

Development and Evaluation of Environmental Barrier Coatings for Silicon Nitride

**Tania Bhatia, Harry Eaton, John Holowczak, Ellen Sun,
and Venkat Vedula**

**United Technologies Research Center
East Hartford, Connecticut**

Presented at DOE EBC Workshop in Nashville on November 18, 2003



Environmental Barrier Coatings: Development and Demonstration

Acknowledgements

Funding Support

DOE – Debbie Haught and Steve Waslo

ONR – Steve Fishman

NASA – Dave Brewer, Bob Draper, and Joe Shaw

Collaborations

Solar – Jeff Price, Josh Kimmel, Mark Van Roode, and Oscar Jimenez

NDE – Bill Ellingson at ANL

Mechanical Testing – Matt Ferber and H.T. Lin at ORNL

Keiser Rig – Karren More and Peter Tortorelli at ORNL

Team Members

Gary Linsey, Xia Tang, Bill Tredway, Tom Lawton, Bob Barth, Mark Hermann, and Shanti Nair (U Mass)



Environmental Barrier Coatings: Development and Demonstration

Outline

- Highlights of EBC developed for silicon carbide (EBC_{SiC})
- Adapting EBC_{SiC} to silicon nitride: Important learnings for EBC_{SiN} development
- EBC for silicon nitride development
- Summary and future challenges



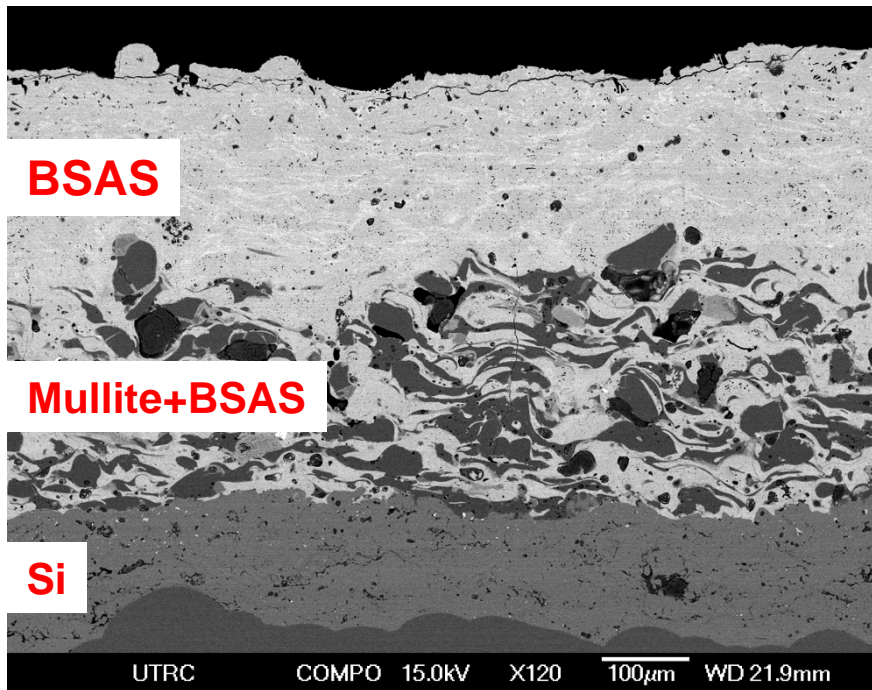
EBC for Silicon Carbide (EBC_{SiC})



Environmental Barrier Coatings: Development and Demonstration

Current state of the art EBC_{SiC}

- Development was initiated under NASA HSCT (High Speed Civil Transport) EPM (Enabling Propulsion Materials) program in mid 1990's for SiC/SiC CMC.
- Scaled-up and improved under DOE/Solar Turbines CSGT (Ceramic Stationary Gas Turbine) program since late 1990's.



Barium Strontium Aluminum Silicate (BSAS)

Intermediate layer (Mullite+BSAS)

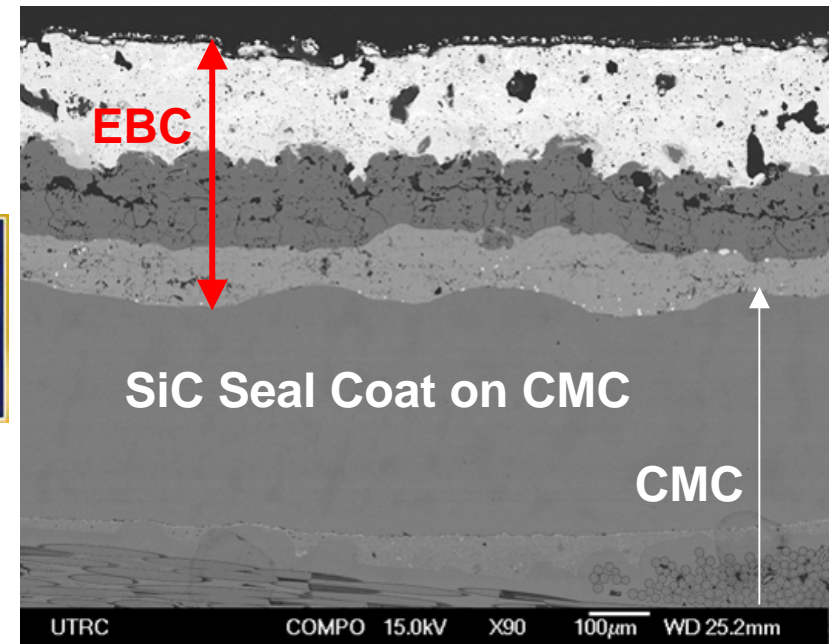
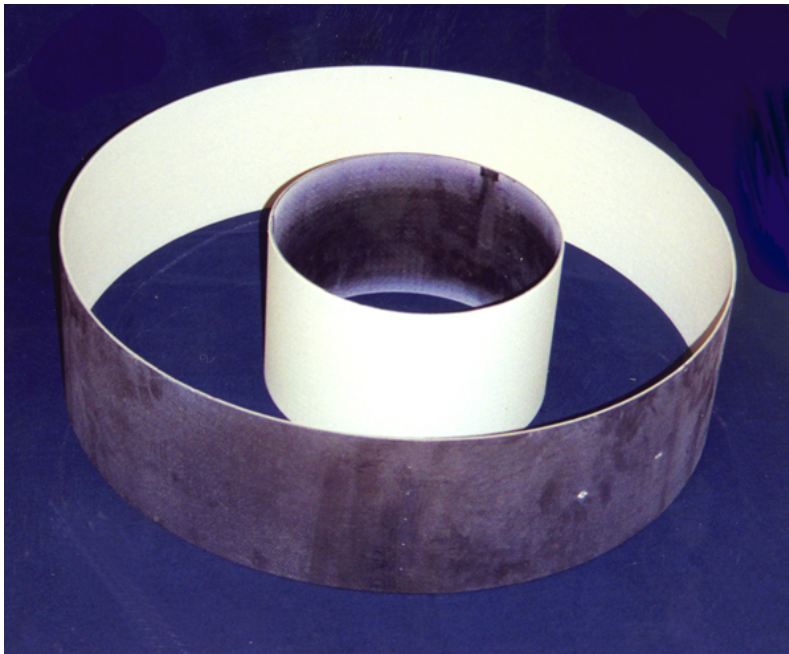
Silicon bond coat



