

Flood Control System Component Optimization: HEC-1 Capability

October 1974

revised: September 1977

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INTRODUCTION

HEC-1 has been augmented to provide the capability of automatically determining the sizes of flood control system measures that result in maximizing total system net economic benefits subject to possible hydrologic performance targets. The system flood control measures that can be automatically sized are:

. Detention storage reservoir(s)

. Pumping plant(s)

Diversion(s)

 Local protection(s), i.e., channel modification, levee, floodwall

This document presents detailed illustrated examples of facility optimization using HEC-1. The examples are designed to assist in data assembly and coding, output interpretation, and study management.

Examples included are constructed in building block sequence to illustrate the relationships between the hydrologic, economic and cost data and demonstrate selected capability. Examples illustrated include:

- Hydrologic Model for existing conditions.

- Economic evaluation of existing conditions.

- Optimization of Reservoir and Pumping Plant with no hydrologic constraints.

- Optimization of Reservoir and Pumping Plant with hydrologic performance constraints.

- Optimization of Reservoir, Pumping Plant and Diversion (unconstrained).

- Optimization of local protection projects; levee and channel modification (unconstrained).

- Optimization of Reservoir, Pumping Plant and local protection projects with uniform local protection level.

The basic reference for HEC-l is the Users Manual listed as reference 1. The input data supplement, reference 2, updates Addendum 6 of reference 1 to include the facility optimization capability. Technical Paper No. 42, reference 3, describes the conceptual basis for the optimization problem and explains the characteristics of the flood control measures (except for the local protection capability that has recently been added) and a field application. Reference 4 summarizes various optimization algorithms and also includes a list of references pertinent to the subject matter presented herein. Reference 5 describes in detail the methodology involved in the calculation of expected annual damages.

BASIC EXAMPLE DESCRIPTION

The study area lies in the flood plain of a large river and is presently protected (to a degree) by a major levee. The levee greatly restricts outflow from the study area. Most of the storm runoff (within the study area) originates from the higher elevations (bluff areas), and most flooding occurs in the lower reaches of the study streams. Development in the flood hazard areas consists of agricultural crops, industrial-commercial areas and residential development. Figure 1 is a general map and schematization of the example area.

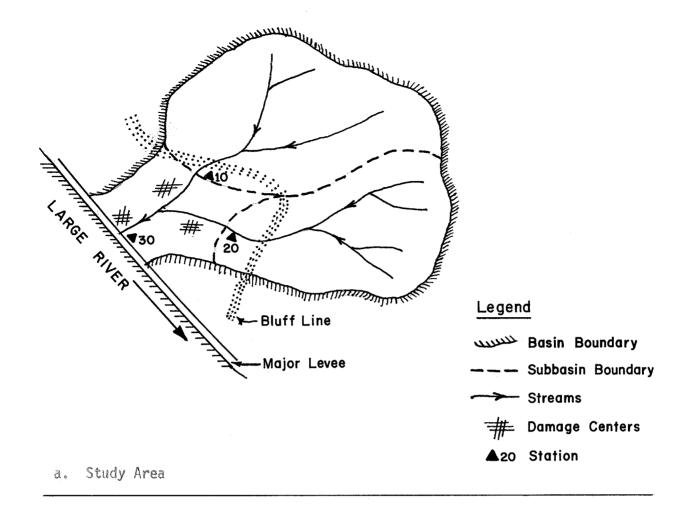
Proposals for protecting vulnerable areas from potential flooding include a detention storage reservoir at station 10, channel modification from station 10 to 30, levee from station 20 to 30, flow diversion (bypass) from station 20 to 30, and a pumping facility with forebay ponding at the basin outlet, station 30 (see Figure 1-a).

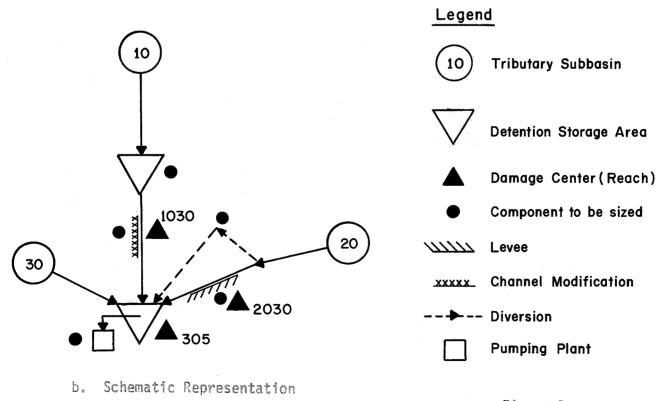
HYDROLOGIC MODEL

The hydrologic model for existing conditions is needed to define the <u>base</u> hydrology and provide a mechanism for evaluating the performance of proposed alternatives. Care must be taken in developing the base model to assure that all feasible alternatives can be easily evaluated and that the pattern hydrologic event is reasonably representative for the area, i.e., will not bias evaluation of alternatives. Data required for coding the basic hydrologic model is given in reference 1.

Since the primary objective of this supplement is illustration of flood control system component optimization, the hydrologic model has been kept simple in that discharge hydrographs of a specific event are read in rather than computed from rainfall-runoff relations during the optimization. (The hydrographs were essentially computed in a previous run). A hypothetical event was synthesized that ranged in frequency from the annual event (1.0 exceedence frequency) in the upper basin reaches to about the 5-year event (.2 exceedence frequency) in the lower basin. Channel routing criteria has been developed for the streams from multiple water surface profile calculations and for the restricted outlet at station 30 from the geometry of the outflow culvert and local topography. Table 1 (Appendix A) contains a tabulation of the hydrologic data for existing conditions.

Exhibit 1, page 1 of 2, is a listing of the HEC-1 input data for the hydrologic model. The hydrologic simulation of existing conditions indicates that for the selected event, the peak flows at stations 10, 20 and 30 are 5,370 cfs, 5,370 cfs and 10,154 cfs, respectively. The maximum storage level achieved at station 30 is 9,557 ac.ft. (maximum storage at station 30 not shown in computer printout included) and the peak outflow is 1,200 cfs.





ECONOMIC EVALUATION—EXISTING CONDITIONS

The economic evaluation for existing conditions provides the base from which economic benefits of alternatives may be evaluated. The economic evaluation of flood damages requires that flow-damage-frequency analysis be performed to develop "expected" (or average) annual damages. Reference 3 and Addendum 3 of reference 1 discuss the general application of flood damage frequency analysis to flood alternative evaluations and describe the concepts embodied in HEC-1.

The information required (in addition to the hydrologic model) is flow (or storage) - damage relationships and exceedence frequency relations at the damage centers. Additional coding is required to set up the multiplan feature of HEC-I and establish the range of floods needed to evaluate the hydrologic and economic effects of alternatives.

The damages in reaches 1030 and 2030 are mostly rural and result from overflow from the respective stream channels. Damage surveys have developed relationships between stage and damages for these reaches for a number of categories of damages. Water surface profile studies developed rating curves for the index stations as shown on Figure 1 so that flow-damage functions, as required by HEC-1, could be developed. The damages at location 305 are mostly urban, commercial and industrial (and are thus large) and occur because of ponding behind the levee. In HEC-1 storage is used instead of stage to represent level and thus a storage-damage function has been developed at this site. Storage is analogous to stage and the function is developed from the usual stage-damage relationship and a site stage-storage relationship.

The required exceedence frequency relationships for stations 10 and 20 were based on a partial duration series analysis because significant damages occur from events that occur more frequently than the annual event. These curves were developed from regional relationships developed in other studies. The required frequency relationship for station 30 is storage-exceedence frequency. This function was derived by developing synthetic events that would reproduce the regional curves at station 10 and 20, simulating the hydrologic operation of the system for these events, and plotting the resulting peak storage levels for these events versus their exceedence frequencies. Table 2 (Appendix A) contains the economic and frequency data for the damage centers.

The determination of the range of floods needed requires evaluation of the exceedence frequency relations, base hydrology and damage relations. The objective in developing the range of floods (multi-plan flood ratios) is to provide for <u>automatic</u> revision of the exceedence frequency relationship so that expected annual damages can be computed for alternative proposals. The procedure used for automatically revising the frequency curve is explained in Addendum 3 of reference 1. To accomplish this, the

ratios should develop floods that cover the range of damaging floods at all damage centers; in our example, the range extends from the six times per year event at damage centers 1030 and 2030 to above the .005 event at 305. The ratios contained in Table 2 (Appendix A) when applied to the synthetic event of the hydrologic model adequately cover the range.

The multi-plan coding has been prepared for two plans, which is necessary for the optimization examples following. The two plans are both for existing conditions which is of course redundant. If the multi-plan capability were being applied by itself, coding should be for as many alternatives as is desired for study. Exhibit 2, pages 1 and 2, are a complete listing of data input with notations as to revisions required from the basic hydrologic model and additions for the multi-plan evaluation.

The output for a multi-plan run includes complete hydrologic simulation for existing conditions and the proposed plan of improvement (none for example) for each of the range of runoff events (nine for the example) and integration of the damage relationships. The results indicate expected annual damages under existing conditions are \$33,580, \$33,580 and \$1,110,210 for damage reaches 1030, 2030 and 305, respectively.

The economic output (printout for station 1030 is page 3 of Exhibit 2) begins with a printout of control codes and includes (1) a listing of data input (ECONOMIC DATA FOR STATION 1030 PLAN 1) which includes exceedance frequency in events per year, peak flow and damages, (2) computation of expected annual damages (FLOOD DAMAGES FOR STATION 1030 PLAN 1) which includes allocation of probability intervals (PROB INT) to the range of flood events (FLOW) and incremental computed damage contribution to expected annual damages (SUM, TYPE 1, etc.) that are based on the product of PROB INT and damage associated with FLOW, and (3) the same information for the alternative plan. If the alternative plan had reduced annual damages, then the benefits (AVG ANN BFT) would be positive and equal to the difference between PLAN 1 and PLAN 2.

FLOOD CONTROL MEASURE OPTIMIZATION

The information required in addition to the hydrologic model and multi-plan economic data for flood control measure optimization are the performance parameters and cost relationships for the flood control features being considered. The mathematical structure for the optimization and the search strategy are discussed in detail in reference 3. It should be remembered (or understood) that economic optimum is achieved when the facilities are sized such that the computed difference between expected annual benefits and expected annual costs is maximized. The solution may proceed unconstrained or it can be constrained such that a minimum hydrologic performance at specified control points must be accomplished simultaneously with the net benefit maximization.

The general technique used is to successively operate the multi-plan simulation in a controlled fashion while automatically adjusting component sizes toward optimum.

SIZING RESERVOIR AND PUMPING PLANT — UNCONSTRAINED

The first optimization example will be the determination of the optimum (economic) sizes for a reservoir located at station 10 and a pumping plant to be located at station 30 that discharges through (or over) the levee. There is no minimum constraining hydrologic performance required. Information must therefore be assembled and coded that will describe, in a general way, the cost and performance of the storage reservoir and a pumping facility.

a. Detention Storage. — The detention storage reservoirs that may be considered with HEC-1 are those for which it is possible to define the operating characteristics as unique functions of the storage contents within the reservoirs. A reservoir with an uncontrolled outlet works exactly meets this requirement. To provide capability for automatic adjustment of operating characteristics (as is required for automatic optimization), a reservoir is characterized by (1) the outflow characteristics of a low level outlet, which is defined by the centerline elevation of the outlet and an orifice equation of the form:

where

C = orifice discharge coefficient

A = outlet area

H = head on low level outlet

g = acceleration of gravity

EXP = exponent dependent on tailwater conditions, 0.5 if no tailwater

and (2) the overflow characteristics of a spillway which is defined by a weir equation of the form:

$$Q = C_*LH_*^{3/2}$$
....(2)

where

C* = weir discharge coefficient

L = length of spillway

 H_* = head on spillway

and (3) the site storage characteristics which are defined by an elevation-storage capacity relationship. For an <u>index storage</u> to be optimized, which is the <u>storage at the elevation of the spillway crest</u>, the above relationships are merged to define the reservoir's outflow as a function of the storage level in the reservoir (Modified Puls method of routing).

Two modes are possible for a reservoir optimization. In the usual mode (for our example) a reservoir that can be characterized by a low level outlet and an overflow weir as described above will be automatically adjusted in its index storage capacity, along with all other system components, to achieve the minimum value of the objective function (defined in reference 3). The alternative mode, not illustrated, permits optimization of the size of the low level outlet assuming the reservoir does not spill, which is appropriate for pondage in low lying areas.

The cost relationships for the reservoir in the usual mode consists of a capital cost function and an associated capital recovery factor for converting the capital cost to annual cost, and the annual cost of operation, maintenance and replacement expressed as a proportion of capital cost. The capital cost function includes land acquisition and construction costs, interest during construction, etc., expressed as a function of the index storage size of the reservoir. The capital cost for a specific reservoir size being evaluated during optimization is interpolated from this function and the equivalent annual cost is computed as the product of the capital cost and the capital recovery factor for the appropriate discount rate. The annual cost of operation, maintenance and replacement is the product of the annual cost of operation and the interpolated capital cost. The total annual cost of the reservoir is the sum of these two costs. Table 3 (Appendix A) contains the data describing the performance and cost of the proposed reservoir.

Pumping Plant — A pumping facility removes volume from the system at a rate equal to the pumping capacity. The performance characteristics of a pumping plant are defined by an initial threshold water level at which the pump is activated and the discharge capacity of the pumping facility. In this analysis, it is assumed that water pumped from the system does not later appear at other locations in the system. The cost of a pumping facility is computed from a capital cost function and an associated capital recovery factor for converting to equivalent annual cost, the annual operation, maintenance and replacement cost that is a proportion of the capital cost, and the annual power cost. The power cost is adjusted if the volume to be pumped changes as the system components sizes are being optimized. It can be demonstrated that no matter the pumping capacity, the power costs would not materially change if the volume to be pumped does not change. The annual power costs are therefore adjusted only for water that is removed from the system by diversions or other pumping facilities. The annual cost is the sum of the equivalent annual cost, annual operation and maintenance cost, and annual power cost. Table 4 (Appendix A) contains the data describing the performance and cost of the proposed pumping plant.

The coding requires initial estimates for the facility sizes (starting values) and a number of control codes to indicate location and type of facility to be sized. The starting values selected were 10,000 ac.ft. and 4,000 cfs for the reservoir and pumping plant, respectively. Exhibit 3, pages 1 and 2, are a listing of the input data for this example including notations of revisions and additions to the data required for the multi-plan evaluation example.

Exhibit 3, pages 3 - 43, are reproductions of the complete output from the optimization run. The output of an optimization run includes:

- 1. The derived optimum size for each facility in the system included in the optimization (page 43).
- Complete hydrologic simulation of the system with and without the optimally sized facilities for the range of floods processed (nine for this example) (pages 6 - 42).
- 3. Economic expected annual damage analysis with and without the optimally sized facilities for each damage center in the system (pages 17, 24 and 41).
- Costs for the derived system facilities (pages 11 and 40).
- 5. A summary of system cost, performance and net benefits (page 42).

The derived optimum sizes are 9,119 ac.ft. for the reservoir and 2,885 cfs for the pumping plant (summary page 43). The total capital cost is \$7,497,000 and system annual net benefits are \$173,000 (benefit cost ratio of 1.26). The derived values were adjusted from the starting values of 10,000 ac.ft. and 4,000 cfs which corresponded to a capital cost of \$8,740,000 and system net benefits of 158,000 (page 43). It is necessary, in each case, to test for possible local optima in the search procedure. This was accomplished by making a separate run with starting values of 3,000 ac.ft. and 500 cfs respectively. The derived sizes were 6,584 ac.ft. and 2,835 cfs costing \$6,591,000 and resulting in annual system net benefits of \$199.000. The results indicated that a local optimum did exist such that additional runs were made with different initial values until it could be reasonably concluded that the proper sizes were 6,584 ac.ft. for the reservoir and 2,835 cfs for the pumping plant.

The hydrologic performance can be characterized by the "degree of protection" provided, i.e., the exceedence frequency of the threshold of damaging flow. At damage center 1030, the zero damage exceedence frequency was reduced from about the 5 times per year event to about the annual event (deduced from page 17 and the additional runs made). Note that damages at station 1030 are quite small in relation to those at 305 and therefore probably had very little influence on the determination of the optimum sizes.

At damage center 305, the frequency of significant damages was reduced from about the 3-year exceedence interval event to about the 10-year event, which incidentally reduced expected annual damages by more than half.

Detailed study of the output can provide insight into the optimization methodology as well as the sensitivity of the system performance to a range of facility sizes. Pages 3 through 6 of Exhibit 3 contain detailed output on the progress of the optimization. The variables for optimization printed on page 3 are defined below and a review of the search procedure (reference 3) and the corresponding results from the output are described.

Variable Definition

NC = Counter denoting stage in search cycle (1-3)

M = Variable that is being adjusted for this cycle (corresponds to fields on J2 card listed above as SYSTEM OPTIMIZATION)

M1 = Next variable to be adjusted (optimized)

VAR(M) = Current value of variable M

VAR(M1) = Current value of variable M1

OBJ DEV = Used in connection with hydrologic performance constraint; described in example in next section

TANCST = Total annual cost of facilities at current values

ANDMG = Total annual damage for all damage centers for facilities at current values

O FTN(NC) = Objective function that is being minimized; in this example it is the sum of TANCST and ANDMG

Search Procedure (see reference 3)

(1) First, trial sizes of all system components are nominated and the entire system is simulated in all of its hydrologic, costs, and economic detail to calculate the value of the objective function, which for unconstrained optimization is the sum of the equivalent annual cost (TANCST) and annual damage (ANDMG).

The first value (NC=1) of the objective function is 1018.883

(2) Then the size of one component is decreased by a small selected amount (1 percent) and the simulation is repeated for the entire system to compute a new value of the objective function. This is repeated again resulting in three unique values of the objective function for small changes in the size of one component.

The values of the variable and objective function are

NC	VAR(M)	O FTN(NC)
1 f(X ₀)	10000	1018.883
2 f($X_0 - \Delta X$)	9900	1018.205
2 f($X_0 - \Delta X$) 3 f($X_0 - 2\Delta X$)	9800	1017.645

(3) From these three values, an estimate is made of the component size that would result in the minimum value of the objective function. The computation of the adjustment is shown in Figure 2 and proceeds as follows:

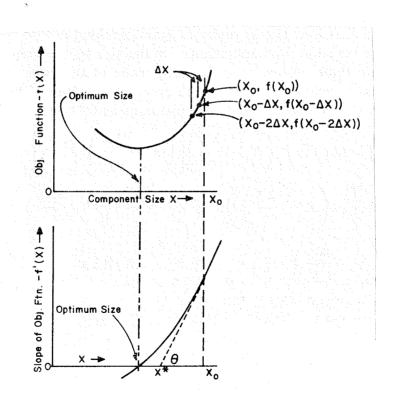


Figure 2.— Adjustment of Component Size by Newton-Raphson Convergence Procedure

$$f''\left(X_o - \frac{\Delta X}{2}\right) = \tan\theta = f'\left(X_o - \frac{\Delta X}{2}\right) \left[\left(X_o - \frac{\Delta X}{2}\right) - X^*\right]^{-1} \dots (3)$$

or
$$X^* = X_o - \left[f' \left(X_o - \frac{\Delta X}{2} \right) \right] \left[f'' \left(X_o - \frac{\Delta X}{2} \right) \right]^{-1} - \frac{\Delta X}{2} \dots \dots (4)$$

and $\triangle X$ = incremental change in X; X = size of variable being optimized; X_O = present size of component X; and X* = projected "new" size for X. The calculation for adjustment of VAR(M) is as follows:

$$f'''(X_0 - \frac{\Delta X}{2}) = [1017.645 - 2(1018.205) + 1018.883]/\Delta X^2 ...(8)$$

$$X_0 = 10000; \Delta X = (.01) (10000) = 100$$

$$X^* = 10000 - \frac{0.678/100}{.118/(100)^2} - \frac{100}{2} = 9380.$$
 (to closest 10) . . .(9)

(4) After adjustment of the size of the system component, the entire system is simulated again in detail to compute the new value of the objective function and, provided the objective function has decreased, the procedure then moves to the second system component whose scale is to be optimized.

The output at this stage reads:

VAR 1 ADJ FROM 10000. to 9384.07

and one cycle for one variable has been completed.

(5) The above procedure is repeated for the second and all subsequent components to be optimized.

Note that the same procedure is repeated for variable 9.

- (6) A single adjustment has now been made for each component for one complete search of the system component sizes. The procedure is then repeated for two more complete system searches.
- (7) The component whose change contributed the most to decreasing the objective function is adjusted next before another complete system search is performed.
- (8) The procedure is terminated when either no more improvement in the objective function can be made (within a tolerance) for the component making the greatest contribution to decreasing the objective function, or the complete search cycle is completed.

Note that occasionally no successful adjustment can be made. If the computed adjustment does not reduce the objective function, its value is successively reduced to the original value, testing for improvement at a number of steps (pages 5 and 6 of Exhibit 3).

The remaining output should be self-explanatory. Remember the output is for two plans (existing and the derived system) for nine flood events which results in 18 hydrologic simulations at each control point and two economic evaluations at all damage centers.

SIZING RESERVOIR AND PUMPING PLANT —— HYDROLOGIC PERFORMANCE CONSTRAINED

The objective for this example is to determine the size of the facilities that will maximize the system net benefits while simultaneously meeting hydrologic performance targets expressed in terms of desired flow (storage) target and corresponding exceedence frequency. This example extends the previous example for the performance targets of

Reach	Target Value	Exceedence Frequency (Events per Year)
1030 305	1200 cfs 5000 ac.ft.	1.0

The starting values were selected as 5000 ac.ft. and 5000 cfs, respectively.

Pages 1 and 2 of Exhibit 4 contain a listing of the input data with notations on coding revised and added. Pages 3 through 28 contain printout of selected pages of the output.

