | 93.5 | 35-140      |     |           |       |
| gamma-BHC (Lindane)                       | 1.43   | 1.00            | "     | 2.00        |               | 71.6 | 40-120      |     |           |       |
| Heptachlor                                | 1.48   | 1.00            | "     | 2.00        |               | 74.2 | 40-120      |     |           |       |
| Aldrin                                    | 1.40   | 1.00            | "     | 2.00        |               | 70.1 | 40-120      |     |           |       |
| Dieldrin                                  | 1.69   | 1.00            | "     | 2.00        |               | 84.5 | 40-120      |     |           |       |
| Endrin                                    | 1.98   | 1.00            | "     | 2.00        |               | 98.8 | 40-120      |     |           |       |
| 4,4'-DDT                                  | 1.82   | 2.00            | "     | 2.00        |               | 90.8 | 40-120      |     |           |       |

SunStar Laboratories, Inc.



Albert Vargas, Senior Project Coordinator

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Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: GA  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
05/20/08 14:45

**Organochlorine Pesticides by EPA Method 8081A - Quality Control  
SunStar Laboratories, Inc.**

| Analyte | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|

**Batch 8051408 - EPA 3510C GCMS/ECD**

**Matrix Spike (8051408-MS1)**

Source: T800629-01

Prepared: 05/14/08

Analyzed: 05/15/08

|                                    |      |      |      |      |      |      |        |  |  |  |
|------------------------------------|------|------|------|------|------|------|--------|--|--|--|
| Surrogate: Tetrachloro-meta-xylene | 1.06 |      | ug/l | 1.00 |      | 106  | 35-140 |  |  |  |
| gamma-BHC (Lindane)                | 1.51 | 1.00 | "    | 2.00 | 0.10 | 70.4 | 20-120 |  |  |  |
| Heptachlor                         | 1.58 | 1.00 | "    | 2.00 | 0.03 | 77.3 | 20-120 |  |  |  |
| Aldrin                             | 1.47 | 1.00 | "    | 2.00 | ND   | 73.4 | 20-120 |  |  |  |
| Dieldrin                           | 1.89 | 1.00 | "    | 2.00 | ND   | 94.4 | 20-120 |  |  |  |
| Endrin                             | 1.97 | 1.00 | "    | 2.00 | ND   | 98.6 | 20-120 |  |  |  |
| 4,4'-DDT                           | 1.83 | 2.00 | "    | 2.00 | 0.03 | 90.0 | 20-120 |  |  |  |

**Matrix Spike Dup (8051408-MSD1)**

Source: T800629-01

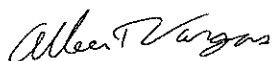
Prepared: 05/14/08

Analyzed: 05/15/08

|                                    |       |      |      |      |      |      |        |      |    |  |
|------------------------------------|-------|------|------|------|------|------|--------|------|----|--|
| Surrogate: Tetrachloro-meta-xylene | 0.994 |      | ug/l | 1.00 |      | 99.4 | 35-140 |      |    |  |
| gamma-BHC (Lindane)                | 1.48  | 1.00 | "    | 2.00 | 0.10 | 69.0 | 20-120 | 1.81 | 30 |  |
| Heptachlor                         | 1.53  | 1.00 | "    | 2.00 | 0.03 | 75.0 | 20-120 | 2.94 | 30 |  |
| Aldrin                             | 1.42  | 1.00 | "    | 2.00 | ND   | 71.1 | 20-120 | 3.26 | 30 |  |
| Dieldrin                           | 1.75  | 1.00 | "    | 2.00 | ND   | 87.4 | 20-120 | 7.69 | 30 |  |
| Endrin                             | 1.85  | 1.00 | "    | 2.00 | ND   | 92.6 | 20-120 | 6.19 | 30 |  |
| 4,4'-DDT                           | 1.70  | 2.00 | "    | 2.00 | 0.03 | 83.6 | 20-120 | 7.17 | 30 |  |

SunStar Laboratories, Inc.

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Albert Vargas, Senior Project Coordinator

Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: GA  
Project Number: [none]  
Project Manager: Debbie Zufelt

Reported:  
05/20/08 14:45

**Polychlorinated Biphenyls by EPA Method 8082 - Quality Control  
SunStar Laboratories, Inc.**

| Analyte | Result | Reporting Limit | Units | Spike Level | Source Result | %REC | %REC Limits | RPD | RPD Limit | Notes |
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|
|---------|--------|-----------------|-------|-------------|---------------|------|-------------|-----|-----------|-------|

**Batch 8051407 - EPA 3510C GCMS/ECD**

**Blank (8051407-BLK1)**

Prepared: 05/14/08 Analyzed: 05/15/08

|   |       |      |      |      |  |      |        |  |  |  |
|---|-------|------|------|------|--|------|--------|--|--|--|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.731 |      | ug/l | 1.00 |  | 73.1 | 35-140 |  |  |  |
| PCB-1016                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1221                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1232                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1242                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1248                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1254                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |
| PCB-1260                                  | ND    | 2.00 | "    |      |  |      |        |  |  |  |

**LCS (8051407-BS1)**

Prepared: 05/14/08 Analyzed: 05/15/08

|   |       |      |      |      |  |      |        |  |  |  |
|---|-------|------|------|------|--|------|--------|--|--|--|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.862 |      | ug/l | 1.00 |  | 86.2 | 40-130 |  |  |  |
| PCB-1016                                  | 9.82  | 2.00 | "    | 10.0 |  | 98.2 | 40-130 |  |  |  |
| PCB-1260                                  | 9.58  | 2.00 | "    | 10.0 |  | 95.8 | 40-130 |  |  |  |

**Matrix Spike (8051407-MS1)**

Source: T800629-01

Prepared: 05/14/08 Analyzed: 05/15/08

|   |       |      |      |      |    |      |        |  |  |  |
|---|-------|------|------|------|----|------|--------|--|--|--|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.753 |      | ug/l | 1.00 |    | 75.3 | 40-130 |  |  |  |
| PCB-1016                                  | 9.09  | 2.00 | "    | 10.0 | ND | 90.9 | 40-130 |  |  |  |
| PCB-1260                                  | 9.21  | 2.00 | "    | 10.0 | ND | 92.1 | 40-130 |  |  |  |

**Matrix Spike Dup (8051407-MSD1)**

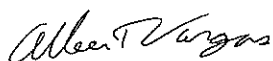
Source: T800629-01

Prepared: 05/14/08 Analyzed: 05/15/08

|   |       |      |      |      |    |      |        |      |    |  |
|---|-------|------|------|------|----|------|--------|------|----|--|
| <i>Surrogate: Tetrachloro-meta-xylene</i> | 0.819 |      | ug/l | 1.00 |    | 81.9 | 40-130 |      |    |  |
| PCB-1016                                  | 9.85  | 2.00 | "    | 10.0 | ND | 98.5 | 40-130 | 7.97 | 30 |  |
| PCB-1260                                  | 9.98  | 2.00 | "    | 10.0 | ND | 99.8 | 40-130 | 8.02 | 30 |  |

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The results in this report apply to the samples analyzed in accordance with the chain of custody document. This analytical report must be reproduced in its entirety.



Albert Vargas, Senior Project Coordinator

Green Analytical  
75 Suttle Street  
Durango CO, 81303

Project: GA  
Project Number: [none]  
Project Manager: Debbie Zufelt


Reported:  
05/20/08 14:45

### Notes and Definitions

DET Analyte DETECTED  
ND Analyte NOT DETECTED at or above the reporting limit  
NR Not Reported  
dry Sample results reported on a dry weight basis  
RPD Relative Percent Difference

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Albert Vargas, Senior Project Coordinator

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## **Appendix 18.D**

Quality Assurance and Quality Control Results for Baseline  
Surface Water Quality Data from 2007 to 2008

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 708-176     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum    | 0.00          | 2.25         | <b>2.00</b>  | <b>113</b>       | <0.10          | <0.10            | <b>NC</b>   |
| Arsenic     | 0.00          | 0.055        | <b>0.050</b> | <b>110</b>       | 0.0030         | 0.0029           | <b>3.39</b> |
| Barium      | 0.00          | 0.050        | <b>0.050</b> | <b>100</b>       | 0.5030         | 0.5030           | <b>0.00</b> |
| Boron       | 0.00          | 2.0          | <b>2.0</b>   | <b>100</b>       | 0.3            | 0.3              | <b>0.00</b> |
| Cadmium     | 0.00          | 0.051        | <b>0.050</b> | <b>102</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium     | 0.00          | 4.9          | <b>5.0</b>   | <b>98</b>        | 90.8           | 90.5             | <b>0.33</b> |
| Chromium    | 0.00          | 0.052        | <b>0.050</b> | <b>104</b>       | 0.005          | 0.005            | <b>0.00</b> |
| Copper      | 0.00          | 0.051        | <b>0.050</b> | <b>102</b>       | 0.0004         | 0.0004           | <b>0.00</b> |
| Iron        | 0.00          | 0.98         | <b>1.00</b>  | <b>98</b>        | <0.05          | <0.05            | <b>NC</b>   |
| Lead        | 0.00          | 0.051        | <b>0.050</b> | <b>102</b>       | 0.0022         | 0.0020           | <b>9.52</b> |
| Magnesium * | 0.00          | 1.4          | <b>1.0</b>   | <b>140</b>       | 16.9           | 16.4             | <b>3.00</b> |
| Manganese   | 0.00          | 1.05         | <b>1.00</b>  | <b>105</b>       | <0.0005        | <0.0005          | <b>NC</b>   |
| Potassium   | 0.00          | 1.0          | <b>1.0</b>   | <b>100</b>       | 2.2            | 2.0              | <b>9.52</b> |
| Selenium    | 0.00          | 0.278        | <b>0.250</b> | <b>111</b>       | 0.009          | 0.009            | <b>0.00</b> |
| Silver      | 0.00          | 0.053        | <b>0.050</b> | <b>106</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium      | 0.00          | 50.3         | <b>50.0</b>  | <b>101</b>       | 19.3           | 18.1             | <b>6.42</b> |
| Zinc        | 0.00          | 0.057        | <b>0.050</b> | <b>114</b>       | 0.232          | 0.228            | <b>1.74</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#    | SRM Data   |            |             |                  | Blank Data   |                 |
|------------|------------|------------|-------------|------------------|--------------|-----------------|
| 709-176    | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum   | 5.16       | 5.00       | <b>103</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic *  | 0.056      | 0.050      | <b>112</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium     | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron      | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium    | 0.054      | 0.050      | <b>108</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium    | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium   | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper     | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron       | 5.04       | 5.00       | <b>101</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead       | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | 0.0001       | 0.0001          |
| Magnesium  | 4.8        | 5.0        | <b>96.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese  | 2.53       | 2.50       | <b>101</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium  | 9.7        | 10.0       | <b>97.0</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium * | 0.278      | 0.250      | <b>111</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver *   | 0.058      | 0.050      | <b>116</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium     | 16.0       | 16.2       | <b>98.8</b> | 90-110 %         | <0.5         | 0.5             |
| Zinc       | 0.06       | 0.05       | <b>110</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.



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## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 708-176     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 3.99         | <b>4.00</b>   | <b>99.8</b>      | 0.16           | 0.14             | <b>13.3</b> |
| Manganese-T | 0.000         | 2.070        | <b>2.00</b>   | <b>104</b>       | 0.008          | 0.007            | <b>13.3</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 708-176     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.04       | 5.00       | 101       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.53       | 2.50       | 101       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.0021     | 0.0020     | 105       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 708-176         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 104          | <b>100</b>  | <b>104</b>       | 460            | 450              | <b>2.20</b> |
| Chloride        | 1             | 101          | <b>100</b>  | <b>100</b>       | 4800           | 4750             | <b>1.05</b> |
| EC              | NMA           | NMA          | NMA         | <b>NMA</b>       | 612            | 608              | <b>0.66</b> |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90</b>        | 0.4            | 0.4              | <b>0.00</b> |
| Nitrate/Nitrite | 0.00          | 1.47         | <b>1.54</b> | <b>95.5</b>      | <0.02          | <0.02            | <b>NC</b>   |
| pH              | NMA           | NMA          | NMA         | <b>NMA</b>       | 7.91           | 7.90             | <b>0.13</b> |
| Phosphorus-T    | 0.00          | 0.29         | <b>0.25</b> | <b>116</b>       | 0.23           | 0.21             | <b>9.09</b> |
| Sulfate         | 0             | 50.0         | <b>50.0</b> | <b>100</b>       | 410            | 400              | <b>2.47</b> |
| TDS             | NMA           | NMA          | NMA         | <b>NMA</b>       | 915            | 910              | <b>0.55</b> |
| TSS             | NMA           | NMA          | NMA         | <b>NMA</b>       | 31500          | 31450            | <b>0.16</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit



# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 708-176         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 324        | 302        | <b>107</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 117        | 117        | <b>100</b>  | 90-110 %         | <10          | 10              |
| EC              | 528        | 561        | <b>94.1</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.48       | 0.50       | <b>96.0</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.32       | 8.40       | <b>99.0</b> | 90-110 %         | NMA          | NMA             |
| Phosphorus-T    | 0.22       | 0.20       | <b>110</b>  | 90-110 %         | <0.05        | 0.05            |
| Sulfate         | 335        | 320        | <b>105</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1235       | 1210       | <b>102</b>  | 90-110 %         | <10          | 10              |
| TSS             | 173        | 158        | <b>109</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#   | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 709-094   | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum  | 0.00          | 2.11         | <b>2.00</b>  | <b>106</b>       | 0.12           | 0.12             | <b>0.00</b> |
| Arsenic   | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0399         | 0.0373           | <b>6.74</b> |
| Barium    | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0013         | 0.0012           | <b>8.00</b> |
| Boron     | 0.0           | 2.0          | <b>2.0</b>   | <b>102</b>       | 74.5           | 74.0             | <b>0.67</b> |
| Cadmium   | 0.00000       | 0.049        | <b>0.050</b> | <b>98</b>        | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium   | 0.0           | 4.9          | <b>5.0</b>   | <b>98</b>        | 428            | 418              | <b>2.36</b> |
| Chromium  | 0.000         | 0.050        | <b>0.050</b> | <b>100</b>       | 0.016          | 0.016            | <b>0.00</b> |
| Copper    | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0110         | 0.009            | <b>20.0</b> |
| Iron      | 0.00          | 0.98         | <b>1.00</b>  | <b>98</b>        | 0.11           | 0.11             | <b>0.00</b> |
| Lead      | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0030         | 0.0028           | <b>6.90</b> |
| Magnesium | 0.0           | 1.1          | <b>1.0</b>   | <b>110</b>       | 13.5           | 13.0             | <b>3.77</b> |
| Manganese | 0.000         | 1.07         | <b>1.00</b>  | <b>107</b>       | 0.371          | 0.371            | <b>0.00</b> |
| Potassium | 0.0           | 1.0          | <b>1.0</b>   | <b>100</b>       | 269.0          | 260.0            | <b>3.40</b> |
| Selenium  | 0.000         | 0.248        | <b>0.250</b> | <b>99.2</b>      | 0.002          | 0.002            | <b>0.00</b> |
| Silver    | 0.00000       | 0.052        | <b>0.050</b> | <b>104</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium    | 0.0           | 49.1         | <b>50.0</b>  | <b>98.2</b>      | 309.0          | 306.0            | <b>0.98</b> |
| Zinc      | 0.000         | 0.051        | <b>0.050</b> | <b>102</b>       | 0.023          | 0.022            | <b>4.44</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

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## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 709-094     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum    | 5.22       | 5.00       | <b>104</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic     | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium      | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron       | 5.3        | 5.0        | <b>106</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium     | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium     | 4.6        | 5.0        | <b>92.0</b> | 90-110 %         | <0.5         | 0.5             |
| Chromium    | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper      | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron        | 4.63       | 5.00       | <b>92.6</b> | 90-110 %         | <0.05        | 0.05            |
| Lead        | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium * | 4.3        | 5.0        | <b>86.8</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese   | 2.67       | 2.50       | <b>107</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium   | 8.9        | 10.0       | <b>89.0</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium    | 0.248      | 0.250      | <b>99.2</b> | 90-110 %         | <0.001       | 0.001           |
| Silver      | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium      | 7.4        | 8.1        | <b>91.4</b> | 90-110 %         | <0.5         | 0.5             |
| Zinc        | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.



# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 708-094     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| PARAMETER   |               |              |              |                  |                |                  |             |
| Iron-T      | 0.00          | 4.15         | <b>4.00</b>  | <b>104</b>       | <0.02          | <0.02            | <b>NC</b>   |
| Manganese-T | 0.000         | 2.05         | <b>2.00</b>  | <b>103</b>       | 0.042          | 0.040            | <b>4.88</b> |
| Mercury-T   | 0.0000        | 0.0021       | <b>0.002</b> | <b>105</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit  
NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 709-094     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.25       | 5.00       | 105       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.61       | 2.50       | 104       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 709-094         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 1             | 101          | <b>100</b>  | <b>100</b>       | 224            | 220              | <b>1.80</b> |
| Chloride        | 1             | 102          | <b>100</b>  | <b>101</b>       | <10            | <10              | <b>NC</b>   |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 625            | 625              | <b>0.00</b> |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90</b>        | 0.3            | 0.3              | <b>0.00</b> |
| Nitrate/Nitrite | 0.00          | 1.95         | <b>1.92</b> | <b>102</b>       | 0.23           | 0.21             | <b>9.09</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 8.02           | 7.95             | <b>0.88</b> |
| Phosphorus-T    | 0.00          | 0.25         | <b>0.25</b> | <b>100</b>       | 0.22           | 0.21             | <b>4.65</b> |
| Sulfate         | 0             | 55.0         | <b>50.0</b> | <b>110</b>       | 14600          | 14400            | <b>1.38</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 355            | 350              | <b>1.42</b> |
| TSS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 33600          | 32800            | <b>2.41</b> |

NMA=Data not applicable to Method.

NA=Data not available.



# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 709-094         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 280        | 283        | <b>98.9</b> | 90-110 %         | <10          | 10              |
| Chloride        | 39         | 38         | <b>103</b>  | 90-110 %         | <10          | 10              |
| EC              | 514        | 561        | <b>91.6</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.51       | 0.50       | <b>102</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.28       | 8.40       | <b>98.6</b> | 90-110 %         | NMA          | NMA             |
| Phosphorus-T    | 0.21       | 0.20       | <b>105</b>  | 90-110 %         | <0.05        | 0.05            |
| Sulfate         | 345        | 320        | <b>108</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1245       | 1210       | <b>103</b>  | 90-110 %         | <10          | 10              |
| TSS *           | 173        | 146        | <b>118</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#   | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 709-141   | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum  | 0.00          | 0.51         | <b>0.50</b>  | <b>102</b>       | 0.19           | 0.16             | <b>17.1</b> |
| Arsenic   | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | <0.0005        | <0.0005          | <b>NC</b>   |
| Barium    | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0398         | 0.0393           | <b>1.26</b> |
| Boron     | 0.0           | 3.9          | <b>4.0</b>   | <b>96.3</b>      | 0.1            | 0.1              | <b>0.00</b> |
| Cadmium   | 0.00000       | 0.0500       | <b>0.050</b> | <b>100</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium   | 0.0           | 5.1          | <b>5.0</b>   | <b>102</b>       | 15.5           | 15.5             | <b>0.00</b> |
| Chromium  | 0.000         | 0.050        | <b>0.050</b> | <b>100</b>       | 0.009          | 0.009            | <b>0.00</b> |
| Copper    | 0.0000        | 0.051        | <b>0.050</b> | <b>102</b>       | 0.0702         | 0.0700           | <b>0.29</b> |
| Iron      | 0.00          | 1.05         | <b>1.00</b>  | <b>105</b>       | 154            | 148              | <b>3.97</b> |
| Lead      | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0003         | 0.0003           | <b>0.00</b> |
| Magnesium | 0.0           | 1.1          | <b>1.0</b>   | <b>107</b>       | 3.0            | 2.9              | <b>3.39</b> |
| Manganese | 0.000         | 2.04         | <b>2.00</b>  | <b>102</b>       | 0.090          | 0.085            | <b>5.71</b> |
| Potassium | 3.0           | 3.9          | <b>1.0</b>   | <b>86.0</b>      | 3.0            | 3.0              | <b>0.00</b> |
| Selenium  | 0.001         | 0.256        | <b>0.250</b> | <b>102</b>       | 0.002          | 0.002            | <b>0.00</b> |
| Silver    | 0.00000       | 0.051        | <b>0.050</b> | <b>102</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium    | 0.0           | 54.3         | <b>50.0</b>  | <b>109</b>       | 90.2           | 90.1             | <b>0.11</b> |
| Zinc      | 0.000         | 0.050        | <b>0.050</b> | <b>100</b>       | 0.019          | 0.019            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 709-141   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum  | 4.95       | 5.00       | <b>99.0</b> | 90-110 %         | <0.10        | 0.10            |
| Arsenic   | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 4.7        | 5.0        | <b>94.0</b> | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 4.77       | 5.00       | <b>95.4</b> | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 4.7        | 5.0        | <b>94.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.57       | 2.50       | <b>103</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 9.3        | 10.0       | <b>93.0</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.254      | 0.250      | <b>102</b>  | 90-110 %         | 0.001        | 0.001           |
| Silver    | 0.054      | 0.050      | <b>108</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.6        | 8.1        | <b>106</b>  | 90-110 %         | <0.5         | 0.5             |
| Zinc      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.



# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 709-141     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| PARAMETER   |               |              |              |                  |                |                  |             |
| Iron-T      | 0.00          | 4.15         | <b>4.00</b>  | <b>104</b>       | 125            | 124              | <b>0.80</b> |
| Manganese-T | 0.000         | 2.050        | <b>2.000</b> | <b>103</b>       | 7.60           | 7.31             | <b>3.89</b> |
| Mercury-T   | 0.0000        | 0.0021       | <b>0.002</b> | <b>105</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit  
NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 709-141     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.25       | 5.00       | 105       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.61       | 2.50       | 104       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| PARAMETER       | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 103          | <b>100</b>  | <b>103</b>       | 139            | 138              | <b>0.72</b> |
| Chloride        | 0             | 104          | <b>100</b>  | <b>104</b>       | <10            | <10              | <b>NC</b>   |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 570            | 560              | <b>1.77</b> |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90.0</b>      | 0.2            | 0.2              | <b>0.00</b> |
| Nitrate/Nitrite | 0.00          | 1.84         | <b>1.92</b> | <b>95.8</b>      | 2.55           | 2.54             | <b>0.39</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 7.64           | 7.61             | <b>0.39</b> |
| Phosphorus-T    | 0.00          | 0.27         | <b>0.25</b> | <b>108</b>       | 0.26           | 0.22             | <b>16.7</b> |
| Sulfate         | 0             | 53           | <b>50</b>   | <b>106</b>       | 2050           | 2050             | <b>0.00</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 330            | 320              | <b>3.08</b> |
| TSS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 8700           | 7700             | <b>12.2</b> |

NMA=Data not applicable to Method.

NA=Data not available.

NC=Not calculated due to results less than the detection limit



# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 709-141         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 296        | 283        | <b>105</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 40         | 38         | <b>106</b>  | 90-110 %         | <10          | 10              |
| EC *            | 495        | 561        | <b>88.2</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.49       | 0.50       | <b>98.0</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.38       | 8.40       | <b>100</b>  | 90-110 %         | NMA          | NMA             |
| Phosphorus-T *  | 4.30       | 5.20       | <b>82.7</b> | 90-110 %         | <0.05        | 0.05            |
| Sulfate *       | 355        | 320        | <b>111</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1215       | 1210       | <b>100</b>  | 90-110 %         | <10          | 10              |
| TSS *           | 173        | 155        | <b>112</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#    | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 071009K001 | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum   | 0.00          | 2.04         | <b>2.00</b>  | <b>102</b>       | <0.1           | <0.1             | <b>NC</b>   |
| Arsenic    | 0.0000        | 0.052        | <b>0.050</b> | <b>104</b>       | 0.0049         | 0.0048           | <b>2.06</b> |
| Barium     | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 3.80           | 3.75             | <b>1.32</b> |
| Boron      | 0.0           | 2.1          | <b>2.00</b>  | <b>105</b>       | 0.3            | 0.3              | <b>0.00</b> |
| Cadmium    | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium    | 0.0           | 5.2          | <b>5.00</b>  | <b>104</b>       | 1.2            | 1.2              | <b>0.00</b> |
| Chromium   | 0.000         | 0.051        | <b>0.050</b> | <b>102</b>       | 0.002          | 0.002            | <b>0.00</b> |
| Copper     | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0430         | 0.0400           | <b>7.23</b> |
| Iron       | 0.00          | 1.06         | <b>1.00</b>  | <b>106</b>       | 102            | 102              | <b>0.00</b> |
| Lead       | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | <0.0001        | <0.0001          | <b>NC</b>   |
| Magnesium  | 0.0           | 1.1          | <b>1.0</b>   | <b>110</b>       | <0.5           | <0.5             | <b>NC</b>   |
| Manganese  | 0.000         | 1.060        | <b>1.0</b>   | <b>106</b>       | 0.069          | 0.068            | <b>1.46</b> |
| Potassium  | 0.0           | 1.0          | <b>1.0</b>   | <b>100</b>       | 0.6            | 0.6              | <b>0.00</b> |
| Selenium   | 0.006         | 2.67         | <b>2.50</b>  | <b>107</b>       | 0.022          | 0.022            | <b>0.00</b> |
| Silver     | 0.00000       | 0.051        | <b>0.050</b> | <b>102</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium     | 0.0           | 1.0          | <b>1.00</b>  | <b>100</b>       | 162            | 161              | <b>0.62</b> |
| Zinc       | 0.000         | 0.052        | <b>0.050</b> | <b>104</b>       | 0.001          | 0.001            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#    | SRM Data   |            |             |                  | Blank Data   |                 |
|------------|------------|------------|-------------|------------------|--------------|-----------------|
| 071009k001 | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum   | 5.30       | 5.00       | <b>106</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic    | 0.054      | 0.050      | <b>108</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium     | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron      | 5.5        | 5.000      | <b>110</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium    | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium    | 5.0        | 5.000      | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium   | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper     | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron       | 5.18       | 5.0        | <b>104</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead       | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium  | 4.9        | 5.0        | <b>98.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese  | 2.76       | 2.50       | <b>110</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium  | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium   | 0.267      | 0.250      | <b>107</b>  | 90-110 %         | 0.006        | 0.001           |
| Silver     | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium     | 8.2        | 8.1        | <b>101</b>  | 90-110 %         | <0.5         | 0.5             |
| Zinc       | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.



# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 071009k001  | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 2.03         | <b>2.00</b>  | <b>102</b>       | 0.15           | 0.15             | <b>0.00</b> |
| Manganese-T | 0.000         | 1.05         | <b>1.00</b>  | <b>105</b>       | 0.080          | 0.080            | <b>0.00</b> |
| Mercury-T   | 0.0000        | 0.0022       | <b>0.002</b> | <b>110</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 071009k001  | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 4.69       | 5.00       | <b>93.8</b> | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.43       | 2.50       | <b>97.2</b> | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | <b>100</b>  | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 071009k001      | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 106          | <b>100</b>   | <b>106</b>       | 99             | 99               | <b>0.00</b> |
| Chloride        | 0             | 101          | <b>100</b>   | <b>101</b>       | 13             | 13               | <b>0.00</b> |
| EC              | NMA           | NMA          | <b>NMA</b>   | <b>NMA</b>       | 1017           | 1015             | <b>0.20</b> |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>   | <b>90.0</b>      | <0.2           | <0.2             | <b>NC</b>   |
| Nitrate/Nitrite | 0.00          | 1.76         | <b>1.92</b>  | <b>91.7</b>      | 0.31           | 0.31             | <b>0.00</b> |
| pH              | NMA           | NMA          | <b>NMA</b>   | <b>NMA</b>       | 8.07           | 8.05             | <b>0.25</b> |
| Phosphorus-T    | 0.00          | 0.27         | <b>0.25</b>  | <b>108</b>       | 0.45           | 0.41             | <b>9.30</b> |
| Sulfate         | 0             | 55.00        | <b>50.00</b> | <b>110</b>       | 390            | 390              | <b>0.00</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>   | <b>NMA</b>       | 605            | 595              | <b>1.67</b> |
| TSS             | NMA           | NMA          | <b>NMA</b>   | <b>NMA</b>       | 132000         | 131000           | <b>0.76</b> |

NMA=Data not applicable to Method.

NA=Data not available.

