

Tailoring the Next Generation Si₃N₄ Ceramics to Enhance Performance

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Supported by The Important Contributions by the Following

Sample fabrication:

M. J. Hoffmann & R. Satet, University of Karlsruhe

D.-S. Park, Korean Institute of Machinery and Materials

K. Hirao & M. Brito, Synergy Ceramics Center, AIST, Japan

Characterization:

HREM, STEM

S. J. Pennycook and N. Shibata (JSPS Research Fellow),

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Y. Ikuhara, University of Tokyo,

Raman spectroscopy

M. J. Lance, Oak Ridge National Laboratory

Theoretical studies:

G. S. Painter and W. A. Shelton, Jr., Oak Ridge National Laboratory

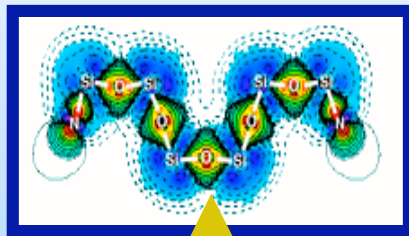
Different Length-Scale Approaches to Enhance the Mechanical Performance of Ceramics (e.g., Si_3N_4)

Enhanced toughness: Self-reinforced Si_3N_4 -based ceramics

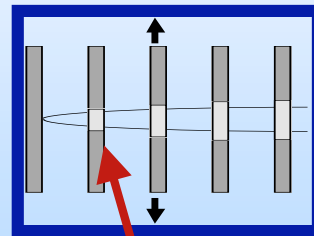
- Micro-scale composite: large elongated grains-- **well documented**
 - Seeding concept (Hirao *et al.*)
 - $\square\square\text{SiAlONs}$: I-Wei Chen *et al.*
- Atomic-scale: Microstructure & interface characteristics
 - Adsorption versus preferential segregation of additives
 - Interfacial debonding & role of Intergranular films (IGF)
 - $\square\square\text{SiAlON}$: Influence of Al:Y ratios in additives
 - $\square\square\text{Si}_3\text{N}_4$: Influence of rare earths

USE PROCESSING TO DEVELOP AND CONTROL THE FORMATION OF A TOUGH/STRONG MICROCOMPOSITE MICROSTRUCTURE

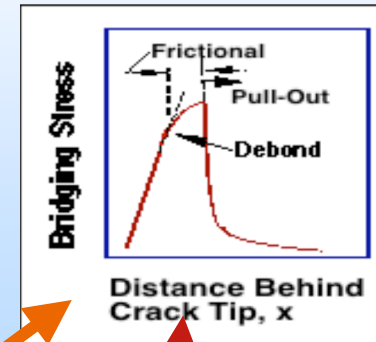
A COMBINATION OF MECHANISMS AT ALL LENGTH SCALES INVOLVED IN TOUGHENING CERAMICS



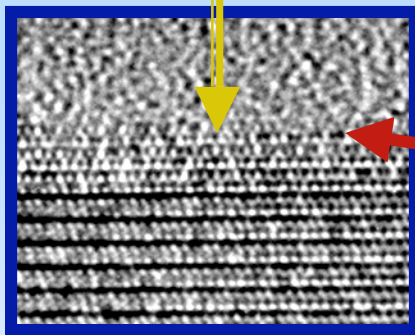
Atomic - scale



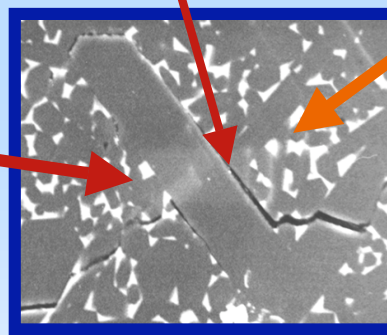
Micro - scale



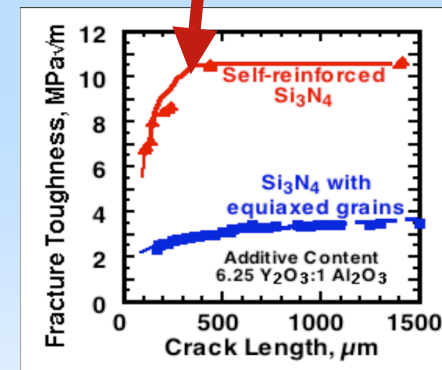
Macro - scale



Atom structure of the interface influences



Interfacial debonding &, thus, bridging of the crack (and crack deflection that affects



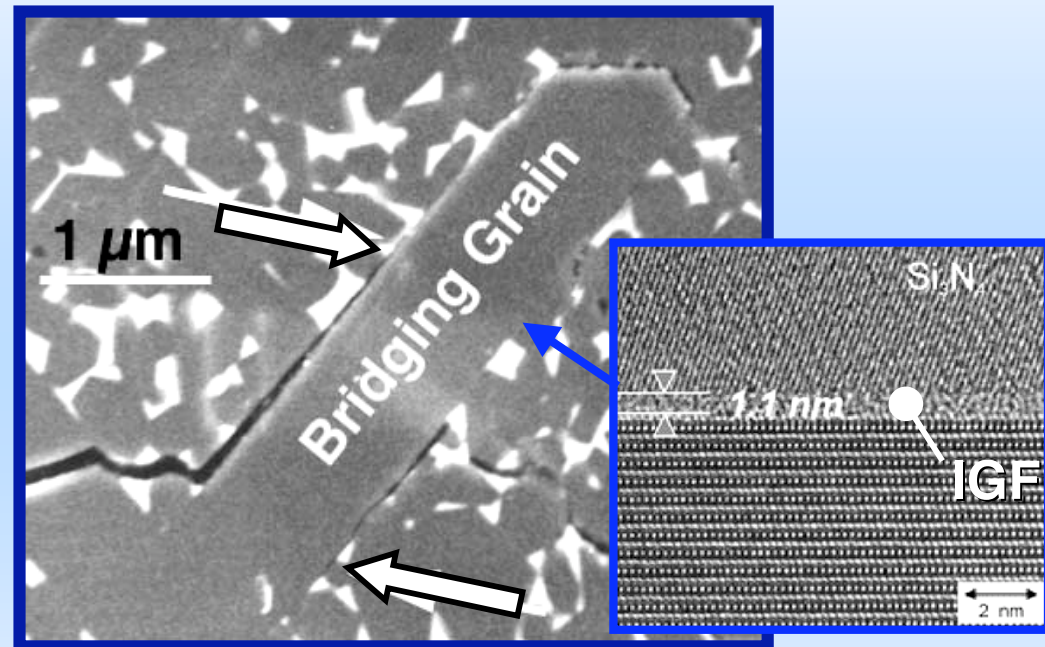
Closure stresses acting on crack &, thus, toughness