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BSAS-based EBC_{SiC} demonstrated for long-term 2200°F applications

- ~50,000 hours field tests in Solar Turbines Centaur 50S engines
 - Bakersfield, CA : 13,937 hours
 - Malden Mills II, MA : 15,144 hours

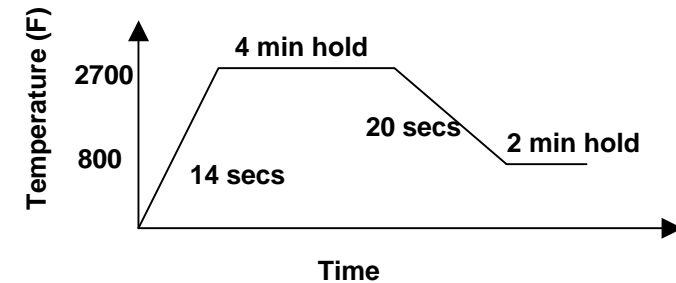
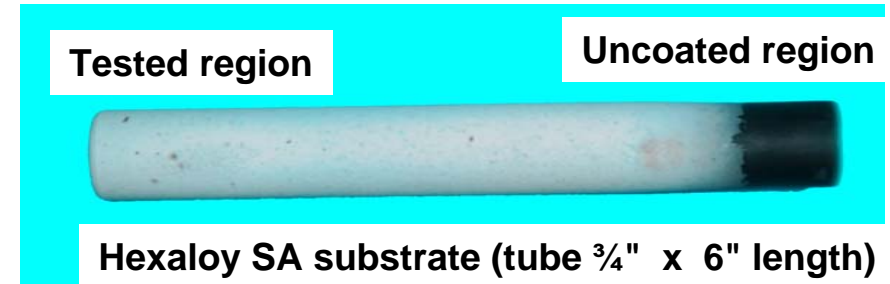
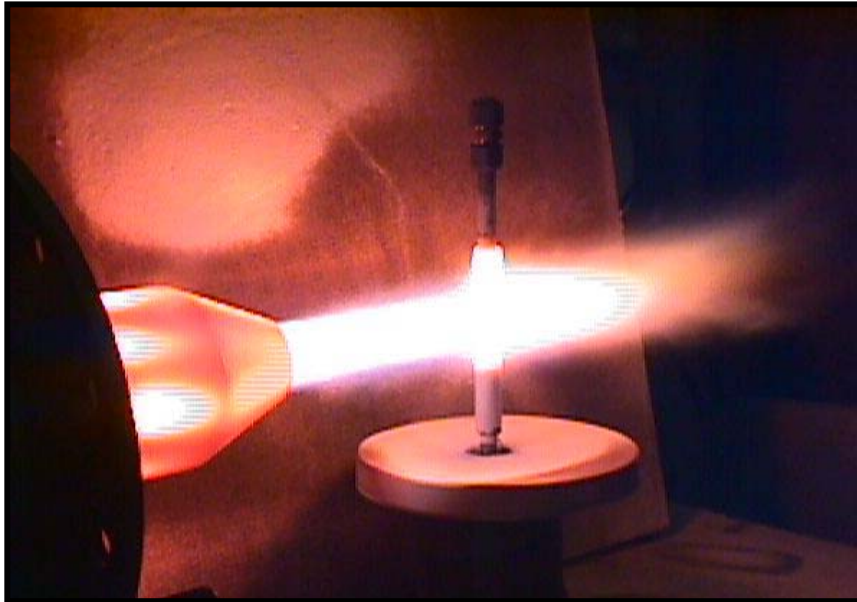


CMC well protected in areas where EBC remained intact



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UTRC burner rig demonstration: BSAS-based coating with mullite thermal barrier survived 100 thermal cycles



- Achieved 2700°F surface temperature with 300°F EBC thermal gradient
- EBC coated monolithic SiC survived 100 atmospheric burner rig thermal cycles

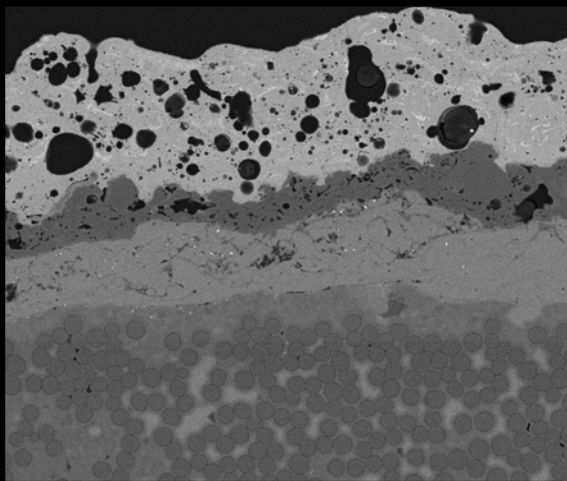


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SAS as “new” steam barrier layer in EBC_{SiC}