NC=Not calculated due to results less than the detection limit



# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 071009k001      | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 290        | 283        | <b>102</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 39         | 37.9       | <b>103</b>  | 90-110 %         | <10          | 10              |
| EC              | 514        | 561        | <b>91.6</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.51       | 0.50       | <b>102</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.38       | 8.40       | <b>100</b>  | 90-110 %         | NMA          | NMA             |
| Phosphorus-T    | 5.61       | 5.32       | <b>105</b>  | 90-110 %         | <0.05        | 0.05            |
| Sulfate         | 340        | 321        | <b>106</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1175       | 1210       | <b>97.1</b> | 90-110 %         | <10          | 10              |
| TSS             | 156        | 173        | <b>90.2</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#    | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 712051326+ | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum   | 0.00          | 2.04         | <b>2.00</b>  | <b>102</b>       | <0.1           | <0.1             | <b>NC</b>   |
| Arsenic    | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0061         | 0.0057           | <b>6.78</b> |
| Barium     | 0.0000        | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.0089         | 0.0085           | <b>4.60</b> |
| Boron      | 0.0           | 2.1          | <b>2.0</b>   | <b>104</b>       | <0.1           | <0.1             | <b>NC</b>   |
| Cadmium    | 0.00000       | 0.049        | <b>0.050</b> | <b>98.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium    | 0.0           | 45.8         | <b>50.0</b>  | <b>91.6</b>      | 22.1           | 21.6             | <b>2.29</b> |
| Chromium   | 0.000         | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.007          | 0.007            | <b>0.00</b> |
| Copper     | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.892          | 0.732            | <b>19.7</b> |
| Iron       | 0.00          | 9.48         | <b>10.0</b>  | <b>94.8</b>      | <0.05          | <0.05            | <b>NC</b>   |
| Lead       | 0.0000        | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.0001         | 0.0001           | <b>0.00</b> |
| Magnesium  | 0.0           | 9.5          | <b>10.0</b>  | <b>95.0</b>      | 1.7            | 1.7              | <b>0.00</b> |
| Manganese  | 0.000         | 1.16         | <b>1.00</b>  | <b>116</b>       | 0.017          | 0.017            | <b>0.00</b> |
| Potassium  | 0.0           | 9.9          | <b>10.0</b>  | <b>99.0</b>      | 3.7            | 3.6              | <b>2.74</b> |
| Selenium   | 0.000         | 0.250        | <b>0.250</b> | <b>100</b>       | 0.179          | 0.170            | <b>5.16</b> |
| Silver     | 0.00000       | 0.0500       | <b>0.050</b> | <b>100</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium     | 0.0           | 481.0        | <b>500</b>   | <b>96.2</b>      | 194            | 190              | <b>2.08</b> |
| Zinc       | 0.000         | 0.050        | <b>0.050</b> | <b>100</b>       | 0.011          | 0.011            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0712051326+ | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum    | 5.16       | 5.00       | <b>103</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic     | 0.0520     | 0.050      | <b>104</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium      | 0.0500     | 0.050      | <b>100</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron       | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium     | 0.05100    | 0.050      | <b>102</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium     | 5.3        | 5.0        | <b>106</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium    | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper      | 0.0500     | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron        | 5.39       | 5.0        | <b>108</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead        | 0.0490     | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium   | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.5         | 0.5             |
| Manganese   | 2.65       | 2.50       | <b>106</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium   | 10.9       | 10.0       | <b>109</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium    | 0.261      | 0.250      | <b>104</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver *    | 0.06000    | 0.050      | <b>120</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium      | 9.0        | 9.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Zinc        | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.



# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 0712051326+ | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 4.21         | <b>4.00</b>   | <b>105</b>       | 42.9           | 40.6             | <b>5.51</b> |
| Manganese-T | 0.000         | 2.16         | <b>2.00</b>   | <b>108</b>       | 1.71           | 1.62             | <b>5.41</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| PARAMETER   | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| 0712051326+ |            |            |           |                  |              |                 |
| Iron-T      | 5.10       | 5.00       | 102       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.65       | 2.50       | 106       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.0021     | 0.0020     | 105       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

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## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 0712051326+     | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 106          | <b>100</b>  | <b>106</b>       | 224            | 220              | <b>1.80</b> |
| Chloride        | 0             | 101          | <b>100</b>  | <b>101</b>       | 210            | 206              | <b>1.92</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 708            | 704              | <b>0.57</b> |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90.0</b>      | <0.2           | <0.2             | <b>NC</b>   |
| Nitrate/Nitrite | 0.00          | 1.90         | <b>1.92</b> | <b>99.0</b>      | 32.1           | 31.4             | <b>2.20</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 8.19           | 8.10             | <b>1.10</b> |
| Phosphorus-T    | 0.29          | 0.54         | <b>0.25</b> | <b>100</b>       | 0.23           | 0.22             | <b>4.44</b> |
| Sulfate         | 0             | 54           | <b>50</b>   | <b>108</b>       | 9800           | 9800             | <b>0.00</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 935            | 930              | <b>0.54</b> |
| TSS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 88000          | 85200            | <b>3.23</b> |

NMA=Data not applicable to Method.

NA=Data not available.

NC=Not calculated due to results less than the detection limit



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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0712051326+     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 274        | 283        | <b>96.8</b> | 90-110 %         | <10          | 10              |
| Chloride        | 37         | 37.9       | <b>97.6</b> | 90-110 %         | <10          | 10              |
| EC              | 556        | 561        | <b>99.1</b> | 90-110 %         | NA           | NA              |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.50       | 0.50       | <b>100</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.30       | 8.40       | <b>98.8</b> | 90-110 %         | NA           | NA              |
| Phosphorus-T    | 5.49       | 5.32       | <b>103</b>  | 90-110 %         | <0.05        | 0.05            |
| Sulfate         | 350        | 321        | <b>109</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1205       | 1210       | <b>99.6</b> | 90-110 %         | <10          | 10              |
| TSS *           | 18.0       | 21.9       | <b>82.2</b> | 90-110 %         | <10          | 10              |

NA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 802-052     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum    | 0.00          | 2.33         | <b>2.00</b>  | <b>117</b>       | 1.69           | 1.65             | <b>2.40</b> |
| Arsenic     | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.0093         | 0.0093           | <b>0.00</b> |
| Barium      | 0.0000        | 0.046        | <b>0.050</b> | <b>92.0</b>      | 0.0344         | 0.0328           | <b>4.76</b> |
| Boron       | 0.1           | 2.3          | <b>2.0</b>   | <b>108</b>       | 0.4            | 0.4              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.044        | <b>0.050</b> | <b>88.0</b>      | 0.00006        | 0.00005          | <b>18.2</b> |
| Calcium *   | 0.0           | 6.9          | <b>5.00</b>  | <b>138</b>       | 82.5           | 82.0             | <b>0.61</b> |
| Chromium    | 0.000         | 0.044        | <b>0.050</b> | <b>88.0</b>      | 0.002          | 0.002            | <b>0.00</b> |
| Copper      | 0.0000        | 0.046        | <b>0.050</b> | <b>92.0</b>      | 0.0174         | 0.0171           | <b>1.74</b> |
| Iron *      | 0.00          | 1.40         | <b>1.00</b>  | <b>140</b>       | <0.05          | <0.05            | <b>NC</b>   |
| Lead        | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.0001         | 0.0001           | <b>0.00</b> |
| Magnesium * | 0.0           | 1.4          | <b>1.0</b>   | <b>140</b>       | 9.1            | 9.0              | <b>1.10</b> |
| Manganese   | 0.000         | 1.20         | <b>1.0</b>   | <b>120</b>       | 0.008          | 0.008            | <b>0.00</b> |
| Potassium * | 0.0           | 1.4          | <b>1.0</b>   | <b>140</b>       | 0.86           | 0.82             | <b>4.76</b> |
| Selenium    | 0.000         | 0.217        | <b>0.250</b> | <b>86.8</b>      | 0.003          | 0.003            | <b>0.00</b> |
| Silver *    | 0.00000       | 0.039        | <b>0.050</b> | <b>78.0</b>      | 0.00005        | 0.00005          | <b>0.00</b> |
| Sodium *    | 0.0           | 70.4         | <b>50.0</b>  | <b>141</b>       | 32.7           | 32.5             | <b>0.61</b> |
| Zinc        | 0.000         | 0.044        | <b>0.050</b> | <b>88.0</b>      | 0.006          | 0.006            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 802.052     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum    | 5.43       | 5.00       | <b>109</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic     | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron       | 5.4        | 5.0        | <b>108</b>  | 90-110 %         | 0.1          | 0.1             |
| Cadmium     | 0.046      | 0.050      | <b>92.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium     | 4.5        | 5.0        | <b>90.0</b> | 90-110 %         | <0.5         | 0.5             |
| Chromium *  | 0.042      | 0.050      | <b>84.0</b> | 90-110 %         | <0.001       | 0.001           |
| Copper      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron        | 4.91       | 5.00       | <b>98.2</b> | 90-110 %         | <0.05        | 0.05            |
| Lead        | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium   | 4.6        | 5.000      | <b>92.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese * | 2.78       | 2.50       | <b>111</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium   | 9.6        | 10.0       | <b>96.0</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium    | 0.244      | 0.250      | <b>97.6</b> | 90-110 %         | <0.001       | 0.001           |
| Silver      | 0.045      | 0.050      | <b>90.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium      | 7.9        | 8.1        | <b>97.5</b> | 90-110 %         | <0.5         | 0.5             |
| Zinc        | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.



# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 802-052     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 3.76         | <b>4.00</b>   | <b>94.0</b>      | 6.00           | 5.61             | <b>6.72</b> |
| Manganese-T | 0.000         | 1.97         | <b>2.00</b>   | <b>98.5</b>      | 1.280          | 1.270            | <b>0.78</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 802-052     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.21       | 5.00       | <b>104</b>  | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.73       | 2.50       | <b>109</b>  | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.0017     | 0.002      | <b>85.0</b> | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 802-052         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 102          | <b>100</b>  | <b>102</b>       | 104            | 100              | <b>3.92</b> |
| Chloride        | 0             | 110          | <b>100</b>  | <b>110</b>       | <10            | <10              | <b>NC</b>   |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | NA             | NA               | <b>NC</b>   |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90.0</b>      | 0.5            | 0.5              | <b>0.00</b> |
| Nitrate/Nitrite | 0.10          | 1.79         | <b>1.82</b> | <b>92.9</b>      | <0.02          | <0.02            | <b>NC</b>   |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 8.76           | 8.67             | <b>1.03</b> |
| Phosphorus-T    | 0.00          | 0.23         | <b>0.25</b> | <b>92.0</b>      | 0.13           | 0.13             | <b>0.00</b> |
| Sulfate         | 0             | 52           | <b>50</b>   | <b>104</b>       | 255            | 250              | <b>1.98</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 1200           | 1180             | <b>1.68</b> |
| TSS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 102000         | 99800            | <b>2.18</b> |

NMA=Data not applicable to Method.

NA=Data not available.

NC=Not calculated due to results less than the detection limit



# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 802-052         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 176        | 186        | <b>94.6</b> | 90-110 %         | <10          | 10              |
| Chloride        | 25         | 25         | <b>101</b>  | 90-110 %         | <10          | 10              |
| EC              | 527        | 561        | <b>93.9</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.51       | 0.50       | <b>102</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.54       | 8.40       | <b>102</b>  | 90-110 %         | NMA          | NMA             |
| Phosphorus-T *  | 4.29       | 5.32       | <b>80.6</b> | 90-110 %         | <0.05        | 0.05            |
| Sulfate         | 335        | 321        | <b>104</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1180       | 1210       | <b>97.5</b> | 90-110 %         | <10          | 10              |
| TSS             | 97         | 104        | <b>93.3</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## METALS SPIKE AND DUPLICATE DATA

| LAB ID#    | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 804-076    | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum-T | 0.00          | 4.22         | <b>4.00</b>  | <b>106</b>       | 1.16           | 1.14             | <b>1.74</b> |
| Arsenic-T  | 0.0000        | 0.047        | <b>0.050</b> | <b>94.0</b>      | <0.0005        | <0.0005          | <b>NC</b>   |
| Barium-T   | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.173          | 0.156            | <b>10.3</b> |
| Boron-D    | 0.3           | 2.7          | <b>2.0</b>   | <b>120</b>       | 0.3            | 0.3              | <b>0.00</b> |
| Cadmium-D  | 0.00000       | 0.045        | <b>0.050</b> | <b>90.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Chromium-D | 0.000         | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.002          | 0.002            | <b>0.00</b> |
| Cobalt-D   | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0028         | 0.0027           | <b>6.92</b> |
| Copper-D   | 0.0000        | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.148          | 0.121            | <b>20.1</b> |
| Lead-D     | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.0001         | 0.0001           | <b>0.00</b> |
| Mercury-T  | 0.000         | 0.002        | <b>0.002</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |
| Selenium-T | 0.000         | 0.250        | <b>0.230</b> | <b>109</b>       | 0.069          | 0.067            | <b>2.94</b> |
| Vanadium-D | 0.0000        | 0.048        | <b>0.050</b> | <b>96.0</b>      | <0.0005        | <0.0005          | <b>NC</b>   |
| Zinc-D     | 0.000         | 0.043        | <b>0.050</b> | <b>86.0</b>      | 0.004          | 0.004            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

## METALS SRM AND BLANK DATA

| LAB ID#    | SRM Data   |            |             |                  | Blank Data   |                 |
|------------|------------|------------|-------------|------------------|--------------|-----------------|
| 804-076    | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum-T | 5.11       | 5.00       | <b>102</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic-T  | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium-T   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron-D    | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium-D  | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Chromium-D | 0.054      | 0.050      | <b>108</b>  | 90-110 %         | <0.001       | 0.001           |
| Cobalt-D   | 0.054      | 0.050      | <b>108</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Copper-D   | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Lead-D     | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Mercury-T  | 0.002      | 0.002      | <b>100</b>  | 90-110 %         | <0.005       | 0.005           |
| Selenium-T | 0.241      | 0.250      | <b>96.4</b> | 90-110 %         | <0.001       | 0.001           |
| Vanadium-D | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Zinc-D     | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.



# Green Analytical Laboratories

## METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 805-056     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum-T  | 0.00          | 4.27         | <b>4.00</b>   | <b>107</b>       | 0.60           | 0.50             | <b>18.2</b> |
| Arsenic-T * | 0.0000        | 3.18         | <b>4.00</b>   | <b>79.5</b>      | 0.0016         | 0.0016           | <b>0.00</b> |
| Barium-T    | 0.0007        | 1.78         | <b>2.00</b>   | <b>89.0</b>      | 0.046          | 0.046            | <b>0.00</b> |
| Boron-D     | 0.3           | 2.1          | <b>2.0</b>    | <b>90.0</b>      | 0.4            | 0.4              | <b>0.00</b> |
| Cadmium-D   | 0.00000       | 0.049        | <b>0.050</b>  | <b>98.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Chromium-D  | 0.000         | 0.049        | <b>0.050</b>  | <b>98.0</b>      | 0.002          | 0.002            | <b>0.00</b> |
| Cobalt-D    | 0.0000        | 0.051        | <b>0.050</b>  | <b>102</b>       | 0.0001         | 0.0001           | <b>0.00</b> |
| Copper-D    | 0.0000        | 0.048        | <b>0.050</b>  | <b>96.0</b>      | 0.001          | 0.001            | <b>0.00</b> |
| Lead-D      | 0.0000        | 0.050        | <b>0.050</b>  | <b>100</b>       | <0.0001        | <0.0001          | <b>NC</b>   |
| Mercury-T   | 0.000         | 0.0023       | <b>0.0020</b> | <b>115</b>       | <0.0002        | <0.0002          | <b>NC</b>   |
| Selenium-T  | 0.001         | 2.98         | <b>3.00</b>   | <b>99.3</b>      | 0.001          | 0.001            | <b>0.00</b> |
| Vanadium-D  | 0.0000        | 0.052        | <b>0.050</b>  | <b>104</b>       | 0.0020         | 0.0020           | <b>0.00</b> |
| Zinc-D      | 0.000         | 0.046        | <b>0.050</b>  | <b>92.0</b>      | 0.002          | 0.002            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

## METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 805-056     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum-T  | 5.12       | 5.00       | <b>102</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic-T   | 0.054      | 0.050      | <b>108</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium-T    | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | 0.0007       | 0.0005          |
| Boron-D     | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium-D   | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Chromium-D  | 0.054      | 0.050      | <b>108</b>  | 90-110 %         | <0.001       | 0.001           |
| Cobalt-D    | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Copper-D    | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Lead-D      | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Mercury-T * | 0.0017     | 0.0020     | <b>85.0</b> | 90-110 %         | <0.005       | 0.005           |
| Selenium-T  | 0.260      | 0.250      | <b>104</b>  | 90-110 %         | 0.001        | 0.001           |
| Vanadium-D  | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Zinc-D      | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#   | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 807-116   | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum  | 0.00          | 2.04         | <b>2.00</b>  | <b>102</b>       | <0.10          | <0.10            | <b>NC</b>   |
| Arsenic   | 0.0000        | 0.047        | <b>0.050</b> | <b>94.0</b>      | 0.0013         | 0.0013           | <b>0.00</b> |
| Barium    | 0.0000        | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.0198         | 0.0198           | <b>0.00</b> |
| Boron     | 0.0           | 2.0          | <b>2.0</b>   | <b>100</b>       | <0.1           | <0.1             | <b>NC</b>   |
| Cadmium   | 0.00000       | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.00030        | 0.00030          | <b>0.00</b> |
| Calcium   | 0.0           | 5.7          | <b>5.0</b>   | <b>114</b>       | 48.2           | 48.0             | <b>0.42</b> |
| Chromium  | 0.000         | 0.048        | <b>0.050</b> | <b>96.0</b>      | <0.001         | <0.001           | <b>NC</b>   |
| Copper    | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.170          | 0.170            | <b>0.00</b> |
| Iron      | 0.00          | 1.16         | <b>1.00</b>  | <b>116</b>       | 0.30           | 0.29             | <b>3.39</b> |
| Lead      | 0.0000        | 0.047        | <b>0.050</b> | <b>94.0</b>      | 0.0013         | 0.0013           | <b>0.00</b> |
| Magnesium | 0.0           | 1.2          | <b>1.0</b>   | <b>115</b>       | 4.6            | 4.6              | <b>0.00</b> |
| Manganese | 0.000         | 1.07         | <b>1.00</b>  | <b>107</b>       | 0.007          | 0.007            | <b>0.00</b> |
| Potassium | 0.0           | 1.0          | <b>1.0</b>   | <b>100</b>       | 6.1            | 6.1              | <b>0.00</b> |
| Selenium  | 0.000         | 0.234        | <b>0.250</b> | <b>93.6</b>      | 0.001          | 0.001            | <b>0.00</b> |
| Silver    | 0.00000       | 0.049        | <b>0.050</b> | <b>98.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium    | 0.0           | 58.4         | <b>50.0</b>  | <b>117</b>       | 112            | 111              | <b>0.90</b> |
| Zinc      | 0.000         | 0.042        | <b>0.050</b> | <b>84.0</b>      | 0.113          | 0.108            | <b>4.52</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 807-116   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum  | 5.09       | 5.00       | <b>102</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.46       | 5.00       | <b>109</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.61       | 2.50       | <b>104</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.4       | 10.0       | <b>104</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.239      | 0.250      | <b>95.6</b> | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.9        | 8.1        | <b>110</b>  | 90-110 %         | <0.5         | 0.5             |
| Zinc *    | 0.043      | 0.050      | <b>86.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 807-116     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 4.38         | <b>4.00</b>   | <b>110</b>       | 0.20           | 0.20             | <b>0.00</b> |
| Manganese-T | 0.000         | 2.11         | <b>2.00</b>   | <b>106</b>       | 2.55           | 2.48             | <b>2.78</b> |
| Mercury-T   | 0.0000        | 0.0021       | <b>0.0020</b> | <b>105</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |            |                  | Blank Data   |                 |
|-------------|------------|------------|------------|------------------|--------------|-----------------|
| 807-116     | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.46       | 5.00       | <b>109</b> | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.61       | 2.50       | <b>104</b> | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | <b>100</b> | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.



# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 807-116         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 100          | <b>100</b>  | <b>100</b>       | 212            | 210              | <b>0.95</b> |
| Chloride        | 0             | 101          | <b>100</b>  | <b>101</b>       | <10            | <10              | <b>NC</b>   |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 723            | 721              | <b>0.28</b> |
| Fluoride        | 0.0           | 1.0          | <b>1.0</b>  | <b>100</b>       | <0.2           | <0.2             | <b>NC</b>   |
| Nitrate/Nitrite | 0.00          | 0.11         | <b>0.10</b> | <b>110</b>       | 0.49           | 0.49             | <b>0.00</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 7.49           | 7.47             | <b>0.27</b> |
| Phosphorus-T    | 0.00          | 0.28         | <b>0.25</b> | <b>112</b>       | 0.09           | 0.08             | <b>11.8</b> |
| Sulfate         | 0             | 50           | <b>50</b>   | <b>100</b>       | 146            | 138              | <b>5.63</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 500            | 480              | <b>4.08</b> |
| TSS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | NA             | NA               | <b>NA</b>   |

NMA=Data not applicable to Method.

NA=Data not available.

NC=Not calculated due to results less than the detection limit

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 807-116         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 362        | 339        | <b>107</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 25         | 23         | <b>110</b>  | 90-110 %         | <10          | 10              |
| EC              | 814        | 829        | <b>98.2</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.50       | 0.50       | <b>100</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 9.09       | 9.29       | <b>97.8</b> | 90-110 %         | NMA          | NMA             |
| Phosphorus-T    | 0.22       | 0.20       | <b>110</b>  | 90-110 %         | <0.05        | 0.05            |
| Sulfate         | 325        | 321        | <b>101</b>  | 90-110 %         | <10          | 10              |
| TDS             | 5050       | 4850       | <b>104</b>  | 90-110 %         | <10          | 10              |
| TSS             | 102        | 110        | <b>92.7</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 808-067     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum    | 0.00          | 2.37         | <b>2.00</b>  | <b>119</b>       | <0.1           | <0.1             | <b>NC</b>   |
| Arsenic     | 0.0000        | 0.056        | <b>0.050</b> | <b>112</b>       | 0.0041         | 0.0040           | <b>2.47</b> |
| Barium      | 0.0000        | 0.054        | <b>0.050</b> | <b>108</b>       | 0.0977         | 0.0945           | <b>3.33</b> |
| Boron       | 0.0           | 2.3          | <b>2.00</b>  | <b>117</b>       | 0.1            | 0.1              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.056        | <b>0.050</b> | <b>112</b>       | 0.00106        | 0.00100          | <b>5.83</b> |
| Calcium     | 0.0           | 5.8          | <b>5.0</b>   | <b>116</b>       | 120.0          | 120.0            | <b>0.00</b> |
| Chromium    | 0.000         | 0.058        | <b>0.050</b> | <b>116</b>       | <0.001         | <0.001           | <b>NC</b>   |
| Cobalt      | 0.00000       | 0.056        | <b>0.050</b> | <b>112</b>       | 0.00079        | 0.00078          | <b>1.27</b> |
| Copper      | 0.0000        | 0.056        | <b>0.050</b> | <b>112</b>       | 0.0068         | 0.0063           | <b>7.63</b> |
| Iron        | 0.00          | 1.17         | <b>1.00</b>  | <b>117</b>       | 0.09           | 0.09             | <b>0.00</b> |
| Lead        | 0.0000        | 0.054        | <b>0.050</b> | <b>108</b>       | 0.0015         | 0.0015           | <b>0.00</b> |
| Magnesium   | 0.0           | 1.2          | <b>1.00</b>  | <b>120</b>       | 14.8           | 14.7             | <b>0.68</b> |
| Manganese * | 0.000         | 1.23         | <b>1.00</b>  | <b>123</b>       | 0.009          | 0.009            | <b>0.00</b> |
| Potassium   | 0.0           | 1.1          | <b>1.00</b>  | <b>110</b>       | 10.8           | 10.8             | <b>0.00</b> |
| Selenium    | 0.000         | 0.286        | <b>0.250</b> | <b>114</b>       | 0.001          | 0.001            | <b>0.00</b> |
| Silver      | 0.00000       | 0.059        | <b>0.050</b> | <b>118</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium      | 0.0           | 59.7         | <b>50.0</b>  | <b>119</b>       | 55.1           | 54.9             | <b>0.36</b> |
| Vanadium    | 0.0000        | 0.055        | <b>0.050</b> | <b>110</b>       | 0.0037         | 0.0037           | <b>0.00</b> |
| Zinc        | 0.000         | 0.056        | <b>0.050</b> | <b>112</b>       | 0.009          | 0.009            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit

NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 808-067   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum  | 5.19       | 5.00       | <b>104</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic   | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |
| Cobalt    | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Copper    | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.37       | 5.00       | <b>107</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.68       | 2.50       | <b>107</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.3       | 10.0       | <b>103</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.239      | 0.250      | <b>95.6</b> | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.7        | 8.1        | <b>107</b>  | 90-110 %         | <0.5         | 0.5             |
| Vanadium  | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Zinc      | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 808-067     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum-T  | 0.00          | 4.34         | <b>4.00</b>   | <b>109</b>       | 3.99           | 3.63             | <b>9.45</b> |
| Arsenic-T   | 0.00          | 0.05         | <b>0.05</b>   | <b>106</b>       | 0.002          | 0.002            | <b>0.00</b> |
| Barium-T    | 0.00          | 0.05         | <b>0.05</b>   | <b>98.0</b>      | 130            | 127              | <b>2.33</b> |
| Boron-T     | 0.00          | 4.40         | <b>4.00</b>   | <b>110</b>       | 0.20           | 0.20             | <b>0.00</b> |
| Iron-T      | 0.00          | 3.94         | <b>4.00</b>   | <b>98.5</b>      | 7.07           | 7.00             | <b>1.00</b> |
| Manganese-T | 0.000         | 2.05         | <b>2.00</b>   | <b>103</b>       | 4.35           | 4.30             | <b>1.16</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |
| Selenium-T  | 0.000         | 0.255        | <b>0.250</b>  | <b>102</b>       | <0.001         | <0.001           | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 808-067     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum-T  | 5.17       | 5.00       | <b>103</b>  | 90-110 %         | <0.05        | 0.05            |
| Arsenic-T   | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.05        | 0.05            |
| Barium-T    | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.05        | 0.05            |
| Boron-T     | 5.30       | 5.00       | <b>106</b>  | 90-110 %         | <0.05        | 0.05            |
| Iron-T      | 5.08       | 5.00       | <b>102</b>  | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.65       | 2.50       | <b>106</b>  | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | <b>100</b>  | 90-110 %         | <0.0002      | 0.0002          |
| Selenium-t  | 0.245      | 0.250      | <b>98.0</b> | 90-110 %         | <0.005       | 0.005           |

NA=Data not available.



# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 808-067         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 106          | <b>100</b>  | <b>106</b>       | 182            | 180              | <b>1.10</b> |
| Chloride        | 0             | 105          | <b>100</b>  | <b>105</b>       | 29             | 27               | <b>7.14</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | NA             | NA               | <b>NA</b>   |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90.0</b>      | <0.2           | <0.2             | <b>NC</b>   |
| Nitrate/Nitrite | 0.00          | 0.11         | <b>0.10</b> | <b>110</b>       | 0.49           | 0.49             | <b>0.00</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 6.85           | 6.83             | <b>0.29</b> |
| Phosphorus-T    | 0.00          | 0.24         | <b>0.25</b> | <b>96.0</b>      | 0.21           | 0.20             | <b>4.88</b> |
| Sulfate         | 0             | 55           | <b>50</b>   | <b>110</b>       | 840            | 820              | <b>2.41</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 240            | 225              | <b>6.45</b> |
| TSS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 1250000        | 1200000          | <b>4.08</b> |

NMA=Data not applicable to Method.

NA=Data not available.

