Coatings for Si3N4 and SiC Ceramics: an Historical Perspective

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Presentation Outline

 Background
 Approaches to Environmental Corrosion
 Recommendations

Advanced Gas Turbines Provide a Material Challenges

- High Temperatures: 1900 to 2500F
- High and Cyclical Stresses: thermal and mechanical
- High Velocity Gases: approaching (exceeding) Mach 1
- High Pressures: ~ 4 to 10 atmospheres (for small turbines)
- Exposure to combustion products
- Combined Temperature, Pressure, Velocity, & Atmosphere which accelerate the detrimental
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Microturbine Requirements Identified Microturbine Peer review, 2002]

OEM	Max	Pressur	Life Goal, hrs
	Temp, F	e, Atm	Overhaul/
GE	2130	4.2	Service
Capstone	2100	4.1	8000 - 11,000/
UTRC [Shi, 2002]	2200	8	45,000 - 80,000
IR	1902	4.8	

Advanced Si₃N₄ Show Significant

creap and oxidation resistance have improved with improved compositions

- Available in gas pressure sintered complex shapes
- Decreasing ionic radius of RE increases oxidation resistance [Cinibulk, 1992]
- Single additive system: reduced oxidation, e.g.., SN282, Lu₂O₃. low Lu ion content glass, oxide growth : 0.004 μm²/hr @ 1400C [Klemm, 2001a]

• Multiple additives system: from S. M. increased oxygen diffusion , e.g., AS800, $Y_2O_3 + La_2O_3 + SrO$, high ion content glass, growth rate 0.4 $\mu m^2/hr$ @ 1400C [Klemm, 2001a]



from S. M. Wiederhorn and M. K. Ferber

Today's Ceramics Are Not Adequate

- Vulnerability to Impact Damage
 - Air Research DARPA program [Richerson et al, 1982b]
 - Allied Signal AGT101 program [Boyd & Kreiner, 1987]
 - Solar Centaur 50S [van Roode et al, 1997]
- Poor resistance to water vapor and oxidation under advanced gas turbine conditions
 - Simulated Engine conditions [Smialek et al, 1999, & Schenk et al, 2001]
 - Allison 501K Engine conditions [Lin et al, 2001]

Environmental Resistance is Major Challenge Water vapor degrades silicon SiC and Si₃N₄ recession under combustor conditions

 H₂O enhances transport of impurities from the atmosphere to the surface

based ceramics

- Increases oxidation rate of silica-formers: Relative to O_2 , H_2O diffusion is ~1/10th, but solubility is ~1000x. Results in bubble formation
- SiO₂ layer volatized by water vapor: SiO₂ + H₂O
 Si(OH)x + SiO



Smialek, et al, Adv Comp Mater, 1999

Unprotected Oxidation Leads to



Smialek, et al, Adv Comp Mater, 1999

Advanced Si₃N₄s are Vulnerable to Recession

•SN282 •AS800 •AS950 •Si₃N4/MoSi2 +Y or Yb

• All recessed at .24 to .6 mg/cm2/hr in a combustion environment, 1400C, 5 bar

[Klemm, 2001a; Schenk et al, ASME 2001-GT-459]



Microturbine Conditions Require EBC Protection



Schenk, et al, 2001

Providing Environmental Resistance is Challenging

- Self healing SiO₂ not effective against water vapor
- Transport in SiO₂ is affected more by low level impurities than Al₂O₃ and Cr₂O₃ [Pareek et al, 1991, Zheng et al, 1992]
- Additives or impurities in surface layers increase oxidation rates, oxygen diffusion rate, change the rate controlling mechanism, and alter the oxide scale structure [Opila et al, 2000]
- Even with low oxygen diffusion coatings, silica will form under coatings
- Si₃N₄ & SiO₂ have low CTE: CTE mismatch leads to interface cracks & debonding

Surface treatments to enhance adherence may

Requirements for Environmental

- Protection Environmental Durability in a hot gas environment
 - Oxidation resistance, low oxygen permeability
 - Resistance to Water vapor
 - Stability against hot gas constituents
 - Low volatility
 - > 10,000 hour life
 - Resistant to erosion, impact
 - Chemical compatibility with SiO₂ that will form on substrate
 - Stable microstructure & phases grain size, porosity, non sintering or cracking
 - Thermal expansion compatibility
 - Must survive cyclic exposure Dave Carruthers and Associates
 Prefer a low elastic modulus

