# Technical Memo Project 0-6132: Task 6 - Test Sections in the Districts 

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| From: | Lubinda F. Walubita |
| Date: | February 10 ${ }^{\text {th }}$, 2011 |
| Subject: | Lab Test, Distress (Crack) Survey, and Construction Reports for the TTI Sections on FM 158 (Brazos County, Bryan District, TX) |



## Summary

This Tech Memo provides a summary of the Lab Test, Distress Survey, and Construction Reports for the CAM Test Sections constructed on FM 158 (E William J. Bryan Pkwy) in the Bryan District. TTI was requested by both the Contractor (Knife River Corporation) and the Bryan District to assist with the mix design. The contactor was initially having problems getting his proposed mix design to pass the Hamburg (HWTT) and Overlay tester (OT) requirements for a CAM design. This was a concern as they had successfully designed and constructed an earlier project with an identical mix design. The Bryan District Lab Engineer asked for an evaluation of the proposed mix to assess if a lower asphalt-binder content would meet the CAM requirements and potentially save the District money.

Based on extensive lab testing by TTI, recording of the construction process, and field tests conducted just after construction, the following conclusions and recommendations were made:
a) The cause of the contractors' problem was that the initial asphalt-binder proposed (Martin PG 76-22) actually graded out as a PG 82-22. While having good performance in the HWTT, the mix made with this asphalt-binder could not pass the OT requirements (<200 cycles).
b) Two alternative PG 76-22 asphalt-binders were evaluated, Valero and Jebro, both of which had no problems passing the HWTT and OT requirements.
c) The contractor elected to use the Jebro PG 76-22 asphalt-binder and the Bryan District's Special Specification Item 3131 with the volumetric design requirement ( $98 \%$ density after 50 gyrations); the optimum asphalt-binder content was found to be $7.1 \%$. At this asphaltbinder content, the HWTT rut depth was 5.4 mm after 20,000 passes and 1000 OT cycles.
d) TTI performed performance tests at a lower target density of $96.5 \%$ on both asphalt-binders (Valero and Jebro) and found that all criteria were met while using approximately $0.5 \%$ less asphalt-binder; i.e., Hamburg < 5.0 mm rutting after 20000 passes and OT > 750 cycles for $6.5 \%$ PG 76-22 Jebro and $6.6 \%$ PG 76-22 Valero, respectively.
e) The District elected to place the mix with a target asphalt-binder content of $6.7 \%$ (Jebro), which is allowable under the CAM spec, where the asphalt-binder is paid for as a separate bid item. The $6.7 \%$ PG 76-22 Jebro asphalt-binder corresponded to $97 \%$ lab density; with Hamburg $=4.3 \mathrm{~mm}$ rutting after 20000 load passes and $\mathrm{OT}=1000$ cycles.
f) The modified CAM mix-design (6.7\% PG 76-22 Jebro) was accordingly placed on the entire project length of about 1.6 miles long as a 1 inch thick overlay (over an about 12 inch thick existing HMA) by Knife River Corporation late 2010 from Dec $10^{\text {th }}$ to $31^{\text {st }}$.
g) Lab test were conducted on plant mixed materials delivered to the project. The measured asphalt-binder content was close to the design value ( $6.55 \%$ versus $6.7 \%$ ) and the measured HWTT and OT also did not differ significantly from the design values.
h) Some construction problems were encountered in the field with equipment malfunctioning, specifically the Roadtec MTD, which had to be changed including switching from using belly-dump to tipper trucks.
i) The ride values on the completed project were a cause for concern. However, it should be noted that this is an urban section with construction occurring under high traffic. The section also has many drainage structures and multiple stop and go intersections.