The derived optimum sizes are 7528 ac.ft. for the reservoir and 6044 cfs for the pumping plant (summary page 28). The total capital cost is \$9,889,000 and system annual net benefits are \$123,000 (benefit cost ratio

of 1.15). The derived values were adjusted from starting values of 5000 ac.ft. and 5000 cfs, respectively. The sensitivity of the solution to starting values was tested by making a separate run with starting values of 10,000 ac.ft. and 7000 cfs, respectively. The derived sizes were 6,007 ac.ft. and 6,570 cfs costing \$9,832,000 and resulting in annual net benefits of \$102,000. The hydrologic performance specified is achieved in that the degree of protection provided is 1.0 years (protection against the annual event) for reach 1030 and .05 (protection against the 20-year event) for reach 305 (see pages 15 and 26 of Exhibit 4).

President A

The output detailing the progress of the optimization contains additional information related to the performance target constraints. The additional variables are (page 3, Exhibit 4):

Variable Definition

ISTA = Station where performance target specified

INT FLOW = Flow corresponding to the target exceedence frequency for the current values of the variables

TRG FLOW = Target flow for the target exceedence frequency

FLW OBJ = Component of penalty applied to objective function because of failure to meet target (illustrated later) for this station

FLW DEV = Difference between INT FLW and TRG FLW

OBJ DEV = Penalty applied to objective function because of failure to meet target (multiply)

The additional printout occurs for all stations where performance targets are specified (as many as desired). The optimization proceeds exactly as the previous (unconstrained) example except that the objective function is penalized whenever the performance targets are not met. Note that the first objective function is extremely large (.951E+06) because of the large penalty from not meeting the target for station 305 while the objective function when optimization is complete (page 10, Exhibit 4) essentially has no penalty (.106E+04). The computation of a value of the objective function for the condition blocked out on page 5 (Exhibit 4) will illustrate the role of the penalty assessment. See reference 3 for a description of the objective function.

FLW OBJ = $[(FLW DEV)/(.10 TRG FLOW)]^4$

Station 1030

FLW OBJ =
$$\left(\frac{12.670}{120}\right)^4 = .0001$$

Station 305

FLW OBJ =
$$\left(\frac{782.138}{500}\right)^4 = 5.988$$

Objective Function Assessment

OBJ DEV = .0001 + 5.988 = 5.988

0 FTN(NC) = (TANCST + ANDMG) (OBJ DEV + 1)

0 FTN(NC) = (774.217 + 265.434) (5.988 + 1) = 7264.80

The printout at the bottom of the pages on which economic output is shown (page 15 for example) summarizes the performance target and final regulated values.

SIZING RESERVOIR, PUMPING PLANT AND DIVERSION

A proposal offered at past public meetings has been to divert a portion of the runoff from subbasin 20 at station 20 into the adjacent watershed (which is presently undeveloped) both to reduce flooding in the downstream reaches and increase wetlands in the adjacent watershed to improve wildlife habitat. This example extends the previous reservoir and pumping plant example (unconstrained) to include a diversion from station 20.

A diversion transfers flow between locations within the system. The performance characteristics are defined by a threshold flow and a diversion capacity. The concept of the diversion relationship is indicated in figure 3. Water diverted may be returned to the system at any downstream location so that it is possible to characterize facilities which would bypass a portion of flood flows around a damage center. Flow may also be permanently diverted from the system, which will be done for this example. The cost is characterized similar to a pumping plant by a capital cost function, a capital recovery factor and annual operation, maintenance and replacement factor.

Table 5 (Appendix A) summarizes the performance and cost data for the proposed diversion.

The coding to include a diversion at station 20 is noted on the listing of input data, pages 1 and 2 of Exhibit 5. Note that it was necessary to include a dummy reservoir at station 20 in order to accommodate the requirements for a diversion.

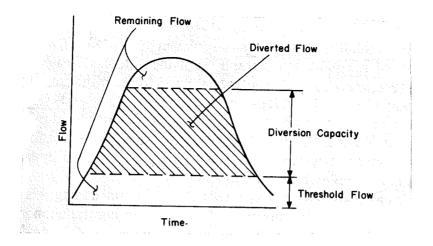


Figure 3. — Effect of Diversion on Flood Hydrograph

Pages 3 through 34 of Exhibit 5 contain selected pages of the output. The derived optimum sizes are 6620 ac.ft. (index storage) for the reservoir, 863 cfs for the diversion and 2250 cfs for the pumping plant (summary page 34). The total capital cost is \$7,099,000 and system net benefits are \$197,000 (benefit cost ratio of 1.33). The derived values were adjusted from starting values of 4000 ac.ft., 500 cfs and 1000 cfs, respectively, for the reservoir, diversion, and pumping plant. The sensitivity of the solution to starting values was tested by making a separate run with new starting values of 10,000 ac.ft., 3000 cfs and 4000 cfs, respectively. The derived sizes were 6648 ac.ft., 1393 cfs and 2160 cfs, respectively, costing \$7,617,000 and resulting in annual net benefits of \$167,000. In comparison with the previously derived values, it appears the diversion should be the smaller size. Additional runs demonstrate the value of testing a few starting values in an effort to locate a reasonable optimum.

The hydrologic performance of the derived system can be characterized by the degree of protection provided, i.e., the exceedence frequency of the threshold of damaging flows. At control point 1030, the 0 damage exceedence frequency was reduced from about the five times per year event to about the annual event (about the same as the example without the diversion). At control point 2030, the 0 damage exceedence frequency was not materially changed from the five times per year event. At control point 305, the frequency of significant damage was reduced from about the 3-year exceedence interval event to between the 10 and 15-year events. The residual damages for the system are reduced to about 1/3 of the damages under existing conditions.

SIZING LOCAL PROTECTION PROJECTS

Local protection projects include levees, floodwalls and channel modifications. Ignoring for the moment natural valley storage effects, the hydrologic and economic effects of local projects are truly local,

i.e., do not interact with the system hydrology. If this is the case, and it will be unless the modification is extensive, then a local project can be completely characterized performance-wise by a design Q (or storage) and a flow (or storage) damage function. Damages are usually negligible below the design flow and follow a curve related to the local site hydraulics and damage potential above this point. A levee or floodwall essentially truncates the damage function below the design flow (basic hydraulic-economic relationship unchanged) while channel modifications lower the relationship in response to the improved conveyance characteristics.

The concept embodied in HEC-1 is that a design flow is associated with a unique damage relationship and therefore if the range of feasible design flows are known, the relationship for a specific design flow within the feasible range could be determined. The relationship (flow or storage-damage) for a specific design flow is determined by interpolating between the relationships defining the feasible range. The relationships defining the feasible range are termed "pattern functions;" the minimum design damage function corresponding to the design flow considered the lowest value feasible and the maximum design damage function corresponding to the design flow considered the highest value feasible.

The local projects considered for this example are a channel modification for reach 1030 and a levee for reach 2030. The pattern damage functions for reach 1030 were developed from water surface profile and economic The minimum design damage function corresponds to a "clear and snag" alternative and was constructed by computing water surface profiles for a smoothed boundary to develop a rating curve at the index station that was subsequently combined with an area, elevation, damage relationship. The design flow associated with this function is 1700 cfs, the lower limit of design flow. The maximum design function corresponds to a 40 ft. bottom width, 2 to 1 side slope channel enlargement and was constructed by computing water surface profiles for modified hydraulic geometry to develop a rating curve that was subsequently combined with an area, elevation, damage relationship. The design flow associated with this function is 8300 cfs, the upper limit of design flow for the enlarged channel. Table 6 (Appendix A) summarizes the performance and cost data for the proposed channel modification for reach 1030. Table 6 also contains a generated damage function for a specific design flow to illustrate the interpolation concept.

The upper and lower pattern damage functions for reach 2030 are the same and correspond to existing conditions. The reason for the correspondence is that the effect of a levee is primarily to truncate the function at the design flow. Some change is possible for various designs if the flow area is greatly restricted by the levees. The example assumes no significant conveyance change from the levees, though the methodology does not require the assumption. Table 7 (Appendix A) summarizes the cost and performance data for the proposed levee reach.

The existing conditions damage relationships, cost and runoff hydrology for reaches 1030 and 2030 have been purposefully made the same so that

the methodology developed for handling local projects can be easily observed. The example contains only local projects (other damage centers and alternatives removed) so that the difference in the derived sizes of the two alternatives should only be due to differences in their performance, i.e., modified damage relationships. A listing of the input data for this example is contained on pages 1 and 2 of Exhibit 6.

Pages 3 through 15 of Exhibit 6 contain selected pages of the output of the optimization run.

The derived optimum sizes are about 5000 cfs design flow for both the channel modification reach and the levee reach. This amounts to about a 0.7 exceedence frequency degree of protection. The total capital cost is \$207,000 and system annual net benefits of \$30,000. The derived values were adjusted from starting values of 2000 cfs design flow for each facility. It is interesting to note that while both facilities began and ended with the same values, the adjustment route to the optimum was different. There was no requirement that they both end up the same size (see pages 3 through 5 of Exhibit 6). In addition, note that while the values derived were the same, the net benefits were different because the damage relationships were quite different. The channel modification cost \$104,000 and had average annual benefits of 27,000 for annual net benefits of \$19,000 (benefit cost ratio of approximately 3.4). The levee cost \$103,000 and had average annual benefits of \$19,000 for annual net benefits of \$11,000 (benefit cost ratio of approximately 2.4).

SIZING RESERVOIR, PUMPING PLANT, DIVERSION, AND UNIFORM PROTECTION LOCAL PROJECTS

This final example includes all the proposed components that have been previously illustrated. The optimization will be unconstrained and the uniform protection level option for the local projects will be used. The uniform protection level option will in effect cause a "degree of protection" to be optimized for the two local protection projects. A complete listing of the input data is contained on pages 1 through 3 of Exhibit 7 and the complete output on pages 4 through 39.

The derived optimum sizes are 6701 ac.ft. for the reservoir, 0.2 exceedence frequency for the levee and channel projects (2947 cfs for the channel modification and 7660 cfs for the levee), 670 cfs for the diversion and 2450 cfs for the pumping plant for a total capital cost of \$7,408,000 and system net benefits of \$196,000 (benefit cost ratio of 1.31). The optimum sizes were adjusted from starting values of 4000 ac.ft. for the reservoir, 0.2 exceedence frequency (uniform protection) for local projects, 500 cfs for the diversion and 1000 cfs for the pumping plant. A comparison of Exhibits 5 and 7 indicates that the inclusion of local projects has very little effect on the optimum sizes of the major facilities (reservoir and pumping plant). The diversion capacity was lowered slightly from that derived in Exhibit 5 which probably means that it is more efficient to protect reach 2030 by the levee project.

OBJECTIVE OF THE FLOOD CONTROL SYSTEM COMPONENT OPTIMIZATION UTILIZING HEC-1

The optimization algorithm (or search procedure) discussed in this training document has been developed to assist the planner in systematically and efficiently screening a large number of possible flood control alternatives. Although there is an upper limit to the number which can be satisfactorily and economically optimized in one particular computer run, it is still possible to analyze a large number of components by grouping. In the Phoenix Urban Study, Los Angeles District Corps of Engineers (reference 6), there were eight upstream storage alternatives to be evaluated. Although each component was analyzed individually, it was possible to determine which component and combination of components were economically feasible by making several runs in groups of two and three components and comparing the economic and hydrologic consequences.

It should be emphasized that the optimization procedure of HEC-1 is a planning tool for determining potential and economically feasible flood control alternatives. Once those that have potential are selected, then a more detailed simulation of the operational and hydraulic characteristics of a particular component will probably be required as various stages of study (leading to design) are undertaken.

REFERENCES

- 1. <u>HEC-1, Flood Hydrograph Package</u>, Users Manual, U.S. Army Corps of Engineers, The Hydrologic Engineering Center, Davis, California, January 1973.
- Input Data Description, Addendum 6 to HEC-1 Users Manual, September 1974.
- 3. Davis, Darryl W., "Optimal Sizing of Urban Flood Control Systems," Technical Paper No. 42, U.S. Army Corps of Engineers, The Hydrologic Engineering Center, Davis, California, March 1974.
- 4. Optimization Model for the Design of Urban Flood-Control Systems, Technical Report CRWR-141, Center for Research in Water Resources, College of Engineering, University of Texas, Austin, Texas, November 1976.
- 5. Expected Annual Flood Damage Computation, Users Manual, U.S. Army Corps of Engineers, The Hydrologic Engineering Center, Davis, California, June 1977.
- 6. <u>Interagency Task Force on Orme Dam Alternatives</u>, Preliminary Flood Control Summary Report, Phoenix Urban Study, Los Angeles District, U.S. Army Corps of Engineers, Los Angeles, California, September 1977.

APPENDIX A

INPUT DATA

1.

TABLE 1
HYDROLOGIC DATA
(Existing Conditions)

DRAINAGE AREA

Subbasin	Area (square miles)
10 20	35.1 35.1
30	TOTAL 10.0 80.2

SUBBASIN RUNOFF SYNTHETIC STORM EVENT (hourly values)

	ow to 0 (cfs)	Int <u>Sta.</u>	flow to 20 (cfs)		flow to 30 (cfs)
24	2200	24	2200	8	730
24	1840	24	1840	8	615
26	1540	26	1540	9	515
33	1250	33	1250	11	415
50	995	50	995	17	330
85	775	85	775	28	255
190	605	190	605	63	200
375	470	375	470	125	155
515	365	515	365	170	120
590	280	590	280	195	93
660	215	660	215	220	72
710	160	710	160	230	54
760	120	760	120	255	41
800	95	800	95	265	32
840	77	840	77	280	26
910	66	910	66	305	22
1040	59	1040	59	350	20
1290	53	1290	53	430	18
1920	49	1920	49	640	16
3000	42	3000	42	1000	14
3950 4600 5080 5360 5370	40 38 35 33 30	3950 4600 5080 5360 5370	40 38 35 33 30	1320 1540 1650 1800 1810	13 12 11 11
5100 4600 3980 3330 2720	30 29 27 25 25	5100 4600 3980 3330 2720	30 29 27 25 25	1690 1530 1330 1110 900	10 10 9 9

TABLE 1 (Continued)

HYDROLOGIC DATA (Existing Conditions)

Reach 10-30 Mod. Puls Routing Criteria								
Storage (ac.ft.)	0	50	475	940	2135	3080	6300	
Outflow (cfs)	0	200	1020	2050	6100	10250	24000	
Reach 20-30 Mod Puls	Routin	ng Crite	ria ^l					
Storage (ac.ft.)	0	50	475	940	2135	3080	6300	
Outflow (cfs)	0	200	1020	2050	6100	10250	24000	

Outflow Culvert	(Sta.	30)	Mod. Pu	ls Routing	<u>Criteria</u>
Storage (ac.ft Outflow (cfs	;.) ;)	0	400 1200	100000 ² 1200	

Storage-outflow data should extend beyond the maximum values computed in the multiflood-multiplan options.

Note that the outflow becomes constant and equal to 1200 cubic feet per second when the detention storage equals or exceeds 400 acre feet.

TABLE 2 ECONOMIC DAMAGE-FREQUENCY DATA (Existing Conditions)

Damage Center 1030

Exceedence Frequency (Events per Yr)	Flow (cfs)	Type 1 Damage (\$1000)	Type 2 Damage (\$1000)	Type 3 Damage (\$1000)
6.000	1030	0.00	0.00	0.00
5.500	1130	0.00	0.00	0.00
4.500	1380	0.10	0.50	1.00
3.500	1740	0.20	0.70	1.50
2.500	2280	0.30	1.50	3.20
1.500	3200	0.30	2.20	4.70
.900	4220	0.40	2.90	6.50
.700	4800	0.50	3.50	7.80
.500	5620	0.60	4.00	9.30
.350	6480	0.70	4.70	11.00
.250	7340	0.80	5.80	13.70
.150	8540	0.90	6.60	15.60
.100	10000	1.00	8.00	19.00
.050	12100	1.20	10.30	23.00
.020	15100	1.50	15.00	27.80
.005	21000	1.80	18.10	30.20

Damage Center 2030

Exceedence Frequency (Events per Yr)	Flow (cfs)	Type 1 Damage (\$1000)
6.000	1030	0.00
5.500	1130	0.00
4.500	1380	1.60
3.500	1740	2.40
2.500	2280	5.00
1.500	3200	7.20
.900	4220	9.80
.700	4800	11.80
.500	5620	13.90
.350	6480	16.40
.250	7340	20.30
.150	8540	23.10
.100	10000	28.00
.050	12100	34.50
.020	15100	44.30
.005	21000	50.10

TABLE 2 (Continued) ECONOMIC DAMAGE-FREQUENCY DATA (Existing Conditions)

Damage Center 305

Exceedence Frequency (Events per yr)	Storage (ac-ft)	Type 1 Damage (\$1000)	Type 2 Damage (\$1000)
.700	1500	0.00	0.00
.600	2300	37.50	10.50
.450	4000	75.00	15.00
.250	7000	1125.00	52.50
.100	12500	3150.00	105.00
.050	20000	5850.00	202.50
.020	28000	7050.00	300.00
.010	37000	9000.00	390.00
.005	50000	10650.00	540.00
.002	76000	11250.00	585.00

Flood Ratios for Multiflood, Multiplan Evaluation

0.25 0.30 0.50 0.70 1.00 1.50 2.20 3.25 4.40

Note that the damage-frequency relationship (for damage center 305) is a function of storage and <u>not</u> discharge.

TABLE 3 RESERVOIR PERFORMANCE AND COST DATA

Low Level Outlet

Area of Opening = 35 ft²
Orfice Coefficient, C,
 in the general expression

Q= C A (2gH)^{Exp.}
 (free discharge) = 0.71
Cenderline Elevation of Orfice = 975 ft
No Tailwater (no submergence)
 Exponent of head (Exp.) = 0.5

Overflow Spillway

Type = Ogee
Length = 35 ft
Weir Coefficient, C,
in the general expression
Q= C L H^{3/2} = 2.86

Cost and Site Characteristics 1

Capacity (ac.ft.)	0	2500	4000	5200	6800	9000	11500	15500	21000	30000
Elevation (ft)	965	1000	1015	1030	1045	1060	1075	1090	1105	1120
Cost (\$1000)	0	1500	2400	3000	3600	4350	4950	5550	6000	7200

Annual Cost Data

Annual Operation and Maintenance = 2.3% of Capital Cost Discount Factor (Capital Recovery) = 5.04%

Constraints

Reservoir size must be in range of 0 to 25,000 ac.ft.

Capacity-elevation data should extend beyond the maximum values computed in the multiflood-multiplan options and the maximum reservoir size designated.

TABLE 4 PUMPING PLANT PERFORMANCE AND COST DATA

Cost and Performance Data

Capacity (cfs)	0	250	500	1000	2000	6000	8000	10000
Cost (\$1000)			1000	1600	2300	6000	7860	8670

Annual Cost Data

Annual Operation and Maintenance = 2.3% of Capital Cost Discount Factor (Capital Recovery) = 5.04% = \$100,000

Sizing and Operation Data

Pumping plant must be between 0 and 10,000 cfs.
Pumps activate at storage level (at station 30) = 1500 ac.ft.

Annual power cost is adjusted based on the difference in computed volumes at the pumping facility as system component sizes vary from specified initial values to optimized values

TABLE 5 DIVERSION PERFORMANCE AND COST DATA

Performance and Cost Data

Capacity (cfs) 0 1250 2500 3750 5000 7500 10000 15000 20000 Cost (\$1000) 0 1500 2600 3400 4200 5200 6100 7500 8300

Annual Cost Data

Annual Operation and Maintenance = 1.5% of Capital Cost Discount Factor (Capital Recovery) = 5.04%

Operation and Constraints

Diversion activation threshold = 1,500 cfs Size limit between 0 and 20,000 cfs

TABLE 6 CHANNEL MODIFICATION COST AND PERFORMANCE DATA

r

Damage Center 1030

Function	Type 3 Damage (\$1000)	00000	0.00	2.69 4.41 6.89 8.11	11.44 15.01 20.02 23.41
Interpolated Damage Function Design Q = 4830cfs	Type 2 Damage (\$1000)	00000	0.00	1.15 1.70 2.63 3.36	4.88 6.71 9.79 12.99
Interpola Desig	Type 1 Damage (\$1000)	00000	0.00 0.00 0.00	0.20 0.29 0.36 0.45	0.63 0.81 1.06 1.40
	Flow (cfs)	1030 1130 1380 1740	2280 3200 4825 4830	5620 6480 7340 8540	10000 12100 15100 21000
Function fs	Type 3 Damage (\$1000)	00000	0.0000	0.00 0.00 0.44	3.50 7.15 12.29 16.86
Maximum Design Damage Function Design Q = 8300cfs	Type 2 Damage (\$1000)	00000	00.00	0.00 0.00 0.25	1.75 3.18 5.04 7.98
Maximum Do	Type 1 Damage (\$1000)	0.00	00.00	0.00	0.25 0.42 0.64 0.99
Eunction fs	Type 3 Damage (\$1000)	0.00	1.73 3.44 5.85 7.23	8.91 10.63 13.11	18.61 22.09 27.00 29.32
Minimum Design Damage Function Design Q = 1700cfs	Type 2 Damage (\$1000)	0.00	0.95 1.73 2.53 2.73	3.53 4.08 5.01 6.16	7.70 9.90 14.08
Minimum Design Design Q	Type 1 Damage (\$1000)	0.00 0.00 0.00	0.14 0.25 0.36 0.43	0.53 0.62 0.82	0.97 1.17 1.43
<u> </u>	Flow (cfs)	1030 1130 1380 1740	2280 3200 4220 4800	5620 6480 7340 8540	10000 12100 15100 21000

1/ In the interpolation scheme zero damages are estimated to occur at a peak flow which is 99.9 percent of the design flow.