Solutions to Corrosion Must Not Conflict with Other Needs for Ceramics

- Reliability
 - High Fracture toughness w/ low scatter
 - Resistance to slow crack growth and creep
 - Oxidation, corrosion resistance
 - Impact resistance
- Formability
 - Complex, thick and thin shapes
 - Stringent dimensional control
 - Smooth aerodynamic surfaces
- Sinterability w/o expensive HIP processing
- Inspectability
- Affordability

All needs must be achieve for success

Approaches to Protection

 Atmosphere control: minimize formation of corrosive species
 Alloy improvements

 In situ or Self Generating protective surface layer

 Protective Coatings

Corrosion (Oxidation) Challenge of C-C, C-SiC, SiC-SiC Vulnerability to attack of fibers, interfaces or matrices via cracks from CTE mismatch and strain cracks.

Approaches:

- Surface coatings: Si₃N₄ and SiC identified as good candidates [Strife et al, 1988]
- Glass forming compounds containing Si, B, Hf, Cr, Ti [Boullion, et al, 2002, Joshi et al, 1996]
- Y₂SiO₅ low CTE, plasma sprayed with YSi_X intermediate layer survived 1 hr at 1800C on C/C
 [Ogura, et al,1995] Spalled in 7 cycles to 1700C [Ogura, et al, 2001]

Self Generating Protection

is Attractive

 Use additives that produce or self repair oxide coating with H₂O resistance.

May not add expensive steps to processing

- Combustion results with Yb₂O₃ sintering additive [Klemm, 2001a]
 - Exposure removed SiO_2 , but left a $Yb_2Si_2O_7$ layer
 - Disilicates has a higher chemical stability, but spalled (CTE $\sim 5 \times 10^{-6}$ /C,

 Combustion results, Yb₂O₃ as sintering additive and disilicate EBC [Klemm, 2001a]

- Homogenious, crack free E- beam coating obtained
- Exposure resulted in cracks from SiO₂ crystallization
- SiO₂ below the EBG was protected, recession

MoSi₂, SiC_p in Si₃N₄ Influence the Oxidation Process

- Both composites form Si₂N₂O interlayer below SiO₂ surface [Klemm, 1997]
 - Si₂N₂O beneath SiO₂ in pure Si₃N₄ is responsible for lower oxidation rate for Si₃N₄ than SiC [Du et al, 1989a, Ogbuji & Opila, 1995]
 - Si₂N₂O has a low oxygen diffusion [Du et al 1989b, Tressler, 1990]
 - Si₂N₂O has good oxidation resistance and high temperature strength (~600 800 MPa) [Park, D. S. et al, 2002; Ohashi et al]

- Si₂N₂O reduces cation driving force to the surface

MoSi₂ phase may provide high temperature ductile-phase

Early Environmental Coatings Addressed Corrosion

Solar study for RB SiC & SiC. [Price et al, 1994]
Plasma sprayed mullite, graded mullite, cordierite, zircon, alumina, yttria, chromia, hafnia, and YSZ
Plasma spraying, 5-15% porosity typical
Best corrosion resistance/adherence to 1204C: Single layer mullite Graded mullite to Al₂O₃ Graded mullite to Y
Best results for mullite adherence with surface prep: 1) SiC particles brazed to surface, or 2) proprietary etching: implies mechanical bond

Surface treatment degraded the strength, but coating restored it
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Alternate Approaches Evaluated

- Slurry coatings containing mullites: cracked in thermal exposure [Federer, '98, '90]
- CVD Ta₂O₅ stable to 1000C, but reactive with Na₂SO₄ [Lee, W.Y. et al, 1995]
- Fully crystallized PS mullite adhered to 1200 hr up to 1300C, still cracks [Lee, K.N. et al, 1995]
- CVD Mullite developed [Mulpuri, R.P et al, 1996]
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 CVD crystalling mullite on SiC provided

Coating Development Continued [Lee, K.N. 2000a, 2002b, 2000c]

- In the 90's, focus shifted to silicon volatility in water vapor:
 - SiC surface roughened by Na₂CO₃ etching for adherence
 - PS mullite lost silica during exposure, high silicon activity(0.3-.04)
 - Mullite w/YSZ top coat suppressed SiO₂ volatization, but H₂O penetrated cracks

Lessons learned:

- PS Mullite bond primarily mechanical, weak,
- Residual amorphous mullite and alumina, impurities resulted in phase instability/shrinkage/cracks
- CTE mismatch (5.6 vs 4.7 ppm/C for mullite and SiC) stresses resulted in the racking point of the stresses resulted in the racking point of the stresses resulted in the racking point of the stresses resulted by the stresses resulted

Modified Mullite System Improves EBC on SiC

- ELESAS attractive alpoint E2002on silica activity (<0.1), crack sealing capability. [Lee,2002a], but reacts with silica
- MoSi₂ /Mullite + BSAS / BSAS delayed onset of accelerated oxidation in water vapor [Lee et al, 2000c; Lee, et al, in press]
- Si found to be excellent bond coat for mullite on SiC
- Si reacts with BSAS, so mullite or mullite + BSAS used as intermediate layer
- Initially mullite+BSAS intermediate layer preferred due to difficulty in achieving crack free mullite
- Both mullite and mullite +BSAS intermediate systems provided ~14,000 hours on SiC/SiC in engine; some EBC volatility & spalling observed [Eaton et al, 2001]
- Long term temperature limit ~1200C, adherence

UTRC Showing EBC Progress on Si₃N₄ Sisi, Nt, al CTEO205 match increase of 1.5 ppm/C from SiC

- EBC on Si₃N₄ FT8 vane: 31 hours/ 15 atm/ 1200 to 1230C/ max velocity ~.7 M: No spalling, strong bond, protected substrate
- 1204C / 2000 hr Keiser rig exposure shows protection on SN, but CTE cracks will reduce long term effectiveness
- At 1350C, Si bond coat oxidizes, Eutectic in BSAS/SiO₂ system estimated at 1350C. Could last few 1000 hours
- BSAS/mullite--B SAS interface stable for 500 hours in 1450C steam Dave Carruthers and Associates
 - System temp capability can be increased by

NASA Focusing on EBC's for SiC/SiC

 Focusing on 1482C (2700F) use temperature, 166C (300F) temperature drop through coating • Currently identifying temperature limit for Si/mullite/BSAS + YSZ systems Si/Mullite EBC crack, provide water vapor path BSAS recession significant above 1400C [Lee et al, in press] • Mullite an effective chemical barrier between mullite + BSAS and YSZ to 1500C Si/Mullite + BSAS/graded_mullite+YSZ/YSZ

Challenges Remain for Si-Mullite-BSAS EBC [Lee, 2002b; Sun et al,

- 2000 Juniform coating thickness, Si porosity on non lineof-sight areas "Smoothing" observed on BSAS topcoat after engine exposure: erosion possible
- Long term stability of multi-component system on multiconstituent Si₃N₄ unknown
- Sintering aids may influence stability of Si bond coat
- Surface treatments to enhance adherence of bond coat often degrade substrate or strength
- 500-750 um thickness
- Implications of slow hexagonal to monoclinic celsian conversion are unknown, particularly for high temperature applications
- Potentially vulnerable to erosion in high velocity areas
 Durability demonstration of BSAS EBC on SN for long term is needed Dave Carruthers and Associates

Critical to optimize the costing for CTT match and

Disilicates Offer Low Oxidation Rates



RE Disilicates show parabolic weight loss in oxidation

Er, Yb show lowest oxidation rate

[Cinibulk, et al, 1992]

Disilicate CTE related to Ionic Radius



Fig. 11. The relationship between CTE and ion radius of lanthanide.

CTE tailoring may be possible with blended RE disilicates

Morimoto, et al, 1995

Disilicate Coating Shows

Promise



 Candidates experimentally screened for water vapor resistance & CTE

- Yb₂Si₂O₇, and Lu₂Si₂O₇ did not lose weight after 15 atm saturated water vapor pressure @ 200C
- Yb2Si2O7 has best @ 是 match with Si3N4 [Fukudome et al]

Yb₂Si₂O₇ Continues to Show Promise

- Yb₂Si₂O₇ Coated SN282 did not cracking or show crystal structure change in cyclic exposure + 20 hr burner rig exposure
- Engine components coated by slurry, ~30µm thick
- Turbine nozzles and combustor liner coated, to be tested in 2002

Y_xSiO_v offers Tailorable CTEs





Ogura, et al, 1999

Lessons Learned for Coatings on Si_3N_4 Leppication methods

 Plasma spray: layered, porous microstructure, strain tolerant, cost effective, scale-up capability, wide use, non uniform thickness, line of sight application.

