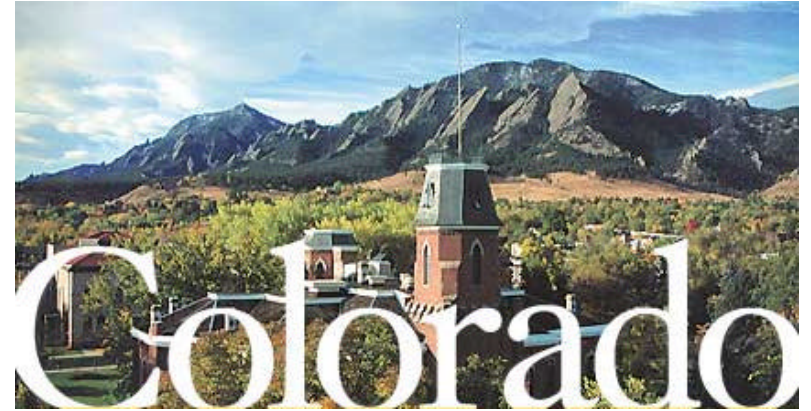


- Materials System Approach
- The Criteria
- Basic Research Issues



Polymer Derived Graded EBCs

Rishi.Raj@Colorado.edu (Boulder)

In Alliance with
Honeywell ES&S (Phoenix AZ)

ORNL-EBC (Nashville)
Nov. 6-7, 2002

THE PROBLEM

Silicon Nitride Vanes

1066°C-1260°C; 8.9 atm, $p_{\text{H}_2\text{O}} = 0.101$

162m/s to 573 m/sec

- 27% of cross section lost in 1818 h
- recession and mechanical degradation
- Si_3N_4 grains are oxidizing and then volatilizing

“Evaluation of Mechanical Reliability of Silicon Nitride Vanes after Field Tests in an Industrial Gas Turbine” Liu, Ferber, Westphal and Macri(ORNL report - I assume)

A Tenet

silica passivation mechanism for oxidation protection is not viable
for the exposed surfaces of Si_3N_4 vanes and blades in humid
combustion environment

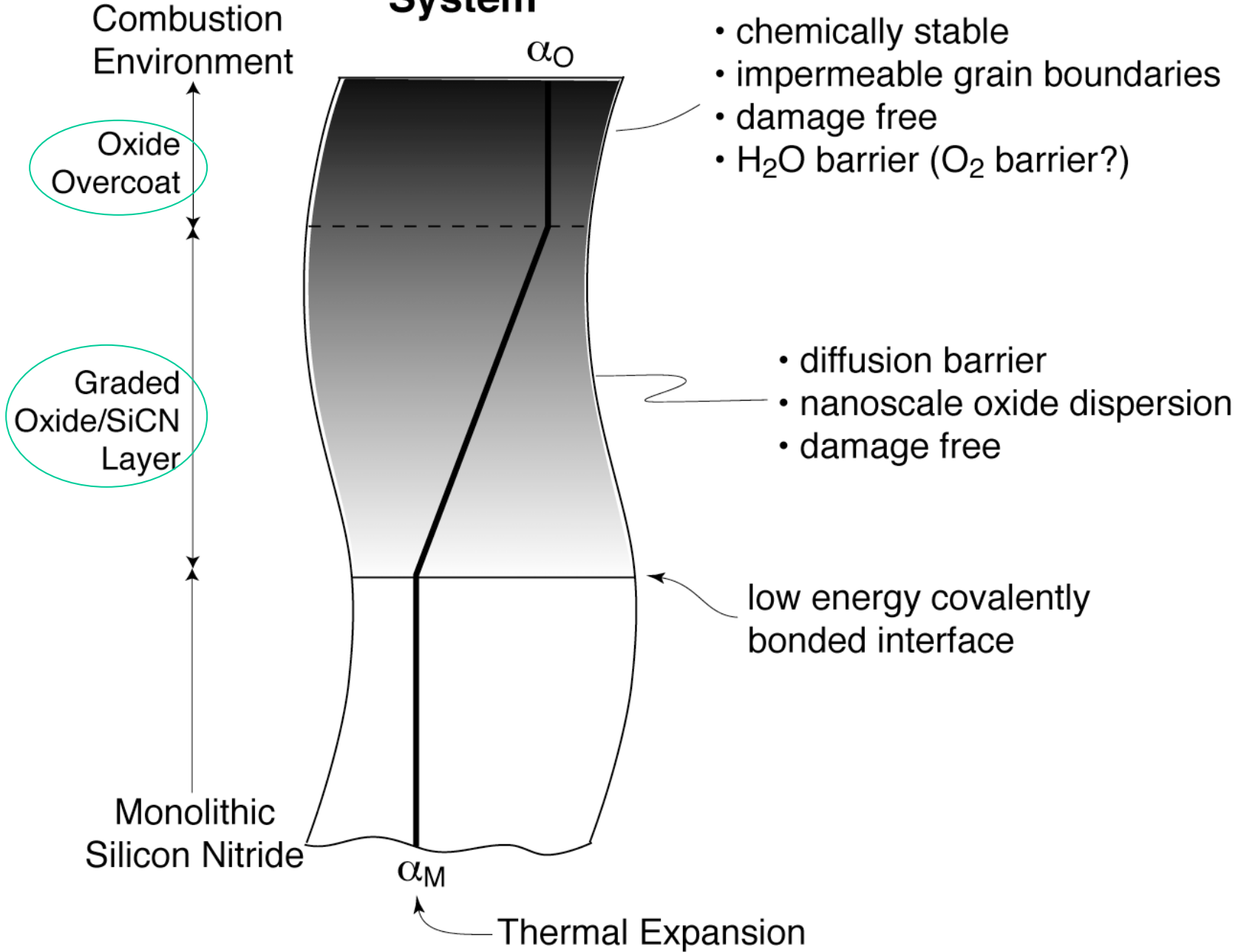
Opila et al. (JACerS)

The Design of a Graded Interface

Objective: prevent silicon nitride (SiO_2) volatilization

- oxide overlayer for chemical stability, isolation from humid environment
- graded interface prevents thermal shock, provides diffusion barrier for oxygen
- interfaces mechanically robust, nucleation barriers to silica formation

The EBC System



Elastic Energy Density is given by:

Monolithic Coating

$$U_v^o = f(\text{Elastic constants}) \cdot \Delta\alpha_o^2 \quad /\text{vol}$$

Graded Coating

$$\Delta\alpha = \Delta\alpha_o \cdot \frac{z}{h}$$

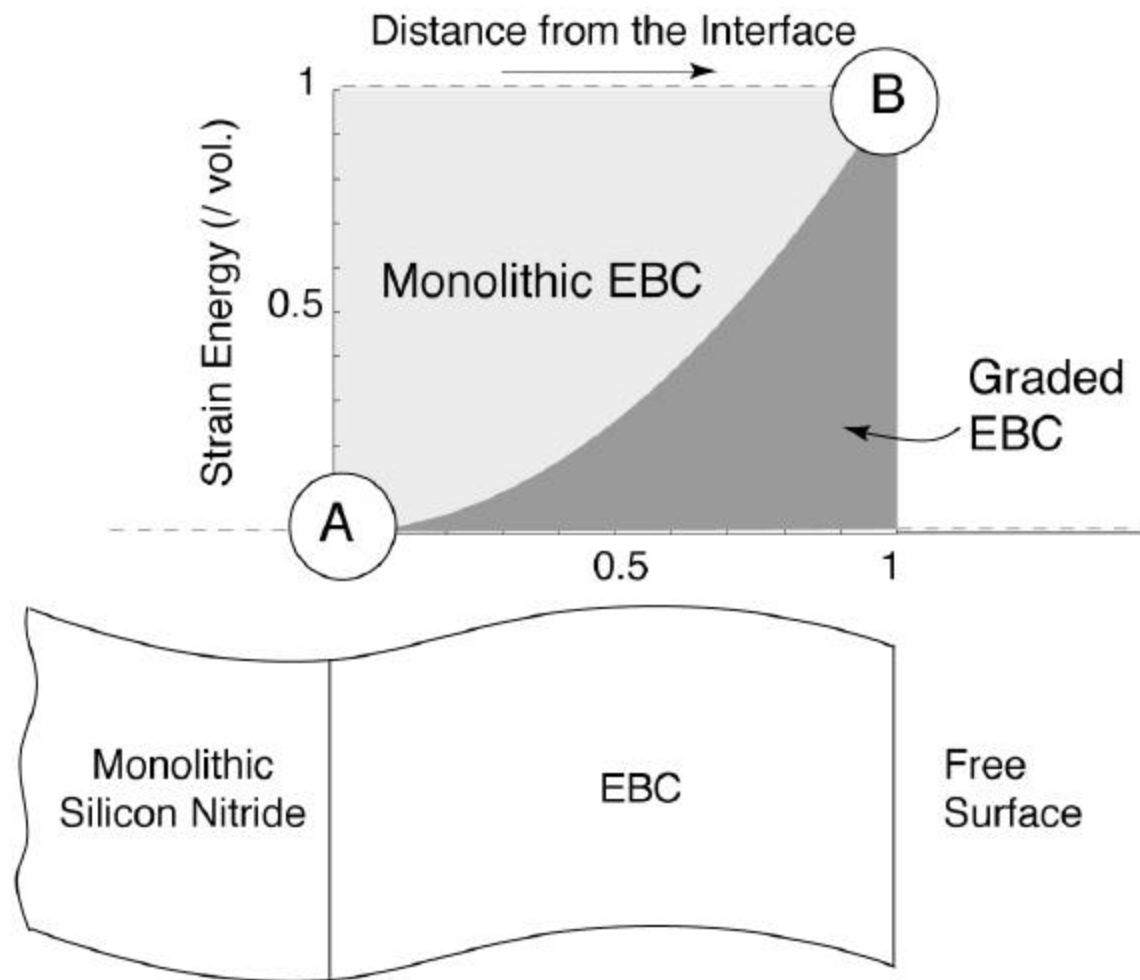
$$U_v(z) = f. \left(\Delta\alpha_o \cdot \frac{z}{h}\right)^2$$