Elongated Grains Act as Reinforcements, Which Toughen the Ceramics When They Debond and Bridge the Crack

Toughness Increased
By Formation Of:

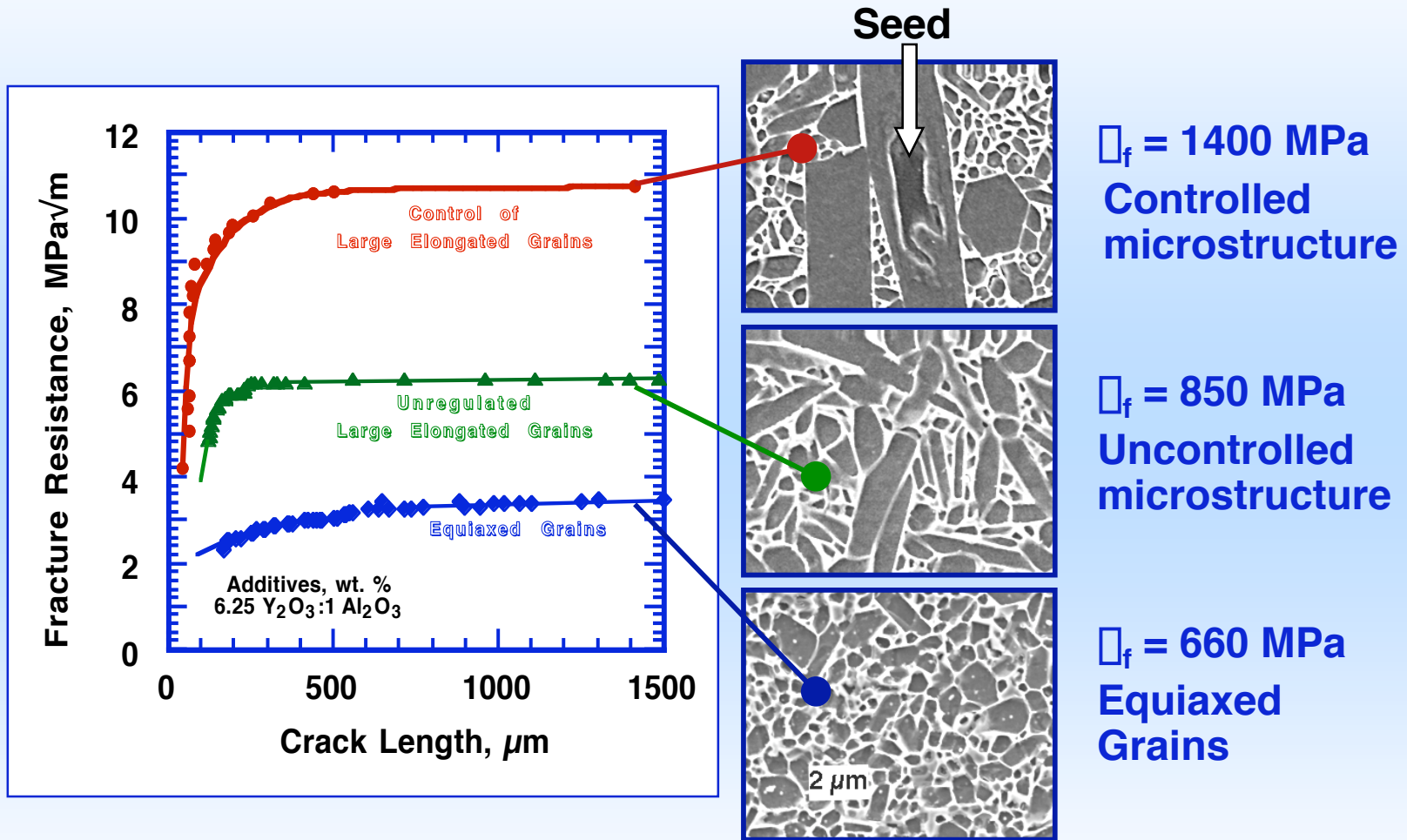
Strong Elastic Bridges
Thin Single Crystals
Can Exhibit Very High
Strengths

Frictional Bridges and
Pull-Out
Friction Effectively
Dissipates Applied
Strain Energy



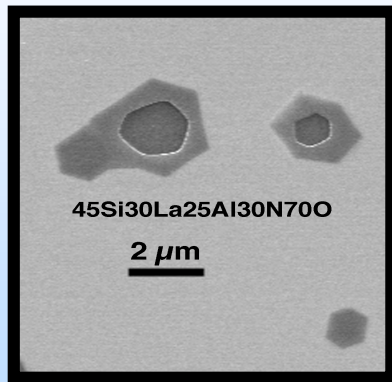
Grains are surrounded by a continuous amorphous intergranular film (IGF) as a result of liquid phase sintering

Large Elongated Grains in Fine Grained Silicon Nitride Matrix: Strong R-Curve, $K_{IC} > 10 \text{ MPa}\sqrt{\text{m}}$, $\sigma_f > 1 \text{ GPa}$ & $m > 30$

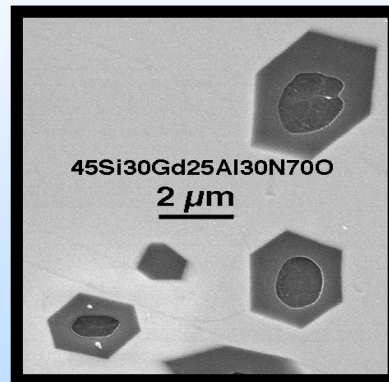


\square -particles are nuclei for the formation of large reinforcing grains.
Rice-like \square -seeds used to control microstructure.

