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Polymer Derived EBCs for Protecting Si_3N_4 in Gas Turbine Environments

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THE PROBLEM

Silicon Nitride Vanes

1066°C-1260°C; 8.9 atm, p_{H2O} = 0.101

162m/s to 573 m/sec

• 27% of cross section lost in 1818 h

recession and mechanical degradation

Si₃N₄ grains are oxidizing and then volatilizing

"Evaluation of Mechanical Reliability of Silicon Nitride Vanes after Field Tests in an Industrial Gas Turbine" Liu, Ferber, Westphal and Macri(ORNL report - I assume)

<u>A Tenet</u>

silica passivation mechanism for oxidation protection is not viable for the exposed surfaces of Si_3N_4 vanes and blades in humid combustion environment

Opila et al. (JACerS)

Design Elements of EBCs

- oxide overlayer: for chemically stable
- graded interface: prevent thermal shock
- diffusion barrier: for oxygen
- *interfaces*: as nucleation barriers to silica



Materials Selection (Oxide Overlayer)

- Transition Metal Oxides (ZrO₂, HfO₂, Ta₂O₅, TiO₂)
- Base Metal Oxides (Al₂O₃, MgO etc.)
- Complex Oxides (YAG, Perovskites, etc.)
- Silicates (Mullite, etc.)

simple oxides are process friendly more likely to be implemented Materials Selection (Bond Layer)

Why PDCs (silicon carbonitride-SiCN)?

- apparently compatible with oxides
- apparently ultra-slow diffusion at ultrahigh temperatures
- reasonable processing experience at Colorado

PDCs (silicon carbonitride-SiCN)?

Missing Science

apparently compatible with oxides

the nature of oxide-SiCN interface not known

• apparently ultra-slow diffusion at ultrahigh temperatures

information is phenomenological not mechanistic

• reasonable processing experience at Colorado

structure of SiCN (and how it relates to process) not known

Where we are and where we are going?

Current Knowledge:

- ultralow diffusivity suggested by resistance to creep and crystallization
- emerging evidence of compatibility with oxides
- emerging knowledge of the fundamental unit of SiCN-SiCO structure

Research Plan:

• ABC* composites to evaluate interfacial reactions after exposure to Keiser Rig - comprehensive evaluation *and* modeling

evaluate thermal shock in ABC composites

*SiCN-Oxide-Si₃N₄ composites

Composition Diagram for SiCN



Silicon Carbonitride (SiCN)

H.-J. Kleebe (CSM)

Wt. Loss at Hi Temperatures

Courtesy: Riedel

Resistance to Crystallization

Summary of Creep Results

- mobile molecules are LARGE (~ 1-2 nm)
- long range diffusion extremely slow

Concepts of Creep in (silicate) Glasses and in Polycrystalline Materials are NOT Applicable crystallization and creep studies show that self diffusivity in SiCN is extremely slow

what is the structural origin? - cannot be explained by diffusion in "glass"

SiCN apparently has a NanoDomain structure which remains intact up to ultrahigh temperatures Schempp, Duerr, Lamparter, Bill and Aldinger (1998):

The Size of NanoDomains from SAXS+SANS

Structure of the NanoDomains?

Two Types of Structures May be Conceptualized

"domain size is controlled by the number of Si-O-C bonds"

Higher Carbon Decreases the Domain Size: Type II

Since the domain size increases with lower carbon (or higher oxygen) the Type II structure is accepted

inference: carbon walls prevent diffusion

Emerging Picture of the Structural Unit in SiCN

a carbon cage structure with sequestered nanodomains of silica or silicon nitride which are unable to coarsen by diffusion, and are too small to nucleate crystals SiCN - Zirconia NanoComposites

SiCN-Zirconia:

Courtesy Kleebe

Oxidation Study of SiCN-ZrO₂

theme: modeling!

Phenomenology:
$$h^2 = k_{xp}t$$
 $k_p = C.k_{xp}$

Reaction is Composition Dependent:

$$SiC_x N_y O_z + (1 + \frac{x}{2} - \frac{z}{2}) O_2 = SiO_2 + xCO + \frac{y}{2}N_2$$
 $\alpha = (1 + \frac{x}{2} - \frac{z}{2})$

Mass Balance and Geometry:

$$V_{OX} = V_{SiO_2} + n_{Zr} \cdot V_{ZrO_2} \qquad \qquad \frac{dh}{dt} = J_{O_2} \cdot \frac{V_{SiO_2} + n_{Zr} \cdot V_{ZrO_2}}{\alpha}$$

Flux Equation:
$$J_{O_2} = \frac{D_{O_2}}{V_{SiO_2}RT} \cdot \frac{\Delta \mu_{O_2}}{h} \cdot \frac{1}{\alpha} \cdot (1 + n_{Zr} \frac{V_{ZrO_2}}{V_{SiO_2}}) \cdot t$$

Final Result:
$$h^2 = \frac{D_{O_2} \cdot \Delta \mu_{O_2}}{RT} \cdot \frac{1}{\alpha} \cdot (1 + n_{Zr} \frac{V_{ZrO_2}}{V_{SiO_2}}) \cdot t$$
$$k_p = \frac{D_{O_2} \cdot \Delta \mu_{O_2}}{RT}$$

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More on the compatibility of Oxides and Non-Oxides in PDC structures.

Influence of 1-5% Silica Flux on Creep Behavior of <u>Polycrystalline</u> Silicon Nitride

OSBORNE, PROC. BRITISH CERAMIC SOC. #25, 1975.

SiCN can tolerate high oxygen content without degradation of HT properties.

Intensity

The Approach

Phase I

The detailed study of ABC composites will provide scientific knowledge of the interface reactions, rate of propagation of the oxidation front (in the Keiser Rig), and the thermal shock behavior.

Basic research issues which will be addressed by the ABC composites.

- Diffusivity study progression of the oxidation overgrowth.
- Thermal Shock study damage as a function of particle size and the three kinds of interfaces (AB, BC and AC).
- Subsurface Nucleation of Silica study nucleation a oxide/SiCN and SiCN/Si₃N₄ interfaces.

Merits of PDC based EBCs

- Low Diffusivity
- Compatibility of SiCN with Oxides

Properties of SiCN as compared to other materials			
Property	SiCN	SiC	Si ₃ N ₄
Density (g/cm ³)	2.35	3.17	3.19
E Modulus (GPa)	140-170	405	314
Poisson's Ratio	0.17	0.14	0.24
CTE (x10-6/K)	~ 3	3.8	2.5
Hardness (GPa)	25	30	28
Fracture Strength (MPa)	500-1200	418	700
Fracture Toughness (MPa.m1/2)	3.5	4 -6	5 - 8
Thermal Shock FOM*	1100-5000	270	890

*FOM=strength/(E-Modulus x CTE)