TABLE 6 (Continued) CHANNEL MODIFICATION COST AND PERFORMANCE DATA

Performance and Cost Data

Capacity (cfs)	1700	5000	5500	700 0	8300	9300
Cost (\$1000)	42	103	149	222	283	340

Annual Cost Data

Annual Operation and Maintenance = 2.3% of Capital Cost Discount Factor (Capital Recovery) = 5.04 %

Design Limits

Minimum Design Q = 1700 cfsMaximum Design Q = 8300 cfs

TABLE 7

LEVEE COST AND PERFORMANCE DATA

Damage Center 2030

Flow (cfs)		nimum Desi mage Funct Damage (\$1000)			Maximum De Damage Fun Damage (\$1000	ction
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2280 3200 4220 4800		5.00 7.20 9.80 11.80			5.00 7.20 9.80 11.80	
5620 6480 7340 8540		13.90 16.40 20.30 23.10			13.90 16.40 20.30 23.10	
10000 12100 15100 21000		28.00 34.50 44.30 50.10			28.00 34.50 44.30 50.10	
Performance and Cost Dat Capacity (cfs) Cost (\$1000)	<u>a</u> 1700 42	5000 103	5500 149	7000 222	8300 283	9300 340

Annual Cost Data

Annual Operation and Maintenance = 2.3% of Capital Cost Discount Factor (Captial Recovery) = 5.04%

Design Limits

Minimum design Q = 1700 cfs

Maximum design Q = 8300 cfs

EXHIBIT 1

HYDROLOGIC MODEL

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EXHIBIT 2

MULTIFLOOD, MULTIPLAN MODEL
(Economic Evaluation of Existing Conditions)

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MYDROGRAPH AT		35,10 90,911		1343. 38,02)(1343. 38,02)(1611. 45.62)(1611. 45.62)(2685. 76.03)(76.03)(3789. 106,44)(3759. 106,44)(5370. 152.06)(5370. 152.06)(8055. 228,09)(8055. 228,09)(334,54)(334,54)(334,54)(334,54)	17453; 494,20)(17453; 494,20)(23628 669.073 23628 669.073
RUUTED TO	680	35.10 90.91)		941. 26,65)(26,65)(1139. 32,24) (32,24) (1940. 54.94)(1940. 54.94)(82.713 (82.713 (82.713 (122.10)(122.10)(122.10)(189,7016 5699, 189,7016	101911 288,583)C 101911 288,583)C	15177, 429,77)(15177, 429,77)(2060% 583,423 2060% 583,423
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нүрадбаарн ат	ŝ	10.00	- ~ ~ ~	453. 12.81) C 453.	543. (15,38)(543.	905. 25.63)(25.63)(1267. 15.88)(1267. 35.88)(1810 51.25)(1810 51.25)(2715. 76.88)(2715. 76.88)(3982. 112,763(3982. 112,763(5883 166.57) 5883 166.57)	7964. 725,323 7964.
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EXHIBIT 3

SIZING RESERVOIR AND PUMPING PLANT (Unconstrained)

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VAR 1 ADJ FROM	10000001	9384.07	N. T.	E O	VARCM)	VAR(M1) •938E+04	083 DEV	TANCST 731.737	ANDMG 284.417	0 FTN(NC)
			์ วูล ช	E O	VAR(M) .396E+04	VAR(M1)	08J DEV	TANCST 729,021	ANDMG 286,506	. 102E+04
			OM.	E O	. 392E+04	VAR(M1)	083 087	TANCST 726 305	ANDMA	D FINCES
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 9	.1016E+04	.1016E+04		.1015E+04					**************************************
VAR 9 ADJ FROM	4000.00 TG	2948,78	2	Ε	. 938E+04	VAR(M1)	08J DEV	TANCST 660,364	ANDMG 344,595	0 FIN(NC)
			20	Σ 0	VAR(M)	VAR(M1)	08J DEV	TANCST 658,880	ANDMG 346.024	0 FTN(NC)
DAJECTIVE FUNCTION FOO VINE				Σ 0	VAR(M)	VAR(M1)	08J DEV	TANCST 657,398	ANDHG 347.476	0 FIN(NC)
	TON VAKLABLE 1	•1005E+04	.1005E+04		.1005E+04					
VAR 1 ADJ FRUM	9384.07 10	9118.64	Σ 0 	Ξ-	VAR(M)	VAR(M1)	08J DEV 0.000	TANCST 656.170	ANDMG 348.714	0 FTN(NC)
			Y O	Ξ-	VAR(M)	VAR(M1)	08J DEV 0.000	TANCST 654,168	ANDMG 350.656	- FTN(NC)
			E O	Ξ	VAR(M) .289E+04	VAR(M1)	08J DEV 0,000	TANCST 652,166	ANDMG 352,606	0 FTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 9	.1005E+04	.1005E+04		.1005E+04					
			Σ υ 2	Σ °	.912E+04	VAR(M1)	083 DEV	TANCST 641,808	ANDMG 363,145	0 FTN(NC)
VAR 9 ADJ FRUM	2948,78 10	2885,32	2-	ο Σ	VAR(M)	VAR(M1) .289E+04	08J DEV	TANCST 651,861	352,917	0 FTN(NC)
			E TO N	₹°	VAR(M)	VAR(M1)	08J DEV 0.000	1ANCST 650.422	ANDMG 354,382	0 FINCAC)
			Σ. T.	Σ σ	VAR(M)	VAR(M1)	083 067	TANCST 648,514	ANDMG 355.885	0 FIN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 1	.100SE+04	.1005E+04		.1004E+04					

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		•	1 ,289€+04		.137E+05	0000	711.373	319,365	.103E+04
		X 0	M1 VAR(M)		VAR(M1)	083 DEV	TANCST 673,724	337,923	0 FIN(NC)
		E O	M1 VAR(M)		VAR(M1) 953E+04	08J DEV	TANCST 658,346	ANDMG 346.654	•
		× •	M1 .289E+(£ ¥	VAR(M1)	081 DEV 0.000	TANCST 651,861	352,917	0 FIN(NC)
		E O	M1 .286E+04	. +04	VAR(M1) 912E+04	08J DEV	TANCST 649,902	ANDMG 354,917	0 FIN(NC)
		E O N	M1 .283E+04		VAR(M1)	083 DEV 0.000	TANCST 647,943	ANDMG 356,916	D FIN(NC)
DBJECTIVE FUNCTION FOR VARIABLE 9	.1005E+04	.1005E+04	.1005E+0	E+04					
		Σ	M1 VARCM) 9 +912E+04		VAR(M1)	083 DEV 0.000	TANCST 749.811	ANDMG 272.677	0 FTN(NC)
		Σ 	M1 VAR(M) 9 .912E+04		VAR(M1) 332E+04	08J DEV 0,000	1ANCST 681,246	325.665	0 FIN(NC)
		¥ →	M1 VAR(M) 9 .912E+04		VAR(M1) 302E+04	08J DEV	TANCST 660,677	344.347	0 F TN(NC)
		E	M1 VAR(M) 9 .912E+04	•	VAR(M1) -	08J DEV	TANCST 651,861	352,917	0 FTN(NC)
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		NC NC	M1 VARCM 9 .894E+0		VAR(M1) 289E+04	UBJ DEV	TANCST 648,514		0 FIN(NC)
OBJECTIVE FUNCTION FOR VARIABLE 1	*1005E+04	.1005E+04	.1004E+0	E+04					
		¥ o	M1 .289E+04		VAR(M1)	08J DEV 0,000	TANCST 711.373	ANDMG 319,365	D FTN(NC)
		¥ 6	M1 . Z89E+	VAR(M) V	VAR(M1) 105E+05	UBJ DEV 0.000	TANCST 673.724	ANDMG 337.923	0 FIN(NC)
		Z O	M1 . Z89E+	E+04 .9	VAR(M1)	08J DEV	TANCST 658,346	346,654	-101E+04
		¥ 6	M1 VAR	V (A)	VAR(M1) 912E+04	08J DEV	TANCST 651,861	352,917	0 FIN(NC)
		₹ 0	M1 .286E+04		VAR(M1) 912E+04	000 ° 0	TANCST 649,902	ANDMG (0 FTW(NC)
		T X O	M1 VAR(M)		VAR(M1) 912E+04	08J DEV 0*000	TANCST 647,943	ANDMG 0 356.916	FTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE 9	.1005E+04	.1005E+04	.1005E+0	70+					

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337,923 .101E+04	TANCST 673,724	083 DEV	VAR(M1)	VAR(M) 289E+04		9 -					
319,365 .103E+04	TANCST 711,373	08J DEV	VAR(M1)	VAR(M) 289E+04	E O	2					
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ANDMG O FTN(NC)	1ANCST 648.514	08J DEV	VAR(M1)	VAR(M) 894E+04	 Σ Σ	S.W					
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352,917 ,100E+04	TANCST 651,861	083 DEV 0,000	VAR(M1)	VAR(M)	E.	27					
344.347 .101E+04	TANCST 660,677	08J DEV 0,000	VAR(M1)	VAR(M)	E -	U					
325,665 .101E+04	TANCST 681.246	083 DEV	VAR(M1)	VAR(M) 912E+04	E =	S.					
272.677 .102E+04	749.811	08J DEV 0.000	VAR(M1)	VAR(M) 912E+04	 K E	2					

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STORAGE: OUTFLUME		1097.		2245. 926.	SYNTHETIC 4657. 1389.	TIC STORAGE 9119.	E OUTFLO₩ 13098, 11189	FUNCTION 16565 20452		2022 2022 2022 2023	25089. 38860.	30000 48060
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MAXIMUM STORAGE #

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MAXIMUM STORAGE #

*HOUR 24#HOUR 72*HOUR TOTAL 6289. 3747. 1736. 178. 106. 49. 1.67. 3.97 4.60 42.34 100.88 116.86 3120. 7435. 8612. 3849. 9171. 10623.	STORAGE # 2271.	OUR 24-HOUR 72-HOUR 555 2545- 71. 557. 72- 75. 5.8 6.75 .32 149.44 171:35 41. 11014- 13585- 15577-	STORAGE = 3067, 2030, PLAN 1, RTID 8	-HOUR 24-HOUR 72-HOUR TOTAL 4262. 8279. 106. 106. 3.78 9.96 9.96 90.00 16430. 18647. 8728. 23001.	STORAGE = 4234. 2030, PLAN 1, RTIO 9	24*HOUR 72 11267, 119, 11,94 303,38 22359, 2
TEAK 6=1 CHS 6699• 62 CHS 190• 1 INCHES 190• 1	MAXIMUM	PEAK 6+H CFS 10191: 05 CMS 1289; 2 Z 10CHES 289; 2 Z MM MM AC-FT 47	MAXIMUM	PEAK 6=H CMS 15177. 145 CMS 430. 4 INCHES 430. 4 MM ACHT 70	MAXIMUM	CFS 20603, 193 CMS 20603, 193 CMS 583, 193 INCHES 583, 130 MM AC#FT 96

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CFS 1664. 1616. 1226. 655. 19. CMS 47. 1616. 1226. 655. 19. AC-FT 802. 2434. 45. 19.30 AC-FT 802. 2434. 40.09. 19.30 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 2 CFS 1968. 546. 1434. 778. 470. 406. CFS 1968. 546. 1434. 778. 778. 4710 3 CC MH OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 3 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 3 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 3 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 AC-FT 804 OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 SUM OF 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 AUGHES 131. 494. 5049. 1675. 1085 CC MH 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 AUGHES 131. 499.35 AC UM 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 AUGHES 131. 499.35 AC UM 3 HYDROGRAPHS AT 30 PLAN 2 RTIO 4 AUGHES 131. 499.35 AC UM 3 HYDROGRAPHS AT 30 PLAN 3 AUGHES 1005 AUGHES 131. 499.35 AUGHES 1240. 4064. 10651. 4063.	ns.	0F 3			Z	110	
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ON THE CONTRACT OF LANGE OF LA	12 PEA 4705 4 100.	6*HDUR 14017* 14017* 1503 41.50 6954* 8578*	24*HOUR 8974* 254* 105*75 17899	72#HDUR 4641 15641 1366-338 28401 28401	TOTAL VOLUME 278464. 7885. 5,38 136.73 23025. 28401.
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W) &	0F 3 HYD	RUGRAPHS	30	PLAN 2	6 01 14
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	or.					-		AVERAGE	<u>ar</u>	Ω		٠		.150			.008		4 L V	PRUB	INI	0000	0.1	150	.119	.075	. 037	0.13	.008	9w0	8
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	PEAK FLOW	AND STORAGE (E)	C S	OF PERIOD) (N CUBIC PEE) AREA IN SQUA	SUMMARY F PER SEC ARE MILES	DR MULTIPL DND (CUBIC (SQUARE K	PLANERS ETERS P OMETERS	TIO ECONOMICER SECOND)	COMPUTATION	8 8 2		
OPERATION	STATION	AREA	N V	RATIO 1	RATIO 2	RATIOS APPRATIOS APPRATIO	PLIED TO PI RATIO 4	LUWS HATIO 5	RATIO 6 1,50	RATIO 7	RATIO B 3.25	RATIO 9
HYDROGRAPH AT	0,	35.10 90,91)	7 ~	1343. 38.02)(1343. 38.02)(16114 45.62)(16118 45.62)(2685. 76.03)(2685. 76.03)(3759. 106,44)(3759. 106,44)(5370. 152.06)(5370. 152.06)(8055. 228.09)(8055. 228.09)	11814. 334.54)(11814. 334.54)(17453. 494.20)(17453. 494.20)(23628. 669.07) 23628. 669.07)
ROUTEO TO	011	35.10 90.91)	~~~~	1343. 38.02)(590. 16.72)(16114 45.62)(6614 18.73)(2685. 76.03)(940. 26.61)(3759. 106.443(1095. 31.013(5370. 152.06)(1340. 37.96)(8055. 228.09) (1599. 45.29) (11814, 334,54)(3113, 88,15)(17453. 494.201(8608. 243.74)(23626. 669.07) 14282. 404.42)
ROUTED TO	1030	35.10	1, 2,	941. 26.65)(529. 14.98)(1139. 32,24)(593, 16,80)(1940. 54.94)(853. 24.15)(2921. 82.71)(1018. 28.84)(4312, 122,10)(1260, 35,67)(6699. 189,70)(1535. 43,47)(10191. 288,58)(2601. 73,67)(15177, 429,773(7263, 205,673(583.423 12276. 347.633
НҮОРОСРАРН АТ	20 (35.10 90.91)	- ~ ~ ~ ~	1343. 38.02)(1343. 38.02)(1611. 45.62)(1611. 45.62)(2685. 76.03)(2685. 76.03)(3759. 106,44)(3759. 106,44)(5370. 152.06)(5370. 152.06)(8055, 228,09)(8055, 228,09)(11814, 334,54)(11814, 334,54)(17453. 494.20)(17453. 494.20)(23628. 669.07) 23628. 669.07)
ROUTED TO	2030	35.10	⊸ ~~``	941. 26.65)(941. 26.65)(1139. 32.24)(1139. 32.24)(1940. 54.94)(1940. 54.94)(2921. 82.71)(2921. 82.71)(4312. 122.10)(4312. 122.10)(189,70)(6669) 189,70)(10191. 288,58)(10191. 288,58)(15177° 429°7730 15177° 429°7730	20603. 583.42) 20603. 563.42)
НУОКОСКАРН АТ	30 (10.00	- ~ ~ ~ ~	453. 12,81) (453. 12,81) (543. 15,38)(543.	905, 25,63)(905, 25,63)(1267。 35.88)(1267。 35.88)(1810. 51.25)(1810. 51.25)(2715. 76.88)(2715. 76.88)(3982, 112,76)(3982, 112,76)(5885, 166,57)(5883, 166,57)(7964. 225.52) 7964. 225.52)
3 COMBINED	30	80.20	_~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	2219. 62.843(1664.	2676. 75.79)(1968. 55.74)(4563. 129,21)(3196. 90,51)(6859. 194.23)(4616. 130.72)(10154, 287,53)(6625, 187,60)(15693. 444.39)(9960. 282.04)(23748, 672,47)(14769, 418,21)(35345 1000.86)(22446 635.59)(48011. 1359.533 34011. 963.083
ROUTED TO	305	80.20	⊸ ~~~	1200° 33,983(33,983(1200. 33.98)(1200.	33,98)(1200, 1200, 33,98)(1200- 33,98)(1200- 33,98)(1200. 33.98)(1200. 33.98)(33.98)(1200, 1200, 33.98)(1200. 33.98)(1200. 33.98)(1200. 33.98)(1200. 33.98)(1200, 33,98) 1200, 33,98)
			* - 7 %	PEAK STORA 1030. (1278.) (749.)	1833.)(1106.)(7887 4424.) 1628.	00 CUBIC 5904 72834) 17054	METERS)** (11788,) (2967, (3660,)	15876, 19583,)(5936, 7322,)(24937. 30760.)(11173.	38699. 47734.)(23406. 28871.)(53876. 66455.) 37569. 46341.)

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AND PERFO	* * * * * * * * * * * * * * * * * * * *		o * * ≥	* * *	MAXIMIZE	TANCST 742.
VSTEM COST AME AS INP	* * * 0		REDUCTION (BENEFITS)	が 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日		ANOWPR SOL
\$ \$ IND	* # 3	. ⊢	EDU	SYSTEM NET BENEFILLS	***** OPTIMIZATION OBJECTIVE	ANFCST 440.
•	SYSTEM CAPITAL COST SYSTEM AMORTIZED CAL SYSTEM ANNUAL D. M. D	OTAL SYSTEM ANNUAL COST	ANNUAL DAM ANNUAL DAM		* * * * * * * * * * * * * * * * * * *	TFCST 8740.
	OTAL SYS		VERAGE A	VERAGE ANNUAL		

EXHIBIT 4

SIZING RESERVOIR AND PUMPING PLANT (Hydrologic Performance Constrained)

							62000	OWDER	N = NEW INPUT DATA	R = REVISED INPUT DATA	()= REVISED INPUT DATA																						
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FLOOD CONTROL SYSTEM CUMPONENT OPTIMIZATION SIZING RESERVOIR AND PUMPING PLANT HYDROLOGIC PERFORMANCE CONSTRAINED	JOB SPECIFICATION NHR NMIN IDAY IHR IMIN METRC IPLT IPRT NSTAN 1 0 0 0 0 3 0 3 JOPER NWT LROPT TRACE 7 0 0	MULTI-PLAN ANALYSES TO BE PERFURMED NPLAN= 2 NRTIU= 9 LRTIO= 1 S	VAR 3 VAR 4 VAR 5 VAR 6 DIV 7 DIV 8 PMP 9 PMP 10 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	FIXED COST INPUT FCAP FDCNT FAN 0. 0.0000 0.0000 0. 0.000	1STA INT FLOW FLW 083 FLW DEV 1050 1050 1224,953	1STA INT FLOW TRG FLOW FLW ORJ FLW DEV 305 7762,425 5000,000 931,715 2762,425	NC M M1 YAR(M) VAR(M1) DBJ DEV TANCST ANDMG U FTN(NC) 1 1 1 .500E+04 .500E+04 931,715 685,365 334,300 .951E+06	18TA INT FLOW TRG FLOW FLW DBJ FLW DEV 1030 1225.118 1200.000 .002 25.118	1STA INT FLOM TRG FLOW FLW ORJ FLW DEV 305 7815.023 5000,000 1004,728 2815,023	NC M M1 VAR(M) VAR(M1) OBJ DEV TANCST ANDMG O FIN(NC) 2 1 1 .495E+04 1004,728 683,630 336,115 .103E+07	1STA INT FLOW TRG FLOW FLW 08J FLW 08J 1030 1625.233	1STA INT FLOW TRG FLOW FLW DBJ FLW DEV 3.05 7867,667 5000,000 1082,021 2867,667	NC M MI VAR(M) VAR(MI) OBJ DEV TANCST ANDMG O FIN(NC) 3 1 1 , 490E+04 1082,021 681,895 337,930 ,110E+07	9811E+06 (1996F+07 (1996F+
FLOOD CONTR SIZING RESE HYDROLOGIC		RT 108=	VAR 1 ***********************************											OBJECTIVE FUNCTION FOR VARIABLE 1

				151A	INT FLOW 1214,982	186 FLUM	000°	FLW DEV
				1STA 305	INT FLOW 6997.027	TRG FLUW 5000,000	FL* 083	75.0 DEV
VAR 1 ADJ FRUM	5000,00 TO	5826,40	2.5	E E	VAR(M) VAR(M1) 500E+04 .583E+04	08J 0EV 254,482	TANCST ANDMG 708,257 307,809	0 FIN(NC) ,260E+06
				187A	INT FLOW 1214,982	TRG FLUW 1200,000	000	FLW DEV
				181A 305	INT FLOW 7061,828	TRG FLOW 5000,000	FLW 083 289,154	FLW DEV 2061,828
			UNZ	E O	VAR(M) VAR(M1) 495E+04 .583E+04	083 DEV 289,154	TANCST ANDMG 704,862 309,993	0 FIN(NC)
				181A 1050	INT FLOW 1214,982	TRG FLUM 1200,000	FLW UBJ.	FLW DEV 14,982
				151A 305	INT FLOW 7126,578	1RG FLUW 5000,000	FLW 083	FLW DEV
			OM N	Ξ-	VAR(M) VAR(M1)	08J DEV	TANCST ANDMG 701,468 311,125	# FTN(NC)
DBJECTIVE FUNCTION FOR VARIABLE	OR VARIABLE 9	*2596E+06	.2945E+06		.3324E+06			
				151A	INT FLOW 1214,982	TRG FLUW 1200,000	000°	FLW DEV 14,982
				18TA 305	INT FLOW 6507,512	1RG FLOW 5000,000	FLW 08J	FLH DEV
VAR 9 ADJ FROM	5000,00 10	5553,52	S-	Σ Σ Τ	VAR(M) VAR(M1) .583£+04 .555E+04	08J DEV 46.763	TANCST ANDMG 745,858 285,003	G FIN(NC)
				181A	INT FLOW 1215,496	1200,000	000°	FLW DEV
				151A	INT FLOW 6549,331	TRG FLUW 5000,000	FLW 08J	FLW DEV
			y N	Σ Σ	VARCM) VAR(M1)	08J 0EV 53.039	TANCST ANDHG 744,354 286,520	0 FINCHC)
				181A 1050	INT FLOW 1216.060	TRG FLOW 1200,000	FLW 08J	FLW DEV
				151A 305	INT PLOW 6391-365	1RG FLOW 5000,000	FLW URJ 59,963	FLW DEV
			2.	M H 1	.571E+04 .555E+04	08J DEV 59,963	TANCST ANDMG 742,870 288,041	0 FTN(NC) ,628E+05
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARTABLE 1	.4924E+05	.55718+05		• 6285E+05			