Prior to construction, TTI researchers had conducted a crack survey and marked out 6 test sections; 3 in the EB direction and 3 in the WB direction. Plans are to periodically monitor the test sections at least twice per year during the cold (crack evaluation) and hot (rutting evaluation) weather seasons, respectively including : (1) visual crack surveys, (2) rut measurements (straightedge), (3) surface profiles (ride quality), (4) GPR, (5) skid measurements (with TxDOT aid), (6) FWD (with TxDOT aid), and (7) coring (where applicable).

## Lessons Learned

1) Not all PG 76-22 asphalt-binders are manufactured equal; it is apparent that material source has an influence. TxDOT currently does not test the upper end, therefore an asphalt-binder can be a PG 82 but still be accepted as a PG 76 .
2) In addition to the $98 \%$ target density, performance tests on future CAM designs should also be run at asphalt-binder contents found at lower densities such as 96.5 or $97 \%$.
3) The Bryan District policy of recommending a PG 76-22 with $1 \%$ lime for CAM designs to be placed as surface layers in high traffic locations appears to be working well; considerations should be made to incorporating these requirements into the Statewide specification Item 365.

## Acknowledgements

Special thanks go to Stephen Kasberg (TxDOT), Darlene Goehl (TxDOT), and Knife River Corporation for permitting and assisting TTI Researchers conduct the survey, record/document the construction process, run field tests, and collect materials including asphalt-binders, aggregates, plant-mixes, and cores for lab testing.

## CAM MIX-DESIGN, SPEC ITEM 3131

Aggregate type:
Aggregate-blend:

Capitol limestone
$21 \%$ Gr5 (Delta pit) + 18\% D-rock (Marble Falls pit)
60\% screenings (Marble Falls pit)
None
1.0\% hydrated lime (Austin White Lime)

Jebro PG 76-22, Valero PG 76-22, and Martin PG 76-22


Fig I-1. Aggregate Gradation.
Table I-1. Asphalt-Binder DSR and BBR Results.

| \# | Source | Actual <br> Tested PG <br> Grade | DSR (High Temp) |  | BBR (Lower Temp) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} \mathbf{G}^{*} \\ (\mathbf{k P a}) \end{gathered}$ | $\begin{gathered} \mathbf{G}^{*} / \operatorname{Sin} \delta(\mathrm{kPa}) \\ (>1.00) \end{gathered}$ | $\underset{(<\mathbf{3 0 0})}{\mathrm{S} \text { (MPa) }}$ | $\begin{aligned} & \hline \text { m-value } \\ & (>0.300) \end{aligned}$ |
| 1 | Jebro PG 76-22 | PG 76-22 | 1.41 | 1.54 | 174 | 0.325 |
| 2 | Valero PG 76-22 | PG 76-22 | 1.55 | 1.61 | 132 | 0.316 |
| 3 | Martin PG 76-22 | PG 82-22 | 1.03 | 1.05 | 77 | 0.317 |

Table I-2. Hamburg and Overlay Results - Jebro PG 76-22.

| $\#$ | Asphalt-Binder <br> Content | Corresponding <br> Lab Density | VMA <br> $(>17)$ | Hamburg <br> @ 20 k <br> $(<\mathbf{1 2 . 5})$ | Overlay <br> Cycles (Avg.) <br> (> 750) | Average OT <br> Peak Loads <br> (lb) |
| :--- | :---: | :---: | :---: | :---: | ---: | ---: |
| 1 | $6.5 \%$ | $96.5 \%$ | 18.7 | 3.2 mm | 600 |  |
| 2 | $6.7 \%$ | $97.0 \%$ | $\mathbf{1 8 . 7}$ | $\mathbf{4 . 3} \mathbf{m m}$ | $\mathbf{1 0 0 0}$ | $\mathbf{7 7 4}$ |
| 3 | $6.9 \%$ | $97.5 \%$ | 18.7 | 5.0 mm | 938 | 640 |
| 4 | $7.1 \%$ | $98.0 \%$ | 18.7 | 5.4 mm | 1000 | 612 |

Table I-3. Hamburg and Overlay Results - Valero PG 76-22.

