



Applications for Si₃N₄ in Turbine Engines and Issues for EBCs Within Them

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Outline

- Overview of potential markets for small gas turbine engine products, UTC product applications, and customer value propositions
- Opportunities and technology requirements
- Engine and ceramic component requirements
- EBC Issues for each major component class



UTC Engine Applications – Axial Configuration Machines



Industrial Gas Turbines



 Ceramics enable increased efficiency and reduced emissions



- UTC has several potential gas turbine engine applications that could employ ceramic turbine components for enhanced customer value
- Primary value achieved through higher efficiency and weight reduction
- Potential value is significant



UTC Engine Applications – Radial Configuration Machines

 Engine Tested With Ceramic Nozzle and Rotor from Kyocera --Operation at T4=2300F Successful



TJ-50 Expendable Turbojet





Applications - Summary

- The potential market for gas turbine engine products incorporating ceramic turbine components is substantial
 - Ceramic turbine technology creates a strong customer value proposition
 - For UTC, significant opportunity exists for CHP, UAV, APU, and IGT products incorporating ceramic turbine technology
- Common technology requirements across diverse range of products encourages an integrated ceramic turbine technology plan to maximize leverage
- Integrated plan has been constructed to reduce critical risks for ceramic turbine technology to TRL 6 by 2006



Ceramic HPT components to be demonstrated in gas generator



Ceramic integrally bladed rotor (IBR), one-piece vane ring, and turbine shroud HPT components are common across UTC small gas turbine engines



Microturbine Component Fabrication Progress

ST5+ Integral vane rings produced by Kyocera USA at high yield/minimal cost

- Integral vane rings address intervane sealing issues w/singlets
- Significantly reduced diamond grinding cost through slash angle elimination
- Acceptable tolerance control achieved via isopress/bisque machining method



Initial Kyocera fabrication trial yields 2 out of 3 engine quality parts, 8.5 inch OD



Small Gas Turbine Engine Duty Cycles Vary Considerably



Engine duty cycle plays key role in determining EBC requirement



Small Gas Turbine Engine Component Requirements

	Vane Ring			IBR			Turbine Shroud		
Characteristic	UAV Engine	APU	Micro- turbine	UAV Engine	APU	Micro- turbine	UAV Engine	APU	Micro- turbine
Max Temperature (F)	> 2200F	> 2100F	> 2000F	1900-2200F	1800-2100F	1700-2000F	2100-2400F	2100F	~2000F
Pressure at Entrance	> 12	> 7	> 6	8 to 10	4 to 6	4 to 5	8 to 10	4 to 6	4 to 5
Life	5,000 hrs	12,000 hrs	30,000 hrs	5,000 hrs	12,000 hrs	30,000 hrs	5,000 hrs	12,000 hrs	30,000 hrs
EBC Required? (Y, N)	Y	Y	Y	TBD	Marginal	Y	Y	Y	Y

Recession Rate
$$\propto \frac{V^{1/2} \bullet P_{H2O}^2}{P_{total}^{1/2}} \bullet e^{-1/KT}$$

- Current application requirements will challenge the limits of current ceramic materials and process technology
- EBC's will be required for all static structures and some IBR components



Recession is effected by pressure, temperature and velocity

Recession rate (um/hr) =
$$\frac{512 \exp(-111000/(8.314 * T) * v^{\frac{1}{2}} * P_{H2O}^2}{P_{total}^{\frac{1}{2}}}$$

WhereT = temperature in Kelvinv = velocity, m/sP = water vapor and total pressure in atmospheres

After M. Ferber, et al. adaptation of NASA/J. Smialek equation for silicon based ceramic recession



Pressure, Velocity and Temperature vary through the turbine stage(s)

Vanes – Stationary reference frame





Blades – Rotating reference frame

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Pressure, Velocity and Temperature vary through the turbine stage(s)



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Pressure, Velocity and Temperature vary through the turbine stage(s)

• Velocity changes & Work Extraction drop pressures

Static Pressure

< 3 Atm.



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> 7 Atm.

Blade material temperatures effected by tip to shroud aerodynamics



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Material recession predicted using temperature, pressure and local velocity





Blade tip recession not seen on Allison tested AGT5 rotor blades



1000 hour AGT5 rotor Photographs courtesy Rolls Royce/Allison ~ 250 hour AGT5 rotor



Possible blade tip/leading edge recession in Solar 100 hour test



As Received AS800 Blade

AS800 Blade after 100 hour test

10x photographs courtesy Mattison Ferber, ORNL



Blade/tip issues a concern for EBC developers

- Turbine tip shrouds (BOAS) will require EBC's due to high temperature hot streaks from the combustor
- Shroud coatings will likely need to be abradable
 - GE showed BSAS based EBC's can abrade during a CMC shroud/metal blade 2MW engine test
 - What environmentally safe grit tips are available?
- Blade tip leading edge a concern, might burn away to a "safe" geometry, not yet analyzed
 - "revised through removal" aerodynamics may continue to promote high heat transfer and further tip loss
 - Effects of enlarged tip clearances significant for small turbine engines



Conclusions

- A broad base of potential applications exist for monolithic ceramics in turbine engines of the future
- P, T & V all change rapidly throughout the turbine hot section, and these changes effect needs/requirements for EBC's
- Local areas of high heat transfer can significantly promote recession
- Blade tip and shroud regions both present unique requirements for the EBC developer
- A systems approach Base material as well as EBCs, are required to meet goals (particularly for blades/rotors)