이 많아 돌릴까지 어린다. 학생이 가능을 하다니게 있으니 말이다.	INT FLOW TRG FLOW FLY 5556+04 17.303 759,453 1512.351 1210.000 22 17.303 759,453 1212.351 1200,000 1212.351 1200,000 1212.351 1200,000 1212.351 1200,000 1200,000 1212.351 1200,000 1200,000 1212.351 1200,000 1200,000 1212.351 1200,000 1200,000 1212.351 1200,000 1200,000 1212.351 1200,000	272-227 1899 272-227 1899 272-227 1899 274-393 237 274-393 237 274-393 1146 274-459 2995
1 ADJ FRUM 5826,40 TO 6360,80 ISTA 1530 1030 1531 1531	.636E+04 17.303 759.4 -636E+04 17.303 759.4 -351 1200.000 -351 1200.000 -355 5000.000 -355 5000.000 -355 1200.000 -351 1200.000 -351 1200.000 -351 1200.000 -351 1200.000 -351 1200.000	272.227 CBJ .000 .036 274.393 .036 .08J .08J .678 .274.459
157A 1030 1030 1 157A 305 1 0 0 1 1 1030 1 1030 1 1030 1 1030 1 1040 1 1040 1 1 1 9 0 1	FLOW TRG FLOW 1351 1200,000 1313 5000,000 1000 1313 5000,000 1200,	CBJ .000 .000 .036 .036 .060 .060 .060 .074.459
151A 505 NC M M1 1030 151A 1030 151A 505 NC M M1 505 NC M M1 1050 151A 1050 151A 11 9 8	FLOW TRG FLUW 5000,000 VAR(M1) GBJ DEV 755,6 FLUW 351 1200,000 FLUW 5839 5000,000 VAR(M1) GBJ DEV TANG VAR(M1) GBJ DEV TANG FLUW 555,656,404 27,678 751,6 FLUW 3551 1200,000	ANDMG 274,393 08.0 08.0 08.0 08.0 67.8 45.9 276.45.9
NC M M1 157A 1030 157A 305 0 .1889E+05 .2373E+05 157A 1050 157A 1505 170 5818,71	VAR(M1) UBJ DEV TANC •636E+04 22.036 755.6 FLOW TRG FLUM •839 5000.000 VAR(M1) UBJ DEV TANC VAR(M1) UBJ DEV TANC FLOW TRG FLUM •656E+04 27.678 751.9	ANDMG 274,393 .000 .000 .678 ANDMG 276,459
151A 1050 1050 305 305 9 .1889E+05 .2373E+05 151A 1050 151A 1050 151A 1199.	FLOW TRG FLUW *351 1200,000 FLOW TRG FLUW *839 5000,000 YAR(M1) 0HJ DEV TANC *656k+04 27,678 751,9 FLOW TRG FLUW *351 1200,000	# 085 * 080 * 080 7.678 ANDMG
181A 305 305 305 181A 1050 181A 1050 181A 1050 181A 1050 181A 1050 181A 181	FLUM TRG FLUM 839 5000,000 VARCM1) UBJ DEV TANC 456E+04 27,678 751,9 FLUM TRG FLUM 351 1200,000	7.678 7.678 ANDMG 276.459
0 .1889E+05 .2373E+05 .1 .1 .2374 .1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0	VARCHI) UBJ DEV TANC .656E+04 27,678 751,9 FLOW TRG FLUW .351 1200,000	ANDMG 274.459
15TA 1050 151A 1050 151A 505 NC M M1 1 9 •	FLOW TRG FLUW .351 1200,000	
18TA 1050 1050 305 9 ADJ FROM 5553,52 TO 5818,71	1200 000	
13TA 305 NC M M1 1 9 8 9 ADJ FROM 5553,52 TO 5818,71		185 el 000 .
9 ADJ FROM 5553,52 TO 5818,71 ISTA	INT FLUM TRG FLUM FL 5731,269 5000,000	LW GBJ FLW DEV 4,576 731,269
VISI CONTRACTOR CONTRA	VAR(M) VAR(M1) OBJ DEY TANCST 636E+04 .582E+64 4.576 777,459	7 ANDMG OF TN(NC) 9 262,641 ,580E+04
	INT FLUW TRG FLUW F1 1212,486 1200,000	LW DBJ FLW DEV
	INT FLOW TRG FLOW F1 5756,224 5000,000	FLM 083 FLW DEV 5,233 756,224
7	VAR(M) VAR(M1) OBJ DEV TANCST 630E+04 \$582E+04 5,233 775,838	8 264.030 .648E+04
Total	INT FLOW TRG FLOW F1212,670	FLW DBJ FLW DEV
	INT FLOW TRG FLOW F 5782.138 5000.000	FLW DBV 5,988 782,138
XY CONTROL OF THE CON	VAR(M) VAR(M1) OBJ DEV TANCST 623E+04 .582E+04 5.988 774.217	7 265,434 .7266+04

			101 101 101 101 101	1212-494	1200.000	FLH DBJ	FLW DEV 12.494
			1.51A 3.05	1NT FLOW 5587,510	TRG FLOW \$000,000	FL# 080	FLW DEV 587.516
VAR 1 ADJ FROM	6360 ₆ 80 TO	6757.05	E O		08J DEV 1,906	TANCST ANDRO	. 303E+04
			10-10-10-10-10-10-10-10-10-10-10-10-10-1	INT FLOW	186 FLOW	000°	FLE DEV
			191A 1905	1 INT FLOX	TRG FLCW \$000,000	FL* 08J	FLW DEV 650,189
			E 6	1 .576E+04 .676E+04	08J DEV 2.860	783.663 256.439	# FTN(NC)
			1030	1212-494	TRG FLUW 1200,000	FLW 084	7 1 2 0 0 E C C C C C C C C C C C C C C C C C
			15TA 305	1 INT FLOW 5712,839	7RG FLUW 5000.000	FLW CBC	712.839
			E O	1 VAR(M) VAR(M1)	08J 0EV	TANCST ANDMG 779.712 258.607	SUSE + OF
OBJECTIVE FUNCTION FOR VARIABLE	OR VARIABLE 9	.3028E+04	.4014E+04	.53288+04			
			4 - ST - C - C - C - C - C - C - C - C - C -	INT FLOW	TRG FLDW 1200,000	FLW DBJ	FLW DEV
			18TA 18TA 1805	A TINT SECON	TRG FLOW 5000,000	7. 8 087. 248.	FLW DEV 430,135
VAR 9 ADJ FROM	5918,71 10	2	NC N	VAR(M) VAR(M1) 9 .676E+04 .596E+04	083 DEV	TANCST ANDMG 797.527 249.265	0 FIN(NU)
			16 10 10 10 10 10	A INT FLOW	1200.000	FLW CBU	FLX DRV
			16TA 305	1 NT FLOX	TRG FLOW 5000,000	FLW UBJ	FLM DEV 453,915
				1 VAR(M) VAR(M1)	08J DEV 679	TANCST ANDMG	0 FTN(NC)
			18TA 1030	INT FLOX	186 FLOW 1200,000	FLW OBJ	FLW DEV
			18TA 305	INT F.OH 5477-721	TRG FLDW 5000,000	FLW OBJ	FLW DEV 477,721
			NC X T	1 VAR(M) VAR(M1)	08J DEV .833	TANCST ANDMG 794.039 251,997	192E+04
OBJECTIVE FUNCTION FOR VARIABLE	OR VARIABLE 1	.1620E+04	.17576+04	•1918E+04			

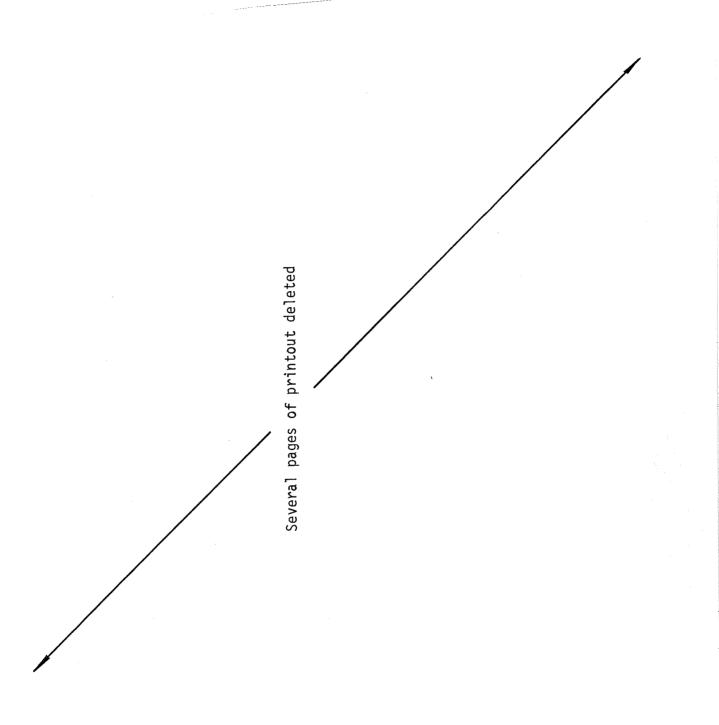
.13956+0

1514 1104 1104 1104 1104 1104 1104 1105 1004 1000				E T OZ	VAREM) VAREMI)	083 DEV	TANCST ANDMG D FIN(NC) 808,501 241,846 114E+04
1876				18TA 1030	21 K	200	LW CBJ FLW
1117E+04				18TA 305	INT FLOW 5294.204	TRG FLUW 5000,000	08J FLW 120 294
1514 117E+04 117E+04 117E+04 117E+04 117E+04 117E+04 117E+04 1187A 117E+04 1180,000 1187A 1187E+04 1180,000 1187A 1180 1180,000 1180 1180,000 1180 1180,000 1180 118				I-		96	ANDMG E. 835. 243.082
1874 110 FLD 1874 1875 1876 1875 1876 1875 1876 1875 1876 1875 1876 1875 1876 1875 1876 1876 1875 1876 1875 1876 1875 1876 1875 1876	OBJECTIVE FUNCTION	FOR VARIABLE 1	,1117E+04	43E+0	1176E+0		
1874 1874 1876 1876 1877 1877 1878				15TA 1030	1NT FLOW 1214,815	186 FLOW	.000
1 ADJ FRUM 7116,73 TO 7336,88				ISTA 305	INT FLOW 5182,446	TRG FLOW 5000,000	M DBJ FL
1574	-	7116.73 TO	7336,88	x o	VAR(M) VAR(M1) 603E+04 .754E+04	083 DE	TANEST ANDMG 15.524 236.794
1517				18TA 1030	INT FLOW 1214.815	TRG FLOW 1200,000	M 080 FLW
1814 VAR(M1) UAB J DEV TANCET ANDHO 1814 1 .003E+04 .734E+04 .018 B15,324 256,794 1814 1815 1214,815 1200,000 .010 1814 1815 1214,815 1200,000 .010 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 1200,000 .0101 1814 1815 .0101 .0101 .0101 1815 .0101 .0101 .0101 .0101 1815 .0101 .0101 .0101 .0101 1816 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 .0101 1817 .0101 .0101 .0101 .0101 .0101 1814 .0101 .0101 .0101 .0101 .0101 .0101 1815 .0101 .0101 .0101 .0101 .0101 .0101 1815 .0101 .0101 .0101 .0101 .0101 .0101 .0101 1815 .0101 .				1STA 30S	INT FLOW 5182,446	TRG FLDW 5000	¥ U8J ¥ \$018
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CTIVE FUNCTION FOR VARIABLE 9 ,1071E+04 ,1113E+04 ,1207E+04				ΣΦ	VAR(M) V	083 DEV	ANDMG 241,265
1STA INT FLOW TRG FLOW 1030 124,815 1200,000 1814 1814 1815 1200,000 1814 1814 1815 1819 FLW FLW DRJ FLW 1815 1815 1800,000 1817 1815 1815 1815 1815 1815 1815 1815	OBJECTIVE FUNCTION		.10715+04	.11136+04	.1207E+04		
1STA INT FLD4 TRG FLDW FLW DBJ FLW 305 5162,435 5000,000 ,011 162, 162, 185 5000,000 FLW DBJ FLW 0 PD				18TA 1030	INT FLOW 1214.815	TRG FLUM	71. 000°
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11 03°C 300	VAR 9 ADJ FRUM	6025,26 10	6044.14	Σ÷	VAR(M) 7546+04	OE 0	ANDMG II 236.138

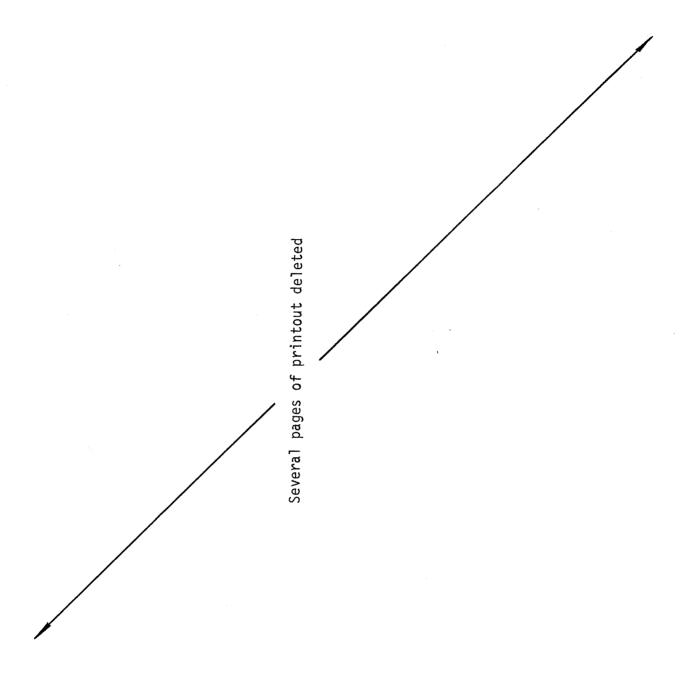
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INT FLOW 1214,815	INT FLOW 5162,435	VAR(M) VAR(M1) .754E+04 .604E+04	INT FLUH 1214,389	INT FLOH 5184,776	VAR(M) VAR(M1) .726E+04 .604E+04	INT FLOW 1213,868	INT FLOW 5207,377	VAR(M) VAR(M1)	.1083E+04	INT FLOW 1215,736	INT FLOW 5128.678	VAR(M1) VAR(M1)	INT FLUM 1215.736	INT FLUW S128.678	VAR(M) VAR(M1) *745E+04 .745E+04	INT FLOW 1215,130	INT FLOW 5150,515
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VAR(M) VAR(M1) .7581+04 .738E+04	INT FLUM 1214.613	INT FLOW 5172,619	VAR(M) VAR(M1) 730E+04 .750E+04	*10685+04	INT FLOW 1216,320	INT FLOW 5106,498	*604E+04 .753E+04	# # # # # # # # # # # # # # # # # # #		JPRT INAME		260. 323.		15.	
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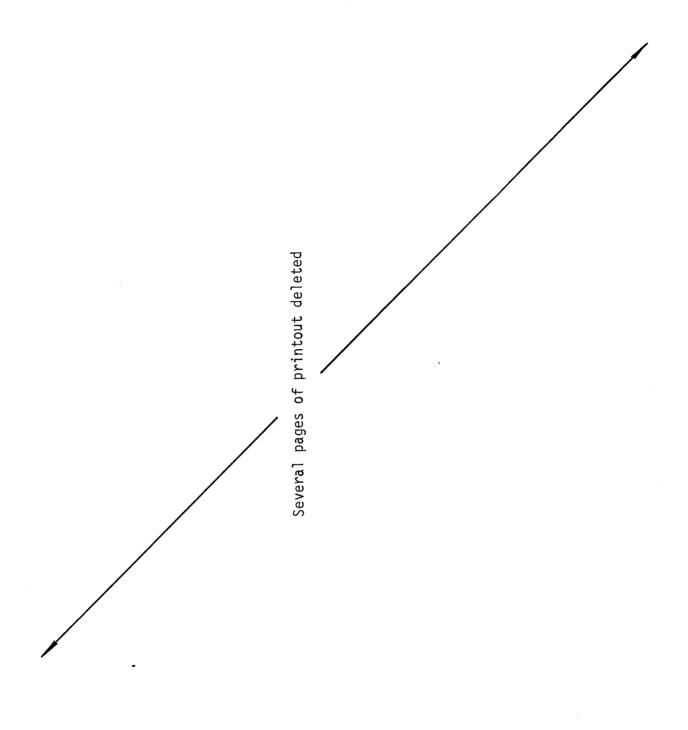
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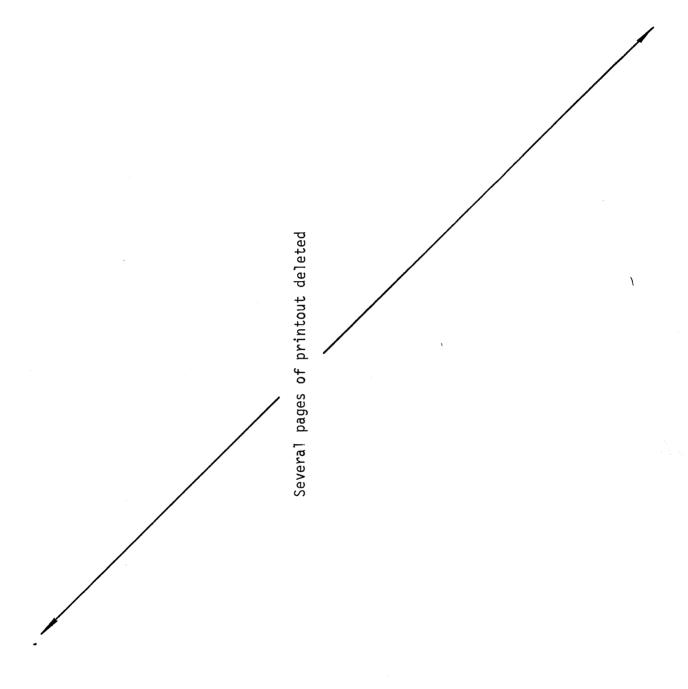
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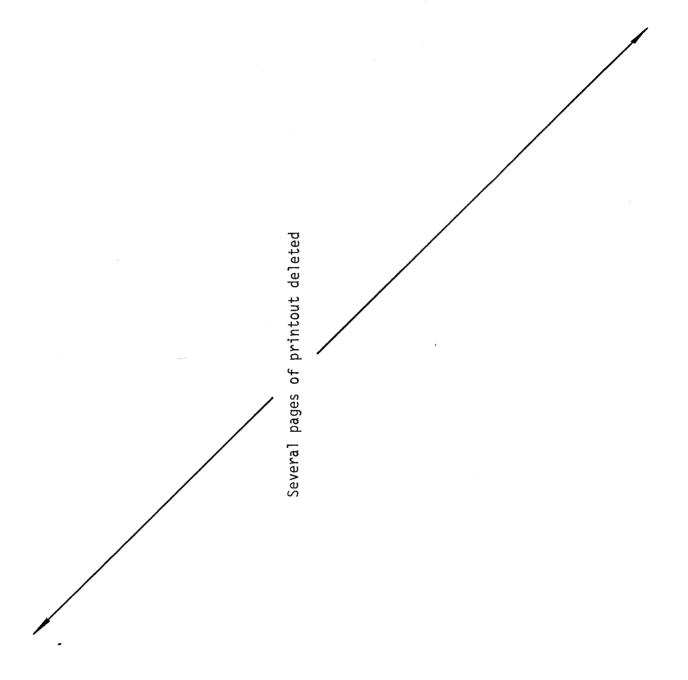
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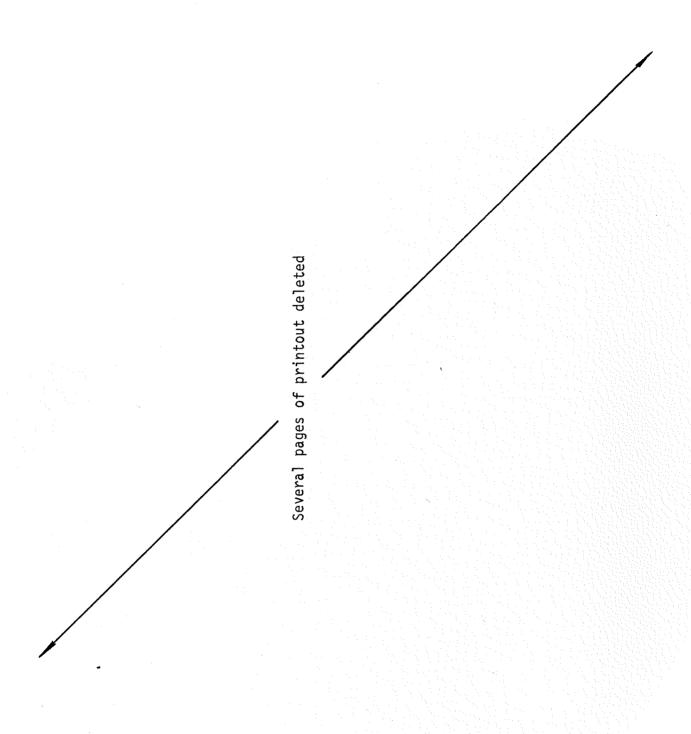
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						(C)	PLAN 1	TYPE 1	00.0		107,26	231,56	2000	106,13	75.28	1064.81	PLAN 2		0.00	00.0	99.		8 . V 0	57.12	52,01	185,77	879.04	
NFLOD 10	305 TYP				10650,000	ANNUAL DAMAGE	305						232.01				305 PI		00.00	0.00	. 85	. .	n co e	3.3B	564.27	94.78	915.43	0.50° # >0
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PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-KATIO ECONOMIC COMPUTATIONS FLOW STORE FLOW IN CUBIC FEET PER SECOND)
AREA IN SWUARE MILES (SQUARE KILOMETERS)

