

## **Summary of AERMOD Implementation Workgroup (AIWG) Case Studies for 1-hour NO<sub>2</sub> and SO<sub>2</sub> NAAQS**

In 2011, EPA redirected the AERMOD Implementation Workgroup (AIWG) with a focus on the new 1-hour NO<sub>2</sub> and SO<sub>2</sub> NAAQS. The purpose of the workgroup was to provide insight into the potential challenges in modeling compliance under the new standards by working with “real world” examples. These examples would then provide a valuable basis to assess EPA’s existing guidance for NO<sub>2</sub> and SO<sub>2</sub> as well as indicate areas for new guidance. The AIWG workgroup was composed of over 50 members with EPA staff from the Regional offices and the Office of Air Quality Planning and Standards (OAQPS), and modelers from state, territorial, and local air quality agencies (see Table 4 for full list of members). The workgroup was co-chaired by Erik Snyder of Region 6 and James Thurman of OAQPS.

The workgroup was charged with completing its work in two phases:

1. Single source modeling case studies,
2. Cumulative modeling scenarios involving multiple facilities and background concentrations

For the first phase, the workgroup compiled a list of facilities that were of most interest to various state and local agencies. The workgroup began with an initial list of facility types and then workgroup members focused on those facility types that were of interest in their state or local area. Table 1 lists the final list of facility types that were modeled by the workgroup as part of the first phase.

**Table 1. Facilities, pollutants and modelers of single source modeling scenarios.**

Facility Type	Pollutant(s)	Modeler(s)
Secondary steel mill	NO <sub>2</sub>	Doris Jung (CO)
Ethanol plant	NO <sub>2</sub> , SO <sub>2</sub>	Dawn Froning (MO); Jennifer Krzak (IA)
Materials recycler	NO <sub>2</sub>	Steven Sherman (IN)
Natural gas turbine	NO <sub>2</sub>	Margaret Valis (NY); Bruce Ferguson (MS)
Coal fired EGU	NO <sub>2</sub> , SO <sub>2</sub>	Eric Milligan (OK); James Thurman (EPA-OAQPS)
Biomass facility	NO <sub>2</sub>	Dennis Becker (MN)
Natural gas processing plant	NO <sub>2</sub>	Krystin Bablinskas (AK); Andy Hawkins (EPA-R7)
Refinery	NO <sub>2</sub> , SO <sub>2</sub>	Glenn Reed (SJV); Leland Villalvazo (SJV)
Natural gas compressors	NO <sub>2</sub>	Ashley Mohr (EPA-R6); Erik Snyder (EPA-R6); Chiu Foong (EPA-R6)
Cement kiln	NO <sub>2</sub>	Dawn Froning (MO); Tracy Price (SC)
Landfill gas turbine	NO <sub>2</sub>	Lisa Landry (NH); Todd Moore (NH)
Fuel oil turbine	NO <sub>2</sub>	Haidar Al-Rawi (TN)
Pulp & paper	SO <sub>2</sub>	Leigh Bacon (AL); Jim Owen (AL)
Flare	SO <sub>2</sub>	Annamaria Coulter (EPA-R2)

For each modeled facility, emissions and source parameters were based on real facilities but were modified by the workgroup to be a generic facility type. For each facility type, there were several modeling scenarios such as addition of controls, changing stack height, varying fence-line distances, etc. Also for NO<sub>2</sub> sources, modeling scenarios involved comparing the use of the Plume Volume Molar Ratio Method (PVPRM) and Ozone Limiting Method (OLM) techniques within AERMOD as the approaches to model NO<sub>x</sub> to NO<sub>2</sub> conversion. Details about the modeling inputs for each scenario are provided for each facility type in Appendix A.

### Summary of findings

A listing of modeled sources with maximum design values for multiple scenarios can be found in Table 2 for NO<sub>2</sub> and Table 3 for SO<sub>2</sub>. A more detailed listing of maximum design values across scenarios for each modeled facility type can be found in Appendix A, which also contains spatial plots for several of the modeled sources. Based on the results of the modeling results, several preliminary observations have been made:

1. Many factors may contribute to NAAQS violations in addition to emissions levels. Other variables such as distance to ambient air (ethanol plant scenarios), urban/rural classification (NO<sub>2</sub> refinery and biomass facility), presence of terrain (refinery), meteorology, downwash influences, and stack heights can affect design value concentrations.

2. Short stacks and small facility footprints (SO<sub>2</sub> ethanol plant) can be problematic in attaining the NAAQS with violations occurring just beyond the fenceline. However, the area showing potential modeled violations in these cases may be very small.
3. In some cases the largest units in terms of emissions are not the major contributors to the maximum design values. Modeling scenarios where controls or stack height changes were made to the larger emitting stacks at times did not affect the maximum design value concentration, which were dominated by smaller units with short stacks (e.g., ethanol plant, coal fired EGU).
4. Increasing stack heights (within GEP regulations) for some sources with short stacks may be as effective as additional emission controls in eliminating modeled violations.
5. For NO<sub>2</sub>, modeling results highlight the importance of the use of the OLM or PVMRM Tier 3 options, the initial NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio, and input ozone background concentrations to modeled design values.

**Table 2. NO<sub>2</sub> modeling results**

Facility	Emissions (tpy)	Maximum DV ( $\mu\text{g}/\text{m}^3$ ) (ppb)	Sensitivity test	Maximum DV ( $\mu\text{g}/\text{m}^3$ ) (ppb)	Comments
Steel mill	Base: 711	318 (169) – OLM; < 1% receptors exceed	65 m stack ht (units > 1 g/s). Emissions unchanged.	250 (133) – PVMRM; 1 receptor exceeds	Sensitivity to NO <sub>x</sub> to NO <sub>2</sub> method
Ethanol plant	Base: 1,180	1,289 (685); 5% receptors exceed	NO <sub>2</sub> /NO <sub>x</sub> ratio 0.5, controls & increased stack ht on one unit; Emissions: 170 tpy	1,289 (685); 5% receptors exceed	50 m fenceline; no change in maximum DV with controls & stack ht increase
Materials recycler	Base: 70	401 (214); NO <sub>2</sub> /NO <sub>x</sub> ratio 0.2; < 1% receptors exceed	Stack ht increase (> 25 m); Emissions unchanged	17 (9)	Violations < 500 m for base case.
Natural gas turbine (NY)	Base: 450	145 (77)	Increase stack ht & controls (390 tpy)	122 (65)	No downwash
Natural gas turbine (MS)	Base: 450	16 (8)	Increase stack ht & controls (390 tpy)		No downwash
Coal EGU	Base 1,870	234 (125); < 1% receptors exceed	Stack ht increase, controls & higher exit velocity (610 tpy)	234 (125); < 1% receptors exceed	No change in maximum DV with controls & stack ht increase
Biomass facility	Base: 240	22 (11)	Stack height increase & no controls (1,220 tpy)	45 (24)	Sensitivities to urban/rural classification & NO <sub>x</sub> to NO <sub>2</sub> algorithm.
Natural gas processing plant	Uncontrolled: 3,190	1,440 (766); 60% receptors exceed	Increase stack ht & controls (330 tpy)	85 (45)	
Refinery	Base: 8,770	189 (100)	Increase stack ht & controls (5200 tpy)	171 (91)	
Natural gas compressors	Uncontrolled (4069)	1,674 (890); 21% receptors exceed;	Increase stack ht & controls (626 tpy)	43 (23)	Violations < 7 km
Cement kiln	Base: 7,170	44 (24)	Controls (2,180 tpy)	8 (4)	
Landfill gas turbine	Base: 80	29 (15)	Increase stack ht; emissions unchanged	4 (2)	
Fuel oil turbine	Less controlled: 2,230	484 (257); 1% receptors exceed	Increase stack ht & controls (1,190 tpy)	337 (179); < 1% receptors exceed	Violations < 2 km
Asphalt plant	Base: 188	470 (250); 20% receptors exceed	Increase stack ht & controls; daytime operation only (38 tpy)	162 (86)	Violations < 1 km; Maximum DV associated with ozone of 80 ppb.

**Table 3. SO<sub>2</sub> modeling results.**

Facility	Emissions (tpy)	Maximum DV ( $\mu\text{g}/\text{m}^3$ ) (ppb)	Sensitivity test	Maximum DV ( $\mu\text{g}/\text{m}^3$ ) (ppb)	Comments
Ethanol plant	Base: 890	296 (113); 1 receptor exceed	65 m stack ht & controls on one unit (195 tpy)	296 (113); 1 receptor exceed	Sensitivity to fenceline distance. 300 m fenceline – no exceedances
Coal EGU (OAQPS)	Uncontrolled: 10,713	905 (346); < 1% receptors exceed	Stack increase, controls & higher exit velocity; Emissions 2,074 tpy	33 (13)	Exceedances < 8km; stack ht=65 m
Coal EGU (OK)	Base: 4,959	48 (18)	Stack increase, controls & higher exit velocity; Emissions 2,074 tpy	28 (11)	
Refinery	Base: 4,020	272 (104)	Stack height increases; emissions unchanged	36 (14)	Sensitivity to urban/rural classification and terrain
Cement kiln	Base: 3,129	34 (13)	Controls; Emissions 348 tpy	4 (2)	
Pulp & paper	Base: 3,403	924 (353); 28% receptors exceed	Stack height increase & controls; Emissions 1,630	212 (81); < 1% receptors violate;	Exceedances < 4 km for base case; Exceedances < 1 km for stack ht increase & controls
Landfill gas turbine	Base: 45	17 (7)	Stack height increases; Emissions unchanged	2 (0.8)	
Fuel oil turbine	Base: 417	257 (98); < 1% receptors exceed;	Stack height increases; Emissions unchanged	178 (63)	Base case exceedances 0.5 to 1 km from source
Flare	Base: 6,083	324 (124); < 1% receptors exceed	65 m stack ht & controls; Emissions 626 tpy	9 (4)	Exceedances 6 to 7 km from source
Asphalt plant	Base: 13	3790 (1449); 27% receptors exceed	Increase stack hts; emissions unchanged	37 (14)	Exceedances < 1 km; results include downwash and continuous operations;

**Table 4. AERMOD Implementation Workgroup (AIWG) Members.**

Name	State	Region
Lisa Landry	NH	1
Todd Moore	NH	1
Ian Cohen	RO	1
Alan Dresser	NJ	2
Margaret Valis	NY	2
Elianeth Rivera	PR	2
Lucia Fernandez	PR	2
Annamaria Coulter	RO	2
Tim Leon-Guerrero	RO	3
Howard Schmidt	RO	3
Michael Kiss	VA	3
Robert Lute	VA	3
Jon McClung	WV	3
Jim Owen	AL	4
Leigh Bacon	AL	4
Cleve Holladay	FL	4
Melody Lovin	FL	4
Pete Courtney	GA	4
Bruce Ferguson	MS	4
Stan Krivo	RO	4
Tracy Price	SC	4
Eric McCann	TN	4
Haidar Al-Rawi	TN	4
Jeff Sprague	IL	5
Ken Ritter	IN	5
Steve Sherman	IN	5
Dennis Becker	MN	5
Ben Dutcher	OH-Dayton	5
Mary Portanova	RO	5
Randy Robinson	RO	5
Gail Good	WI	5

Name	State	Region
Yvette McGehee	LA	6
Eric Peters	NM	6
Eric Milligan	OK	6
Ashley Mohr	RO	6
Erik Snyder*	RO	6
Jennifer Krzak	IA	7
Sergio Guerra	KS	7
Assem Abdul	MO	7
Bern Johnson	MO	7
Dawn Froning	MO	7
Lisa Alam	NE	7
Andy Hawkins	RO	7
Doris Jung	CO	8
Cyra Cain	MT	8
Gail Tonnesen	RO	8
Josh Nall	WY	8
Glenn Reed	CA- SJV	9
Leland Villalvazo	CA- SJV	9
Ralph DeSiena	CA-San Diego	9
Steve Moore	CA-San Diego	9
Carol Bohnenkamp	RO	9
Scott Bohning	RO	9
Cleve Holladay	RO	9
Krystin Bablinskas	AK	10
Kevin Schilling	ID	10
Clint Bowman	WA	10
Ranil Dhammapala	WA	10
Jim Hodina	NA	NACAA
Misti Duvall	NA	NACAA
George Bridgers	NA	OAQPS
James Thurman*	NA	OAQPS
Roger Brode	NA	OAQPS
Tyer Fox	NA	OAQPS
* AIWG co-chairs		

# **Appendix A: Model Inputs for Phase 1 Case Studies**

Following are the model inputs for the various single source scenarios modeled by AIWG.

## **Steel mill**

Pollutant(s): NO<sub>2</sub>

Terrain: Yes

Meteorology: Alva, OK (2006-2010)

Ozone data: Oklahoma (2006-2010)

Scenarios:

1. Base
2. Increase in stack height to 45 for stack with emissions > 2 g/s (Stack ht 2)
3. Increase in stack height to 65 m for stacks with emissions > 2 g/s (Stack ht 3)

All scenarios modeled with 0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio and results were compared using OLM and PVMRM



Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)
C1423	POINT	2	21	530	0.001	2	45	65
C1424	POINT	2	21	530	0.001	2	45	65
C1520	POINT	2	20	310	2	12	45	65
C1521	POINT	4	34	380	8	5	45	65
C1523	POINT	0.5	12	480	0.01	1	12	12
C1524	POINT	0.00005	67	290	10	0.4	67	67
C1525	POINT	2	52	510	6	2	52	65
C1526	POINT	3	27	810	5	3	45	65
C1528	POINT	2	54	690	10	2	54	65
C1529	POINT	0.3	33	460	7	1	33	33
C1530	POINT	0.1	33	490	6	0.5	33	33
C1531	POINT	0.3	33	480	7	1	33	33

#### Steel mill volume sources

Source	Type	NOx (g/s)	Center of volume (m)	$\sigma_y$ (m)	$\sigma_z$ (m)
C1532	VOLUME	0.2	25	35	23
C1522	VOLUME	1	38	7	1
C1527	VOLUME	1	24	62	14

## Ethanol plant

Pollutant(s): NO<sub>2</sub>, SO<sub>2</sub>

Terrain: Yes

Meteorology: Moline, IL (2000-04), Springfield, MO (2005-09), St. Louis, MO (2005-09), and Waterloo, IA (2000-04)

Ozone: Moline: 0.067 ppm; Springfield, Hillcreset (2005-09); St. Louis, Maryland Heights (2005-09); Waterloo, 0.066 ppm

Scenarios (both pollutants):

1. Base
2. Increase stack height to 65 for C0004 (Stack ht 2)
3. Controlled emissions for C0004 with 65 m stack height (NO<sub>x</sub> 2 and SO<sub>2</sub> 2 with Stack ht 2)
4. Additional controls for C0004 with 65 m stack height (NO<sub>x</sub> 3 and SO<sub>2</sub> 3 with Stack ht 2)

All scenarios modeled with the following sensitivities:

1. 300 m vs. 50 m fenceline

Additionally for NO<sub>2</sub>, the following were modeled:

2. 0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio for all sources vs. 0.05 ratio for C0004 and 0.1 for other sources
3. 0.25 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio vs. 0.5 ratio for all sources (50 m fenceline only)

All scenarios modeled with four different meteorological datasets listed above.

Source	Type	NOx (g/s)	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	NOx 2 (g/s)	SO <sub>2</sub> 2 (g/s)	NOx 3 (g/s)	SO <sub>2</sub> 3 (g/s)
C0001	POINT	0.1	0.01	11	800	7	0.8	11	0.1	0.01	0.1	0.01
C0002	POINT	0.01	0.5	11	800	5	0.6	11	0.01	0.5	0.01	0.5
C0003	POINT	1.2	0.1	2	700	64	0.1	2	1.2	0.1	1.2	0.1
C0004	POINT	32	25	43	440	22	3	65	9	5	3	2.5

Ethanol plant volume source

Source	Type	NOx (g/s)	SO <sub>2</sub> (g/s)	Center of volume (m)	$\sigma_y$ (m)	$\sigma_z$ (m)
C0005	VOLUME	0.625401	0.005	25	2	16

## Materials recycler

Pollutant(s): NO<sub>2</sub>

Terrain: Flat

Meteorology: Indianapolis, IN (2006-10)

Scenarios:

1. Base
2. Increase stack heights #1 (Stack ht 2)
3. Increase stack heights #2 (Stack ht 3)

All scenarios modeled with 0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio, PVMRM, and 40 ppb ozone concentration.

Source	Type	NO <sub>x</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)
C0001	POINT	0.6	3	700	40	0.25	15	25
C0002	POINT	0.2	3	680	30	0.2	15	25
C0003	POINT	0.4	3	650	12	0.2	15	25
C0004	POINT	0.6	3.75	920	20	0.2	20	32
C0005	POINT	0.2	3	680	32	0.2	15	25

## Natural gas turbine

Pollutant(s): NO<sub>2</sub>

Terrain: Yes

Meteorology: NY – Poughkeepsie, NY (2006-10); MS – Mobile, AL (2005-09)

Ozone: NY – Millbrook, NY (2006-10); MS – Average seasonal/hour of day

Scenarios:

1. Base
2. Increase stack heights #1 (Stack ht 2)
3. Increase stack heights #2 (Stack ht 3)
4. Scenario 3 stack heights with controlled emissions (NO<sub>x</sub> 2 and Stack ht 3)

New York also modeled sensitivities

1. Base with 100% and 80% conversion
2. Base with OLM with 0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio (no downwash)
3. Scenarios 2-4 with PVMRM comparing 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio (with and without downwash) and 0.1 ratio (with downwash)

Mississippi modeled all scenarios with 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio and 0.1 ratio

Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)	NOx 2 (g/s)
C0001	POINT	3	25	700	25	4	45	65	2.4
C0002	POINT	3	25	700	25	4	45	65	2.4
C0003	POINT	3	25	700	25	4	45	65	2.4
C0004	POINT	1	25	400	12	3	45	45	1
C0005	POINT	1	25	400	12	3	45	45	1
C0006	POINT	1	25	400	12	3	45	45	1
C0007	POINT	1	25	400	12	3	45	45	1
H01	POINT	0.02	6	700	10	0.2	6	6	0.02
H02	POINT	0.02	6	700	10	0.2	6	6	0.02
H03	POINT	0.02	6	700	10	0.2	6	6	0.02

## Coal EGU

Pollutant(s): NO<sub>2</sub>, SO<sub>2</sub>

Terrain: Yes

Meteorology: OAQPS – Charleston, SC (2005-09); OK- Springfield, MO (2006-10)

Ozone: OAQPS – Spartanburg, SC; OK – NEOF (2006-10)

Scenarios:

1. Base
2. Increase stack heights #1 (Stack ht 2)
3. Controlled emissions with base stack heights (NO<sub>x</sub> 2 and SO<sub>2</sub> 2 with Stack ht 1)
4. Scenario 2 stack heights with controlled emissions (NO<sub>x</sub> 2 and SO<sub>2</sub> 2 and Stack ht 2)
5. Scenario 3 emissions with further increase in stack ht (NO<sub>x</sub> 2 and SO<sub>2</sub> 2 and Stack ht 3)
6. Scenario 5 with higher exit velocity and new diameter ((NO<sub>x</sub> 2 and SO<sub>2</sub> 2, Stack ht 3, Stack velocity 2 and Diameter 2)

Note, controlled emissions for Oklahoma modeling for SO<sub>2</sub> were 112 g/s. OAPQS also modeled all NO<sub>2</sub> scenarios with 100% and 80% conversion. OAQPS also modeled all SO<sub>2</sub> scenarios with uncontrolled emissions (290 g/s) for C0001. For SO<sub>2</sub>, OAQPS modeled the base scenario with a 65 m stack height for base emissions and uncontrolled emissions.

Source	Type	NOx (g/s)	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)	NOx 2 (g/s)	SO <sub>2</sub> 2 (g/s)	Stack velocity 2 (m/s)	Diameter 2 (m)
C0001	POINT	45	140	150	350	25	7	200	250	9	57	30	6
C0002	POINT	5	2.5	100	600	20	2	140	25	5	2.5	30	1.5
C0003	POINT	3	0.125	6	700	45	0.3	6	25	3	0.125	45	0.3
C0004	POINT	0.3	0.02	5	700	45	0.15	5	25	0.3	0.02	45	0.15
C0005	POINT	0.3	0.01	5	700	45	0.15	5	25	0.3	0.01	45	0.15

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## Biomass facility

Pollutant(s): NO<sub>2</sub>

Terrain: Flat

Meteorology: Twin-Cities, MN (2006-10);

Ozone: 40 ppb

Scenarios:

1. Base
2. Increase stack heights #1 (Stack ht 2)
3. Scenario 2 stack heights with no controls on emissions ( NO<sub>x</sub> 2 and Stack ht 2)

All three scenarios were also modeled with the following sensitivities:

1. Urban vs. rural
2. 100% and 80% conversion
3. OLM vs. PVMRM with 0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio
4. OLM vs. PVMRM with 0.15 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Source	Type	NO <sub>x</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	NO <sub>x</sub> 2 (g/s)
C0001	POINT	7	55	400	18	2	80	35
C0002	POINT	0.01	9	780	105	0.2	9	0.01
C0003	POINT	0.01	9	710	52	0.2	9	0.01

## Natural gas processing plant

Pollutant(s): NO<sub>2</sub>

Terrain: Flat

Meteorology: Barrow, AK (2001-05)

Ozone: AK hourly data and 40 and 80 ppb constant concentrations

Scenarios:

1. Base
2. Increase stack heights #1 (Stack ht 2)
3. Increase stack heights #2 (Stack ht 3)
4. Increase stack heights #3 (Stack ht 4)
5. Base stack parameters with uncontrolled emissions (NO<sub>x</sub> 2 and Stack ht 1)

All scenarios modeled with PVMRM with the following in-stack ratios:

1. 0.1 vs. 0.25

The base scenario was also modeled with a 0.25 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio and using a constant ozone concentration of 40 vs. 80 ppb.

Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)	Stack ht 4 (m)	NOx 2 (g/s)
C0001	POINT	0.1	6	530	3	0.6	6	6	6	1
C0002	POINT	1	8	650	19	1	17	35	55	10
C0003	POINT	0.5	7	830	26	0.3	7	35	55	5
C0004	POINT	1	8	650	19	1	17	35	55	10
C0005	POINT	1	8	730	37	0.4	17	35	55	10
C0006	POINT	1	8	650	19	1	17	35	55	10
C0007	POINT	0.7	6	840	35	0.3	17	35	55	7
C0008	POINT	1	7	730	39	0.3	17	35	55	10
C0009	POINT	1	8	730	37	0.4	17	35	55	10
C0010	POINT	0.6	7	720	33	0.3	17	35	55	6
C0011	POINT	0.6	7	720	33	0.3	17	35	55	6
C0012	POINT	0.6	7	720	33	0.3	17	35	55	6
C0013	POINT	0.01	6	530	2	0.2	6	6	6	0.01
C0014	POINT	0.04	17	1280	20	0.4	17	17	17	0.04
C0015	POINT	0.1	6	530	4	1	6	6	6	0.1
C0016	POINT	0.2	6	530	3	1	6	6	6	0.2

## Refinery

Pollutant(s): NO<sub>2</sub>, SO<sub>2</sub>

Terrain: Flat, Elevated

Meteorology: Bakersfield, CA (2005-09)

Ozone: Bakersfield, CA (2005-09)

Scenarios:

For NO<sub>2</sub>:

1. Base
2. Stack height increase #1 (Stack ht 2)
3. Stack height increase #2 (Stack ht 3)
4. Controlled emissions with base stack heights (NO<sub>x</sub> 2 and Stack ht 1)
5. Controlled emissions with Scenario 3 stack heights (NO<sub>x</sub> 2 and Stack ht 3)

All scenarios were modeled comparing OLM vs. PVMRM and flat vs. including terrain. The NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio was 0.1

For SO<sub>2</sub>:

1. Base
2. Stack height increase #1 (Stack ht 2)
3. Stack height increase #2 (Stack ht 3)

4. Uncontrolled emissions with Scenario 3 stack heights (NO<sub>x</sub> 2 and Stack ht 3)

5. Uncontrolled emissions with base stack heights (NO<sub>x</sub> 2 and Stack ht 3)

All SO<sub>2</sub> scenarios were modeled comparing urban vs. rural dispersion and flat vs. use of terrain.

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NO<sub>2</sub> refinery emissions

Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2(m)	Stack ht 3(m)	NOx 2 (g/s)
C0001	POINT	12	12	500	9	3	45	65	2.4
C0002	POINT	12	12	500	9	3	45	65	2.4
C0003	POINT	17	18	500	10	3	45	65	3.4
C0004	POINT	17	18	510	10	3	45	65	3.4
C0005	POINT	6	29	470	23	4	29	45	6
C0006	POINT	0.2	29	400	2	2	29	29	0.2
C0007	POINT	0.2	29	400	2	2	29	29	0.2
C0008	POINT	0.2	29	400	2	2	29	29	0.2
C0009	POINT	1	78	1300	20	4	78	78	1
C0010	POINT	0.1	48	500	4	0.7	48	48	0.1
C0011	POINT	0.04	48	500	5	0.5	48	48	0.04
C0012	POINT	6	49	510	12	3	49	49	6
C0013	POINT	4	45	510	10	3	45	45	4
C0014	POINT	2	45	600	6	2	45	45	2
C0015	POINT	1	41	640	5	2	41	41	1
C0016	POINT	2	47	650	8	2	47	47	2
C0017	POINT	0.5	41	650	3	2	41	41	0.5
C0018	POINT	17	76	480	25	2	76	76	3.4
C0019	POINT	1	30	700	12	1	30	30	1
C0020	POINT	0.5	30	700	7	1	30	30	0.5
C0021	POINT	1	54	700	9	2	54	54	1
C0022	POINT	1	44	550	6	0.7	44	44	1
C0023	POINT	19	54	560	50	2	54	65	3.8
C0024	POINT	3	24	440	25	2	24	24	3
C0025	POINT	2	18	400	13	2	18	18	2

Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2(m)	Stack ht 3(m)	NOx 2 (g/s)
C0026	POINT	2	24	440	24	2	24	24	2
C0027	POINT	2	34	500	7	2	34	34	2
C0028	POINT	0.5	42	540	7	1	42	42	0.5
C0029	POINT	7	78	490	11	3	78	78	7
C0030	POINT	1	61	700	30	1	61	61	1
C0031	POINT	1	61	680	30	1	61	61	1
C0032	POINT	0.5	41	583	5	1	41	41	0.5
C0033	POINT	1	76	1300	20	0.3	76	76	1
C0034	POINT	2	0	1300	20	0.3	0	0	2
C0035	POINT	1	76	1300	20	0.3	76	76	1
C0036	POINT	1	76	1300	20	0.3	76	76	1
C0037	POINT	2	76	1300	20	0.4	76	76	2
C0038	POINT	1	76	1300	20	0.4	76	76	1
C0039	POINT	0.5	69	1300	20	1	69	69	0.5
C0040	POINT	2	49	620	9	2	49	49	2
C0041	POINT	2	49	590	9	2	49	49	2
C0042	POINT	1	49	570	5	2	49	49	1
C0043	POINT	1	49	600	5	2	49	49	1
C0044	POINT	3	55	560	8	3	55	55	3
C0045	POINT	0.5	34	600	3	2	34	34	0.5
C0046	POINT	0.5	34	620	3	2	34	34	0.5
C0047	POINT	0.2	0	250	0	0	0	0	0.2
C0048	POINT	8	49	470	27	4	49	49	8
C0049	POINT	1	34	850	9	2	34	34	1
C0050	POINT	1	34	1000	10	2	34	34	1
C0051	POINT	1	55	620	6	3	55	55	1
C0052	POINT	1	60	570	6	2	60	60	1

Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2(m)	Stack ht 3(m)	NOx 2 (g/s)
C0053	POINT	11	31	530	34	2	45	31	2.2
C0054	POINT	1	30	750	20	1	30	30	1
C0055	POINT	0.5	30	760	7	1	30	30	0.5
C0056	POINT	0.5	40	505	5	2	40	40	0.5
C0057	POINT	2	56	530	6	3	56	56	2
C0058	POINT	2	56	520	6	3	56	56	2
C0059	POINT	11	108	450	12	4	108	108	2.2
C0060	POINT	2	60	570	12	2	60	60	2
C0061	POINT	2	46	500	27	1	46	46	2
C0062	POINT	2	46	500	27	1	46	46	2
C0063	POINT	2	46	500	27	1	46	46	2
C0064	POINT	0.3	44	600	12	1	44	44	0.3
C0065	POINT	0.5	63	500	12	1	63	63	0.5
C0066	POINT	0.2	43	490	12	1	43	43	0.2
C0067	POINT	0.4	42	600	12	1	42	42	0.4
C0068	POINT	3	81	500	6	3	81	81	3
C0069	POINT	3	81	500	6	3	81	81	3
C0070	POINT	3	81	500	6	3	81	81	3
C0071	POINT	4	68	480	10	3	68	68	4
C0072	POINT	1	46	480	10	1	46	46	1
C0073	POINT	2	61	430	10	1	61	61	2
C0074	POINT	1	46	680	14	1	46	46	1
C0075	POINT	3	37	520	39	2	37	37	3
C0076	POINT	3	37	520	40	2	37	37	3
C0077	POINT	3	37	520	39	2	37	37	3
C0078	POINT	0.1	16	580	12	0.3	16	16	0.1
C0079	POINT	5	30	750	14	2	30	45	5



Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2(m)	Stack ht 3(m)	NOx 2 (g/s)
C0080	POINT	12	29	790	9	3	45	65	2.4
C0081	POINT	0.02	1	700	17	0.2	1	1	0.02
C0082	POINT	0.03	1	700	17	0.2	1	1	0.03
C0083	POINT	0.02	1	700	17	0.2	1	1	0.02
C0084	POINT	0.5	34	600	3	2	34	34	0.5

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SO<sub>2</sub> refinery emissions

Source	Type	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 1 (m)	Stack ht 1 (m)	SO <sub>2</sub> 2 (g/s)
C0001	POINT	0.3	14	480	6	2	14	14	0.3
C0002	POINT	0.3	14	480	6	2	14	14	0.3
C0003	POINT	0.5	46	600	6	3	46	46	0.5
C0006	POINT	0.4	39	780	5	2	39	39	0.4
C0007	POINT	0.2	46	670	5	3	46	46	0.2
C0009	POINT	0.03	22	480	4	1	22	22	0.03
C0010	POINT	0.06	45	480	3	2	45	45	0.06
C0011	POINT	0.08	43	480	4	2	43	43	0.08
C0015	POINT	0.12629	46	450	8	2	46	46	0.12629
C0017	POINT	0.2	52	480	14	1	52	52	0.2
C0018	POINT	0.3	45	480	6	2	45	45	0.3
C0020	POINT	0.05	14	500	4	2	14	14	0.05
C0024	POINT	0.1	46	480	8	1	46	46	0.1
C0029	POINT	1	58	500	7	1	58	65	1
C0030	POINT	2	58	500	7	1	58	65	2
C0031	POINT	0.3	32	1100	4	2	32	32	0.3
C0034	POINT	0.08	50	480	7	2	50	50	0.08
C0035	POINT	0.08	50	480	7	2	50	50	0.08
C0036	POINT	0.4	66	480	13	3	66	66	0.4
C0037	POINT	0.2	66	480	13	3	66	66	0.2
C0041	POINT	0.0003	9	1000	4	1	9	9	0.0003
C0043	POINT	4	58	500	12	2	58	65	50
C0044	POINT	0.000288	66	1270	20	5	66	66	0.000288
C0045	POINT	0.2	46	450	5	3	46	46	0.2
C0046	POINT	0.2	46	450	5	3	46	46	0.2

Source	Type	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 1 (m)	Stack ht 1 (m)	SO <sub>2</sub> 2 (g/s)
C0048	POINT	0.01	23	1100	7	2	23	23	0.01
C0057	POINT	4	58	500	12	2	58	65	50
C0061	POINT	0.2	34	700	12	2	34	34	0.2
C0063	POINT	3	46	1270	20	14	46	65	3
C0064	POINT	0.3	46	1270	20	4	46	46	0.3
C0066	POINT	0.1	46	450	4	2	46	46	0.1
C0068	POINT	0.0003	18	1100	18	2	18	18	0.0003
C0069	POINT	0.0003	18	1100	18	2	18	18	0.0003
C0072	POINT	0.03	34	770	3	1	34	34	0.03
C0073	POINT	0.1	34	600	2	2	34	34	0.1
C0074	POINT	0.05	34	620	1	2	34	34	0.05
C0076	POINT	0.06	30	610	6	1	30	30	0.06
C0077	POINT	0.04	31	580	2	1	31	31	0.04
C0078	POINT	0.04	31	580	2	1	31	31	0.04
C0081	POINT	2	61	480	18	3	61	65	2
C0086	POINT	0.2	61	480	18	3	61	61	0.2
C0087	POINT	2	38	430	24	4	50	65	2
C0088	POINT	0.2	32	420	12	2	32	32	0.2
C0089	POINT	0.2	32	420	12	2	32	32	0.2
C0090	POINT	0.0004	1	250	0	0	1	1	0.0004

SO<sub>2</sub> refinery volume sources

Source	Type	SO <sub>2</sub> (g/s)	Center of volume (m)	$\sigma_y$ (m)	$\sigma_z$ (m)
C0004	VOLUME	0.00002	1	19	0.4
C0005	VOLUME	0.00002	1	5	0.4
C0008	VOLUME	0.00002	1	15	0.4
C0012	VOLUME	0.00002	1	12	0.4
C0013	VOLUME	0.00002	1	11	0.4
C0014	VOLUME	0.00002	1	11	0.4
C0016	VOLUME	0.00002	1	15	0.4
C0019	VOLUME	0.00002	1	23	0.4
C0021	VOLUME	0.00002	1	9	0.4
C0022	VOLUME	0.00002	1	24	0.4
C0023	VOLUME	0.00002	1	24	0.4
C0025	VOLUME	0.00002	1	11	0.4
C0026	VOLUME	0.00002	1	9	0.4
C0027	VOLUME	0.00002	1	16	0.4
C0028	VOLUME	0.00002	1	16	0.4
C0032	VOLUME	0.00002	1	14	0.4
C0033	VOLUME	0.00002	1	25	0.4
C0038	VOLUME	0.00002	1	17	0.4
C0039	VOLUME	0.00002	1	17	0.4
C0040	VOLUME	0.00002	1	7	0.4
C0042	VOLUME	0.00002	1	18	0.4
C0047	VOLUME	0.00002	1	39	0.4
C0049	VOLUME	0.00002	1	23	0.4
C0050	VOLUME	0.00002	1	23	0.4
C0051	VOLUME	0.00002	1	6	0.4
C0052	VOLUME	0.00002	1	18	0.4

Source	Type	SO <sub>2</sub> (g/s)	Center of volume (m)	$\sigma_y$ (m)	$\sigma_z$ (m)
C0053	VOLUME	0.00002	1	20	0.4
C0054	VOLUME	0.00002	1	20	0.4
C0055	VOLUME	0.00002	1	20	0.4
C0056	VOLUME	0.00002	1	20	0.4
C0058	VOLUME	0.00002	1	5	0.4
C0059	VOLUME	0.00002	1	6	0.4
C0060	VOLUME	0.00002	1	14	0.4
C0062	VOLUME	0.00002	1	13	0.4
C0065	VOLUME	0.00002	1	17	0.4
C0067	VOLUME	0.00002	1	25	0.4
C0070	VOLUME	0.00002	1	14	0.4
C0071	VOLUME	0.00002	1	9	0.4
C0075	VOLUME	0.00002	1	14	0.4
C0079	VOLUME	0.00002	1	9	0.4
C0080	VOLUME	0.00002	1	9	0.4
C0082	VOLUME	0.000009	1	20	0.4
C0083	VOLUME	0.000006	1	35	0.4
C0084	VOLUME	0.000006	1	35	0.4
C0085	VOLUME	0.000006	1	35	0.4

## Natural gas compressors

Pollutant(s): NO<sub>2</sub>

Terrain: Yes

Meteorology: Austin, TX (1983-84; 1986-88)

Ozone: NEOKN

Scenarios:

1. Base
2. Less controls for 3 of 4 stations and stack height increase #2 (NO<sub>x</sub> 2 and stack ht 3)
3. Stack height increase #1 (Stack ht 2)
4. Stack height increase #2 (Stack ht 3)
5. Less controls for 3 of 4 stations and base stack heights (NO<sub>x</sub> 3 and stack ht 1)

All scenarios modeled with 0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio and PVMRM

Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	NOx 2 (g/s)	Stack ht 2 (m)	Stack ht 3 (m)	NOx 3 (g/s)
F1C001	POINT	0.1	8	900	39	0.4	2.8	35	17	2.8
F1C002	POINT	0.1	8	900	39	0.4	2.8	35	17	2.8
F1C003	POINT	0.1	8	900	39	0.4	2.8	35	17	2.8
F1C004	POINT	0.1	8	900	39	0.4	2.8	35	17	2.8
F1C005	POINT	0.1	8	900	39	0.4	2.8	35	17	2.8
F1C006	POINT	0.01	4	800	3	1	0.01	4	4	0.01
F1C007	POINT	0.01	4	500	5	0.3	0.01	4	4	0.01
F1C008	POINT	0.01	4	500	5	0.3	0.01	4	4	0.01
F1C009	POINT	0.03	9	1000	9	0.7	0.03	9	9	0.03
F2C001	POINT	1	8	900	31	0.4	2.8	35	17	2.8
F2C002	POINT	1	8	900	31	0.4	2.8	35	17	2.8
F2C003	POINT	1	8	900	31	0.4	2.8	35	17	2.8
F2C004	POINT	1	8	900	31	0.4	2.8	35	17	2.8
F2C005	POINT	1	8	900	31	0.4	2.8	35	17	2.8
F2C006	POINT	1	8	900	31	0.4	2.8	35	17	2.8
F2C007	POINT	0.4	8	900	31	0.4	2.8	35	17	2.8
F2C008	POINT	0.4	8	900	31	0.4	2.8	35	17	2.8
F2C009	POINT	0.4	8	900	31	0.4	2.8	35	17	2.8
F2C010	POINT	0.4	8	900	31	0.4	2.8	35	17	2.8
F2C011	POINT	1	8	900	31	0.4	2.8	35	17	1
F2C012	POINT	0.1	8	800	20	0.1	0.1	35	17	0.1
F2C013	POINT	0.01	5	800	6	0.2	0.01	5	5	0.01
F2C014	POINT	0.01	5	800	6	0.2	0.01	5	5	0.01
F2C015	POINT	0.01	5	800	6	0.2	0.01	5	5	0.01
F2C016	POINT	0.01	5	800	6	0.2	0.01	5	5	0.01
F3C001	POINT	0.4	11	700	34	0.5	5.2	35	17	5.2
F3C002	POINT	0.4	11	700	34	0.5	5.2	35	17	5.2

Source	Type	NOx (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	NOx 2 (g/s)	Stack ht 2 (m)	Stack ht 3 (m)	NOx 3 (g/s)
F3C003	POINT	0.4	11	700	34	0.5	5.2	35	17	5.2
F3C004	POINT	0.4	11	700	34	0.5	5.2	35	17	5.2
F3C005	POINT	0.4	11	700	34	0.5	5.2	35	17	5.2
F3C006	POINT	0.4	11	700	34	0.5	5.2	35	17	5.2
F3C007	POINT	0.4	12	700	34	0.5	5.2	35	17	5.2
F3C008	POINT	0.4	12	700	34	0.5	5.2	35	17	5.2
F3C009	POINT	0.3	12	700	34	0.5	5.9	35	17	5.9
F3C010	POINT	0.3	12	700	34	0.5	5.9	35	17	5.9
F3C011	POINT	0.3	12	700	43	0.5	7.9	35	17	7.9
F3C012	POINT	0.3	12	700	43	0.5	7.9	35	17	7.9
F3C013	POINT	0.01	3	500	3	0.3	0.01	3	3	0.01
F3C014	POINT	0.01	3	500	3	0.3	0.01	3	3	0.01
F3C015	POINT	0.01	3	500	3	0.3	0.01	3	3	0.01
F3C016	POINT	0.003	3	500	3	0.3	0.003	3	3	0.003
F4C001	POINT	0.4	11	700	44	0.5	0.4	35	17	0.4
F4C002	POINT	0.3	12	700	34	0.5	0.3	35	17	0.3
F4C003	POINT	0.3	12	700	34	0.5	0.3	35	17	0.3
F4C004	POINT	0.5	14	700	45	0.5	0.5	35	14	0.5
F4C005	POINT	0.5	14	700	45	0.5	0.5	35	14	0.5
F4C006	POINT	0.5	14	700	45	0.5	0.5	35	14	0.5
F4C007	POINT	0.5	14	700	45	0.5	0.5	35	14	0.5
F4C008	POINT	0.3	14	700	45	0.5	0.3	35	14	0.3
F4C009	POINT	0.3	14	700	45	0.5	0.3	35	14	0.3
F4C010	POINT	0.3	14	700	34	0.5	0.3	35	14	0.3
F4C011	POINT	0.3	14	700	34	0.5	0.3	35	14	0.3
F4C012	POINT	0.003	3	500	4	0.3	0.003	3	3	0.003
F4C013	POINT	0.01	3	500	5	0.3	0.01	3	3	0.01



## **Cement kiln**

Pollutant(s): NO<sub>2</sub>, SO<sub>2</sub>

Terrain: Yes

Meteorology: Charleston, SC (2002-06)

Ozone: Spartanburg, SC (2002-06)

Scenarios (both pollutants):

1. Base
2. Controls (NO<sub>x</sub> 2 and SO<sub>2</sub> 2)
3. Additional controls (NO<sub>x</sub> 3 and SO<sub>2</sub> 3)

NO<sub>2</sub> base scenario modeled with PVMRM and:

1. Comparison of NO<sub>2</sub>/NO<sub>x</sub> in-stack ratios of 0.05, 0.1, 0.25, and 0.5
2. Comparison of ozone concentrations of 40 and 80 ppb with NO<sub>2</sub>/NO<sub>x</sub> ratio of 0.1

Scenario 2 modeled with NO<sub>2</sub>/NO<sub>x</sub> in-stack ratios of 0.05 and 0.1

Scenario 3 modeled with NO<sub>2</sub>/NO<sub>x</sub> ratios of 0.05, 0.1, 0.25, and 0.5

Source	Type	NOx (g/s)	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	NOx 1 (g/s)	NOx 2 (g/s)	SO <sub>2</sub> 2 (g/s)	SO <sub>2</sub> 3 (g/s)
C0001	POINT	190	75	160	375	16	6	57	25	25	8
C0002	POINT	15	15	160	360	12	2.5	5	2	5	2
C0003	POINT	0.2	0	90	375	17	2	0.2	0.2		
C0004	POINT	0.2	0	90	375	17	2	0.2	0.2		

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### Landfill gas turbine

Pollutant(s): NO<sub>2</sub>, SO<sub>2</sub>

Terrain: Yes

Meteorology: Pease AFB, NH (2000-04)

Ozone: 40 ppb

Scenarios (both pollutants):

1. Base
2. Stack height increase #1 (Stack ht 2)
3. Stack height increase #2 (Stack ht 3)

For NO<sub>2</sub>, comparisons were made for PVMRM with NO<sub>2</sub>/NO<sub>x</sub> in-stack ratios of 0.05 and 0.1 for all scenarios

Source	Type	NO <sub>x</sub> (g/s)	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)
C0001	POINT	0.6	0.4	13	600	27	1.3	35	65
C0002	POINT	0.6	0.4	13	600	27	1.3	35	65
C0003	POINT	0.6	0.4	13	600	27	1.3	35	65
C0004	POINT	0.5	0.1	10	700	3.5	1.5	30	65

## Fuel oil turbine

Pollutant(s): NO<sub>2</sub>, SO<sub>2</sub>

Terrain: Yes

Meteorology: Bristol, TN (2004-08)

Ozone: 60 ppb and Sullivan County, TN (2004-08)

NO<sub>2</sub> Scenarios:

1. Base
2. Stack height increase #1 (Stack ht 2)
3. Stack height increase #2 (Stack ht 3)
4. Scenario 3 heights with increased emissions (NO<sub>x</sub> 2 and Stack ht 3)

All NO<sub>2</sub> scenarios also compared:

1. OLM with 60 ppb ozone concentrations with NO<sub>2</sub>/NO<sub>x</sub> in-stack ratios of 0.05 and 0.1
2. PVMRM with 60 ppb ozone concentrations with NO<sub>2</sub>/NO<sub>x</sub> in-stack ratios of 0.05 and 0.1
3. PVMRM with actual ozone concentrations with NO<sub>2</sub>/NO<sub>x</sub> in-stack ratios of 0.05 and 0.1

SO<sub>2</sub> scenarios:

1. Base
2. Stack height increase #1 (Stack ht 2)

### 3. Stack height increase #2 (Stack ht 3)

Source	Type	NOx (g/s)	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)	NOx 2 (g/s)
C0001	POINT	10	4	25	700	25	4	45	65	20
C0002	POINT	10	4	25	700	25	4	45	65	20
C0003	POINT	10	4	25	700	25	4	45	65	20
C0004	POINT	1	0	25	400	12	3	45	45	1
C0005	POINT	1	0	25	400	12	3	45	45	1
C0006	POINT	1	0	25	400	12	3	45	45	1
C0007	POINT	1	0	25	400	12	3	45	45	1
H01	POINT	0.02	0	6	700	10	0.2	6	6	0.02
H02	POINT	0.02	0	6	700	10	0.2	6	6	0.02
H03	POINT	0.02	0	6	700	10	0.2	6	6	0.02

## **Asphalt plant**

Pollutant(s): NO<sub>2</sub>, SO<sub>2</sub>

Terrain: Yes

NO<sub>2</sub> Meteorology: San Juan, NM (1993)

SO<sub>2</sub> Meteorology: Alva, OK (2010), Boise, ID (2005), Empire Abo, NM (1993-1994), San Juan, NM (1993), Val Verde, NM (1993)

Ozone: San Juan (1993-1994), 40 and 60 ppb

NO<sub>2</sub> & SO<sub>2</sub> scenarios:

1. Base
2. Stack height increase #1 (Stack ht 2)
3. Stack height increase #2 (Stack ht 3)
4. Stack height increase #1 with controls (NO<sub>2</sub> only) (Stack ht 2 + NO<sub>x</sub> 2)

All scenarios for both pollutants modeled as continuous and daytime operations (12 hour operation). All NO<sub>2</sub> scenarios also modeled as continuous operations with 40 and 60 ppb ozone concentrations. All SO<sub>2</sub> scenarios modeled with and without downwash for continuous operations (no downwash for daytime operations for SO<sub>2</sub>). Base scenario for SO<sub>2</sub> also modeled with alternate fuel (0.5 % sulfur content)

Source	Type	NOx (g/s)	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)	NOx 2 (g/s)
C0001	POINT	4	0.07	6	400	25	0.9	25	45	0.8
C0002	POINT	0.1	0.3	0.3	800	30	0.2	5	15	0.1
C0003	POINT	1.4	0.01	3	650	85	0.3	3	3	1.4

DRAFT

## Pulp & paper

Pollutant(s): SO<sub>2</sub>

Terrain: Yes

Meteorology: Mobile, AL (2001-05)

Scenarios:

1. Base
2. Increase stack height #1 (Stack ht 2)
3. Increase stack height #2 (Stack ht 3)
4. Scenario 3 stack heights and controlled emissions (SO<sub>2</sub> 2 and Stack ht 3)

Source	Type	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)	SO <sub>2</sub> 2 (g/s)
C0001	POINT	2	30	350	13	1.3	45	65	2
C0002	POINT	8	30	340	7	1.4	45	65	8
C0003	POINT	7	29	350	7	2	45	65	7
C0004	POINT	28	85	460	12	5	120	120	8
C0005	POINT	28	85	460	12	5	120	120	8
C0006	POINT	5	72	440	17	2.5	120	120	5
C0007	POINT	5	72	440	17	2.5	120	120	5
C0008	POINT	14	76	350	12	4	120	120	3
C0009	POINT	0.5	8	483	0	0.4	8	8	0.5
C0010	POINT	0.2	67	350	9	1	67	67	0.2
C0011	POINT	0.2	67	350	9	1	67	67	0.2



## Flare

Pollutant(s): SO<sub>2</sub>

Terrain: Yes

Meteorology: Poughkeepsie, NY (2006-10)

Scenarios:

1. Base
2. Increase stack height #1 (Stack ht 2)
3. Increase stack height #2 (Stack ht 3)
4. Scenario 3 stack heights and controlled emissions (SO<sub>2</sub> 2 and Stack ht 3)

Source	Type	SO <sub>2</sub> (g/s)	Stack ht 1 (m)	Stack temperature (K)	Stack velocity (m/s)	Diameter (m)	Stack ht 2 (m)	Stack ht 3 (m)	SO <sub>2</sub> 2 (g/s)
FLARE	POINT	175	25	1000	45	2.69	45	65	18

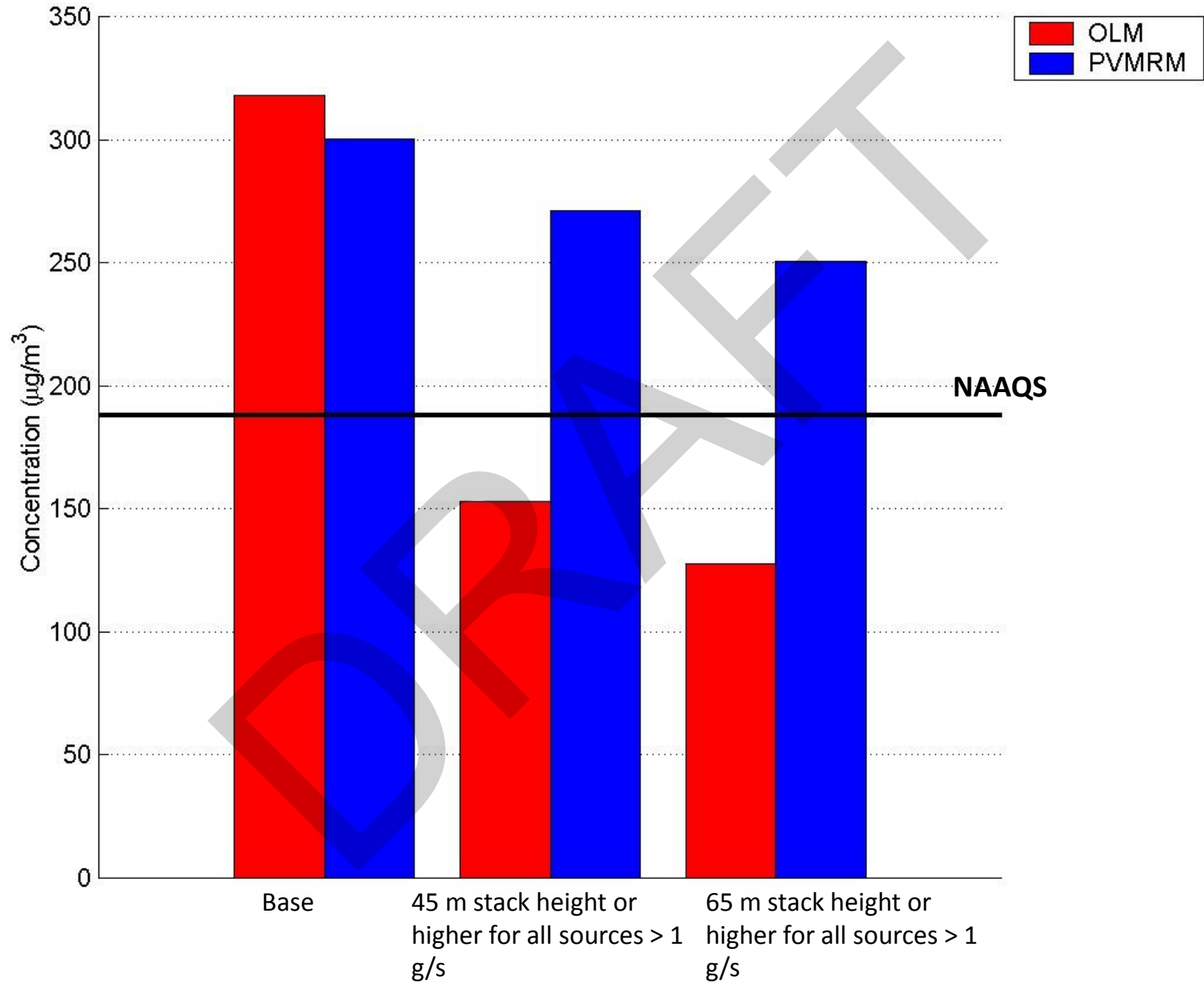
# Appendix B: AIWG Phase 1 Results

## Single Source Case Studies

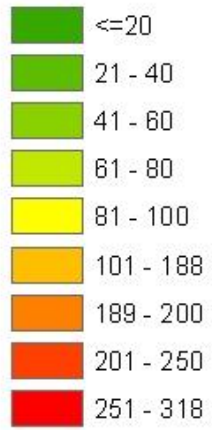
NO<sub>2</sub> results

DRAFT

# Steel Mill: NO<sub>2</sub>

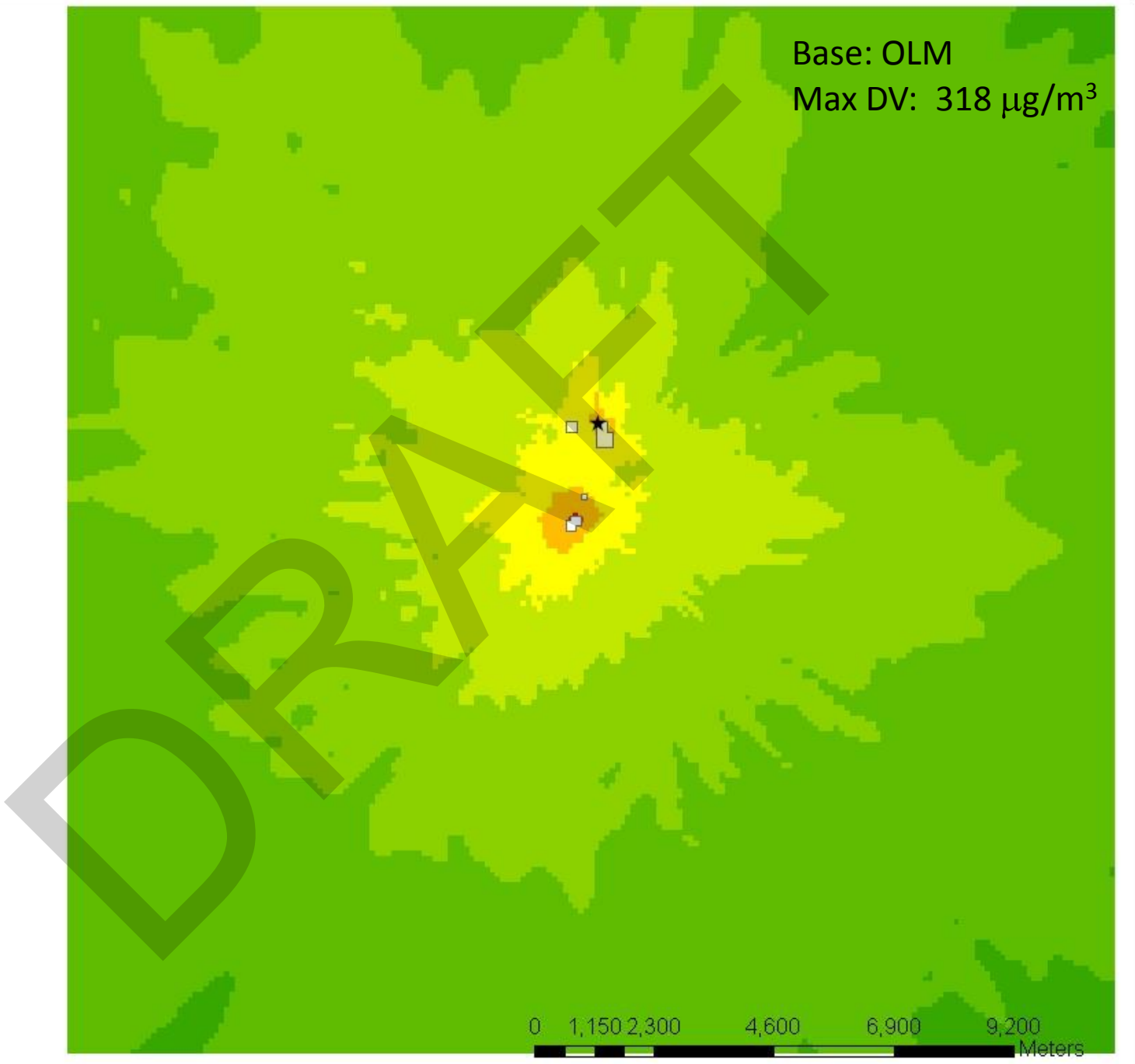


# Legend



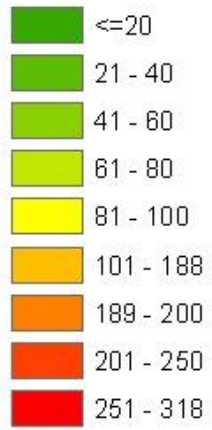
Base: OLM

Max DV: 318  $\mu\text{g}/\text{m}^3$

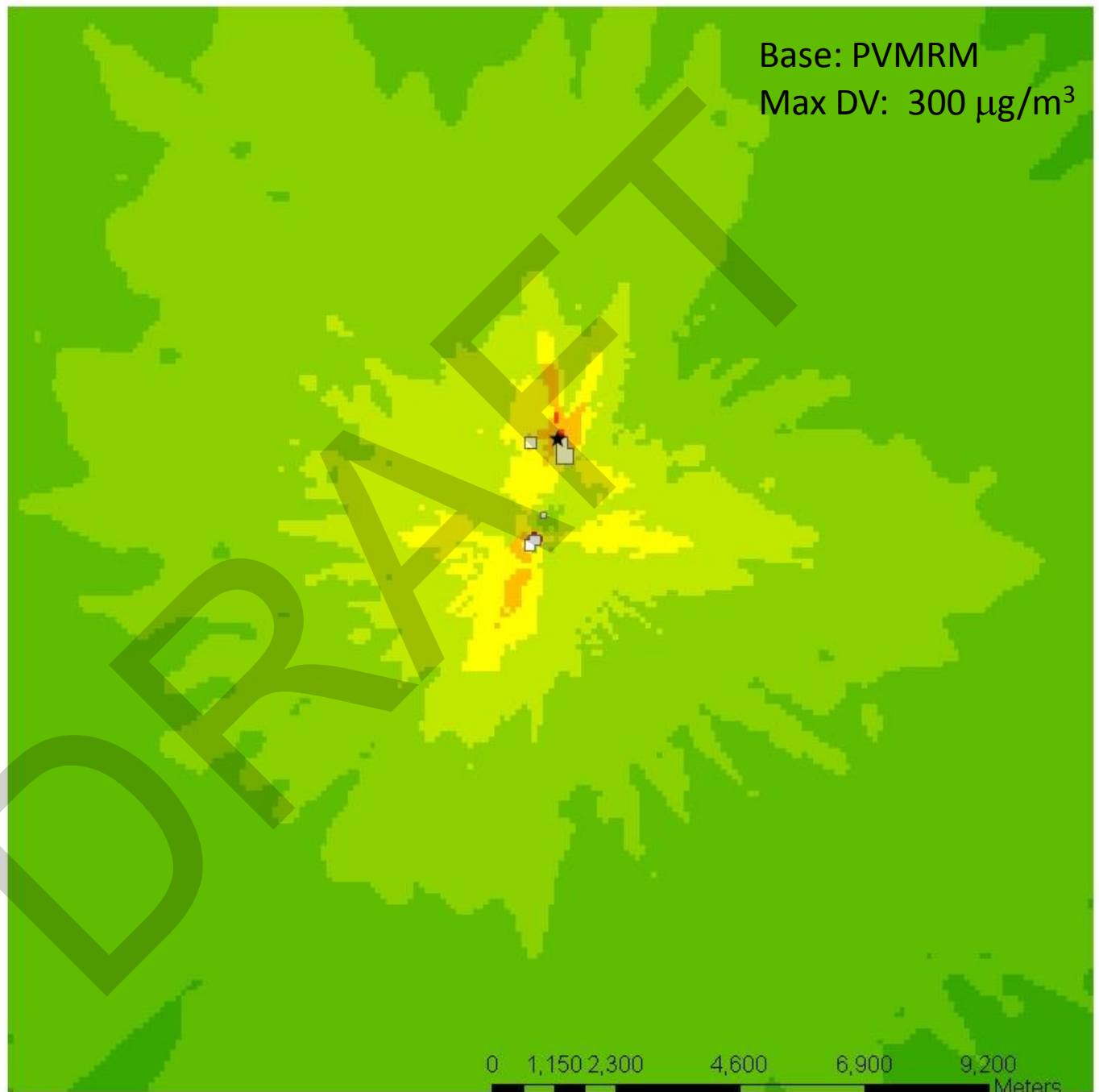


0 1,150 2,300 4,600 6,900 9,200 Meters

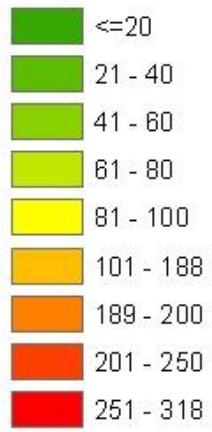
# Legend



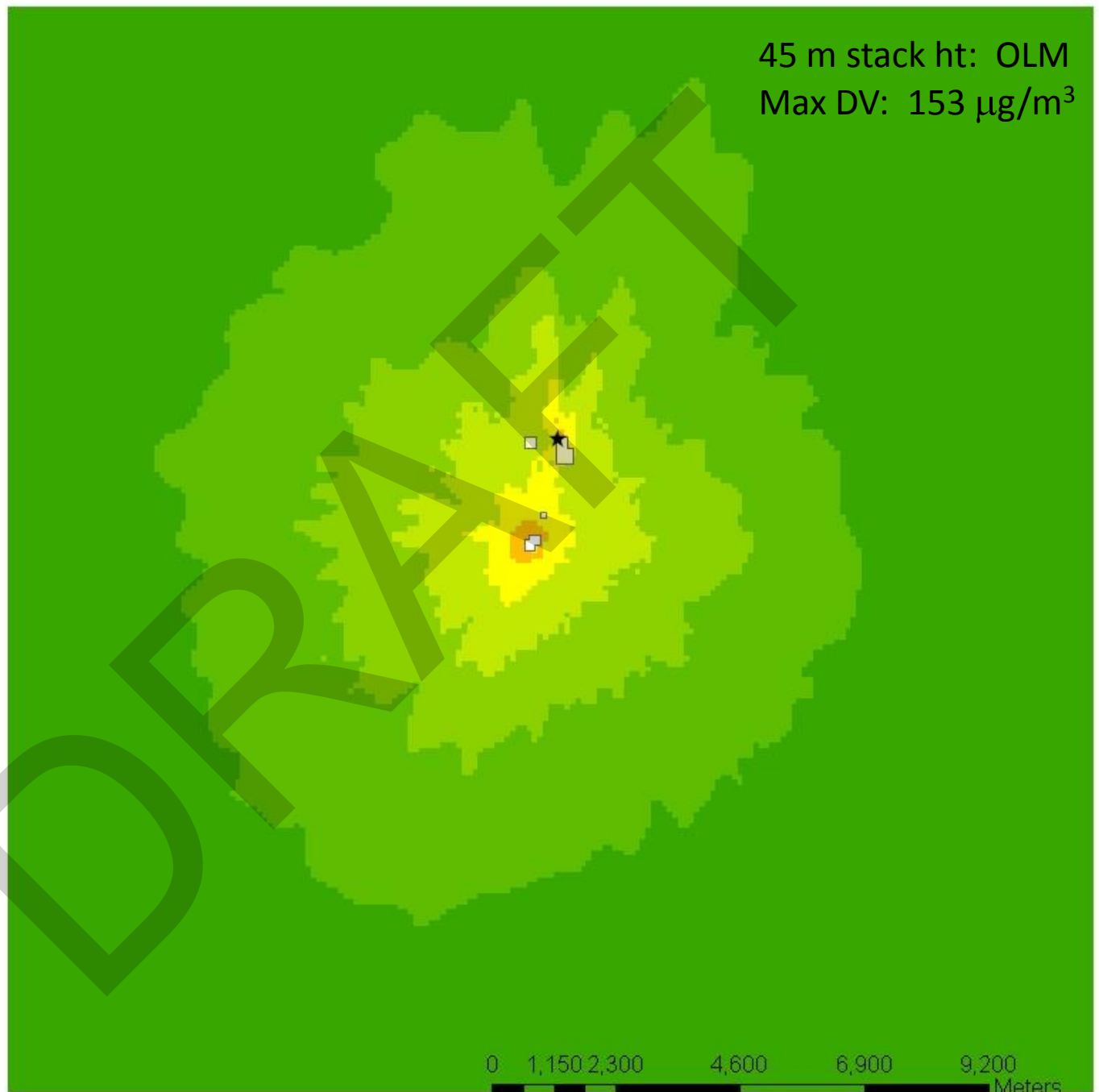
Base: PVMRM  
Max DV: 300  $\mu\text{g}/\text{m}^3$



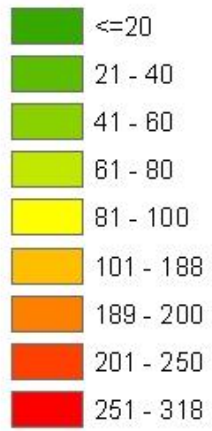
# Legend



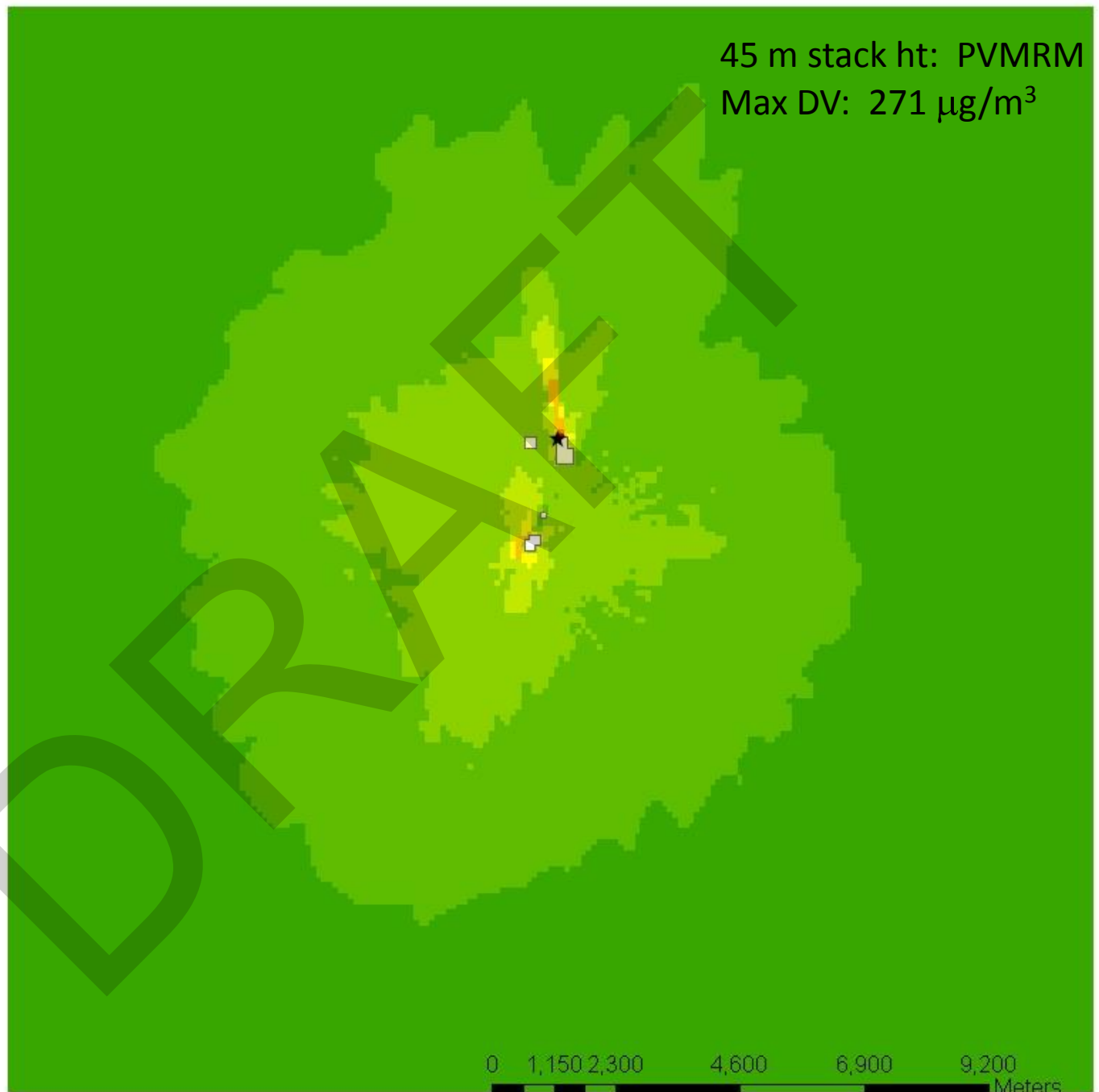
45 m stack ht: OLM  
Max DV: 153  $\mu\text{g}/\text{m}^3$



### Legend



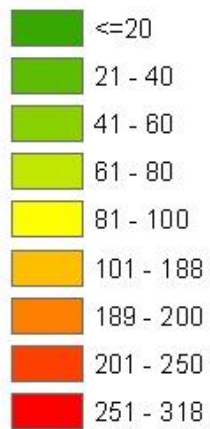
45 m stack ht: PVMRM  
Max DV: 271  $\mu\text{g}/\text{m}^3$



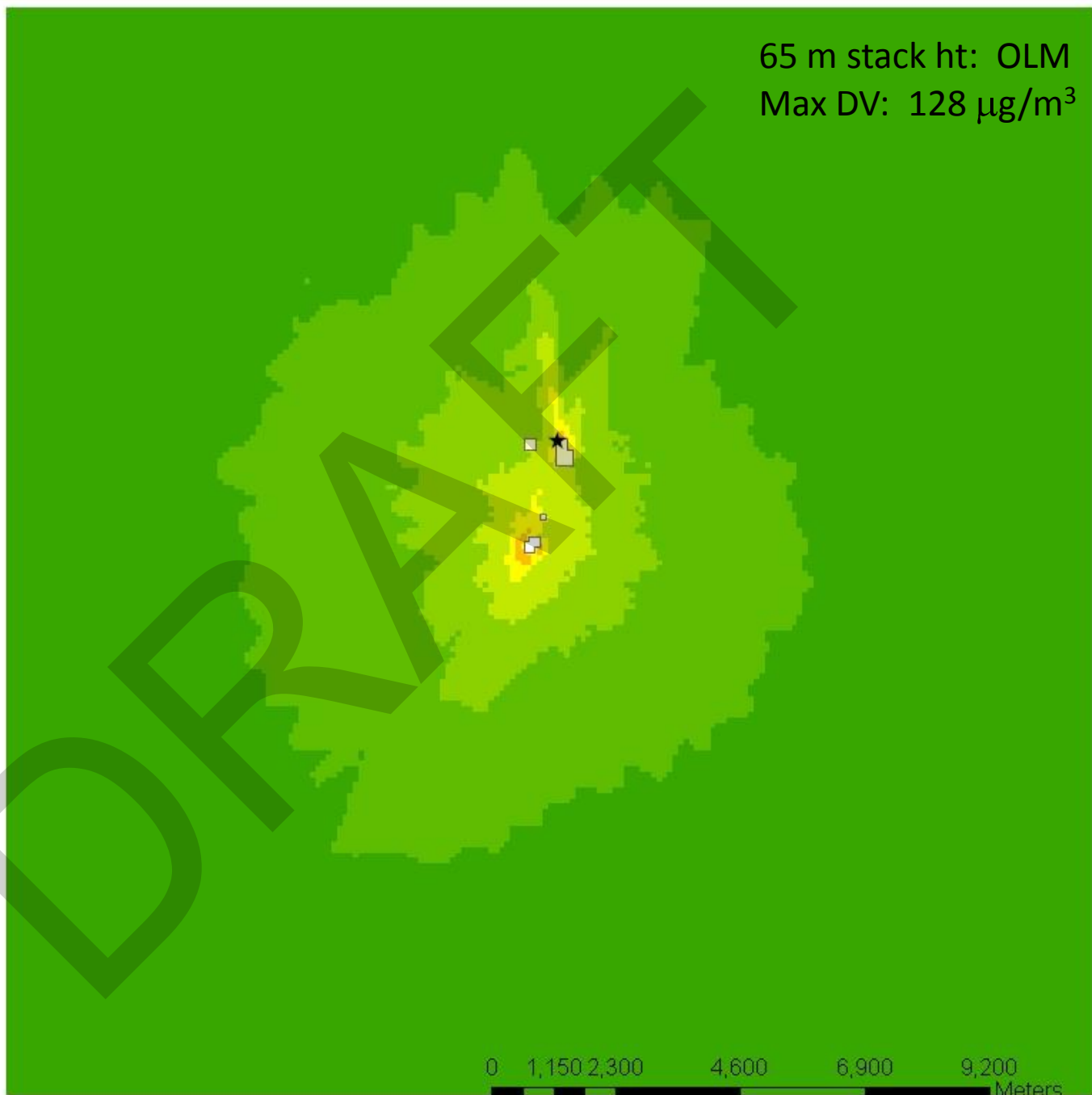
0 1,150 2,300 4,600 6,900 9,200  
Meters



# Legend

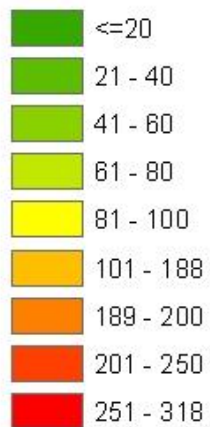


65 m stack ht: OLM  
Max DV: 128  $\mu\text{g}/\text{m}^3$

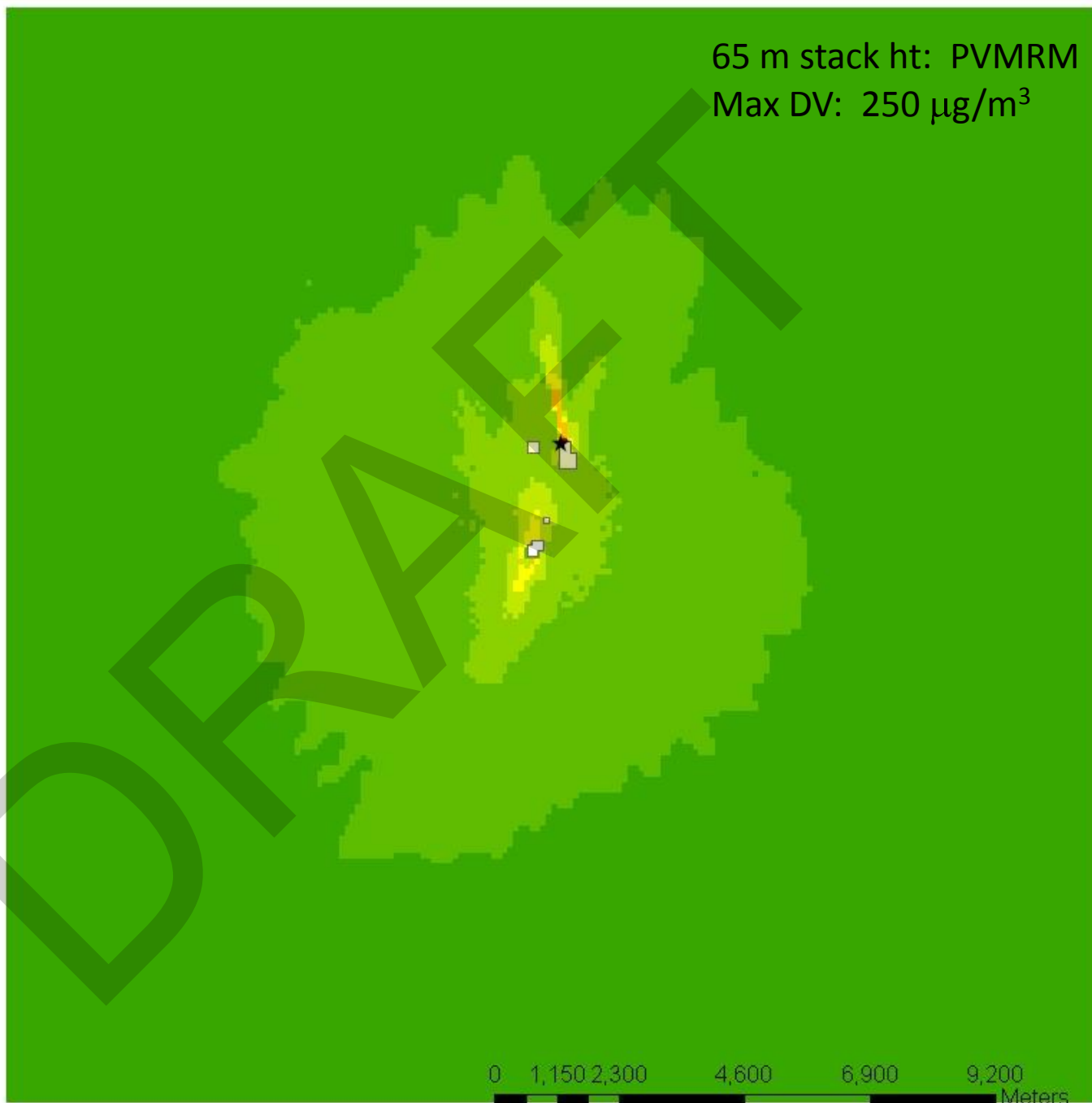


0 1,150 2,300 4,600 6,900 9,200  
Meters

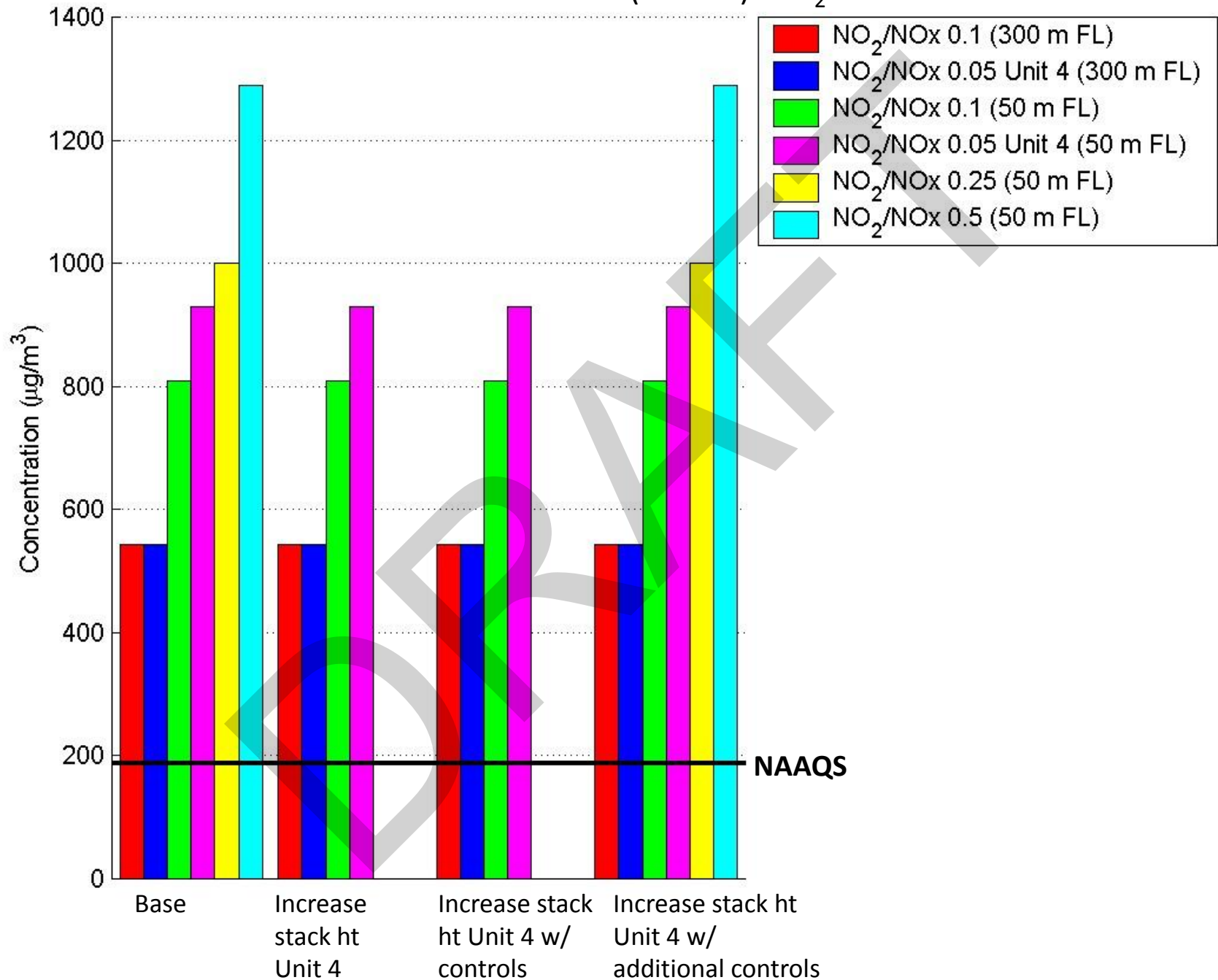
### Legend



65 m stack ht: PVMRM  
Max DV: 250  $\mu\text{g}/\text{m}^3$



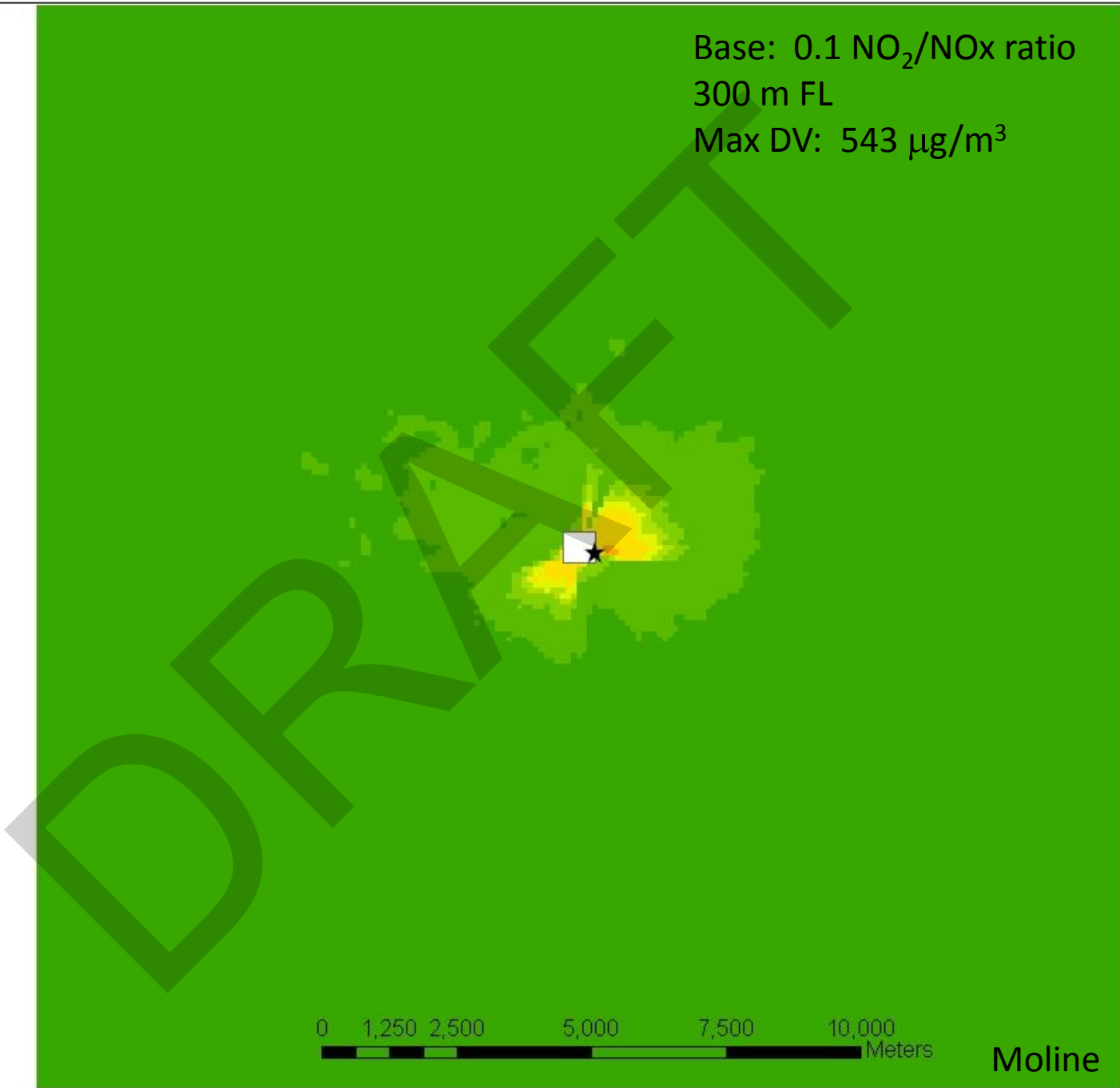
# Ethanol Plant (Moline): NO<sub>2</sub>



Base: 0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 543 μg/m<sup>3</sup>

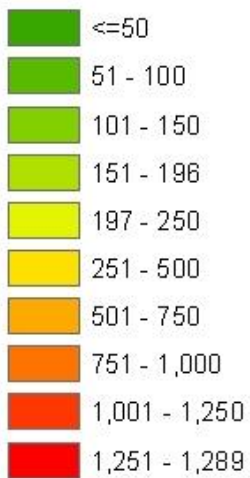
**Legend**

- <=50
- 51 - 100
- 101 - 150
- 151 - 196
- 197 - 250
- 251 - 500
- 501 - 750
- 751 - 1,000
- 1,001 - 1,250
- 1,251 - 1,289



Base 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio unit #4  
300 m FL  
Max DV: 543 μg/m<sup>3</sup>

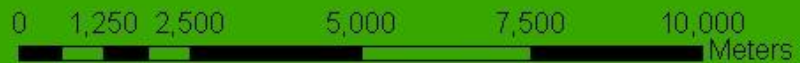
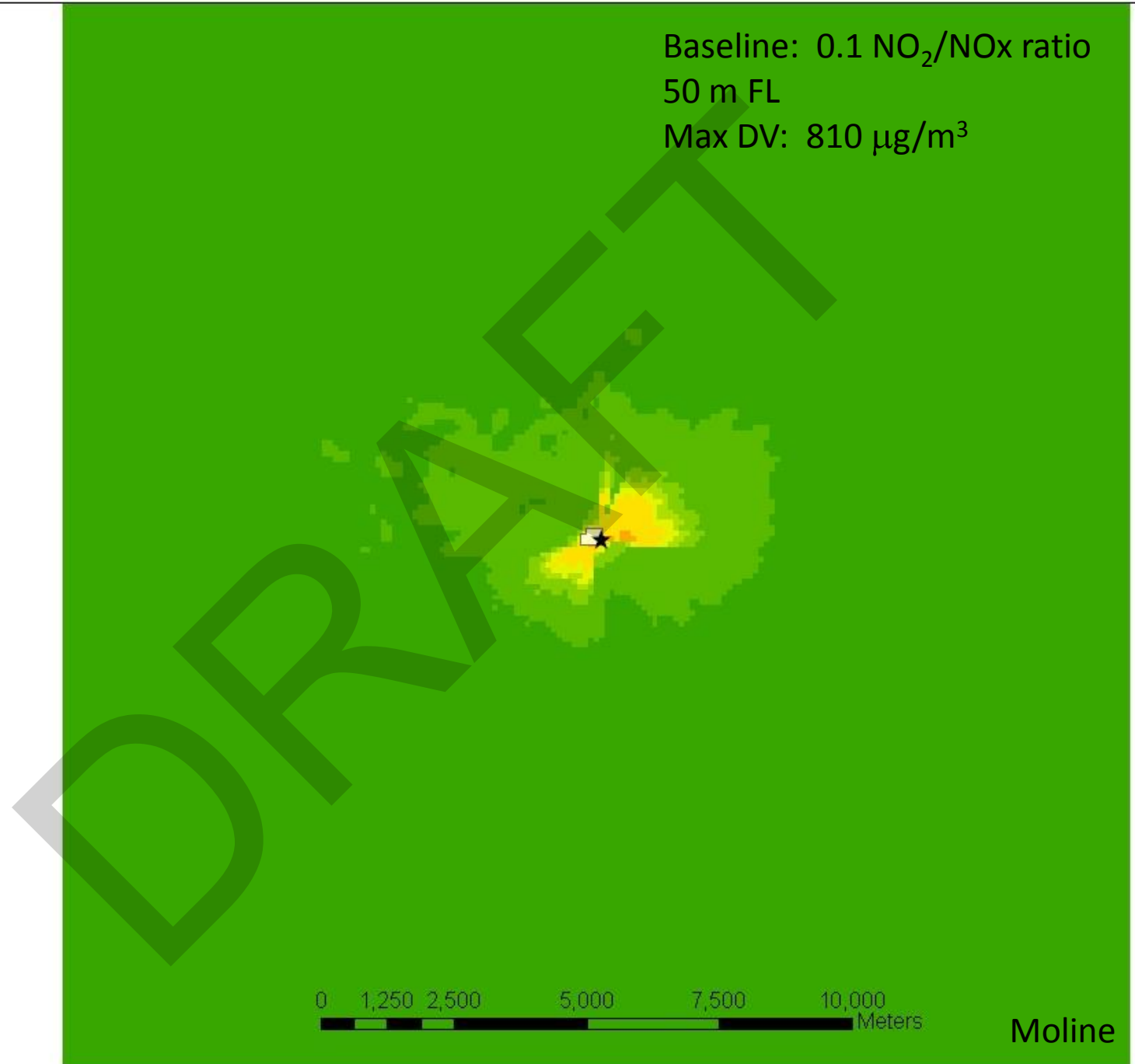
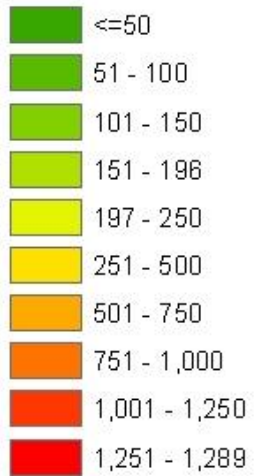
### Legend



Moline

Baseline: 0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 810 μg/m<sup>3</sup>

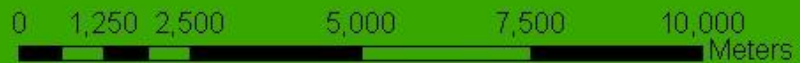
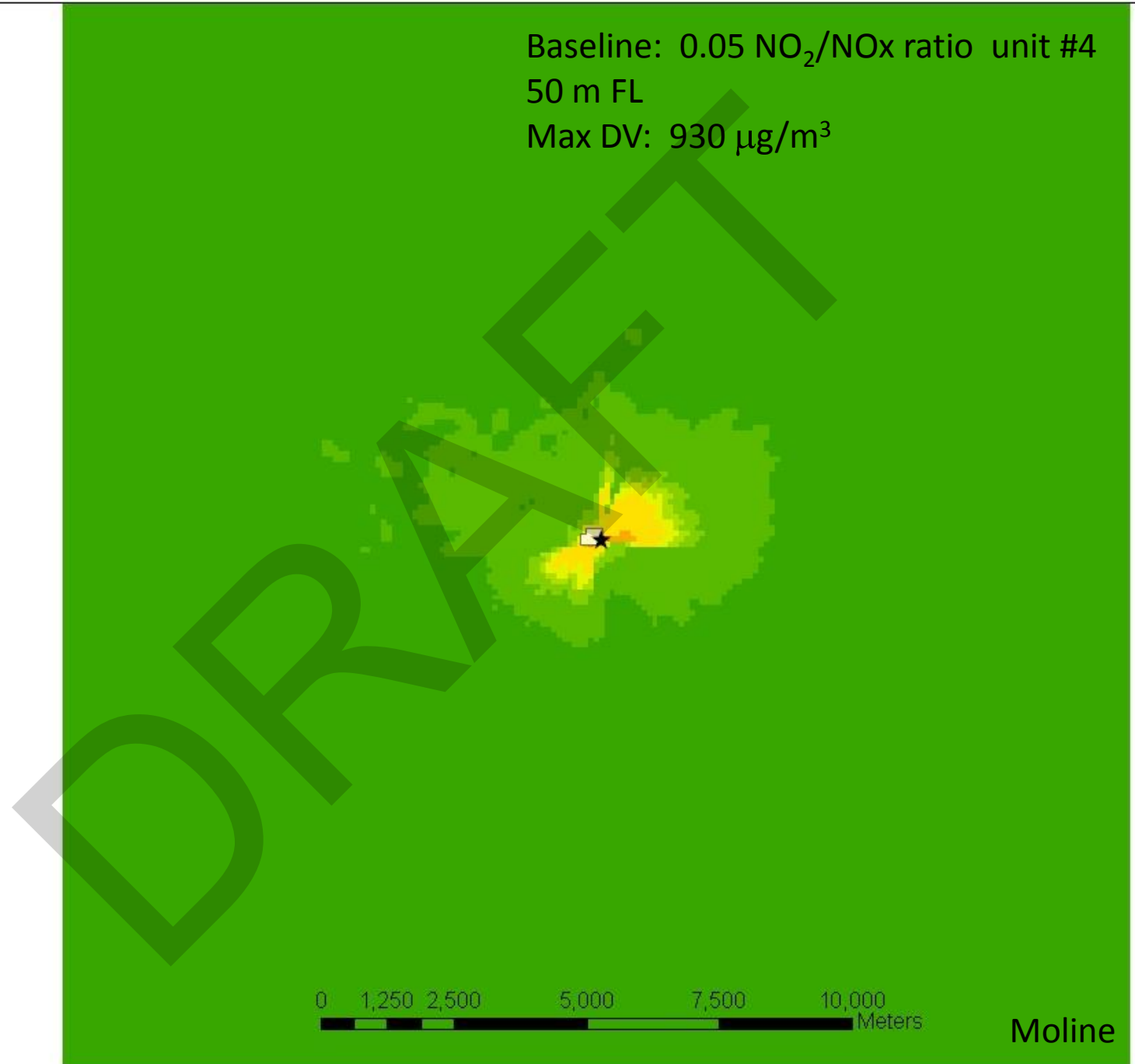
### Legend



Moline

Baseline: 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio unit #4  
50 m FL  
Max DV: 930 μg/m<sup>3</sup>









### Legend

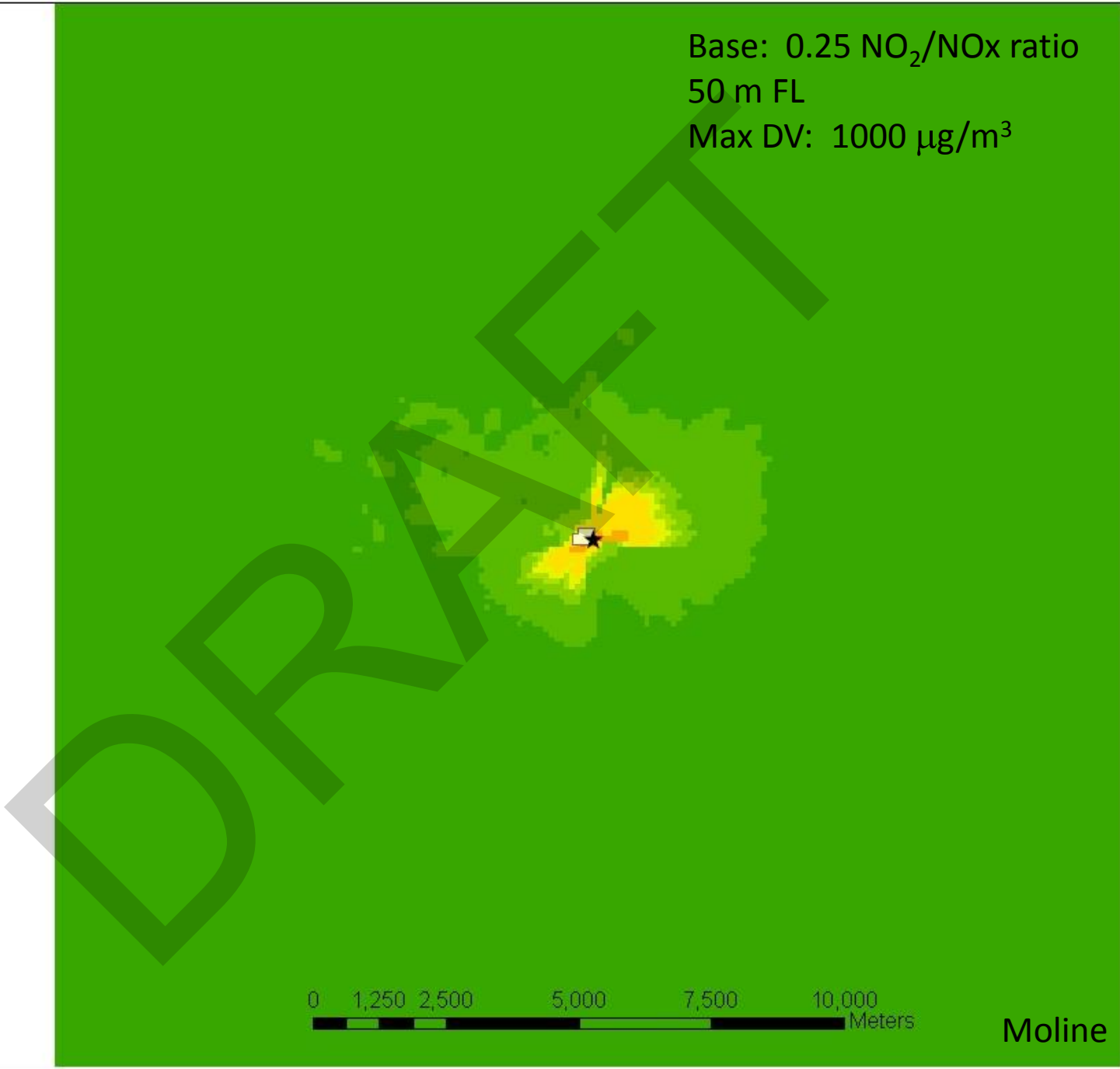


Moline

Base: 0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1000 μg/m<sup>3</sup>

**Legend**

-  <=50
-  51 - 100
-  101 - 150
-  151 - 196
-  197 - 250
-  251 - 500
-  501 - 750
-  751 - 1,000
-  1,001 - 1,250
-  1,251 - 1,289

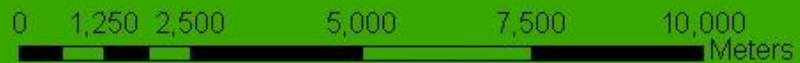
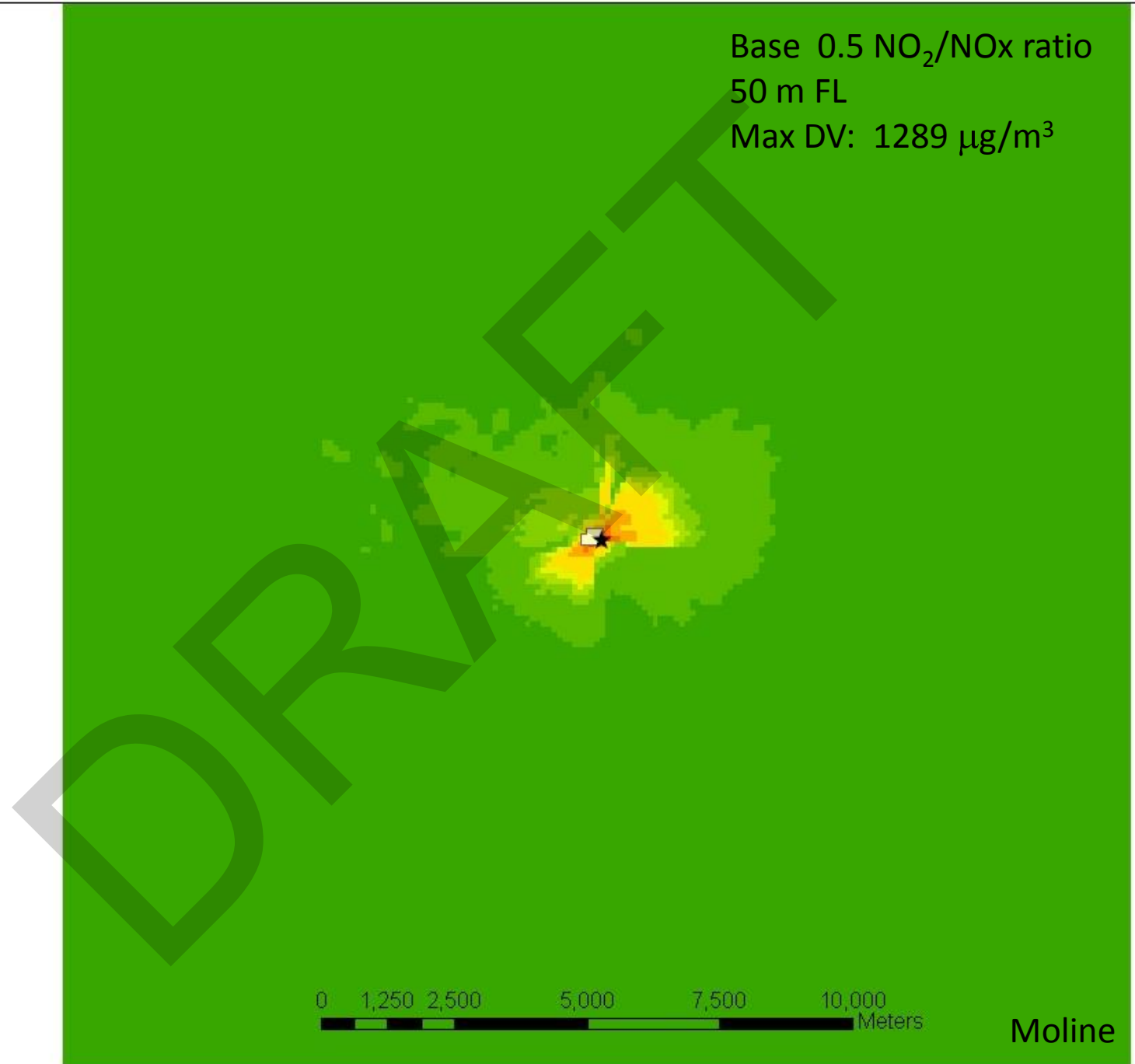
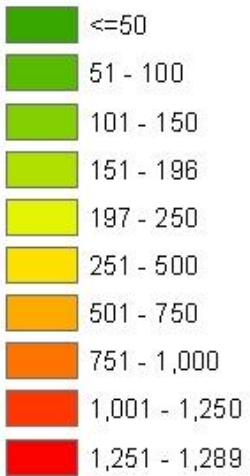


Moline



Base 0.5 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1289 μg/m<sup>3</sup>

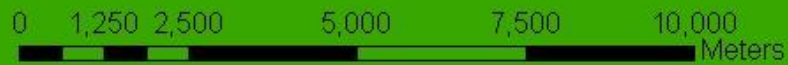
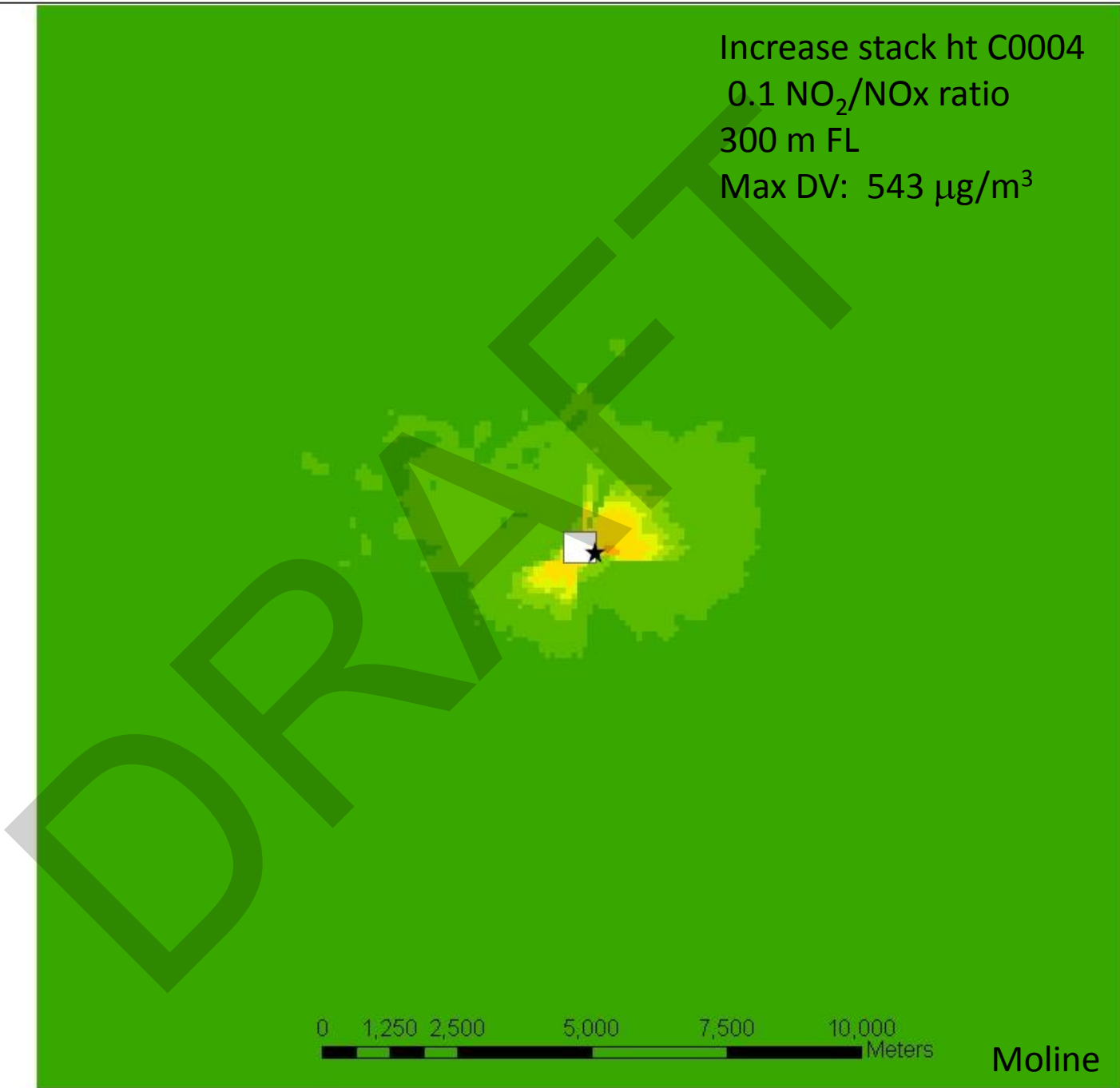
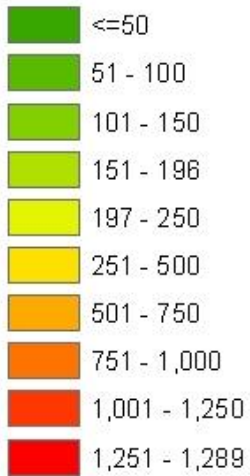
### Legend



Moline

Increase stack ht C0004  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 543 μg/m<sup>3</sup>

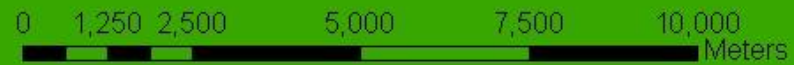
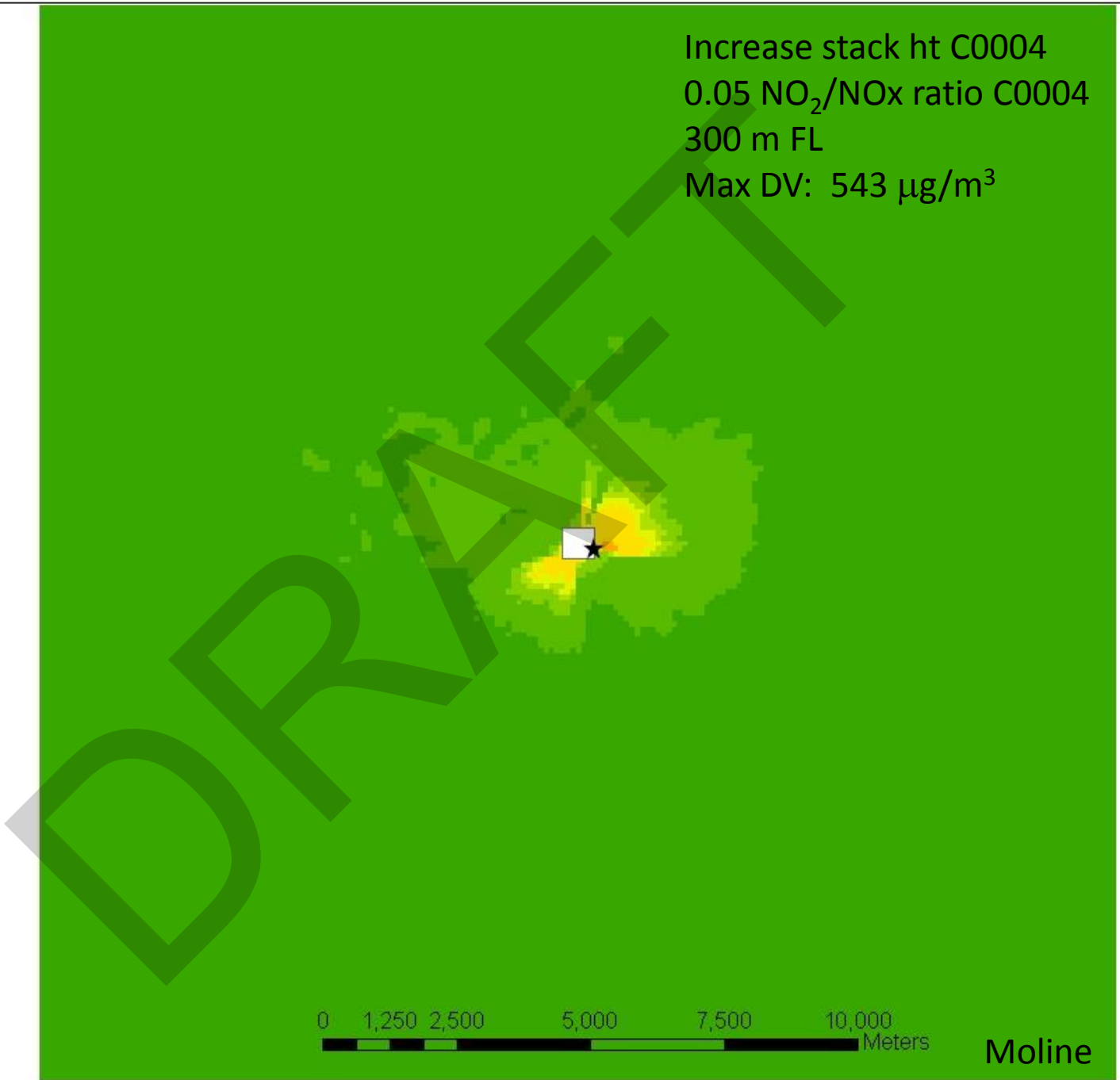
### Legend



Moline

Increase stack ht C0004  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 543 μg/m<sup>3</sup>

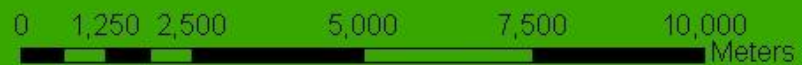
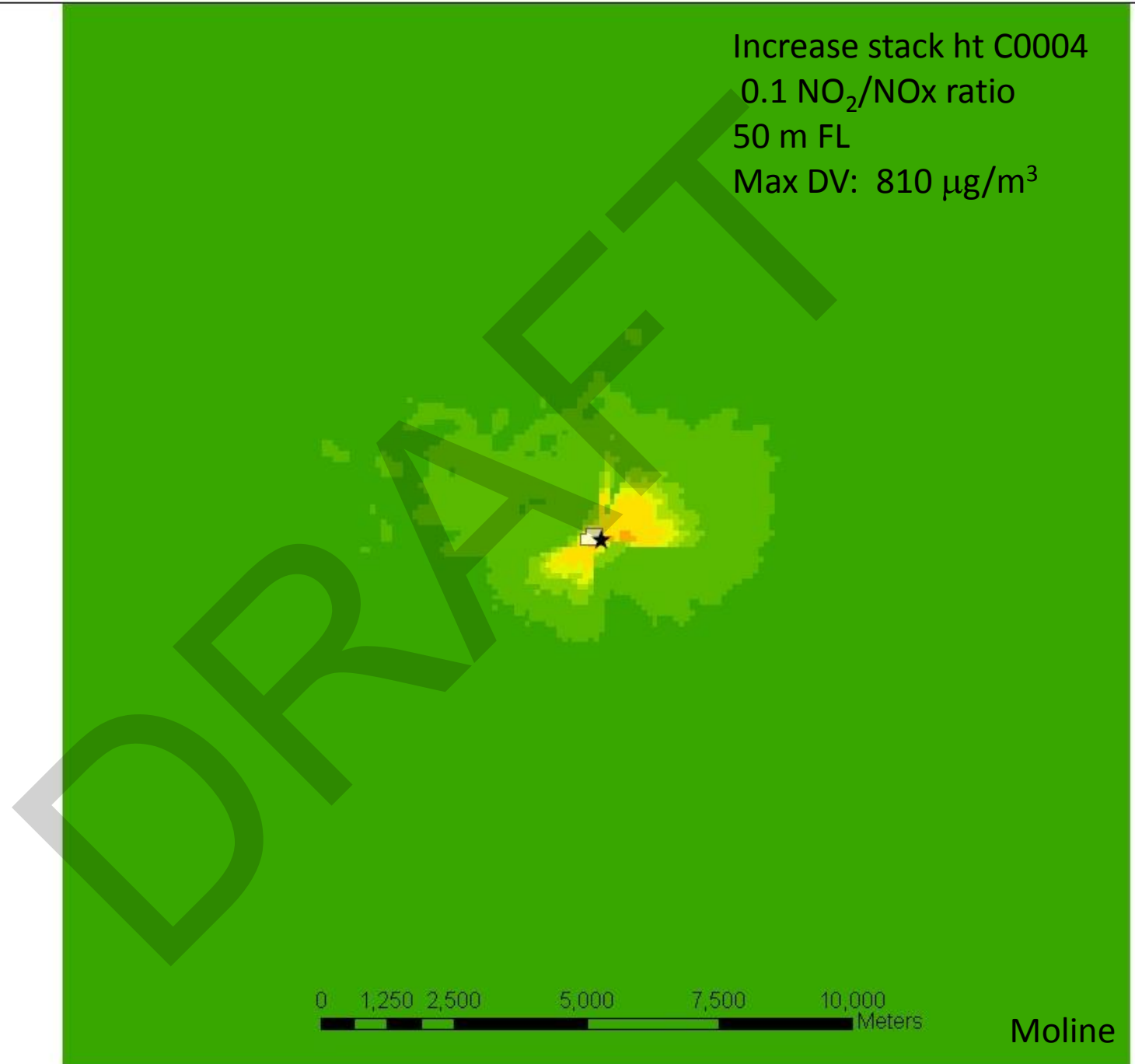
### Legend



Moline

Increase stack ht C0004  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 810 μg/m<sup>3</sup>

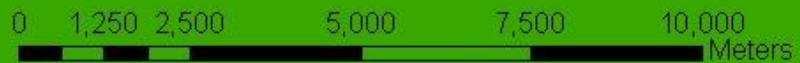
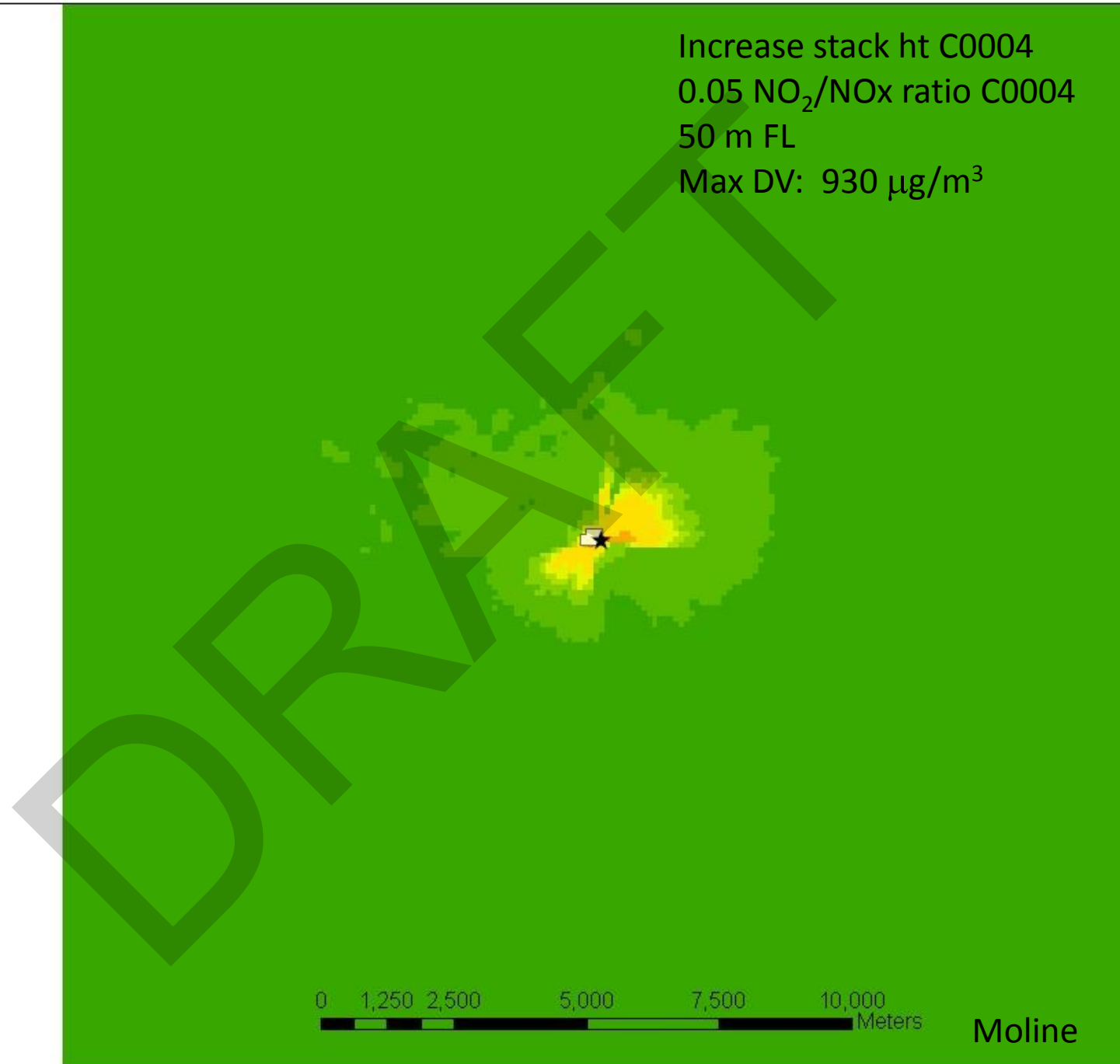
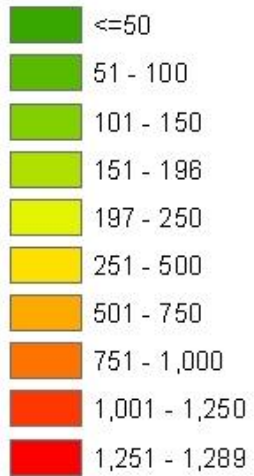
### Legend



Moline

Increase stack ht C0004  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 930 μg/m<sup>3</sup>

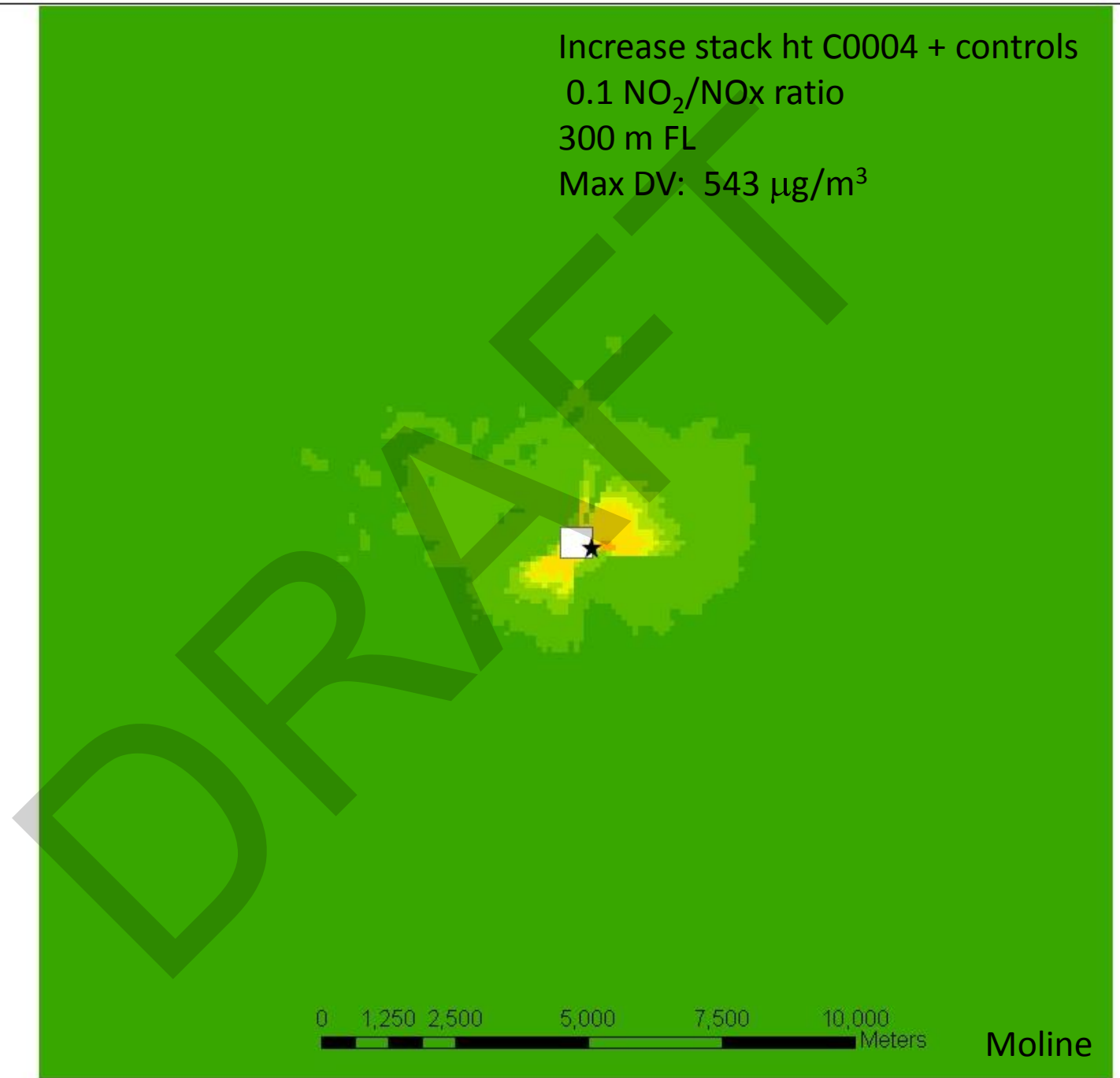
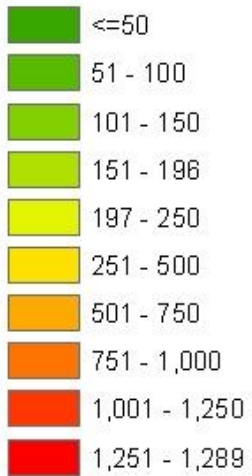
### Legend



Moline

Increase stack ht C0004 + controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 543 μg/m<sup>3</sup>

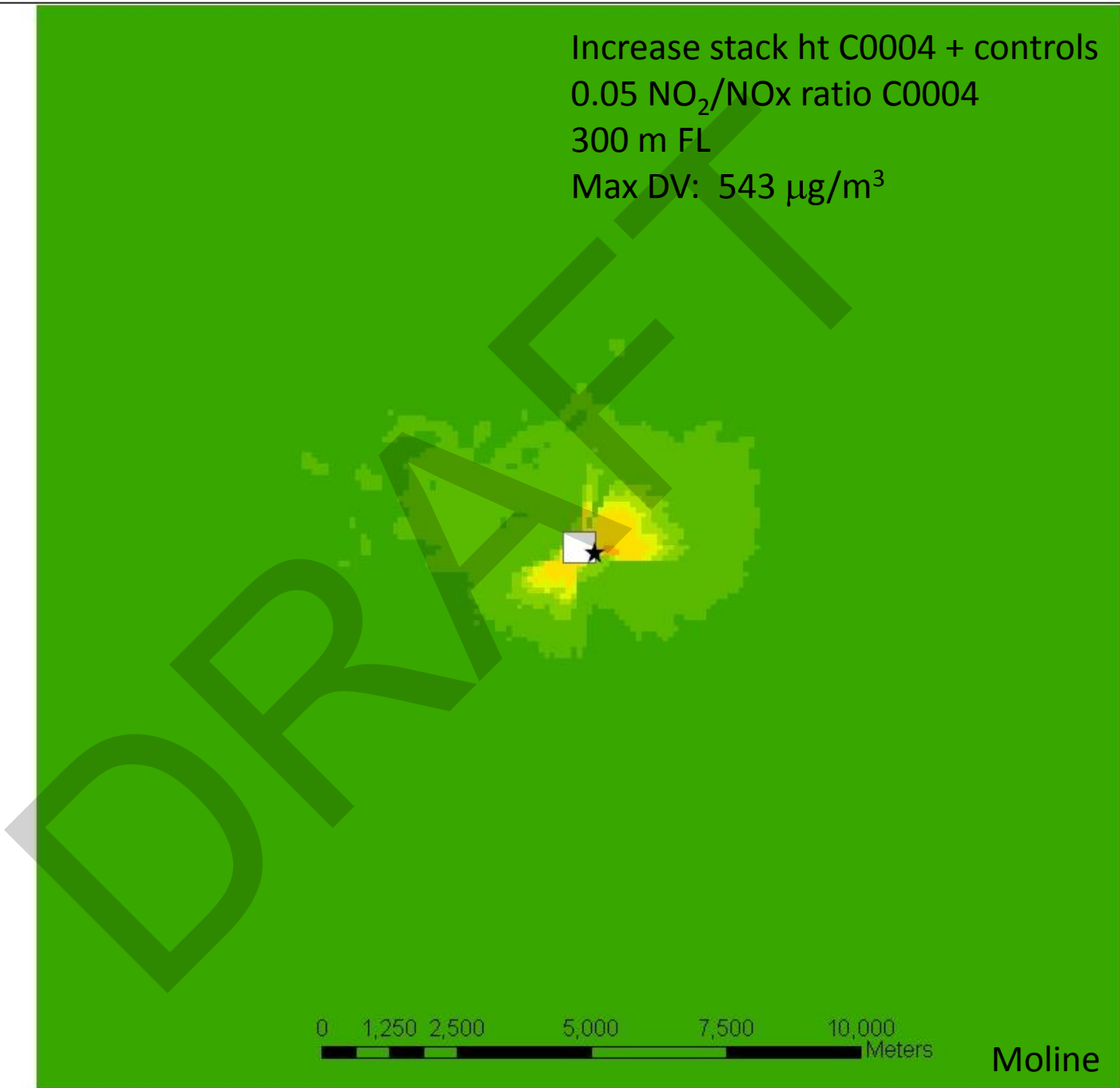
### Legend



Moline

Increase stack ht C0004 + controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 543 μg/m<sup>3</sup>

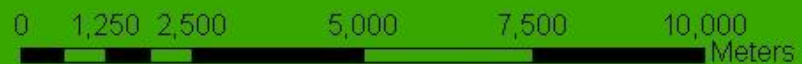
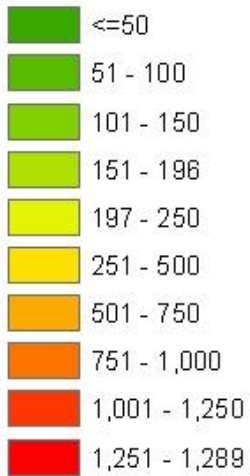
**Legend**



Moline

Increase stack ht C0004 + controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 810 μg/m<sup>3</sup>

### Legend

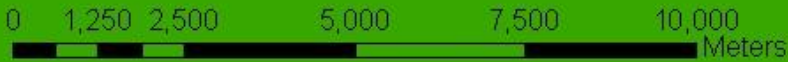
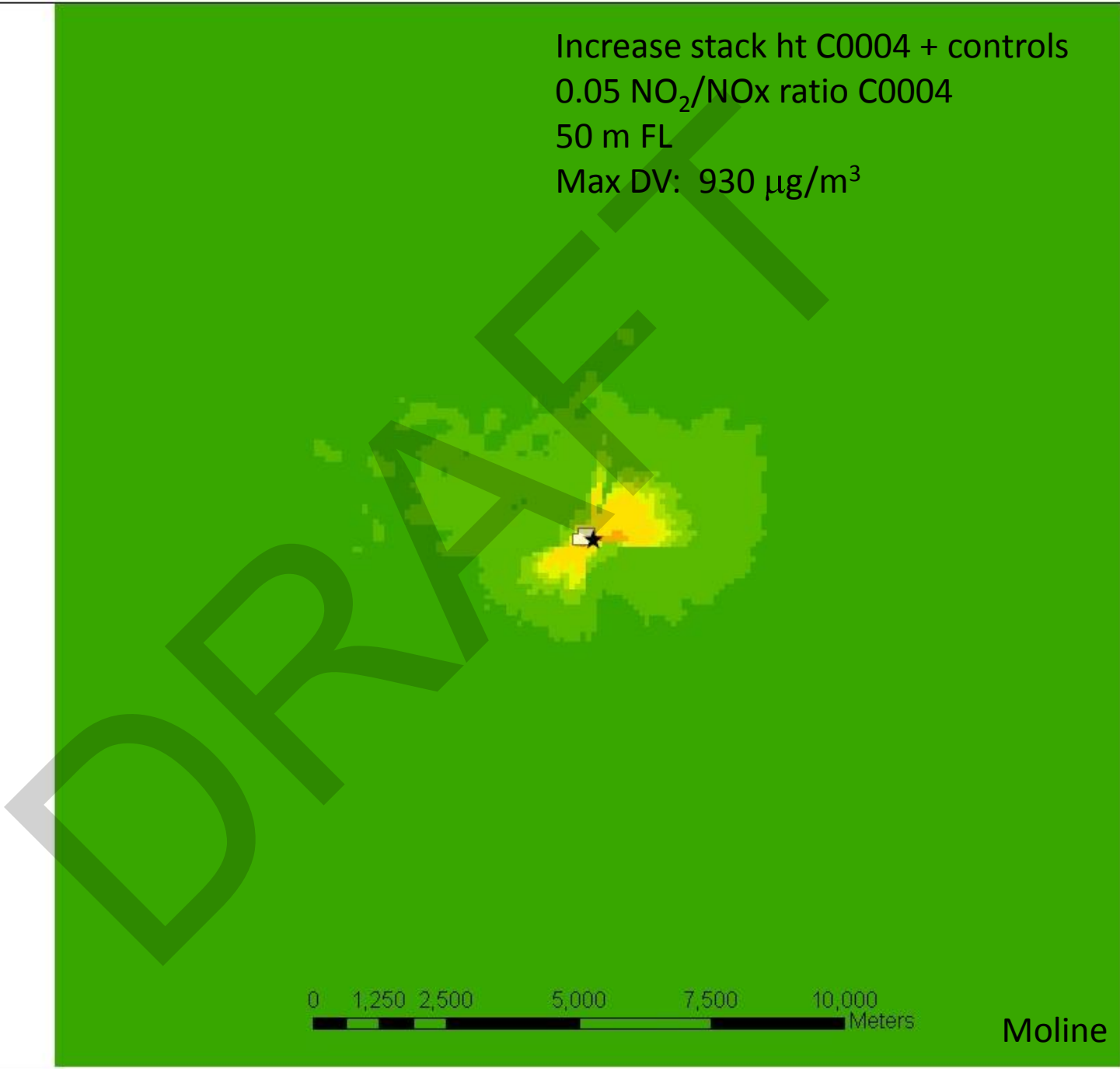