NC=Not calculated due to results less than the detection limit

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 808-067         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 360        | 339        | <b>106</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 23         | 23         | <b>101</b>  | 90-110 %         | <10          | 10              |
| EC *            | NA         | NA         | <b>NA</b>   | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.48       | 0.50       | <b>96.0</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 9.03       | 8.90       | <b>101</b>  | 90-110 %         | NMA          | NMA             |
| Phosphorus-T    | 4.75       | 5.32       | <b>89.3</b> | 90-110 %         | <0.05        | 0.05            |
| Sulfate         | 350        | 321        | <b>109</b>  | 90-110 %         | <10          | 10              |
| TDS             | 5040       | 4850       | <b>104</b>  | 90-110 %         | <10          | 10              |
| TSS             | 102        | 110        | <b>92.7</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#   | Spike Data    |              |                |                  | Duplicate Data |                  |             |
|-----------|---------------|--------------|----------------|------------------|----------------|------------------|-------------|
| 904-012   | Sample Result | Spike Result | Spike Conc.    | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum  | 0.00          | 2.00         | <b>2.0000</b>  | <b>100</b>       | <0.10          | <0.10            | <b>NC</b>   |
| Arsenic   | 0.0000        | 0.0490       | <b>0.0500</b>  | <b>98.0</b>      | 0.0018         | 0.0017           | <b>5.71</b> |
| Barium    | 0.0000        | 0.0500       | <b>0.0500</b>  | <b>100</b>       | 0.1011         | 0.0973           | <b>3.83</b> |
| Boron     | 0.0           | 2.1          | <b>2.00</b>    | <b>105</b>       | 0.2            | 0.2              | <b>0.00</b> |
| Cadmium   | 0.00000       | 0.05200      | <b>0.05200</b> | <b>100</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium   | 0.0           | 24.8         | <b>25.00</b>   | <b>99.2</b>      | 6.5            | 6.1              | <b>6.35</b> |
| Chromium  | 0.000         | 0.047        | <b>0.050</b>   | <b>94.0</b>      | 0.011          | 0.011            | <b>0.00</b> |
| Cobalt    | 0.00000       | 0.04800      | <b>0.05000</b> | <b>96.0</b>      | 0.00024        | 0.00023          | <b>4.26</b> |
| Copper    | 0.0000        | 0.0450       | <b>0.0500</b>  | <b>90.0</b>      | 0.4630         | 0.4490           | <b>3.07</b> |
| Iron      | 0.00          | 5.00         | <b>5.00</b>    | <b>100</b>       |                |                  | <b>NC</b>   |
| Lead      | 0.0000        | 0.0480       | <b>0.0500</b>  | <b>96.0</b>      | 0.0003         | 0.0003           | <b>0.00</b> |
| Magnesium | 0.0           | 4.9          | <b>5.00</b>    | <b>98.0</b>      | 1.1            | 1.1              | <b>0.00</b> |
| Manganese | 0.00000       | 1.10000      | <b>1.00000</b> | <b>110</b>       | 0.03400        | 0.03400          | <b>0.00</b> |
| Potassium | 0.0           | 4.9          | <b>5.00</b>    | <b>98.0</b>      | 4.5            | 4.3              | <b>4.55</b> |
| Selenium  | 0.000         | 0.241        | <b>0.250</b>   | <b>96.4</b>      | 0.017          | 0.016            | <b>6.06</b> |
| Silver    | 0.00000       | 0.04900      | <b>0.05000</b> | <b>98.0</b>      |                |                  | <b>NC</b>   |
| Sodium    | 0.0           | 249.0        | <b>250.00</b>  | <b>99.6</b>      | 603.0          | 567.0            | <b>6.15</b> |
| Vanadium  | 0.00000       | 0.04600      | <b>0.05000</b> | <b>92.0</b>      | 0.00310        | 0.00290          | <b>6.67</b> |
| Zinc      | 0.000         | 0.047        | <b>0.050</b>   | <b>94.0</b>      | 0.009          | 0.009            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 904-012   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum  | 5.20       | 5.00       | <b>104</b>  | 90-110 %         | <0.10        | 0.10            |
| Arsenic   | 0.0500     | 0.0500     | <b>100</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.0540     | 0.0500     | <b>108</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.05200    | 0.05000    | <b>104</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.001       | 0.001           |
| Cobalt    | 0.05000    | 0.05000    | <b>100</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Copper    | 0.0480     | 0.0500     | <b>96.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.30       | 5          | <b>106</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.0520     | 0.0500     | <b>104</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 4.9        | 5.0        | <b>98.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.700      | 2.500      | <b>108</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.1       | 10.0       | <b>101</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.256      | .25        | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.04700    | 0.05000    | <b>94.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.3        | 8.1        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Vanadium  | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.005       | 0.005           |
| Zinc      | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.



# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 904-012     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Aluminum-T  | 0.00          | 3.72         | <b>4.00</b>  | <b>93.0</b>      | 0.28           | 0.26             | <b>7.41</b> |
| Arsenic-T   | 0.000         | 0.047        | <b>0.050</b> | <b>94.0</b>      | 0.003          | 0.003            | <b>6.90</b> |
| Barium-T    | 0.000         | 0.051        | <b>0.050</b> | <b>102</b>       | 0.272          | 0.252            | <b>7.63</b> |
| Iron-T      | 0.05          | 3.60         | <b>4.00</b>  | <b>88.8</b>      | 1.91           | 1.90             | <b>0.52</b> |
| Manganese-T | 0.00          | 1.90         | <b>2.00</b>  | <b>95.0</b>      | 0.29           | 0.24             | <b>18.9</b> |
| Mercury-T   | 0.000         | 0.002        | <b>0.002</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |
| Selenium-T  | 0.000         | 8.310        | <b>8.00</b>  | <b>104</b>       | <0.001         | <0.001           | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |            |                  | Blank Data   |                 |
|-------------|------------|------------|------------|------------------|--------------|-----------------|
| 904-012     | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Aluminum-T  | 5.16       | 5.00       | <b>103</b> | 90-110 %         | <0.005       | 0.005           |
| Arsenic-T   | 0.055      | 0.050      | <b>110</b> | 90-110 %         | <0.005       | 0.005           |
| Barium-T    | 0.055      | 0.050      | <b>110</b> | 90-110 %         | <0.005       | 0.005           |
| Iron-T      | 5.03       | 5.00       | <b>101</b> | 90-110 %         | 0.05         | 0.05            |
| Manganese-T | 2.670      | 2.500      | <b>107</b> | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.0021     | 0.0020     | <b>105</b> | 90-110 %         | <0.005       | 0.005           |
| Selenium-T  | 7.30       | 6.70       | <b>109</b> | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 904-012         | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 105          | <b>100</b>   | <b>105</b>       | 308            | 306              | <b>0.65</b> |
| Chloride        | 0             | 100          | <b>100</b>   | <b>100</b>       | 18             | 18               | <b>0.00</b> |
| EC              | NMA           | NMA          | <b>NMA</b>   | <b>NMA</b>       | 798            | 798              | <b>0.00</b> |
| Fluoride        | 0.3           | 1.3          | <b>1.0</b>   | <b>100</b>       | 1.6            | 1.6              | <b>0.00</b> |
| Nitrate/Nitrite | 0.00          | 0.11         | <b>0.10</b>  | <b>110</b>       | 0.17           | 0.17             | <b>0.00</b> |
| pH              | NMA           | NMA          | <b>NMA</b>   | <b>NMA</b>       | 8.26           | 8.23             | <b>0.36</b> |
| Phosphorus-T    | 0.00          | 0.24         | <b>0.25</b>  | <b>96.0</b>      | 0.11           | 0.10             | <b>9.52</b> |
| Sulfate         | 0             | 52.00        | <b>50.00</b> | <b>104</b>       | 6900           | 6900             | <b>0.00</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>   | <b>NMA</b>       | 1790           | 1760             | <b>1.69</b> |
| TSS             | NMA           | NMA          | <b>NMA</b>   | <b>NMA</b>       | 11.0           | 9.7              | <b>12.6</b> |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 904-012         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 139        | 146        | <b>95.2</b> | 90-110 %         | <10          | 10              |
| Chloride        | 76         | 76         | <b>100</b>  | 90-110 %         | <10          | 10              |
| EC              | 1515       | 1470       | <b>103</b>  | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.50       | 0.50       | <b>100</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.99       | 9.19       | <b>97.8</b> | 90-110 %         | NMA          | NMA             |
| Phosphorus-T    | 0.20       | 0.20       | <b>100</b>  | 90-110 %         | <0.05        | 0.05            |
| Sulfate         | 335        | 321        | <b>104</b>  | 90-110 %         | <10          | 10              |
| TDS             | 3795       | 3770       | <b>101</b>  | 90-110 %         | <10          | 10              |
| TSS             | 123        | 133        | <b>92.5</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.



## **Appendix 18.E**

Monitoring Well and Vibrating Wire Piezometer Completion Diagrams



**NORWEST**  
Applied Hydrology

KF2007-01

COMPLETION DIAGRAM & LITHOLOGIC LOG

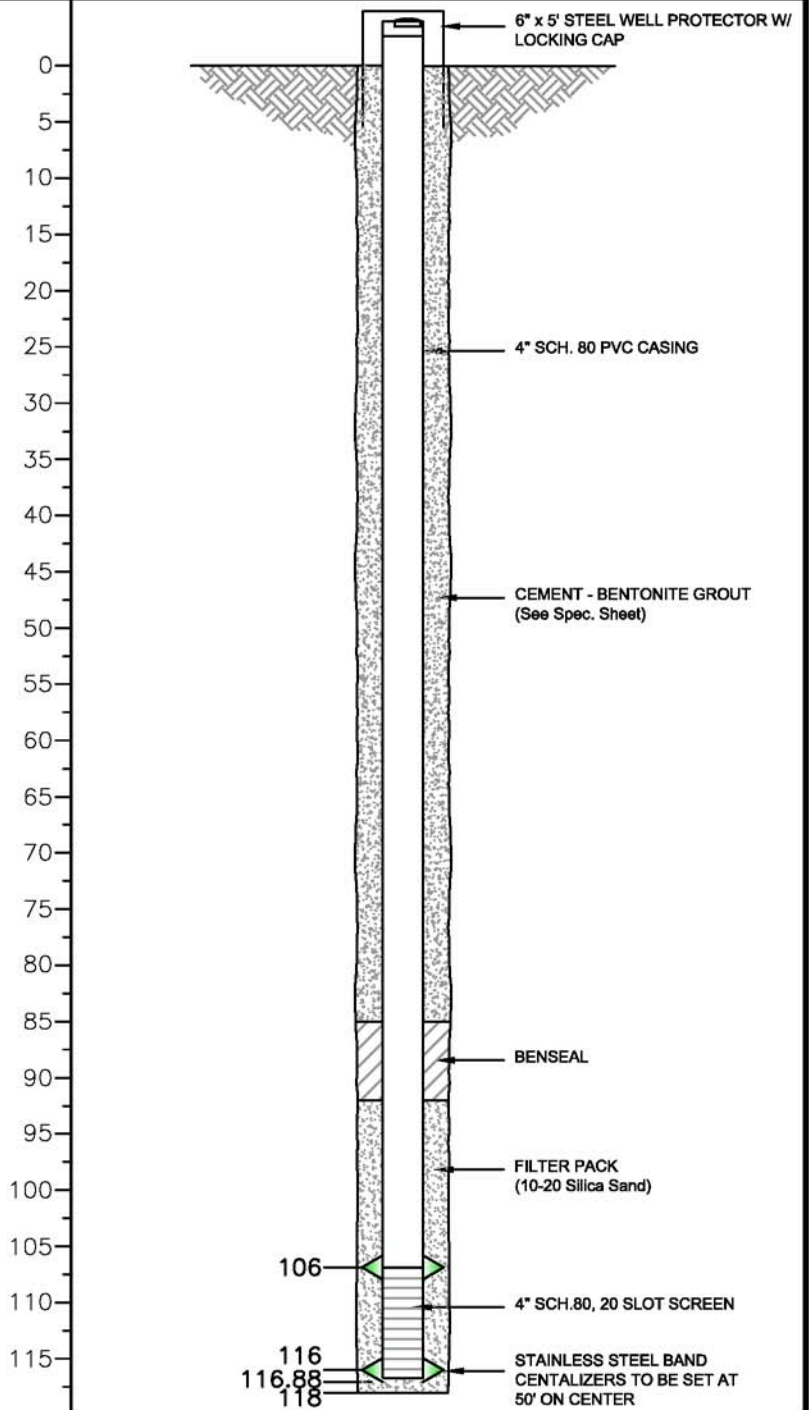
PROJECT: NAVAJO MINE EXTENSION  
 DRILLING CO: MO-TE  
 DRILLER: BOB  
 CLIENT SUPERVISOR: COLLETTE BROWN  
 GEOLOGIST/SUPERVISOR: JOEL SOBOL  
 AHA JOB#: 4010-00060-10  
 DRILLING METHOD: AIR ROTARY  
 BORING STARTED: 7/28/07

WELL TYPE: MONITOR WELL  
 WELLHEAD TYPE: PROTECTIVE HEAD COVER  
 WELL COMPLETED: 7/28/07  
 WELL DEVELOPED: 7/28/07  
 DATE SURVEYED: 8/29/07  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: 4" SCH 80 PVC  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 4"  
 CASING MATERIAL: SCH 80 PVC  
 BORING DIAMETER: 8-3/4"  
 TOP OF CASING ELEV. (FT): 5459.96  
 GROUND ELEVATION (FT): 5457.22  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1984390.9290  
 EASTING (FT): 307986.0078

LITHOLOGY LOG

|  |  |
|--|--|
|  |  |
|--|--|



COMPLETION DIAGRAM & LITHOLOGIC LOG

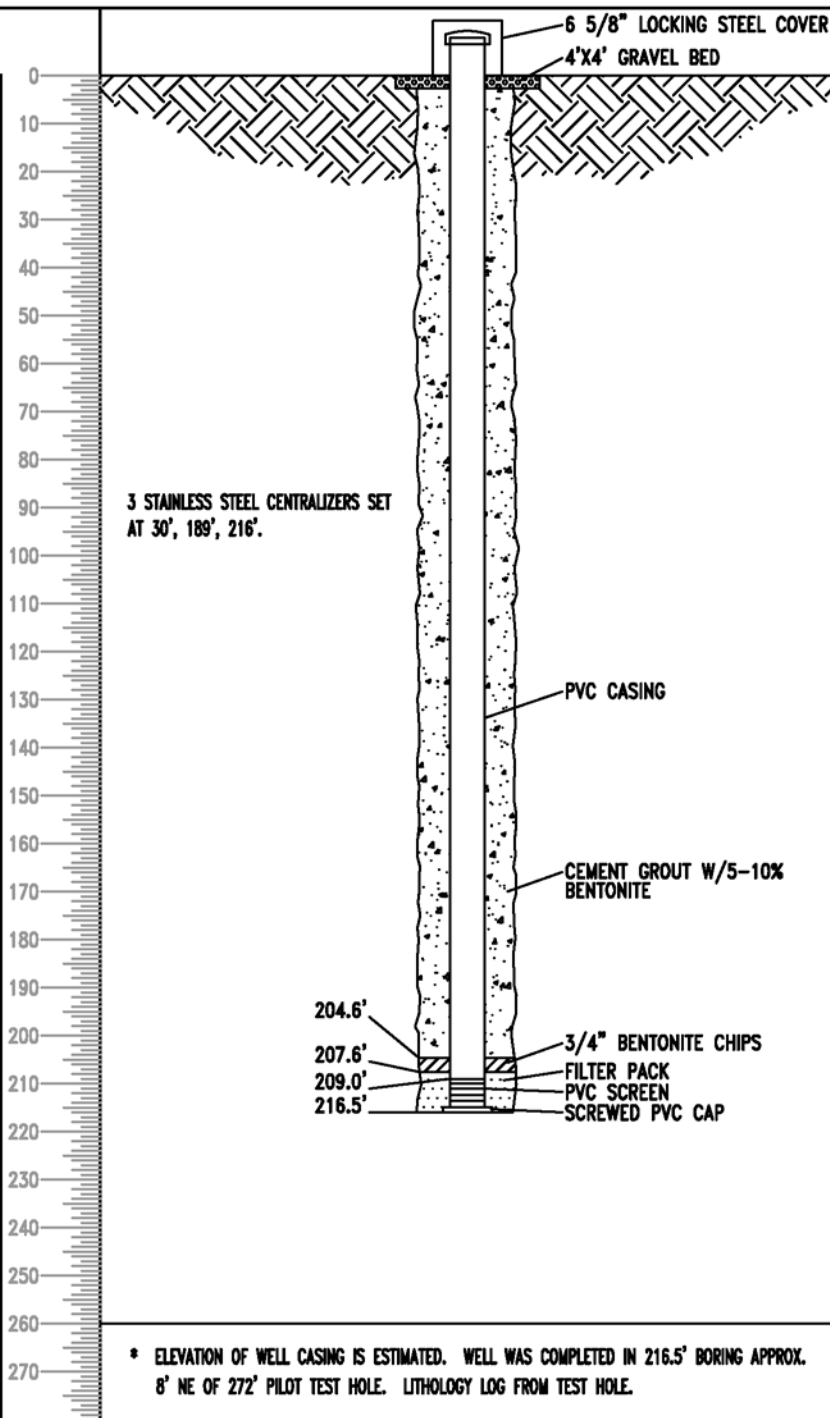
PROJECT: NO NAME  
 DRILLING CO: SHARPE DRILLING  
 DRILLER: RUSS SHARPE  
 CLIENT SUPERVISOR: RON VANVALKENBURG  
 GEOLOGIST/SUPERVISOR: IAN PEARSON  
 AHA JOB#: 43-4B  
 DRILLING METHOD: AIR ROTARY  
 BORING STARTED: 3/22/98

WELL TYPE: MONITORING  
 WELLHEAD TYPE: STICKUP (1.5')  
 WELL COMPLETED: 3/23/98  
 WELL DEVELOPED: 3/28/98  
 DATE SURVEYED: \_\_\_\_\_  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: SCH 80 PVC  
 FILTER PACK: 30-60 SAND

CASING DIAMETER: 4"  
 CASING MATERIAL: SCH 80 PVC  
 BORING DIAMETER: 7 7/8"  
 TOP OF CASING ELEV. (FT): 5507.04  
 GROUND ELEVATION (FT): 5505.89  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1,974,600.26  
 EASTING (FT): 303,887.43

LITHOLOGY LOG

|  |  |  |  |
|--|--|--|--|
|  |  |  |  |
|--|--|--|--|



\* ELEVATION OF WELL CASING IS ESTIMATED. WELL WAS COMPLETED IN 216.5' BORING APPROX. 8' NE OF 272' PILOT TEST HOLE. LITHOLOGY LOG FROM TEST HOLE.

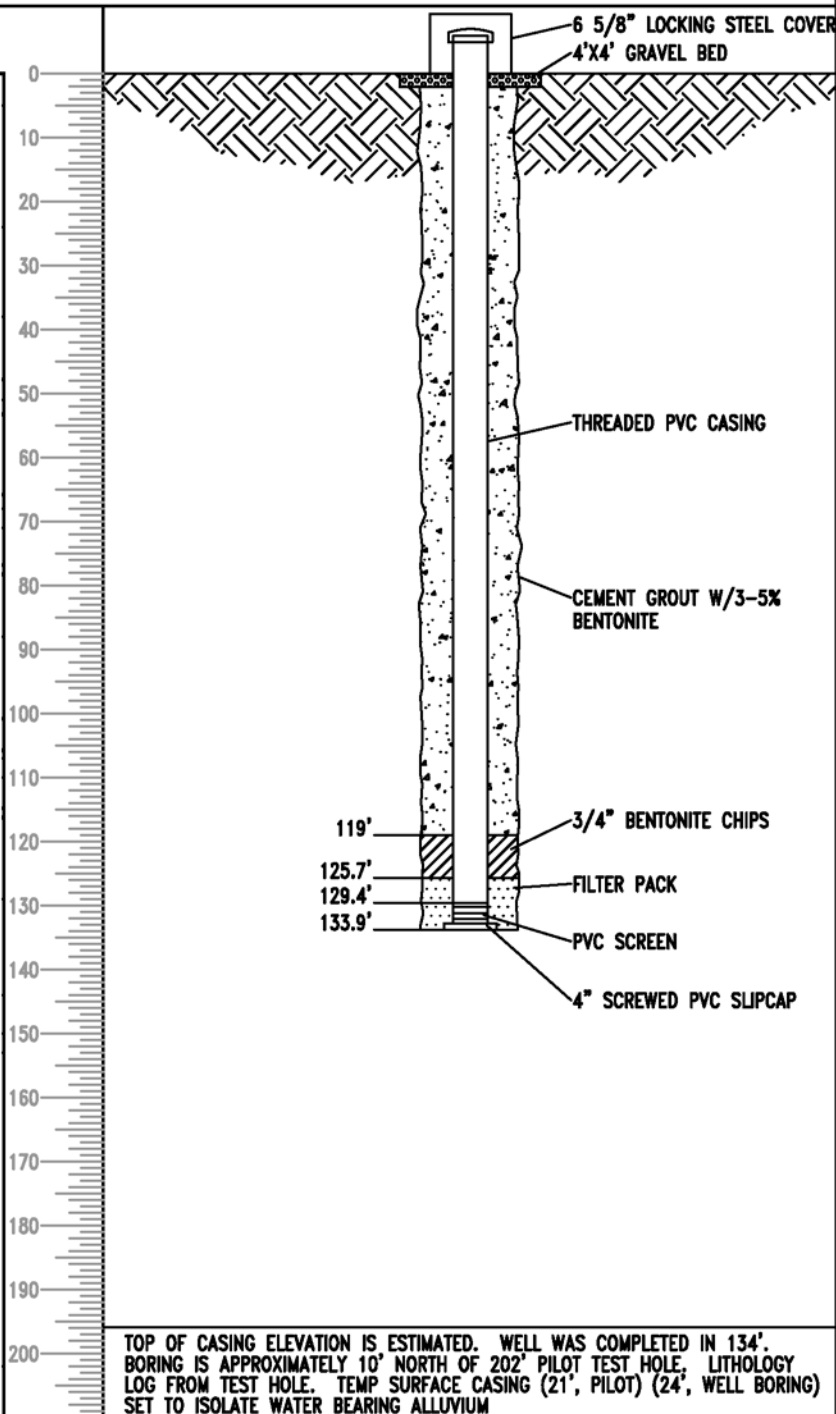
COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NO NAME  
 DRILLING CO: SHARPE DRILLING  
 DRILLER: RUSS SHARPE  
 CLIENT SUPERVISOR: RON VANVALKENBURG  
 GEOLOGIST/SUPERVISOR: IAN PEARSON  
 AHA JOB#: 43-4B  
 DRILLING METHOD: AIR ROTARY  
 BORING STARTED: 3/25/98

WELL TYPE: MONITORING  
 WELLHEAD TYPE: STICKUP (2.3')  
 WELL COMPLETED: 3/27/98  
 WELL DEVELOPED: 3/28/98  
 DATE SURVEYED: \_\_\_\_\_  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: SCH 80 PVC  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 4"  
 CASING MATERIAL: SCH 80 PVC  
 BORING DIAMETER: 7 7/8"  
 TOP OF CASING ELEV. (FT): 5425.53  
 GROUND ELEVATION (FT): 5423.45  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1,984,271.05  
 EASTING (FT): 304,599.17

LITHOLOGY LOG







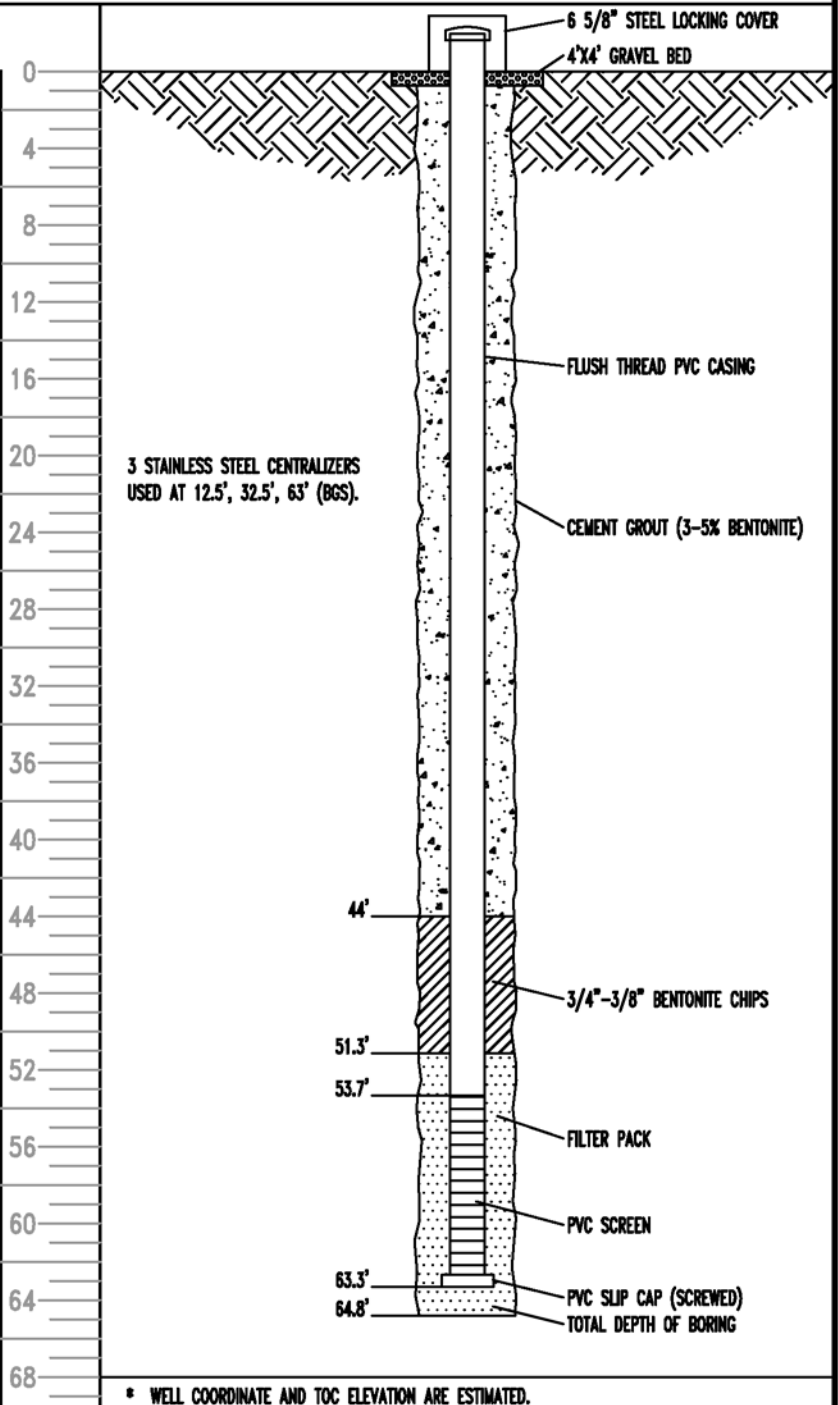
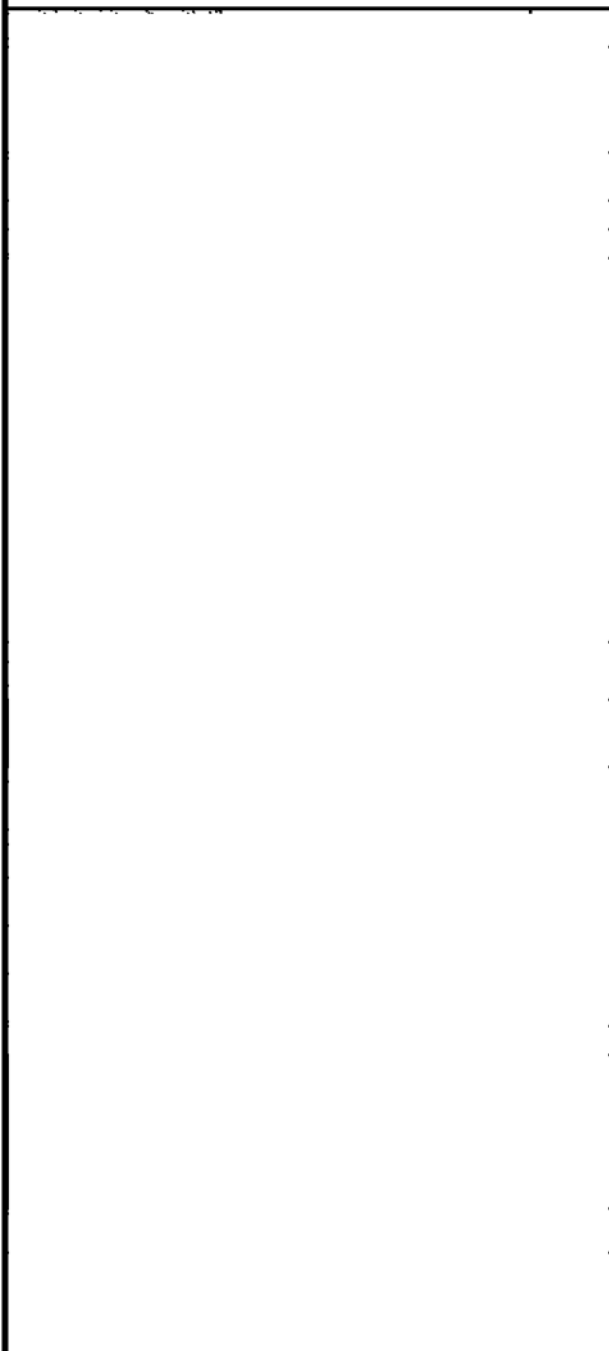
COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NO NAME  
 DRILLING CO: SHARPE DRILLING  
 DRILLER: RUSS SHARPE  
 CLIENT SUPERVISOR: RON VANVALKENBURG  
 GEOLOGIST/SUPERVISOR: IAN PEARSON  
 AHA JOB#: 43-4B  
 DRILLING METHOD: AIR ROTARY  
 BORING STARTED: 3/27/98

WELL TYPE: MONITORING  
 WELLHEAD TYPE: STICKUP (1.7')  
 WELL COMPLETED: 3/28/98  
 WELL DEVELOPED: 3/28/98  
 DATE SURVEYED: \_\_\_\_\_  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: SCH 80 PVC  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 4"  
 CASING MATERIAL: SCH 80 PVC  
 BORING DIAMETER: 7 7/8"  
 TOP OF CASING ELEV. (FT): 5353.38  
 GROUND ELEVATION (FT): 5351.81  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1,990,163.70  
 EASTING (FT): 300,368.91

LITHOLOGY LOG



\* WELL COORDINATE AND TOC ELEVATION ARE ESTIMATED.