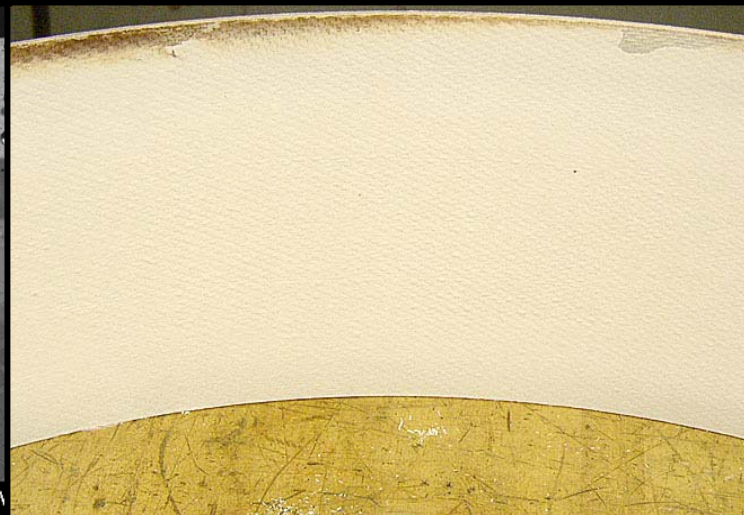
- SAS believed to provide better EBC life than BSAS
- SAS-based EBC has been applied to Solar Centaur 50S liners
- Plasma spray parameters for SAS system optimized

SAS-based EBC 2002

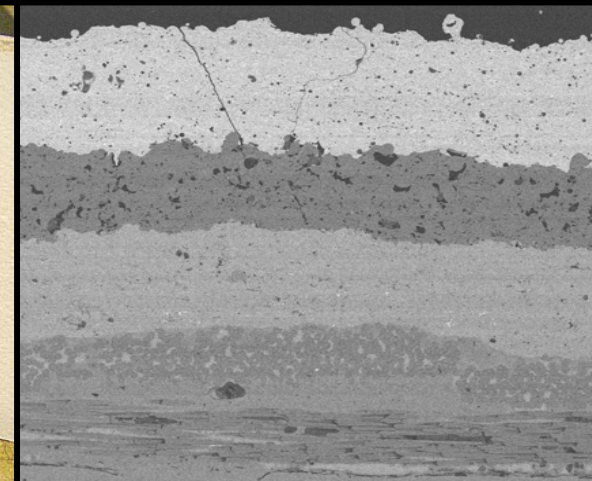


COMPO 20.0KV X200 100µm

2002 SAS EBC after 8368 hours:
Solar Centaur 50S liners



Process improvement in
SAS top layer 2003



COMPO 20.0KV X60 100µm WD

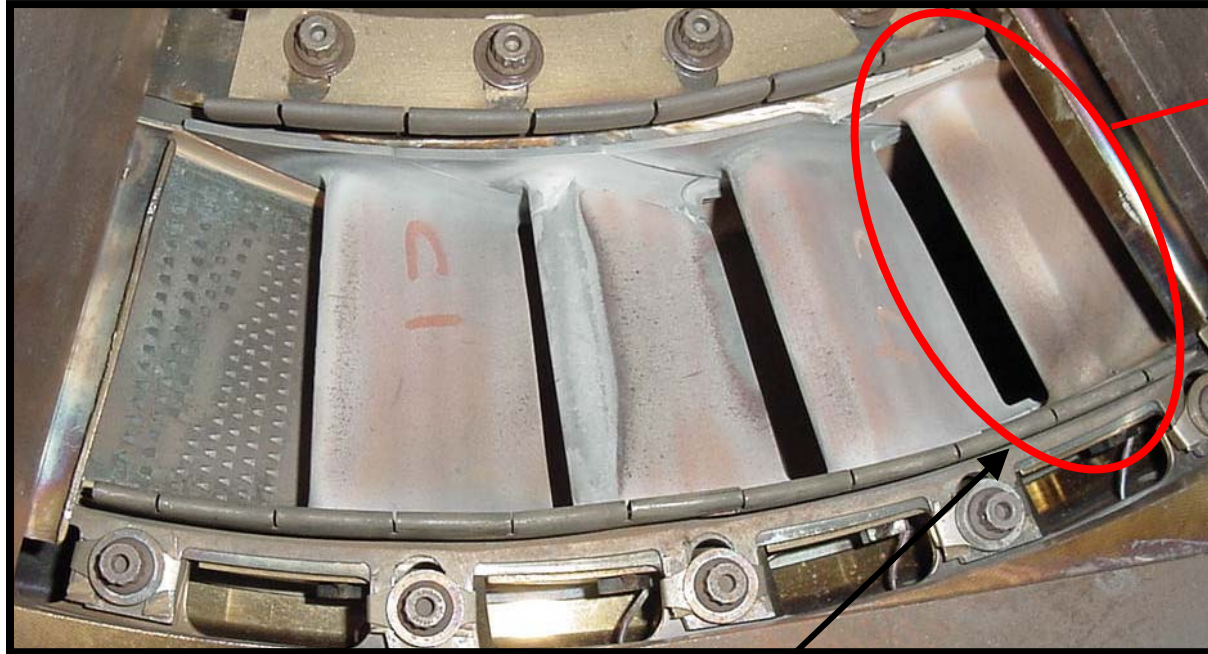


Applying EBC_{SiC} to Si₃N₄



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EBC_{SiC} applied to cooled FT8 Si₃N₄ vanes and survived two trip shutdowns



- SN282 vanes uncoated
- AS800 vane coated with EBC_{SiC}
- 30 hours at 70% power (1230°C at coated vane), 2 trip shutdowns from ~60% power, 1 hour at 80% power (1260°C at coated vane)

