Floodwall and Levee Performance Analysis, Physical Modeling









Physical Modeling Team



Michael K. Sharp, PhD, PE
Wipawi Vanadit-Ellis, MS
Wayne Hodo
Henry Blake
David Daily
Dave Carnell



R. Scott Steedman, PhD FREng FICE Kevin Stone, PhD



Prof Tarek H. Abdoun, PhD
Prof Thomas F. Zimmie, PhD, PE
Inthuorn Sasanakul, PhD
Javier Ubilla, MS
Marcelo Gonzalez, MS
Hassan Radwan
Alex Sankovich
Dominic Moffitt



Prof Dr Ir Frans Barends Paul Schaminée , MSc Adam Bezuijen, MSc









Physical (Centrifuge) Modeling

Work Plan

- Use workshops to develop model concept, model design and technical approach
- Obtain block samples of peat layer, test
- Specify materials (clay, sand, flood wall)
- Finalize trial model sections
- Carry out trial models of London North, 17th Street
- Evaluate results from trials and refine plan
- Complete full series of model tests, collate and present photo and instrumental data for comparison with numerical modeling













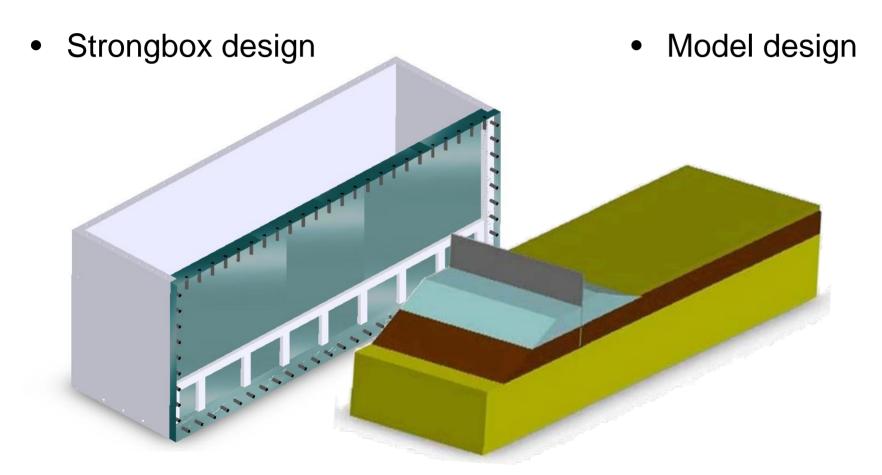








Simulation of Field Conditions





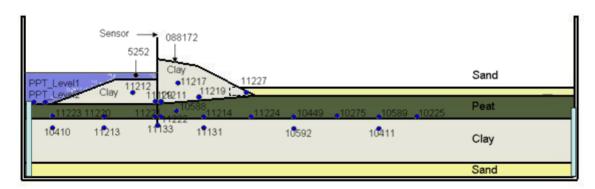


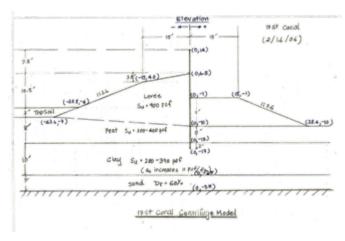




Design Considerations

- Geometry of the model soil profile and details of the levee
- Establishing initial conditions
- Instrumentation techniques
- Flood conditions















Material Considerations



 Sand – use a fine Nevada sand, a widely used laboratory sand



 Flood wall – use steel or aluminium plate, circa 1/4" thick at 1/50 scale



- Peat use peat cut from block samples recovered from the site
- Clay use a laboratory kaolin clay, consolidated to the correct strength profile







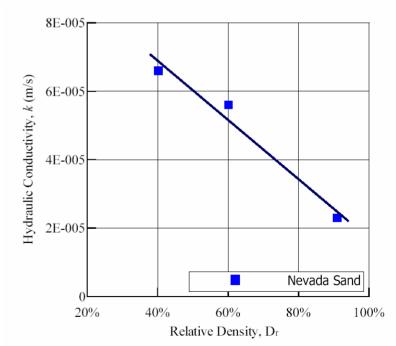


Sand

 Key material parameters are relative density and permeability

D_{10}	0.08 mm	
D_{50}	0.15 mm	
Specific gravity, Gs	2.67	
Max. void ratio, emax	0.887	
Min. void ratio, emin	0.511	
Max. dry density	17.33 kN/m ³	
Min. dry density	13.87 kN/m ³	













