

A satellite image of a hurricane over the Gulf of Mexico. The hurricane is a large, circular storm system with a distinct eye and a dense, swirling cloud structure. The surrounding ocean is dark blue, and the landmasses of North and Central America are visible in shades of green and brown. The text is overlaid on the image.

Standard Project Hurricane

Nancy J. Powell, PE
Chief, Hydrologic Engineering Section
New Orleans District



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- **Meteorological parameters for the SPH are contained in National Hurricane Research Project Report 33, “Meteorological Considerations Pertinent to Standard Project Hurricane, Atlantic and Gulf Coasts of the United States”, 1959.**
- **After Hurricane Betsy in 1965 the Weather Bureau revised the wind field parameters, but did not change the other characteristics of the SPH.**

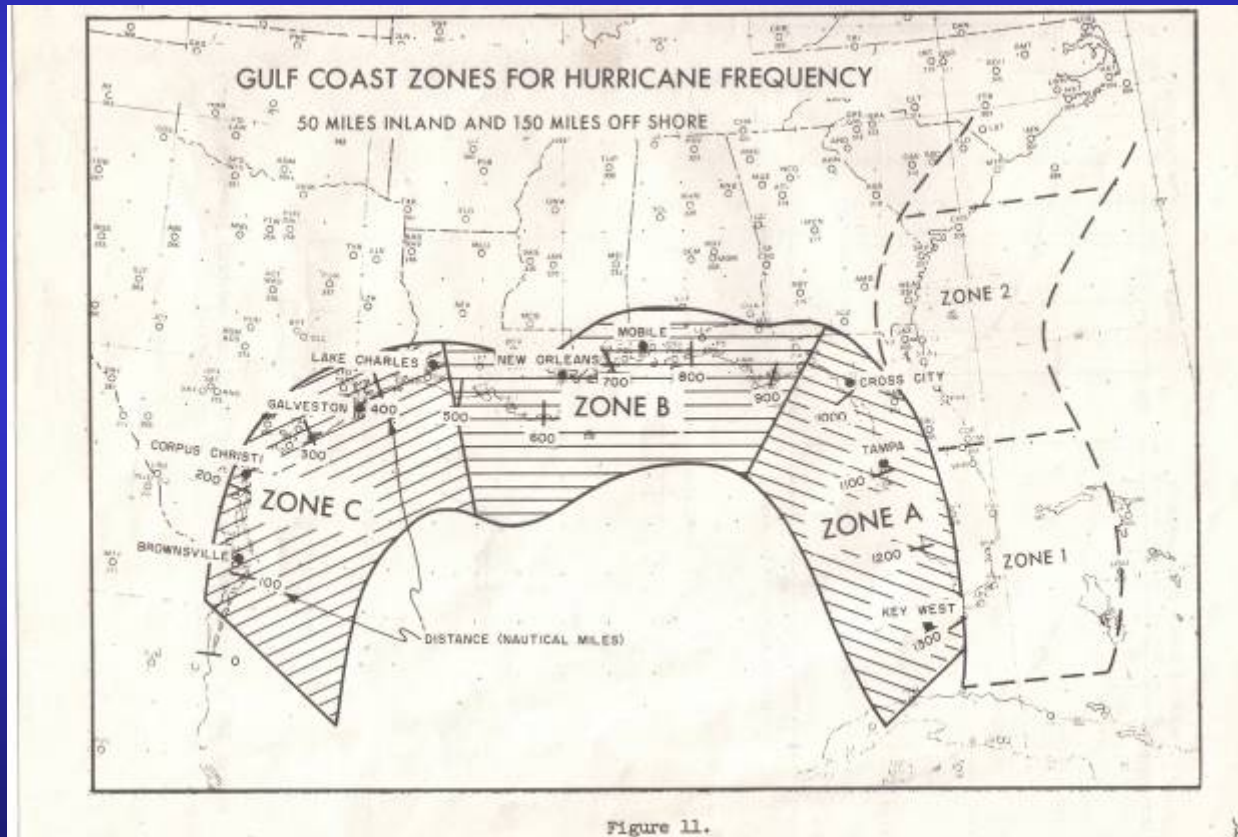


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- Gulf Coast was divided into three zones.