graded interface
for thermal shock
resistance -
ANALYSIS

	Energy Density /vol	Total Energy /area
Monolithic	$f. \Delta\alpha_o^2$	$f. \Delta\alpha_o^2 \cdot h$
Graded	$f. \left(\Delta\alpha_o \cdot \frac{z}{h}\right)^2$	$\frac{1}{3} f. \Delta\alpha_o^2 \cdot h$

h= total EBC thickness

	Strain Energy	Strain Energy Gradient
A: cracks cannot nucleate	LOW	POS.
B: cracks cannot grow	HIGH	NEG.



Materials Selection (Oxide Overlayer)

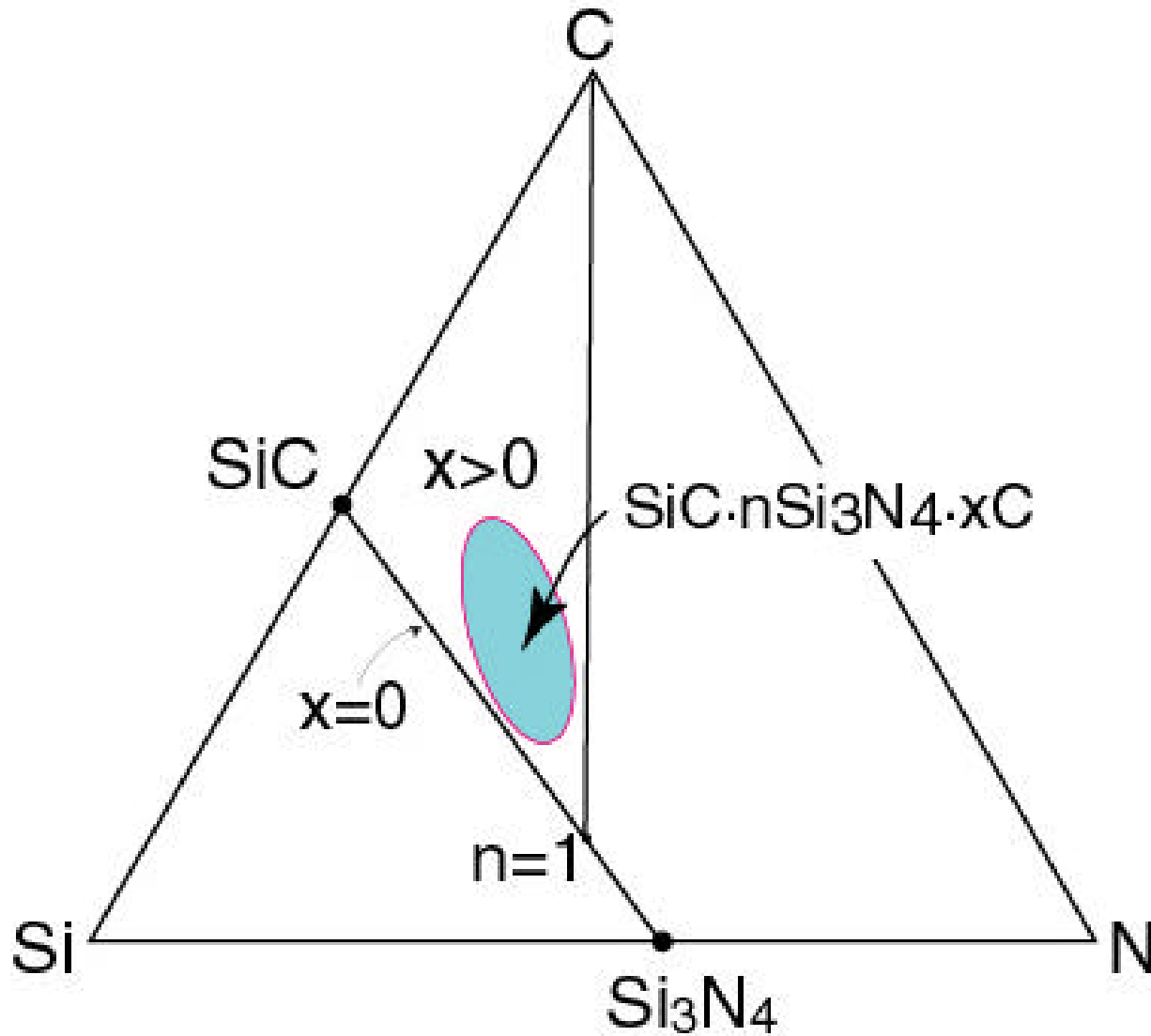
- Transition Metal Oxides (ZrO_2 , HfO_2 , Ta_2O_5 , TiO_2)
- Base Metal Oxides (Al_2O_3 , MgO etc.)
- Complex Oxides (YAG, Perovskites, etc.)
- Silicates (Mullite, etc.)

*simple oxides are process friendly -
more likely to be implemented*

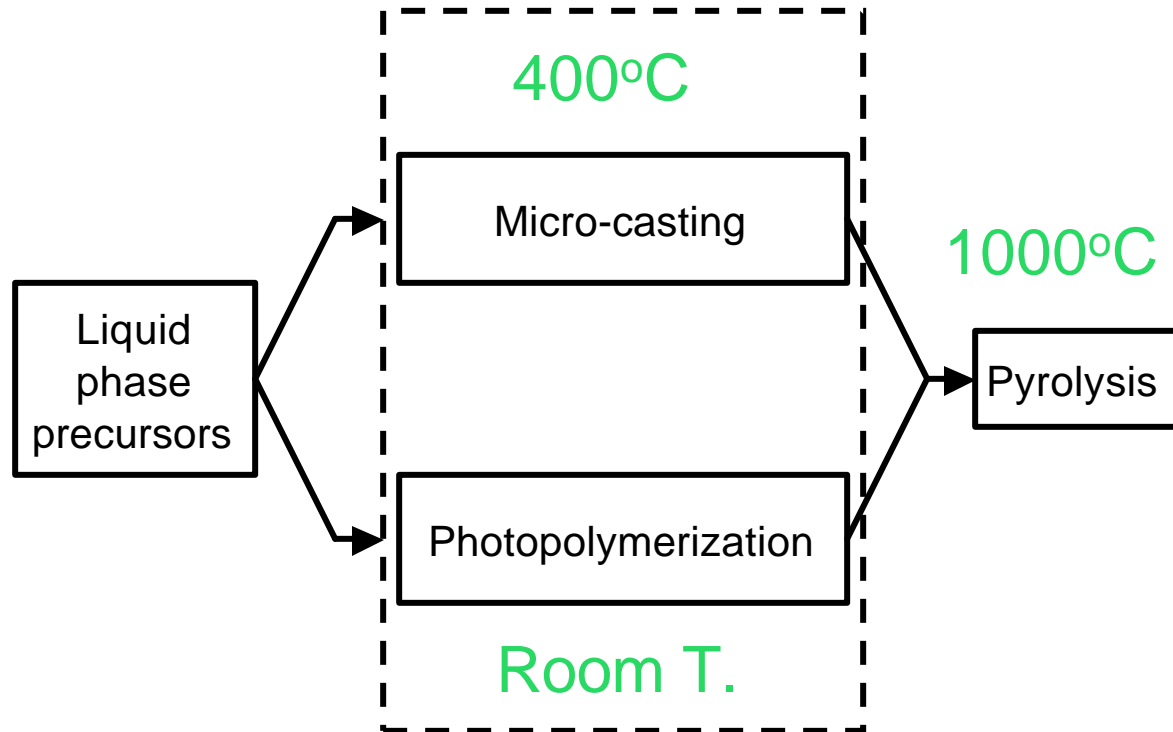
Why PDCs for the Gradient Layer?