Flood wall

 Use solid plate, in aluminium or steel

Scaling bending stiffness gives:

(EI)
$$_{\text{model}} = (EI)_{\text{field}}/N^3$$

$$N^3.E_m.d_m^3/12 = (EI)_f$$

Sheet piles in the field (Hoesch 12) have I = 65.4 in⁴, hence bending stiffness of $EI = 2 \times 10^9$ psi

Model wall in aluminium at 1/50 scale is around 1/4" thick.









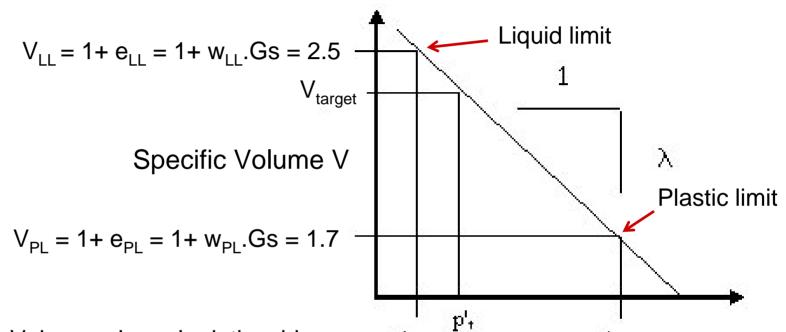


Initial Conditions for Kaolin

e void

Volume

solid



 p_{PL}

Exploiting the Volume – Log p' relationship:

$$p'_{PL}/p'_{t} = (Su)_{PL}/(Su)_{t} = exp [(V_{target}-V_{PL})/\lambda]$$

effective confining pressure p'

 p'_{PL}

Based on knowledge of the undrained strength Su: Undrained strength at Liquid limit $(Su)_{LL} = 1.7 \text{ kPa}$ Undrained strength at Plastic limit $(Su)_{PL} = 170 \text{ kPa}$









Peat

- Cut from block samples excavated from the field
- Key properties strength, stiffness and permeability
- Re-consolidated to original conditions in centrifuge flight









Floodwall and Levee Performance Analysis, Physical Modeling

Model Preparation and Preliminary Results









Presentation Outline

- London North Model
 - Model Preparation
 - Preliminary Results
 - Preliminary Observations
- 17th Street
 - Model Preparation
 - Preliminary Results
 - Preliminary Observations

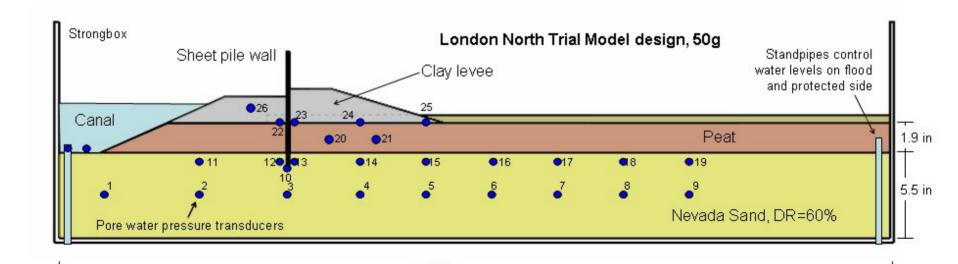








- Two trial models were tested one model at each facility (RPI & ERDC)
- Levee: Synthetic clay (match field conditions based on lab test, CPT, etc)
- Swamp/Marsh: Actual field material
- Beach: Fine sand such as Nevada Sand