Pressure Side

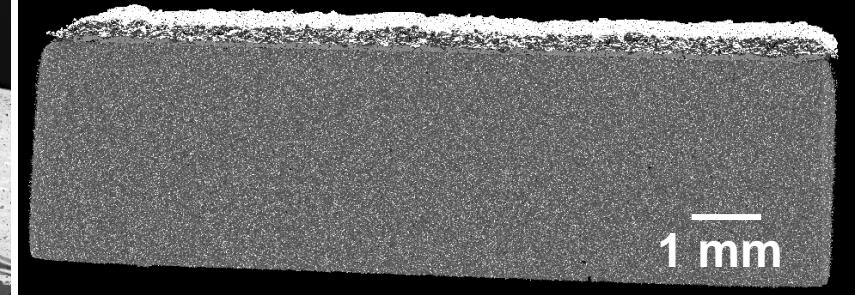
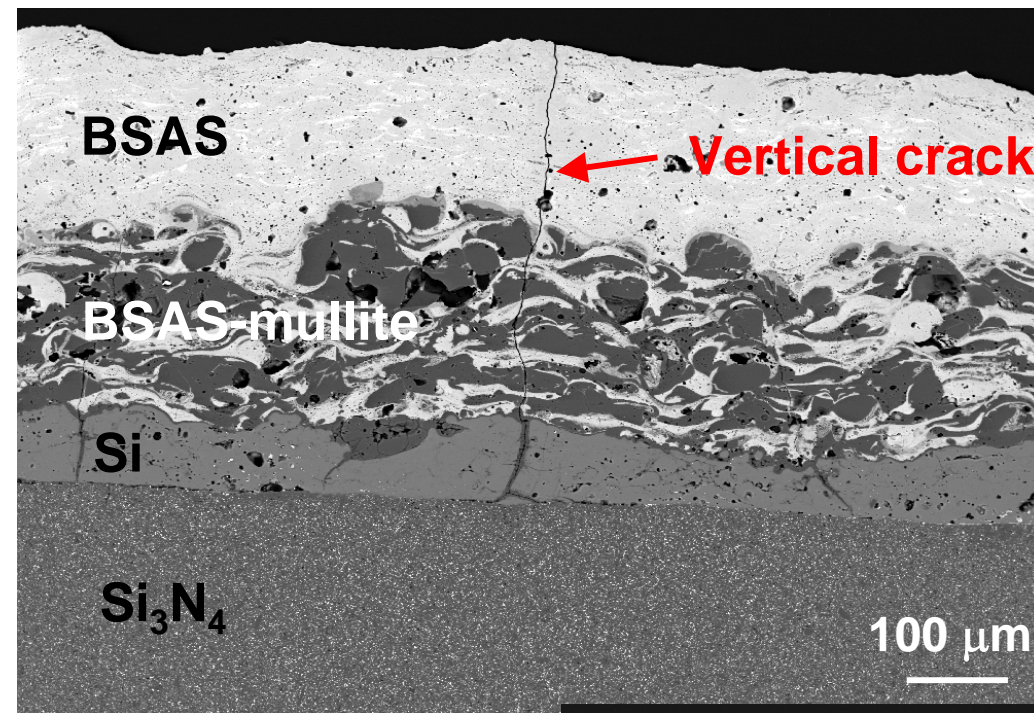


Suction Side



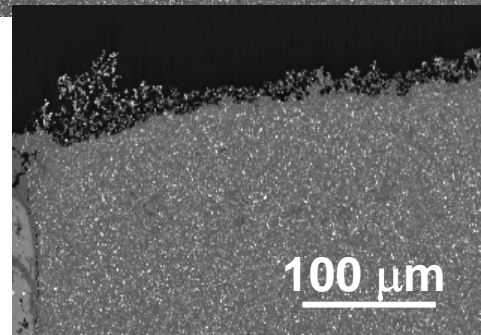
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Adapting EBC_{SiC} to silicon nitride: Effective protection in ORNL Keiser Rig



- Coating remained intact except through thickness cracks due to CTE mismatch
- No oxidation observed in the AS800 substrate underneath crack-free regions after 2000-hr steam exposure at 1200°C indicating effective barrier function

Uncoated surface after 1500-hr steam exposure at 1200°C



Results provided by
Karren More, ORNL



Environmental Barrier Coatings: Development and Demonstration

EBC_{SiC} on Solar's CSGT Si₃N₄ nozzles: FEA undertaken to model the effect of EBC on component

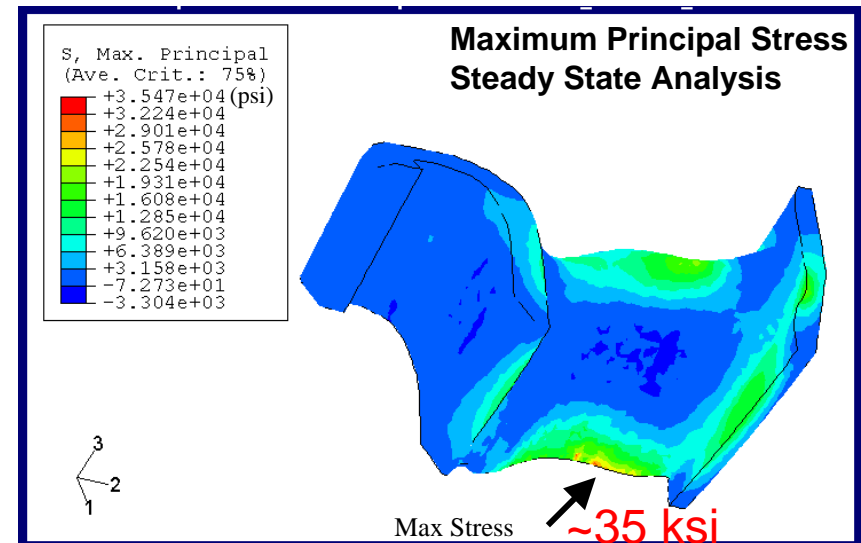
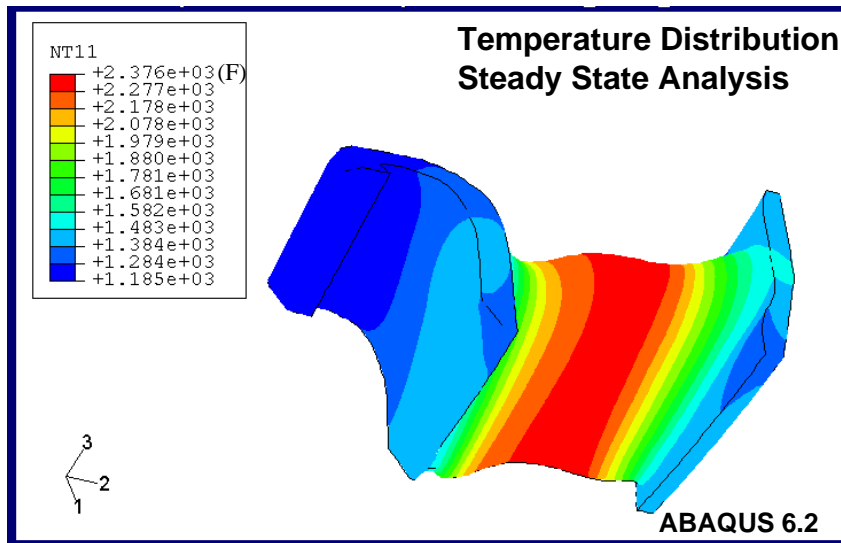
- Background
 - Majority of SN282 nozzles survived Solar's proof test (>90%)
 - Nozzles with EBC_{SiC} failed the proof test during transient heating
- Motivation
 - Determine the effect of EBC on thermal gradients and stresses in nozzle during proof test