- compatible with oxides
- liquid precursors: CVD, dip coating, for step-coverage
- low energy interfaces with oxides, Si_3N_4
- ultra-slow diffusion at ultrahigh temperatures

Composition Diagram for SiCN



The PDC Process



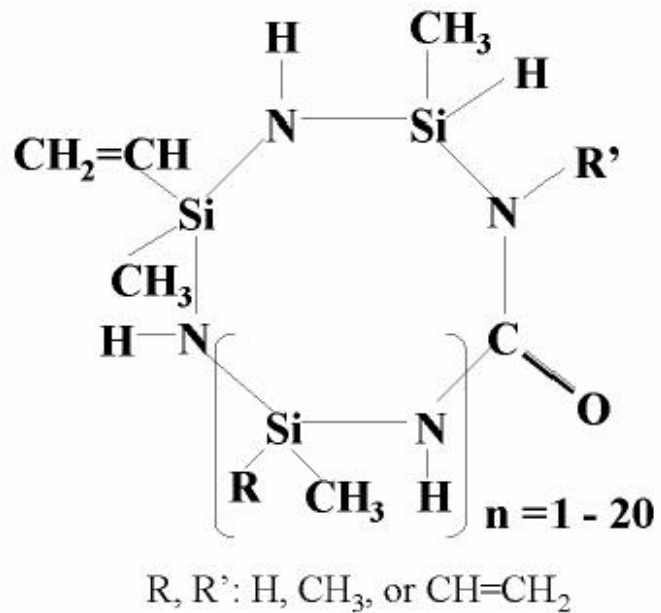
**Liquid
Precursor**

**Plastic
Net-Shape**

**Ultrahigh T.
Ceramic**

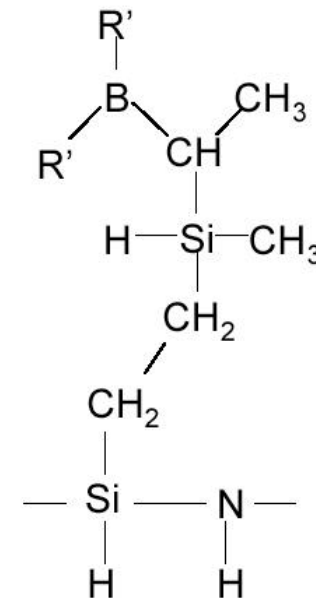
Organic Precursors for SiCN

CERASET

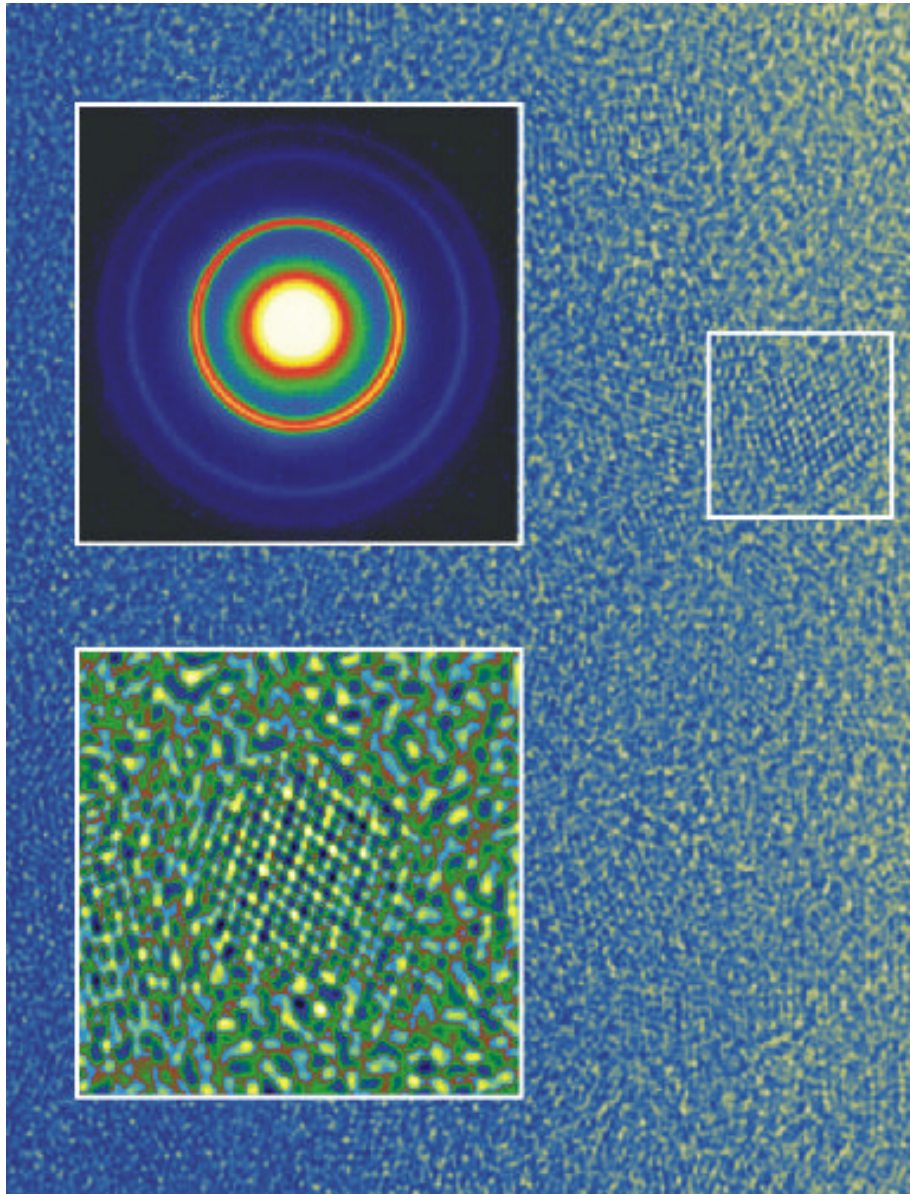


SiCN

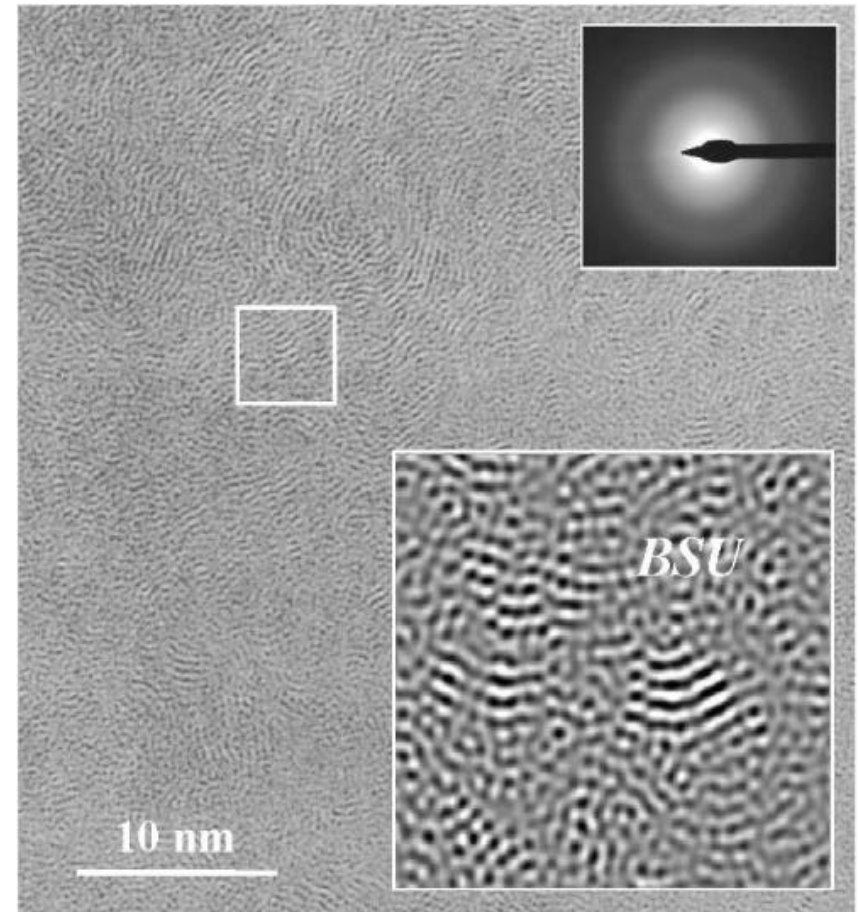
PBMS



SiCN Doped with B



Special Issue JACerS, Oct. 20 01
 Ultrahigh Temperature PDCs



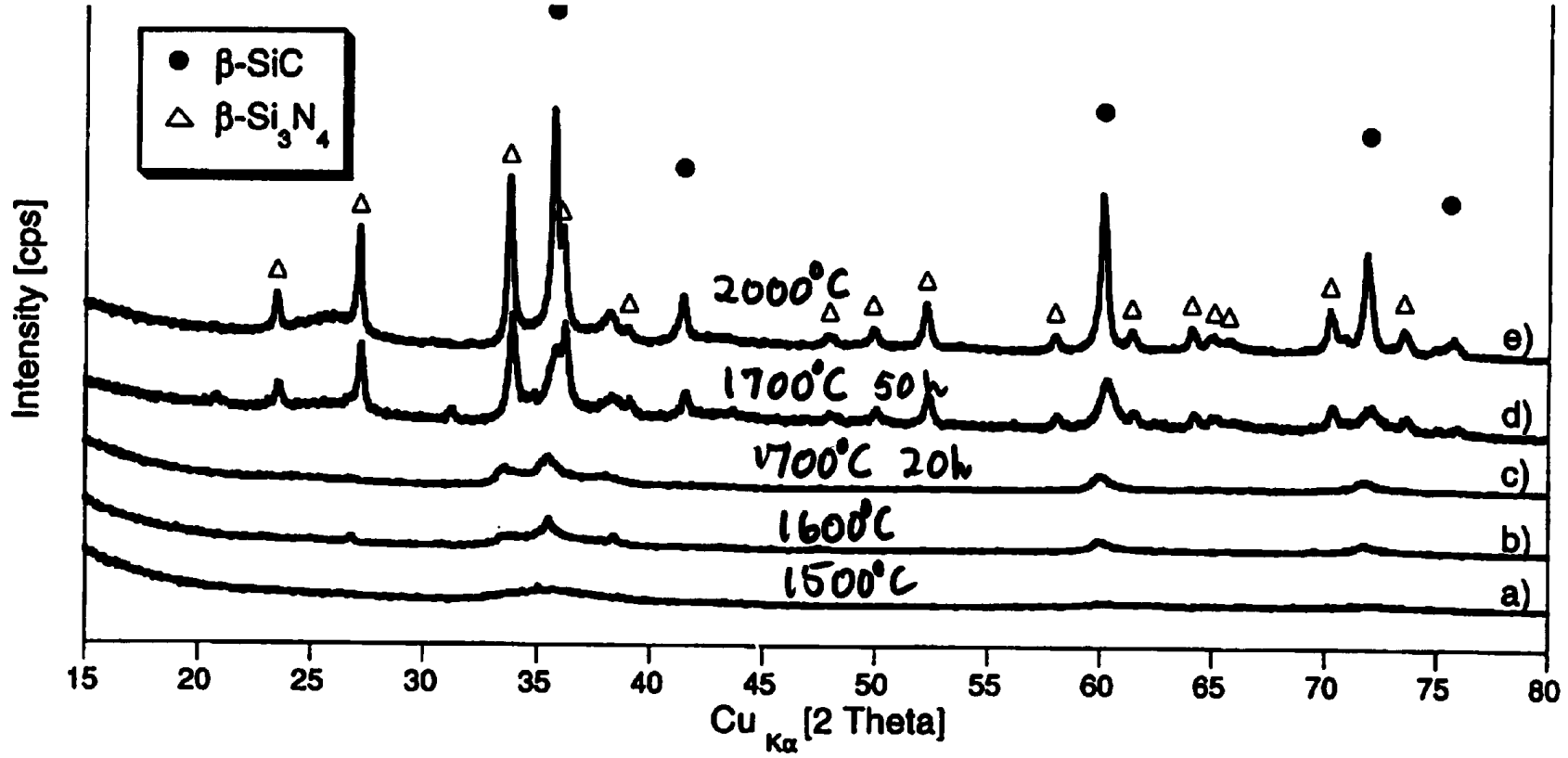
H.-J. Kleebe (CSM)

Nanostructure Stable to
 UltraHigh Temperatures
 (Extremely Low Mobility)