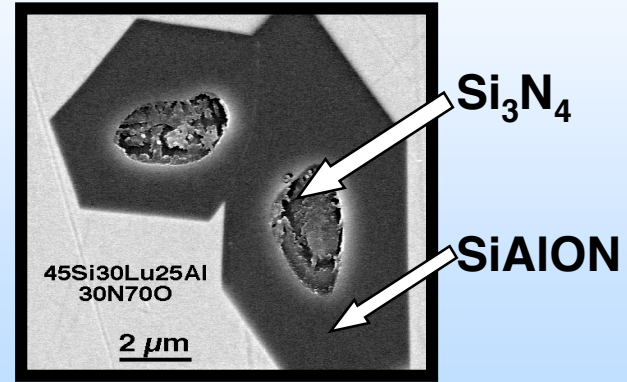
Size and Shape of Reinforcing Grains Altered by Sintering Additives



Lu

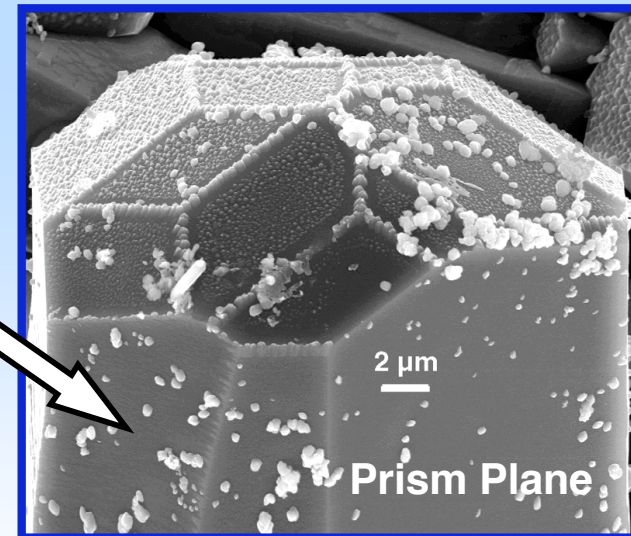


Gd



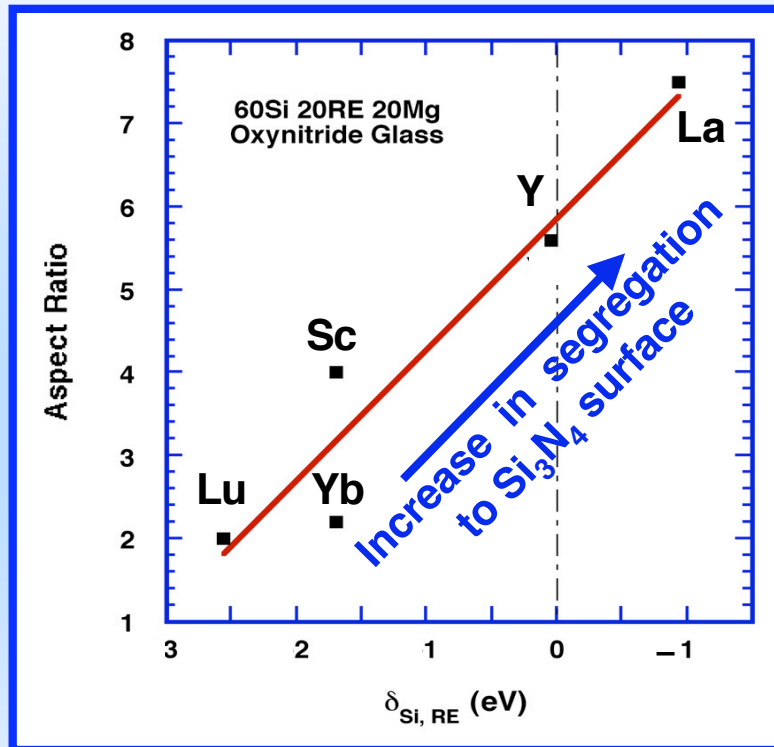
La

- c-axis growth is fast diffusion controlled
- diametrical growth is slow interface reaction controlled on smooth prism planes
- Same behavior: RE + Me oxide additives where Me = Al or Mg
- So what's behind the effects of RE elements?



RE Segregation to Si_3N_4 Prism Surface Is a Critical Factor in the Anisotropy of Grain Growth

-- Formation of Elongated Reinforcements



Now can predict effects rather than trial and error.

Painter, Becher and Shelton, 2003

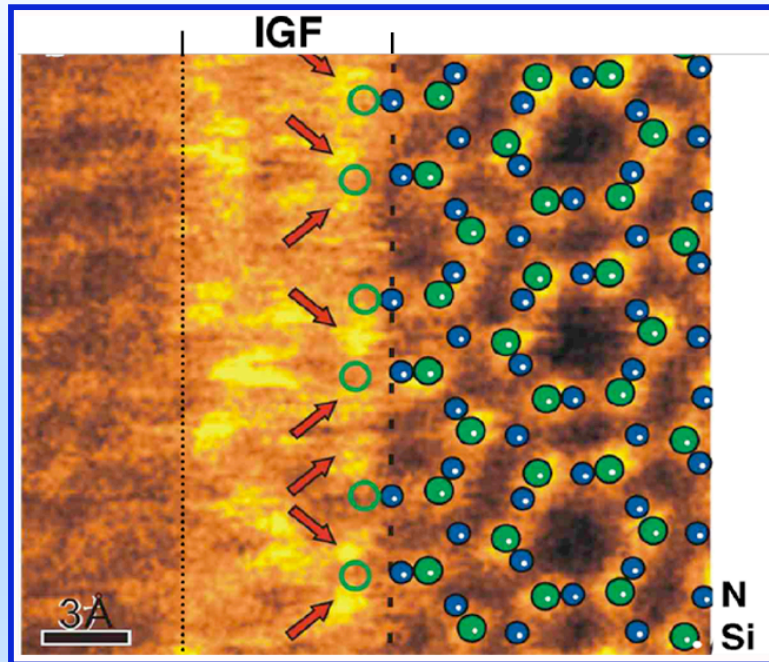
Why?

- Diametrical growth is controlled by reaction rate at prism surface.
- RE form strong bonds with N on terminal surfaces & most do.
- RE with strongest attraction vs. Si for prism surface limit diametrical growth most effectively.