Environmental Barrier Coatings: Development and Demonstration

FEA of the SN282 nozzles (Uncoated)

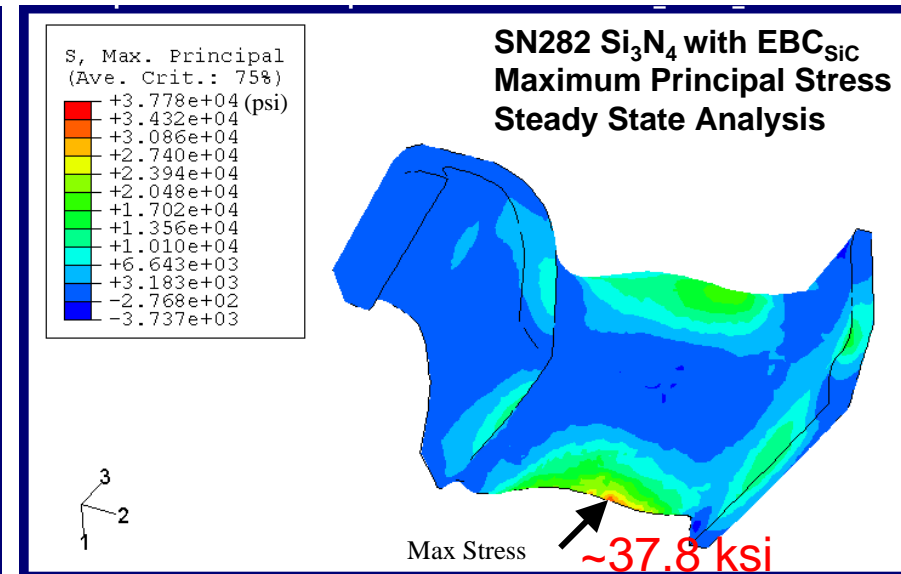
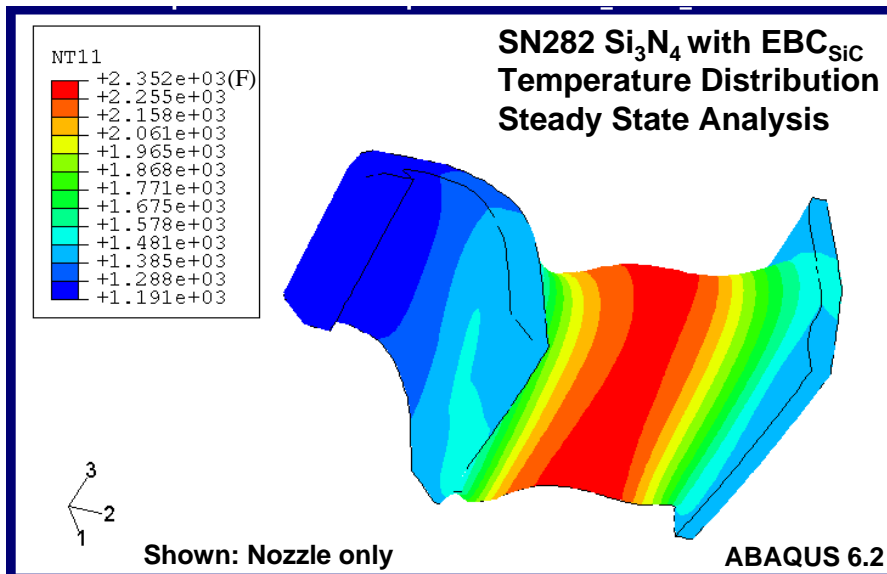
- Solid model and thermal boundary conditions for proof test obtained from Solar Turbines, Inc.
- Predicted steady state temperature gradients and stresses match Solar results
- Maximum stress at vane trailing edge



Environmental Barrier Coatings: Development and Demonstration

FEA of the SN282 nozzles with EBC_{SiC}

- UTRC generated solid model for the nozzle with 15 mil EBC
- SN282 with EBC leads to a nozzle temperature decrease of 24°F and principal stress increase by ~7%
- Assumptions
 - Hot-pressed BSAS properties used for EBC
 - Effect of silicon layer not included



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Residual stress effects on steady-state thermal stress