48 in



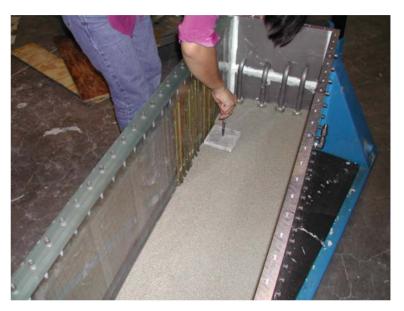


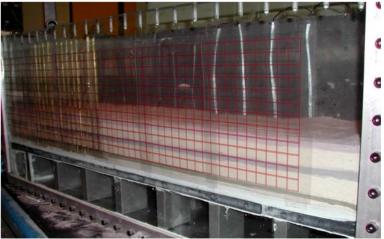




Sand Placement















Peat Placement









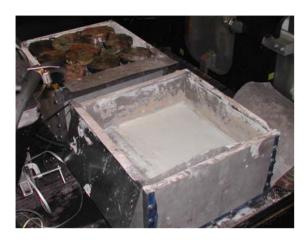
















Clay Levee Placement













New Orleans Levee Centrifuge Models London North Test



Rensselaer Polytechnic Institute CEES Center

http://nees.rpi.edu/









New Orleans Levee Centrifuge Models London North Test



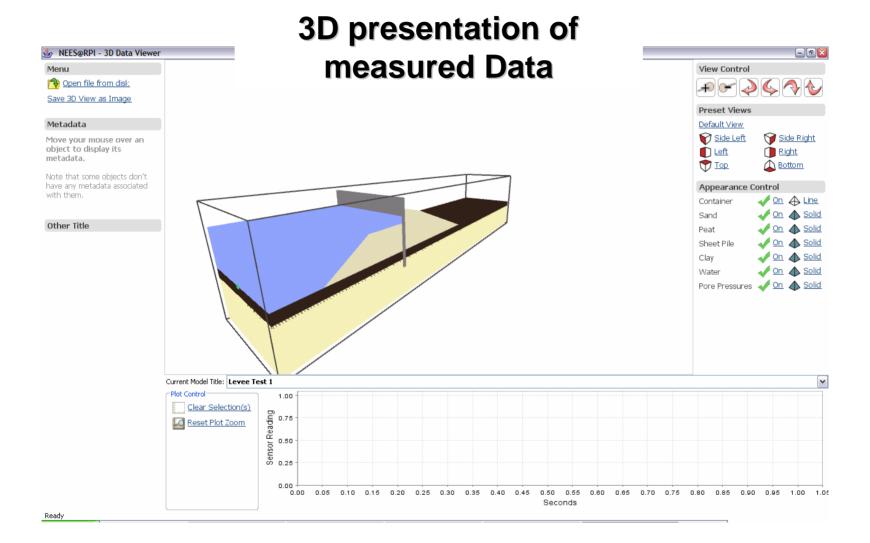
US Army Engineer Research and Development Center