| $\#$ | Asphalt- <br> Binder <br> Content | Corresponding <br> Lab Density | VMA <br> $(>17)$ | Hamburg <br> $@$ 20 k <br> $(<\mathbf{1 2 . 5})$ | Overlay <br> Cycles (Avg.) <br> $(>750)$ | Average OT <br> Peak Loads <br> (lb) |
| :--- | :---: | :---: | :---: | :---: | ---: | ---: |
| 1 | $6.5 \%$ | $96.5 \%$ | 19.0 | 4.5 mm | 736 | 580 |
| 2 | $6.7 \%$ | $97.5 \%$ | 18.1 | 4.9 mm | 951 | 630 |
| 3 | $6.9 \%$ | $98.0 \%$ | 18.1 | 5.7 mm | 956 | 553 |
| 4 | $7.1 \%$ | $98.4 \%$ | 18.4 | 7.4 mm | 1000 | 563 |

Table I-4. Hamburg and Overlay Results - Martin PG 76-22.

| $\#$ | Asphalt-Binder <br> Content | Corresponding <br> Lab Density | VMA <br> $(>\mathbf{1 7})$ | Hamburg <br> @ 20 k <br> $(<\mathbf{1 2 . 5})$ | Overlay <br> Cycles (Avg.) <br> $(>750)$ | Average OT <br> Peak Loads <br> (lb) |
| :--- | :---: | :---: | :---: | :---: | ---: | ---: |
| 1 | $6.5 \%$ | $96.7 \%$ | 18.4 | 2.9 mm | 132 | 815 |
| 2 | $6.7 \%$ | $98.5 \%$ | 17.2 | 3.6 mm | 169 | 770 |
| 3 | $6.9 \%$ | $98.9 \%$ | 17.4 | 4.1 mm | 173 | 696 |
| 4 | $7.1 \%$ | $99.0 \%$ | 17.6 | 4.4 mm | 173 | 835 |

NB: All Hamburg and OT samples were molded and tested at $7 \pm 1 \% \mathrm{AV}$.


Fig I-2. Hamburg and OT Results for Jebro PG 76-22.


Fig I-3. Hamburg and OT Results for Valero PG 76-22.


Fig I-4. Hamburg and OT Results for Martin PG 76-22.


Fig I-5. OT Pictures.

NB: All Hamburg and OT samples were molded and tested at $7 \pm 1 \%$ AV.

Table I-5. Mix-design Sheet - Combined Gradation

| SAMPLED BY: | TI |  | SPEC ITEM: 3131 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SAMPLE LOCATION: | TI |  | SPECIAL PROVISION: |  |  |  |
| MATERIAL CODE: | TI |  | MIX TYPE: CAM |  |  |  |
| MATERIAL NAME: | CRACK ATTENUATING MIXTURE |  |  |  |  |  |
| PRODUCER: | KNIFE RIVER - BRYAN PLANT(TTI) |  |  |  |  |  |
| AREA ENGINEER: |  |  | PROJECT MANAGER: |  |  |  |
| COURSEILIFT: |  | STATION: |  | T. FROM CL: | CONTRACTOR DESIGN \# : | KRC 205 |


$\square$ Table I-6. Mix-design Sheet - Summary (Jebro PG 76-22)

| Target Density, \%: | 98.0 |
| ---: | :---: |
| Number of Gyrations: | 50 |




| Effective Specific Gravity: | 2.774 |
| :---: | :---: |
| Optimum Asphalt Content : | 7.1 |
| VMA @ Optimum AC: | 18.6 |

Estimated Percent of Stripping, \%:

| Interpolated Values |  |
| ---: | :---: |
| Specific Gravity (Ga): | 2.429 |
| Max. Specific Gravity (Gr): | 2.482 |
| Theo. Max. Specific Gravity (Gt): | 2.479 |