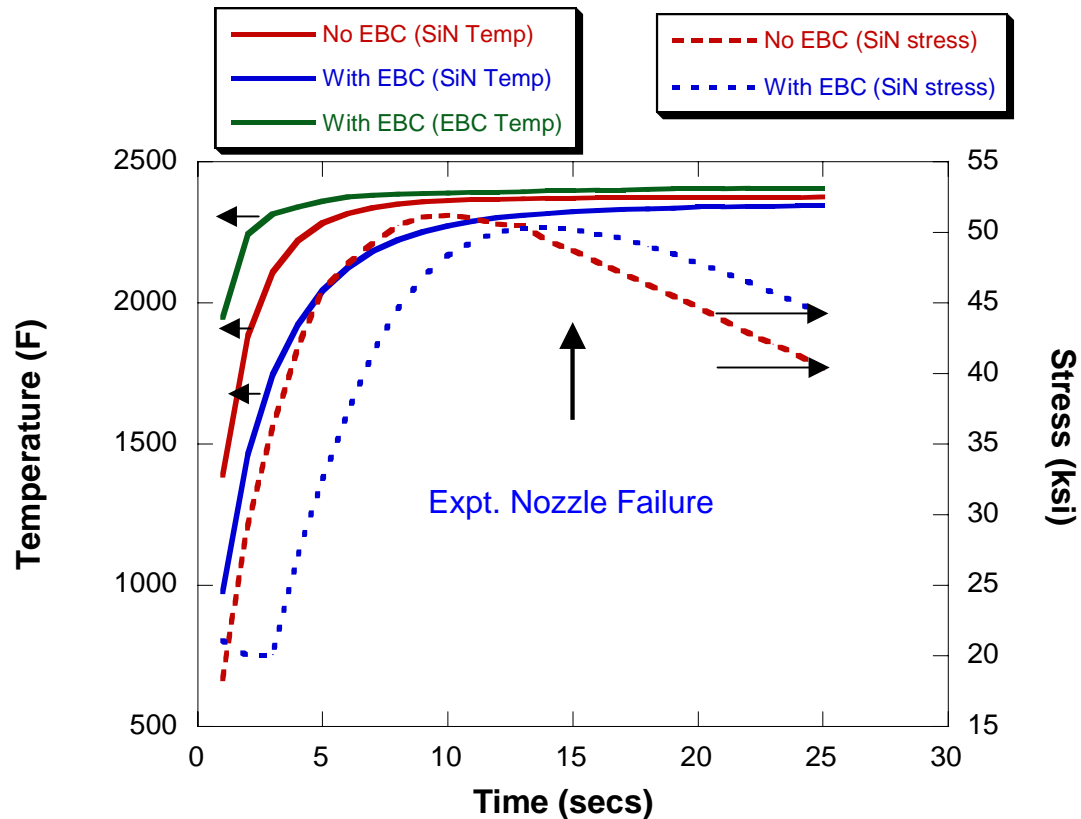
Nozzle Analysis	Analysis Step	Temperatures (F)		Location of Max. Stress	Max. Principal Stress (ksi)
		Nozzle	EBC		
No EBC	RT to operation	2376/1185	-	Nozzle TE	35.5
With EBC: Residual Stress	APS to RT	RT	RT	Coating	23 - 25
	RT to operation	2352/1191	2413/1255	Nozzle TE	37.8
With EBC: No Residual Stress	RT to operation	2352/1191	2413/1255	Nozzle TE	52.8

- Nozzle thermal stress: Between 37.8 and 52.8 ksi
- Strong function of residual stress relaxation in EBC and silicon nitride
- Thermoelastic analysis includes effects of thermal gradients and CTE/Elastic mismatch only



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Transient analysis (Start-up) of Solar nozzles

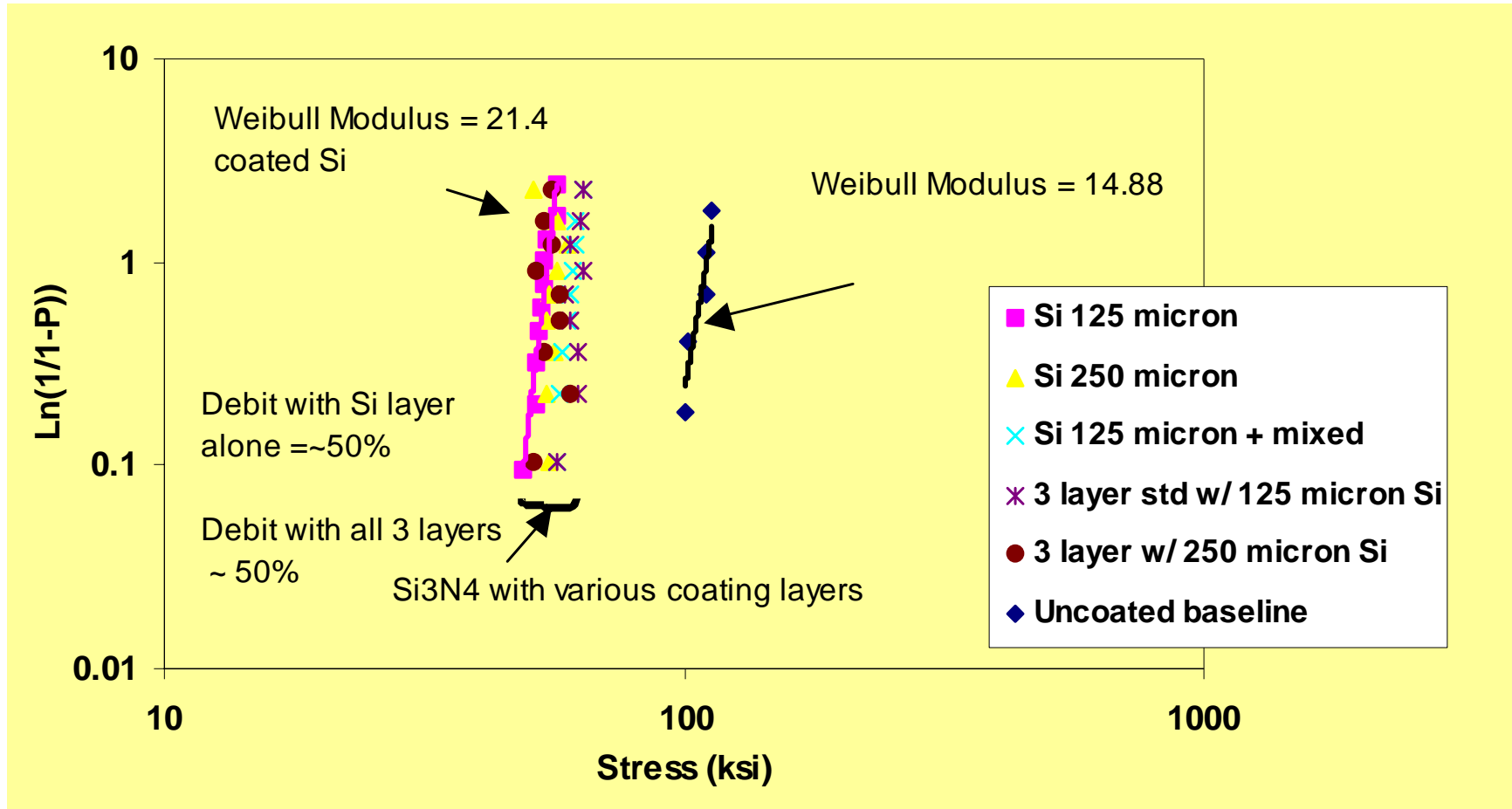


- Transient stress during heating is ~35% higher than steady state stress
- The time at which transient stress peaks (~15 secs) matches the experimental failure of nozzle during heat-up