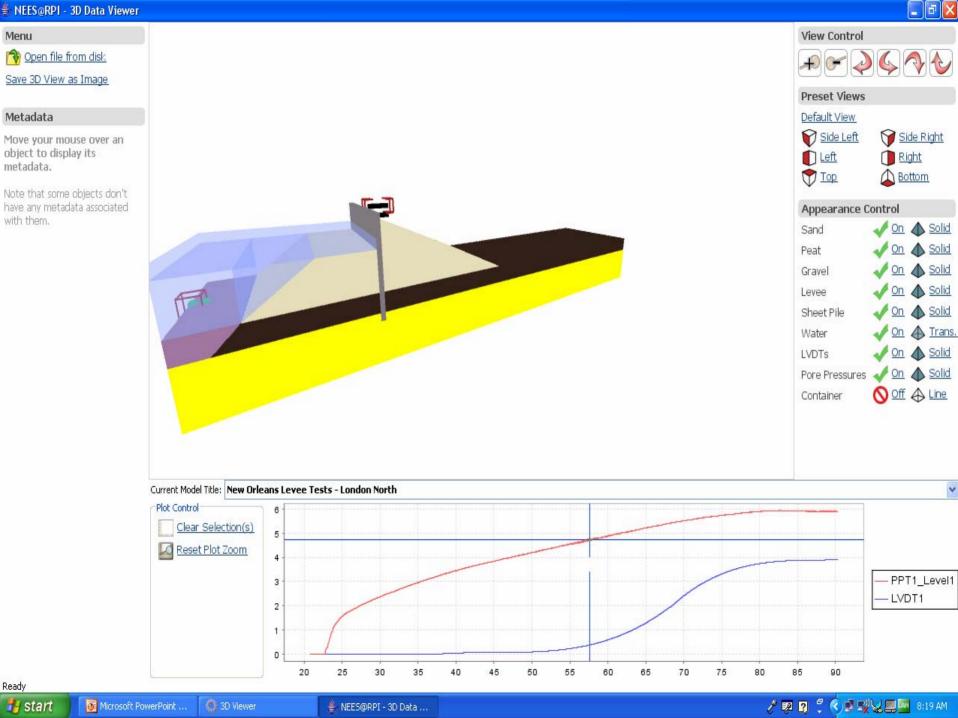


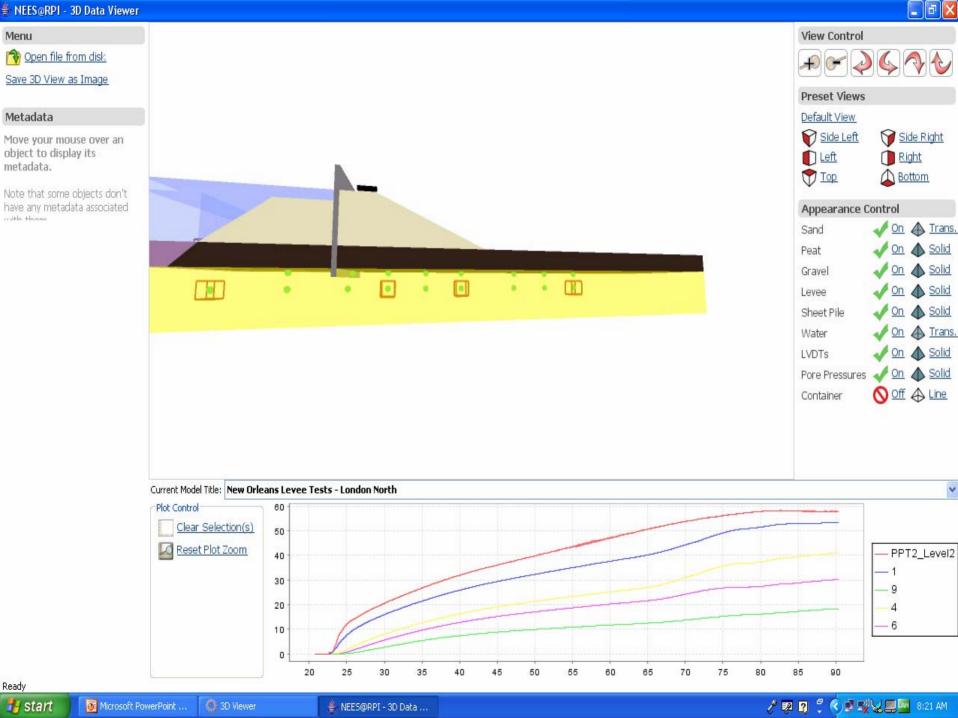


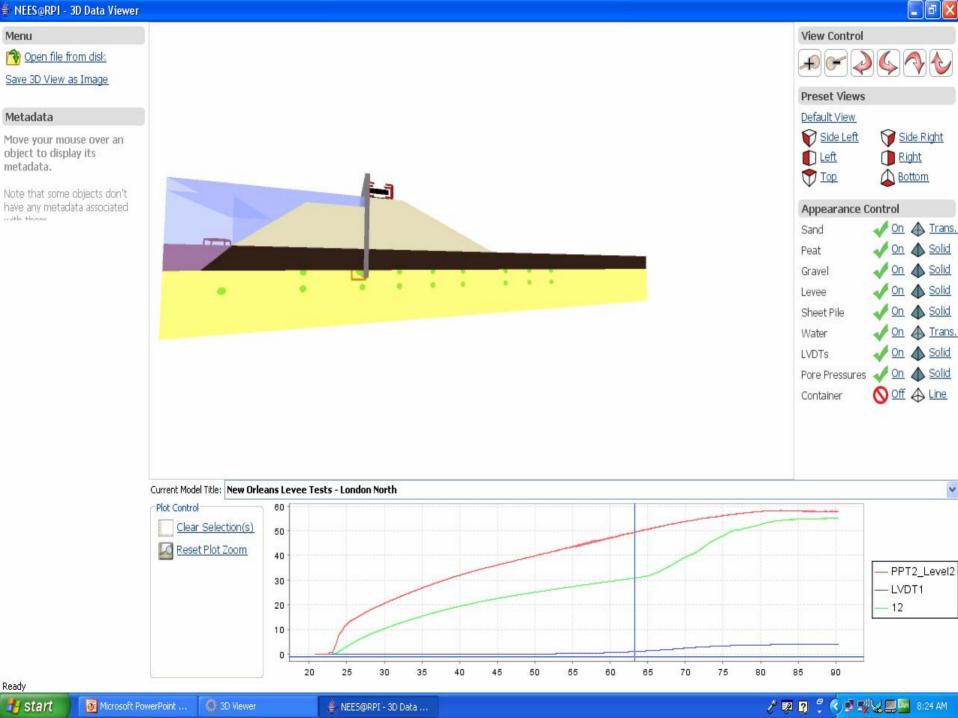


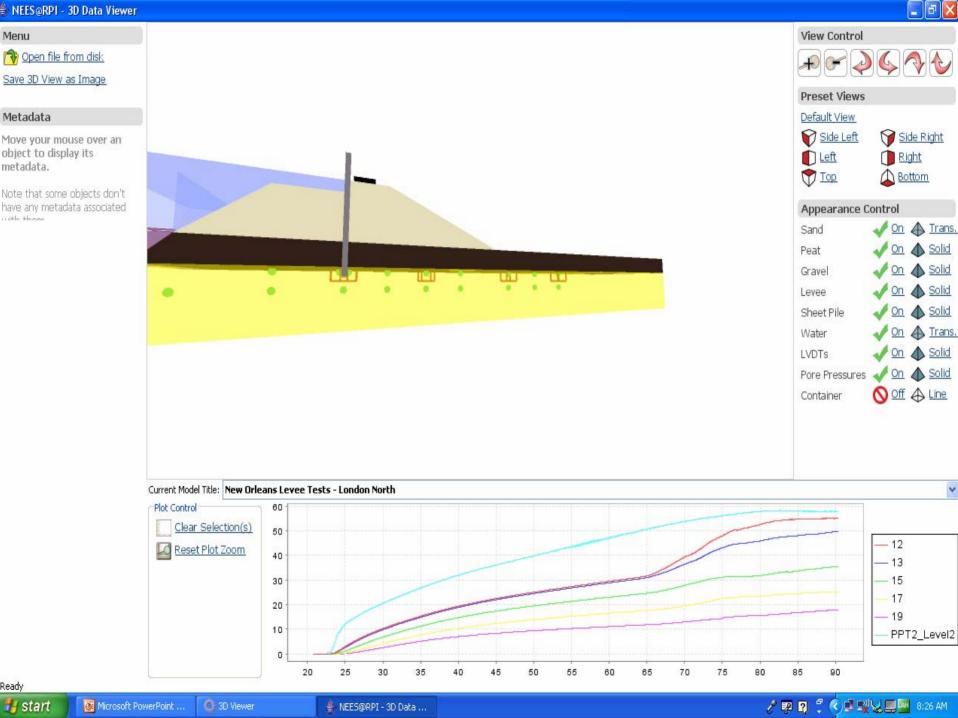


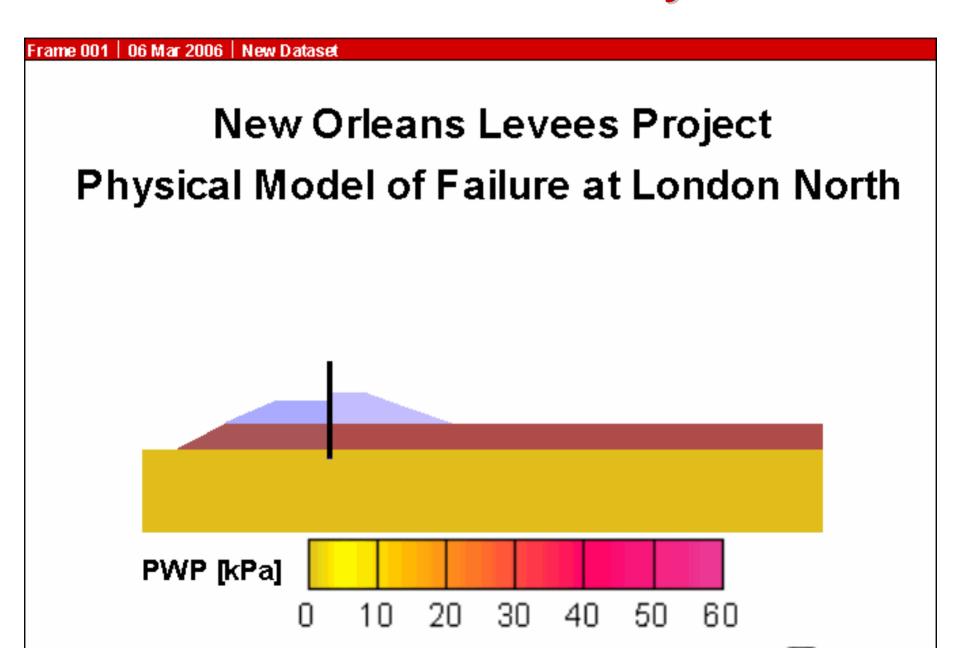


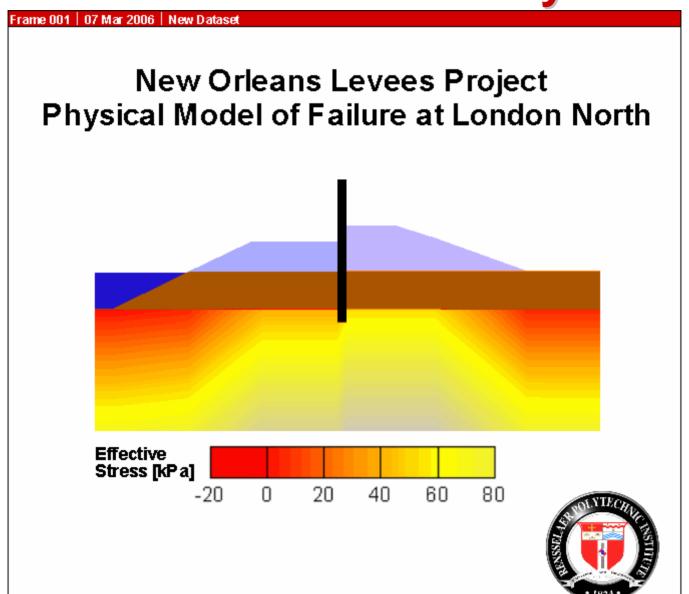




















London North: Preliminary Observations