OPERATION	STATION	A REA	₹ ત	RATIO 1	RATTO 2	RATIOS AP	PLIED TO FL KATIO 4	LOWS RATIO S	KAT10 6	RATIO 7	RATIO 8	RATIO 9
HYDROGRAPH AT	S	35.10 90.91)	- ~	1343, 38,02)(1343, 38,02)(1611, 45,62)(1611, 45,52)(2685. 76.03)(2685. 76.03)(3759. 106,44)(3759.	5370. 152.06)(5370. 152.06)(8085, 228,09)(8055, 228,09)	354.54) 354.54) 11814.	17453, 494,20)(17453,	659.073 659.073
ROUTED TO		35.10 90.91)	-~~	1343. 38.02)(588.	1611. 45.62)(663. 18.78)(76.65. 76,03)0 919. 26,03)0	3759. 106,44) 1086. 30,74)	5370. 152,06)(1329. 37,63)(8055, 228,09)(1522, 45,93)(11814. 334.54)(5264. 149.06)(
ROUTED TO	1050	35.10 90.91)	- N	941. 26.65)(526. 14.90)(1139. 32,24). 595.	1940. 54.94)(847. 83.99)(2921. 82.711(1008. 28.54)(4312. 122.10) (1257. 55,58) (6699. 189.70) 1548. 43.83)	288.58) 4177.	2233	20 60 3 3 4 4 2 1 4 5 0 6
HYOROGRAPH AT	, S	35.10	- 2	1343. 38.02)(38.02)(1611. 45.62)(1611. 45.62)(2685. 76,05)(2685. 76,03)(3759. 106,44)(3759. 106,44)(5370. 152.06)(5370. 152.06)(8055, 228.09)(8055, 828.09)(332	17453 494.2016 17453,	MOMO
AGUTEO TO	2030	35.10 90.91)		941. 26.65)(26.65)(1139. 32,24)(1139. 32,24)(1940. 54.94)C 54.94)	82.71) (82.71) (82.71) (4312. 122.10) 4312. 122.10)	6699, 189,703(6699, 189,70)(288,58)(10191, 10191, 288,58)(0 10 0 10
HYDROGRAPH AT	ñ	10.00 25.90)	- ~	453. 12.81) C 453. 12.81) C	543, 15,38)(15,38)(905. 25.63)(25.63)(1267. 35.88)(1267. 35.88)(1610. 51,25)(1610. 51,25)(2715. 76.88)(2715. 76.88)(8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	5883 5883 5883	727
3 COMBINED	30	80.20 207.72)	- '	2219. 62.84)(1664. 47.12)(2676. 75.79)(1968. 55.74)(4563. 129.21)(3201. 90.54)(6859. 194,233(4613. 130,613(10154, 267,533(6620, 187,463(15693. 444.39); 9953. 281.84)(M N J W	1000,86) 24899 705,06)	37.0 (40.0)
ROUTED TO	305	807.72)	- ~	1200. 33.98)(1200. 33.98)(1200. 53,98)(1200. 33,98)(1200. 33.98)(1200. 33.98)(1200, 33,98)(1200, 33,98)(1200. 33,98)(1200. 33,98)(1200. 33.96)(1200. 33.98)(1200. 33.98)(1200. 33.98)(1200; 1200; 13.98)C	33.900 33.900 33.900
			ā	EAK STORAG 1036. 1278.) C 608.	GES IN ACRE 1480. 1833.)(1108.)(FEET (100 3587, 4424,)(1628, 2008,)(0 CUBIC ME 5904, 7283,1 1672, 2062,1	TERS)** 11785,1 11786,1 1775, 2189,1	15876. 19583.)(3021. 3727.)(24937, 30760,)(7774, 9589,)(38699 47734,)(19064 25515,)(53876 56455 32355 39909

SYSTEM COST AND PERFORMANCE SUMMARY (UNITS SAME AS INPUT - NORMALLY 1000'S OF DOLLARS)	ARY UF DOLLARS)	
DTAL SYSTEM CAPITAL COST * * * * * * * * * * *	,6889	
TAL SYSTEM ANDRIIZED CAPITAL COST * * * * * * * *	*867	
TAL SYSTEM ANNUAL DAMBRER AND REPLACEMENT COST *	323.	
TAL SYSTEM ANNUAL COST * * * * * * * * * * * *		931
VERAGE ANNUAL DAMAGES EXISTING CONDITIONS * * *	2211	
VERAGE ANNUAL DAMAGES OPTIMIZED SYSTEM * * * *	233.	
ANNIAL DAMAGE REDUCTION (BENEFITS) * * * *		986
VERAGE ANNUAL SYSTEM NET BENEFITS * * * * * * * *		123.
OPTIMIZATION OBJECTIVE - MAXIMIZE SYSTEM NET BENEFITS FOR TARGET PROTECTION LEVEL ****	TARGET PRUTE	7110N LEVEL ****
TFC9T ANFCST ANOMPR TANCST ANDGBS	ANDMG	TBNETS NTBNET

EXHIBIT 5

SIZING RESERVOIR, PUMPING PLANT AND DIVERSION
(Unconstrained)

A.										<u>LEGEND</u>		N = NEW INPUT DATA	R = REVISED INPUT	Jan Deviced	C- VENTSEN																							
					290	3000	7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2	2						30000	1120	7200						. 35	4480	2			4.7		11.0			500	3000	2720	280	27	,
•	3.0) }		-	5.5	1920	3330	9	₩						21000	1105	0009		0				ن •	6430	3	٠		0.4		? .		· -	• •	1920	3330	30.0	67	U
	3,25				-	0627	•	. In	2					050	15500	109	5550						`~	4800		'n		3,5		7.8			175	٠,	3980	674	53	2.0
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OPTIMIZATION	AND DIVERSION
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		• 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0 • 0		15T ANDMG O FIN(NC)	157 ANDMG O FTN(NC) 70 634.120 .1076+04	181 ANDMG G FIN(NC)
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N O	3.25 4.40	» ^ I Q		083 DEV	083 DEV	080 DEV
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.1066E+04

.1065E+04

.1064E+04

OBJECTIVE FUNCTION FOR VARIABLE 1

VAR 1 ADJ FRUM	4000,00 10	5055,27	NO AZ AZ	VAR(M)	VARCH13	08J DEV	TANCST 469.391	ANDMG 0 582,004	. 10SE+04
			NO N	VAR(M) 495E+03	VAR(M1)	08J DEV	TANCST 469,027	ANDMG 0 582,496	0 FIN(NC)
			NC M M1	VAR(M) . 490E+03	VAR(M1)	08J DEV	TANCST 468,664	ANDMG 0	0 FIN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	OR VARIABLE 7	.1051E+04	*1052E+04	.1052E+04					
VAR 7 ADJ FRUM	500.00 TB	750.00	NC M M	VARCM) . 100E+04	VAR(M1) .750E+03	083 DEV	TANCST 487,619	ANDMG ()	105E+04
			N W W	VAR(M)	VAR(M1)	083 DEV	TANCST	ANDMG 0 559,987	FIN(NC) .105E+04
			NC M MI	VAR(M) .980E+03	VAR(M1)	083 DEV	1ANCS7	ANDMG 0 561,207	0 FIN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	OR VARIABLE 9	.1046E+04	.1047E+04	.1047E+04					
VAR 9 ADJ FRUM	1000,00 10	1500,00	E H CON	VARCM)	VAR(M1) .150E+04	08J DEV 0.000	TANCST 513,309	ANDMG 0 505,468	0 FTN(NC)
			E ON	VAR(M) .500E+04	VAR(M1)	08J DEV 0.000	TANCST 511.556	ANDMG 03	FTN(NC) • 1026+04
			NC M MI 3 1 9	VAR(M)	VAR(M1)	08J DEV	TANCST 509,803	ANDMG 0 509,724	. 10ZE+04
OBJECTIVE FUNCTION FOR VARIABLE	JR VARIABLE 1	.1019E+04	.10198+04	.1020E+04					
VAR 1 ADJ FROM	5055.27 10	7582,91	NC A A	VAR(M) .750E+03	VAR(M1) .758E+04	084 DEV	TANCST S77,444	ANDMG 0.	0 FIN(NC)
			NC 4 3	VAR(M)	VAR(M1)	083 080	TANCST 576,896	ANDMG 0	. 101E+04
			NC X X X	VAR(M) .735E+03	VAR(M1) .758E+04	08J DEV	TANCST 576,349	ANDMG 0	FIN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	IR VARIABLE 7	.1005E+04	*1005E+04	.1005E+04					

		NC M M1	VARCM)	VAR(M1)	000 ° 0	TANCST 004.961	ANDMG O FTN(NC) 400.764 .101E+04
VAR 7 ADJ FRUM 750.00 TG	0 862,50	A A W	VAR(M)	VAR(M1) .863E+03	083 DEV 0•000	1ANCS1 585,680	ANDMG O FTN(NC) 418,435 .100E+04
		NC M M1	VAR(M)	VAR(M1)	08J DEV	TANCST 584,910	ANDMG O FTN(NC) 419.866 .100E+04
		NC ON HI	VAR(M)	VAR(M1) .863E+03	08J DEV	TANCST 584,139	ANDMG O FIN(NC)
DBJECTIVE FUNCTION FOR VARIABLE 9	9 .1004E+04	*1005E+04	.1005E+04				
VAR 9 ADJ FRUM 1500.00 TO	09°0522	NC A	VAR(M) .758E+04	VAR(M1)	0000 0	TANCST 628,344	ANDMG O FIN(NC) 357,691 ,986£+03
		NC M M1	VARCM)	VAR(M1)	083 DEV	TANCST 626,570	ANDMG O FIN(NC) 359.038 .986E+03
		NC M M1	VAR(M)	VAR(M1)	083 DEV 0,000	TANCST 624,795	ANDMG O FIN(NC) 350,389 ,985E+03
OBJECTIVE FUNCTION FOR VARIABLE 1	1 .9860E+03	. 9856E+03	*9852E+03				
		NC NEW	VAR(M)	VAR(M1)	08J DEV	TANCST 564,209	ANDMG D FTN(NC) 432,969 .997E+03
VAR 1 ADJ FRUM 7582,91 TO	6824,62	NO A H	VAR(M)	VAR(M1)	083 DEV 0.000	TANCST 610,603	ANDMG O FIN(NC) 371,331 ,982E+03
		NC X X X	VAR(M) .854E+03	VAR(M1) .682E+04	GBJ DEV	TANCST 609,970	ANDMG O FTN(NC) 371,968 ,982E+03
		NC N N N N N N N N N N N N N N N N N N	VAR(M) .845E+03	VAR(M1) .682E+04	08J DEV	TANCST 609,337	ANDMG O FIN(NC) 372,543 ,962E+03
OBJECTIVE FUNCTION FOR VARIABLE 7	.98196+03	.9819E+03	.9819E+03				
		NC M MI	VAR(M)	VAR(M1)	08J DEV 0,000	TANCST 641.426	ANDMG O FIN(NC) 346.294 .988E+03
		NC DE T	VAR(M) .225E+04	VAR(M1)	08J DEV	TANCST 620,095	ANDMG O FTN(NC) 364,329 .984E+03
		E O I	VAR(M)	VAR(M1)	083 DEV	TANCST 613,450	ANDMG O FIN(NC) 369,048 ,982E+03
		NC M M	VAR(M) .225E+04	VAR(M1) .863E+03	083 DEV	TANCST 610,603	ANDMG O FIN(NC)
		NO N	VAR(M) .223E+04	VAR(M1) .863E+03	08J DEV 0.000	TANCST 609.075	ANDMG O FTN(NC) 372,993 ,9826+03
		NC M #1	VAR(M)	VAR(M1)	08J DEV 0,000	TANCST 607.547	ANDMG O FTN(NC) 374,569 ,982E+03
OBJECTIVE FUNCTION FOR VARIABLE 9	.9819E+03	.9821E+03	.9821E+03				

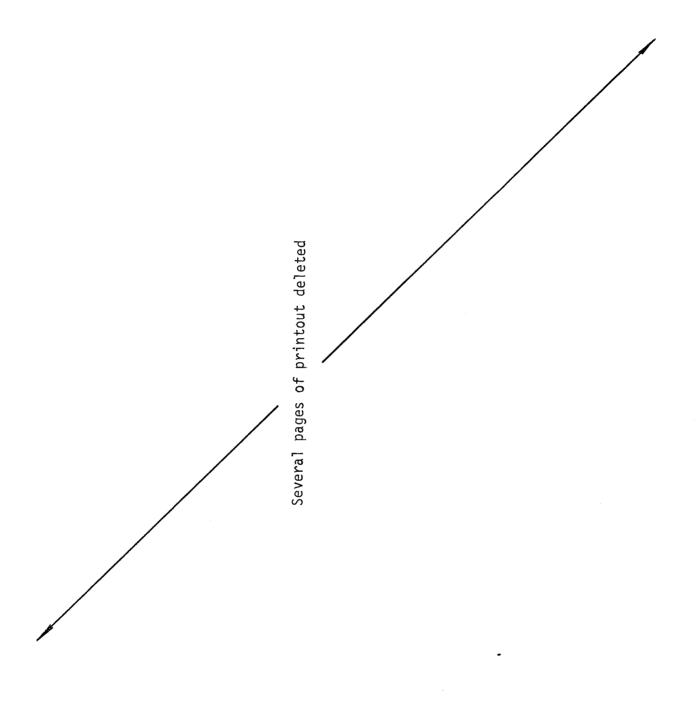
		N N	Σ 1 2	VAR(M)	VAR(M1)	08J DEV	1ANCST	ANDMG 1	PTN(NC)
		2 -	E TO	VARCM)	VAR(M1)	08J DEV	TANCST 633,517	350.327	0 FIN(NC)
		Š	F F	VAR(M)	VAR(M1)	087 DEV 0.000	TANCST 617,477	364.816	0 FIN(NC) .982E+03
		S L	E O	VAR(M)	VAR(M1)	083 DEV 0,000	TANCST 610,603	371.331	982E+63
		Ų N	Ξ° Σ ··	VAR(M)	VAR(M1)	08J DEV	TANCST 608,900	372.610	982E+03
		U M	Σ	VAR(H)	VAR(H1)	08J DEV 0.000	TANCST 607,137	373.910	981E+03
OBJECTIVE FUNCTION FOR VARIABLE 1 .981	8198+03 ,98156	15E+03		.9810E+03					
		Q -	Σ	VAR(M) .863E+03	VAR(M1)	083 087	TANCST 546.666	ANDMG 454,123	100E+04
		S.	Σ . Σ	VAR(M)	VAR(M1)	083 050	TANCST 593,204	390.554	. 984E+63
VAR 1 ADJ FRUM 6824.62 TO 66	51 9 •88	υ 	# T	VAR(M) .863£+03	VAR(M1)	083 DEV	1ANCS1 605,380	STS.403	981E+03
		N N	E Z	VAR(M)	VAR(M1)	083 DEV	TANCS1	ANDHG 376.040	0 FTN(NC) .981E+03
		D W	7 W	VAR(M)	VAR(M1)	083 DEV	TANCST 604,114	376,619	0 FIN(NC)
OBJECTIVE FUNCTION FOR VARIABLE 7 ,980	808E+03 .980	08E+03		.9807E+03					
		u →	π ο π ο 7	VAR(M)	VAR(M1)	08J DEV	TANCST 636,203	350,384	. 987E+03
		Z -	E O	VAR(M)	VAR(M1) .992E.+03	08J DEV	TANCST 614,872	ANDMG 368,428	0 FTN(NC) .983E+03
		U →	3 × 0 ×	VAR(M)	VAR(M1)	08J DEV	1ANCST 608.227	ANDMG 373.110	.981E+03
		U ↔ Z	Σ Φ	VAR(M)	VAR(M1)	000.0	TANCST 605,380	ANDMG 375.403	981E+03
		U N	π. Σ 0 3	VAR(M)	VAR(M1) .863E+03	083 DEV 0.000	TANCST 603.852	ANDMG 577.068	FINENC)
		S W	E O	VAR(M)	VAR(M1) .863E+03	08J DEV	TANCST 602,325	ANDHG 378,649	0 FTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE 9 .980	9808E+03 .98	.98095+03		.9810E+03					

ANDMG O FIN(NC) 312.015 .994E+03	ANDMG O FIN(NC) 354,389 .983E+03	368,885 .981E+03	375,403 ,981E+03	377,223 ,981E+03	ANDMG O FTN(NC) 379,187 ,981E+03		374,796 981E+03	ANDMG G FTN(NC)	ANDHG O FTN(NC) 375,348 .981E+03					
TANCST 681.762	TANCST 628.294	TANCST 612,254	TANCST 605,380	TANCST 603,688	TANCST 601,999		TANCST 606,020	TANCST 605,572	TANCST 605,438	**		IAUTO 0		2000 2000 2000 2000
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VAR(M) .662E+04	VAR(M)	VAR(M)	VAR(M) . 602E+04	VAR(M)	VAR(M)	.9812E+03	VAR(M) .863E+03	VAR(M)	VAR(M) *863E+03	长女女女	NOI	LT JPRT 0	READ FROM TAPE	48. 260. 1150. 151. 151.
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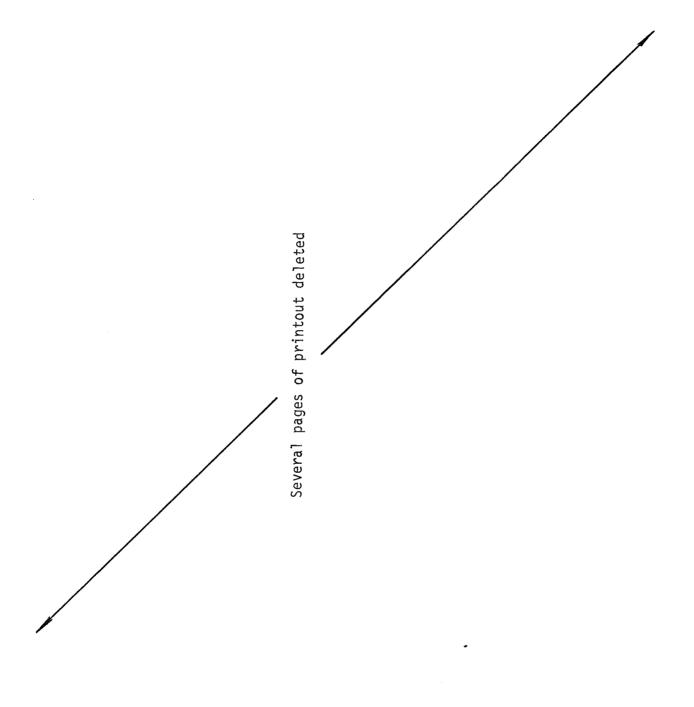
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MAXIMUM STORAGE #



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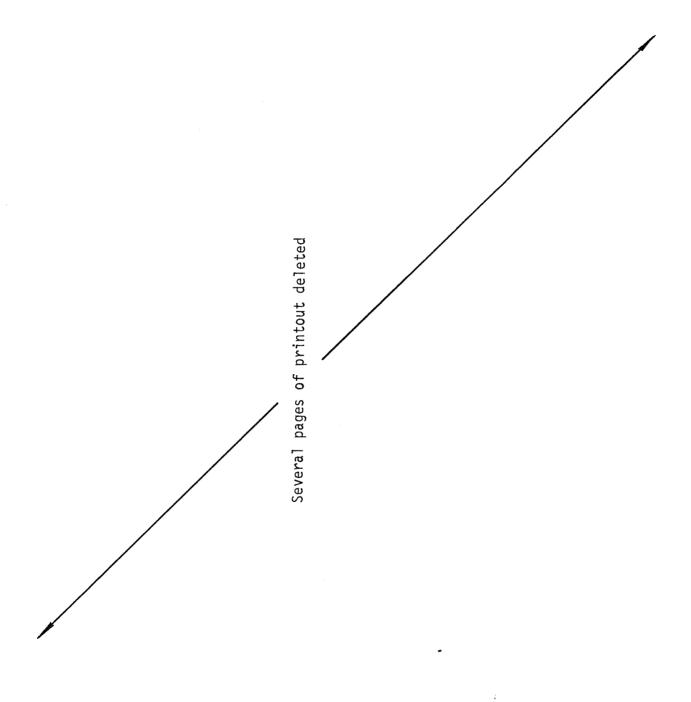
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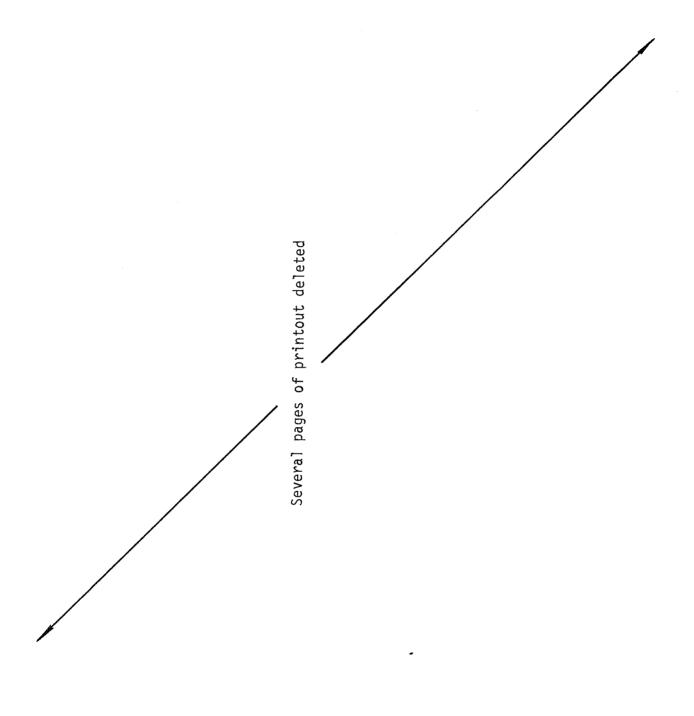
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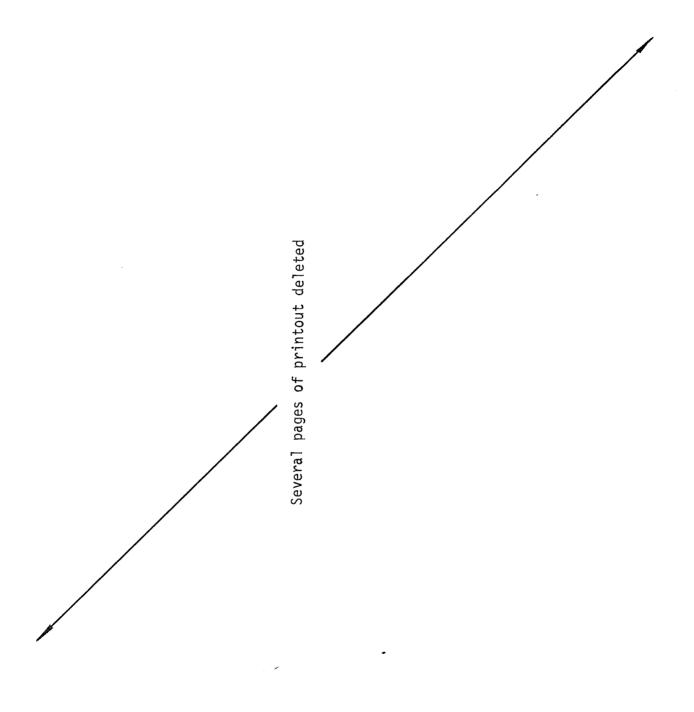