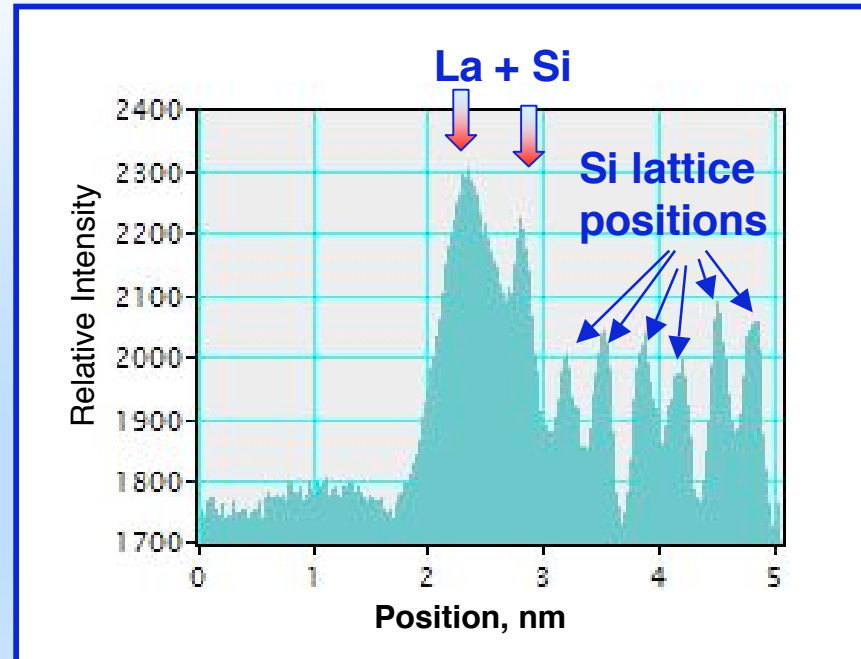
Thus, Lu predicted to avoid prism surfaces and have little effect on grain growth.

La should prefer Si_3N_4 surface and limit diametrical growth.

La Not Only Present Within IGF But Prefers Si_3N_4 Terminal Surface As Predicted by Theory



HAADF STEM Image



$\square \square \text{Si}_3\text{N}_4$ (7.0 wt% La_2O_3 + 2.0 wt%MgO)

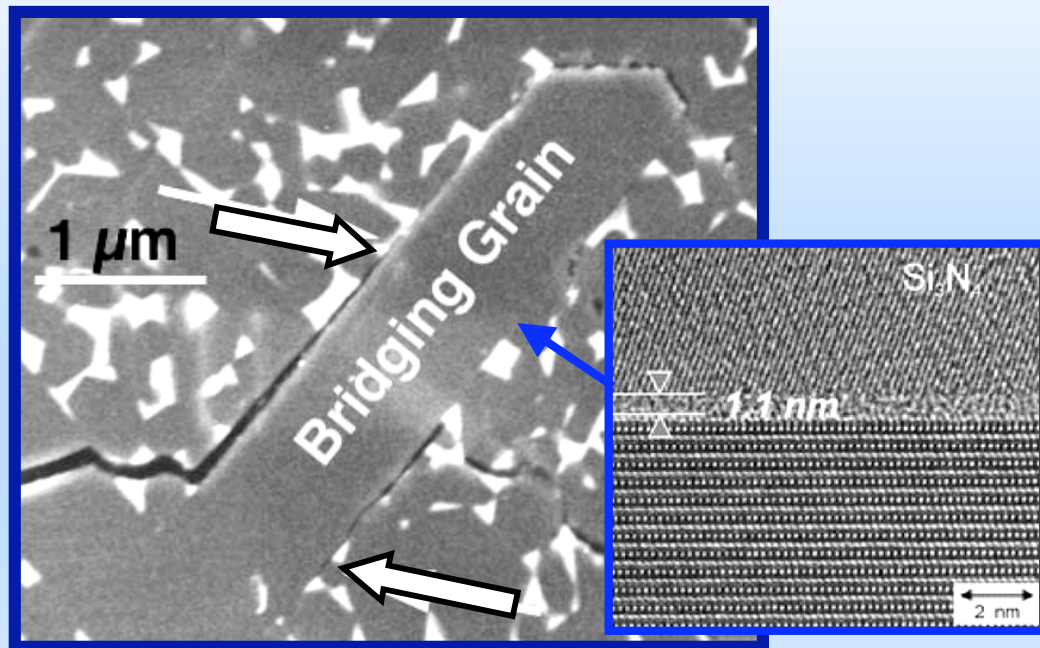
La (arrows note La locations) prefer Si_3N_4 terminal surface.
Representative line scan across IGF illustrating maximum
 $\square \square \square$ La content at each interface and minimum within IGF.

Shibata & Pennycook, 2003

More Than a Reinforced Microstructure Is Required - The Reinforcing Grains Must Also Debond from the Matrix

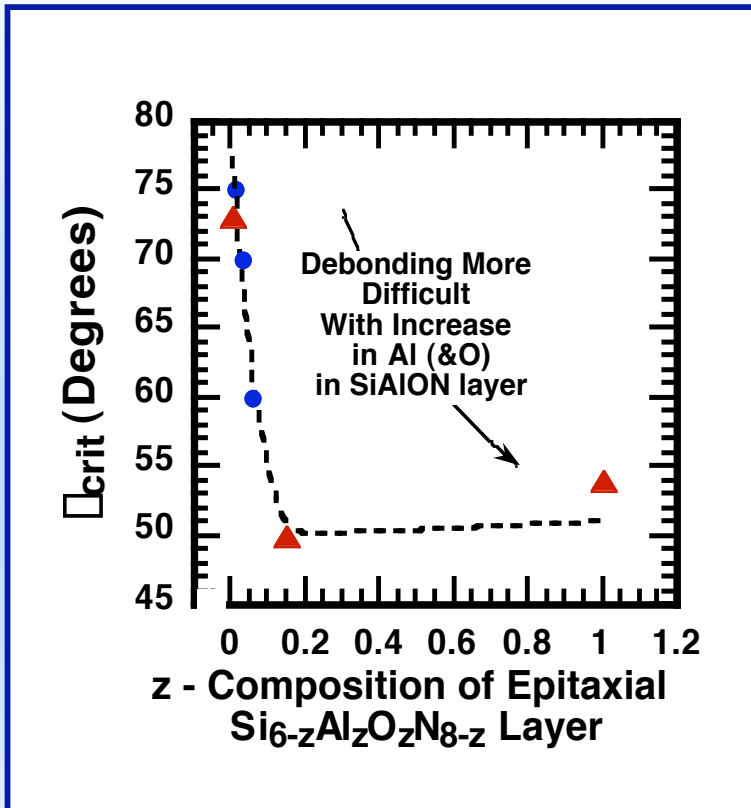
1 to 2 nanometer thick intergranular film (IGF) surrounds Si_3N_4 grains.