The Amorphous State

X-ray powder diffraction of $\text{Si}_{3.0}\text{B}_{1.0}\text{C}_{4.3}\text{N}_{2.0}$ after annealing

in nitrogen at (a) 1500°C, (b) 1600°C, (c) 1700°C for 20 hours,
and in argon (d) 1700°C for 50 hours and (e) 2000°C for 2 hours.
(Courtesy Riedel)



Properties of SiCN as compared to other materials

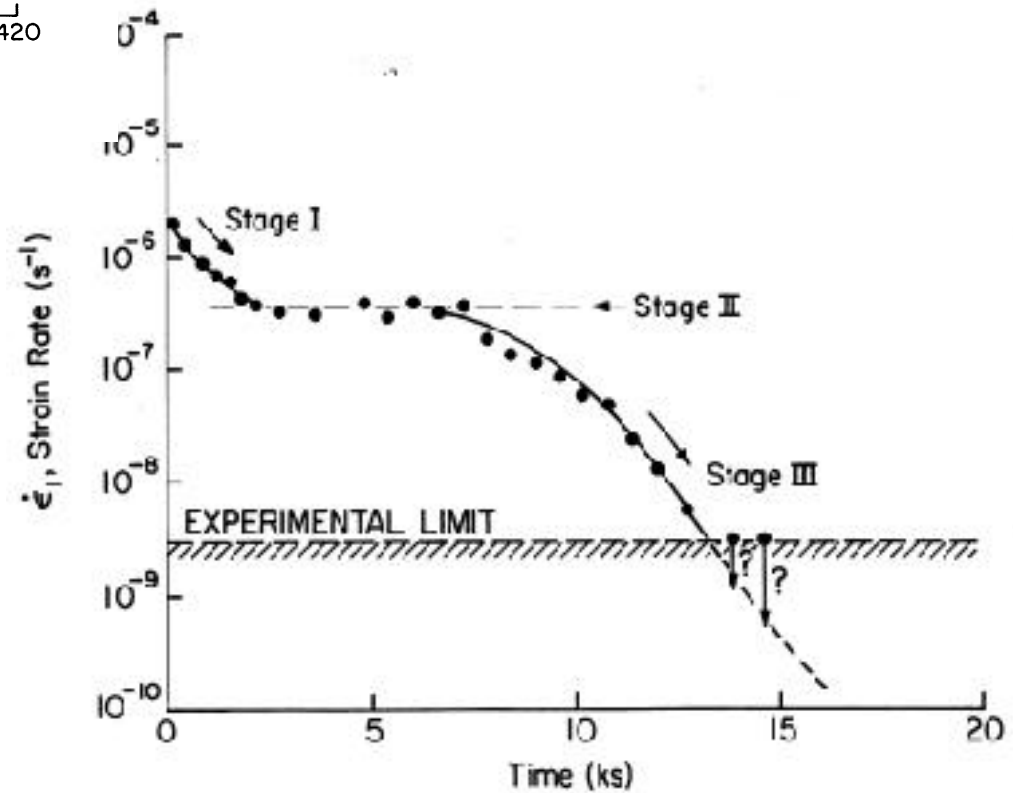
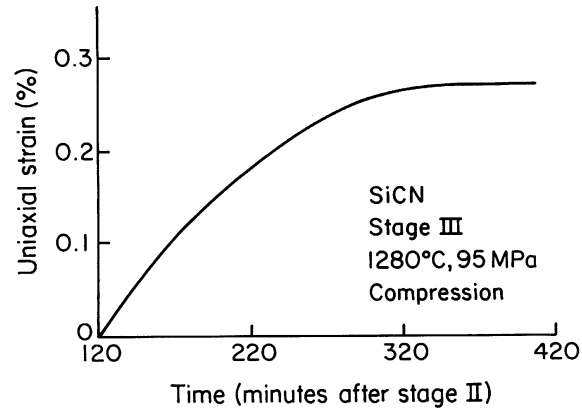
Property	SiCN	SiC	Si ₃ N ₄
Density (g/cm ³)	2.35	3.17	3.19
E Modulus (GPa)	140-170	405	314
Poisson's Ratio	0.17	0.14	0.24
CTE (x10 ⁻⁶ /K)	~ 3	3.8	2.5
Hardness (GPa)	25	30	28
Fracture Strength (MPa)	500-1200	418	700
Fracture Toughness (MPa.m ^{1/2})	3.5	4 - 6	5 - 8
Thermal Shock FOM*	1100-5000	270	890