Remarks: $\square$

Table I-6. Mix-design Sheet - Summary (Valero PG 76-22)

| Target Density, \%: | 98.0 |
| ---: | :---: |
| Number of Gyrations: | 50 | | -arn cone |
| :--- | :--- |


|  |  |  |  |  |  |  | Mixture Evaluation @ Optimum Asphalt Content |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TEST SPECIMENS |  |  |  |  |  |  | Indirect Tensile <br> Strength (psi) | Hamburg Wheel Tracking Test |  | Overlay Tester Min. Number of Cycles |
| Asphalt Content (\%) | Specific Gravity Of <br> Specimen (Ga) | Maximum Specific Gravity (Gr) | Effective Gravity (Ge) | Theo. Max. Specific Gravity (Gt) | Density from Gt (Percent) | VMA (Percent) |  | Number of cycles | Rut depth (mm) |  |
| 6.5 | 2.380 | 2.480 | 2.748 | 2.479 | 96.0 | 19.0 |  |  |  |  |
| 6.7 | 2.409 | 2.472 | 2.747 | 2.471 | 97.5 | 18.1 |  |  |  |  |
| 6.9 | 2.416 | 2.465 | 2.747 | 2.464 | 98.1 | 18.1 |  | Fig. 3 | Fig. 3 | Fig. 3 |
| 7.1 | 2.418 | 2.454 | 2.742 | 2.457 | 98.4 | 18.2 |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |


| Effective Specific Gravity: |  |
| ---: | :---: |
| 2.746 |  |
| Optimum Asphalt Content : | 6.9 |
| VMA @ Optimum AC: | $\mathbf{1 8 . 1}$ |

## Estimated Percent of Stripping, \%:

| Interpolated Values |  |
| ---: | :---: |
| Specific Gravity (Ga): | 2.415 |
| Max. Specific Gravity (Gr): | 2.466 |
| Theo. Max. Specific Gravity (Gt): | 2.465 |

Remarks:

Table I-6. Mix-design Sheet - Summary (Martin PG 76-22)


| Effective Specific Gravity: | 2.749 |  |  |
| ---: | :---: | :---: | :---: |
| Optimum Asphalt Content : |  |  | $\mathbf{6 . 6}$ |
| VMA @ Optimum AC: | $\mathbf{1 7 . 6}$ |  |  |
| Interpolated Values |  |  |  |
| Specific Gravity (Ga): | 2.427 |  |  |
| Max. Specific Gravity (Gr): | 2.480 |  |  |
| Theo. Max. Specific Gravity (Gt): | 2.476 |  |  |

$\qquad$

Remarks:

## APPENDIX II: DISTRESS SURVEY REPORT

## PROJECT DETAILS

Table II-1. Project and Location Details.

| Item | Details | GPS Coordinates |
| :--- | :--- | :--- |
| Hwy name | FM 158 (W. J. Bryan Pkwy) | - |
| Total project length | $\cong 1.6$ miles | - |
| Project limits | Praire Rd (just west of SH 6 bypass) to <br> Business SH 6 (Texas Avenue) | - |
| Project start location | SH 6 bypass (Bryan USPS) | $\mathrm{N} \mathrm{30}^{\circ} 40.307 ' ;$ W 096 20.603' |
| Project end location | Texas Avenue (Brazos County Health Dept.) | $\mathrm{N} 30^{\circ} 40.446^{\prime} ; \mathrm{W} \mathrm{096}{ }^{\circ} 22.134^{\prime}$ |

## CRACK (TRANSVERSE) MAPPING

## Test Section 01a (FM 158, EB Outside Lane)

Length
1042 ft
Start point: $\quad$ N $30^{\circ} 40.446$ '; W $096^{\circ} 22.1344^{\prime \prime}$
(Landmark: Brazos County Health Dept.; intersection of WJ Bryan Pkwy. \& N. Houston Ave.)
End point: $\quad \mathrm{N} 30^{\circ} 40.422^{\prime}$; W $096^{\circ} 21.950^{\prime}$
(Landmark: St. Joseph elementary school; intersection of WJ Bryan Pkwy \& Pierce Ave.)