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FRED PEAK
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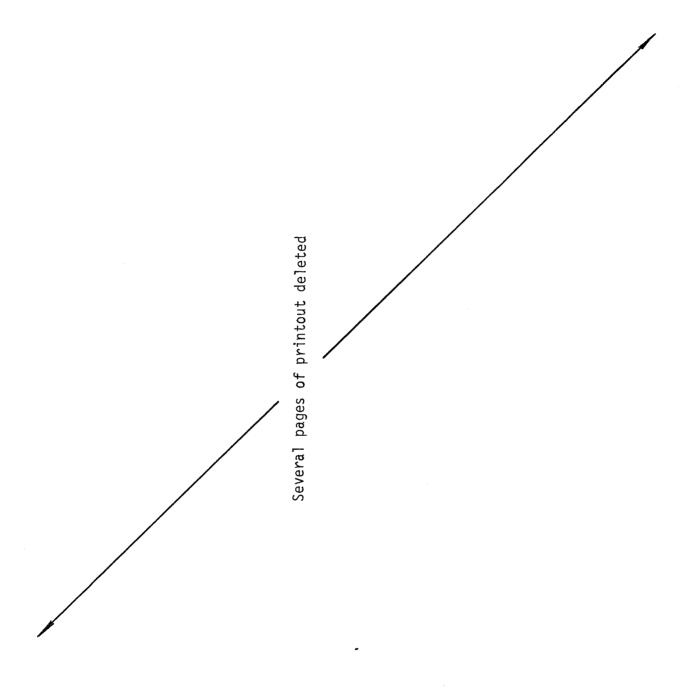
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PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIU ECONOMIC CUMPUTATIONS FLOW IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND)
AREA IN SQUARE MILES (SQUARE KILOMETERS)

OPERATION	STATION	AREA	PLAN	RATIO 1	RATIO 2	RATIUS APE RATIO 3	PPLIED TO FL	OWS RATIO S	RATIO 6 1.50	RAT10 7 2.20	RAT10 8 3,25	RATIO 9
HYDROGRAPH AT	2	35.10		1343. 38.02)(1343. 38.02)(1611. 45.62)(1611. 45.62)(2685. 76.03)(2685. 76.03)(3759. 106.44)(3759. 106.44)(5370. 152.06)(5370. 152.06)(8055 228.09)(8055, 228.09)(11814, 334,54)(11814, 334,54)(17453. 494.20)(17453. 494.20)(23628* 669.07) 23628. 669.07)
ROUTED TO		35.10 90.91)	~~~~~	1343, 38,02)(588, 16,65)	1611. 45.62)(666. 18.86)(2685, 76,03)(909, 25,73)(3759. 106.44)(1085. 30.72)(5370. 152.06)(1324. 37.48)(8055, 228,09)(1758, 49,78)(11814, 334,54)(6435, 182,21)(17453, 494,20)(12179, 344,86)(23628. 669.07) 18164. 514.34)
ROUTED TO	1030	35.10	-~~~	941. 26.65)(525. 14.86)(1139 32,24)(594, 16,83)	1940. 54.94)(838. 23.73)(2921 82,71)(1005, 28,47)(4312. 122.10)(1252. 35.46)(6699, 189,70)(1583, 44,83)(10191. 288.58)(5038. 142.65)(15177 429,773 10185, 288,413(20603. 563.423 15470.
HYDROGRAPH AT	, 02	35.10		1343. 38.02)(1343. 38.02)(1611. 45.62)(1611. 45.62)(2685, 76.03)(2685, 76.03)(3759. 106,44)(3759. 106,44)(5370. 152.06)(5370. 152.06)(8055. 228.09)(8055. 228.09)	11814. 334.54)(11814. 334.54)(17453 494.201 17453 494.201	23628, 669,073 23628, 669,073
ROUTED TO	5 0 2	35.10 90.91)	_ `~ `	1343. 38.02)(1346. 38.12)(1611, 45,62)(1549, 43,86)(2685. 76.03)(1830. 51.82)(3759. 106.44)(2903. 82.20)(5370. 152.063(4524. 128.12)(8055. 228.09)(7215. 204.32)(11814. 334.54)(10985. 311.07)(17453. 494.20)(16640.	23628 669.07) 22833.
ROUTED TO	2030	35,10	ม ัก ั	26.65)(26.65)(26.61)(1139. 32.24)(1115. 31.56)(1940. 54.94)(1430. 40.49)(2921. 82.711(2080. 58,901(4312. 122.10)(3507. 99.31)(6699, 189,70)(5756, 162,98)(10191. 288.58)(9253. 262.02)(15177. 429.77)(14254. 403.64)(20603 583,423 19694 557,673
HYDRUGRAPH AT	30	10.00	- " ~ "	453, 12,81)(453, 12,81)(543 15,38)(543 15,38)(25,63)(25,63)(25,63)(1267. 35.88)(1267. 35.88)(1810. 51.25)(1810. 51.25)(2715, 76,88)(2715, 76,88)(3982. 112,76)(3982. 112,76)(5883, 166,573(5883, 166,573(225,552) 225,552) 225,552)
3 COMBINED) 8	80.20 207.72)	→~~	2219. 62.84)(1660. 46.99)(2676. 75.79)(1939. 54.90)(4563, 129,21)(2602, 73,67)(6859; 194,23)(3752; 106,25)(10154. 287.53)(5793. 164.05)(15693, 444,39)(8998, 254,81)(23748. 672.47)(14293. 404.74)(35345, 1000,80)(25799, 730,54)(480118 1359.53) 385358 1091.19)
ROUTED TO	302	80.20	7 2	1200. 33.98)(1200. 33.98)(1200. 33.98)(1200. 33.98)(1200. 33.98)(1200. 33,98)(1200. 33,98)(1200. 33,98)(1200. 33,98)(1200. 33,98)(1200. 33,98)(1200. 33,98)(1200. 33.98)(1200. 33.98)(33,98)(33,98)(33,98)(1200 33,983 1200
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SYSTEM OPTIMIZATION RESULTS VAR 3 VAR 4 VAR 5 VAR 6 DIV 7 0. 0. 0. 663,	SYSTEM COST AND PERFORMANCE SUMMARY (UNITS SAME AS INPUT - NORMALLY 1000'S OF GOLLARS)	7099.	* 1	SYSTEM ANNUAL COST * * * * * * * * * * * * * * * * * * *	S ** EXISTING CONDITIONS * * * 1177.	AVERAGE ANNUAL DAMAGES OPTIMIZED SYSTEM * * * * 375. AVERAGE ANNUAL DAMAGE REDUCTION (BENEFITS) * * * *	SYSTEM NET BENEFITS * * * * * * *	***** OPTIMIZATION CRIEFFIUE . MAXIMIZE SYCIEM NOT RENEFETS		
4AR 1 VAR 2 VA 5620. 0.		TOTAL SYSTEM CAPITAL COST * * *		TOTAL SYSTEM ANNUAL COST	AVERAGE ANNUAL DAMAGES	AVERAGE ANNUAL DAMAGE AVERAGE ANNUAL DAMAGE	AVERAGE ANNUAL SYSTEM	N FAC		

NTBNFT 113.

18NF18 546.

ANDMG 632.

TANCST

ANDMPR 201.

EXHIBIT 6

SIZING LEVEE AND CHANNEL MODIFICATION (Unconstrained)

	8		v	1290 1920	3330	10-10-10-10-10-10-10-10-10-10-10-10-10-1	5.						4800 5620								2620				7.23			
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	05.		ir e	910	3100 777	•	ê	Ē	***	3080 10050			3200)))	n eo	ω <u>π</u>	4.4	•	9300	540	21000	.25	.73	17,51	20°44		•	7,98
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· 通過的記載的	0 . 50 - 2000	TENTIAL	· Au	710			~ ~	TENT		000 800	-		1130	100	•	0 4	٠	15.6	00	507 -	9540	0 A	•	6.16 0	15.03	00.	•	ر درج
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- 21.0°) () () (2000	000	- :# T (T	•			> 1				***		5620			•				5650		13.9		13.9				170	40	0111	75.	-0									AMAGE REACI	RDER TO CON	EVEE IN REI	AMAGES.
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33	5	050	5	3.		AND/OR BYDA	-		940	2050	9).r	.0.s	1740	12100	7,	34.5	.0504	7000	222	1740	12100	3 •	34.5	= u ~ ∑		ERAY POU		-)	۸ د د ک	- W	• ^ •	; ;		FOREBAY		UGH LEVEE								
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FLCOD CONTROL SYSTEM COMPONENT OPTIMIZATION SIZING LEVEE AND CHANNEL MOIFICATION UNCONSTRAINED

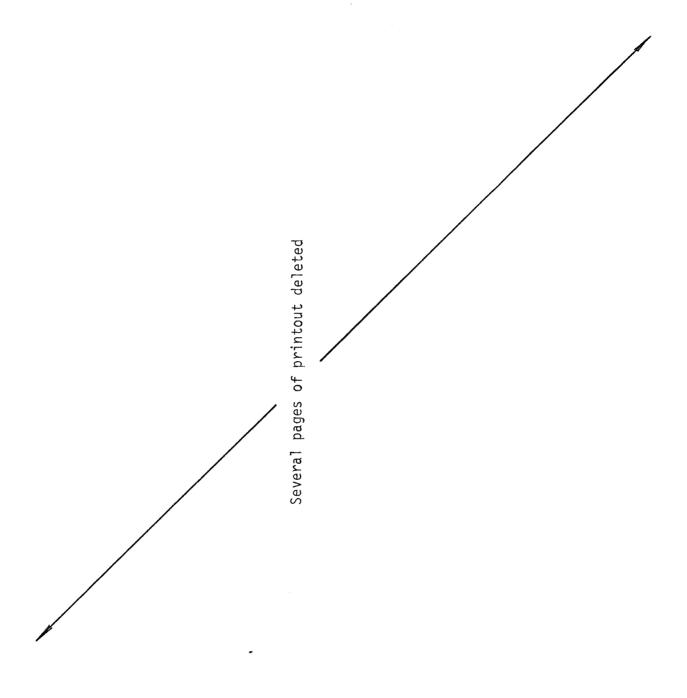
			JOPER NWT LROPT TRACE	TAN REIKC THU CROPT TRACE	2			
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			FCAP FDCDS	INPUT FAN				
			EN U	MI VAREMS	VAR(H1)	083 DEV	TANCST 6,980	ANDMG OF TN(NC) 52,791 ,598E+02
			E NI	MI VAR(M)	VAR(M1)	08J DEV	TANCST 6.953	ANDMG O FIN(NC) 52.965 .599E+02
			E NI	MI VAR(M)	VAR(M1)	08J DEV	1ANCST 6,925	53,165 . 601E+02
DBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 2	.5977E+02	. 5992E+02	*6009E+02				
VAR 2 ADJ FROM	2000.00 TO	2104,43	E M	M1 VAR(H) 2 .200E+04	VAR(M1)	OBJ DEV	7.121 7.121	ANDHG O FTN(NC) 51,766 ,589E+02
			EM UN Z	MI VAR(M)	VAR(M1)	DBJ DEV 0,000	TANCST 7.094	ANDMG O FIN(NC) 51.766 .5898+02
			EM UM Z	M1 VAR(M)	VAR(M1)	08J DEV	TANCST 7,067	SI.912 SPOE+02
OBJECTIVE FUNCTION	FUNCTION FOR VARIABLE 3	.5889E+02	.5886E+02	.5898E+02				
VAR 3 ADJ FROM	2000,00 10	1986,30	Σ N	MI VAR(M)	VARCH1)	OBJ DEV	TANCST 7.103	51.766 .589E+02
			ΣN UN Z	MI VAR(M)	VAR(H1)	UBJ DEV	TANCST 7.074	ANDMG D FTN(NC) 51,972 .590E+02
			EN UM	N: VAR(M)	VAR(M1)	084 DEV	TANCST 7.046	ANDMG () FIN(NC) 52,179 ,5925+02
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 2	CAR7F402	CO+3E-00E	C C T 4C C C C F				

			EM	VAR(M)	VAR(M1)	58J DEV	1 ANCOT	ANDHG 43.966	O FINCNCS
VAR & ADJ FRUM	2104.43 10	3156,65							
			E M	VARCM)	VAR(M1)	000 0 0 000	TANCST 8,503	ANDMG 44.112	STANCED.
			E M	VARCH)	VAR(M1)	08J DEV	TANCST 8.477	ANDWG 44.255	0 FIN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 3	.5250E+02	*5262E+02	\$273E+02					
VAR 3 ADJ FROM	1986.30 TO	2979,44	EN CP	*316E+04	VAR(M1)	000.000	1ANCST 9.878	37.259	0 FIN(NC)
			E AL	VAR(M)	VAR(M1)	08J DEV	TANCST 9,835	37.416	0 FIN(NC)
			E N UM	VARCH)	VAR(M1)	000°0	1ANCS1	37.596	O FINENCS
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 2	.4712E+02	.47256+02	.4739E+02					
VAR 2 ADJ FROM	3156,63 10	4734.97	E W	VAR(M)	VARCH13 4473E+04	000.000	1ANCS1	30,881	AZ9E+02
			N W W	VARCED +295E+04	VAR(M1)	000°0	TANCST	31 . Ou 7	# FINCHC)
			E M	VAR(M)	VAR(M1)	08J 0EV	TANCST.	N S S S S S S S S S S S S S S S S S S S	# FTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 3	4290E+02	.4303E+02	.4315E+02					
VAR 3 ADJ FROM	2979•44 10	4469.17	E N E N	VAREM) .473E+04	VAR(M1)	000.0	14.041	23.604	0 FTW(NC)
			E N	VAR(M)	VARCM1)	OBJ DEV	TANCST 13.976	ANDMG 23.744	# FTN(NC)
			N N N N N N N N N N N N N N N N N N N	VARCED.	VAR(M1)	083 057	TANCST 13.912	ANDAG 33.888	# FTN(NC)
OBJECTIVE FUNCTION FOR	FOR VARIABLE 2	.3764E+02	.3772E+02	*3780E+02					
			E M	VAR(M)	. 701E+04	083 DEV	TANCST 23.176	19.277	0 FIN(NC)
			E S	VARCM)	VAR(M1)	08J DEV	TANCST 17.223	ANDMG 21.880	391E+02
VAR 2 ADJ FROM	4734.97.10	4939,90	₩ EM UH	VAR(M)	VAR(M1)	084 DEV 0.000	TANCST 14,319	W NO S NO	.374E+02
			E M	VAH(M)	VAR(M1)	000°0	14.258	ANDHG 23.247	TTNCNC MASE + 02
			E M	VARCH)	VAR(M1)	000000	TANCST 14.197	ANDHS 23.438	. FTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	FOR VARIABLE 3	.3737E+02	.37516+02	.3764E+02					

			2 -	EN	VAR(R)	VARCHI)	08J DEV	7ANC87	ANDHG 16.449	0 FINCHC)
VAR & ADJ FROM	4469,17 TO	91 N 9 . St		EM EN	*494E+04	VAR(M1)	000.000	TANCST 15.081	ANDMG 20,683	0 FIN(NC)
			2-	Σ W Σ Σ Σ	VAR(M) .514E+04	VAR(M1)	090 080 0*000	TANCS1	ANDMG 20.683	.367E+02
			Š	EN	VARCM)	VAR(M1)	083 DEV 0,000	TANCST 15,634	ANDRG 20,913	0 FTM(NC)
			UM Z	ΞM	VAR(M)	VAR(M1)	083 DEV 0.000	14NCST	ANDMG 21.141	O FINENCY
OBJECTIVE FUNCTION FOR VARIABLE	VARIABLE 3	.3666#+02	.3655E+0	ſŒ.	.3643£+02					
			y - z	E N	VAR (M)	VAR(M1)	081 DEV	12,904	ANDMG 28,100	n FTM(NC)
			2	ΞM EN	VAR(M)	VAR(M1)	000 000	14 SST	22.653	O FTM(NC)
VAR 3 ADJ FROM	5139,54 TO	4985,36	SN →	Σ M Σ	VAR(M)	VAR(M1) . 499E+04	08J.DEV 0.000	15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ANDMG-21.366	0 FIN(NC) ,364E+02
			U ~ Z	ΣN	VAR(M)	VAR(M1)	080 0EV	1ANCS1	ANDHG 21.366	FTN (NC)
			2~	E N	VAR(M)	VAR(M1)	083 DEV	14NCST	Z L G L G	G FIN(NC)
			UP Z	E N	VAR(M)	VAR(M1)	OBJ DEV	1ANCS1	ANDMG 21.619	0 FIN(NC)
OBJECTIVE FUNCTION FOR	VARIABLE 2	.36396+02	.36438+02	Ru.	3650E+02					
VAR Z ABJ FROM	4939,90 10	2016	U → Z	E W	VAK(M) 4098+04	VAR(M1) SORE+04	OBJ DEV 0,000	15.210	ANDAG 21.154	STN(NC)
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MAXIMUM STURAGE #



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			### DATA FOR STATION 1030 PLAN 1 PEAK STATION 1030 PLAN 1 1900 1300 0.000 0.	PLAN 1 TYPE 2 TYPE 3 TYPE 2 TYPE 3 TY	PEAK SUM 317PPE 1 TYPE 2 TYPE 2 0.000 1030. 1330. 10.000 0.000 0.000 1.500. 1340. 2.400 2.000 0.	EG PEAK SUM TYPE 1 TYPE 2 TYPE 8 0.000 0.0
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			### DATA FOR STATION 1030 PLAN 1 PEAK SUM 174PE 1 TYPE 2 130. 0.000 0.	PLAN 1 TYPE 2 TYPE 3 TYPE 3 TYPE 3 TYPE 3 TYPE 3 TYPE 4 TYPE 2 TYPE 3 TYPE 4 TYPE 4 TYPE 5 TY	PEAK SUM TYPE 1 TYPE 2 TYPE 2 0.000 1030. 1380. 1380. 1.600 0.000 0.000 0.000 0.000 1.800. 1740. 2.400 0.000	PEAK SUM TYPE 1 TYPE 2 TYPE 8 1030 0.000 0
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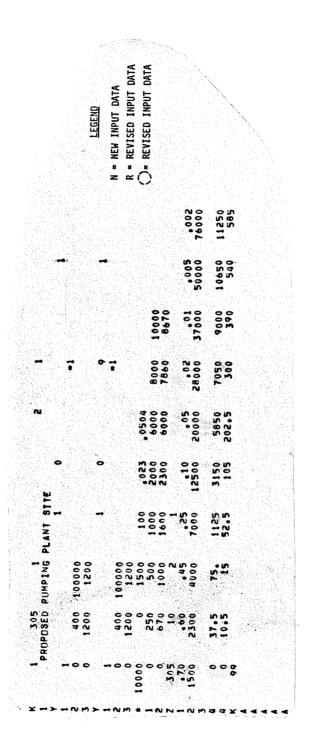
EXHIBIT 7