IGF plays a critical role in the debonding of the interfaces and in grain growth.

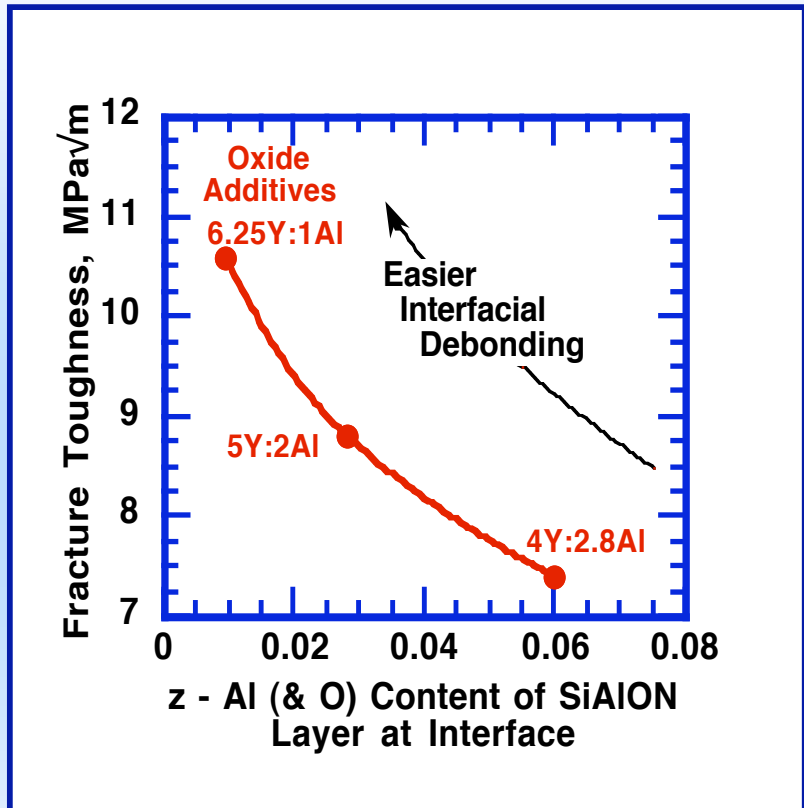


Arrows highlight the end of debonded interfaces of a bridging grain in the crack-tip wake.

IGF Composition Dominates Interface Debonding & Toughness (e.g., $Y_2O_3 + Al_2O_3$ Additive System)



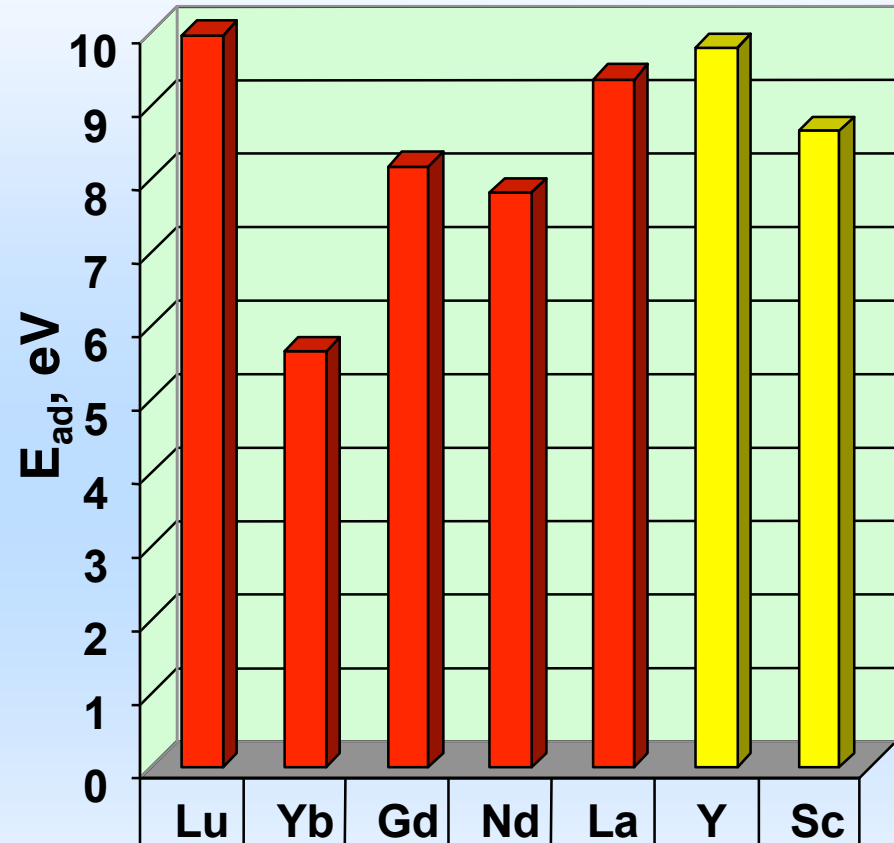
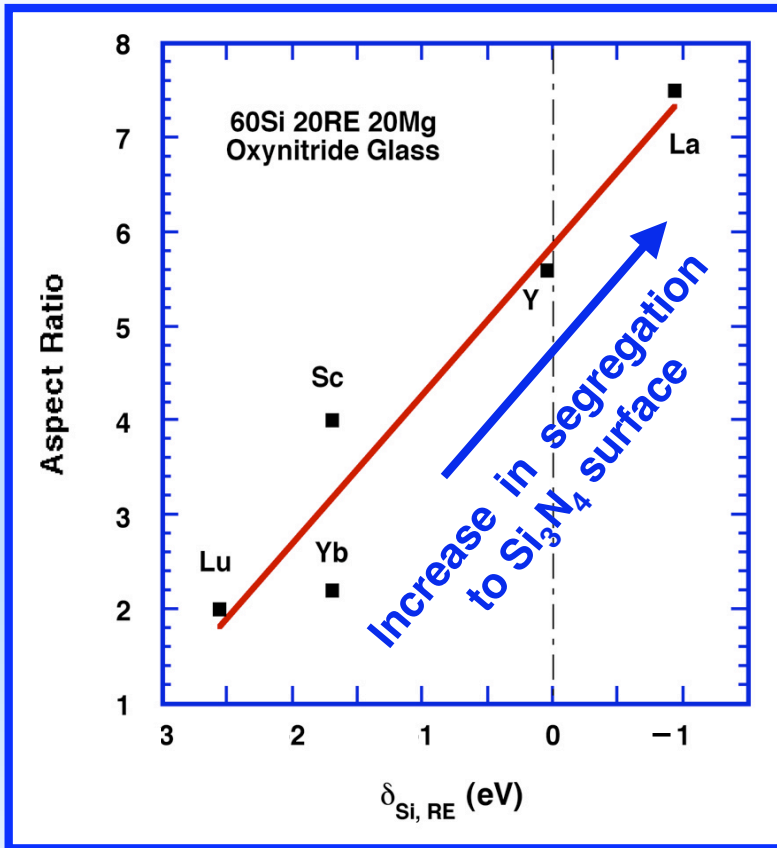
Example:
 Si_3N_4
 with
 combined
 additives
 of
 Al_2O_3
 +
 Y_2O_3