Moline



Increase stack ht C0004 + controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 930 μg/m<sup>3</sup>

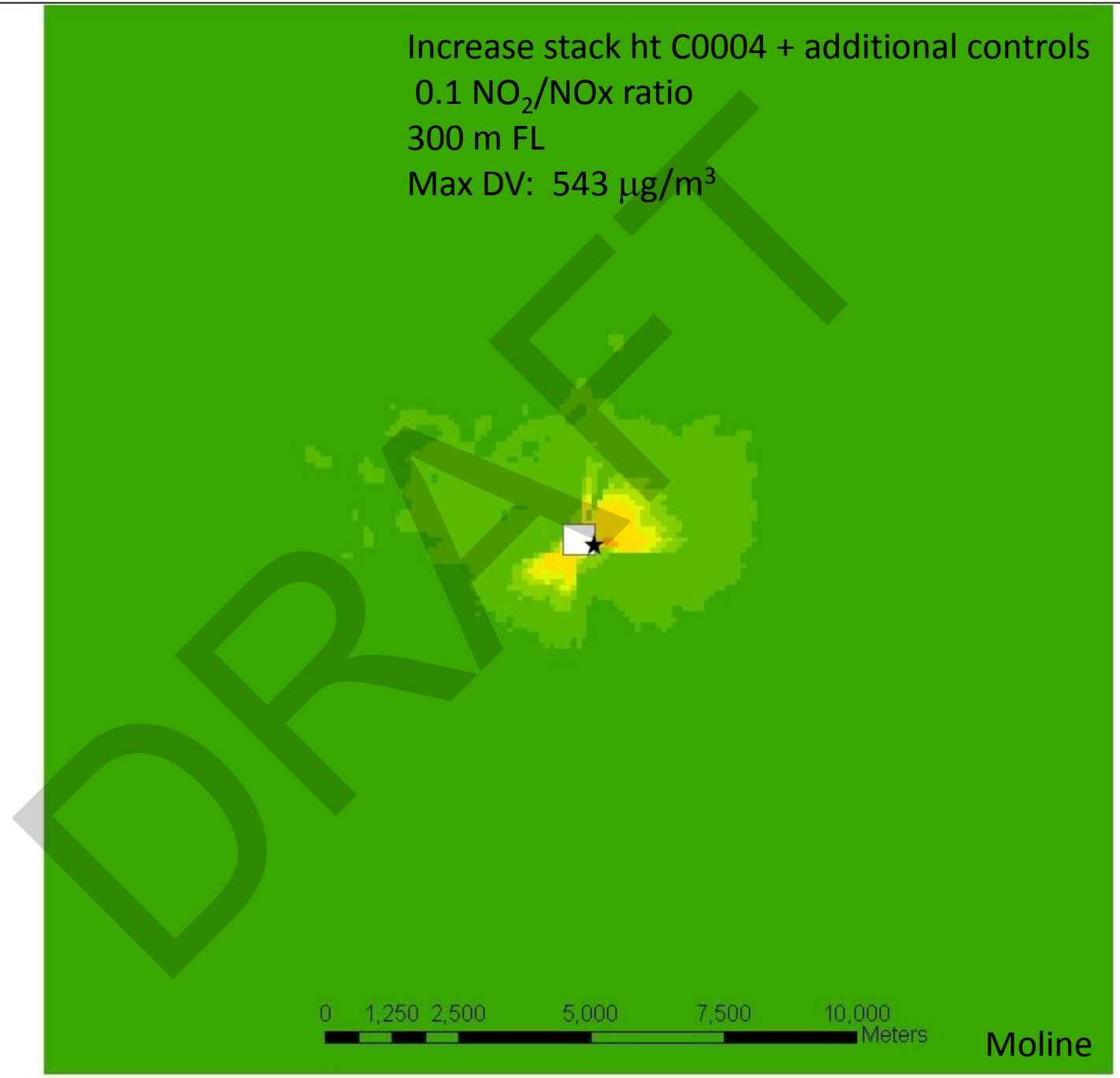
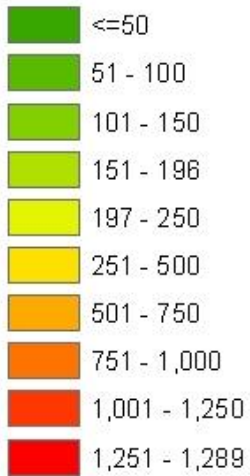
**Legend**



Moline

Increase stack ht C0004 + additional controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 543 μg/m<sup>3</sup>

**Legend**



Moline

Increase stack ht C0004 + additional controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 543 μg/m<sup>3</sup>

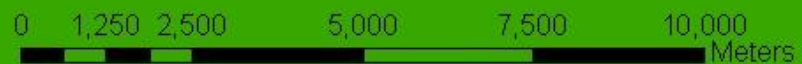
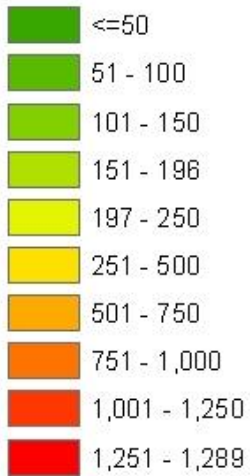
### Legend



Moline

Increase stack ht C0004 + additional controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 810 μg/m<sup>3</sup>

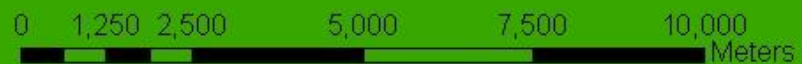
### Legend



Moline

Increase stack ht C0004 + additional controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 930 μg/m<sup>3</sup>

### Legend



Moline

Increase stack ht C0004 + additional controls  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1000 μg/m<sup>3</sup>

### Legend



0 1,250 2,500 5,000 7,500 10,000 Meters

Moline

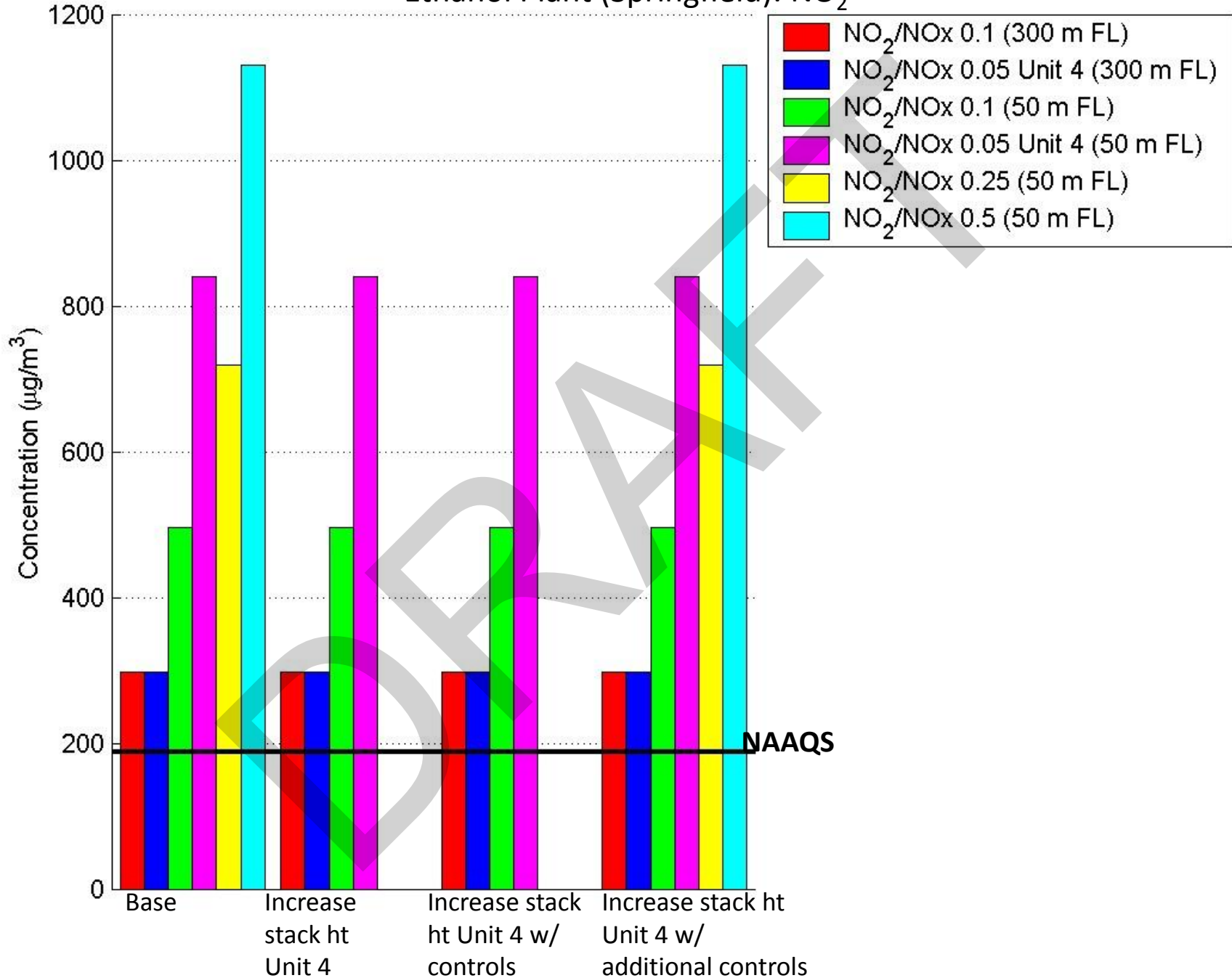
Increase stack ht C0004 + additional controls  
0.50 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1000 μg/m<sup>3</sup>

### Legend



Moline

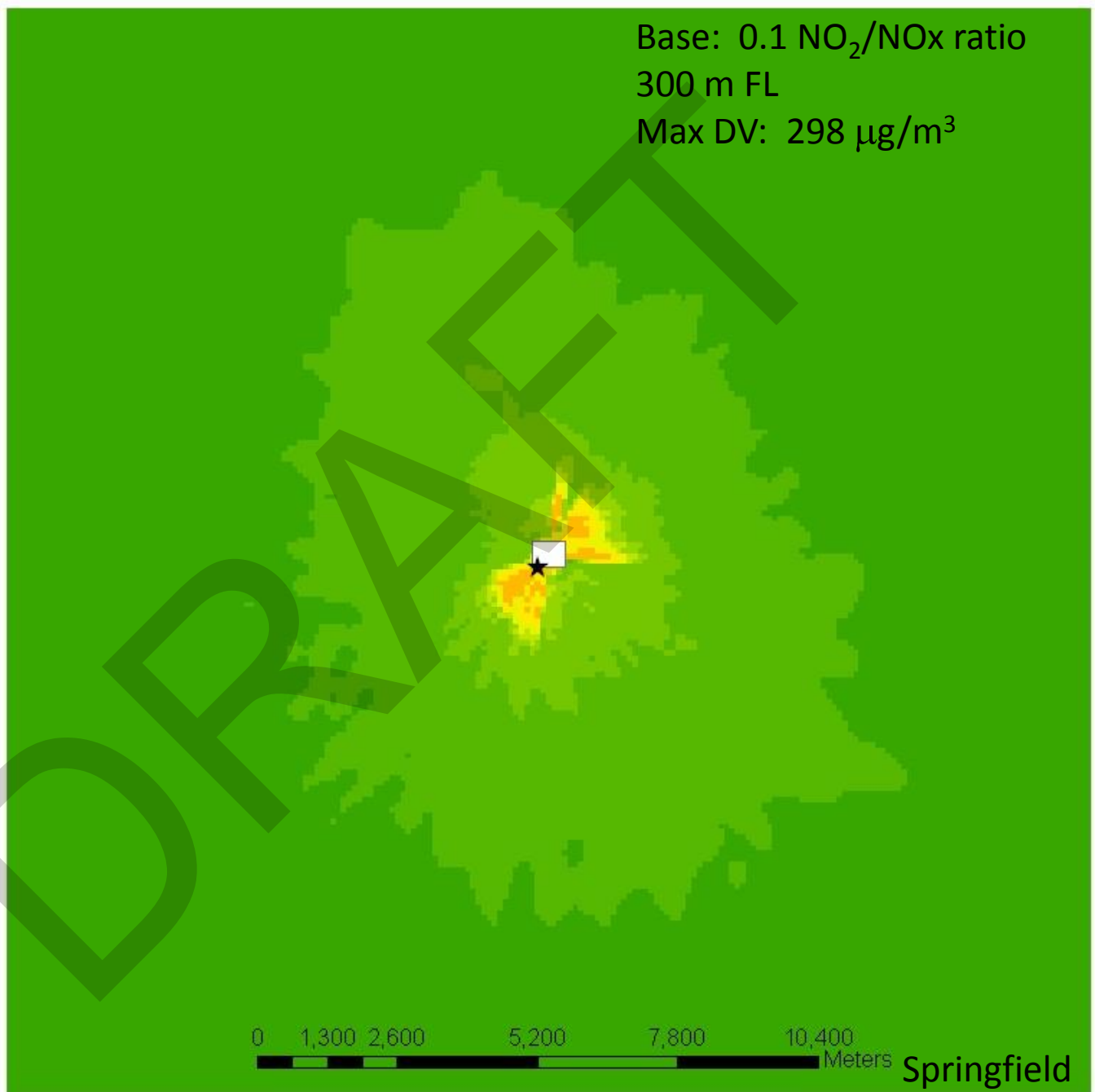
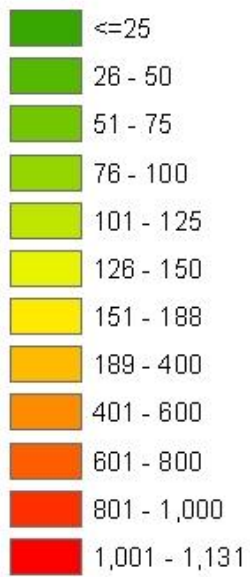
# Ethanol Plant (Springfield): NO<sub>2</sub>





Base: 0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 298 μg/m<sup>3</sup>

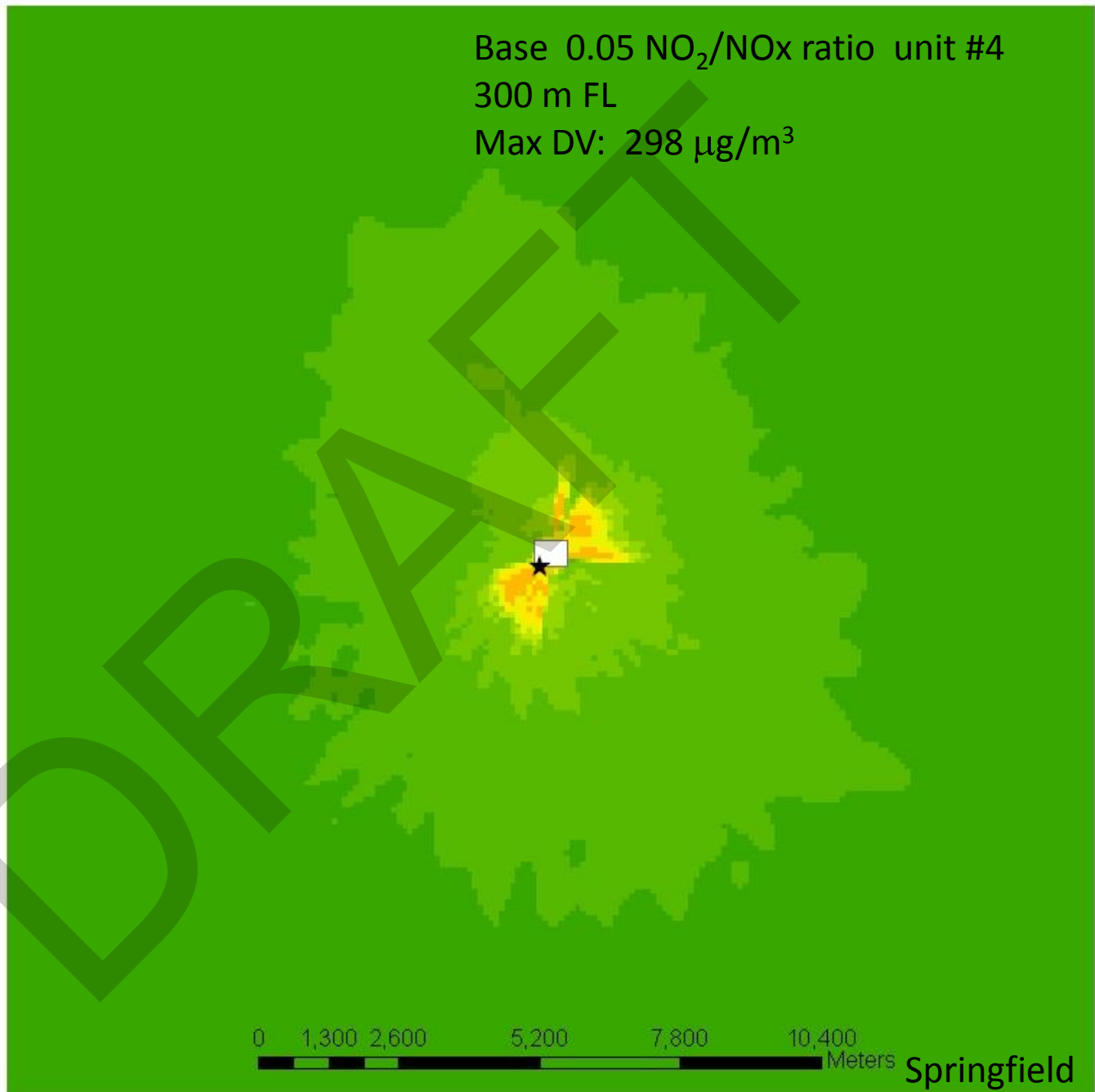
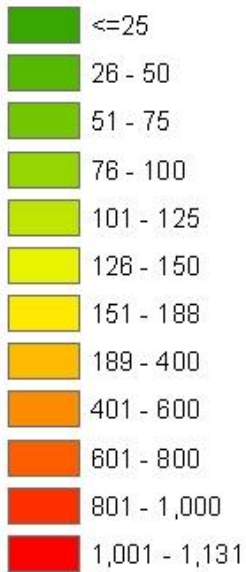
**Legend**



Springfield

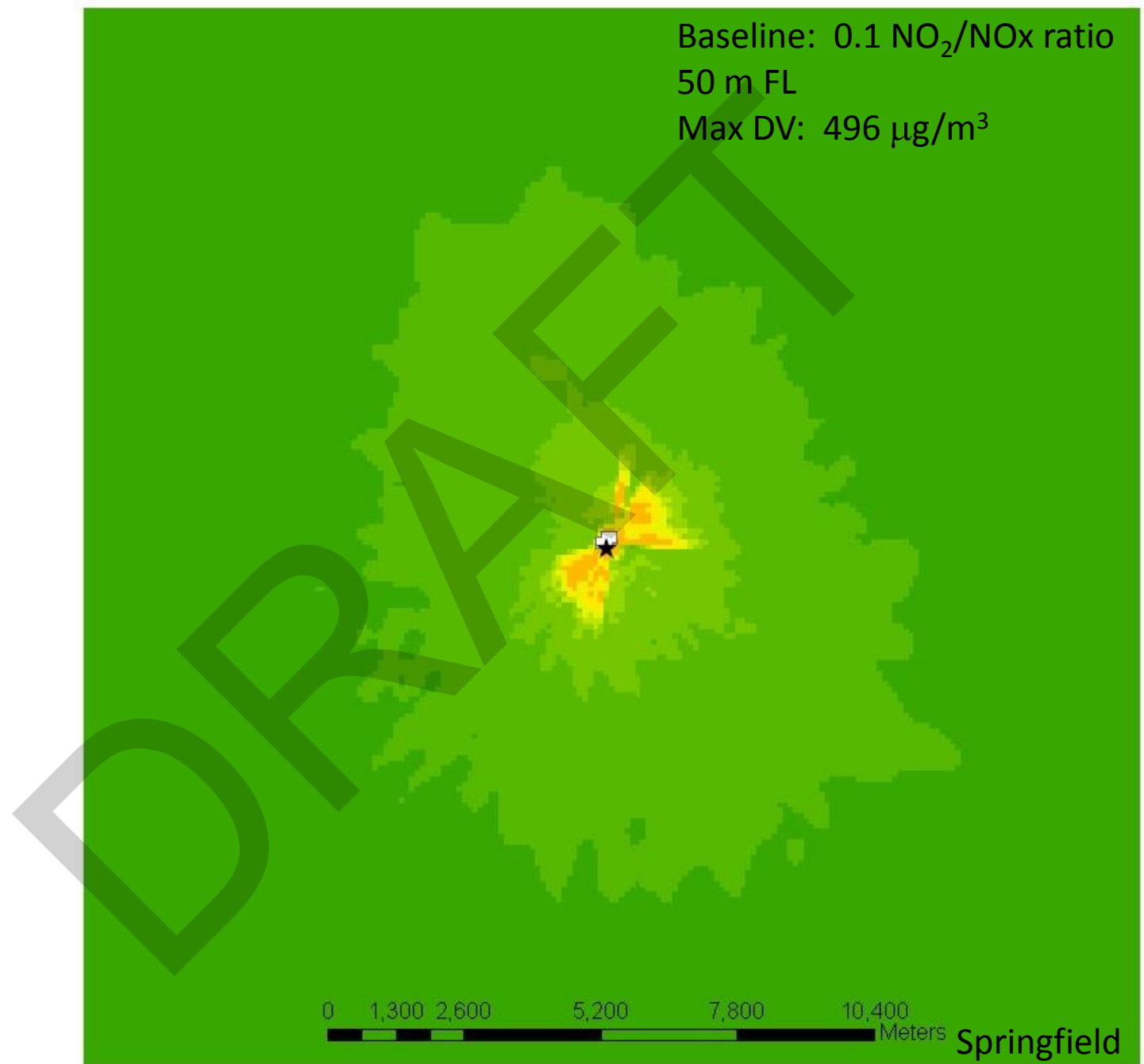
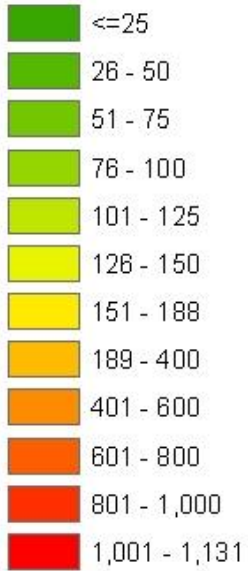
Base 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio unit #4  
300 m FL  
Max DV: 298 μg/m<sup>3</sup>

**Legend**



Baseline: 0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 496 μg/m<sup>3</sup>

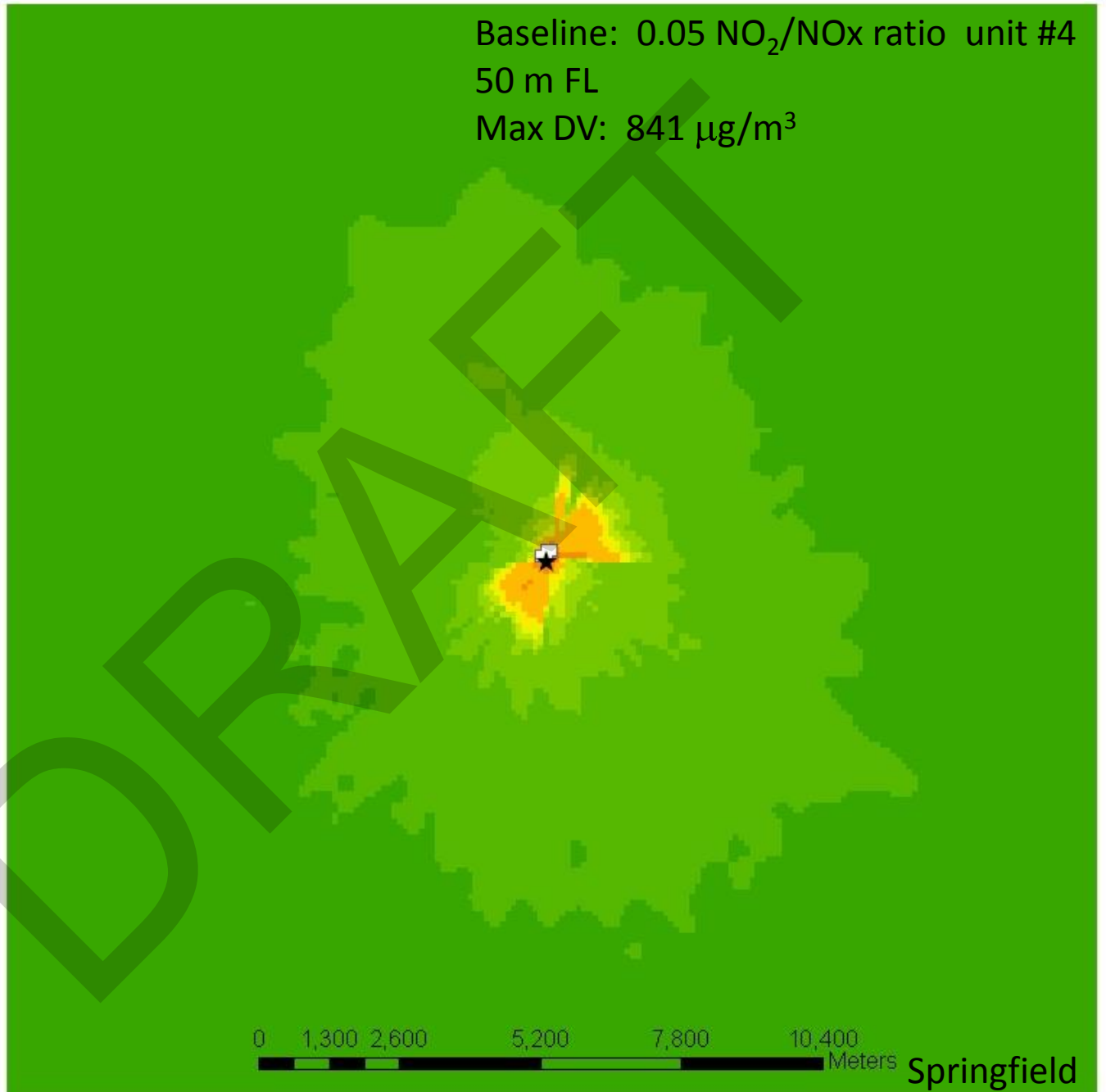
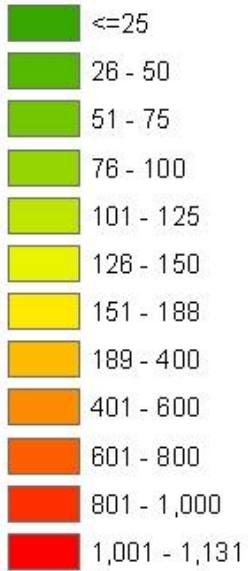
### Legend



Springfield

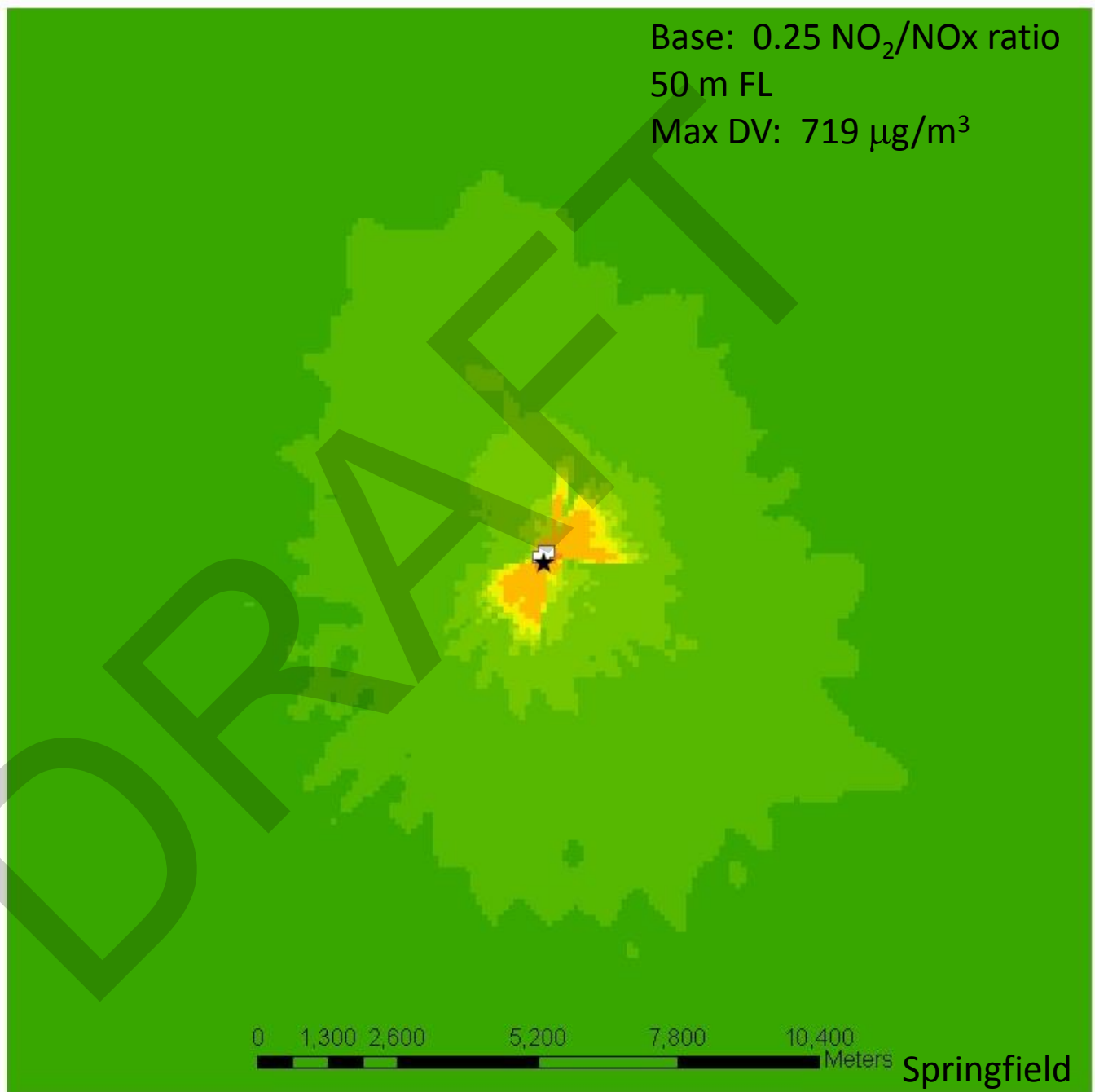
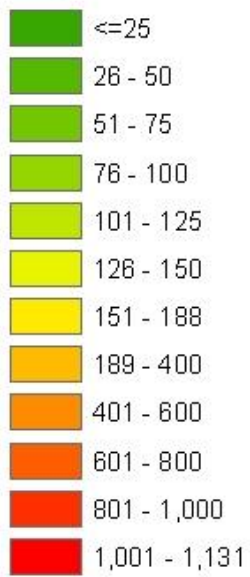
Baseline: 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio unit #4  
50 m FL  
Max DV: 841 μg/m<sup>3</sup>

### Legend



Base: 0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 719 μg/m<sup>3</sup>

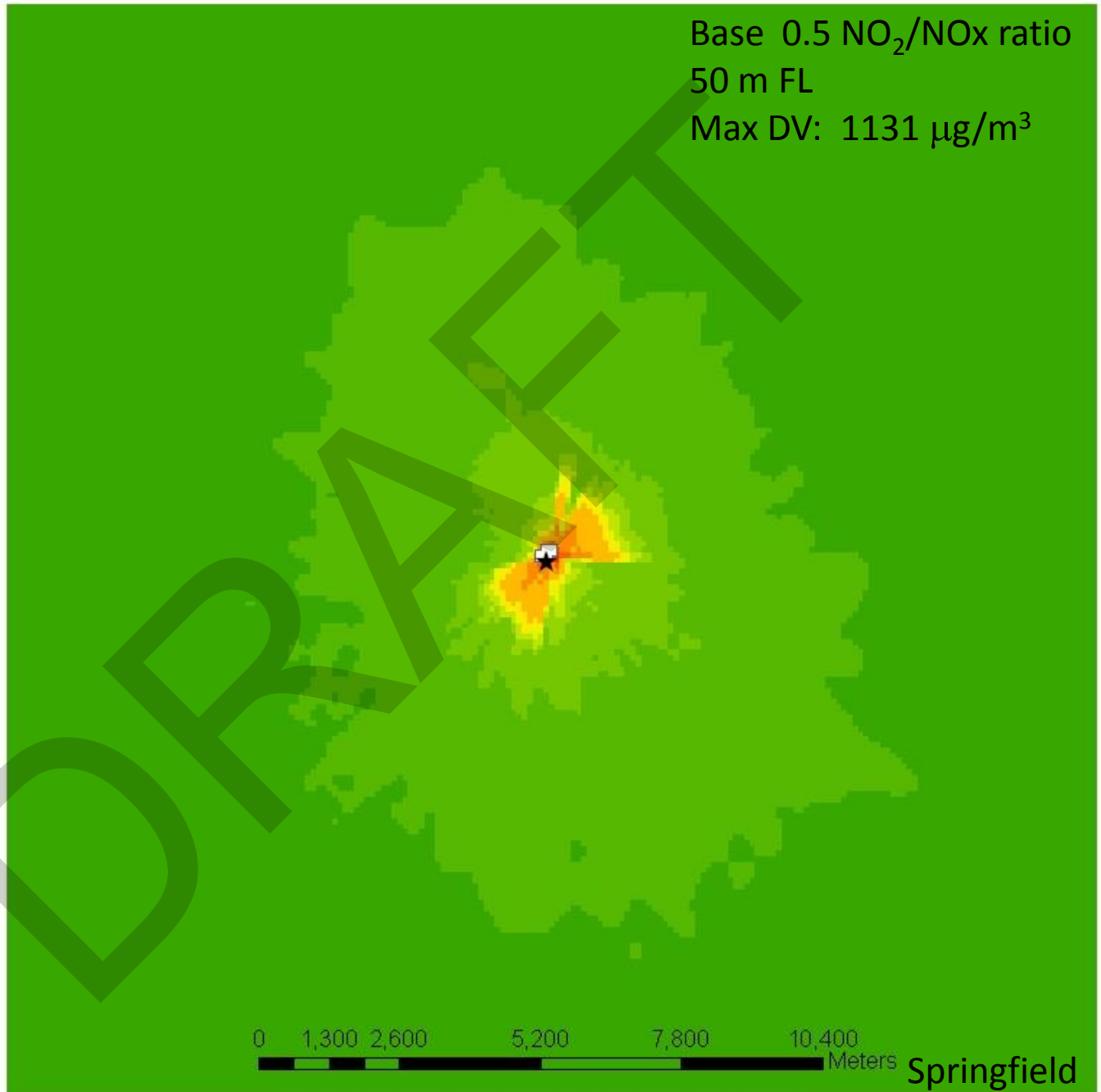
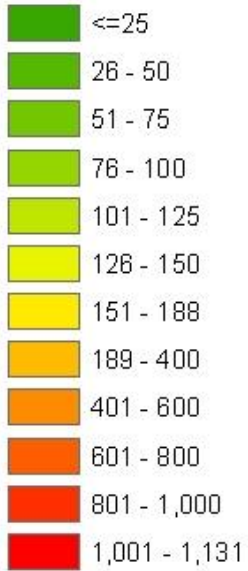
**Legend**



Springfield

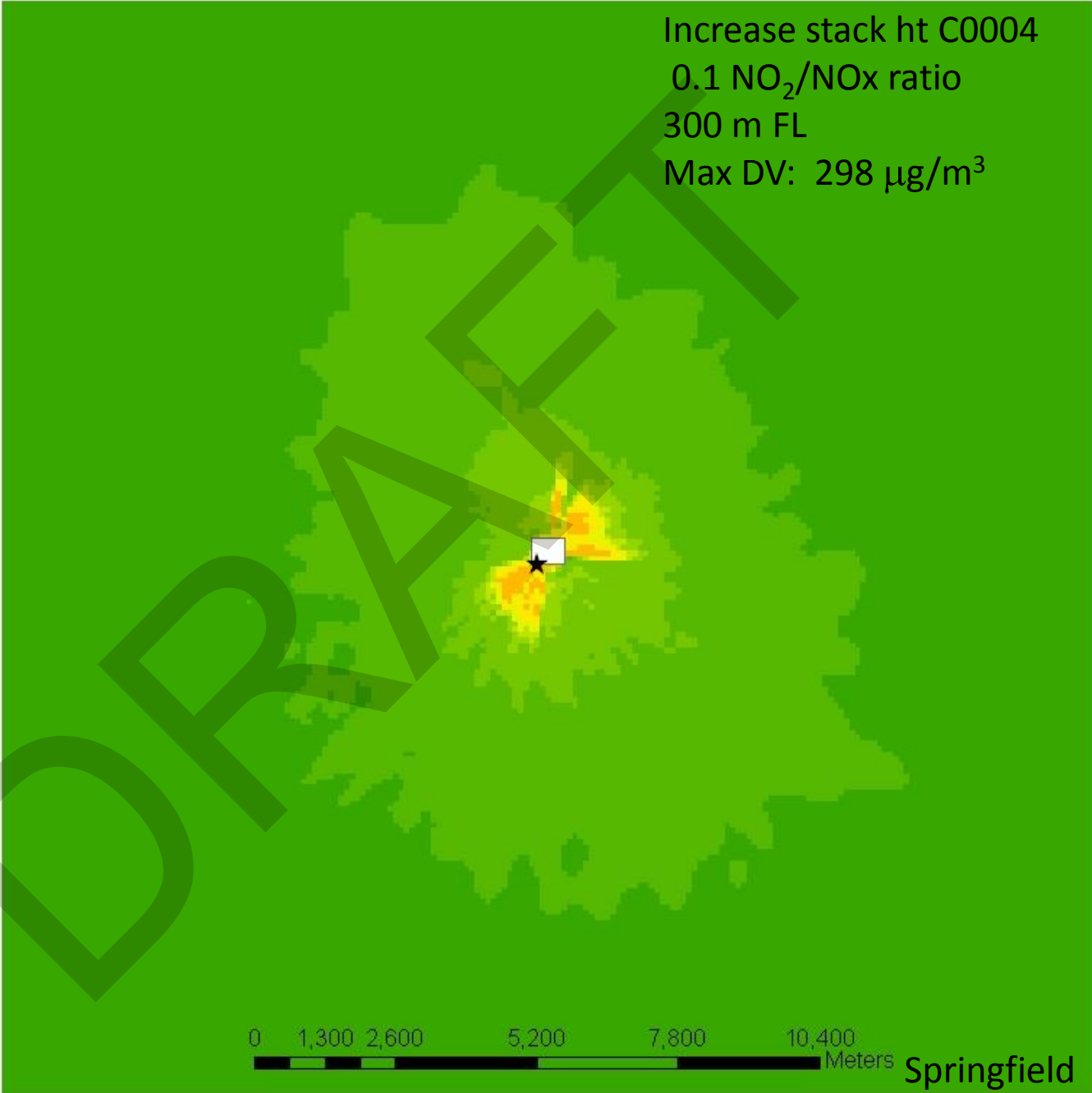
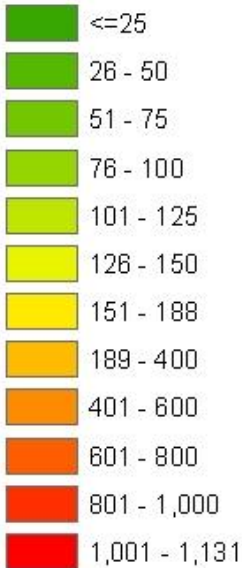
Base 0.5 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1131 μg/m<sup>3</sup>

### Legend



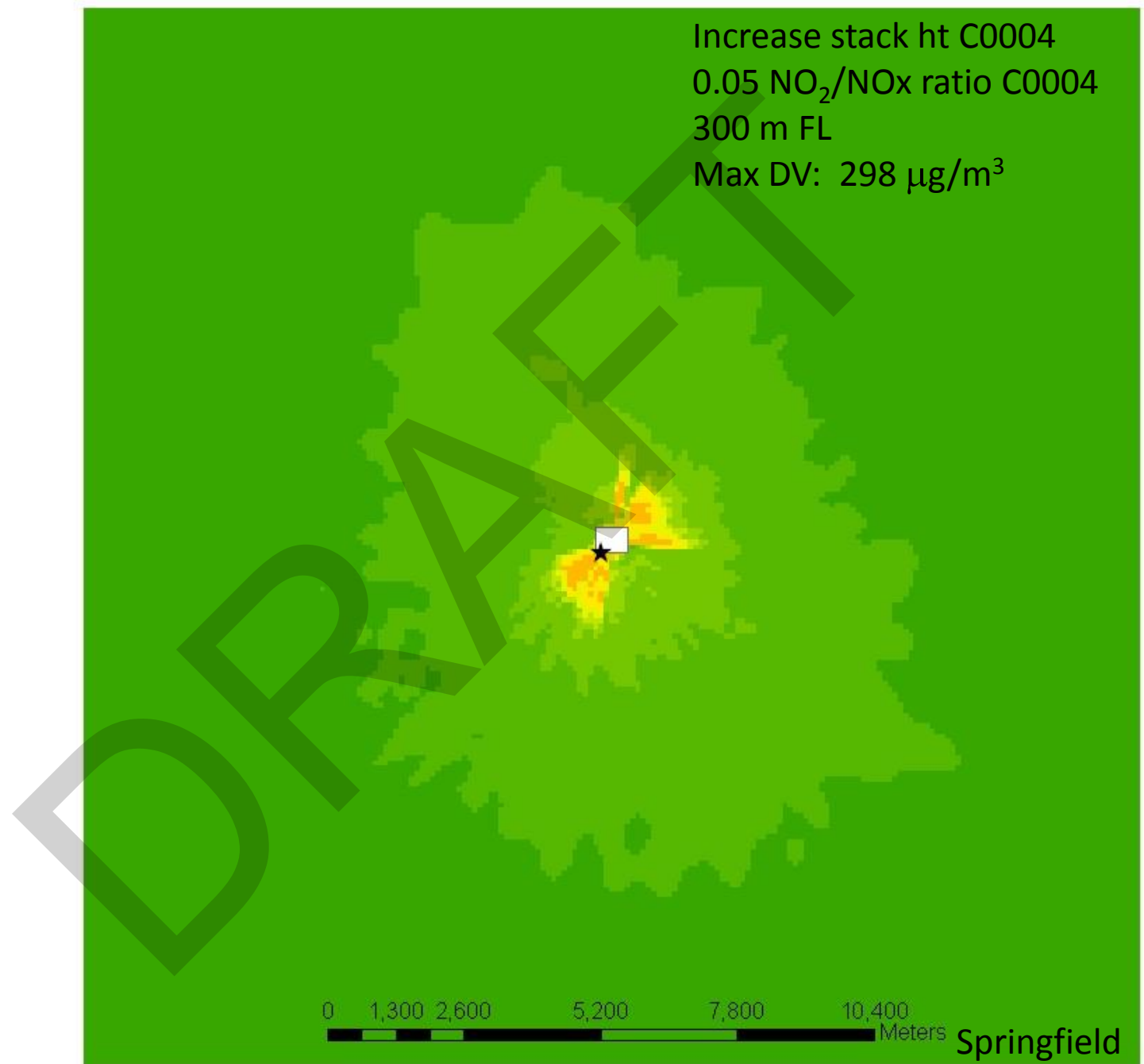
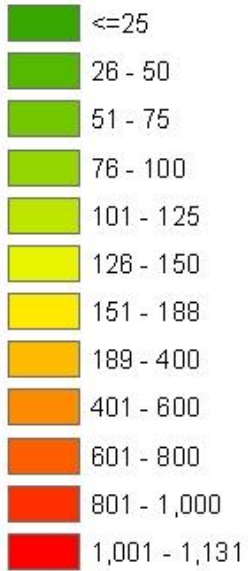
Increase stack ht C0004  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 298 μg/m<sup>3</sup>

**Legend**



Increase stack ht C0004  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 298 μg/m<sup>3</sup>

**Legend**

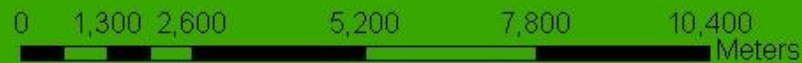
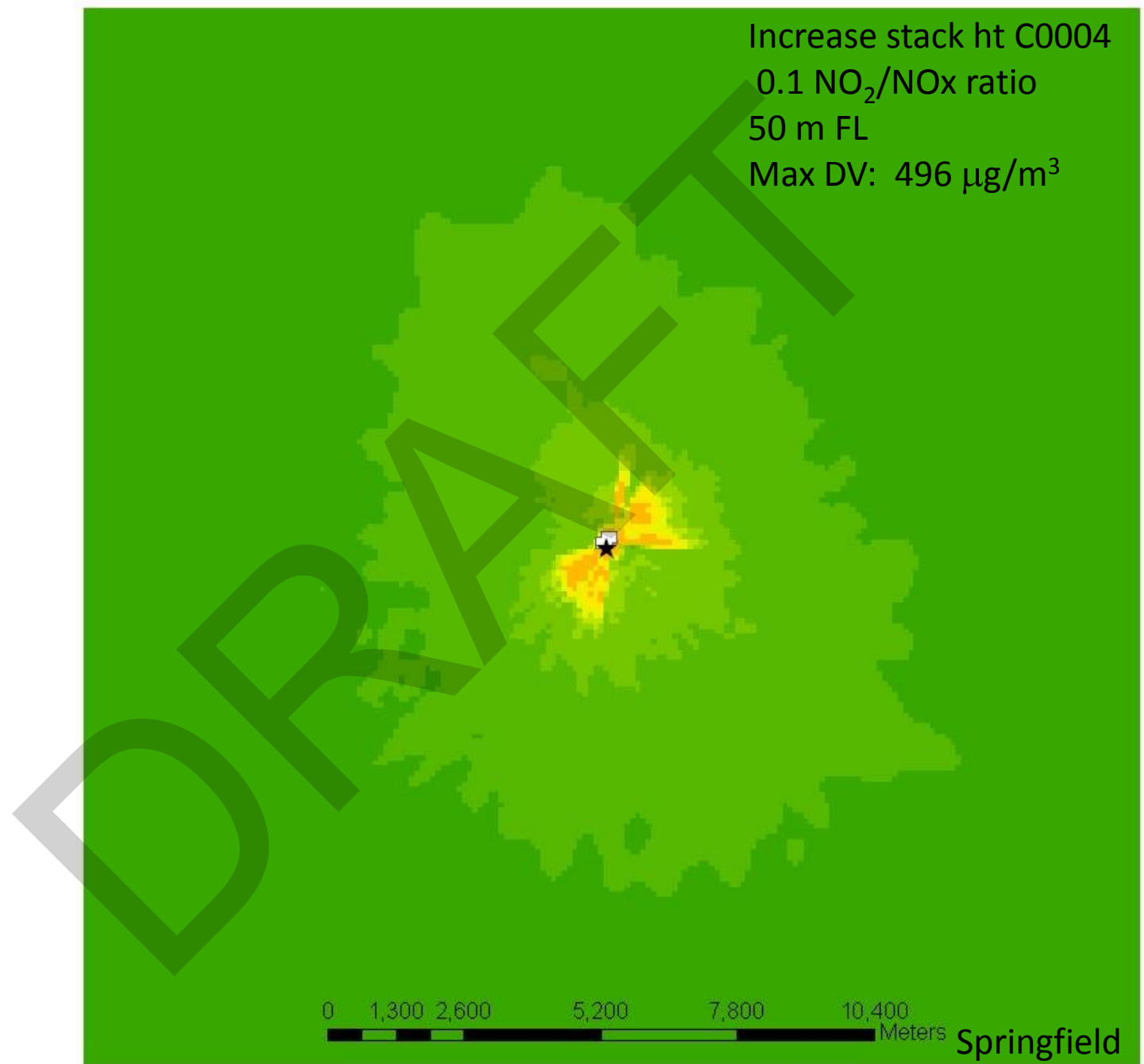
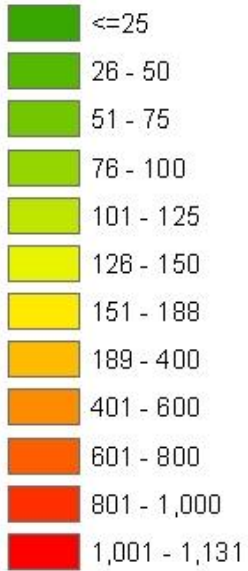


Springfield



Increase stack ht C0004  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 496 μg/m<sup>3</sup>

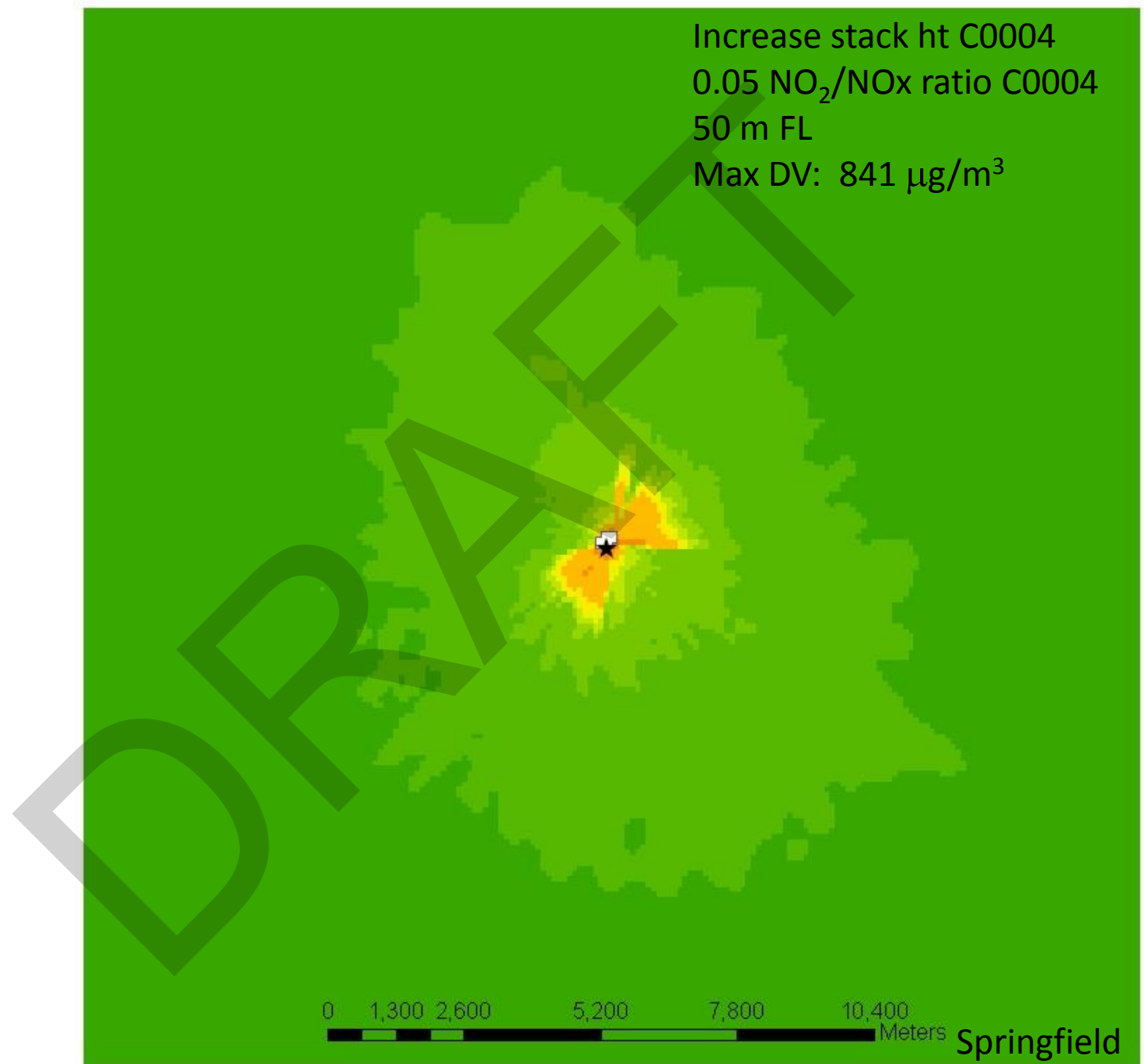
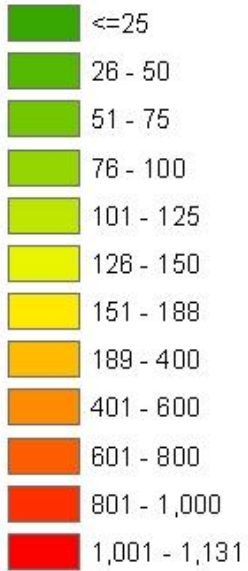
**Legend**



Springfield

Increase stack ht C0004  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 841 μg/m<sup>3</sup>

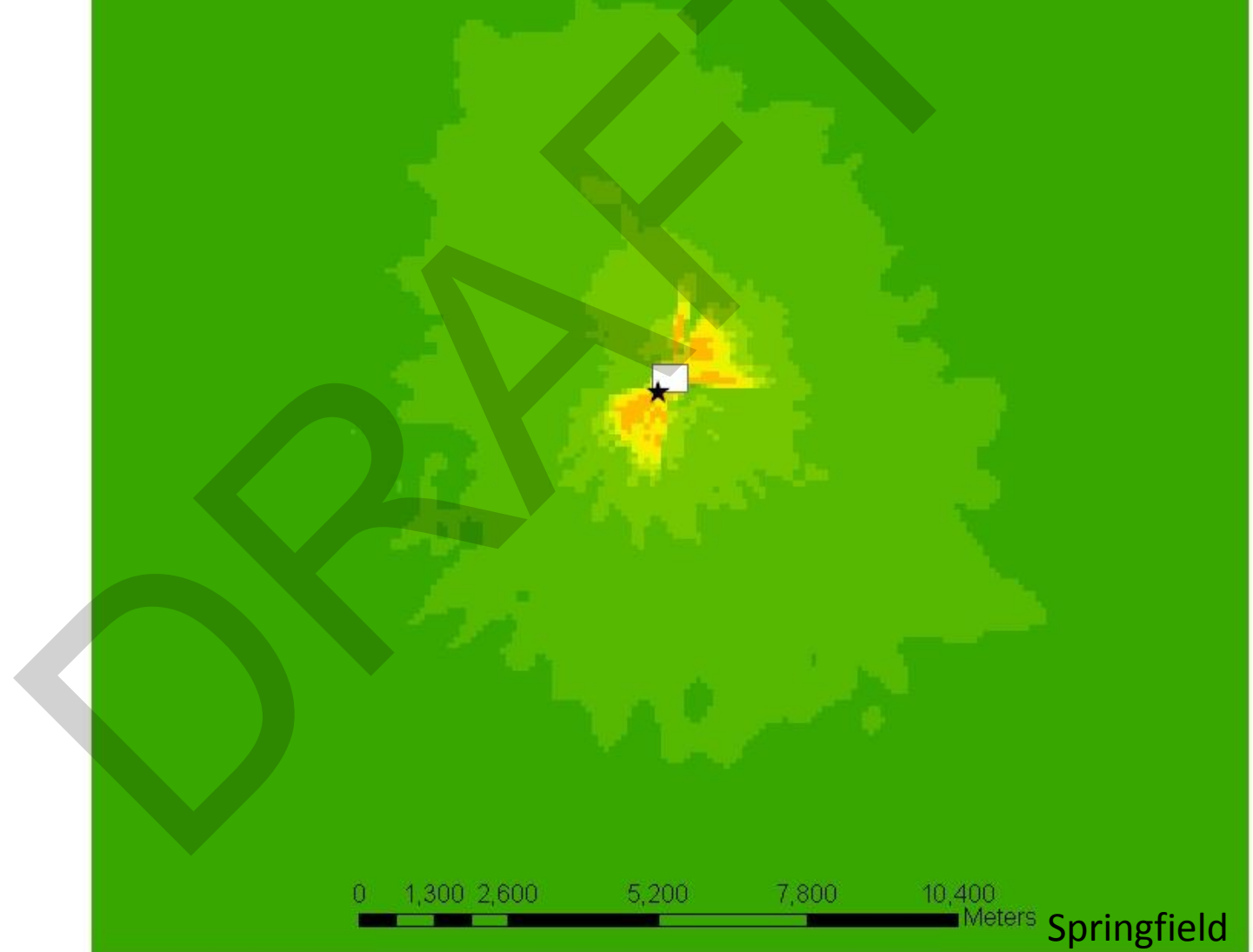
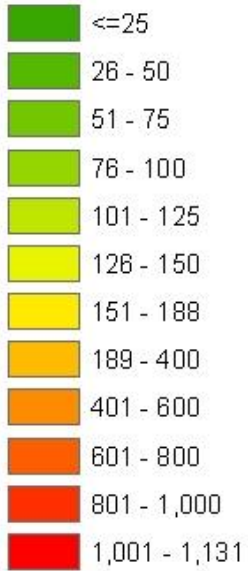
**Legend**



Springfield

Increase stack ht C0004 + controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 298 μg/m<sup>3</sup>

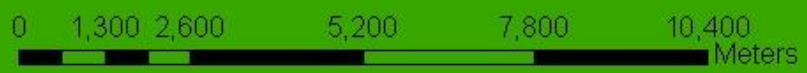
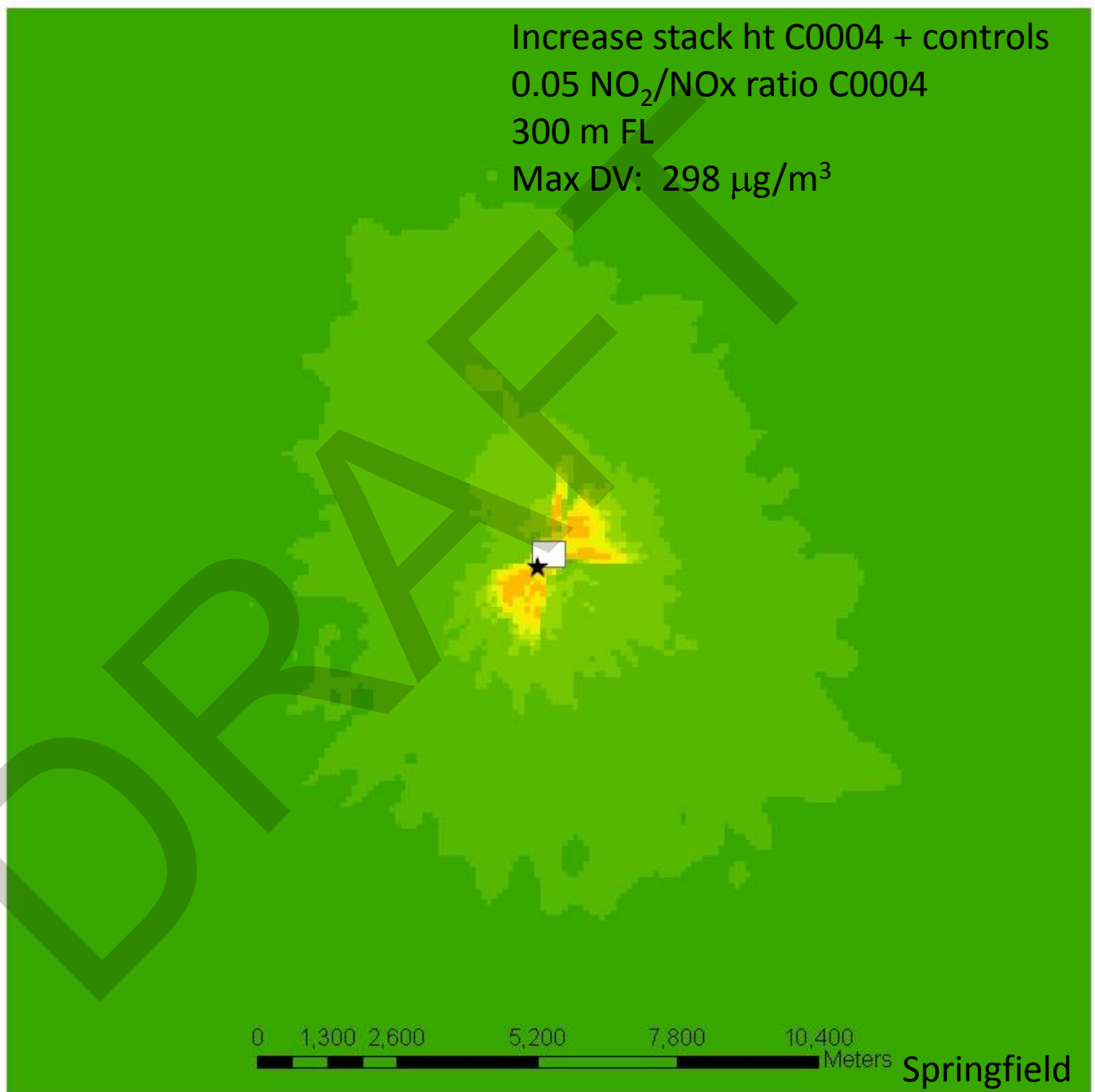
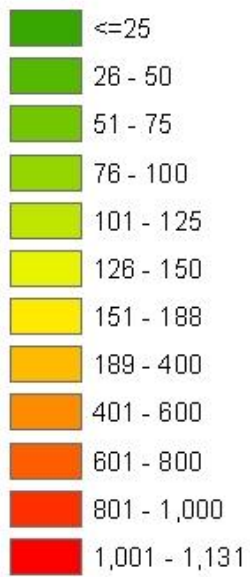
**Legend**



Springfield

Increase stack ht C0004 + controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 298 μg/m<sup>3</sup>

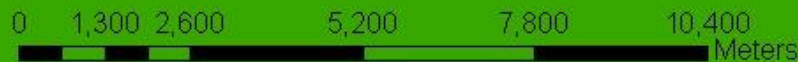
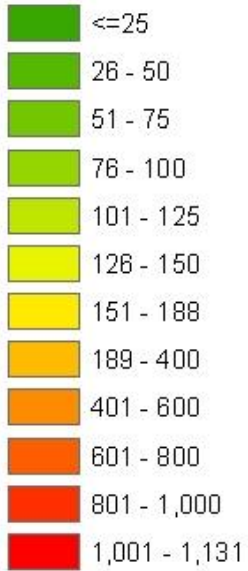
**Legend**



Springfield

Increase stack ht C0004 + controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 496 μg/m<sup>3</sup>

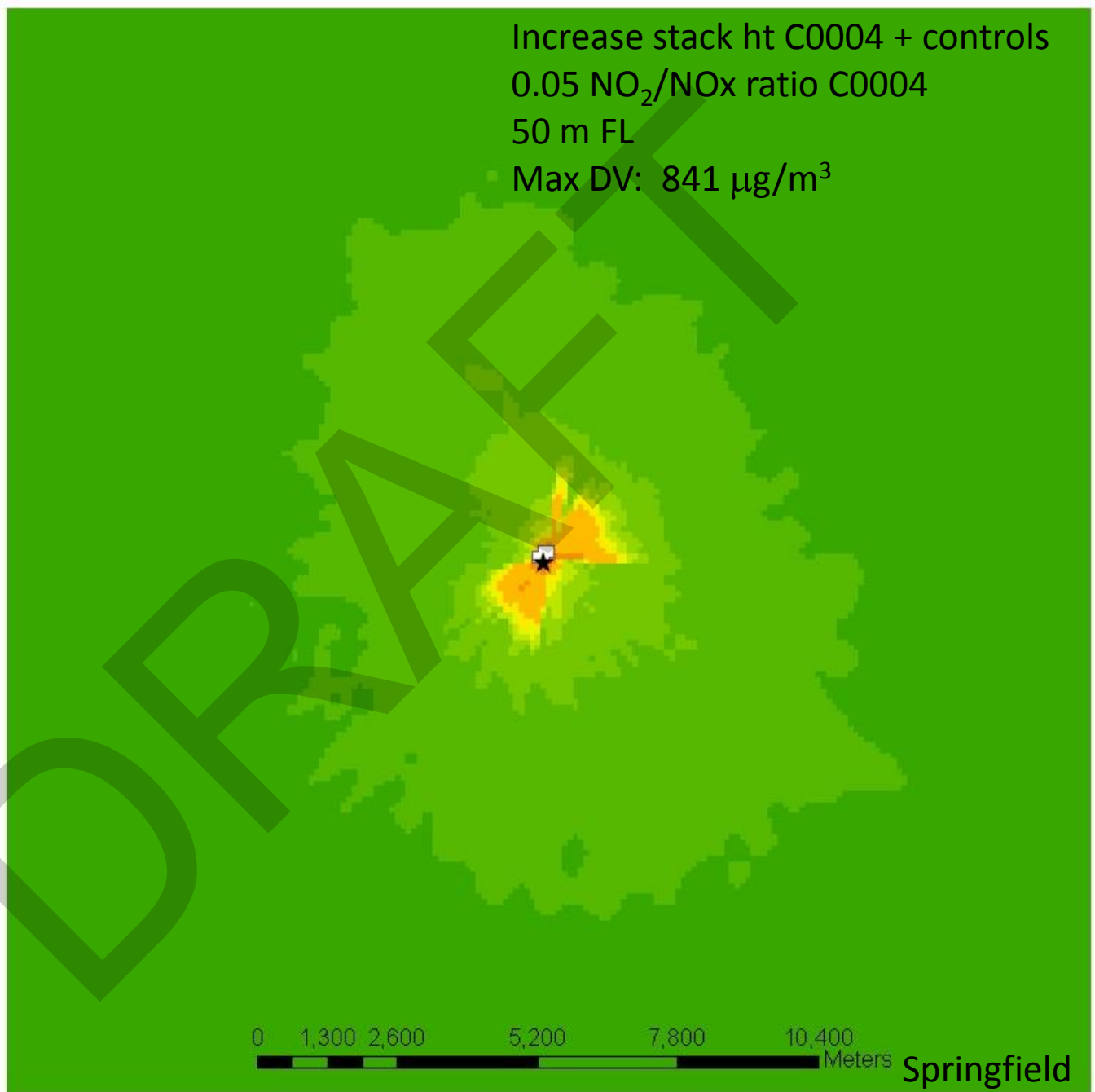
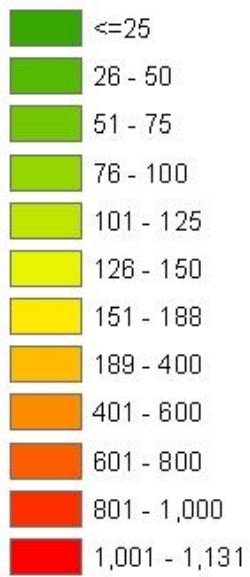
**Legend**



Springfield

Increase stack ht C0004 + controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 841 μg/m<sup>3</sup>

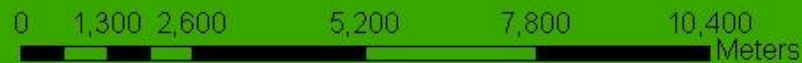
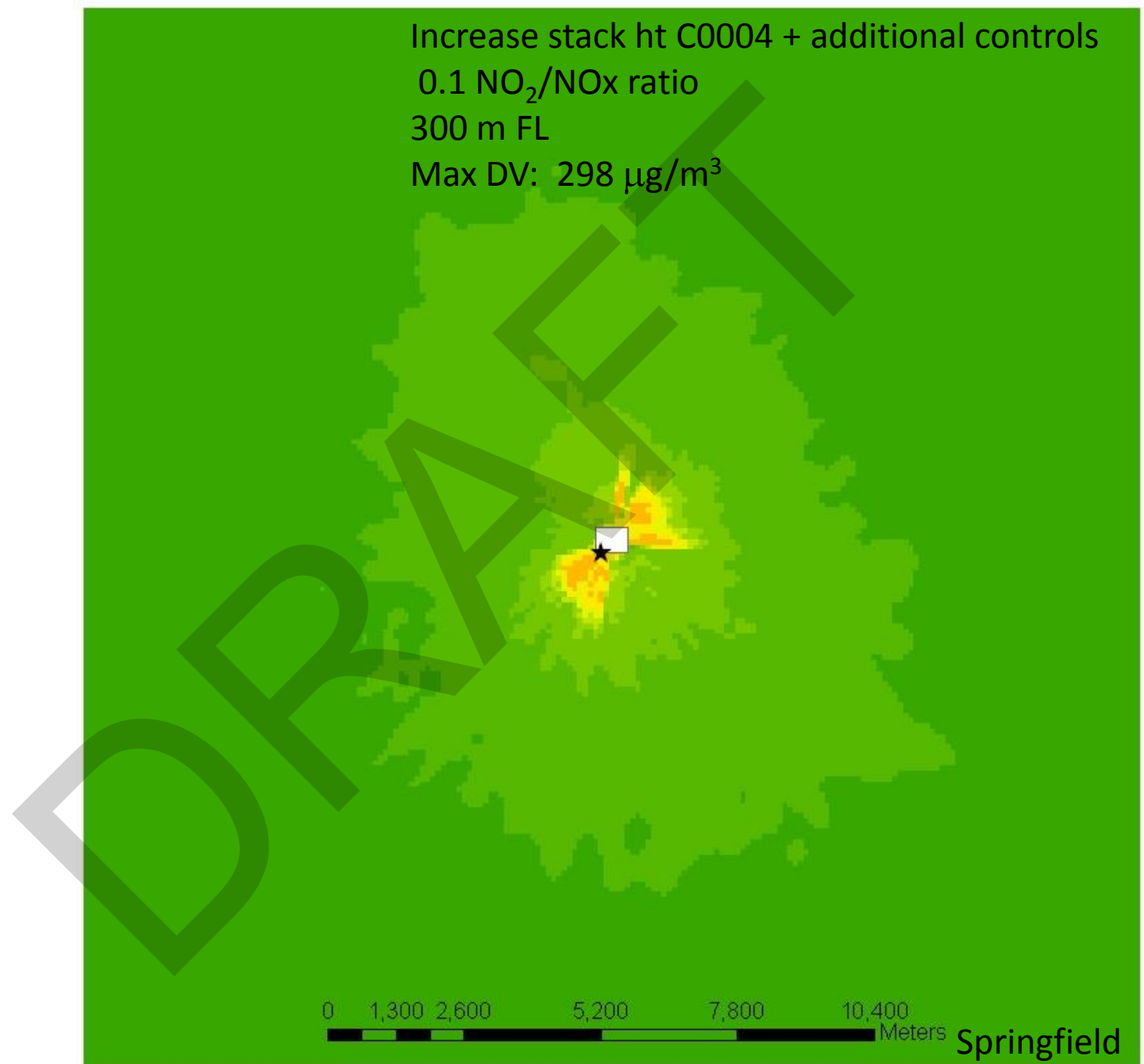
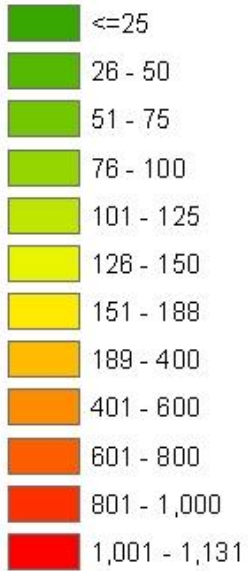
**Legend**



Springfield

Increase stack ht C0004 + additional controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 298 μg/m<sup>3</sup>

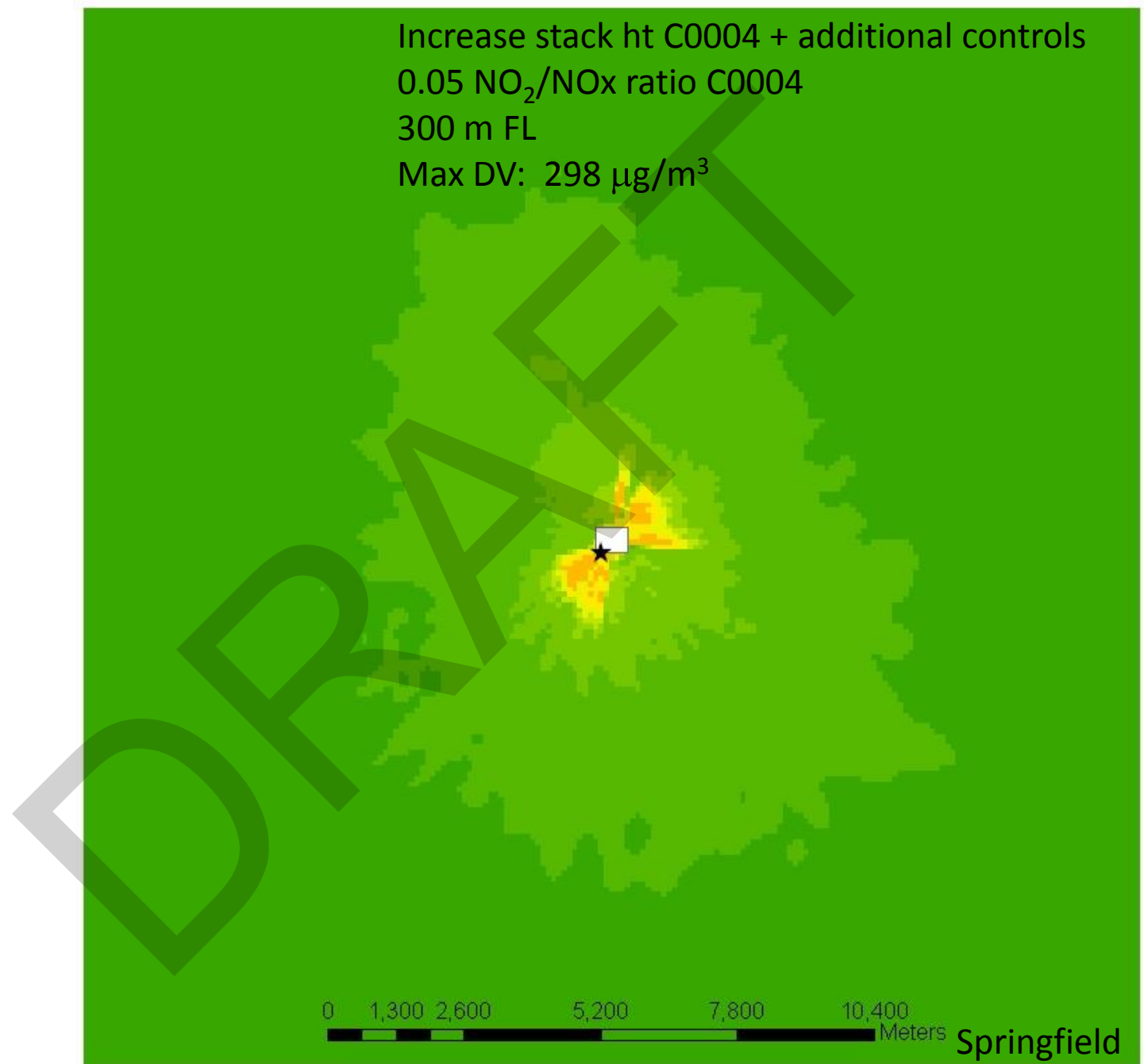
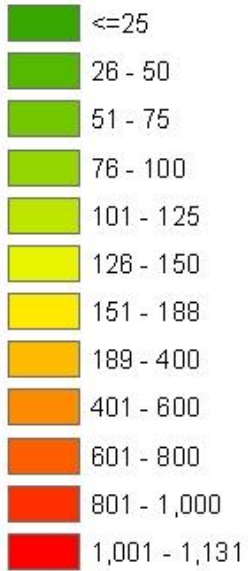
**Legend**



Springfield

Increase stack ht C0004 + additional controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 298 μg/m<sup>3</sup>

**Legend**

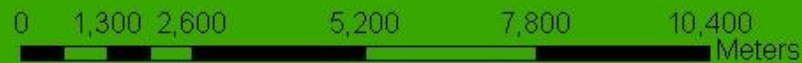
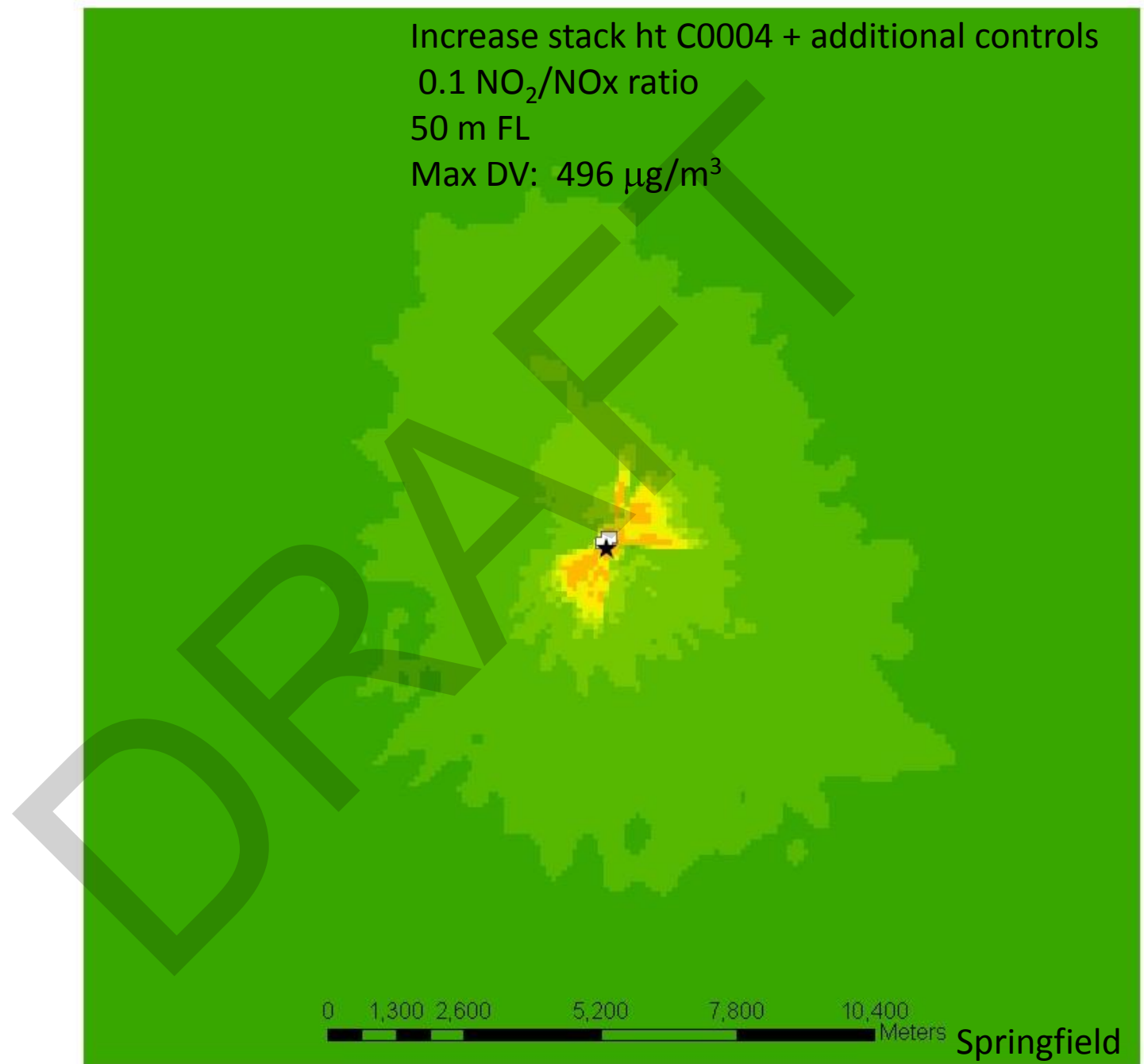
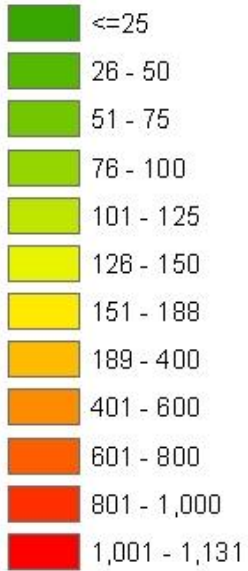


Springfield



Increase stack ht C0004 + additional controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 496 μg/m<sup>3</sup>

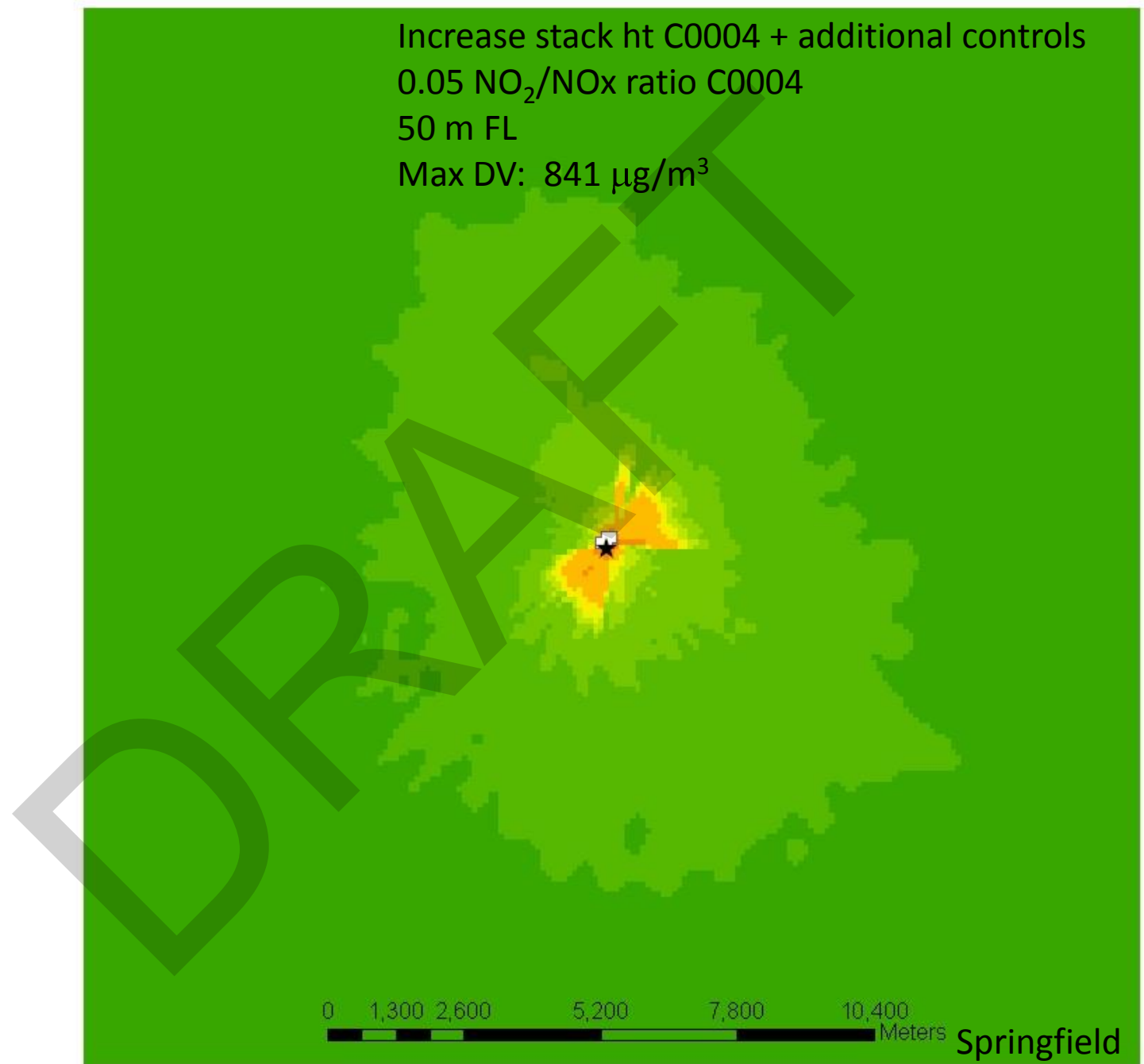
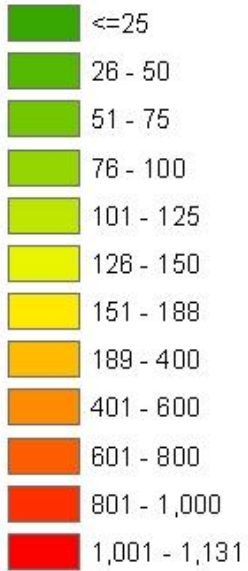
**Legend**



Springfield

Increase stack ht C0004 + additional controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 841 μg/m<sup>3</sup>

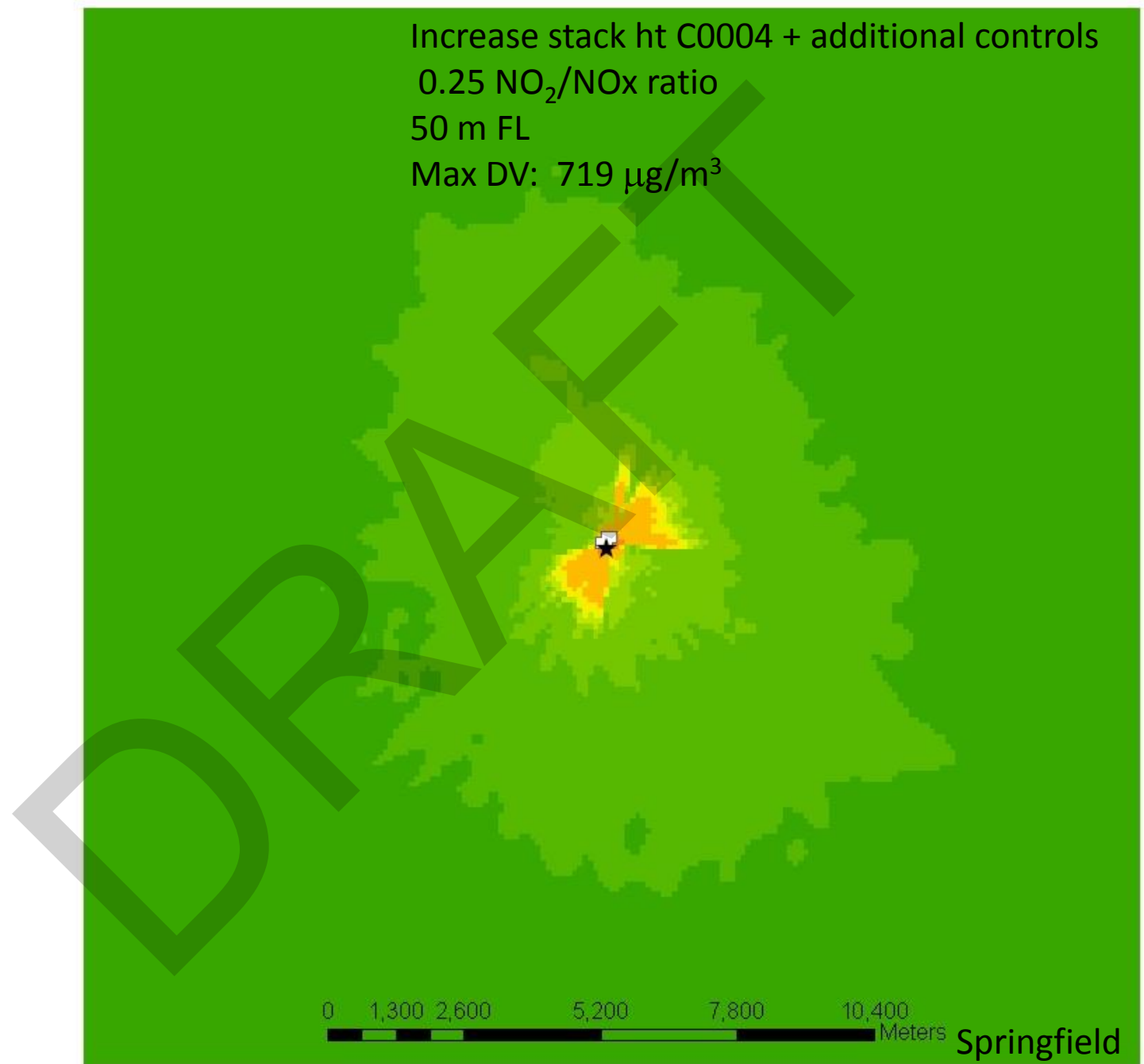
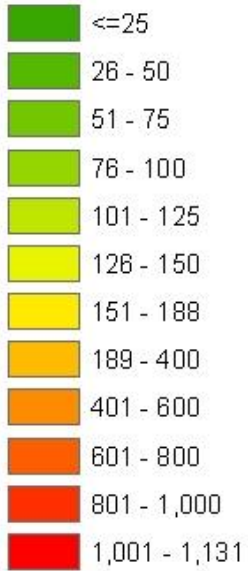
**Legend**



Springfield

Increase stack ht C0004 + additional controls  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 719 μg/m<sup>3</sup>

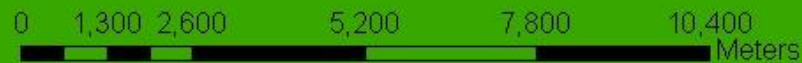
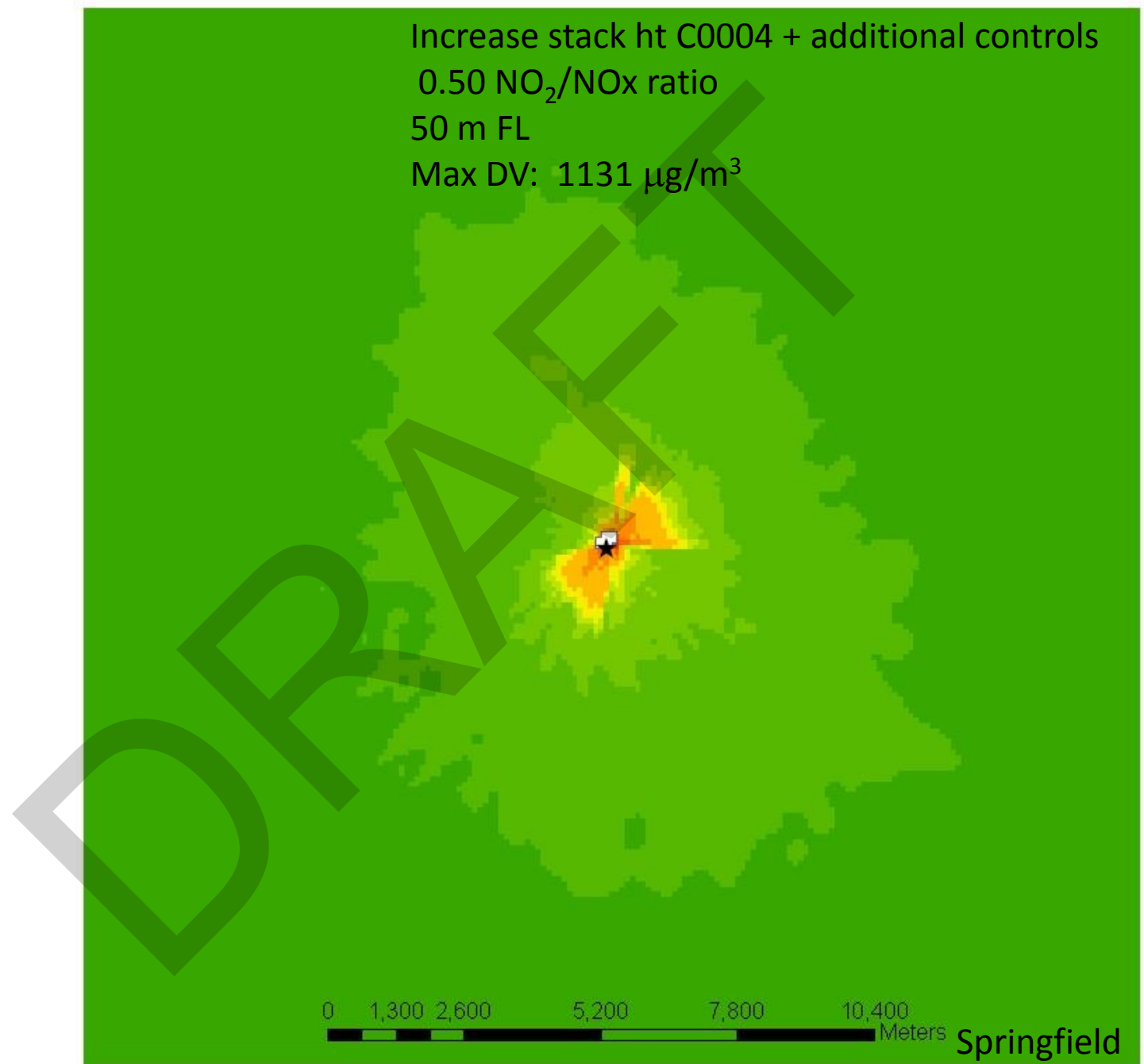
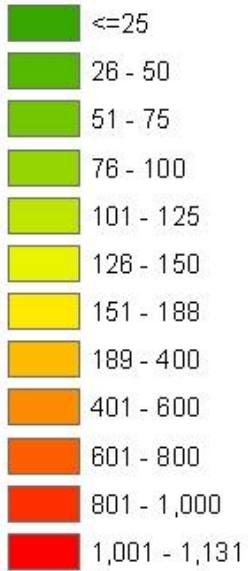
**Legend**



Springfield

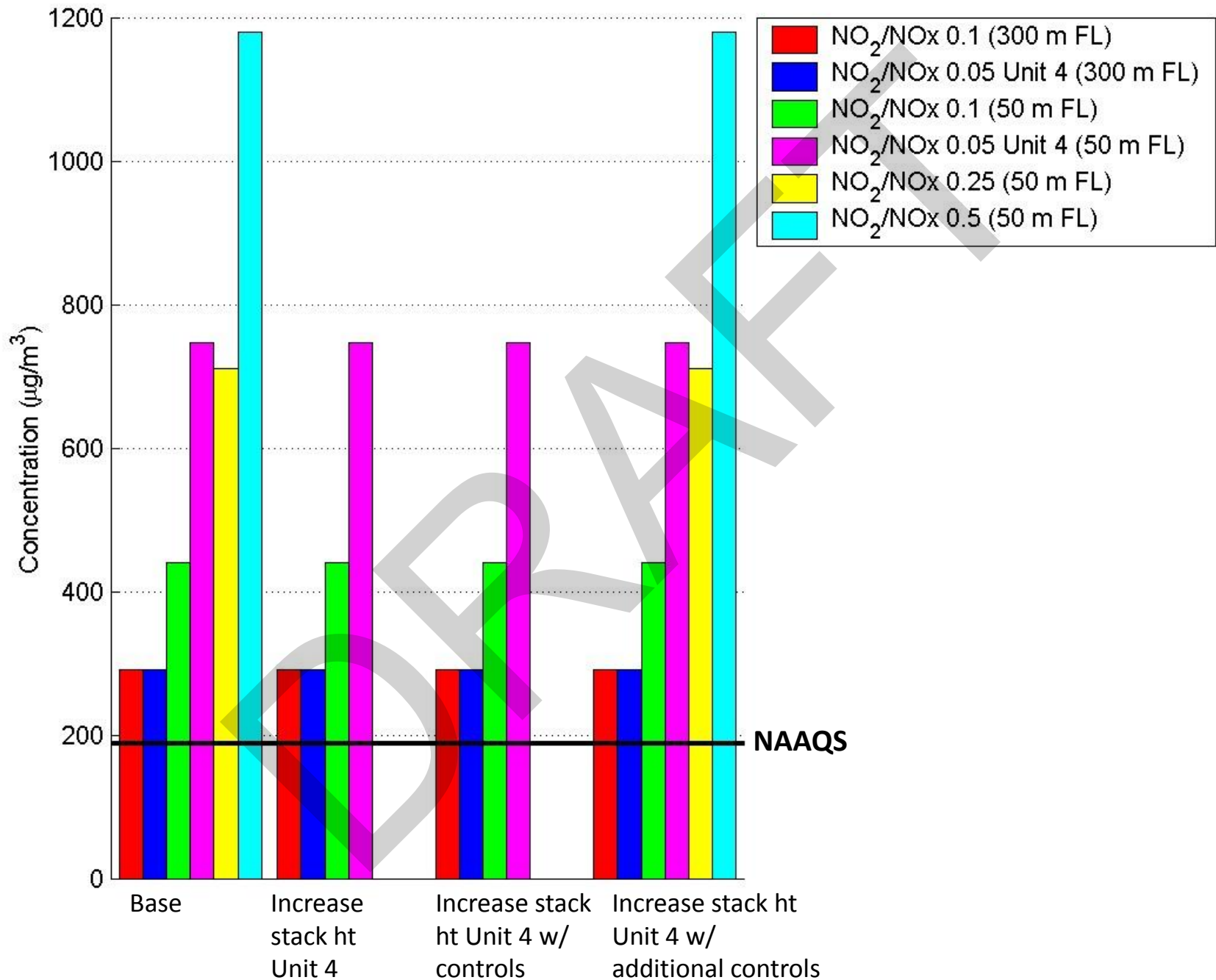
Increase stack ht C0004 + additional controls  
0.50 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1131 μg/m<sup>3</sup>

**Legend**



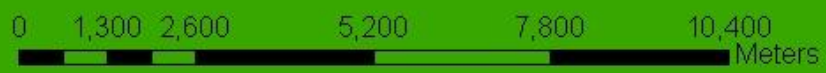
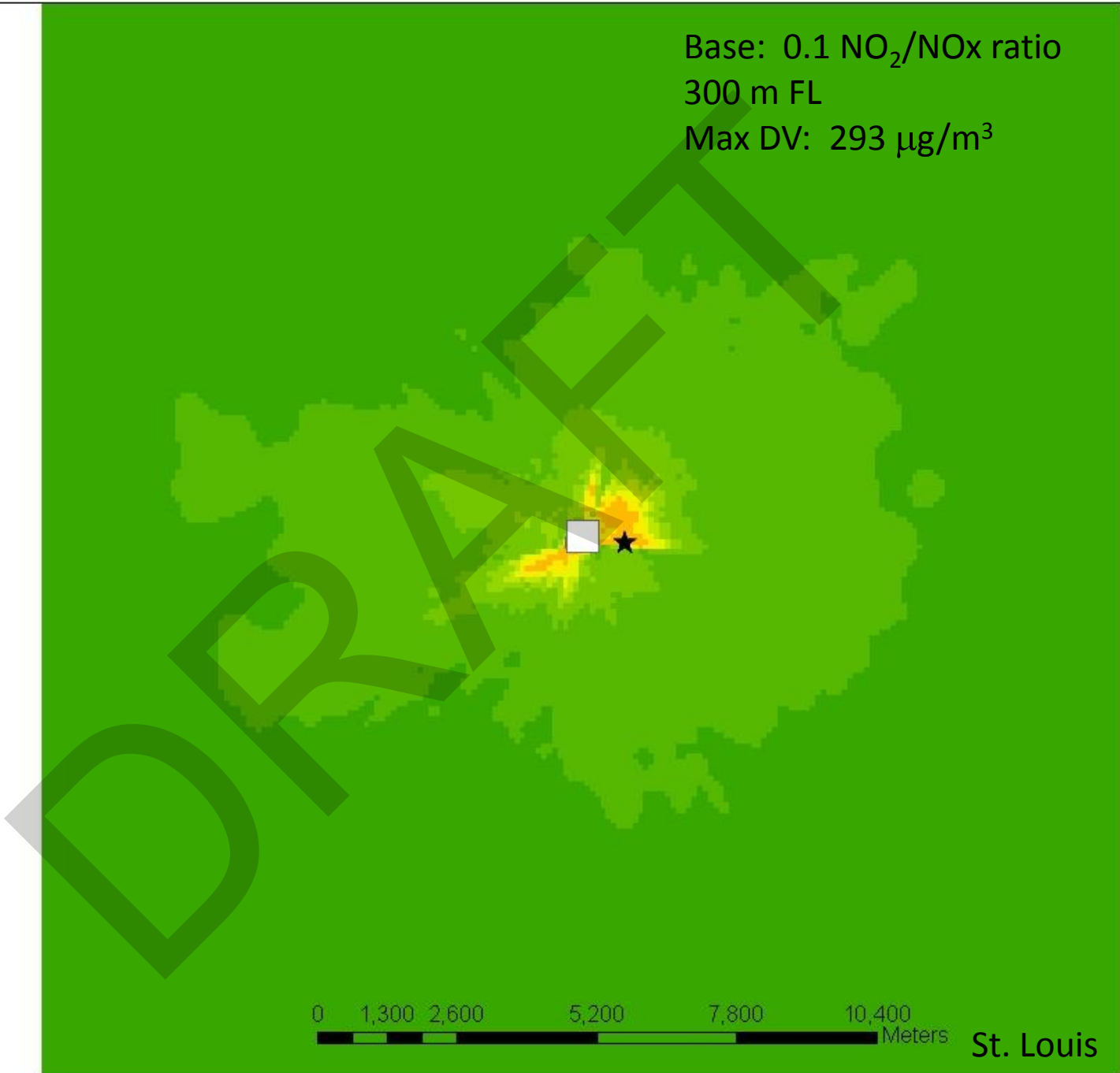
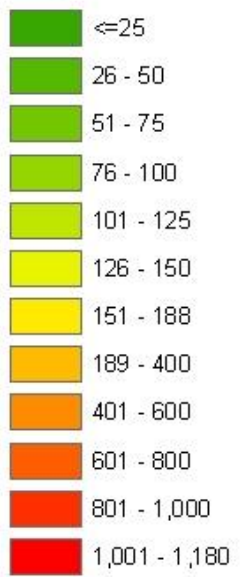
Springfield

# Ethanol Plant (St. Louis): NO<sub>2</sub>



Base: 0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 293 μg/m<sup>3</sup>

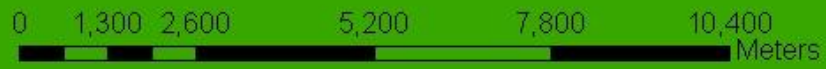
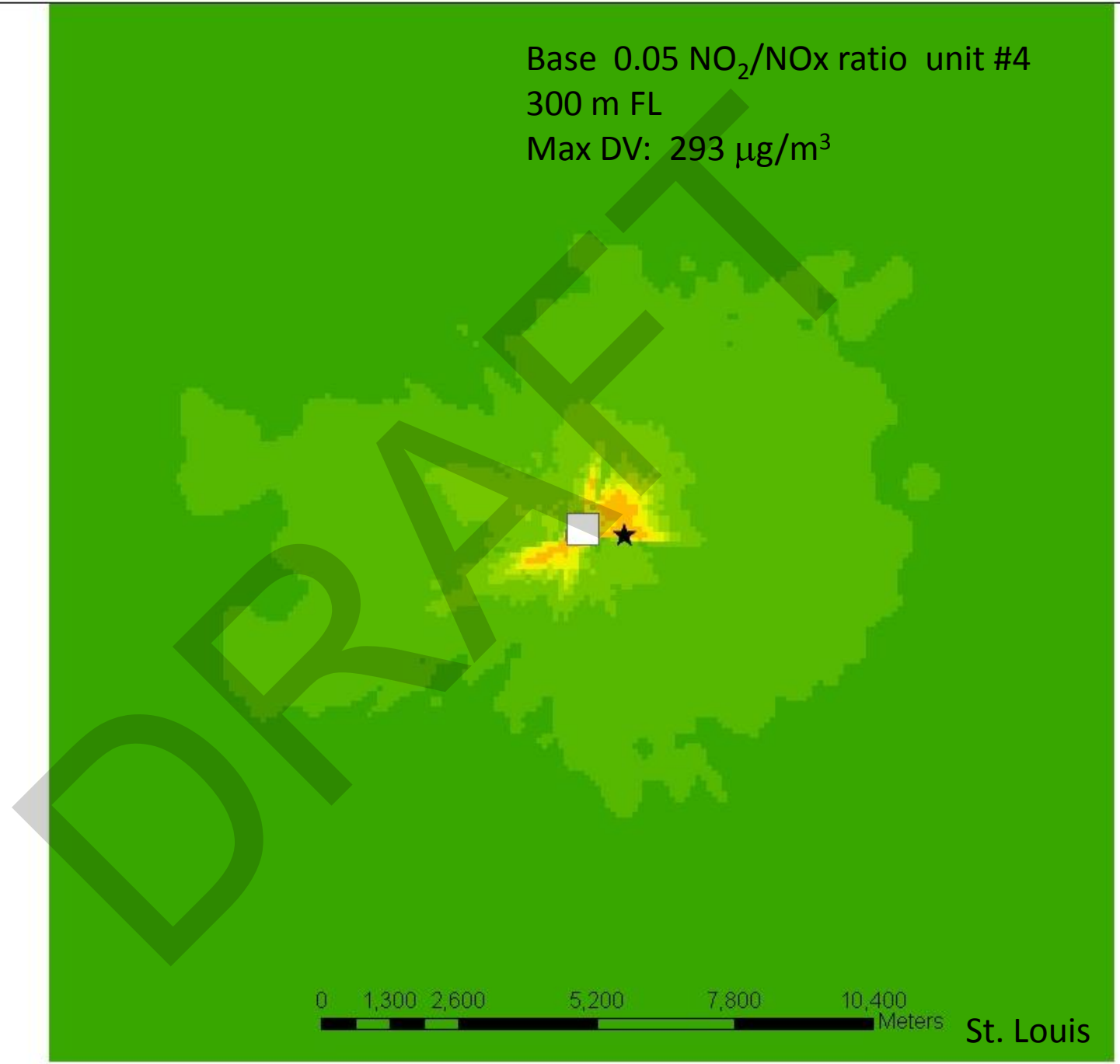
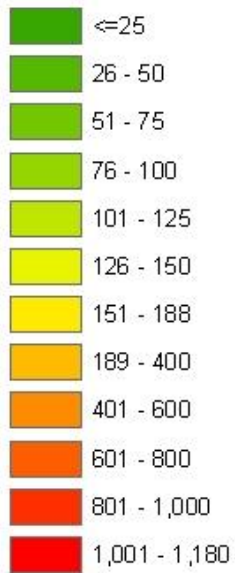
**Legend**



St. Louis

Base 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio unit #4  
300 m FL  
Max DV: 293 μg/m<sup>3</sup>

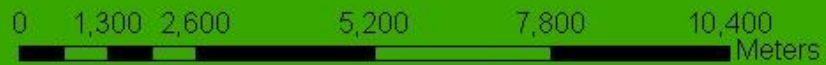
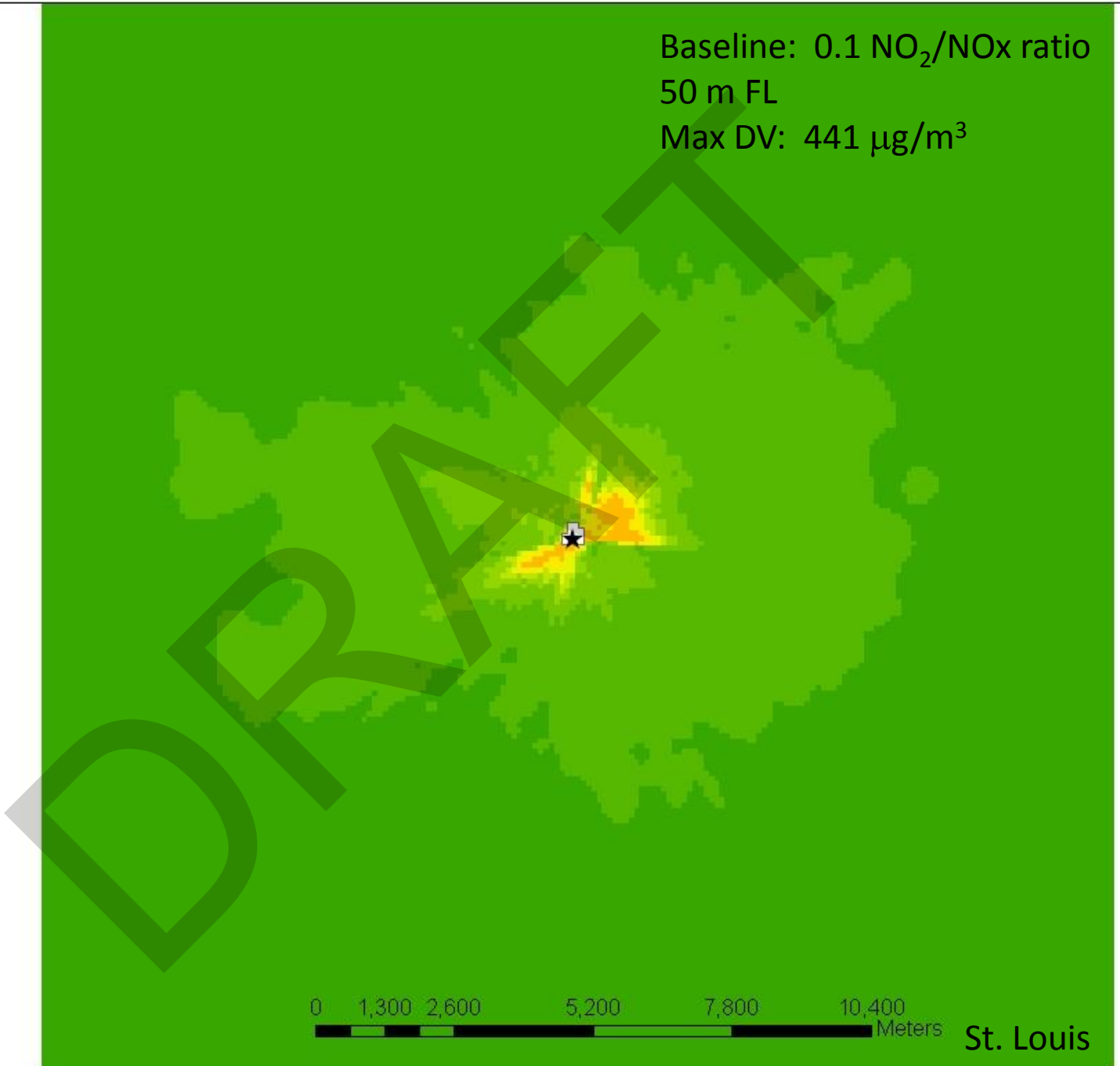
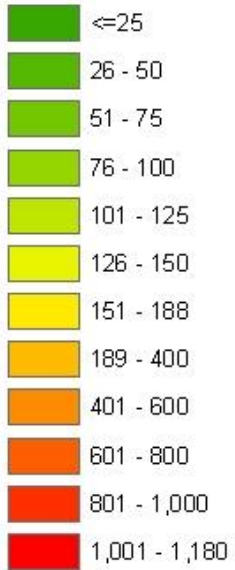
**Legend**



St. Louis

Baseline: 0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 441 μg/m<sup>3</sup>

### Legend

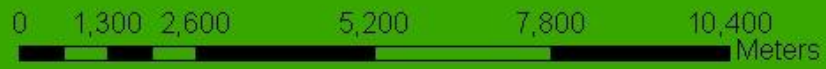
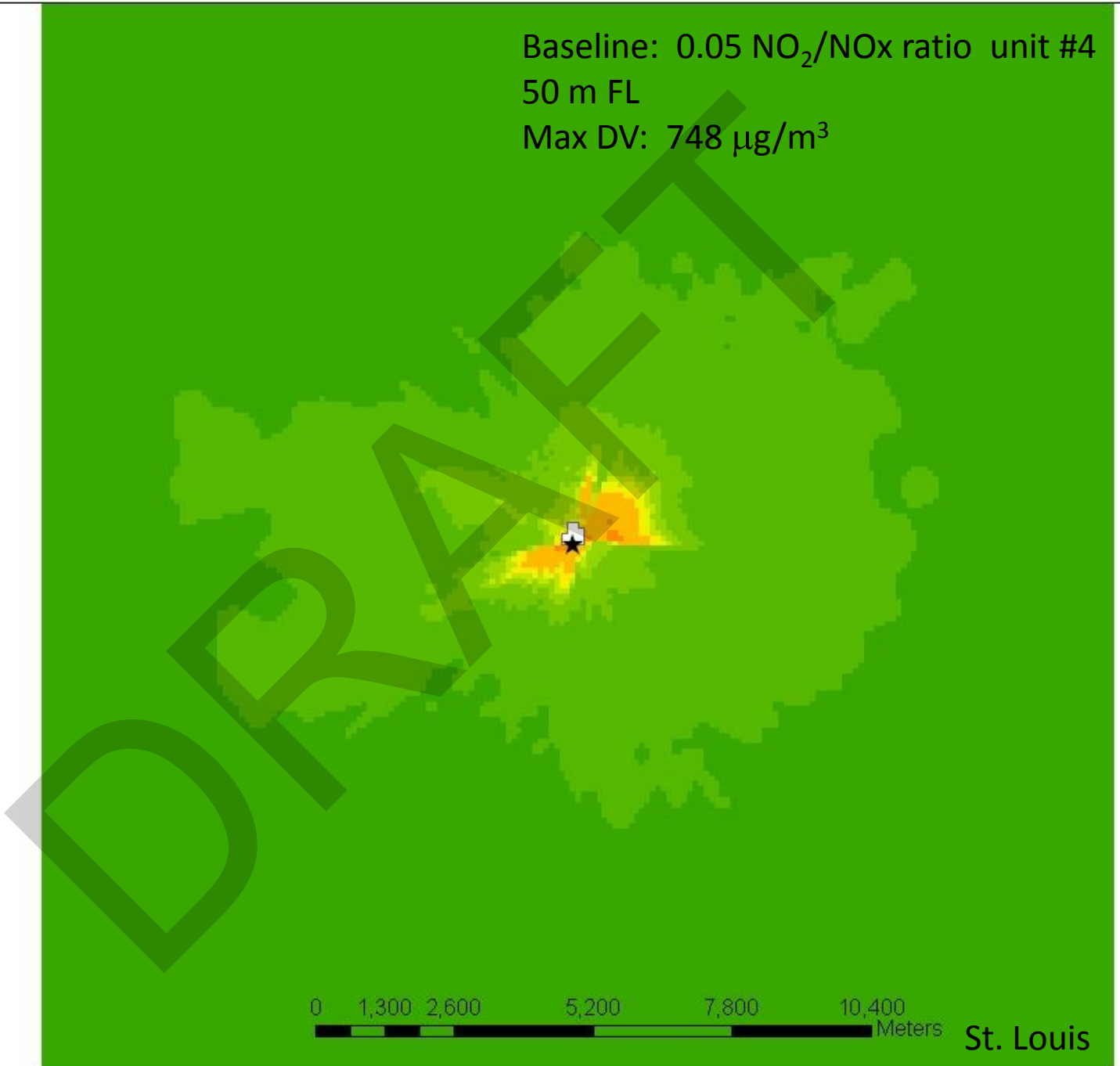
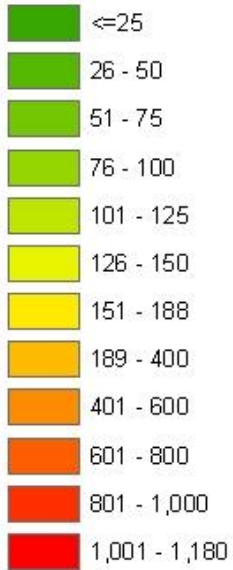


St. Louis



Baseline: 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio unit #4  
50 m FL  
Max DV: 748 μg/m<sup>3</sup>

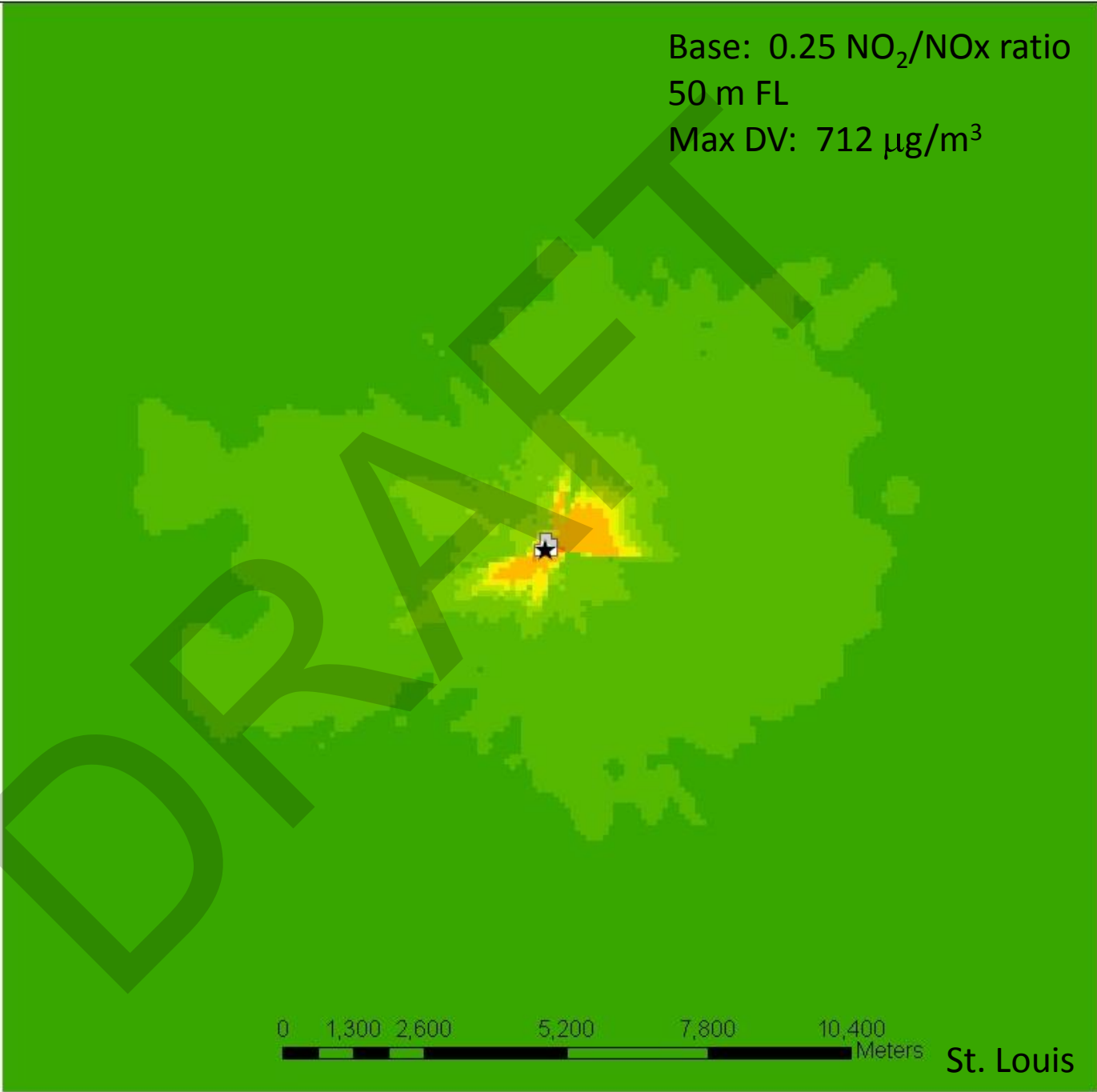
### Legend



St. Louis

Base: 0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 712 μg/m<sup>3</sup>

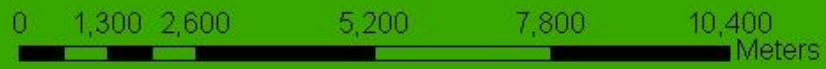
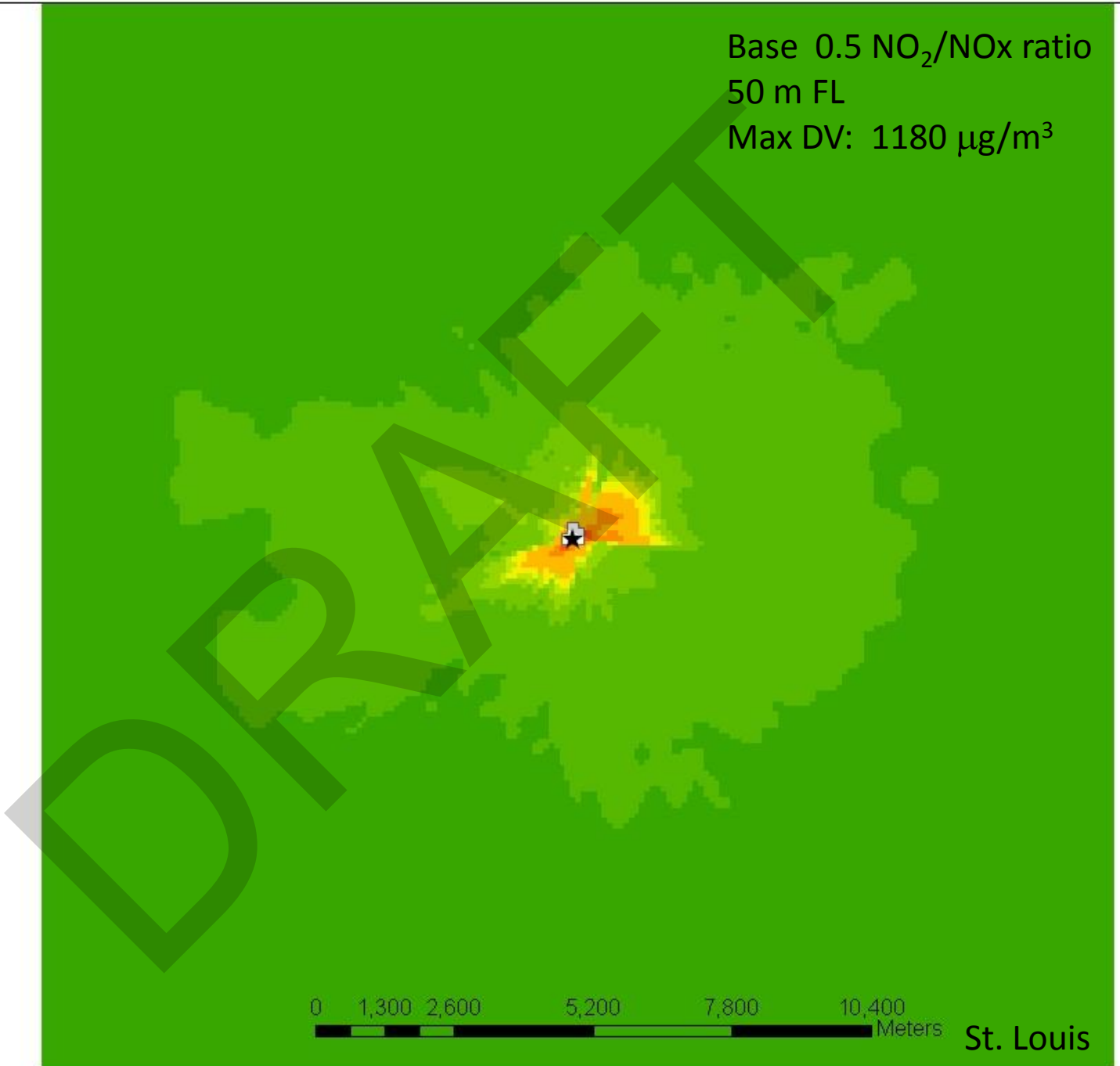
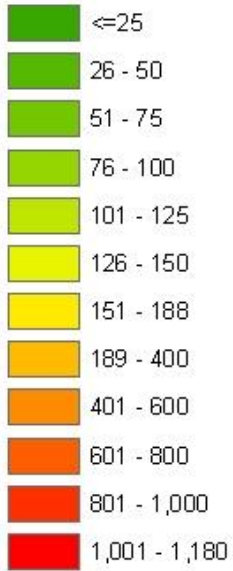
**Legend**



St. Louis

Base 0.5 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1180 μg/m<sup>3</sup>

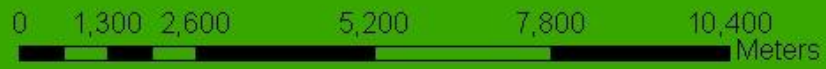
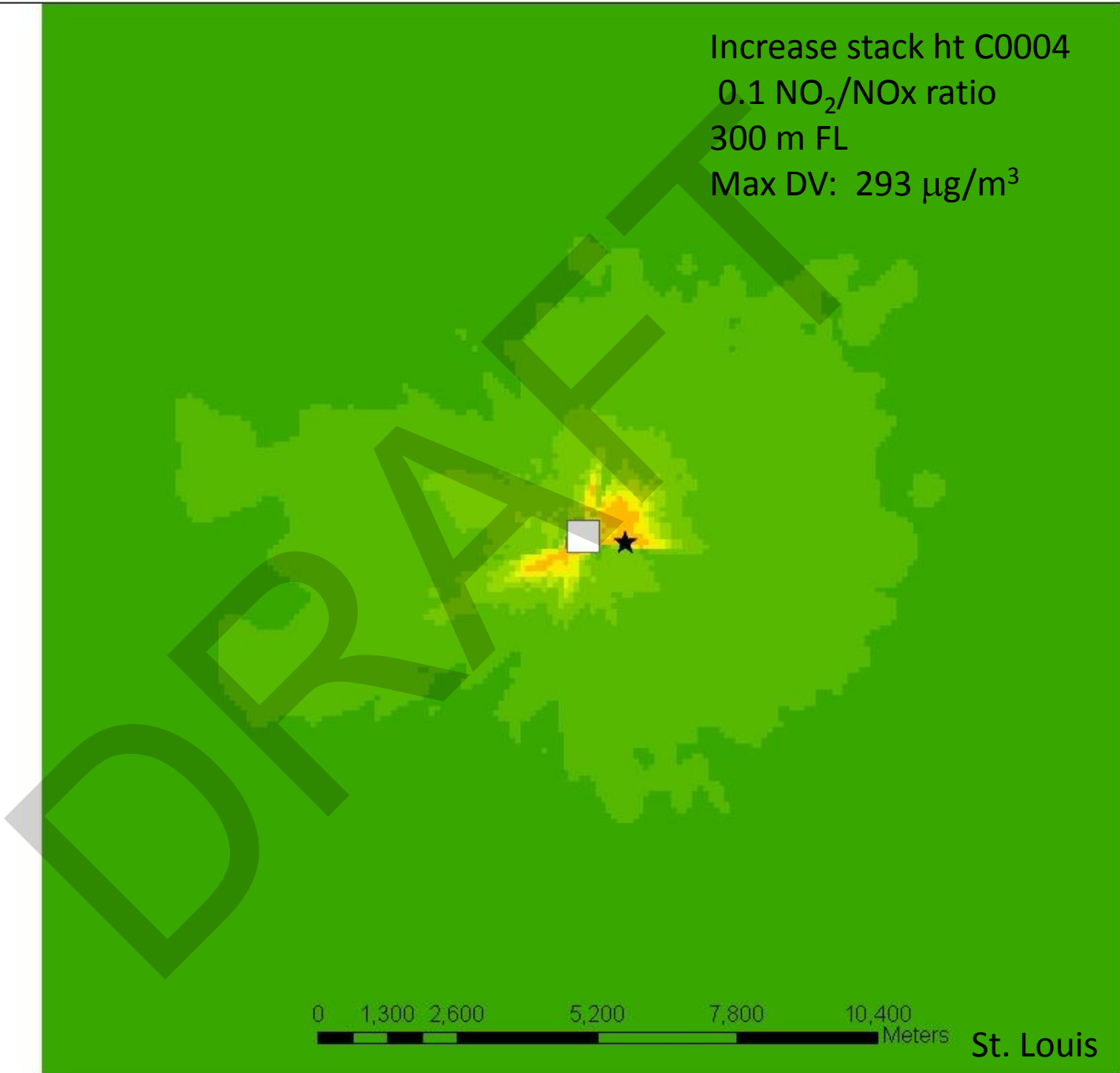
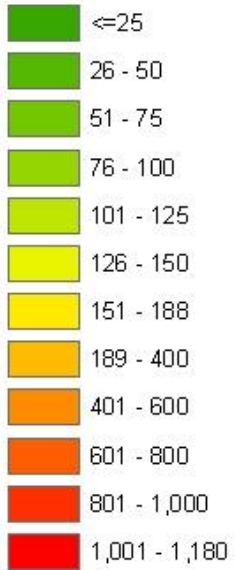
### Legend



St. Louis

Increase stack ht C0004  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 293 μg/m<sup>3</sup>

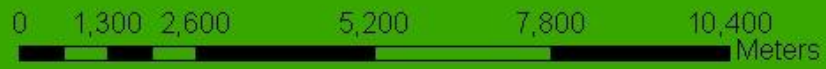
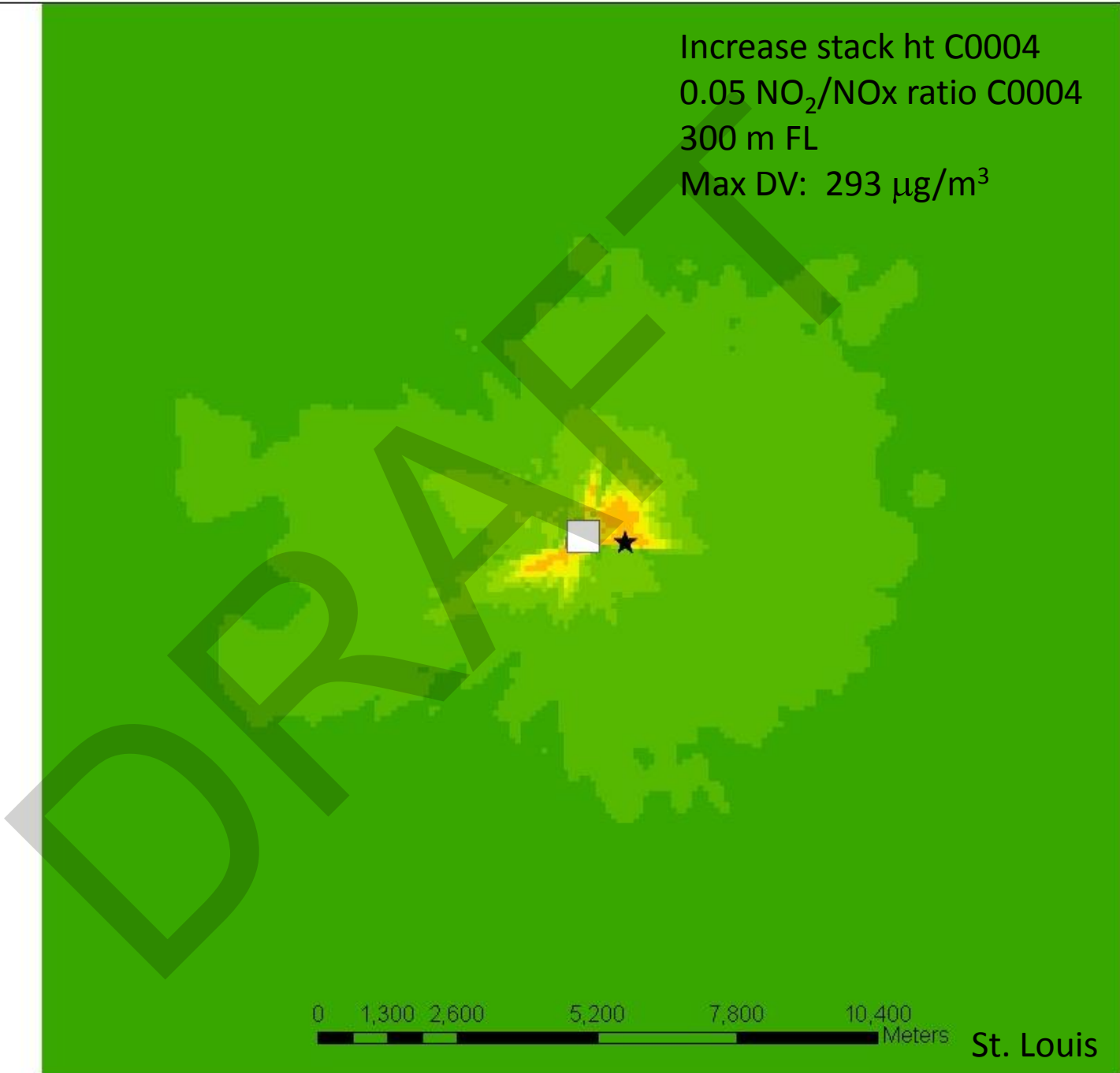
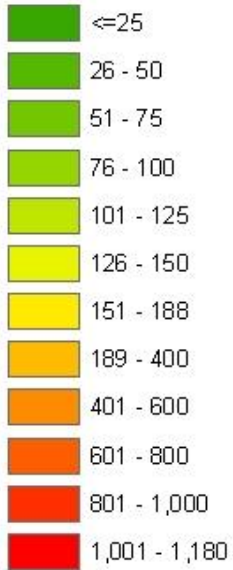
### Legend



