HNF-FMP-07-32540-R0



FMP (FACILITY MODIFICATION PACKAGE) FORM Page 1 of 4												
Design	Package Ide	ntification			unananaen ek	e de la companya de l	Print Harman Transport Harman School (1994)					
1. Mod Title: Pallets, 48 x 48 and 56 x 56 Key Words: N/A 8. Release: Release CACN _1 ARR 13 2001 (12)									12)	98		
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4. Area 5. Building 6. System No. 7. FM 200G N/A N/A K D			7. FMP /				Design Authority Print/Signature/Date			polos		
9. USQ F	Required?	USQ 🗌 CX	×Ν	IA.	No.:							
10. Environmental-Activity Screening Form Completed? YES X NO If Yes, is the Environmental-Activity Form Attached? YES NO												
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12. Change Description (description and reason for requested change): H-2-832930 PROVIDED FOR INITAL RELEASE OF DRAWING SET.												
Approv	als						·					
13. FMP Author K D HEIN 12/21/02 R STEEN 11/20 F HAMADA 2/22/07 F HAMADA 2/27/07												
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14. Document Index												
Action	ction Document Sh/Pg			Rev	E/S		FMP Section	FMP Section Title		Release To Work?		
	-2-832930		1,2	0	S	N/A						
N/A	15. Related FMPs/Changes: N/A 17. Lead Engineering Discipline: 18. Affected Engineering Disciplines:											
N/A N/A												
Modification Bases												
19. Engineering Request or Proposal:												
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Submit List to Document Control for Project Status? YES X NO												

	FMP (FACILI	TY MODIFICATI	ON PACKAGE) FO	RM (continued)					
21. Potentially Affected Documents Not Changed By This FMP:									
	Document Type	Document Number/Revision	Document Owner (Organization)	Technical Authority Notified	Date				
N/A		N/A	N/A	N/A	Notified N/A				
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22.	Conceptual Evaluations:		I		· · · · · · · · · · · · · · · · · · ·				
N/	A								
23.	Functions, Requirements, and Design Cr	iteria:							
	Functions:								
	USED FOR STORAGE AND TRANS	SPORT OF DRUMS							
	Requirements:								
	MUST HAVE LOAD CAPACITY OF	12,000 LBS. M	UST MEET CERTAIN S	SECTIONS OF ASME MH	1 (2005) -				
1	SEE DWG NOTES ON SHT 1	,			(2000)				
	Design Criteria:								
	SEE DWG NOTES ON SHT 1								
24.	Post-Installation Acceptance Test Criteria:		•						
	Design Verification:	· · · · · · · · · · · · · · · · · · ·							
	Design Verification Checklist Questions a. Are the assumptions, functions, requirem b. Does the design meet the stated assump c. Were the design inputs correctly incorpor d. Is the design output reasonable compare e. Have suitable materials, parts, processes f. Have manufacture, maintenance, and ope g. Are all affected active design documents	tions, functions, requirementated into the design? d to the design inputs? s, and inspections and testerability been adequately	nents, and design criteria? X YES	YES NO XYES NO XYES NO XYES NO NO					
The the	view of the design has been performed. verification completed by the method(s) stated functions, requirements, and design verifier Print/Signature/Date	noted that this FMP is a	requirements, and design of accurate, and the design defined by the second seco	riteria meet the stated engine ined by this FMP and related o	ering request. documents meets				
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HNF-FMP-07-32540-RO

These calculations demonstrate the adequacy of the pallet currently ordered and used for SWOC. Throughout the calculations, it is assumed that the wood used is Western White Pine. Western White Pine has the least desirable mechanical properties of wood allowed by ASME MH1, *Pallets, Slip Sheets, and Other Bases for Unit Loads*, (2005). This assumption builds conservatism, while bounding other wood selections allowed by MH1. Some other data was gleaned from *Machinery's Handbook*, 26th Addition (2000).

Credit is taken for Administrative controls in place for limiting a single pallet to 4000 lbs, and that they can be stacked a maximum of 3 high.

The fasteners used are 3 mm (D) x 2.75 in (L), helically threaded and hardened.

1) Force required for shearing fasteners.

Assume the fastener material is low carbon steel (1025), with an ultimate tensile strength (UTS) of 70 ksi. Further assume that Shear is .75 of UTS. A pure shearing load for pallet fasteners is <u>highly</u> unlikely.

Shear =
$$\underbrace{Pi \times D^2 \times .75UTS}_{4}$$
 = $\underbrace{3.14(.118)^2 \times .75(70 \text{ ksi})}_{4}$ = 575 lbs.

Minimum 3 fasteners are used per connection point, so Shear = 3X, or 1725 lbs.

2) Wood Failure between Fasteners - Shear Loading

Wood Tear (WT) = $(p - D) \times t \times S(t)$, where S(t) = Tensile Strength of Pine Perp to Grain, p = distance between fasteners (3 ea) on a 2 x 6 pallet.

$$S(t) = 330 \text{ psi}$$
 So, $WT = (1.375 - .118) \times 1.5 \times 330 = 622 \text{ lbs.}$

3) Force Withdrawal Resistance (FWI) See MH1 for values and definitions

4) Fastener Withdrawal Resistance Value (FWRF), Single fastener. See MH1 for values and definitions

FWRF = 222.2 x FWI x (GS^{2.25}) x P / (MC-3)
FWRF = 222.2 x 113 x
$$(40/62.4)^{2.25}$$
 x 1.5 / (20 - 3)
FWRF = 818 lbf

5) Fastener Head Pull-Through Resistance Value (HPRF) Single fastener. See MH1 for values and definitions

HPRF =
$$1.25 \times 10^6 \times T \times (GD^{2.25}) \times (HD^2 - WD^2) / (MC - 3)$$

HPRF = $1.25 \times 10^6 \times .75 \times (40/62.4)^{2.25} \times (.28^2 - .118^2) / (20 - 3)$
HPRF = 1307 lbf

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6) Crushing Pallet Material Perp to the Grain - Machinery's Handbook offers a range of 190 psi to 470 psi.

Pallet Stringers are 48 in long 2 x 4 members. Actual dimensions of a finished 2 x 4 is 1 1/2 x 3 1/2.

Single stringer contact area with a single deck board = $5 \frac{1}{2}$ in x $1 \frac{1}{2}$ in = 8.25 in²

The 48 x 48 pallet has 4 total stringers and 4 bottom deck boards, making 16 areas of contact, so Total Area = $16 \times 8.25 = 132$ in²

The Admin Control for pallets is 4000 lbs max per pallet, and a maximum of 3 stacks high, for a total of 12,000 lbs.

The maximum pressure exerted on the bottom pallet is $12,000 \text{ lbs} / 132 \text{ in}^2 = 91 \text{ psi} \ll 190 \text{ psi}$. This offers a safety factor in excess of 2 even if the lowest crushing strength value is used.

Calculations 1 and 2 demonstrate an intuitively obvious dynamic, that in a shear load condition, the material between fasteners would fail before the fastener would. Again, shear loading for pallets is highly unlikely, and is an off-normal condition for pallet use.

Calculations 3, 4 and, 5 offer performance criteria for the pallet in use at SWOC. They provide the forces needed for fastener pullout and fastener head pull-through for a single fastener. The drawing requires a minimum 3 fasteners at each attachment location between stringer and deck board, and this attribute increases each of the criteria by the total number of fasteners.

Calculation 6 demonstrates that, under maximum static loading, the pallet material will not crush due to overloading.

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