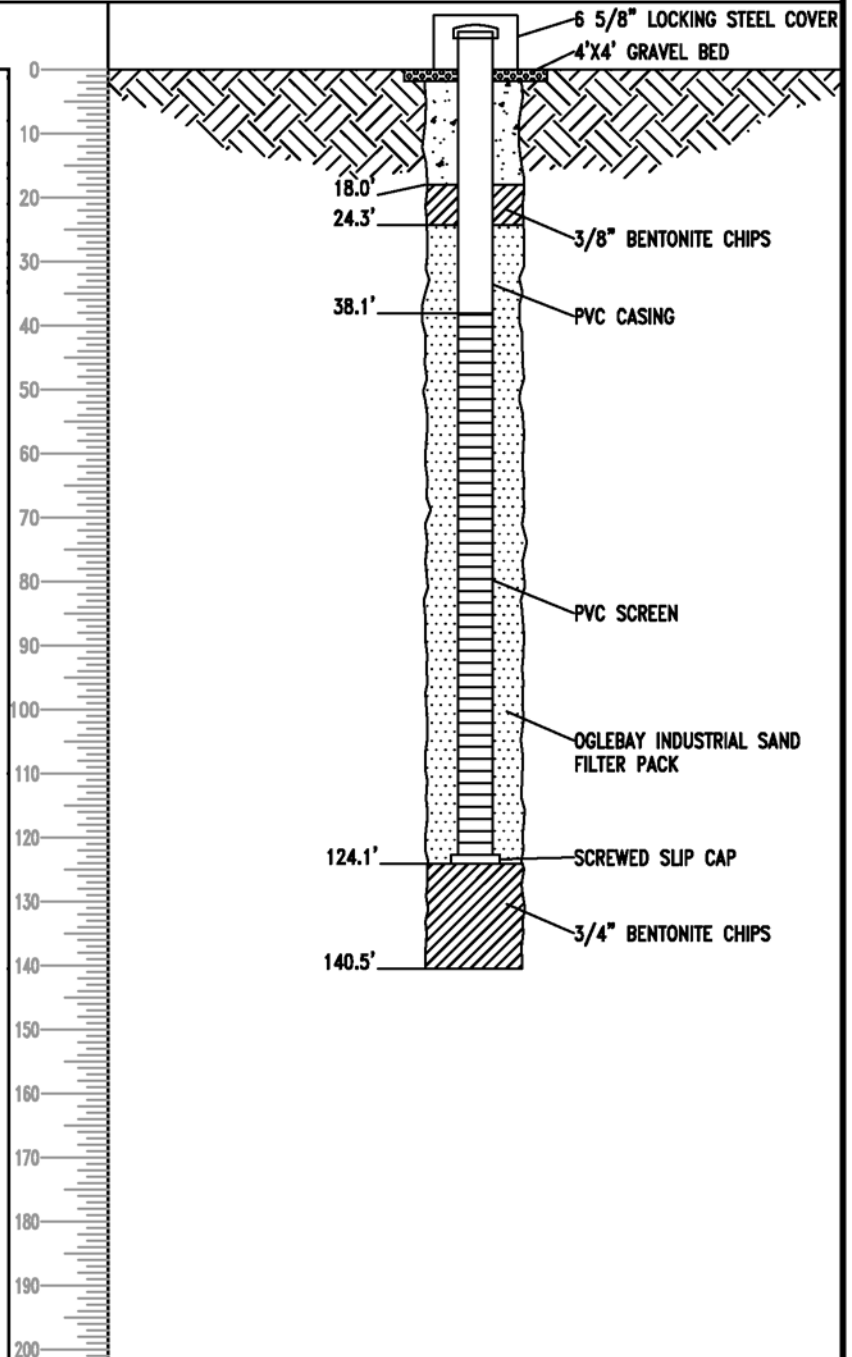
COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NO NAME  
 DRILLING CO: SHARPE DRILLING  
 DRILLER: RUSS SHARPE  
 CLIENT SUPERVISER: RON VALVALKENBURG  
 GEOLOGIST/SUPERVISOR: IAN PEARSON  
 AHA JOB#: 43-4B  
 DRILLING METHOD: AIR ROTARY  
 BORING STARTED: 3/20/98

WELL TYPE: MONITORING  
 WELLHEAD TYPE: STICKUP (1.6')  
 WELL COMPLETED: 3/21/98  
 WELL DEVELOPED: 3/28/98  
 DATE SURVEYED: \_\_\_\_\_  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: SCH 80 PVC  
 FILTER PACK: 30-60 SAND

CASING DIAMETER: 4"  
 CASING MATERIAL: SCH 80 PVC  
 BORING DIAMETER: 7 7/8"  
 TOP OF CASING ELEV. (FT): 5366.46  
 GROUND ELEVATION (FT): 5365.20  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1,993,801.95  
 EASTING (FT): 290,787.30

LITHOLOGY LOG



\* COORDINATES AND CASING ELEVATIONS ARE ESTIMATED (NOT SURVEYED)  
 NO CENTRALIZERS WERE USED

COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NAVAJO MINE EXTENSION  
 DRILLING CO: MO-TE  
 DRILLER: BOB  
 CLIENT SUPERVISOR: COLLETTE BROWN  
 GEOLOGIST/SUPERVISOR: JOEL SOBOL  
 AHA JOB#: 4010-00060-10  
 DRILLING METHOD: AIR ROTARY  
 BORING STARTED: 7/29/07

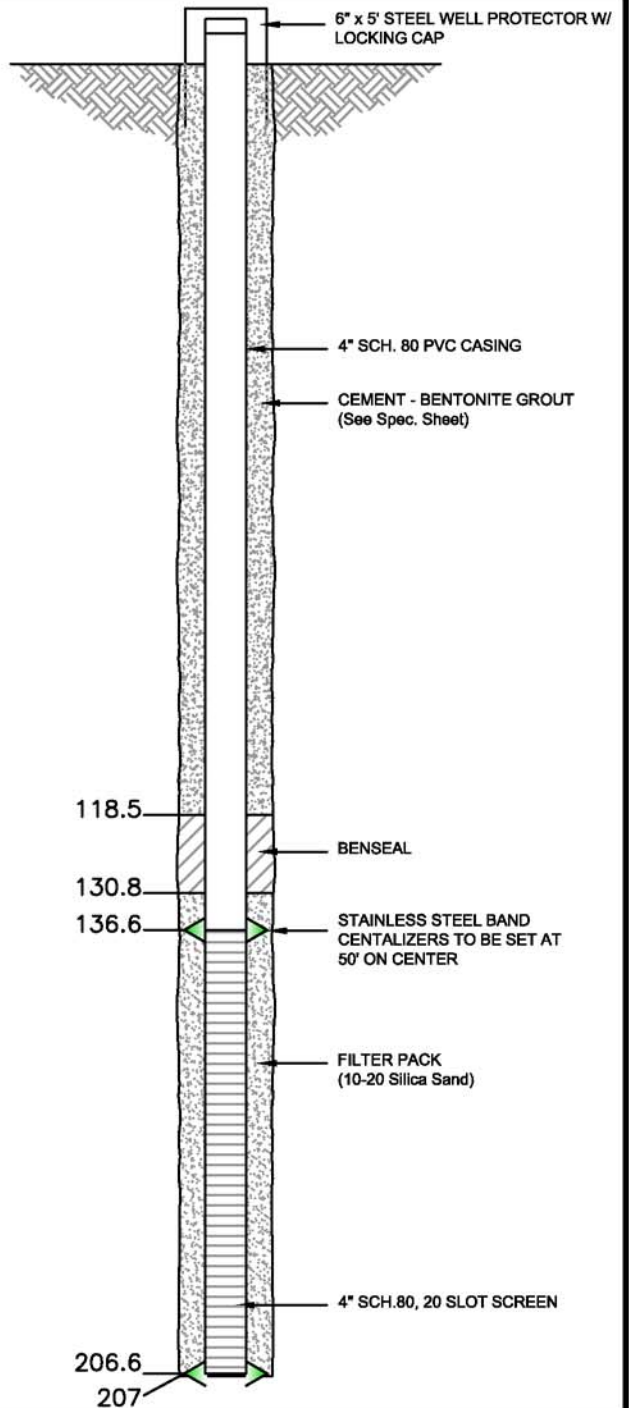
WELL TYPE: MONITORING WELL  
 WELLHEAD TYPE: PROTECTIVE HEAD COVER  
 WELL COMPLETED: 7/29/07  
 WELL DEVELOPED: 7/29/07  
 DATE SURVEYED: 8/29/07  
 SCREEN SLOT SIZE: 0.02"  
 SCREEN TYPE: 4" SCH 80 PVC MILL SLOT  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 4"  
 CASING MATERIAL: 4" SCH 80 PVC  
 BORING DIAMETER: 8-3/4"  
 TOP OF CASING ELEV. (FT): 5355.71'  
 GROUND ELEVATION (FT): 5352.97  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1995102.5555  
 EASTING (FT): 302595.6035

LITHOLOGY LOG

|  |  |
|--|--|
|  |  |
|--|--|

0  
5  
10  
15  
20  
25  
30  
35  
40  
45  
50  
55  
60  
65  
70  
75  
80  
85  
90  
95  
100  
105  
110  
115  
120  
125  
130  
135  
140  
145  
150  
155  
160  
165  
170  
175  
180  
185  
190  
195  
200  
205







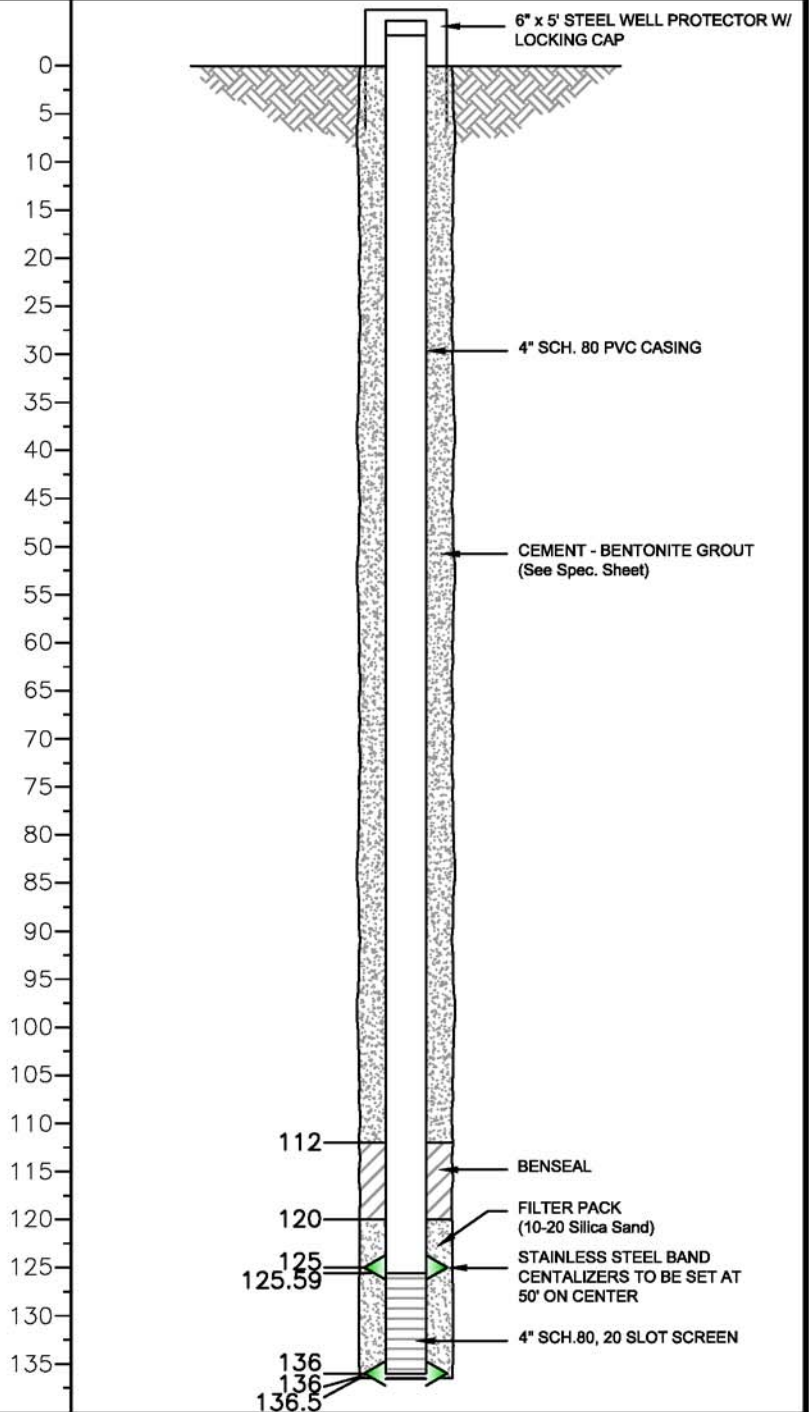
COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NAVAJO MINE EXTENSION  
 DRILLING CO: MO-TE  
 DRILLER: BOB  
 CLIENT SUPERVISOR: COLLETTE BROWN  
 GEOLOGIST/SUPERVISOR: JOEL SOBOL  
 AHA JOB#: 4010-00060-10  
 DRILLING METHOD: AIR ROTARY  
 BORING STARTED: 7/24/07

WELL TYPE: MONITORING WELL  
 WELLHEAD TYPE: PROTECTIVE HEAD COVER  
 WELL COMPLETED: 8/2/07  
 WELL DEVELOPED: 8/2/07  
 DATE SURVEYED: 8/29/07  
 SCREEN SLOT SIZE: 0.02"  
 SCREEN TYPE: 4" SCH 80 PVC MILL SLOT  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 4"  
 CASING MATERIAL: 4" SCH 80 PVC  
 BORING DIAMETER: 8-3/4"  
 TOP OF CASING ELEV. (FT): 5470.23  
 GROUND ELEVATION (FT): 5467.83  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1982884.7045  
 EASTING (FT): 295091.1864

LITHOLOGY LOG



112  
120  
125  
125.59  
136  
136  
136.5

BENSEAL  
 FILTER PACK  
(10-20 Silica Sand)  
 STAINLESS STEEL BAND  
CENTALIZERS TO BE SET AT  
50' ON CENTER  
 4" SCH.80, 20 SLOT SCREEN

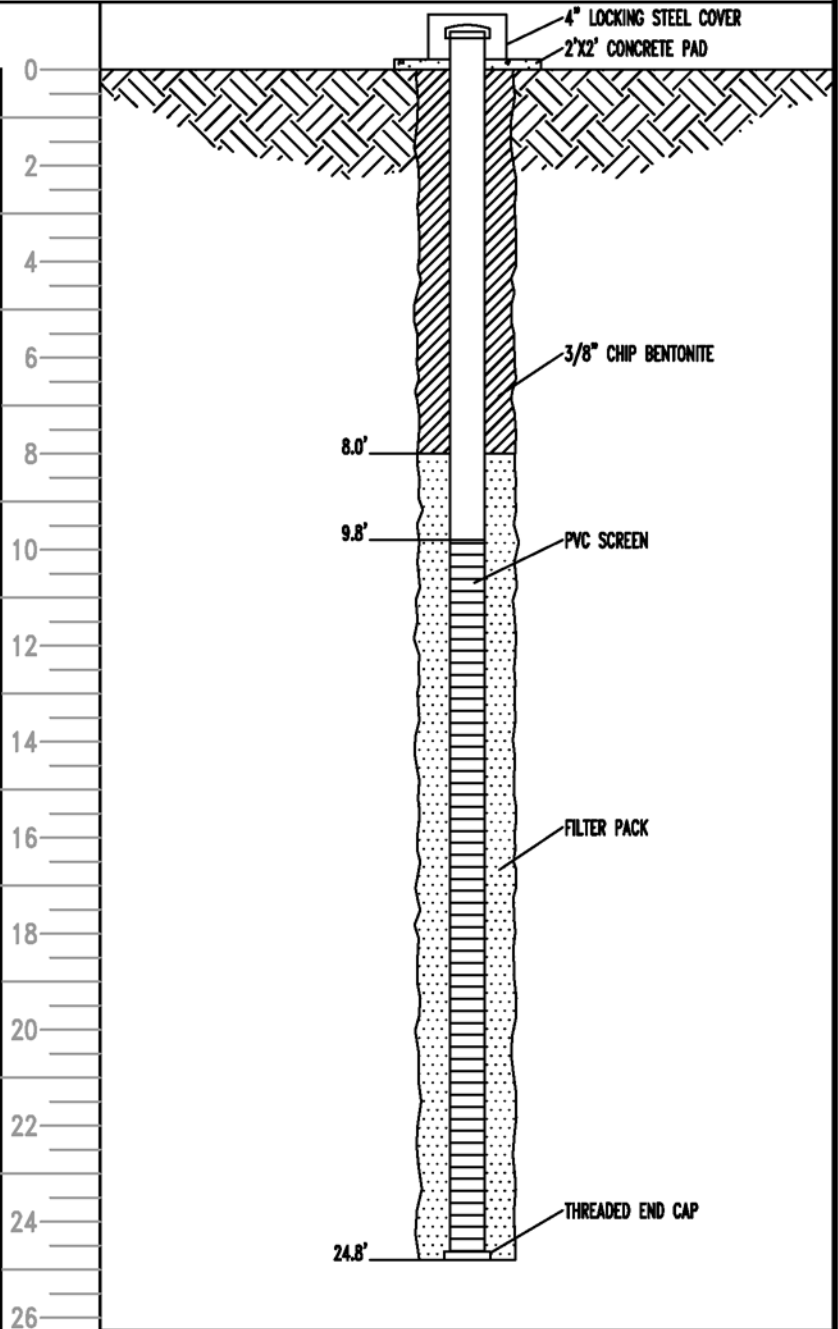
COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NO NAME  
 DRILLING CO: PHILIP SERVICES CORP  
 DRILLER: KELLY PADILLA  
 CLIENT SUPERVISOR: RON VANVALKENBURG  
 GEOLOGIST/SUPERVISOR: IAN PEARSON  
 AHA JOB#: 43-4B  
 DRILLING METHOD: HOLLOW STEM AUGER  
 BORING STARTED: 3/25/98

WELL TYPE: MONITORING  
 WELLHEAD TYPE: STICKUP (1.6')  
 WELL COMPLETED: 3/25/98  
 WELL DEVELOPED: WELL DRY  
 DATE SURVEYED: \_\_\_\_\_  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: SCH 40 PVC  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 2"  
 CASING MATERIAL: SCH 40 PVC  
 BORING DIAMETER: 7 1/2"  
 TOP OF CASING ELEV. (FT): 5431.63  
 GROUND ELEVATION (FT): 5430.46  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1,976,857.28  
 EASTING (FT): 296,773.43

LITHOLOGY LOG



\* SURVEY COORDINATES AND ELEVATION ARE ESTIMATED. WELL WAS DRY AT COMPLETION AND AS OF 3/30/98



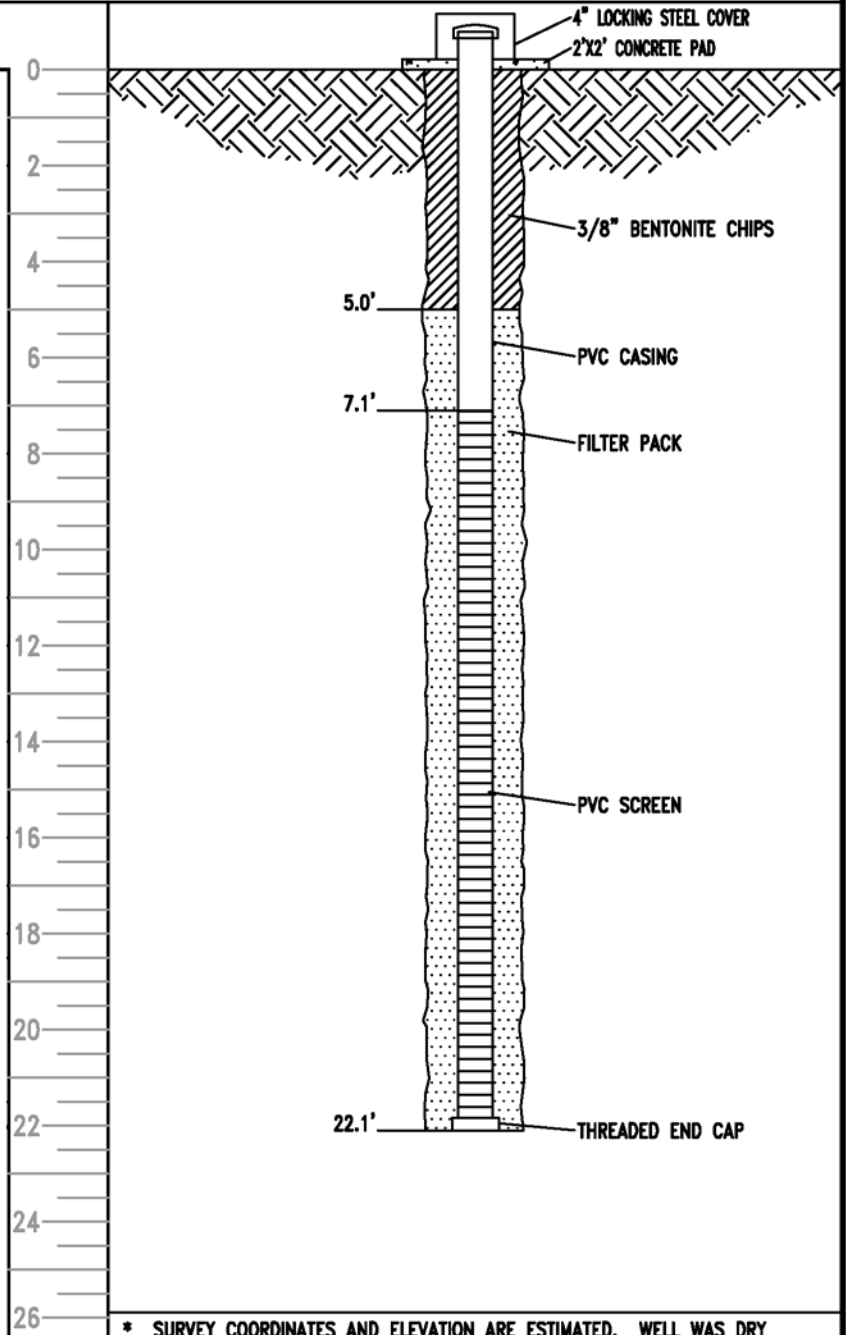
COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NO NAME  
 DRILLING CO: PHILIP SERVICES CORP  
 DRILLER: KELLY PADILLA  
 CLIENT SUPERVISOR: RON VANVALKENBURG  
 GEOLOGIST/SUPERVISOR: IAN PEARSON  
 AHA JOB#: 43-4B  
 DRILLING METHOD: HOLLOW STEM AUGER  
 BORING STARTED: 3/25/98

WELL TYPE: MONITORING  
 WELLHEAD TYPE: STICKUP (1.5')  
 WELL COMPLETED: 3/25/98  
 WELL DEVELOPED: WELL DRY  
 DATE SURVEYED: \_\_\_\_\_  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: SCH 40 PVC  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 2"  
 CASING MATERIAL: SCH 40 PVC  
 BORING DIAMETER: 7 1/2"  
 TOP OF CASING ELEV. (FT): 5455.97  
 GROUND ELEVATION (FT): 5454.68  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1,975,404.71  
 EASTING (FT): 299,547.33

LITHOLOGY LOG



\* SURVEY COORDINATES AND ELEVATION ARE ESTIMATED. WELL WAS DRY AT COMPLETION AND AS OF 3/30/98

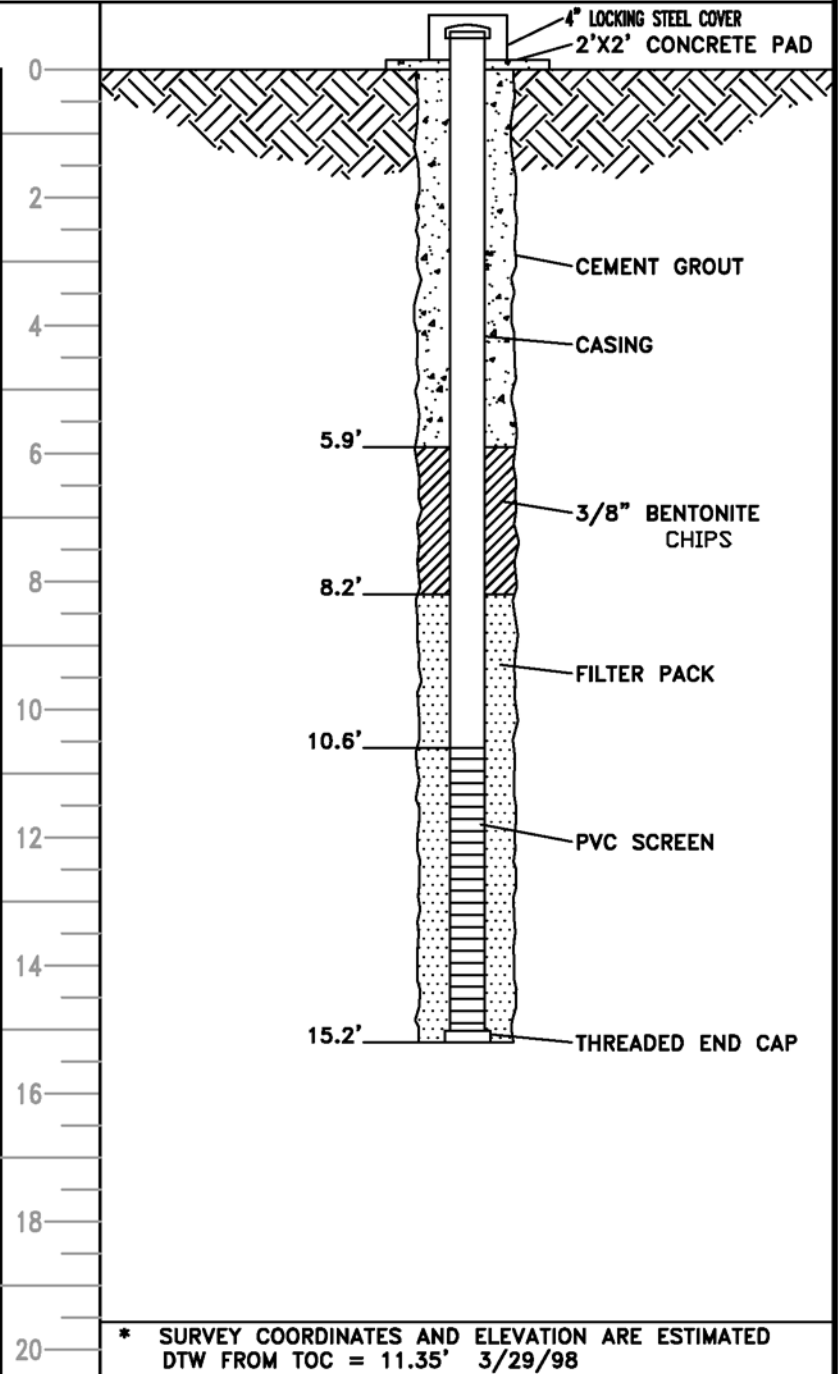
COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NO NAME  
 DRILLING CO: PHILIP SERVICES  
 DRILLER: KELLY PADILLA  
 CLIENT SUPERVISOR: RON VANVALKENBURG  
 GEOLOGIST/SUPERVISOR: IAN PEARSON  
 AHA JOB#: 43-4B  
 DRILLING METHOD: HOLLOW STEM AUGER  
 BORING STARTED: 3/25/98

WELL TYPE: MONITORING  
 WELLHEAD TYPE: STICKUP (1.7')  
 WELL COMPLETED: 3/25/98  
 WELL DEVELOPED: 3/28/98  
 DATE SURVEYED: \_\_\_\_\_  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: SCH 40 PVC  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 2"  
 CASING MATERIAL: SCH 40 PVC  
 BORING DIAMETER: 7 1/2"  
 TOP OF CASING ELEV. (FT): 5352.90  
 GROUND ELEVATION (FT): 5351.24  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1,990,260.27  
 EASTING (FT): 300,409.16