Environmental Barrier Coatings: Development and Demonstration

Strength debit in EBC_{SiC} coated Si_3N_4 discovered



Environmental Barrier Coatings: Development and Demonstration

Failure probability of EBC_{SiC} coated SN282 solar nozzle determined to be close to 100%

CARES/LIFE Analysis

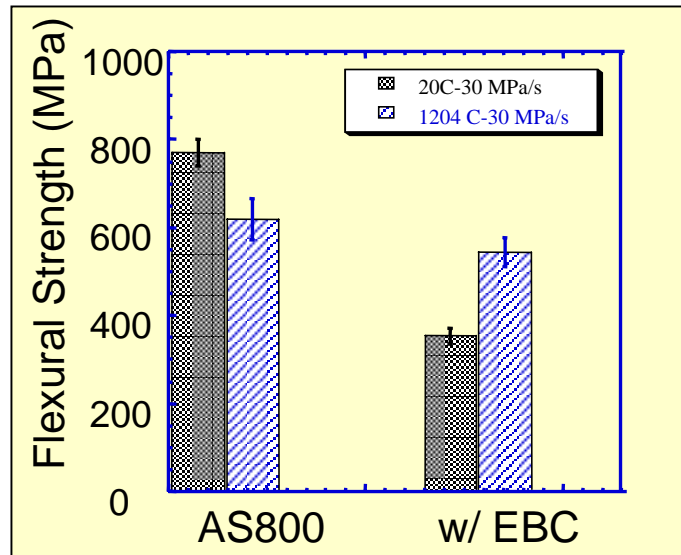
Material/ Property		As-processed SN282 (source: Kyocera)	SN282 with EBC (source: ORNL)
Strength (ksi)	RT	92	10
	2552 F	68	Not Available
Weibull Modulus (estimate)		10	10
Over-all Vane Failure Probability	RT	3.10E-04	1.00E+00
	2552 F	6.30E-03	-----

- Reasons for nozzle failure:
 - (a) Strength debit in SN282 with EBC
 - (b) Higher thermal stresses in coated nozzles
- Thermal stress strongly dependent on CTE mismatch between EBC and substrate and weakly dependent on modulus mismatch
- Thermal stress increases by 6 to 48% for coated nozzles, depending on the extent of residual stress relaxation



EBC_{SiC} debits silicon nitride strength

- Coating and substrate are not compatible in thermal expansion behavior.
 - CTE of EBC_{SiC} : ~5.0 ppm/°C
 - CTE of Si₃N₄ : ~ 3.2 ppm/°C
- EBC debits the strength of silicon nitride :
 - > 50% debit at room temperature
 - ~15% debit at high temperature



Results Provided by
H. T. Lin, ORNL

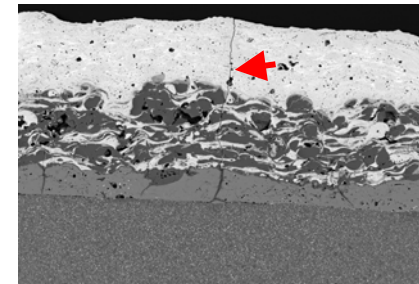
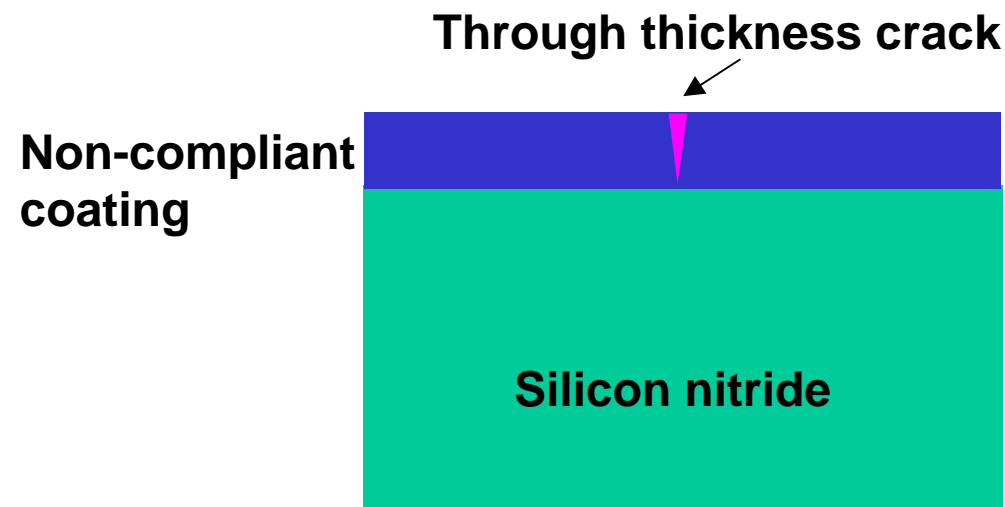
- EBC strength debit observed for different grades of silicon nitride: AS800, SN282 and NT154 (Room Temperature)



Environmental Barrier Coatings: Development and Demonstration

Mechanisms causing RT strength knockdown identified

- Limited effect of surface preparation
- Thermal expansion mismatch between coating and substrate induces cracks in the coating. The cracks in the coating may act as strength controlling flaws and reduce substrate strength.
- Further investigation of chemical interaction between coating and substrate
- Coating system under development to mitigate substrate strength knockdown