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- **The central pressure index (CPI) is the principal intensity criterion for defining the SPH index.**
- **The CPI is the estimated minimum pressure for individual hurricanes in each zone.**
- **For any hurricanes, the CPI was determined from observations of minimum pressure at a given location; computations based on observational data; or by estimate in event that the hurricane passed through a zone where there were insufficient pressure observations to complete a computation but enough evidence to warrant an estimate.**



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- **Period of Analysis – 1900 through 1956**
- **A list of storms for which the CPI was less than or equal to 29 inches was developed for each zone.**
- **In Zone B, 23 storms were identified with CPI < 29 inches.**
- **However, two storms, Audrey and Hilda, were not used in the frequency analysis; the parameters for these storms were not available at the time of SPH derivation.**

$$P = \frac{100(M - 0.5)}{Y}$$



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- A frequency analysis of CPI occurrences per 100 years was developed for each zone using the formula

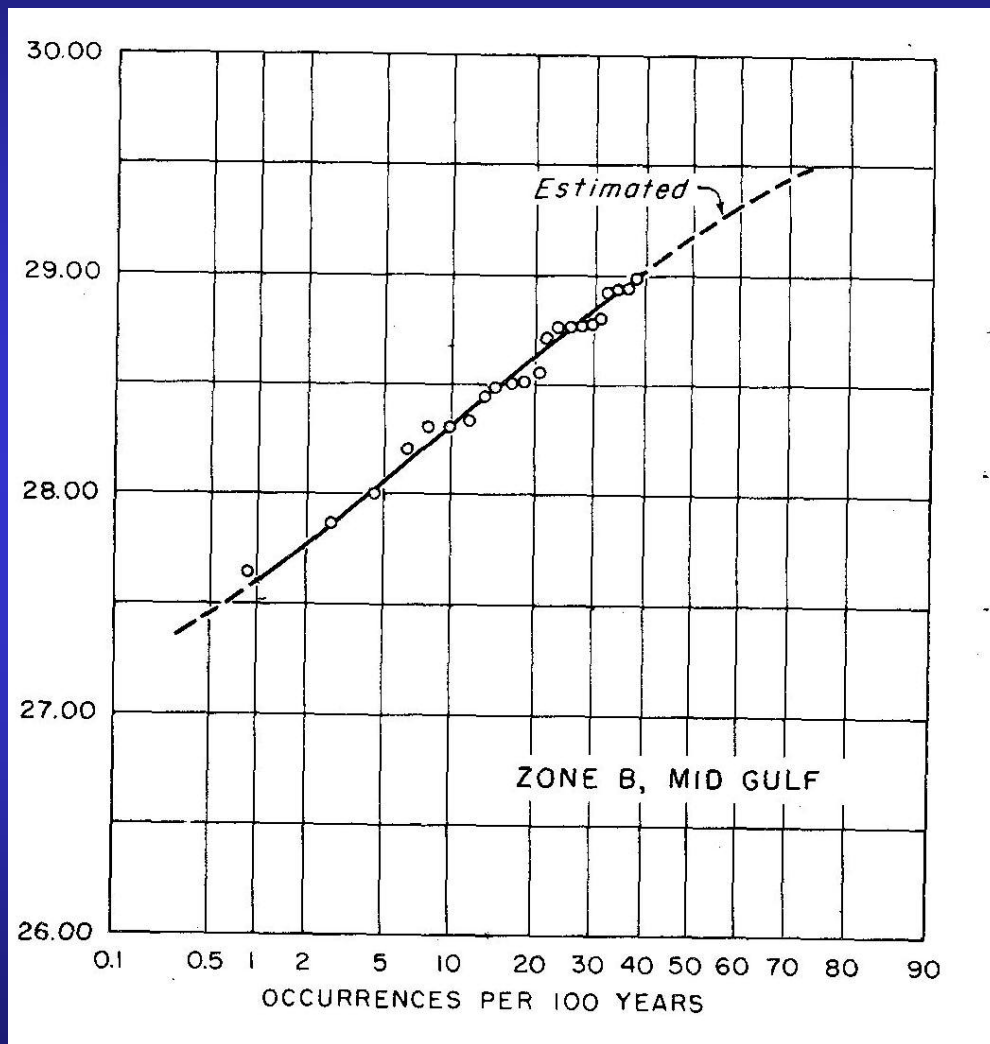
$$P = \frac{100(M - 0.5)}{Y}$$

- P = percent chance of occurrence per year
- M = number of the event (rank)
- Y = the number of years of record (57)