*FOM=strength/(E-Modulus x CTE)

Creep Studies in Uniaxial Compression

Creep Rate Declines with Time

SiCN, 1350°C, 100 MPa



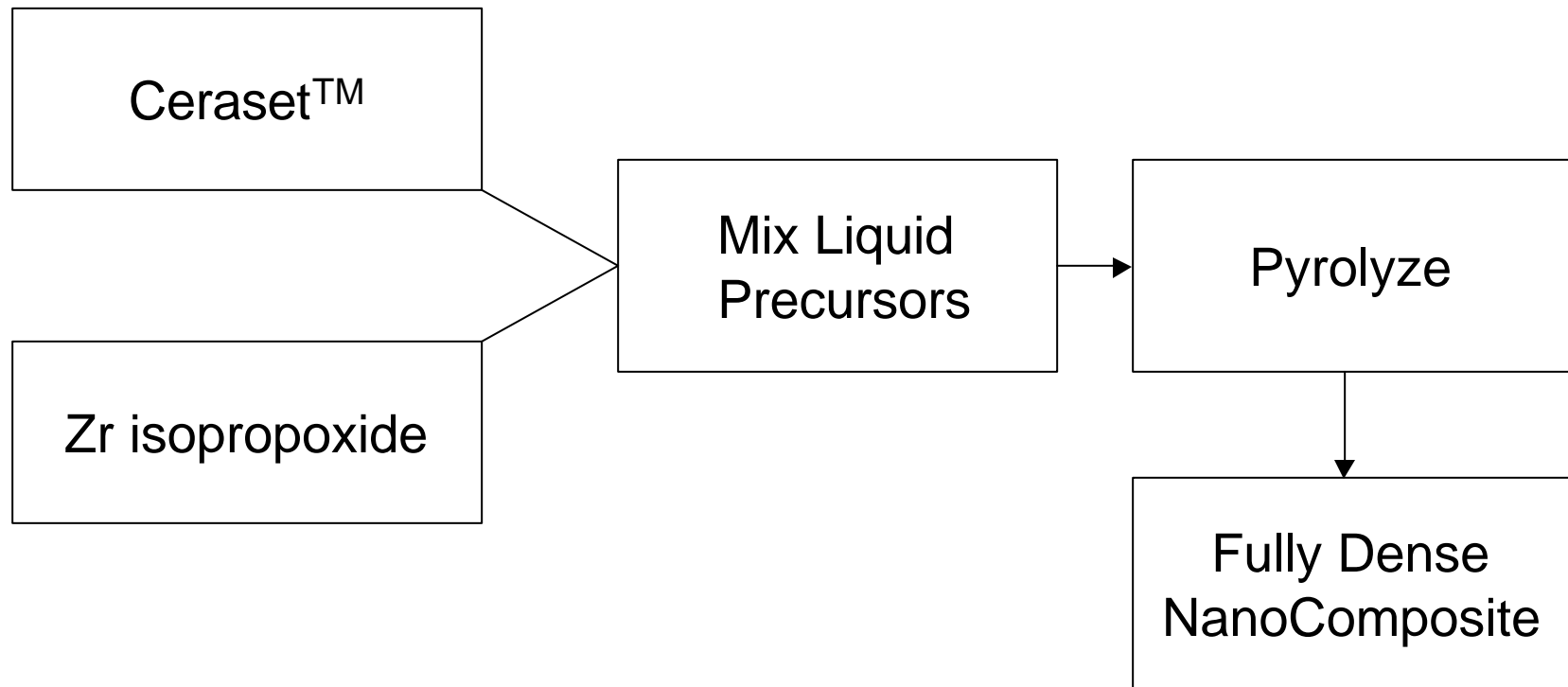
Summary of Creep Results

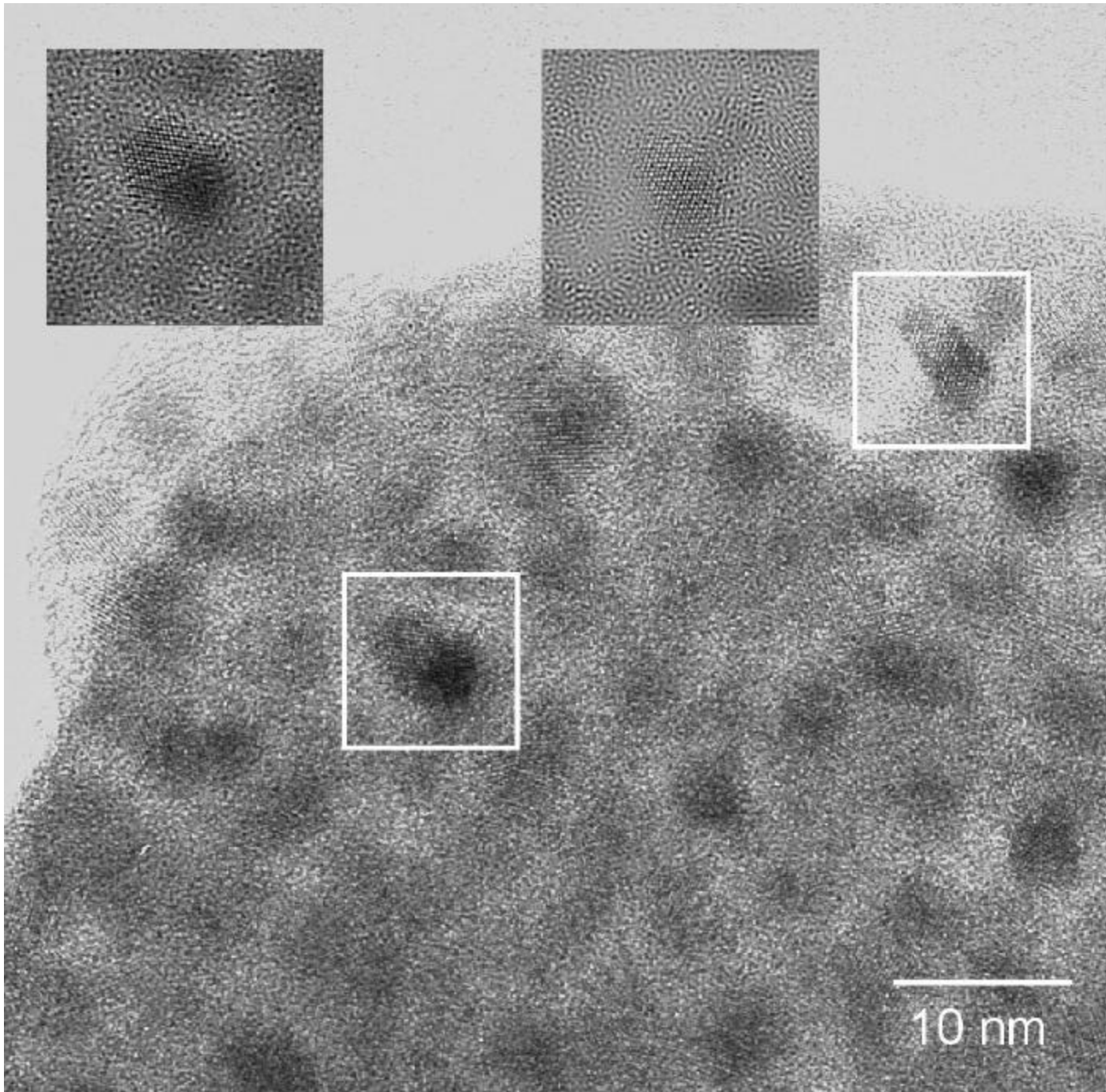
- mobile molecules are LARGE (~ 1-2 nm)
- long range diffusion extremely slow