LITHOLOGY LOG







# NORWEST

Applied Hydrology

# PA-2

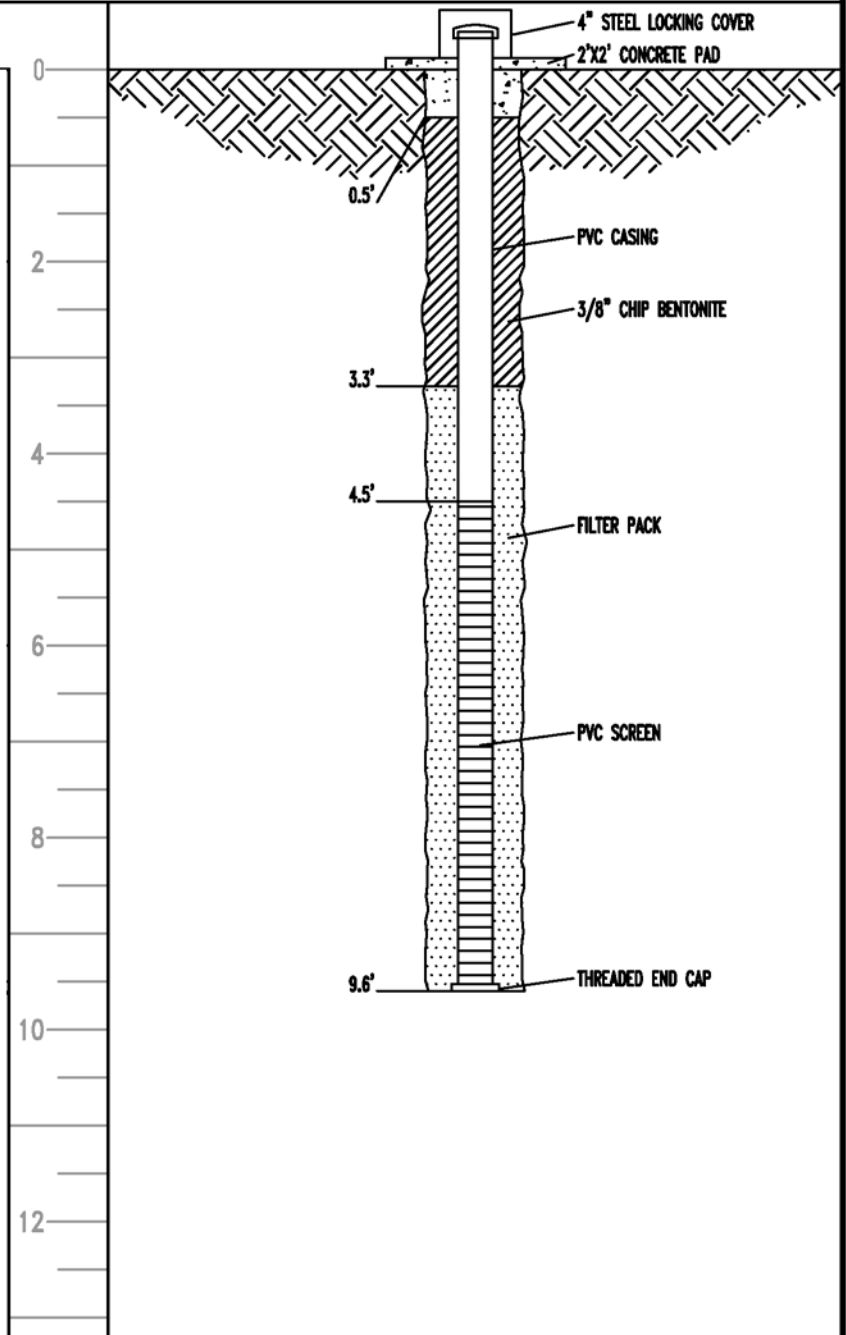
## COMPLETION DIAGRAM & LITHOLOGIC LOG

PROJECT: NO NAME  
 DRILLING CO: PHILIP SERVICES CORP  
 DRILLER: KELLY PADILLA  
 CLIENT SUPERVISOR: RON VANVALKENBURG  
 GEOLOGIST/SUPERVISOR: IAN PEARSON  
 AHA JOB#: 43-4B  
 DRILLING METHOD: HOLLOW STEM AUGER  
 BORING STARTED: 3/25/98

WELL TYPE: MONITORING  
 WELLHEAD TYPE: STICKUP (2.15')  
 WELL COMPLETED: 3/25/98  
 WELL DEVELOPED: 3/28/98  
 DATE SURVEYED: \_\_\_\_\_  
 SCREEN SLOT SIZE: 0.02" MILL SLOT  
 SCREEN TYPE: SCH 40 PVC  
 FILTER PACK: 10-20 SILICA SAND

CASING DIAMETER: 2"  
 CASING MATERIAL: SCH 40 PVC  
 BORING DIAMETER: 7 1/2"  
 TOP OF CASING ELEV. (FT): 5431.43  
 GROUND ELEVATION (FT): 5429.60  
 LOCATION: AREA 4 SOUTH  
 NORTHING (FT): 1,980,957.17  
 EASTING (FT): 306,702.95

### LITHOLOGY LOG



\* SURVEY COORDINATES AND ELEVATION ARE ESTIMATED  
 DTW FROM TOC = 7.69' 3/30/98

## **Appendix 18.F**

Aquifer Testing Results from 1998 and 2007

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**HYDRAULIC TESTING RESULTS FOR NAVAJO MINE EXTENSION PROJECT  
AUGUST 2007**

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Hydraulic testing of the Pictured Cliffs Sandstone (PCS) and the No. 8 coal seam was performed at BHP Navajo Coal Company's Navajo Mine Extension Project from August 14-18, 2007 on the following wells: Kpc2007-01, Kpc2007-02, Kpc2007-03, and Kf2007-01. The analyses of the test results were performed using codes in the Aqtesolv software package show good agreement with the previous findings.

Results:

Well Kpc2007-01 (Pictured Cliffs Sandstone)

A solution was obtained using the Theis Method, which assumes an extensive and homogeneous confined aquifer. The test was run with an average variable pumping rate of 0.95 gpm, results are attached. The solution indicates a transmissivity of 0.576 ft<sup>2</sup>/day and a hydraulic conductivity of 0.0074 ft/day ( $2.6 \times 10^{-6}$  cm/sec)

Well Kpc2007-02 (Pictured Cliffs Sandstone)

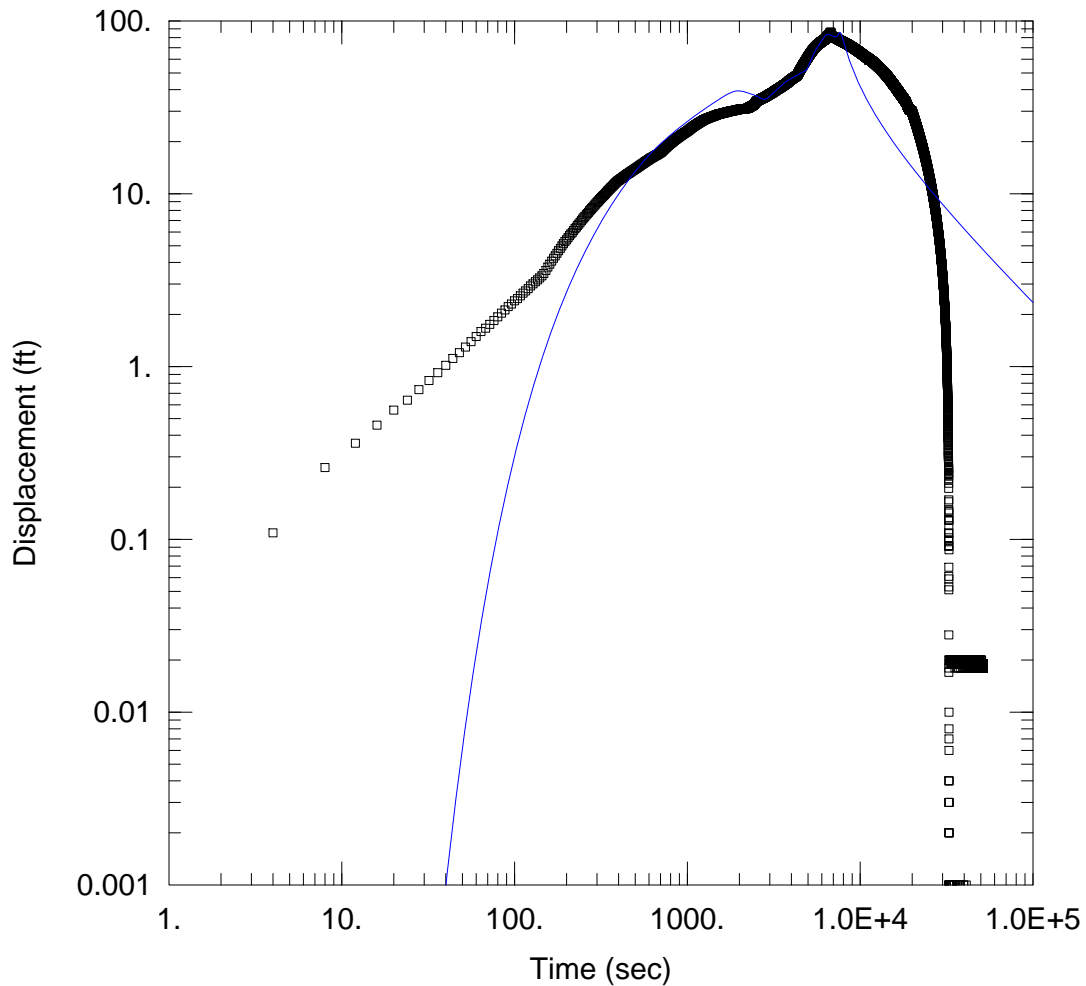
The drawdown rate in this well during pumping exactly matched casing volume dewatering, and recovery after pumping was very slow. Consequently, the results could not be interpreted as a pumping test. Instead, the recovery portion was analyzed using the Bouwer-Rice method for slug tests in confined aquifers. The results are attached. The very low hydraulic conductivity value of 0.0001 ft/day ( $3.51 \times 10^{-8}$  cm/sec) was obtained from this test, indicating the formation is either exceptionally tight or the screen interval is compromised by cement. Wet cement was found at the bottom of this well and the pH of the entire water column was 11.8.

Well Kpc2007-03 (Pictured Cliffs Sandstone)

A slug test was performed at this well due to the low yield of the PCS combined with a water column of only 7 feet in the well based on an initial water level measurement of 129 ft. and a total well depth of 136 ft. A slug was made up with two-inch PVC, open at the top and packed with sand, and this was let below the water and later raised above it for falling and rising head tests. The Bouwer-Rice solution obtained the best fit to the data, and gave a hydraulic conductivity of 0.004 ft/day ( $1.4 \times 10^{-6}$  cm/sec); the Hvorslev method gave 0.09 ft/day. The results are attached.

Well Kf2007-01 (No. 8A Seam)

This test showed delayed initial response, an abrupt "catch-up", and a faster than expected recovery. The later portion of the pumping test gave favorable fits to type curves for the Neuman-Witherspoon (leaky aquitard) and Papadopulos-Cooper (including well bore storage). The early pumping and recovery anomalies may be due to poor development and movement of coal fines during pumping, washout or fracturing of coals. The pumping rate was variable but averaged 1.5 gpm. Transmissivities determined for the variable rate interpretations of the Neuman-Witherspoon and Papadopulos-Cooper methods were 1.92 ft<sup>2</sup>/day and 1.398 ft<sup>2</sup>/day, respectively. A hydraulic conductivity value of 0.056 ft/day ( $2.0 \times 10^{-5}$  cm/sec) was obtained from the Papadopulos-Cooper test results.



WELL TEST ANALYSIS

Data Set: S:\...\Theis\_UpdatedFlowRates\_Kpc2007-01.aqt

Date: 10/29/08

Time: 08:48:36

WELL DATA

Pumping Wells

Observation Wells

| Well Name  | X (ft) | Y (ft) |
|------------|--------|--------|
| Kpc2007-01 | 0      | 0      |

| Well Name    | X (ft) | Y (ft) |
|--------------|--------|--------|
| □ Kpc2007-01 | 0      | 0      |

SOLUTION

Aquifer Model: Confined

Solution Method: Theis

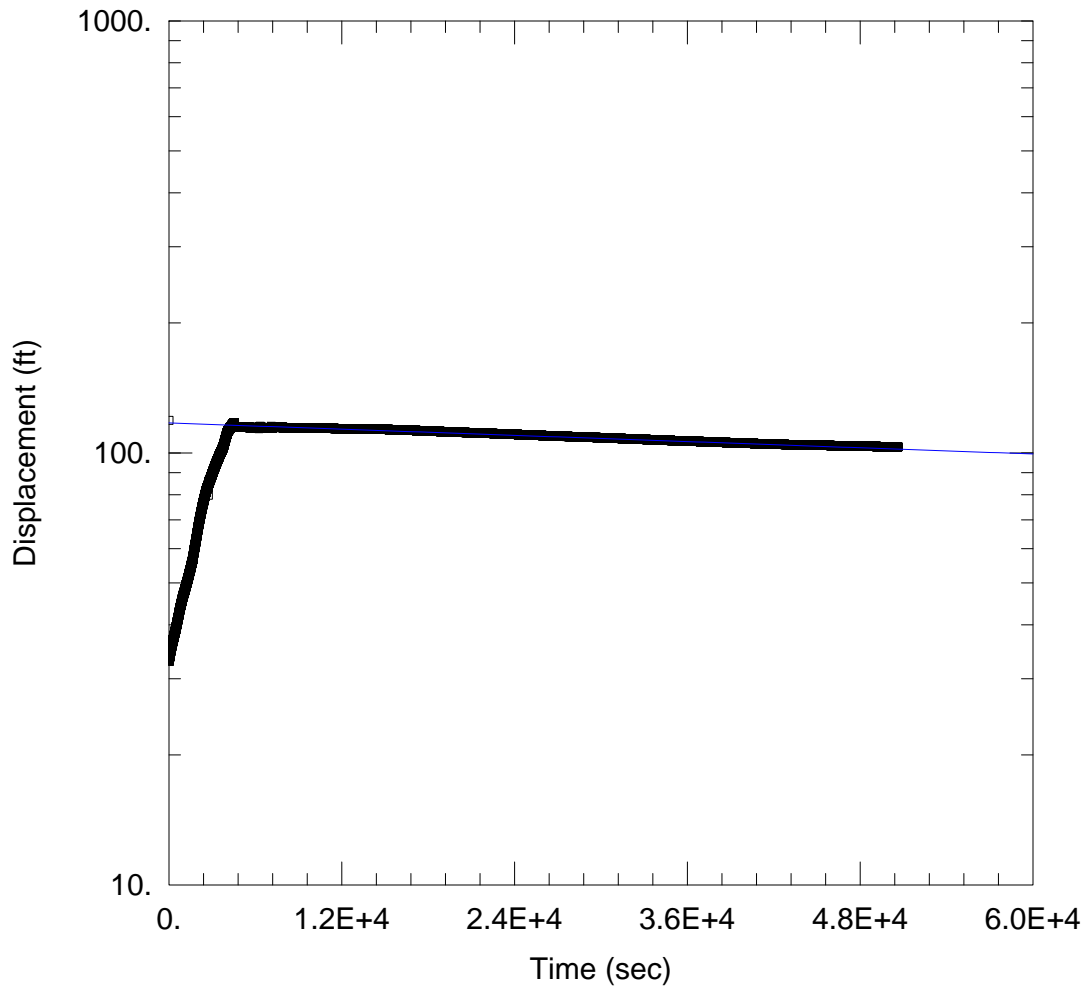
T = 0.5761 ft<sup>2</sup>/day

S = 0.0662

Kz/Kr = 1.

b = 70. ft





### WELL TEST ANALYSIS

Data Set: S:\...\BouwerRice\_Slug\_Kpc2007-02\_10-29-08.aqt  
 Date: 10/29/08 Time: 08:52:45

### PROJECT INFORMATION

Test Well: Kpc2007-02  
 Test Date: 8/17/2007

### AQUIFER DATA

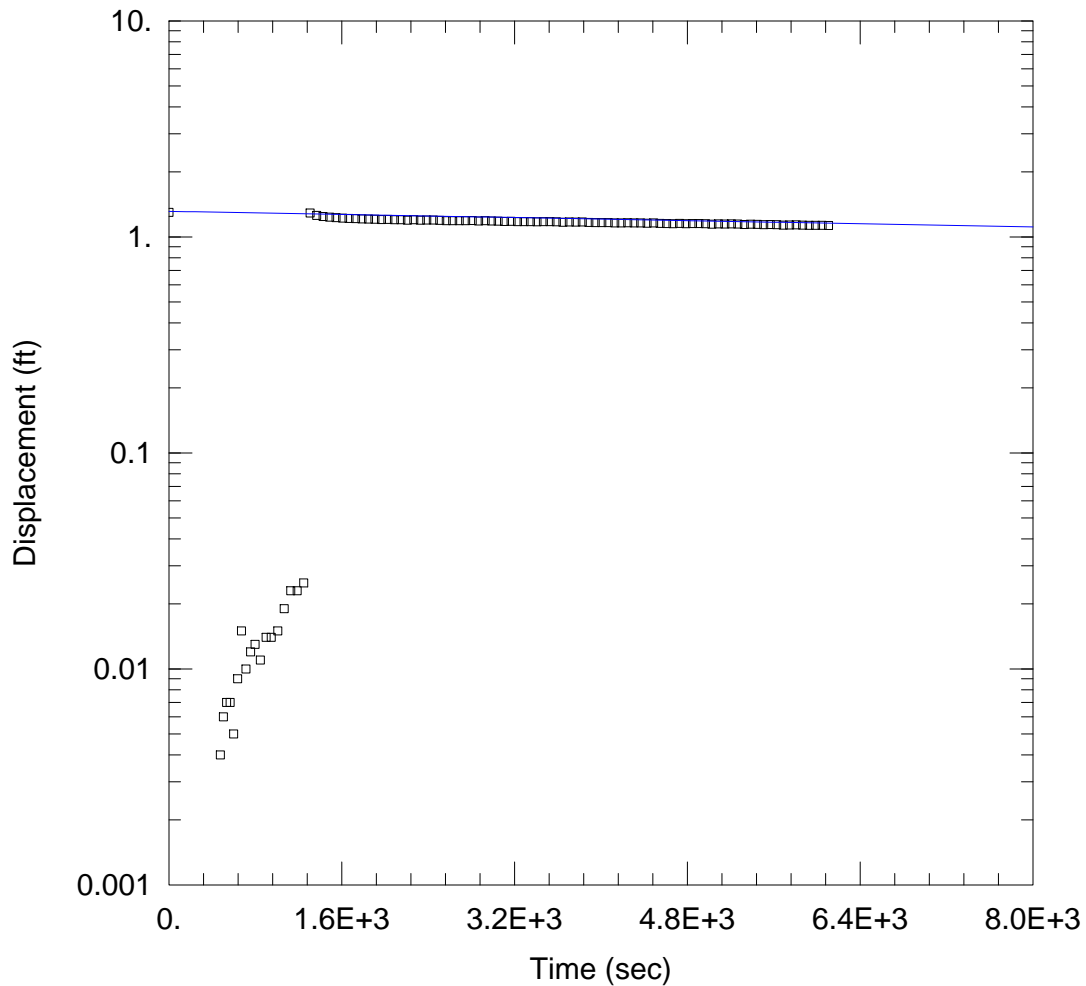
Saturated Thickness: 78. ft Anisotropy Ratio (Kz/Kr): 1.

### WELL DATA (Kpc2007-02)

Initial Displacement: 119. ft Static Water Column Height: 152.2 ft  
 Total Well Penetration Depth: 319. ft Screen Length: 70. ft  
 Casing Radius: 0.1208 ft Well Radius: 0.3645 ft

### SOLUTION

Aquifer Model: Confined Solution Method: Bouwer-Rice  
 K = 0.0001109 ft/day y0 = 117.3 ft



WELL TEST ANALYSIS

Data Set: S:\...\BouwerRice\_Kpc2007-03.aqt

Date: 10/29/08

Time: 08:55:00

PROJECT INFORMATION

Test Well: Kpc2007-03

Test Date: 8/17/2007

AQUIFER DATA

Saturated Thickness: 10. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (Kpc2007-03)

Initial Displacement: 1.3 ft

Static Water Column Height: 129.4 ft

Total Well Penetration Depth: 135. ft

Screen Length: 10. ft

Casing Radius: 0.12 ft

Well Radius: 0.364 ft

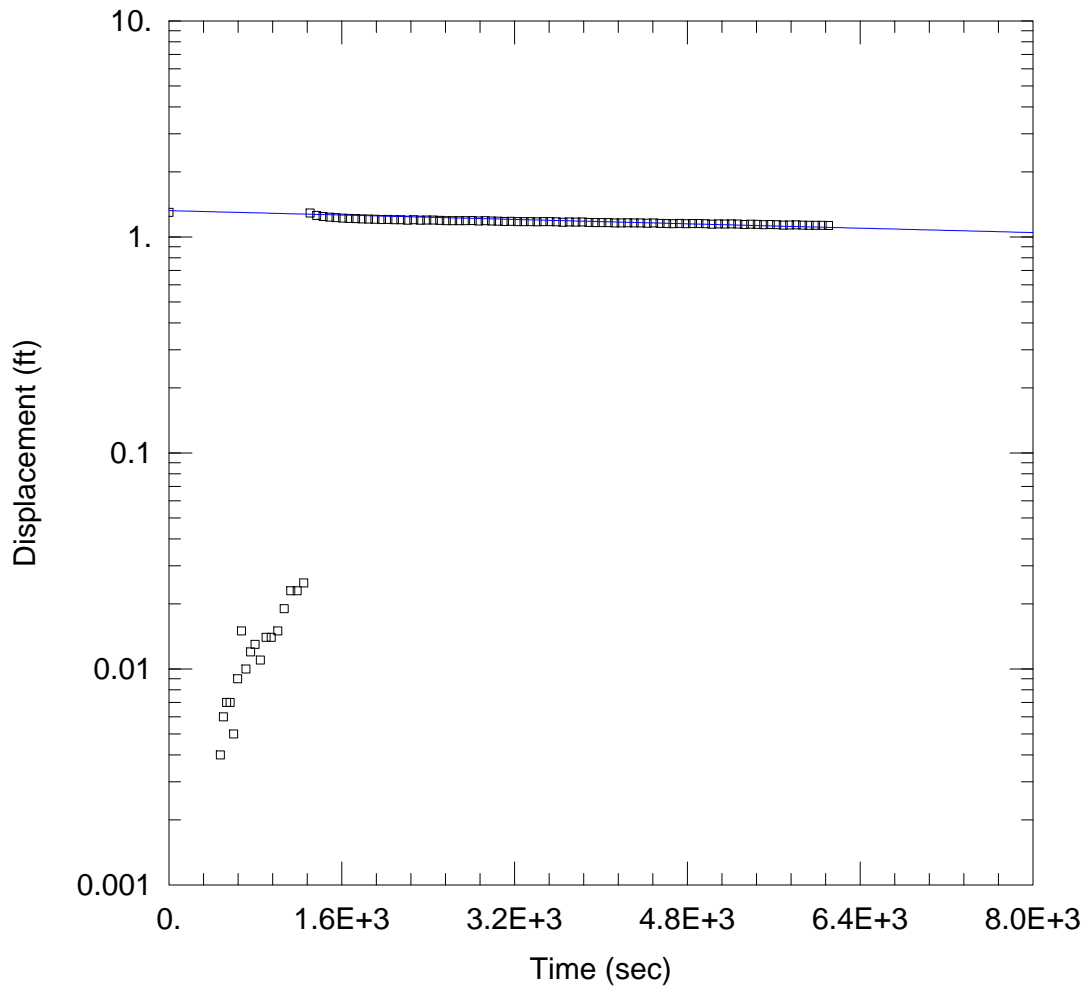
SOLUTION

Aquifer Model: Confined

Solution Method: Bouwer-Rice

K = 0.004462 ft/day

y0 = 1.314 ft



WELL TEST ANALYSIS

Data Set: S:\...\Hvorslev\_Kpc2007-03.aqt  
 Date: 10/29/08

Time: 08:55:41

PROJECT INFORMATION

Test Well: Kpc2007-03  
 Test Date: 8/17/2007

AQUIFER DATA

Saturated Thickness: 10. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (Kpc2007-03)

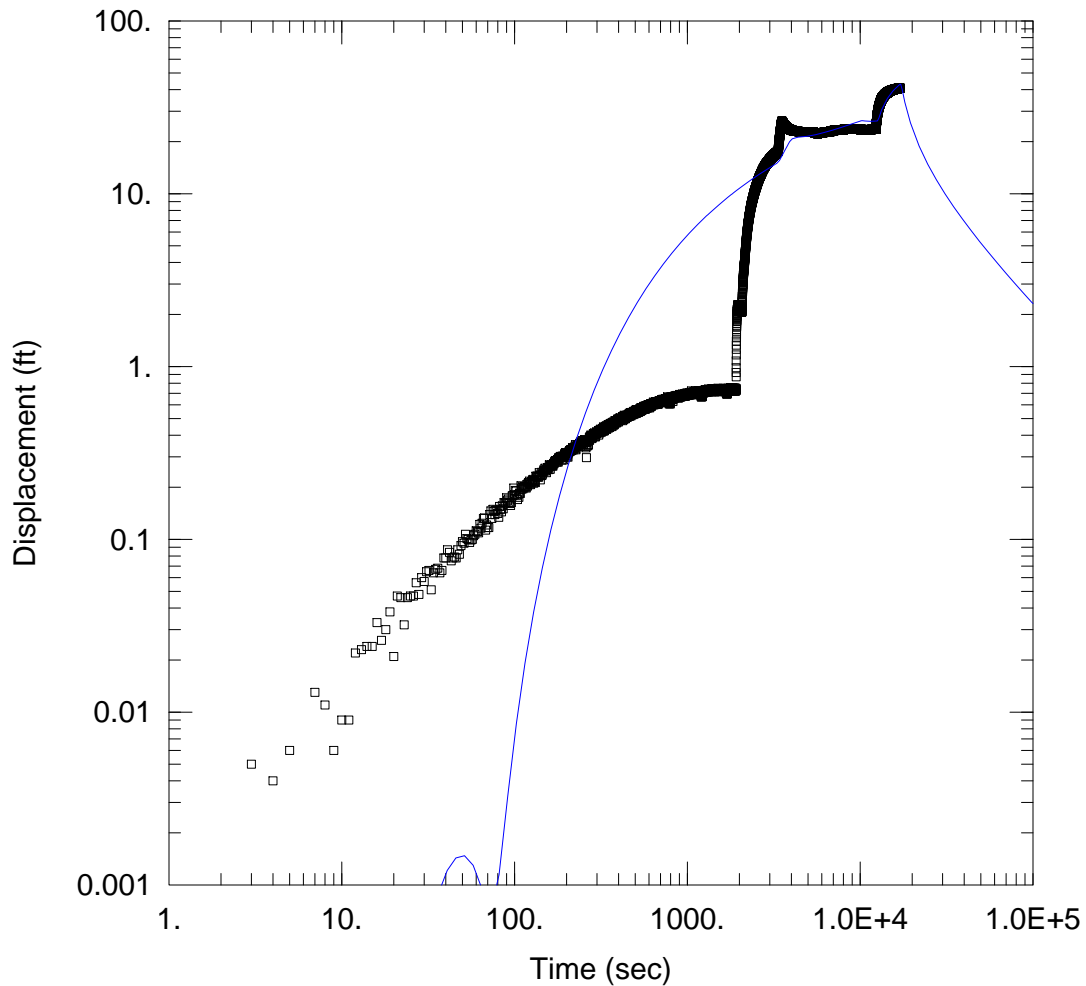
Initial Displacement: 1.3 ft  
 Total Well Penetration Depth: 135. ft  
 Casing Radius: 0.12 ft

Static Water Column Height: 129.4 ft  
 Screen Length: 10. ft  
 Well Radius: 0.364 ft

SOLUTION

Aquifer Model: Confined  
 K = 0.008505 ft/day

Solution Method: Hvorslev  
 y0 = 1.323 ft



### WELL TEST ANALYSIS

Data Set: S:\...\NeumanWitherspoon\_Kf2007-01.aqt

Date: 10/29/08

Time: 08:59:56

### PROJECT INFORMATION

Test Well: Kf2007-01

Test Date: 8/17/2007

### AQUIFER DATA

Saturated Thickness: 10. ft  
 Aquitard Thickness (b'): 1. ft

Anisotropy Ratio (Kz/Kr): 1.  
 Aquitard Thickness (b''): 1. ft

### WELL DATA

#### Pumping Wells

#### Observation Wells

| Well Name | X (ft) | Y (ft) |
|-----------|--------|--------|
| Kf2007-01 | 0      | 0      |

| Well Name   | X (ft) | Y (ft) |
|-------------|--------|--------|
| □ Kf2007-01 | 0      | 0      |