St. Louis

Increase stack ht C0004  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 293 μg/m<sup>3</sup>

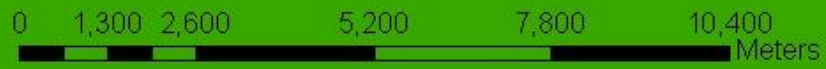
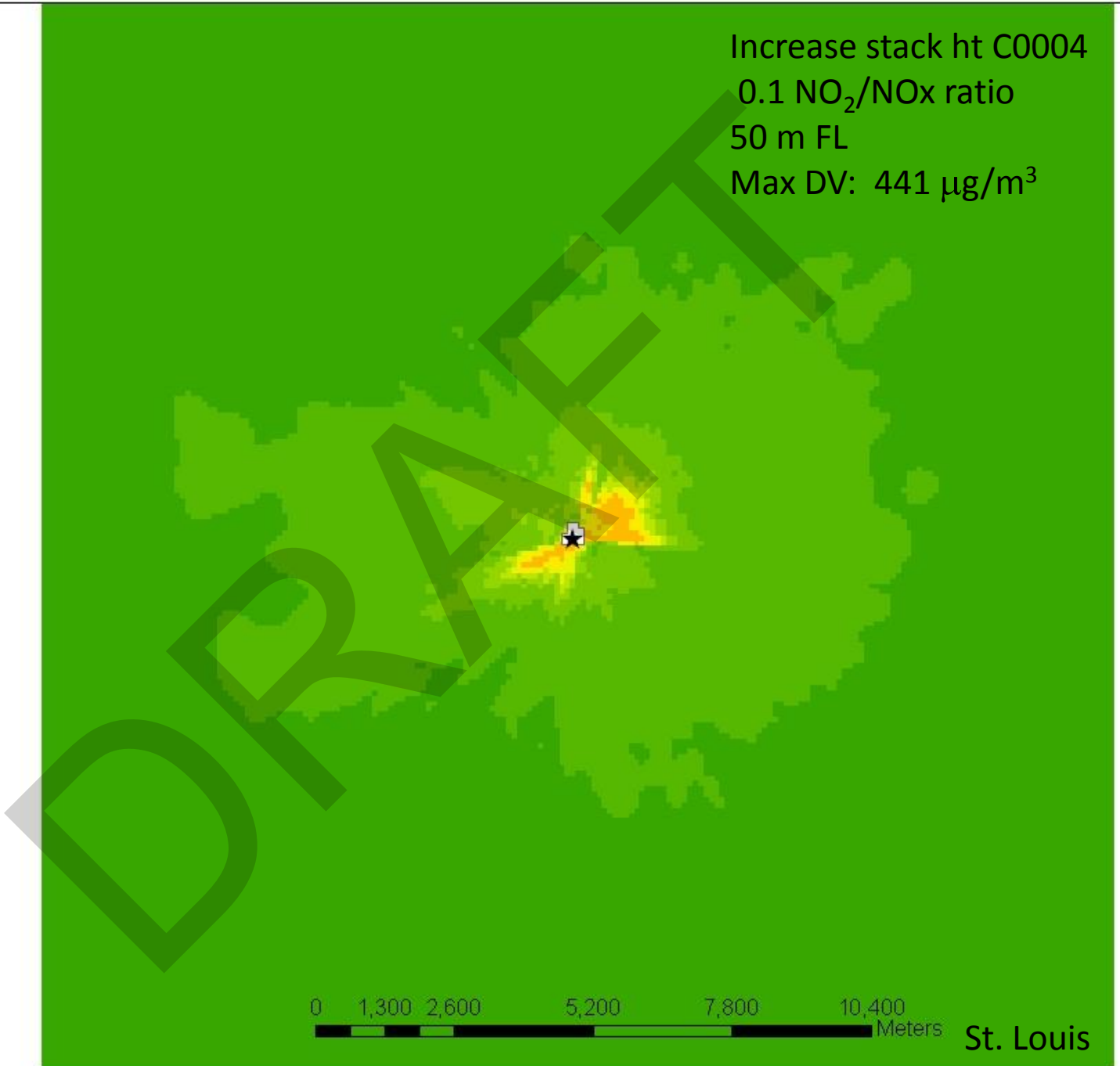
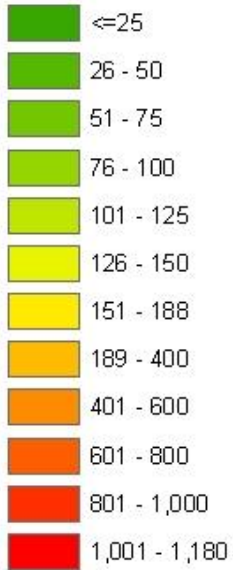
### Legend



St. Louis

Increase stack ht C0004  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 441 μg/m<sup>3</sup>

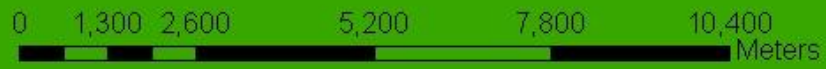
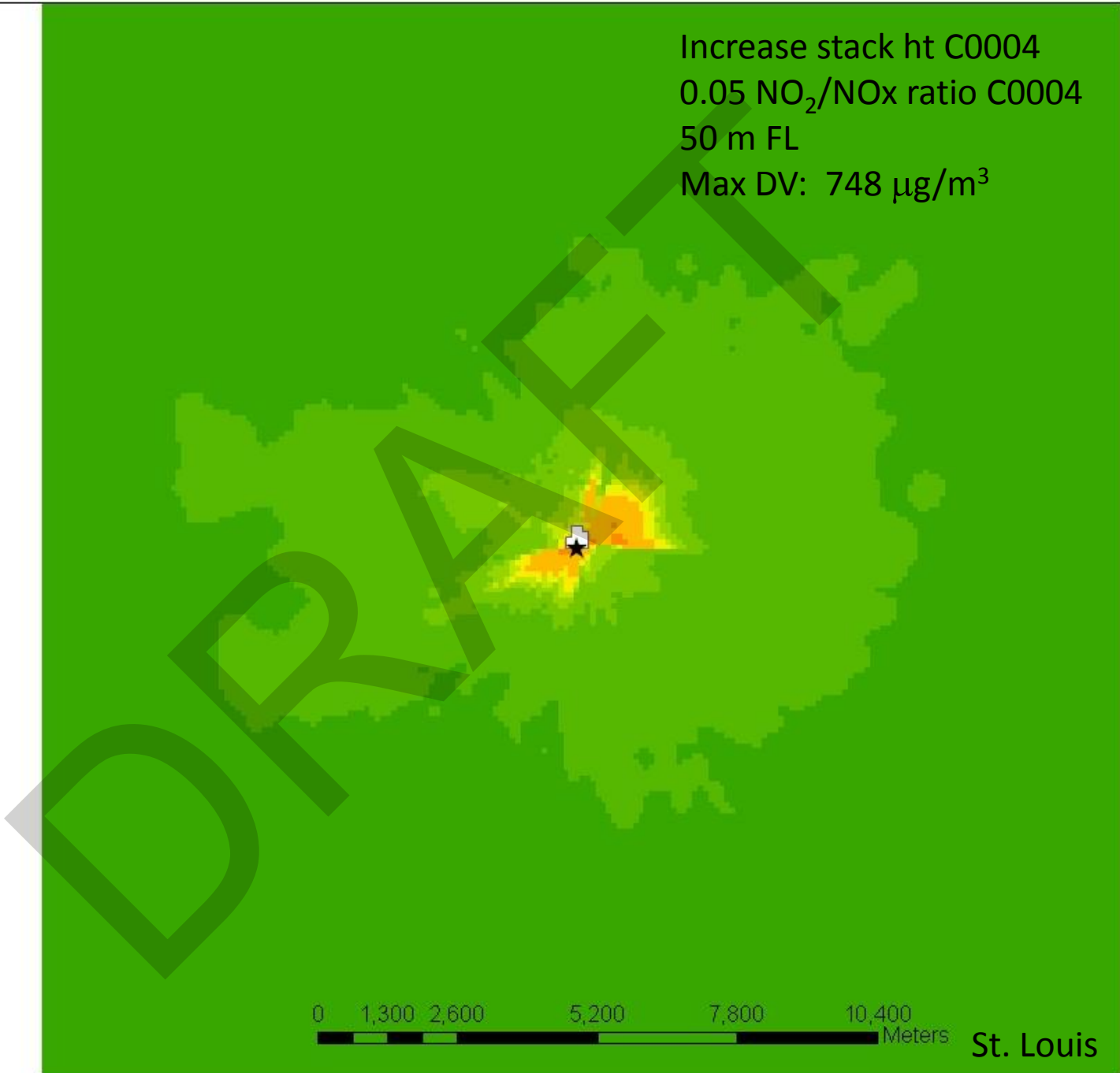
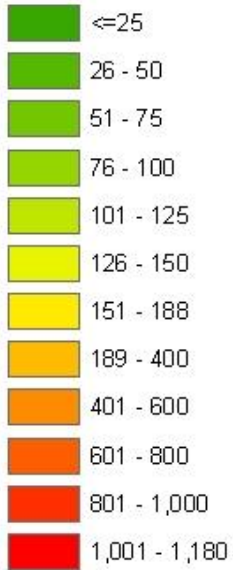
### Legend



St. Louis

Increase stack ht C0004  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 748 μg/m<sup>3</sup>

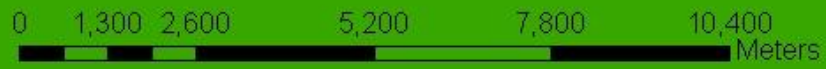
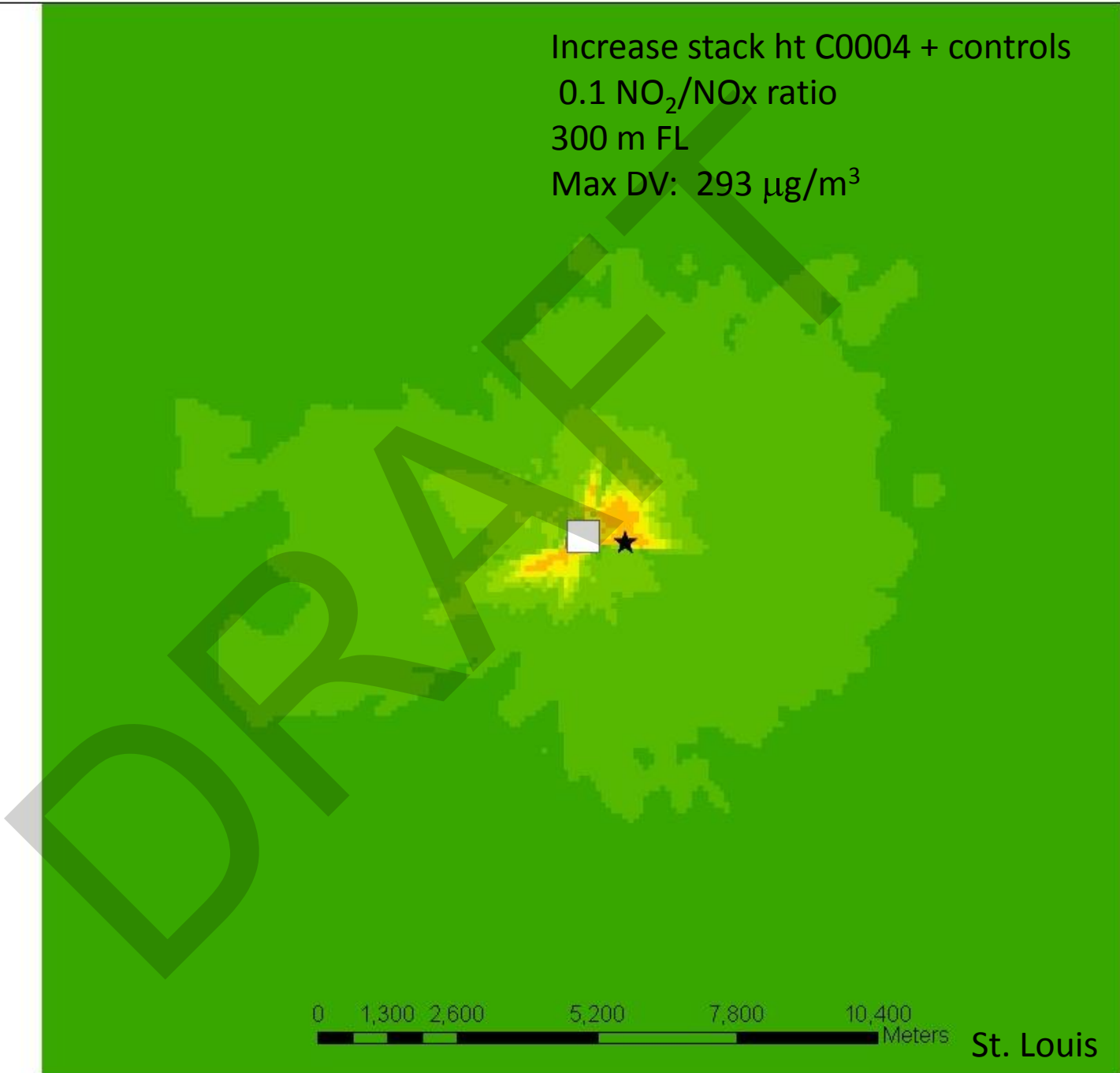
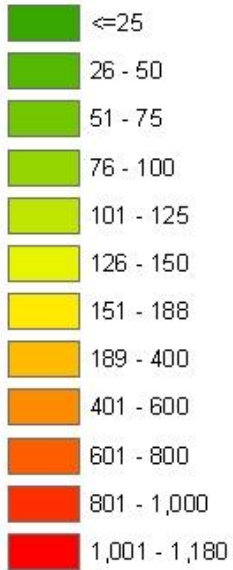
### Legend



St. Louis

Increase stack ht C0004 + controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 293 μg/m<sup>3</sup>

**Legend**

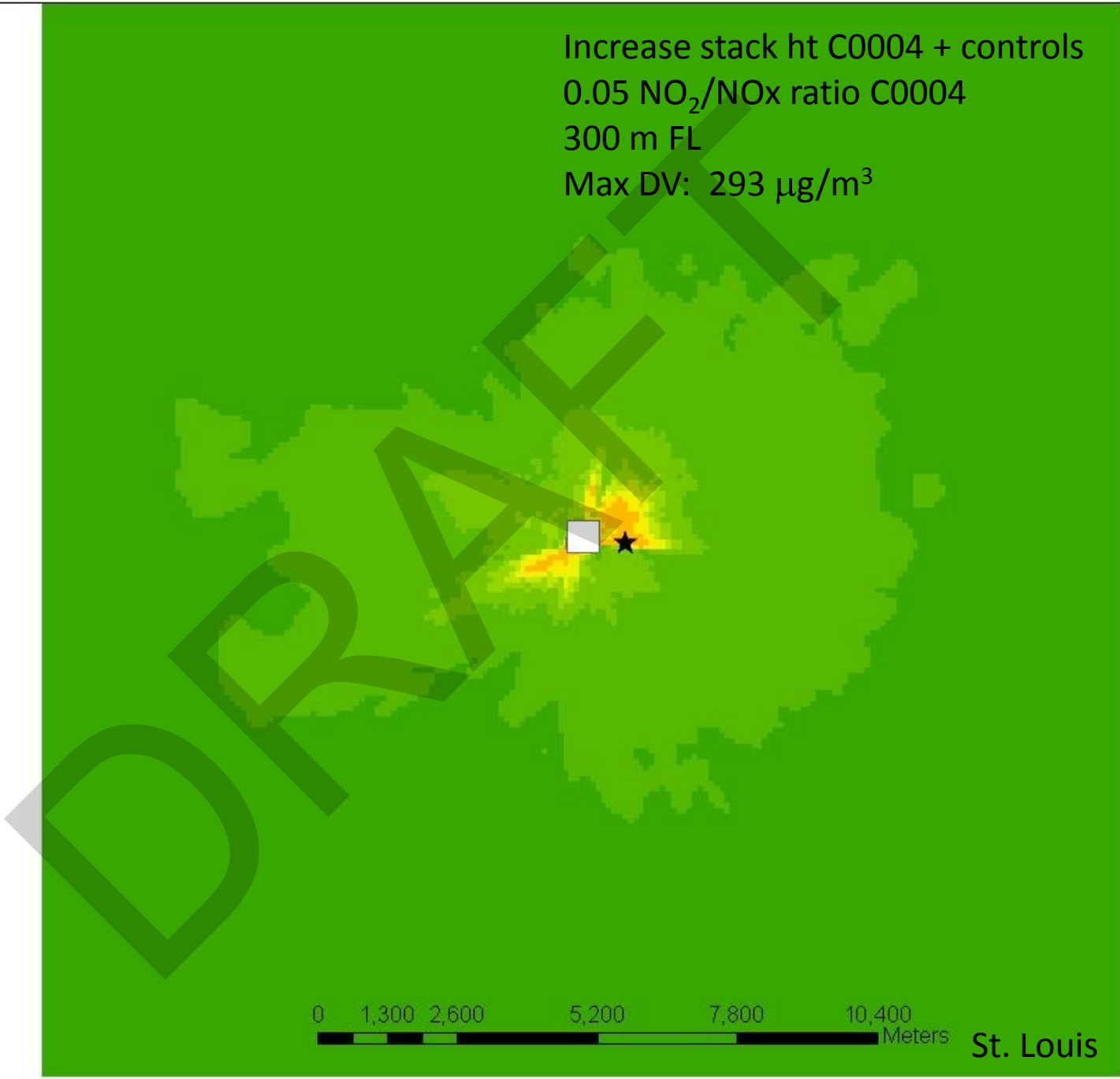
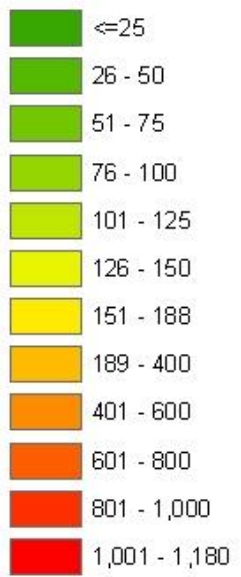


St. Louis



Increase stack ht C0004 + controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 293 μg/m<sup>3</sup>

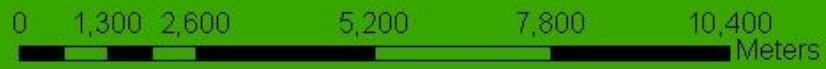
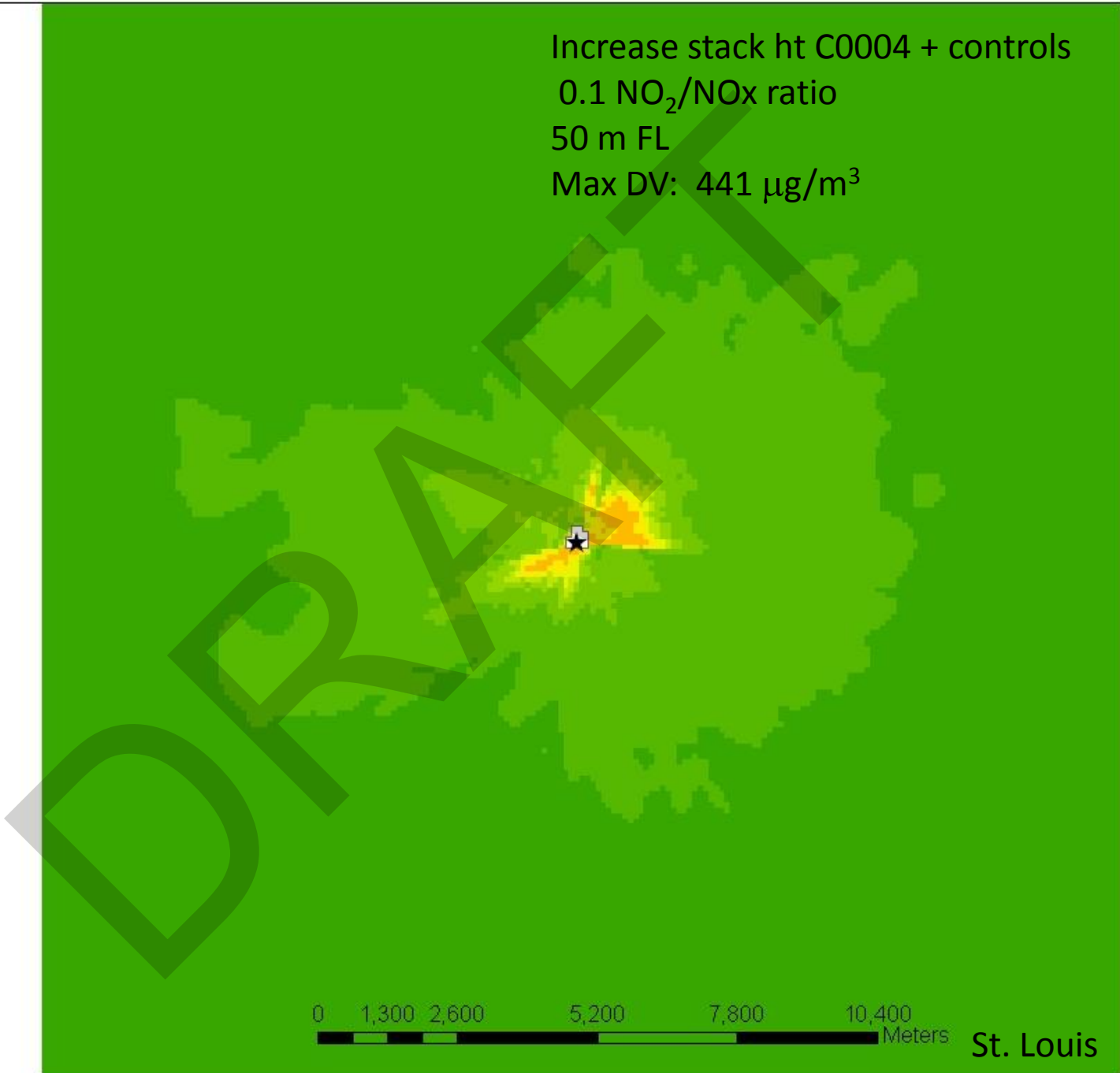
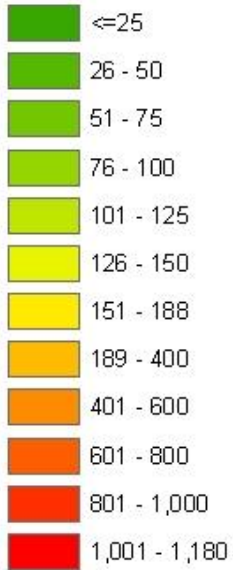
**Legend**



St. Louis

Increase stack ht C0004 + controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 441 μg/m<sup>3</sup>

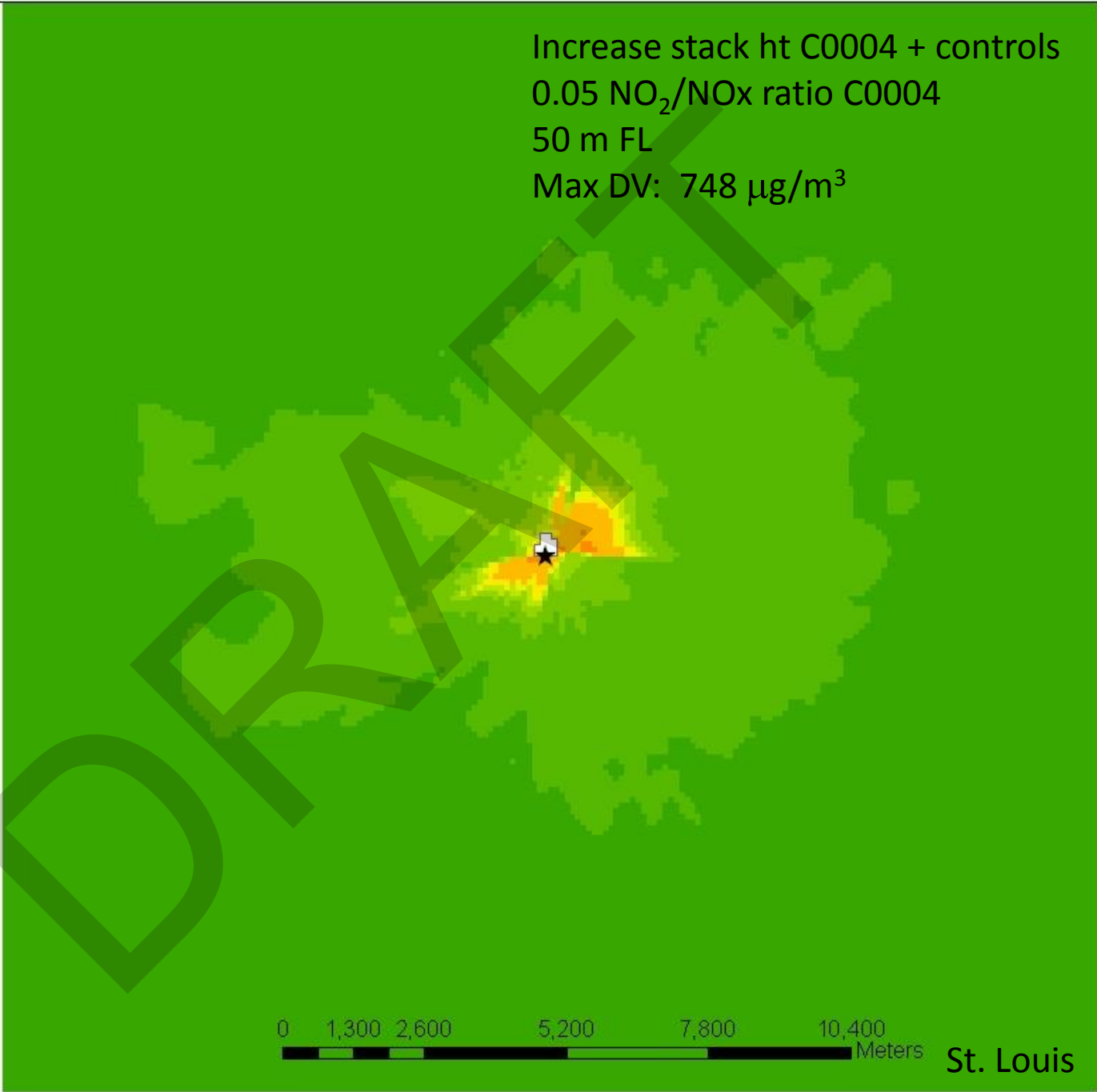
**Legend**



St. Louis

Increase stack ht C0004 + controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 748 μg/m<sup>3</sup>

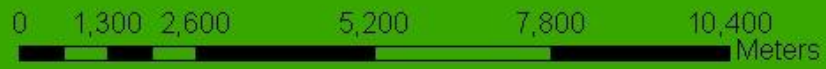
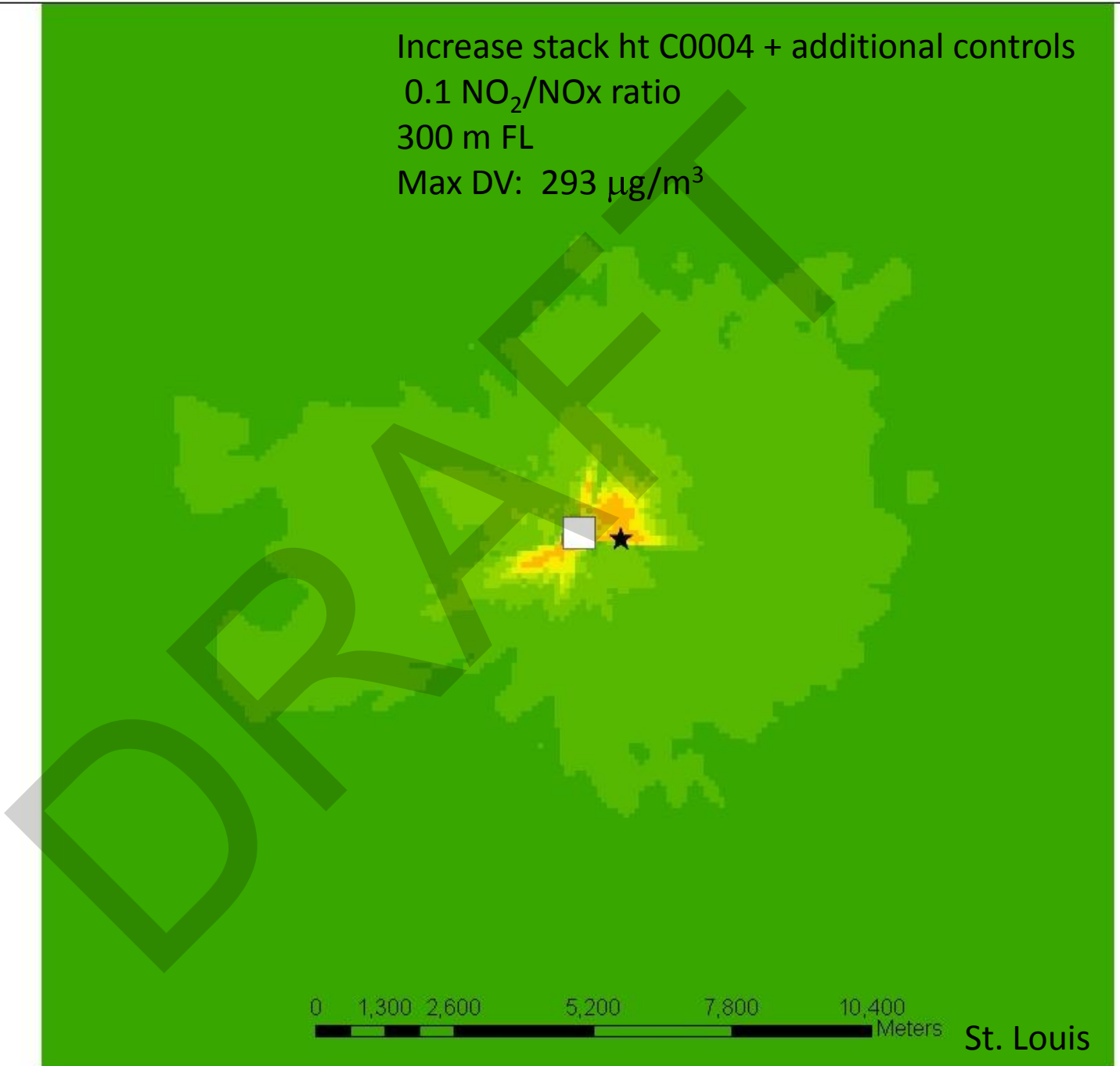
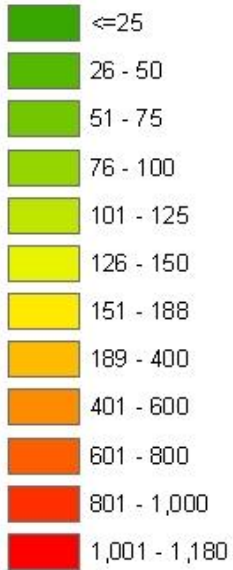
**Legend**



St. Louis

Increase stack ht C0004 + additional controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 293 μg/m<sup>3</sup>

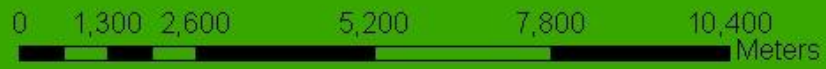
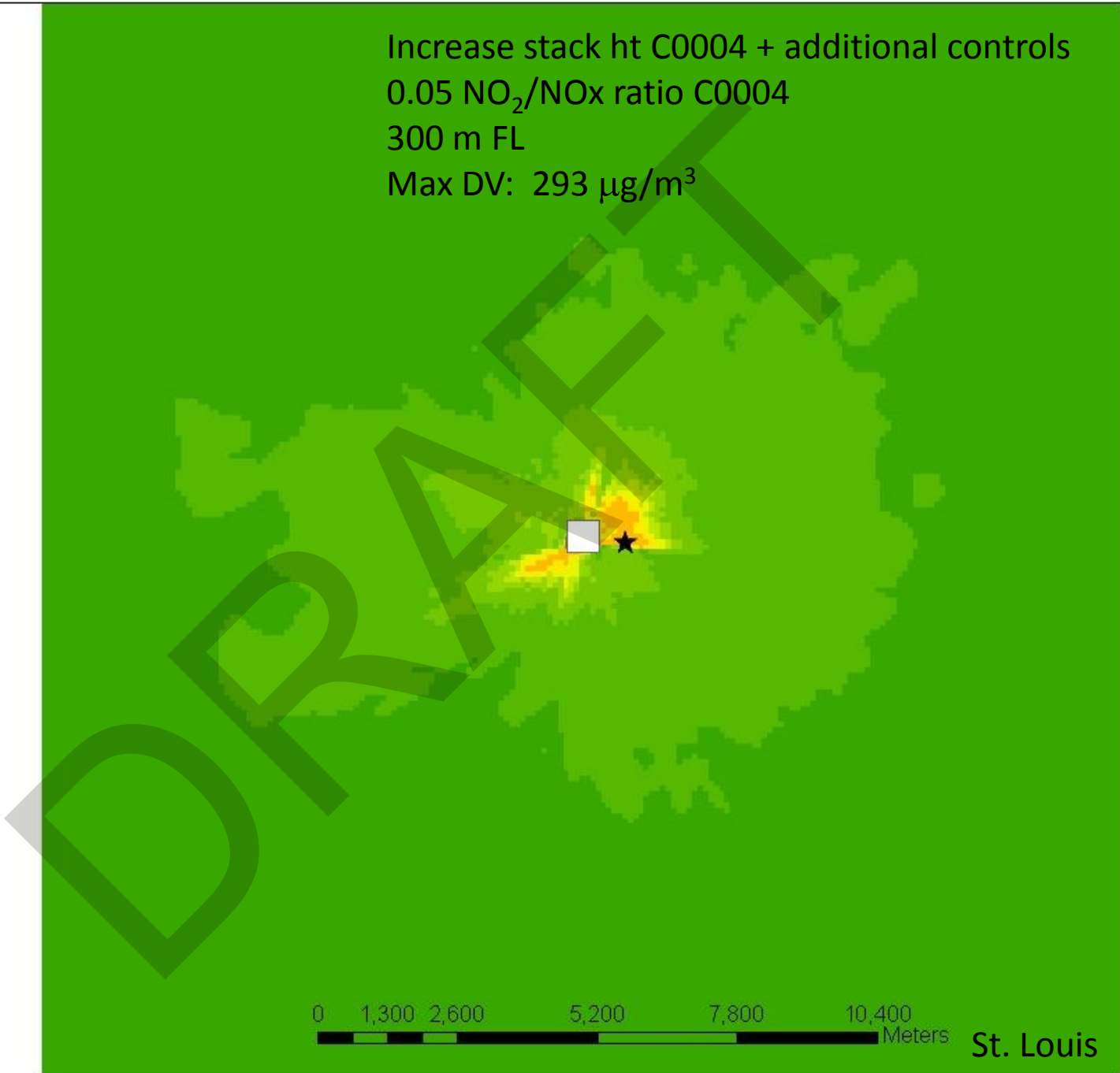
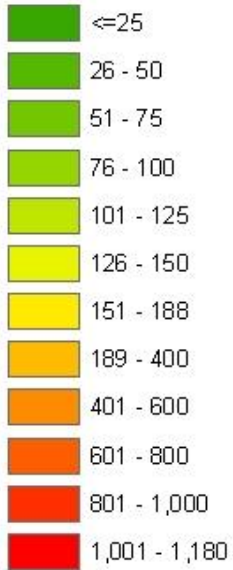
**Legend**



St. Louis

Increase stack ht C0004 + additional controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 293 μg/m<sup>3</sup>

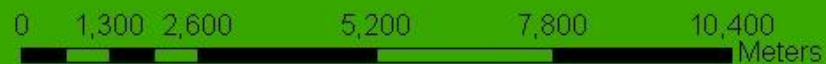
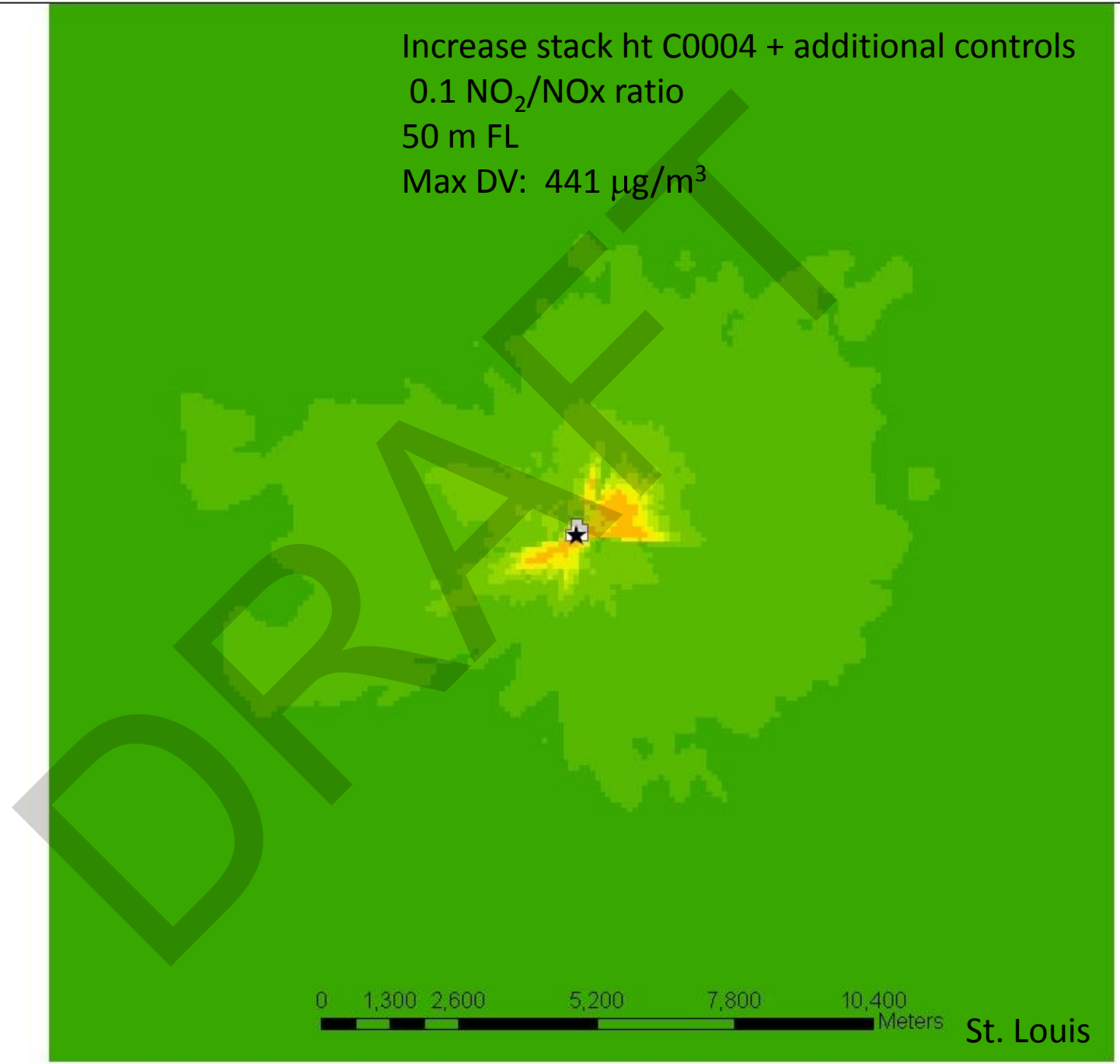
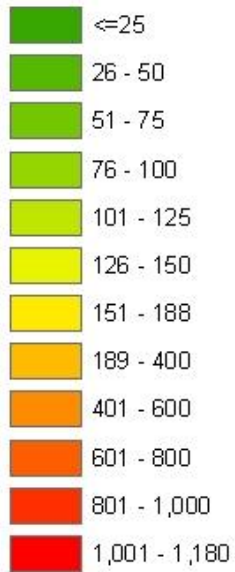
**Legend**



St. Louis

Increase stack ht C0004 + additional controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 441 μg/m<sup>3</sup>

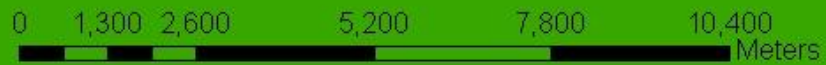
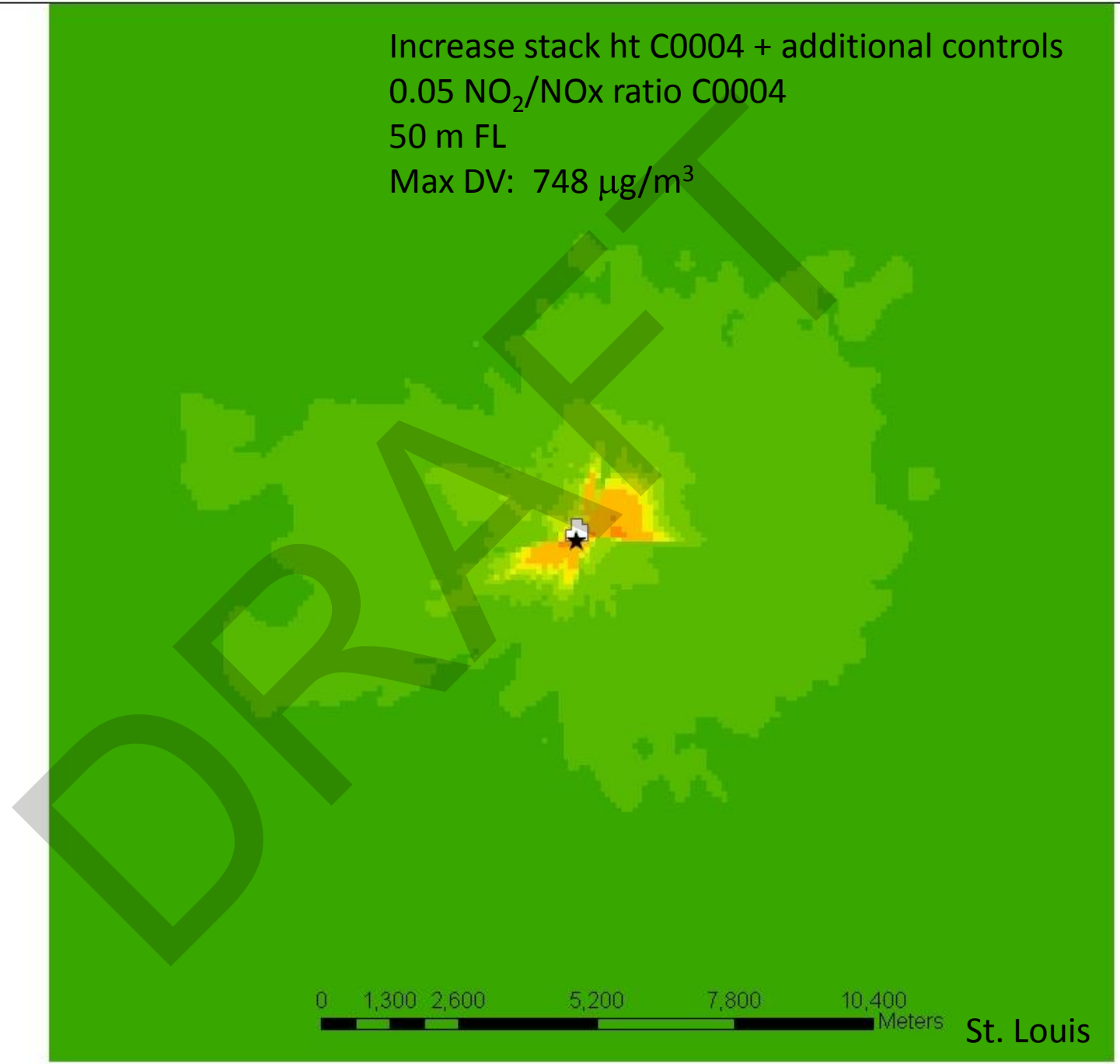
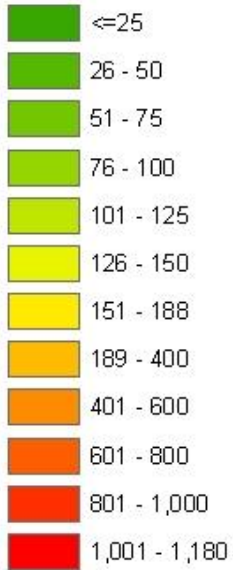
**Legend**



St. Louis

Increase stack ht C0004 + additional controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 748 μg/m<sup>3</sup>

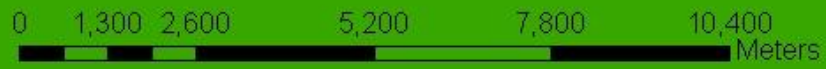
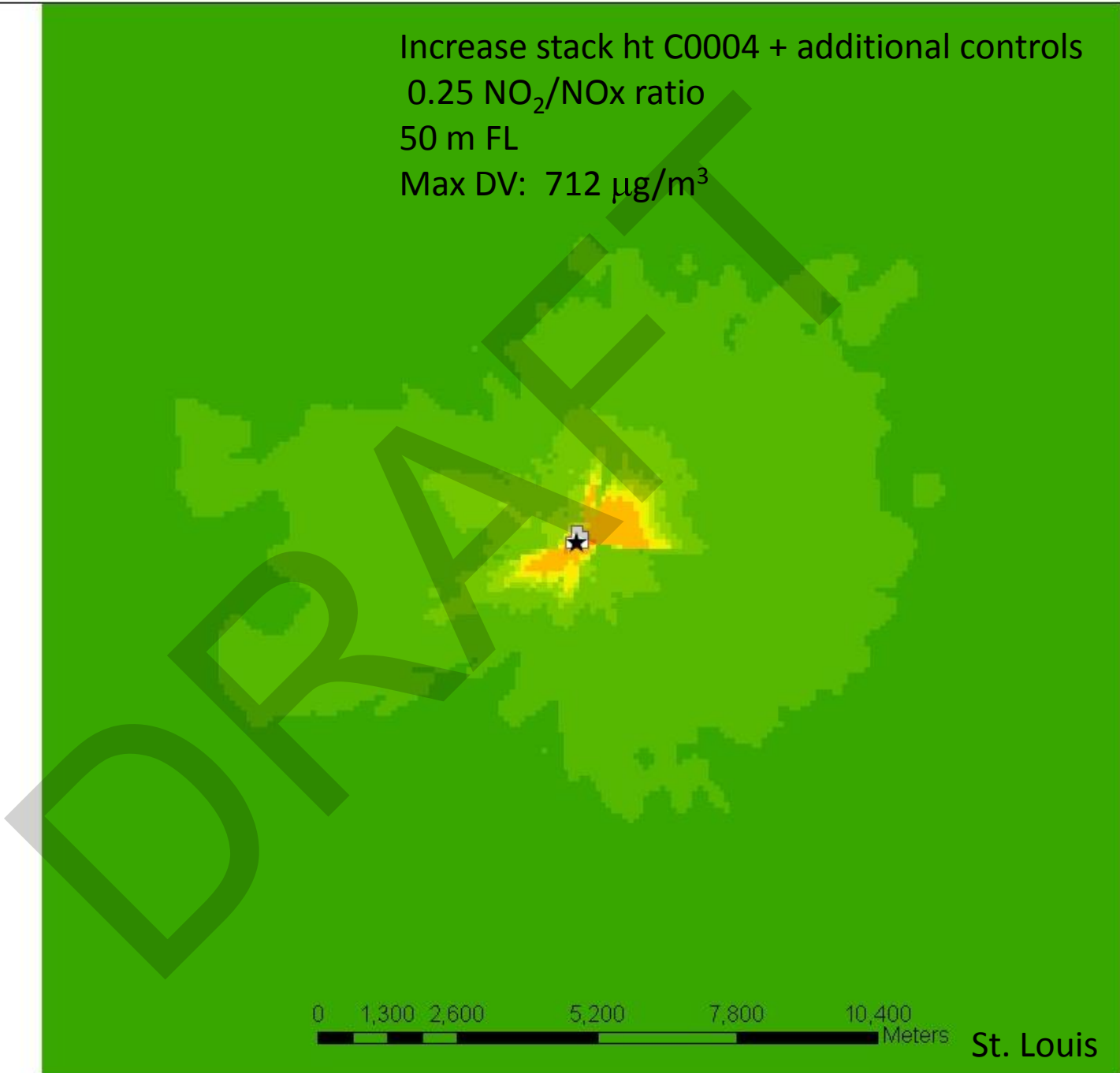
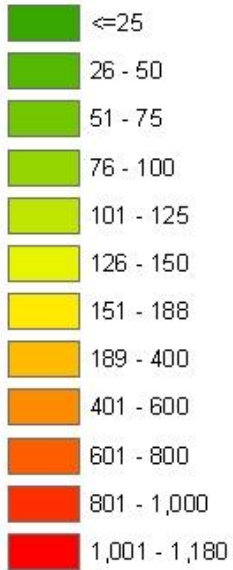
**Legend**



St. Louis

Increase stack ht C0004 + additional controls  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 712 μg/m<sup>3</sup>

**Legend**

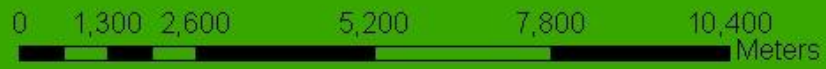
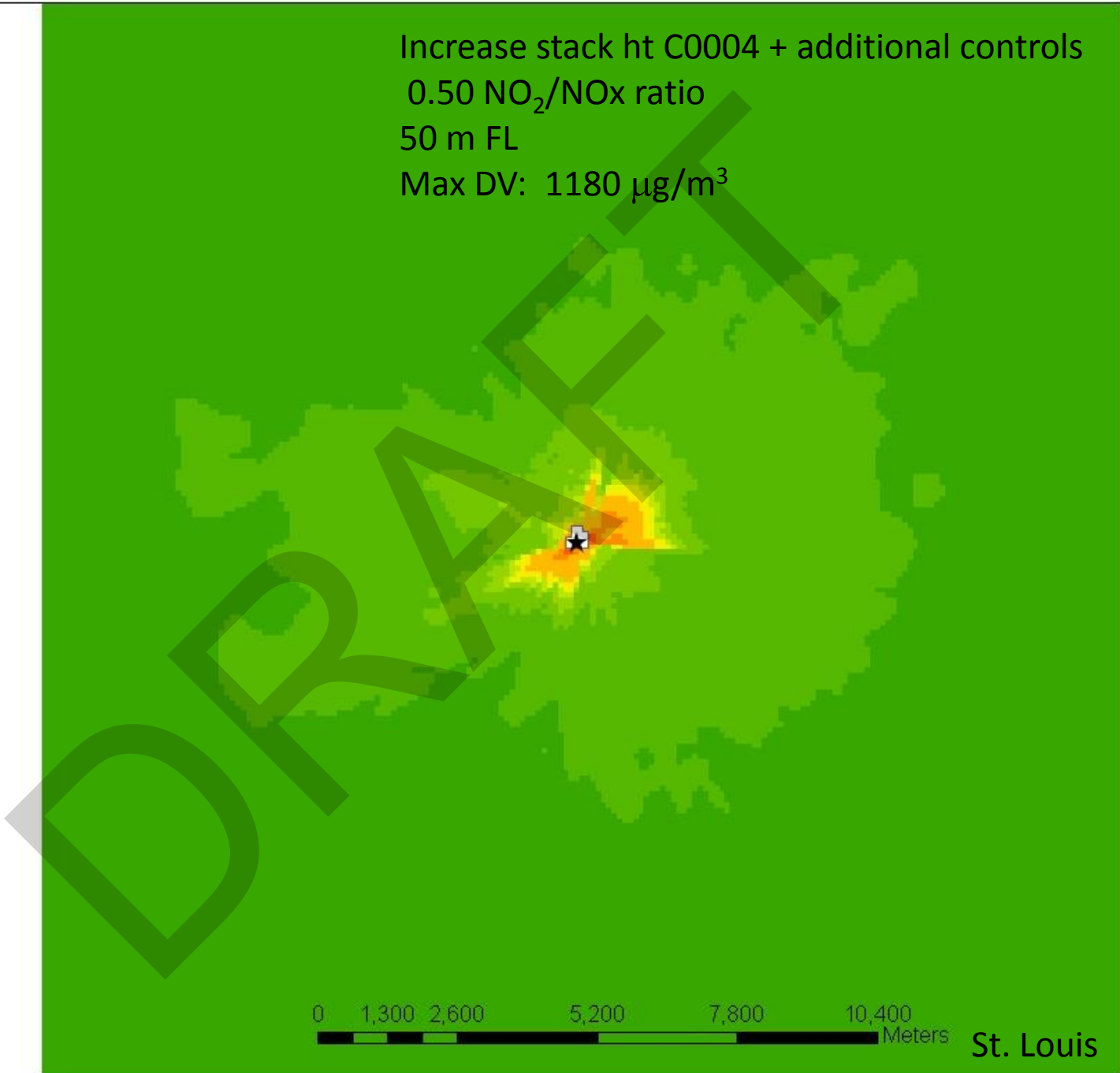
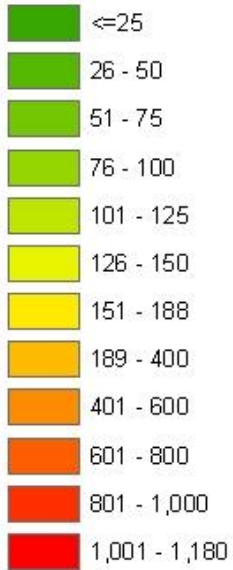


St. Louis



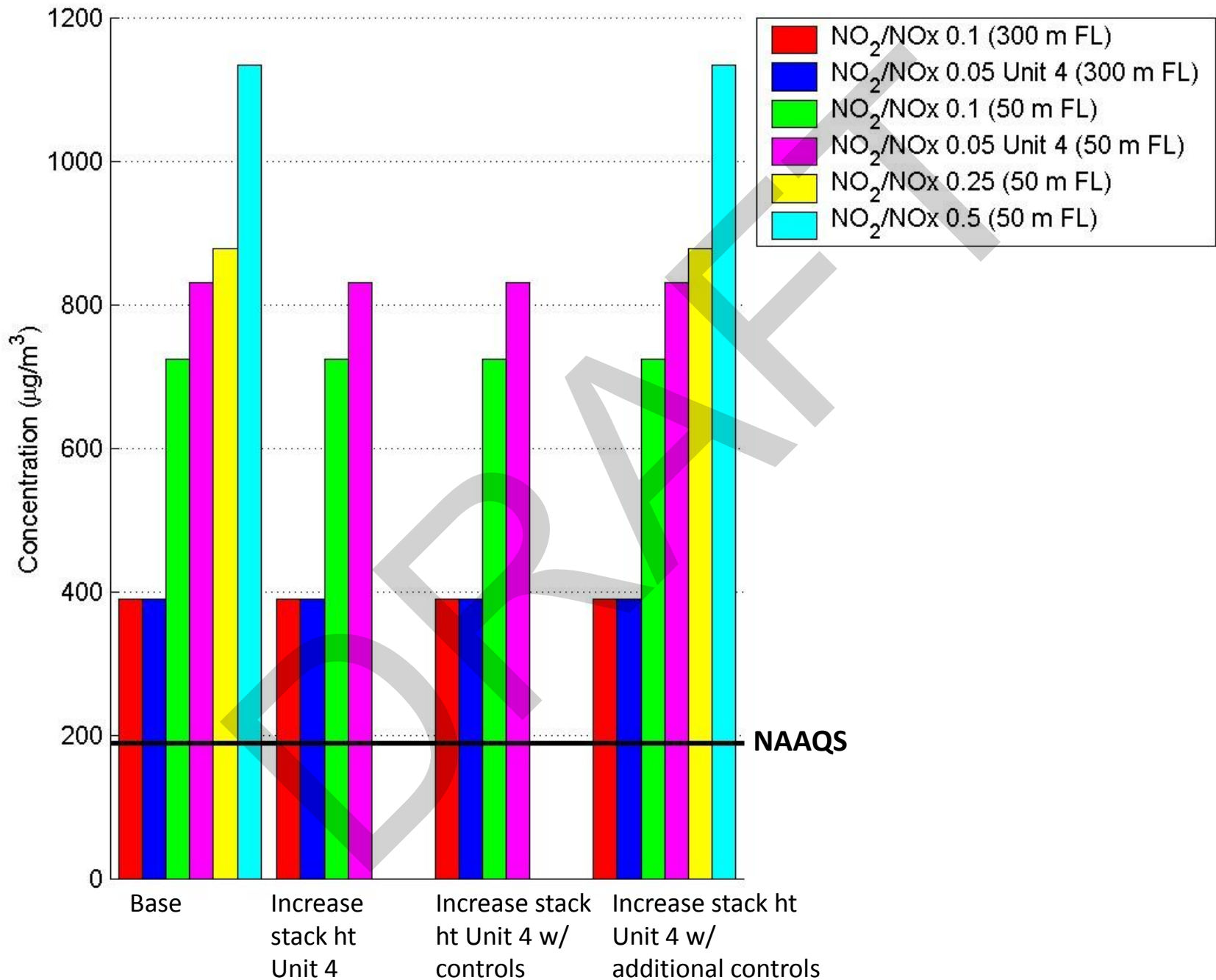
Increase stack ht C0004 + additional controls  
0.50 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1180 μg/m<sup>3</sup>

**Legend**















St. Louis

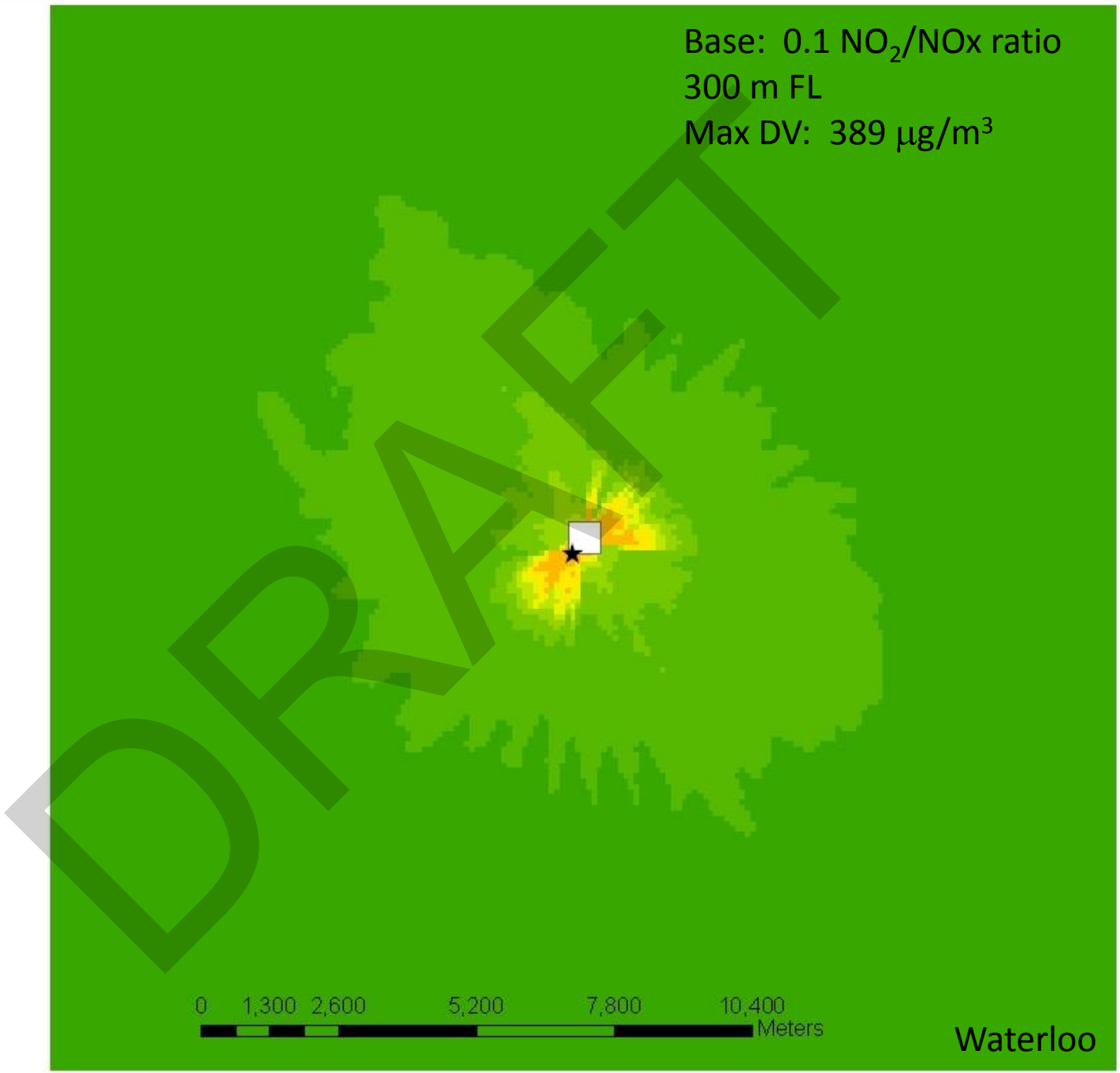
# Ethanol Plant (Waterloo): NO<sub>2</sub>



Base: 0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 389 μg/m<sup>3</sup>

**Legend**

-  <=25
-  26 - 50
-  51 - 75
-  76 - 100
-  101 - 125
-  126 - 150
-  151 - 196
-  197 - 400
-  401 - 600
-  601 - 800
-  801 - 1,000
-  1,001 - 1,134

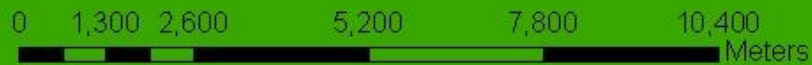
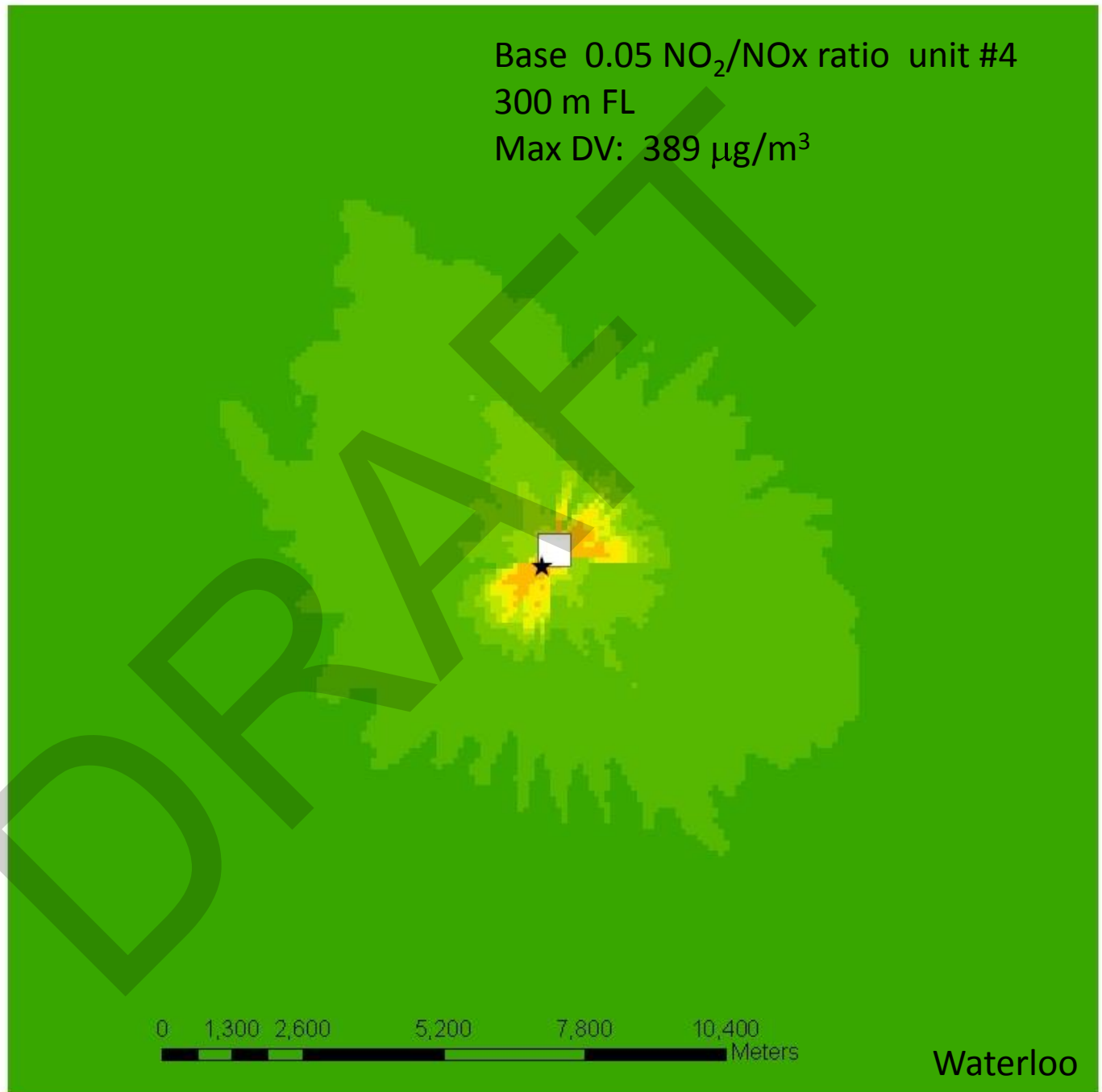
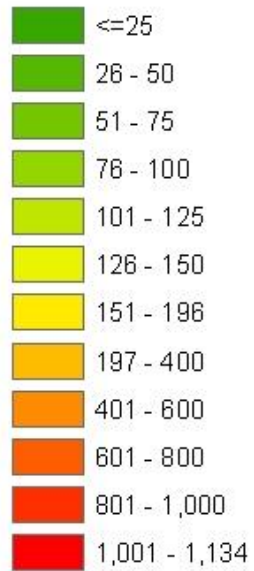


0 1,300 2,600 5,200 7,800 10,400 Meters

Waterloo

Base 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio unit #4  
300 m FL  
Max DV: 389 µg/m<sup>3</sup>

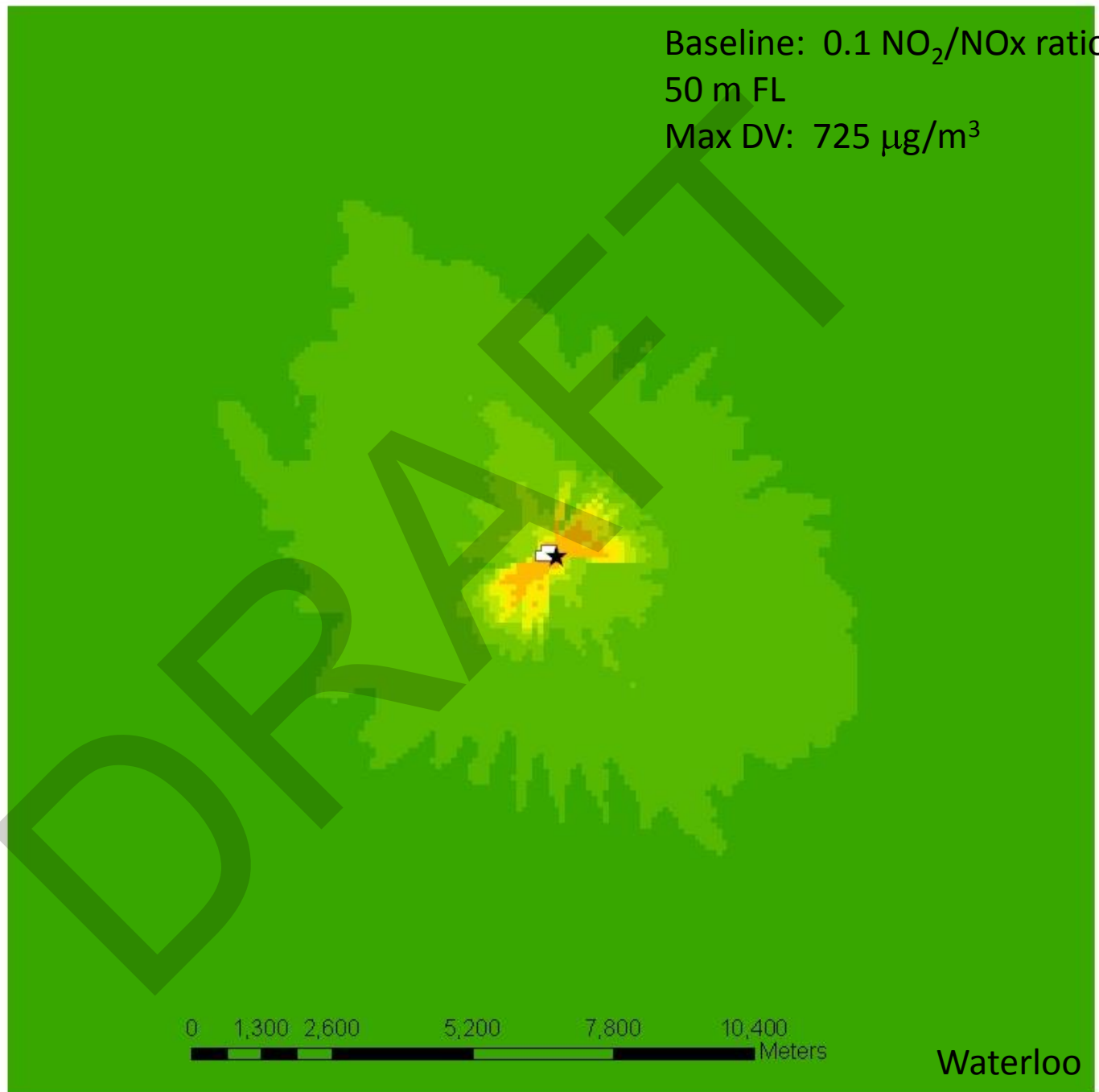
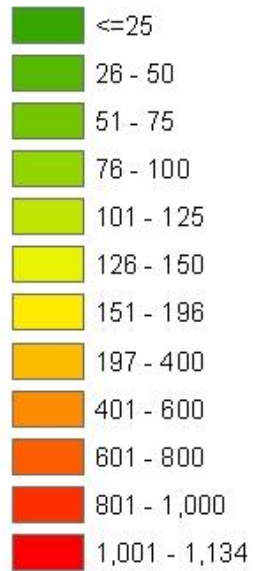
**Legend**



Waterloo

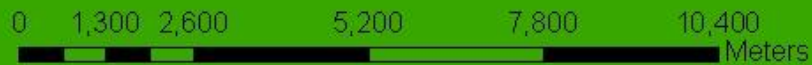
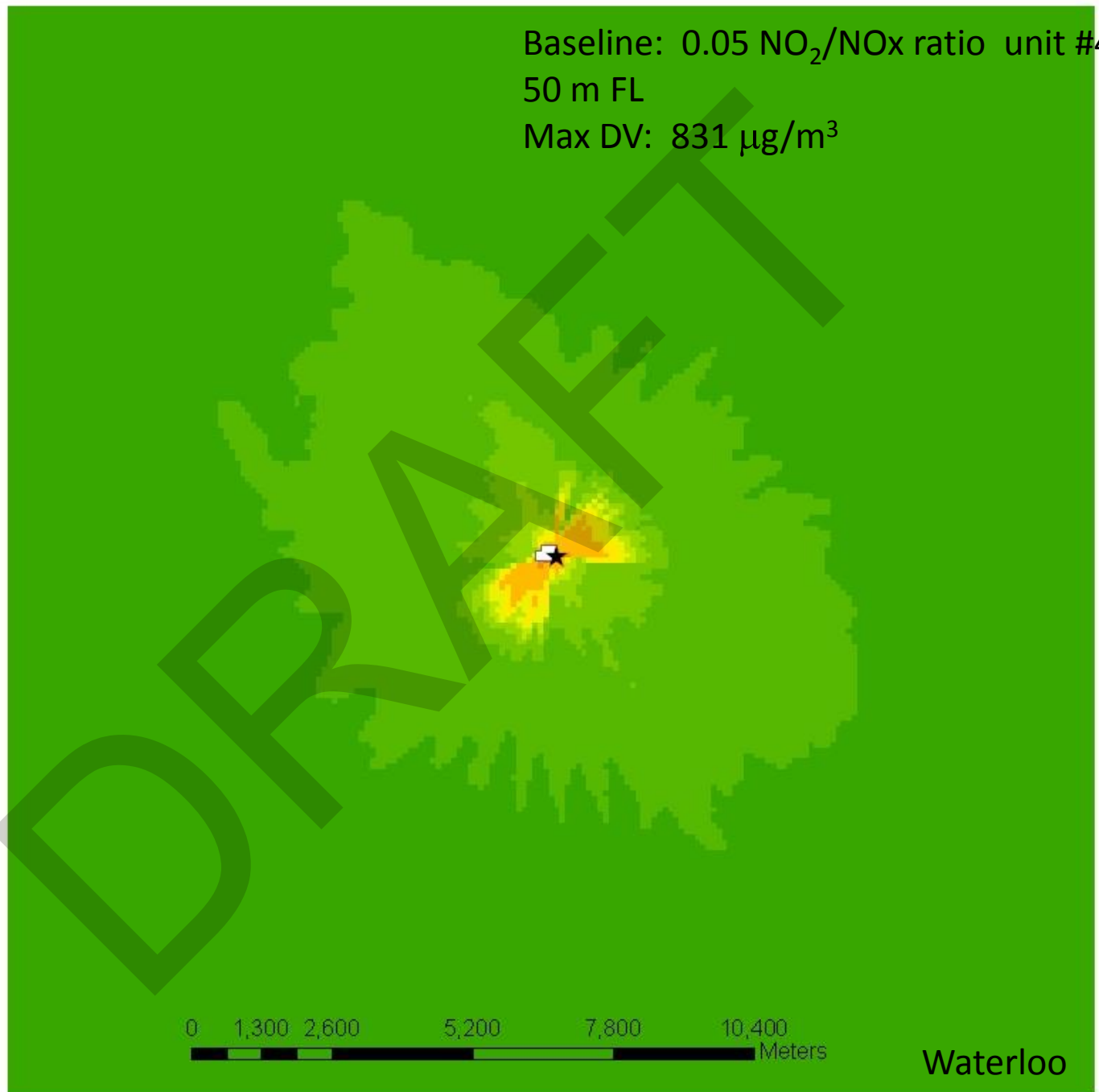
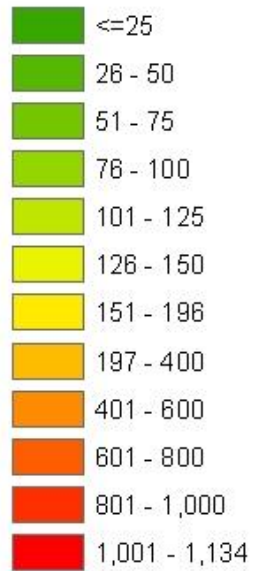
Baseline: 0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 725 μg/m<sup>3</sup>

### Legend



Baseline: 0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio unit #4  
50 m FL  
Max DV: 831 µg/m<sup>3</sup>

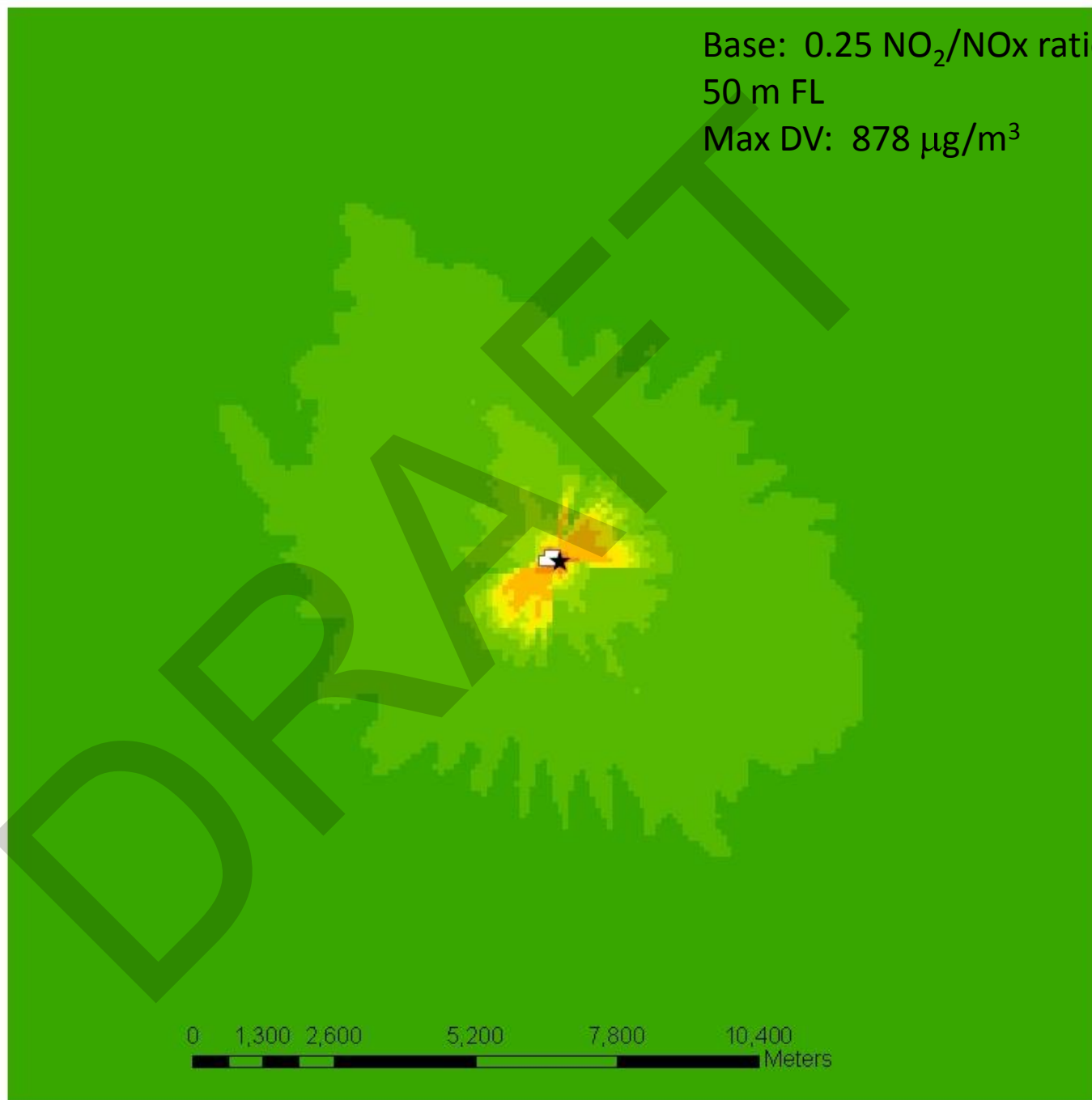
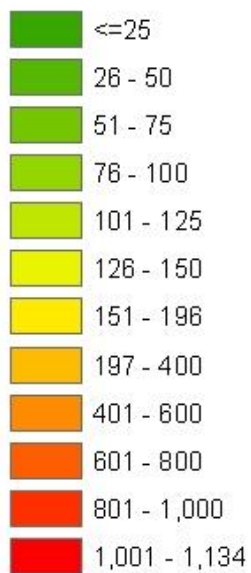
### Legend



Waterloo

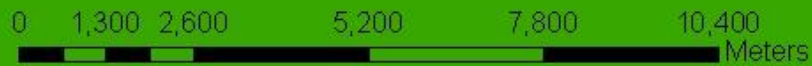
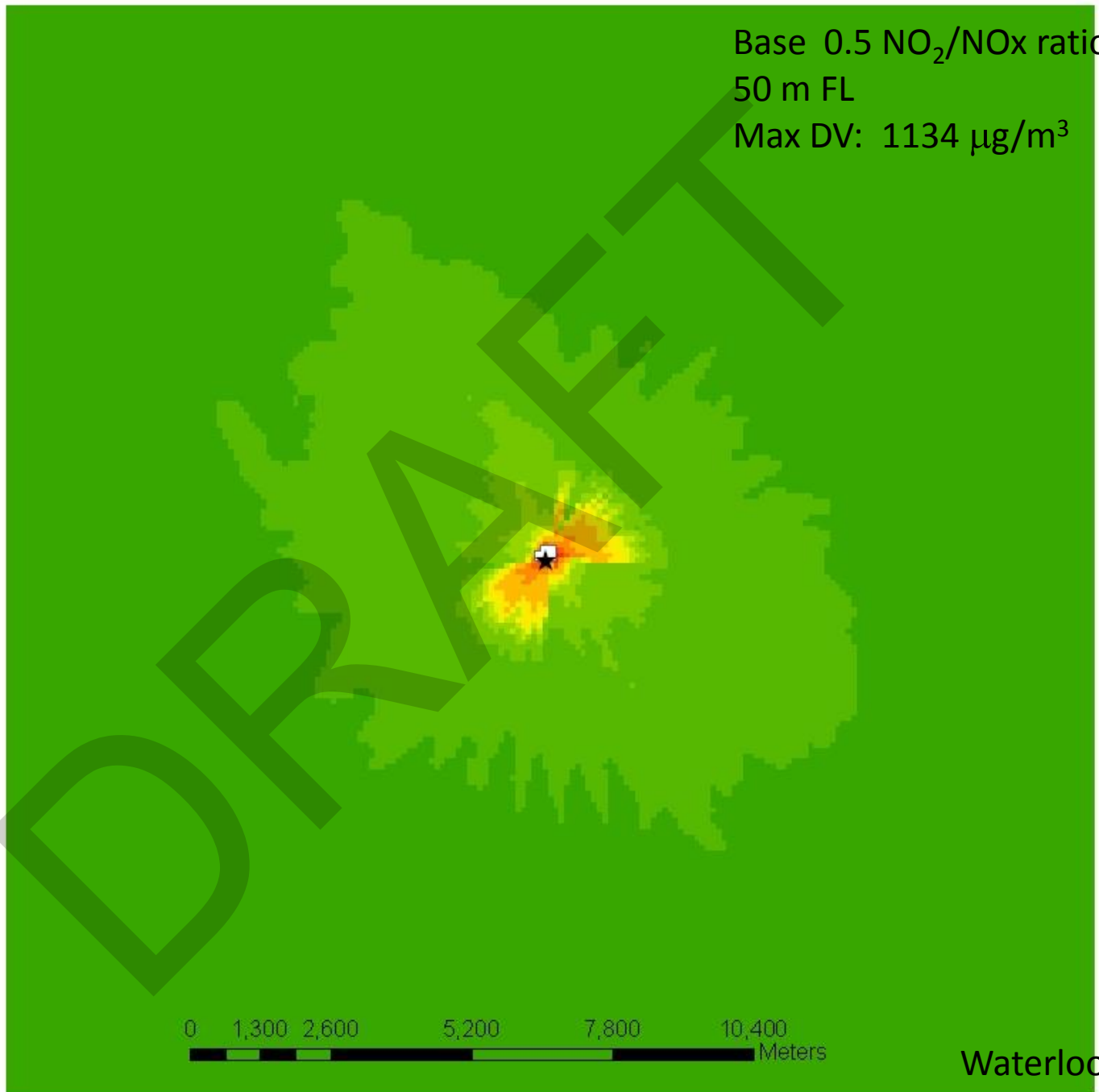
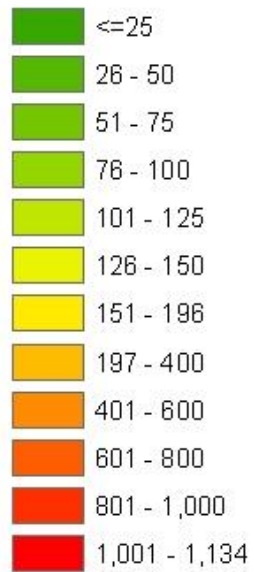
Base: 0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 878 μg/m<sup>3</sup>

### Legend



Base 0.5 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1134 µg/m<sup>3</sup>

### Legend

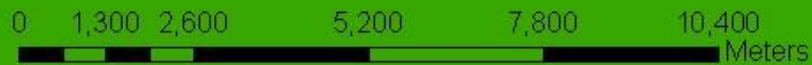
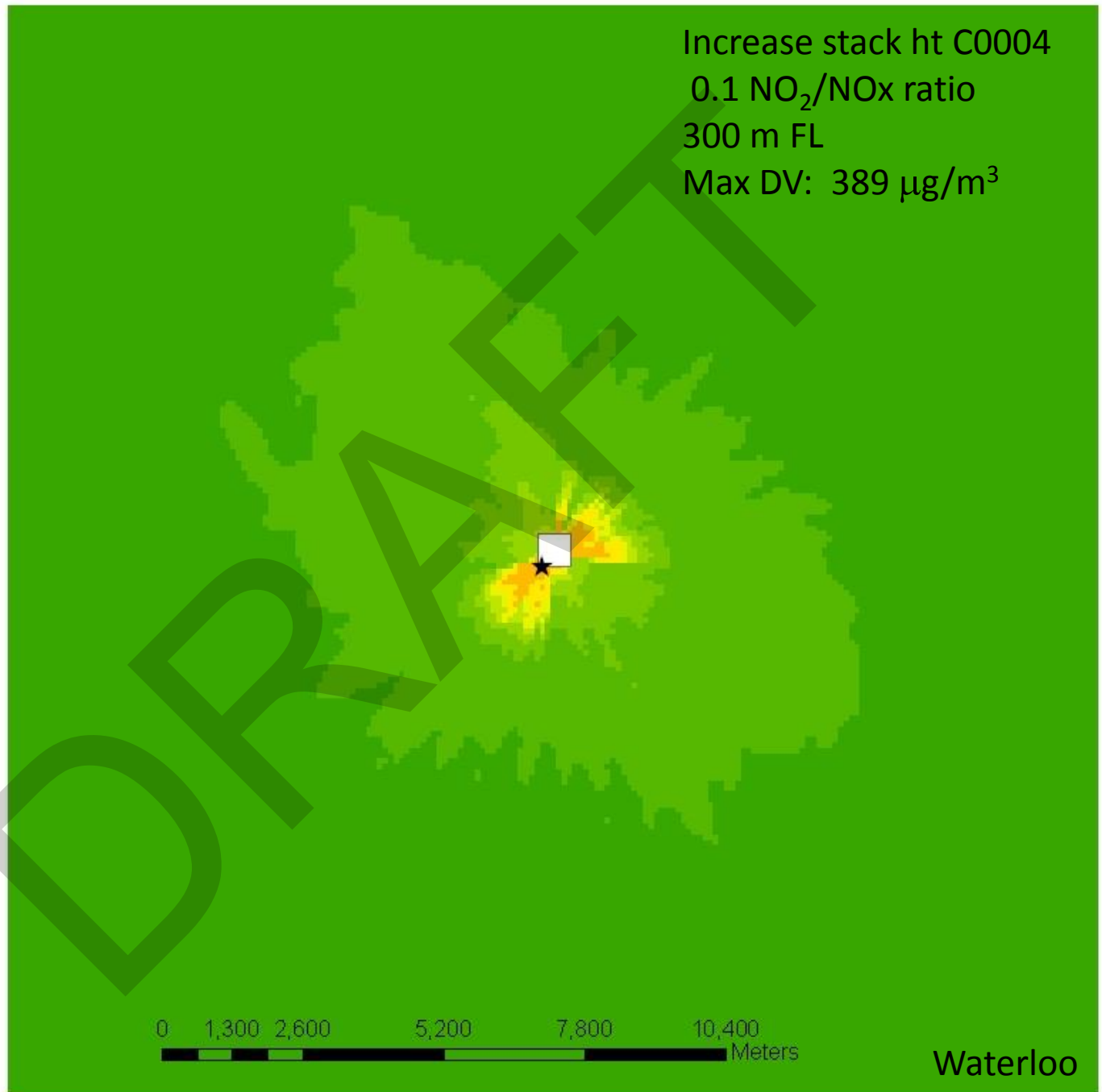
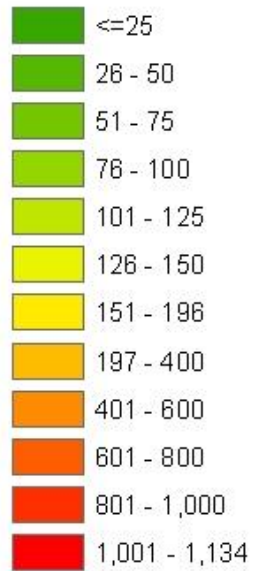


Waterloo



Increase stack ht C0004  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 389 μg/m<sup>3</sup>

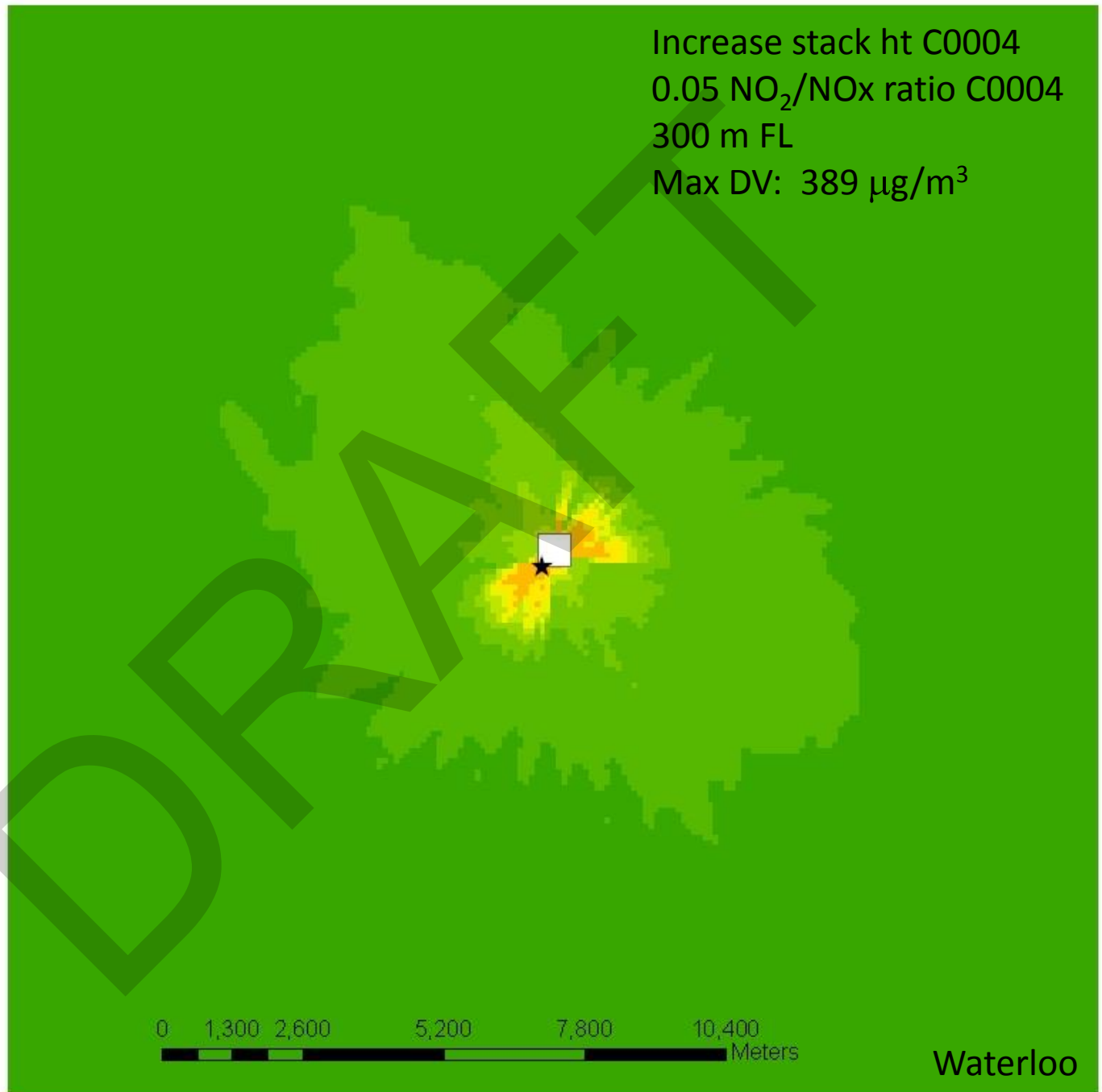
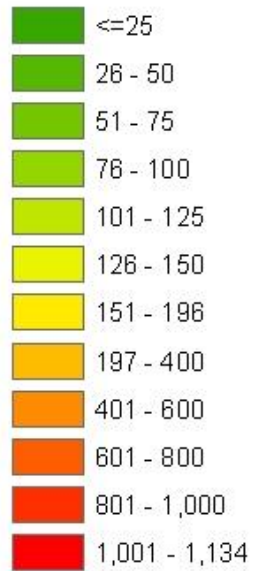
**Legend**



Waterloo

Increase stack ht C0004  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 389 μg/m<sup>3</sup>

**Legend**



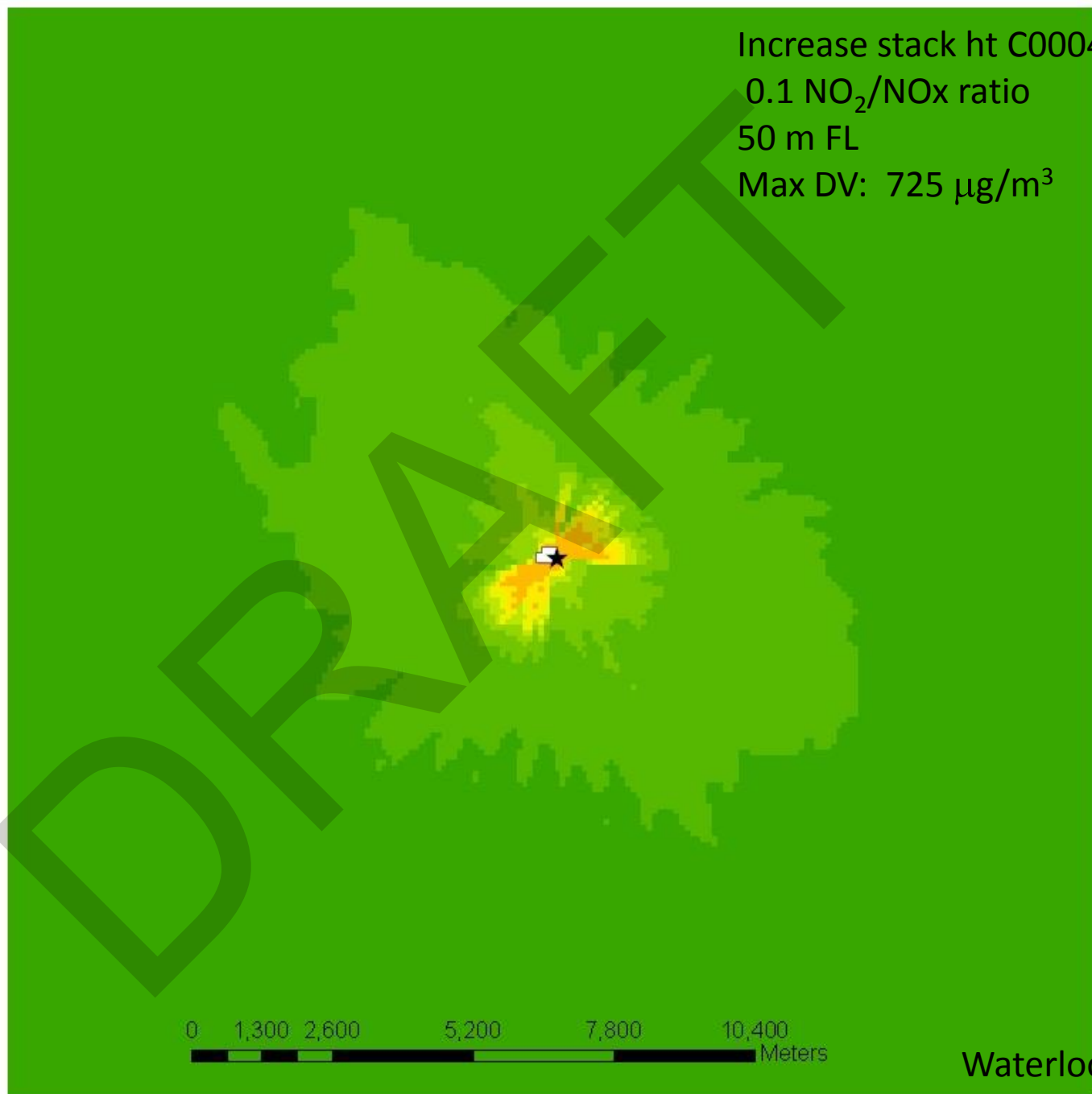
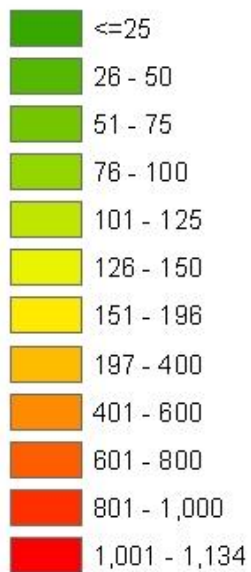
Increase stack ht C0004

0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio

50 m FL

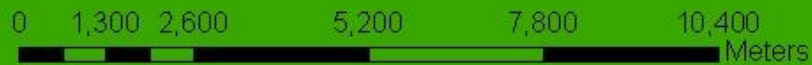
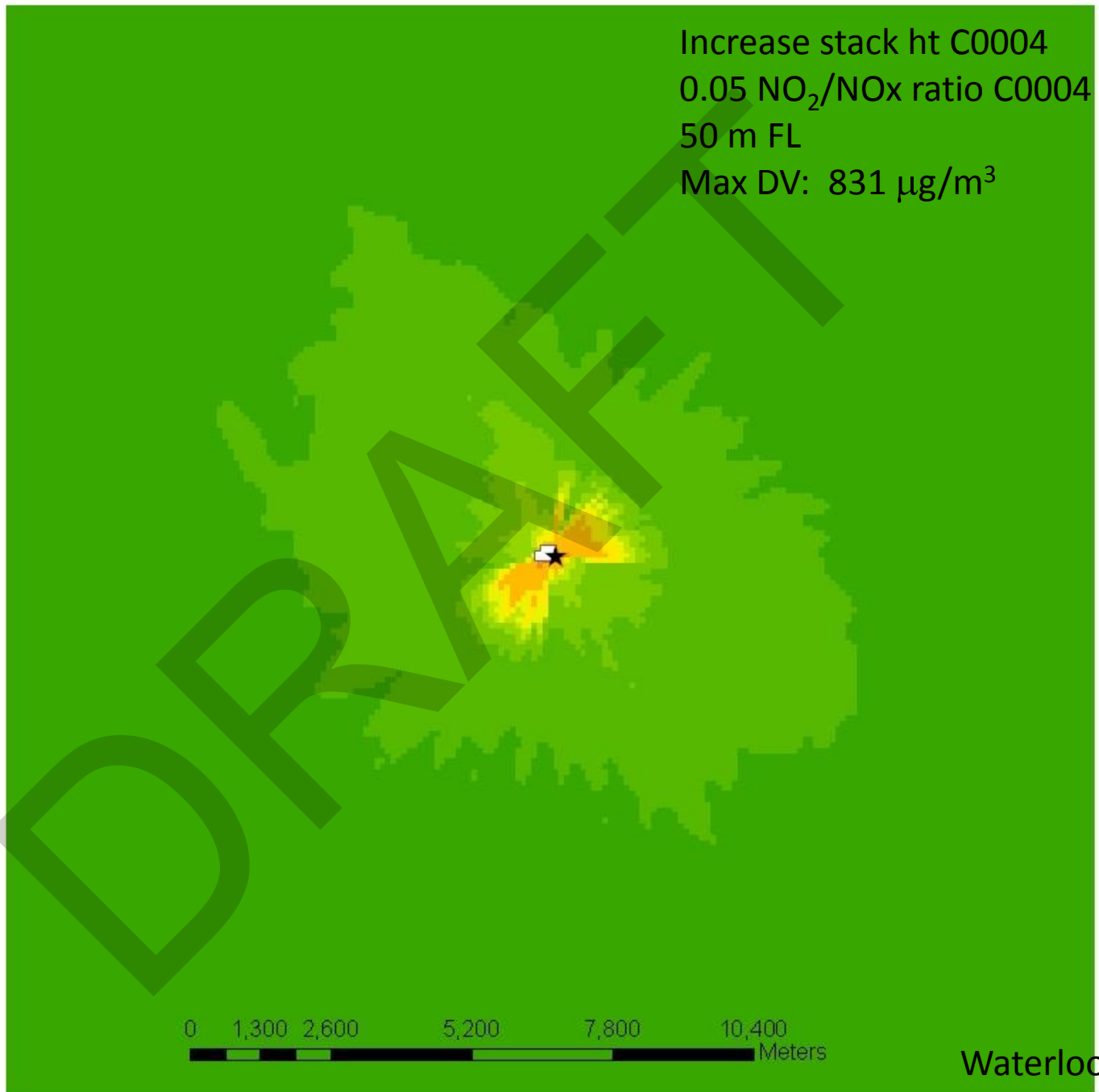
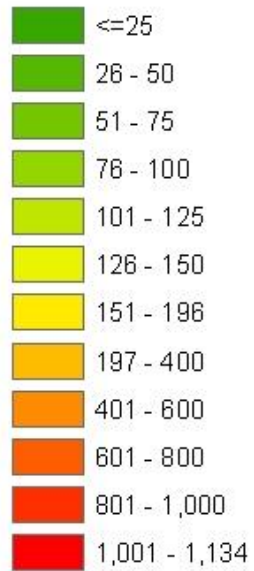
Max DV: 725 μg/m<sup>3</sup>

### Legend



Increase stack ht C0004  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 831 μg/m<sup>3</sup>

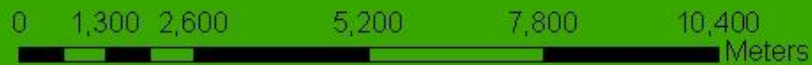
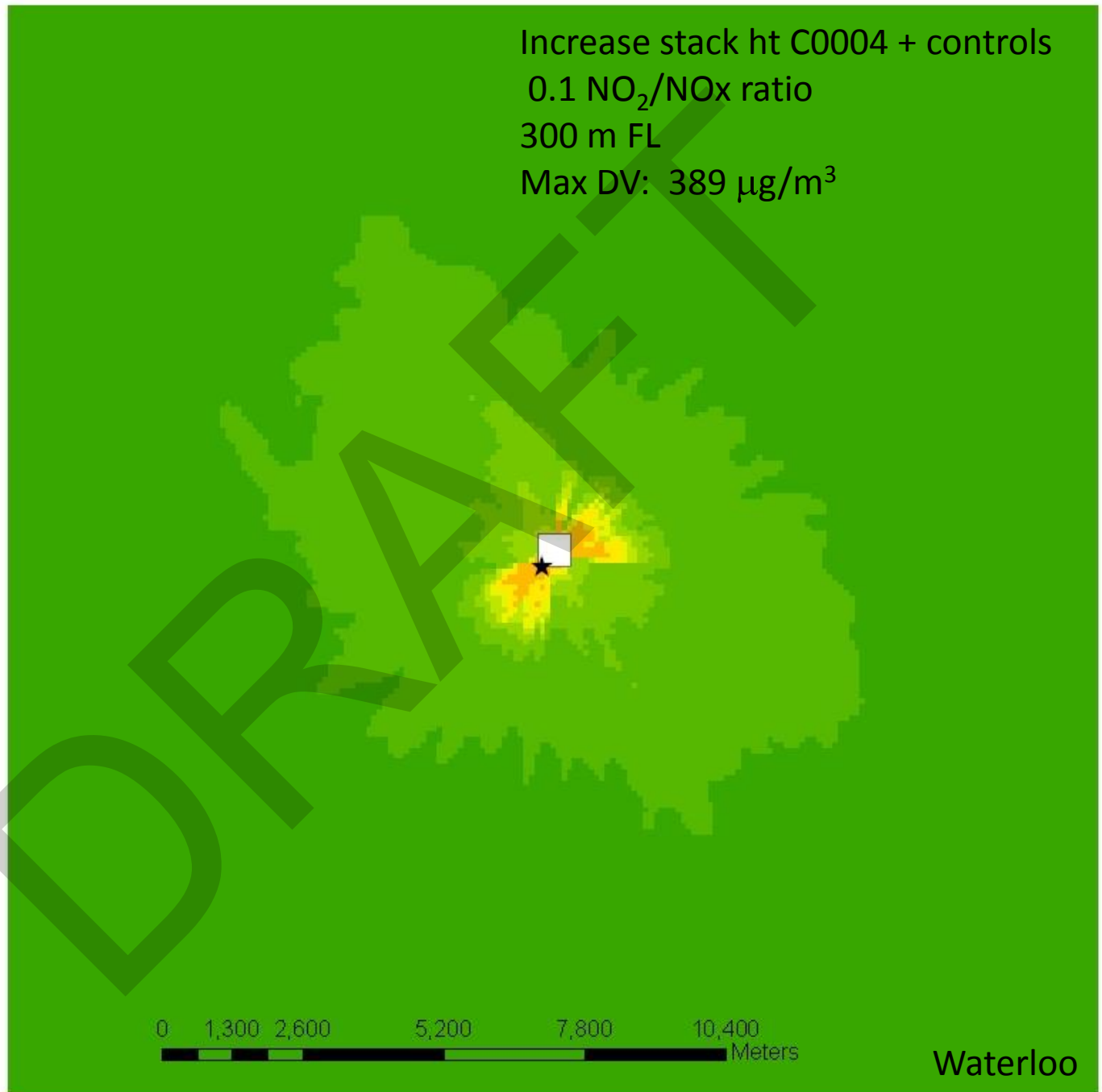
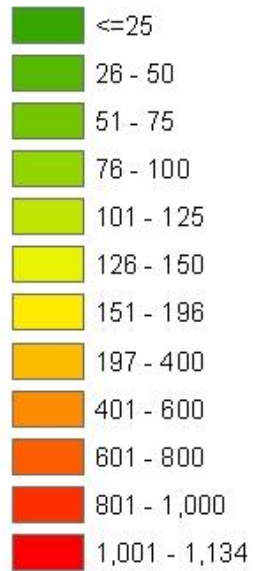
**Legend**



Waterloo

Increase stack ht C0004 + controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 389 μg/m<sup>3</sup>

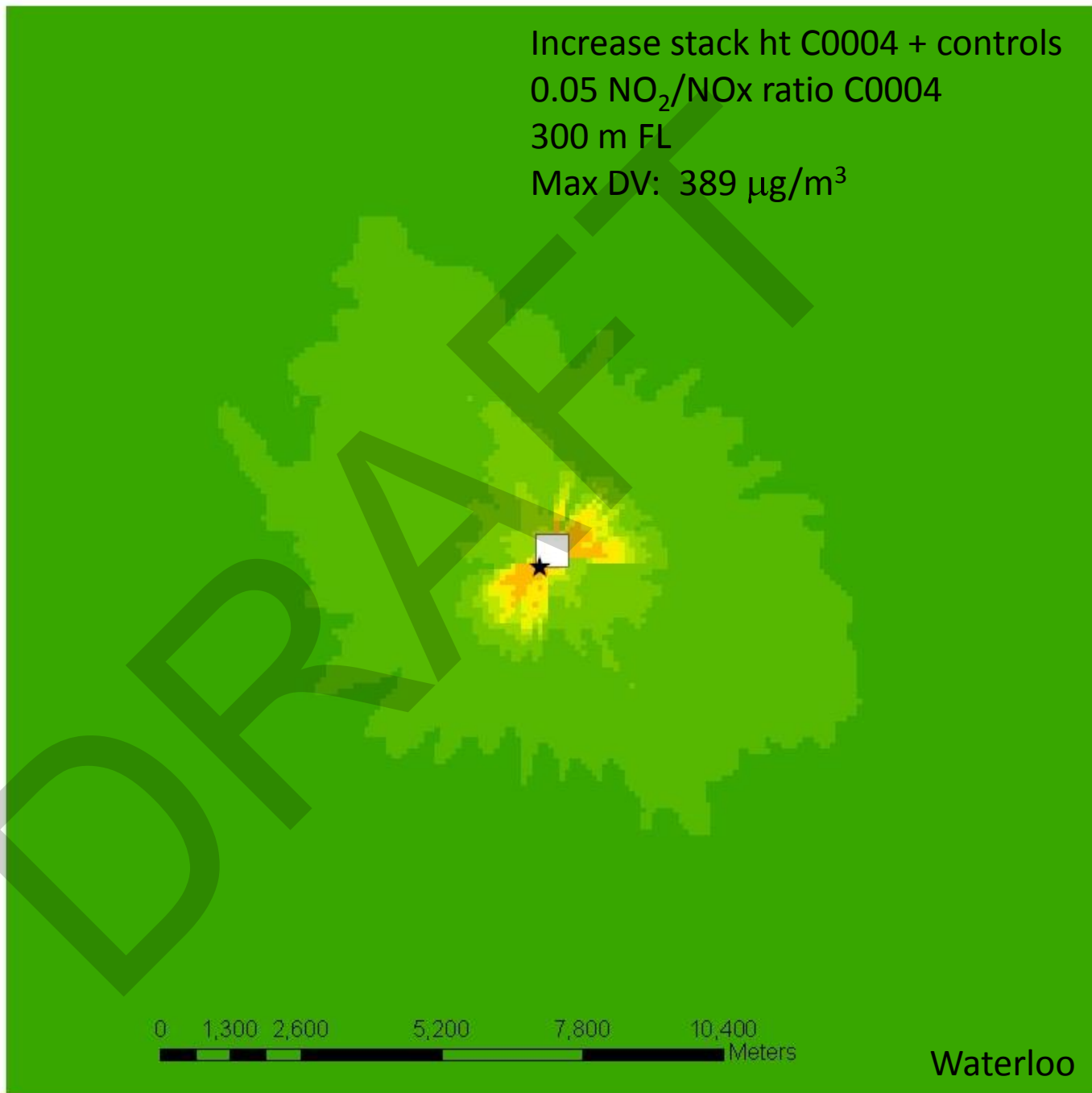
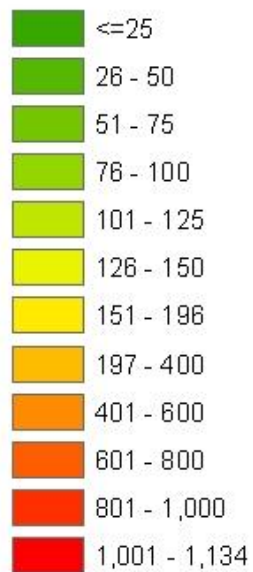
**Legend**



Waterloo

Increase stack ht C0004 + controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 389 μg/m<sup>3</sup>

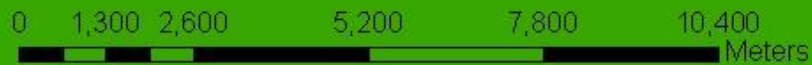
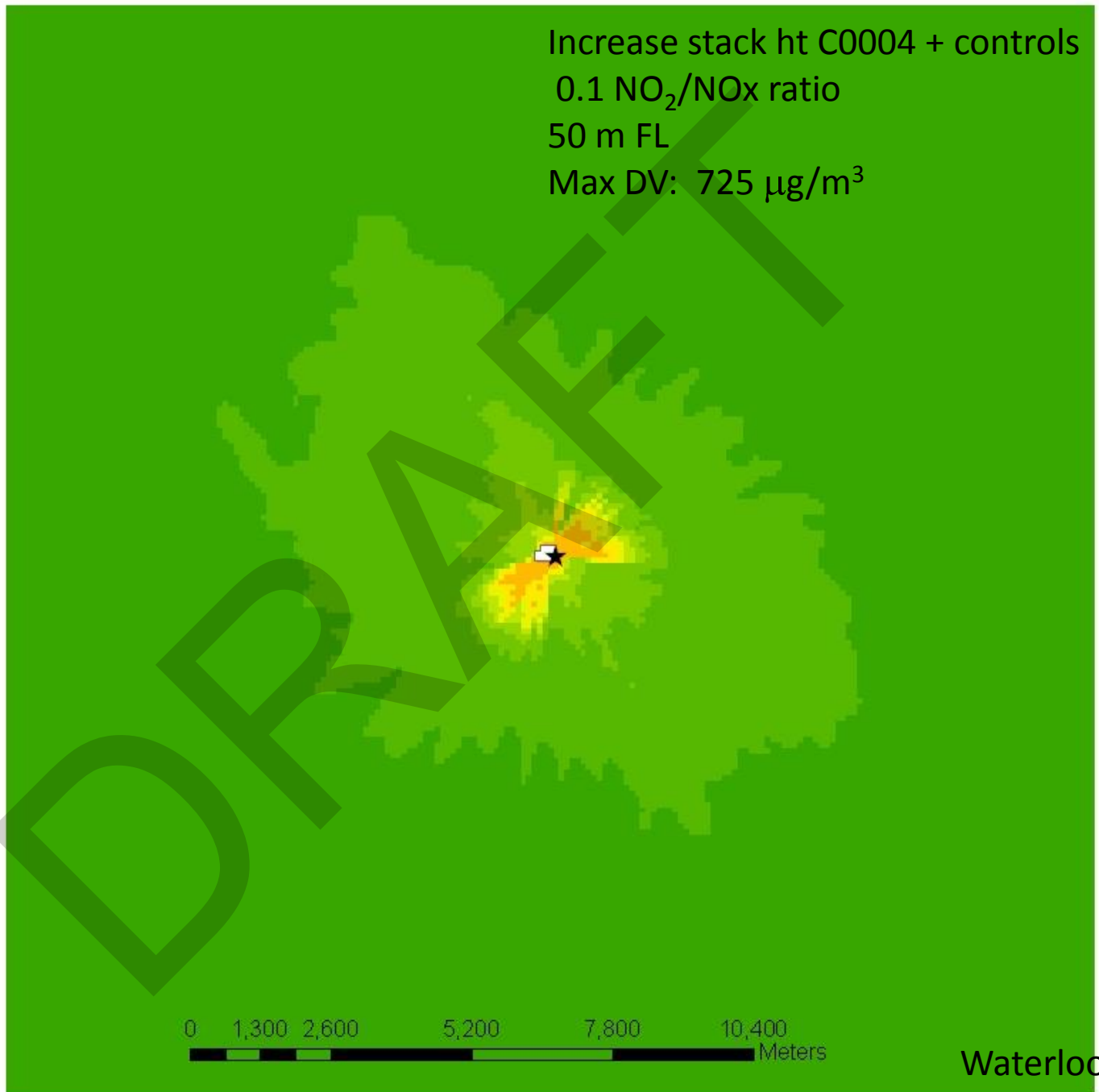
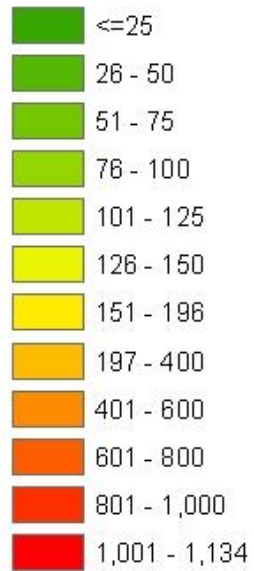
**Legend**



Waterloo

Increase stack ht C0004 + controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 725 μg/m<sup>3</sup>

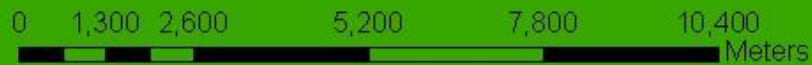
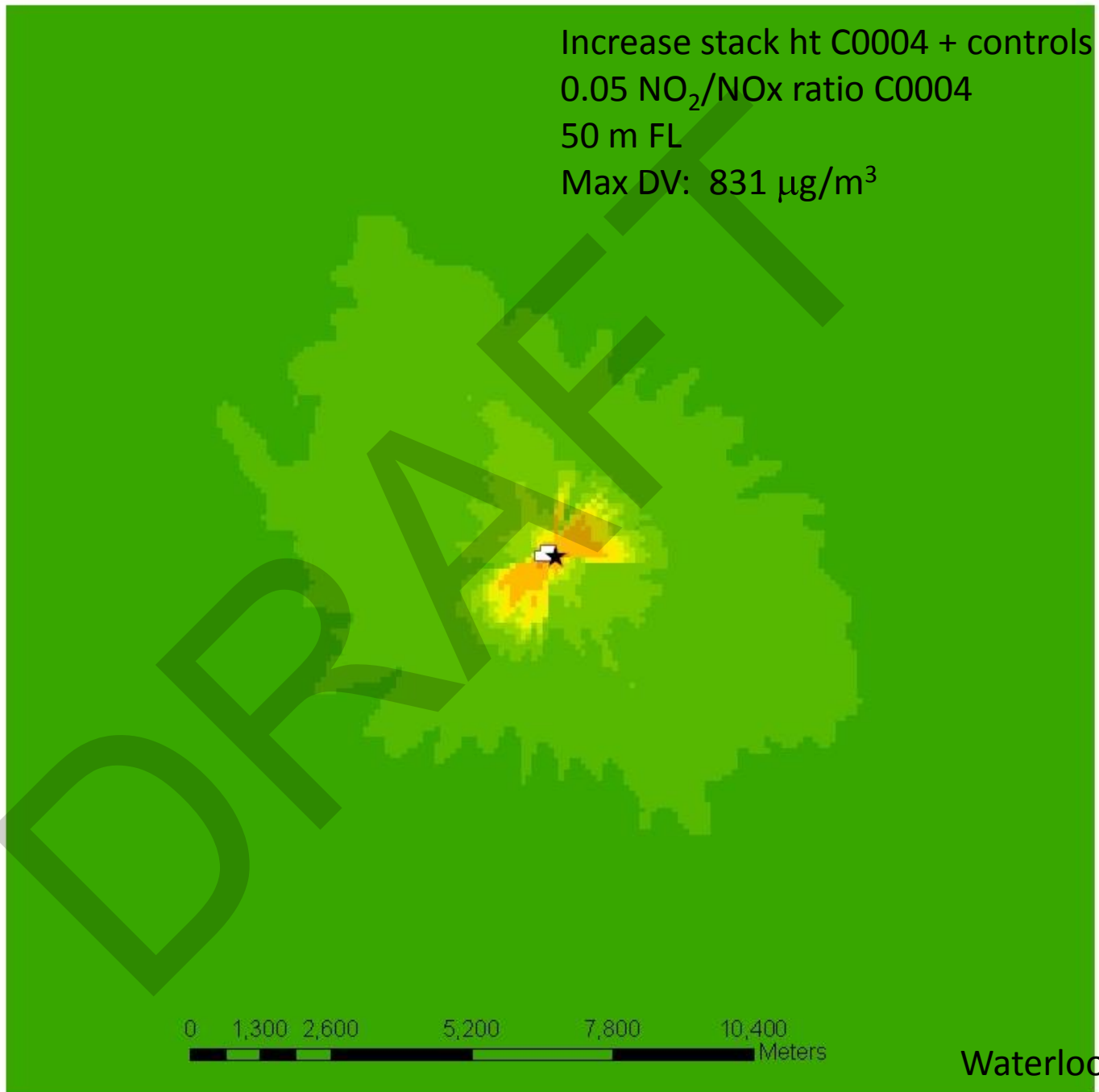
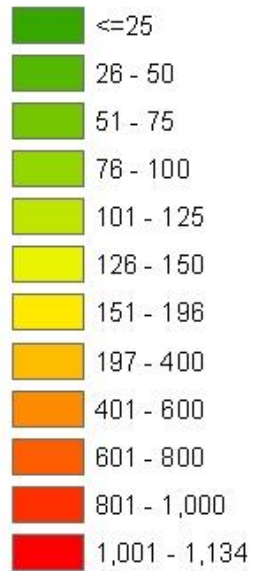
**Legend**



Waterloo

Increase stack ht C0004 + controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 831 μg/m<sup>3</sup>

**Legend**

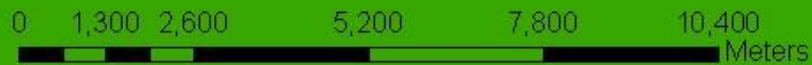
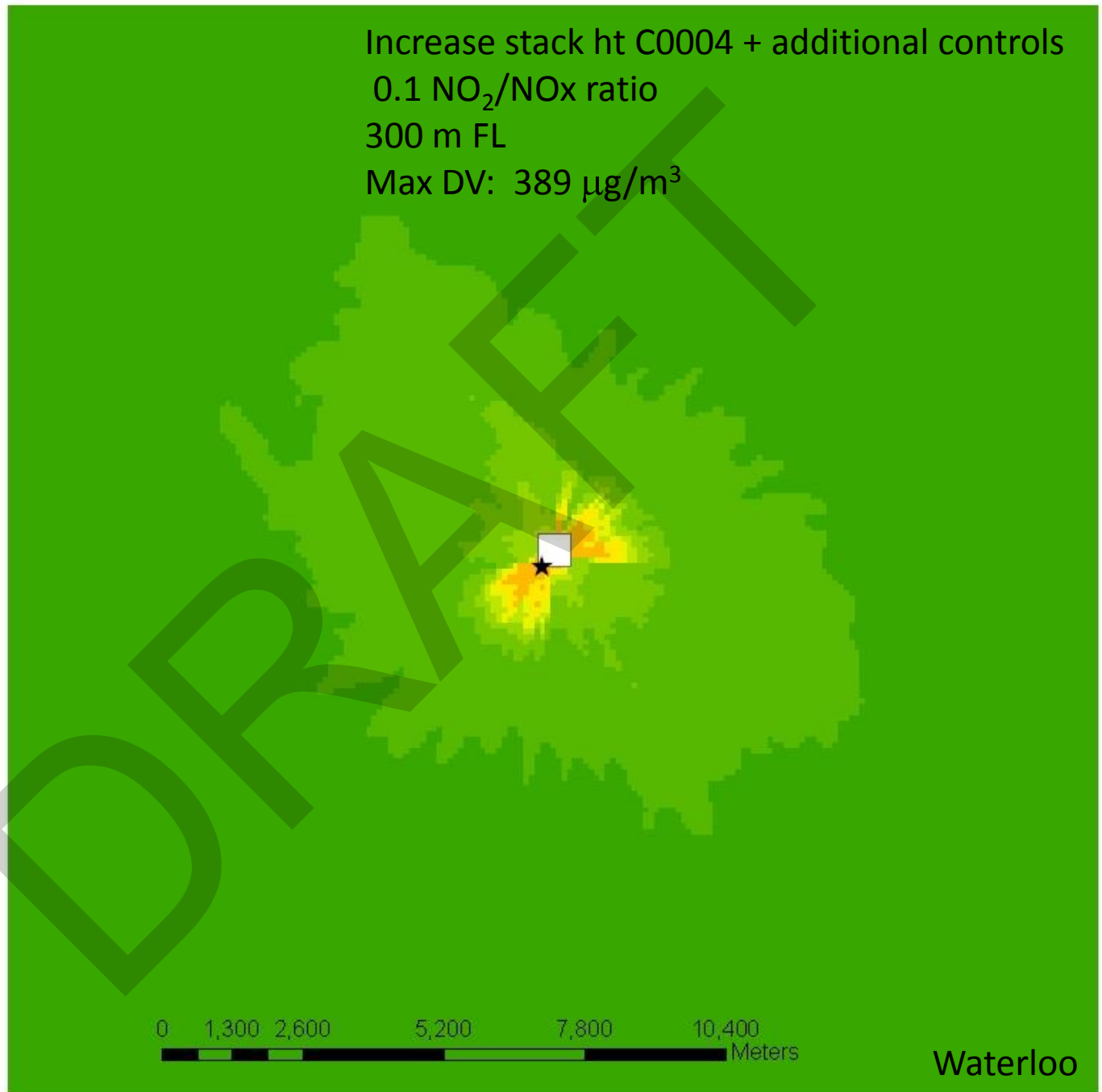
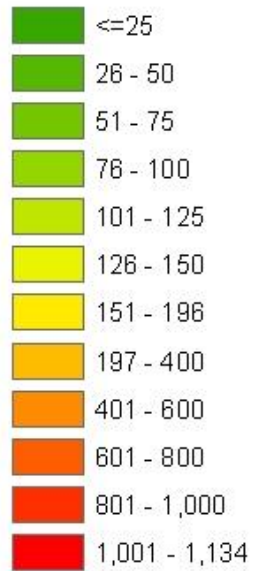


Waterloo



Increase stack ht C0004 + additional controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
300 m FL  
Max DV: 389 μg/m<sup>3</sup>

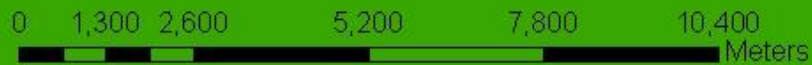
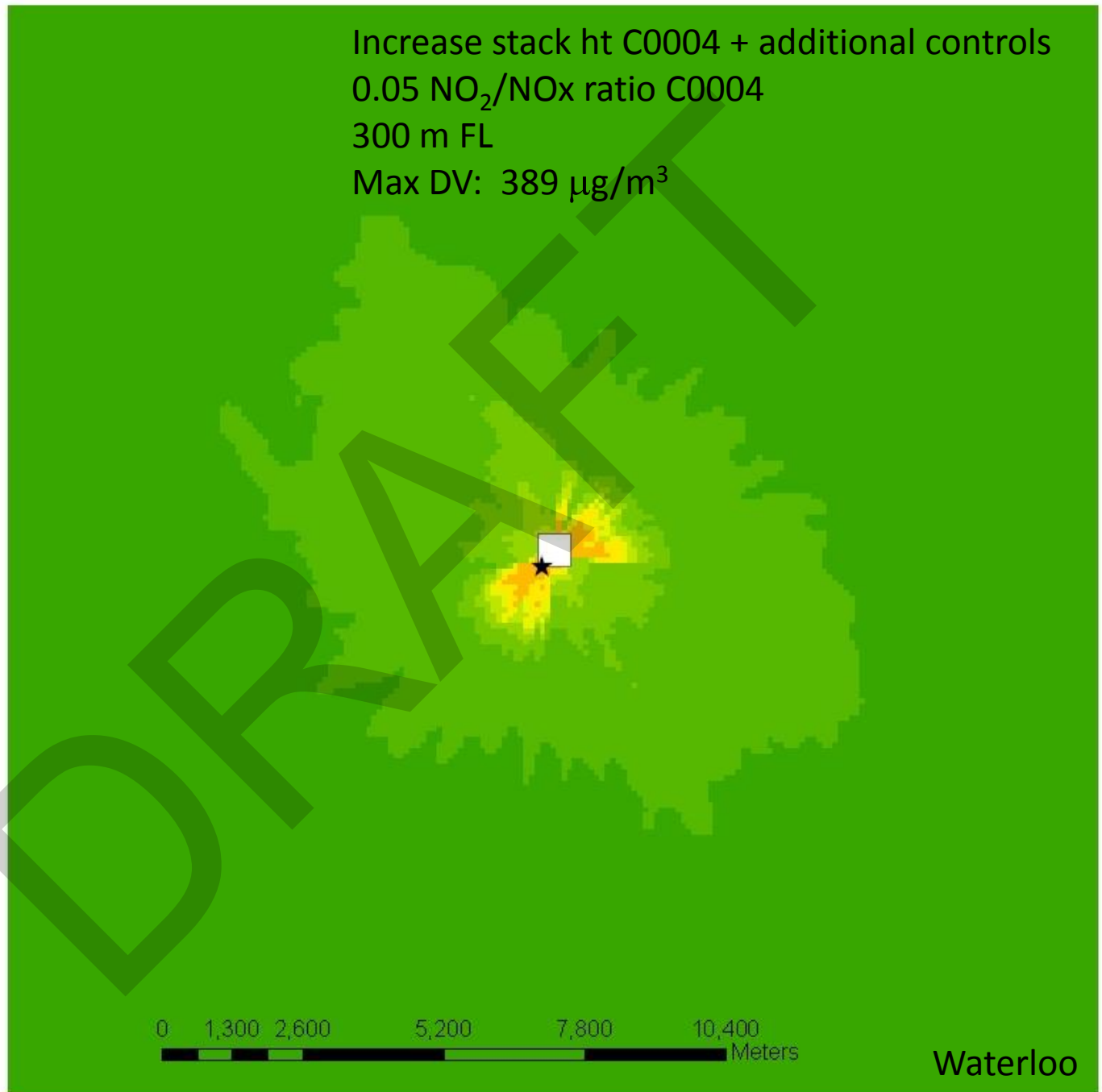
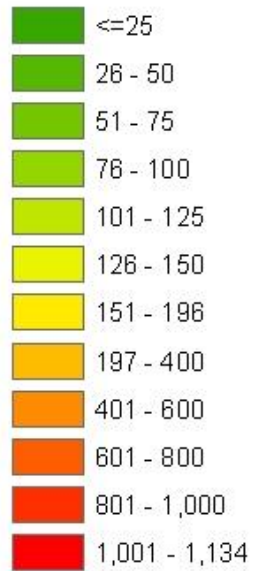
**Legend**



Waterloo

Increase stack ht C0004 + additional controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
300 m FL  
Max DV: 389 μg/m<sup>3</sup>