SIZING RESERVOIR, PUMPING PLANT, DIVERSION
AND UNIFORM PROTECTION LOCAL PROJECTS

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FLOC 2312	FLOOD CONTROL SYSTEM CUMPONENT OPTIMIZATION SIZING RESERVOIR, PUMPING FLANT, DIVERSION AND UNIFORM PROTECTION LOCAL PRUJECTS(LEYEE AND CHAMNEL MODIFICATION) UNCONSTRAINED	JUB SPECTFICATION NOT WHEN WAIN 10AY THE JAIN NETEC JPLT IPRT NSTAN O	MULTI-PLAN ANALYSES TO BE PERFORMED NPLAN= 2 NRTIU= 9 (RTIO= 1	VAR 1 VAR 2 VAR 3 VAR 4 VAR 5 VAR 6 DIV 7 DIV 8 RWP 9 PWF 10 = 4000. = 200. 0. = 1000. 0. = 1000.	FIXED COST INPUT FAN FCAP FDCNT FAN 0. 0.0000 0.0000	1814 INT FLOW FLW GBJ FLW GBJ 1030 6015.571 0.000 0.000	ISTA INT FLOW TRG FLOW FLW UBJ FLW DEV 7808.356 0.000 0.000	NC M N1 VAR(M1) OBJ DEV TANEST ANDMG OFTNING) 1 1 1 .400E+04 0.000 464.697 600.574 .107E+04	1050 6054.577 TRG FLUM FLM 06.0 0.000 0.000 0.000	1574 INT FLOW FLW FLW 093 FLW 080 0.000 0.000	NC M M VAR(M) VAR(M) UBJ DEV TANCST ANDMG II FTN(NC) 2 1 1 .396E+04 0.000 463.166 602.957 .107E+04	187A 1NT FLOW 1RG FLOW FLW ORU FLW DEV 0.000 0.000	ISTA INT FLOW FLAW FLAW FLAW FLAW DBJ 6.000 0.000	NC H M1 VAR(M1) VAH(M1) OBJ DEV TANCST ANDHG G FINING) 3 1 1 .392E+04 0,000 461,657 605,347 ,107E+04
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			18TA 1030	1017 FLON	TRG FLUW 0,000	FLM CBJ	FLW DEV
			1STA 2030	INT FLOW 7808.356	TRG FLOW	FLW DBJ	FLW DEV
VAR 1 ADJ FROM	4000,000	5190,33		.200E+03 .519E+04	08J DEV	500.169 548,857	0 FIN(NC)
			18TA 1030	INT FLOW 4646,889	TRG FLOW 0.000	FLW 083	FLE DEV
			102 2030	INT FLOW 7839-689	TRG FLOW 0.000	FLW 08J	FLH DEV
			¥ N	*198E+03 *519E+04	08J DEV 0.000	TANCST ANDMG 500,340 548,643	0 FTN(NC)
			181A 1030	127 FLO3	TRG FLUW 0.000	FLW 085	FLW DEV
			ISTA 2030	127 FLOW 7871-148	TRG FLUW 0.000	FL* 08.	FLW DEV
			E N	.196E+03 .519E+04	08J DEV	SOO,491 548,624	105E+04
OBJECTIVE FUNCTION FOR WARIABLE	FOR VARIABLE 2	.1049E+04	.1049E+04	.1049E+04			
			18TA 1030	INT FLOM	78G FLOW 0.000	FLW 085	PLM DEV
			181A 2030	1NT FLOW 7834,109	TRG FLOW 0,000	FLW CBJ	FLW DEV
VAR 2 ADJ FROM	200,00 TO	198,36	- C - C - C - C - C - C - C - C - C - C	.500E+03 .198E+03	08J DEV	TANCST ANDMG 500.313 540.647	0 FTN(NC)
			19TA 1030	INT FLOW 4641,270	TRG FLOW	000°0	FLX DEV
			19TA 2030	INT FLOW 7839,954	TRG FLOW 0.000	000°0	FLW 0EV 0.000
			N N N N N N N N N N N N N N N N N N N	.495E+03 .198E+03	08J DEV	TANCST ANDMG	0 FTN(NC)
			1914 1030	INT FLOW 4641,270	TRG FLOW	000°0	FLW DEV
			19TA 2030	INT FLOR 7645.600	TRG FLOW 0.000	FL* OBJ	FL# DEV
			T N E N	VAR(M) VAR(M1)	083 DEV	TANCST ANDMG 499, 626 549, 541	- 105E+04
OBJECTIVE FUNCTION FOR VARIABLE	OR VARIABLE 7	*1049E+04	*1049E+04	•1049E+04			

			1030	INT FLOW 4641.270	TRG FLUW 0.000	FLW UBJ	FLW 060
			18TA 2030	INT FLOW 7578-270	TRG FLOW	FL* 085	FLE DEV
VAR 7 ADJ FROM	\$00°.00 TD	750,00	NC A	VAR(M) VAR(M1)	UBJ DEV 0.000	TANCST ANDMG 517.659 527.738	0 FTN(NC) .105E+04
			4 m o	1NT FLOW 4641,270	TRG FLUM	780 M L W 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	> 000 .000 .000
			# # # # # # # # # # # # # # # # # # #	INT FLOW 7578-270	TRG FLOW 0,000	FLW CBJ	FL 0.000
				.990E+03 .750E+03	08J DEV 0.000	TANCST ANDMG (516,779 528,959	0 FTN(NC)
			18TA 1030	INT FLOW 4641,270	TRG FLOW	FLW 08J	FLW DEV
			181A 2030	7578-270 7578-270	TRG FLOW 0.000	7000°	>0 20 30 31
			NC & KW	.980E+03 .750E+03	000.000	TANCST ANDMG C	FINCNC)
OBJECTIVE FUNCTION F	FUNCTION FOR VARIABLE 9	.104SE+04	.1046E+04	•1046E+04			
			18TA 1030	INT FLOW 4641.270	TRG FLOW	FLW 08J	FL W DE C
			18TA 2030	INT FLOW 7578,270	TRG FLOW	FL* 080.	FL # 066
VAR 9 ADJ FRUM	1000,00 TC	1500,00		.519E+04 .150E+04	083 DEV	TANCOT ANDMG O	FTNCNC)
			1030	INT FLOM	TRG FLOW	7800 M 14	FLW DEV
			15TA 2030	127 FLOW	TRG FLUW 0.000		720 0000 0000
			NC 2 %	.514E+04 .150E+04	053 DEV 0,000	541.629 476.321	0 FTN(NC)
			181 4030	INT FLOW 4758,866	TRG FLOW	FL* C8.	FLW DEV
			18TA 2030	INT FLOW 7578,270	TRG FLOW 0,000	FLW 083	FL# DEV
			NC H H	.509E+04 .150E+04	08J DEV	SSO. 912 478.401	D FTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	DR VARTABLE 1	.10186+04	.1018E+04	.1018E+04			

FLW DEV	FLW DEV	*101E+04	FLW DEV	>0.00.0	. 101E+04	FLM DEV 0.000	FLE DE C	. FTN(NC)		FLW DEV	FLE DEV	0 FTN(NC)	900°0	FLW DEV	O FINCED.	FLH DEV 0.000	FLW DEV	FTN(NC)	FLW DEV 0.000	FLW DEV
0000°0	7000°0 LLW 08J	TANCST ANDRG CO. 101. 189	7000°0	FL# 083.	TANCST ANDMG C	FLW 08J 0.000	7. V 08.	TANCST ANDMG 0 605.017 401.700		FL# 085	000°0	TANCST ANDMG O	7000° 31'*	FLW 08J	TANCST ANDHG O	000°0	FLW DB.		FL* 08J	760°0
TRG FLOW 0,000	7RG FLOW 0,000	08J DEV 0.000	TRG FLOW	TRG FLOW 0,000	083 DEV	TRG FLUW 0,000	TRG FLUW 0.000	083 DEV		TRG FLOW 0,000	TRG FLOW 0.000	06J DEV	TRG FLUW 0,000	TRG FLOW	08J DEV	TRG FLOW 0,000	TRG FLOW	08J DEV 0,000	TRG FLOW 0,000	TRG FLOW 0.000
1NT FLUM 2576,749	INT FLOW 7578.270	.198E+03 .779E+04	INT FLOW 2599,856	INT FLOW 7609,217	.196E+03 .779E+04	INT FLOW 2621,135	INT FLOW 7640.290	*194E+03 .779E+04	.1007E+04	INT FLOW 2566,451	1NT PLOW 7560.181	VAR(M) VAR(M1)	INT FLOW 2575.053	INT FLOW 7572.839	.750E+03 .199E+03	INT FLOW 2577.640	INT FLOW 7576.641	.750E+03 .198E+03	INT FLOW 2570,749	INT FLOW 7578.270
181A 1030	18TA 2030	- Σ Σ N	187A 1030	187A 2030	# - E ∩	181A 1030	181A 2030	Ξ- Σ·N	₹	187A 1030	ISTA 2030	- N W L	187A 1030	187A 2030	M M M	18TA 1030	181A 2030	 E E	157A	187A 2030
		<u>v</u> -			2~			S.w.	- 1007E+0			UZ-			2 - 2			9 -		
		7785,49							.1007E+04											
		5190,33 10							OR VARTABLE 2											
		1 ADJ FROM							OBJECTIVE FUNCTION FOR VARIABLE											
		VAR							OBJEC											4 * \$ * * 4 * \$ * *

		NC I I	TSOE+03 .198E+03	087 DEV	604.746 401.783	STNCNC)
		18TA 1030	INT FLOW 2578.749	7RG FLUW 0.000	000° 0 000°	FLW DEV
		181A 2030	INT FLOW 7585-949	TRG FLUW	760°0	FLW DEV
			.743E+03 .198E+03	090 0EV	FOR STATE SON STATE	-101E+04
		18TA 1030	1NT FLOX 2578,749	TRG FLOW	FLW 085	FLH DEV
		157A 2030	INT FLOW 7593.627	TRG FLUW 0.000	FL* 08.0	FLW DEV
		NC M M1	VAR(M) VAR(M1) .735E+03 .198E+03	08J DEV 0.000	TANCST ANDMG 603,703 402,920	-101E+04
OBJECTIVE FUNCTION FOR VARIABLE 7 .100	.1007E+04 .2007E+0	E+04	.1007E+04			
		181A 1030	1NT FLOW 2578,749	TRG FLOW 0.000	000°0	FLW DEV
		ISTA 2030	1NT FLOW 7531,575	TRG FLUW 0,000	FLW 086.	FLW DEV
7 AbJ FRGM 750.00 TG	70.5° 6 8	NC M M1	VAR(M) VAR(M1) .150E+04 .796E+03	08J DEV 0.000	TANCST ANDHG 607.922 398.339	FTNCNC)
		181A 1030	INT FLOW 2578,749	TRG FLOW	700 800 81 8	FLW DEV
		1STA 2030	INT FLOW 7531.575	186 FLOW	000°0	FLW DEV
		E O	VAR(M1) VAR(M1)	083 DEV	TANCST ANDMG	O FINCHES
		1STA 1050	1NT FLOW 2576,749	TRG FLOM	FLW CB.	FL* 0EV
		181A 2030	INT FLOW 7531.575	TRG FLDW 0,000	000°0	FLW DEV
		N S O S O S	.147E+04 .796E+03	085 DEV 0.000	TANCST ANDMG 606,381 401,193	0 FTN(NC)
COLUMN FUNCTION OF CALCALANT SYSTEMS	10067004	40	-1008E+04			

PLW OOO	V. DEV	0 FIN(NC)	FLW DEV	FLW DEV	0 FIN(NC)	FLM DEV	FLW DEV	987E+03		FLW DEV	FLW DEV 0.000	FININGS	FLW DEV 0.000	FLW DEV	983E+03	FLW DEV	FLW DEV 0.000	. 983E+03	FLW DEV
780 ×14	760.00	TANCST ANDMG 650,586 336,824	FLW 08.1	000°0	TANCST ANDMG 648,803 338,191	FL# 03.	760°0.	TANCST ANDMG 647.015 339.542		FLW GBJ		TANCST ANDRG 589.190.406.938	FL* 08.	780 * 74	632,730 350,530	000°0	FL# 085	TANCST ANDMG 632.874 350.434	FL* 083
TRG FLUM 0.000	TRG FLOW	08J DEV 0.000	TRG FLOW 0,000	TRG FLOW 0.000	000.0	7RG FLOW 0.000	786 FLOW	08J DEV 0.000		TRG FLOW 0,000	TRG FLOW	08J DEV 0,000	TRG FLOW	TRG FLOW 0.000	OBJ DEV 0.000	TRG FLOW	TRG FLOW 0.000	083 054	TRG FLOW
INT FLOM 2578,749	INT FLOW 7531,575	VAR(M) VAR(M1) .779E+04 .225E+04	INT FLOW 2006,145	INT FLOW 7531,575	.771E+04 .225E+04	INT FLOW 2631,587	INT FLOW 7531,575	.763E+04 .255E+04	.9866E+03	INT FLOW 4641,267	INT FLOW 7531,575	.198E+03 .519E+04	INT FLOW 2846,968	INT FLOW 7531,575	VAR(M) VAR(M1)	INT FLOW 2874,189	INT FLOW 7562,481	.196E+03 .731E+04	INT FLOW
18TA 1030	151A 2030	TH TO	181 1030	ISTA 2030	T C C C C C C C C C C C C C C C C C C C	1 STA 1030	191A 2030	N N N N N N N N N N N N N N N N N N N	.9870E+03	181A 1030	ISTA 2030	Y N	1030	1818 2030	NC 3	1874 1030	18TA 2030	X X X X X	ISTA.
		2250,00							. 9874E+03						70.00				
		1500,00 TD							OBJECTIVE FUNCTION FOR VARIABLE 1						7785,49 10				
		9 ADJ FROM							VE FUNCTION						VAR 1 ADJ FROM				

고개화 병 회사가 하고 사용했다. 이 이 기의 경유화회사 하다 하면 전체하기를 된다. 그는 이 경우를 받아 하는 그 소문화 경우 그 아니다. 한 사용을 하다 다	
1935E+03 1940	E N UN
1874	9833£+0
1874	
1814 1914	7.2
1574	
1574 INT FLOW 0,000 652,726 350,553 150,000 0,000 652,726 350,553 150,000 1030 652,726 350,553 1530,000 0,000 652,726 350,553 1530 2030 7531,332 0,000 652,726 350,553 1530 7531,332 0,000 652,729 350,537 1530 7531,332 0,000 652,729 350,537 1530 7531,557 0,000 652,729 350,537 1530 7531,557 0,000 652,730 350,537 1530 7531,557 0,000 652,730 350,530 1530 7531,557 0,000 652,730 350,530 1530 7531,557 0,000 652,730 350,530 1530 7531,557 0,000 652,730 350,530 1530 7531,557 0,000 652,730 7531,557 0,000 652,730 7531,557 0,000 652,730 7531,059 1531 786,649 768 76,000 652,776 351,059 1531 786,649 768 76,000 652,776 351,059 1531 786,649 768 76,000 652,776 351,059 1531 786,649 768 76,000 652,776 351,059 1531 786,649 768 76,000 652,776 76,000	
NC	Äž
1874 INT FLOW TRG FLOW FLW OBJ 2030 2846.754 0.000 0.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST ANDMG O.000 NC M M1 VAR(M) VAR(M1) 08J DEV TANCST SS1.059 1STA INT FLOW TRG FLOW FLW OBJ 2030 75346.966 0.000 632.176 351.059 1STA INT FLOW TRG FLOW FLW OBJ 2030 7547.776 351.623 351.625	
187A	
M 1	
15TA INT FLOW TRG FLOW FLW OBJ 2030 2846,968 TRG FLOW 0,000 1STA INT FLOW TRG FLOW FLW OBJ 2030 7531,575 350,530 1STA 1NT FLOW TRG FLOW FLW OBJ 1030 2846,968 0,000 0,000 1STA INT FLOW TRG FLOW FLW OBJ 2030 7539,649 0,000 632,776 351,059 1STA INT FLOW TRG FLOW FLW OBJ 2030 7539,649 0,000 632,776 351,059 1STA INT FLOW TRG FLOW FLW OBJ 2030 7547,796 0,000 0,000 1STA 7547,796 TANCST ANDMG 7 2 ,780E+03 ,198E+03 0,000 631,623 351,596	
1STA INT FLOW TRG FLOW 0,000 M M1 VAR(M) VAR(M1) 0BJ DEV TANCST ANDHG C 1STA 2796E+03 .198E+03 0,000 632,730 350,830 1STA 2846,968 TRG FLOW FLW OBJ 2030 7539,649 0,000 632,176 351,059 1STA 1NT FLOW TRG FLOW FLW OBJ 2030 7547,796 0,000 632,176 351,059	
M MI	
1814 INT FLOW TRG FLOW FLW OBJ 1834 INT FLOW TRG FLOW FLW OBJ 2836 T539.649 6.000 0.000 0.000 M M1 VAR(M) VAR(M1) OBJ DEV TANCRT S51.059 1814 INT FLOW TRG FLOW FLW OBJ 18314 INT FLOW TRG FLOW FLW OBJ 2836 7547.796 0.000 0.000 M M1 VAR(M) VAR(M1) OBJ DEV TANCRT ANDMG C 7 2 .780E.03 .198E.03 0.000 631.623 351.596	E ~
191A INT FLOW TRG FLOW FLW O0000 2030 7539.649 0.000 0.000 0.000 M M1 VAR(M) VAR(M1) OBJ DEV TANCST ANDMG C 1STA INT FLOW TRG FLOW FLW OBJ 1030 2846.966 0.000 0.000 ISTA INT FLOW TRG FLOW FLW OBJ 2030 7547.796 0.000 0.000 M M1 VAR(M) V/R(M1) OBJ DEV TANCST ANDMG C 7 2 .780E+03 .198E+03 0.000 631.623 351.596	
M MI VAR(M) VAR(MI) OBJ DEV TANCST ANDMG C 7 2 .788E+03 .198E+03 0.000 632,176 351,059 ISTA INT FLOW TRG FLOW FLW OBJ 2.050 ISTA INT FLOW TRG FLOW FLW OBJ 2.050 7547,796 0.000 0.000 631,623 351,596 7 2 .780E+03 .198E+03 0.000 631,623 351,596	
1314 INT FLOW TRG FLOW FLW UBJ 1030 2846,968 0.000 1514 INT FLOW TRG FLOW FLW GBJ 2030 7547,796 0.000 0.000 H M1 VAR(M) V/R(M1) GBJ DEV TANCST ANDMG 7 2 .780E+03 .198E+03 0.000 631,623 351,596	
1514 INT FLOW TRG FLOW FLW UBJ 2030 7547,796 0.000 0.000 M MI VAR(M) V/R(MI) UBJ DEV TANCST ANDMG C 7 2 ,740E+03 198E+03 0.000 631,623 351,596	
H MI VAR(M) V/R(MI) OBJ DEV TANCST ANDMG (7 2 ,760E+03 ,198E+03 0,000 631,623 351,596	4 N
	Σr

INT FLOW TRG FLOW 7558.355 0.000 VAR(M) VAR(M1) OBJ DEV .2255+04 .7695+03 0.000	181A 2030 M M1
**************************************	181A 1030
FLOW 9,355	151A 2030
VAR(M) VAR(M1) UBJ DEV .223E+04 .769E+03 0.000	<u> </u>
INT FLOW TRG FLOW 2846,968	191A 1030
INT FLOW TRG FLOW 7558,355	181A 2030
.221E+04 .769E+03 0000	Ξ^
•9833E+03	
INT FLOW TRG FLOW 2846,968	81A 030
INT FLOW TRG FLOW 7558,355	187A 2030
.701E+04 .338E+04 0.000	Ξ°
INT FLOW TRG FLOW 2846,968	1030
INT FLOW TRG FLOW 7558,355	181A 2030
.701E+04 .259E+04 0.000	 Σ
INT FLOW TRG FLOW 2846,968 0,000	STA 030
INT FLOW TRG FLOW 7558.355	1STA 2030
.701E+04 .235E+04 0.000	∓ o

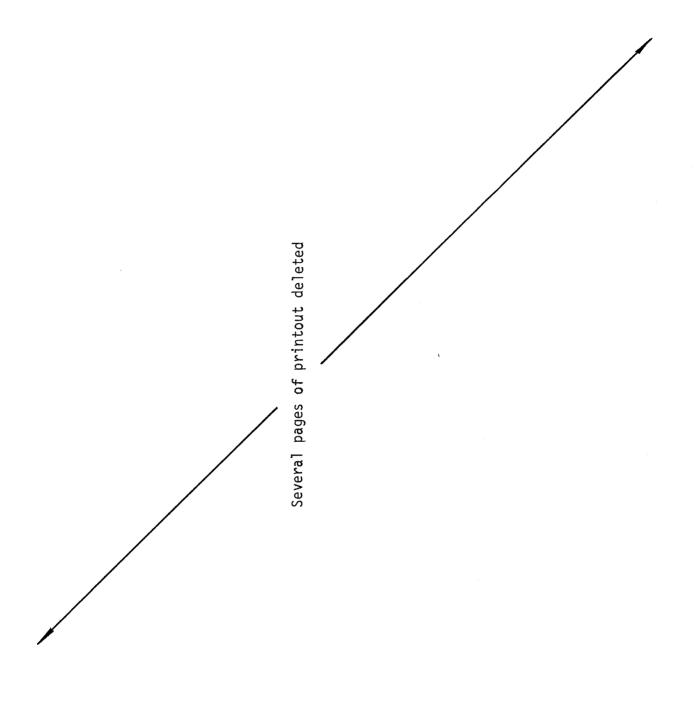
		181 1030	O 2871-174	TRG FLOW	FL# 08.	FLW DEV
		151A 2030	A INT FLOW 0 7558,355	TRG FLOW 0.000	,000,0 0,000	FLW DEV
		E -	M1 VARCM) VARCM13	08J DEV 0.000	TANCST ANDHG 636.174 346.555	່ດີ
		187A 1030	A T T T 0	TRG FLOW	780.0°0	FLW DEV
		187A 2030	0 INT FLOW 0 7558,355	TRG FLOW 0.000	000°0	FLW DEV
		Z	M1 VAR(M) VAR(M1) 9 .687E+04 .235E+04	083 DEV	1ANCST ANDMG 634.567 347.815	PARENCO 982E+03
OBJECTIVE FUNCTION FOR VARIABLE 1	.9831E+03	.9827E+03	.9624E+03			
		191A 1030	A INT FLOW 0 4836.753	TRG FLOW 0.000	780 M14	FLW DEV
		1 8 T X X X X X X X X X X X X X X X X X X	A INT FLOW 7558,355	TRG FLOW	000°0	FLW DEV
		EN ON	1 VAR(M) VAR(M1) 1 .198E+03 .503E+04	08J DEV 0.000	588.787 407.956	0 FTN(NC)
		ISTA 1030	A 1NT FLOW 0 3177,182	TRG FLOW	7000 0000 014	FLW DEV
		18TA 2030	A 1NT FLOW 0 7550,355	TRG FLOW 0.000	000°0 60°0	FLH DEV
VAR 1 ADJ FROM 7006.94 TO	6412,47	E NO	1 VAR(M) VAR(M1) 1 .198E+03 .641E+04	08J DEV	TANCOT ANDMG	0 FIN(NC)
		18TA 1030	A 1NT FLOW 0 3208,106	TRG FLUW 0,000	CBC .000.0	FLW DEV
		19TA 2030	A INT FLOW 0 7589,284	TRG FLOW	FL* 080	FLW DEV 0.000
		E N	1 .196E+03 .641E+04	08J DEV	1ANCST ANDMG 623,598 358,206	O FINCHC)
		181A 1030	ANN TELOS	TRG FLOW	.000°0	FLW DEK
		1STA 2030	A INT FLOW 7620.339	TRG FLUW	FL E CB.	FLW DEV
		EN	1 VAR(M) VAR(M1)	081 DEV	TANCST ANDMG 623.748 SS8.187	0 FTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE 2	.9817E+03	.9818E+03	.9619E+03			