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- The radius to region of maximum winds (R) is an index of hurricane size and is an important factor in the generation of waves and tides.
- R was determined for the storms with CPI values less than 29 inches.
- R was determined from observations at a wind reporting station or by computations made from the pressure field.

$$P = \frac{100(M - 0.5)}{y}$$



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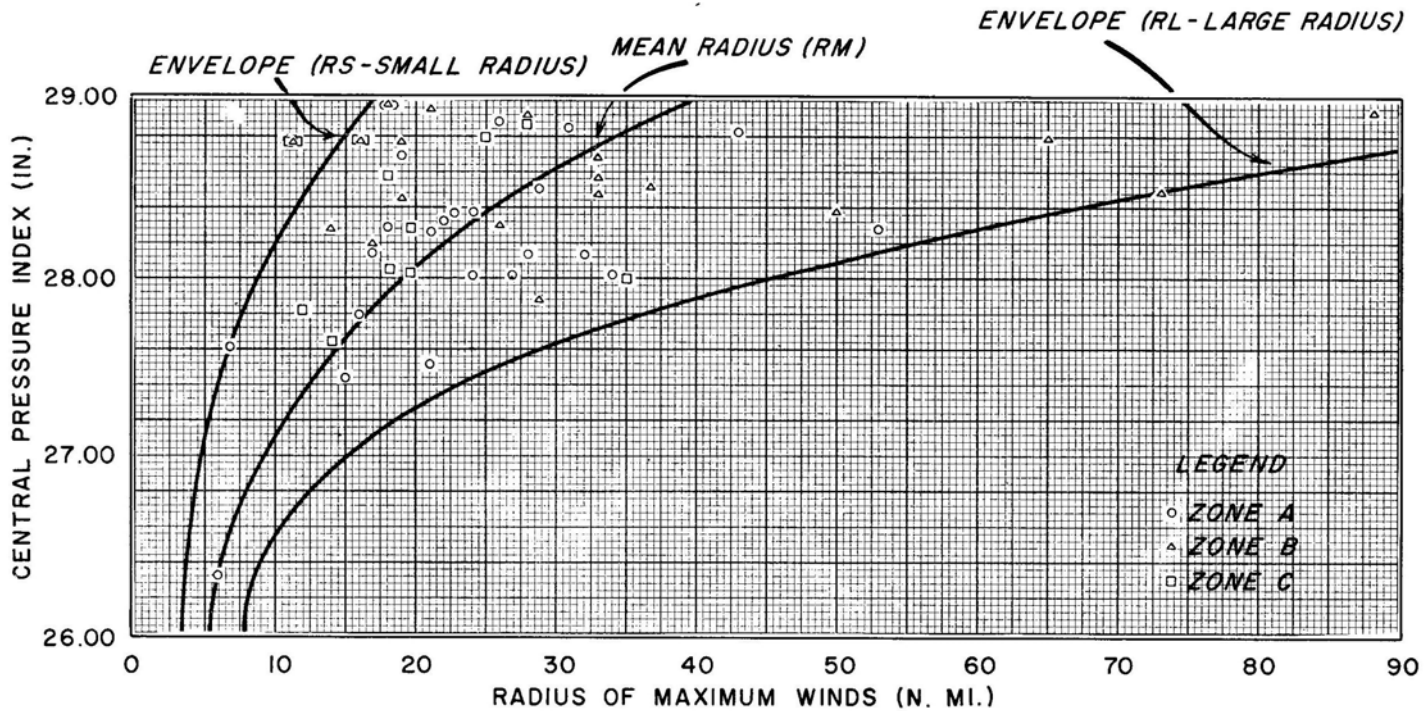


Figure 17. - Variation of radius of maximum winds with central pressure index, Gulf Coast, 1900-1956.