### SOLUTION

Aquifer Model: Leaky

Solution Method: Neuman-Witherspoon

T = 1.92 ft<sup>2</sup>/day

S = 0.3391

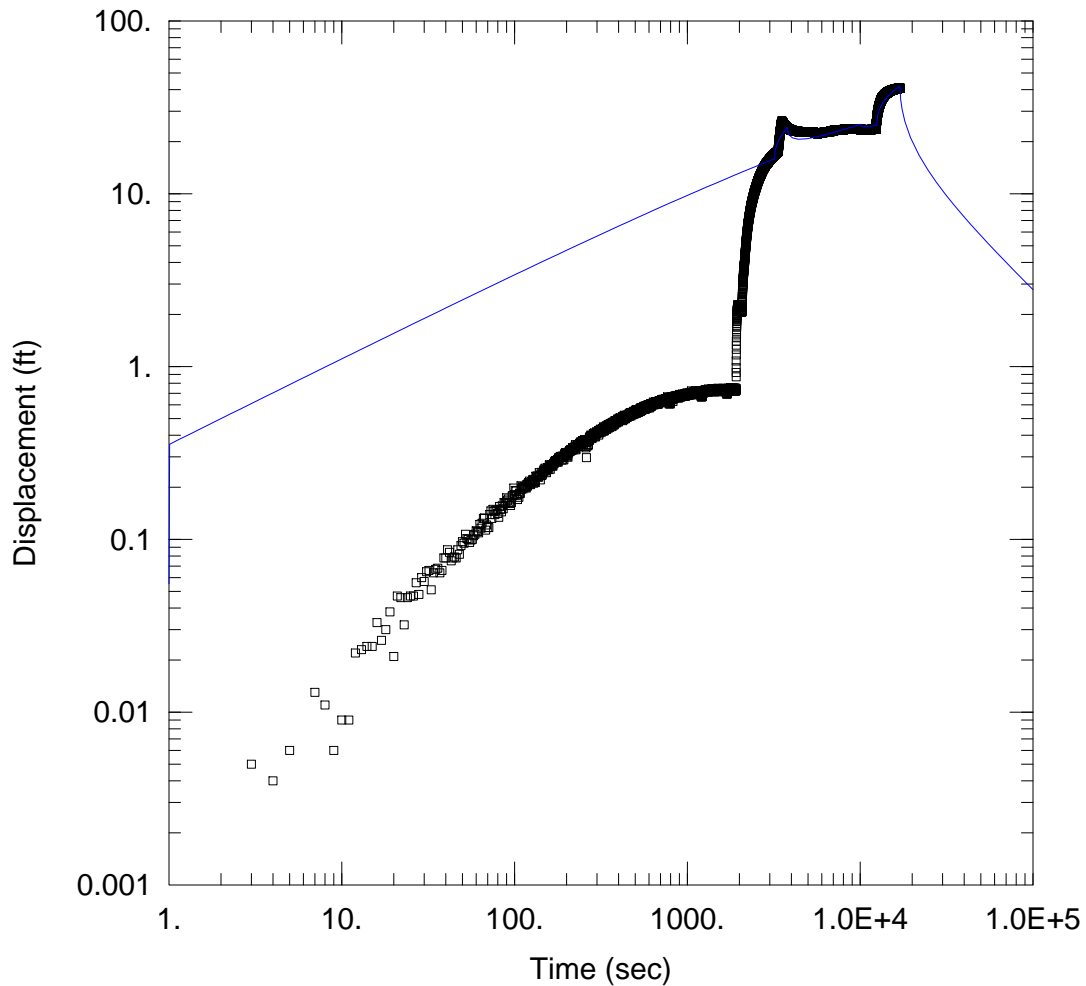
r/B = 1.0E-5

β = 1.0E-5

T2 = 1. ft<sup>2</sup>/day

S2 = 1.0E-10





WELL TEST ANALYSIS

Data Set: S:\...\PapadopoulosCooper\_Kf2007-01.aqt  
 Date: 10/29/08 Time: 09:01:09

PROJECT INFORMATION

Test Well: Kf2007-01  
 Test Date: 8/17/2007

AQUIFER DATA

Saturated Thickness: 10. ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA

| Pumping Wells |        |        | Observation Wells |        |        |
|---------------|--------|--------|-------------------|--------|--------|
| Well Name     | X (ft) | Y (ft) | Well Name         | X (ft) | Y (ft) |
| Kf2007-01     | 0      | 0      | □ Kf2007-01       | 0      | 0      |

SOLUTION

Aquifer Model: Confined Solution Method: Papadopoulos-Cooper  
 $T = 1.398 \text{ ft}^2/\text{day}$   $S = 1.$   
 $r(w) = 0.364 \text{ ft}$   $r(c) = 0.12 \text{ ft}$

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**PUMPING TEST RESULTS FOR PINABETE ALLUVIAL WELLS  
MAY 16, 1998**

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Pumping tests of wells PA-1 and PA-2 completed in Pinabete Alluvium were performed at BHP Navajo Coal Company's Area 4 South on May 16, 1998. The analyses of the test results were performed using codes in the Aqtesolv software package.

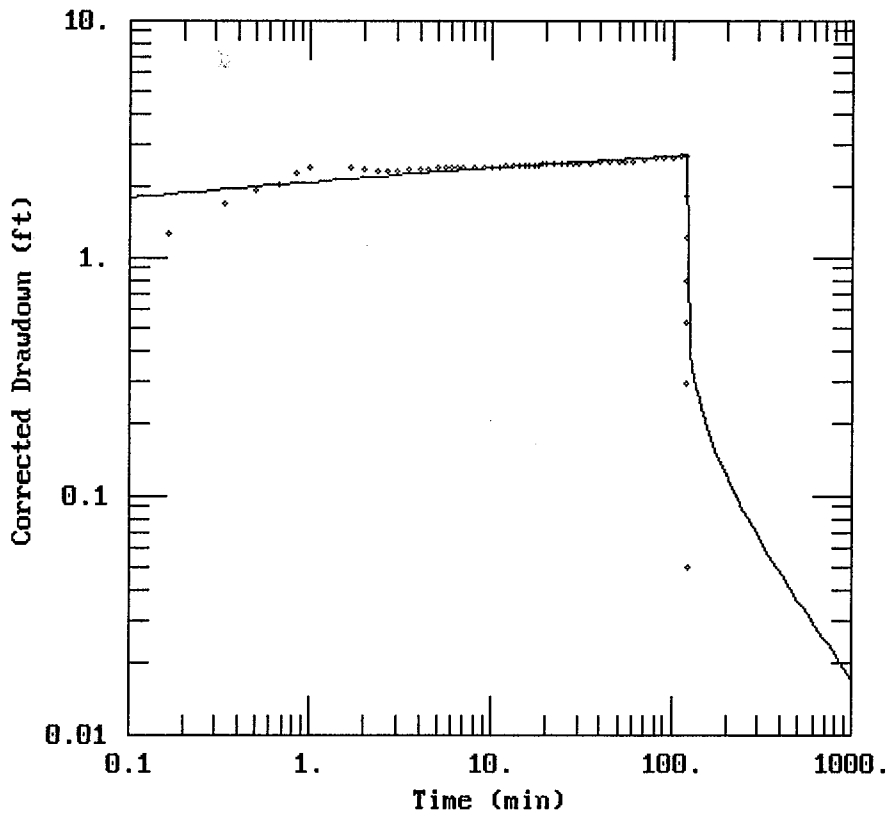
Results:

Well PA-1 (Pinabete Alluvium)

A solution was obtained using the Theis Method. The test was run with a constant pumping rate of 2.0 gpm, results are attached. The solution indicates a transmissivity of 230.7 ft<sup>2</sup>/day and a hydraulic conductivity of 51.3 ft/day ( $1.8 \times 10^{-2}$  cm/sec). The results are attached.

Well PA-2 (Pinabete Alluvium)

A solution was obtained using the Theis Method. The test was run with a constant pumping rate of 0.75 gpm, results are attached. The solution indicates a transmissivity of 75.62 ft<sup>2</sup>/day and a hydraulic conductivity of 11.5 ft/day ( $4.1 \times 10^{-3}$  cm/sec). The results are attached.



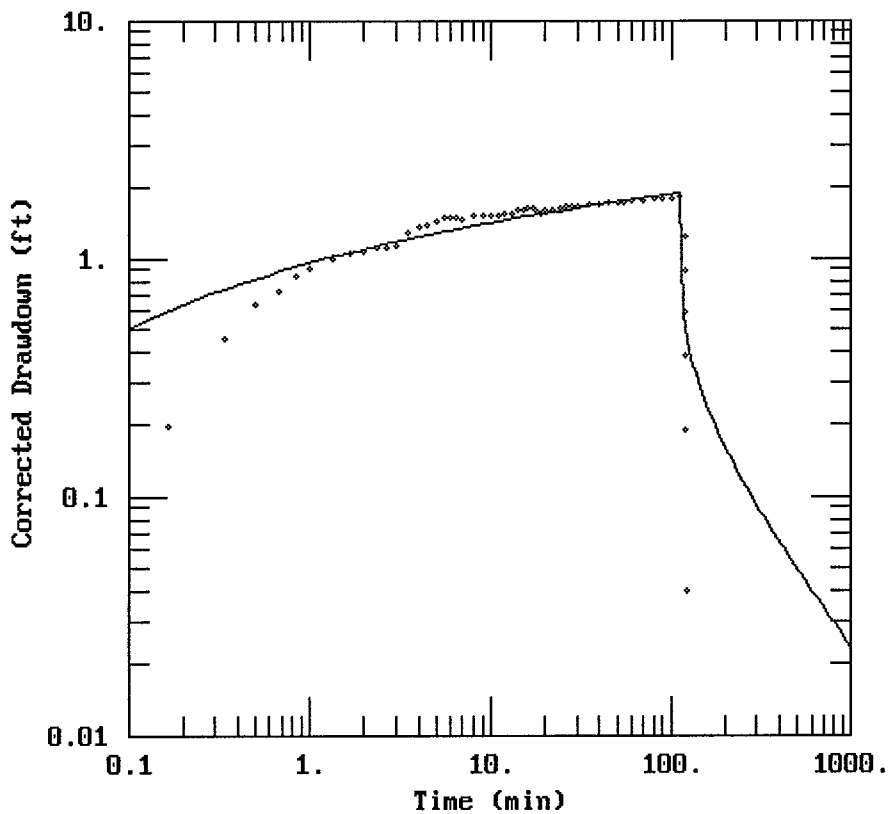
DATA SET:  
 PA1P&REC.AQT  
 08/25/98

AQUIFER MODEL:  
 Unconfined  
 SOLUTION METHOD:  
 Theis

PROJECT DATA:  
 test date: 5/16/98  
 test well: PA-1  
 obs. well: PA-1

TEST DATA:  
 $Q = 0.2674 \text{ ft}^3/\text{min}$   
 $r = 0. \text{ ft}$   
 $r_c = 0.08333 \text{ ft}$   
 $r_w = 0.08333 \text{ ft}$   
 $b = 7. \text{ ft}$

PARAMETER ESTIMATES:  
 $T = 230.7 \text{ ft}^2/\text{day}$   
 $S = 7.791\text{E-}06$



DATA SET:  
PA2P&REC.AQT  
08/25/98

AQUIFER MODEL:  
Unconfined  
SOLUTION METHOD:  
Theis

PROJECT DATA:  
test date: 5/16/98  
test well: PA-2  
obs. well: PA-2

TEST DATA:  
 $Q = 0.1003 \text{ ft}^3/\text{min}$   
 $r = 0. \text{ ft}$   
 $r_c = 0.08333 \text{ ft}$   
 $r_w = 0.08333 \text{ ft}$   
 $b = 7.5 \text{ ft}$

PARAMETER ESTIMATES:  
 $T = 57.62 \text{ ft}^2/\text{day}$   
 $S = 0.1073$



## **Appendix 18.G**

Quality Assurance and Quality Control Results for Baseline  
Groundwater Quality Data from 2007 to 2008

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#   | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 708-122   | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic   | 0.0000        | 0.049        | <b>0.050</b> | <b>98</b>        | 0.054          | 0.054            | <b>0.00</b> |
| Barium    | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.052          | 0.051            | <b>1.94</b> |
| Boron     | 0.0           | 1.8          | <b>2.0</b>   | <b>88</b>        | 0.3            | 0.3              | <b>0.00</b> |
| Cadmium   | 0.00000       | 0.048        | <b>0.050</b> | <b>96</b>        | 0.052          | 0.050            | <b>3.92</b> |
| Calcium   | 0.0           | 5.2          | <b>5.0</b>   | <b>104</b>       | 83.9           | 83.7             | <b>0.24</b> |
| Chromium  | 0.000         | 0.052        | <b>0.050</b> | <b>104</b>       | 0.055          | 0.052            | <b>5.61</b> |
| Copper    | 0.0000        | 0.051        | <b>0.050</b> | <b>102</b>       | 0.054          | 0.052            | <b>3.77</b> |
| Iron      | 0.00          | 1.05         | <b>1.00</b>  | <b>105</b>       | <0.05          | <0.05            | <b>NC</b>   |
| Lead      | 0.0000        | 0.051        | <b>0.050</b> | <b>102</b>       | 0.052          | 0.052            | <b>0.00</b> |
| Magnesium | 0.0           | 1.1          | <b>1.0</b>   | <b>106</b>       | 12.4           | 12.4             | <b>0.00</b> |
| Manganese | 0.00000       | 1.06         | <b>1.00</b>  | <b>106</b>       | 0.030          | 0.030            | <b>0.00</b> |
| Potassium | 0.0           | 1.20         | <b>1.00</b>  | <b>120</b>       | 1.4            | 1.2              | <b>15.4</b> |
| Selenium  | 0.000         | 0.245        | <b>0.250</b> | <b>98</b>        | 0.264          | 0.255            | <b>3.47</b> |
| Silver    | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | 0.052          | 0.052            | <b>0.00</b> |
| Sodium    | 0.0           | 53.9         | <b>50.0</b>  | <b>108</b>       | 19.9           | 19.7             | <b>1.01</b> |
| Uranium   | 0.00000       | 0.052        | <b>0.050</b> | <b>104</b>       | 0.054          | 0.052            | <b>3.77</b> |
| Zinc      | 0.000         | 0.050        | <b>0.050</b> | <b>100</b>       | 0.052          | 0.050            | <b>3.92</b> |

NC=Not calculated due to results less than the detection limit

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#    | SRM Data   |            |            |                  | Blank Data   |                 |
|------------|------------|------------|------------|------------------|--------------|-----------------|
| 708-122    | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic    | 0.054      | 0.050      | <b>108</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium     | 0.053      | 0.050      | <b>106</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron      | 5.10       | 5.00       | <b>102</b> | 90-110 %         | <0.1         | 0.1             |
| Cadmium    | 0.051      | 0.050      | <b>102</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium    | 5.3        | 5.0        | <b>106</b> | 90-110 %         | <0.5         | 0.5             |
| Chromium * | 0.057      | 0.050      | <b>114</b> | 90-110 %         | <0.001       | 0.001           |
| Copper     | 0.054      | 0.050      | <b>108</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron       | 5.45       | 5.00       | <b>109</b> | 90-110 %         | <0.05        | 0.05            |
| Lead       | 0.052      | 0.050      | <b>104</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium  | 5.20       | 5.00       | <b>104</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese  | 2.61       | 2.50       | <b>104</b> | 90-110 %         | <0.005       | 0.005           |
| Potassium  | 10.3       | 10.0       | <b>103</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium   | 0.269      | 0.250      | <b>108</b> | 90-110 %         | <0.001       | 0.001           |
| Silver     | 0.054      | 0.050      | <b>108</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium     | 8.8        | 8.1        | <b>109</b> | 90-110 %         | <0.5         | 0.5             |
| Uranium    | 0.052      | 0.050      | <b>104</b> | 90-110 %         | <0.00001     | 0.00001         |
| Zinc       | 0.053      | 0.050      | <b>106</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 708-122     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| PARAMETER   |               |              |               |                  |                |                  |             |
| Iron-T      | 0.00          | 4.20         | <b>4.00</b>   | <b>105</b>       | 1.10           | 1.10             | <b>0.0</b>  |
| Manganese-T | 0.000         | 2.20         | <b>2.00</b>   | <b>110</b>       | 0.055          | 0.053            | <b>3.70</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 708-122     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.00       | 5.00       | 100       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.610      | 2.500      | 104       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |       |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------|
| 708-122         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD % |
| Alkalinity      | 0             | 99           | 100         | 99               | 1820           | 1800             | 1.10  |
| Chloride        | 0             | 99           | 100         | 99               | <10            | <10              | NC    |
| EC              | NMA           | NMA          | NMA         | NMA              | 3570           | 3560             | 0.28  |
| Fluoride        | 0.0           | 1.1          | 1.0         | 110              | <0.2           | <0.2             | NC    |
| Nitrate/Nitrite | 0.09          | 0.17         | 0.10        | 80               | <0.02          | <0.02            | NC    |
| pH              | NMA           | NMA          | NMA         | NMA              | 8.20           | 8.19             | 0.12  |
| Sulfate         | 0             | 52           | 50          | 104              | 520            | 500              | 3.92  |
| TDS             | NMA           | NMA          | NMA         | NMA              | 2230           | 2215             | 0.67  |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 708-122         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 332        | 352        | <b>94.3</b> | 90-110 %         | <10          | 10              |
| Chloride        | 119        | 112        | <b>106</b>  | 90-110 %         | <10          | 10              |
| EC              | 527        | 561        | <b>93.9</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.49       | 0.50       | <b>98.0</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.33       | 8.40       | <b>99.2</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 330        | 320        | <b>103</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1290       | 1220       | <b>106</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 708-154     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic     | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | <0.0005        | <0.0005          | <b>NC</b>   |
| Barium      | 0.1130        | 0.159        | <b>0.050</b> | <b>92.0</b>      | 0.1130         | 0.1120           | <b>0.89</b> |
| Boron       | 0.0           | 2.0          | <b>2.0</b>   | <b>100</b>       | 0.3            | 0.3              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.047        | <b>0.050</b> | <b>94.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium     | 0.0           | 5.6          | <b>5.0</b>   | <b>112</b>       | 200.0          | 195.0            | <b>2.53</b> |
| Chromium    | 0.000         | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.005          | 0.005            | <b>0.00</b> |
| Copper      | 0.1050        | 0.150        | <b>0.050</b> | <b>90.0</b>      | 0.1090         | 0.1050           | <b>3.74</b> |
| Iron        | 0.00          | 1.14         | <b>1.00</b>  | <b>114</b>       | 0.64           | 0.61             | <b>4.80</b> |
| Lead        | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0030         | 0.0030           | <b>0.00</b> |
| Magnesium * | 0.0           | 1.6          | <b>1.0</b>   | <b>161</b>       | 21.1           | 20.2             | <b>4.36</b> |
| Manganese   | 0.00000       | 1.050        | <b>1.000</b> | <b>105</b>       | 0.00800        | 0.00700          | <b>13.3</b> |
| Potassium   | 0.0           | 1.1          | <b>1.0</b>   | <b>110</b>       | 13.7           | 13.5             | <b>1.47</b> |
| Selenium    | 0.000         | 0.263        | <b>0.250</b> | <b>105</b>       | <0.001         | <0.001           | <b>NC</b>   |
| Silver      | 0.00000       | 0.049        | <b>0.050</b> | <b>98</b>        | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium      | 0.0           | 57.7         | <b>50.0</b>  | <b>115</b>       | 58.5           | 56.7             | <b>3.13</b> |
| Uranium     | 0.00000       | 0.047        | <b>0.050</b> | <b>94</b>        | 0.00069        | 0.00069          | <b>0.00</b> |
| Zinc        | 0.000         | 0.051        | <b>0.050</b> | <b>102</b>       | <0.001         | <0.001           | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit

NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 708-154   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.4        | 5.0        | <b>108</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.46       | 5.00       | <b>109</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.53       | 2.50       | <b>101</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 11.0       | 10.0       | <b>110</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.273      | 0.250      | <b>109</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 17.2       | 16.2       | <b>106</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 708-154     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 2.08         | <b>2.00</b>   | <b>104</b>       | 0.16           | 0.14             | <b>13.3</b> |
| Manganese-T | 0.000         | 1.05         | <b>1.00</b>   | <b>105</b>       | 0.008          | 0.007            | <b>13.3</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 708-154     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.04       | 5.00       | 101       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.53       | 2.50       | 101       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |       |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------|
| 708-154         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD % |
| Alkalinity      | 0             | 102          | 100         | 102              | 312            | 310              | 0.64  |
| Chloride        | 0             | 99           | 100         | 99               | 15             | 15               | 0.00  |
| EC              | NMA           | NMA          | NMA         | NMA              | 1370           | 1370             | 0.00  |
| Fluoride        | 0.5           | 1.5          | 1.0         | 100              | 0.8            | 0.8              | 0.00  |
| Nitrate/Nitrite | 0.00          | 0.10         | 0.10        | 100              | <0.02          | <0.02            | NC    |
| pH              | NMA           | NMA          | NMA         | NMA              | 9.55           | 9.55             | 0.00  |
| Sulfate         | 0             | 50           | 50          | 100              | 3900           | 3900             | 0.00  |
| TDS             | NMA           | NMA          | NMA         | NMA              | 530            | 520              | 1.90  |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.



# Green Analytical Laboratories

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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 708-154         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 340        | 352        | <b>96.6</b> | 90-110 %         | <10          | 10              |
| Chloride        | 119        | 112        | <b>106</b>  | 90-110 %         | <10          | 10              |
| EC              | 519        | 561        | <b>92.5</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.46       | 0.50       | <b>92.0</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.31       | 8.40       | <b>98.9</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 335        | 320        | <b>105</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1240       | 1220       | <b>102</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 0711161252+ | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic     | 0.0000        | 0.051        | <b>0.050</b> | <b>102</b>       | <0.0005        | <0.0005          | <b>NC</b>   |
| Barium      | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.229          | 0.229            | <b>0.00</b> |
| Boron       | 0.0           | 2.3          | <b>2.0</b>   | <b>115</b>       | 0.3            | 0.3              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | 0.00007        | 0.00006          | <b>15.4</b> |
| Calcium     | 0.0           | 5.2          | <b>5.0</b>   | <b>104</b>       | 23.7           | 23.7             | <b>0.00</b> |
| Chromium    | 0.000         | 0.050        | <b>0.050</b> | <b>100</b>       | 0.002          | 0.002            | <b>0.00</b> |
| Copper      | 0.0000        | 0.051        | <b>0.050</b> | <b>102</b>       | 2.43           | 2.40             | <b>1.24</b> |
| Iron        | 0.00          | 1.06         | <b>1.00</b>  | <b>106</b>       | 4.83           | 4.82             | <b>0.21</b> |
| Lead        | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0008         | 0.0008           | <b>0.00</b> |
| Magnesium   | 0.0           | 1.1          | <b>1.0</b>   | <b>110</b>       | 4.8            | 4.7              | <b>2.11</b> |
| Manganese   | 0.00000       | 1.04         | <b>1.00</b>  | <b>104</b>       | 3.68           | 3.51             | <b>4.73</b> |
| Potassium   | 0.0           | 1.0          | <b>1.0</b>   | <b>100</b>       | 4.7            | 4.6              | <b>2.15</b> |
| Selenium    | 0.000         | 0.255        | <b>0.250</b> | <b>102</b>       | <0.005         | <0.005           | <b>NC</b>   |
| Silver      | 0.00000       | 0.052        | <b>0.050</b> | <b>104</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium      | 0.0           | 52.9         | <b>50.0</b>  | <b>106</b>       | 242            | 240              | <b>0.83</b> |
| Uranium     | 0.00000       | 0.051        | <b>0.050</b> | <b>102</b>       | 0.00021        | 0.00021          | <b>0.00</b> |
| Zinc        | 0.000         | 0.051        | <b>0.050</b> | <b>102</b>       | 0.079          | 0.076            | <b>3.87</b> |

NC=Not calculated due to results less than the detection limit

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0711161252+ | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic     | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron       | 5.10       | 5.00       | <b>102</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium     | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium     | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium    | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.001       | 0.001           |
| Copper      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron        | 5.11       | 5.00       | <b>102</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead        | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium   | 4.8        | 5.0        | <b>96.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese   | 2.57       | 2.50       | <b>103</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium   | 9.8        | 10.0       | <b>98.0</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium    | 0.256      | 0.250      | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver      | 0.054      | 0.050      | <b>108</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium      | 8.3        | 8.1        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium     | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.00001     | 0.00001         |
| Zinc        | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 0711161252+ | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 3.74         | <b>4.00</b>   | <b>93.5</b>      | 8.99           | 8.69             | <b>3.39</b> |
| Manganese-T | 0.000         | 1.820        | <b>2.00</b>   | <b>91.0</b>      | 4.78           | 4.64             | <b>2.97</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| PARAMETER   | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| 0711161252+ |            |            |           |                  |              |                 |
| Iron-T      | 5.11       | 5.00       | 102       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.57       | 2.50       | 103       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 0711161252+     | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 103          | <b>100</b>  | <b>103</b>       | 1750           | 1750             | <b>0.00</b> |
| Chloride        | 0             | 99           | <b>100</b>  | <b>99</b>        | 308            | 304              | <b>1.31</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 644            | 643              | <b>0.16</b> |
| Fluoride        | 0.2           | 1.1          | <b>1.0</b>  | <b>92</b>        | 1.0            | 1.0              | <b>0.00</b> |
| Nitrate/Nitrite | 0.04          | 0.13         | <b>0.10</b> | <b>90</b>        | <0.02          | <0.02            | <b>NC</b>   |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 9.56           | 9.56             | <b>0.00</b> |
| Sulfate         | 0             | 54           | <b>50</b>   | <b>108</b>       | 2500           | 2500             | <b>0.00</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 5820           | 5730             | <b>1.56</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0711161252+     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 276        | 283        | <b>97.5</b> | 90-110 %         | <10          | 10              |
| Chloride        | 39         | 37.9       | <b>103</b>  | 90-110 %         | <10          | 10              |
| EC              | 568        | 561        | <b>101</b>  | 90-110 %         | NMA          | NMA             |
| Fluoride        | 2.0        | 2.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.50       | 0.50       | <b>100</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.34       | 8.40       | <b>99.3</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 325        | 321        | <b>101</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1240       | 1210       | <b>102</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 0711060903+ | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic     | 0.0000        | 0.051        | <b>0.050</b> | <b>102</b>       | 0.0050         | 0.0050           | <b>0.00</b> |
| Barium      | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0530         | 0.0500           | <b>5.83</b> |
| Boron       | 0.0           | 0.5          | <b>0.5</b>   | <b>100</b>       | 0.5            | 0.5              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.052        | <b>0.050</b> | <b>104</b>       | <0.005         | <0.005           | <b>NC</b>   |
| Calcium     | 0.0           | 2.4          | <b>2.5</b>   | <b>96.0</b>      | 91.4           | 91.3             | <b>0.11</b> |
| Chromium    | 0.000         | 0.047        | <b>0.050</b> | <b>94.0</b>      | 0.002          | 0.002            | <b>0.00</b> |
| Copper      | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0100         | 0.0090           | <b>10.5</b> |
| Iron        | 0.00          | 0.50         | <b>0.50</b>  | <b>100</b>       | <0.05          | <0.05            | <b>NC</b>   |
| Lead        | 0.0000        | 0.052        | <b>0.050</b> | <b>104</b>       | 0.0002         | 0.0002           | <b>0.00</b> |
| Magnesium   | 0.0           | 0.5          | <b>0.5</b>   | <b>100</b>       | 13.1           | 13.1             | <b>0.00</b> |
| Manganese   | 0.00000       | 0.285        | <b>0.250</b> | <b>114</b>       | 2.10000        | 2.10000          | <b>0.00</b> |
| Potassium   | 0.0           | 0.5          | <b>0.5</b>   | <b>100</b>       | 1.4            | 1.4              | <b>0.00</b> |
| Selenium    | 0.000         | 0.254        | <b>0.250</b> | <b>102</b>       | 0.006          | 0.006            | <b>0.00</b> |
| Silver      | 0.00000       | 0.057        | <b>0.050</b> | <b>114</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium      | 0.0           | 25.4         | <b>25.0</b>  | <b>102</b>       | 16.4           | 16.4             | <b>0.00</b> |
| Uranium     | 0.00000       | 0.053        | <b>0.050</b> | <b>106</b>       | 0.00274        | 0.00270          | <b>1.47</b> |
| Zinc        | 0.000         | 0.052        | <b>0.050</b> | <b>104</b>       | 0.011          | 0.010            | <b>9.52</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0711060903+ | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic     | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium      | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron       | 5.000      | 5.000      | <b>100</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium     | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium     | 5.000      | 5.000      | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium    | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.001       | 0.001           |
| Copper      | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron        | 5.160      | 5.000      | <b>103</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead        | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | 0.0001       | 0.0001          |
| Magnesium   | 4.850      | 5.000      | <b>97.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese   | 2.560      | 2.500      | <b>102</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium   | 9.900      | 10.000     | <b>99.0</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium    | 0.255      | 0.250      | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver      | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium      | 8.200      | 8.100      | <b>101</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium     | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.00001     | 0.00001         |
| Zinc        | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#       | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|---------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 0711060903+   | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T        | 0.00          | 3.75         | <b>4.00</b>   | <b>93.8</b>      | 46.9           | 45.3             | <b>3.47</b> |
| Manganese-T * | 0.000         | 1.960        | <b>2.00</b>   | <b>98.0</b>      | 14.4           | 11.7             | <b>20.7</b> |
| Mercury-T     | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | 0.0002         | 0.0002           | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| PARAMETER   | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| 0711060903+ |            |            |           |                  |              |                 |
| Iron-T      | 4.97       | 5.00       | 99.4      | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.59       | 2.50       | 104       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 0711060903+     | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 104          | <b>100</b>  | <b>104</b>       | 111            | 109              | <b>1.82</b> |
| Chloride        | 0             | 103          | <b>100</b>  | <b>103</b>       | 152            | 150              | <b>1.32</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 1250           | 1250             | <b>0.00</b> |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90</b>        | 0.2            | 0.2              | <b>0.00</b> |
| Nitrate/Nitrite | 0.16          | 0.24         | <b>0.10</b> | <b>80</b>        | 1.97           | 1.92             | <b>2.57</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 7.53           | 7.51             | <b>0.27</b> |
| Sulfate         | 0             | 54           | <b>50</b>   | <b>108</b>       | 96             | 94               | <b>2.11</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 415            | 405              | <b>2.44</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.



# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0711060903+     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 290        | 283        | <b>102</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 36         | 37.9       | <b>95.0</b> | 90-110 %         | <10          | 10              |
| EC              | 580        | 561        | <b>103</b>  | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.52       | 0.50       | <b>104</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.36       | 8.40       | <b>100</b>  | 90-110 %         | NMA          | NMA             |
| Sulfate         | 340        | 321        | <b>106</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1200       | 1210       | <b>99.2</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 0712051332+ | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic     | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0060         | 0.0060           | <b>0.00</b> |
| Barium      | 0.0000        | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.0090         | 0.0090           | <b>0.00</b> |
| Boron       | 0.8           | 2.8          | <b>2.00</b>  | <b>100</b>       | <0.1           | <0.1             | <b>NC</b>   |
| Cadmium     | 0.00000       | 0.049        | <b>0.050</b> | <b>98.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium     | 0.0           | 45.8         | <b>50.0</b>  | <b>91.6</b>      | 22.1           | 21.6             | <b>2.29</b> |
| Chromium    | 0.000         | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.007          | 0.007            | <b>0.00</b> |
| Copper      | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0890         | 0.0730           | <b>19.8</b> |
| Iron        | 0.00          | 9.48         | <b>10.0</b>  | <b>94.8</b>      | 48.60          | 45.10            | <b>7.47</b> |
| Lead        | 0.0000        | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.0001         | 0.0001           | <b>0.00</b> |
| Magnesium   | 0.0           | 9.5          | <b>10.0</b>  | <b>95.1</b>      | 1.7            | 1.7              | <b>0.00</b> |
| Manganese   | 0.00000       | 1.150        | <b>1.00</b>  | <b>115</b>       | 51.10000       | 50.00000         | <b>2.18</b> |
| Potassium   | 0.0           | 9.9          | <b>10.0</b>  | <b>99.3</b>      | 3.7            | 3.6              | <b>2.74</b> |
| Selenium    | 0.000         | 0.250        | <b>0.250</b> | <b>100</b>       | 0.179          | 0.170            | <b>5.16</b> |
| Silver      | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium      | 0.0           | 481          | <b>500</b>   | <b>96.2</b>      | 194.0          | 190.0            | <b>2.08</b> |
| Uranium     | 0.00000       | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.01400        | 0.01400          | <b>0.00</b> |
| Zinc        | 0.000         | 0.051        | <b>0.050</b> | <b>102</b>       | 0.011          | 0.011            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0712051332+ | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic     | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Barium      | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron *     | 5.7        | 5.0        | <b>114</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium     | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium     | 5.3        | 5.0        | <b>106</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium    | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron        | 5.39       | 5.0        | <b>108</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead        | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium   | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.5         | 0.5             |
| Manganese * | 2.91       | 2.50       | <b>116</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium   | 10.9       | 10.0       | <b>109</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium    | 0.261      | 0.250      | <b>104</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver *    | 0.061      | 0.050      | <b>122</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium *    | 9.0        | 8.1        | <b>111</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium     | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.00001     | 0.00001         |
| Zinc        | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| PARAMETER   | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 4.20         | <b>4.00</b>   | <b>105</b>       | 42.9           | 40.6             | <b>5.51</b> |
| Manganese-T | 0.000         | 2.170        | <b>2.000</b>  | <b>109</b>       | 1.71           | 1.62             | <b>5.41</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |            |                  | Blank Data   |                 |
|-------------|------------|------------|------------|------------------|--------------|-----------------|
| 0712051332+ | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.10       | 5.00       | <b>102</b> | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.650      | 2.500      | <b>106</b> | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | <b>100</b> | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 0712051332+     | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 106          | <b>100</b>  | <b>106</b>       | 138            | 137              | <b>0.73</b> |
| Chloride        | 0             | 101          | <b>100</b>  | <b>101</b>       | 210            | 206              | <b>1.92</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 12400          | 12400            | <b>0.00</b> |
| Fluoride        | 0.2           | 1.1          | <b>1.0</b>  | <b>89</b>        | <0.2           | <0.2             | <b>NC</b>   |
| Nitrate/Nitrite | 0.04          | 0.13         | <b>0.10</b> | <b>90</b>        | 0.07           | 0.06             | <b>15.4</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 7.05           | 7.04             | <b>0.14</b> |
| Sulfate         | 0             |              | <b>50</b>   | <b>0</b>         | 9800           | 9800             | <b>0.00</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 355            | 350              | <b>1.42</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0712051332+     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 274        | 283        | <b>96.8</b> | 90-110 %         | <10          | 10              |
| Chloride        | 37         | 37.9       | <b>97.6</b> | 90-110 %         | <10          | 10              |
| EC              | 556        | 561        | <b>99.1</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 2.2        | 2.0        | <b>110</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.54       | 0.50       | <b>108</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.22       | 8.40       | <b>97.9</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 350        | 321        | <b>109</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1360       | 1210       | <b>112</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 0712070915+ | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Calcium     | 0.0           | 45.8         | <b>50.0</b> | <b>91.6</b>      | 22.6           | 22.1             | <b>2.24</b> |
| Iron        | 0.00          | 9.49         | <b>10.0</b> | <b>94.9</b>      | 48.6           | 45.1             | <b>7.47</b> |
| Magnesium   | 0.0           | 9.5          | <b>10.0</b> | <b>95.0</b>      | 1.7            | 1.7              | <b>0.00</b> |
| Potassium   | 0.0           | 9.9          | <b>10.0</b> | <b>99.3</b>      | 3.7            | 3.6              | <b>2.74</b> |
| Sodium      | 0.0           | 481          | <b>500</b>  | <b>96.2</b>      | 194.0          | 190.0            | <b>2.08</b> |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |            |                  | Blank Data   |                 |
|-----------|------------|------------|------------|------------------|--------------|-----------------|
| PARAMETER | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Calcium   | 5.3        | 5.0        | <b>105</b> | 90-110 %         | <0.5         | 0.5             |
| Iron      | 5.40       | 5.0        | <b>108</b> | 90-110 %         | <0.05        | 0.05            |
| Magnesium | 5.2        | 5.0        | <b>104</b> | 90-110 %         | <0.5         | 0.5             |
| Potassium | 10.9       | 10.0       | <b>109</b> | 90-110 %         | <0.5         | 0.5             |
| Sodium *  | 9.0        | 8.1        | <b>111</b> | 90-110 %         | <0.5         | 0.5             |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 0712070915+     | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 104          | <b>100</b>  | <b>104</b>       | 212            | 210              | <b>0.95</b> |
| Chloride        | 0             | 100          | <b>100</b>  | <b>100</b>       | <10            | <10              | <b>NC</b>   |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 702            | 700              | <b>0.29</b> |
| Fluoride        | 0.0           | 1.0          | <b>1.0</b>  | <b>100</b>       | 0.5            | 0.5              | <b>0.00</b> |
| Nitrate/Nitrite | NA            | NA           | <b>NA</b>   | <b>NA</b>        | NA             | NA               | <b>NA</b>   |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 5.28           | 5.25             | <b>0.57</b> |
| Sulfate         | 0             | 53           | <b>50</b>   | <b>106</b>       | 600            | 590              | <b>1.68</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 335            | 325              | <b>3.03</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 0712070915+     | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 272        | 283        | <b>96.1</b> | 90-110 %         | <10          | 10              |
| Chloride        | 38         | 37.9       | <b>100</b>  | 90-110 %         | <10          | 10              |
| EC              | 547        | 561        | <b>97.5</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | NA         | NA         | <b>NA</b>   | 90-110 %         | NA           | NA              |
| pH              | 8.30       | 8.40       | <b>98.8</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 330        | 321        | <b>103</b>  | 90-110 %         | <10          | 10              |
| TDS *           | 1010       | 1210       | <b>83.5</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 802-077     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic     | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.051          | 0.048            | <b>6.06</b> |
| Barium      | 0.0000        | 0.046        | <b>0.050</b> | <b>92.0</b>      | 0.054          | 0.051            | <b>5.71</b> |
| Boron       | 0.1           | 2.3          | <b>2.0</b>   | <b>108</b>       | 0.4            | 0.4              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.047        | <b>0.050</b> | <b>94.0</b>      | 0.047          | 0.047            | <b>0.00</b> |
| Calcium *   | 0.0           | 6.9          | <b>5.0</b>   | <b>138</b>       | 82.5           | 82.0             | <b>0.61</b> |
| Chromium    | 0.000         | 0.044        | <b>0.050</b> | <b>88.0</b>      | 0.050          | 0.045            | <b>10.5</b> |
| Copper      | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.059          | 0.054            | <b>8.85</b> |
| Iron *      | 0.00          | 1.40         | <b>1.00</b>  | <b>140</b>       | <0.05          | <0.05            | <b>NC</b>   |
| Lead        | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.047          | 0.046            | <b>2.15</b> |
| Magnesium * | 0.0           | 1.4          | <b>1.0</b>   | <b>140</b>       | 9.1            | 9.0              | <b>1.10</b> |
| Manganese * | 0.00000       | 1.20         | <b>1.00</b>  | <b>120</b>       | 0.008          | 0.008            | <b>0.00</b> |
| Potassium * | 0.0           | 1.4          | <b>1.00</b>  | <b>140</b>       | 0.9            | 0.8              | <b>11.8</b> |
| Selenium    | 0.000         | 0.216        | <b>0.250</b> | <b>86.4</b>      | 0.250          | 0.233            | <b>7.04</b> |
| Silver      | 0.00000       | 0.040        | <b>0.050</b> | <b>80.0</b>      | 0.046          | 0.043            | <b>6.74</b> |
| Sodium *    | 0.1           | 70.4         | <b>50.0</b>  | <b>141</b>       | 32.7           | 32.5             | <b>0.61</b> |
| Uranium     | 0.00000       | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.050          | 0.047            | <b>6.19</b> |
| Zinc        | 0.000         | 0.044        | <b>0.050</b> | <b>88.0</b>      | 0.051          | 0.048            | <b>6.06</b> |

NC=Not calculated due to results less than the detection limit

NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 802-077   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.4        | 5.0        | <b>108</b>  | 90-110 %         | 0.1          | 0.1             |
| Cadmium   | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 4.5        | 5.0        | <b>90.0</b> | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.046      | 0.050      | <b>92.0</b> | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 4.91       | 5.00       | <b>98.2</b> | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 4.6        | 5.0        | <b>92.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.70       | 2.50       | <b>108</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 9.7        | 10.0       | <b>97.0</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.239      | 0.250      | <b>95.6</b> | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.045      | 0.050      | <b>90.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 7.9        | 8.1        | <b>97.5</b> | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.053      | 0.050      | <b>106</b>  | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.046      | 0.050      | <b>92.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| PARAMETER   | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.20          | 3.70         | <b>4.00</b>   | <b>87.5</b>      | 9.60           | 9.40             | <b>2.11</b> |
| Manganese-T | 0.020         | 1.90         | <b>2.00</b>   | <b>94.0</b>      | 5.100          | 5.000            | <b>1.98</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 802-077     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.24       | 5.00       | 105       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.700      | 2.500      | 108       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 802-077         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 101          | <b>100</b>  | <b>101</b>       | 1320           | 1290             | <b>2.30</b> |
| Chloride        | 0             | 109          | <b>100</b>  | <b>109</b>       | 10             | 10               | <b>0.00</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | NA             | NA               | <b>NA</b>   |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90</b>        | 1.0            | 1.0              | <b>0.00</b> |
| Nitrate/Nitrite | 0.03          | 0.12         | <b>0.10</b> | <b>90</b>        | 11.80          | 11.50            | <b>2.58</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 8.11           | 8.08             | <b>0.37</b> |
| Sulfate         | 0             | 48           | <b>50</b>   | <b>96</b>        | 90             | 88               | <b>2.25</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 460            | 450              | <b>2.20</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 802-077         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 179        | 186        | <b>96.2</b> | 90-110 %         | <10          | 10              |
| Chloride        | 27         | 24.7       | <b>109</b>  | 90-110 %         | <10          | 10              |
| EC              | 536        | 561        | <b>95.5</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 2.0        | 2.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.52       | 0.50       | <b>104</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.35       | 8.40       | <b>99.4</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 340        | 321        | <b>106</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1320       | 1210       | <b>109</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 802-089     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic     | 0.0000        | 0.043        | <b>0.050</b> | <b>86.0</b>      | 0.0011         | 0.0010           | <b>9.52</b> |
| Barium      | 0.0000        | 0.044        | <b>0.050</b> | <b>88.0</b>      | 0.0151         | 0.0150           | <b>0.66</b> |
| Boron       | 0.1           | 2.3          | <b>2.0</b>   | <b>110</b>       | 0.4            | 0.4              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.044        | <b>0.050</b> | <b>88.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium *   | 0.0           | 6.9          | <b>5.0</b>   | <b>138</b>       | 82.5           | 82.0             | <b>0.61</b> |
| Chromium    | 0.000         | 0.041        | <b>0.050</b> | <b>82.0</b>      | 0.005          | 0.005            | <b>0.00</b> |
| Copper      | 0.0000        | 0.047        | <b>0.050</b> | <b>94.0</b>      | 0.0161         | 0.0161           | <b>0.00</b> |
| Iron *      | 0.00          | 1.40         | <b>1.00</b>  | <b>140</b>       | <0.05          | <0.05            | <b>NC</b>   |
| Lead        | 0.0000        | 0.043        | <b>0.050</b> | <b>86.0</b>      | 0.0001         | 0.0001           | <b>0.00</b> |
| Magnesium * | 0.0           | 1.4          | <b>1.0</b>   | <b>140</b>       | 9.1            | 9.0              | <b>1.10</b> |
| Manganese   | 0.00000       | 1.200        | <b>1.00</b>  | <b>120</b>       | 0.00800        | 0.00800          | <b>0.00</b> |
| Potassium * | 0.0           | 1.4          | <b>1.0</b>   | <b>140</b>       | 0.9            | 0.8              | <b>11.8</b> |
| Selenium    | 0.000         | 0.222        | <b>0.250</b> | <b>88.8</b>      | 0.012          | 0.012            | <b>0.00</b> |
| Silver      | 0.00000       | 0.041        | <b>0.050</b> | <b>82.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium *    | 0.1           | 70.4         | <b>50.0</b>  | <b>141</b>       | 32.7           | 32.5             | <b>0.61</b> |
| Uranium     | 0.00000       | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.02240        | 0.02140          | <b>4.57</b> |
| Zinc        | 0.000         | 0.042        | <b>0.050</b> | <b>84.0</b>      | 0.075          | 0.074            | <b>1.34</b> |

NC=Not calculated due to results less than the detection limit  
 NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 802-089   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium *  | 0.044      | 0.050      | <b>88.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.4        | 5.0        | <b>108</b>  | 90-110 %         | 0.1          | 0.1             |
| Cadmium   | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 4.5        | 5.0        | <b>90.0</b> | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.046      | 0.050      | <b>92.0</b> | 90-110 %         | <0.001       | 0.001           |
| Copper *  | 0.043      | 0.050      | <b>86.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.24       | 5.00       | <b>105</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead *    | 0.044      | 0.050      | <b>88.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 4.6        | 5.0        | <b>92.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.73       | 2.50       | <b>109</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 9.7        | 10.0       | <b>97.0</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.261      | 0.250      | <b>104</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 7.9        | 8.1        | <b>97.3</b> | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| PARAMETER   | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 3.70         | <b>4.00</b>  | <b>92.5</b>      | 9.60           | 9.40             | <b>2.11</b> |
| Manganese-T | 0.020         | 1.90         | <b>2.00</b>  | <b>94.0</b>      | 5.10           | 5.00             | <b>1.98</b> |
| Mercury-T   | 0.0000        | 0.002        | <b>0.002</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 802-089     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.24       | 5.00       | 105       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.73       | 2.50       | 109       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 802-089         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 101          | <b>100</b>  | <b>101</b>       | 226            | 222              | <b>1.79</b> |
| Chloride        | 0             | 109          | <b>100</b>  | <b>109</b>       | 32             | 32               | <b>0.00</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | NA             | NA               | <b>NA</b>   |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90</b>        | 0.3            | 0.3              | <b>0.00</b> |
| Nitrate/Nitrite | 0.03          | 0.13         | <b>0.10</b> | <b>100</b>       | 11.8           | 11.5             | <b>2.58</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 5.90           | 5.86             | <b>0.68</b> |
| Sulfate         | 0             | 48           | <b>50</b>   | <b>96</b>        | 90             | 88               | <b>2.25</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 460            | 450              | <b>2.20</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |            |                  | Blank Data   |                 |
|-----------------|------------|------------|------------|------------------|--------------|-----------------|
| 802-089         | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 179        | 186        | <b>96</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 27         | 24.7       | <b>109</b> | 90-110 %         | <10          | 10              |
| EC              | 539        | 561        | <b>96</b>  | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b> | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.52       | 0.50       | <b>104</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.35       | 8.40       | <b>99</b>  | 90-110 %         | NMA          | NMA             |
| Sulfate         | 340        | 321        | <b>106</b> | 90-110 %         | <10          | 10              |
| TDS             | 1320       | 1210       | <b>109</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#   | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 802-039   | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic   | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.0005         | 0.0005           | <b>0.00</b> |
| Barium    | 0.0000        | 0.044        | <b>0.050</b> | <b>88.0</b>      | 0.0080         | 0.0080           | <b>0.00</b> |
| Boron *   | 0.0           | 2.0          | <b>2.0</b>   | <b>100</b>       | 0.17           | 0.13             | <b>26.7</b> |
| Cadmium   | 0.00000       | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.00011        | 0.00010          | <b>9.52</b> |
| Calcium   | 0.0           | 51.3         | <b>50.0</b>  | <b>103</b>       | 110.0          | 109.0            | <b>0.91</b> |
| Chromium  | 0.000         | 0.046        | <b>0.050</b> | <b>92.0</b>      | <0.001         | <0.001           | <b>NC</b>   |
| Copper    | 0.0001        | 0.047        | <b>0.050</b> | <b>93.8</b>      | 0.0060         | 0.0060           | <b>0.00</b> |
| Iron      | 0.00          | 9.76         | <b>10.0</b>  | <b>97.6</b>      | 0.08           | 0.08             | <b>0.00</b> |
| Lead      | 0.0001        | 0.042        | <b>0.050</b> | <b>83.8</b>      | 0.0007         | 0.0007           | <b>0.00</b> |
| Magnesium | 0.0           | 9.7          | <b>10.0</b>  | <b>97.0</b>      | 7.3            | 7.3              | <b>0.00</b> |
| Manganese | 0.00000       | 1.110        | <b>1.00</b>  | <b>111</b>       | 0.00900        | 0.00800          | <b>11.8</b> |
| Potassium | 0.0           | 9.6          | <b>10.0</b>  | <b>96.0</b>      | 1.7            | 1.7              | <b>0.00</b> |
| Selenium  | 0.000         | 0.226        | <b>0.250</b> | <b>90.4</b>      | <0.001         | <0.001           | <b>NC</b>   |
| Silver    | 0.00000       | 0.044        | <b>0.050</b> | <b>88.0</b>      | <0.0005        | <0.0005          | <b>NC</b>   |
| Sodium    | 0.0           | 484          | <b>500</b>   | <b>96.8</b>      | 320.0          | 314.0            | <b>1.89</b> |
| Uranium   | 0.00000       | 0.044        | <b>0.050</b> | <b>88.0</b>      | 0.00030        | 0.00030          | <b>0.00</b> |
| Zinc      | 0.000         | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.023          | 0.023            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit

NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 802-039   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.045      | 0.050      | <b>90.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.2        | 5.00       | <b>104</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | 0.0001       | 0.0001          |
| Iron      | 5.19       | 5.00       | <b>104</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.045      | 0.050      | <b>90.0</b> | 90-110 %         | 0.0001       | 0.0001          |
| Magnesium | 4.8        | 5.0        | <b>96.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.65       | 2.50       | <b>106</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.1       | 10.0       | <b>101</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.233      | 0.250      | <b>93.2</b> | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.044      | 0.050      | <b>88.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.8        | 8.1        | <b>109</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 802-039     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 3.76         | <b>4.00</b>   | <b>94.0</b>      | 6.01           | 5.61             | <b>6.88</b> |
| Manganese-T | 0.000         | 1.97         | <b>2.00</b>   | <b>98.5</b>      | 1.29           | 1.27             | <b>1.56</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |            |                  | Blank Data   |                 |
|-------------|------------|------------|------------|------------------|--------------|-----------------|
| 802-039     | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.21       | 5.00       | <b>104</b> | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.730      | 2.500      | <b>109</b> | 90-110 %         | <0.005       | 0.005           |
| Mercury-T * | 0.002      | 0.002      | <b>118</b> | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |       |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------|
| 802-039         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD % |
| Alkalinity      | 0             | 102          | 100         | 102              | 308            | 306              | 0.65  |
| Chloride        | 0             | 101          | 100         | 101              | <10            | <10              | NC    |
| EC              | NMA           | NMA          | NMA         | NMA              | NA             | NA               | NA    |
| Fluoride        | 1.7           | 2.7          | 1.0         | 106              | 0.5            | 0.5              | 0.00  |
| Nitrate/Nitrite | 0.17          | 0.27         | 0.10        | 100              | 6.03           | 5.91             | 2.01  |
| pH              | NMA           | NMA          | NMA         | NMA              | 7.44           | 7.41             | 0.40  |
| Sulfate         | 0             |              | 50          | 0                | 104            | 104              | 0.00  |
| TDS             | NMA           | NMA          | NMA         | NMA              | 1200           | 1180             | 1.68  |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 802-039         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 176        | 186        | <b>94.6</b> | 90-110 %         | <10          | 10              |
| Chloride        | 25         | 24.7       | <b>101</b>  | 90-110 %         | <10          | 10              |
| EC              | 527        | 561        | <b>93.9</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 2.0        | 2.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.50       | 0.50       | <b>100</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 8.36       | 8.40       | <b>100</b>  | 90-110 %         | NMA          | NMA             |
| Sulfate         | 320        | 321        | <b>99.7</b> | 90-110 %         | <10          | 10              |
| TDS             | 1180       | 1210       | <b>97.5</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#    | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 805-117    | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic    | 0.0000        | 0.053        | <b>0.050</b> | <b>106</b>       | <0.0005        | <0.0005          | <b>NC</b>   |
| Barium     | 0.0000        | 0.046        | <b>0.050</b> | <b>92.0</b>      | 0.0250         | 0.0240           | <b>4.08</b> |
| Boron      | 0.0           | 2.0          | <b>2.0</b>   | <b>100</b>       | 0.7            | 0.7              | <b>0.00</b> |
| Cadmium    | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium    | 0.0           | 5.5          | <b>5.0</b>   | <b>110</b>       | 89.8           | 89.7             | <b>0.11</b> |
| Chromium   | 0.000         | 0.050        | <b>0.050</b> | <b>100</b>       | 0.004          | 0.004            | <b>0.00</b> |
| Copper     | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.4300         | 0.4030           | <b>6.48</b> |
| Iron       | 0.00          | 1.09         | <b>1.00</b>  | <b>109</b>       | <0.05          | <0.05            | <b>NC</b>   |
| Lead       | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0003         | 0.0003           | <b>0.00</b> |
| Magnesium  | 0.0           | 1.1          | <b>1.0</b>   | <b>110</b>       | 13.1           | 13.1             | <b>0.00</b> |
| Manganese  | 0.00000       | 1.060        | <b>1.00</b>  | <b>106</b>       | 0.05100        | 0.05100          | <b>0.00</b> |
| Potassium  | 0.0           | 1.0          | <b>1.0</b>   | <b>100</b>       | 0.8            | 0.8              | <b>0.00</b> |
| Selenium * | 0.000         | 0.261        | <b>0.250</b> | <b>104</b>       | 0.007          | 0.005            | <b>33.3</b> |
| Silver     | 0.00000       | 0.047        | <b>0.050</b> | <b>94.0</b>      | 0.00006        | 0.00005          | <b>18.2</b> |
| Sodium     | 0.0           | 54.7         | <b>50.0</b>  | <b>109</b>       | 52.0           | 51.8             | <b>0.39</b> |
| Uranium    | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | 0.01060        | 0.00950          | <b>10.9</b> |
| Zinc       | 0.000         | 0.054        | <b>0.050</b> | <b>108</b>       | 0.024          | 0.022            | <b>8.70</b> |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |            |                  | Blank Data   |                 |
|-----------|------------|------------|------------|------------------|--------------|-----------------|
| 805-117   | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.053      | 0.050      | <b>106</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.053      | 0.050      | <b>106</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.1        | 5.0        | <b>102</b> | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.051      | 0.050      | <b>102</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.1        | 5.00       | <b>102</b> | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.051      | 0.050      | <b>102</b> | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.050      | 0.050      | <b>100</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.42       | 5.00       | <b>108</b> | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.051      | 0.050      | <b>102</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 5.0        | 5.0        | <b>100</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.54       | 2.50       | <b>102</b> | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.3       | 10.0       | <b>103</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.257      | 0.250      | <b>103</b> | 90-110 %         | <0.001       | 0.001           |
| Silver *  | 0.059      | 0.050      | <b>118</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.7        | 8.1        | <b>107</b> | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.052      | 0.050      | <b>104</b> | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.050      | 0.050      | <b>100</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 805-117     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 3.96         | <b>4.00</b>   | <b>99.0</b>      | 4.13           | 4.09             | <b>0.97</b> |
| Manganese-T | 0.000         | 1.94         | <b>2.00</b>   | <b>97.0</b>      | 0.035          | 0.034            | <b>2.90</b> |
| Mercury-T   | 0.0000        | 0.0022       | <b>0.0020</b> | <b>110</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 805-117     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.23       | 5.00       | 105       | 90-110 %         | 0.06         | 0.05            |
| Manganese-T | 2.540      | 2.500      | 102       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 805-117         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 108          | <b>100</b>  | <b>108</b>       | 238            | 238              | <b>0.00</b> |
| Chloride        | 0             | 99           | <b>100</b>  | <b>99</b>        | 11             | 11               | <b>0.00</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 515            | 510              | <b>0.98</b> |
| Fluoride        | 0.0           | 1.0          | <b>1.0</b>  | <b>100</b>       | 1.3            | 1.3              | <b>0.00</b> |
| Nitrate/Nitrite | 0.04          | 0.13         | <b>0.10</b> | <b>90</b>        | 0.07           | 0.06             | <b>15.4</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 7.79           | 7.75             | <b>0.51</b> |
| Sulfate         | 0             | 54           | <b>50</b>   | <b>108</b>       | 3300           | 3300             | <b>0.00</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 3120           | 3080             | <b>1.29</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 805-117         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 187        | 186        | <b>101</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 25         | 24.7       | <b>101</b>  | 90-110 %         | <10          | 10              |
| EC              | 826        | 829        | <b>100</b>  | 90-110 %         | NMA          | NMA             |
| Fluoride        | 0.9        | 1.0        | <b>90.0</b> | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.51       | 0.50       | <b>102</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 9.11       | 9.29       | <b>98.1</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 325        | 321        | <b>101</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1100       | 1170       | <b>94.0</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#    | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 805-126    | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic    | 0.0000        | 0.053        | <b>0.050</b> | <b>106</b>       | <0.0005        | <0.0005          | <b>NC</b>   |
| Barium     | 0.0000        | 0.046        | <b>0.050</b> | <b>92.0</b>      | 0.0250         | 0.0240           | <b>4.08</b> |
| Boron      | 0.0           | 2.0          | <b>2.0</b>   | <b>100</b>       | 0.7            | 0.7              | <b>0.00</b> |
| Cadmium    | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium    | 0.0           | 5.4          | <b>5.0</b>   | <b>108</b>       | 89.8           | 89.7             | <b>0.11</b> |
| Chromium   | 0.000         | 0.050        | <b>0.050</b> | <b>100</b>       | 0.004          | 0.004            | <b>0.00</b> |
| Copper     | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0432         | 0.0430           | <b>0.46</b> |
| Iron       | 0.00          | 1.09         | <b>1.00</b>  | <b>109</b>       | <0.05          | <0.05            | <b>NC</b>   |
| Lead       | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0003         | 0.0003           | <b>0.00</b> |
| Magnesium  | 0.0           | 1.1          | <b>1.0</b>   | <b>110</b>       | 13.1           | 13.1             | <b>0.00</b> |
| Manganese  | 0.00000       | 1.060        | <b>1.00</b>  | <b>106</b>       | 0.05100        | 0.05100          | <b>0.00</b> |
| Potassium  | 0.0           | 1.0          | <b>1.0</b>   | <b>100</b>       | 0.8            | 0.8              | <b>0.00</b> |
| Selenium * | 0.000         | 0.261        | <b>0.250</b> | <b>104</b>       | 0.007          | 0.005            | <b>33.3</b> |
| Silver     | 0.00000       | 0.047        | <b>0.050</b> | <b>94.0</b>      | 0.00006        | 0.00005          | <b>18.2</b> |
| Sodium     | 0.0           | 54.7         | <b>50.0</b>  | <b>109</b>       | 52.0           | 51.8             | <b>0.39</b> |
| Uranium    | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | 0.01060        | 0.00950          | <b>10.9</b> |
| Zinc       | 0.000         | 0.054        | <b>0.050</b> | <b>108</b>       | 0.024          | 0.022            | <b>8.70</b> |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |            |                  | Blank Data   |                 |
|-----------|------------|------------|------------|------------------|--------------|-----------------|
| 805-126   | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.053      | 0.050      | <b>106</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.053      | 0.050      | <b>106</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.1        | 5.0        | <b>102</b> | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.051      | 0.050      | <b>102</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.1        | 5.0        | <b>102</b> | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.051      | 0.050      | <b>102</b> | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.050      | 0.050      | <b>100</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.42       | 5.00       | <b>108</b> | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.051      | 0.050      | <b>102</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 5.0        | 5.0        | <b>100</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.54       | 2.50       | <b>102</b> | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.3       | 10.0       | <b>103</b> | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.257      | 0.250      | <b>103</b> | 90-110 %         | <0.001       | 0.001           |
| Silver *  | 0.059      | 0.050      | <b>118</b> | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.7        | 8.1        | <b>107</b> | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.052      | 0.050      | <b>104</b> | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.052      | 0.050      | <b>104</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| PARAMETER   | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| 805-126     |               |              |               |                  |                |                  |             |
| Iron-T      | 0.00          | 4.18         | <b>4.00</b>   | <b>105</b>       | 1.32           | 1.30             | <b>1.53</b> |
| Manganese-T | 0.000         | 1.06         | <b>1.00</b>   | <b>106</b>       | 0.051          | 0.051            | <b>0.00</b> |
| Mercury-T   | 0.0000        | 0.0022       | <b>0.0020</b> | <b>110</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| PARAMETER   | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.05       | 5.00       | 101       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.660      | 2.500      | 106       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 805-126         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 108          | <b>100</b>  | <b>108</b>       | 238            | 238              | <b>0.00</b> |
| Chloride        | 0             | 99           | <b>100</b>  | <b>99</b>        | 11             | 11               | <b>0.00</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 515            | 510              | <b>0.98</b> |
| Fluoride        | 0.0           | 1.0          | <b>1.0</b>  | <b>100</b>       | 1.3            | 1.3              | <b>0.00</b> |
| Nitrate/Nitrite | 0.04          | 0.13         | <b>0.10</b> | <b>90</b>        | 0.08           | 0.08             | <b>0.00</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 7.79           | 7.75             | <b>0.51</b> |
| Sulfate         | 0             | 54           | <b>50</b>   | <b>108</b>       | 3300           | 3300             | <b>0.00</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 3120           | 3080             | <b>1.29</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.