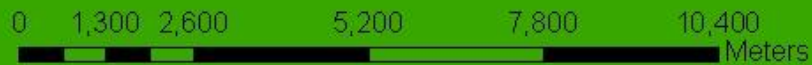
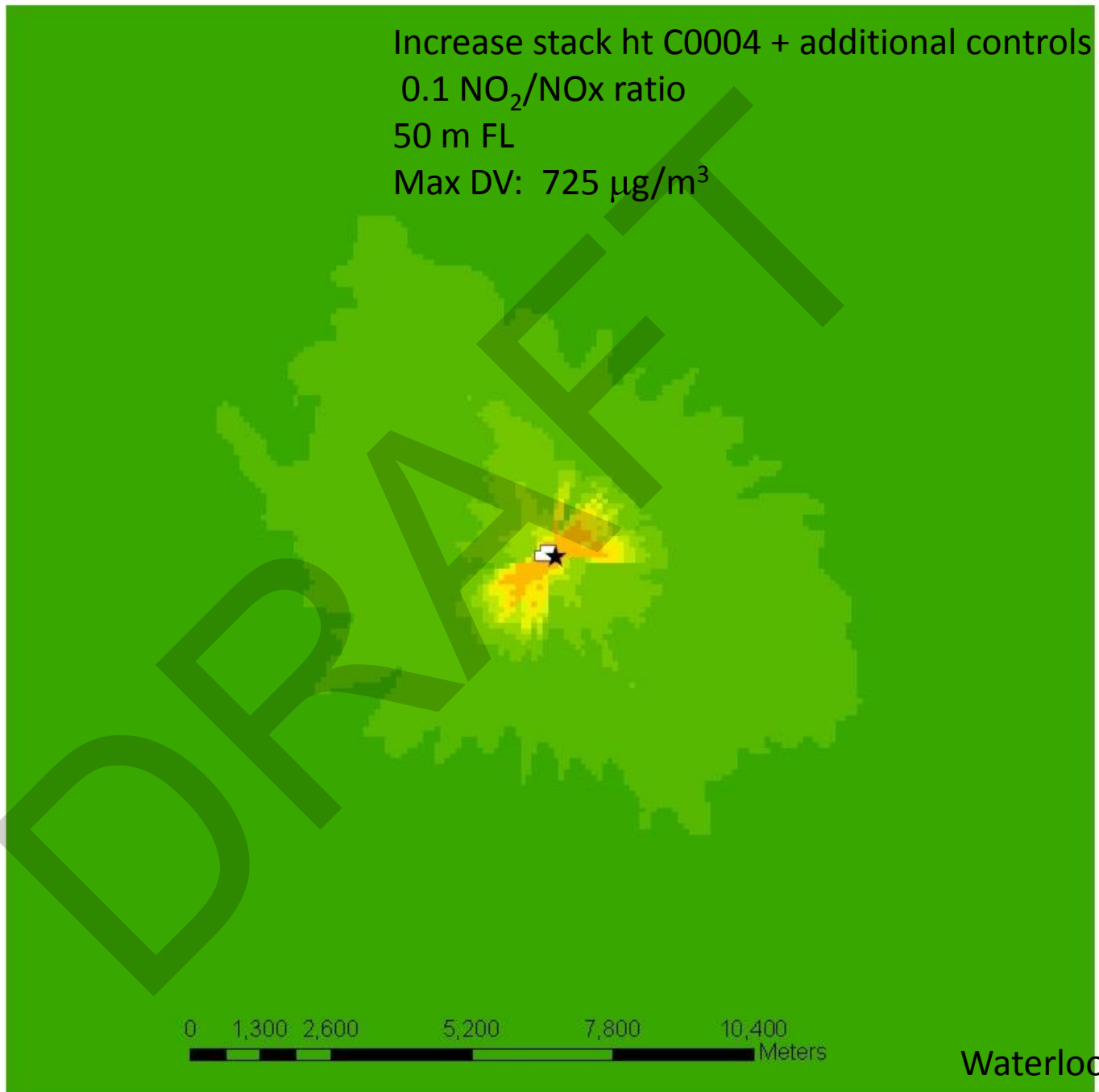
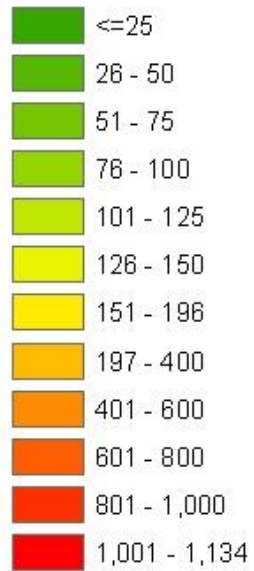
**Legend**



Waterloo

Increase stack ht C0004 + additional controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 725 μg/m<sup>3</sup>

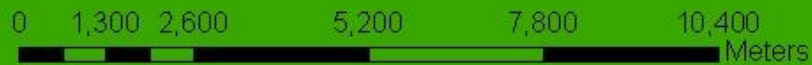
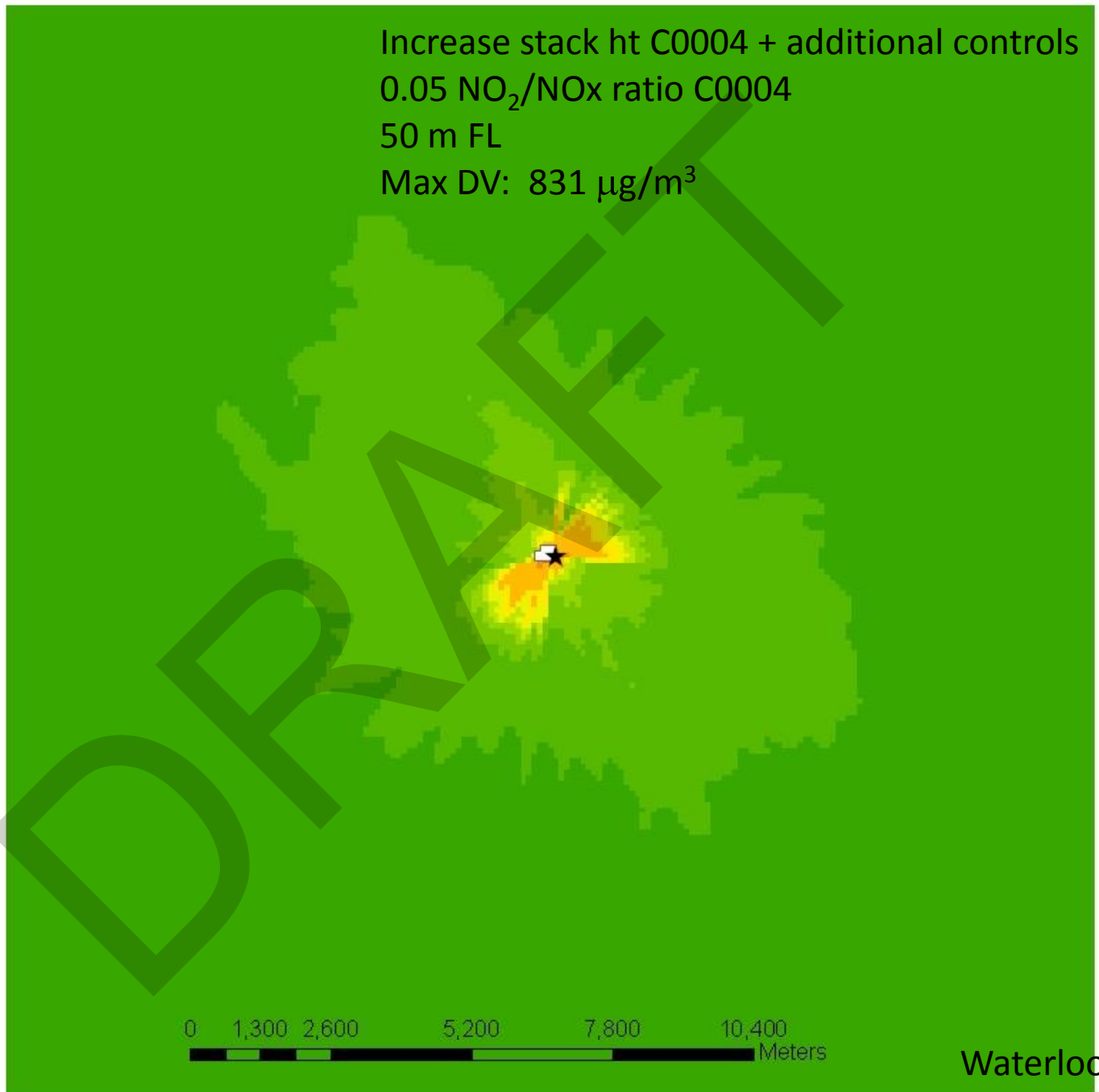
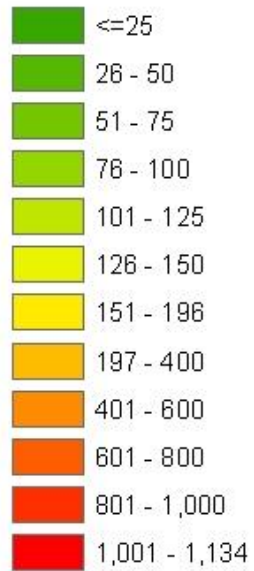
**Legend**



Waterloo

Increase stack ht C0004 + additional controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio C0004  
50 m FL  
Max DV: 831 μg/m<sup>3</sup>

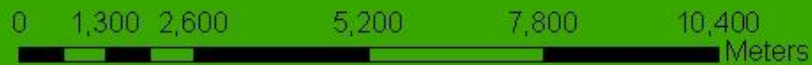
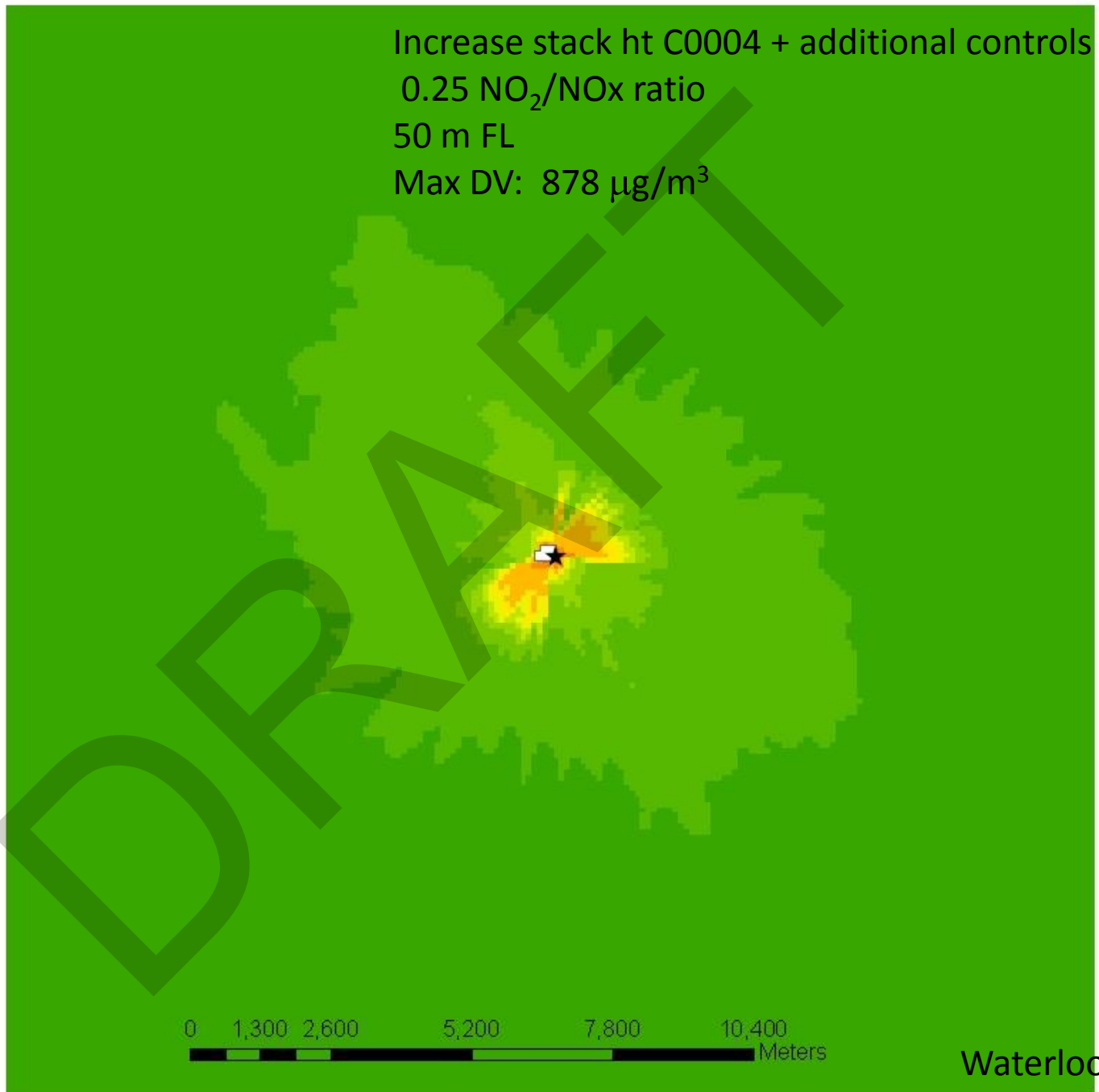
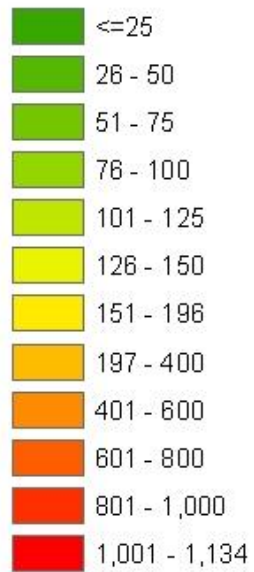
**Legend**



Waterloo

Increase stack ht C0004 + additional controls  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 878 μg/m<sup>3</sup>

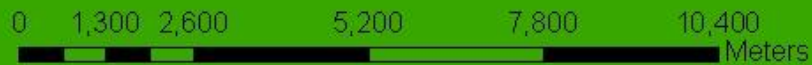
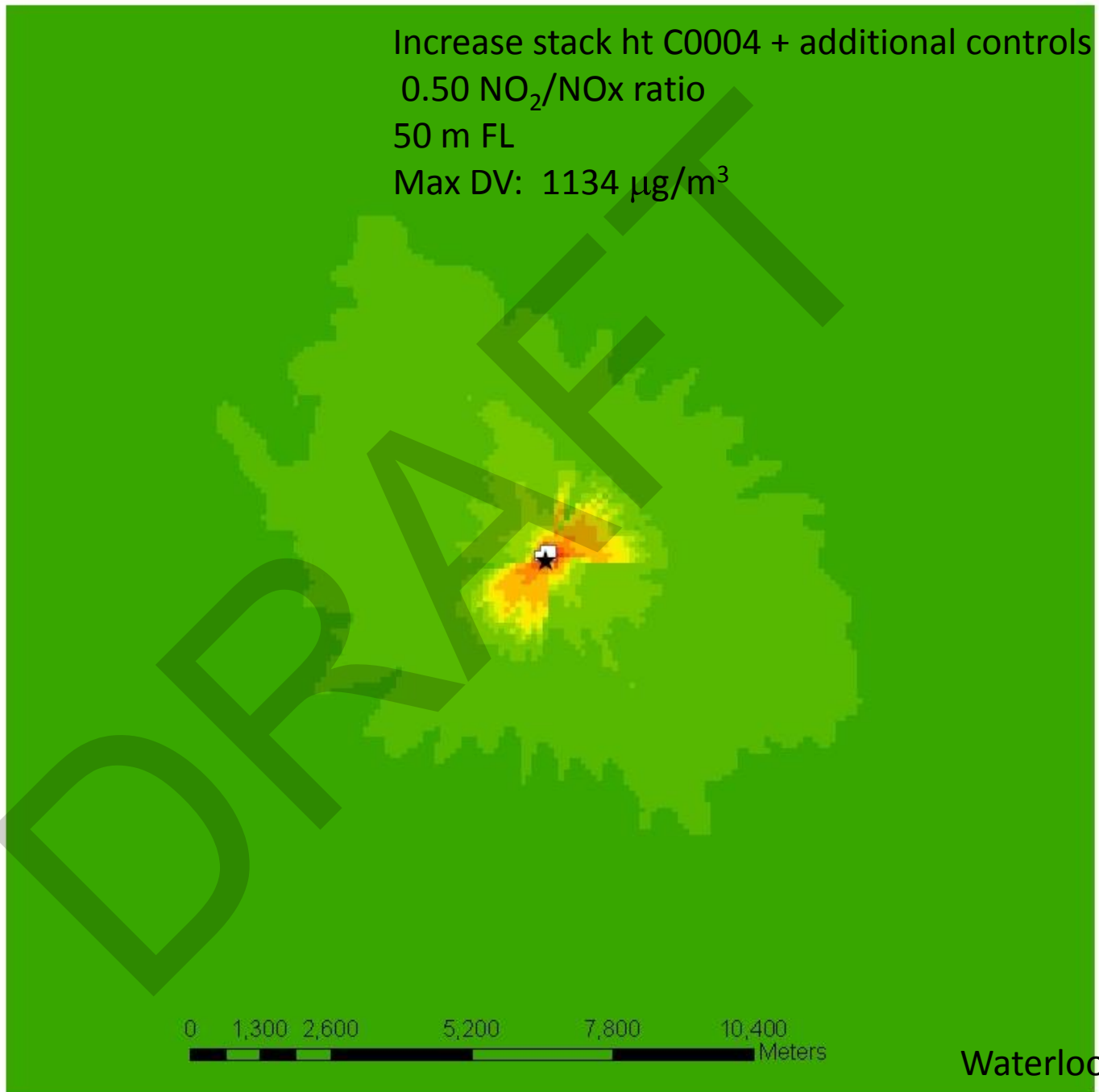
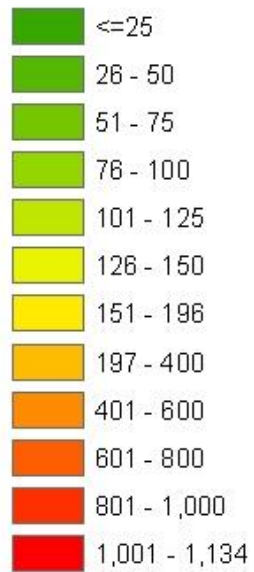
**Legend**



Waterloo

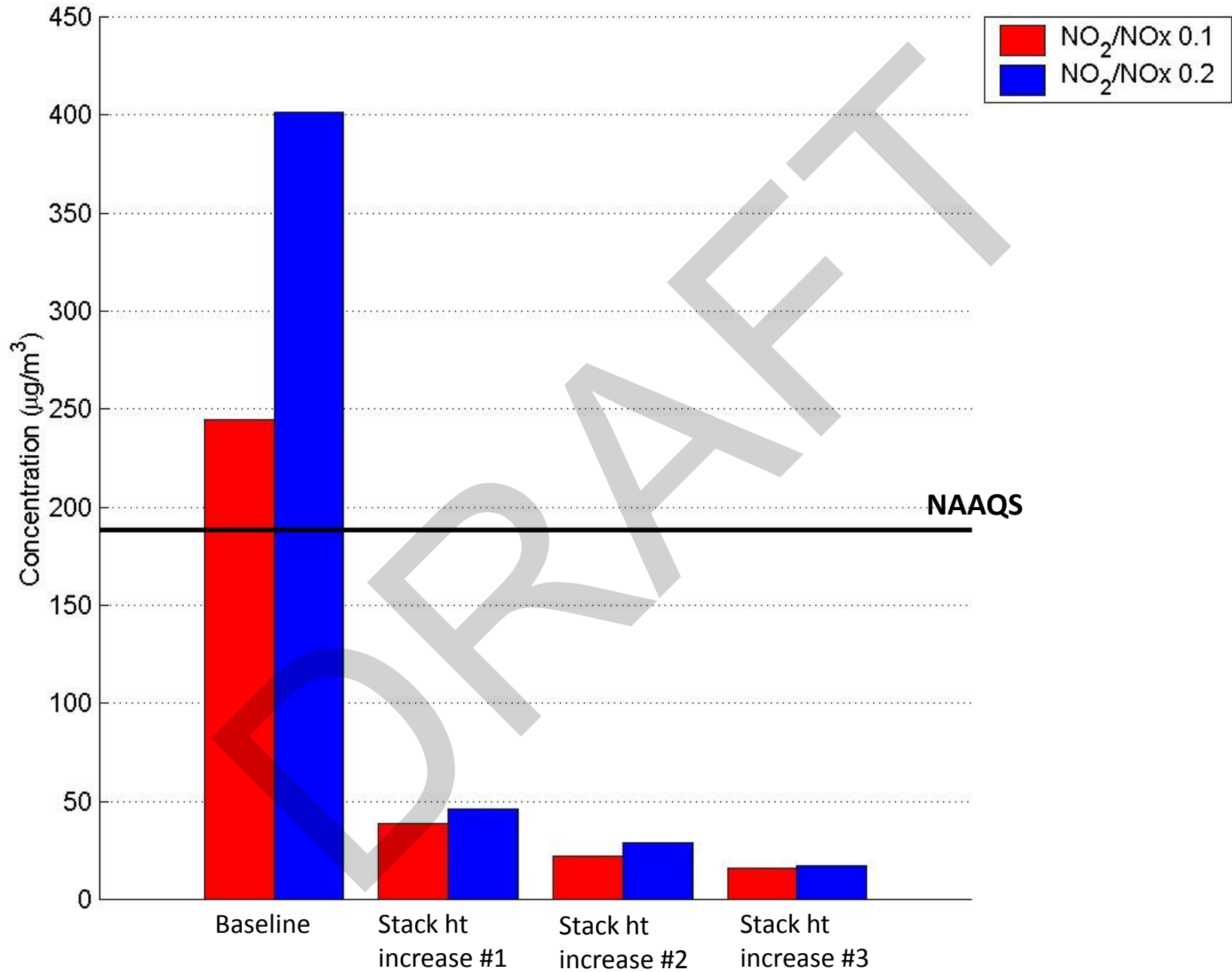
Increase stack ht C0004 + additional controls  
0.50 NO<sub>2</sub>/NO<sub>x</sub> ratio  
50 m FL  
Max DV: 1134 μg/m<sup>3</sup>

**Legend**

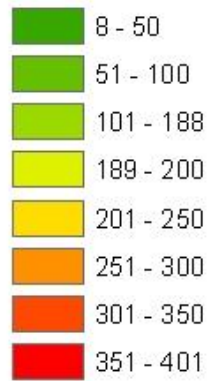


Waterloo

# Materials Recycler: NO<sub>2</sub>



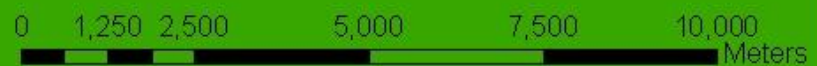
**Legend**



Base

0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 244 μg/m<sup>3</sup>



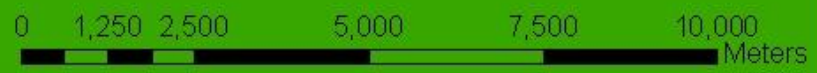


**Legend**

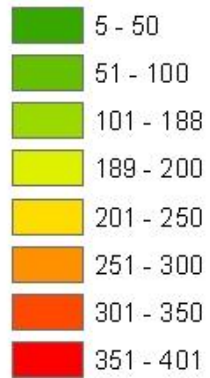


Base  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 401 μg/m<sup>3</sup>

DRAFT

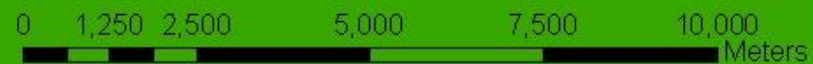


**Legend**



Stack ht increase #1  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 39 μg/m<sup>3</sup>

DRAFT

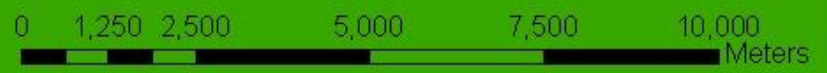


**Legend**



Stack ht increase #1  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 46 μg/m<sup>3</sup>

DRAFT



**Legend**



Stack ht increase #2  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 22 μg/m<sup>3</sup>

DRAFT

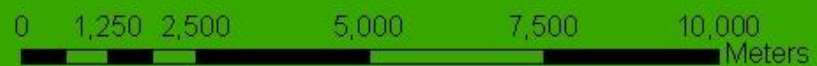


**Legend**



Stack ht increase #2  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 29 μg/m<sup>3</sup>

DRAFT

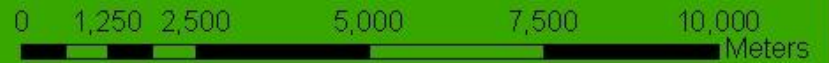


**Legend**



Stack ht increase #3  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 16 µg/m<sup>3</sup>

DRAFT



**Legend**

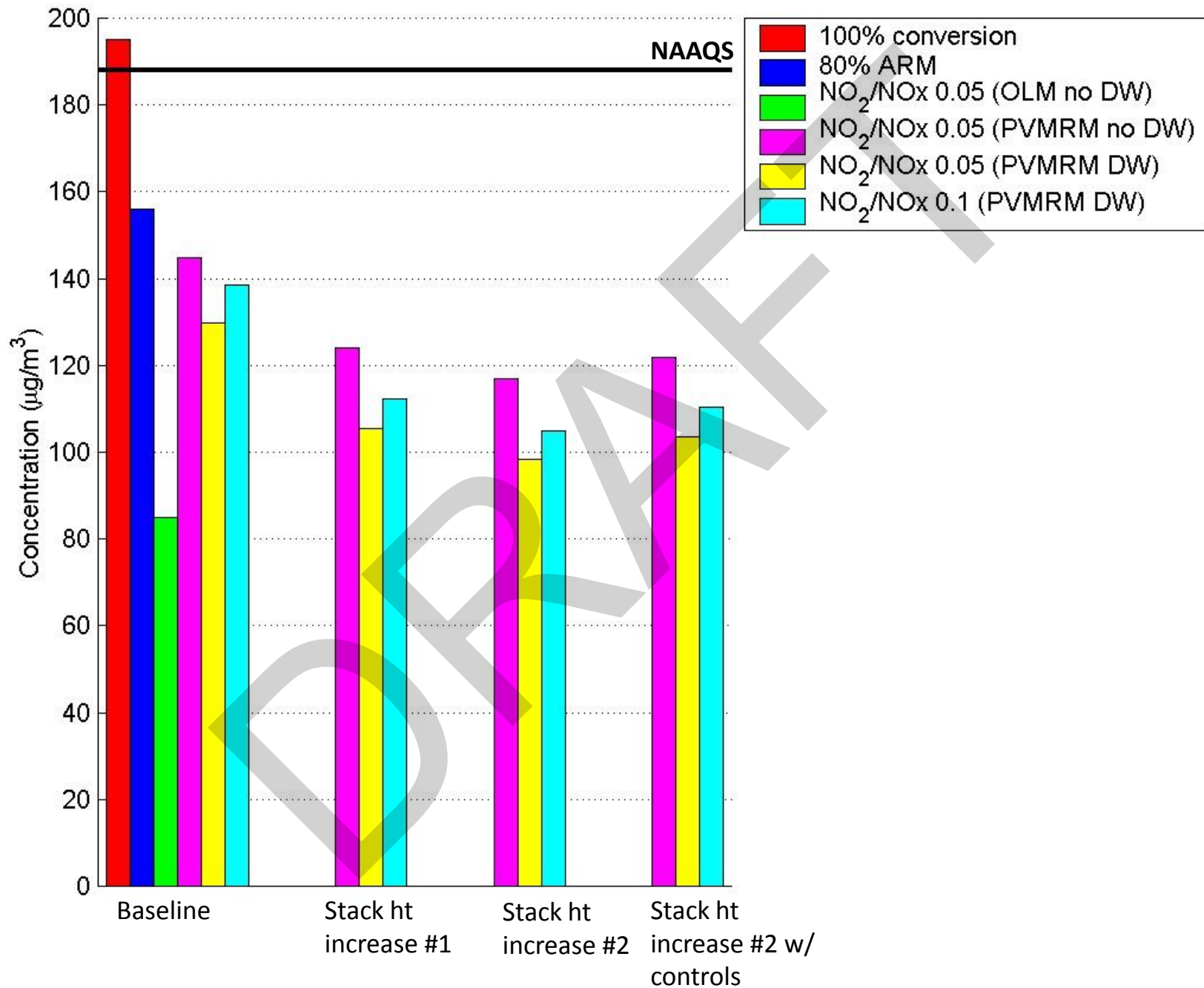


Stack ht increase #3  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 17 μg/m<sup>3</sup>

DRRAFT

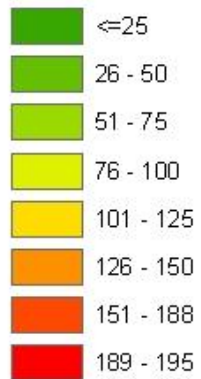


# Natural Gas Turbine (Poughkeepsie): NO<sub>2</sub>

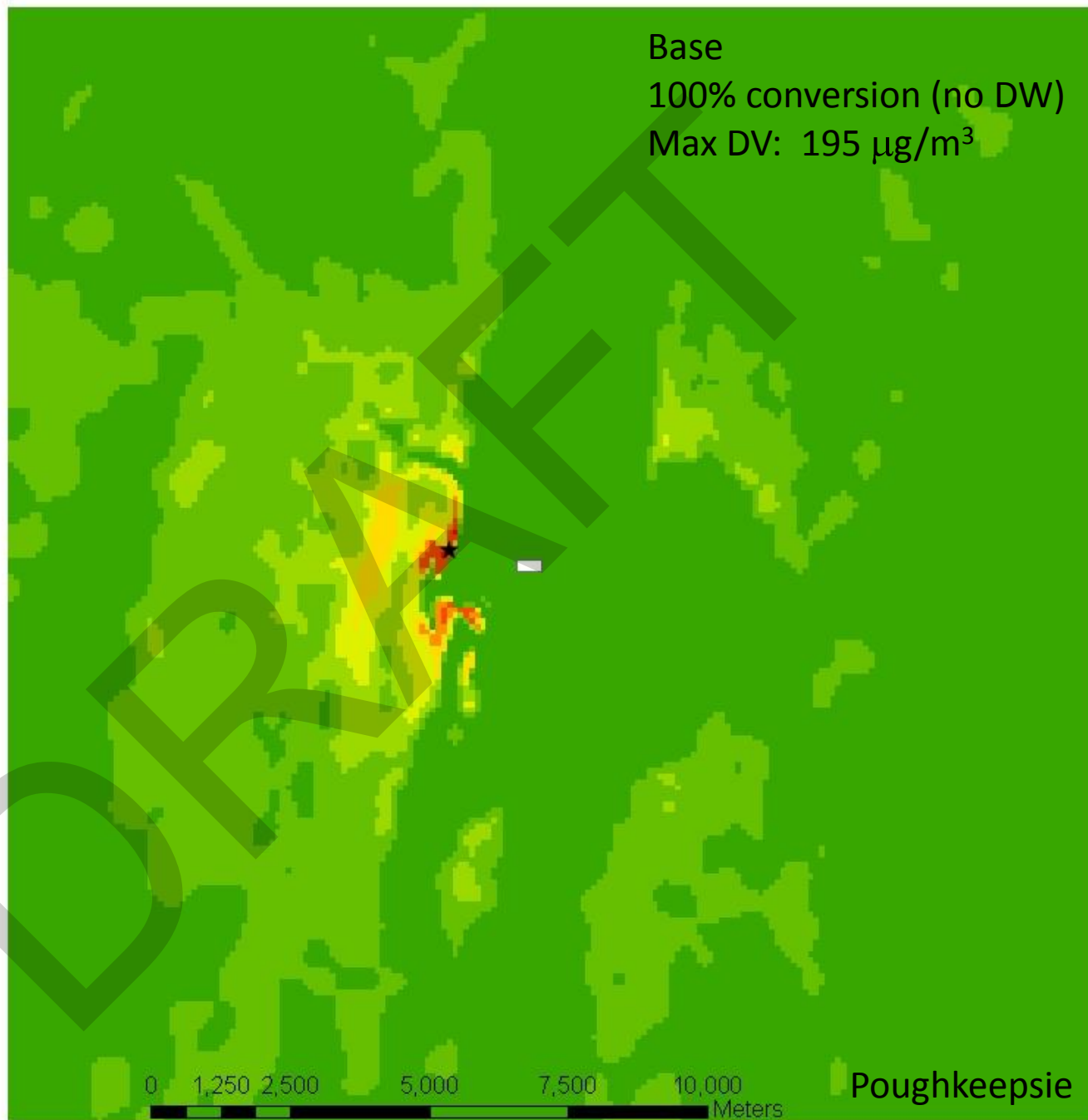




**Legend**



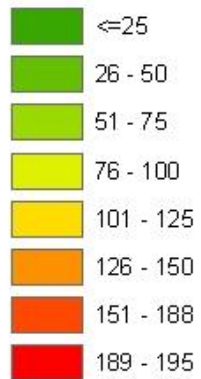
Base  
100% conversion (no DW)  
Max DV: 195 µg/m<sup>3</sup>



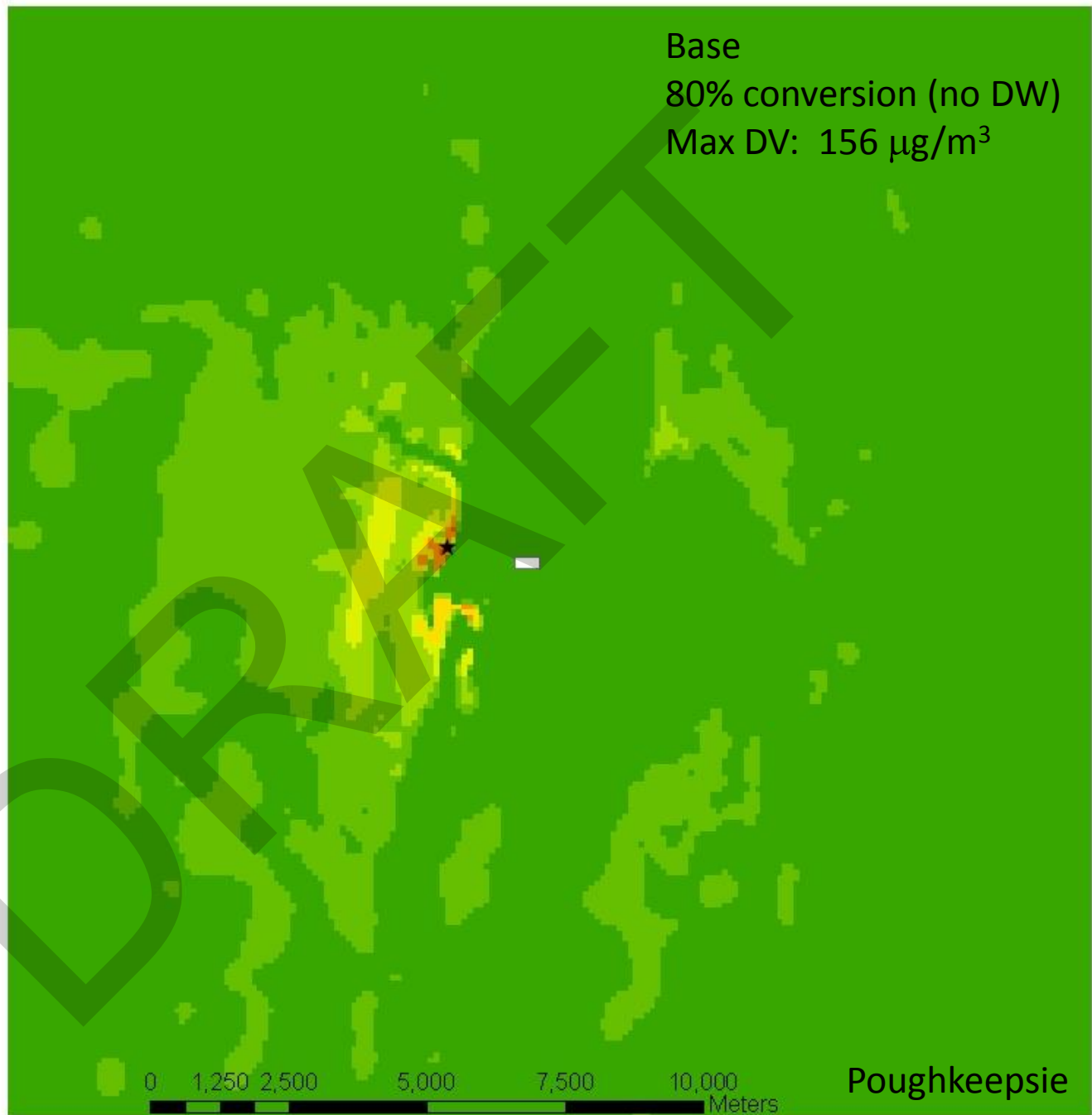
0 1,250 2,500 5,000 7,500 10,000 Meters

Poughkeepsie

### Legend



Base  
80% conversion (no DW)  
Max DV: 156  $\mu\text{g}/\text{m}^3$

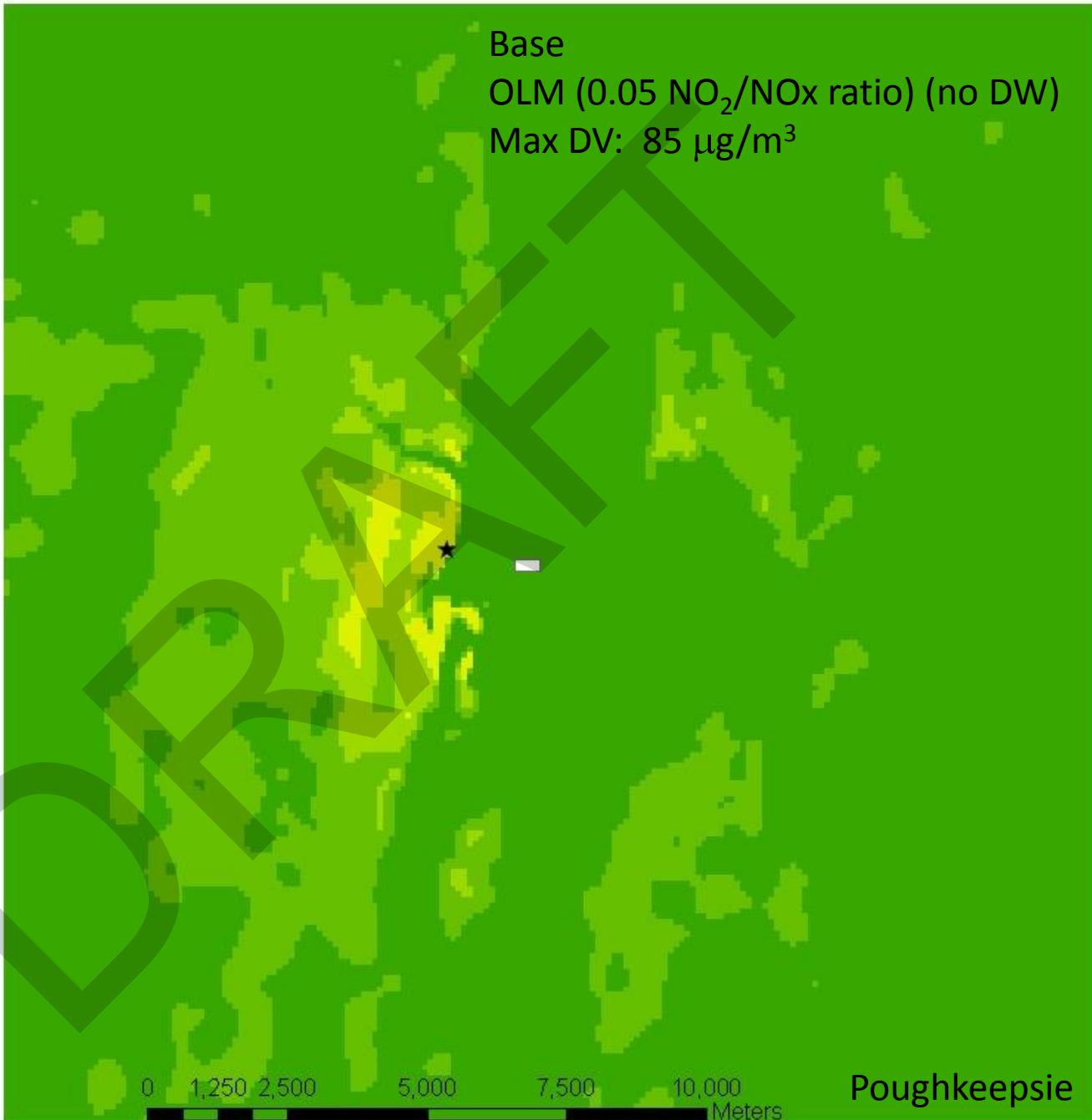
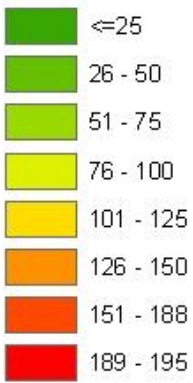


0 1,250 2,500 5,000 7,500 10,000 Meters

Poughkeepsie

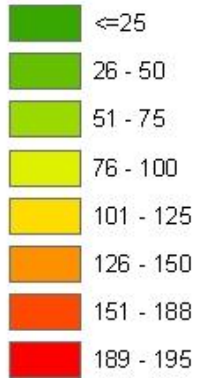
Base  
OLM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 85 μg/m<sup>3</sup>

**Legend**

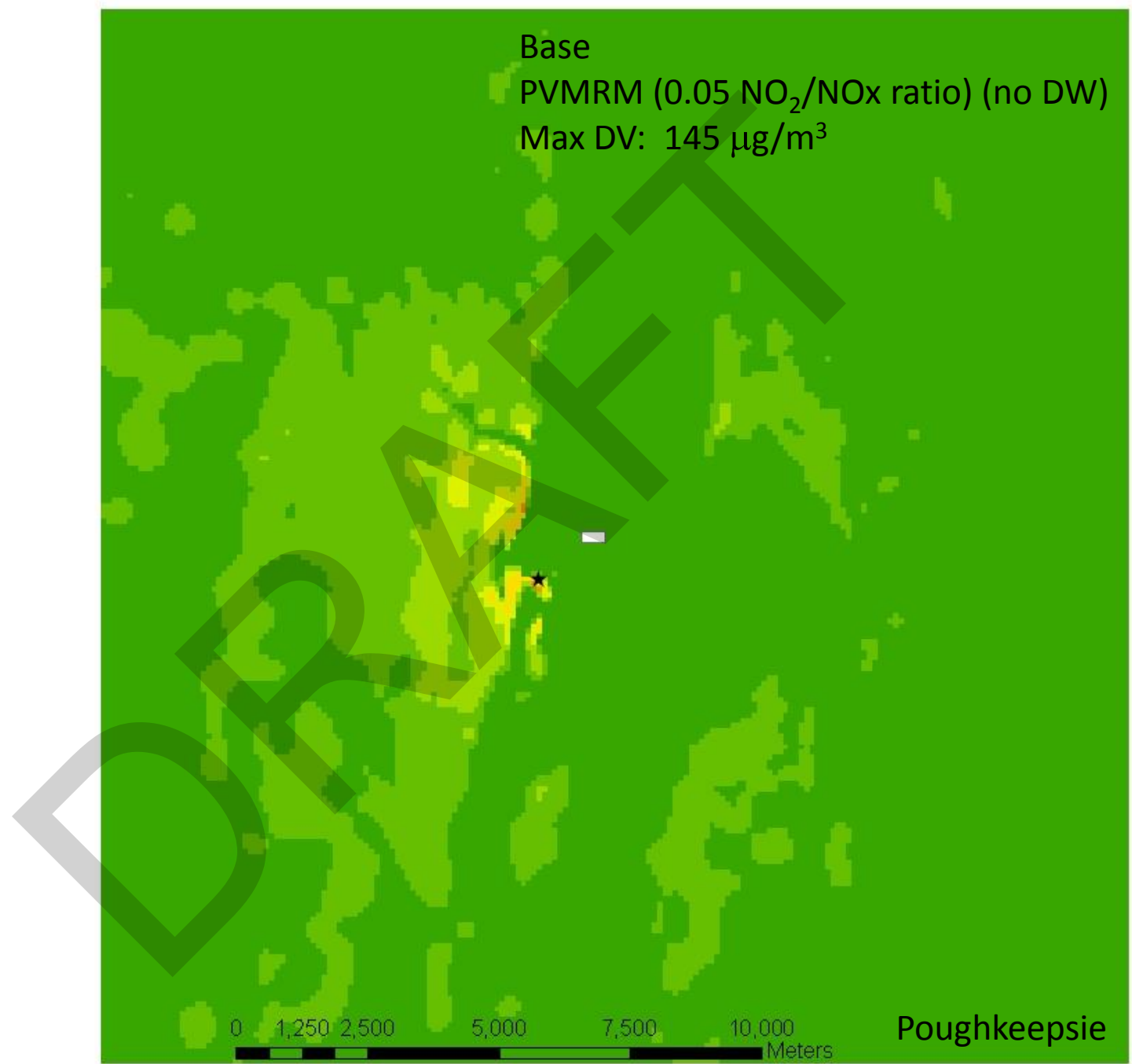


Poughkeepsie

**Legend**



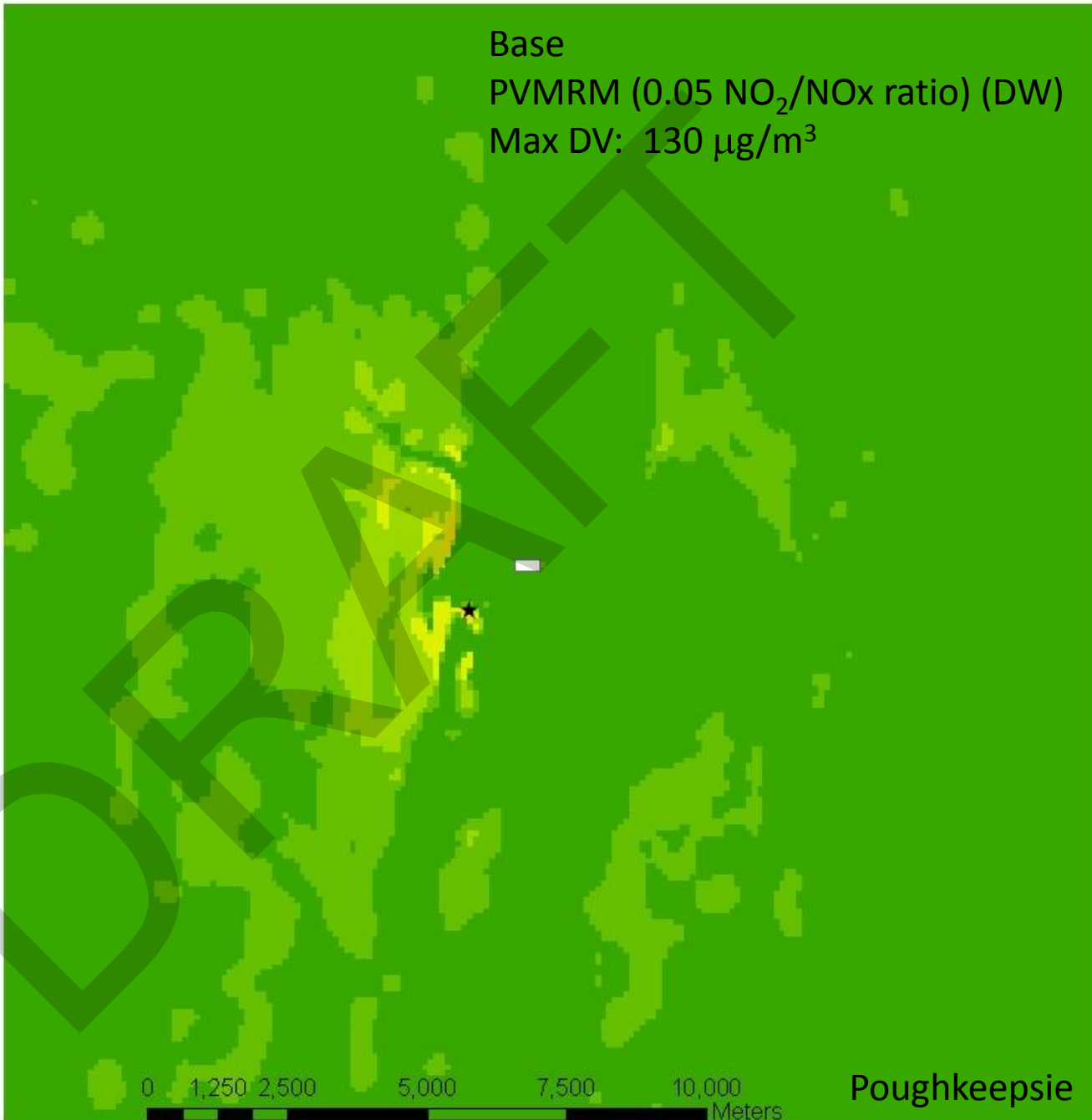
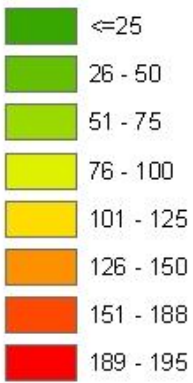
Base  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 145 µg/m<sup>3</sup>



Poughkeepsie

Base  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 130 µg/m<sup>3</sup>

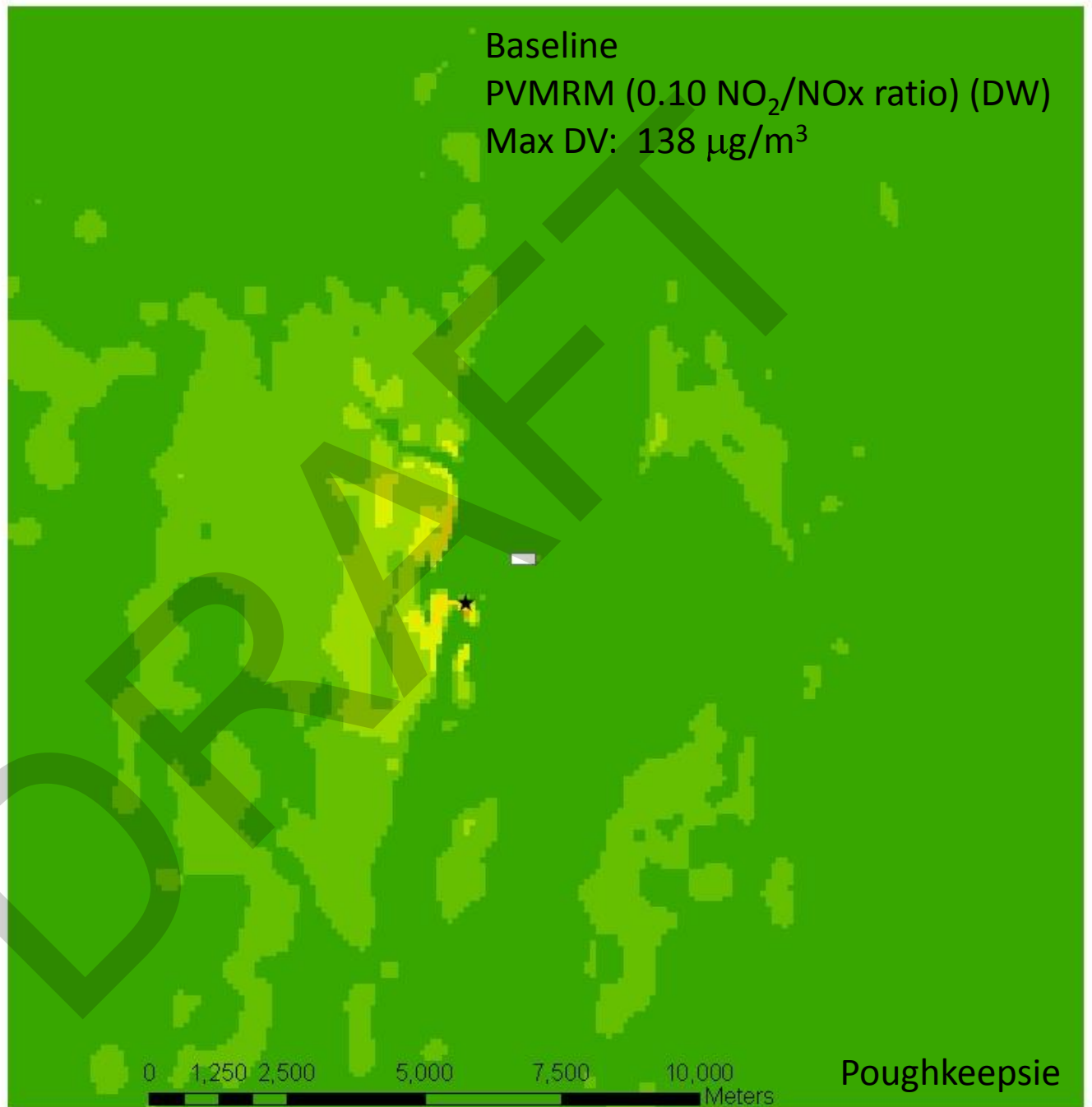
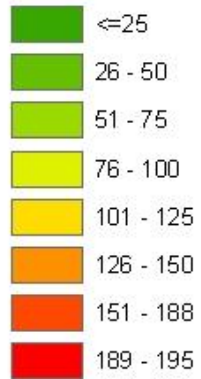
**Legend**



Poughkeepsie

Baseline  
PVMRM (0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 138 µg/m<sup>3</sup>

**Legend**



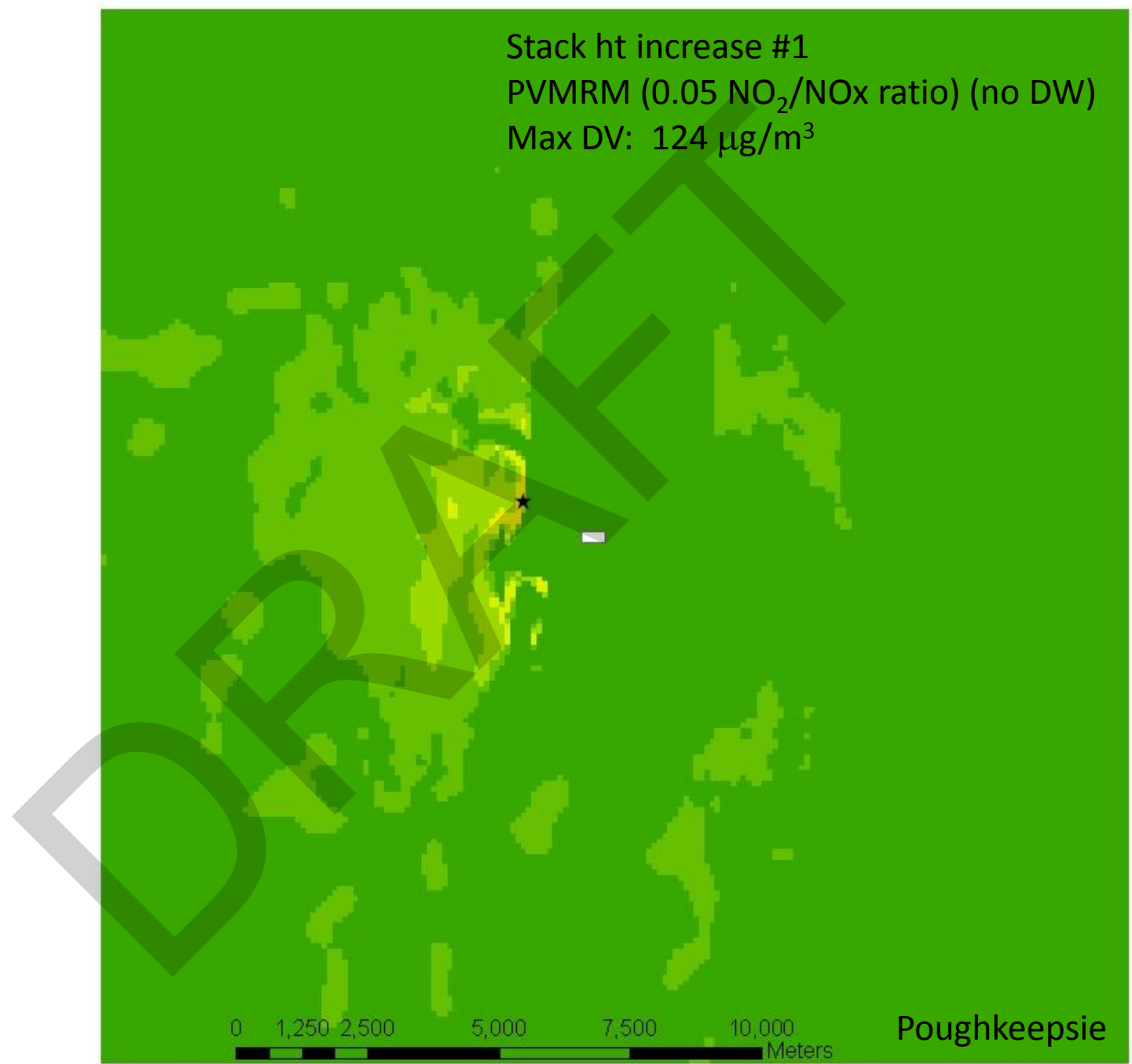
0 1,250 2,500 5,000 7,500 10,000 Meters

Poughkeepsie

**Legend**



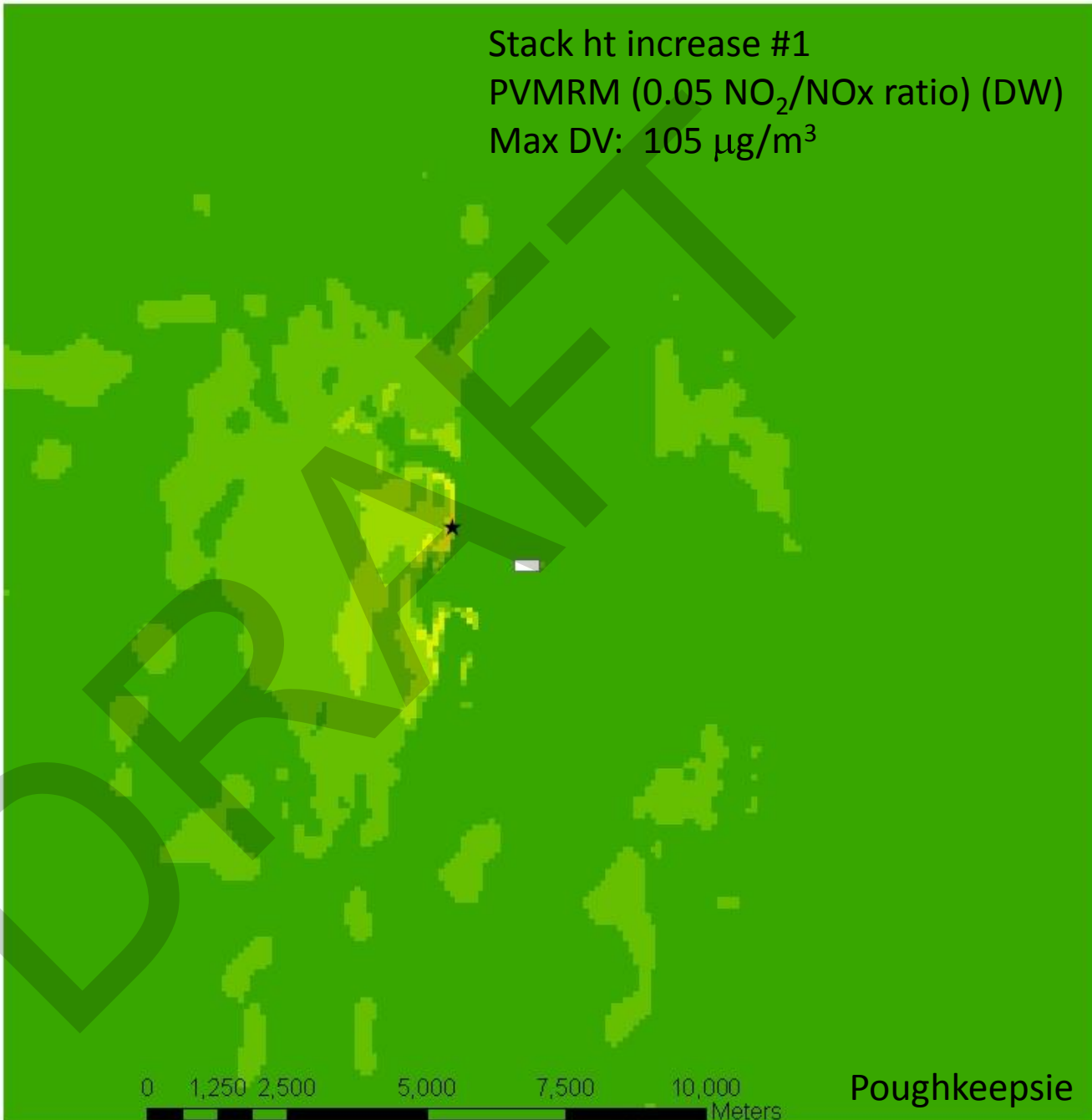
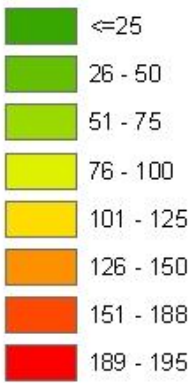
Stack ht increase #1  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 124 μg/m<sup>3</sup>



Poughkeepsie

Stack ht increase #1  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 105 μg/m<sup>3</sup>

**Legend**



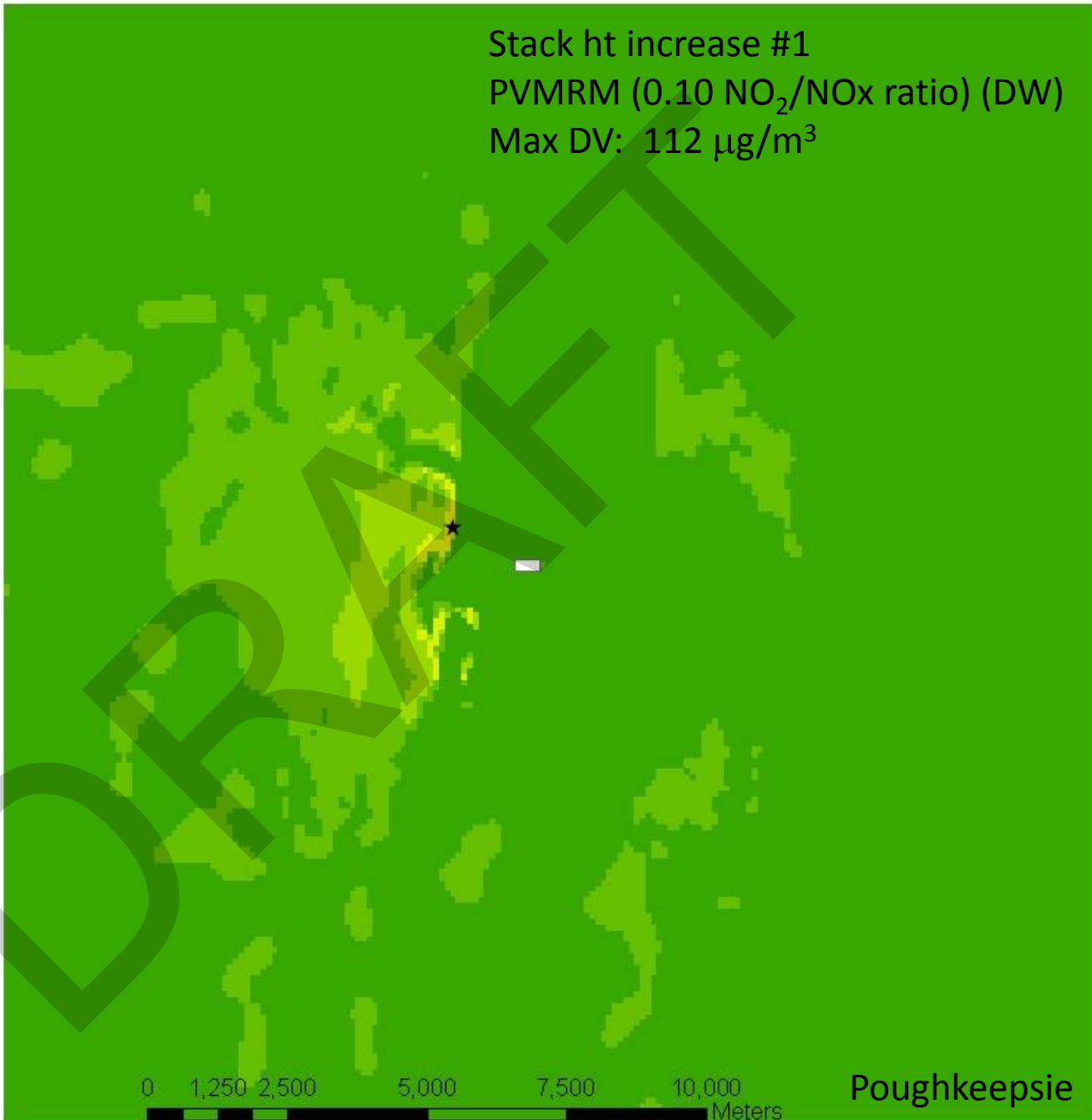
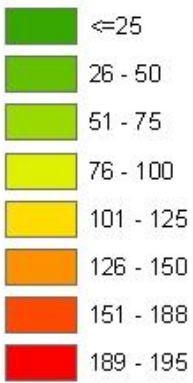
0 1,250 2,500 5,000 7,500 10,000 Meters

Poughkeepsie



Stack ht increase #1  
PVMRM (0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 112 µg/m<sup>3</sup>

**Legend**

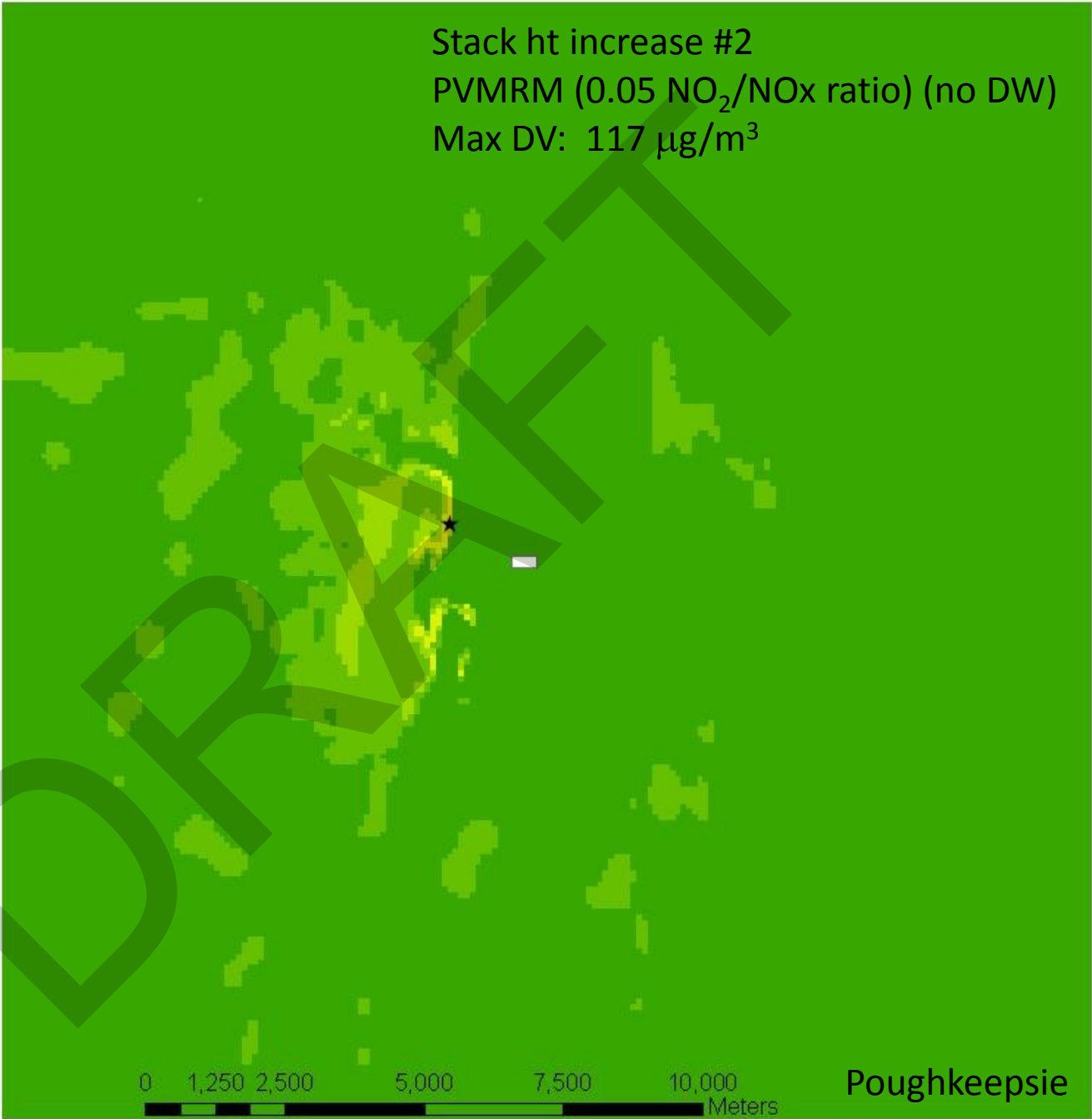
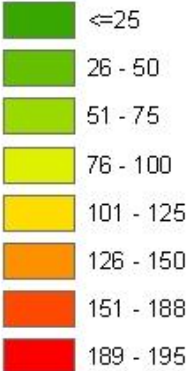


0 1,250 2,500 5,000 7,500 10,000 Meters

Poughkeepsie

Stack ht increase #2  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 117 µg/m<sup>3</sup>

**Legend**

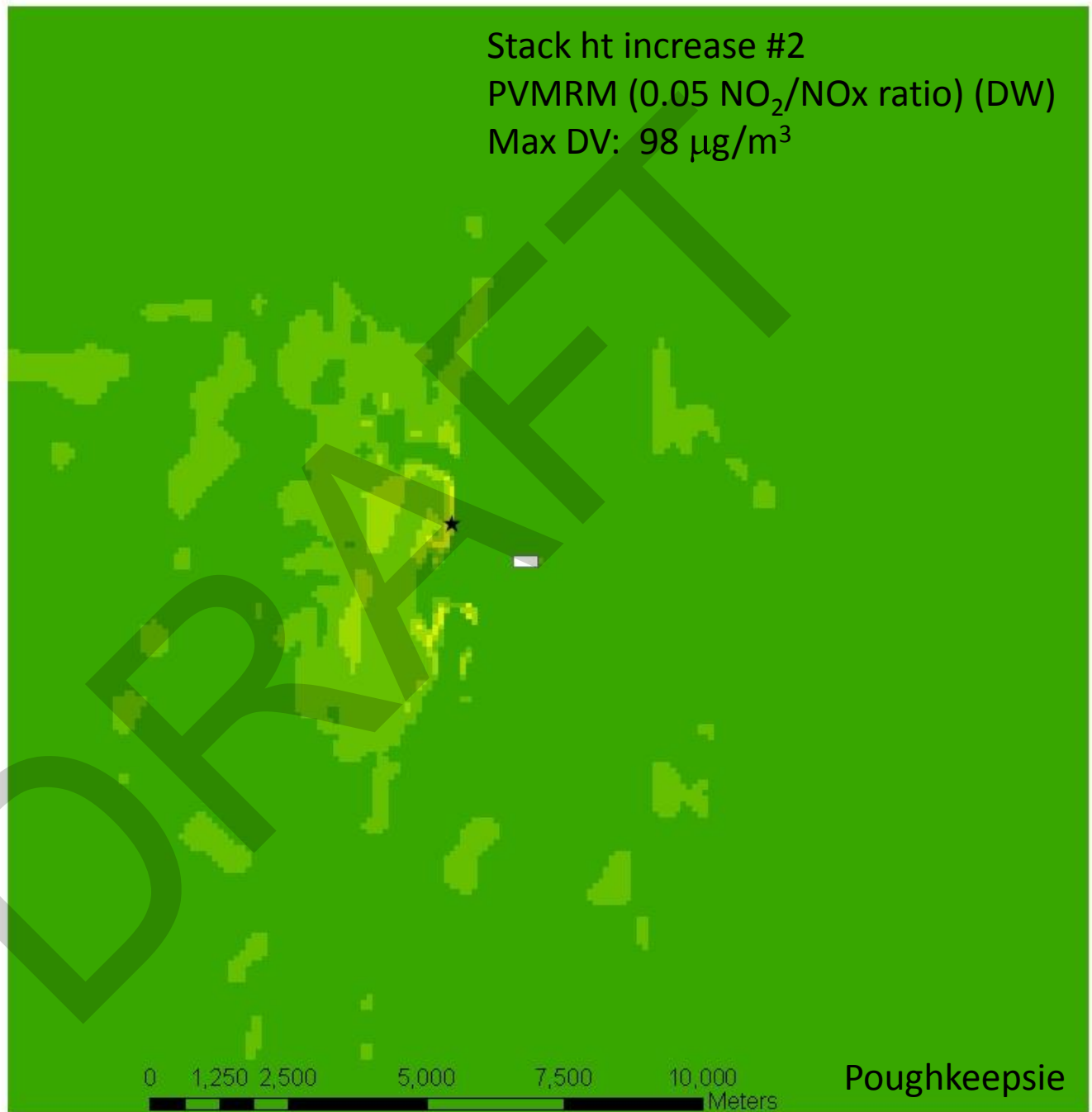
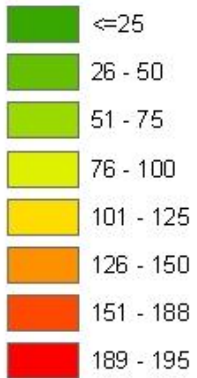


0 1,250 2,500 5,000 7,500 10,000 Meters

Poughkeepsie

Stack ht increase #2  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 98 μg/m<sup>3</sup>

**Legend**

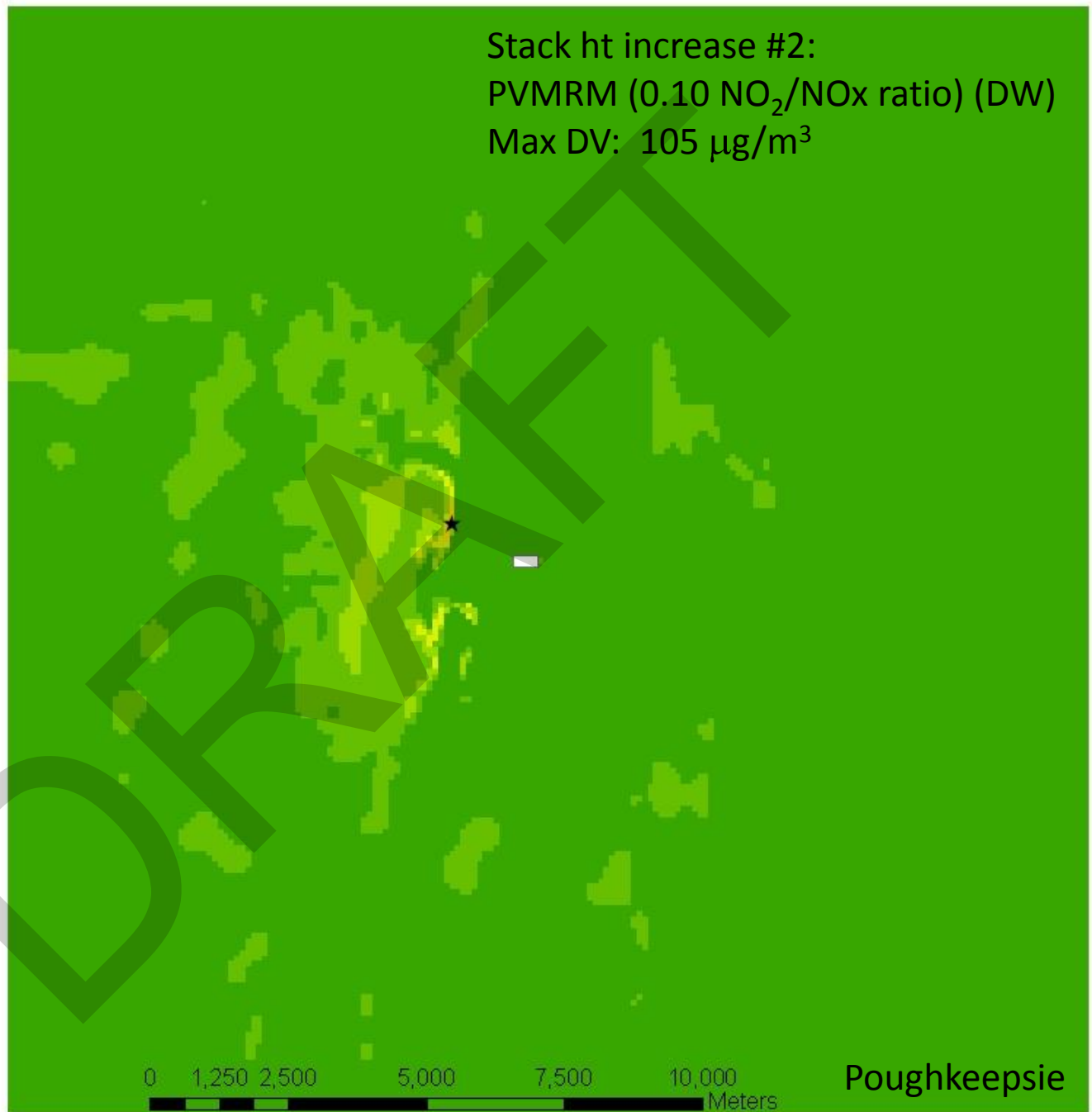
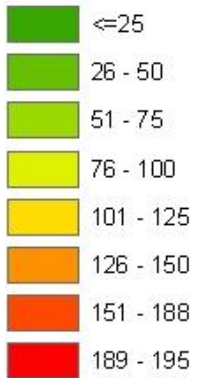


0 1,250 2,500 5,000 7,500 10,000 Meters

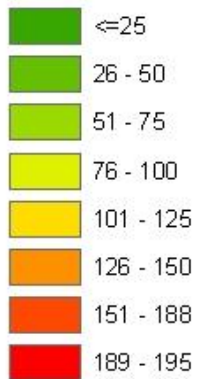
Poughkeepsie

Stack ht increase #2:  
PVMRM (0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 105 µg/m<sup>3</sup>

**Legend**



**Legend**



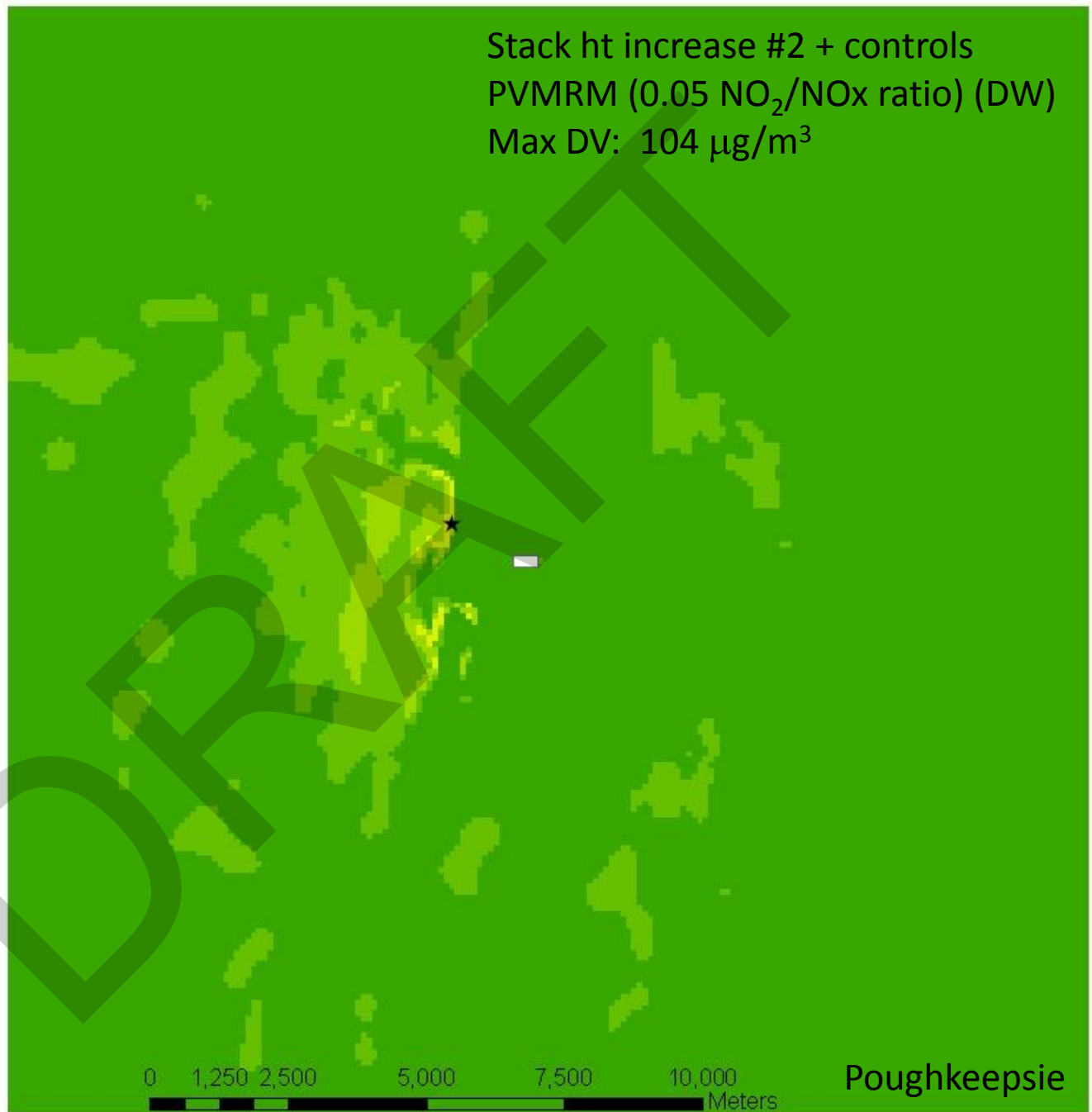
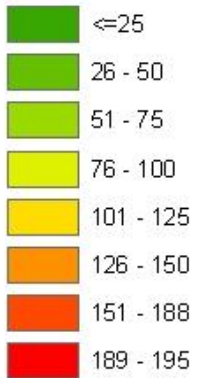
Stack ht increase #2 + controls  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 122 μg/m<sup>3</sup>



Poughkeepsie

Stack ht increase #2 + controls  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 104 μg/m<sup>3</sup>

**Legend**

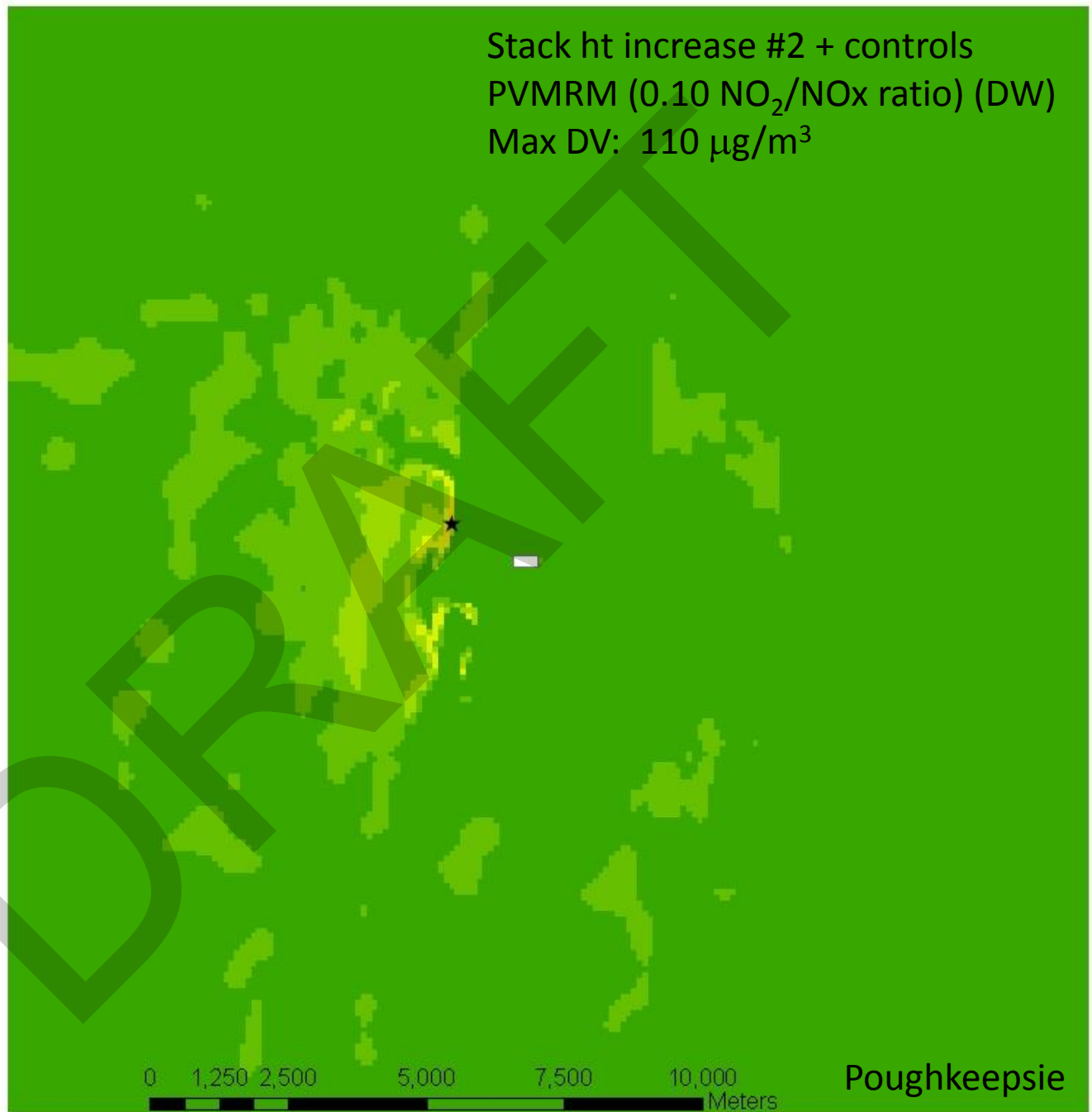
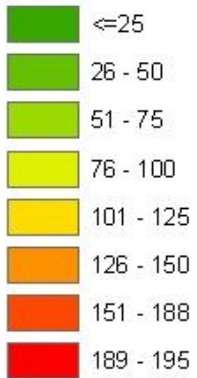


0 1,250 2,500 5,000 7,500 10,000 Meters

Poughkeepsie

Stack ht increase #2 + controls  
PVMRM (0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 110 µg/m<sup>3</sup>

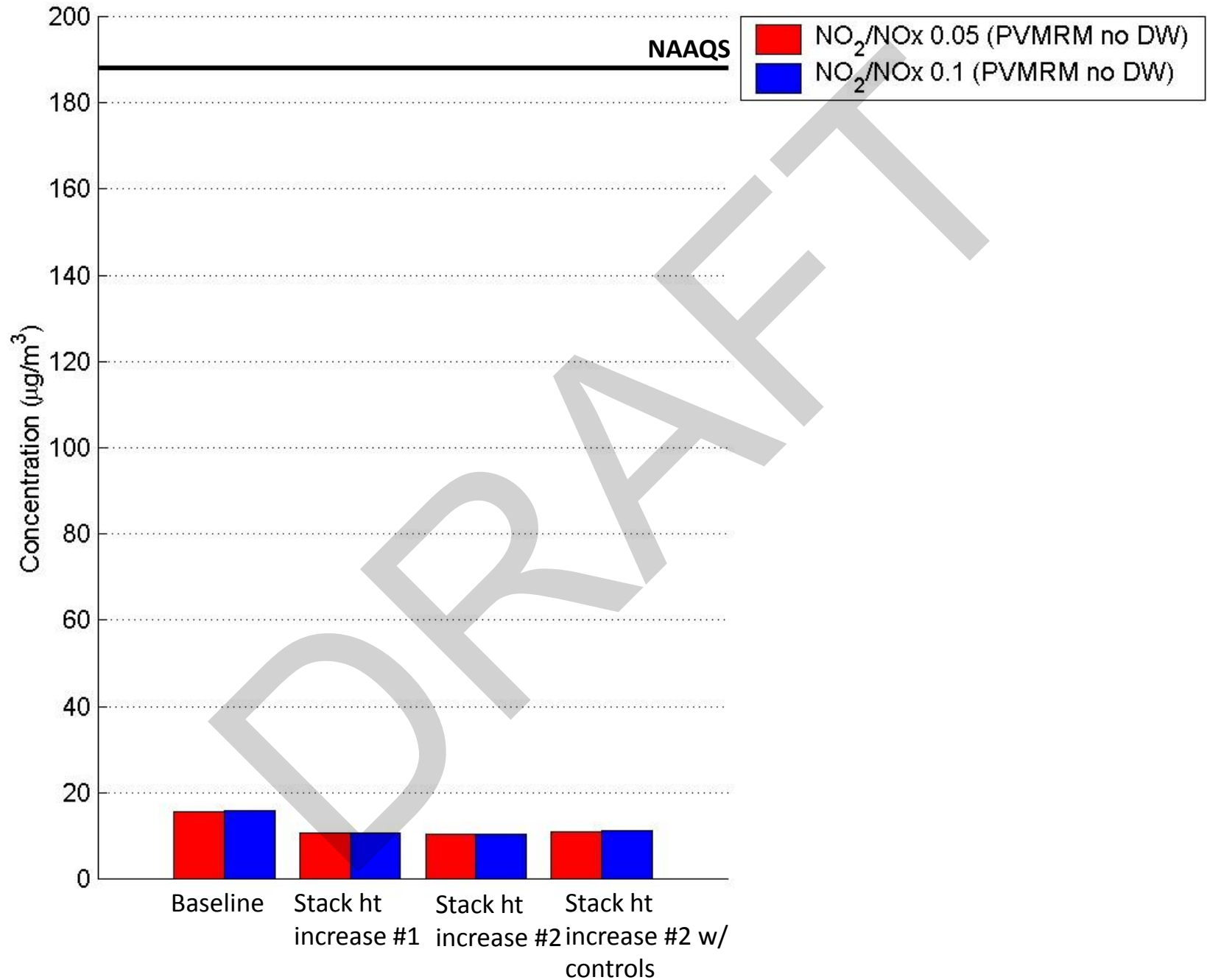
**Legend**



0 1,250 2,500 5,000 7,500 10,000 Meters

Poughkeepsie

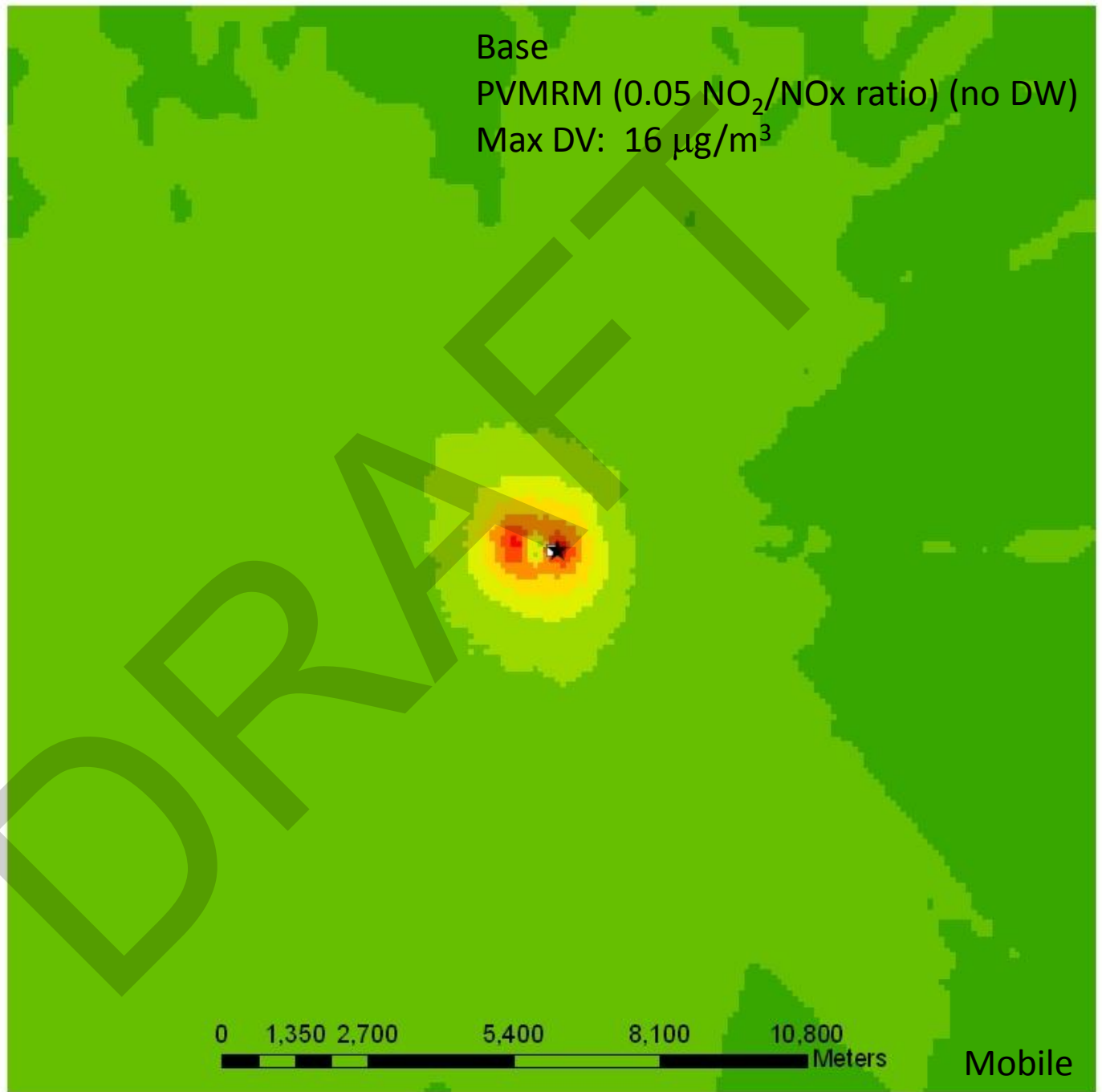
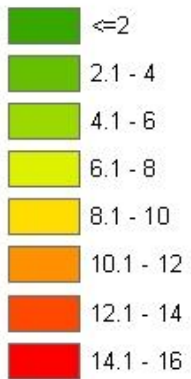
# Natural Gas Turbine (Mobile): NO<sub>2</sub>





Base  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 16 μg/m<sup>3</sup>

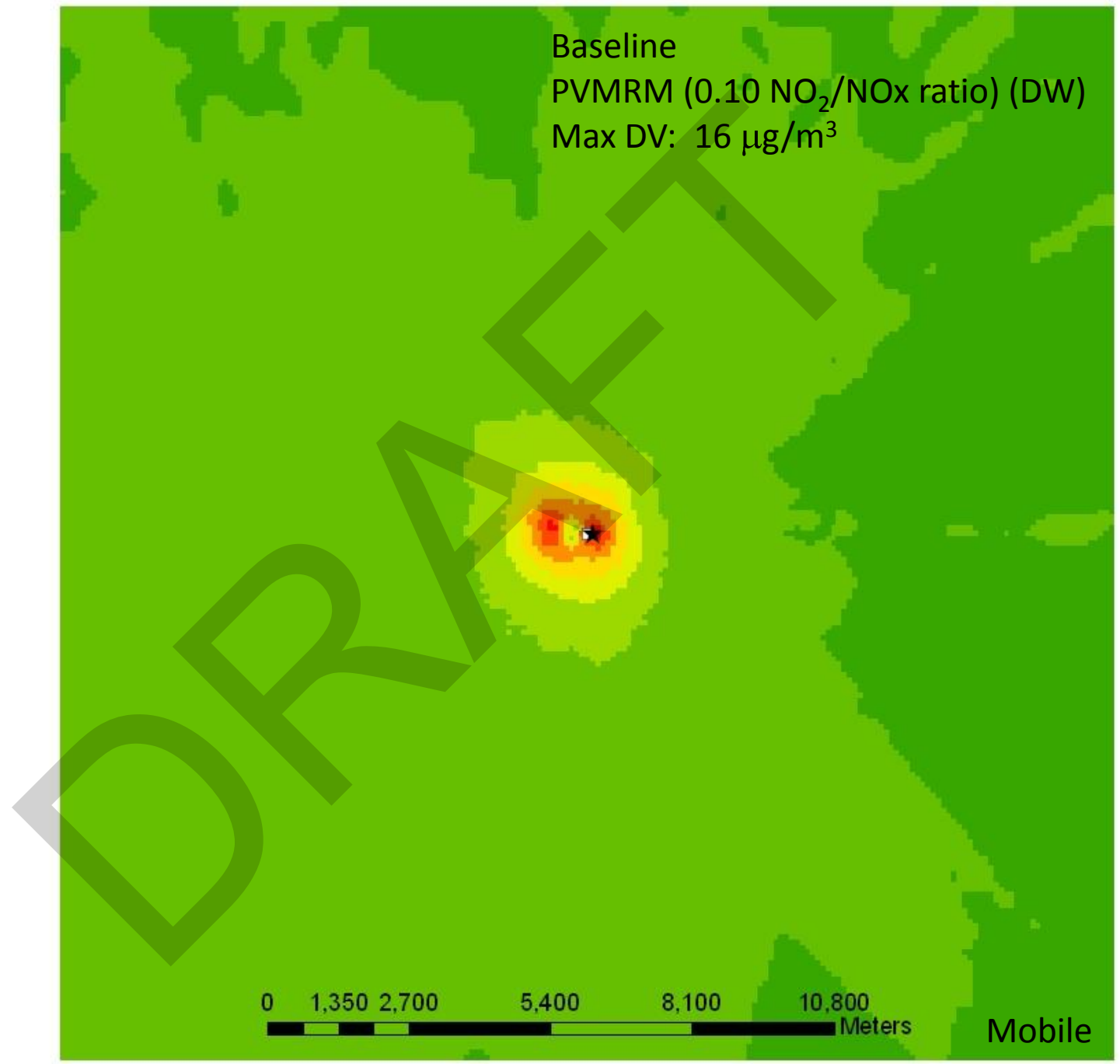
**Legend**



Mobile

Baseline  
PVMRM (0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 16 μg/m<sup>3</sup>

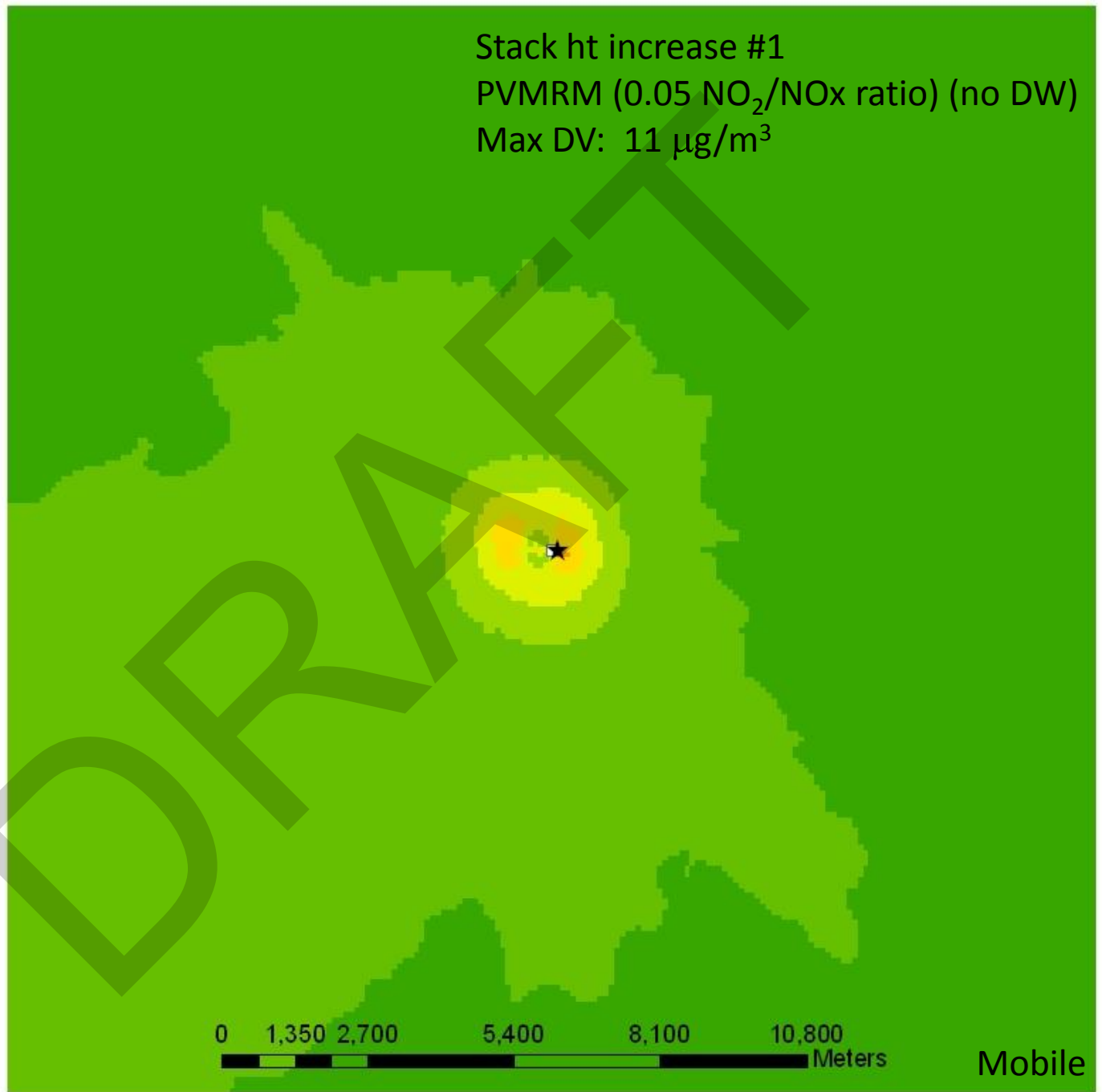
**Legend**



Mobile

Stack ht increase #1  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 11 μg/m<sup>3</sup>

**Legend**

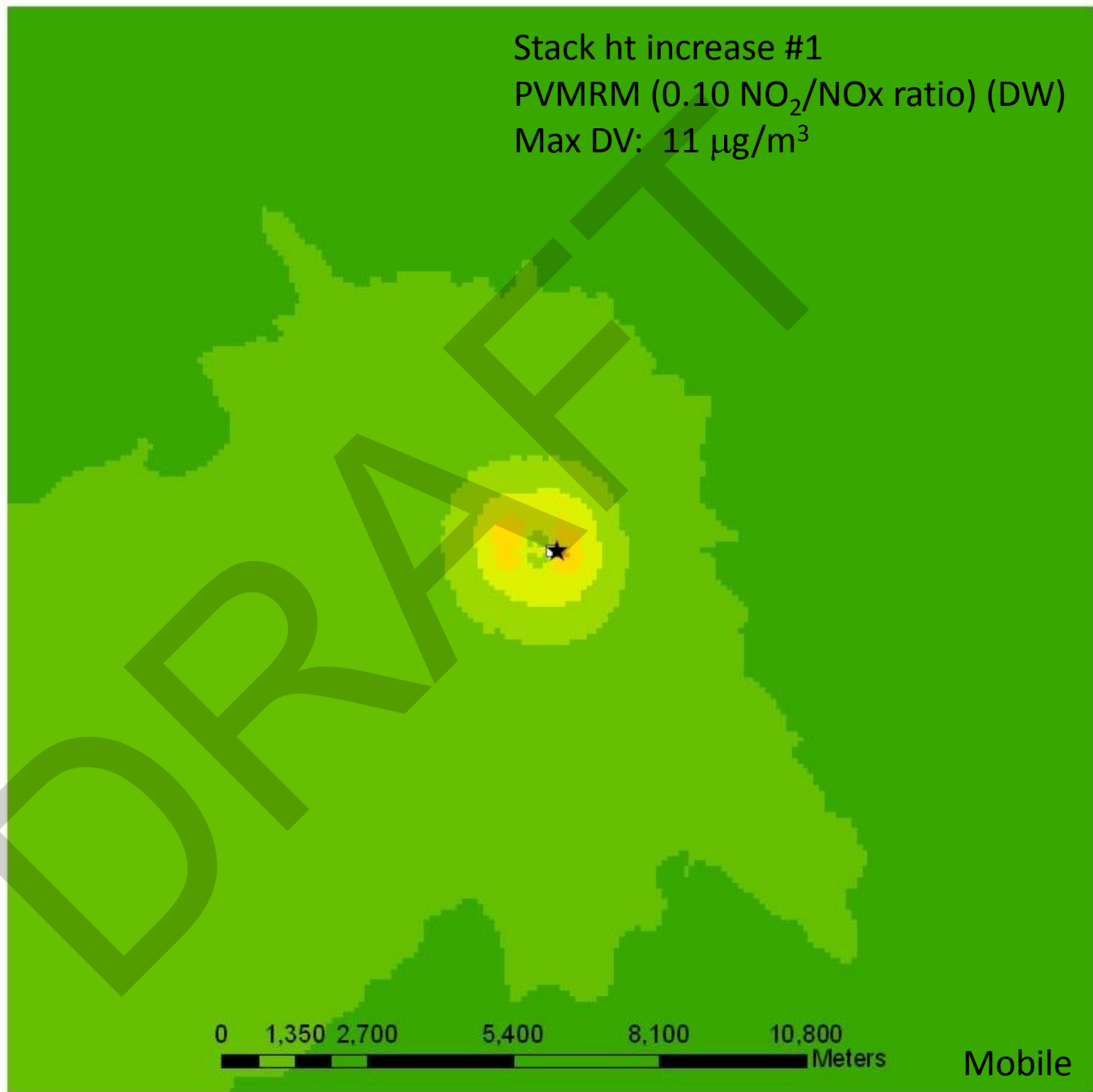
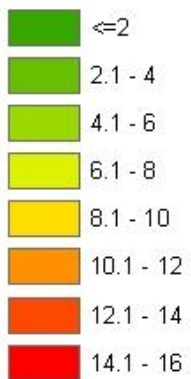


0 1,350 2,700 5,400 8,100 10,800  
Meters

Mobile

Stack ht increase #1  
PVMRM (0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 11 μg/m<sup>3</sup>

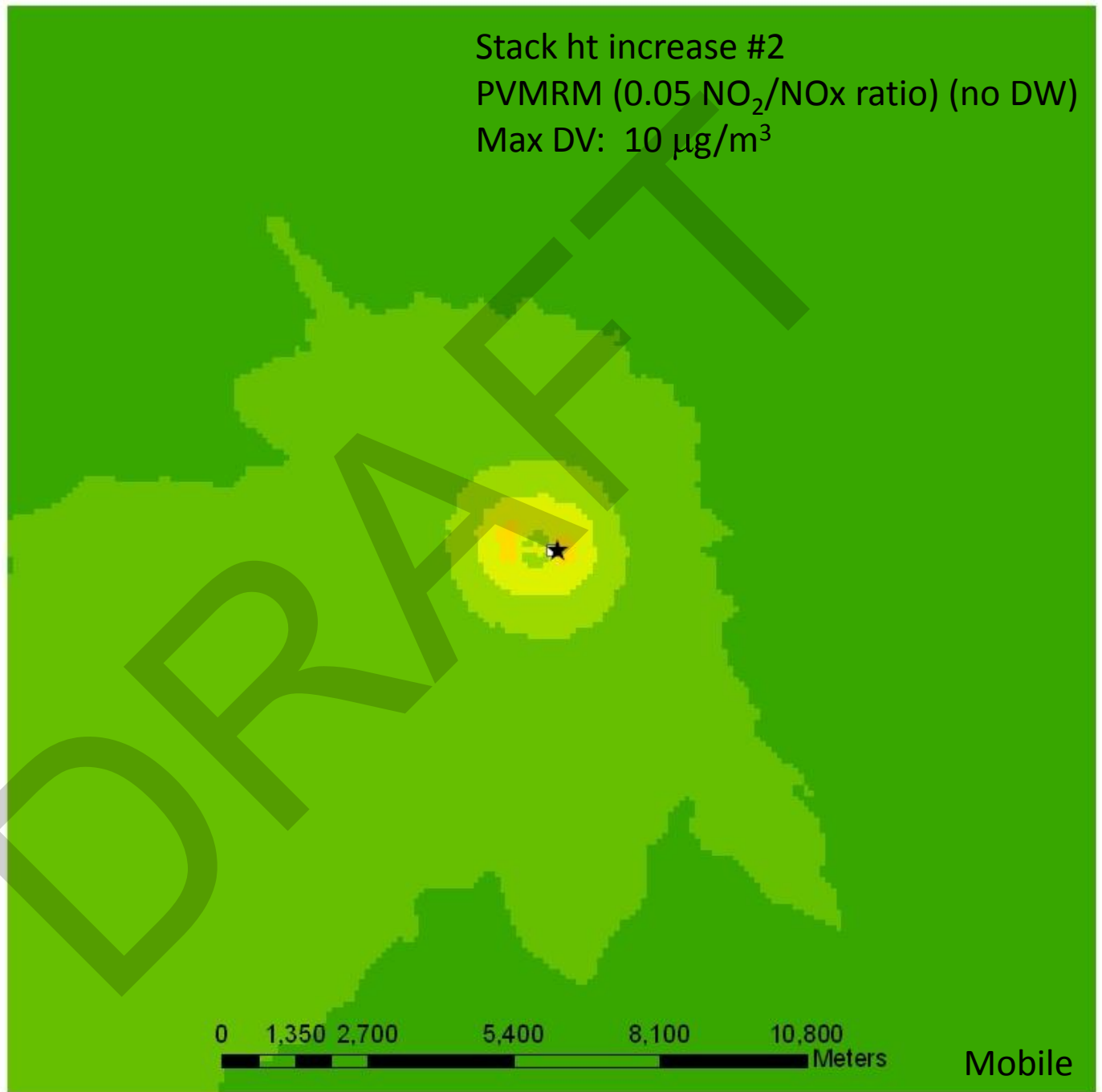
**Legend**



Mobile

Stack ht increase #2  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 10 μg/m<sup>3</sup>

**Legend**

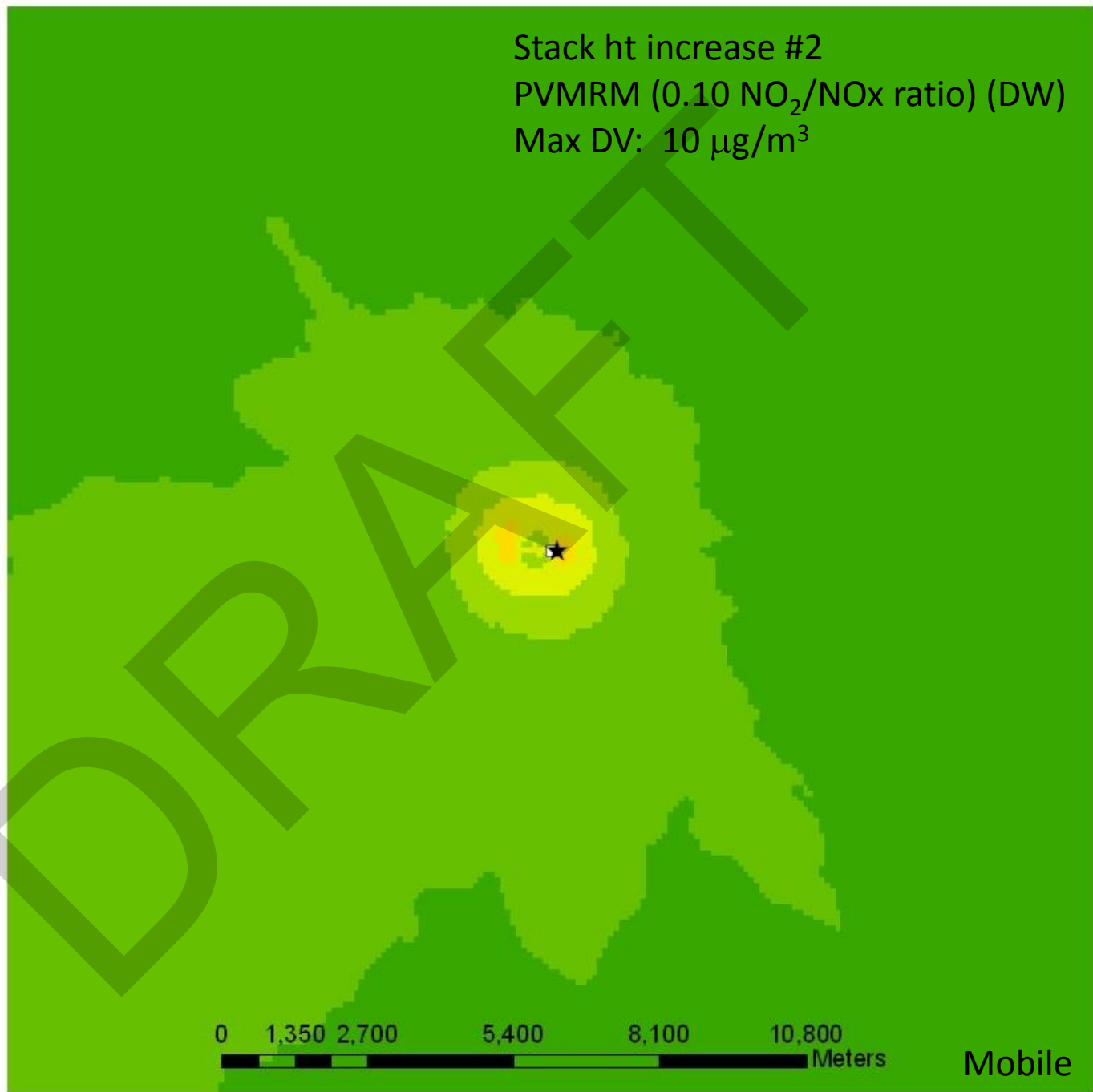
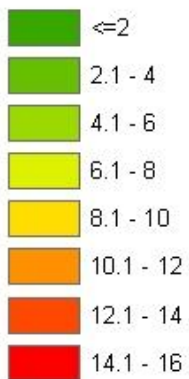


0 1,350 2,700 5,400 8,100 10,800  
Meters

Mobile

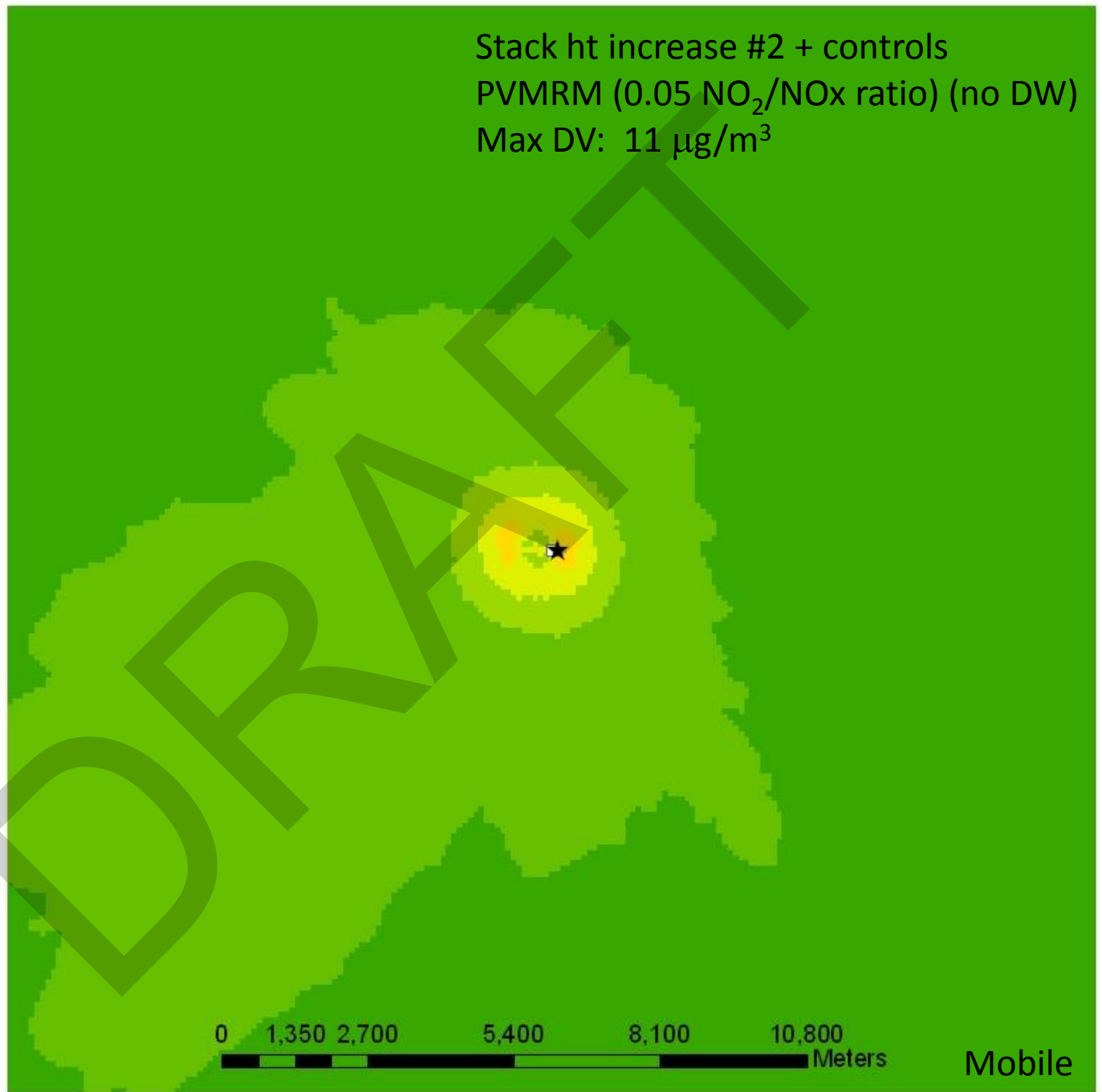
Stack ht increase #2  
PVMRM (0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio) (DW)  
Max DV: 10 μg/m<sup>3</sup>

**Legend**



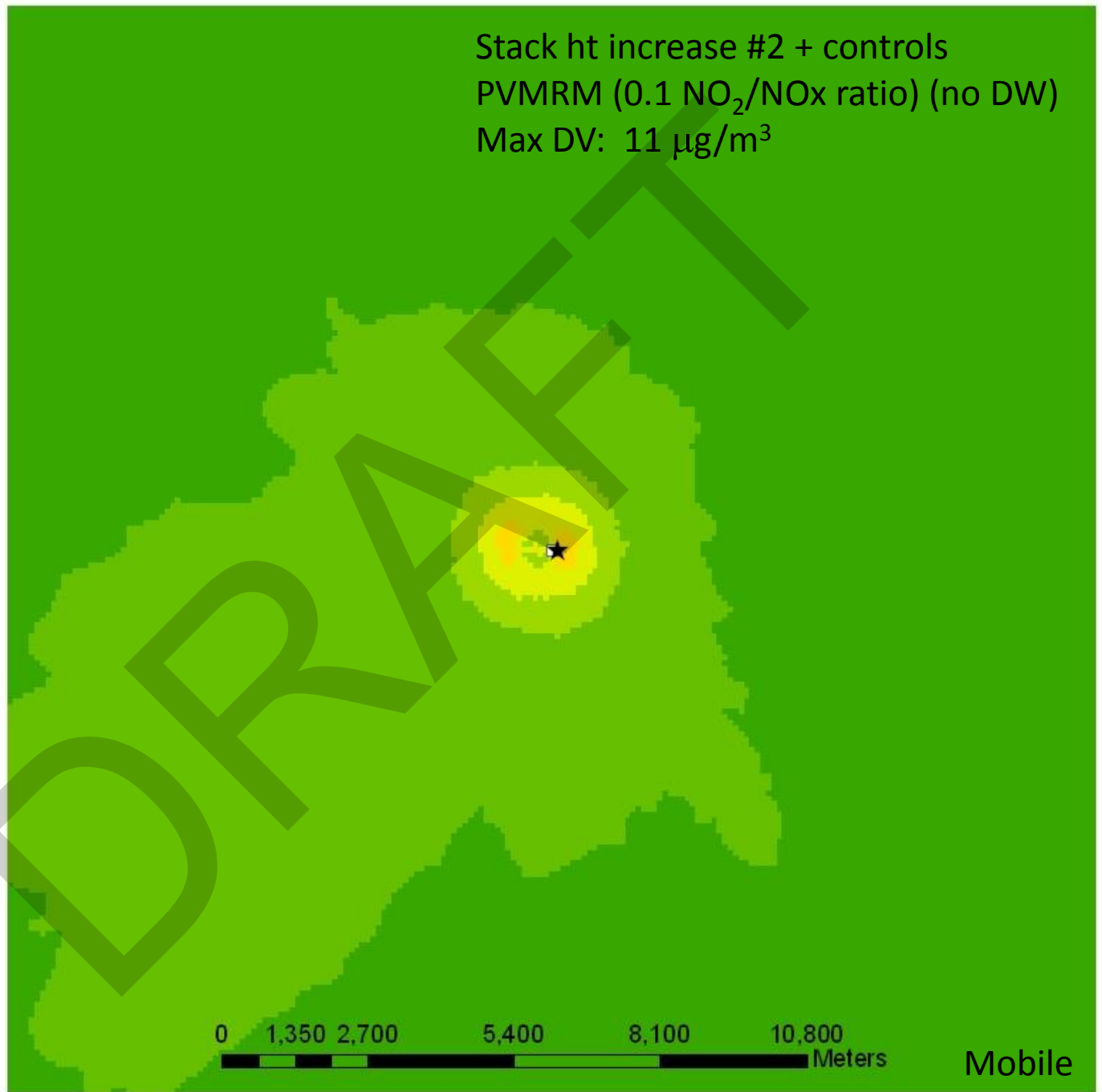
Stack ht increase #2 + controls  
PVMRM (0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 11 μg/m<sup>3</sup>

**Legend**



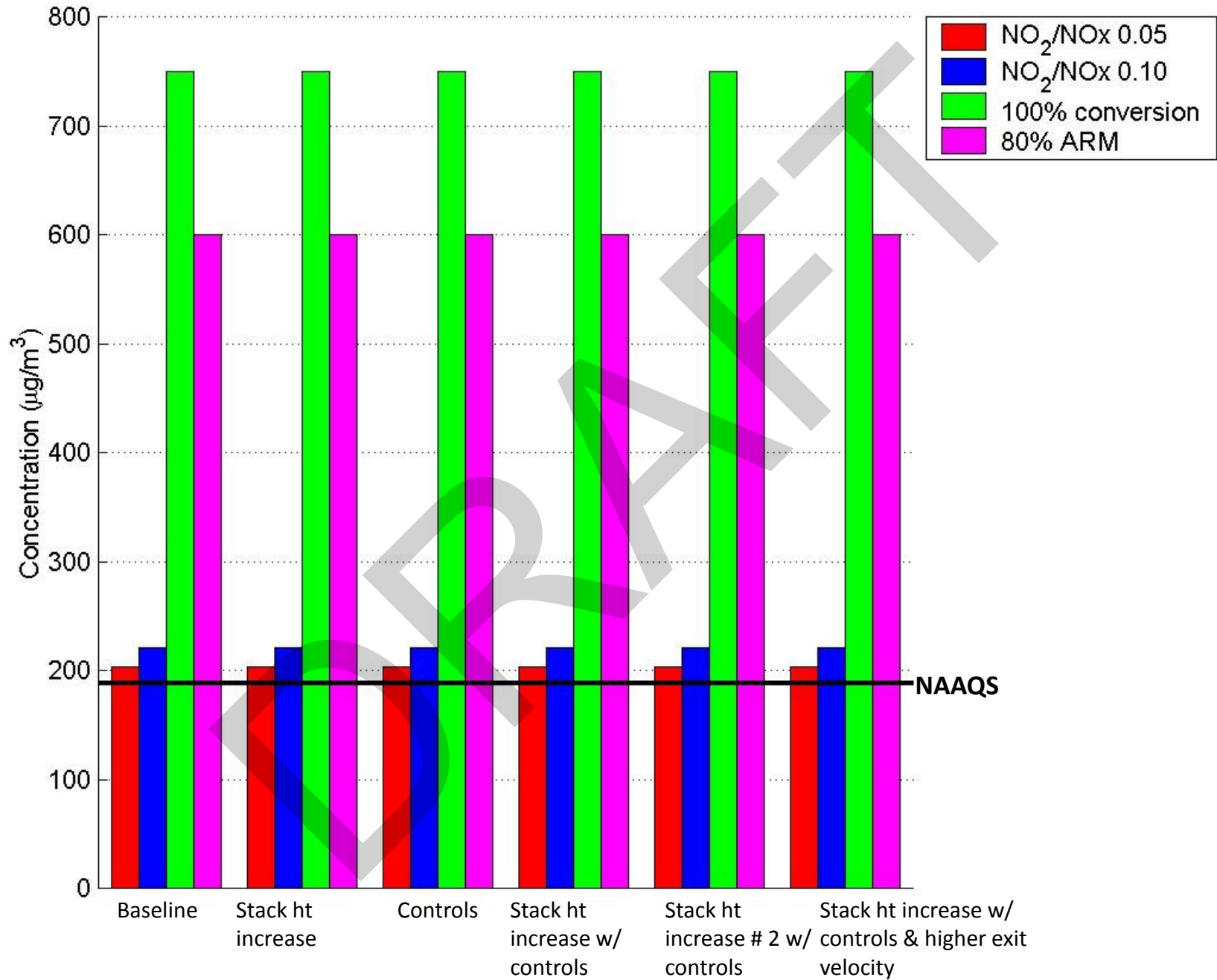
Stack ht increase #2 + controls  
PVMRM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio) (no DW)  
Max DV: 11 μg/m<sup>3</sup>