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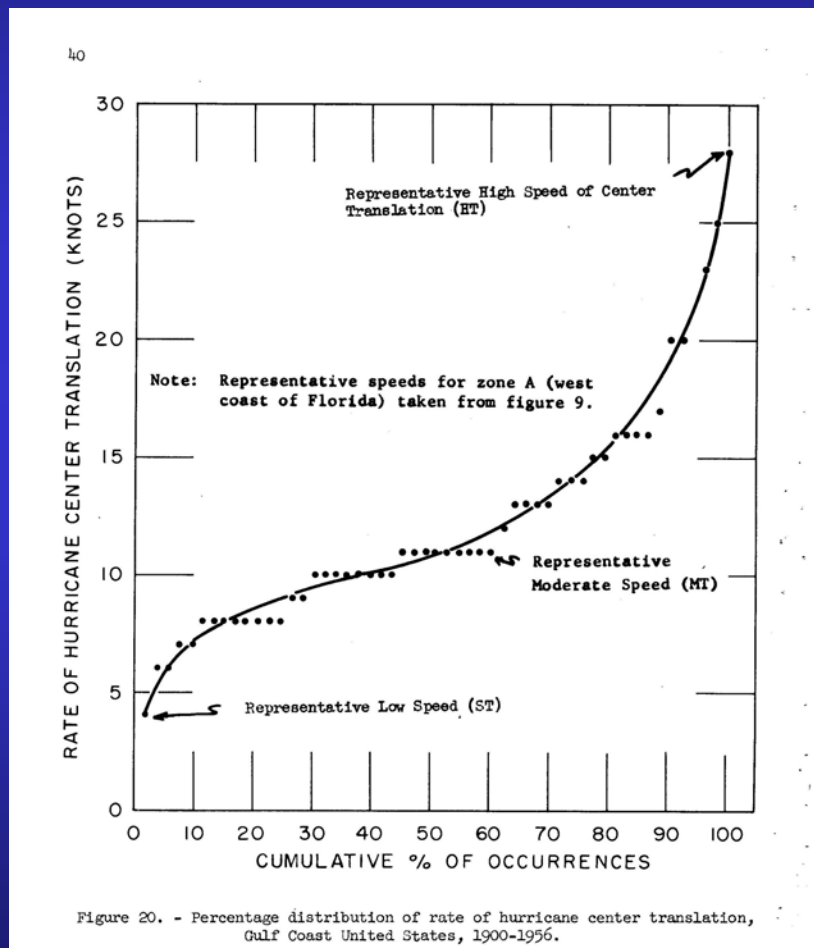


- **The forward speed of translation of the hurricane centers is determined as the average speed for the period from 2 hours before to 2 hours after the hurricane enters the coast.**
- **Due to the limited latitudinal variation and limited data available, all of the Gulf coast hurricane forward speeds were used.**



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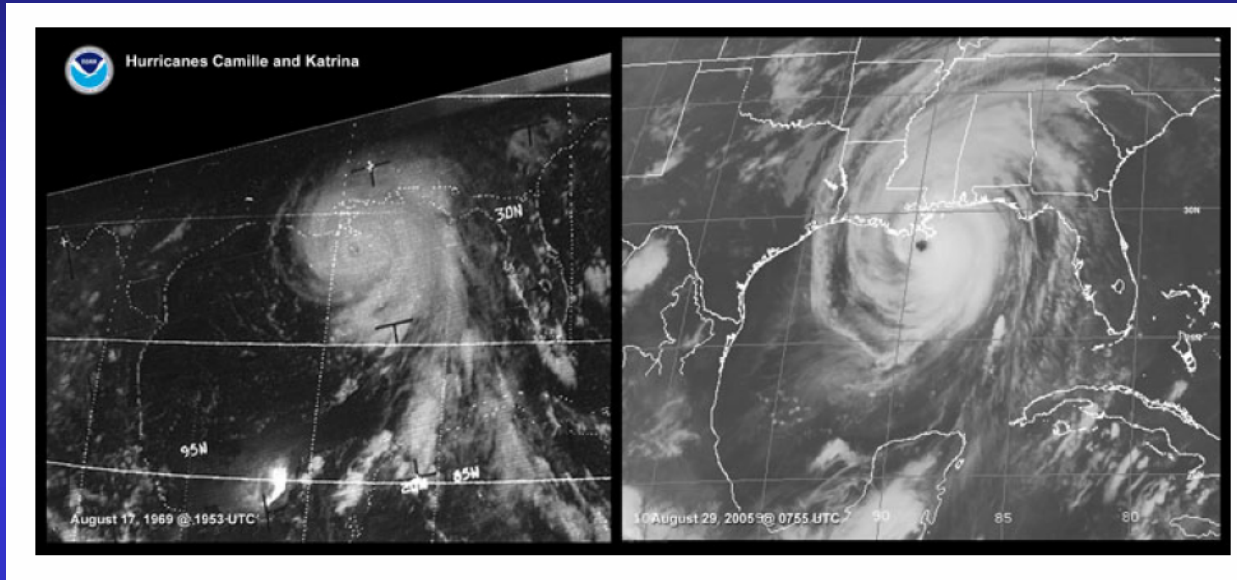
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SPH vs Katrina