Table II-2. Transverse Crack Mapping on Test Section 01a (FM 158, EB Outside Lane).

| Crack\# | Distance from Crack\#1 (ft) | GPS Location | Severity |
| :---: | :---: | :---: | :--- |
| 1 | 0 | $\mathrm{~N} \mathrm{30}{ }^{\circ} 40.446^{\prime} ; \mathrm{W} \mathrm{096}{ }^{\circ}$ 22. 134' | High |
| 2 | 147 | - | Medium |
| 3 | 166 | - | High |
| 4 | 188 | - | Medium |
| 5 | 260 | - | Medium |
| 6 | 331 | - | Medium |
| 7 | 407 | - | Low |
| 8 | 558 | - | Low |
| 9 | 743 | - | Low |
| 10 | 830 | - | Low |
| 11 | 900 | - | Low |
| 12 | 1042 | N $30^{\circ} 40.422^{\prime} ; \mathrm{W} 096^{\circ} 21.950^{\prime \prime}$ | High |

## Test Section 01b (FM 158, WB Inside Lane)

Length:
1075 ft
Start point: $\quad$ N $30^{\circ} 40.324$; W $096^{\circ}$ 20. $566^{\prime}$ (Landmark: Church of Nazarene; 2122 WJ Bryan Pkwy) End point: $\quad \mathrm{N} 30^{\circ} 40.298^{\prime}$; W $096^{\circ}$ 20. 763' (Landmark: 2100 WJ Bryan Pkwy/Vacant Building)

Table II-3. Transverse Crack Mapping on Test Section 01b (FM 158, WB Inside Lane).

| Crack\# | Distance from Crack\#1 (ft) | GPS Location | Severity |
| :--- | ---: | :--- | :--- |
| 1 | 0 | N $30^{\circ}$ 40. 307'; W 096 ${ }^{\circ}$ 20. 603' | Low |
| 2 | 23 | - | Medium |
| 3 | 104 | - | High |
| 4 | 200 | - | High |
| 5 | 241 | - | Medium |
| 6 | 304 | - | Medium |
| 7 | 368 | - | Medium |
| 8 | 404 | - | High |
| 9 | 486 | - | High |
| 10 | 549 | - | Low |
| 11 | 605 | - | Low |
| 12 | 635 | - | Low |
| 13 | 690 | - | Medium |
| 14 | 770 | - | Medium |
| 15 | 789 | - | High/Right on the |
|  |  |  | pedestrian crossing on |
| 16 | 828 | - | Nash St. |
| 17 | 858 |  | High |
| 18 | 881 | - | Medium |
| 19 | 922 | - | Medium |
| 20 | 970 | - | High |
| 21 | 1015 | - | High |
| 22 | 1031 | - | Medium |
| 23 | 1057 | - | Medium |
| 24 | 1064 | - | High |
| 25 | 1075 | $\mathrm{~N} 30^{\circ} 40.298^{\prime} ;$ W $096^{\circ} 20.736^{\prime}$ | High |

## Test Section 02a (FM 158, EB Inside \& Outside Lane)

Length
1021 ft
Start point: $\quad$ N $30^{\circ} 40.334$; W $096^{\circ} 21.580^{\prime}$ (Landmark: Sue Haswell Park parking lot)
End point: $\quad \mathrm{N} 30^{\circ} 40.328^{\prime}$; W $096^{\circ} 21.387^{\prime}$
(Landmark: Haswell pool parking lot; Crossing of WJ Bryan Pkwy \& Coulter Dr.)