Interface Strength Decreases as
 Reduce Al & O content of
 epitaxial SiAlON growth layer.

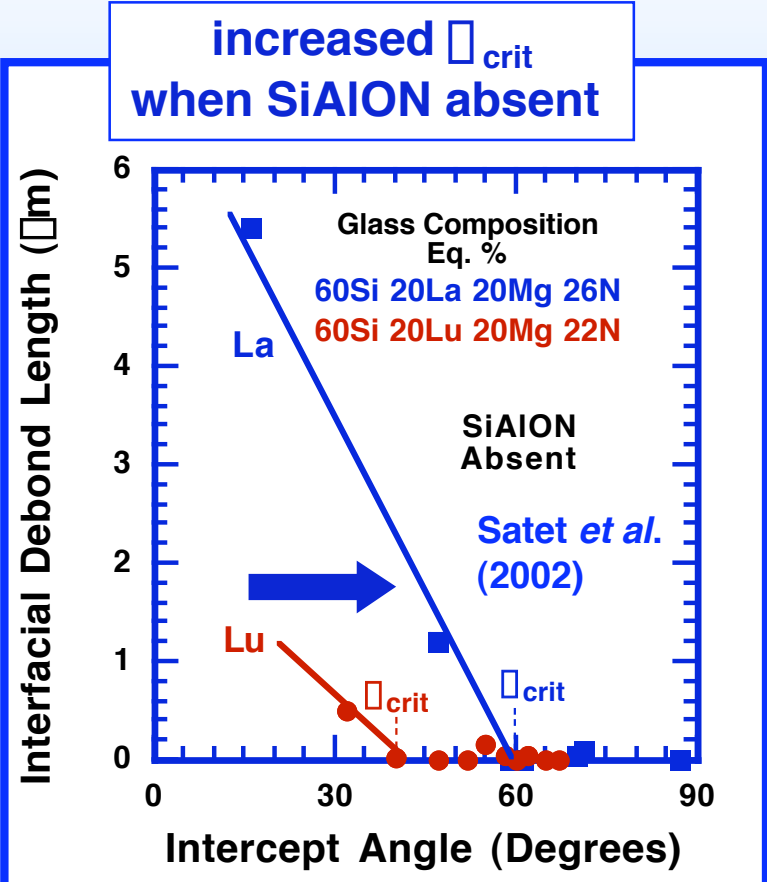
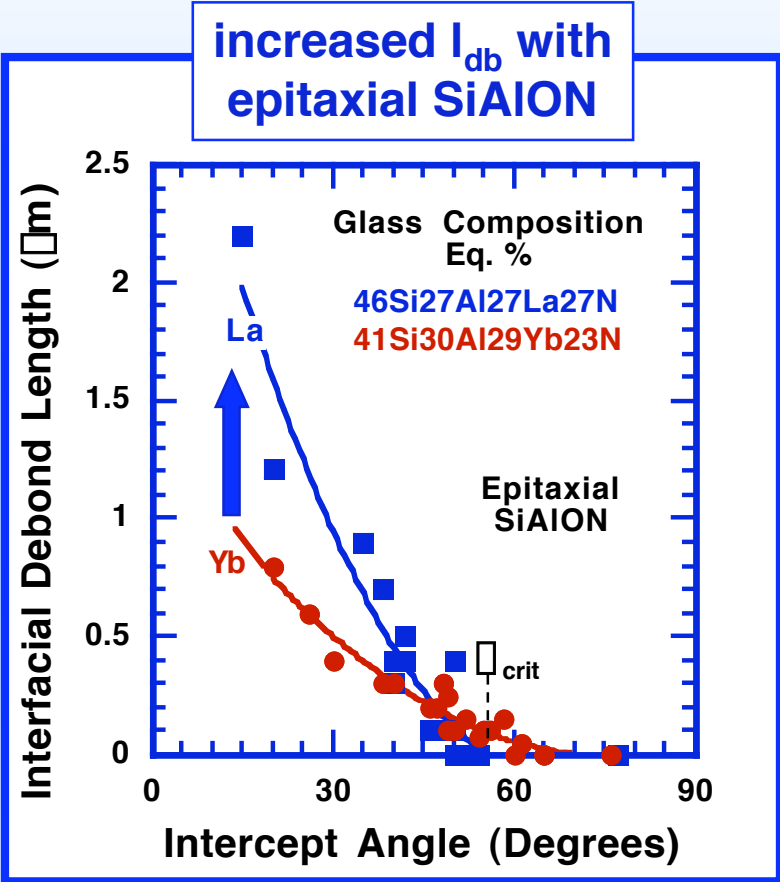
Fracture Toughness Increases as
 raise $Y_2O_3 : Al_2O_3$ ratio of additives
 in self-reinforced Si_3N_4 .