**Legend**

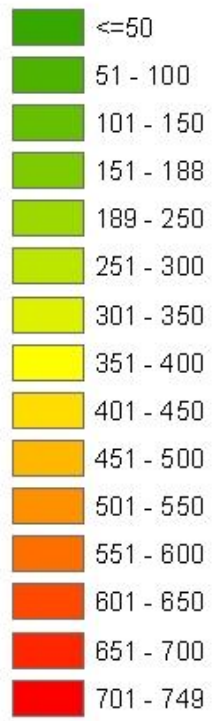




# Coal EGU (OAQPS): NO<sub>2</sub>



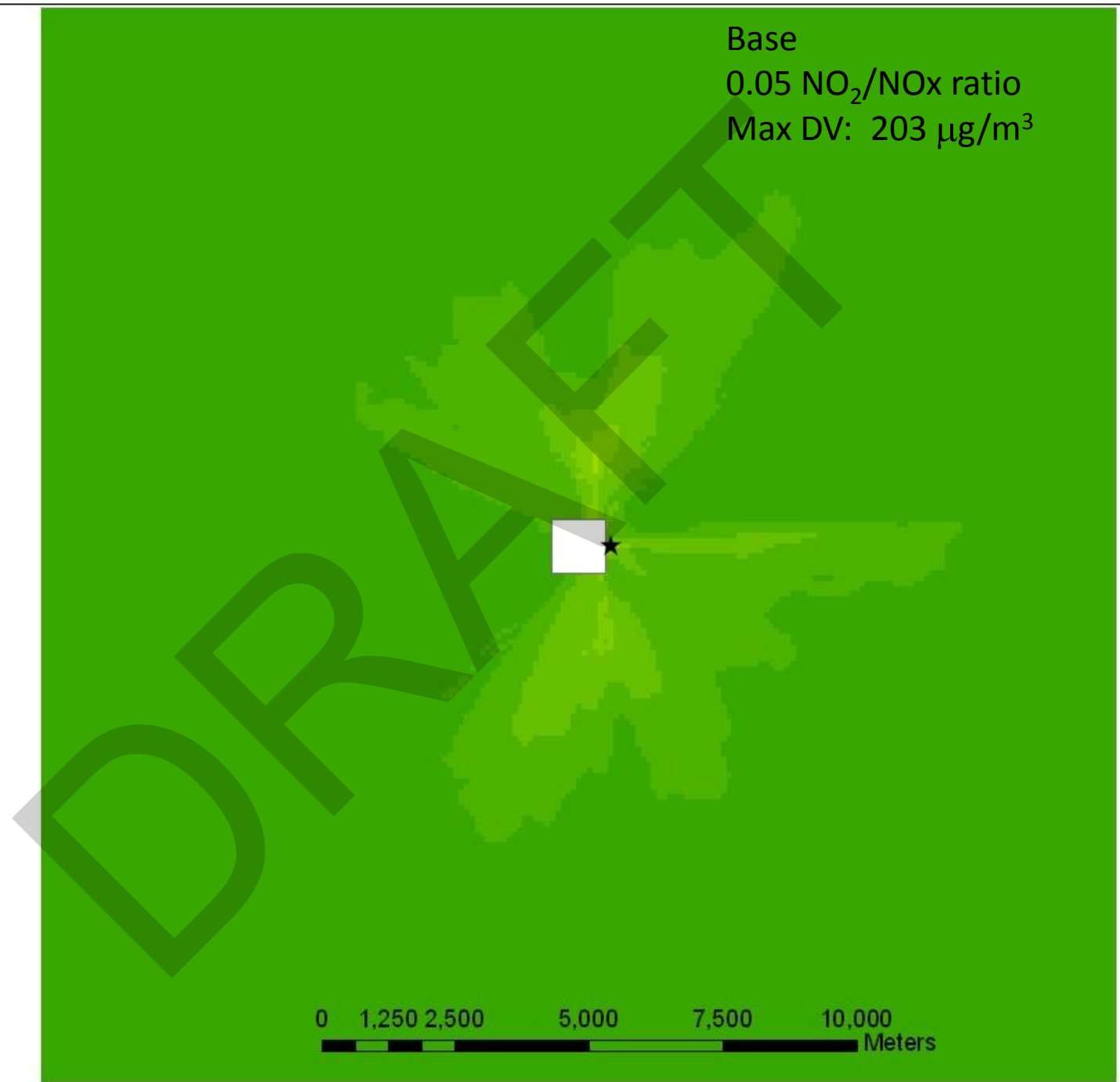
### Legend



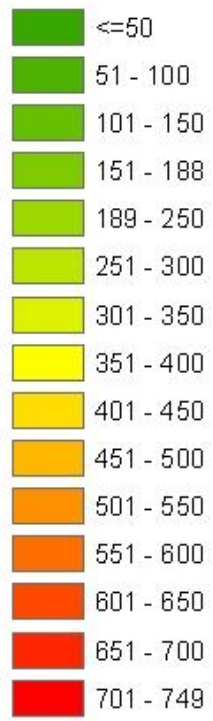
Base

0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 203 μg/m<sup>3</sup>



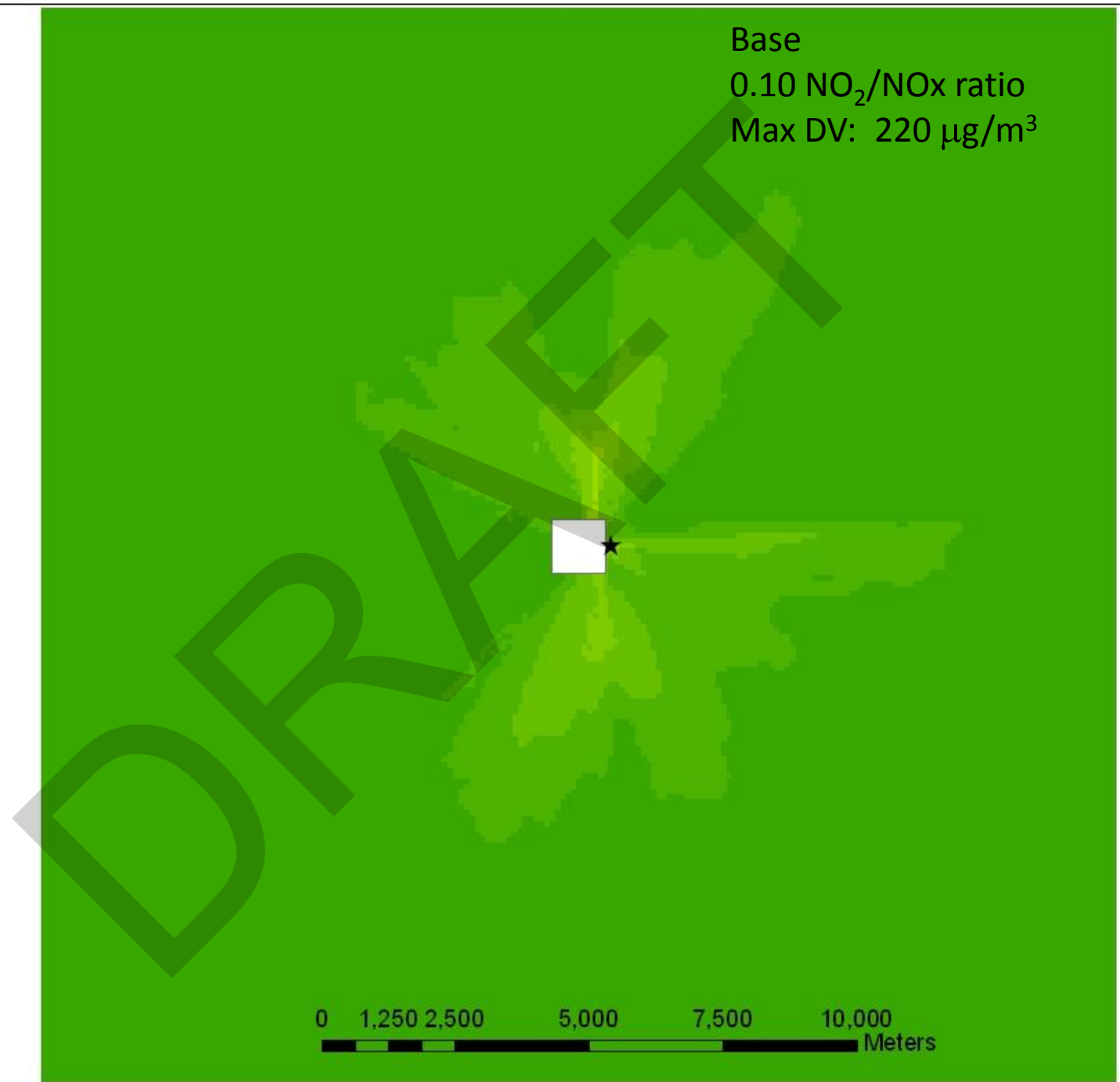
### Legend



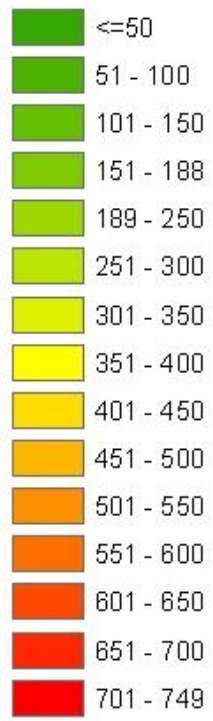
Base

0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio

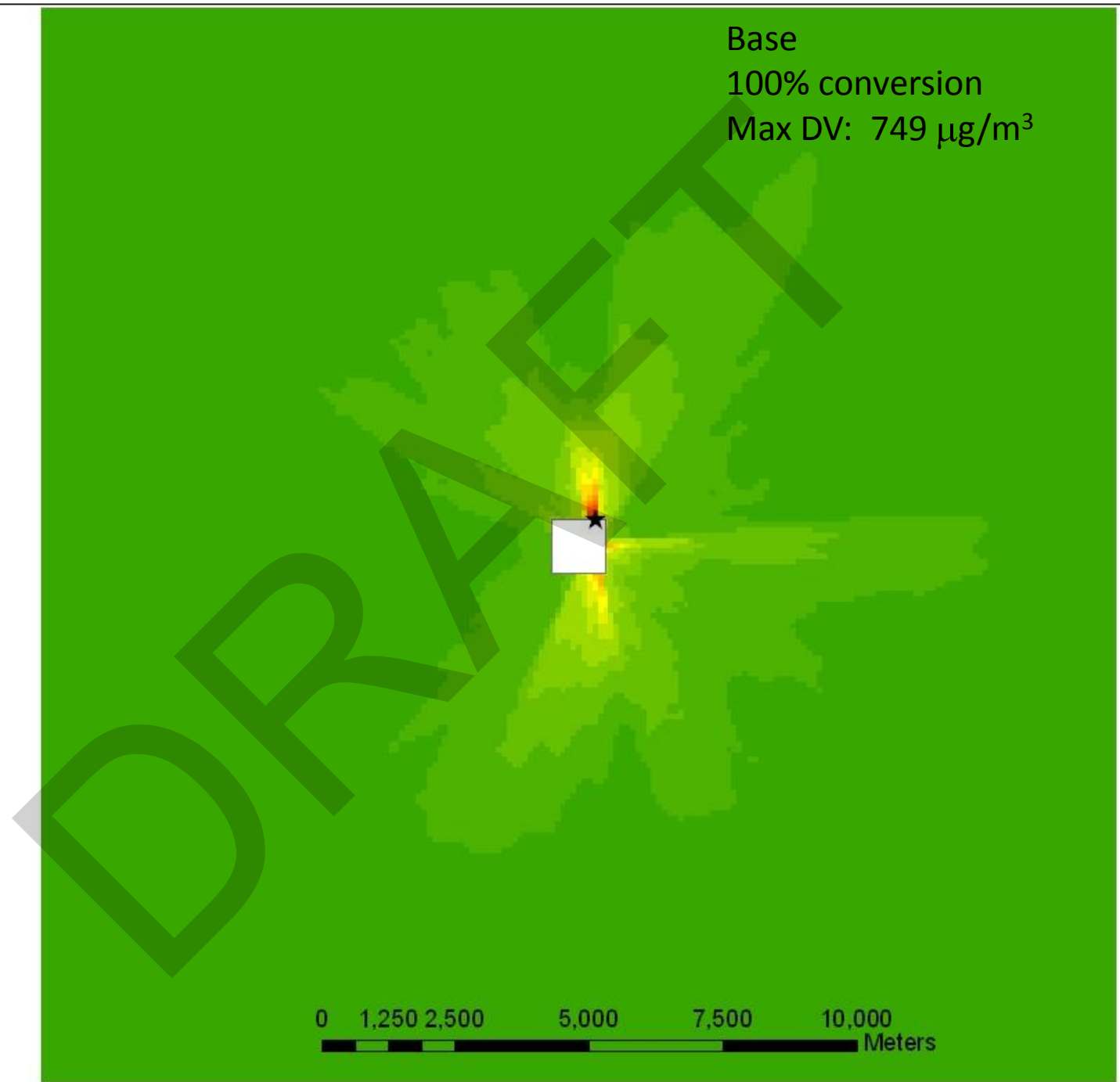
Max DV: 220 μg/m<sup>3</sup>



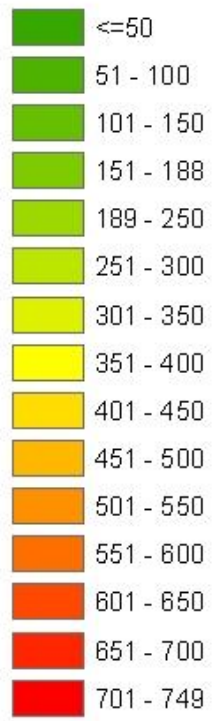
### Legend



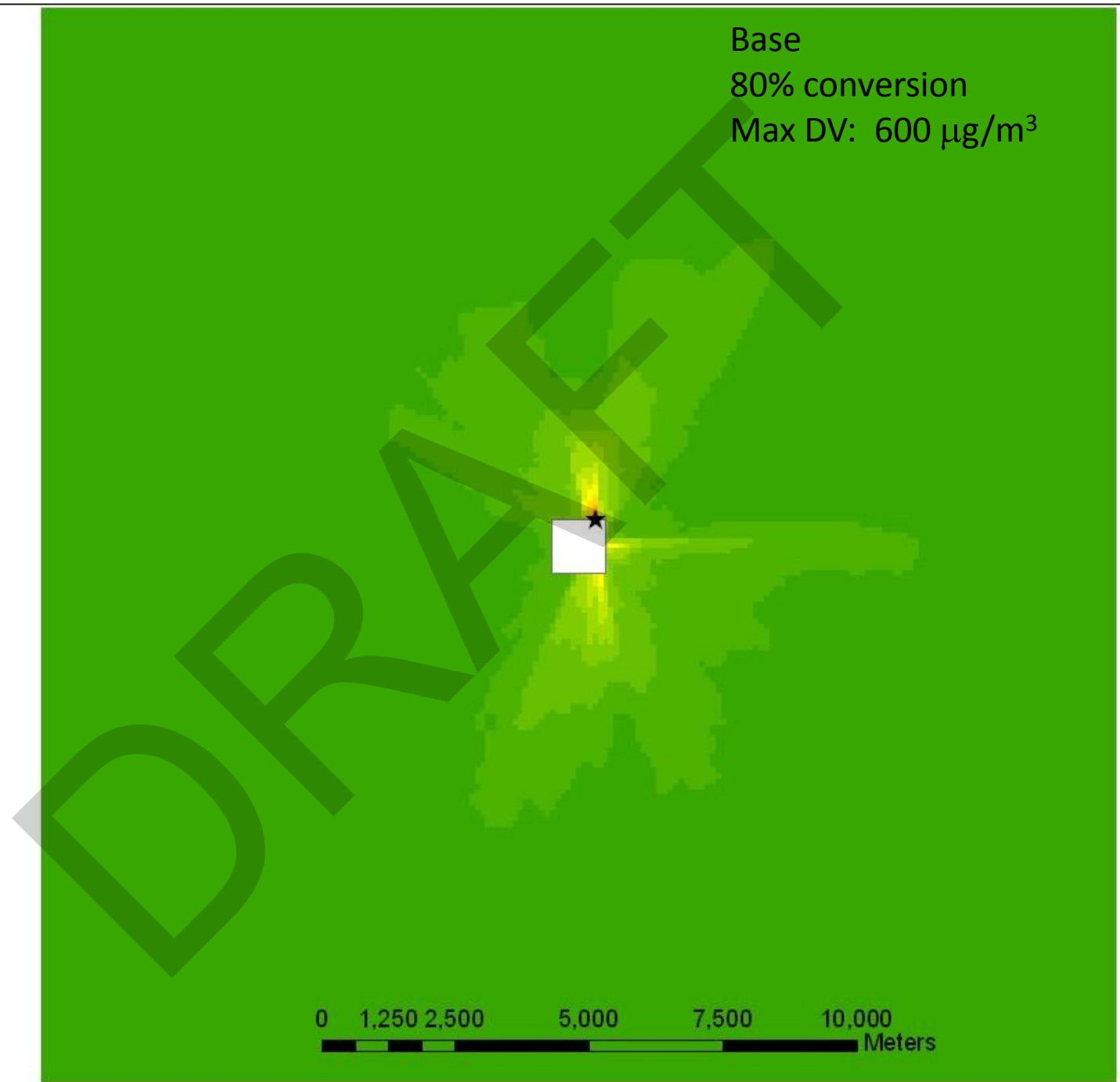
Base  
100% conversion  
Max DV: 749  $\mu\text{g}/\text{m}^3$



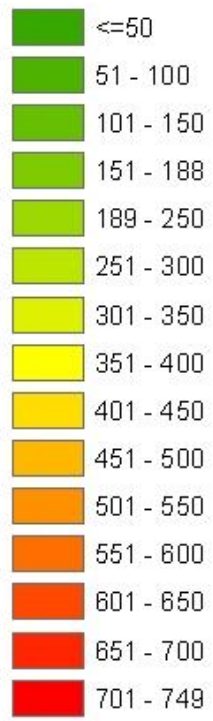
### Legend



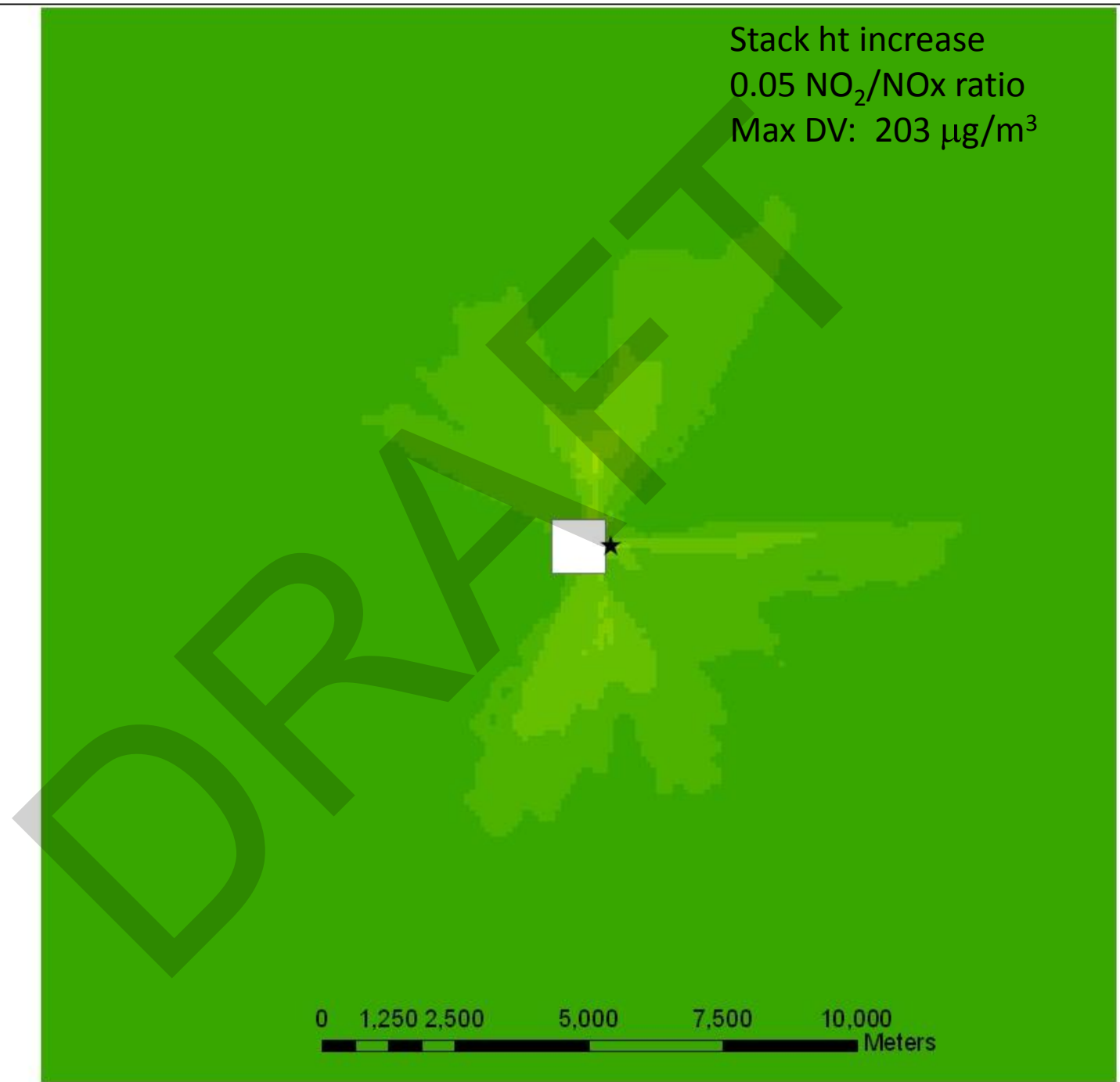
Base  
80% conversion  
Max DV: 600  $\mu\text{g}/\text{m}^3$



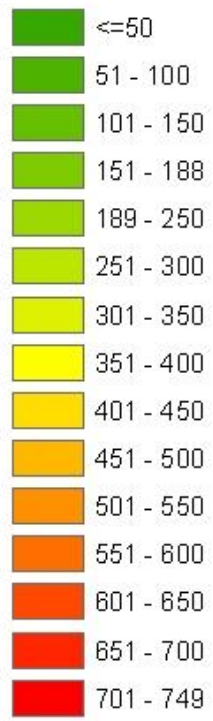
**Legend**



Stack ht increase  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 203 μg/m<sup>3</sup>



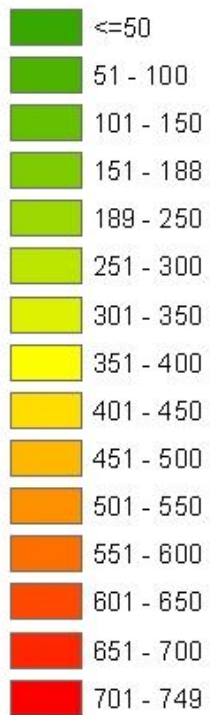
### Legend



Stack ht increase  
0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 220 μg/m<sup>3</sup>



### Legend



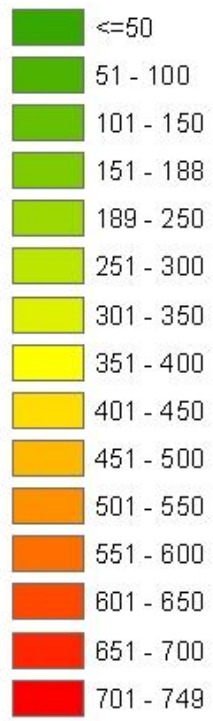
Stack ht increase  
100% conversion  
Max DV: 749  $\mu\text{g}/\text{m}^3$



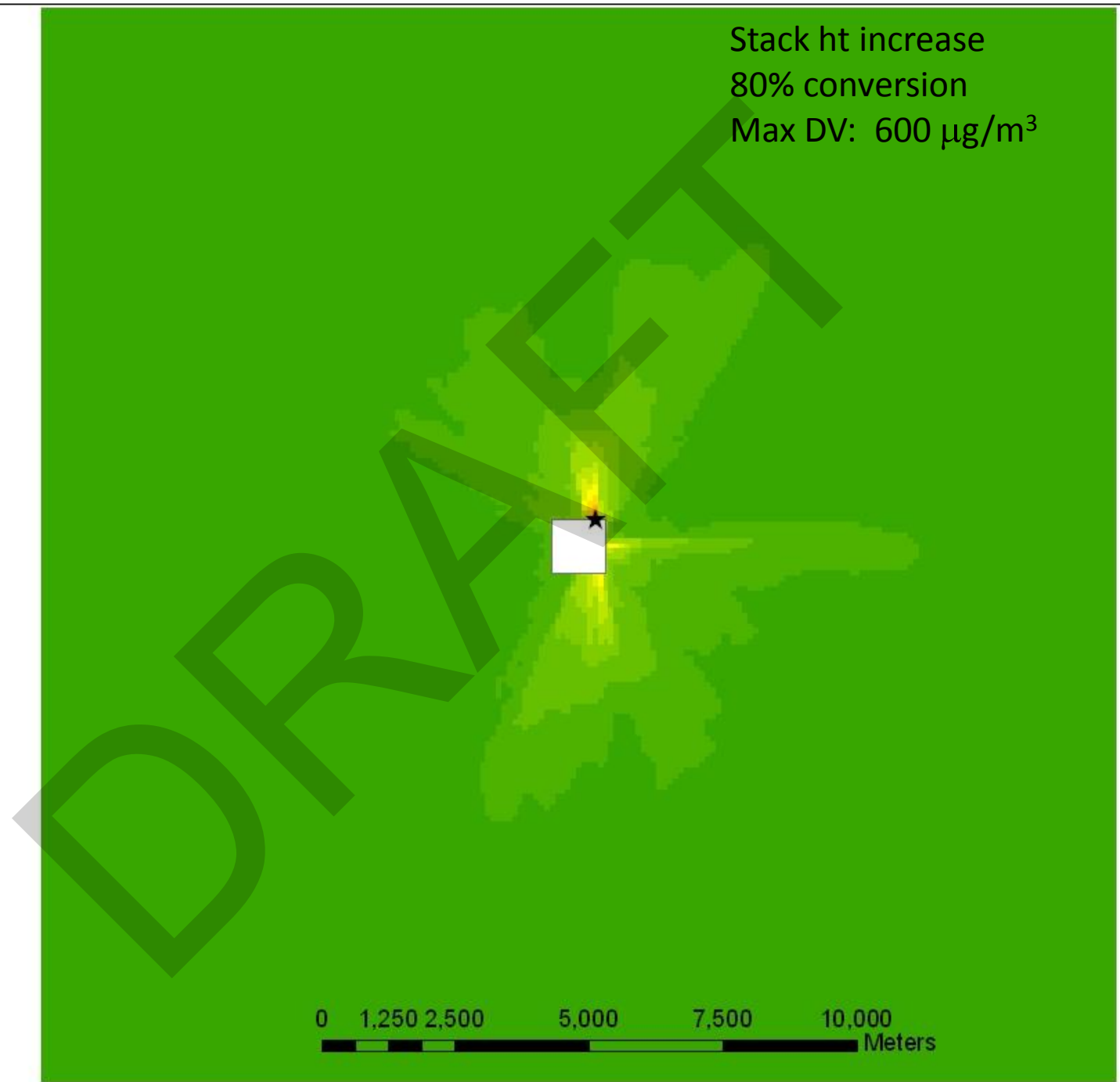
0 1,250 2,500 5,000 7,500 10,000  
Meters



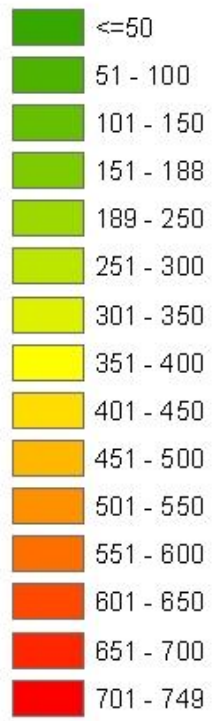
### Legend



Stack ht increase  
80% conversion  
Max DV: 600 µg/m<sup>3</sup>



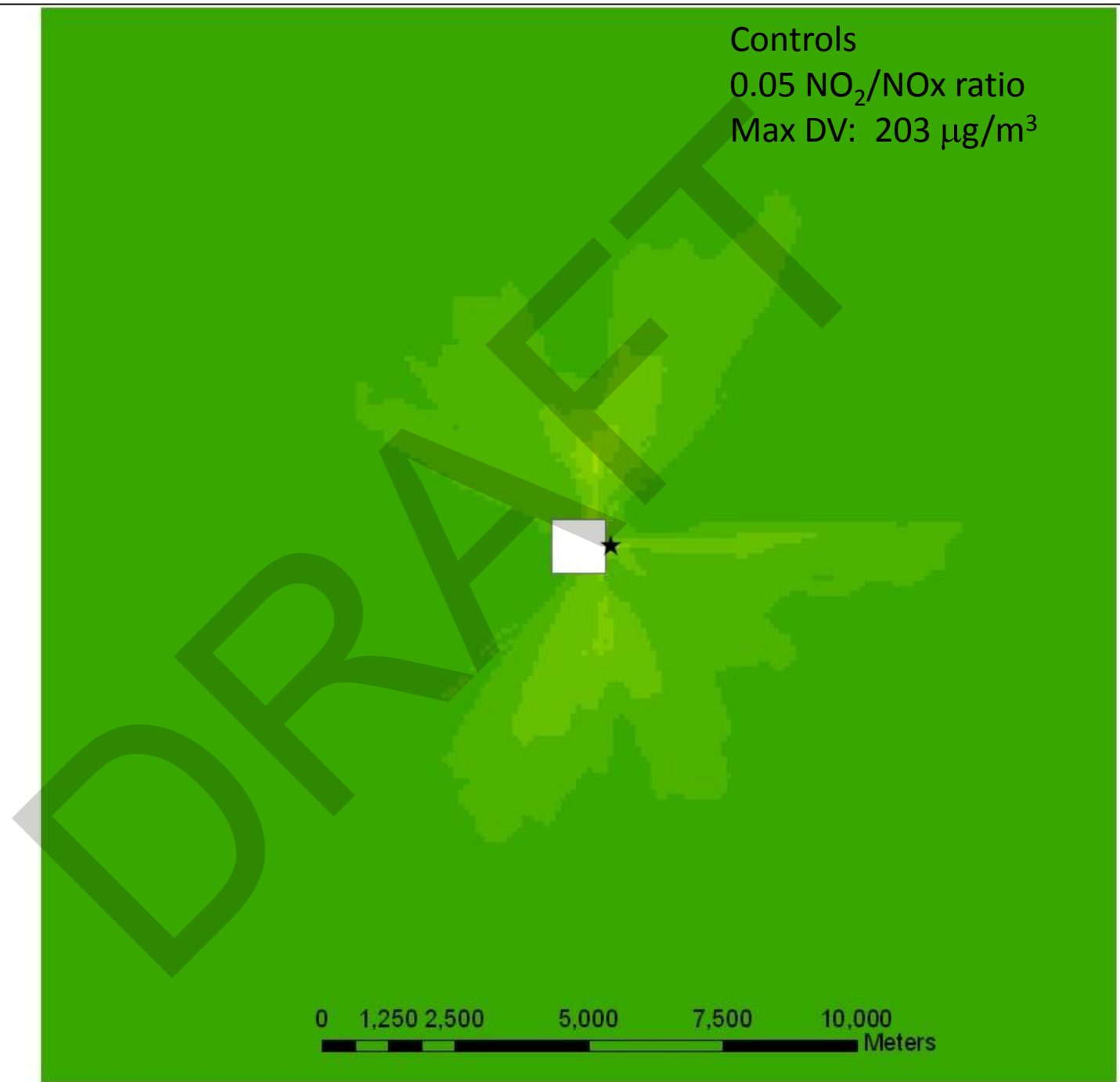
### Legend



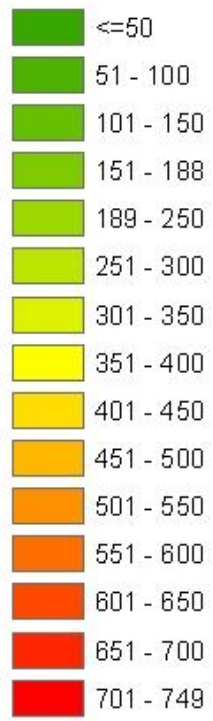
Controls

0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 203 μg/m<sup>3</sup>



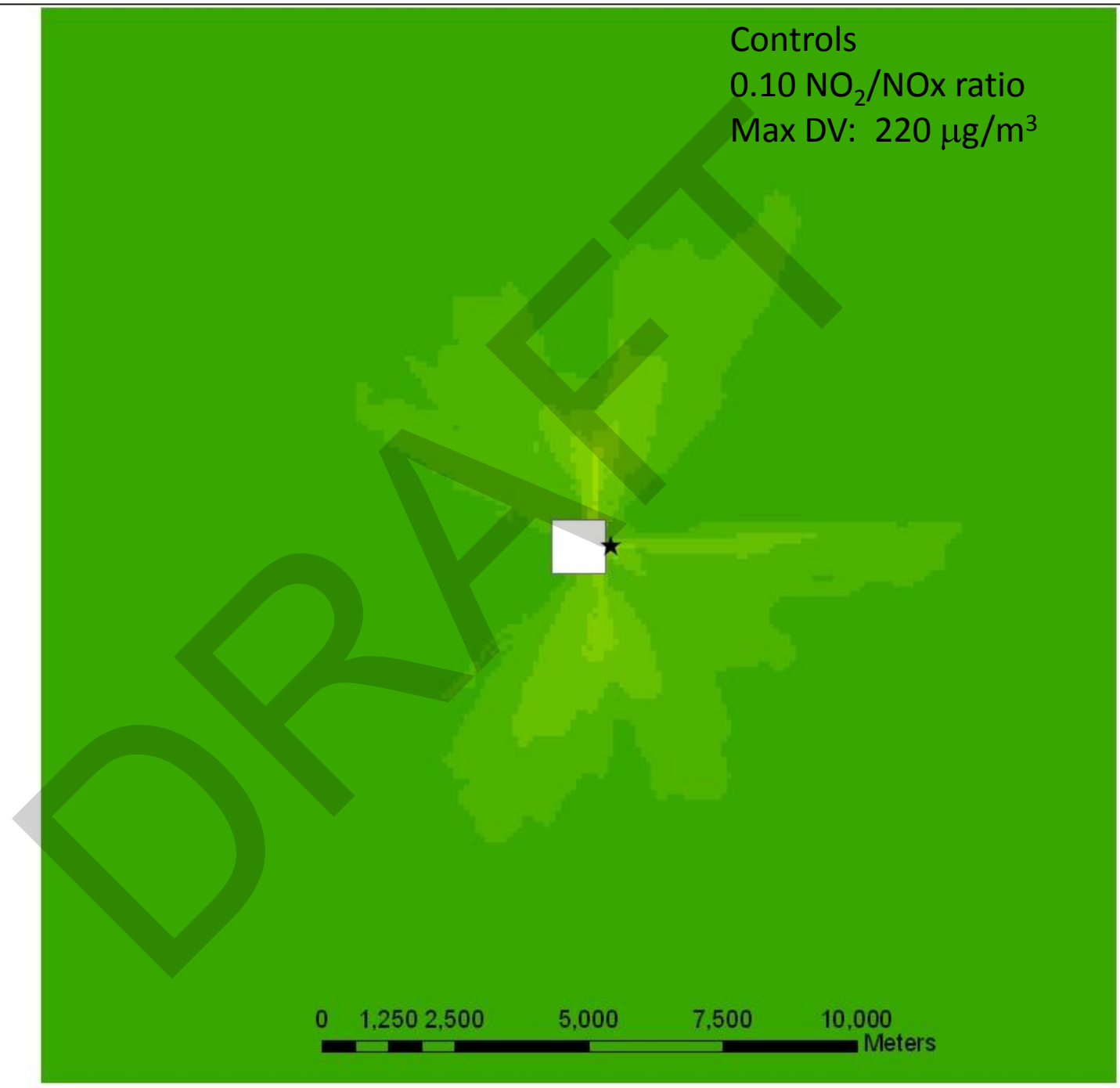
### Legend



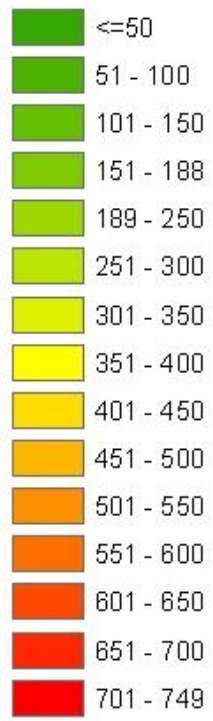
Controls

0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 220 μg/m<sup>3</sup>



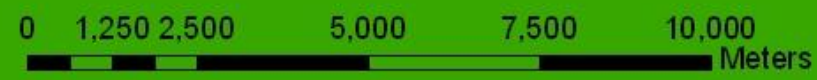
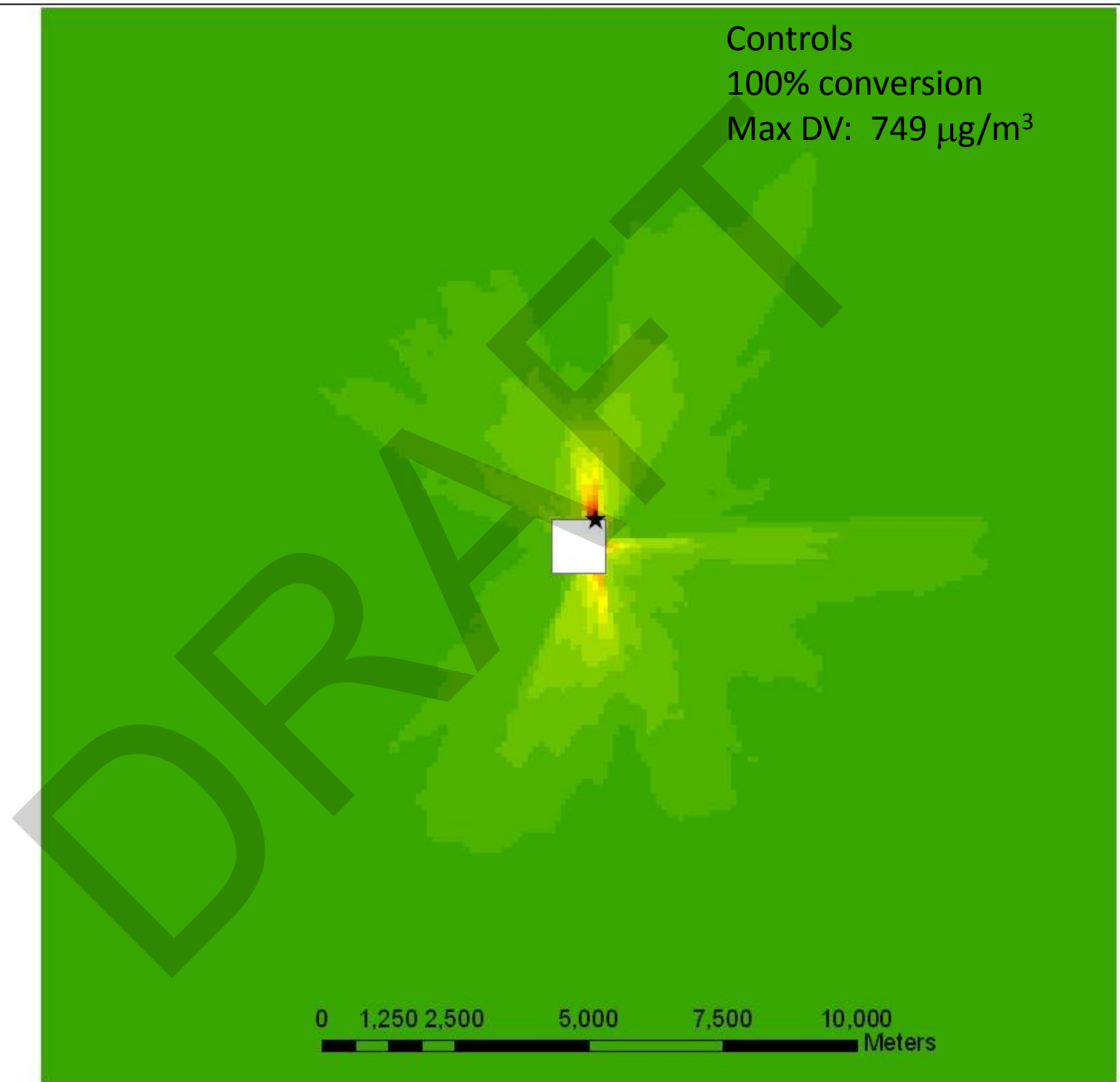
### Legend



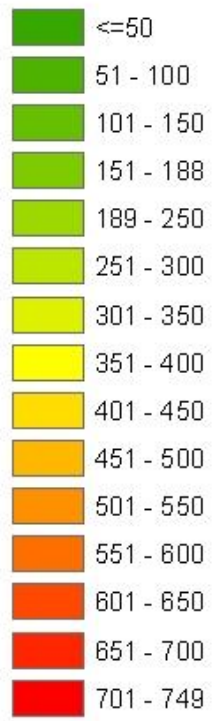
Controls

100% conversion

Max DV: 749  $\mu\text{g}/\text{m}^3$



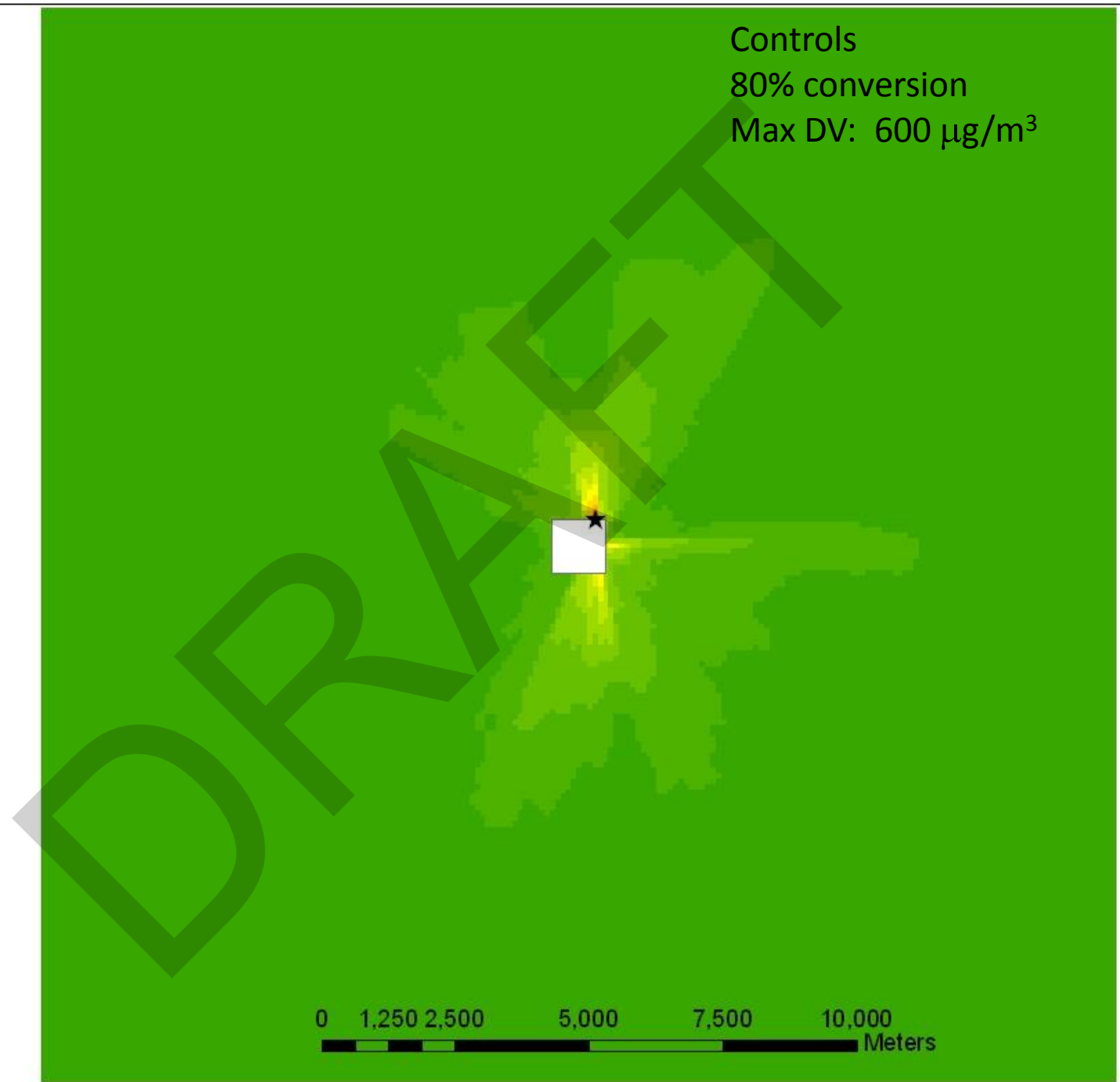
### Legend



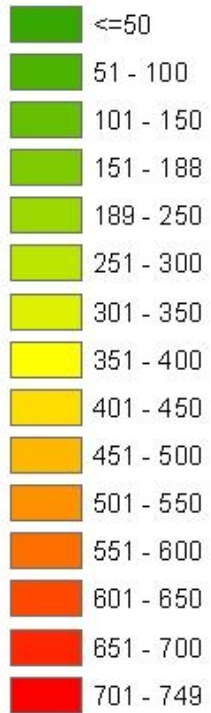
Controls

80% conversion

Max DV: 600  $\mu\text{g}/\text{m}^3$



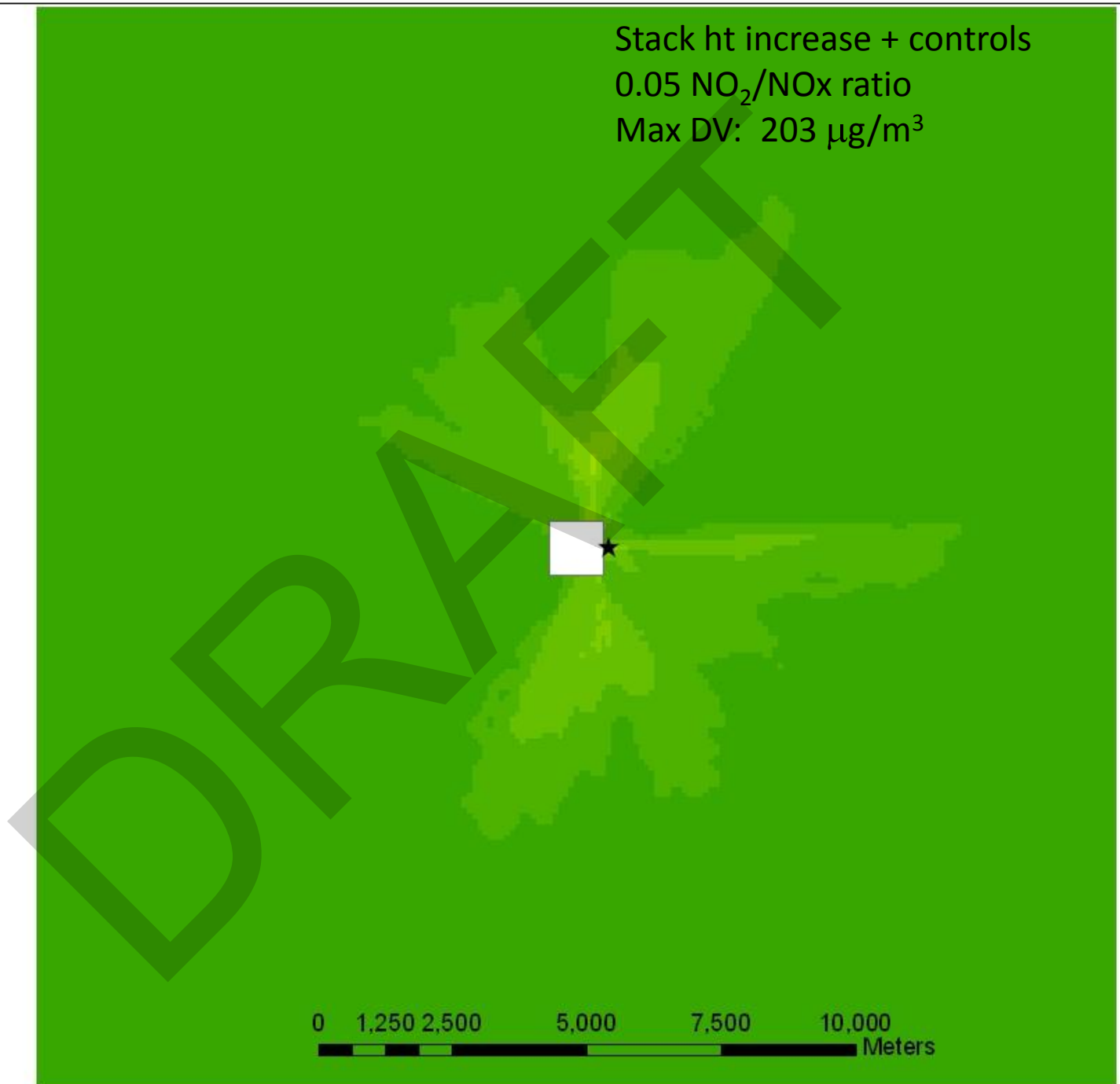
### Legend



Stack ht increase + controls

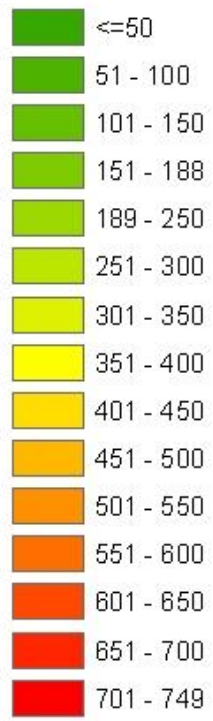
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 203 μg/m<sup>3</sup>



0 1,250 2,500 5,000 7,500 10,000  
Meters

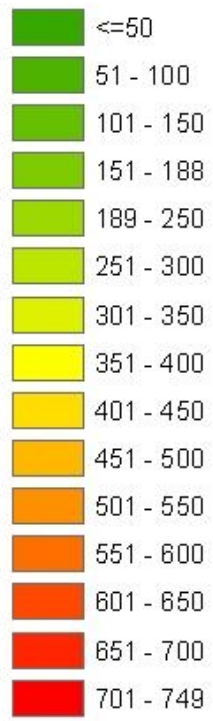
### Legend



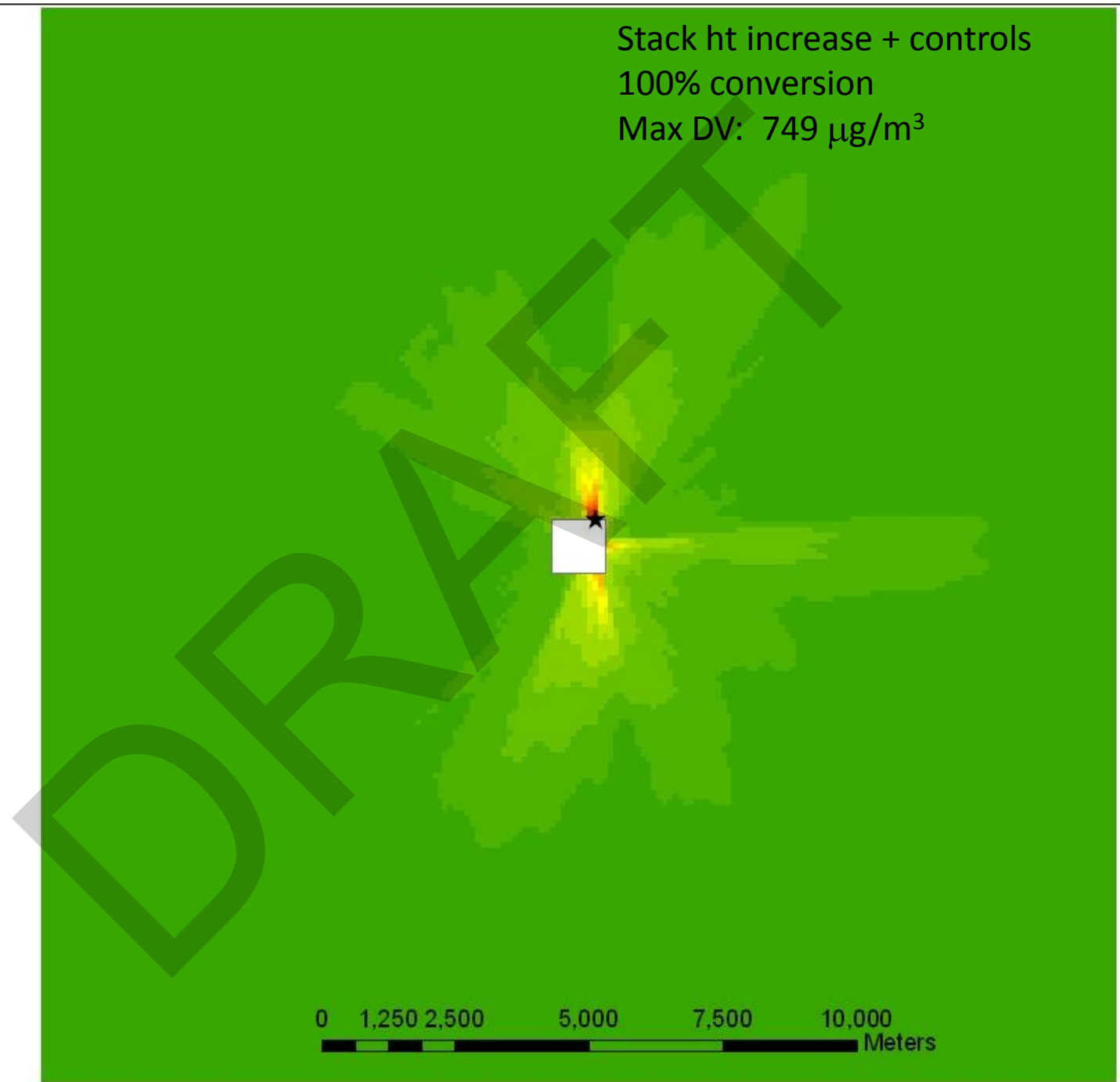
Stack ht increase + controls  
0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 220 μg/m<sup>3</sup>



### Legend

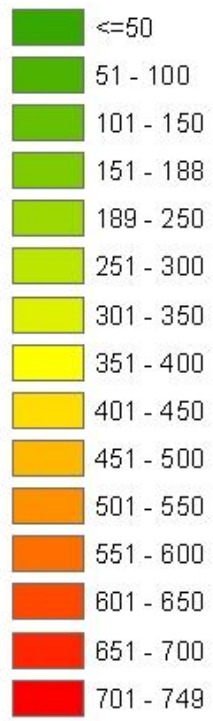


Stack ht increase + controls  
100% conversion  
Max DV: 749  $\mu\text{g}/\text{m}^3$

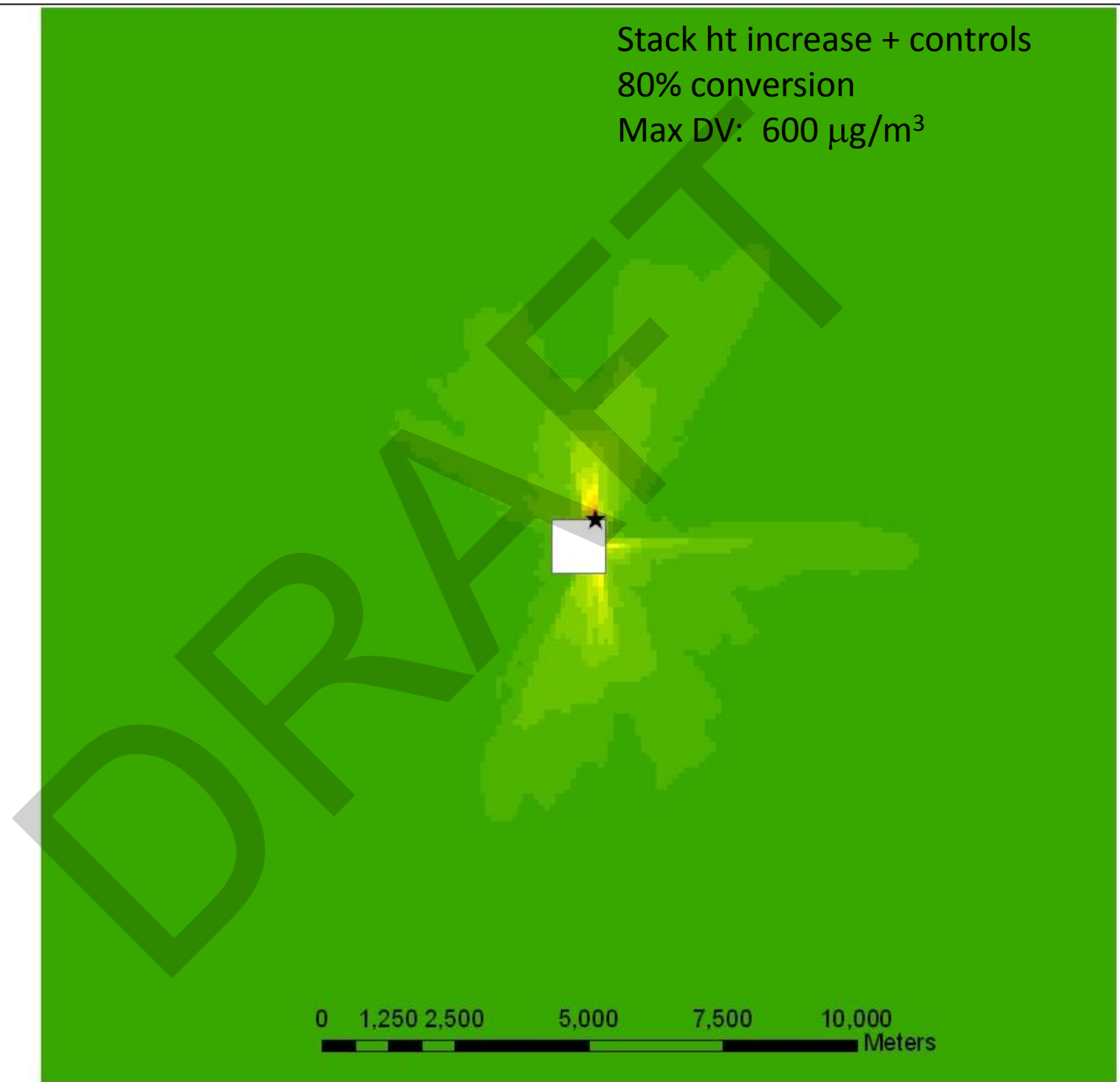




**Legend**



Stack ht increase + controls  
80% conversion  
Max DV: 600  $\mu\text{g}/\text{m}^3$

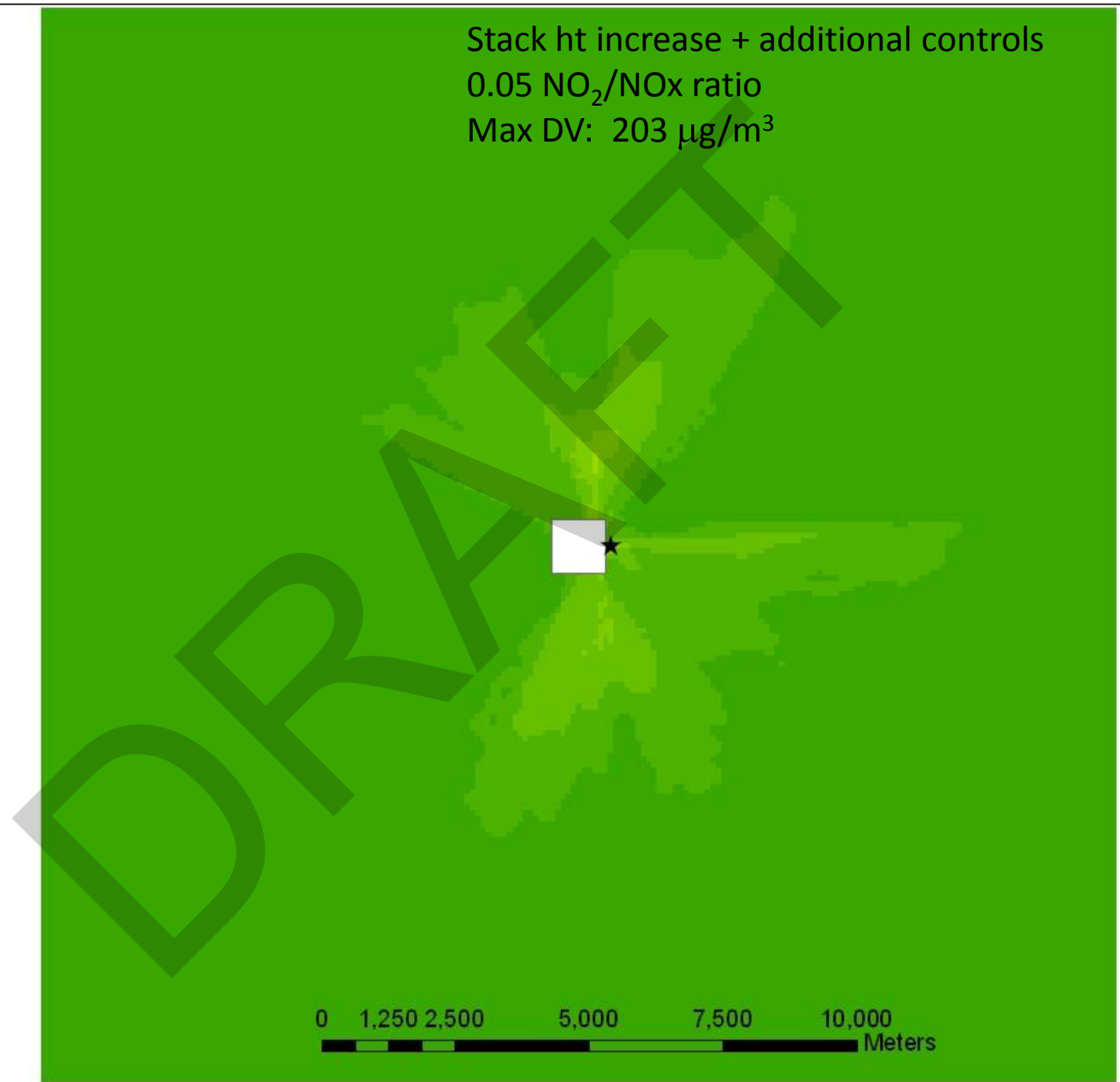


# Stack ht increase + additional controls

0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio

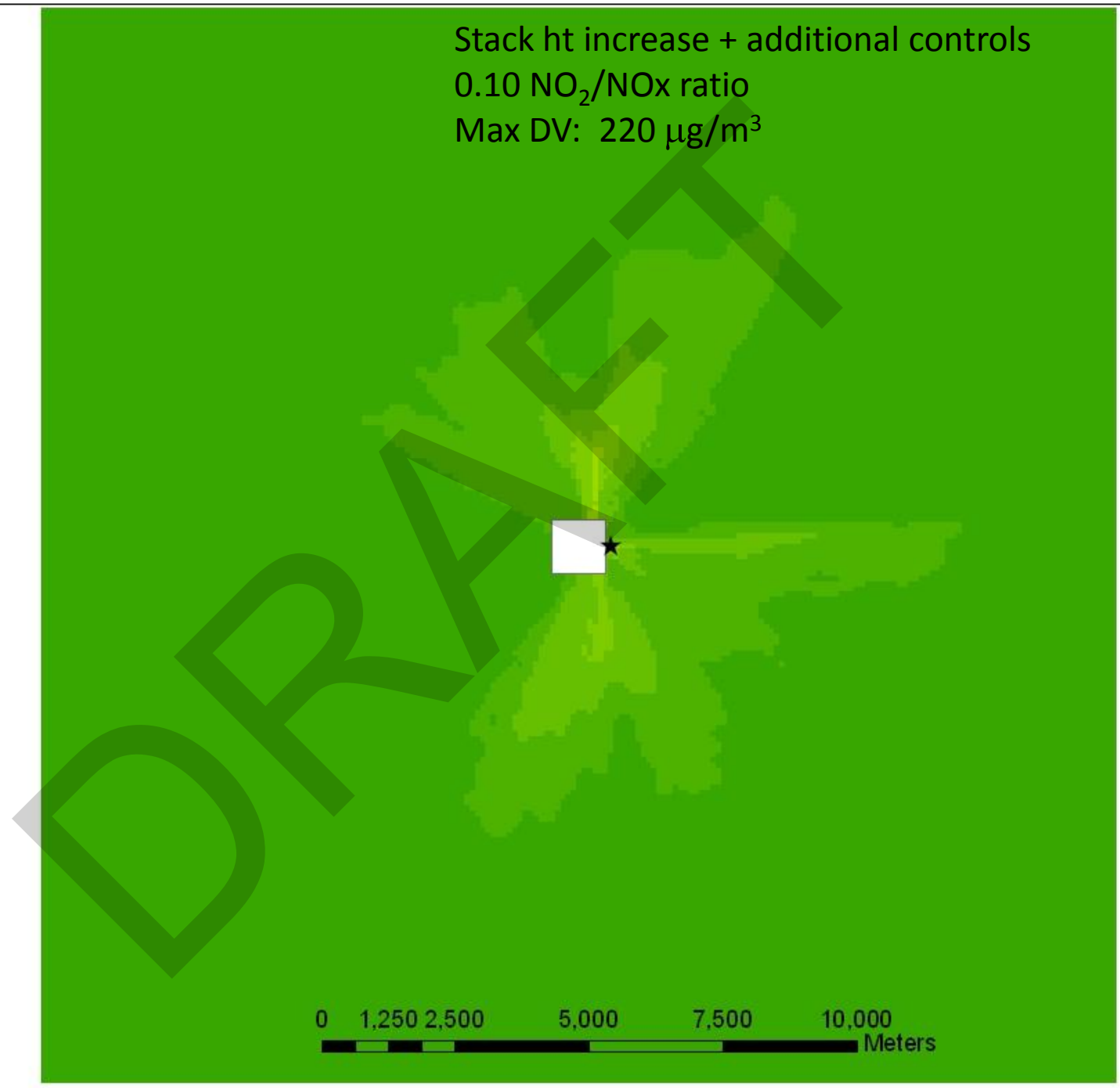
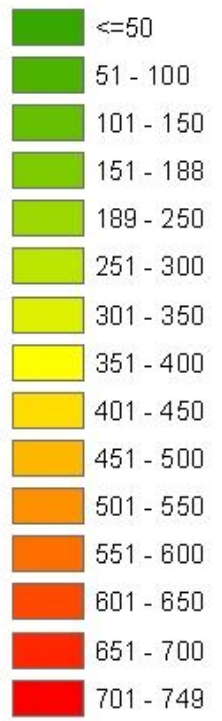
Max DV: 203 μg/m<sup>3</sup>

## Legend



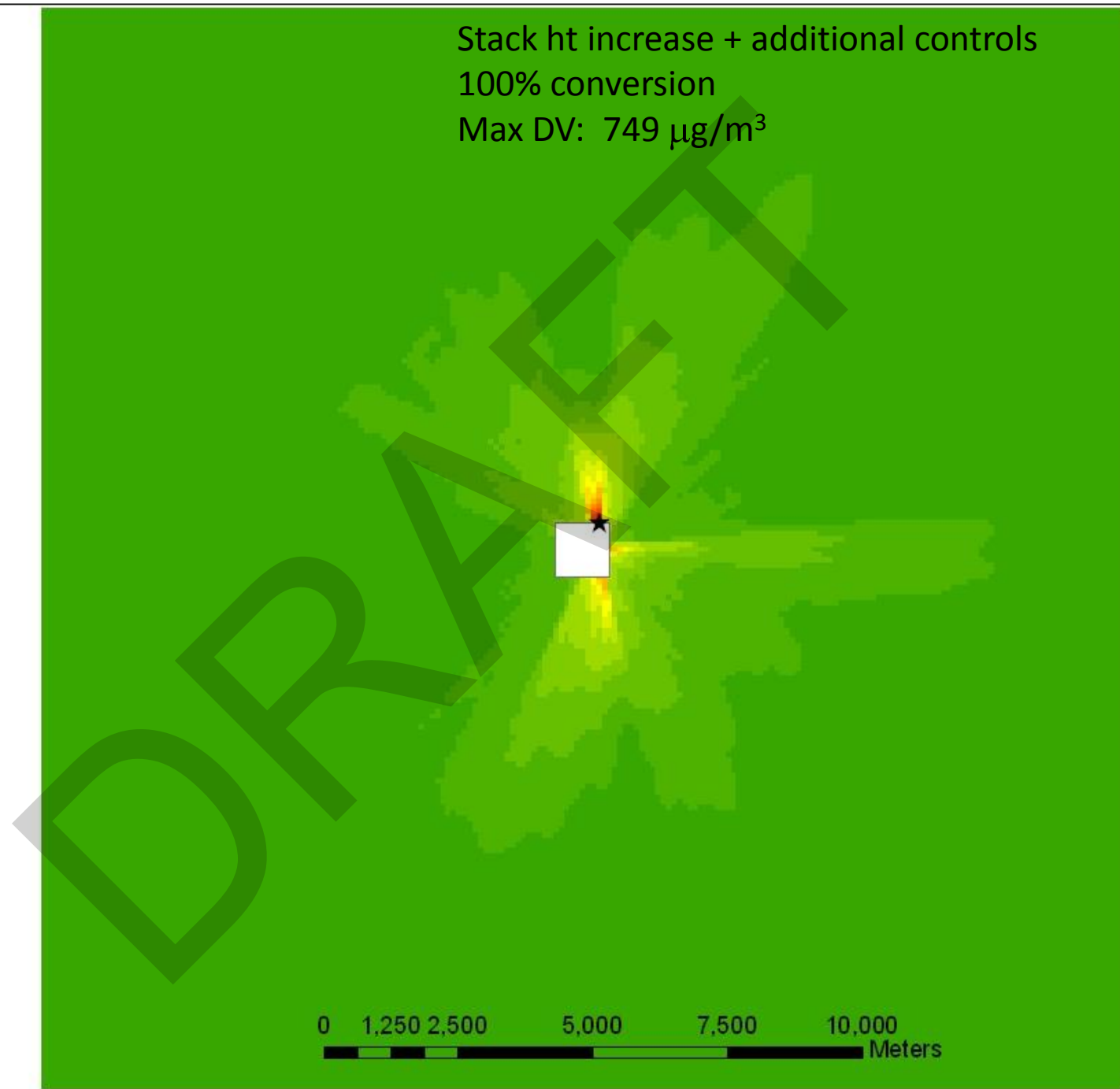
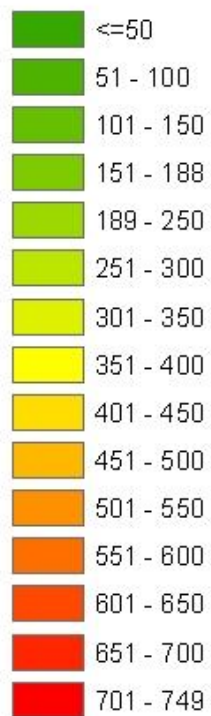
Stack ht increase + additional controls  
0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 220 μg/m<sup>3</sup>

**Legend**



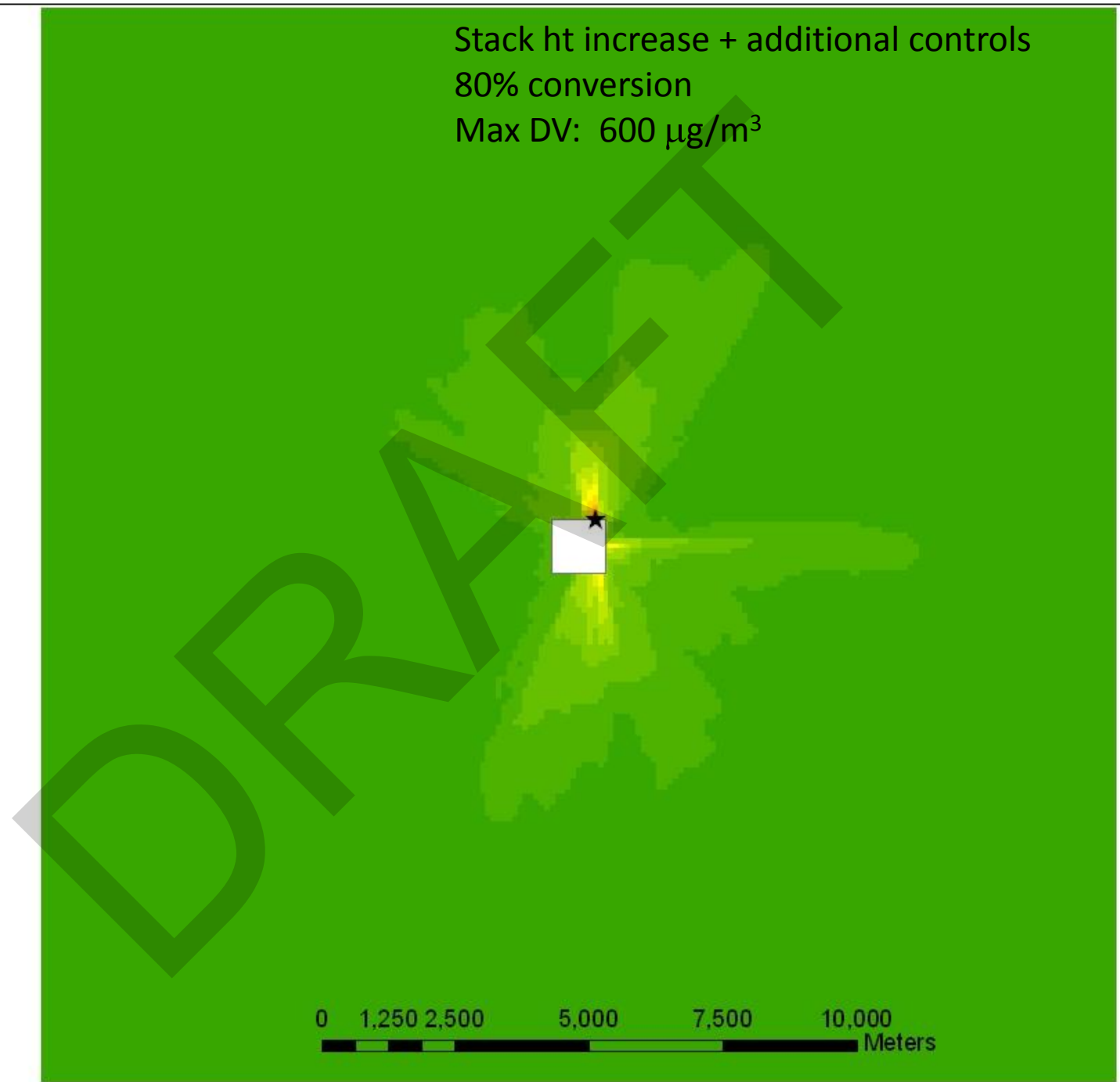
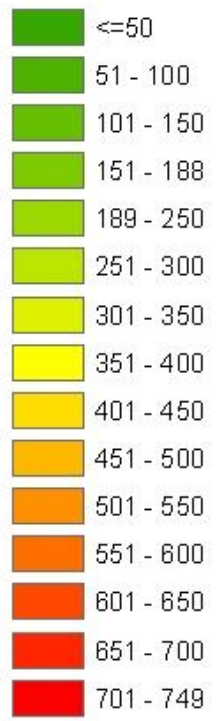
Stack ht increase + additional controls  
100% conversion  
Max DV: 749  $\mu\text{g}/\text{m}^3$

**Legend**



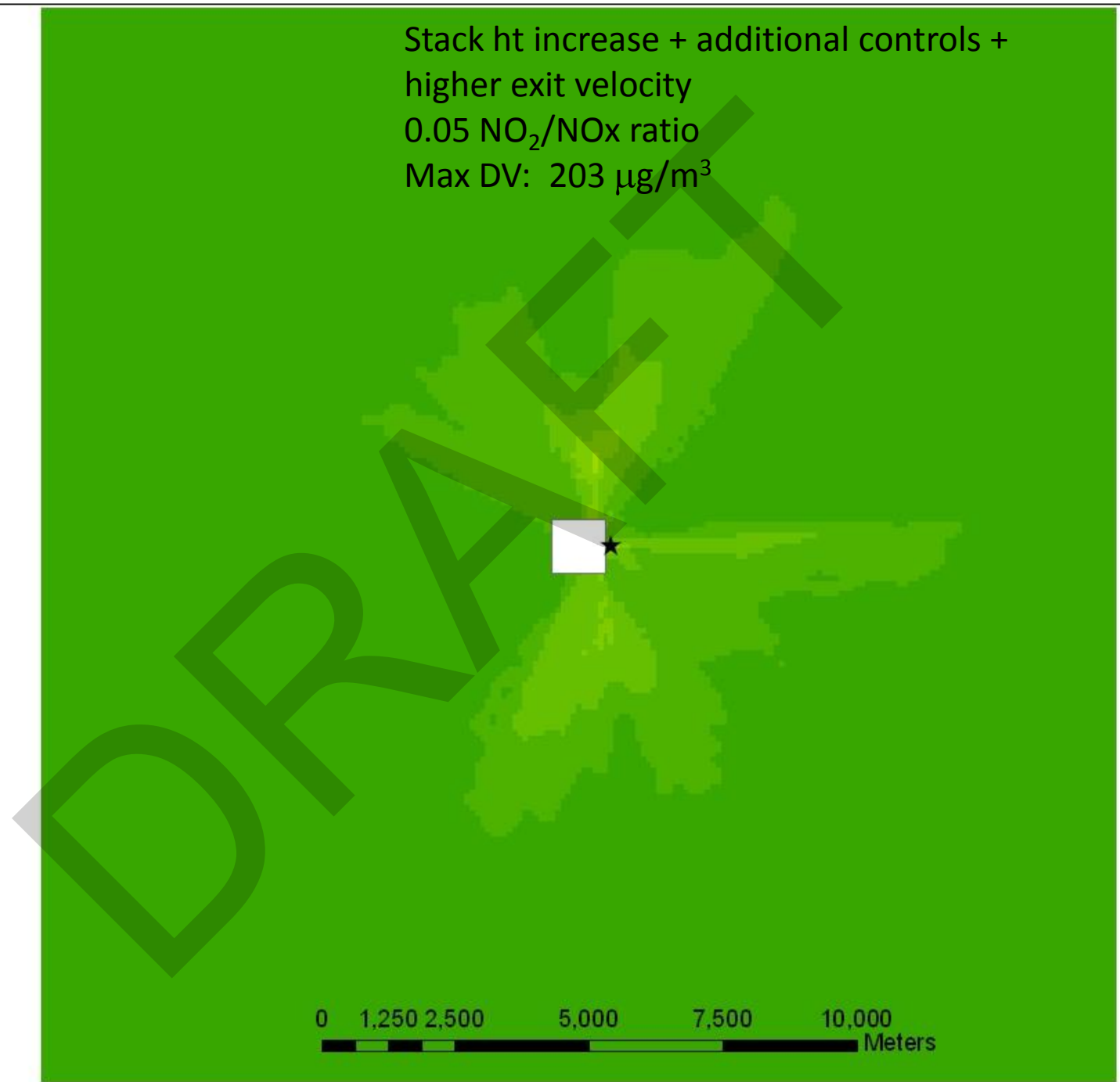
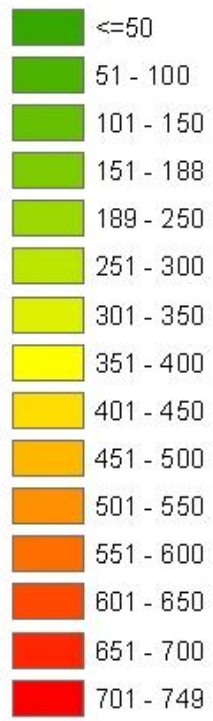
Stack ht increase + additional controls  
80% conversion  
Max DV: 600  $\mu\text{g}/\text{m}^3$

**Legend**



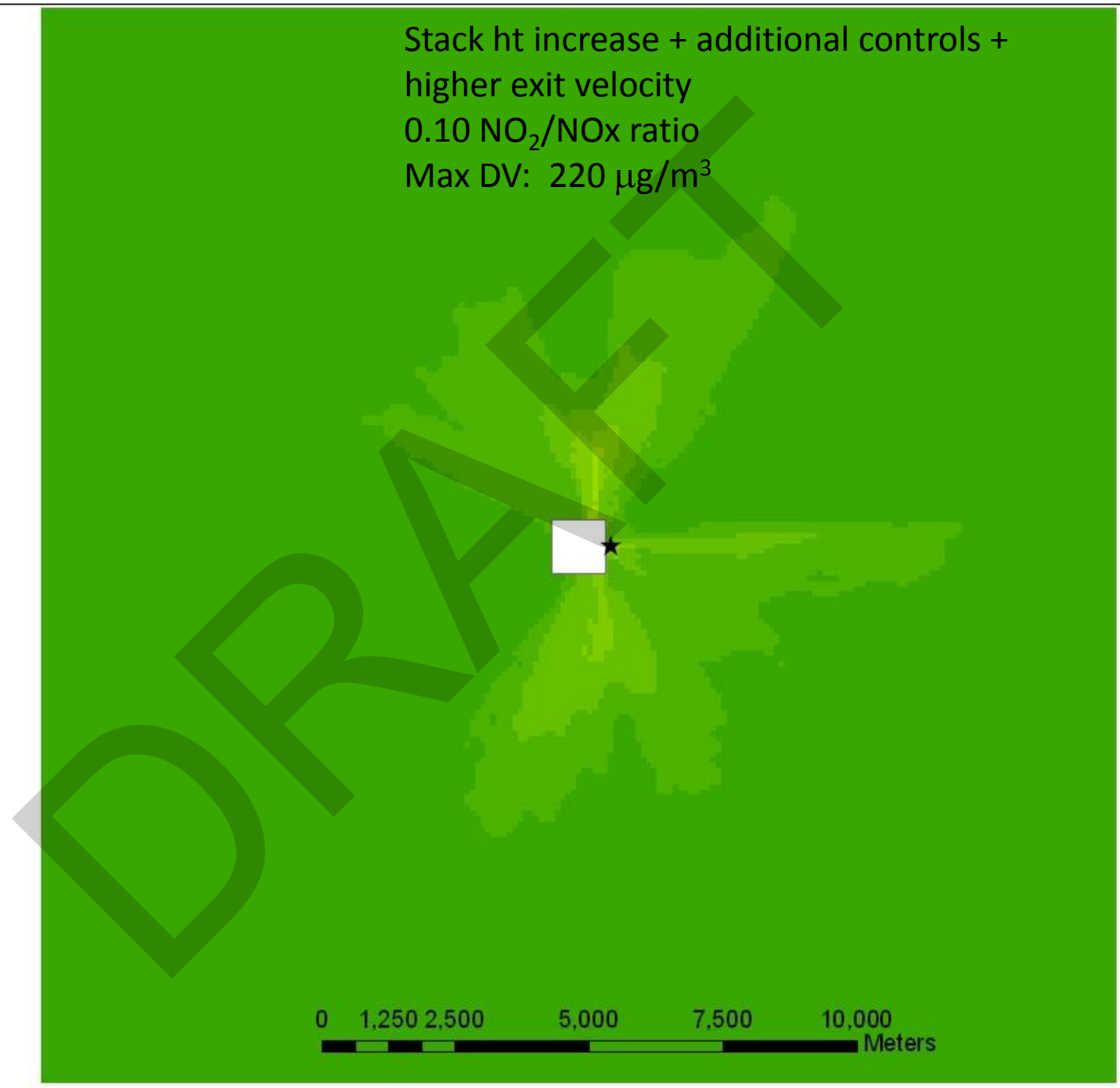
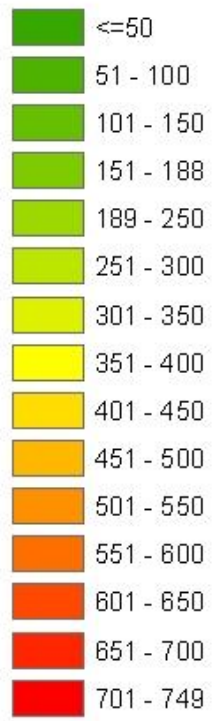
Stack ht increase + additional controls +  
higher exit velocity  
0.05 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 203 μg/m<sup>3</sup>

**Legend**



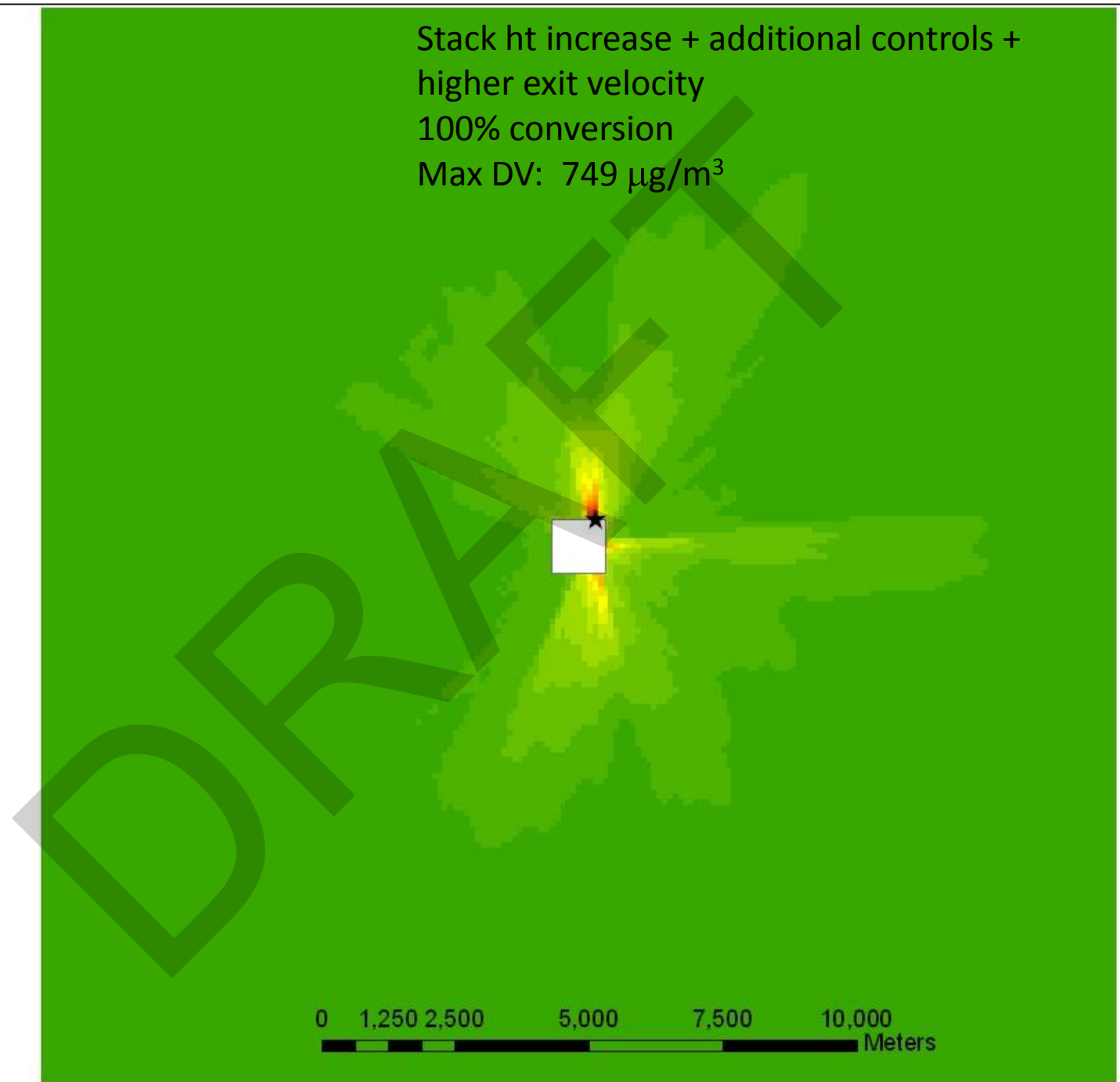
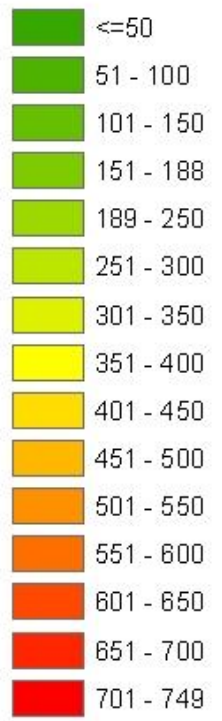
Stack ht increase + additional controls +  
higher exit velocity  
0.10 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 220 μg/m<sup>3</sup>

**Legend**



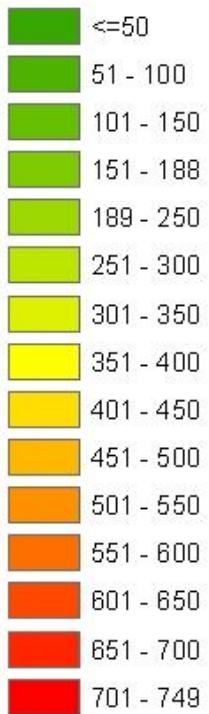
Stack ht increase + additional controls +  
higher exit velocity  
100% conversion  
Max DV: 749  $\mu\text{g}/\text{m}^3$

**Legend**





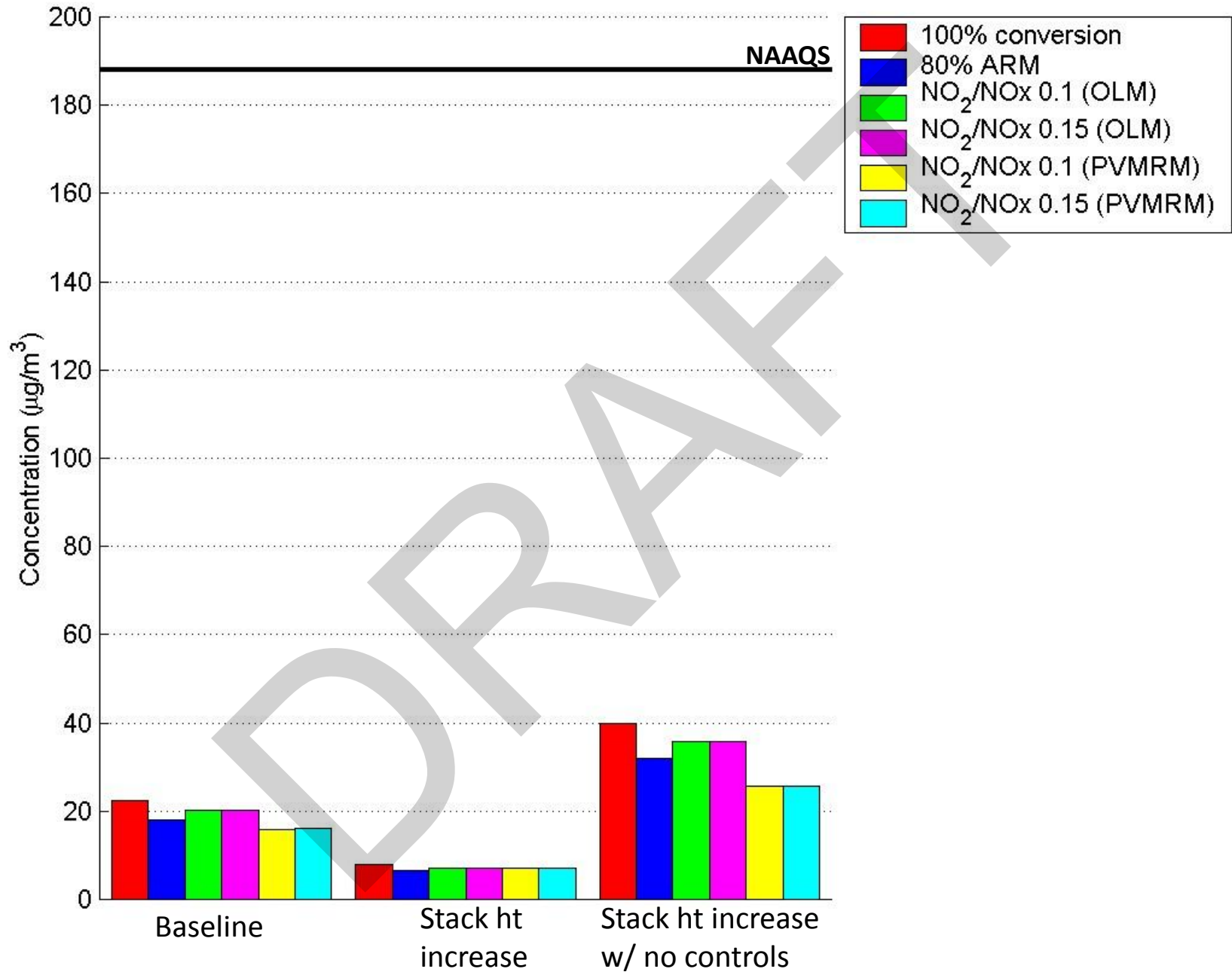
### Legend



Stack ht increase + additional controls +  
higher exit velocity  
80% conversion  
Max DV:  $600 \mu\text{g}/\text{m}^3$

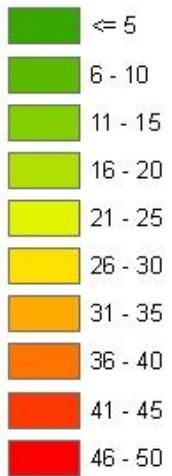


# Biomass facility (rural): NO<sub>2</sub>



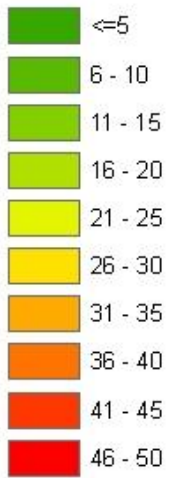
Base (Rural)  
100% conversion  
Max DV: 22  $\mu\text{g}/\text{m}^3$

### Legend



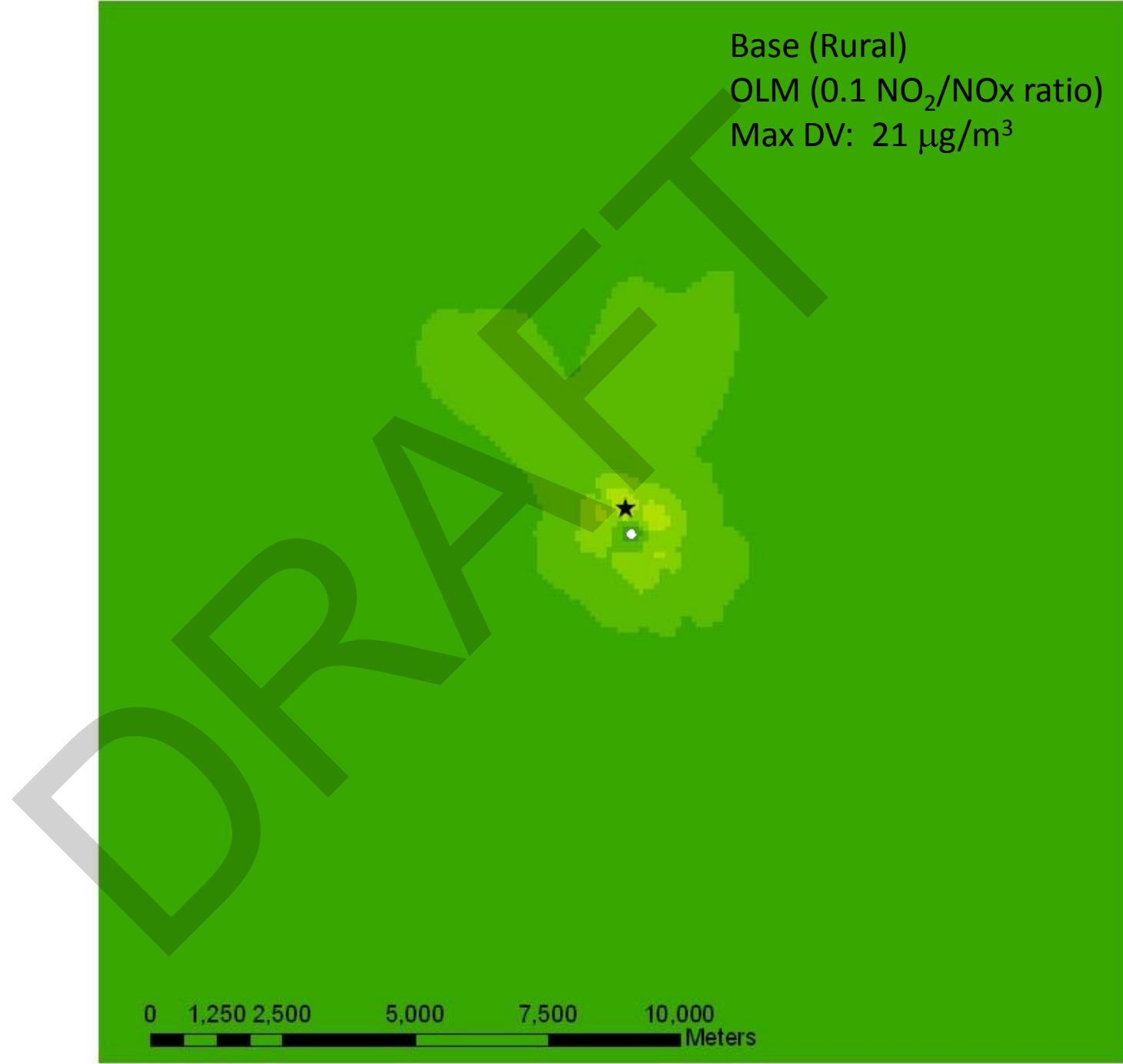
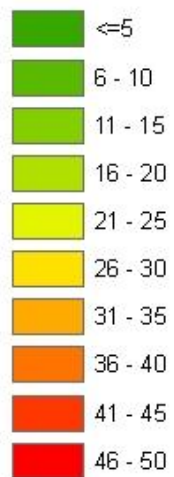
Base (Rural)  
80% conversion  
Max DV: 18  $\mu\text{g}/\text{m}^3$

### Legend



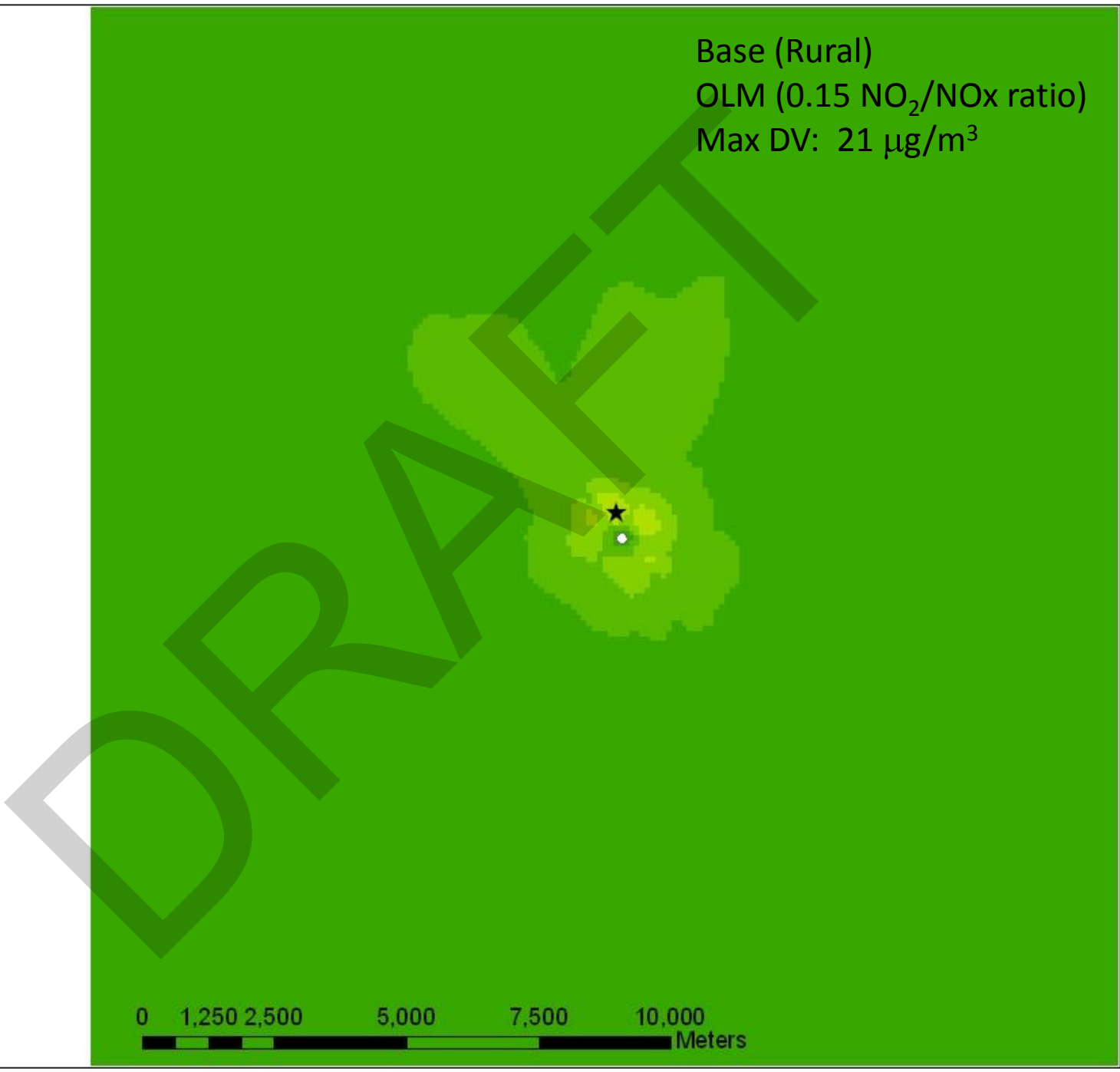
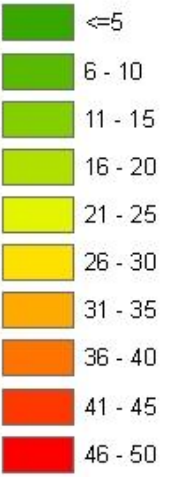
Base (Rural)  
OLM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 21 μg/m<sup>3</sup>

### Legend



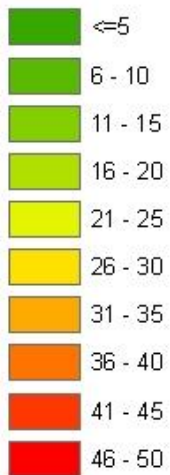
Base (Rural)  
OLM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 21 μg/m<sup>3</sup>

**Legend**



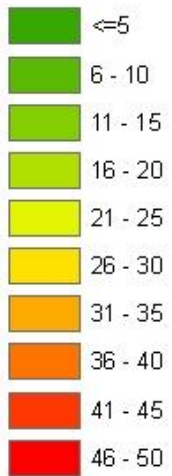
Base (Rural)  
PVMRM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 16 μg/m<sup>3</sup>

**Legend**



Base (Rural)  
PVMRM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 16 μg/m<sup>3</sup>

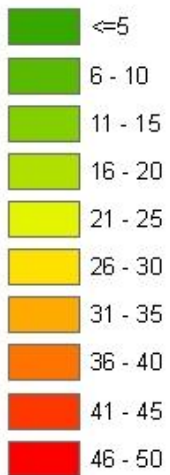
### Legend





Stack ht increase (Rural)  
100% conversion  
Max DV: 8  $\mu\text{g}/\text{m}^3$

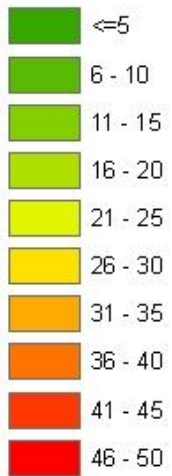
### Legend



0 1,250 2,500 5,000 7,500 10,000 Meters

Stack ht increase (Rural)  
80% conversion  
Max DV: 6  $\mu\text{g}/\text{m}^3$

### Legend

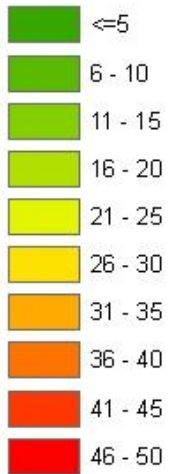


0 1,250 2,500 5,000 7,500 10,000 Meters



Stack ht increase (Rural)  
OLM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 7 μg/m<sup>3</sup>

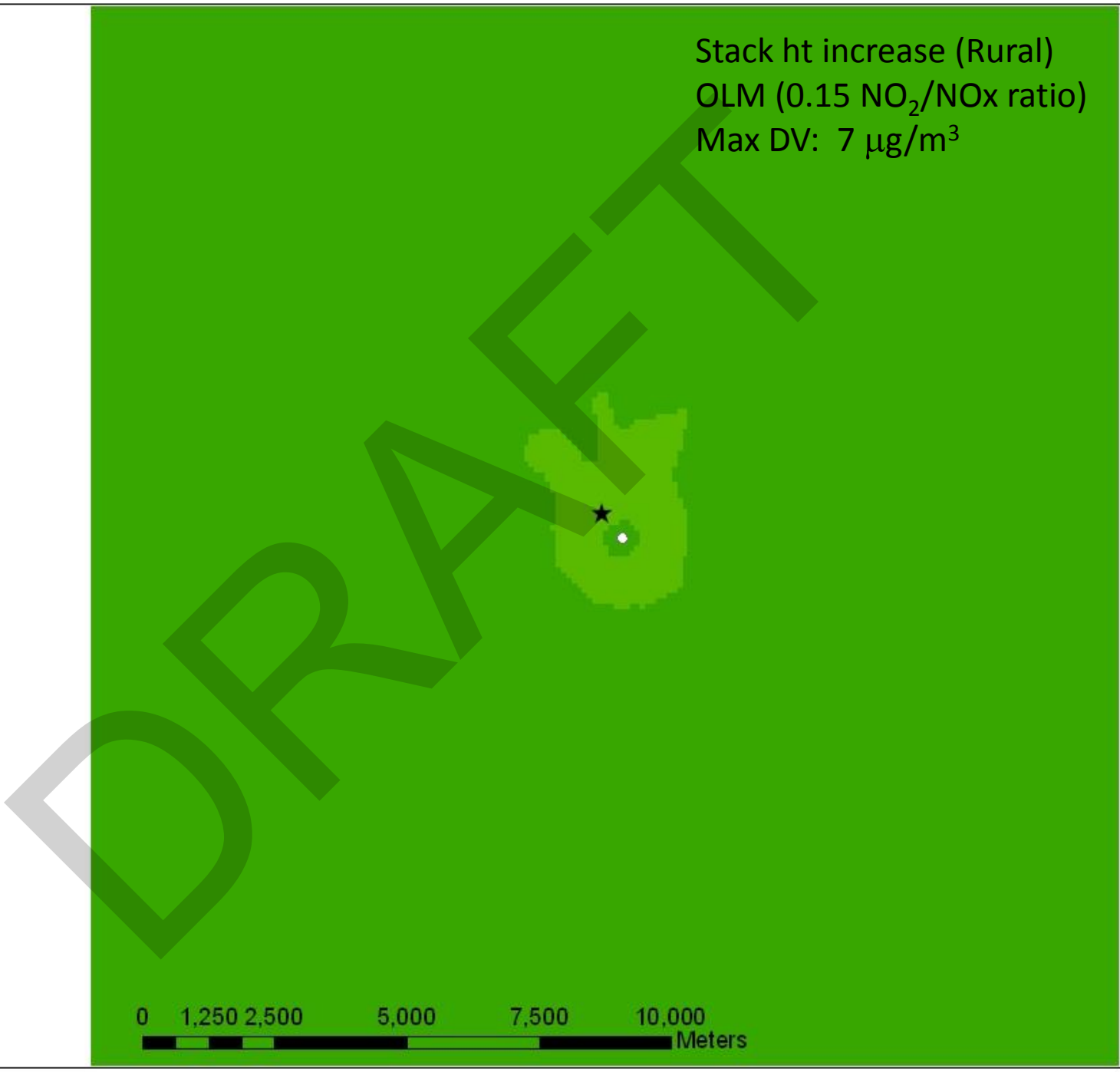
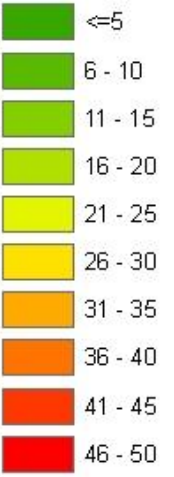
### Legend



0 1,250 2,500 5,000 7,500 10,000 Meters

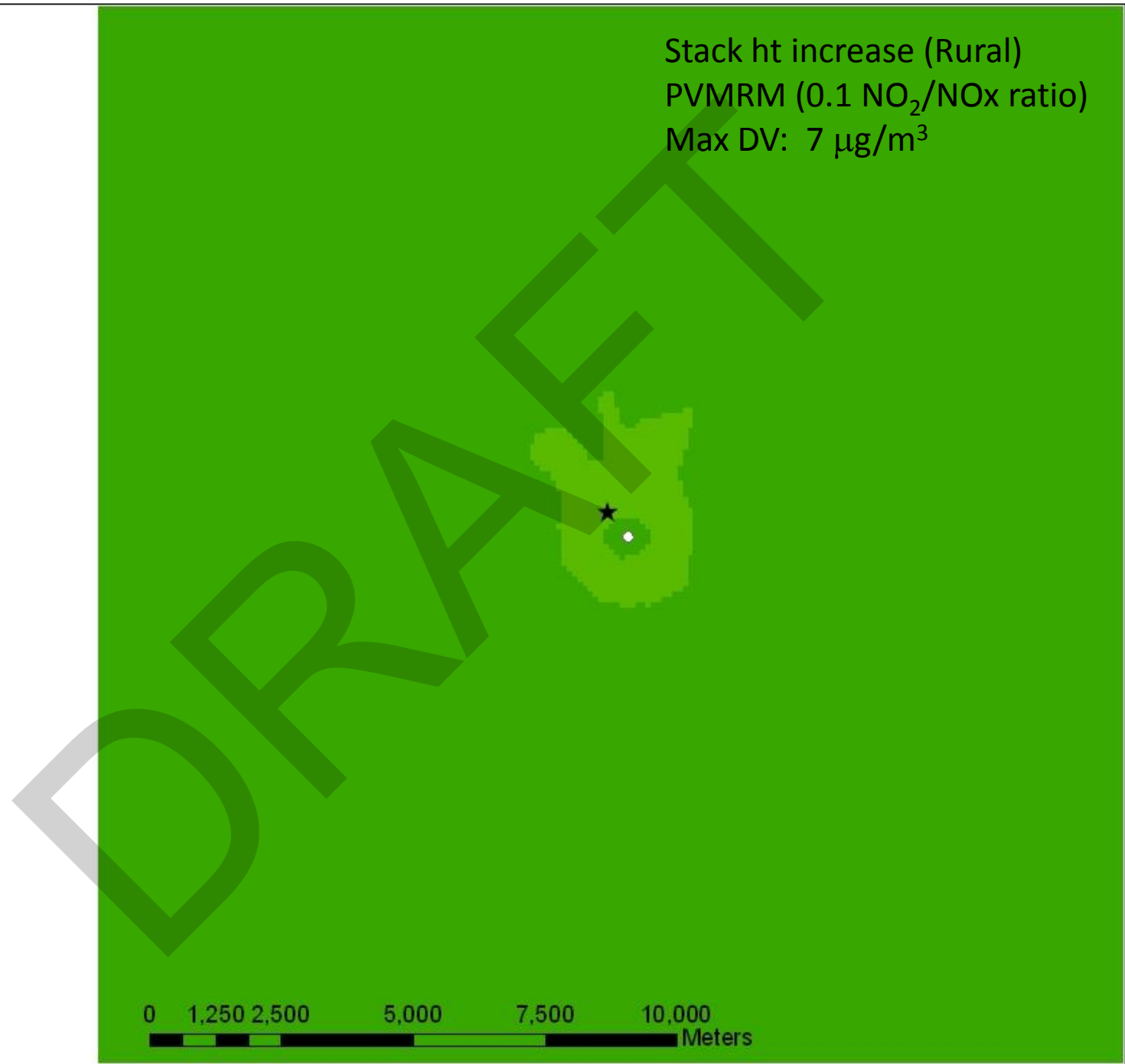
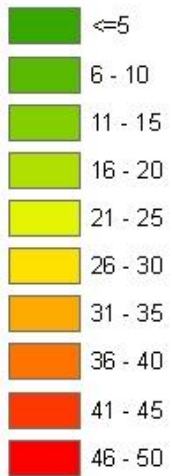
Stack ht increase (Rural)  
OLM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 7 μg/m<sup>3</sup>

**Legend**



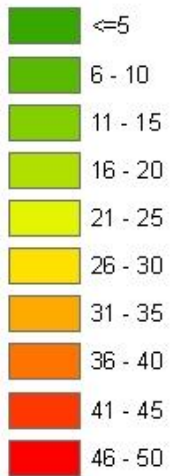
Stack ht increase (Rural)  
PVMRM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 7 μg/m<sup>3</sup>

### Legend



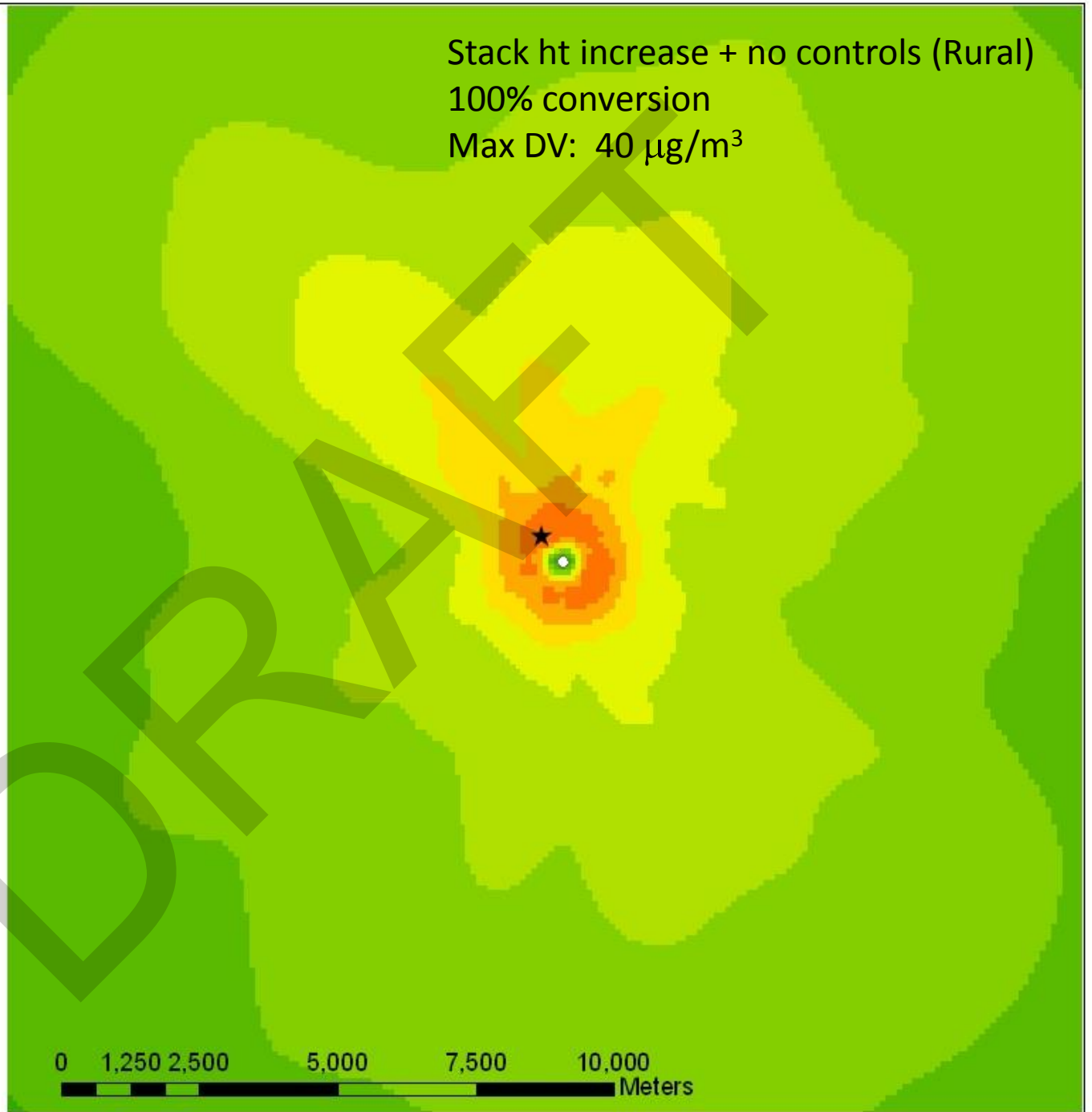
Stack ht increase (Rural)  
PVMRM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 7 μg/m<sup>3</sup>

### Legend



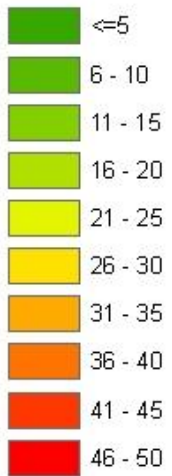
Stack ht increase + no controls (Rural)  
100% conversion  
Max DV: 40  $\mu\text{g}/\text{m}^3$

**Legend**



Stack ht increase + no controls (Rural)  
80% conversion  
Max DV: 32  $\mu\text{g}/\text{m}^3$

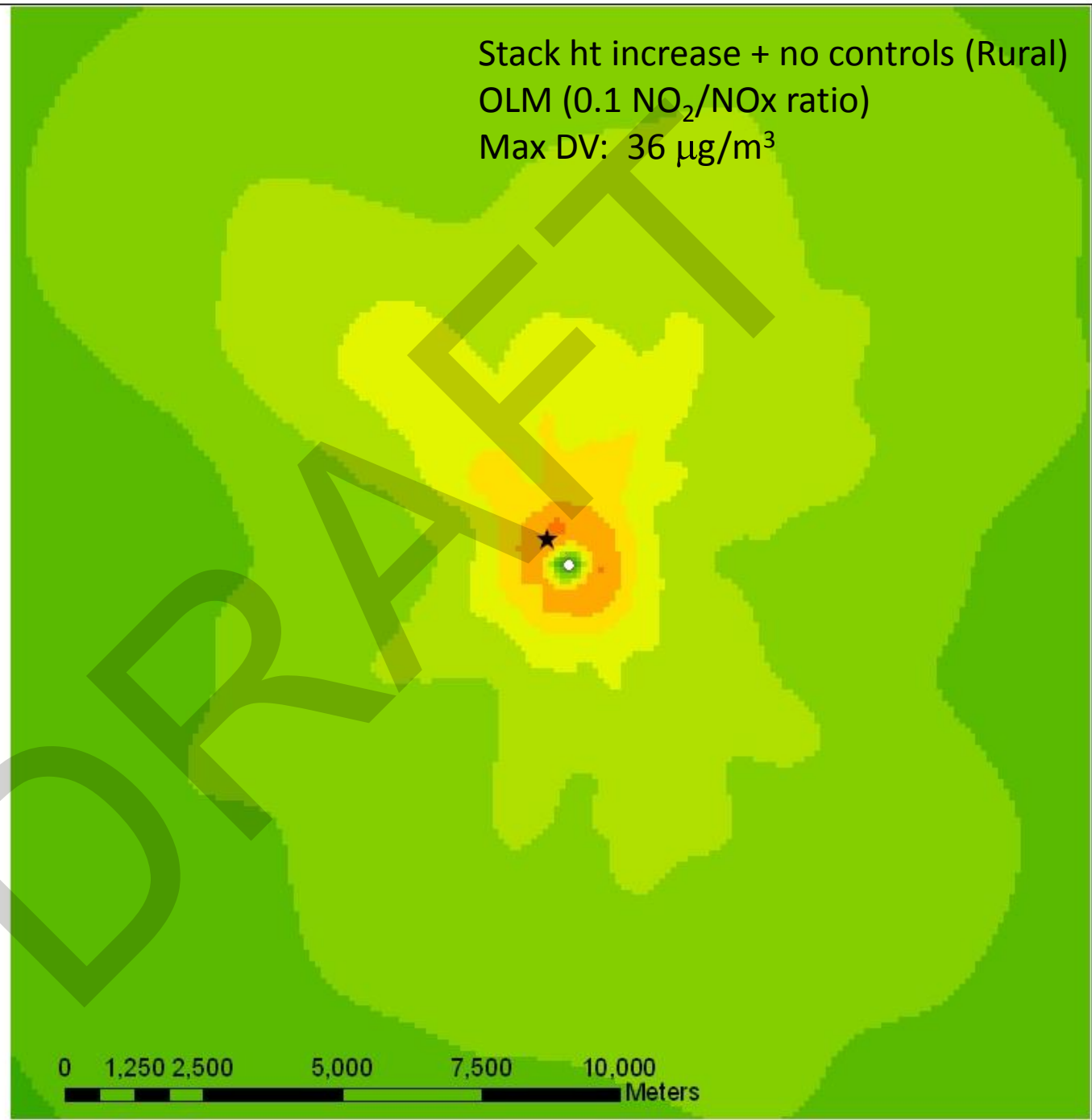
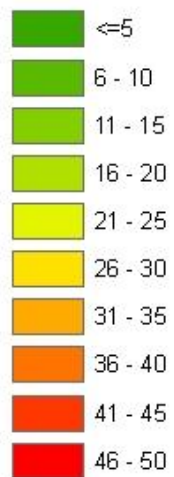
**Legend**





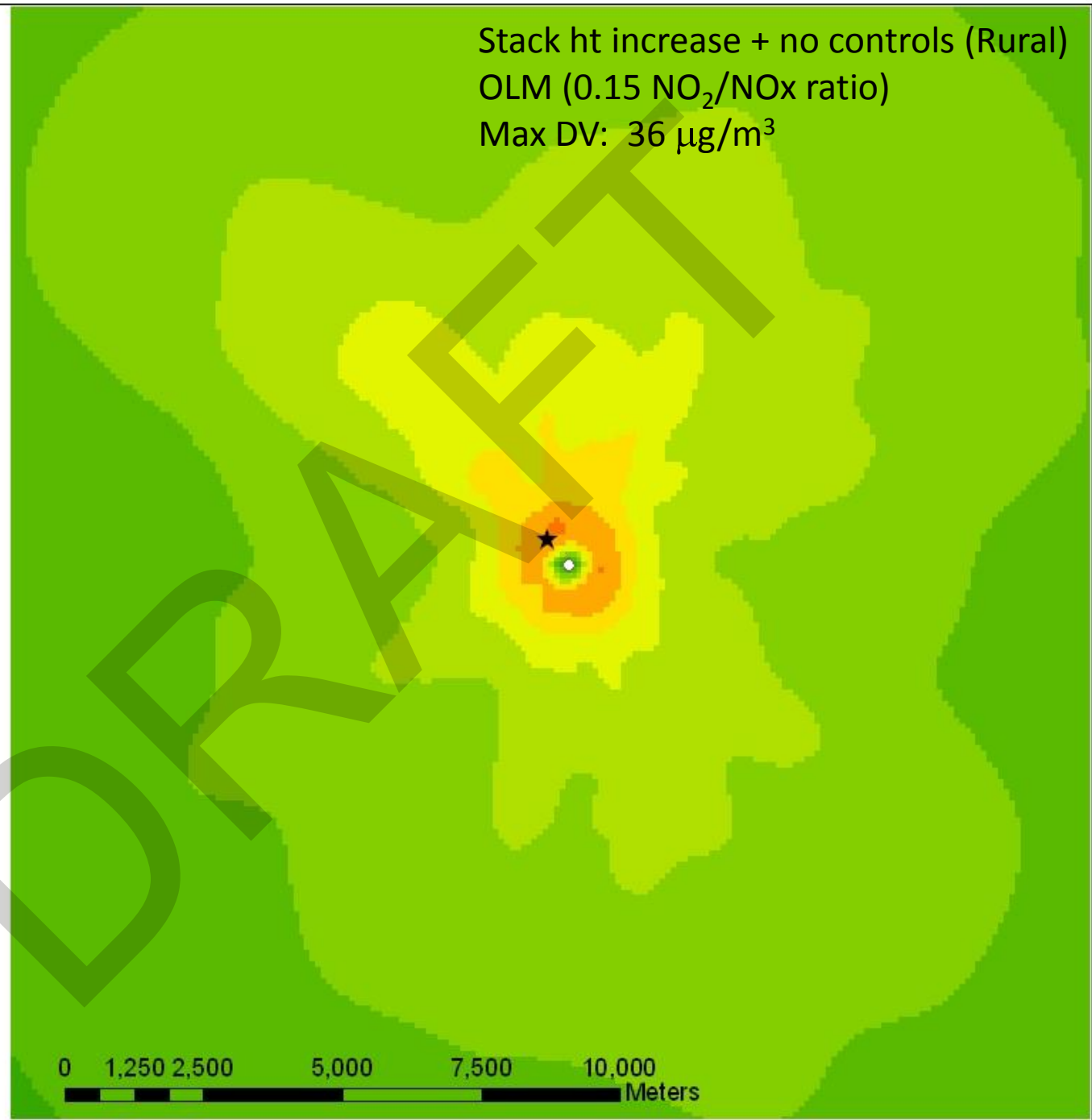
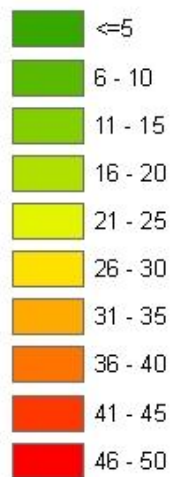
Stack ht increase + no controls (Rural)  
OLM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 36 μg/m<sup>3</sup>

### Legend



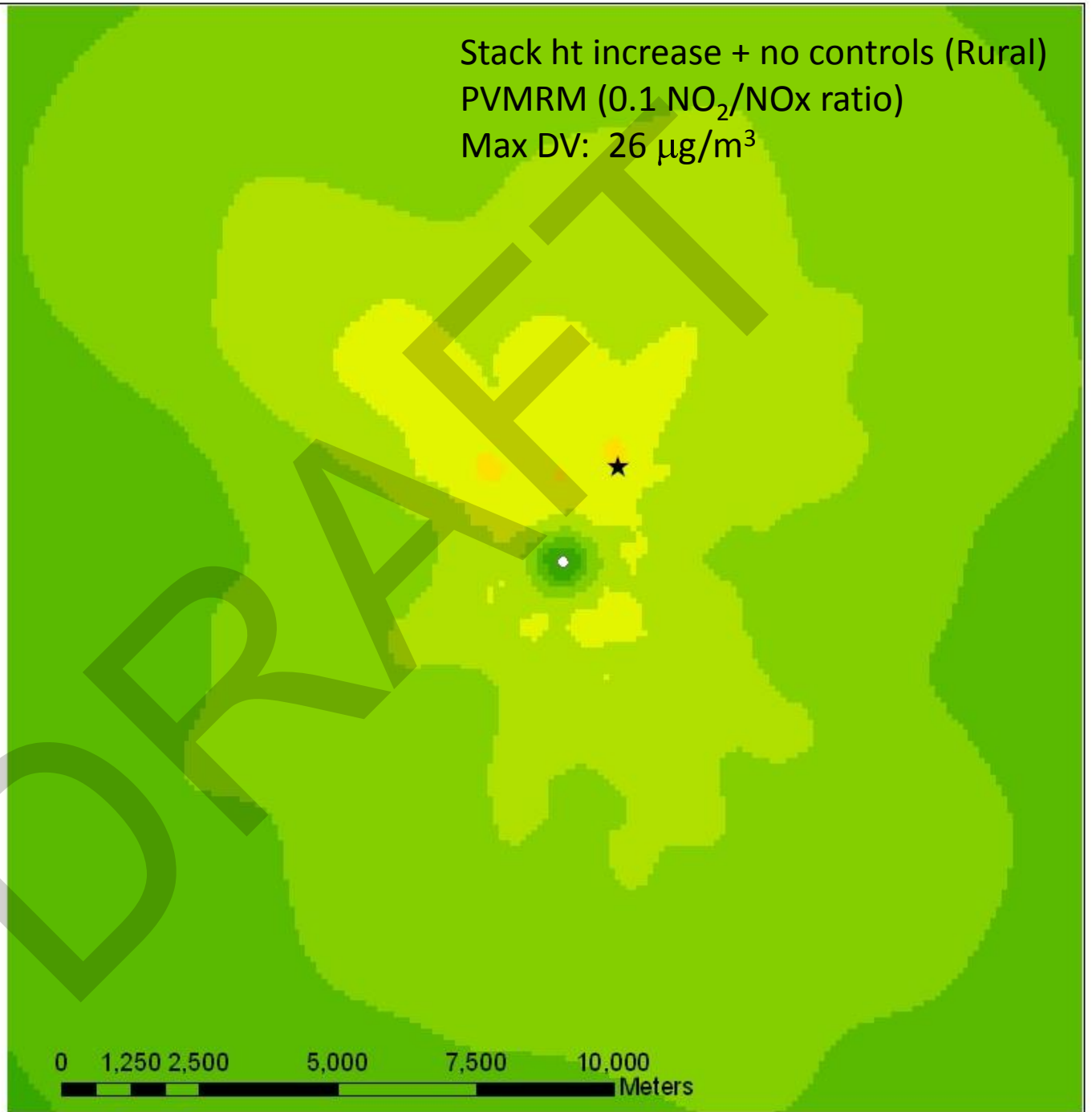
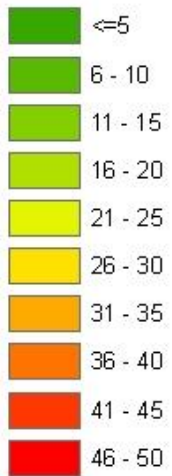
Stack ht increase + no controls (Rural)  
OLM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 36 μg/m<sup>3</sup>

### Legend



Stack ht increase + no controls (Rural)  
PVMRM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 26 μg/m<sup>3</sup>

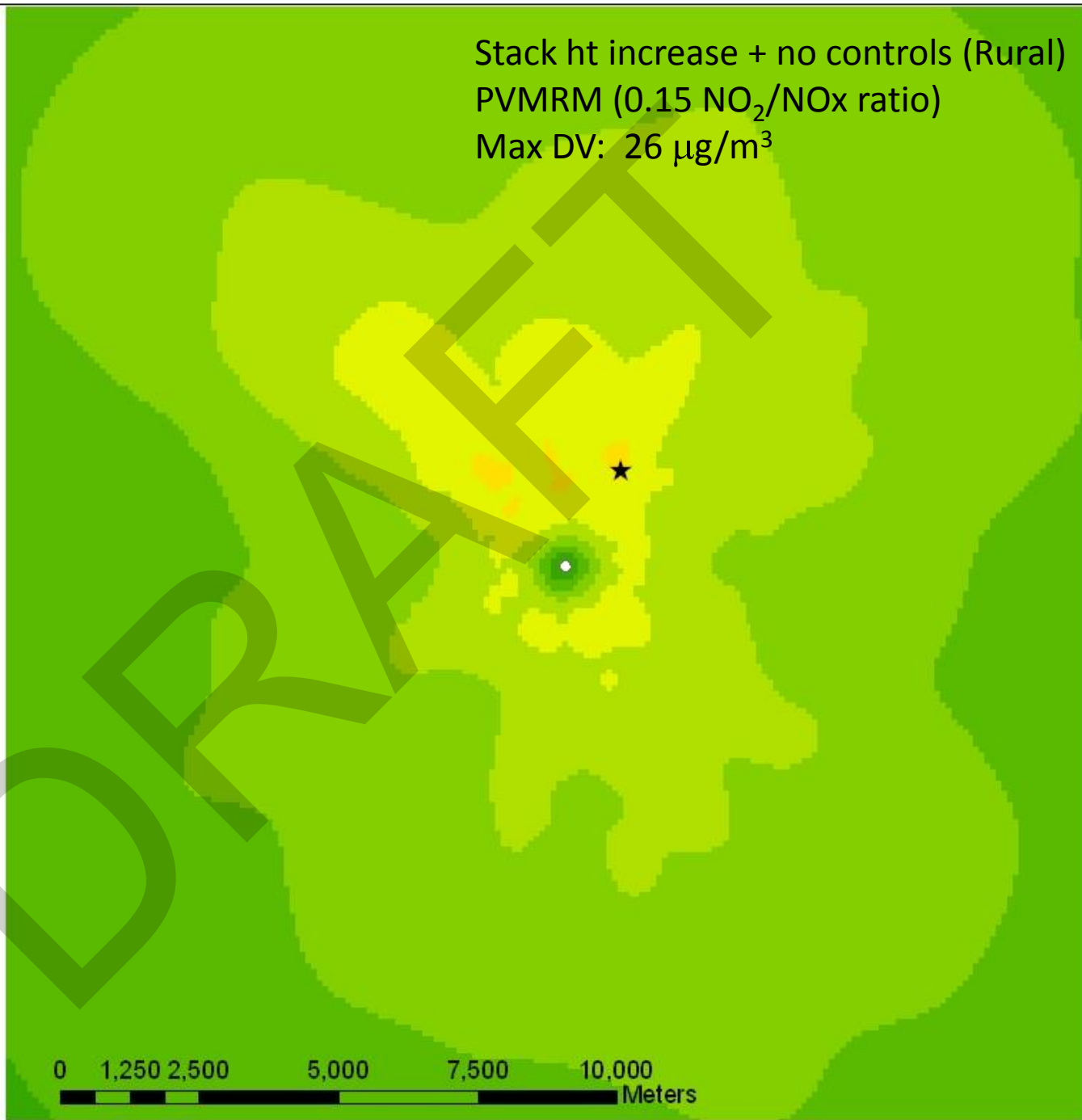
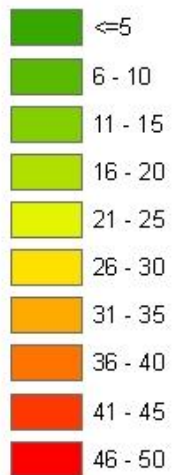
### Legend



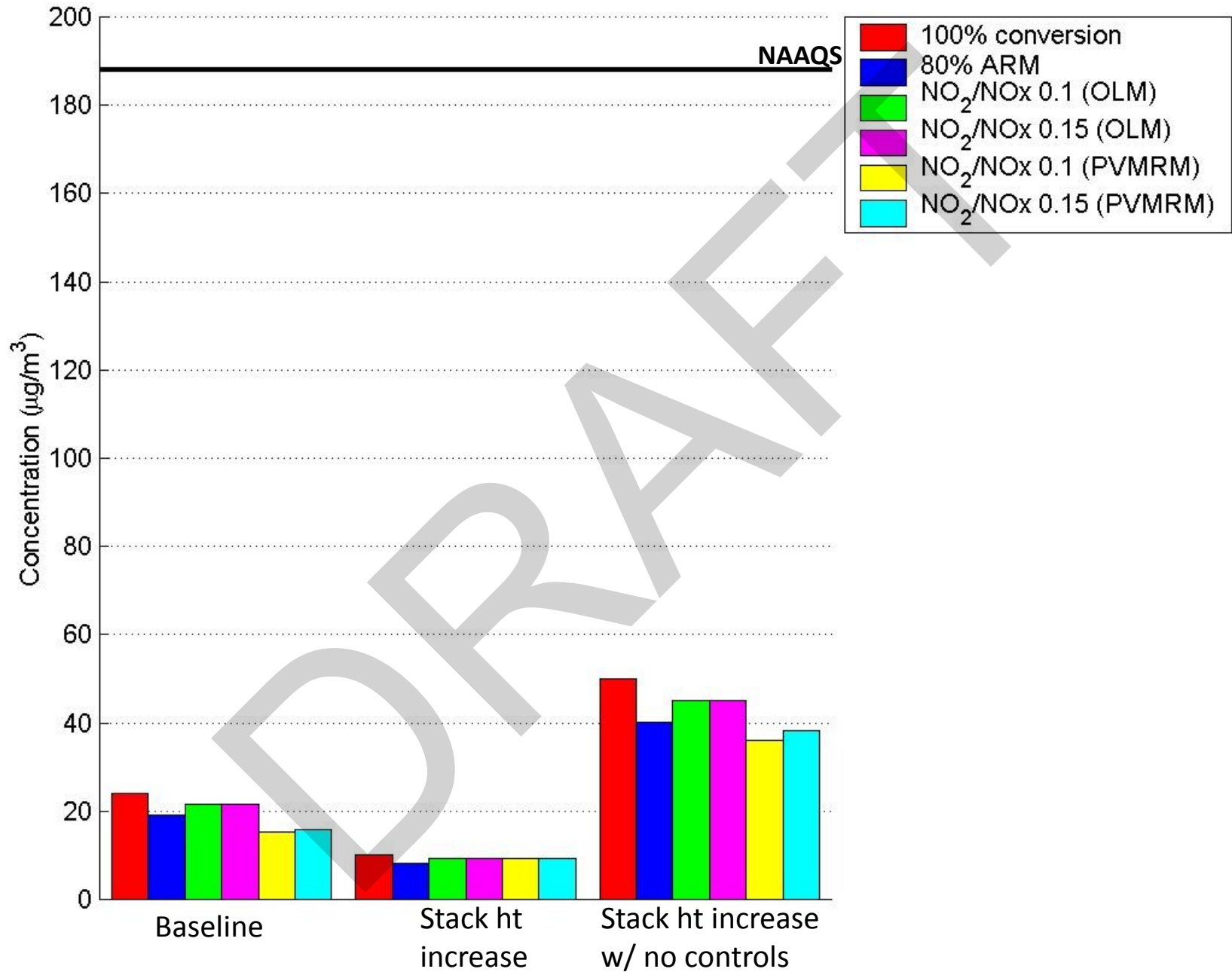
0 1,250 2,500 5,000 7,500 10,000 Meters

Stack ht increase + no controls (Rural)  
PVMRM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 26 μg/m<sup>3</sup>