# Green Analytical Laboratories

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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |            |                  | Blank Data   |                 |
|-----------------|------------|------------|------------|------------------|--------------|-----------------|
| 805-126         | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 187        | 186        | <b>101</b> | 90-110 %         | <10          | 10              |
| Chloride        | 25         | 24.7       | <b>101</b> | 90-110 %         | <10          | 10              |
| EC              | 826        | 829        | <b>100</b> | 90-110 %         | NMA          | NMA             |
| Fluoride        | 0.9        | 1.0        | <b>90</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.51       | 0.50       | <b>102</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 9.11       | 9.29       | <b>98</b>  | 90-110 %         | NMA          | NMA             |
| Sulfate         | 325        | 321        | <b>101</b> | 90-110 %         | <10          | 10              |
| TDS             | 1100       | 1170       | <b>94</b>  | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 808-094     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic     | 0.0000        | 0.053        | <b>0.050</b> | <b>106</b>       | 0.0042         | 0.0040           | <b>4.88</b> |
| Barium      | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0977         | 0.0945           | <b>3.33</b> |
| Boron       | 0.0           | 2.3          | <b>2.0</b>   | <b>117</b>       | 0.1            | 0.1              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.051        | <b>0.050</b> | <b>102</b>       | 0.00107        | 0.00100          | <b>6.76</b> |
| Calcium     | 0.0           | 5.8          | <b>5.0</b>   | <b>116</b>       | 120.0          | 120.0            | <b>0.00</b> |
| Chromium    | 0.000         | 0.052        | <b>0.050</b> | <b>104</b>       | <0.001         | <0.001           | <b>NC</b>   |
| Copper      | 0.0000        | 0.052        | <b>0.050</b> | <b>104</b>       | 0.0068         | 0.0063           | <b>7.63</b> |
| Iron        | 0.00          | 1.17         | <b>1.00</b>  | <b>117</b>       | 0.10           | 0.09             | <b>10.5</b> |
| Lead        | 0.0000        | 0.056        | <b>0.050</b> | <b>112</b>       | 0.0016         | 0.0015           | <b>3.28</b> |
| Magnesium   | 0.0           | 1.2          | <b>1.0</b>   | <b>120</b>       | 14.7           | 14.6             | <b>0.68</b> |
| Manganese * | 0.00000       | 1.24         | <b>1.00</b>  | <b>124</b>       | 0.00900        | 0.00900          | <b>0.00</b> |
| Potassium   | 0.0           | 1.1          | <b>1.0</b>   | <b>106</b>       | 10.8           | 10.8             | <b>0.00</b> |
| Selenium    | 0.000         | 0.276        | <b>0.250</b> | <b>110</b>       | 0.001          | <0.001           | <b>NC</b>   |
| Silver      | 0.00000       | 0.052        | <b>0.050</b> | <b>104</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium      | 0.0           | 59.7         | <b>50.0</b>  | <b>119</b>       | 55.1           | 54.9             | <b>0.36</b> |
| Uranium     | 0.00000       | 0.056        | <b>0.050</b> | <b>112</b>       | 0.00427        | 0.00427          | <b>0.00</b> |
| Zinc        | 0.000         | 0.056        | <b>0.050</b> | <b>112</b>       | 0.009          | 0.009            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 808-094   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.3        | 5.0        | <b>106</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.38       | 5.00       | <b>108</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.69       | 2.50       | <b>108</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.3       | 10.1       | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.239      | 0.250      | <b>95.6</b> | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.7        | 8.1        | <b>107</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| PARAMETER   | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| 808-094     |               |              |               |                  |                |                  |             |
| Iron-T      | 0.00          | 3.94         | <b>4.00</b>   | <b>98.5</b>      | 7.10           | 7.00             | <b>1.42</b> |
| Manganese-T | 0.000         | 2.05         | <b>2.00</b>   | <b>103</b>       | 4.400          | 4.300            | <b>2.30</b> |
| Mercury-T   | 0.0000        | 0.0022       | <b>0.0020</b> | <b>110</b>       | <0.0005        | <0.0005          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 808-094     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.09       | 5.00       | 102       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.65       | 2.50       | 106       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 808-094         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 106          | <b>100</b>  | <b>106</b>       | 182            | 180              | <b>1.10</b> |
| Chloride        | 0             | 105          | <b>100</b>  | <b>105</b>       | 1210           | 1180             | <b>2.51</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 386            | 385              | <b>0.26</b> |
| Fluoride        | 0.0           | 0.9          | <b>1.0</b>  | <b>90</b>        | 3.1            | 2.9              | <b>6.67</b> |
| Nitrate/Nitrite | 0.00          | 0.11         | <b>0.10</b> | <b>110</b>       | 0.04           | 0.04             | <b>0.00</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 7.79           | 7.78             | <b>0.13</b> |
| Sulfate         | 0             | 54           | <b>50</b>   | <b>108</b>       | 3050           | 2950             | <b>3.33</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 240            | 225              | <b>6.45</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

# Green Analytical Laboratories

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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |            |                  | Blank Data   |                 |
|-----------------|------------|------------|------------|------------------|--------------|-----------------|
| 808-094         | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 360        | 339        | <b>106</b> | 90-110 %         | <10          | 10              |
| Chloride        | 23         | 22.8       | <b>101</b> | 90-110 %         | <10          | 10              |
| EC *            | NA         | NA         | <b>NA</b>  | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b> | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.50       | 0.50       | <b>100</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 9.05       | 8.90       | <b>102</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 340        | 321        | <b>106</b> | 90-110 %         | <10          | 10              |
| TDS             | 5040       | 4850       | <b>104</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 808-103     | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic     | 0.0000        | 0.053        | <b>0.050</b> | <b>106</b>       | 0.0042         | 0.0040           | <b>4.88</b> |
| Barium      | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0977         | 0.0945           | <b>3.33</b> |
| Boron       | 0.0           | 2.3          | <b>2.000</b> | <b>117</b>       | 0.1            | 0.1              | <b>0.00</b> |
| Cadmium     | 0.00000       | 0.051        | <b>0.050</b> | <b>102</b>       | 0.00107        | 0.00100          | <b>6.76</b> |
| Calcium     | 0.0           | 5.8          | <b>5.0</b>   | <b>116</b>       | 120.0          | 120.0            | <b>0.00</b> |
| Chromium    | 0.000         | 0.052        | <b>0.050</b> | <b>104</b>       | <0.001         | <0.001           | <b>NC</b>   |
| Copper      | 0.0000        | 0.052        | <b>0.050</b> | <b>104</b>       | 0.0068         | 0.0063           | <b>7.63</b> |
| Iron        | 0.00          | 1.17         | <b>1.00</b>  | <b>117</b>       | 0.10           | 0.09             | <b>10.5</b> |
| Lead        | 0.0000        | 0.056        | <b>0.050</b> | <b>112</b>       | 0.0016         | 0.0015           | <b>3.28</b> |
| Magnesium   | 0.0           | 1.2          | <b>1.0</b>   | <b>120</b>       | 14.7           | 14.6             | <b>0.68</b> |
| Manganese * | 0.00000       | 1.24         | <b>1.00</b>  | <b>124</b>       | 0.00900        | 0.00900          | <b>0.00</b> |
| Potassium   | 0.0           | 1.1          | <b>1.0</b>   | <b>110</b>       | 10.8           | 10.8             | <b>0.00</b> |
| Selenium    | 0.000         | 0.276        | <b>0.250</b> | <b>110</b>       | 0.001          | <0.001           | <b>NC</b>   |
| Silver      | 0.00000       | 0.052        | <b>0.050</b> | <b>104</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium      | 0.0           | 59.7         | <b>50.0</b>  | <b>119</b>       | 55.1           | 54.9             | <b>0.36</b> |
| Uranium     | 0.00000       | 0.056        | <b>0.050</b> | <b>112</b>       | 0.00427        | 0.00427          | <b>0.00</b> |
| Zinc        | 0.000         | 0.056        | <b>0.050</b> | <b>112</b>       | 0.009          | 0.009            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 808-103   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.3        | 5.0        | <b>106</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.38       | 5.00       | <b>108</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.69       | 2.50       | <b>108</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.3       | 10.0       | <b>103</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.239      | 0.250      | <b>95.6</b> | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.7        | 8.1        | <b>107</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 808-103     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 3.94         | <b>4.00</b>   | <b>98.5</b>      | 7.10           | 7.00             | <b>1.42</b> |
| Manganese-T | 0.000         | 2.05         | <b>2.00</b>   | <b>103</b>       | 4.40           | 4.30             | <b>2.30</b> |
| Mercury-T   | 0.0000        | 0.0022       | <b>0.0020</b> | <b>110</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |           |                  | Blank Data   |                 |
|-------------|------------|------------|-----------|------------------|--------------|-----------------|
| 808-103     | SRM Result | True Value | SRM % Rec | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 5.09       | 5.00       | 102       | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.65       | 2.50       | 106       | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | 100       | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |       |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------|
| 808-103         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD % |
| Alkalinity      | 0             | 111          | 100         | 111              | 405            | 400              | 1.24  |
| Chloride        | 0             | 105          | 100         | 105              | 1210           | 1180             | 2.51  |
| EC              | NMA           | NMA          | NMA         | NMA              | 894            | 885              | 1.01  |
| Fluoride        | 0.0           | 0.9          | 1.0         | 90               | 3.1            | 2.9              | 6.67  |
| Nitrate/Nitrite | 0.00          | 0.11         | 0.10        | 110              | 0.04           | 0.04             | 0.00  |
| pH              | NMA           | NMA          | NMA         | NMA              | 8.07           | 8.07             | 0.00  |
| Sulfate         | 0             | 54           | 50          | 108              | 3400           | 3300             | 2.99  |
| TDS             | NMA           | NMA          | NMA         | NMA              | 255            | 255              | 0.00  |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.



# Green Analytical Laboratories

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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------------|------------|------------|-------------|------------------|--------------|-----------------|
| 808-103         | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 348        | 339        | <b>103</b>  | 90-110 %         | <10          | 10              |
| Chloride        | 23         | 22.8       | <b>101</b>  | 90-110 %         | <10          | 10              |
| EC              | NA         | NA         | <b>NA</b>   | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b>  | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.50       | 0.50       | <b>100</b>  | 90-110 %         | <0.02        | 0.02            |
| pH              | 9.02       | 8.90       | <b>101</b>  | 90-110 %         | NMA          | NMA             |
| Sulfate         | 340        | 321        | <b>106</b>  | 90-110 %         | <10          | 10              |
| TDS             | 1060       | 1170       | <b>90.6</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#   | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 811-106   | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic   | 0.0000        | 0.051        | <b>0.050</b> | <b>102</b>       | 0.0019         | 0.0016           | <b>17.1</b> |
| Barium    | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.1310         | 0.1260           | <b>3.89</b> |
| Boron     | 0.0           | 2.1          | <b>2.0</b>   | <b>105</b>       | 1.2            | 1.2              | <b>0.00</b> |
| Cadmium   | 0.00000       | 0.049        | <b>0.050</b> | <b>98.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium   | 0.0           | 5.8          | <b>5.0</b>   | <b>116</b>       | 85.5           | 85.4             | <b>0.12</b> |
| Chromium  | 0.000         | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.010          | 0.010            | <b>0.00</b> |
| Copper    | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0066         | 0.0063           | <b>4.65</b> |
| Iron      | 0.00          | 1.16         | <b>1.00</b>  | <b>116</b>       | 0.40           | 0.40             | <b>0.00</b> |
| Lead      | 0.0000        | 0.050        | <b>0.050</b> | <b>100</b>       | 0.0018         | 0.0017           | <b>5.71</b> |
| Magnesium | 0.0           | 0.9          | <b>1.0</b>   | <b>90.0</b>      | 15.0           | 14.9             | <b>0.67</b> |
| Manganese | 0.00000       | 1.06         | <b>1.00</b>  | <b>106</b>       | 0.08000        | 0.08000          | <b>0.00</b> |
| Potassium | 0.0           | 1.2          | <b>1.0</b>   | <b>120</b>       | 0.3            | 0.3              | <b>0.00</b> |
| Selenium  | 0.000         | 0.250        | <b>0.250</b> | <b>100</b>       | 0.030          | 0.029            | <b>3.39</b> |
| Silver    | 0.00000       | 0.053        | <b>0.050</b> | <b>106</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium    | 0.0           | 58.7         | <b>50.0</b>  | <b>117</b>       | 27.8           | 27.8             | <b>0.00</b> |
| Uranium   | 0.00000       | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.00409        | 0.00394          | <b>3.74</b> |
| Zinc      | 0.000         | 0.052        | <b>0.050</b> | <b>104</b>       | 0.310          | 0.299            | <b>3.61</b> |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 811-106   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.2        | 5.0        | <b>104</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.046      | 0.050      | <b>92.0</b> | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.41       | 5.00       | <b>108</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.62       | 2.50       | <b>105</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.8       | 10.0       | <b>108</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.246      | 0.250      | <b>98.4</b> | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.6        | 8.1        | <b>106</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| 811-106     | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 4.01         | <b>4.00</b>   | <b>100</b>       | 6.60           | 5.60             | <b>16.4</b> |
| Manganese-T | 0.000         | 2.12         | <b>2.00</b>   | <b>106</b>       | 0.121          | 0.112            | <b>7.73</b> |
| Mercury-T   | 0.0000        | 0.0021       | <b>0.0020</b> | <b>105</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| PARAMETER   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 4.94       | 5.00       | <b>98.8</b> | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.62       | 2.50       | <b>105</b>  | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | <b>100</b>  | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

# Green Analytical Laboratories

## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 811-106         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 102          | <b>100</b>  | <b>102</b>       | 1580           | 1570             | <b>0.63</b> |
| Chloride        | 0             | 96           | <b>100</b>  | <b>96</b>        | 580            | 560              | <b>3.51</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 711            | 709              | <b>0.28</b> |
| Fluoride        | 0.0           | 1.0          | <b>1.0</b>  | <b>100</b>       | 0.5            | 0.5              | <b>0.00</b> |
| Nitrate/Nitrite | 0.00          | 0.12         | <b>0.10</b> | <b>120</b>       | 0.66           | 0.65             | <b>1.53</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 8.01           | 8.00             | <b>0.12</b> |
| Sulfate         | 0             | 51           | <b>50</b>   | <b>102</b>       | 1850           | 1800             | <b>2.74</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 310            | 310              | <b>0.00</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.

# Green Analytical Laboratories

## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |            |                  | Blank Data   |                 |
|-----------------|------------|------------|------------|------------------|--------------|-----------------|
| 811-106         | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 186        | 179        | <b>104</b> | 90-110 %         | <10          | 10              |
| Chloride        | 48         | 47.5       | <b>101</b> | 90-110 %         | <10          | 10              |
| EC *            | NA         | NA         | <b>NA</b>  | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b> | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.52       | 0.50       | <b>104</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 7.37       | 7.40       | <b>100</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 325        | 321        | <b>101</b> | 90-110 %         | <10          | 10              |
| TDS             | 3340       | 3100       | <b>108</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.

# Green Analytical Laboratories

## DISSOLVED METALS SPIKE AND DUPLICATE DATA

| LAB ID#   | Spike Data    |              |              |                  | Duplicate Data |                  |             |
|-----------|---------------|--------------|--------------|------------------|----------------|------------------|-------------|
| 811-115   | Sample Result | Spike Result | Spike Conc.  | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Arsenic   | 0.0000        | 0.045        | <b>0.050</b> | <b>90.0</b>      | 0.0008         | 0.0008           | <b>0.00</b> |
| Barium    | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0174         | 0.0167           | <b>4.11</b> |
| Boron     | 0.0           | 2.2          | <b>2.0</b>   | <b>110</b>       | 0.3            | 0.2              | <b>8.33</b> |
| Cadmium   | 0.00000       | 0.050        | <b>0.050</b> | <b>100</b>       | <0.00005       | <0.00005         | <b>NC</b>   |
| Calcium   | 0.0           | 5.1          | <b>5.0</b>   | <b>102</b>       | 101.0          | 101.0            | <b>0.00</b> |
| Chromium  | 0.000         | 0.052        | <b>0.050</b> | <b>104</b>       | <0.001         | <0.001           | <b>NC</b>   |
| Copper    | 0.0000        | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.0091         | 0.0079           | <b>14.1</b> |
| Iron      | 0.00          | 1.00         | <b>1.00</b>  | <b>100</b>       | <0.05          | <0.05            | <b>NC</b>   |
| Lead      | 0.0000        | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.0000         | 0.0000           | <b>0.00</b> |
| Magnesium | 0.0           | 1.0          | <b>1.0</b>   | <b>100</b>       | 16.5           | 16.4             | <b>0.61</b> |
| Manganese | 0.00000       | 1.080        | <b>1.00</b>  | <b>108</b>       | <0.005         | <0.005           | <b>NC</b>   |
| Potassium | 0.0           | 1.0          | <b>1.0</b>   | <b>100</b>       | 1.8            | 1.7              | <b>5.71</b> |
| Selenium  | 0.000         | 0.235        | <b>0.250</b> | <b>94.0</b>      | 0.006          | 0.006            | <b>0.00</b> |
| Silver    | 0.00000       | 0.049        | <b>0.050</b> | <b>98.0</b>      | <0.00005       | <0.00005         | <b>NC</b>   |
| Sodium    | 0.0           | 53.1         | <b>50.0</b>  | <b>106</b>       | 445.0          | 444.0            | <b>0.22</b> |
| Uranium   | 0.00000       | 0.048        | <b>0.050</b> | <b>96.0</b>      | 0.01230        | 0.01200          | <b>2.47</b> |
| Zinc      | 0.000         | 0.049        | <b>0.050</b> | <b>98.0</b>      | 0.007          | 0.007            | <b>0.00</b> |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.



# Green Analytical Laboratories

## DISSOLVED METALS SRM AND BLANK DATA

| LAB ID#   | SRM Data   |            |             |                  | Blank Data   |                 |
|-----------|------------|------------|-------------|------------------|--------------|-----------------|
| 811-115   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Arsenic   | 0.048      | 0.050      | <b>96.0</b> | 90-110 %         | <0.0005      | 0.0005          |
| Barium    | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.0005      | 0.0005          |
| Boron     | 5.1        | 5.0        | <b>102</b>  | 90-110 %         | <0.1         | 0.1             |
| Cadmium * | 0.056      | 0.050      | <b>112</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Calcium   | 5.0        | 5.0        | <b>100</b>  | 90-110 %         | <0.5         | 0.5             |
| Chromium  | 0.050      | 0.050      | <b>100</b>  | 90-110 %         | <0.001       | 0.001           |
| Copper    | 0.052      | 0.050      | <b>104</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Iron      | 5.30       | 5.00       | <b>106</b>  | 90-110 %         | <0.05        | 0.05            |
| Lead      | 0.051      | 0.050      | <b>102</b>  | 90-110 %         | <0.0001      | 0.0001          |
| Magnesium | 4.9        | 5.0        | <b>98.0</b> | 90-110 %         | <0.5         | 0.5             |
| Manganese | 2.59       | 2.50       | <b>104</b>  | 90-110 %         | <0.005       | 0.005           |
| Potassium | 10.6       | 10.0       | <b>106</b>  | 90-110 %         | <0.5         | 0.5             |
| Selenium  | 0.256      | 0.250      | <b>102</b>  | 90-110 %         | <0.001       | 0.001           |
| Silver    | 0.055      | 0.050      | <b>110</b>  | 90-110 %         | <0.00005     | 0.00005         |
| Sodium    | 8.5        | 8.1        | <b>105</b>  | 90-110 %         | <0.5         | 0.5             |
| Uranium   | 0.049      | 0.050      | <b>98.0</b> | 90-110 %         | <0.00001     | 0.00001         |
| Zinc      | 0.047      | 0.050      | <b>94.0</b> | 90-110 %         | <0.001       | 0.001           |

NA=Data not available.

# Green Analytical Laboratories

## TOTAL METALS SPIKE AND DUPLICATE DATA

| LAB ID#     | Spike Data    |              |               |                  | Duplicate Data |                  |             |
|-------------|---------------|--------------|---------------|------------------|----------------|------------------|-------------|
| PARAMETER   | Sample Result | Spike Result | Spike Conc.   | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Iron-T      | 0.00          | 3.97         | <b>4.00</b>   | <b>99.3</b>      | 4.40           | 3.90             | <b>12.0</b> |
| Manganese-T | 0.000         | 2.08         | <b>2.00</b>   | <b>104</b>       | 0.100          | 0.100            | <b>0.00</b> |
| Mercury-T   | 0.0000        | 0.0020       | <b>0.0020</b> | <b>100</b>       | <0.0002        | <0.0002          | <b>NC</b>   |

NC=Not calculated due to results less than the detection limit.

NA=Data not available.

# Green Analytical Laboratories

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## TOTAL METALS SRM AND BLANK DATA

| LAB ID#     | SRM Data   |            |             |                  | Blank Data   |                 |
|-------------|------------|------------|-------------|------------------|--------------|-----------------|
| PARAMETER   | SRM Result | True Value | SRM % Rec   | Acceptance Range | Blank Result | Reporting Limit |
| Iron-T      | 4.89       | 5.00       | <b>97.8</b> | 90-110 %         | <0.05        | 0.05            |
| Manganese-T | 2.59       | 2.50       | <b>104</b>  | 90-110 %         | <0.005       | 0.005           |
| Mercury-T   | 0.002      | 0.002      | <b>100</b>  | 90-110 %         | <0.0002      | 0.0002          |

NA=Data not available.

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## WET CHEM SPIKE AND DUPLICATE DATA

| LAB ID#         | Spike Data    |              |             |                  | Duplicate Data |                  |             |
|-----------------|---------------|--------------|-------------|------------------|----------------|------------------|-------------|
| 811-115         | Sample Result | Spike Result | Spike Conc. | Spike % Recovery | Sample Result  | Duplicate Result | RPD %       |
| Alkalinity      | 0             | 102          | <b>100</b>  | <b>102</b>       | 1580           | 1570             | <b>0.63</b> |
| Chloride        | 0             | 103          | <b>100</b>  | <b>103</b>       | 23             | 22               | <b>4.44</b> |
| EC              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 626            | 624              | <b>0.32</b> |
| Fluoride        | 0.0           | 1.0          | <b>1.0</b>  | <b>100</b>       | 1.5            | 1.5              | <b>0.00</b> |
| Nitrate/Nitrite | 0.00          | 0.12         | <b>0.10</b> | <b>120</b>       | 0.66           | 0.65             | <b>1.53</b> |
| pH              | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 7.78           | 7.76             | <b>0.26</b> |
| Sulfate         | 0             | 52           | <b>50</b>   | <b>104</b>       | 9600           | 9400             | <b>2.11</b> |
| TDS             | NMA           | NMA          | <b>NMA</b>  | <b>NMA</b>       | 5620           | 5560             | <b>1.07</b> |

NMA=Data not applicable to Method.

NC=Not calculated due to results less than the detection limit.



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## WET CHEM SRM AND BLANK DATA

| LAB ID#         | SRM Data   |            |            |                  | Blank Data   |                 |
|-----------------|------------|------------|------------|------------------|--------------|-----------------|
| 811-115         | SRM Result | True Value | SRM % Rec  | Acceptance Range | Blank Result | Reporting Limit |
| Alkalinity      | 186        | 179        | <b>104</b> | 90-110 %         | <10          | 10              |
| Chloride        | 23         | 20.9       | <b>110</b> | 90-110 %         | <10          | 10              |
| EC *            | NA         | NA         | <b>NA</b>  | 90-110 %         | NMA          | NMA             |
| Fluoride        | 1.0        | 1.0        | <b>100</b> | 90-110 %         | <1.0         | 1.0             |
| Nitrate/Nitrite | 0.52       | 0.50       | <b>104</b> | 90-110 %         | <0.02        | 0.02            |
| pH              | 7.37       | 7.40       | <b>100</b> | 90-110 %         | NMA          | NMA             |
| Sulfate         | 345        | 321        | <b>107</b> | 90-110 %         | <10          | 10              |
| TDS             | 3340       | 3100       | <b>108</b> | 90-110 %         | <10          | 10              |

NMA=Data not applicable to Method.

NA=Data not available.