- Similar model responses are recorded in both the RPI & ERDC models confirming the repeatability of the physical models.
- As the water level rose to flood levels, a crack formed down the front of the wall.
- Failure of the wall is associated with an increase in the hydrostatic pressure (uplift) under the downstream levee.



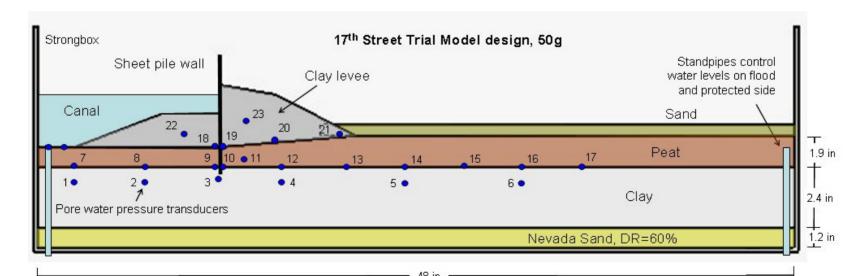






17th Street: Model Preparation

- One trial model was tested at RPI. A second model is under construction at ERDC
- Levee: Synthetic clay (match field conditions based on lab test, CPT, etc)
- Swamp/Marsh: Actual field material
- Lacustrine: Synthetic clay (match field conditions)
- Beach: Fine sand such as Nevada Sand