Concepts of Creep in (silicate) Glasses and in Polycrystalline Materials are NOT Applicable

SiCN - Zirconia NanoComposites

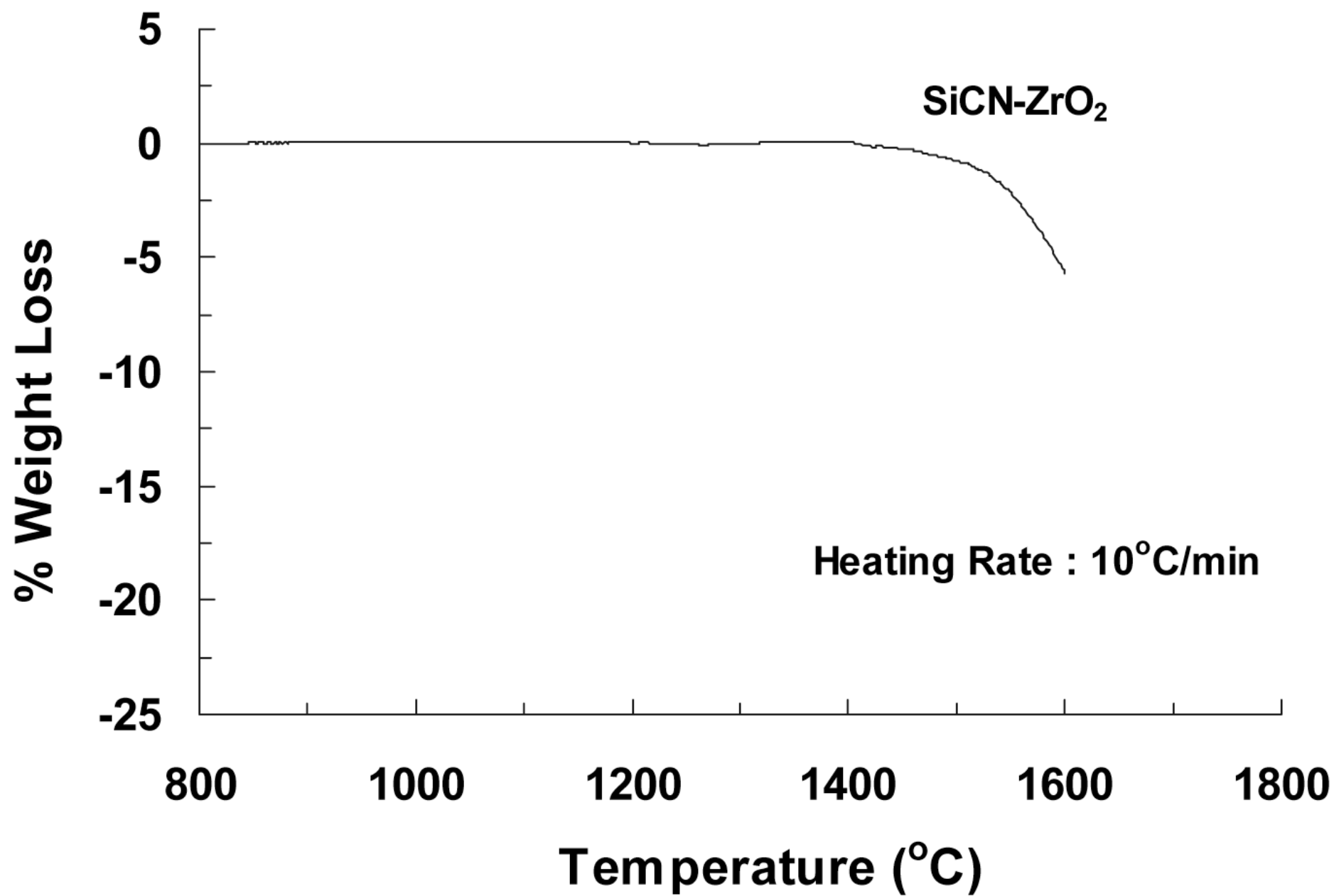
The Process





SiCN-Zirconia:

Courtesy
Kleebe



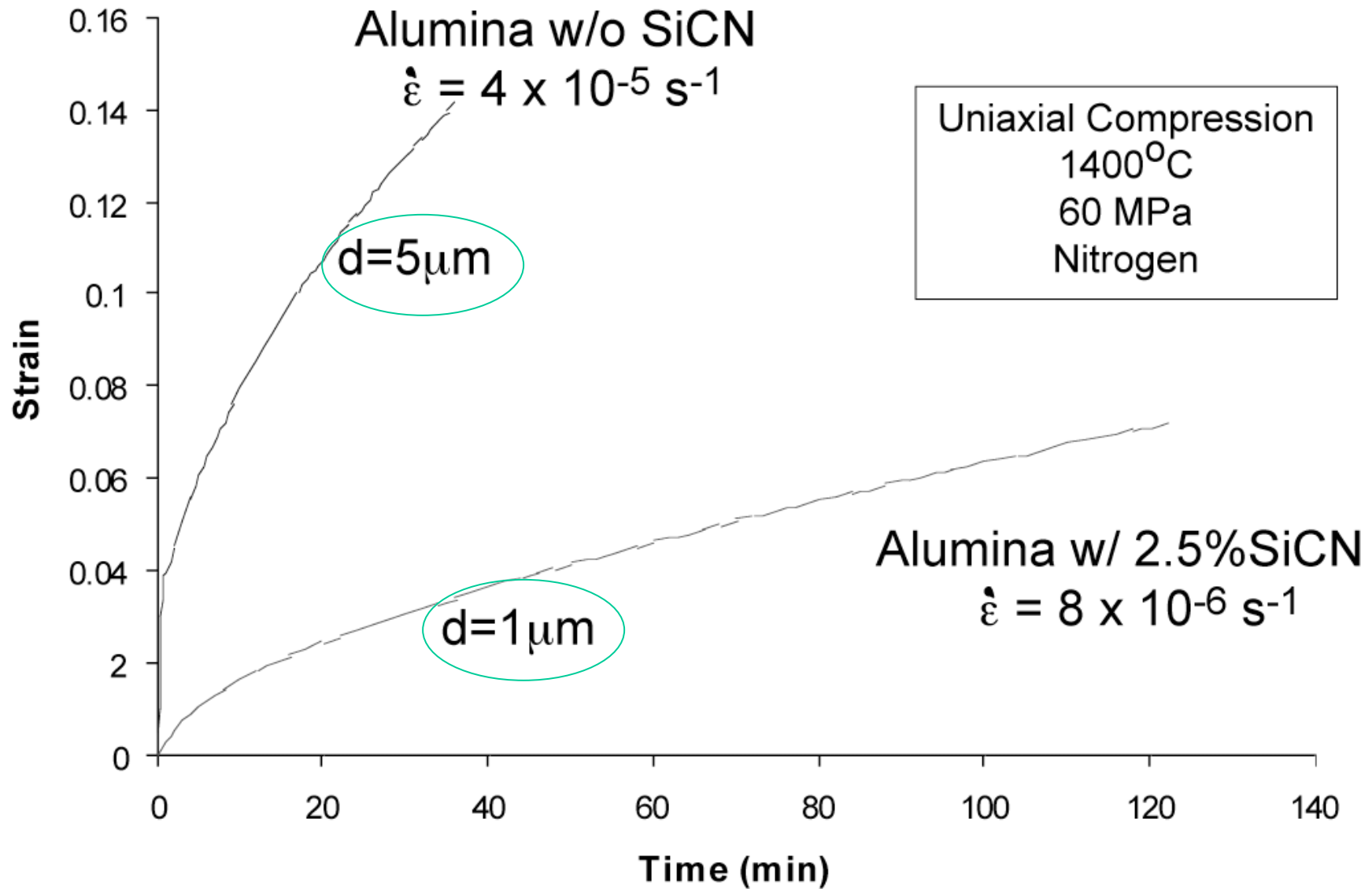
Summary of SiCN-ZrO₂ Results

- nanoscale oxide phase (will not thermal shock)
- high strength (2-3 GPa)
- thermally stable