### Legend

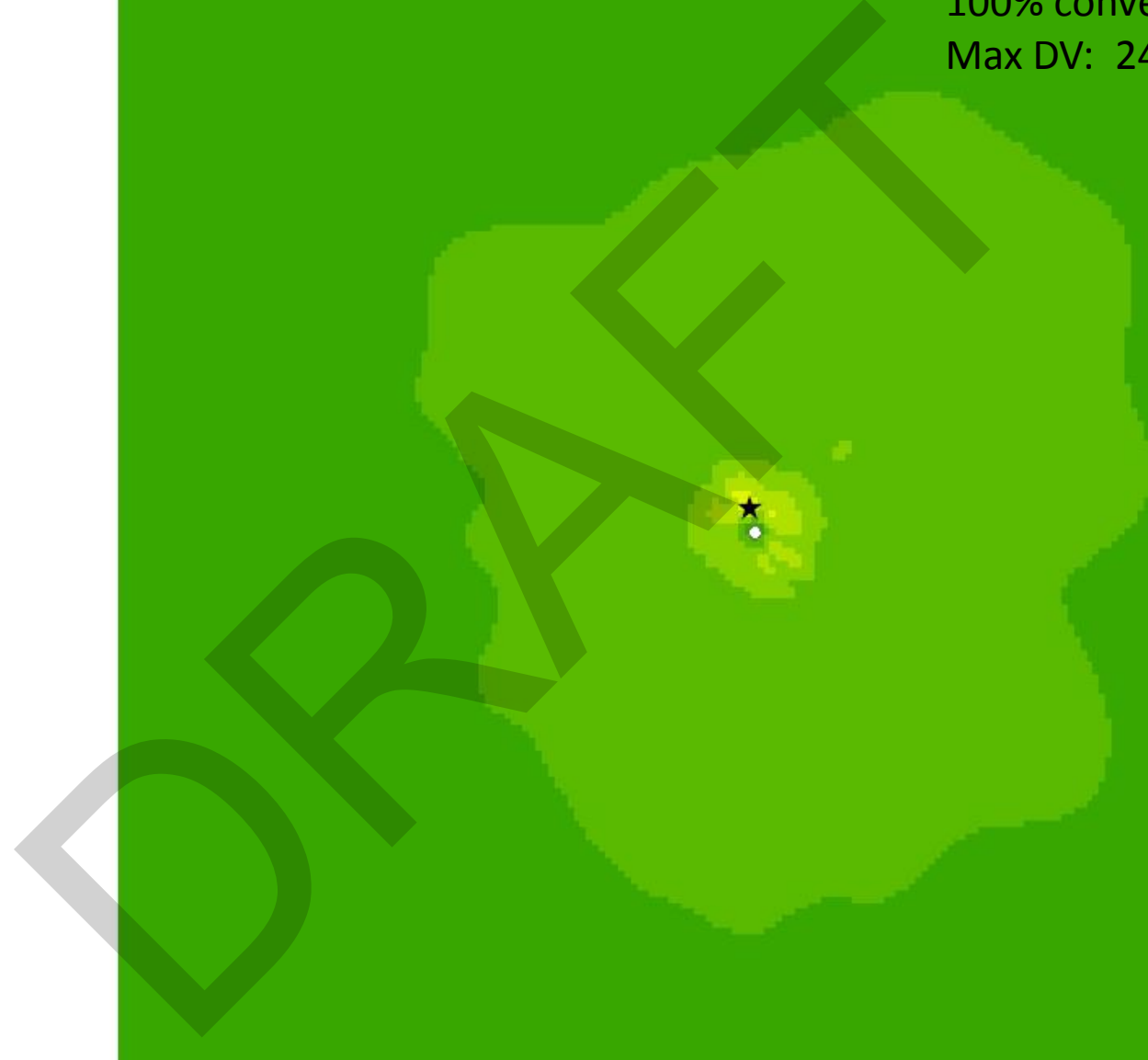
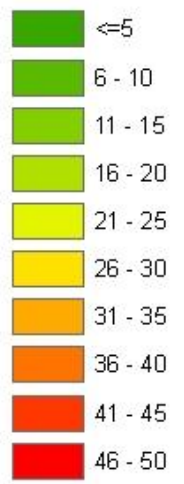


# Biomass facility (urban): NO<sub>2</sub>



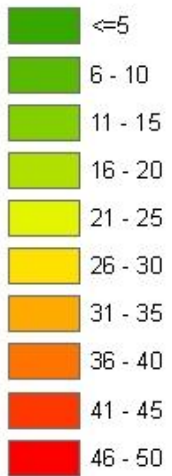
Base (Urban)  
100% conversion  
Max DV: 24  $\mu\text{g}/\text{m}^3$

### Legend



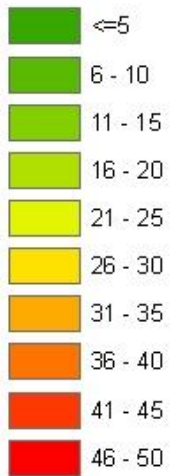
Base (Urban)  
80% conversion  
Max DV: 19  $\mu\text{g}/\text{m}^3$

### Legend



Base (Urban)  
OLM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 22 μg/m<sup>3</sup>

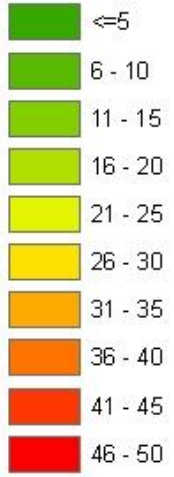
### Legend





Base (Urban)  
OLM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 22 μg/m<sup>3</sup>

**Legend**

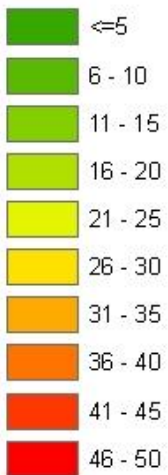


DRAFT



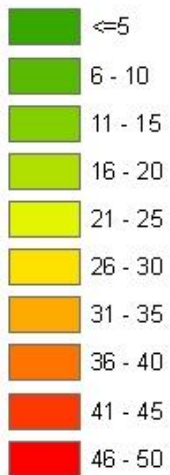
Base (Urban)  
PVMRM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 15 μg/m<sup>3</sup>

### Legend



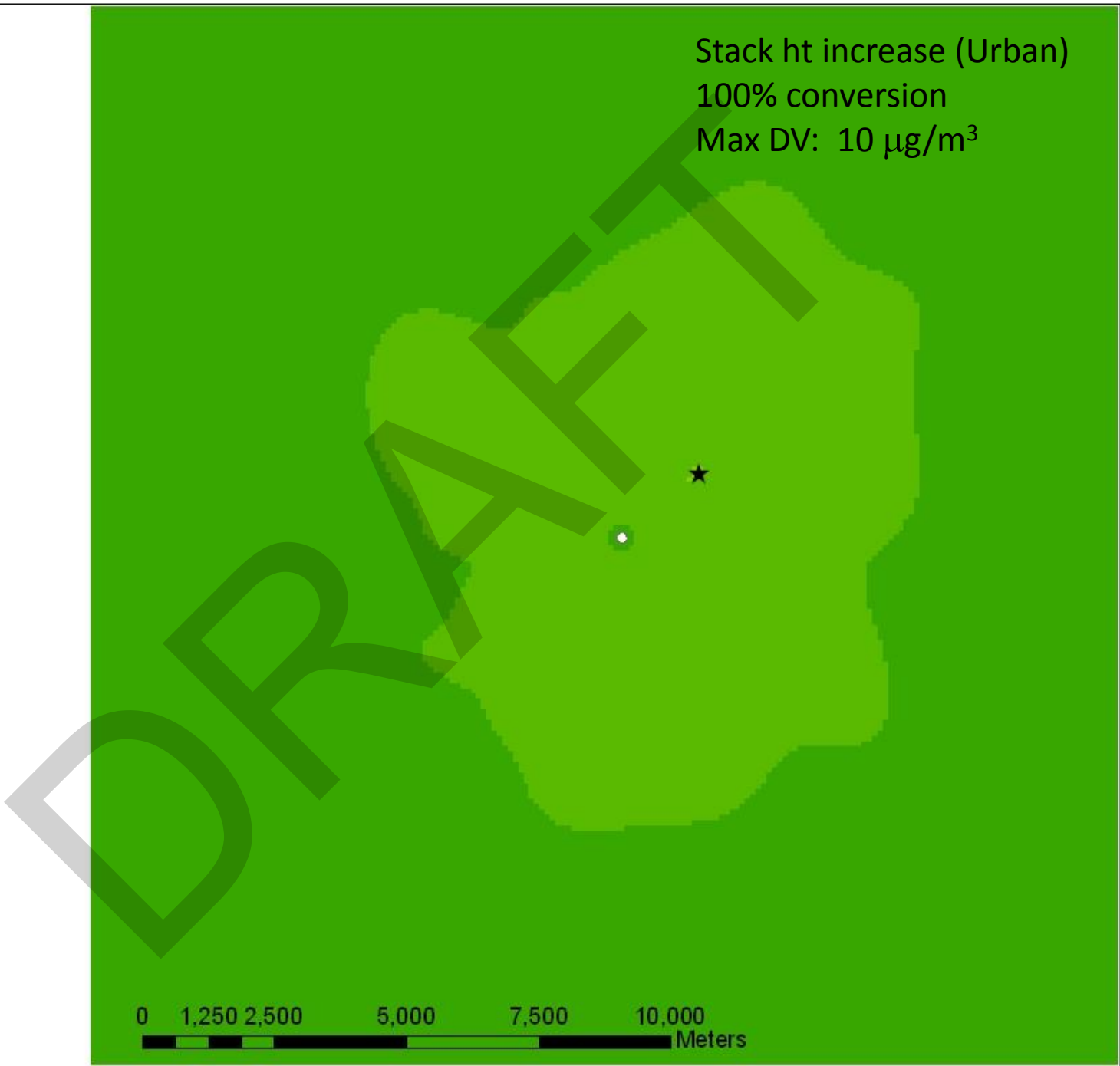
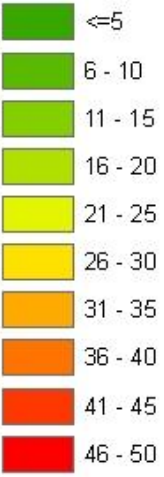
Base (Urban)  
PVMRM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 16 μg/m<sup>3</sup>

### Legend



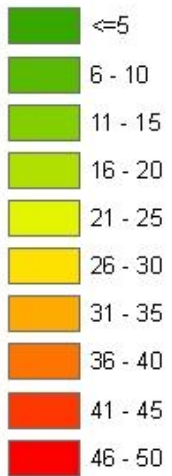
Stack ht increase (Urban)  
100% conversion  
Max DV: 10  $\mu\text{g}/\text{m}^3$

**Legend**



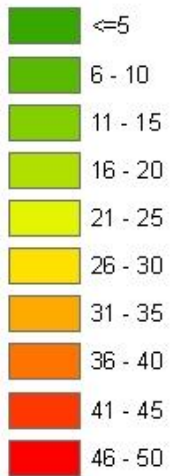
Stack ht increase (Urban)  
80% conversion  
Max DV: 8  $\mu\text{g}/\text{m}^3$

### Legend



Stack ht increase (Urban)  
OLM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 9 μg/m<sup>3</sup>

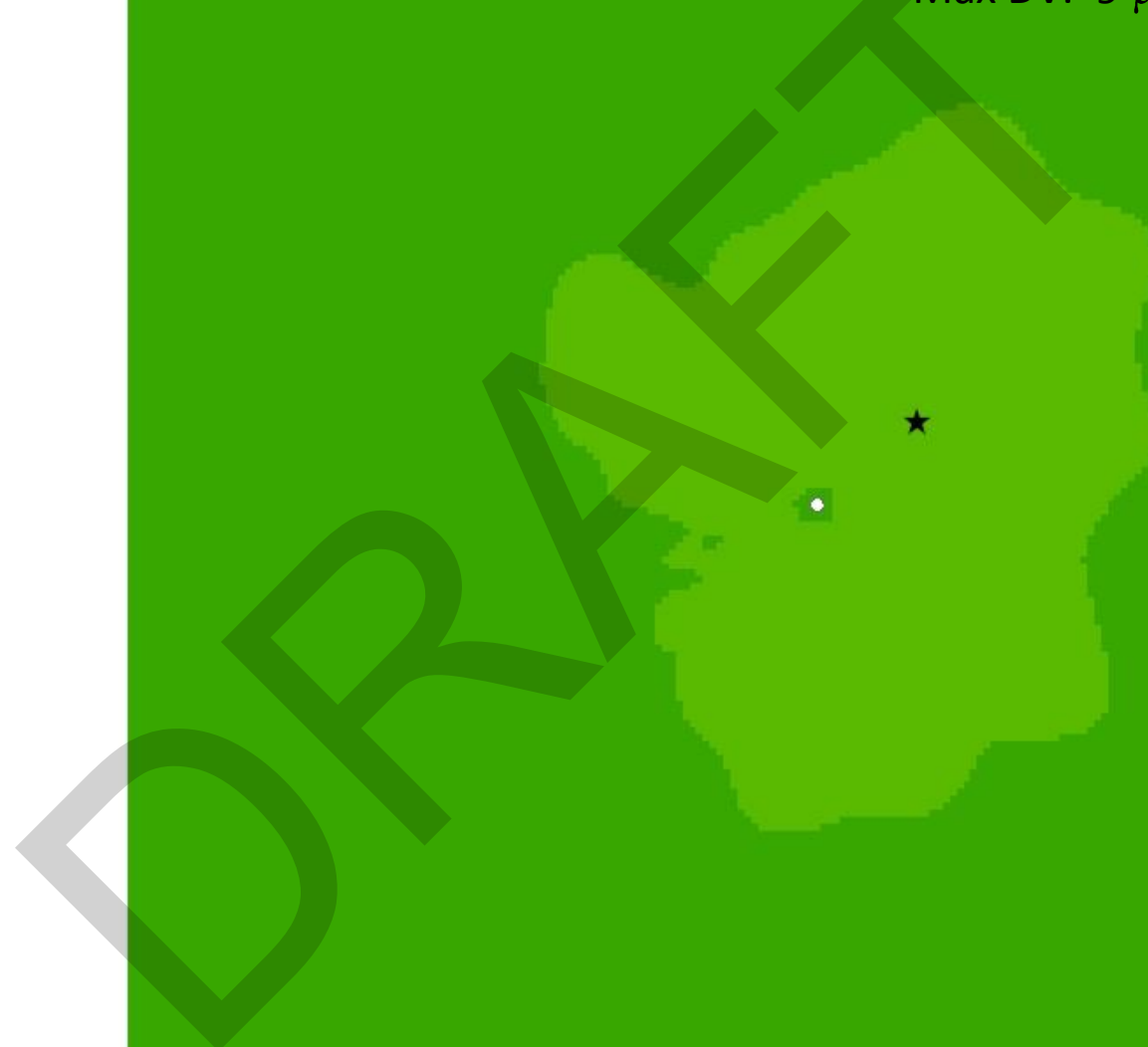
### Legend



Stack ht increase (Urban)  
OLM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 9 μg/m<sup>3</sup>

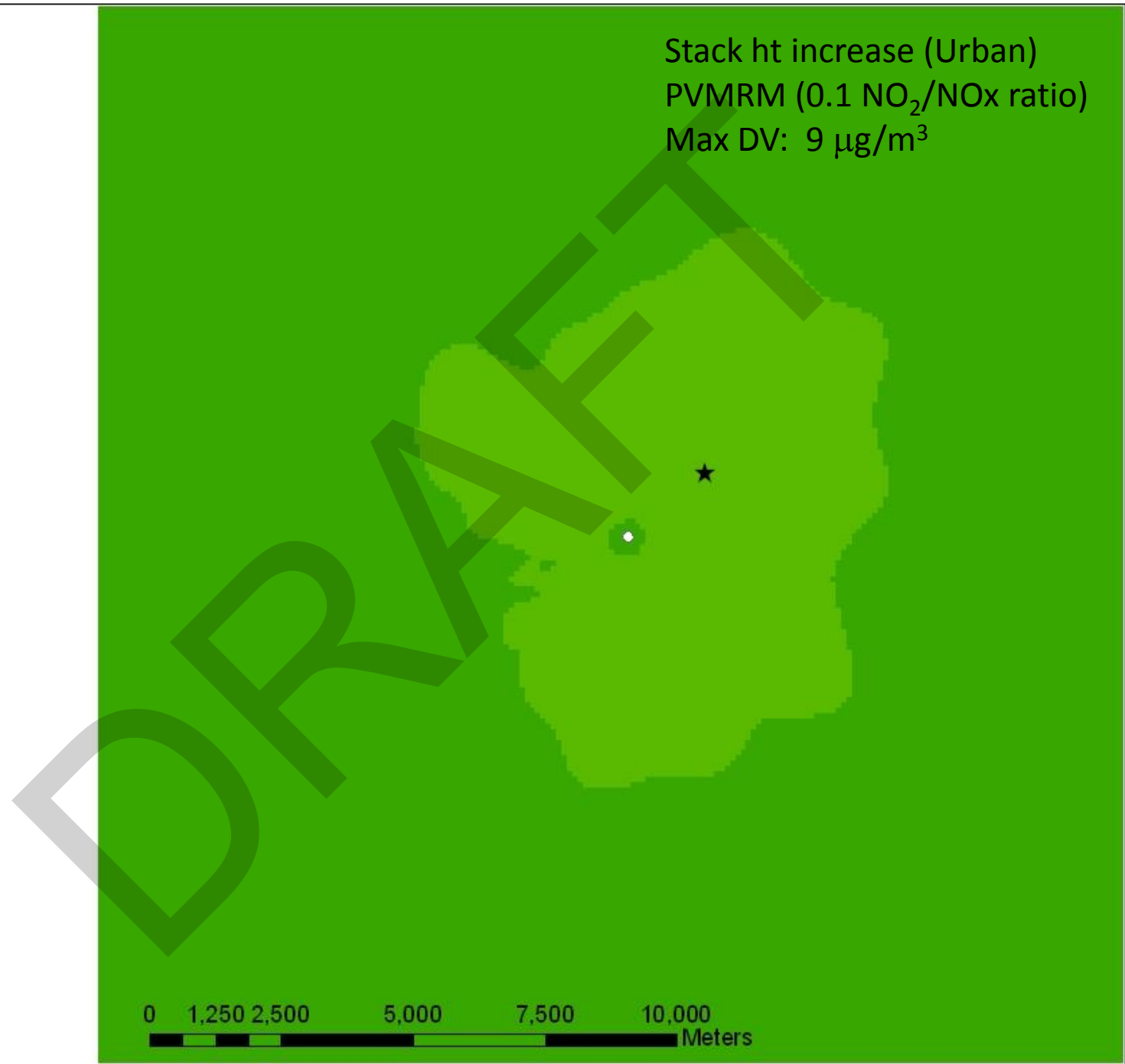
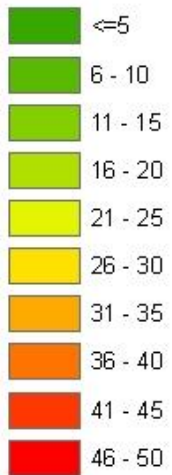
**Legend**

- ≤5
- 6 - 10
- 11 - 15
- 16 - 20
- 21 - 25
- 26 - 30
- 31 - 35
- 36 - 40
- 41 - 45
- 46 - 50



Stack ht increase (Urban)  
PVMRM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 9 μg/m<sup>3</sup>

### Legend

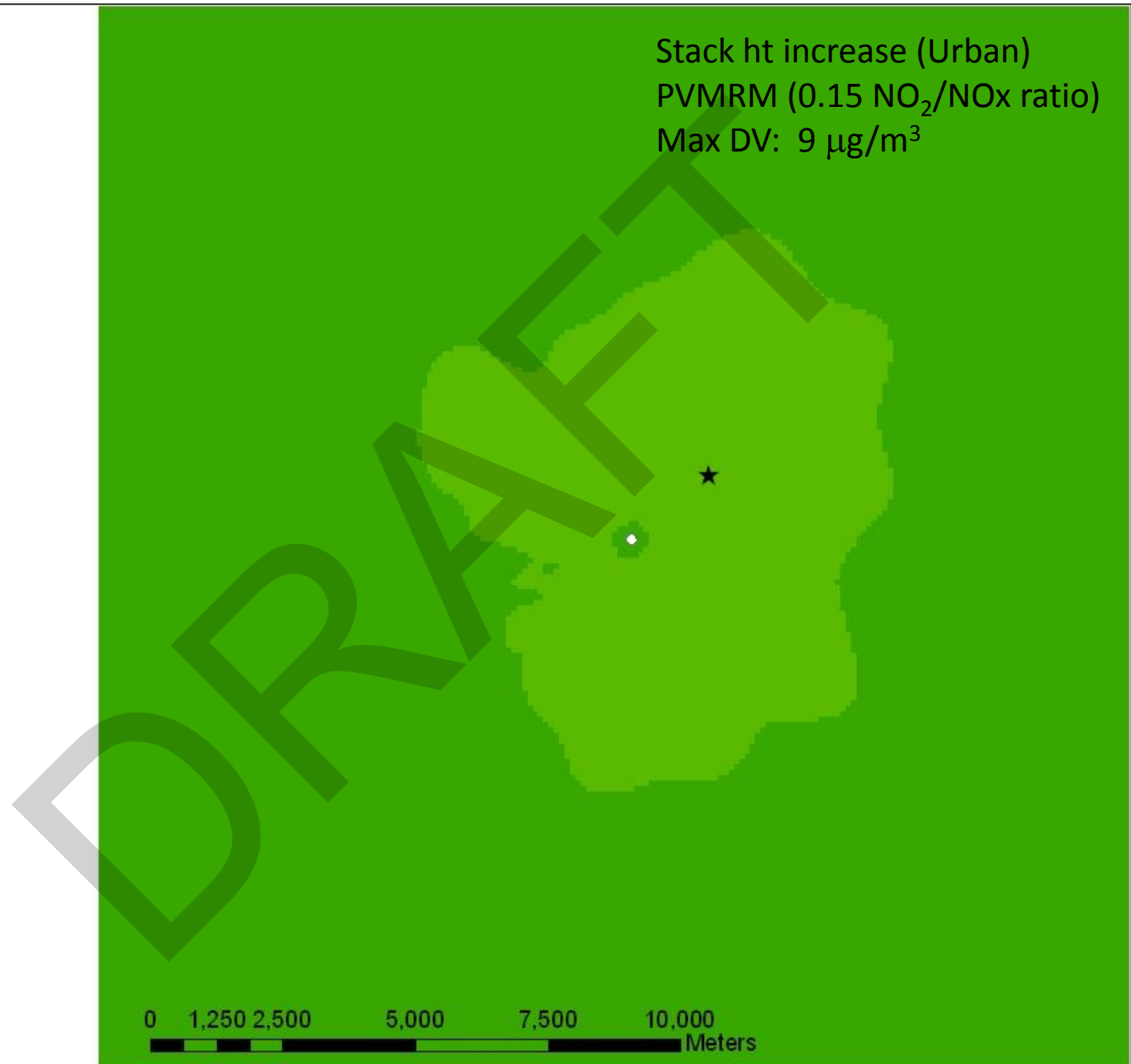
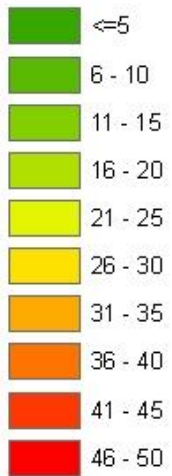


0 1,250 2,500 5,000 7,500 10,000 Meters



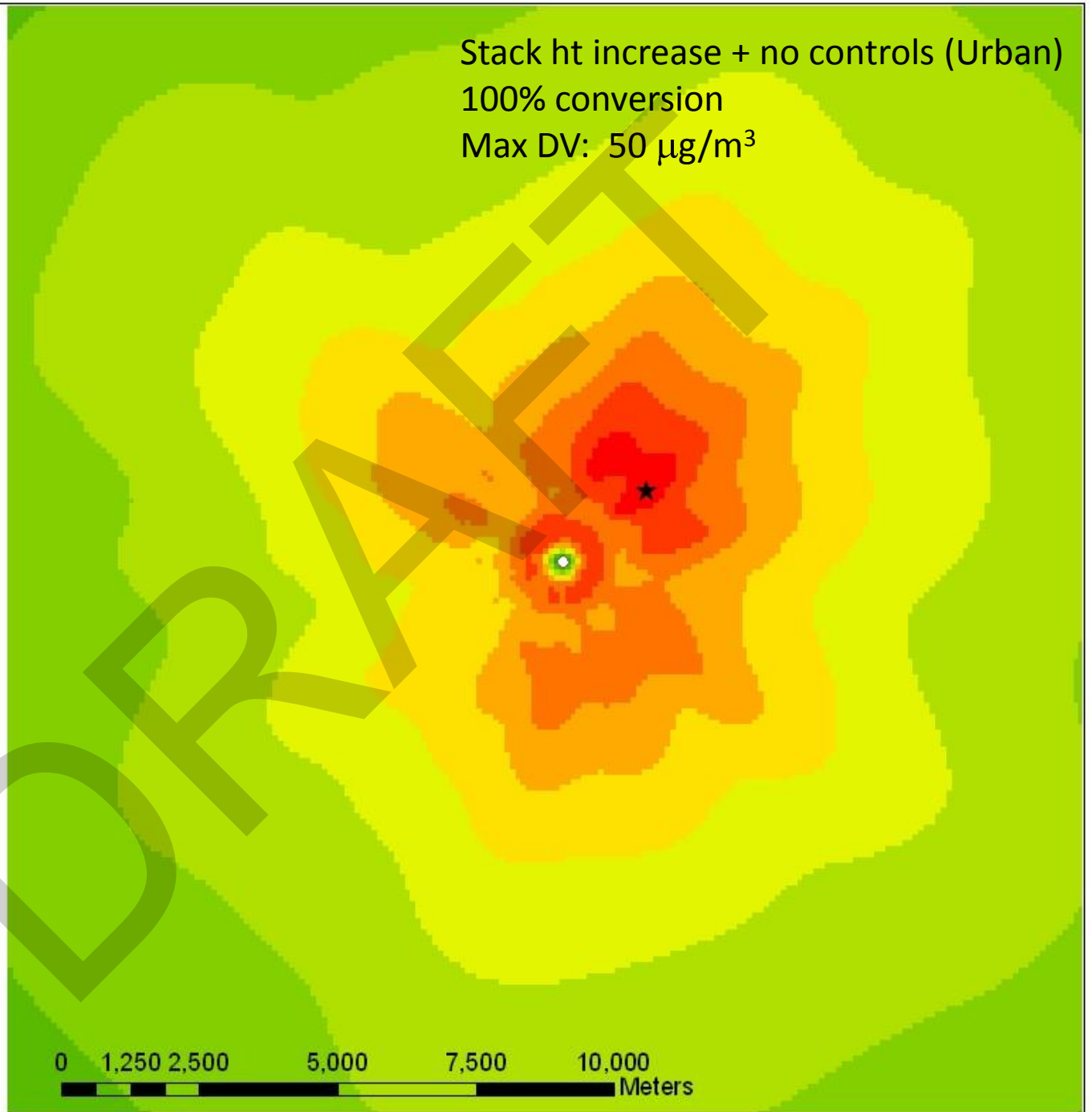
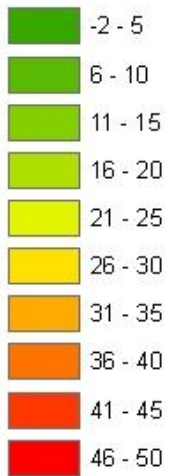
Stack ht increase (Urban)  
PVMRM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 9 μg/m<sup>3</sup>

### Legend



Stack ht increase + no controls (Urban)  
100% conversion  
Max DV: 50  $\mu\text{g}/\text{m}^3$

**Legend**



Stack ht increase + no controls (Urban)  
80% conversion  
Max DV: 40  $\mu\text{g}/\text{m}^3$

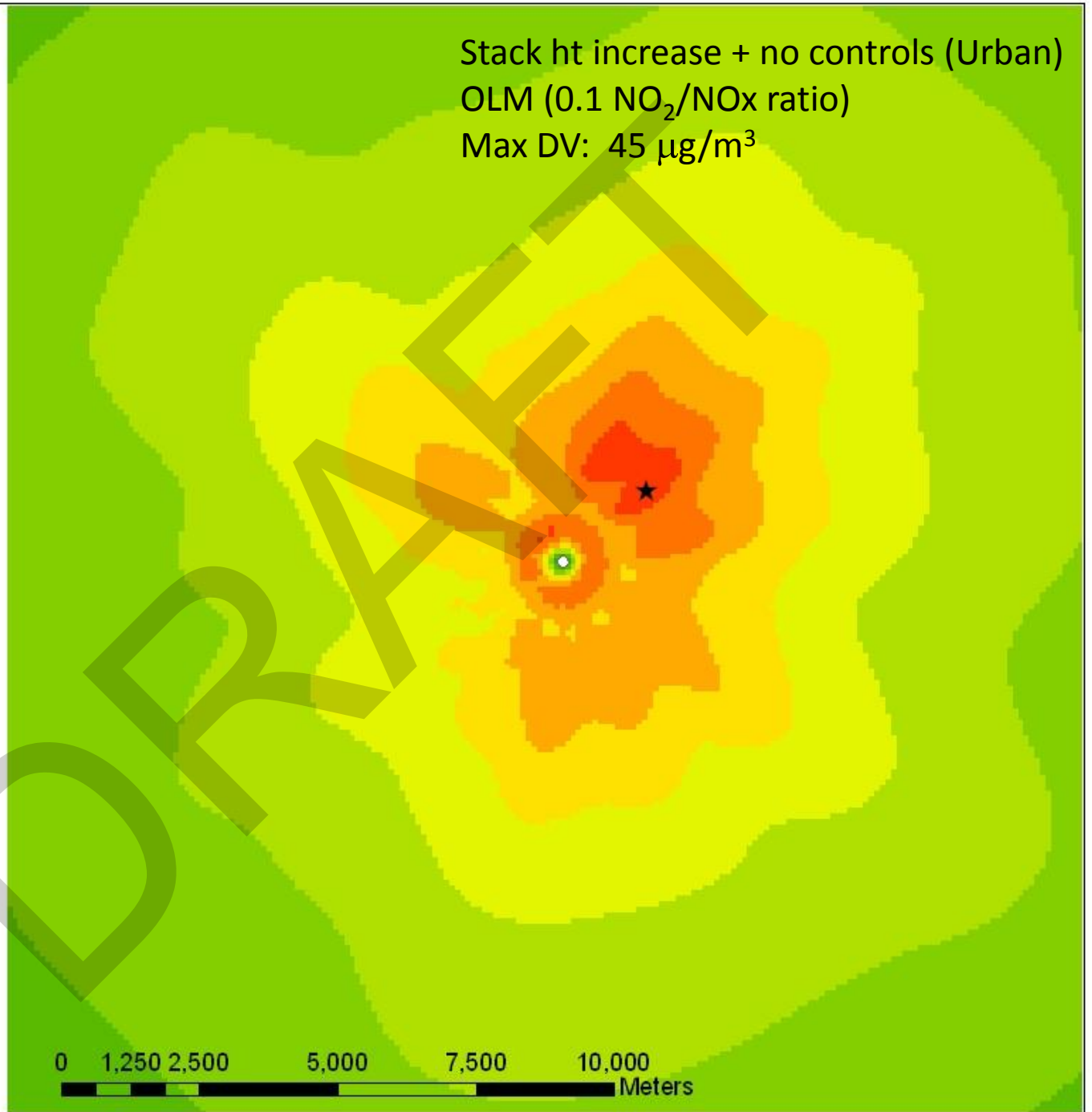
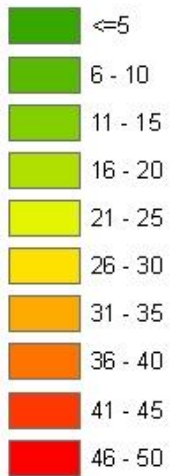
### Legend



0 1,250 2,500 5,000 7,500 10,000 Meters

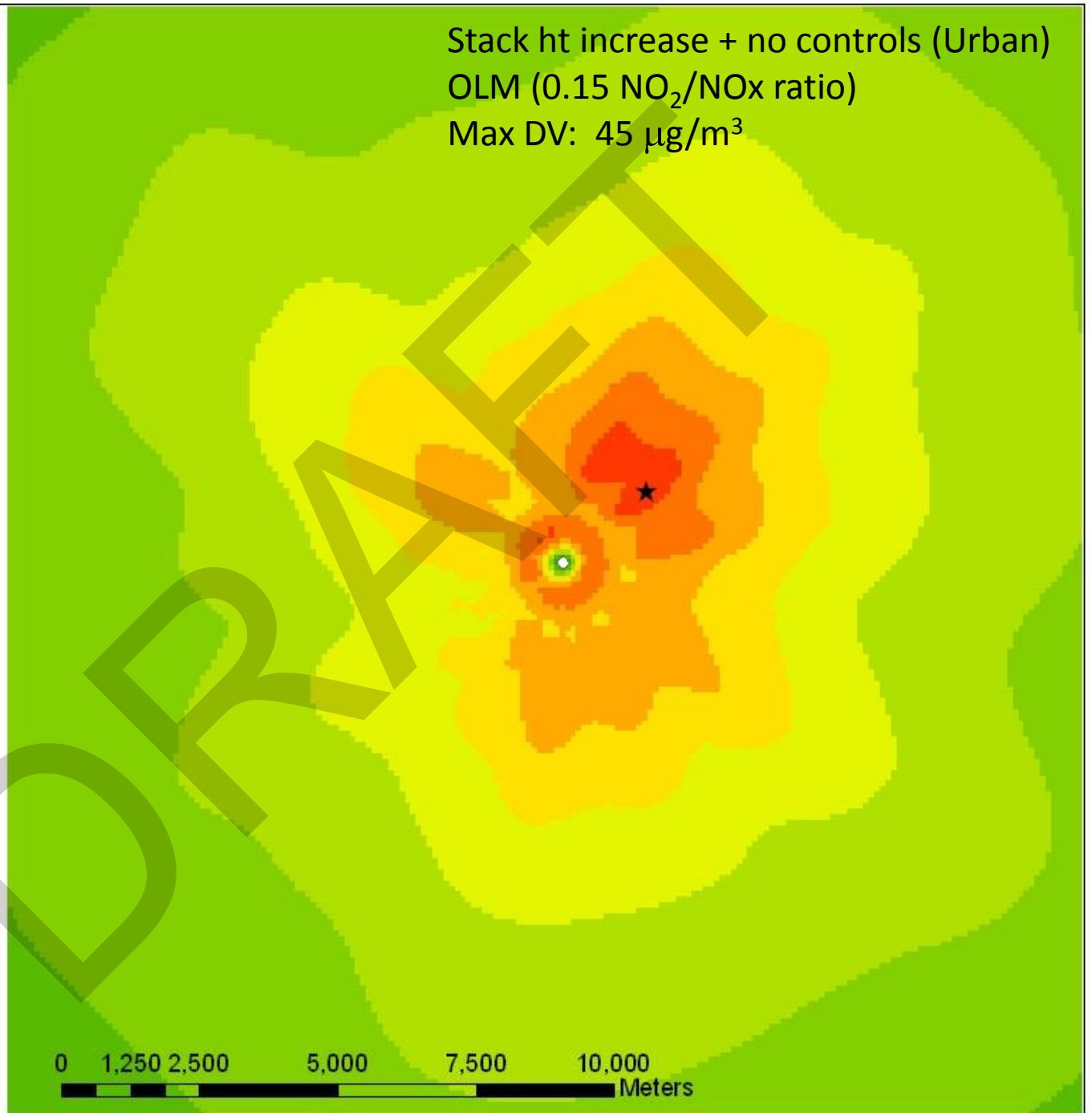
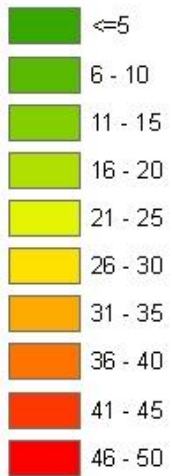
Stack ht increase + no controls (Urban)  
OLM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 45 μg/m<sup>3</sup>

### Legend



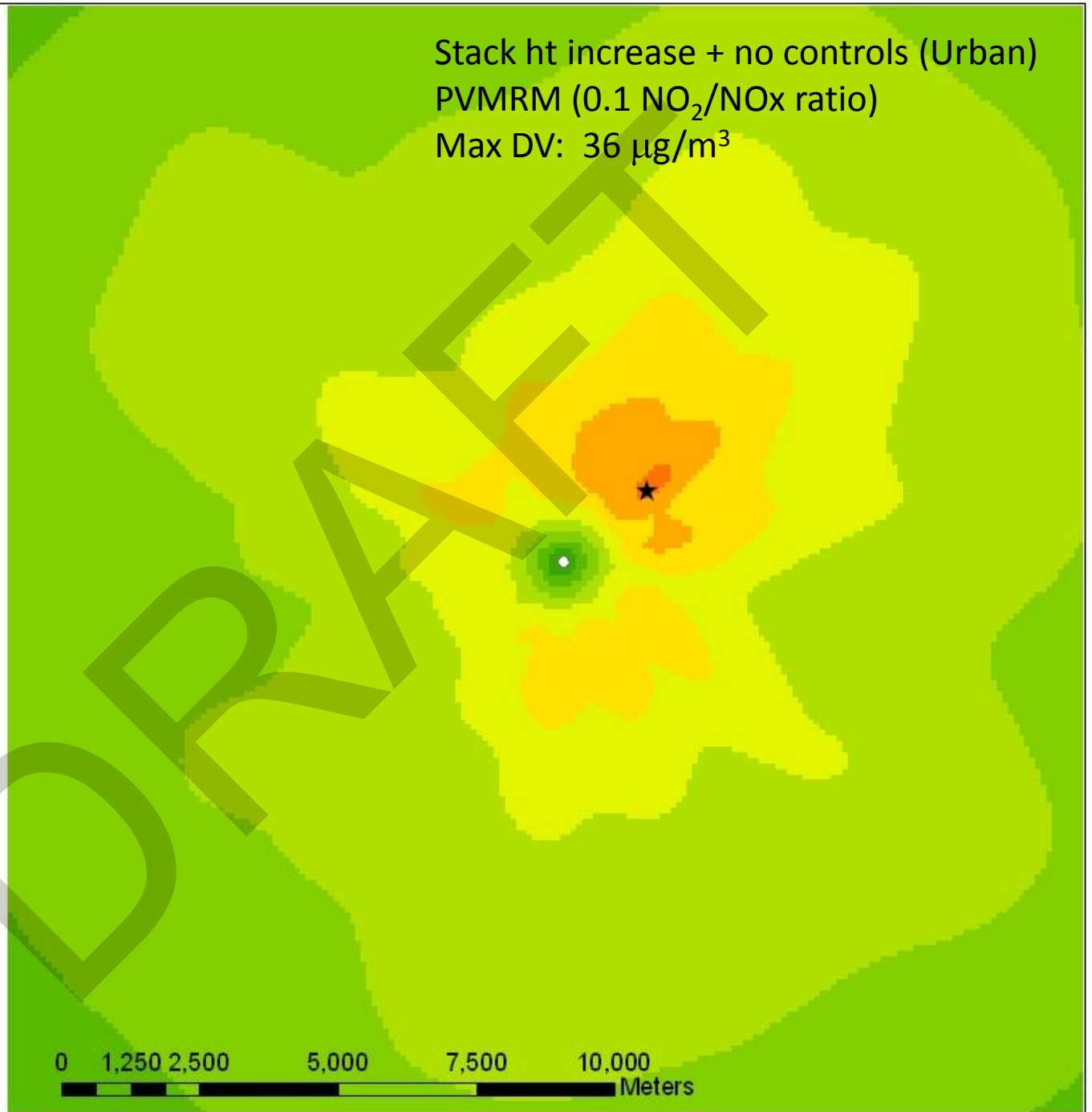
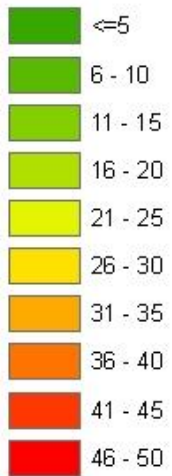
Stack ht increase + no controls (Urban)  
OLM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 45 μg/m<sup>3</sup>

### Legend



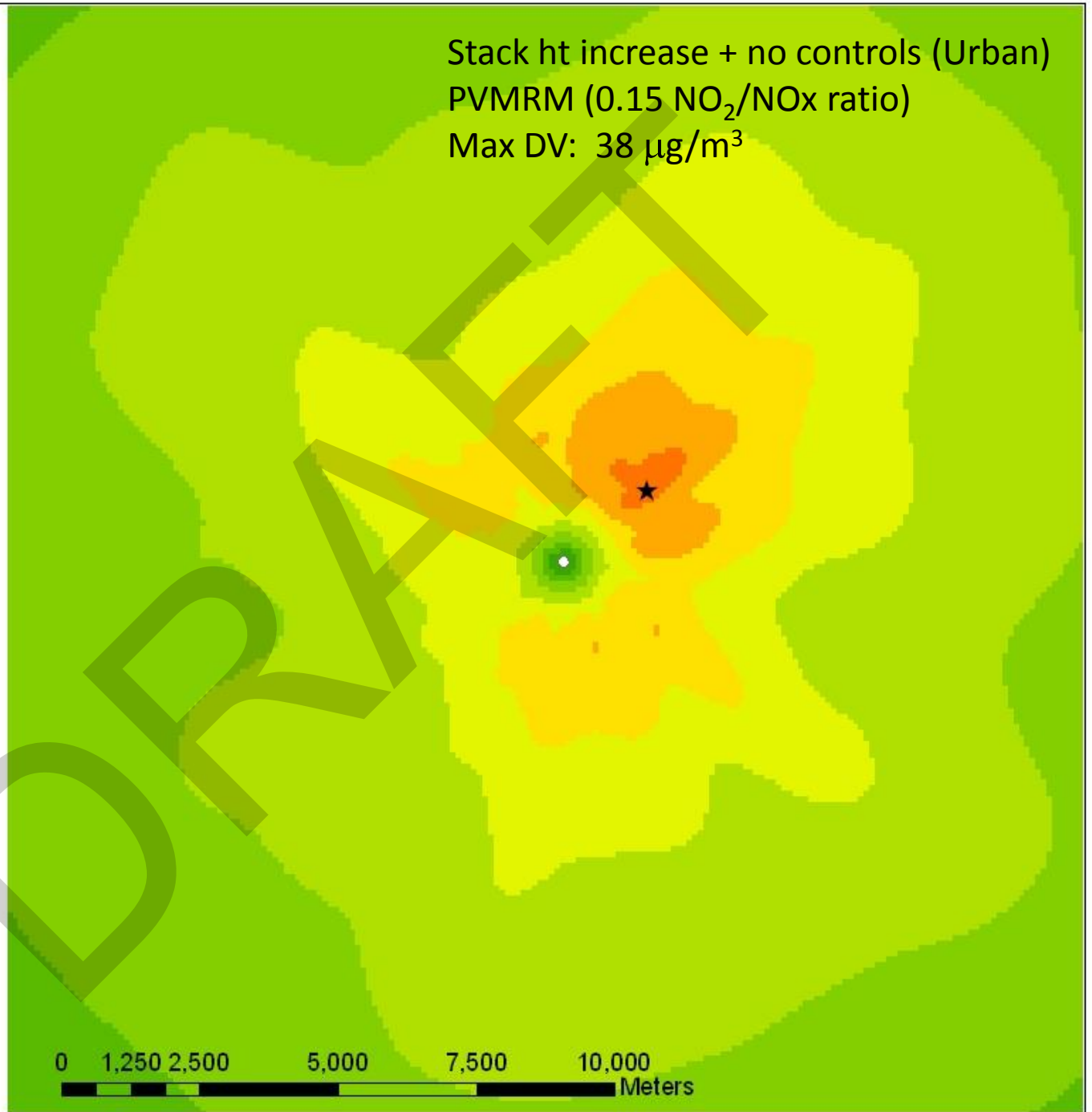
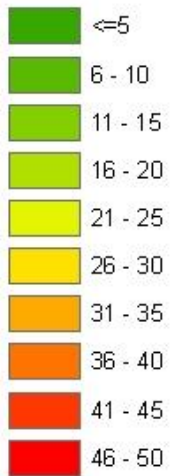
Stack ht increase + no controls (Urban)  
PVMRM (0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 36 μg/m<sup>3</sup>

### Legend

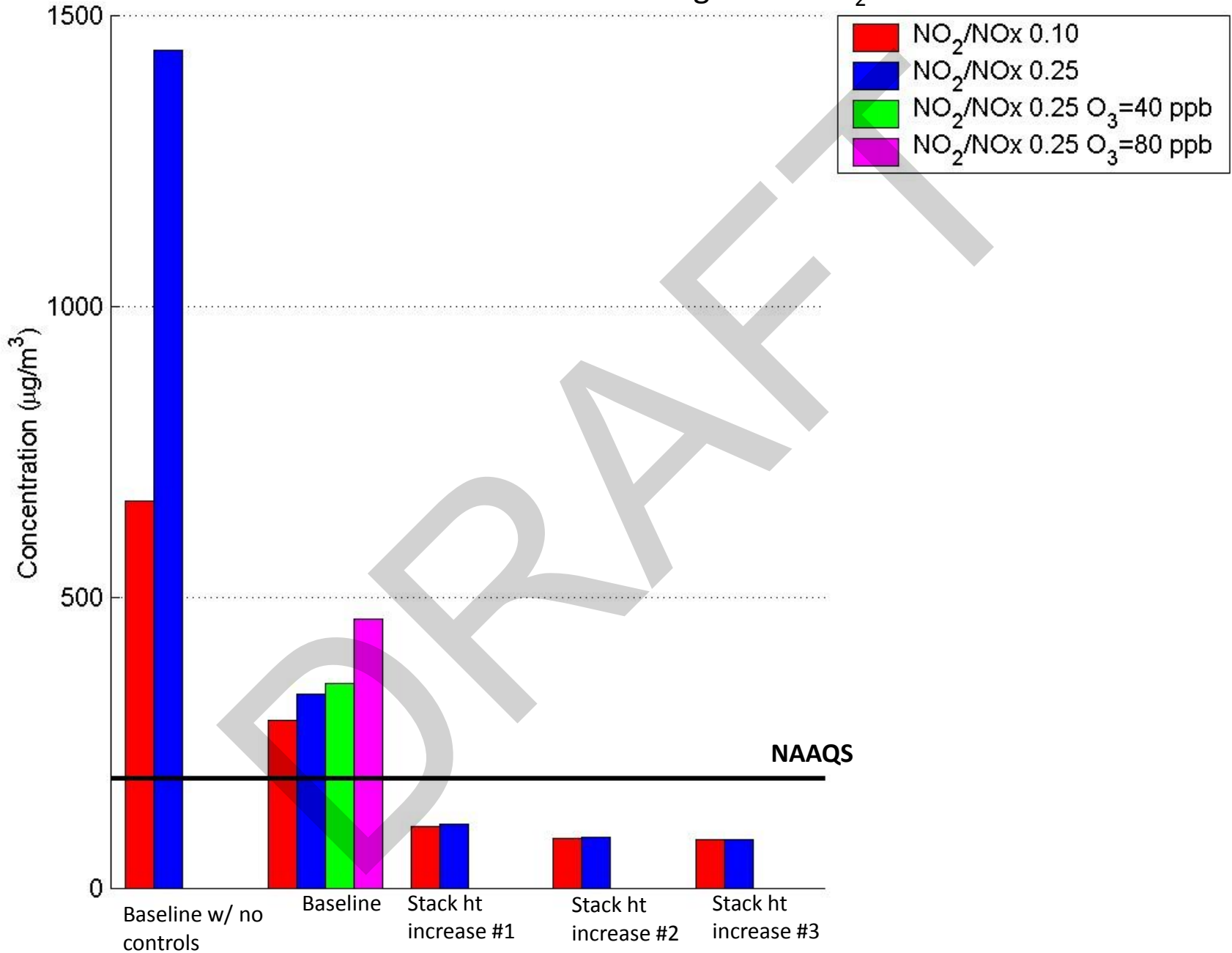


Stack ht increase + no controls (Urban)  
PVMRM (0.15 NO<sub>2</sub>/NO<sub>x</sub> ratio)  
Max DV: 38 μg/m<sup>3</sup>

### Legend



# Natural Gas Processing Plant: NO<sub>2</sub>





### Legend



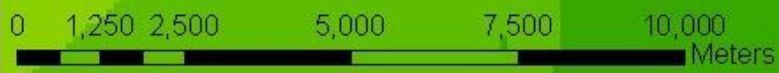
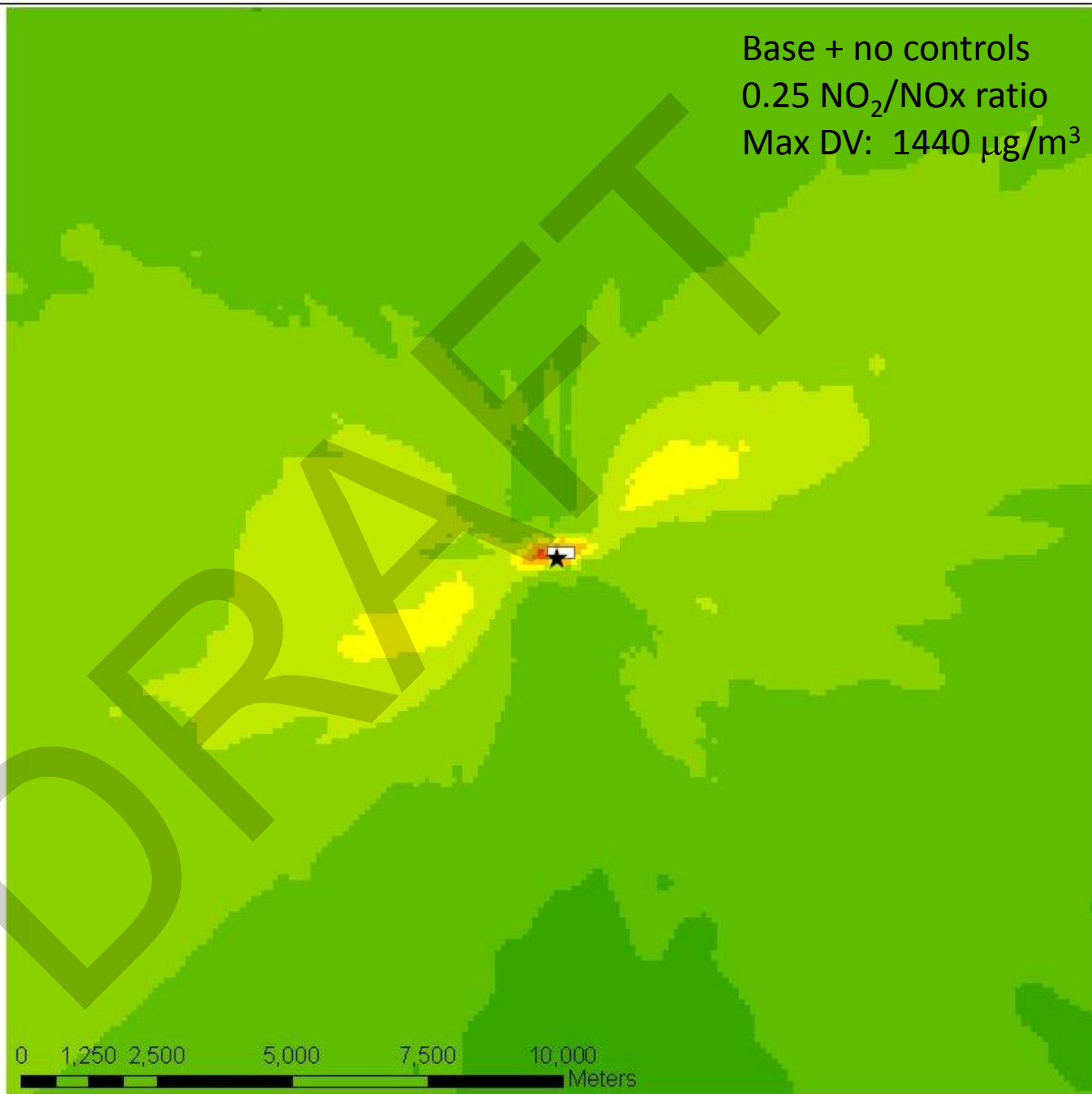
Base + no controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 665 µg/m<sup>3</sup>



### Legend



Base + no controls  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 1440 μg/m<sup>3</sup>



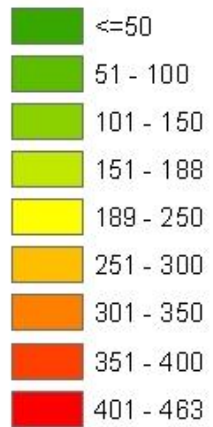
### Legend



Base  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 289 µg/m<sup>3</sup>



### Legend



Base  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 335 µg/m<sup>3</sup>

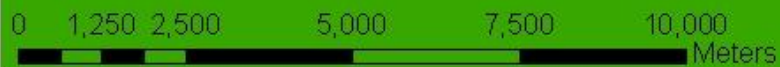


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### Legend



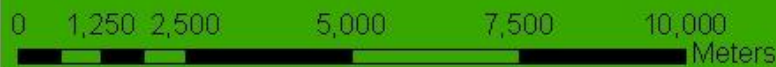
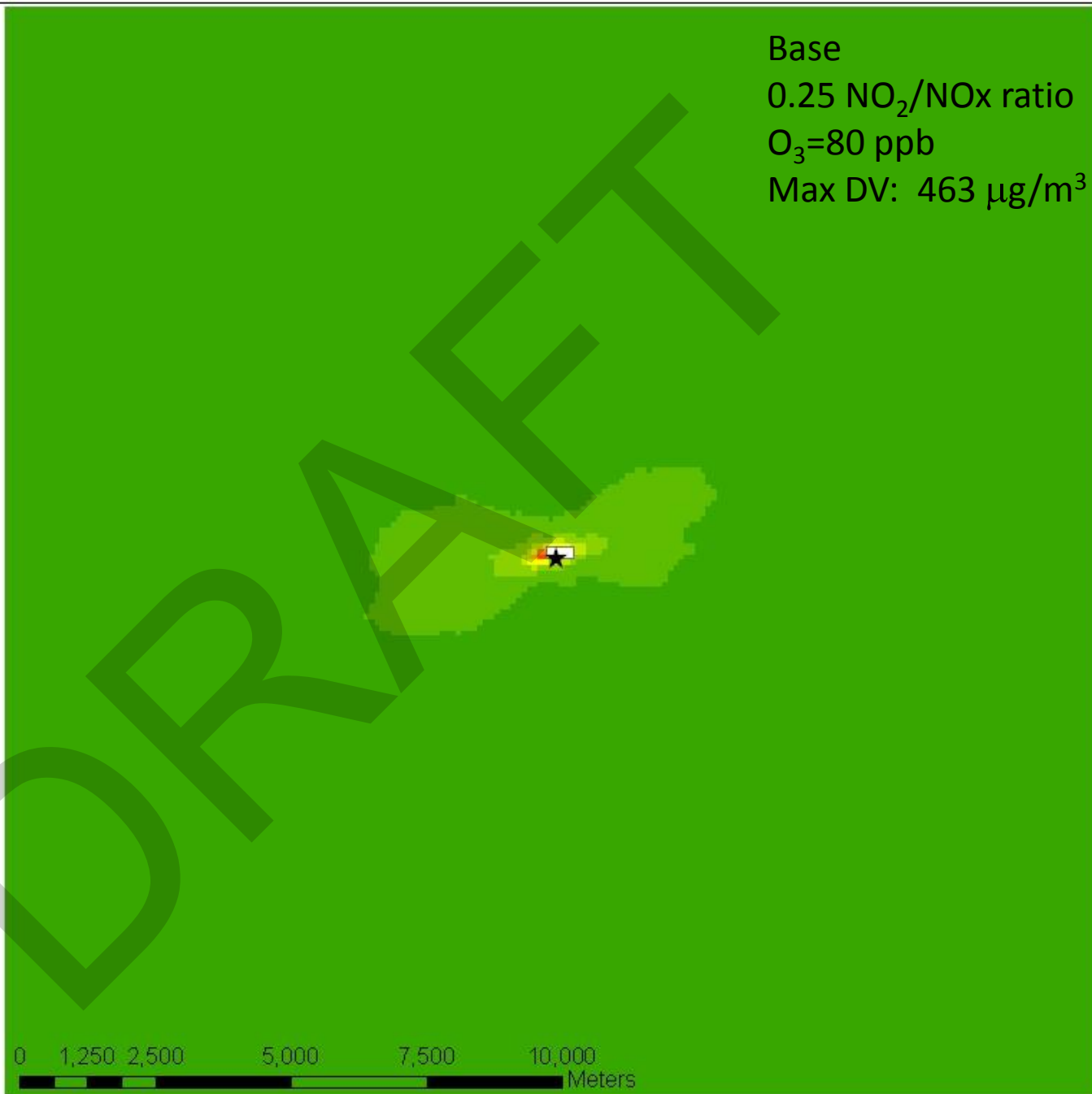
Base  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=40 ppb  
Max DV: 351 μg/m<sup>3</sup>



### Legend



Base  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=80 ppb  
Max DV: 463 μg/m<sup>3</sup>



### Legend

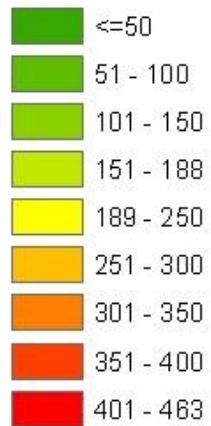


Stack ht increase #1  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 106 µg/m<sup>3</sup>

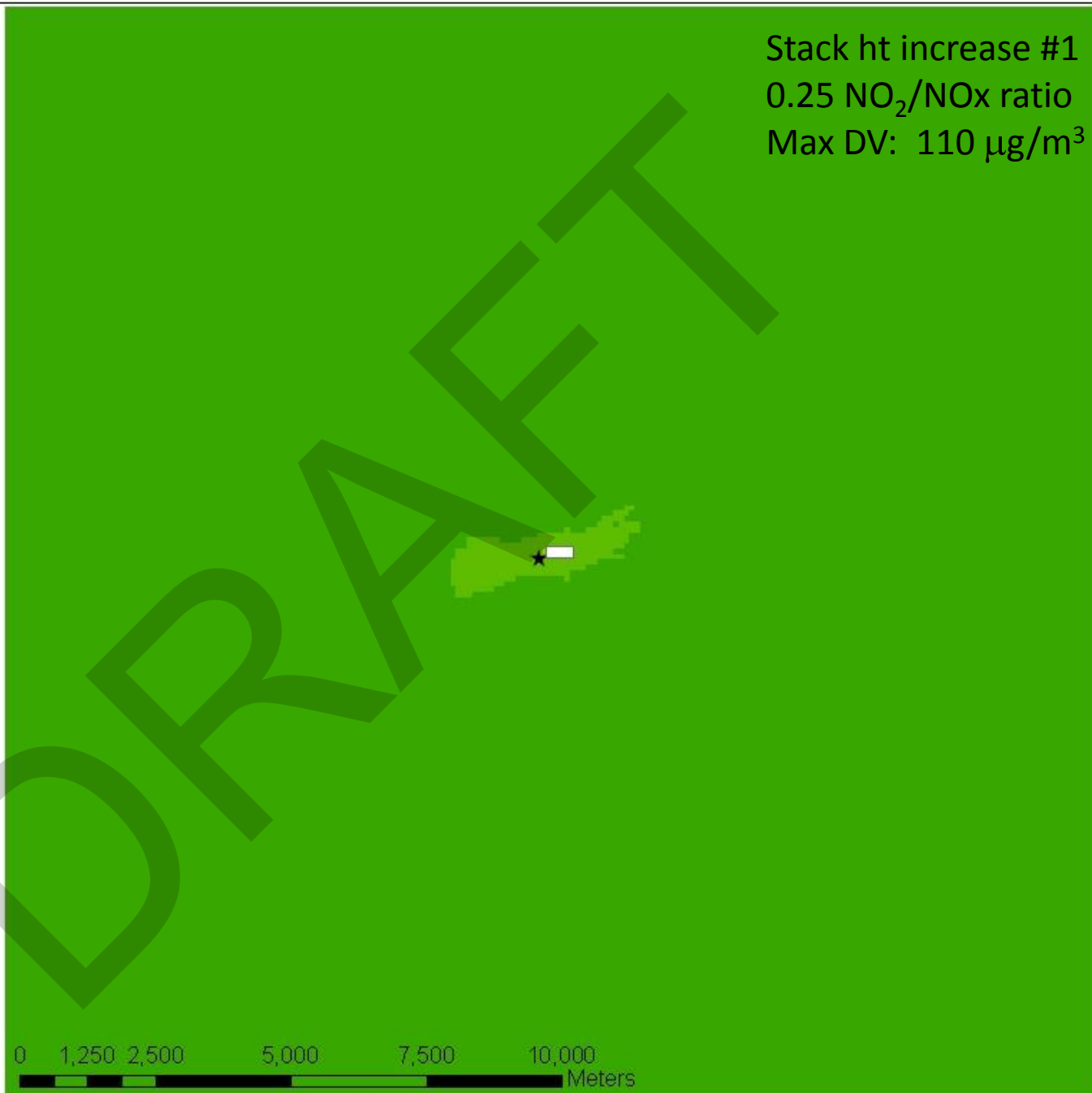


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### Legend



Stack ht increase #1  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 110 µg/m<sup>3</sup>

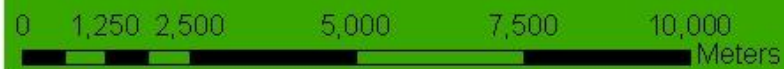




### Legend

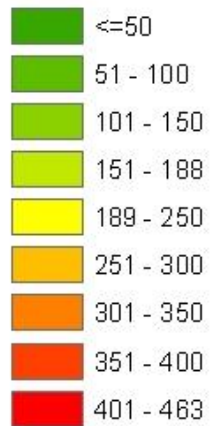


Stack ht increase #2  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 86 μg/m<sup>3</sup>

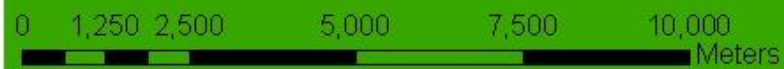


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### Legend



Stack ht increase #2  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 88 μg/m<sup>3</sup>

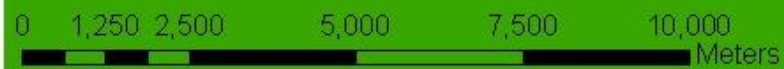


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### Legend

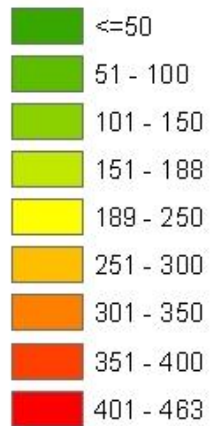


Stack ht increase #3  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 85 μg/m<sup>3</sup>

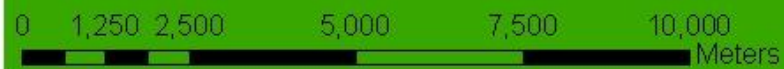


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### Legend

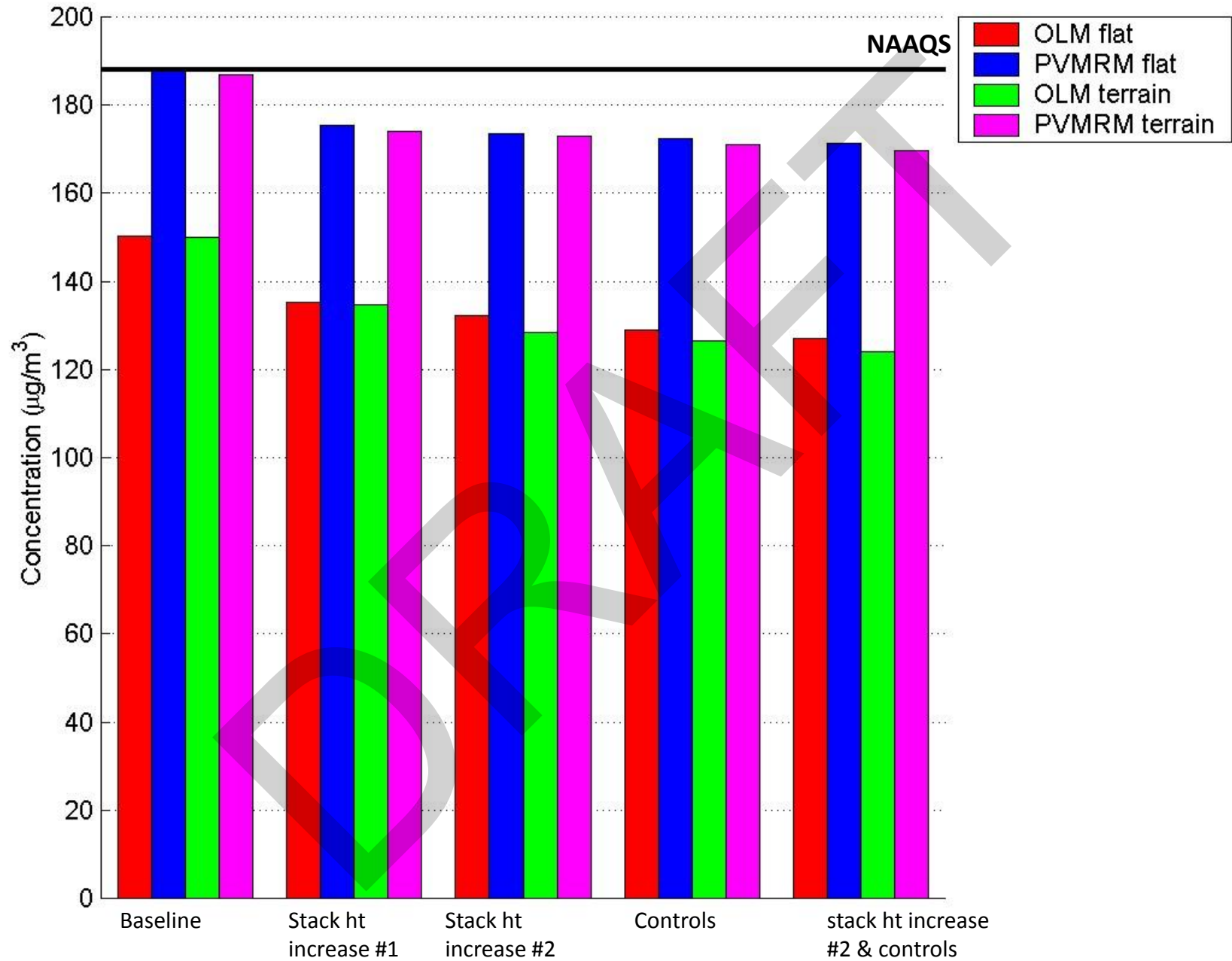


Stack ht increase #3  
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 85 μg/m<sup>3</sup>

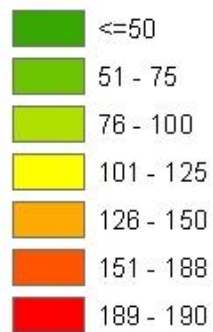


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# Refinery: NO<sub>2</sub>

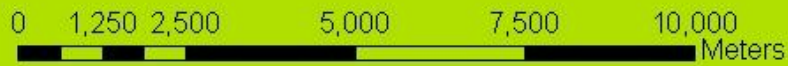


### Legend

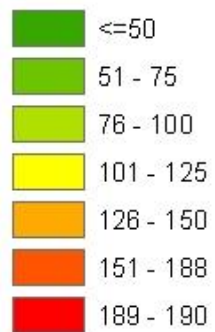


Base  
OLM/Flat  
Max DV: 150  $\mu\text{g}/\text{m}^3$

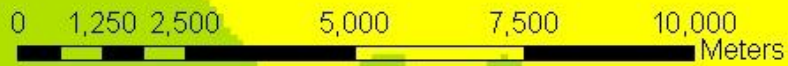
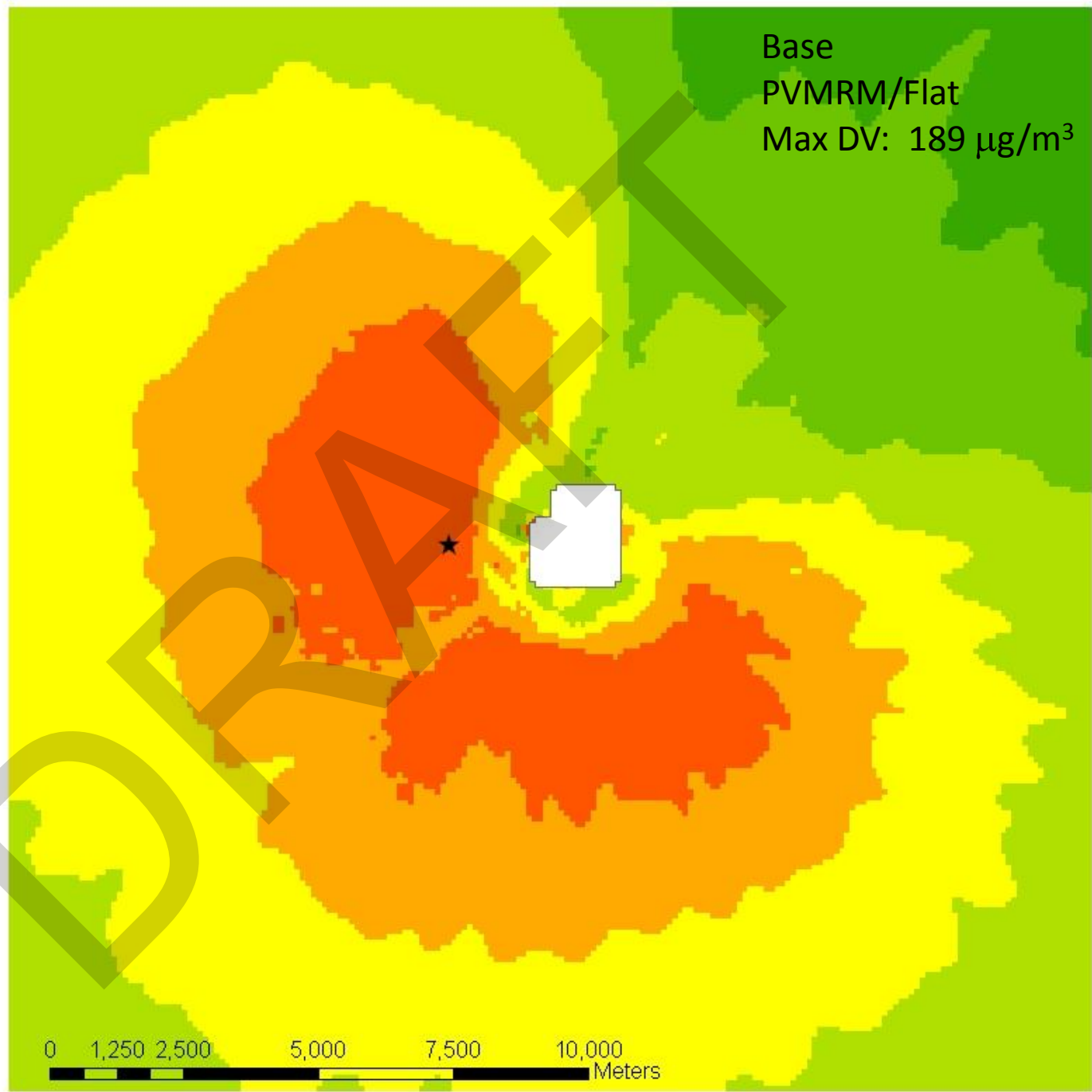
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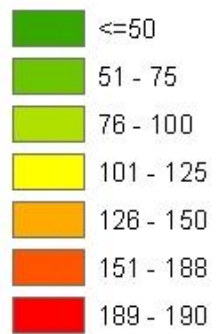
**Legend**



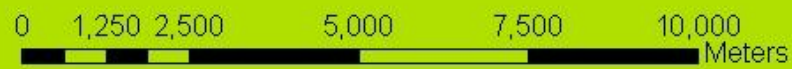
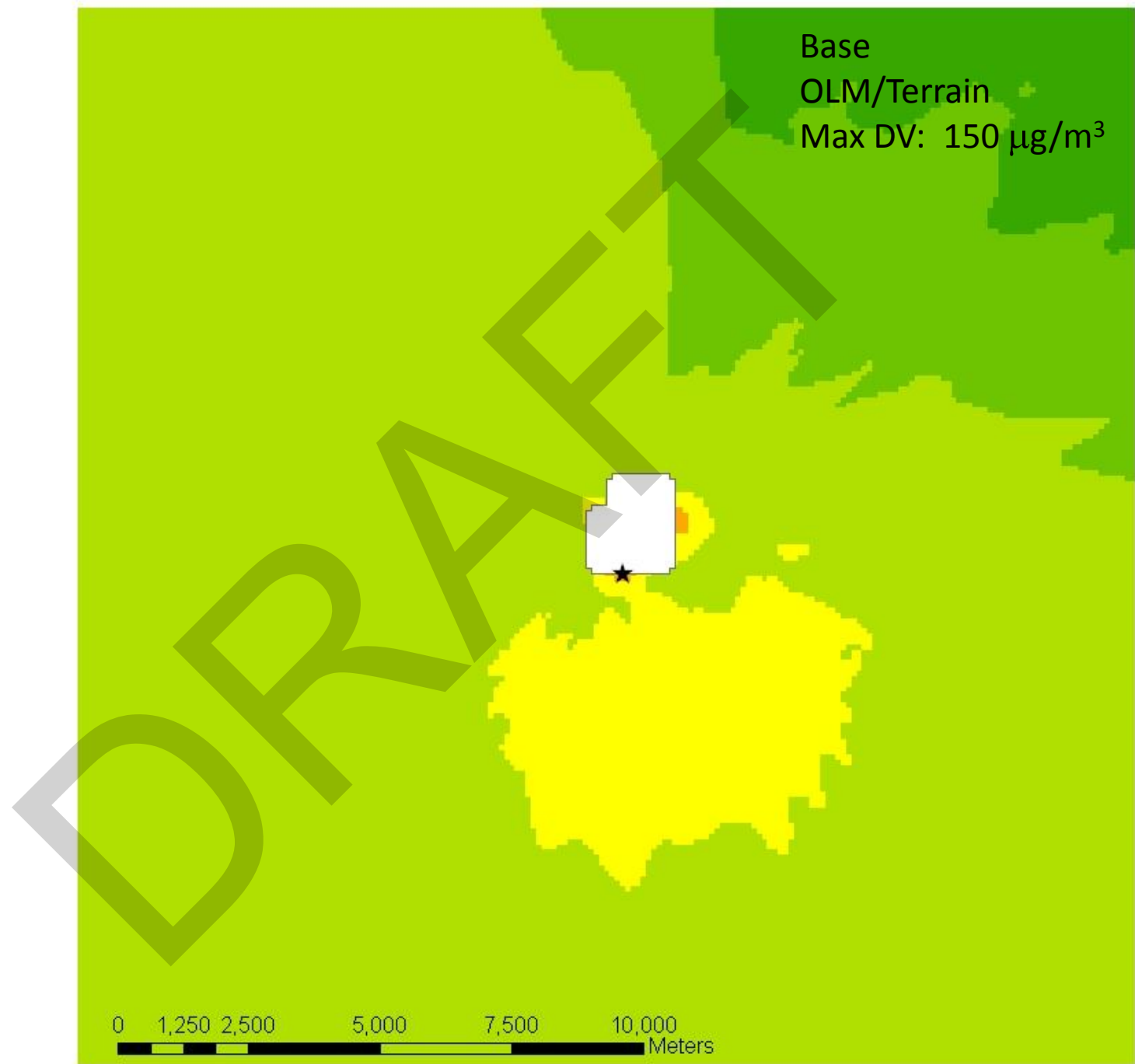
Base  
PVMRM/Flat  
Max DV: 189  $\mu\text{g}/\text{m}^3$



### Legend

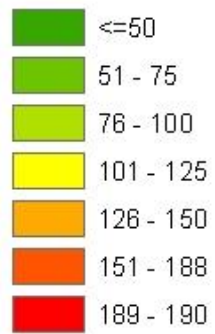


Base  
OLM/Terrain  
Max DV: 150  $\mu\text{g}/\text{m}^3$

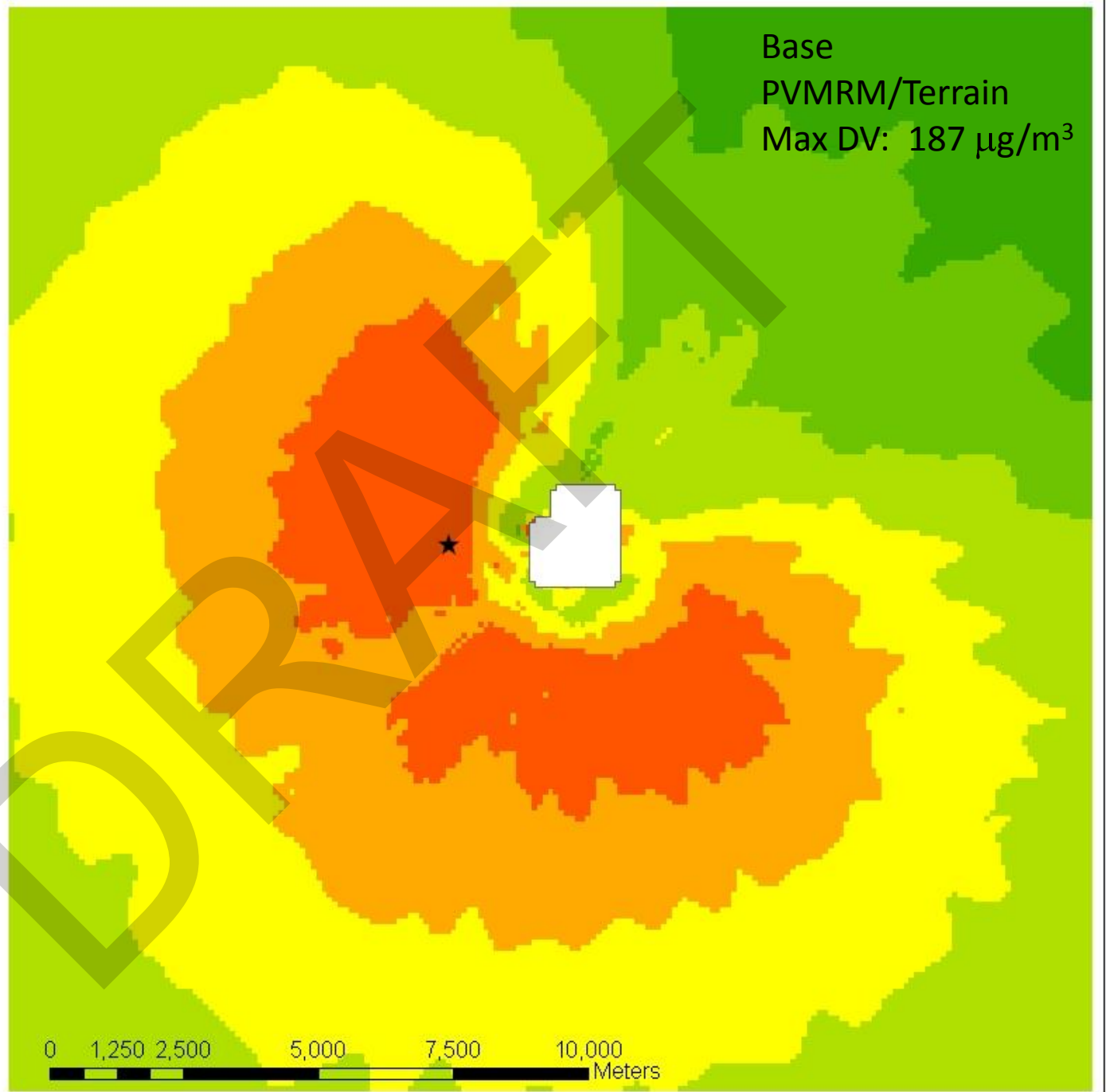




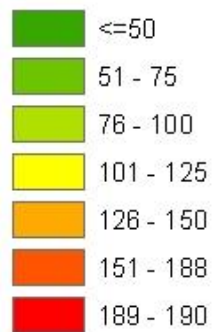
### Legend



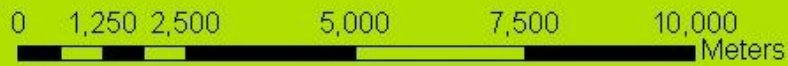
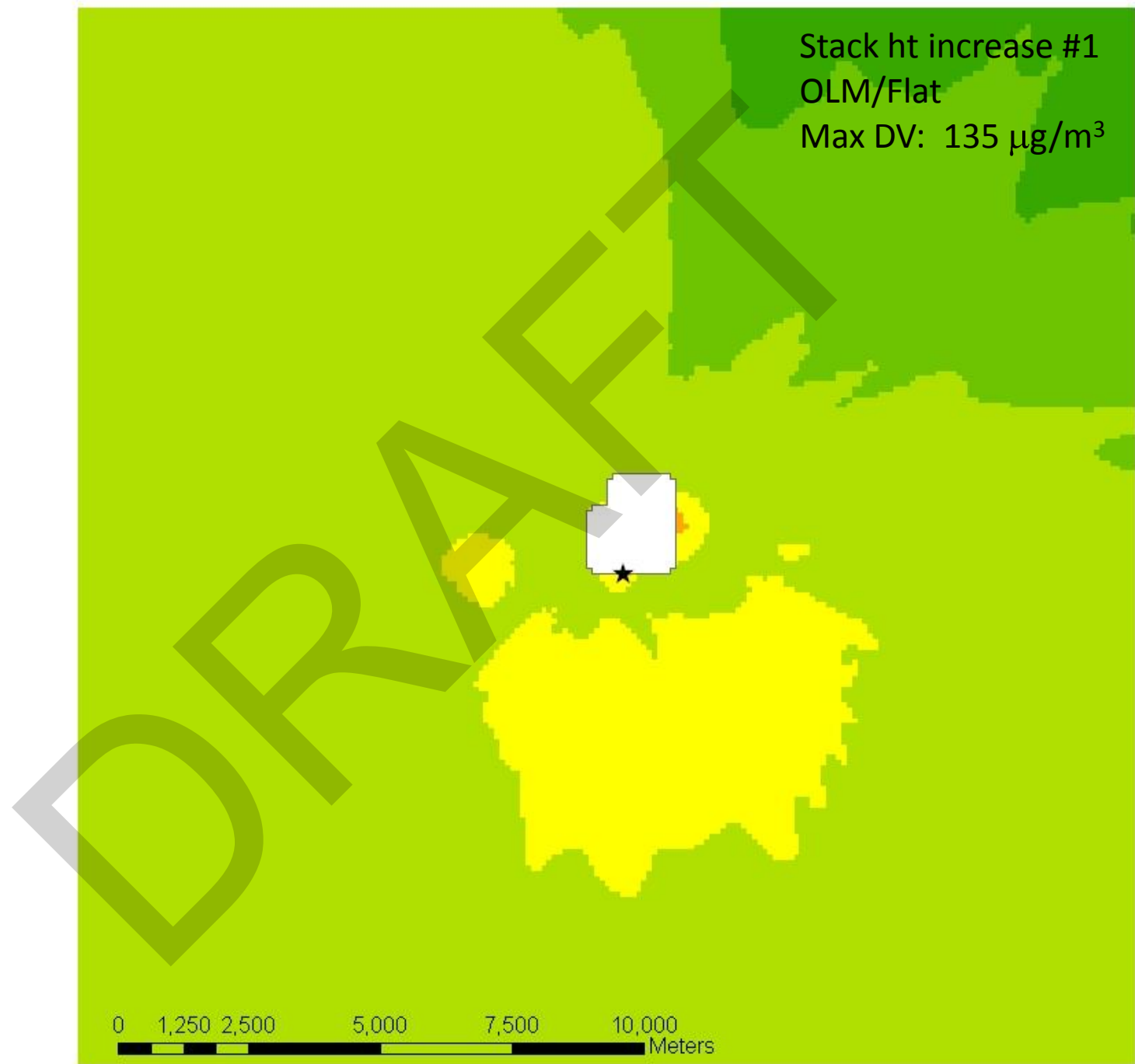
Base  
PVMRM/Terrain  
Max DV: 187  $\mu\text{g}/\text{m}^3$



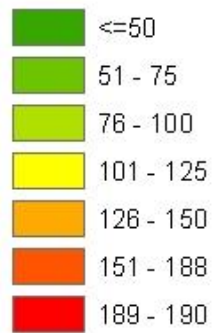
**Legend**



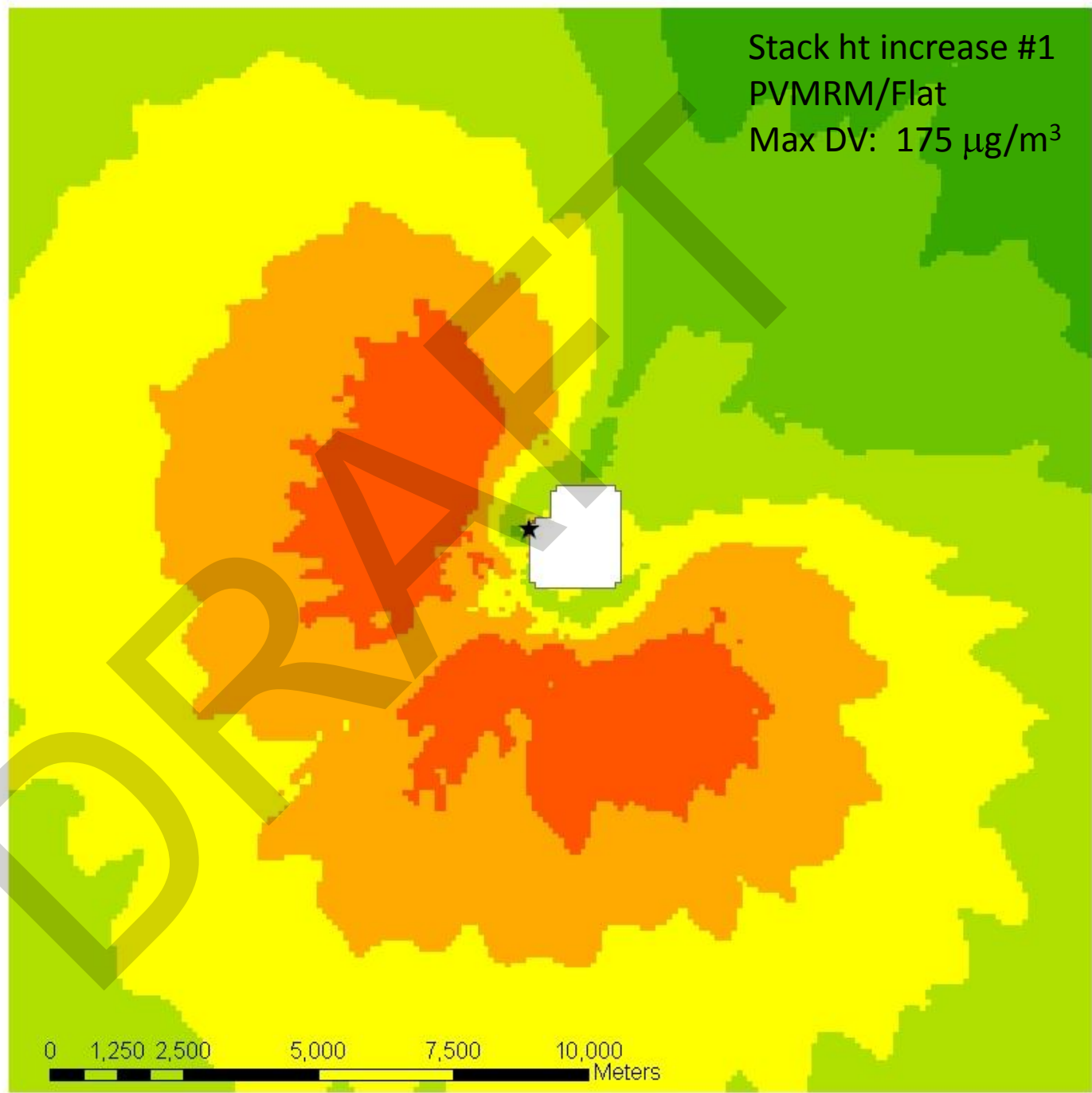
Stack ht increase #1  
OLM/Flat  
Max DV: 135  $\mu\text{g}/\text{m}^3$



### Legend

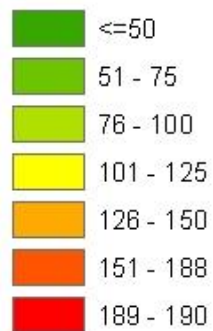


Stack ht increase #1  
PVMRM/Flat  
Max DV:  $175 \mu\text{g}/\text{m}^3$

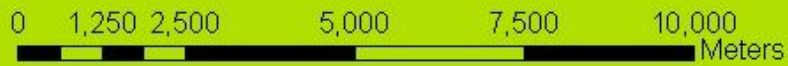
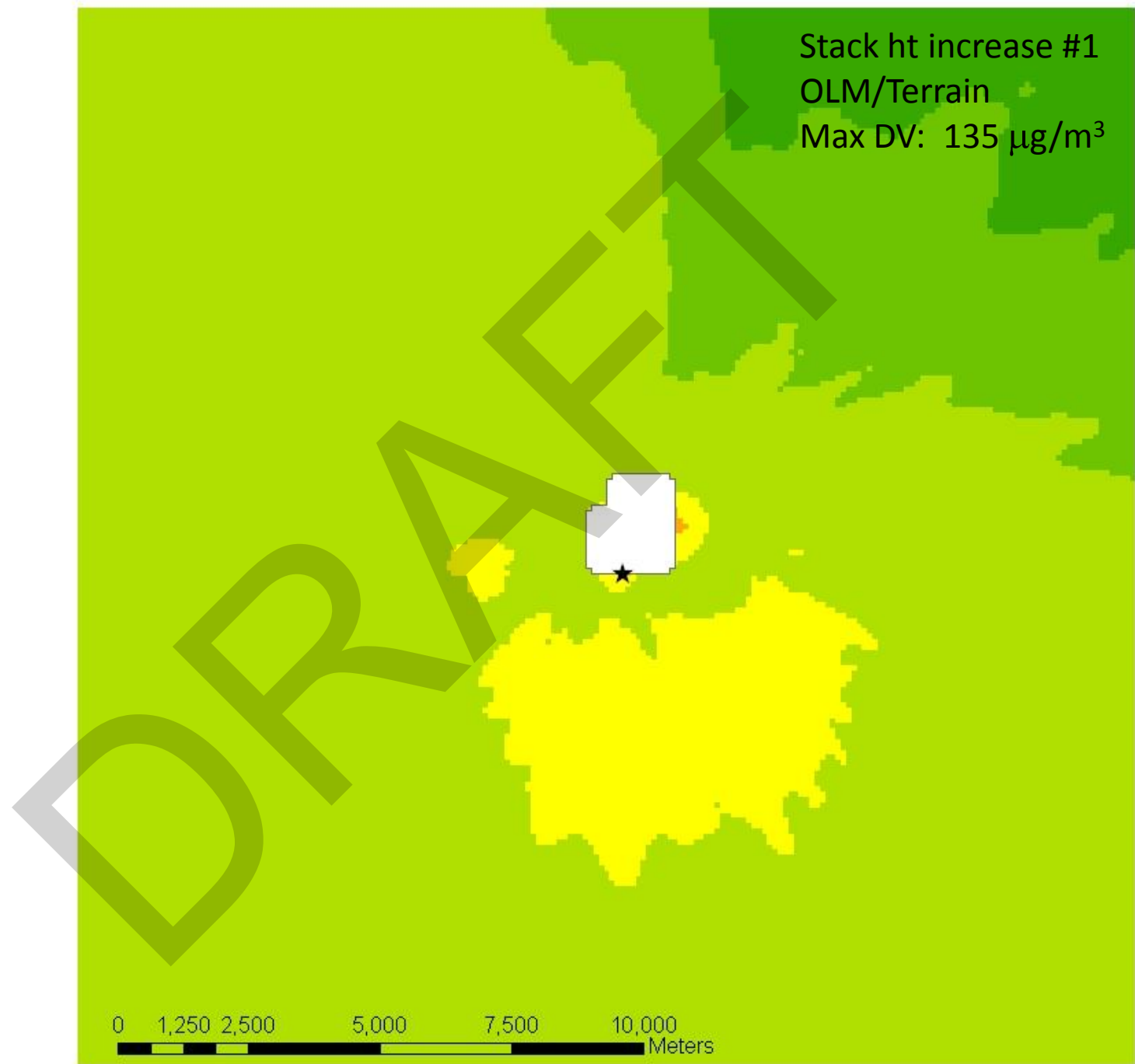


0 1,250 2,500 5,000 7,500 10,000  
Meters

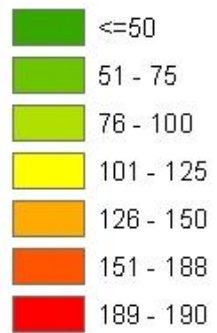
**Legend**



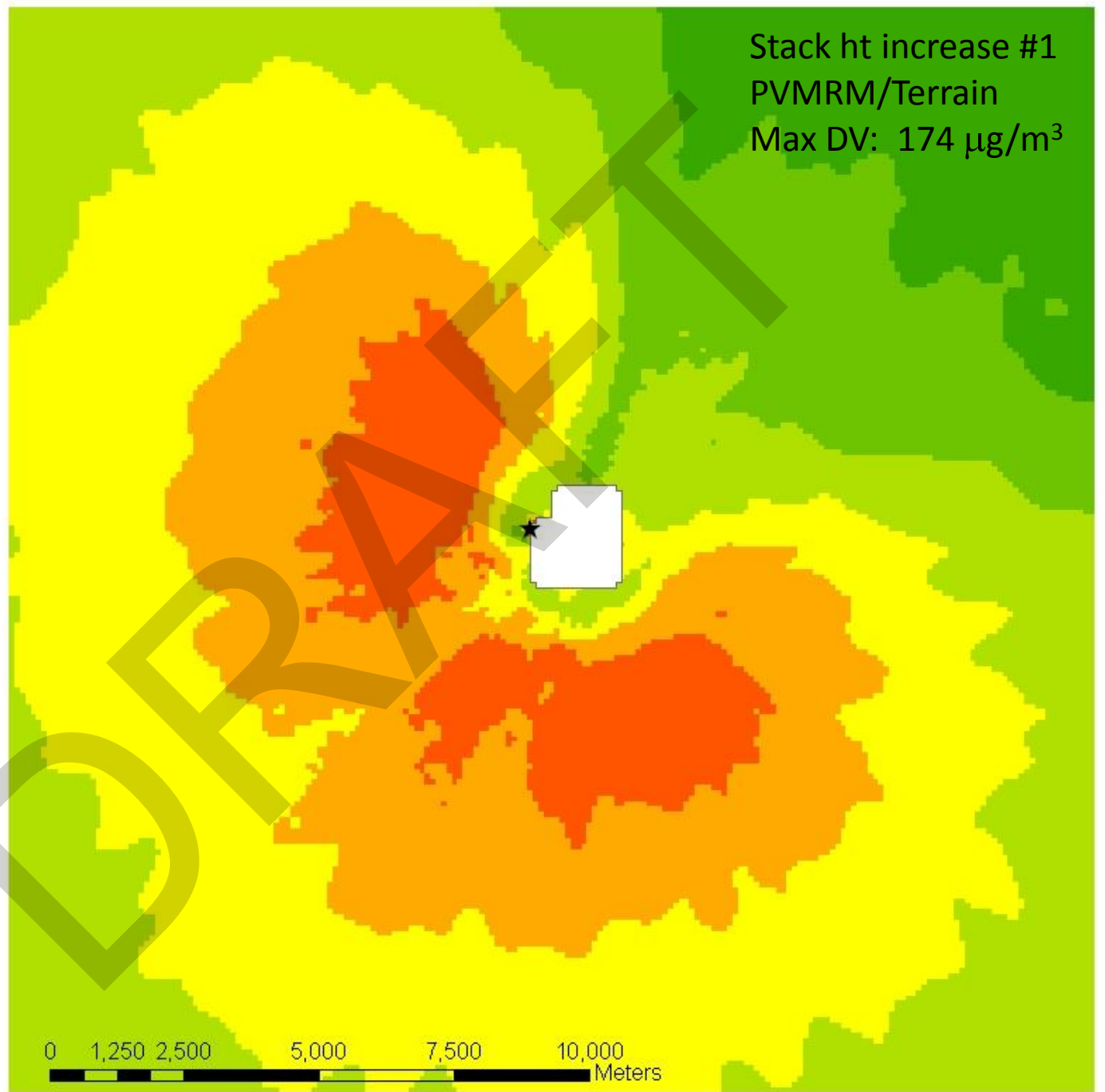
Stack ht increase #1  
OLM/Terrain  
Max DV: 135  $\mu\text{g}/\text{m}^3$



### Legend



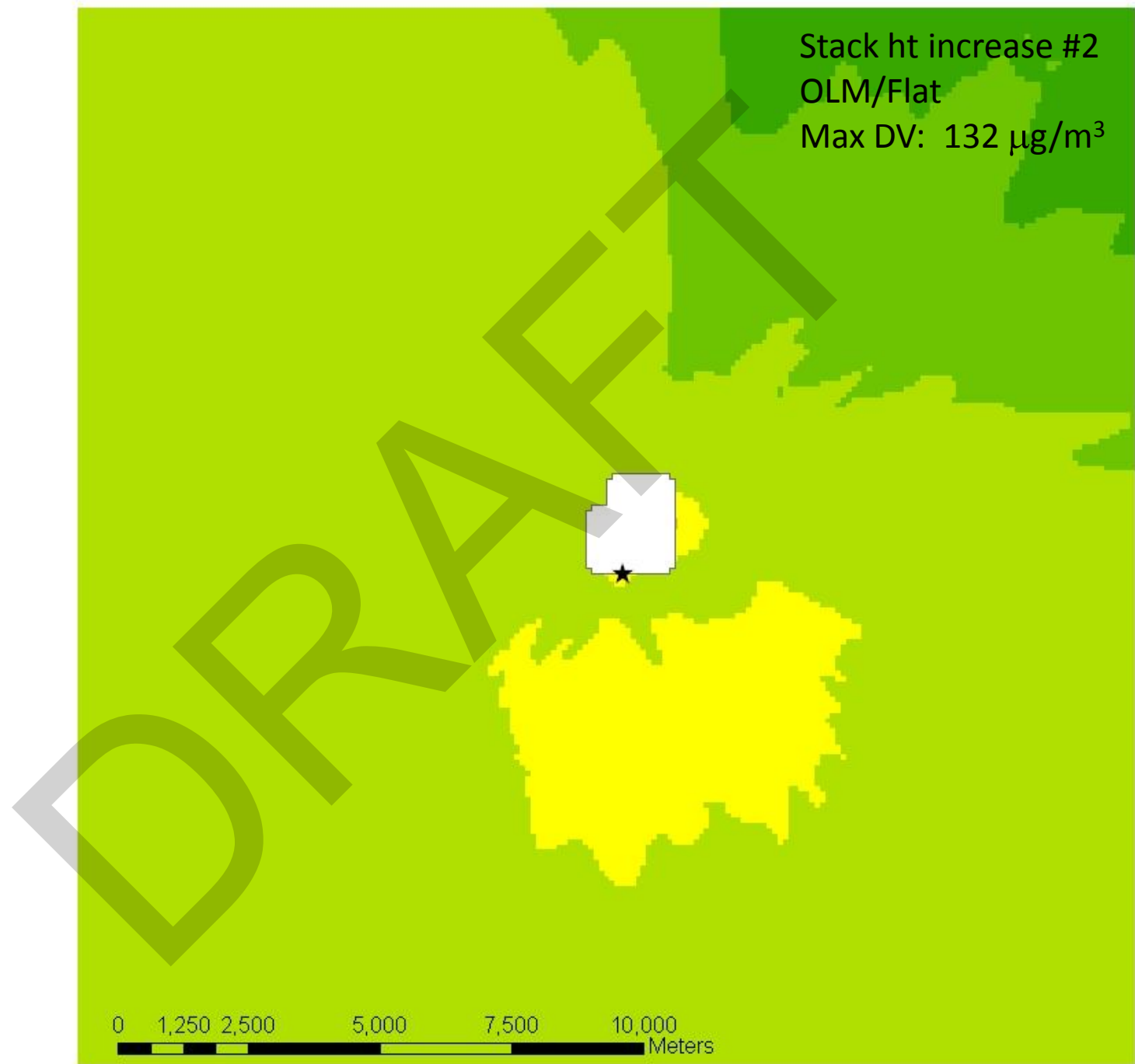
Stack ht increase #1  
PVMRM/Terrain  
Max DV:  $174 \mu\text{g}/\text{m}^3$



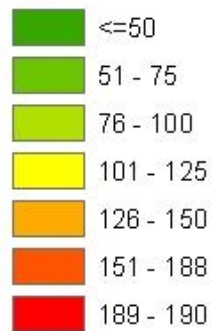
### Legend



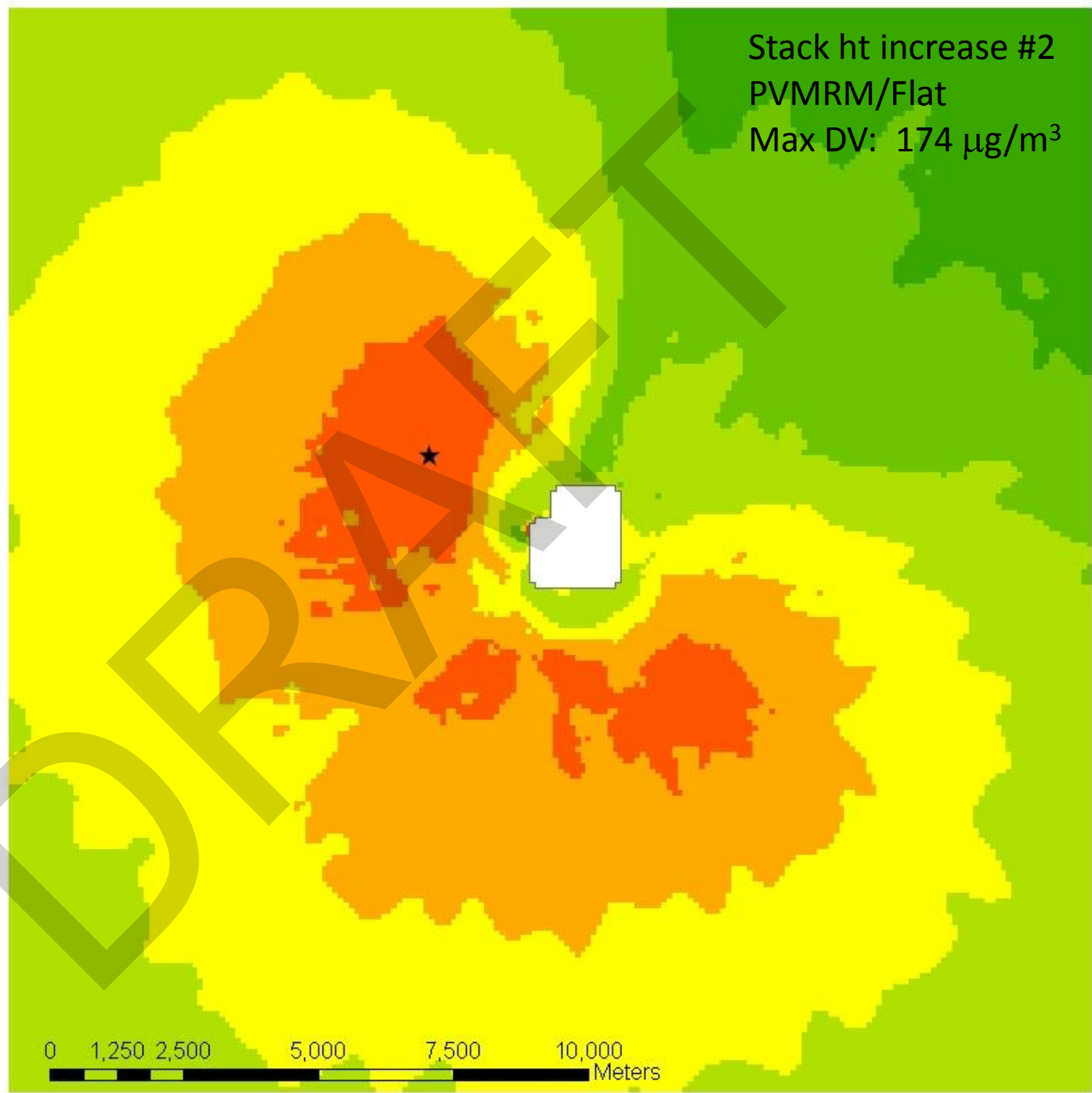
Stack ht increase #2  
OLM/Flat  
Max DV: 132  $\mu\text{g}/\text{m}^3$



### Legend

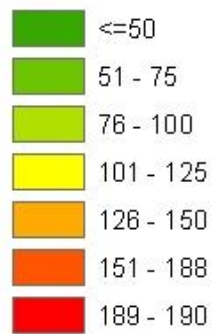


Stack ht increase #2  
PVMRM/Flat  
Max DV: 174  $\mu\text{g}/\text{m}^3$

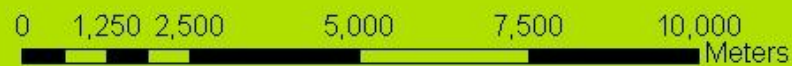
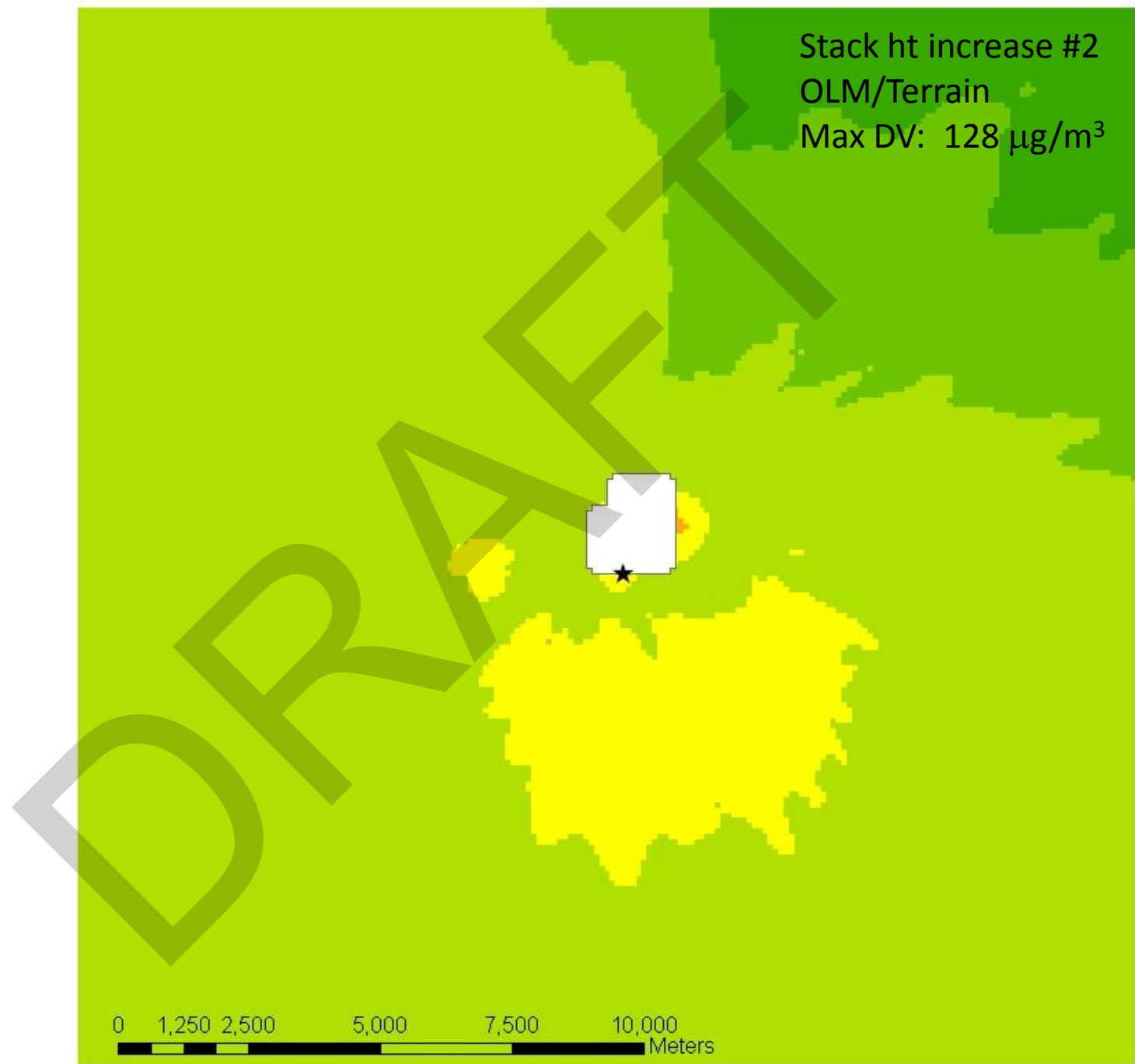


0 1,250 2,500 5,000 7,500 10,000  
Meters

### Legend

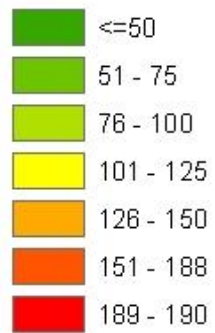


Stack ht increase #2  
OLM/Terrain  
Max DV: 128  $\mu\text{g}/\text{m}^3$

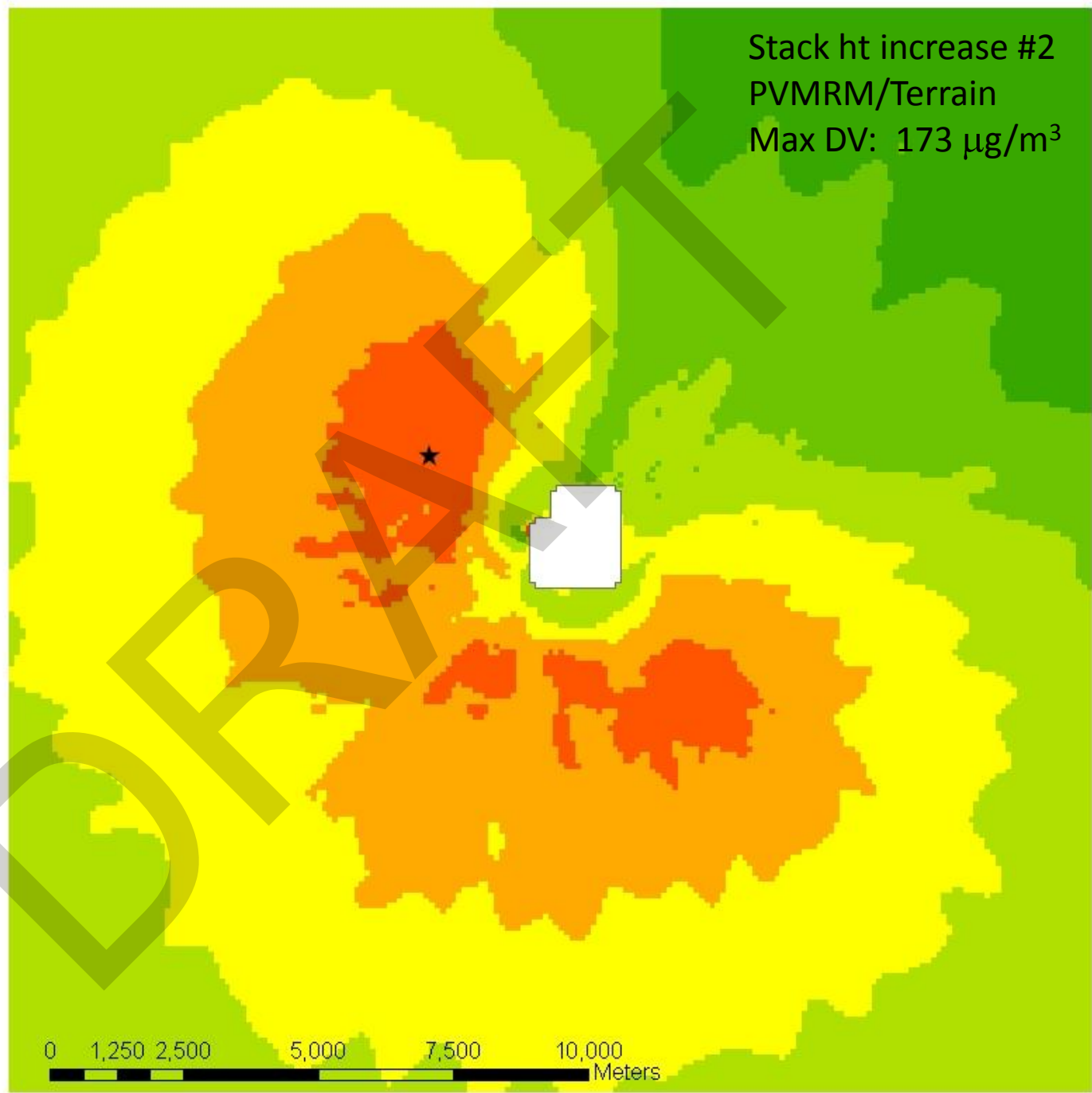




### Legend



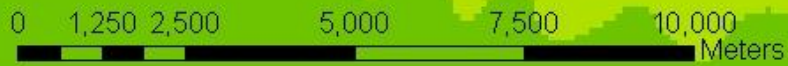
Stack ht increase #2  
PVMRM/Terrain  
Max DV: 173  $\mu\text{g}/\text{m}^3$



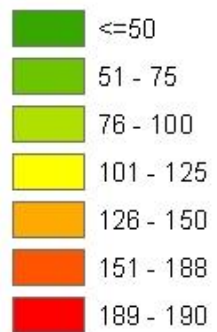
### Legend



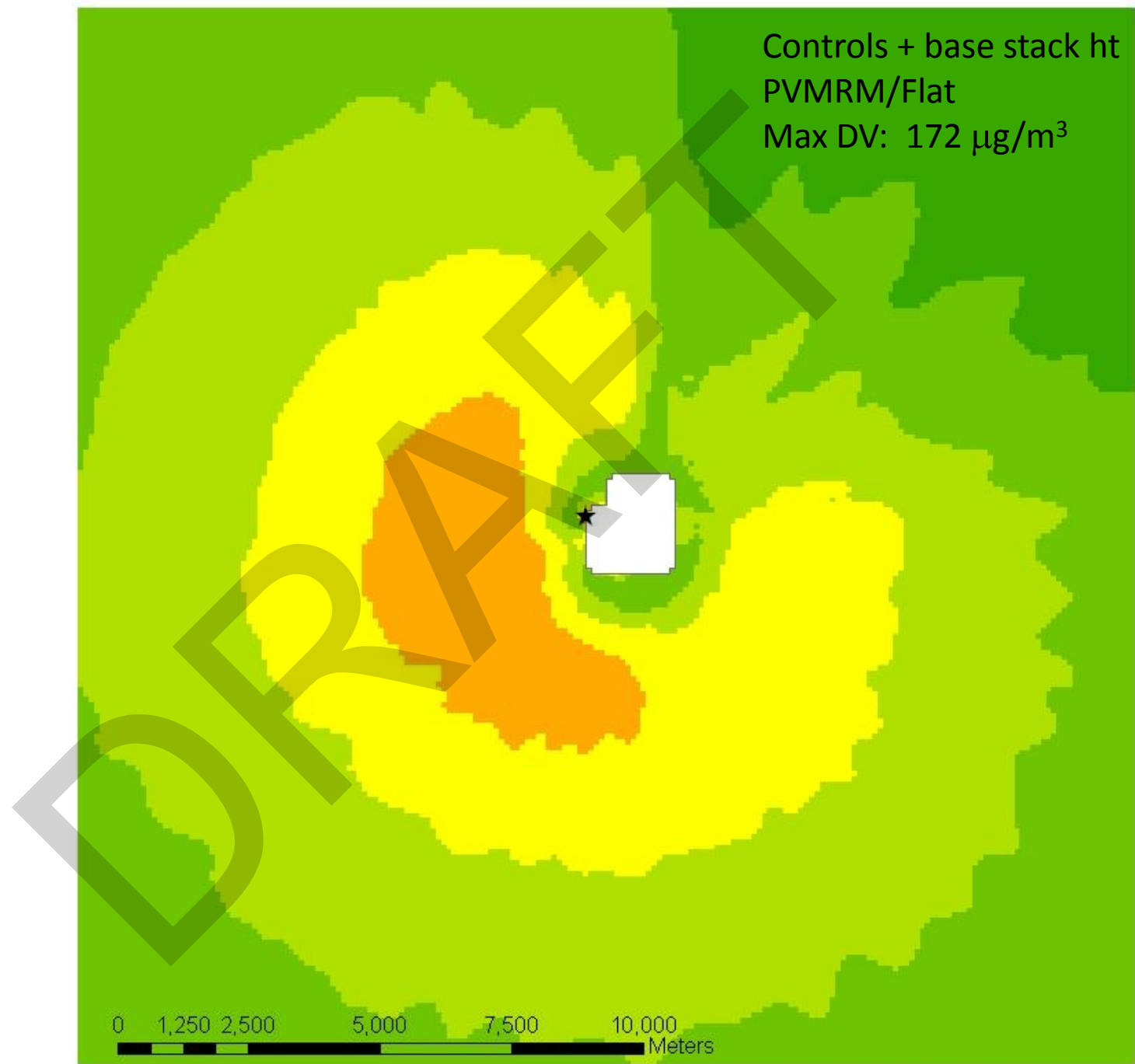
Controls + base stack ht  
OLM/Flat  
Max DV: 129  $\mu\text{g}/\text{m}^3$



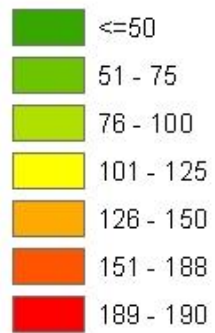
### Legend



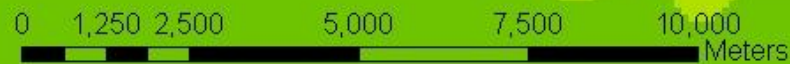
Controls + base stack ht  
PVMRM/Flat  
Max DV: 172  $\mu\text{g}/\text{m}^3$



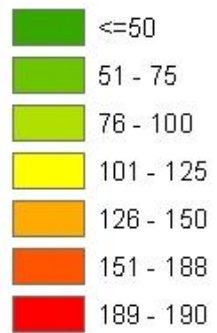
### Legend



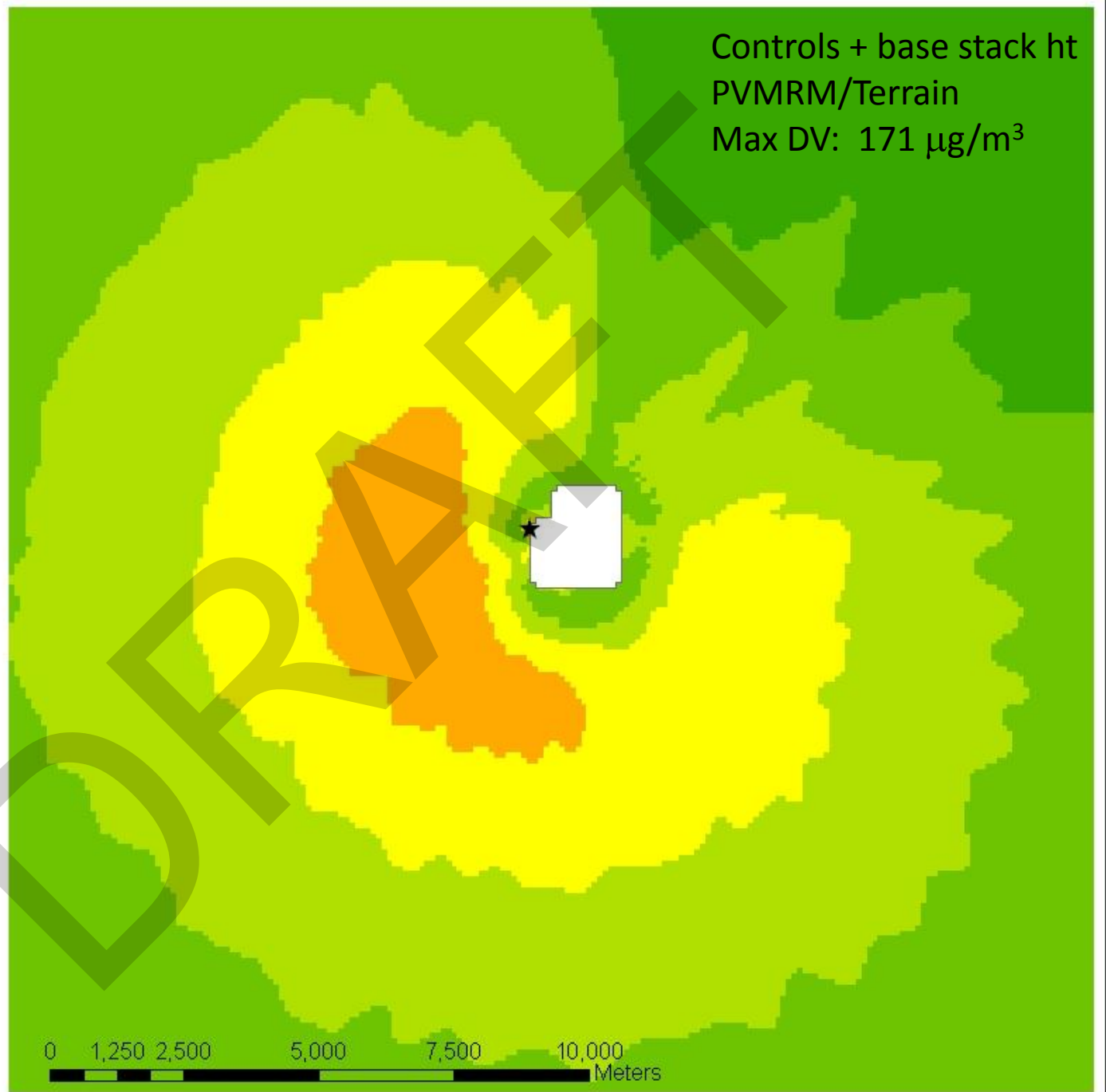
Controls + base stack ht  
OLM/Terrain  
Max DV: 127  $\mu\text{g}/\text{m}^3$



### Legend



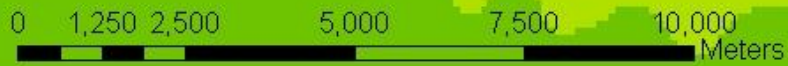
Controls + base stack ht  
PVMRM/Terrain  
Max DV: 171  $\mu\text{g}/\text{m}^3$



**Legend**

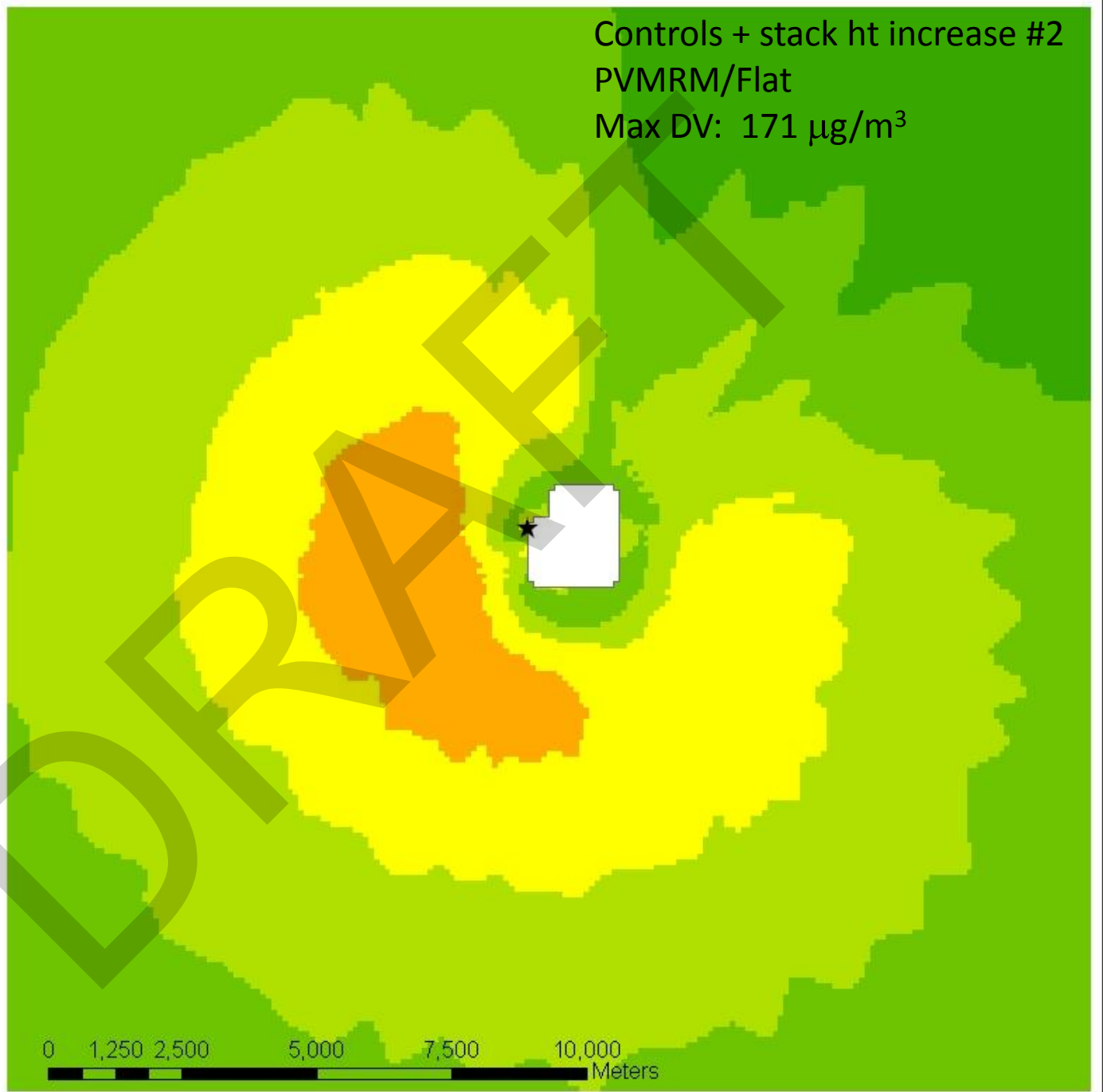
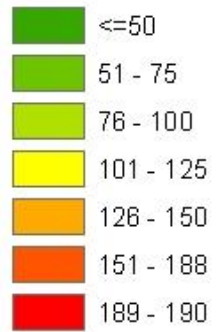


Controls + stack ht increase #2  
OLM/Flat  
Max DV: 127  $\mu\text{g}/\text{m}^3$

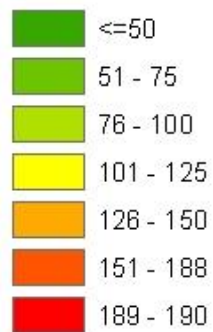


Controls + stack ht increase #2  
PVMRM/Flat  
Max DV: 171  $\mu\text{g}/\text{m}^3$

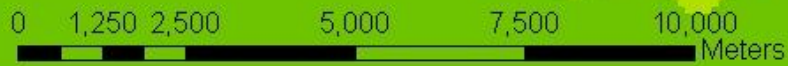
**Legend**



**Legend**



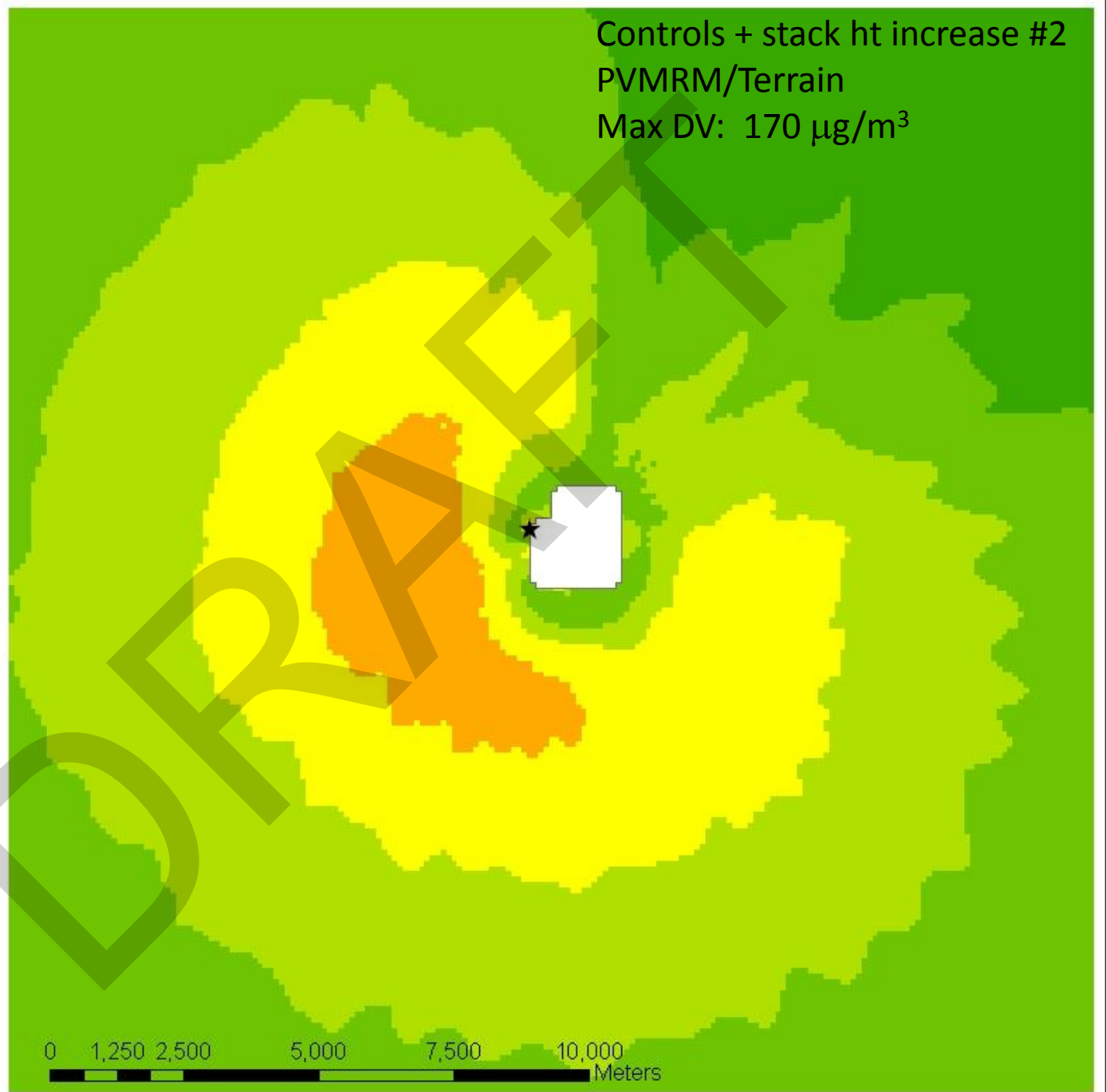
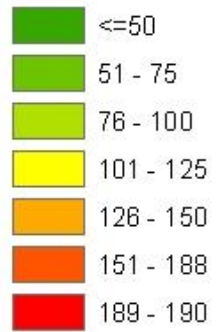
Controls + stack ht increase #2  
OLM/Terrain  
Max DV: 124  $\mu\text{g}/\text{m}^3$