Table II-4. Transverse Crack Mapping on Test Section 02a (FM 158, EB Lane).

| Inside Lane |  |  | Outside Lane |  |  |
| :---: | :---: | :--- | :---: | :---: | :--- |
| Crack \# | Distance from Crack <br> \#1 (ft) | Severity | Crack \# | Distance from Crack \#1 (ft) | Severity |
| 1 | 0 | High | 1 | 0 | High |
| 2 | 292 | High | 2 | 13 | Medium |
| 3 | 243 | Medium | 3 | 37 | High |
| 4 | 295 | High | 4 | 117 | High |
| 5 | 548 | High | 5 | 201 | Medium |
| 6 | 657 | Low | 6 | 292 | High |
| 7 | 715 | Medium | 7 | 295 | High |
| 8 | 74 | Low | 8 | 438 | Low |
| 9 | 455 | High | 9 | 548 | High |
| 10 | 821 | Low | 10 | 685 | High |
| 11 | 1021 | High | 11 | 715 | High |
|  |  |  | 12 | 741 | High |
|  |  |  | 13 | 755 | High |
|  |  |  | 14 | 878 | High |

## Test Section 02b (FM 158, WB Inside \& Outside Lane)

Length: $\quad 1058 \mathrm{ft}$
Start point: $\quad \mathrm{N} 30^{\circ} 40.413$; W $096^{\circ} 21.469^{\prime}$ (Landmark: Crossing of WJ Bryan Pkwy \& Taliaferro St.)
End point: $\quad$ N $30^{\circ} 40.410^{\prime}$; W $096^{\circ} 21.664^{\prime}$ (Landmark: Entrance to Sue Haswell Park; Road bifurcation)
Table II-5. Transverse Crack Mapping on Test Section 02b (FM 158, WB Lane).

| Inside Lane |  |  | Outside Lane |  |  |
| :---: | ---: | :--- | ---: | ---: | :--- |
| Crack \# | Distance from <br> Crack \#1 (ft) | Severity | Crack \# | Distance from <br> Crack \#1 (ft) | Severity |
| 1 | 0 | Low | 1 | 0 | High |
| 2 | 239 | Medium | 2 | 447 | Medium |
| 3 | 294 | High | 3 | 663 | Medium |
| 4 | 583 | Medium | 4 | 704 | Low |
| 5 | 704 | High | 5 | 711 | Low |
| 6 | 860 | Low | 6 | 717 | Low |
| 7 | 917 | Low | 7 | 726 | Medium |
| 8 | 950 | Low | 8 | 745 | High |
| 9 | 975 | Medium | 9 | 764 | Medium |
| 10 | 992 | Medium | 10 | 776 | Medium |
| 11 | 995 | Low | 11 | 992 | Medium |
| 12 | 1058 | Medium | 12 | 1052 | Medium |

## Test Section 03a (FM 158, EB Inside Lane)

Length:
1159 ft
Start point: N $30^{\circ} 40.295^{\prime}$; W $096^{\circ}$ 20. 836' (Electric substation; Crossing of WJ Bryan Pkwy. \& Long Dr.) End point: $\quad \mathrm{N} 30^{\circ} 40.307^{\prime}$; W $096^{\circ}$ 20.603' (Landmark: Bryan USPS)

Table II-6. Transverse Crack Mapping on Test Section 03a (FM 158, EB Inside Lane).

| Crack\# | Distance from Crack\#1 (ft) | GPS Location | Severity |
| :--- | ---: | ---: | :--- |
| 1 | 0 | N 30 $40.295^{\prime} ;$ W 096 ${ }^{\circ}$ 20. 836' | Medium |
| 2 | 30 |  | Low |
| 3 | 43 |  | Medium |
| 4 | 110 |  | High |
| 5 | 150 |  | High |
| 6 | 252 |  | High |
| 7 | 293 |  | High |
| 8 | 353 |  | High |
| 9 | 381 |  | Medium |
| 10 | 397 |  | Low |
| 11 | 430 |  | Low |
| 12 | 469 |  | Low |
| 13 | 489 |  | High |
| 14 | 503 |  | Low |
| 15 | 550 |  | Medium |
| 16 | 558 |  | Medium |
| 17 | 584 |  | High |
| 18 | 651 |  | High |
| 19 | 665 |  | Low |
| 20 | 705 |  | High |
| 21 | 734 |  | High |