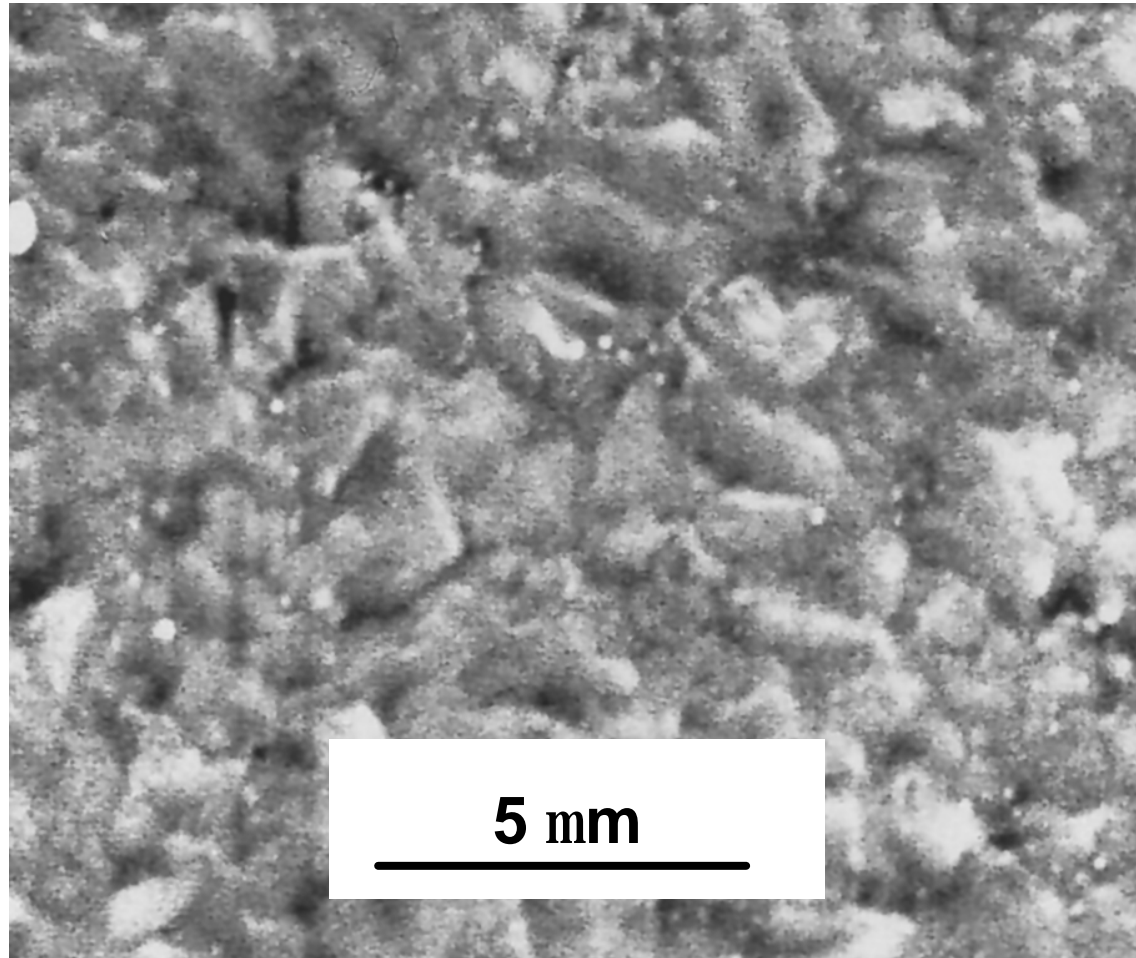
Al₂O₃ - SiCN Composites

- Al₂O₃ powder and SiCN liquid precursor-hot press
- compare grain growth w/ and w/o SiCN
- compare creep w/ and w/o SiCN

SiCN at Alumina-Grain Boundaries Reduces "d"-Normalized Creep Rate by 1/100 to 1/1000



Alumina w/ 2.5% SiCN



appearance unlike polycrystalline alumina

Preliminary Results from Al₂O₃ - SiCN Composites

- grain boundary kinetic phenomena (creep and grain growth) retarded by SiCN interfacial phase
- Al₂O₃ and SiCN form low-energy interfaces

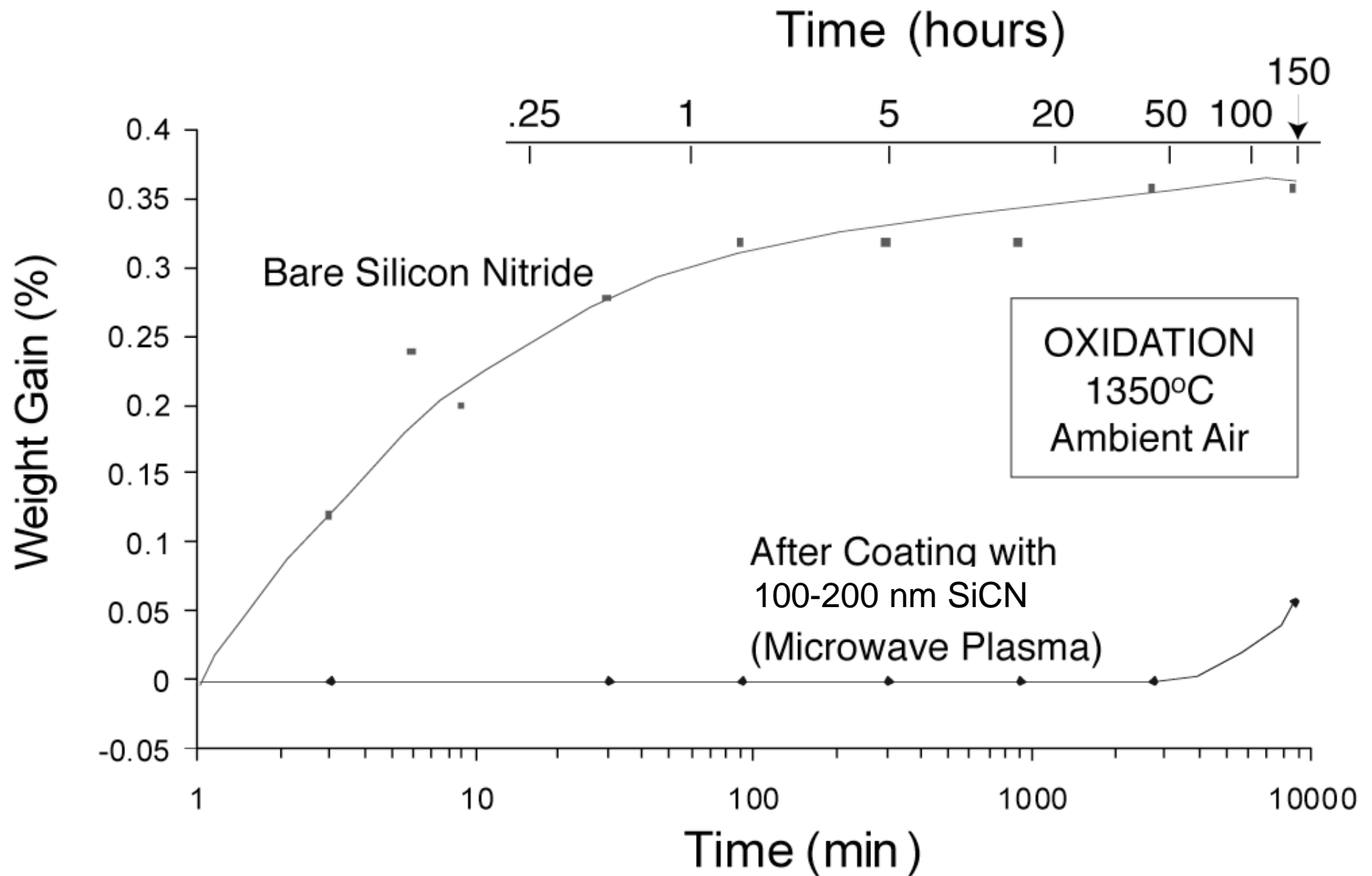
Oxides and SiCN good candidates for graded interfaces