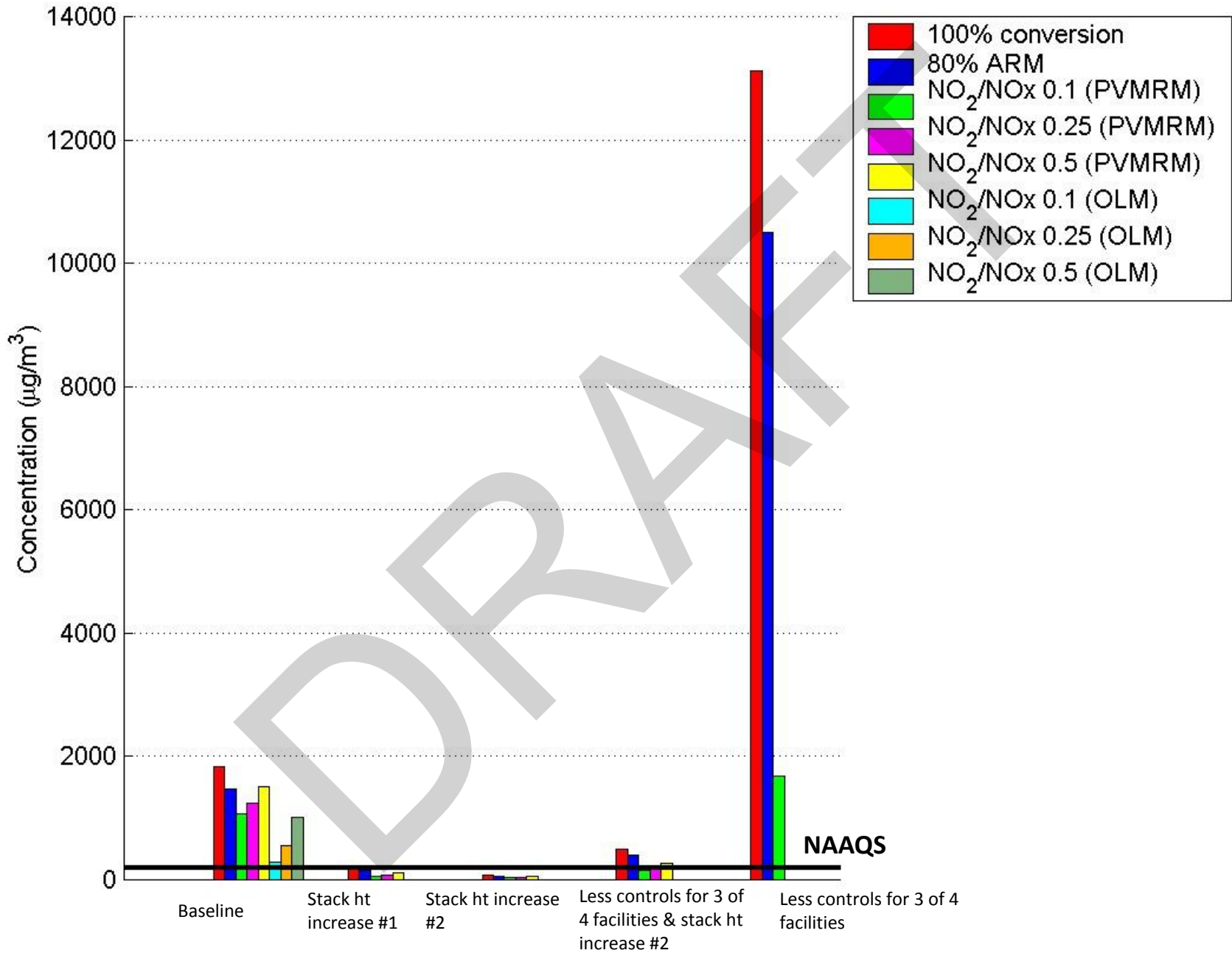
Controls + stack ht increase #2  
PVMRM/Terrain  
Max DV: 170  $\mu\text{g}/\text{m}^3$

**Legend**

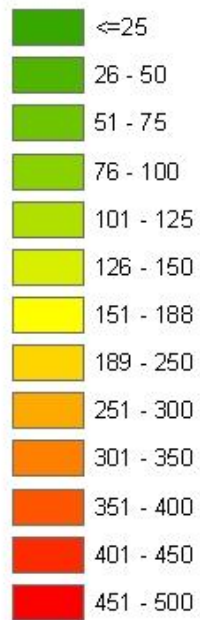


0 1,250 2,500 5,000 7,500 10,000  
Meters

# Natural Gas Compressor Station (All): NO<sub>2</sub>



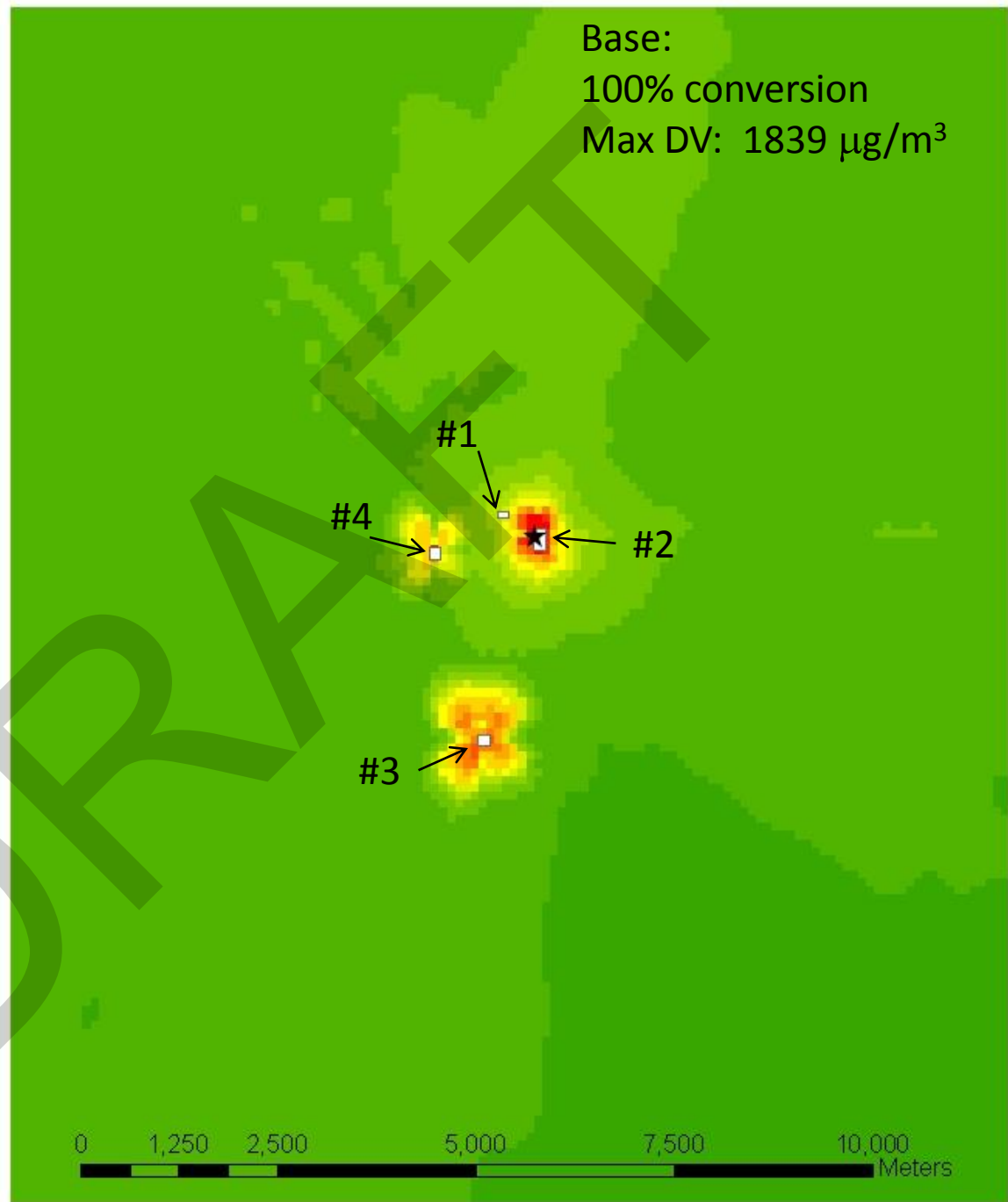
### Legend



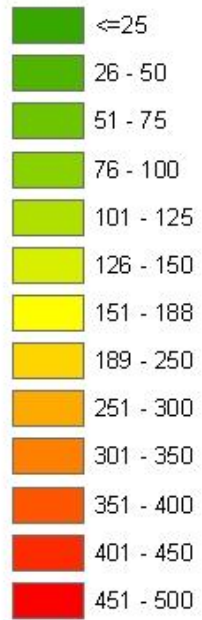
Base:

100% conversion

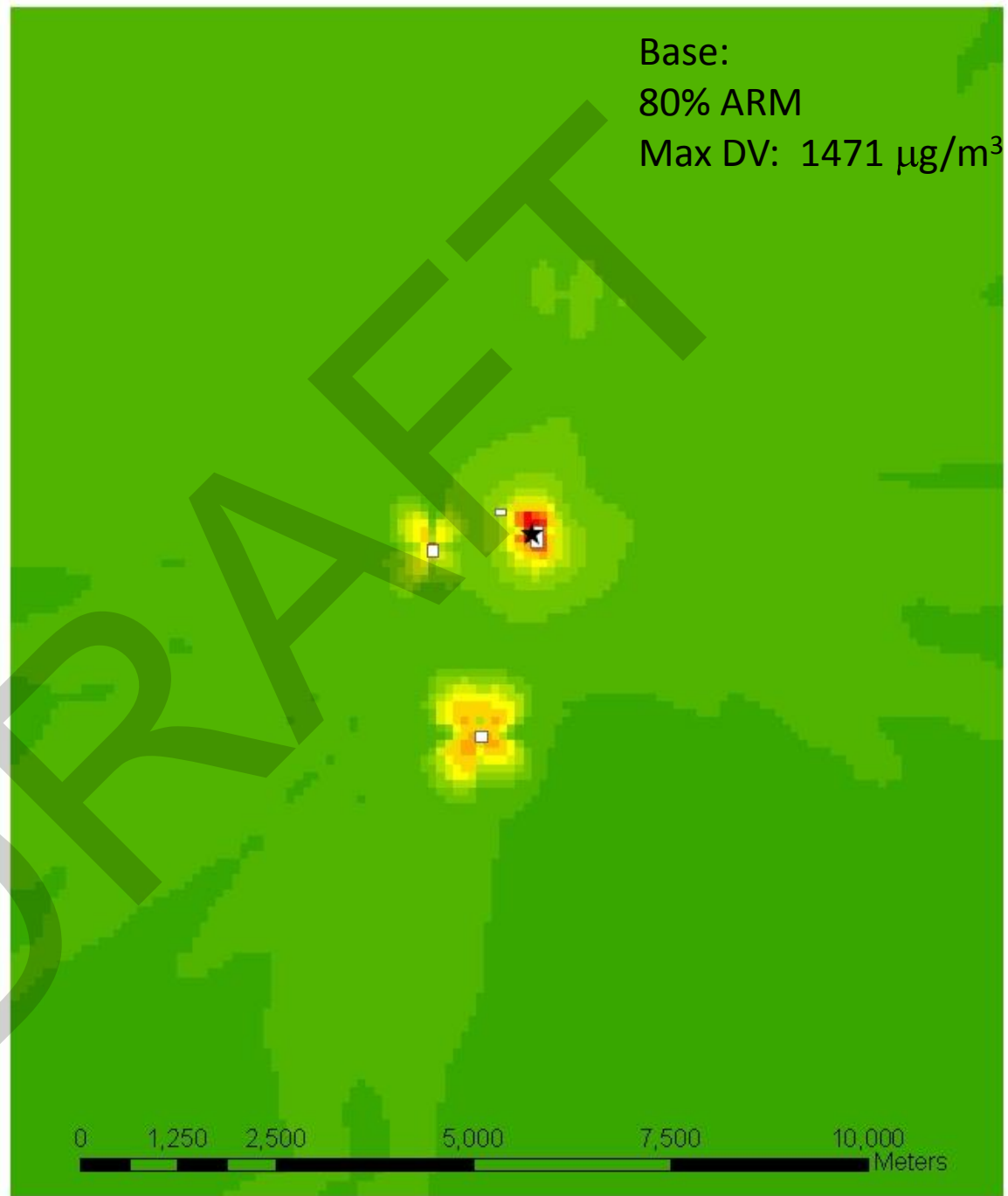
Max DV: 1839  $\mu\text{g}/\text{m}^3$



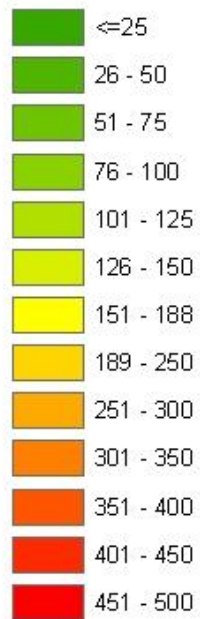
### Legend



Base:  
80% ARM  
Max DV: 1471  $\mu\text{g}/\text{m}^3$



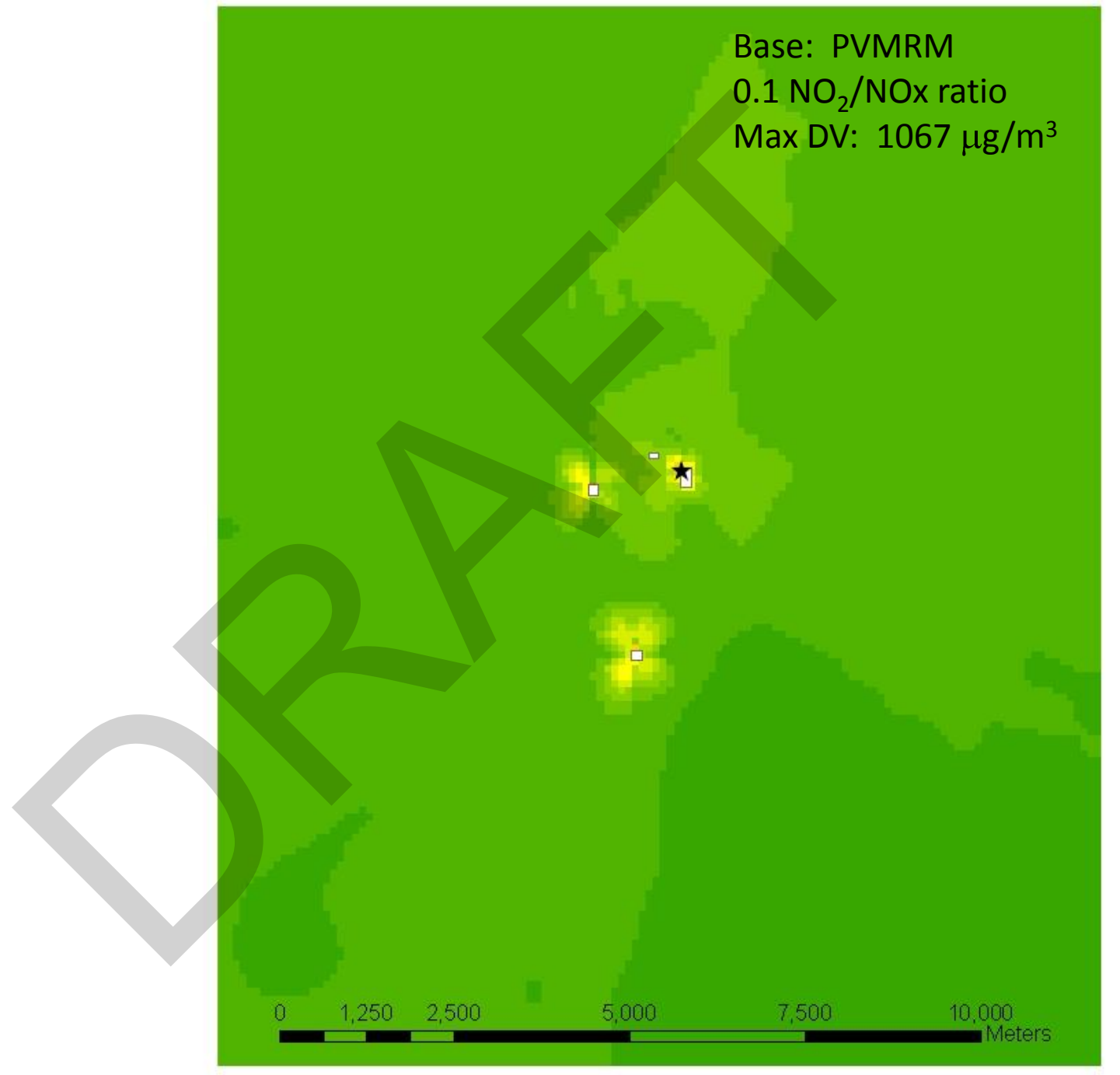
### Legend



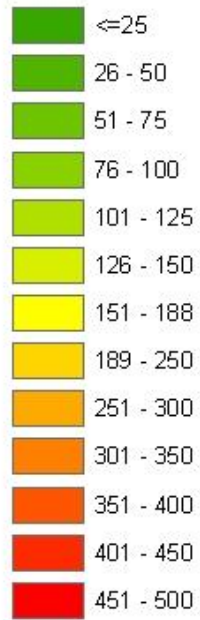
Base: PVMRM

0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 1067 μg/m<sup>3</sup>



### Legend



Base: PVMRM

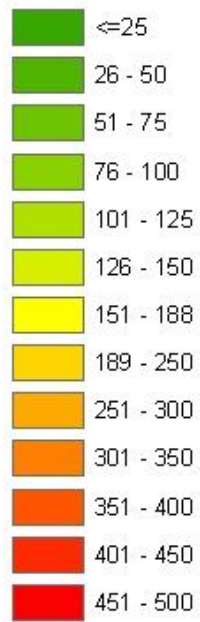
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 1245 μg/m<sup>3</sup>



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### Legend



Base: PVMRM

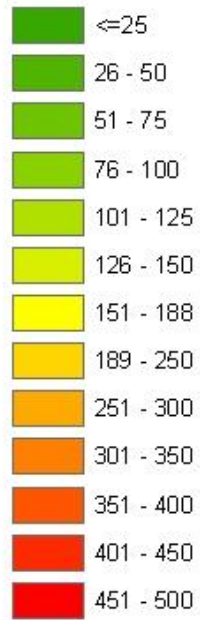
0.5 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 1519 μg/m<sup>3</sup>

0 1,250 2,500 5,000 7,500 10,000 Meters

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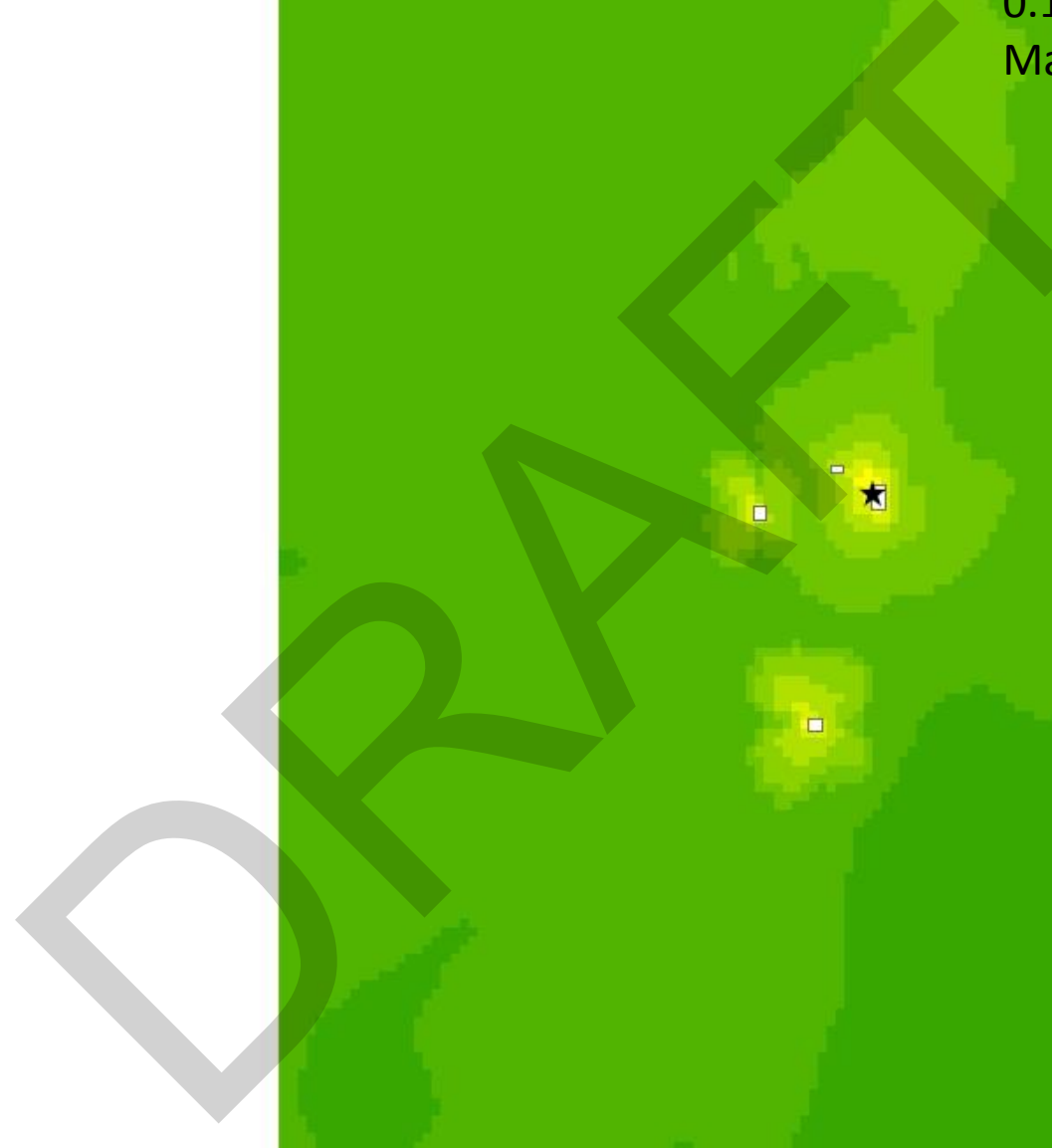
### Legend



Base: OLM

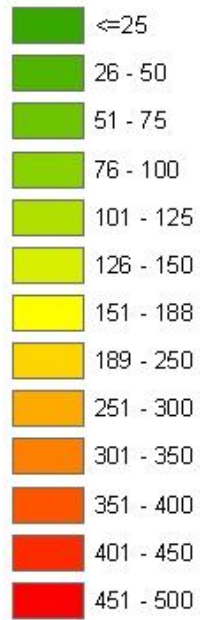
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 293 μg/m<sup>3</sup>





### Legend



Base: OLM

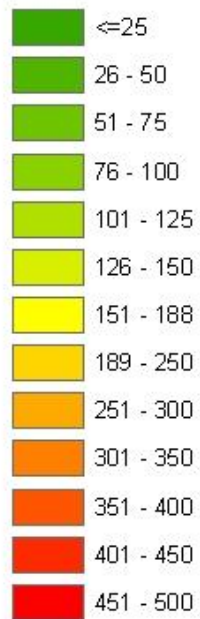
0.25 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 556 μg/m<sup>3</sup>



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### Legend



Base:

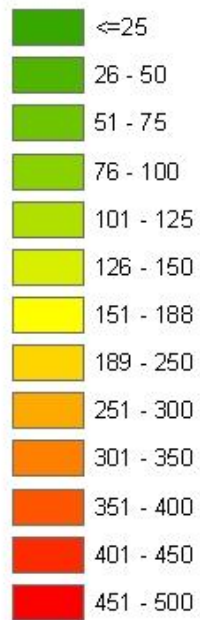
OLM 0.5 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 1012 μg/m<sup>3</sup>

0 1,250 2,500 5,000 7,500 10,000 Meters

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### Legend

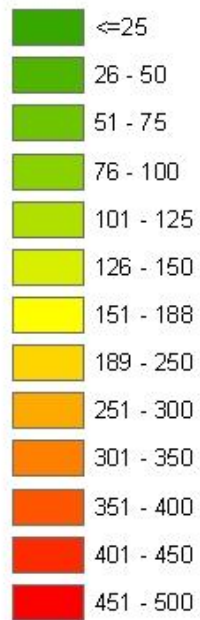


Stack ht increase #1  
100% conversion  
Max DV: 191  $\mu\text{g}/\text{m}^3$

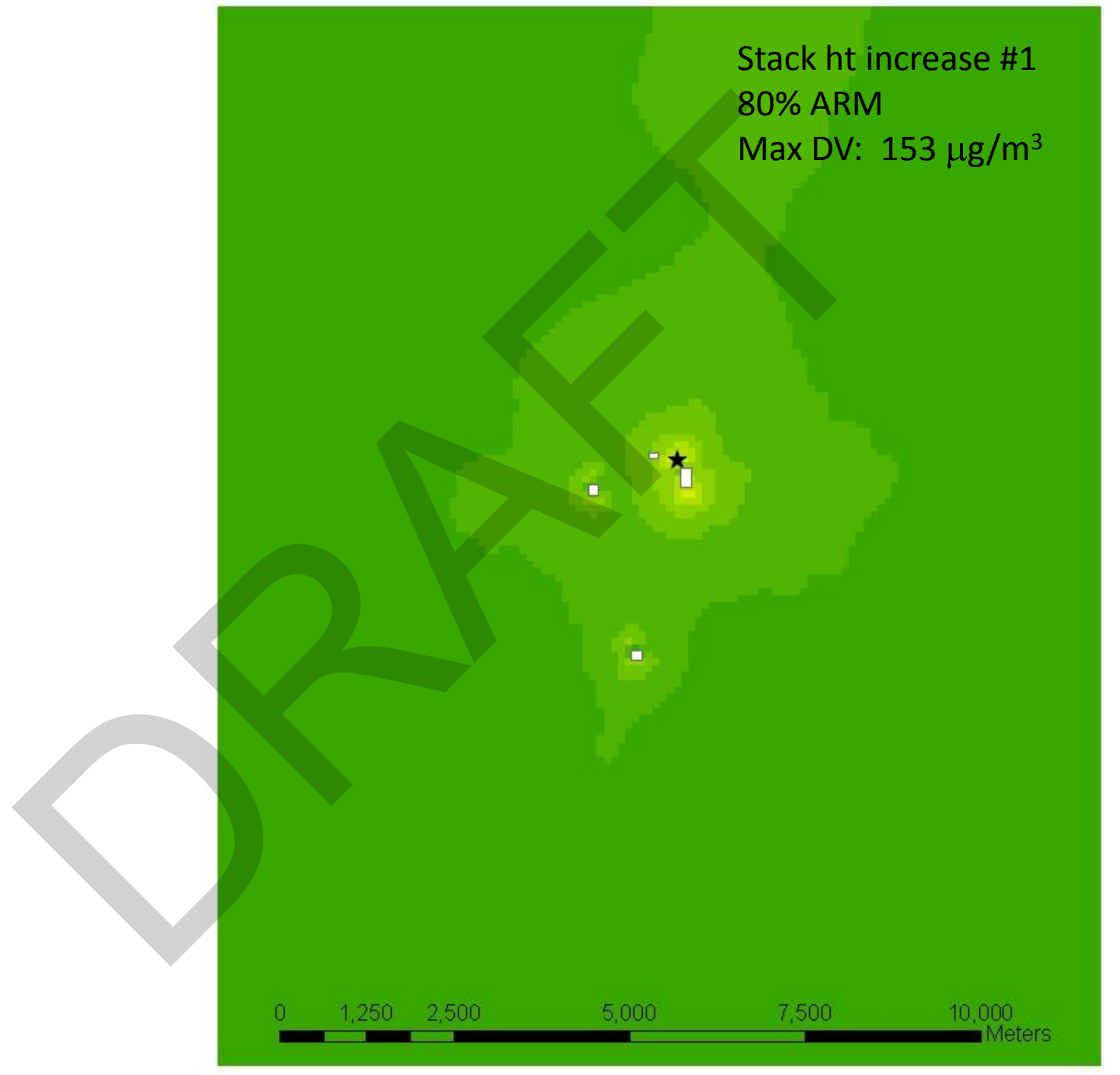
0 1,250 2,500 5,000 7,500 10,000 Meters

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### Legend



Stack ht increase #1  
80% ARM  
Max DV: 153  $\mu\text{g}/\text{m}^3$



### Legend



Stack ht increase #1

PVMRM

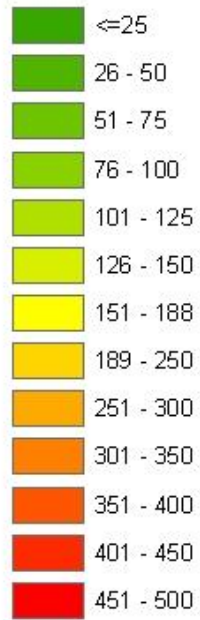
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 65 μg/m<sup>3</sup>



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### Legend



Stack ht increase #1

PVMRM

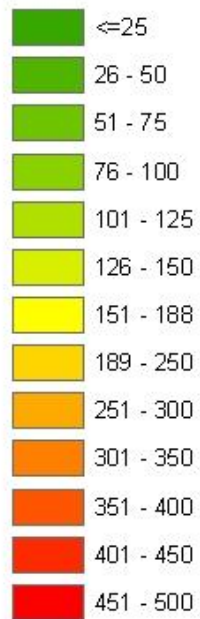
0.25 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 83  $\mu\text{g}/\text{m}^3$

0 1,250 2,500 5,000 7,500 10,000 Meters



### Legend



Stack ht increase #1

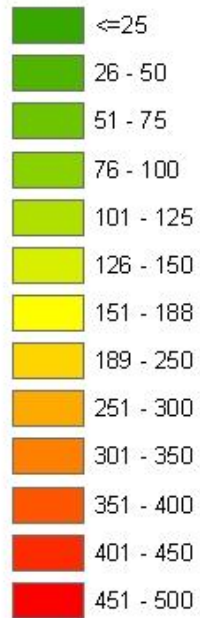
PVMRM

0.5 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 121 μg/m<sup>3</sup>

0 1,250 2,500 5,000 7,500 10,000 Meters

### Legend

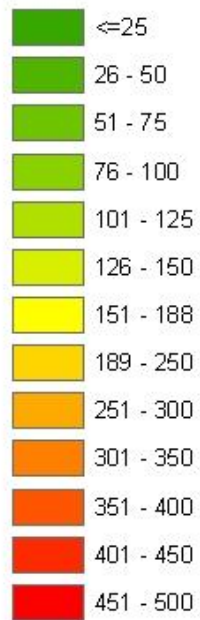


Stack ht increase #2  
100% conversion  
Max DV: 73  $\mu\text{g}/\text{m}^3$

0 1,250 2,500 5,000 7,500 10,000 Meters



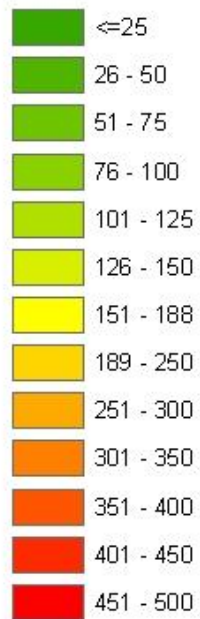
### Legend



Stack ht increase #2  
80% ARM  
Max DV: 58  $\mu\text{g}/\text{m}^3$

0 1,250 2,500 5,000 7,500 10,000 Meters

### Legend



Stack ht increase #2

PVMRM

0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 43 μg/m<sup>3</sup>



### Legend

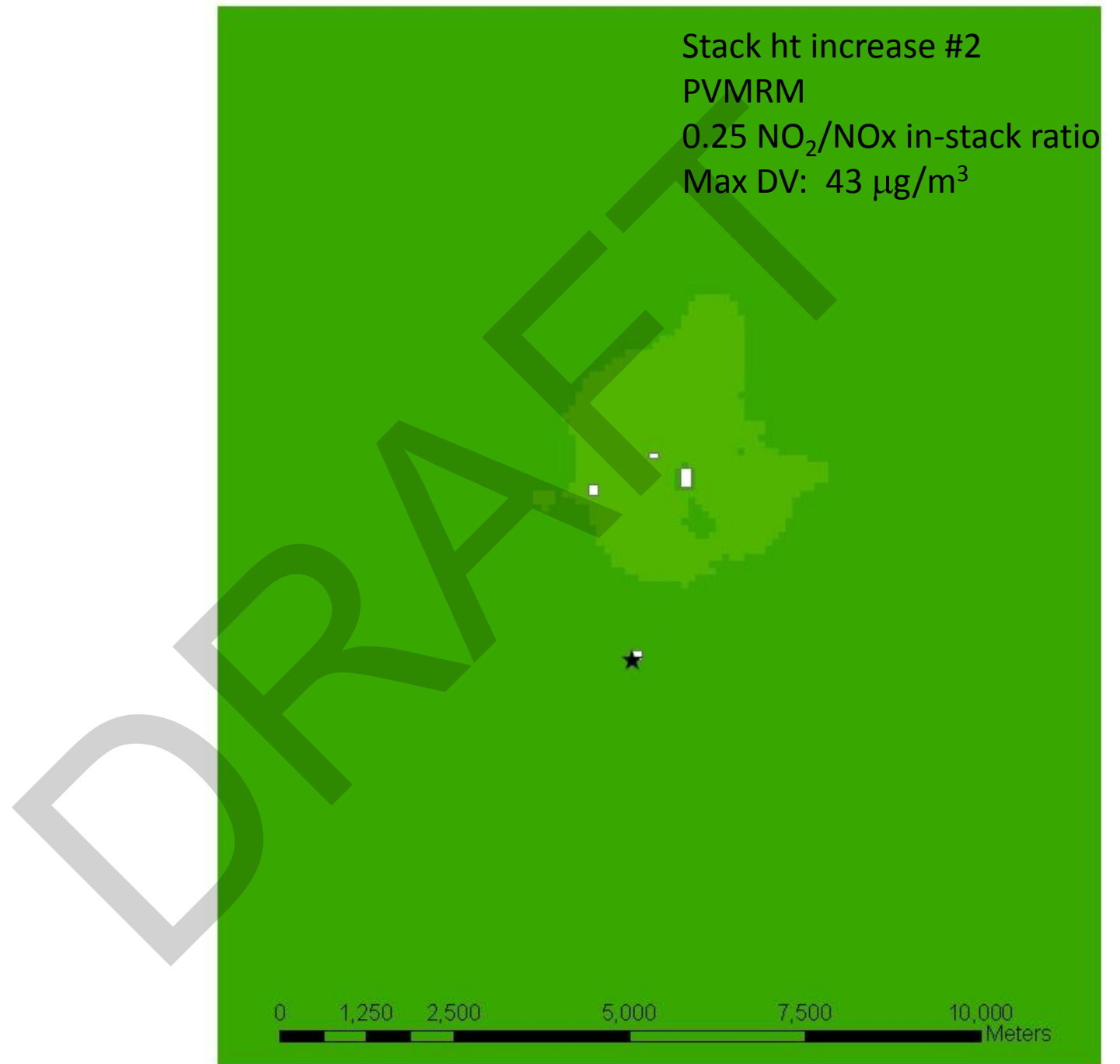


Stack ht increase #2

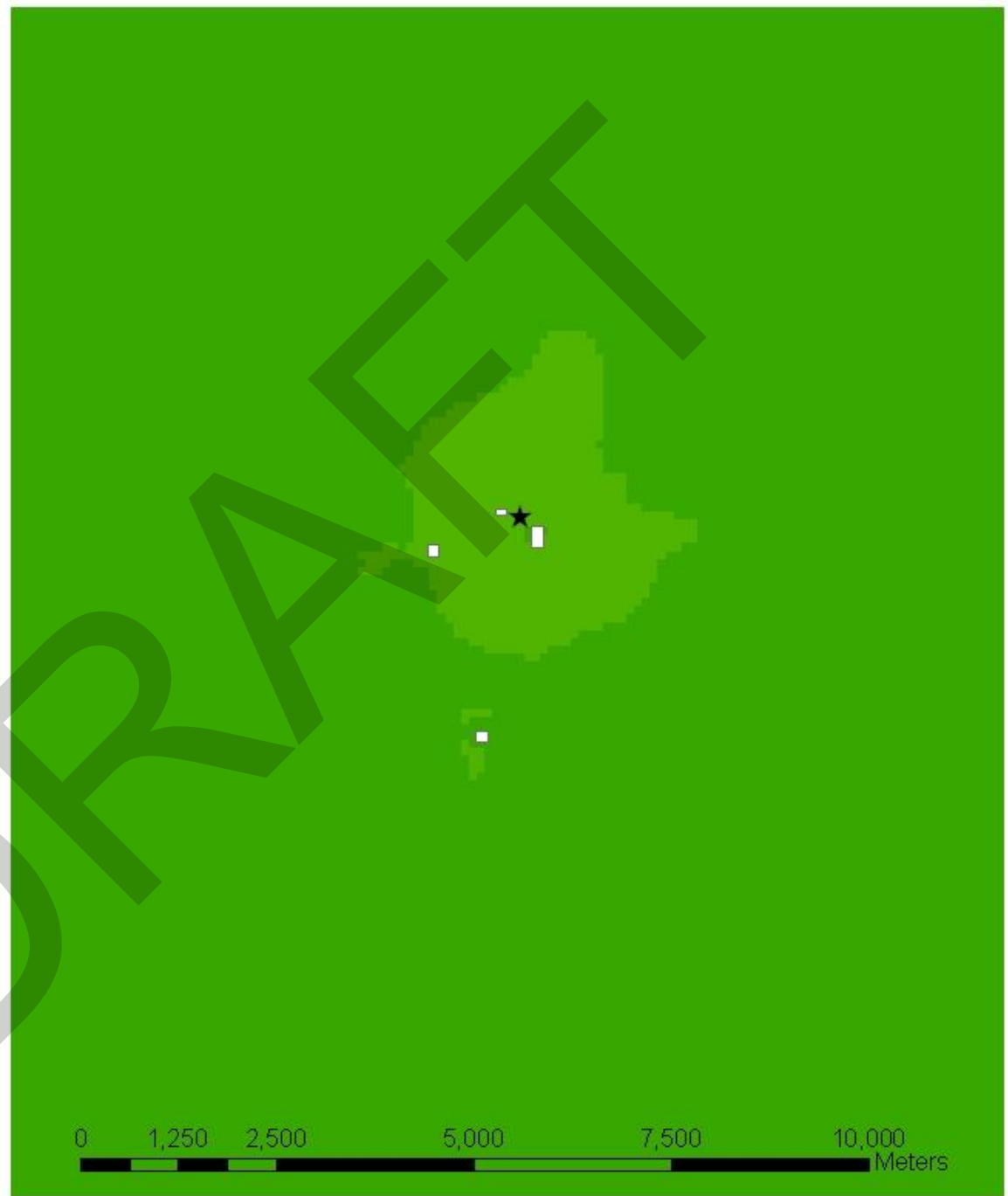
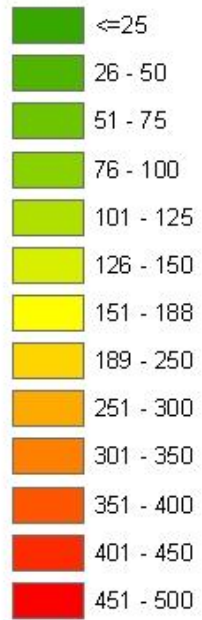
PVMRM

0.25 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 43 μg/m<sup>3</sup>

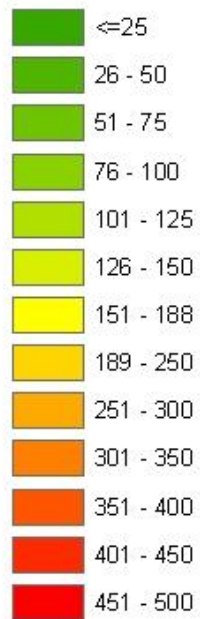


## Legend



0 1,250 2,500 5,000 7,500 10,000 Meters

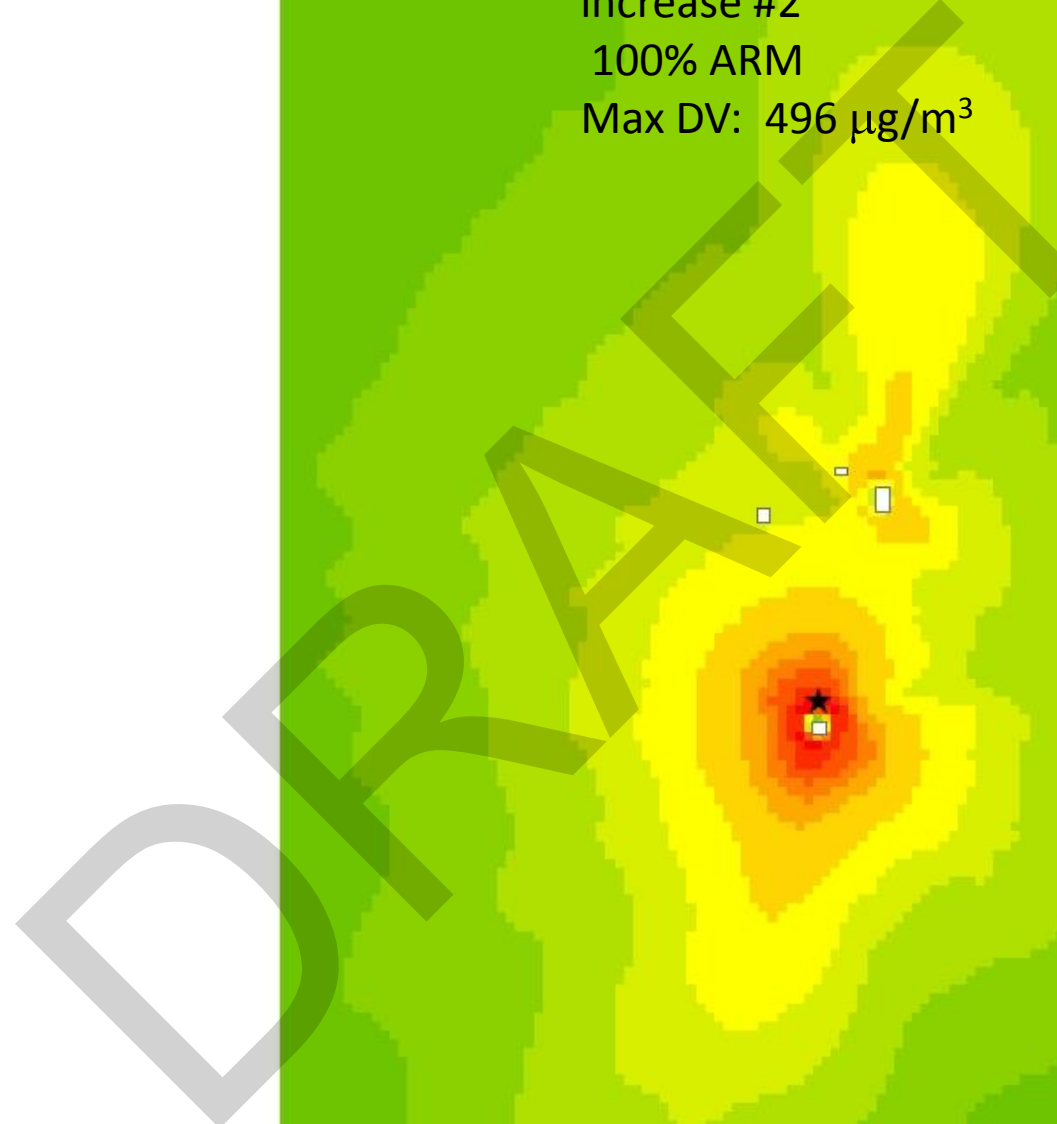
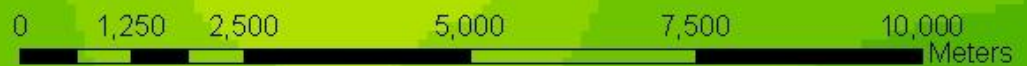
### Legend



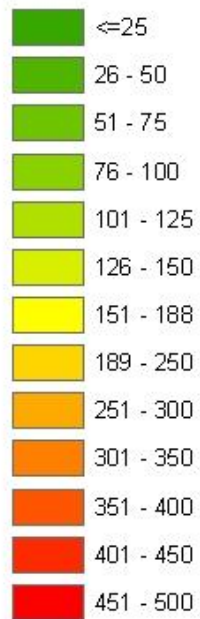
Less controls for 3 of 4 facilities & stack ht  
increase #2

100% ARM

Max DV:  $496 \mu\text{g}/\text{m}^3$



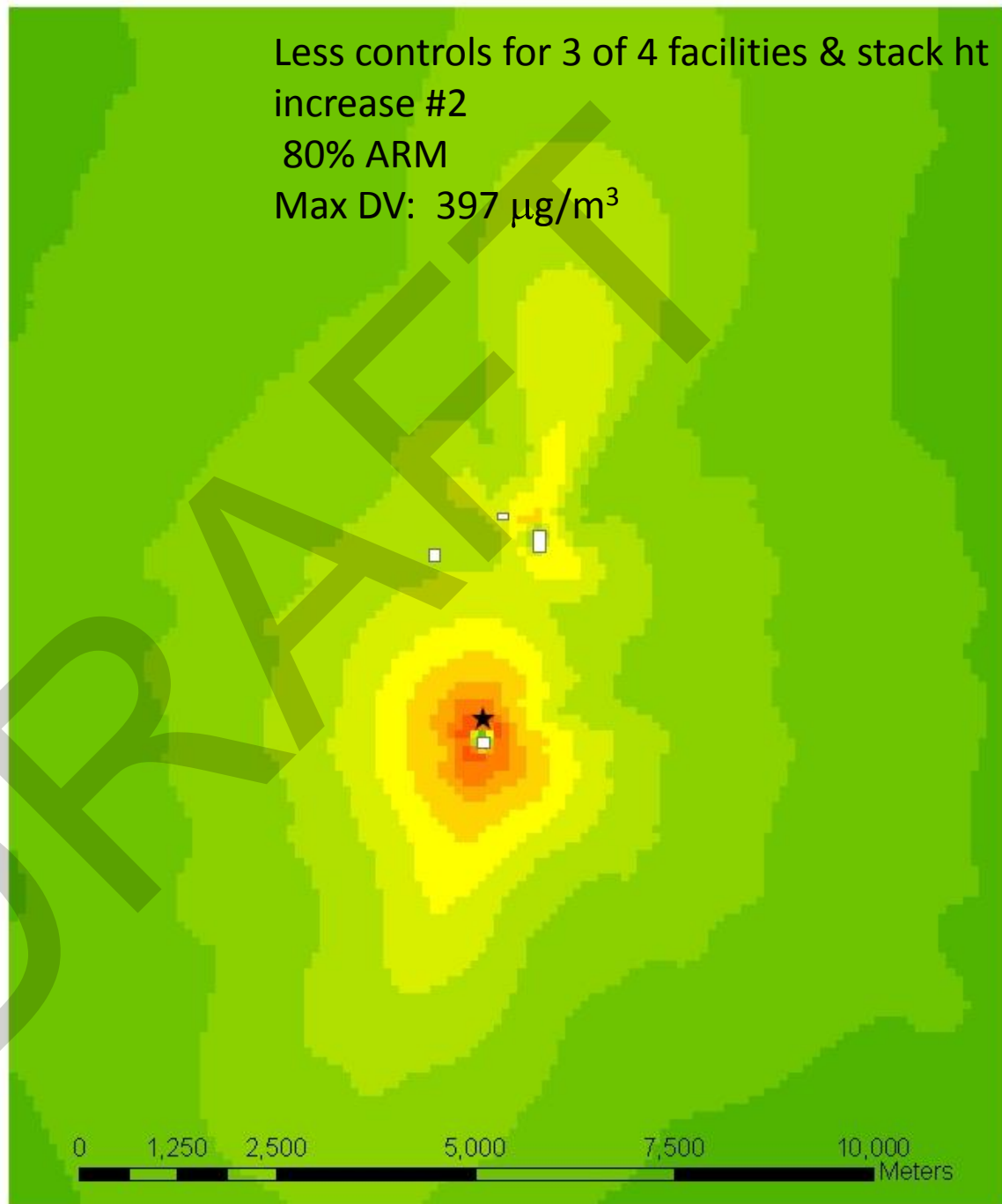
### Legend



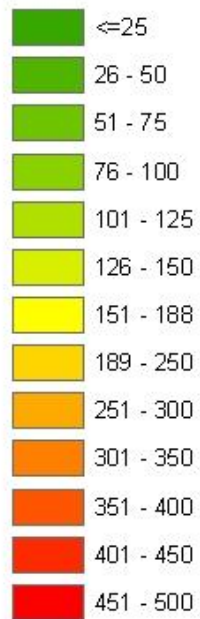
Less controls for 3 of 4 facilities & stack ht  
increase #2

80% ARM

Max DV:  $397 \mu\text{g}/\text{m}^3$



### Legend



Less controls for 3 of 4 facilities & stack ht  
increase #2

PVMRM

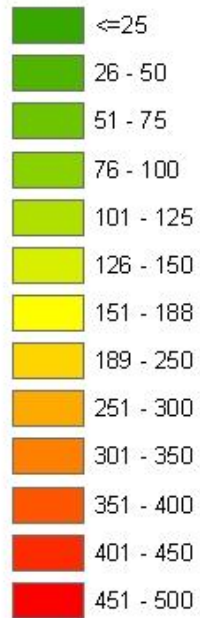
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 163 μg/m<sup>3</sup>

0 1,250 2,500 5,000 7,500 10,000 Meters

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### Legend

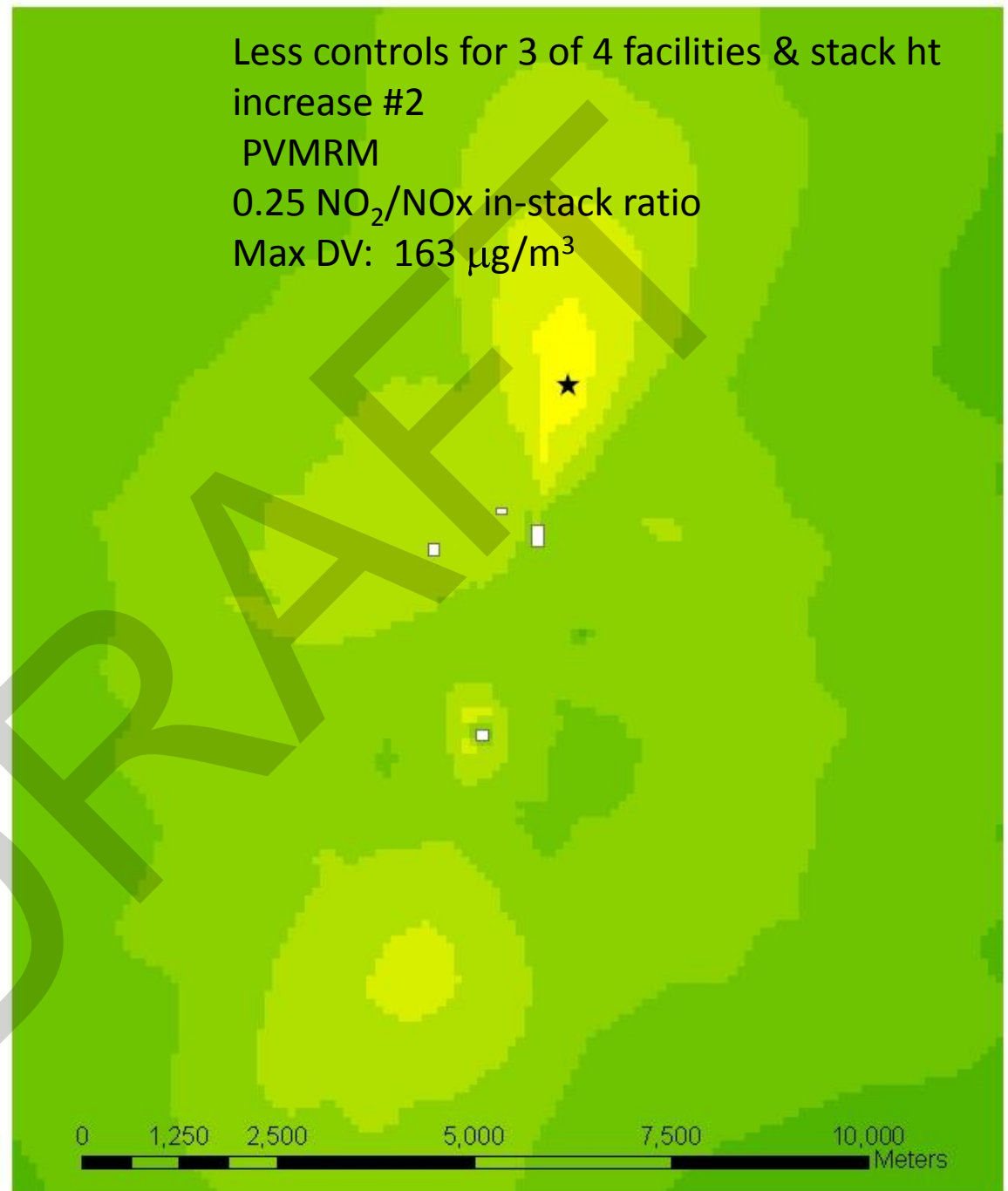


Less controls for 3 of 4 facilities & stack ht  
increase #2

PVMRM

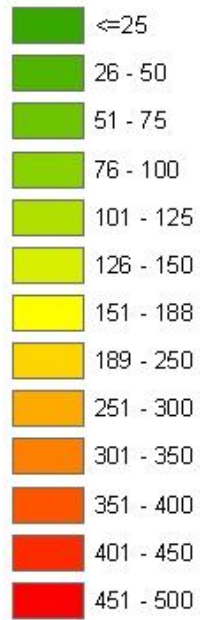
0.25 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 163 μg/m<sup>3</sup>





### Legend



Less controls for 3 of 4 facilities & stack ht  
increase #2

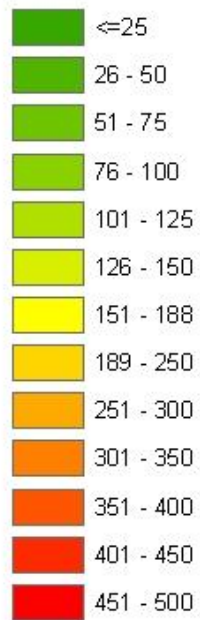
PVMRM

0.5 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

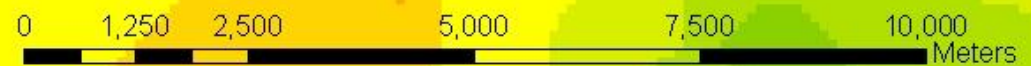
Max DV: 1262 μg/m<sup>3</sup>

0 1,250 2,500 5,000 7,500 10,000 Meters

### Legend

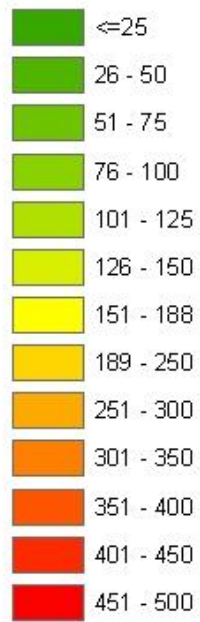


Less controls for 3 of 4 facilities  
100% conversion  
Max DV: 13129  $\mu\text{g}/\text{m}^3$

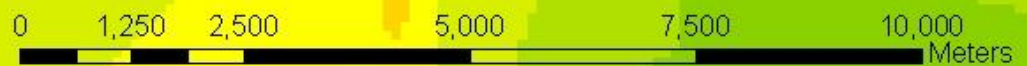


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### Legend

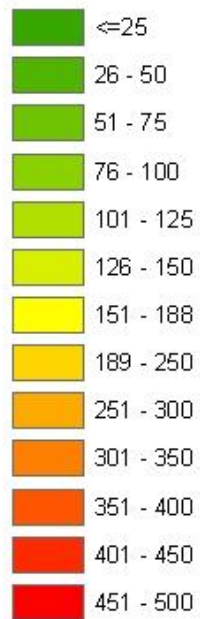


Less controls for 3 of 4 facilities  
80% ARM  
Max DV: 10503  $\mu\text{g}/\text{m}^3$

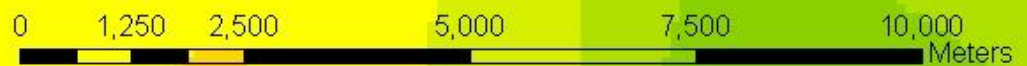


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### Legend

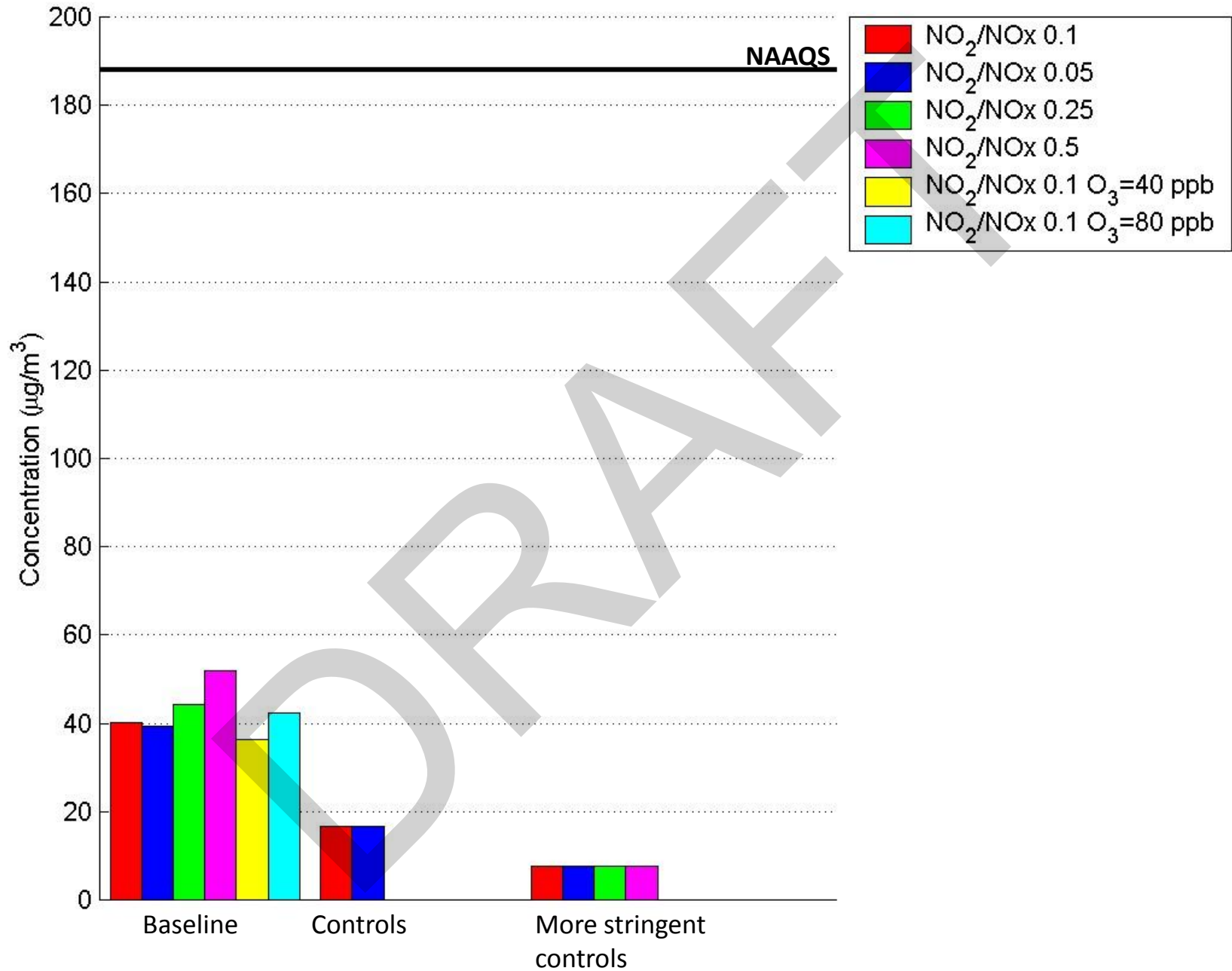


Less controls for 3 of 4 facilities  
PVMRM  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 1674 μg/m<sup>3</sup>



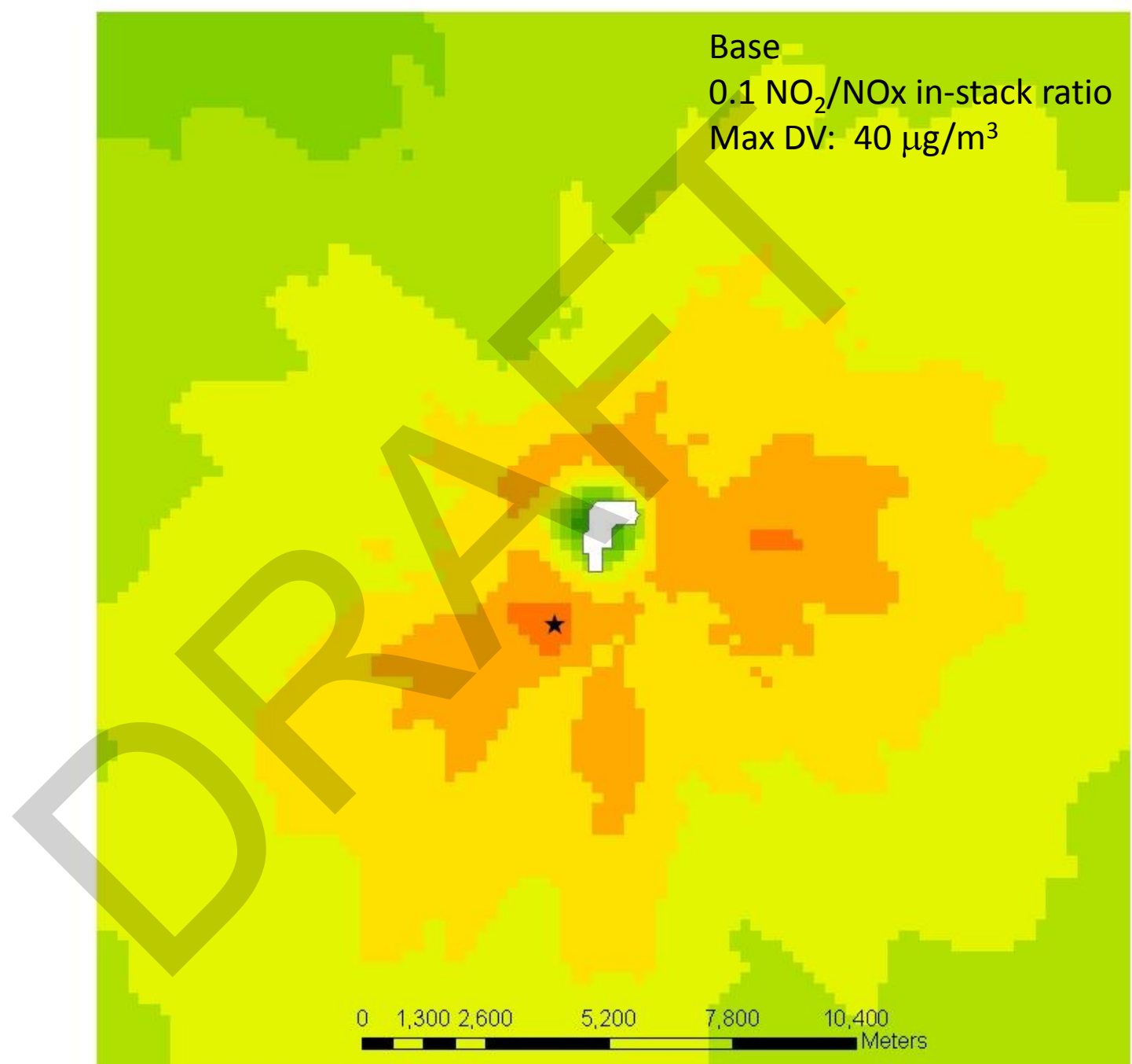
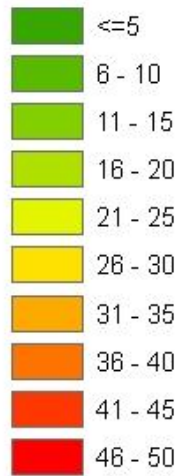
DRAFT

# Cement Kiln: NO<sub>2</sub>



Base  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 40 μg/m<sup>3</sup>

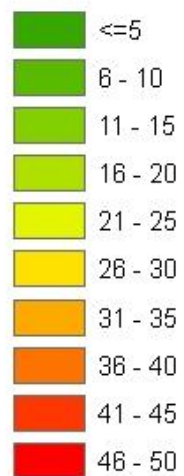
### Legend



0 1,300 2,600 5,200 7,800 10,400 Meters

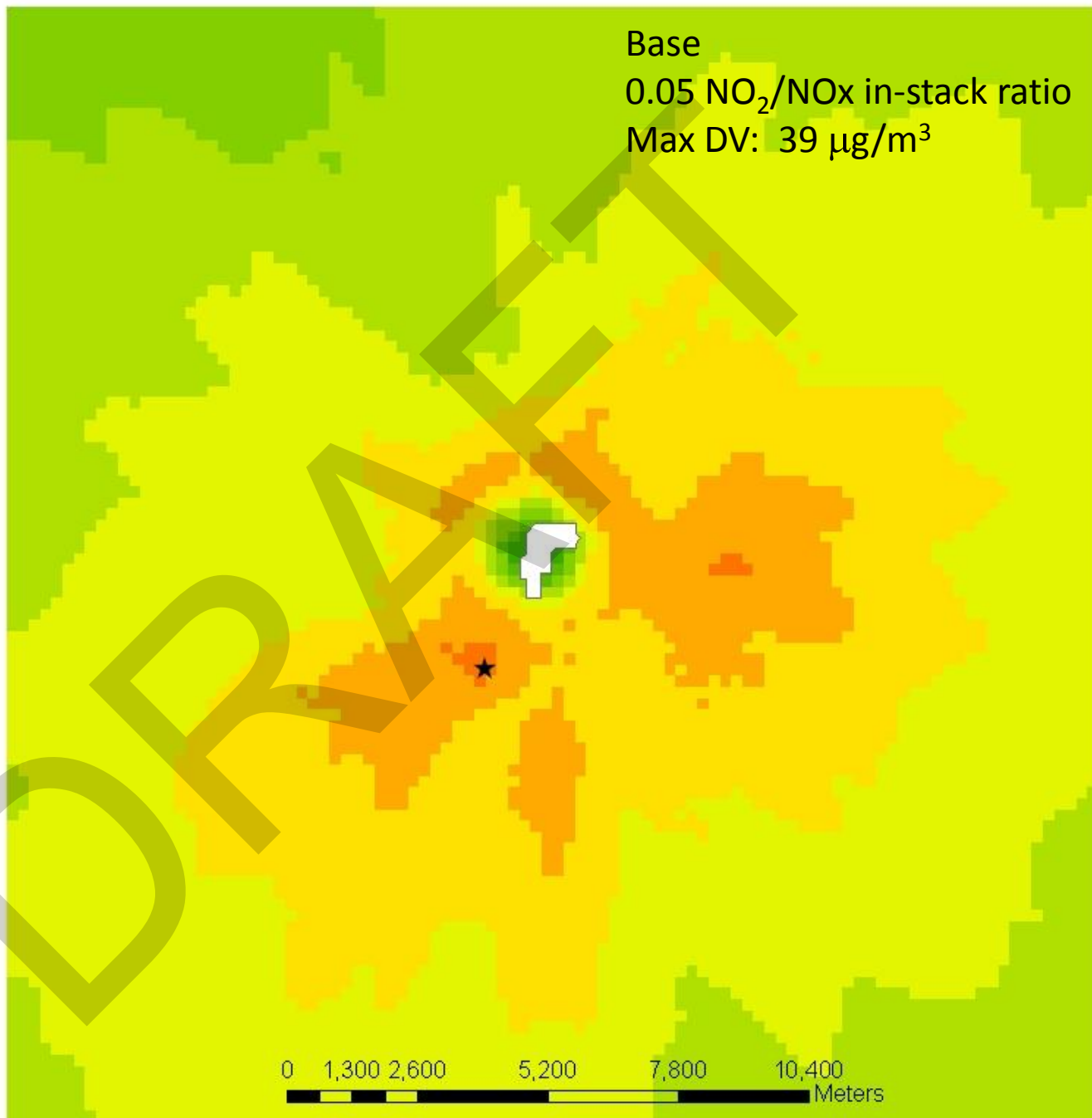
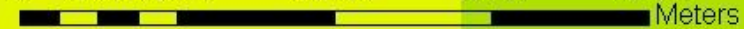
Base  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 39 μg/m<sup>3</sup>

### Legend



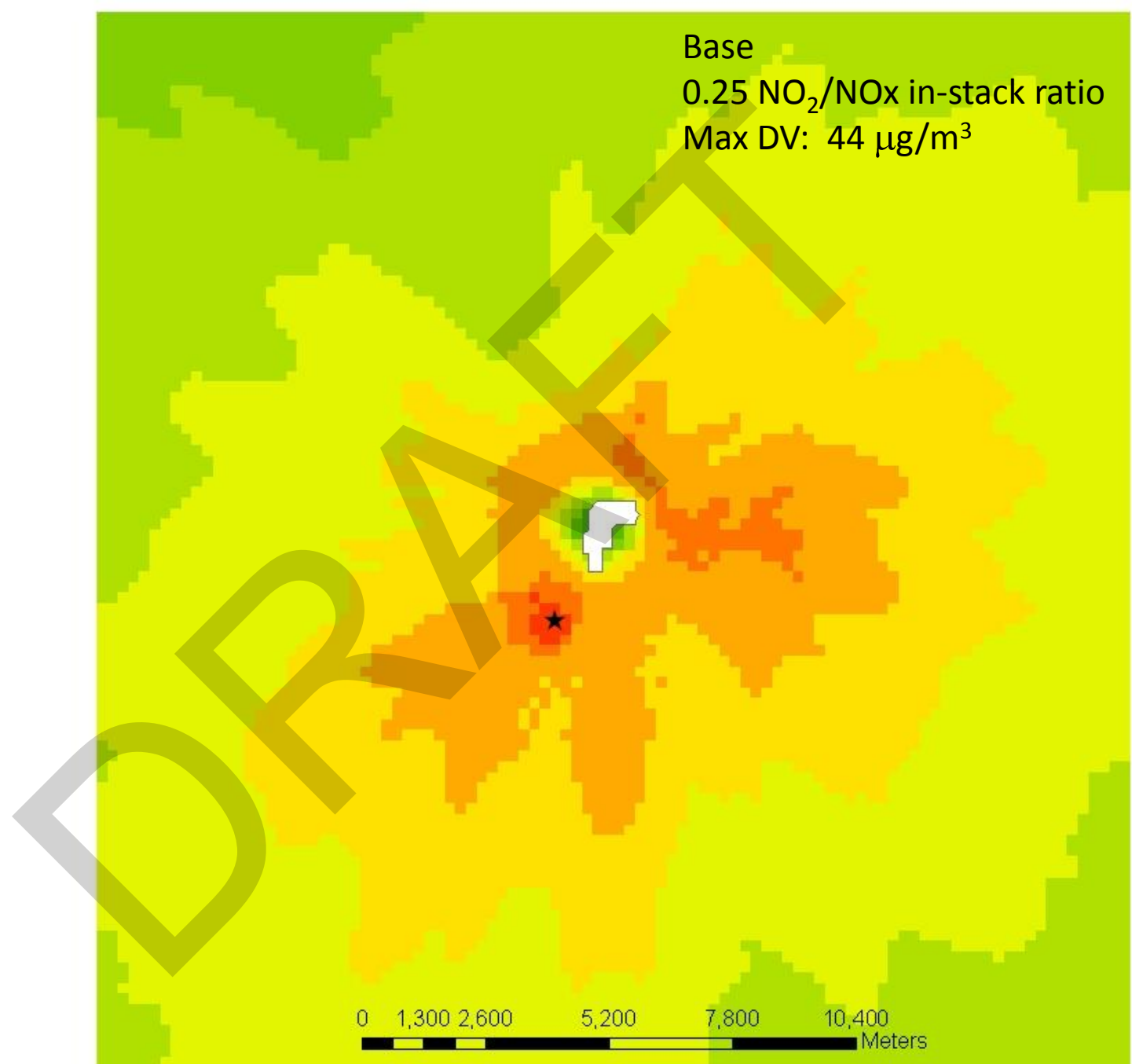
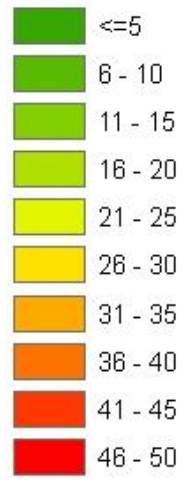
DRAFT

0 1,300 2,600 5,200 7,800 10,400 Meters



Base  
0.25 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 44 μg/m<sup>3</sup>

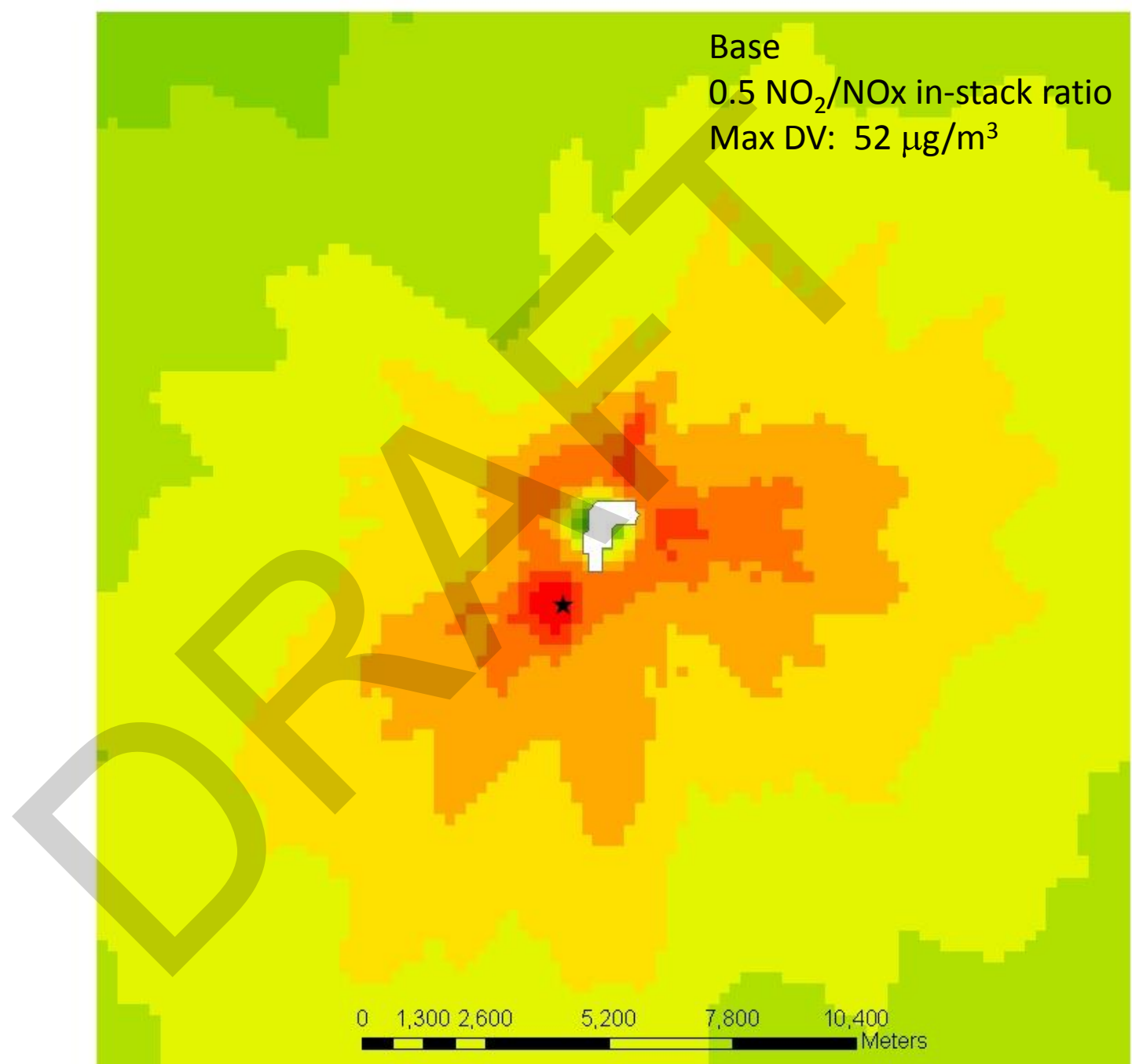
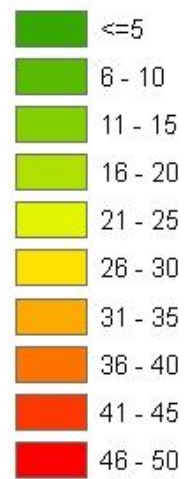
**Legend**





Base  
0.5 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 52 μg/m<sup>3</sup>

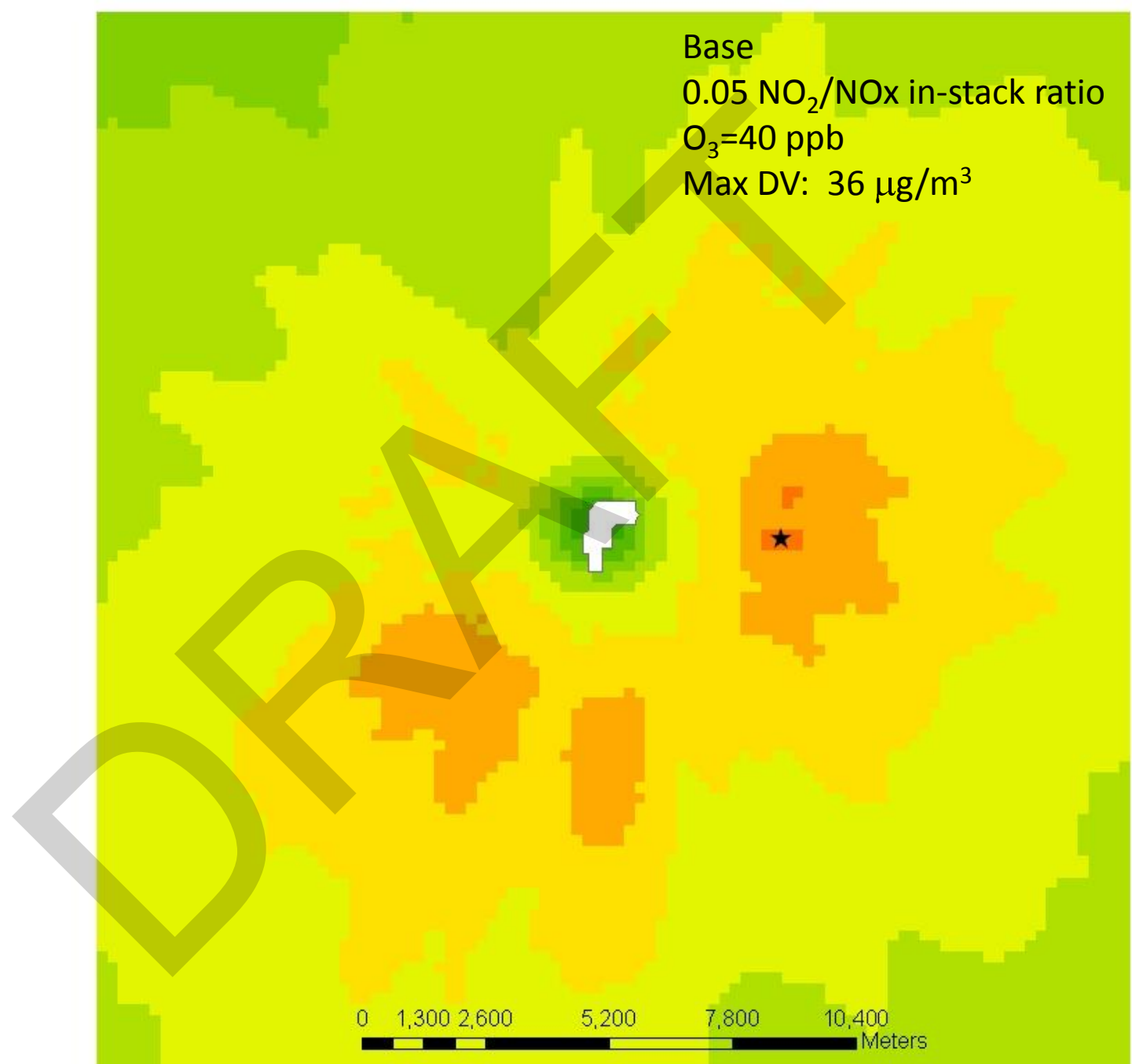
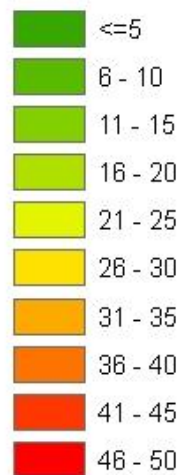
**Legend**



0 1,300 2,600 5,200 7,800 10,400  
Meters

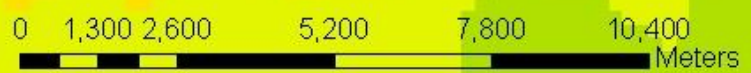
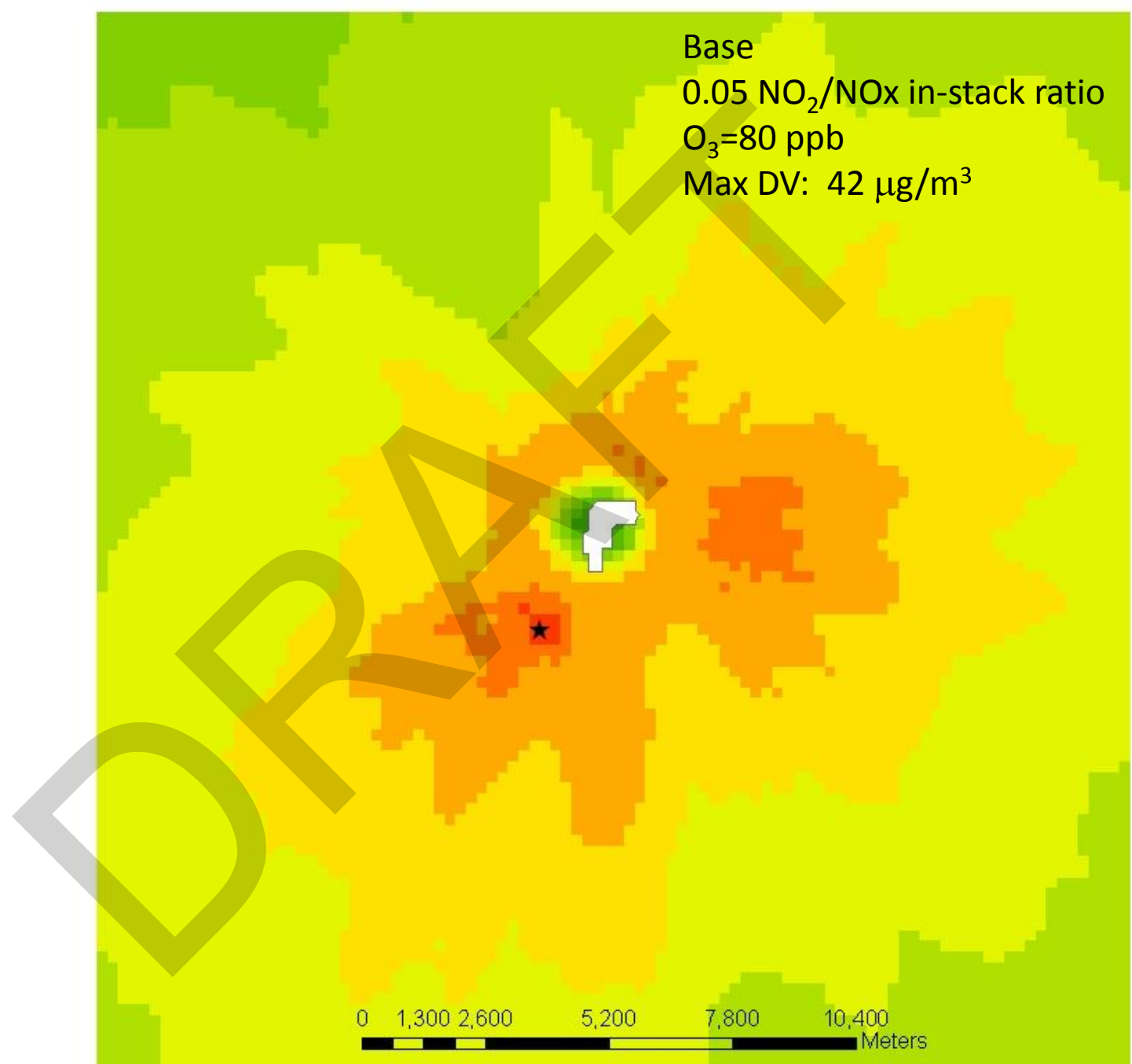
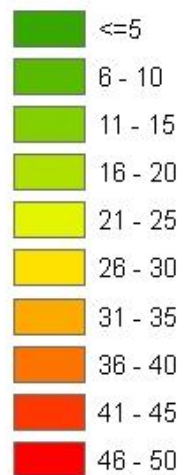
Base  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
O<sub>3</sub>=40 ppb  
Max DV: 36 μg/m<sup>3</sup>

**Legend**



Base  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
O<sub>3</sub>=80 ppb  
Max DV: 42 μg/m<sup>3</sup>

**Legend**

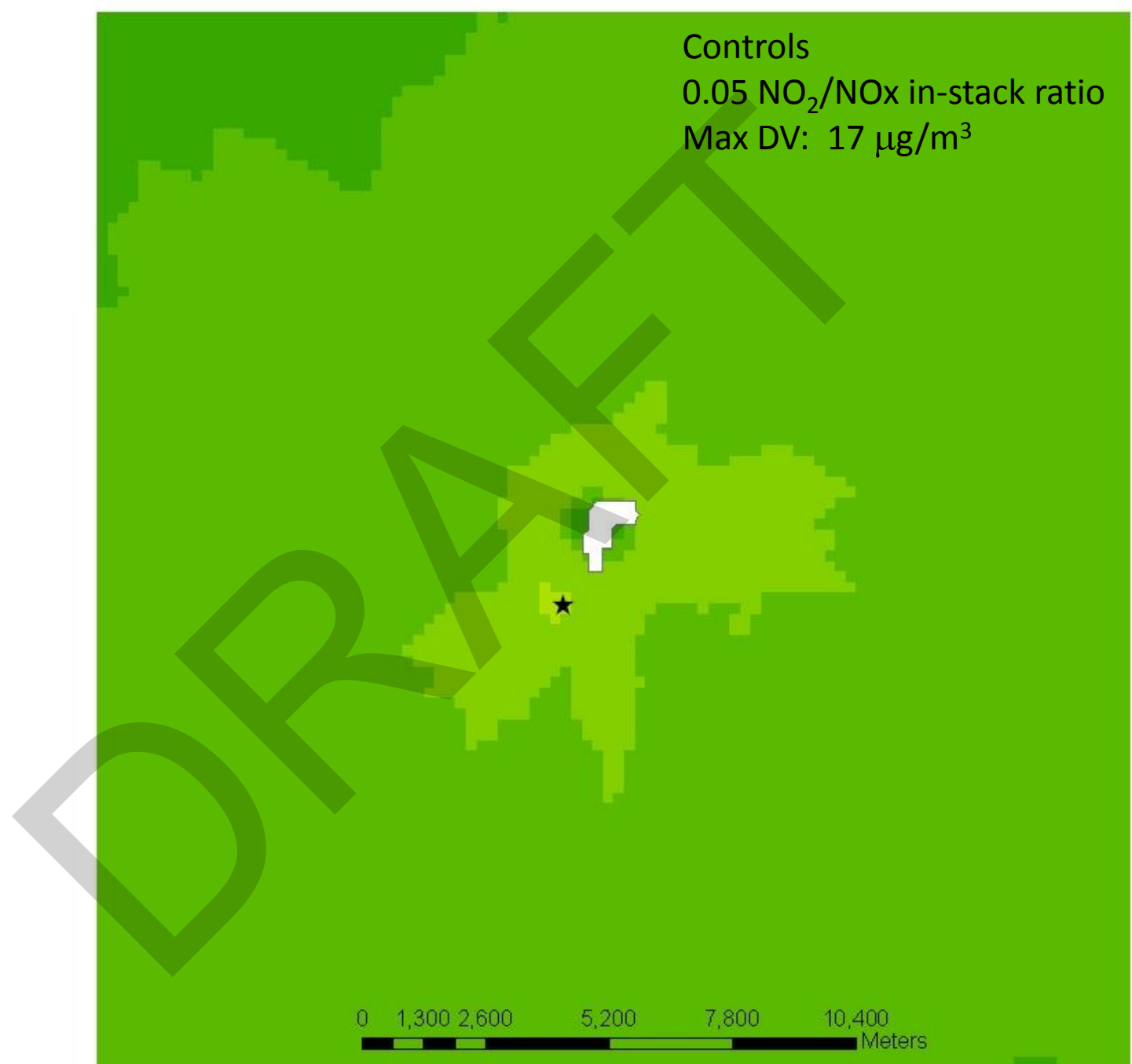
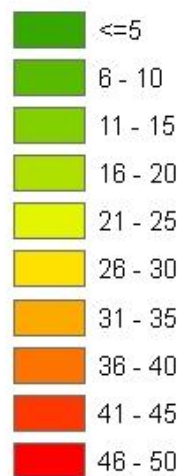


Controls

0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 17 μg/m<sup>3</sup>

**Legend**



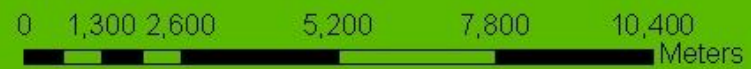
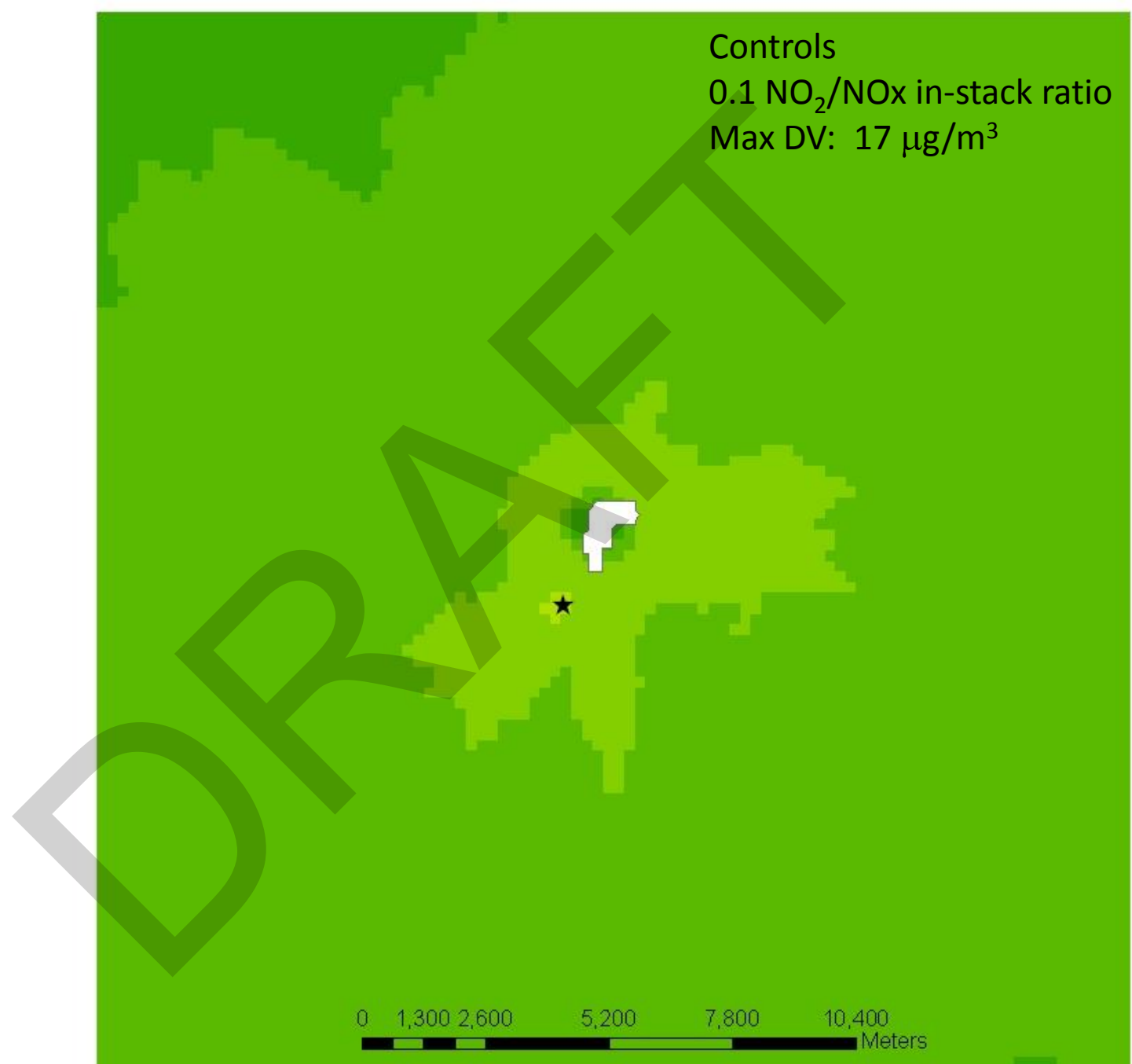
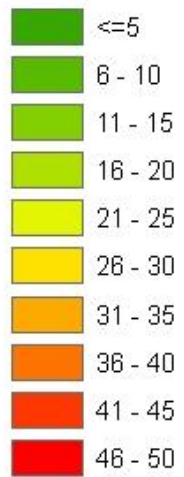
0 1,300 2,600 5,200 7,800 10,400 Meters

Controls

0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

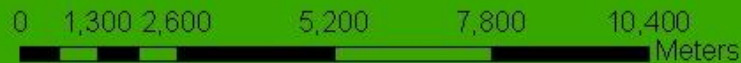
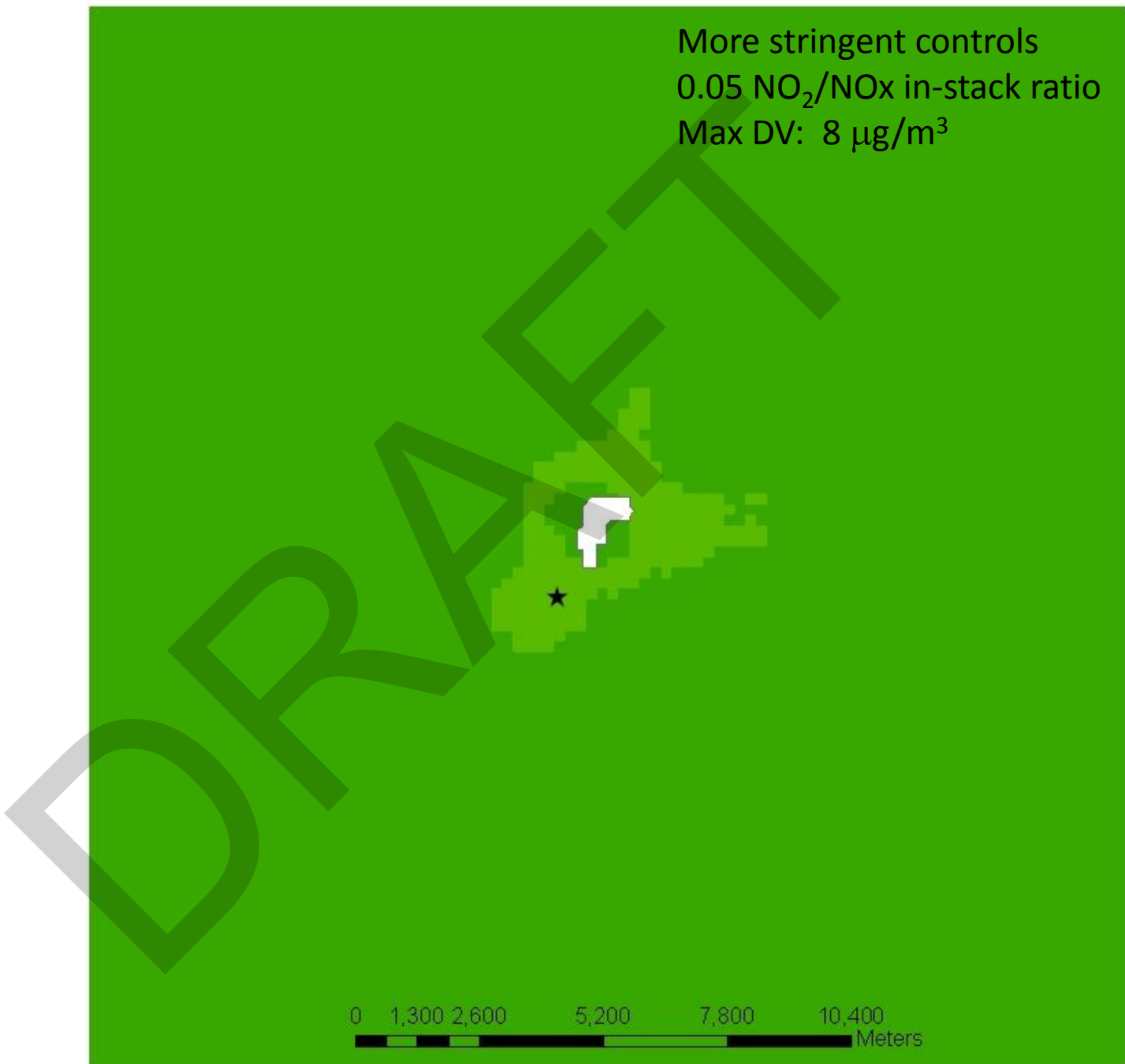
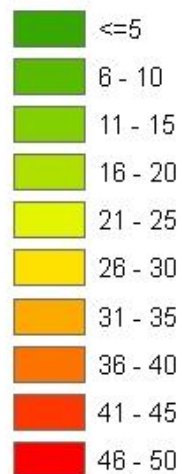
Max DV: 17 μg/m<sup>3</sup>

**Legend**



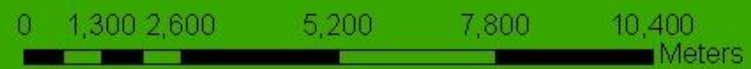
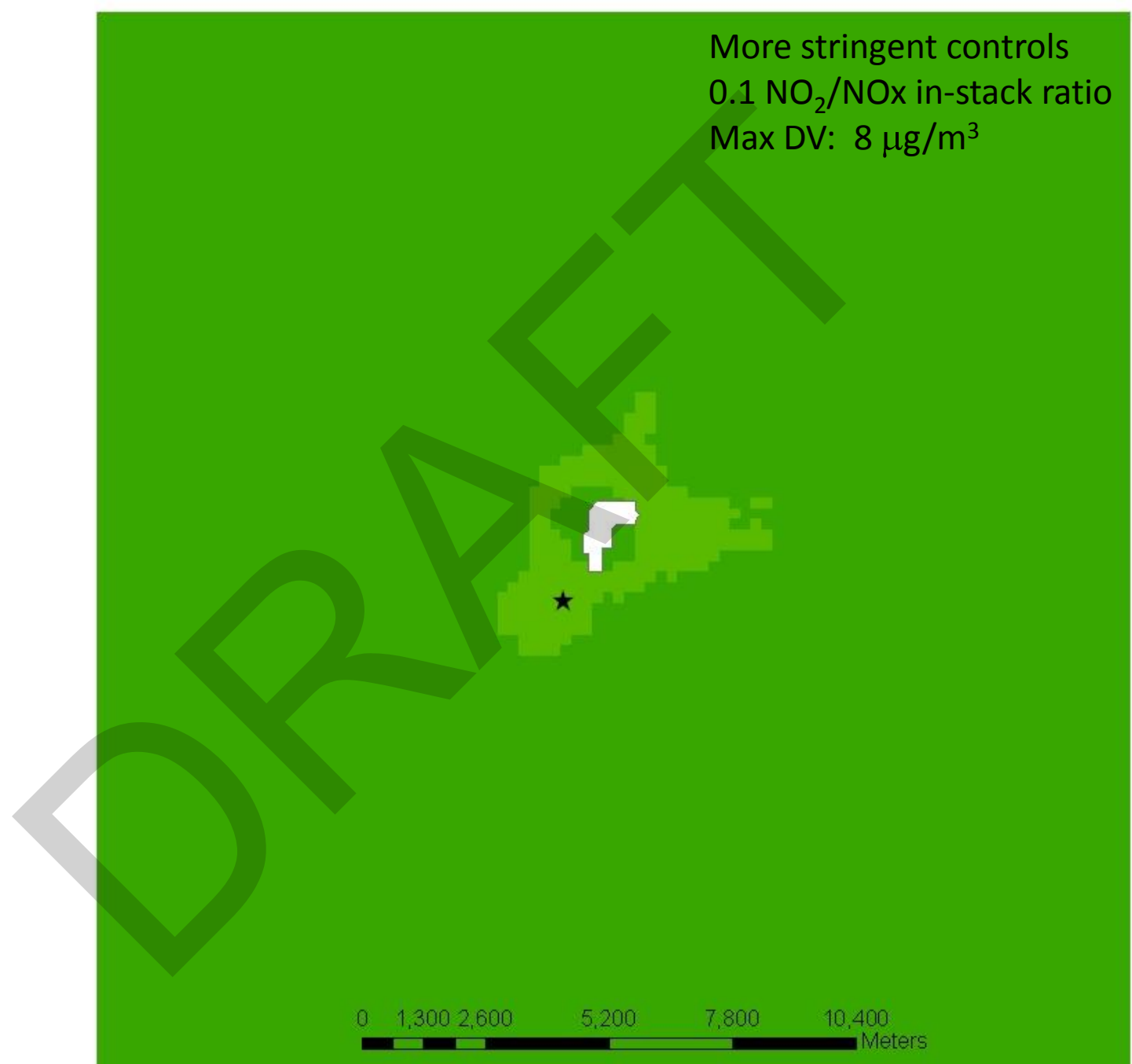
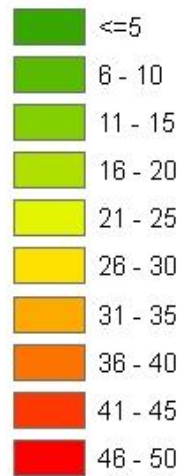
More stringent controls  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 8 μg/m<sup>3</sup>

**Legend**



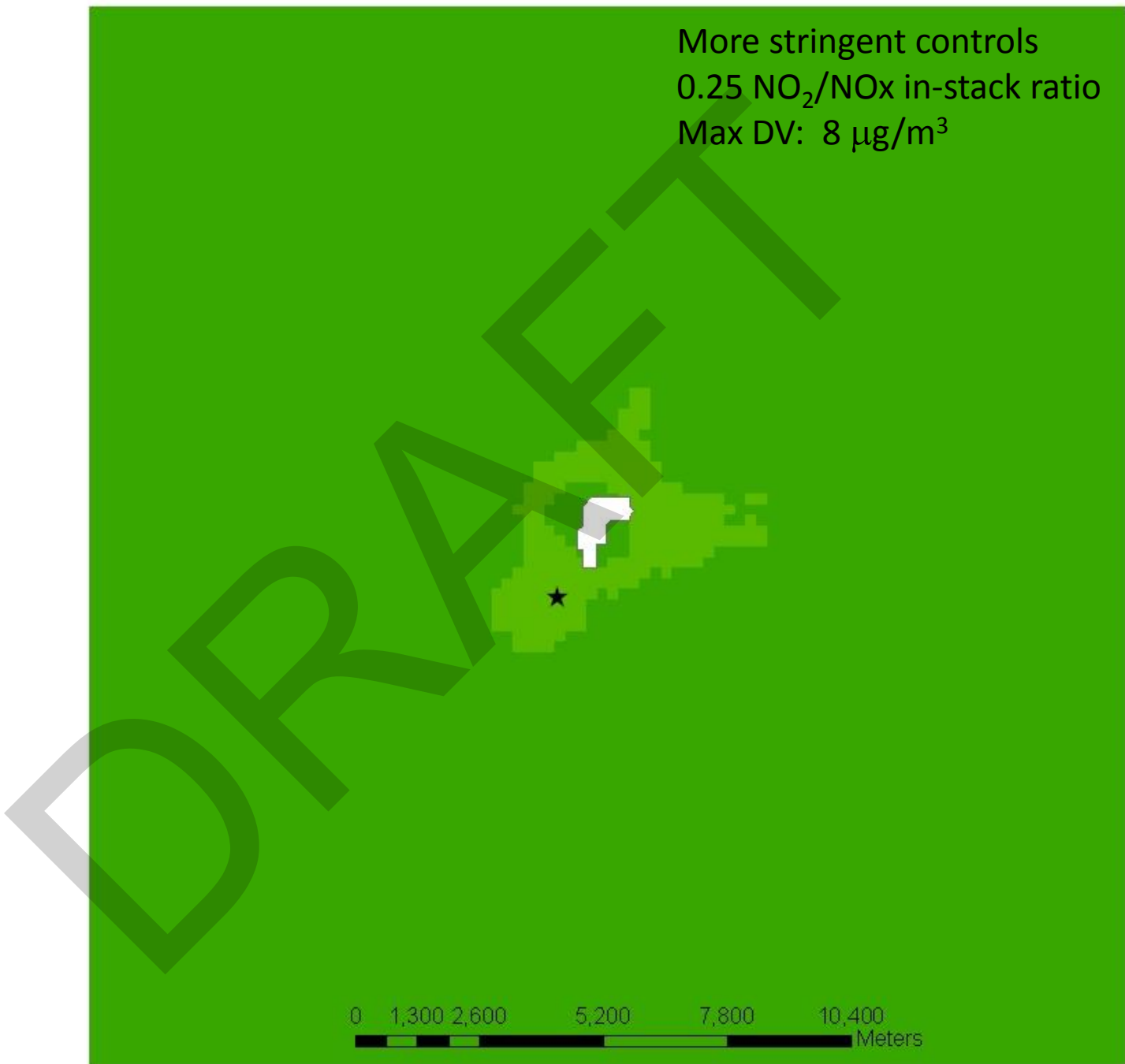
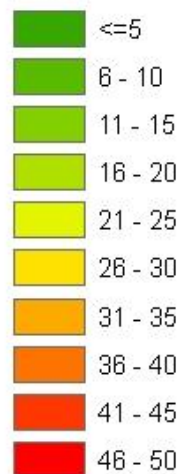
More stringent controls  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 8 μg/m<sup>3</sup>

### Legend



More stringent controls  
0.25 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 8 μg/m<sup>3</sup>

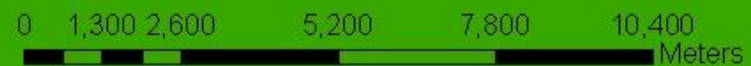
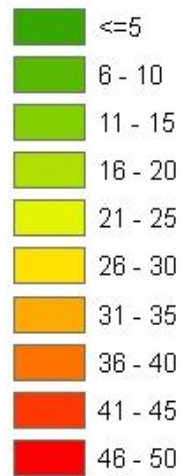
**Legend**



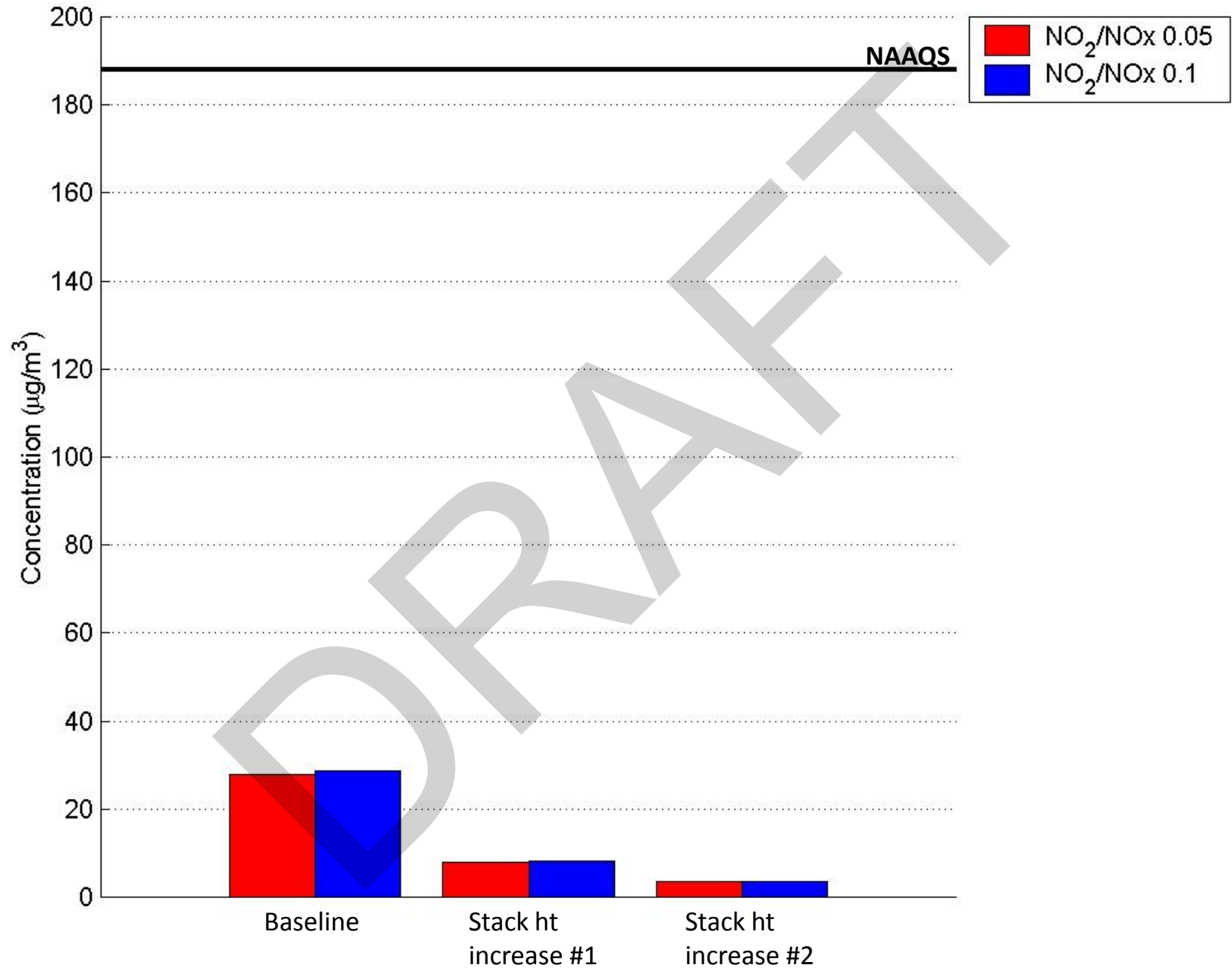


More stringent controls  
0.5 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 8 μg/m<sup>3</sup>

### Legend








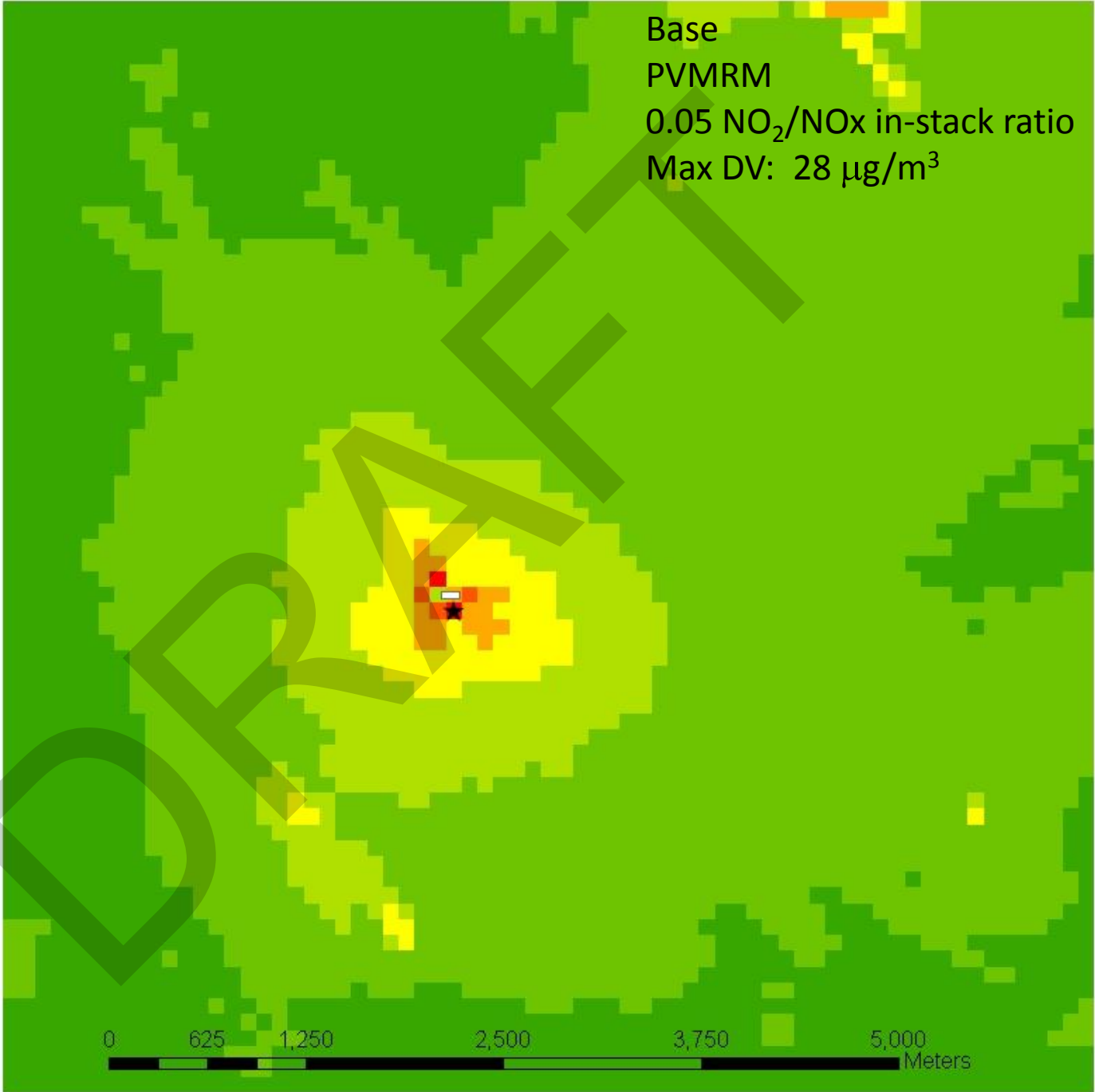
# Landfill Gas Turbine: NO<sub>2</sub>



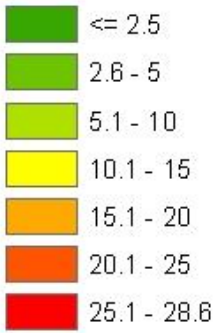
Base  
PVMRM  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 28 μg/m<sup>3</sup>

**Legend**

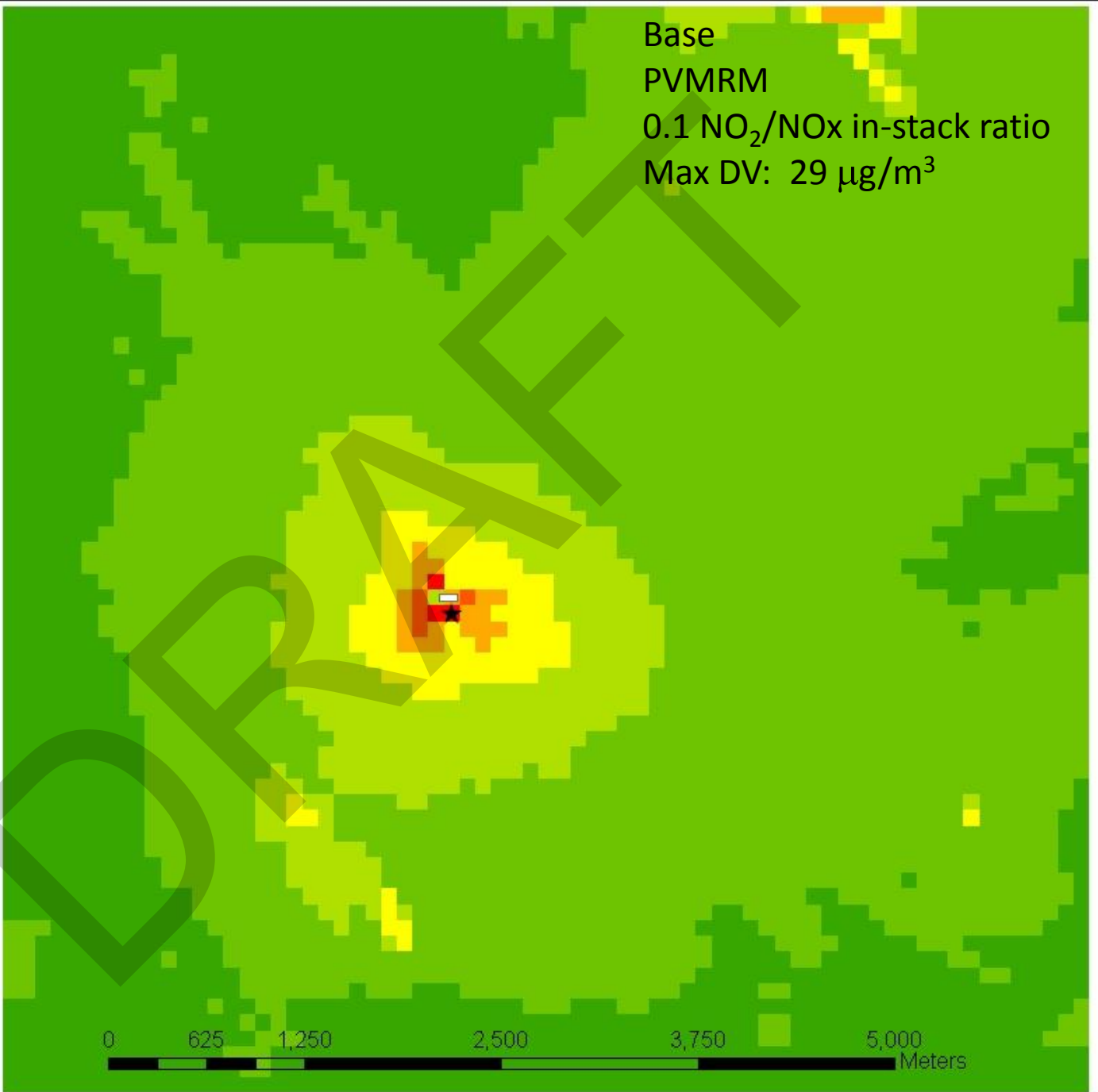
-  <= 2.5
-  2.6 - 5
-  5.1 - 10
-  10.1 - 15
-  15.1 - 20
-  20.1 - 25
-  25.1 - 28.6



**Legend**

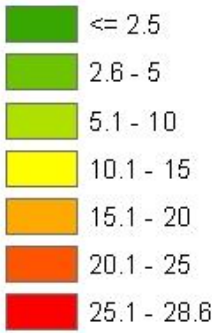


Base  
PVMRM  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 29 μg/m<sup>3</sup>



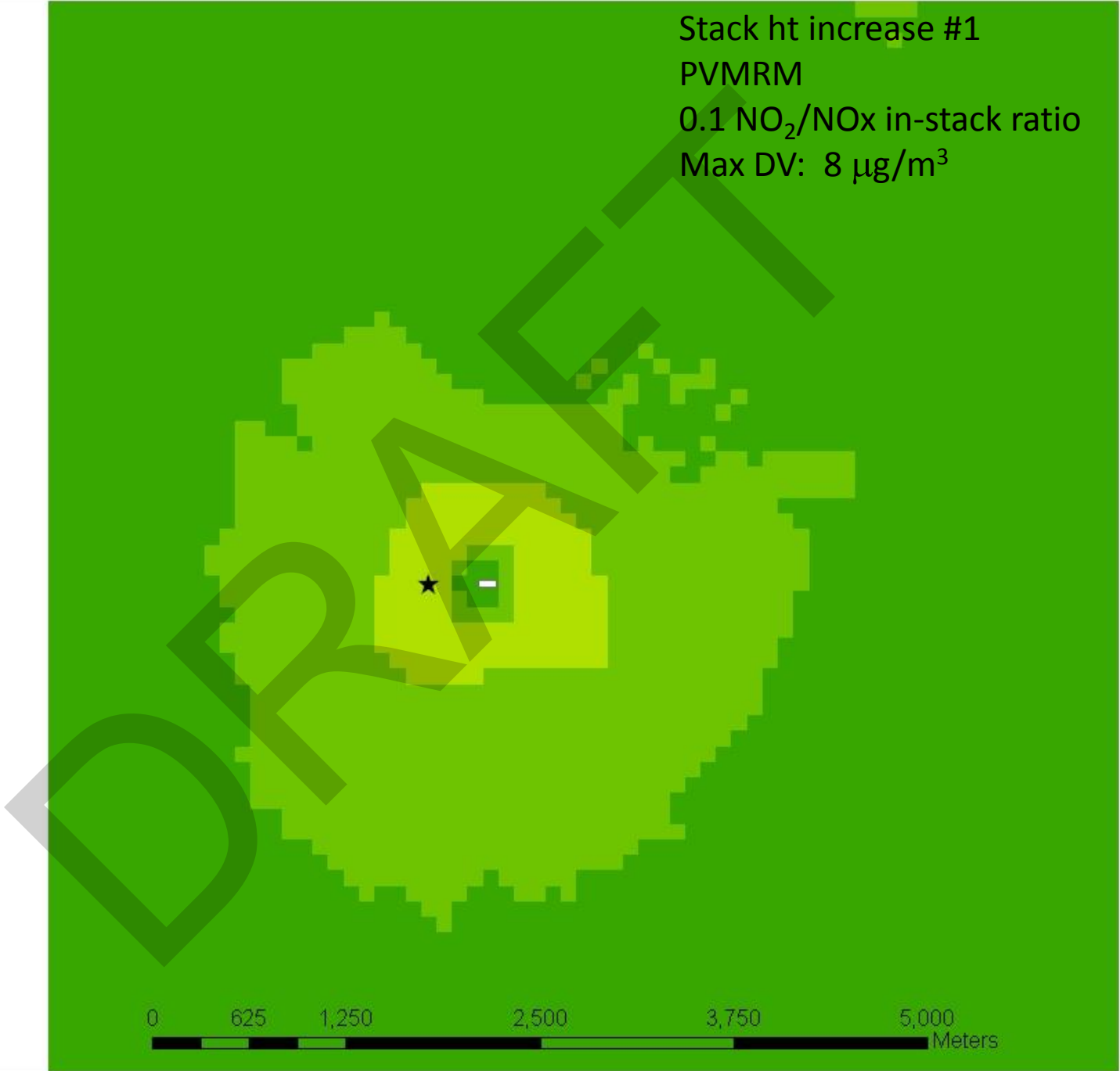
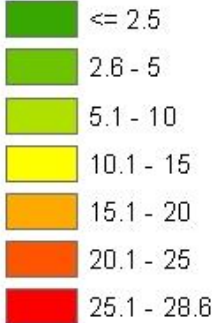
Stack ht increase #1  
PVMRM  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 8 μg/m<sup>3</sup>

**Legend**



Stack ht increase #1  
PVMRM  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 8 μg/m<sup>3</sup>

**Legend**



Stack ht increase #2  
PVMRM  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 4 μg/m<sup>3</sup>

**Legend**



0 625 1,250 2,500 3,750 5,000 Meters

Stack ht increase #2  
PVMRM  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 4 μg/m<sup>3</sup>

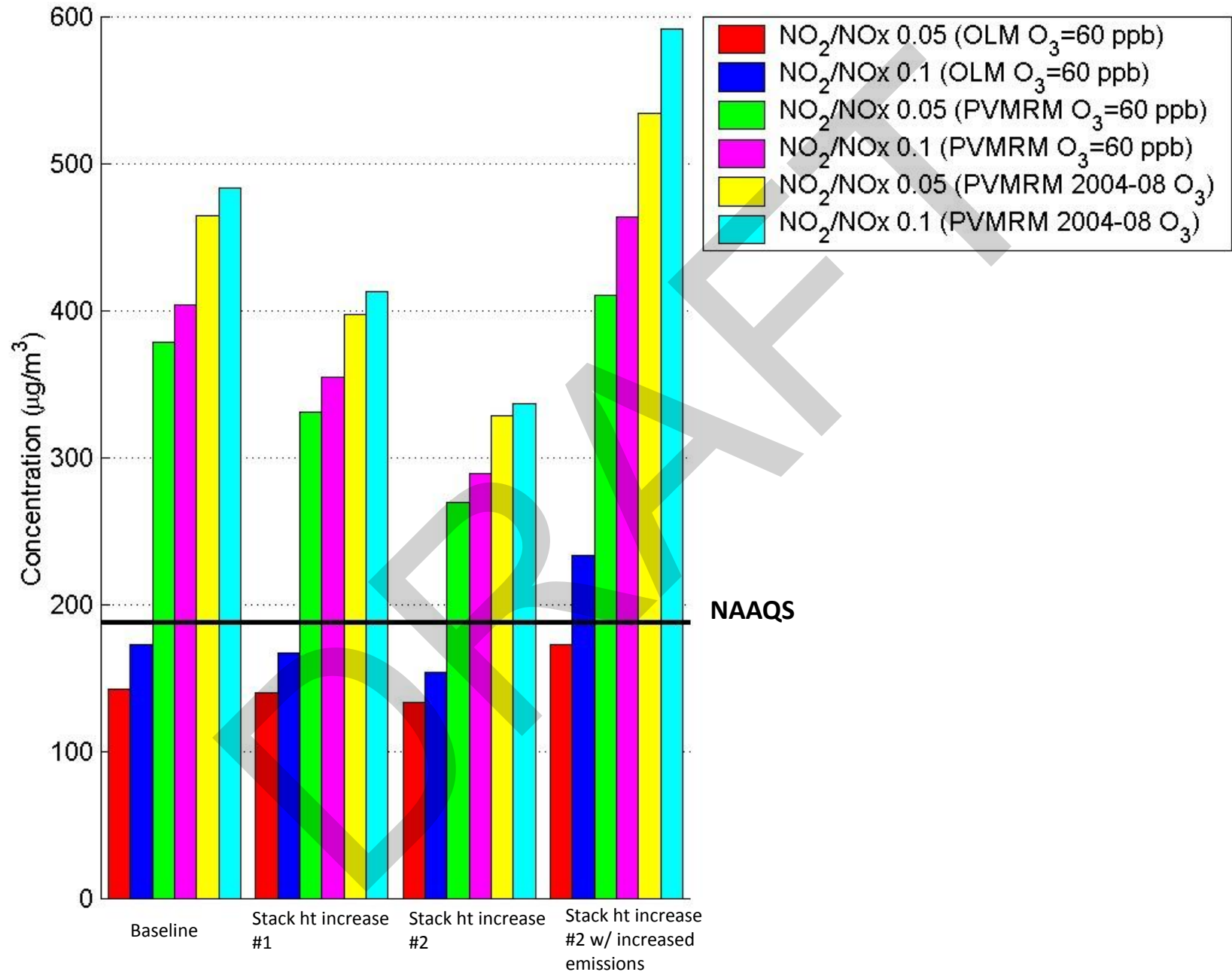
**Legend**



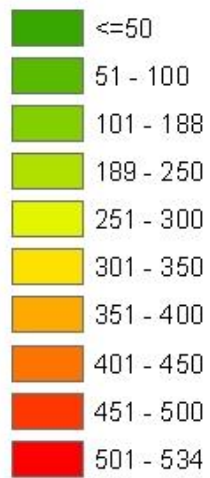
0 625 1,250 2,500 3,750 5,000 Meters



# Fuel Oil Turbine: NO<sub>2</sub>



### Legend

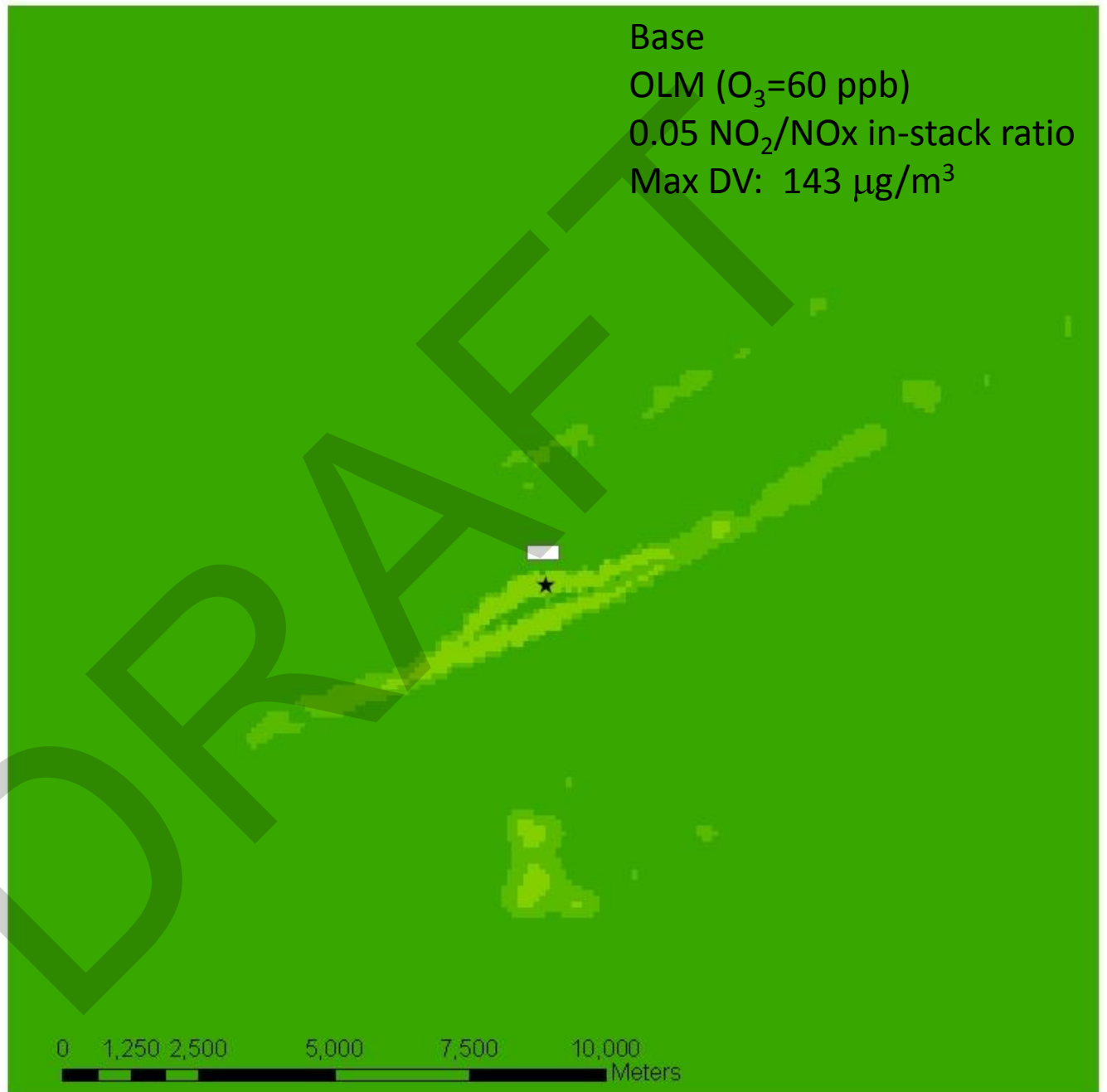


Base

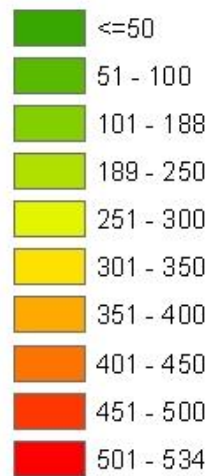
OLM ( $O_3=60$  ppb)