Table II-6 (Continued).
Transverse Crack Mapping on Test Section 03a (FM 158, EB Inside Lane).

| Crack\# | Distance from Crack\#1 (ft) | GPS Location | Severity |
| :--- | ---: | :--- | :--- |
| 22 | 830 |  | High |
| 23 | 850 |  | Low |
| 24 | 951 |  | Medium |
| 25 | 1011 |  | Medium |
| 26 | 1033 |  | Medium |
| 27 | 1077 |  | Low |
| 28 | 1086 |  | High |
| 29 | 1121 |  | Low |
| 30 | 1159 | $\mathrm{~N} 30^{\circ} 40.307^{\prime} ; \mathrm{W} 096^{\circ} 20.603^{\prime}$ | High |

## Test Section 03b (FM 158, WB Outside Lane)

| Length: | 1185 ft |
| :--- | :--- |
| Start point: | $\mathrm{N} 30^{\circ} 40.422^{\prime}$; W $096^{\circ}$ 21. 950' |
| (Landmark: St. Joseph elementary school; intersection of WJ Bryan Pkwy \& Pierce Ave.) |  |
| End point: | $\mathrm{N} 30^{\circ} 40.466^{\prime}$; W $096^{\circ}$ 22. 163' (Landmark: Brazos County Health Dept.) |

Table II-7. Transverse Crack Mapping on Test Section 03b (FM 158, WB Outside Lane).

| Crack\# | Distance from Crack\#1 (ft) | GPS Location | Severity |
| :---: | :---: | :---: | :---: |
| 1 | 0 | $\mathrm{~N} 30^{\circ} 40.422^{\prime} ; \mathrm{W} \mathrm{096}{ }^{\circ} 21.950^{\prime}$ | Medium |
| 2 | 104 | - | High |
| 3 | 301 | - | High |
| 4 | 322 | - | High |
| 5 | 346 | - | Low |
| 6 | 379 | - | High |
| 7 | 770 | - | Low |
| 8 | 872 | - | Medium |
| 9 | 1131 | - | Low |
| 10 | 1185 | $\mathrm{~N} 30^{\circ} 40.466^{\prime} ; \mathrm{W} 096^{\circ} 22.163^{\prime}$ | High |



Figure II-1. Example of Cracking on Section 1 - FM 158 WB @ Intersection of Nash Dr. and William J. Bryan Pkwy.


Figure II-2. Example of Cracking on Section 3 - FM 158 WB Adjacent to Brazos County Health Center.


Figure II-3. Example of Cracking on Section 1 - FM 158 EB Intersection of William J. Bryan Pkway and Pierce St.


Figure II-4. GPR Test Run on WB Outside Lane Prior to Overlay Placement.


Figure II-4. GPR Test Run on EB Outside Lane Prior to Overlay Placement.

## APPENDIX III: CONSTRUCTION REPORT

Highway:
FM 158 (W. J. Bryan Pkwy)
Construction Date: $\quad$ Winter 2010 (Dec $10^{\text {th }}$ through $31^{\text {st }}$, 2010)
Contractor:
Construction:
HMA mix:
Bid price:

Knife River Corporation
1-inch thick HMA overlay with intermittent Mill \& Inlay on some sections
CAM (Item 3131)
$\$ 80 /$ ton for the PG 76-22 asphalt and $\$ 93 /$ ton for the aggregate

Table III-1. QC/QA Test Results on Plant-Mix, Cores, \& In-situ HMA Mat.