Key Issues must be economical, and applicable to small, complex shapes

• CTE mismatch is a significant concern.

 Mechanical bonds are typically weak, especially when CTE mismatch is large. Mechanical bonding to rougher surfaces improves adherence but may reduce strength of

Lessons cont'd

- Low modulus systems help, e.g.. BSAS, mullite + BSAS
- Si, and possibly MoSi₂, are beneficial bond coatings
- During combustion atmosphere exposures, sintering additives can remain and concentrate on the surface, providing a possible means o developing a protective surface oxide
- Phase changes, such as amorphous to crystalline, can be problematic.
- Systematic, continuous improvement approach such as NASA & UTRC appears to be fruitful
- Disilicates, which are compatible with substrates,

Lessons cont'd

A successful coating will require:

- A chemical bond to provide good adherence to SiO₂
- A CTE match or low modulus for strain tolerance
- A top coating for water vapor resistance
 A TBC for higher temperature applications
- These requirements may be met in a single or multiple layer coating.

Cyclic Testing has not been adequately Addressed [He et al]

- Thermally grown oxides often develop at substrate-coating interface during high temperature exposure
- Growth strains may relax at high temperatures.
- Upon cool down, other components of the coating may yield with temperature dependent yield strength
- Tensile stresses increase with cyclic exposures
 This effect is not evaluated in static durability testing

Alternate Systems Worth Assessing

- RE disilicates
- YAG, YBAG, ZrSiO₂ (ZrSiO₂ incompatible with SiC, harmful to mullite [Price et al])
- YAISi Amorphous YAS showed no degradation in 250C /15 atmosphere steam for 8700 hrs [Armstrong]
- CaMqAlSi system
- Others
- others

Bond Coat: Si₂N₂O, MoSi₂, disilicates,

Alternate Application Methods Worth Assessing

- Focus on application methods suitable for complex shapes:
 - Displacement Reactions [Tiegs, Lowden]
 - Liquid metal
 - Pack cementation
 - Gas phase
 - Slurry, [Armstrong] sol gel, or polymer precursors applications
 - Dip coating
 - Spray coating
 - Spin coating
 - Vacuum infiltration
 - Reaction sintering of multilayer dipped coatings [Asayama et al, 2002]

Analytical Screening Approaches Should be Included

Examples

 Coatings for fiber coating candidates analytically screened for Thermodynamic, Physical, Mechanical, Stability [Gonczy et al, 2002]
 Ceramic Materials analyzed for Chemical Stability in H₂ and H₂ + H₂O [Misra, 1990]

Recommendations for Improved Environmental Resistance

Roadmap for Improved Materials Data Base for

Environmental Resistance

- Establish a database resource for thermodynamic, physical, and chemical properties important to coating analysis and evaluation
- Data base:
 - For candidate bond coats: assess chemical bond to SiO₂
 - CTE
 - Silica activity
 - Water vapor resistance
 - Chemical & phase stability couples
 - Bond strength
- Perform testing to characterize the effect of the protection system on fast fracture and time dependent properties for use in life analysis codes
- Continue the development of test techniques to measure

Roadmap of <u>Material</u> <u>Development</u> for Environmental Resistance

- Screen and analyze candidates and candidate couples based on database knowledge
- Identify thermo-chemical data base needs
- Perform experimental evaluations of couples for bonding, chemical and phase stability, cyclic durability
- Perform experimental multilayer compatibility & stability evaluations
- Consider a porous surface layer between the substrate and EBC to provide strain tolerance
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 and potential impact energy absorption?

Roadmap for <u>Design and Life</u>
<u>Prediction</u> for Environmental
<u>Resistance</u>
Determine coating bonding strength requirements for static and rotating parts

 Effect of protection system on fast fracture and time dependent properties

 Incorporate the effect of coatings into the life analysis codes

Roadmap for <u>Non Destructive</u>
Evaluation for Environmental
Resistance
Continue the development of NDE methods to assess coating adherence and integrity
Continue to correlate coating bonding and

- Continue to correlate coating bonding and integrity in service with NDE results
- Develop effective methods to detect coating deterioration before it becomes critical.

Develop a low cost method to assess
Costing thick page (upiformity on complete the second second

Roadmap for Fabrication and **Process Development for Environmental Resistance** Develop Low cost, robust application methods suitable for complex shapes Surface treatments to improve adherence without inducing strength loss System must be cost competitive

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