**Many RE Have High Binding Energies at Si_3N_4 Prism Plane;
Stronger Tendency to Segregate \rightarrow Weaker Interface**



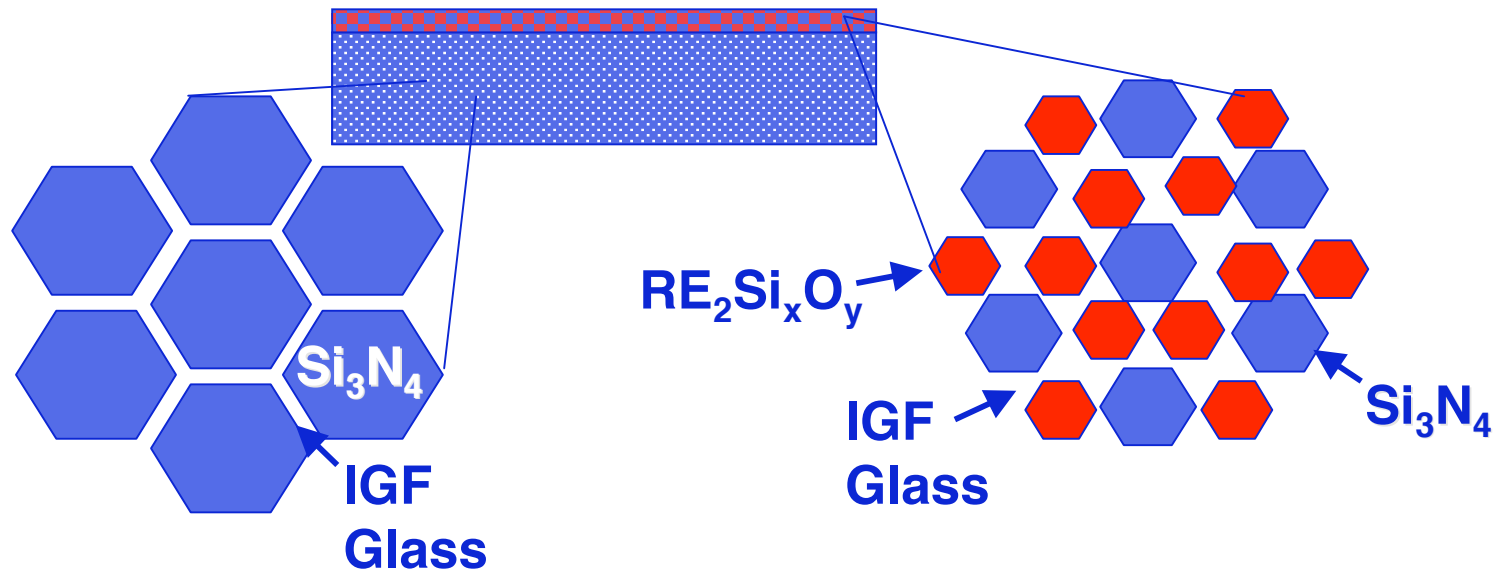
Increasing Weakness of Interface: Lu \rightarrow Sc \rightarrow Y \rightarrow La

Rare Earths Predicted to Alter Interfacial Debonding Behavior



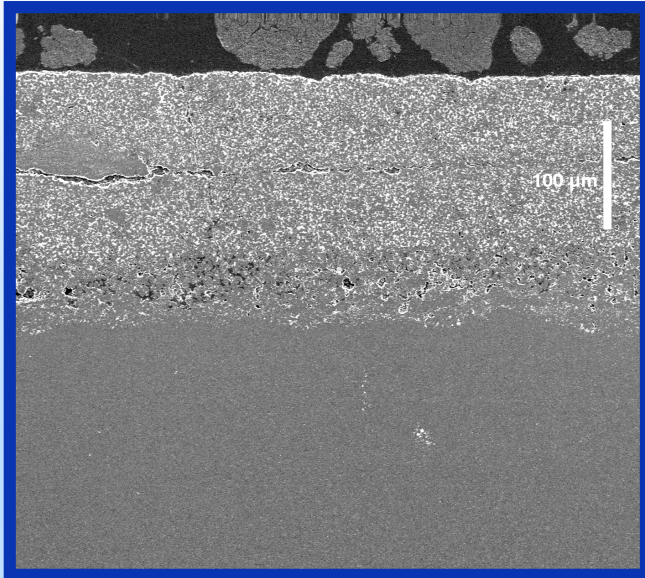
RE to N bonding at Si_3N_4 surface weakens interface, especially effective with increasing RE segregation to the interface.

Tailored Si_3N_4 Surfaces to Improved EBC Performance

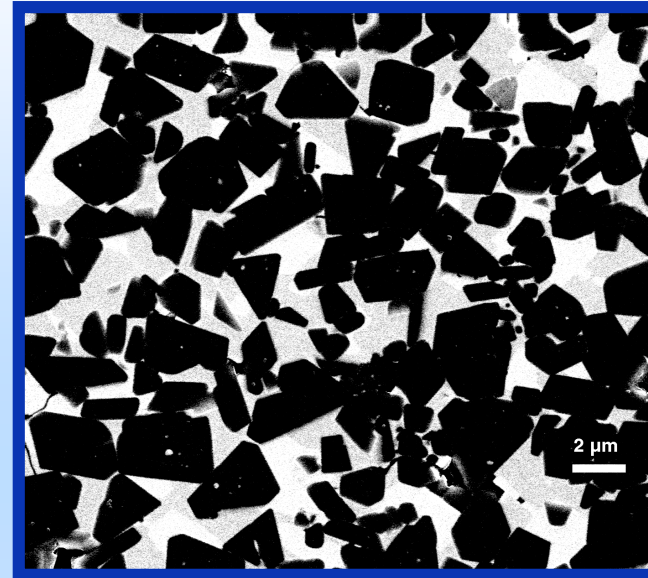


	α , ppm/ $^{\circ}\text{C}$	E, GPa	T_g , $^{\circ}\text{C}$
Si_3N_4	2.9 - 3.1	350	
$\text{RE}_2\text{Si}_2\text{O}_7$	3.8 - 9.5	130 - 155	
SiREMe Oxynitride			
IGF Glass	3.5 - 7 ⁺	120 - 165	850 - 1050

Surface Region of Si₃N₄ Ceramic with High RE Silicate Content Has Greater Thermal Expansion Coefficient



As-sinter-forged Si₃N₄ with
8 wt.% Lu₂O₃ + 2 wt.% SiO₂ with
~
200 μm surface layer.