17th Street: Model Preparation

Clay Placement











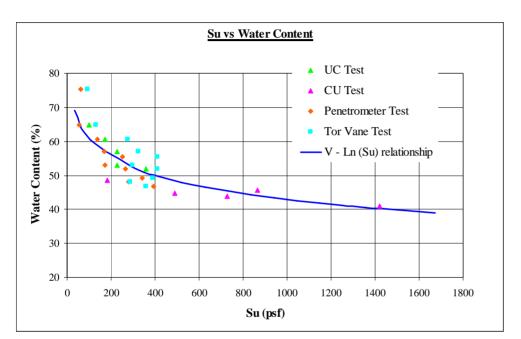








17th Street: Model Preparation Clay Placement









Shear Strength Estimation of Clay Layer @17th street

Location	Water	Estimate	Estimate
	Content (%)	S _u (kPa)	S _u (psf)
Surface (after Consol.)	75	3-5	70-110
Surface (after Testing)	64	5-7	110-140
Middle (after Testing)	59	9-12	200-250
Bottom (after Testing)	57	12-15	250-310









17th Street: Model Preparation

Peat Placement















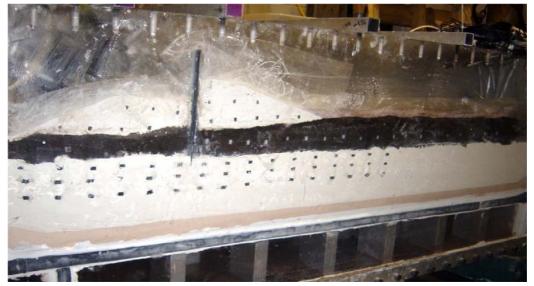


17th Street: Model Preparation





Clay Levee Placement





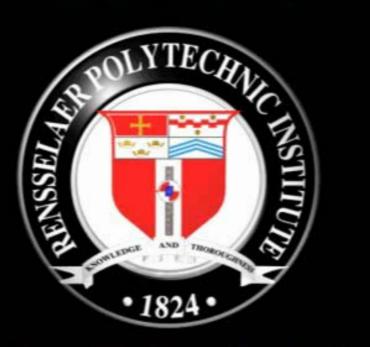






17th Street: Preliminary Results

New Orleans Levee Centrifuge Models 17th Street Test



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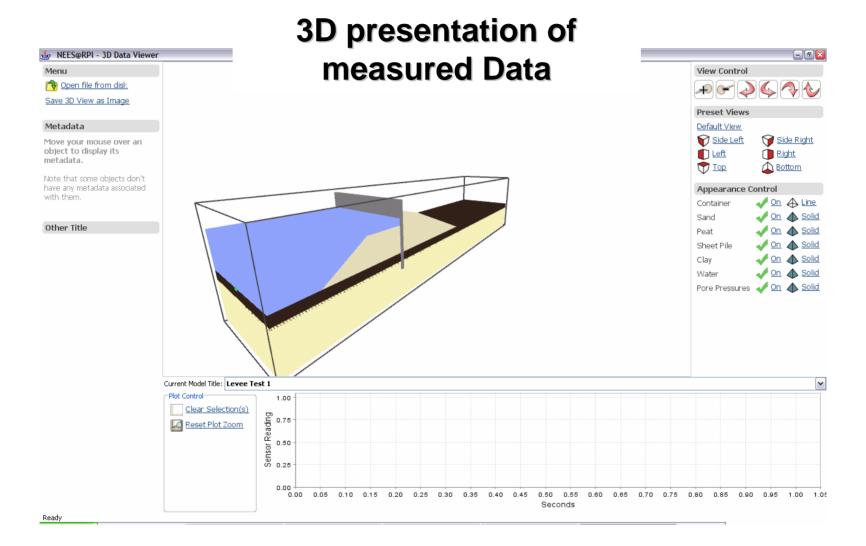








17th Street: Preliminary Results





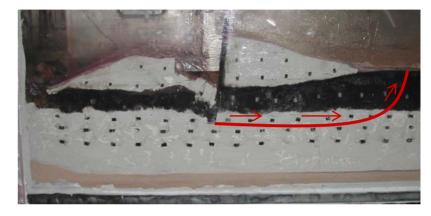






17th Street: Preliminary Observations

- The wall experienced limited tilt and limited increase in the hydrostatic pressure under the downstream levee.
- Shear failure occurred in the clay layer comparable to the field observation.













Future Plans

- To fully understand the failure mechanisms
- •To integrate the physical model results with the overall performance assessment of the levees
- Provide practical insights to Task Force Guardian