FL* 060	> 000° 0	# TN(NC)	FLW DEV	FLW DEV	0 FTN(NC)	FLW DEV	FLW DEV	.982Ev03	FLW DEV	FLW DEV	PTN(NC)	FLW DEC	FLW DEV	. PENCHES	7. 0.00 0.00	FLW DEV	SOUTH OF THE POST	
FL* 08.0	700	423,393 358,432	000°0	FLW 083	FRICAT ANDRO C	FLW 083	FLM GBJ	1ANCST ANDHG C 623.445 358.320	**************************************	FLW CBJ.	TANCST ANDHG D 623,450 358,295	000°0	FL: 000,	TANCST ANDMG O 622.915 358.821	76 B 08.0	000.4 0.4 0.4	TANCST ANDMG O	
TRG FLOW	TRG FLOW 0.000	000.00	TRG FLOW 0.000	TRG FLOW	08.0 0 EV	TRG FLOM	TRG FLOW	084 DEV	186 FLOW	TRG FLOW 0.000	000,000	7RG FLDW 0,000	TRG FLOW 0.000	080 DEV	TRG FLDW 0.000	TRG FLUW 0.000	081 057	
INT FLOW 3165,333	INT FLOW 7546,458	.769E+03 .199E+03	INT FLOW 3173,623	INT FLOW 7554.784	.769E+03 .199E+03	INT FLOW 3176,114	INT FLOW 7557,284	.769E+03 .198E+03	1NT FLOW 3177,182	INT FLOW 7558,355	VAR(M) VAR(M1)	INT FLOW 3177.182	INT FLOW 7566,234	.762E+03 .198E+03	INT FLOW 3177,182	INT FLOW 7574,112	.754E+03 .'98E+03	.9817E+03
181A 1030	18TA 2030	Er U=	181A 1030	151A 2030	E P	187A 1030	181A 2030	Er	181A 1030	131A 2030	- N E K	187A 1030	157A 2030	IN	187A 1030	181A 2030	Z N E N E N	+03
		2			- N		.	2-			Š -			Ž			Ž	.9817E+03
																		.9817E+03
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				181A 1030	1NT FLOW 3177-182	TRG FLOW	FLE 000.	FLW DEV
				181A 2030	INT FLOW 7660.243	TRG FLOW	FLW 083	FLW DEV 0.000
VAR 7 ADJ FROM	769,45 70	669.92	X-,	ī.	VAR(M) VAR(MI) .235E+04 .670E+03	08J DEV	14NC87 ANDMG	0 FTW(NC) 961E+03
				ISTA 1030	INT FLOW 3177,182	TRG FLOW	PLW 08J	FL# DEV
			- N	1STA 2030	INT FLOW 7660.243	TRG FLOW 0.000	780°0 #14	FLE 0.000
			¥ O U N Z	I D	VAR(M) VAR(M1)	083 DEV 0.000	TANCST ANDMG	981E+03
				181A 1030	INT FLOW 3177:182	TRG FLO#	000°0	> 000°0
				187A 2030	INT FLOA 7660.243	TRG FLOW 0.000	7000	FLH DEV
			Z O	Ξ ^	VAR(M) VAR(M))	083 DEV	TANCST ANDMG	0 FTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE	OR VARIABLE 9	.9812E+03	.9813E+03		.9613E+03			
				187A 1030	INT FLOW 31777,182	TRG FLOM 0.000	000°0	FLW DEV
				191A 2030	INT FLOW 7660,243	TRG FLOW	FLW 083	FLW DEV
			N-	 E E	.641E+04 .353E+04	083 DEV 0,000	TANCST ANDES	0 FTN (NC)
				187A 1030	INT FLOW 3177-182	TRG FLOW	7000	PLE 0000
			→ ~	151A 2030	INT FLDW 7660,243	TRG FLOW 0.000	FLW 08J	FLW DEV
			¥ →	ʰ.	.641E+04 .270E+04	083 DEV 0,000	ALO.481 341.930	0 FIN(NC)
				131A 1030	INT FLOW 3177,182	TRG FLOW	000°0	FLW DEV
			-	51A	INT FLOW 7660,243	TRG FLDW	000°0	FLW DEV
VAR 9 ADJ FROM	2351,25 TO	2457.06	N C	 X E =	VAR(M) VAR(M1)	060.000	TANCST ANDHG (623,719 357,326	O FINING)

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		18TA 2030	INT FLOM 7660.243	TRG FLOW	FLM 084	FLW DEV
	0 -	Ξ' Ξ-	.641E+04 .641E+04	08J DEV 0.000	623.719 357.326	0 FTN(NC)
		181	INT FLOW S249,430	7RG FLUW 0.000	000°0	FLW DEV
		181A 2030	INT FLOW 7660,243	TRG FLOW 0.000	FLW 08J	FL# DEV
	UN Z	Σ Σ	.635E+04 .635E+04	083 DEV	14NCST ANDHG 622.184 359.276	0 FTN(NC)
		1STA 1030	INT FLOW 3323,478	TRG FLOW	000°0	FLW DEV
		181A 2030	INT FLOW 7660,243	TRG FLOW 0.000	0000°0	FLW DEV
	Z A	Ξ-	.628E+04 .628E+04	08J DEV	TANCST ANDMG 620,651 361,229	PTN(NC)
OBJECTIVE FUNCTION FOR VARIABLE 1	9810E+03 .981SE+03	2	.9819E+03			
		18TA 1030	INT FLOW 1822.015	TRG FLOW	7.80 BJ	FLW DEV
		181A 2030	INT FLOW 7660.243	TRG FLUM 0,000	780°0 814	FL 0.000
	O	E N	VAR(M) VAR(M1)	083 DEV	TANCST ANDMG 693,019 299,569	0 FTN(NC)
	•	187A 1030	1NT FLOW 2719,713	TRG FLDW 0.000	FLW 08.	FLW DEV
		18TA 2030	INT FLOW 7660.243	TRG FLUM 0.000	700 800 *0	FLW DEV
	0. -	E E EN	.198E+03 .737E+04	08J DEV	TANCST ANDMG	0 FTN(NC)
		18TA 1030	INT FLOW 2946.830	TRG FLUW 0.000	FLW 0BJ	FLW DEV.
		187A 2030	INT FLOW 7660.243	TRG FLOW	000°0	FLW DEV
ADJ FROM 6412 47 TO	NC 1	Ξ N	.198E+03 .670E+04	08J DEV	TANCST ANDMG 630,790 350,087	FTN(NC)

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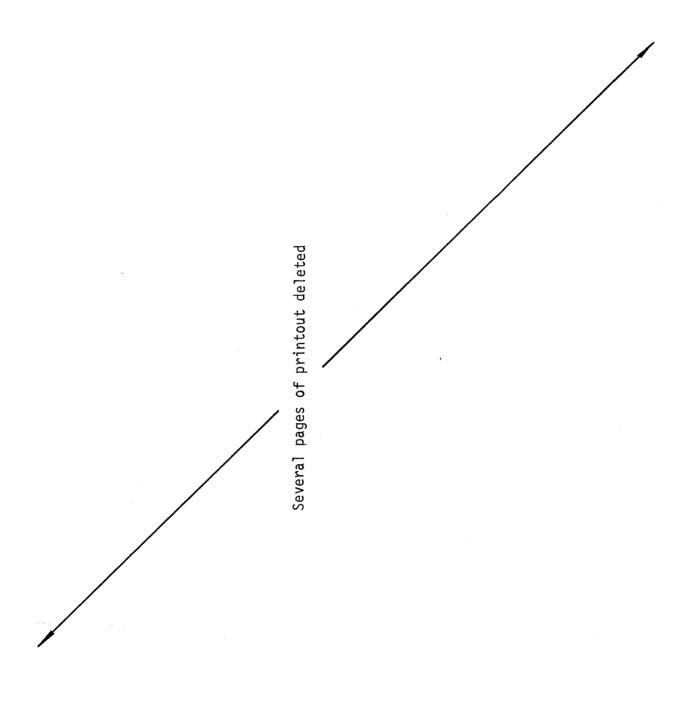


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MAXIMUM STUNAGE # 11437.

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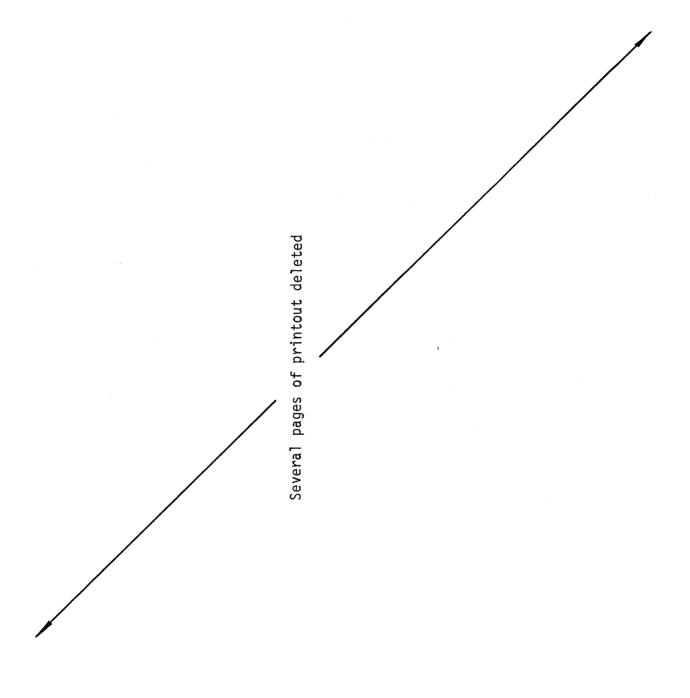


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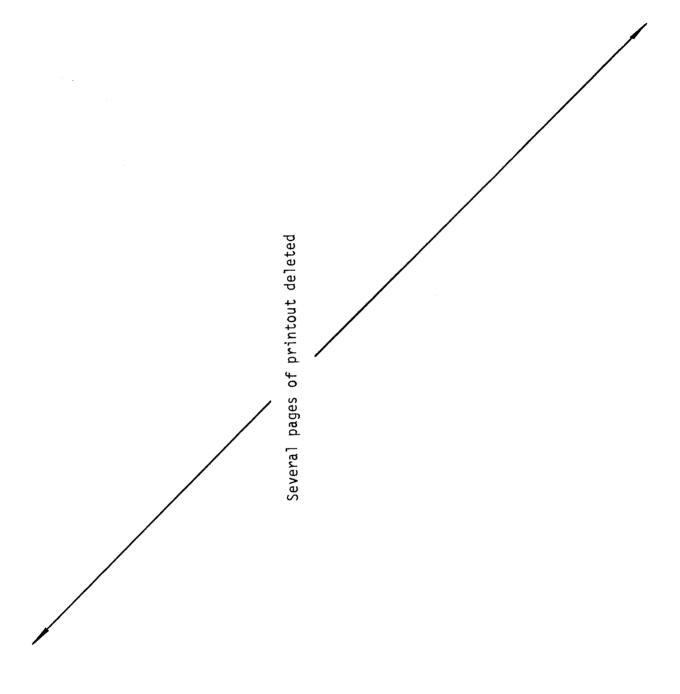
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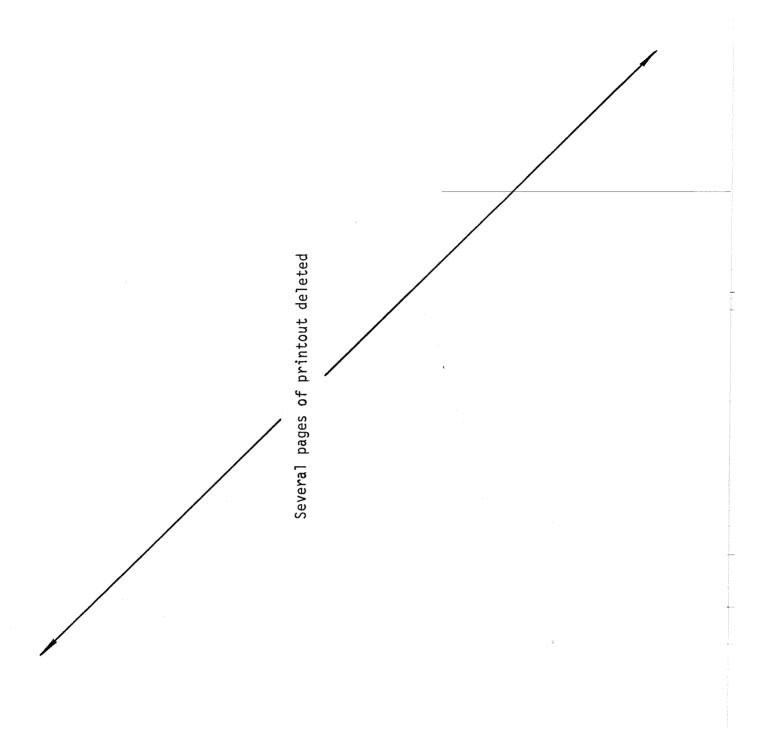


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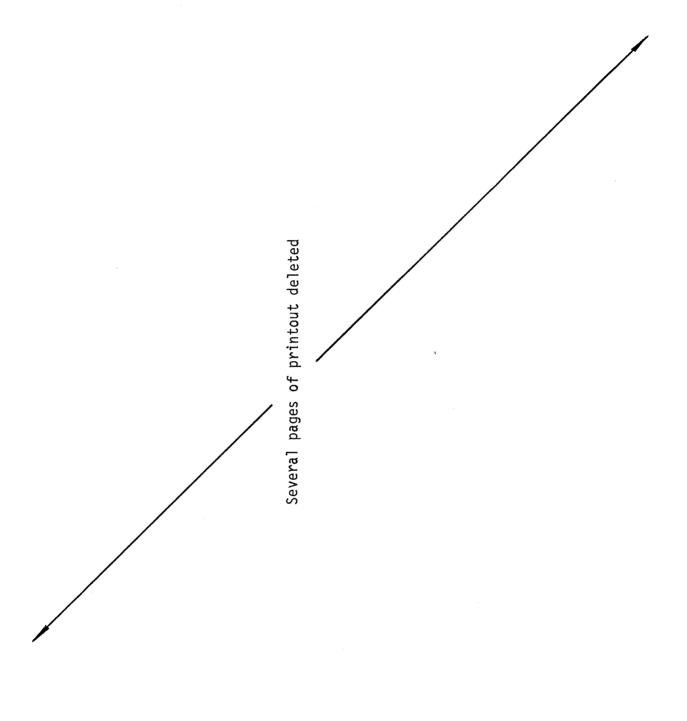


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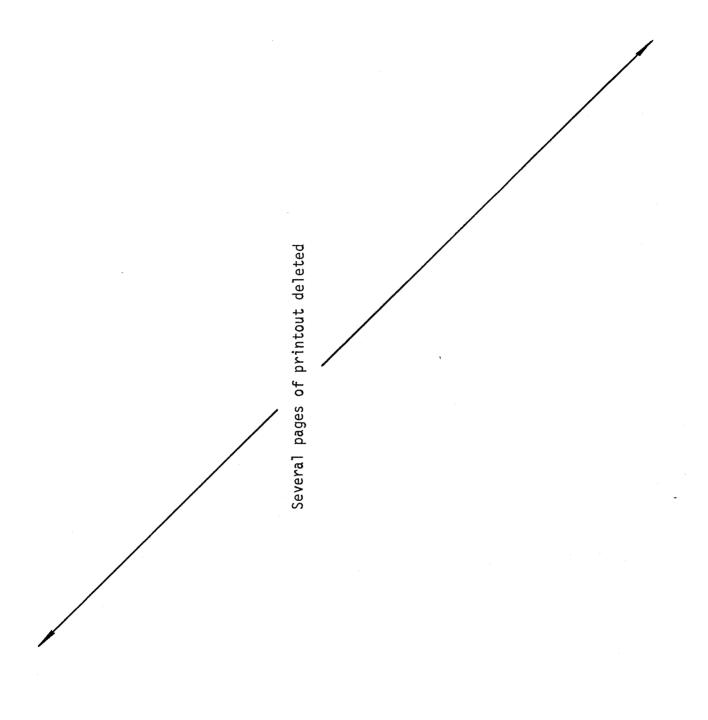


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ROUTED TO	<u>.</u>	35.10 90.915	- `~`	1343, 38,021(588, 16,651(1611. 45,62)(566. 18,85)(2685. 76.03)(910. 25.75)(3759. 106.44) 1084. 30.70)(5370. 152.06)(1324. 37.48)(8055, 228,09)(1656, 46,89)(11814 334,54)(6328, 179,20)(17453 494.2016 12033 340.7316	23628. 669.073 18039. 510.803
ROUTED TO	1030	35.10	_ ~	26.65)(525. 14.87)(1139. 32,24)(594.	1940. 54.94)(839. 23.76)(2921. 82.713(1005. 28.46)(4312. 122.10) 1252. 35.47)	189.70)(1574. 44.58)(10191. 288.58)(4949. 140.13)(15177 429.771 10079 285,41)(20603. 583.42) 15369. 435.19)
HYDROGRAPH 47	c N	35.10 90.91)	_ ~	1343, 38,02)(1343, 38,02)(45,62)(45,62)(76.03)(76.03)(76.03)(3759. 106.44)(3759.	5370. 152.06)(5370. 152.06)(8055. 228.09)(8055.	11814, 334,54)(11814, 334,54)(17453. 494.20)(17453. 494.20)(23628. 669.073 23628. 669.073
ROUTED TO	â	35.10	- "	1343. 38.02)(1346. 38.12)(1611. 45.62)(1549. 43.86)(76.033 57.293	3759. 106,44)(3096. 87,68)(5370. 152.06) C 4717. 133.56) C	8055. 228.0910. 7408.	11614. 334.54)(11178. 316.53)(17453 494.20)C 16833 476.65)C	23628. 669.07) 23026.
RUUTED TO	2030 C	35.10 90.91)	- ~	941. 26,65)(940. 26,61)(32.24) 1115. 31.56)	1940. 54.94)(1500. 42.46)(2921. 82.711(2280. 64.57)(122.10) 122.10) 3691. 104.51)	189.70)(5939. 168.16)(10191 288.583) 9455 267.743	15177 429.773 14455 409.313	20603. 583.423 19892. 563.283
HYDROGRAPH	S	10.00 25.90)	- "	12,81)(12,81)(12,81)(15,38)(15,38)(15,38)(25.63)(25.63)(25.63)(1267. 35.88)(1267. 35.88)(1810. 51.25)(1810. 51.25)(2715 76.88)(2715 76.88)(3982 112.761 3982 112.76)(5883 166.57) 5883 166.37)	7964. 225.52) 225.52)
3 COMBINED	Š	207.723	- "	2219. 62.84)(1660.	2676. 75.79)(1939. 54.90)(4563, 129,21)(2712, 76,81)(6859. 194,23)(3947. 111,75)(10154, 287,53)(5974, 169,15)(15693. 444.39)(9178. 259.89)	23748, 672,47)(14377, 407,11)(35345 1000.86)(25809.	480111 1359.533 38550.
AGUTED TO	305	207.723		1200. 33.98)(1200. 33.98)(1200. 33.98)(1200. 33.98)(1200 33,98)(1200 33,98)(1200. 33,98)(1200. 33,98)(1200. 33,98)(1200. 33,98)(33,98)(33,98)(33,98)(1200. 33.98)(1200. 33.98)(33.98)(33.98)(33.98)	12003 134,983 12003
				PEAK STURA 1036. 1278.)(749.)(CES IN ACR 1486. 1833.)(1882. 1088.)(E FEET (10 3587, 4424,)(1954,	00 CUBIC ME 5904. 7283.)(1630. 2011,)(7ERS)*** 11788.)(2654.	15876, 19583,)(5563, 6911,)(30760.) 13184. 16263.)	4786999 877369 817069	58876 66455 39996 49334

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2457.												NTBNFT 112.
8 · 0					631.			N N	1961	# ***		18NF 18 57.7
DIV 7 670.	SYSTEM COST AND PERFORMANCE SUMMARY Same as input . Normally 1000's of Dollars)	7408.	373.	257.		.117.	350			***** OPTIMIZATION OBJECTIVE - MAXIMIZE SYSTEM NET BENEFITS \$***		ANDMG 601.
RESULTS VAR 6 0.	MANCE SUMPLY 100018		*	•	•			4		S E MILON		ANDG88
SYSTEM OPTIMIZATION RESULTS AR 4 VAR 5 VAR 6 0.00	AND PERFOR	*	# #	CEMENT COS	*	*	*			MAXIMIZE		14NCST 465.
SYSTEM OP	STEM COST ME AS INPU	* * *	L COST * *	AND REPLA	** ** **	STING COND	THIZED SYS	ION (BENEF)	BEZEF1138)BJECTIVE		ANDMPR
VAR 3	SY (UN115 SA	L CUST *	ZED CAPITA	D,M,POWER	t * lsoo	GES EX1	GES OP1	GE REDUCTI		NO 1 T A T I ON		ANFCST 254.
× × × × × × × × × × × × × × × × × × ×		SYSTEM CAPITAL COST * * * * *	SYSTEM AMORTIZED CAPITAL COST	SYSTEM ANNUAL D.M. POWER AND REPLACEMENT COST	SYSTEM ANNUAL COST * *	AVERAGE ANNUAL DAMAGES EXISTING CONDITIONS	ANNUAL DAMAGES OPTIMIZED SYSTEM	AVERAGE ANNUAL DAMAGE REDUCTION (BENEFITS)	AVERAGE ANNUAL SYSTEM NET	1 0 * * * * * * * * * * * * * * * * * * *		1FCST 5034
VAR 1 6701.		TOTAL SYS	TOTAL SYS	TOTAL SYS	TOTAL SYS	AVERAGE	AVERAGE	AVERAGE	AVERAGE			