The SiCN - Si₃N₄ Interface

Thin Film SiCN on Si₃N₄

- processed by liquid injection/microwave plasma CVD
- 0.1-0.2 μm thick film of SiCN on Si₃N₄
- compare oxidation of bare and coated Si₃N₄

Oxidation Protection from SiCN Thin-Films on Silicon-Nitride



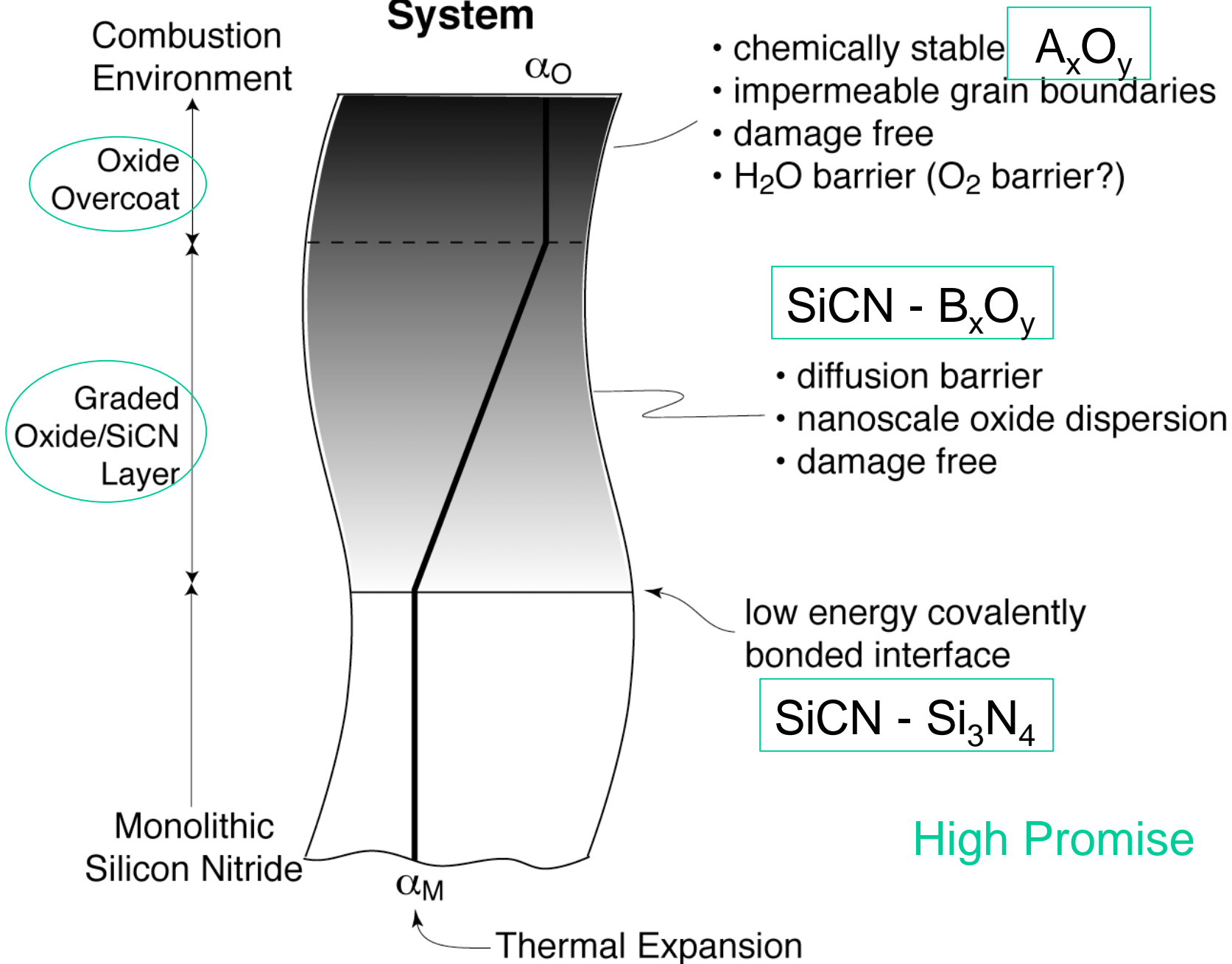
Summary of Results:

- good bonding of film to substrate
(SiO_2 cannot nucleate at the $\text{SiCN}/\text{Si}_3\text{N}_4$ interface)

or

- SiCN effective as oxygen diffusion barrier

The EBC System

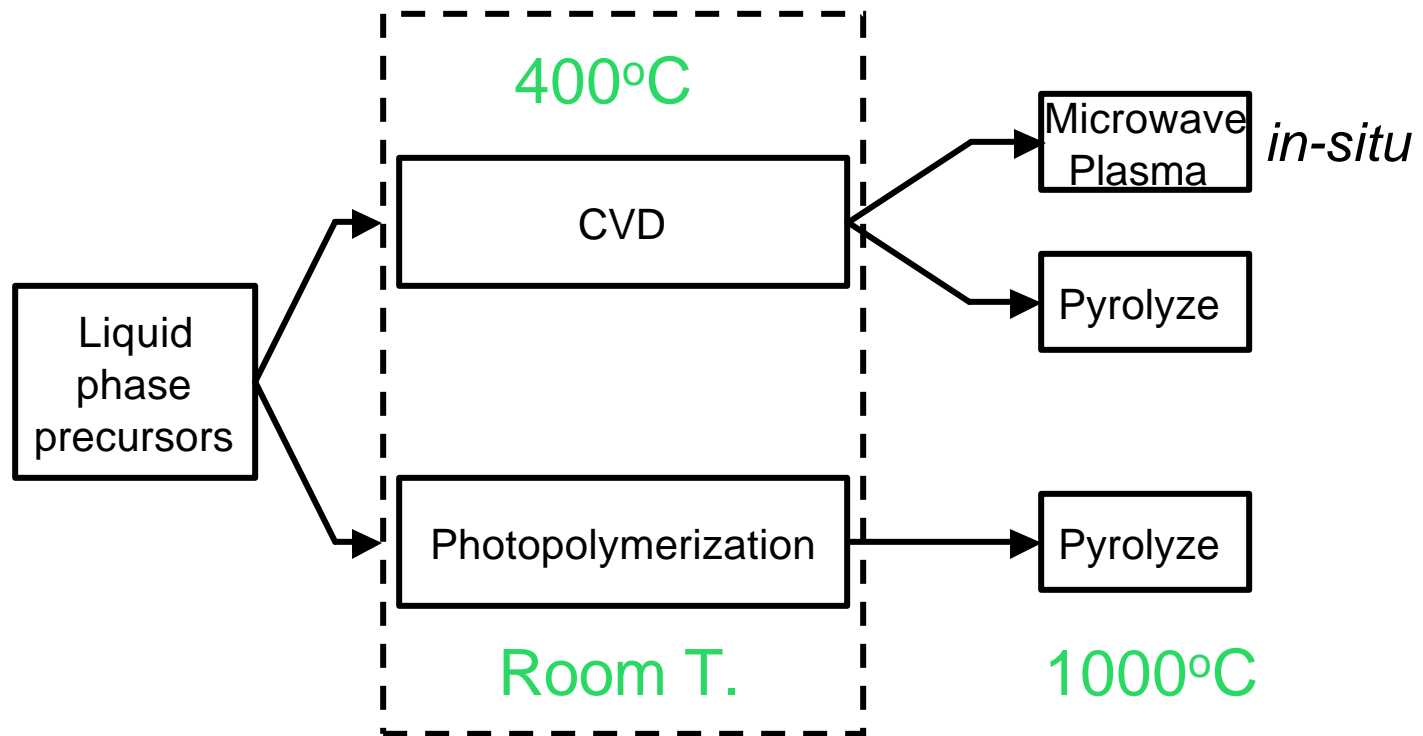


What are the basic research issues?

Objective: Suppress Volatilization (prevent silica growth)

- **The surface oxide-overlayer** - damage free? -chemically stable? - diffusion barrier?
- **The oxide/SiCN *interface*** - prevents nucleation of silica?
- **The graded PDC/oxide interlayer** - damage free? -immune to thermal shock? - effective diffusion barrier? - PDC & oxide phase equilibria?
- **The SiCN/Si₃N₄ *interface*** - prevents nucleation of silica? - not attacked by the sintering additives?
- Processing - graded construction? - step coverage? - low cost?

the graded PDC coating process



**Liquid
Precursor**

**Polymer
Films**

**Ultrahigh T.
Coatings**