| \# | Item | Truck\# 09 | Truck\# 18 |
| :---: | :---: | :---: | :---: |
| 1 | Design AC (PG 76-22 Jebro)= <br> Avg. Ignition Oven AC $($ uncorrected $)=$ <br> (Tolerance $\pm 0.3 \%$ ) | $\begin{aligned} & \hline 6.7 \% \\ & 6.5 \% \end{aligned}$ | $\begin{aligned} & \hline 6.7 \% \\ & 6.64 \% \end{aligned}$ |
| 2 | Hamburg on plant-mix after 2000 passes $=$ OT on plant-mix = | $\begin{aligned} & 2.9 \mathrm{~mm} \\ & 738 \text { cycles } \end{aligned}$ | $\begin{array}{\|l\|} \hline 5.8 \mathrm{~mm} \\ 854 \text { cycles } \end{array}$ |
| 3 | Lab design density $=97 \%$ <br> Avg. HMA mat density during construction (PQI) $=92 \%$ <br> Avg. core density (TTI) $=94.1 \%$ <br> Avg. core density on section where Paver had stopped due to change of MTD $=91.3 \%$ |  |  |
| 4 | Avg. PVMNT surface temperature during construction $=67^{\circ} \mathrm{F}$ Avg. HMA mat temperature during construction $=290^{\circ} \mathrm{F}$ Production temperature $\cong 320^{\circ} \mathrm{F}$ |  |  |
| 5 | Compaction pattern $=6$ vibratory passes ( 14 ton steel wheel roller) Final compacted HMA mat $=1$ inch |  |  |

Table III-2. Aggregate Gradation Extractions on Plant-Mixes.

| Sieve <br> Size | Sieve Size (mm) | Design Passing (\%) | Spec - Passing (\%) |  | Plant-Mix (Passing) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Lower | Upper | Truck\# 9 | Truck\# 18 |
| 3/8" | 9.5 | 98.7 | 98 | 100 | 96.8\% | 98.4\% |
| \#4 | 4.75 | 73.6 | 70 | 90 | 65.5\% | 69.7\% |
| \#8 | 2.36 | 55.3 | 40 | 65 | 45.7\% | 48.5\% |
| \#16 | 1.18 | 37.5 | 20 | 45 | 34.5\% | 36.3\% |
| \#30 | 0.06 | 22.2 | 10 | 30 | 28.7\% | 30.4\% |
| \#50 | 0.03 | 10.7 | 10 | 20 | 23.8\% | 25.3\% |
| \#200 | 0.0075 | 4.4 | 2 | 10 | 5.9\% | 6.8\% |

Table III-3. Average High-Speed Profiles (IRI) Measured Just after Construction.

| Lane | Avg. Left WP (in/mi) | Avg. Right WP (in/mi) | Average (in/mi) |
| :--- | ---: | ---: | ---: |
| EB Inside | 93.2 | 86.7 | 89.9 |
| EB Outside | 84.9 | 109.4 | 97.2 |
| WB Inside | 83.9 | 83.9 | 83.9 |
|  |  |  | 124.5 |
| EB Outside | 102.0 |  | 113.2 |
| Overall avg. |  |  |  |



Figure III-1. Example of Milling Operation and Milled-Off section.


Figure III-2. MTD and Truck Types.


Figure III-3. Paver, IR Bar, and Compactor.


Figure III-4. Final Compacted HMA Overlay Mat (1-Inch thick).


Temperature Class Diagram


Figure III-5. Example of Infra-Red Thermal Profiles.
Time Diagram


Figure III-6. Example of a Temperature Time Diagram.
Speed Diagram


Figure III-7. Example of a Paver Speed Diagram.


Figure III-8. GPR on EB Outside Lane Just after Construction.


Figure III-9. GPR on WB Outside Lane Just after Construction.


Distance ( ft )
Figure III-10. IRI Plots (Just after Construction, Jan 2011).
Note: Looks like it is not easy get good ride in urban sections with all of the drainage and tight curves. Nonetheless, it is a low speed road ( $35-40 \mathrm{mph}$ ).


Figure III-11. Comparisons of Core Densities.