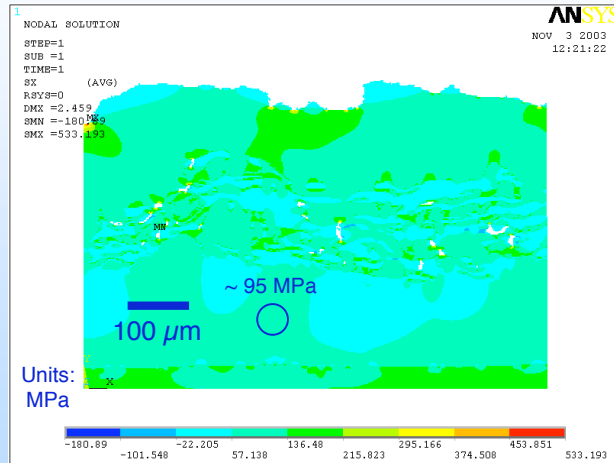
□-Si₃N₄ grains (dark) in a matrix
consisting of possibly two phases.
Two shades of gray indicate two Lu
levels (e.g., Lu₂SiO₅ vs. Lu₂Si₂O₇?) as
confirmed by EDS.

Linear Thermal Expansion Coefficient, ppm/°C

Si ₃ N ₄	2.9 - 3.1	RE Silicates	3.8 - 7+	Surface region	~ 4
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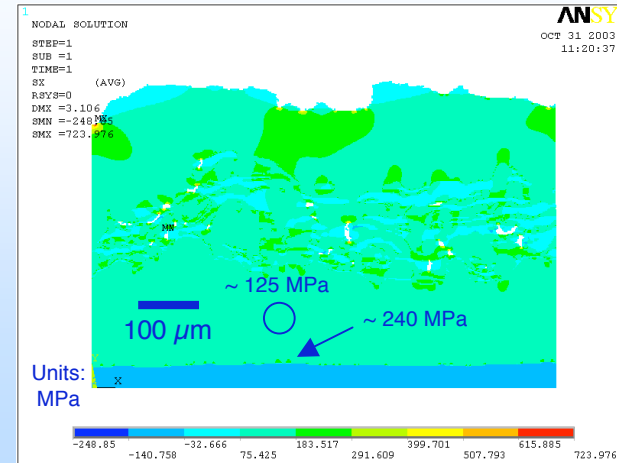
Reducing Residual Stress Fields in EBC-Si₃N₄ System by Surface Modification

CTE_{Si} = 4.0 ppm/C, CTE_{Si₃N₄} = 3.8 ppm/C

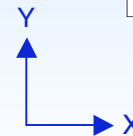
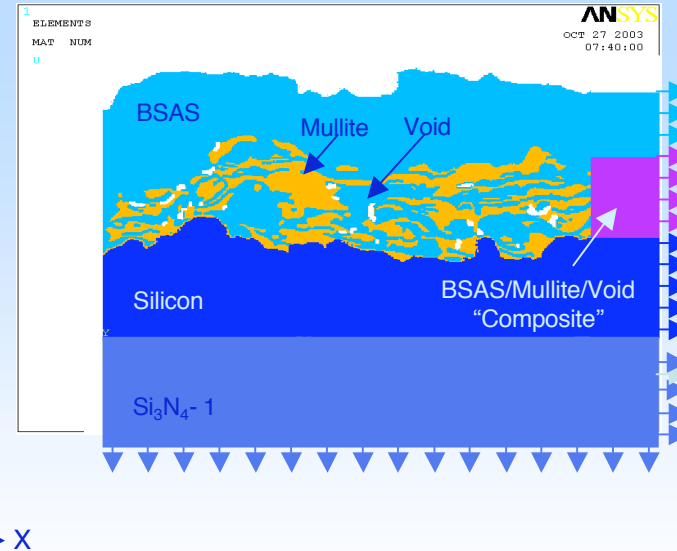
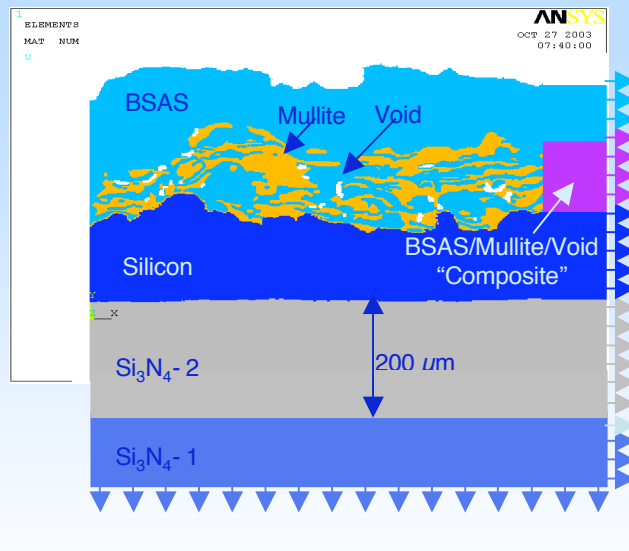


With tailored surface region

CTE_{Si} = 4.9 ppm/C, CTE_{Si₃N₄} = 2.9 ppm/C



Without tailored surface region



μ-FEA Reconstructed Model

Summary

- Can tailor the microstructure and mechanical properties of silicon nitride ceramics by selection of additives.
- Seeding used to control self-reinforced microstructure
- Additives influence grain growth and fracture properties
 - $\text{Si}_{6-z}\text{Al}_z\text{O}_z\text{N}_{8-z}$ formation with Al_2O_3 additions increase interface strength and reduce toughness as z increases.
 - Increasing RE segregation to Si_3N_4 surface sites: Lu \rightarrow La
 - Limits diametrical grain growth, which combined with
 - High E_{ad} leads to *decrease* in interface strength &
 - Increased toughness.
- Tailoring the composition of surface region of Si_3N_4 component may offer approach to improving EBC performance.