	SPH	Katrina
Wind speed	101 mph	127 mph
Central pressure	27.60 inches	27.17 inches
Radius max winds	30 N miles	25 to 30 N miles
Forward speed	15 mph	15 mph

One Team: Relevant, Ready, Responsive, Reliable



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- **Design elevation**
 - Stillwater or wind tide level
 - Runup height from waves, if present
 - Freeboard
- **Stillwater elevation**
 - Tide
 - Pressure setup
 - Setup due to winds
 - Buildup

$$S = 1.165 \times 10^{-3} \frac{V^2 F}{D} NZ \cos \theta$$

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- Setup due to winds computed using a general wind tide equation

$$S = 1.165 \times 10^{-3} \frac{V^2 F}{D} NZ \cos \theta$$

- S = wind setup in feet
- V = windspeed in statute miles per hour
- F = fetch length in statute miles
- D = average depth of fetch in feet
- θ = angle between direction of wind and the fetch
- N = planform factor, generally equal to unity
- Z = surge adjustment factor



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- Two historical storms along the Mississippi coast, the September 1915 and September 1947 hurricanes, were used to establish and verify procedure.
- The computed maximum surge height was compared to the observed high water marks from these storms.
- Z , surge adjustment factor, was computed so that computed maximum surge height agreed with observed high water marks.



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- Procedure was applied to Louisiana coast.
- Chalmette Loop levee reach.
- Three storms, September 1915, September 1947, and September 1956, were used to compute Z, surge adjustment factors, for four locations.
- Setup due to winds was computed.
- Maximum surge elevation was computed.



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- **Wave runup calculations were made using model study data developed by Saville and presented in CERC Technical Report 4.**
- **For the Chalmette Loop**
 - **Average depth of fetch = 9.7 to 16.3 ft**
 - **Significant wave height = 4.6 to 7.0 ft**
 - **Wave period = 5.2 to 6.4 ft**
 - **Wave runup height = 4.3 to 4.7 ft**



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- **Design elevation, Chalmette Loop**
 - **IHNC to Paris Road**
 - ◆ **Maximum Surge Elevation = 13.0 ft MSL**
 - ◆ **No wave runup**
 - ◆ **Freeboard = 1 ft**
 - ◆ **Design Elevation = 14.0 ft MSL**
 - **Paris Road to Bayou Lawler (MRGO reach)**
 - ◆ **Maximum Surge Elevation = 12.5 – 13.0 ft MSL**
 - ◆ **Wave Runup Height = 4.3 to 4.7 ft**
 - ◆ **Design Elevation = 17.5 MSL**



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- **For the Chalmette Extension, the presence of coastal wetlands was considered in the development of the maximum surge elevation at the location of the protection system.**
 - **Maximum surge height would occur near the coastline.**
 - **The surge height would decrease inland.**
- **From a study of high water marks at the coastline and inland, a simple relationship between maximum surge height and distance inland was developed.**
- **A weighted mean decrease in surge height of 1 ft per 2.75 miles was determined.**



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- For the three interior drainage canals in Orleans Parish, step backwater calculations were made using HEC-2 to compute maximum water surface elevations during the SPH event.
- Starting water surface elevation in Lake Pontchartrain = 11.5 ft NGVD (maximum wind tide elevation in the lake at that location)
- Future work, such as floodproofing, raising bridges, and additional pump capacity, was considered in the analysis.
- No wave runup.
- 2 ft of freeboard was added.

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