Environmental Barrier Coatings: Development and Demonstration

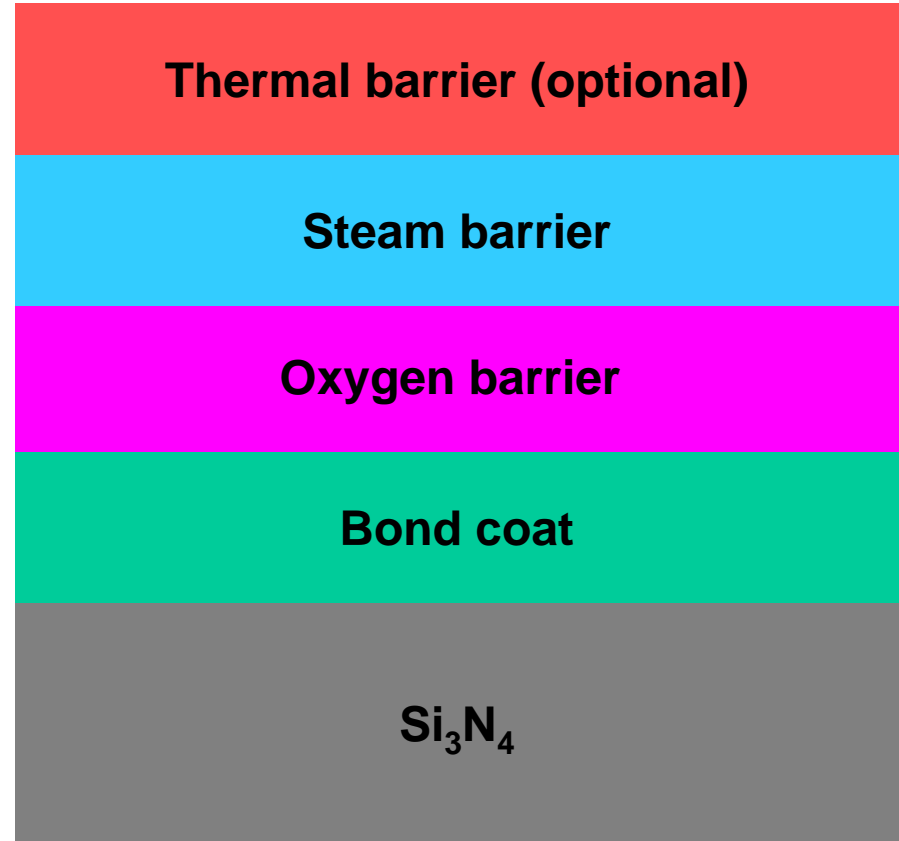
Current EBC approaches for Si_3N_4

Bond Coat

- Eliminate cracking in coating
- Reducing CTE mismatch

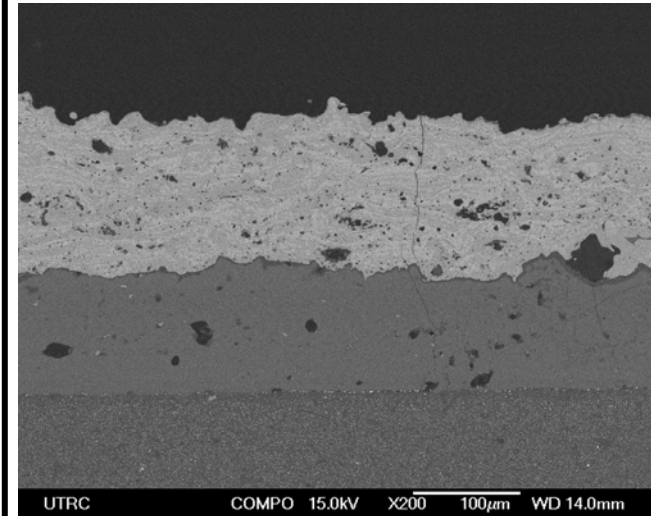
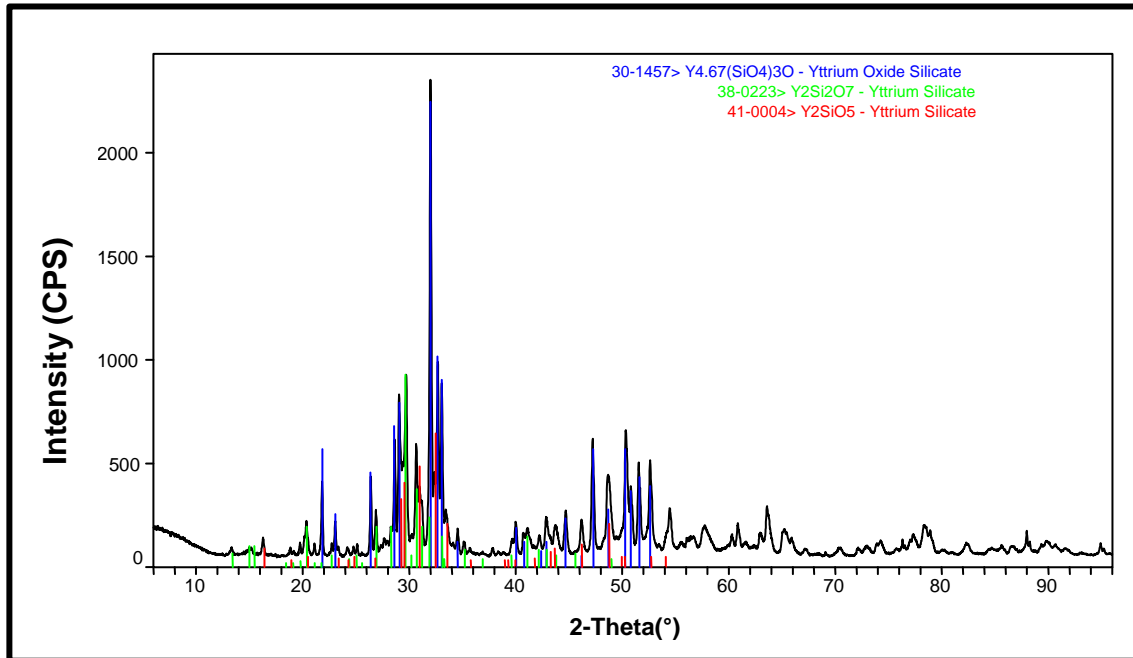
Top Coat

- CTE matched moisture and oxidation barrier layers



Environmental Barrier Coatings: Development and Demonstration

Barrier layer with CTE matching: Plasma spray parameters for crystalline yttrium silicate developed



- Under ordinary conditions, plasma spraying results in amorphous phase
- Achieving the “correct” phase assemblage critical to developing crack free, adherent coatings



EBC for silicon nitride – Summary and challenges

- The key limitation in the applicability of EBC for silicon carbide to silicon nitride materials is the CTE mismatch between the coating and the silicon nitride.
- Promising approaches to develop EBC systems for silicon nitride have been identified (bond coat and barrier layer)
- Coating system needs optimization:
 - bond layer adhesion to substrate
 - chemical compatibility and stability
 - thermal cycling
 - effect on substrate properties
- Understanding and predicting recession mechanisms in complex silicates in high pressure and high velocity environments required for life prediction