0.05  $NO_2/NO_x$  in-stack ratio

Max DV:  $143 \mu g/m^3$



## Legend

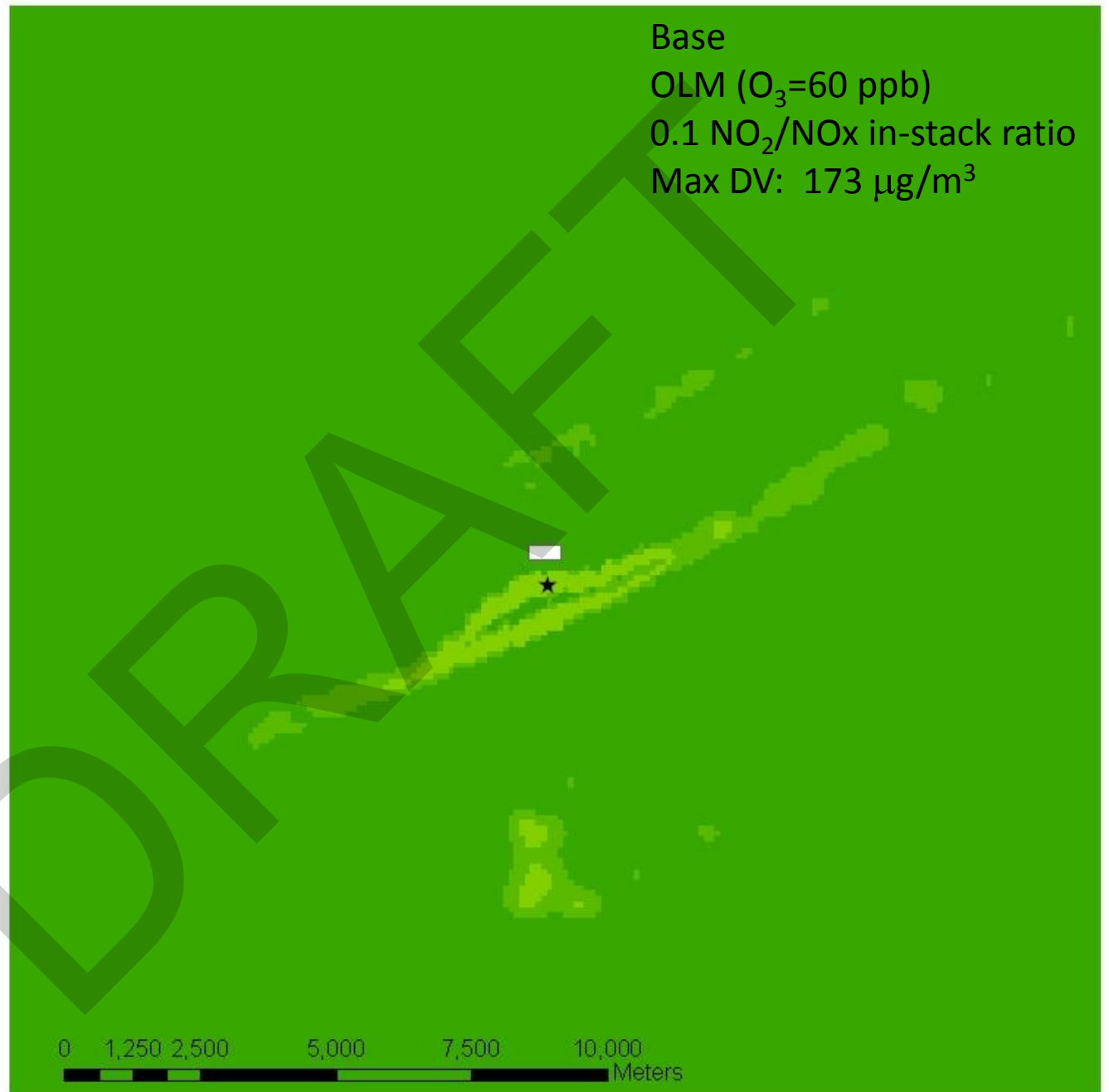


Base

OLM ( $O_3=60$  ppb)

0.1  $NO_2/NO_x$  in-stack ratio

Max DV:  $173 \mu g/m^3$



## Legend

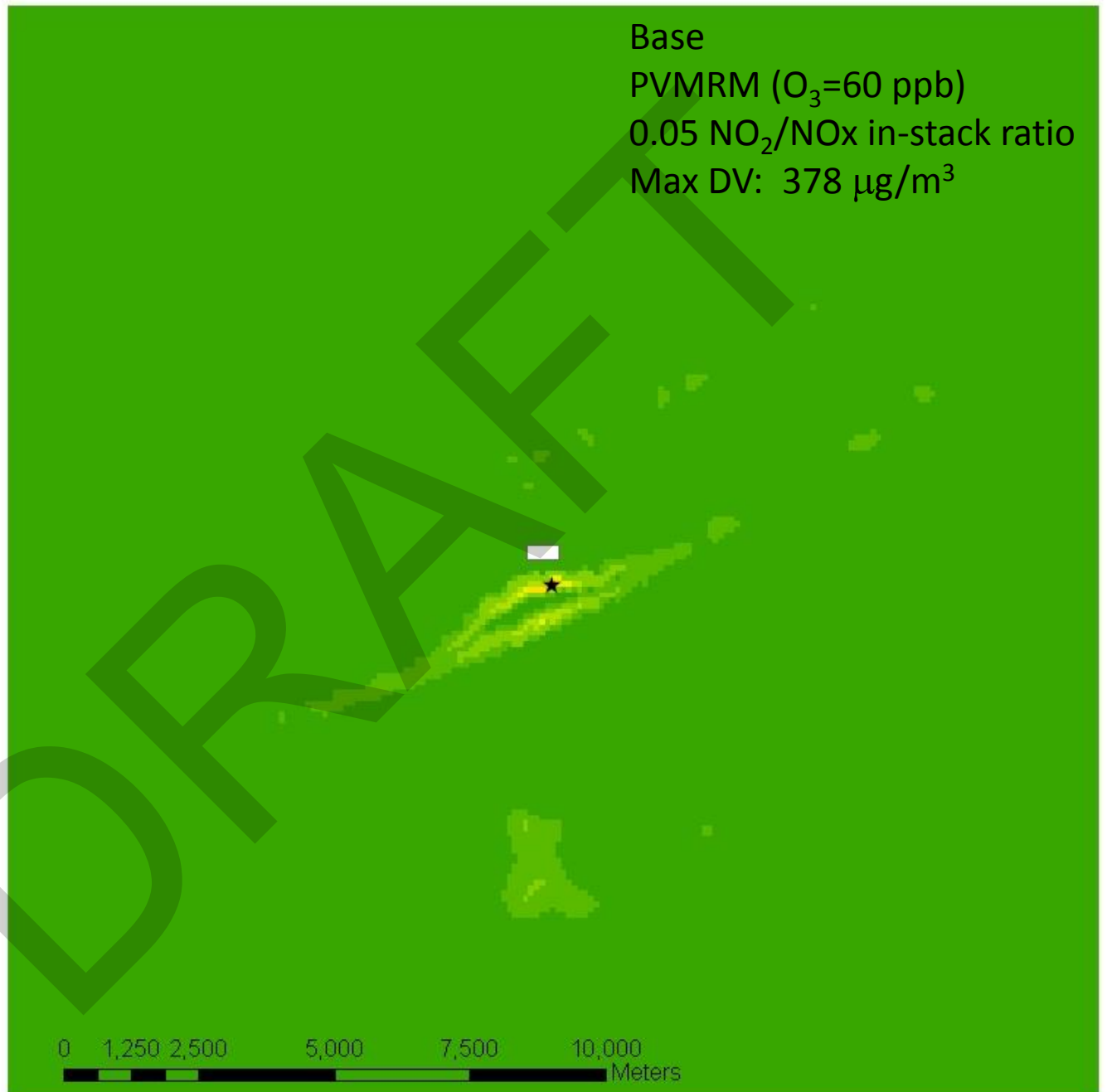


Base

PVMRM ( $O_3=60$  ppb)

0.05  $NO_2/NO_x$  in-stack ratio

Max DV:  $378 \mu g/m^3$



0 1,250 2,500 5,000 7,500 10,000 Meters

## Legend

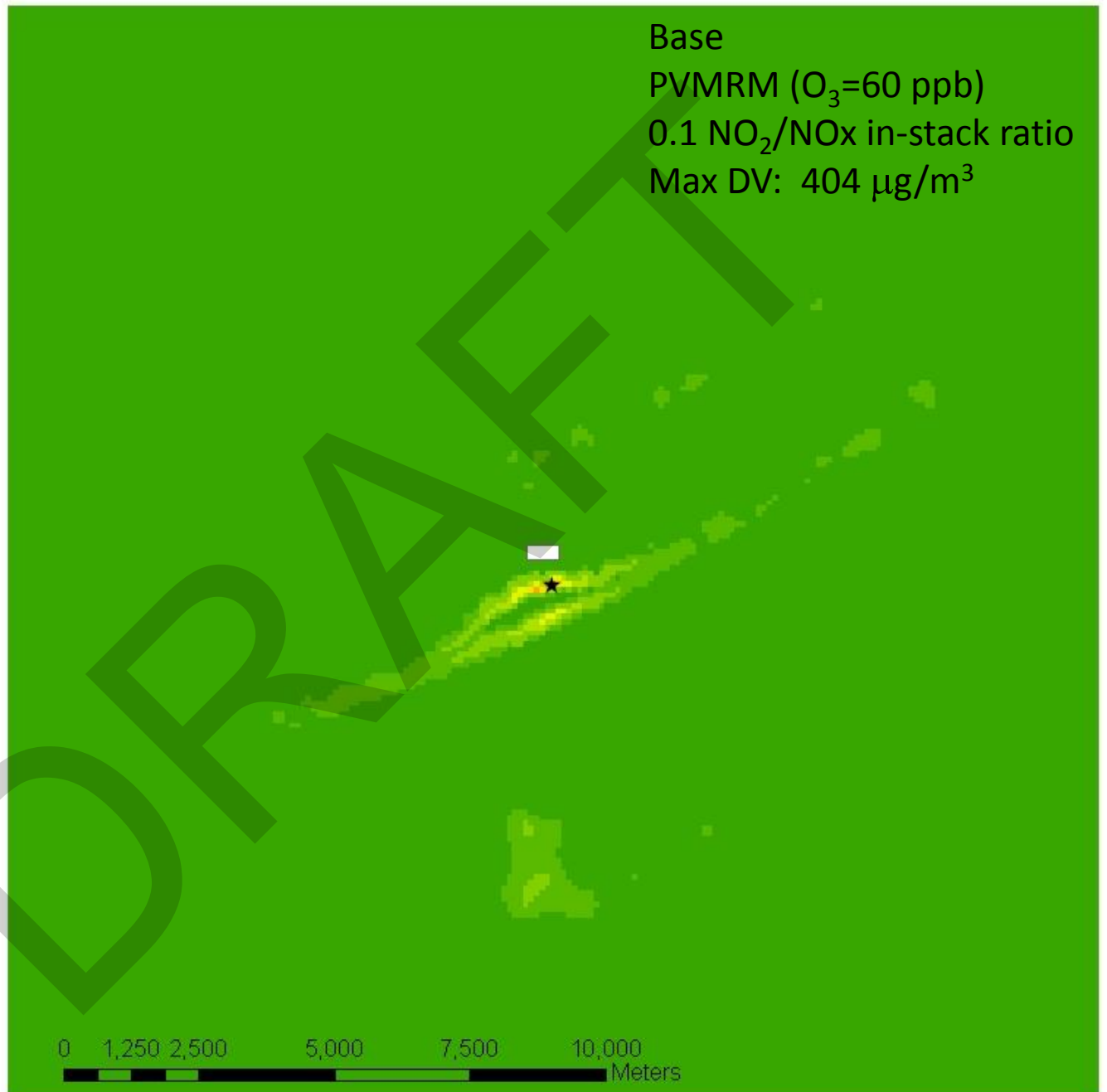


Base

PVMRM ( $O_3=60$  ppb)

0.1  $NO_2/NO_x$  in-stack ratio

Max DV:  $404 \mu\text{g}/\text{m}^3$



## Legend

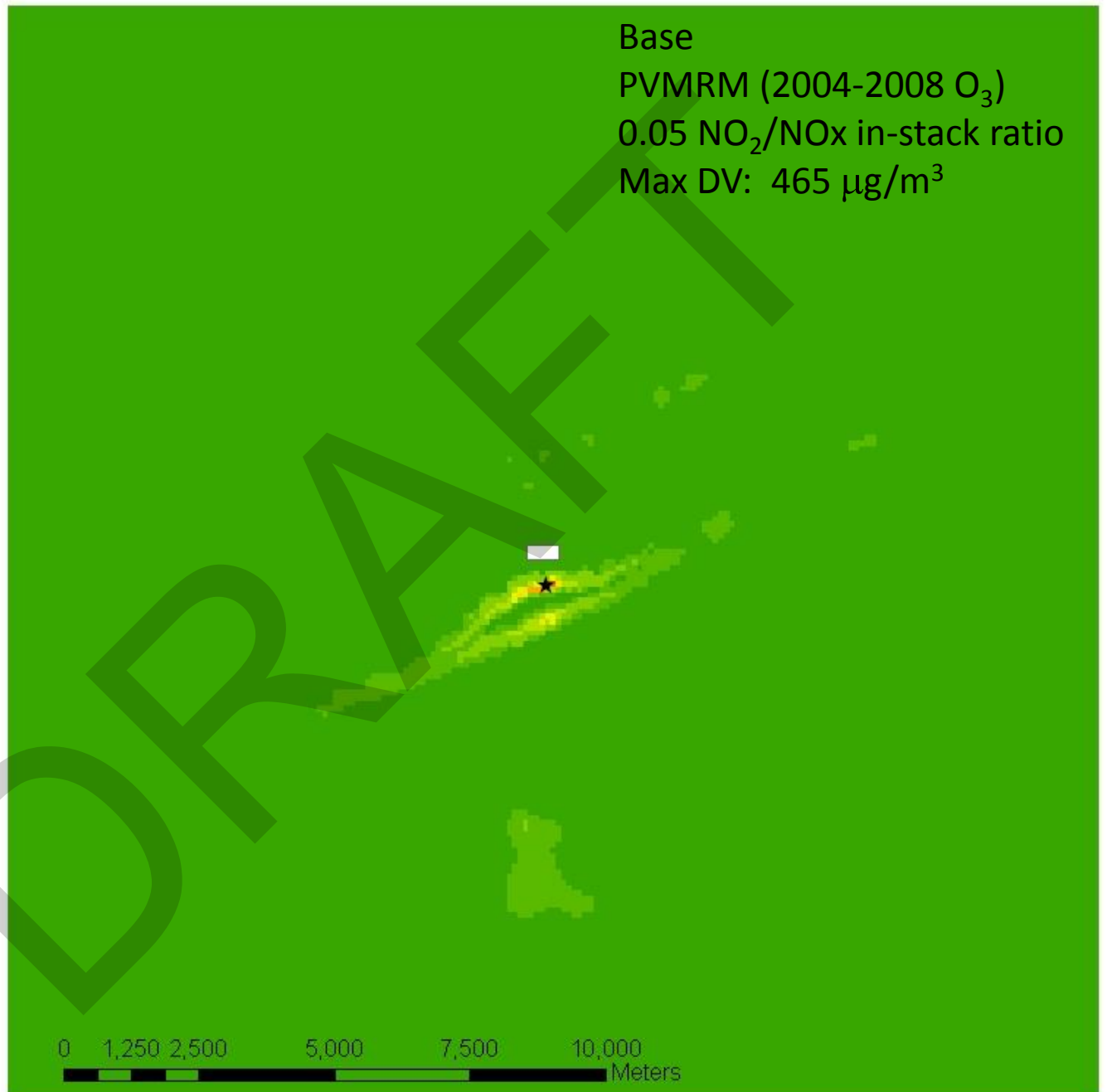


Base

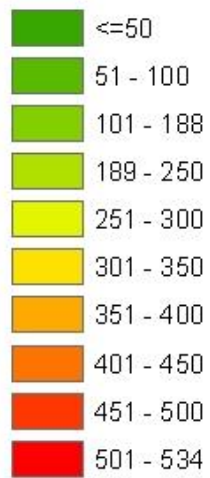
PVMRM (2004-2008 O<sub>3</sub>)

0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 465 μg/m<sup>3</sup>



# Legend

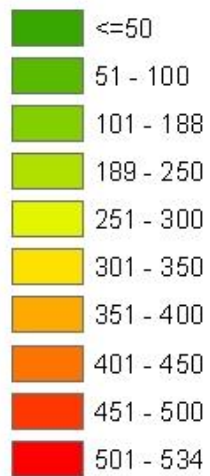


Base

PVMRM (2004-2008 O<sub>3</sub>)  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 484 μg/m<sup>3</sup>



## Legend



Stack ht increase #1

OLM ( $O_3=60$  ppb)

0.05  $NO_2/NO_x$  in-stack ratio

Max DV:  $140 \mu g/m^3$





## Legend

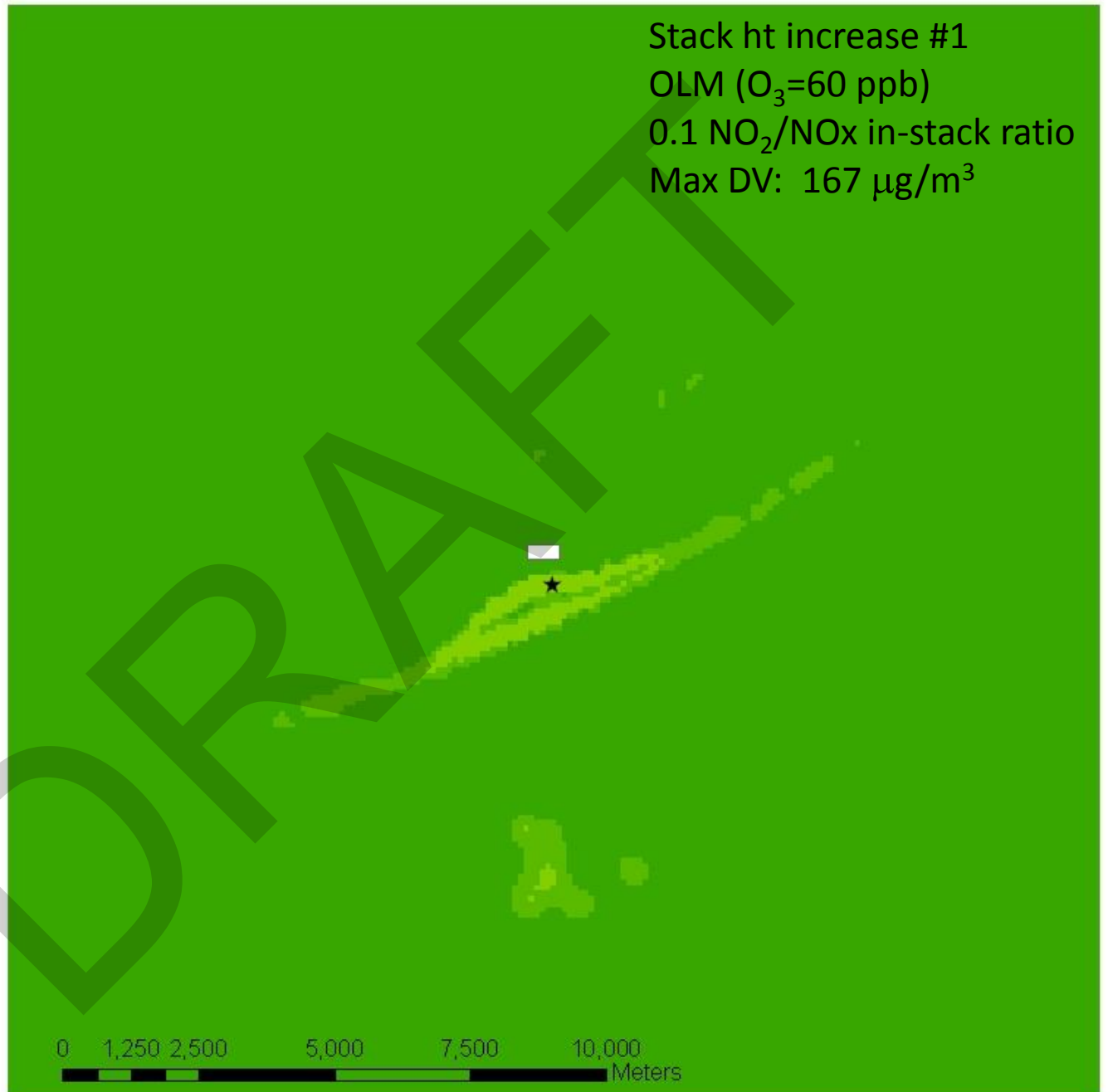


Stack ht increase #1

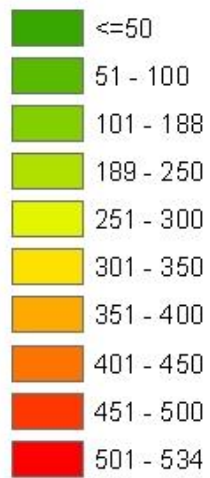
OLM ( $O_3=60$  ppb)

0.1  $NO_2/NO_x$  in-stack ratio

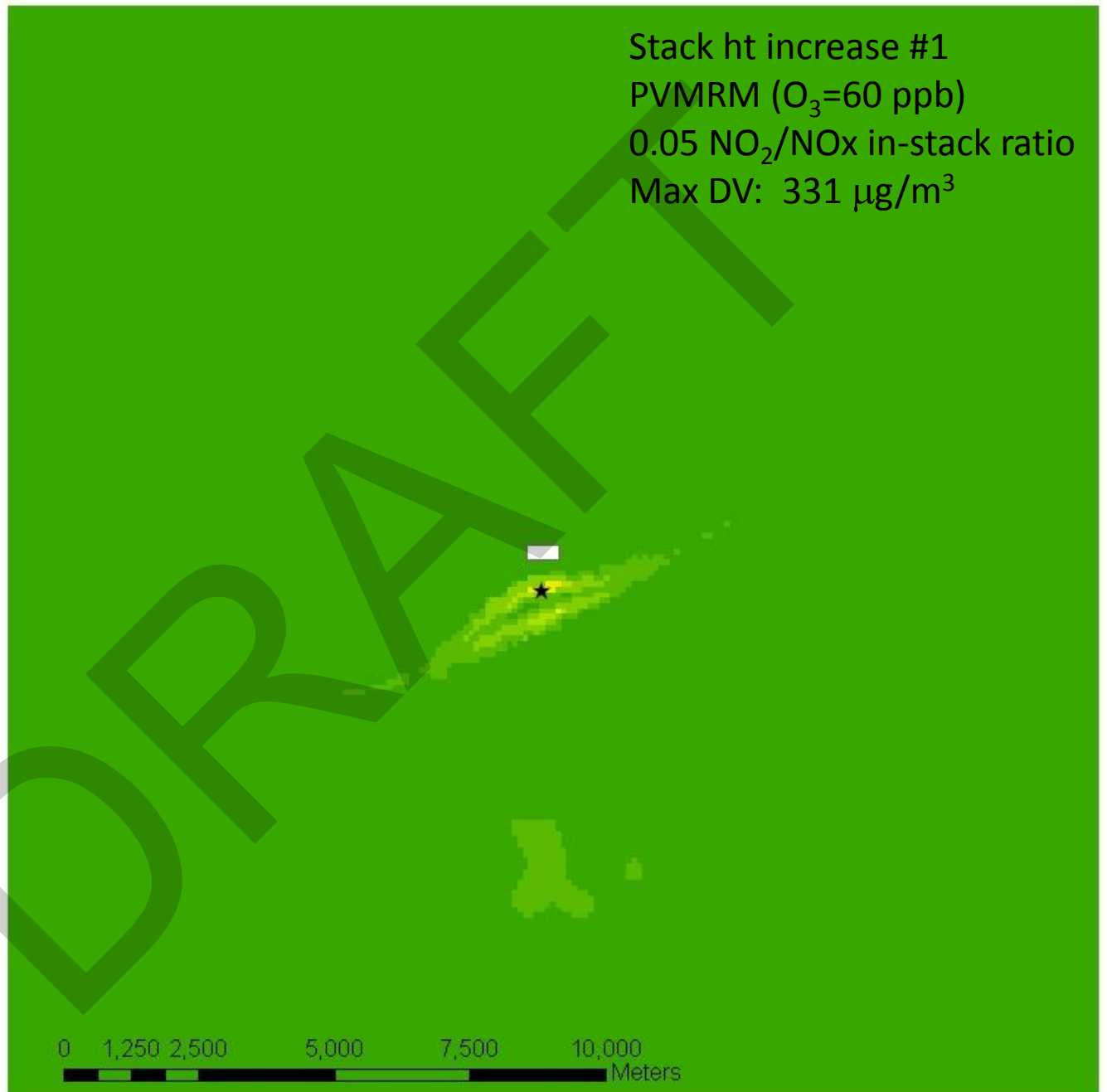
Max DV:  $167 \mu\text{g}/\text{m}^3$



### Legend



Stack ht increase #1  
PVMRM ( $O_3=60$  ppb)  
0.05  $NO_2/NO_x$  in-stack ratio  
Max DV:  $331 \mu g/m^3$

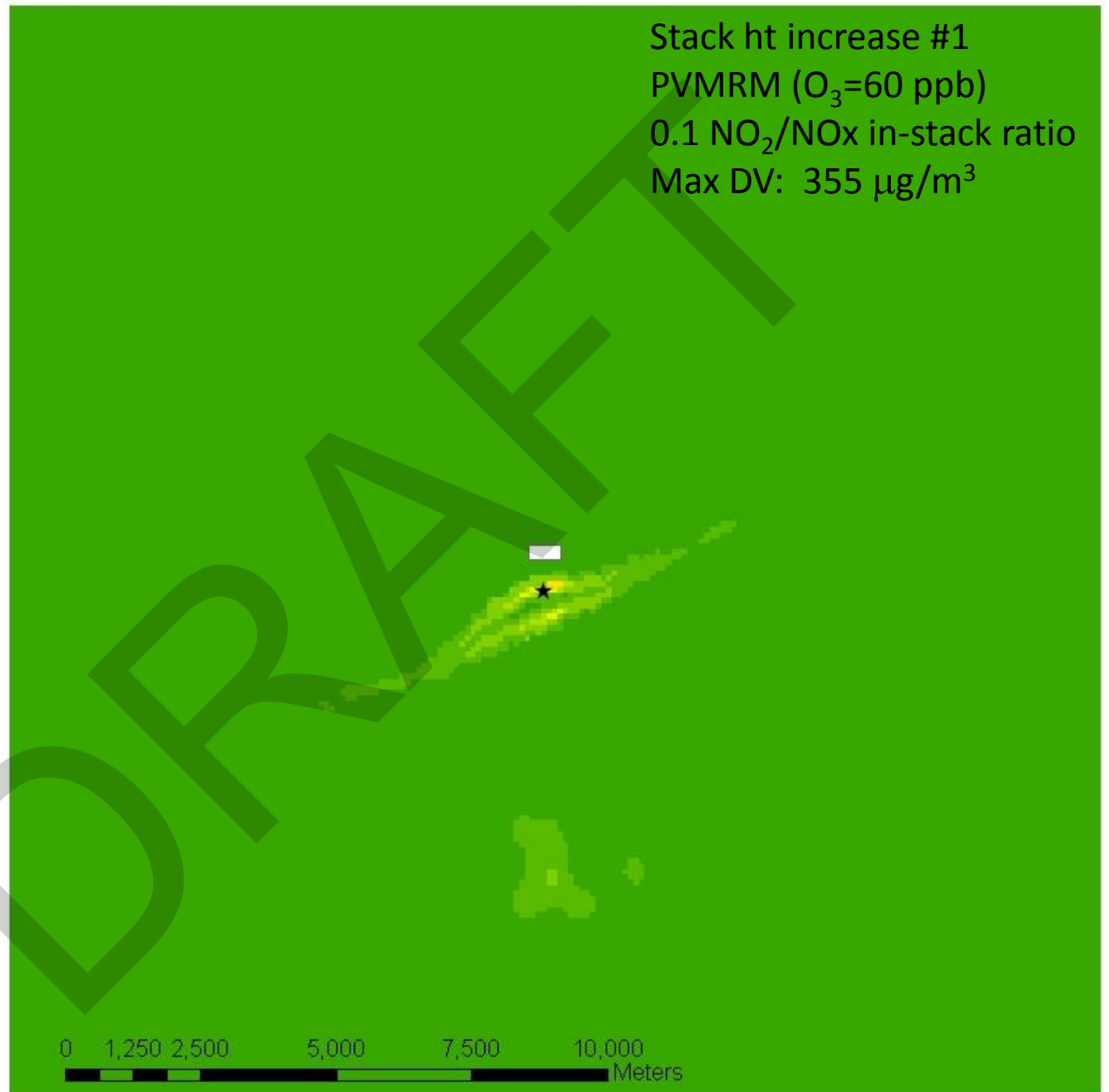


0 1,250 2,500 5,000 7,500 10,000  
Meters

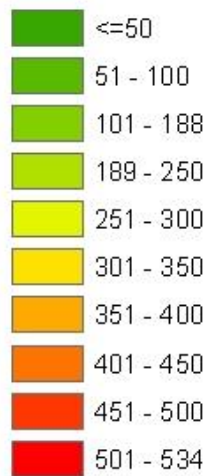
## Legend



Stack ht increase #1  
PVMRM ( $O_3=60$  ppb)  
0.1  $NO_2/NO_x$  in-stack ratio  
Max DV:  $355 \mu g/m^3$



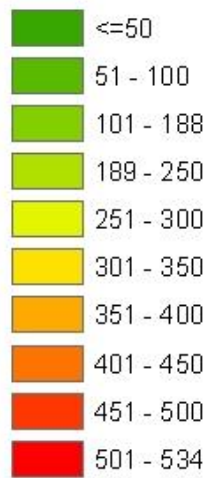
## Legend



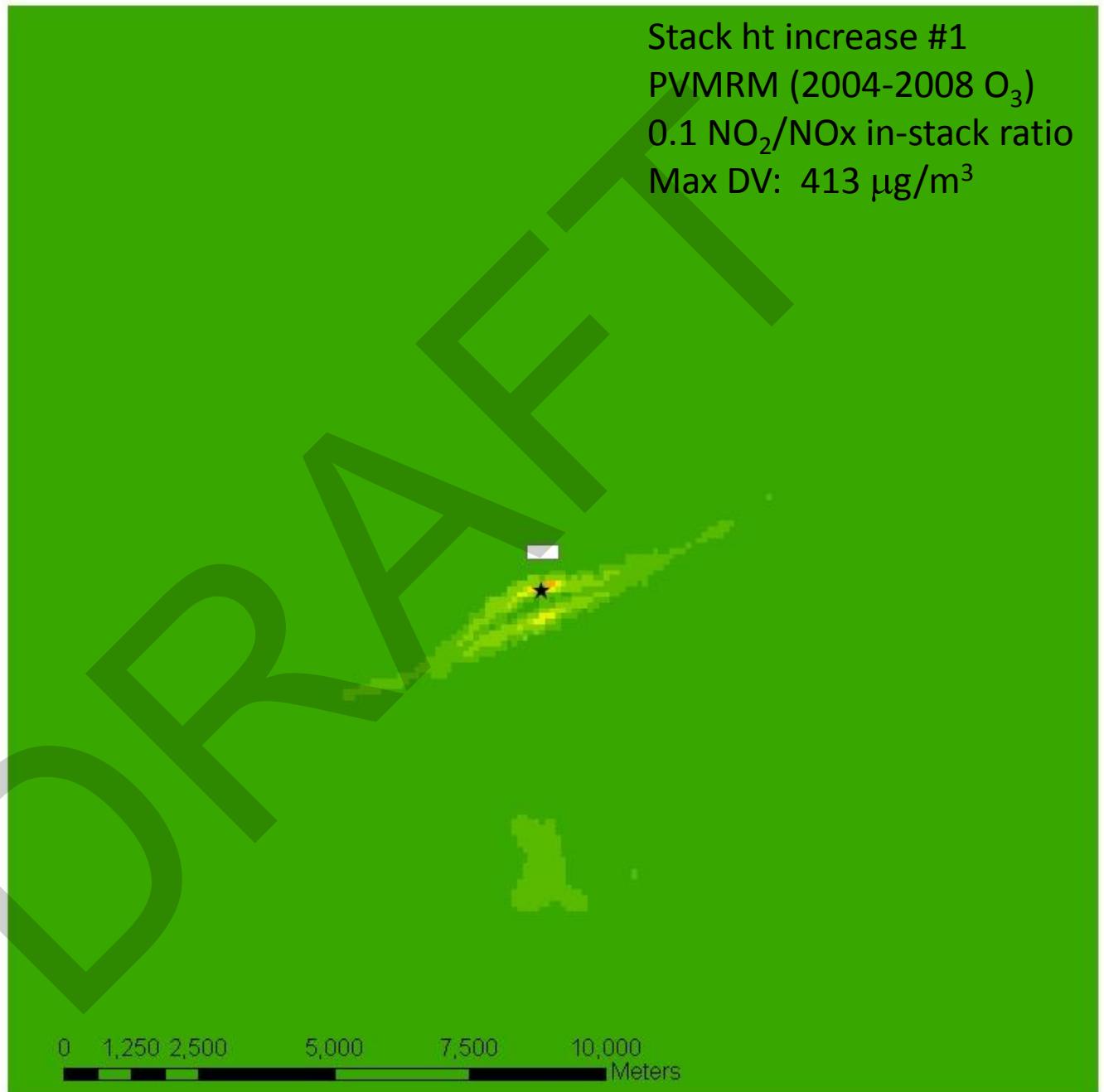
Stack ht increase #1  
PVMRM (2004-2008 O<sub>3</sub>)  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 398 μg/m<sup>3</sup>



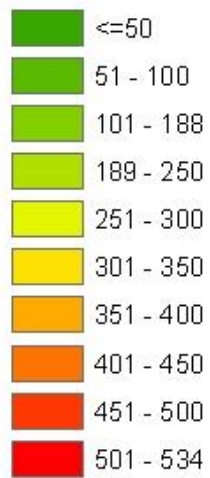
# Legend



Stack ht increase #1  
PVMRM (2004-2008 O<sub>3</sub>)  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 413 μg/m<sup>3</sup>



# Legend

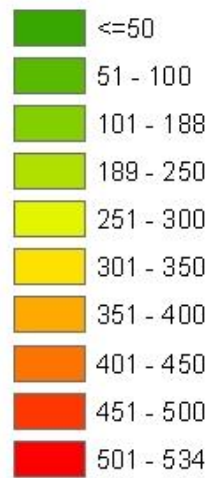


Stack ht increase #2  
OLM ( $O_3=60$  ppb)  
0.05  $NO_2/NO_x$  in-stack ratio  
Max DV:  $133 \mu g/m^3$



0 1,250 2,500 5,000 7,500 10,000  
Meters

## Legend

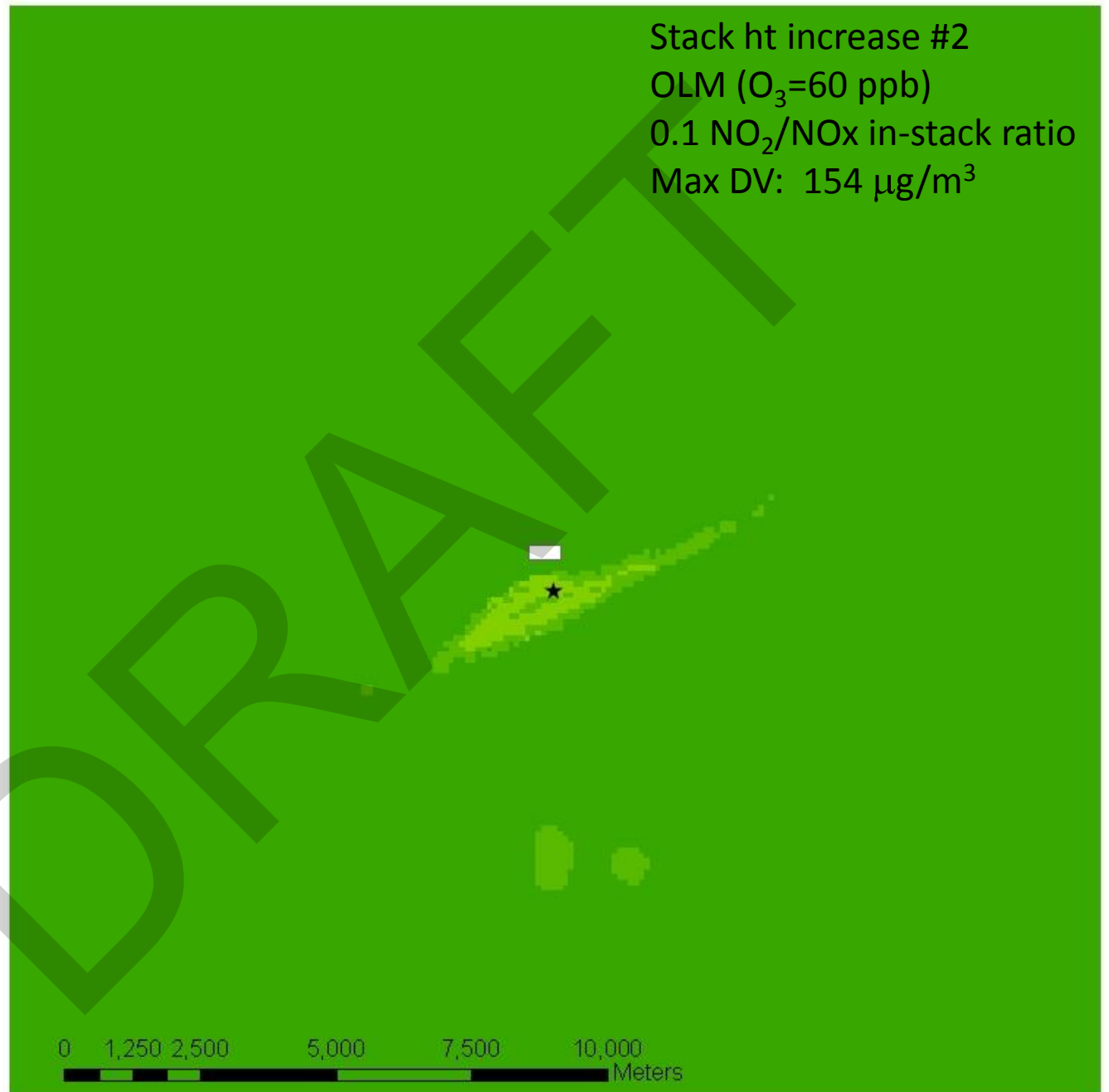


Stack ht increase #2

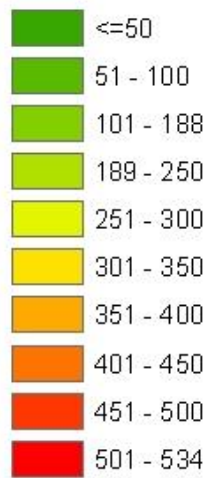
OLM ( $O_3=60$  ppb)

0.1  $NO_2/NO_x$  in-stack ratio

Max DV:  $154 \mu g/m^3$



## Legend



Stack ht increase #2  
PVMRM ( $O_3=60$  ppb)  
0.05  $NO_2/NO_x$  in-stack ratio  
Max DV:  $269 \mu g/m^3$

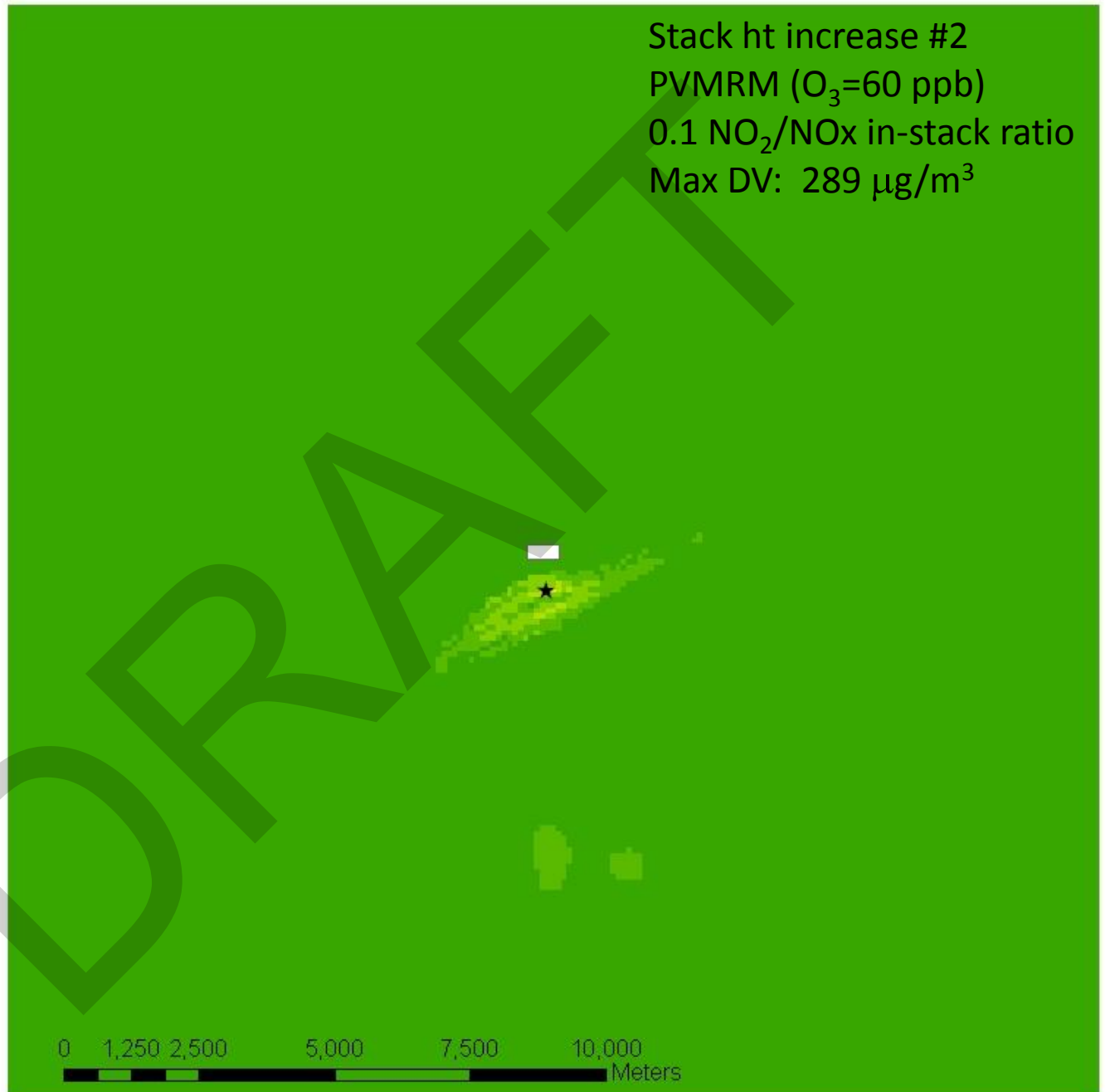




### Legend



Stack ht increase #2  
PVMRM ( $O_3=60$  ppb)  
0.1  $NO_2/NO_x$  in-stack ratio  
Max DV:  $289 \mu g/m^3$



0 1,250 2,500 5,000 7,500 10,000  
Meters

## Legend

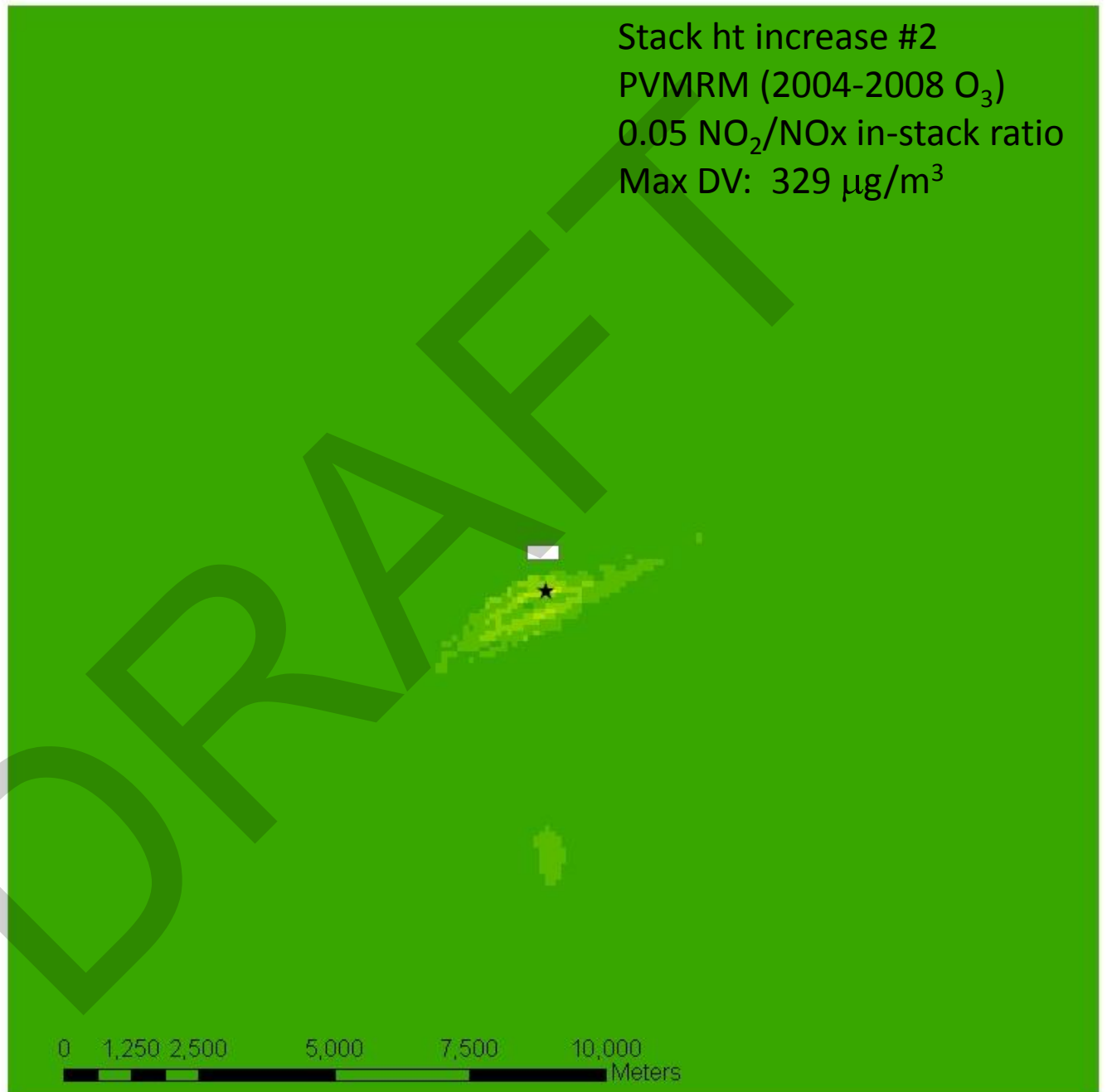


Stack ht increase #2

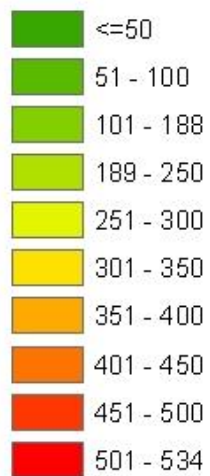
PVMRM (2004-2008 O<sub>3</sub>)

0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio

Max DV: 329 μg/m<sup>3</sup>



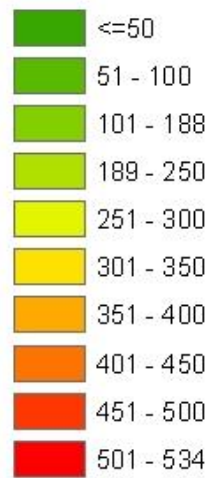
### Legend



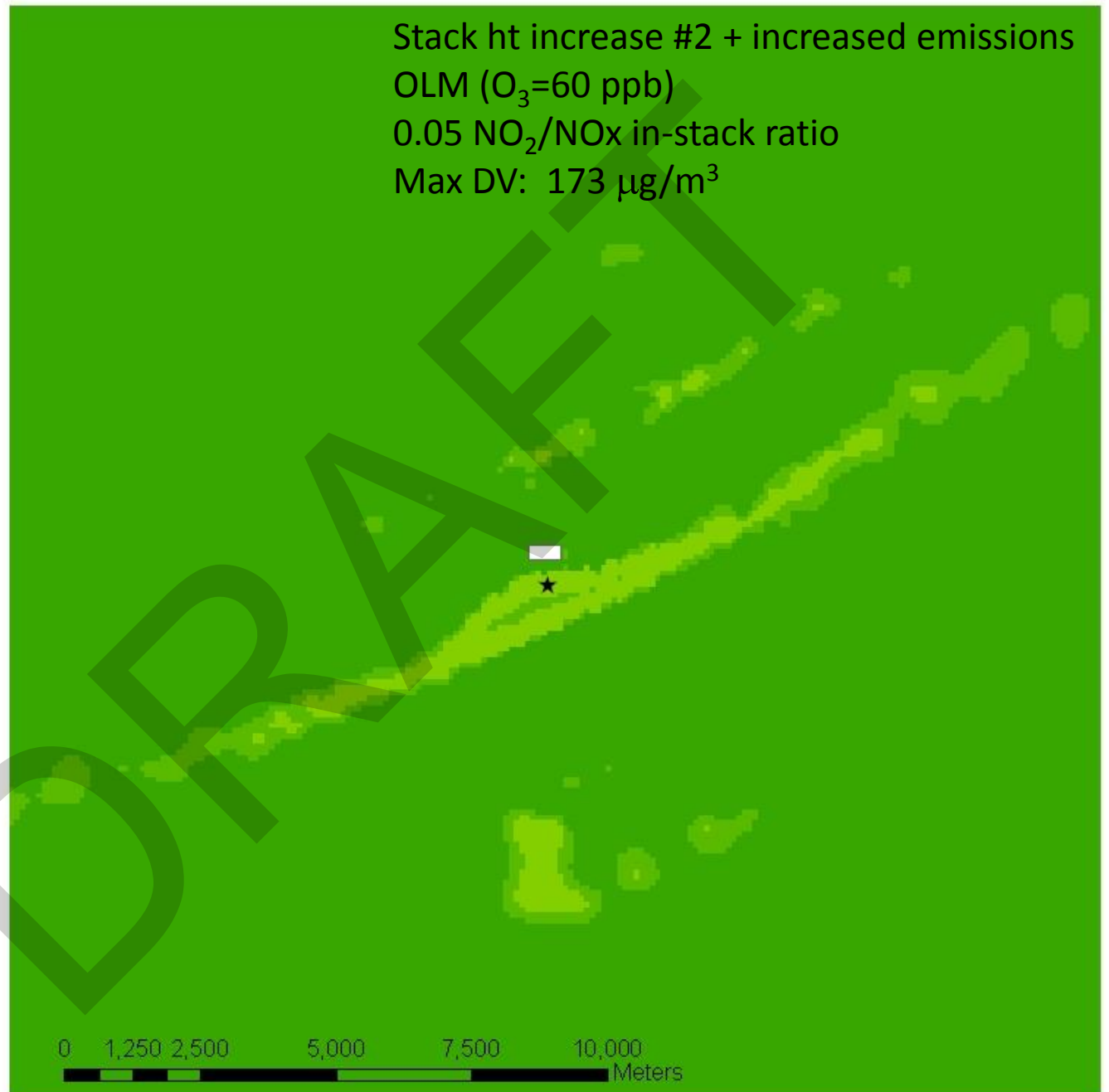
Stack ht increase #2  
PVMRM (2004-2008 O<sub>3</sub>)  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 338 μg/m<sup>3</sup>



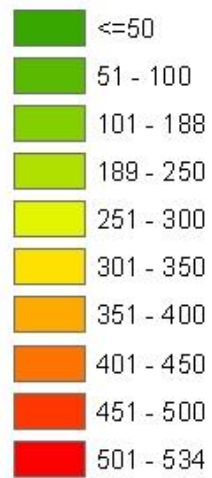
## Legend



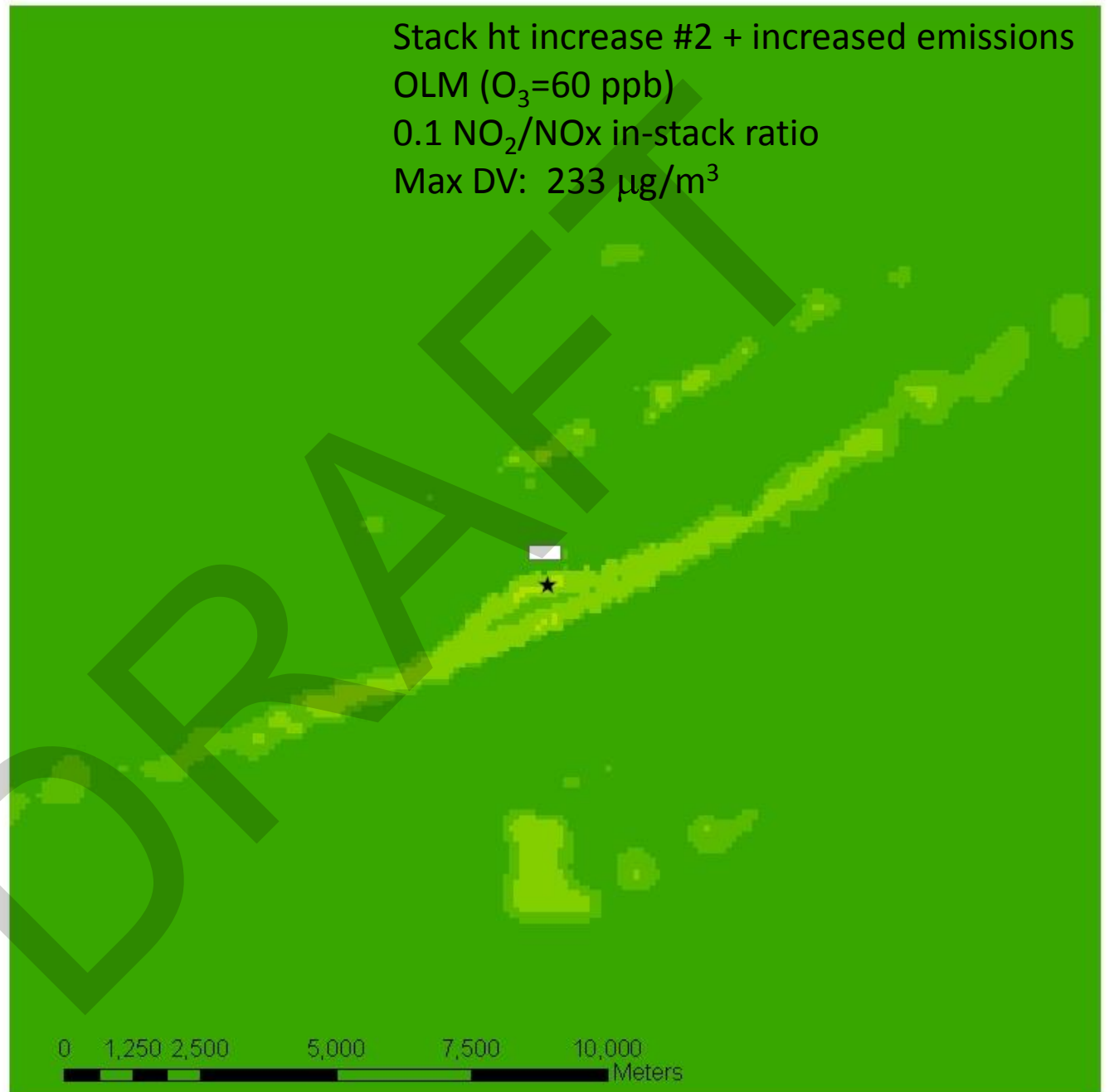
Stack ht increase #2 + increased emissions  
OLM ( $O_3=60$  ppb)  
0.05  $NO_2/NO_x$  in-stack ratio  
Max DV:  $173 \mu g/m^3$



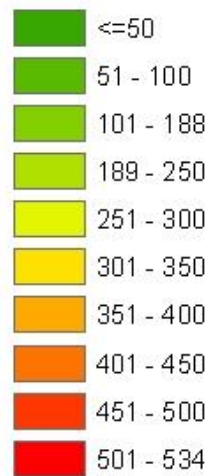
## Legend



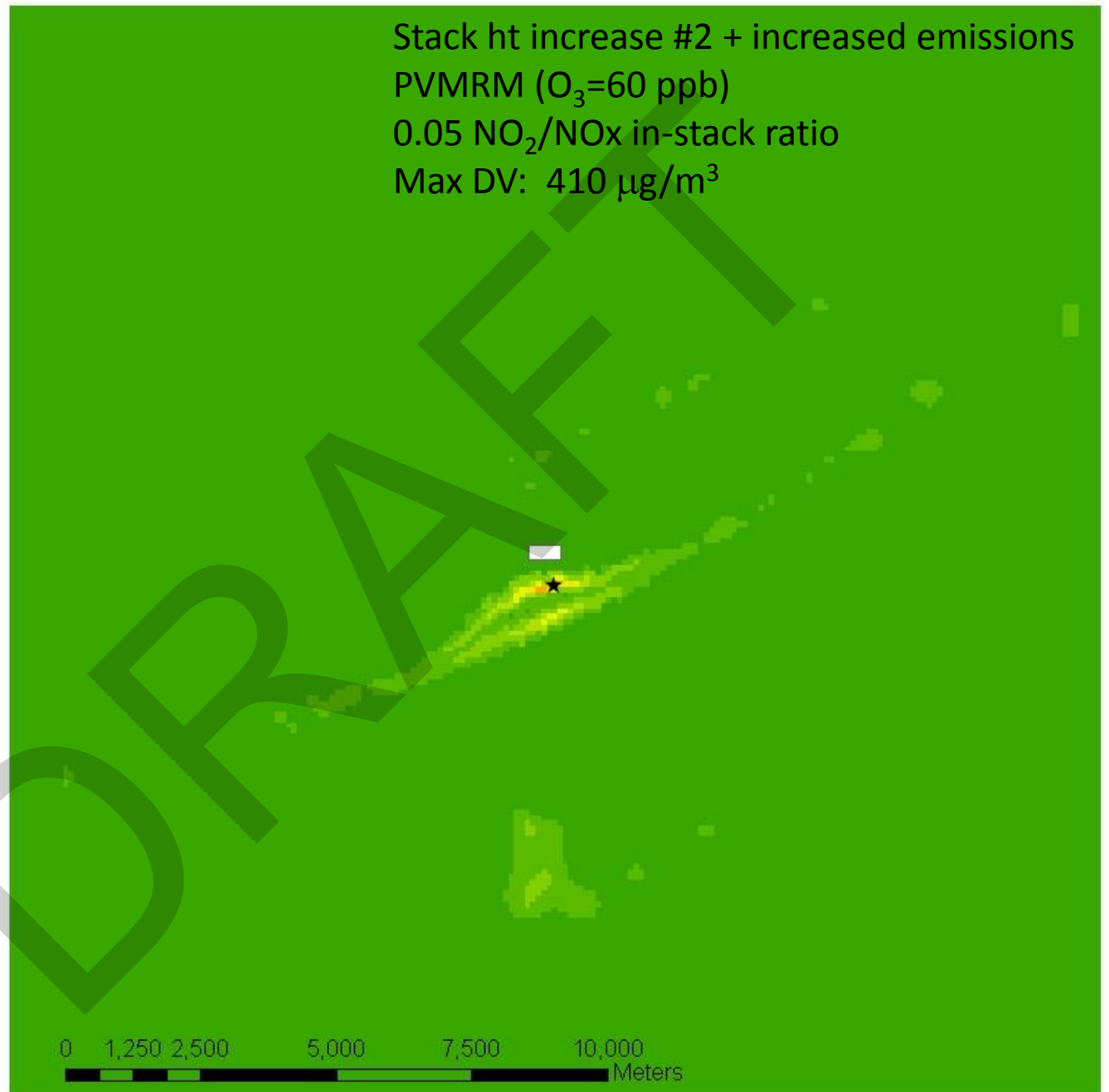
Stack ht increase #2 + increased emissions  
OLM ( $O_3=60$  ppb)  
0.1  $NO_2/NO_x$  in-stack ratio  
Max DV:  $233 \mu g/m^3$



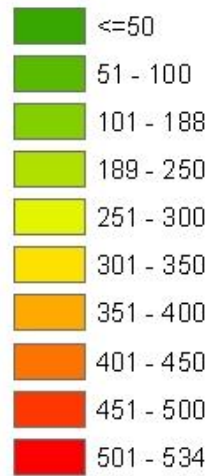
## Legend



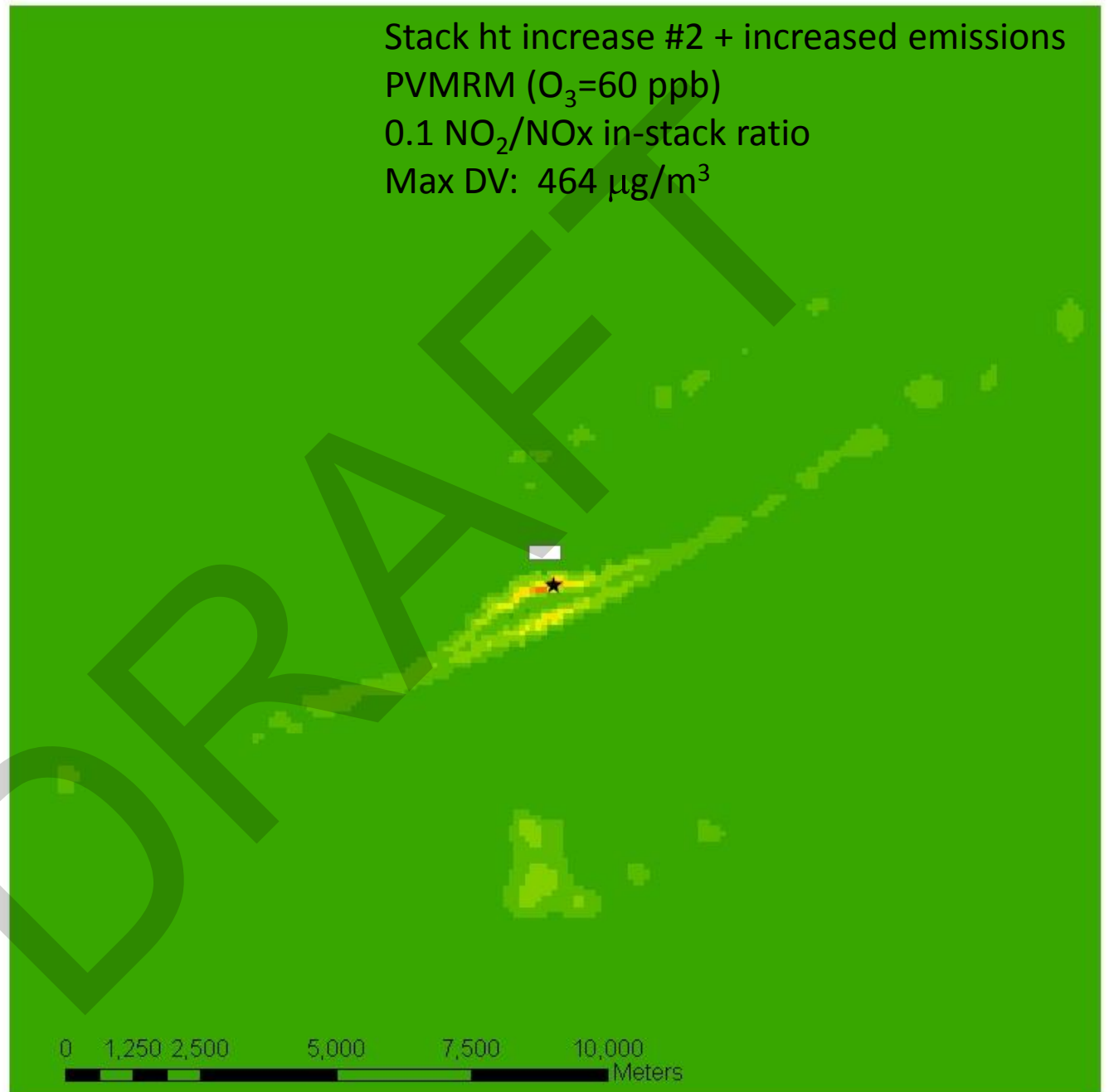
Stack ht increase #2 + increased emissions  
PVMRM ( $O_3=60$  ppb)  
0.05  $NO_2/NO_x$  in-stack ratio  
Max DV:  $410 \mu g/m^3$



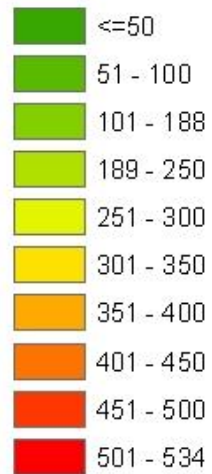
## Legend



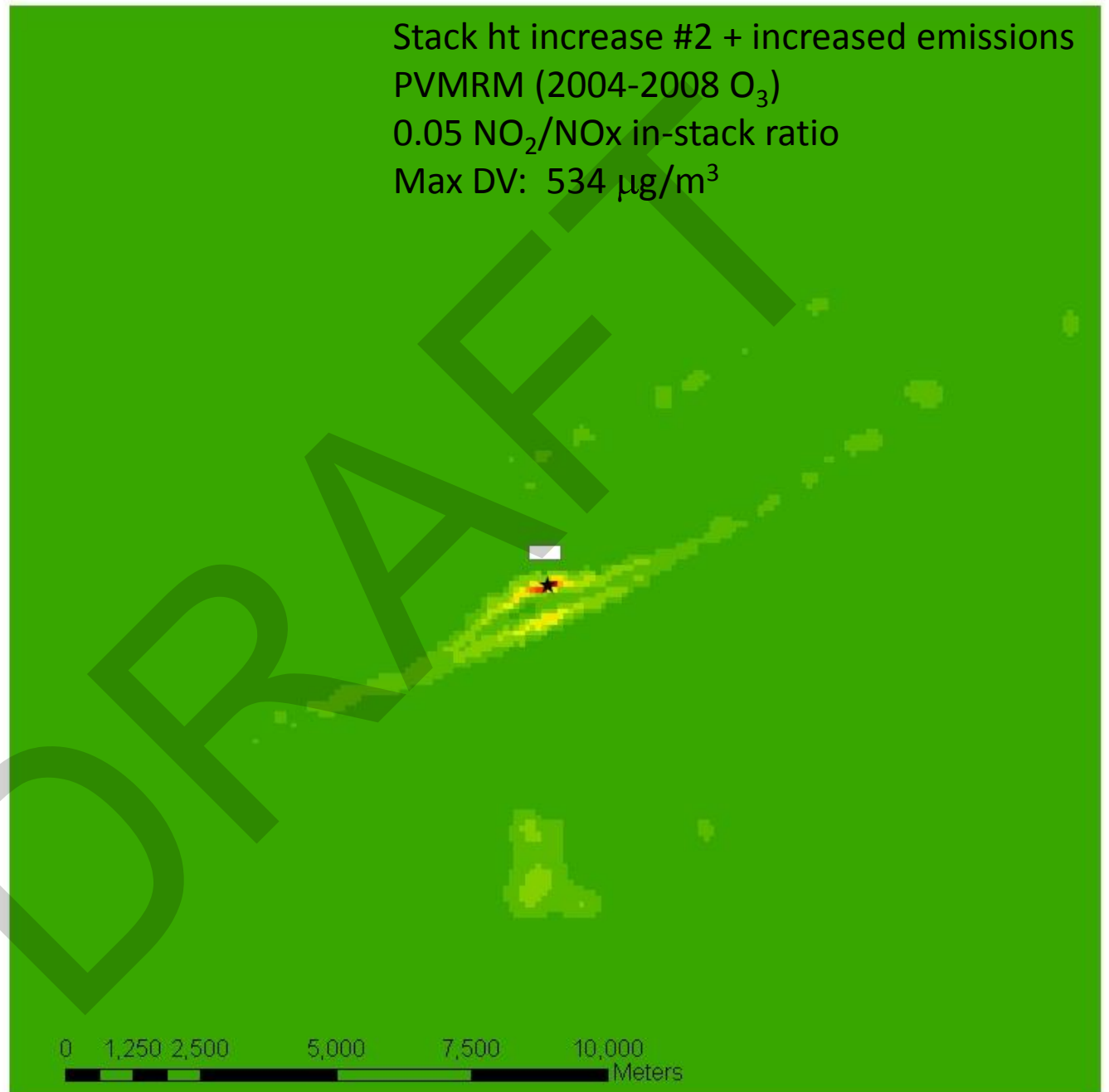
Stack ht increase #2 + increased emissions  
PVMRM ( $O_3=60$  ppb)  
0.1  $NO_2/NO_x$  in-stack ratio  
Max DV:  $464 \mu g/m^3$



## Legend

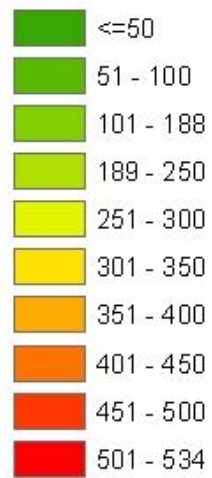


Stack ht increase #2 + increased emissions  
PVMRM (2004-2008 O<sub>3</sub>)  
0.05 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 534 μg/m<sup>3</sup>

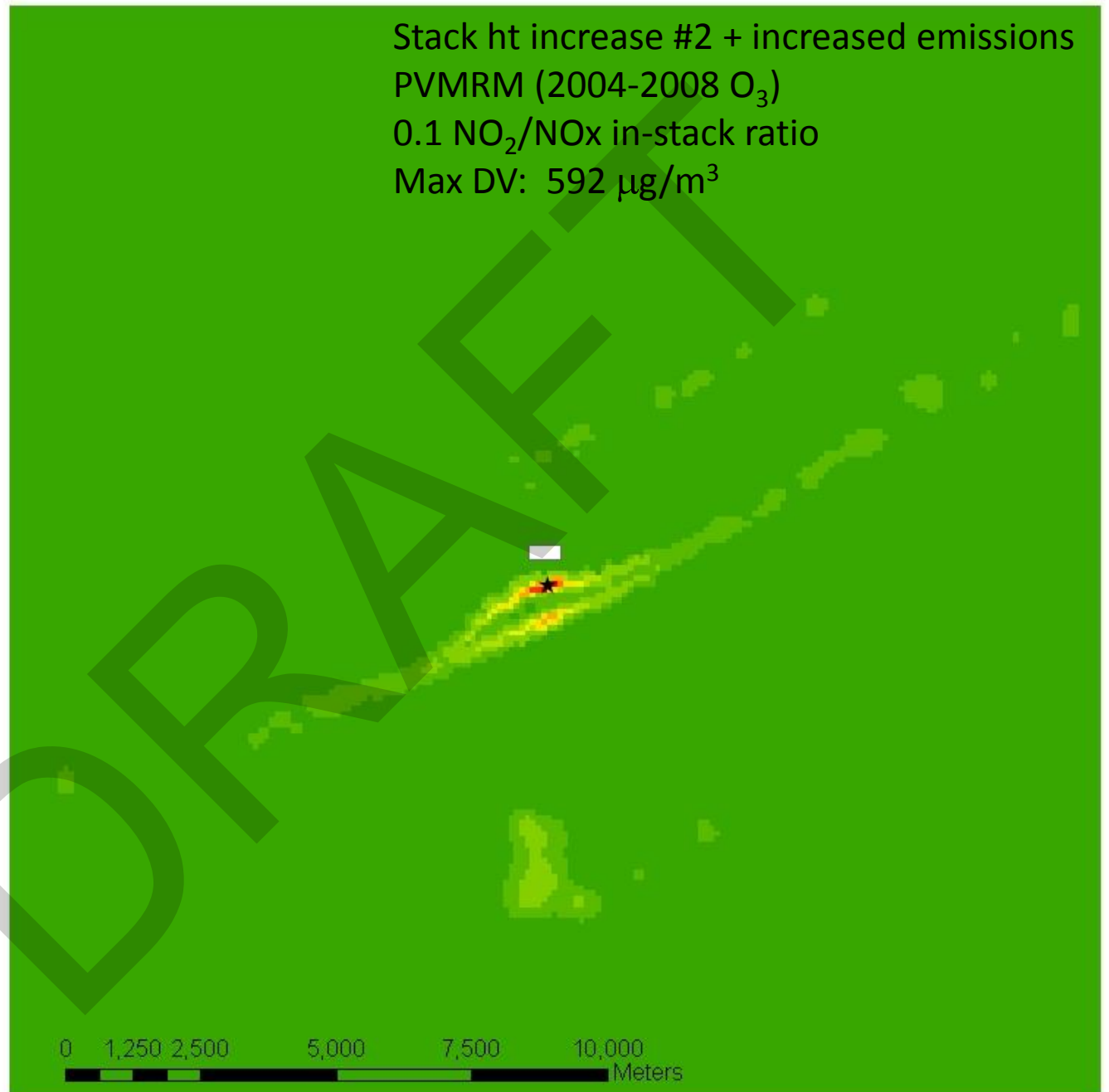




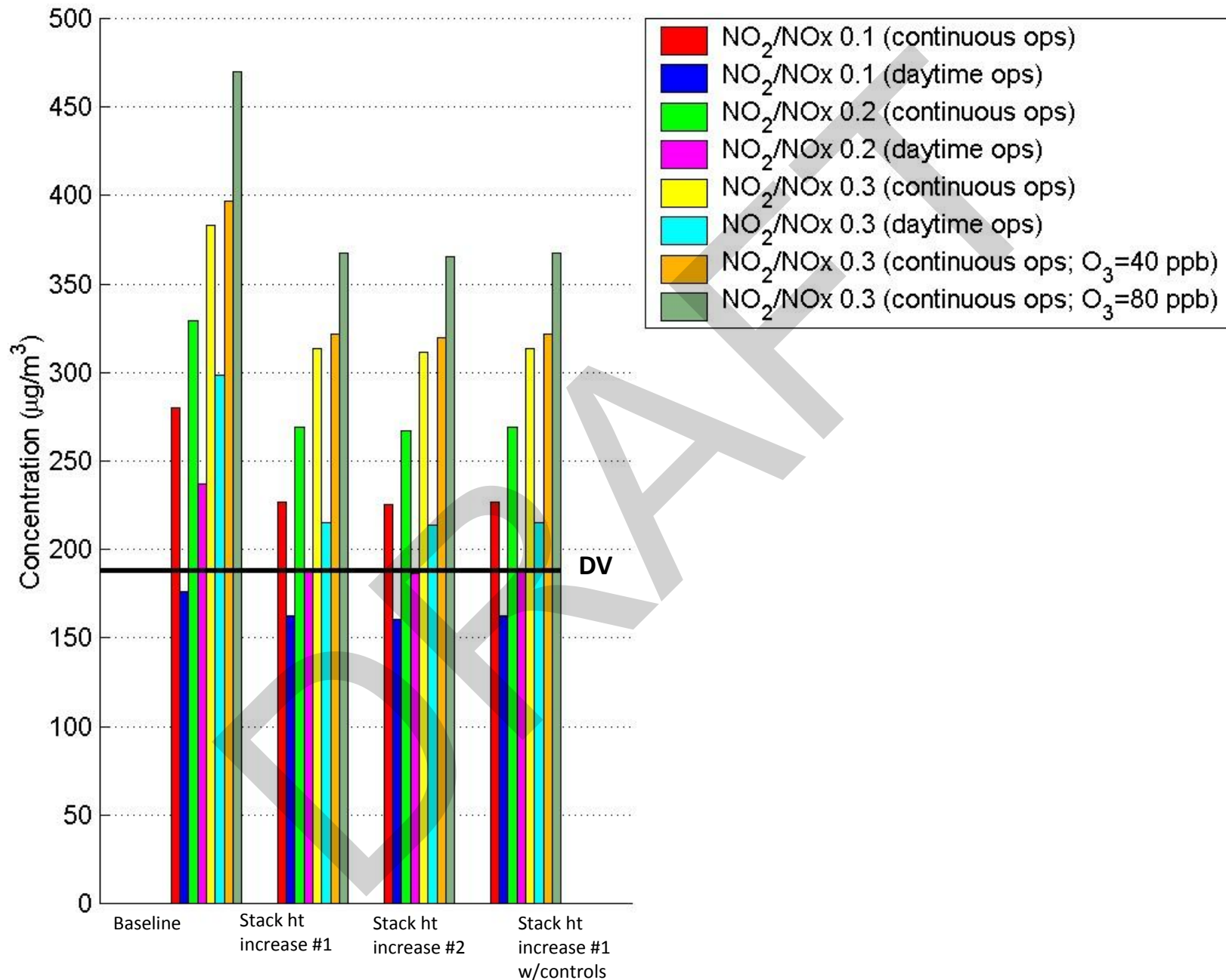
## Legend



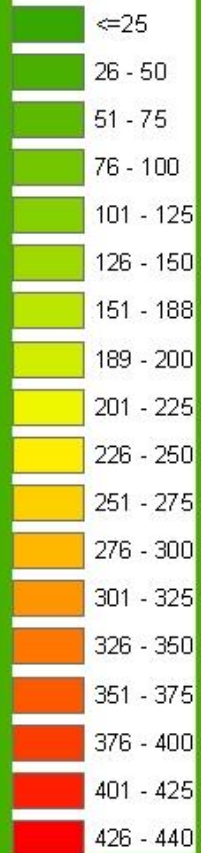
Stack ht increase #2 + increased emissions  
PVMRM (2004-2008 O<sub>3</sub>)  
0.1 NO<sub>2</sub>/NO<sub>x</sub> in-stack ratio  
Max DV: 592 μg/m<sup>3</sup>



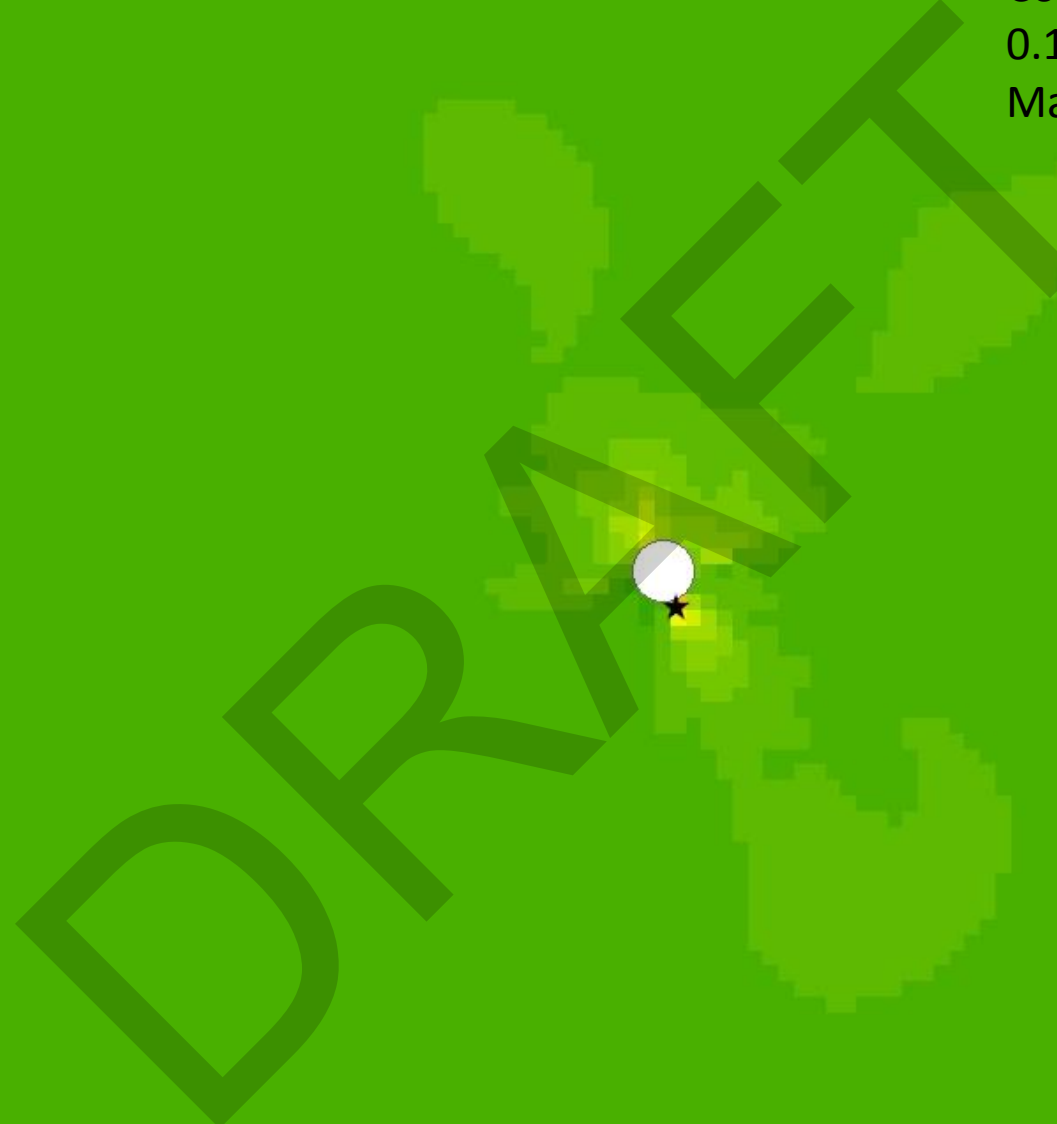
# Asphalt Plant (San Juan): NO<sub>2</sub>



**Legend**



Base  
Continuous operations  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 280 µg/m<sup>3</sup>



### Legend

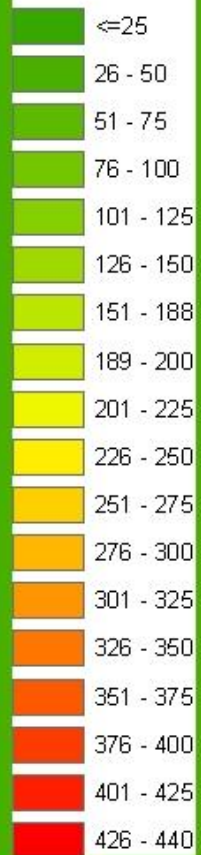


Base  
Daytime operations  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 176 μg/m<sup>3</sup>

DRAFT



### Legend



Base

Continuous operations

0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 329 μg/m<sup>3</sup>



### Legend



Base

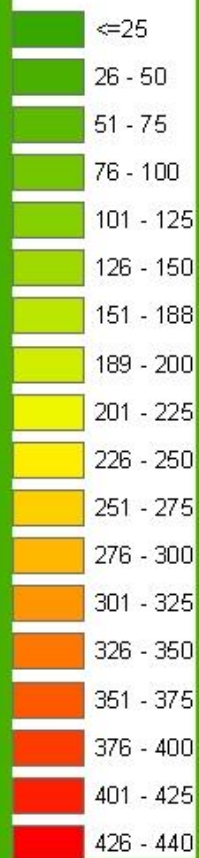
Daytime operations

0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 237 μg/m<sup>3</sup>



### Legend



Base

Continuous operations

0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio

Max DV: 383 µg/m<sup>3</sup>



### Legend



Base  
Daytime operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 299  $\mu\text{g}/\text{m}^3$





### Legend



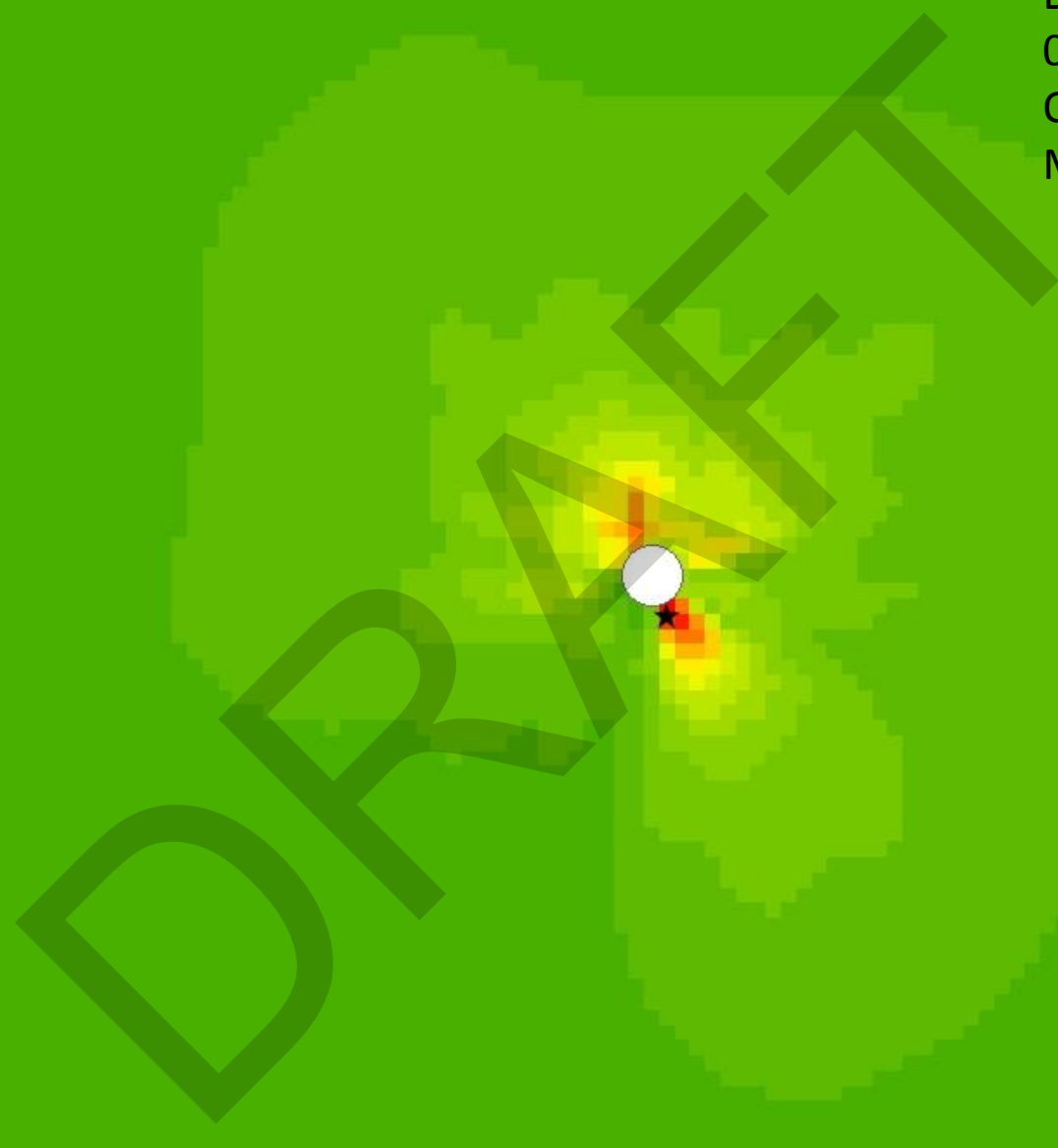
Base  
Continuous operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=40 ppb  
Max DV: 397 μg/m<sup>3</sup>



**Legend**

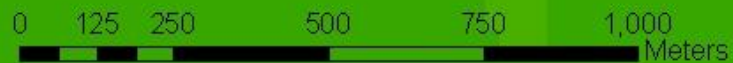
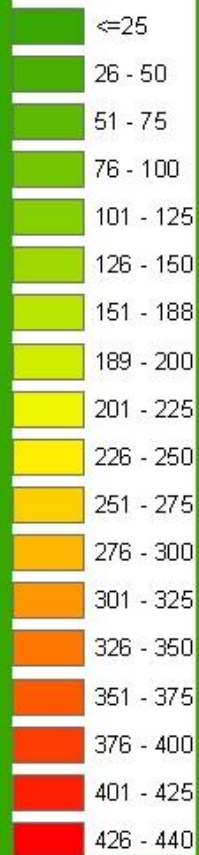


Base  
Daytime operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=80 ppb  
Max DV: 470 μg/m<sup>3</sup>

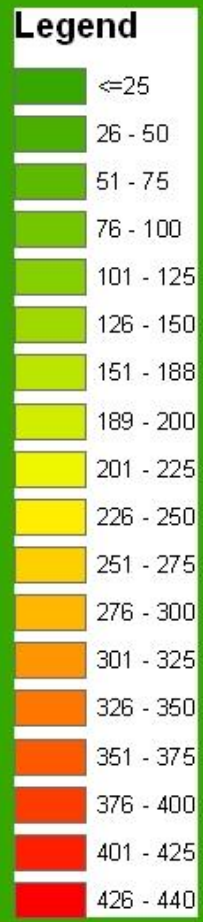


Stack ht increase #1  
Continuous operations  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 227 μg/m<sup>3</sup>

**Legend**

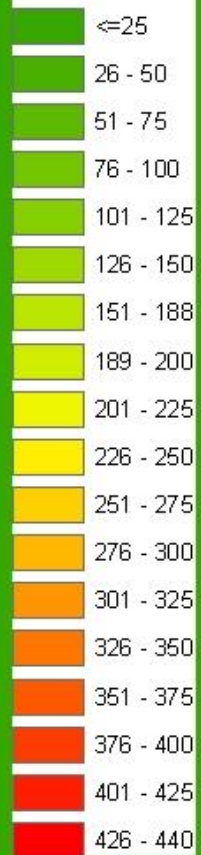


Stack ht increase #1  
Daytime operations  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 162 μg/m<sup>3</sup>

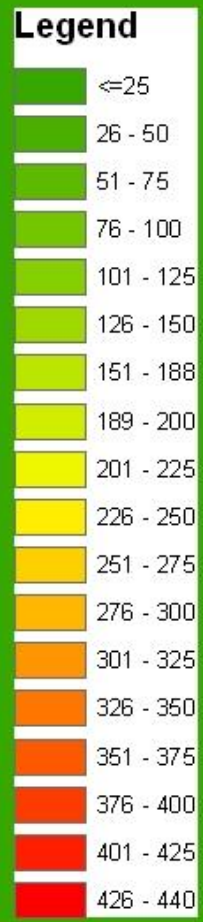


Stack ht increase #1  
Continuous operations  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 269 μg/m<sup>3</sup>

**Legend**

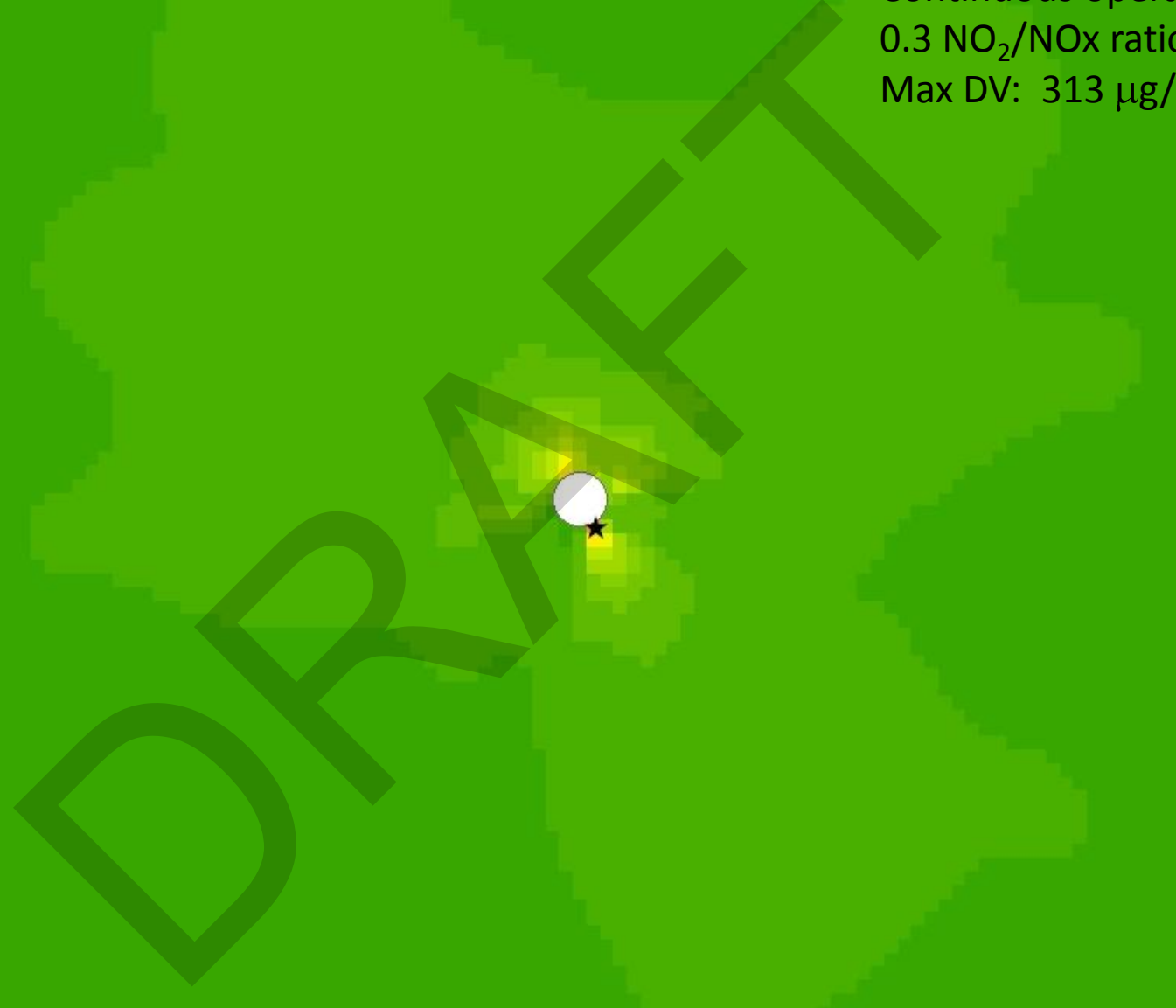
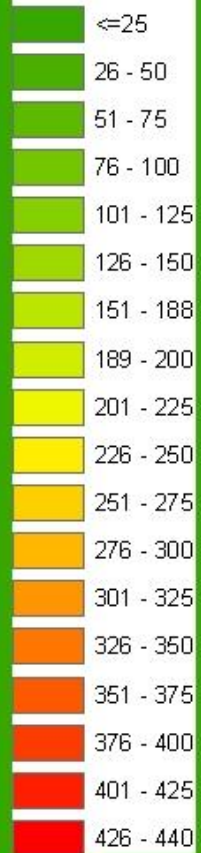


Stack ht increase #1  
Daytime operations  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 188 μg/m<sup>3</sup>



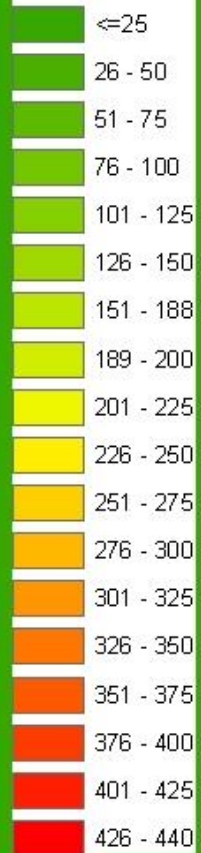
Stack ht increase #1  
Continuous operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 313 μg/m<sup>3</sup>

**Legend**



Stack ht increase #1  
Daytime operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 215 μg/m<sup>3</sup>

**Legend**





**Legend**



Stack ht increase #1  
Continuous operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=40 ppb  
Max DV: 322 μg/m<sup>3</sup>



**Legend**

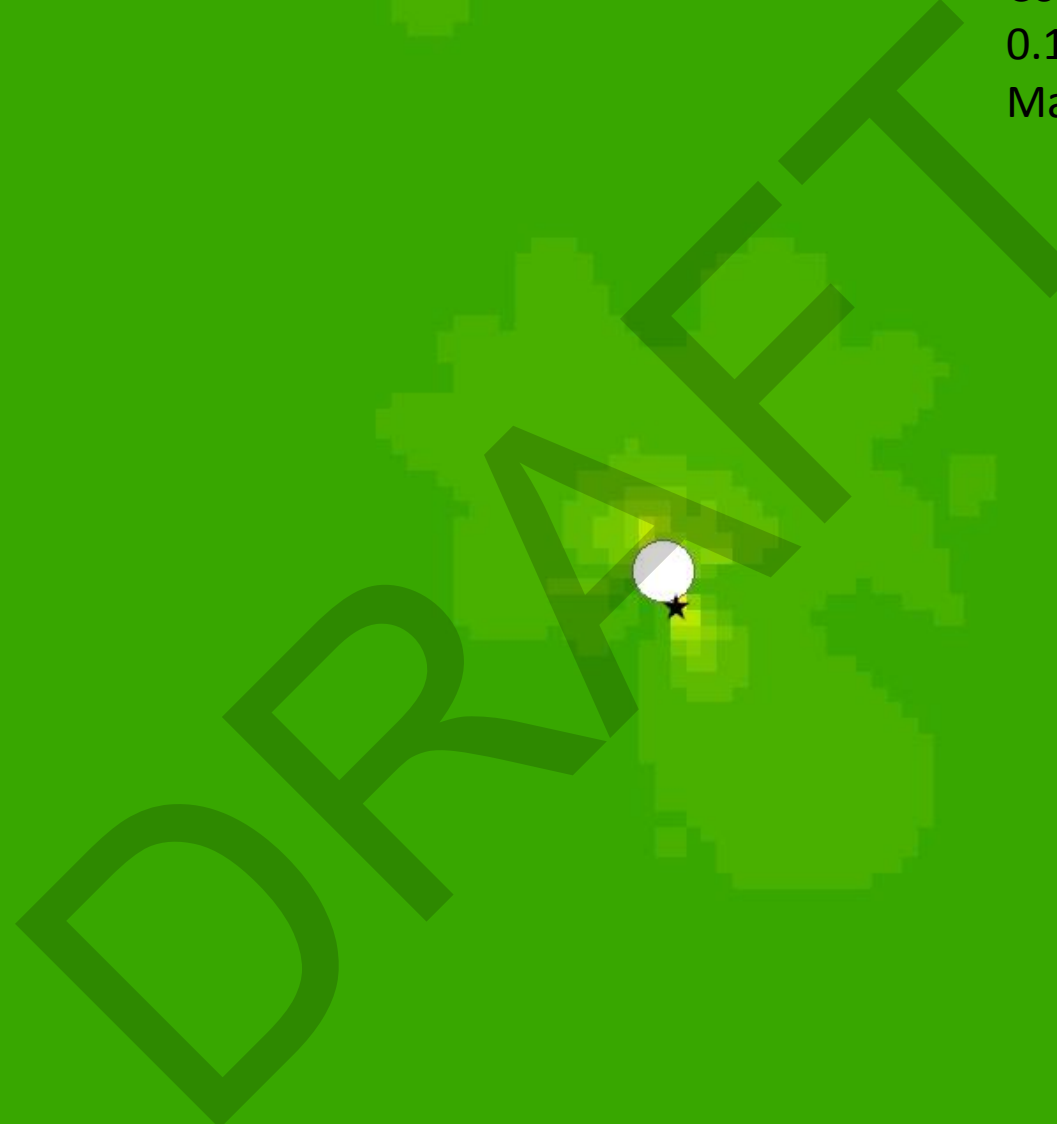
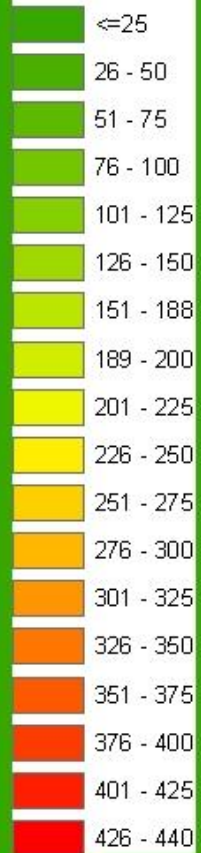


Stack ht increase #1  
Daytime operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=80 ppb  
Max DV: 368 μg/m<sup>3</sup>

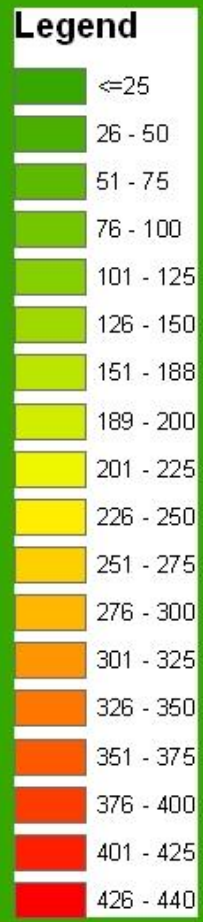


Stack ht increase #2  
Continuous operations  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 225 μg/m<sup>3</sup>

**Legend**

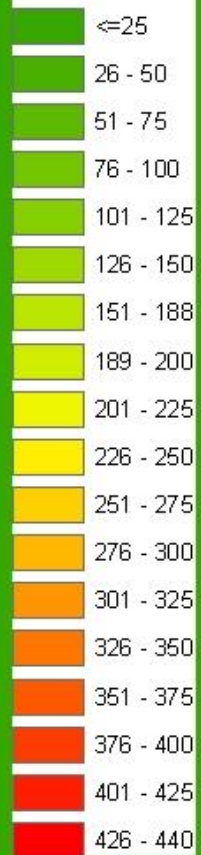


Stack ht increase #2  
Daytime operations  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 160 μg/m<sup>3</sup>



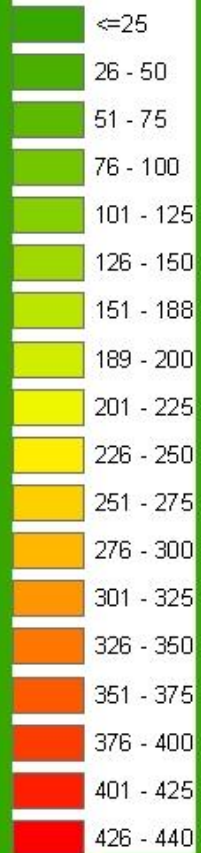
Stack ht increase #2  
Continuous operations  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 267 μg/m<sup>3</sup>

**Legend**



Stack ht increase #2  
Daytime operations  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 187 μg/m<sup>3</sup>

### Legend



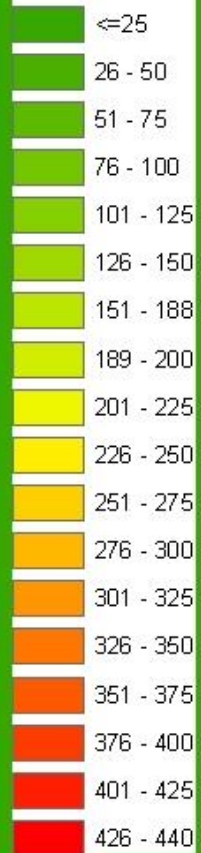
Stack ht increase #2  
Continuous operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 311 µg/m<sup>3</sup>

**Legend**



Stack ht increase #2  
Daytime operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 214 μg/m<sup>3</sup>

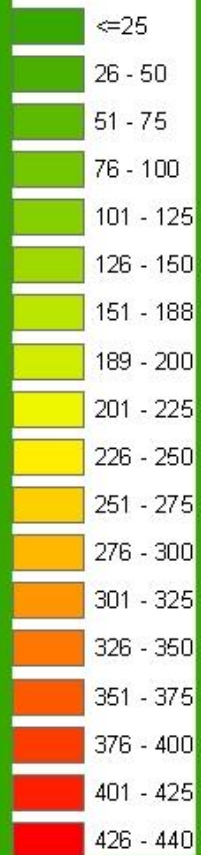
**Legend**



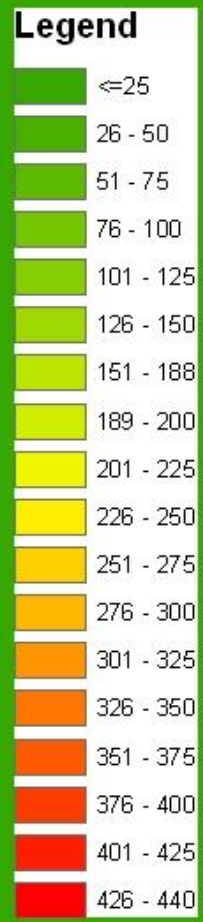


Stack ht increase #2  
Continuous operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=40 ppb  
Max DV: 320 μg/m<sup>3</sup>

### Legend



Stack ht increase #2  
Daytime operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=80 ppb  
Max DV: 365 μg/m<sup>3</sup>



Stack ht increase #1 + controls  
Continuous operations  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 227 μg/m<sup>3</sup>



Stack ht increase #1 + controls  
Daytime operations  
0.1 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 162 μg/m<sup>3</sup>

**Legend**

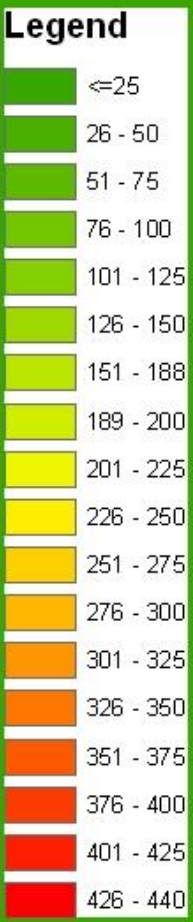


Stack ht increase #1 + controls  
Continuous operations  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 269 μg/m<sup>3</sup>

**Legend**



Stack ht increase #1 + controls  
Daytime operations  
0.2 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 188 μg/m<sup>3</sup>



Stack ht increase #1 + controls  
Continuous operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 313 μg/m<sup>3</sup>

**Legend**



Stack ht increase #1 + controls  
Daytime operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
Max DV: 215 μg/m<sup>3</sup>

**Legend**





Stack ht increase #1 + controls  
Continuous operations  
0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio  
O<sub>3</sub>=40 ppb  
Max DV: 322 μg/m<sup>3</sup>

**Legend**



Stack ht increase #1 + controls

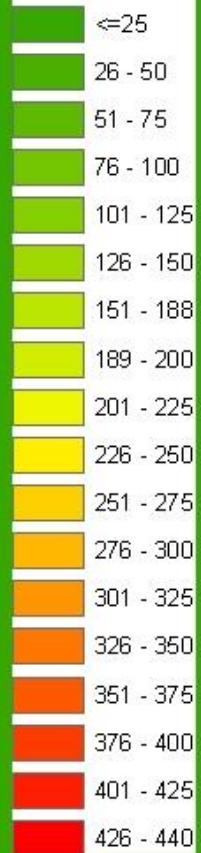
Daytime operations

0.3 NO<sub>2</sub>/NO<sub>x</sub> ratio

O<sub>3</sub>=80 ppb

Max DV: 368 μg/m<sup>3</sup>

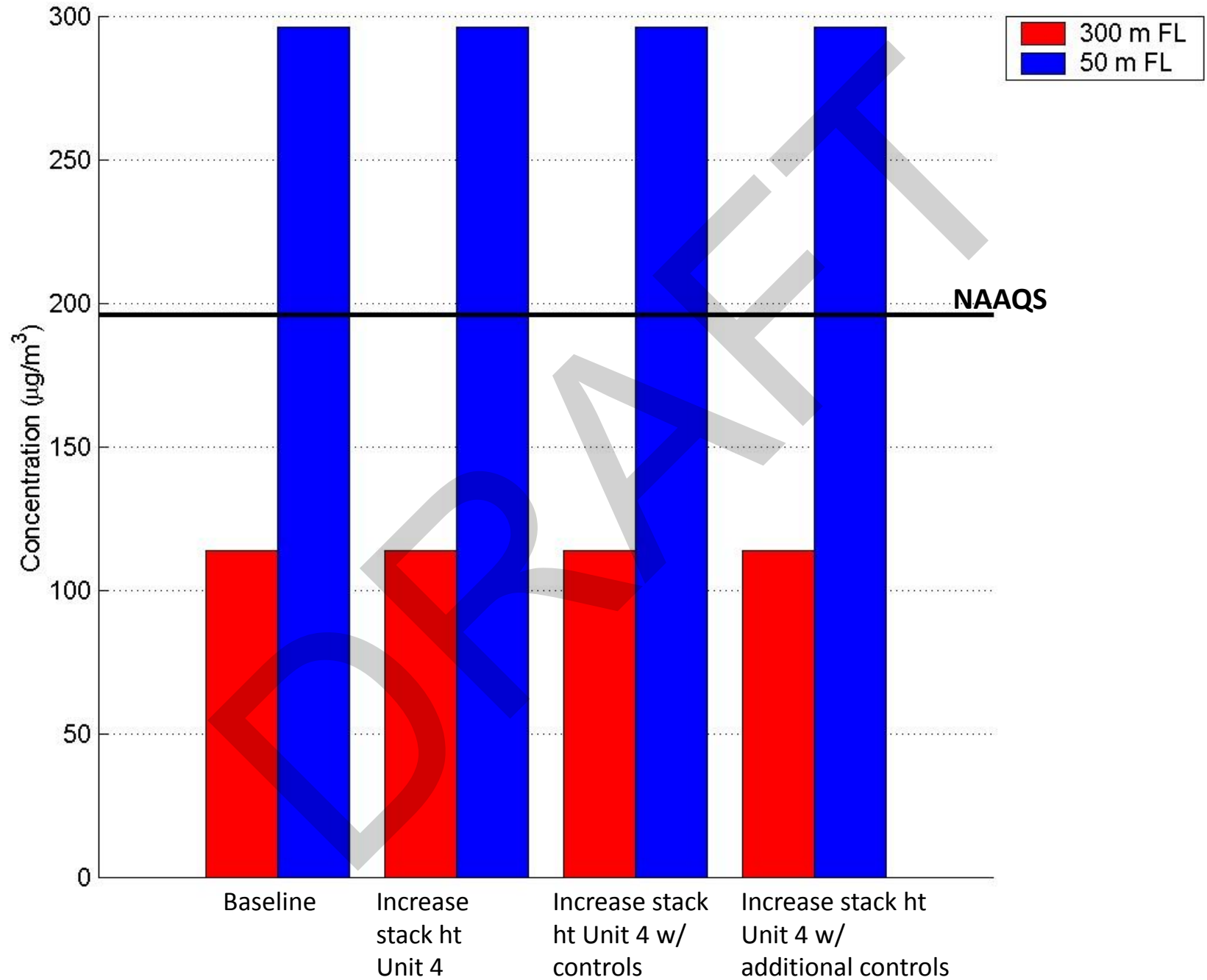
**Legend**



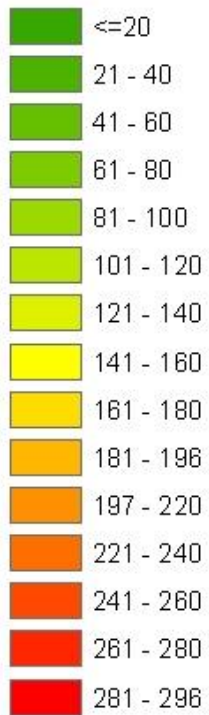
SO<sub>2</sub> results

DRAFT

# Ethanol Plant (Moline): SO<sub>2</sub>



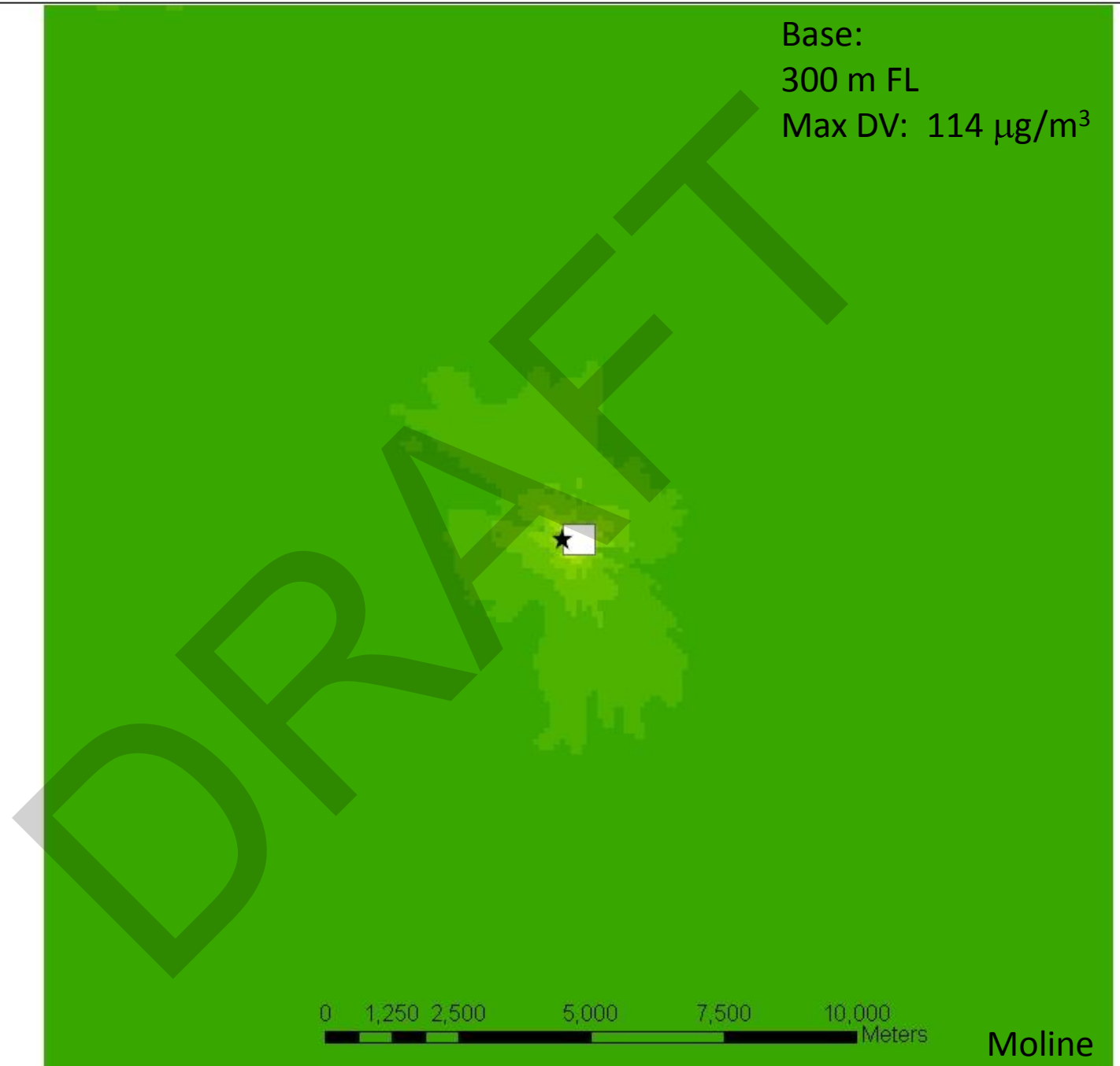
### Legend



Base:

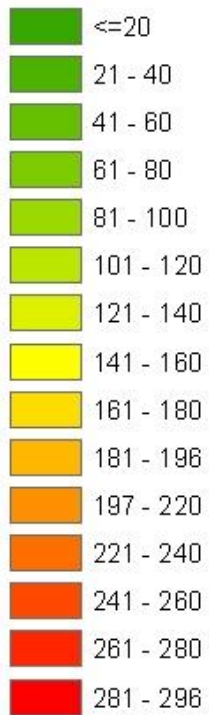
300 m FL

Max DV: 114  $\mu\text{g}/\text{m}^3$



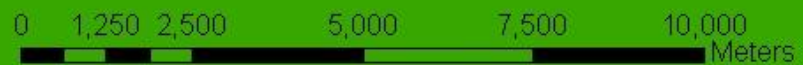
Moline

**Legend**



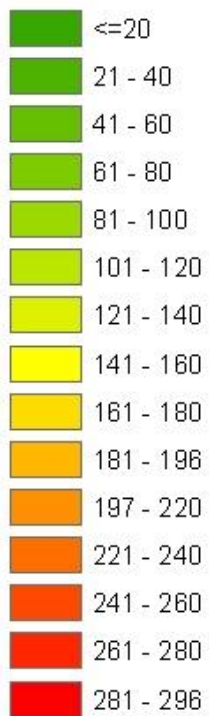
Base  
50 m FL  
Max DV: 296  $\mu\text{g}/\text{m}^3$

DRAFT



Moline

### Legend

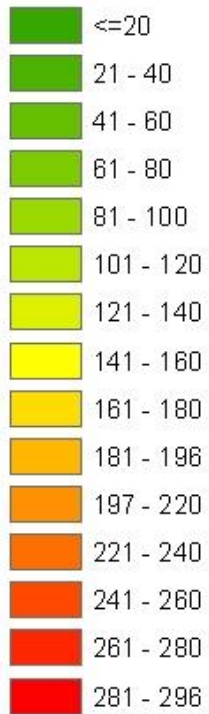


Increase stack ht C0004  
300 m FL  
Max DV: 114  $\mu\text{g}/\text{m}^3$

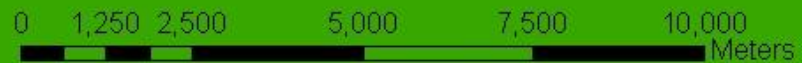


Moline

**Legend**



Increase stack ht C0004  
50 m FL  
Max DV: 296 µg/m<sup>3</sup>

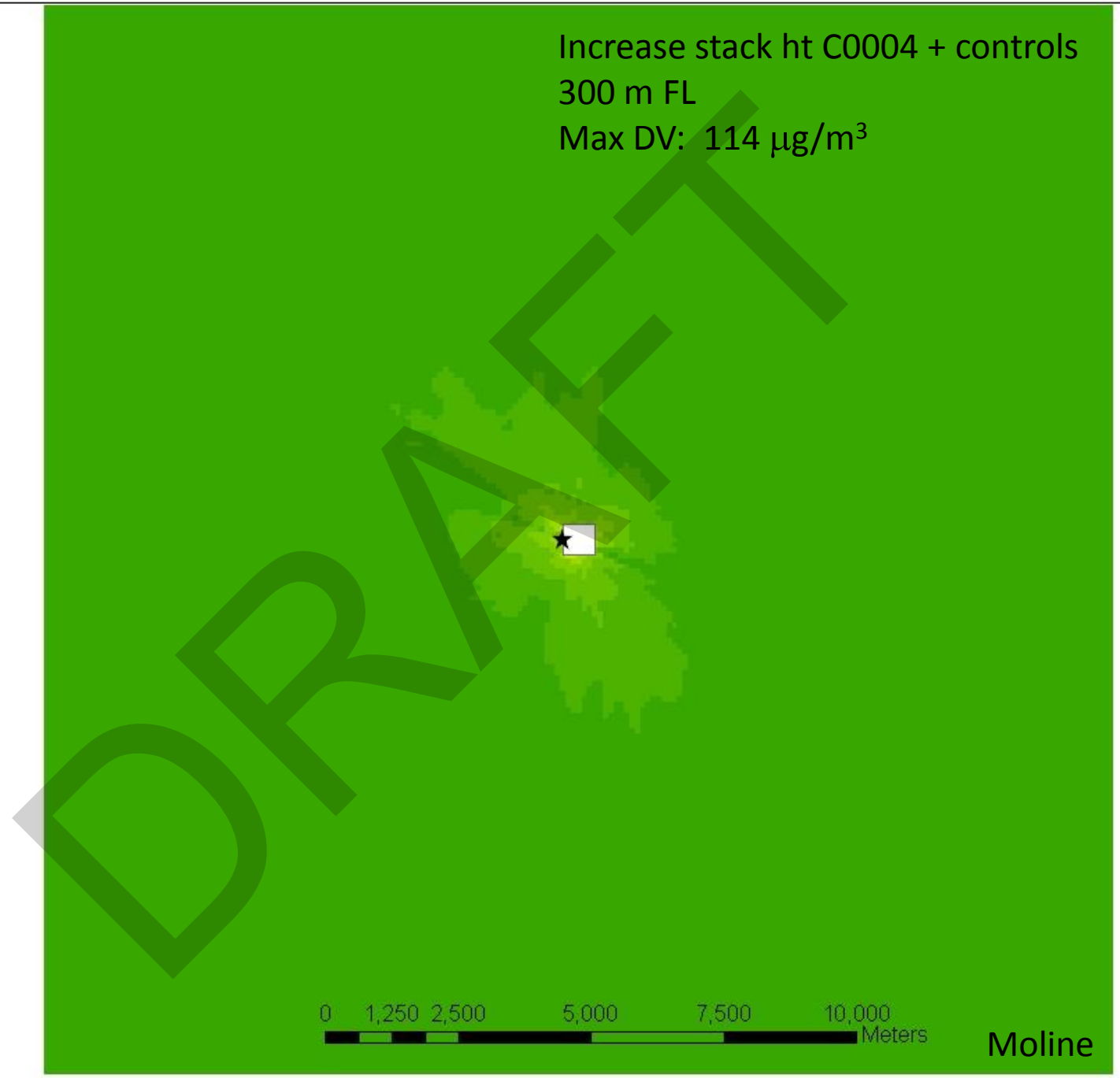
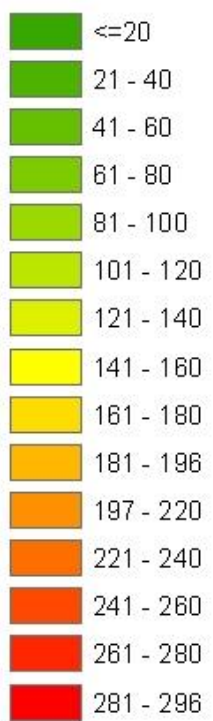


Moline



Increase stack ht C0004 + controls  
300 m FL  
Max DV: 114  $\mu\text{g}/\text{m}^3$

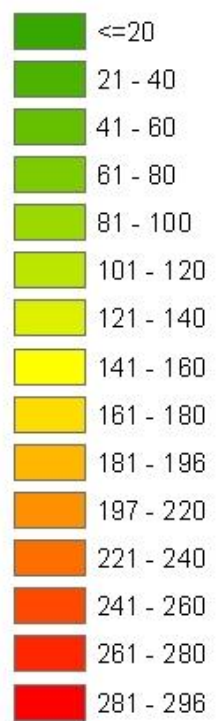
**Legend**



Moline

Increase stack ht C0004 + controls  
50 m FL  
Max DV: 296  $\mu\text{g}/\text{m}^3$

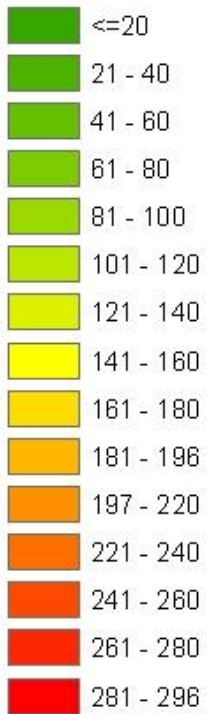
**Legend**



Moline

Increase stack ht C0004 + additional controls  
300 m FL  
Max DV: 114  $\mu\text{g}/\text{m}^3$

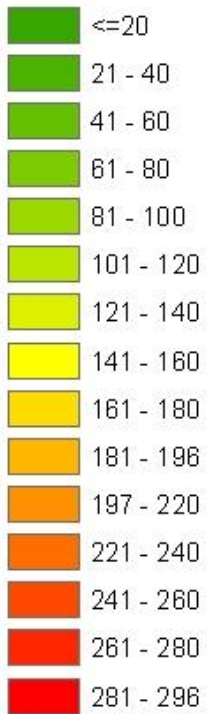
**Legend**



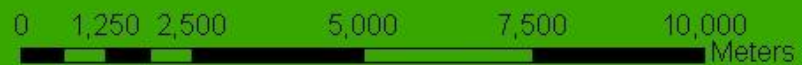
Moline

Increase stack ht C0004 + additional controls  
50 m FL  
Max DV: 296  $\mu\text{g}/\text{m}^3$

**Legend**

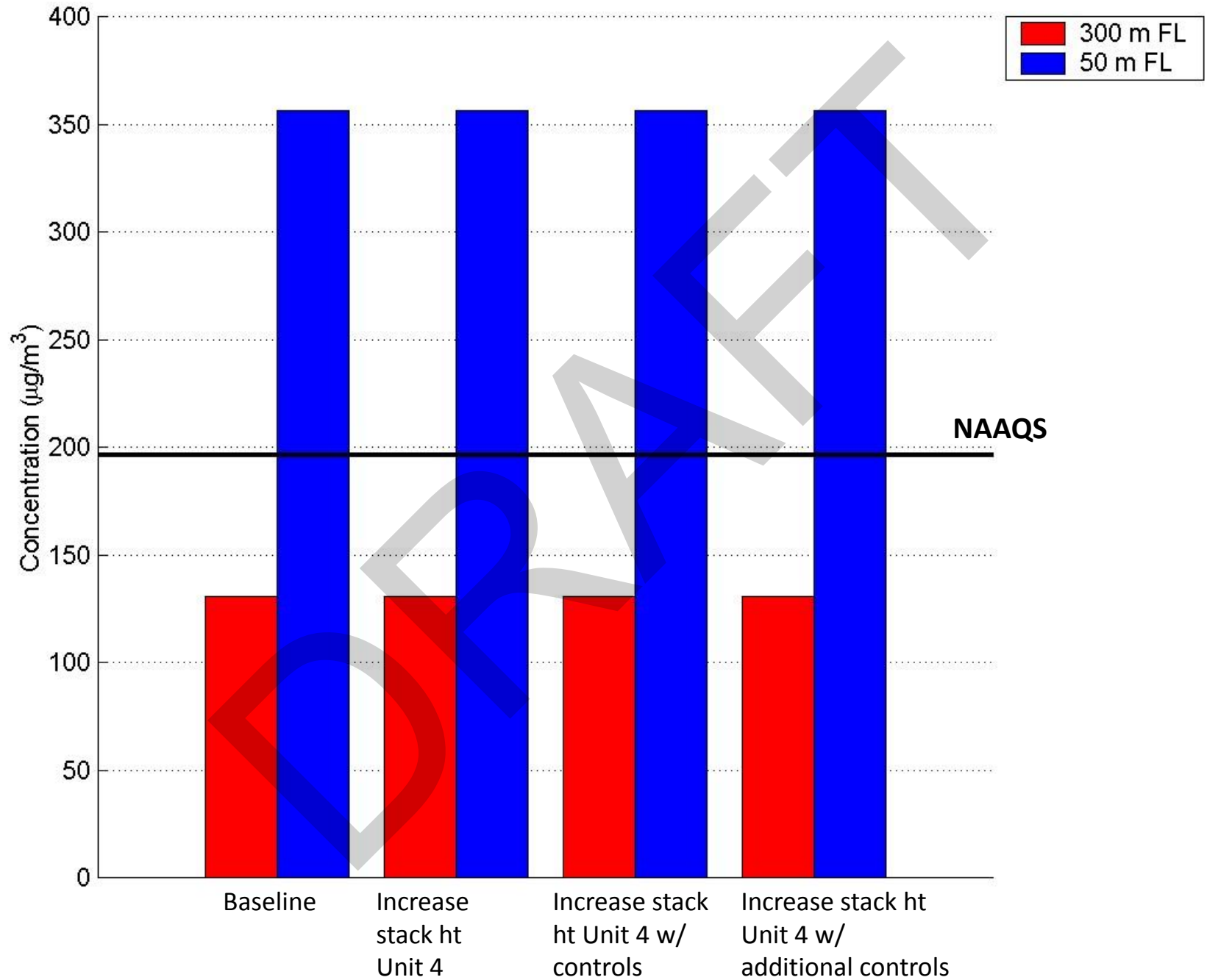


DRAFT



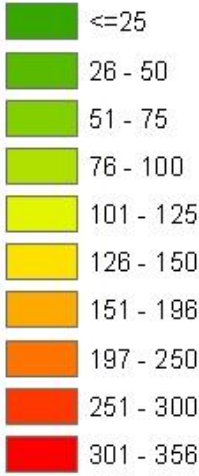
Moline

# Ethanol Plant (Springfield): SO<sub>2</sub>



Base:  
300 m FL  
Max DV: 131  $\mu\text{g}/\text{m}^3$

**Legend**



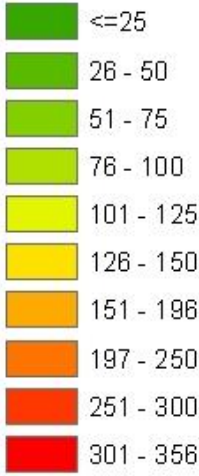
DRAFT



Springfield

Base  
50 m FL  
Max DV: 356  $\mu\text{g}/\text{m}^3$

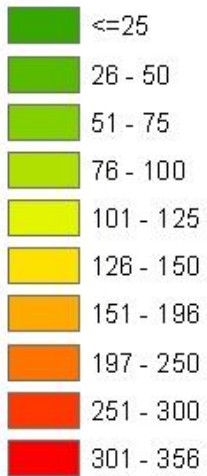
**Legend**



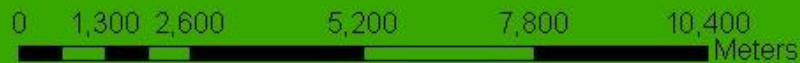
Springfield

Increase stack ht C0004  
300 m FL  
Max DV: 131  $\mu\text{g}/\text{m}^3$

### Legend



DRAFT

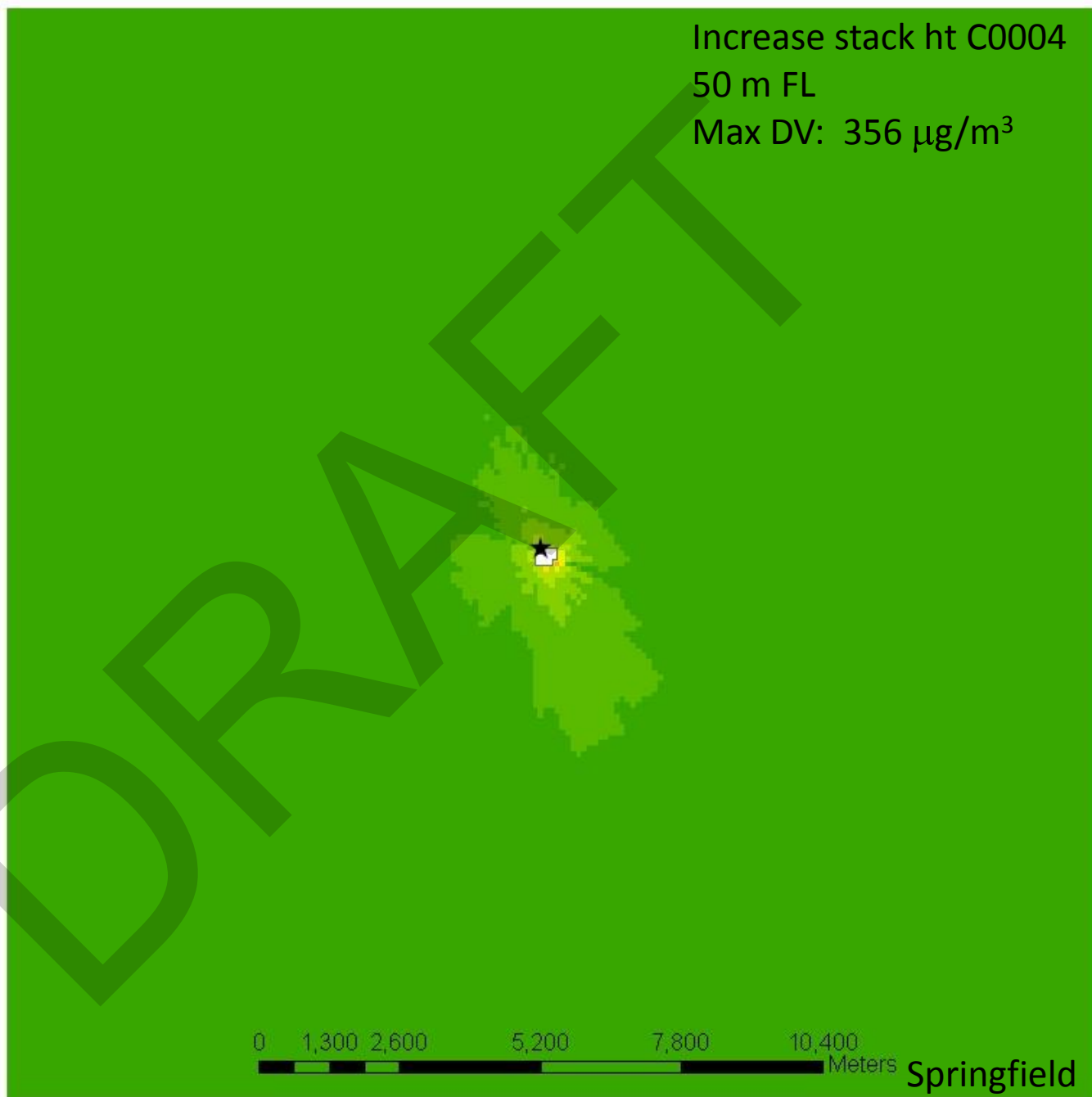
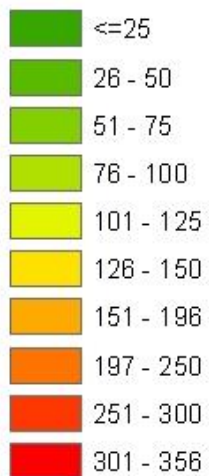


Springfield



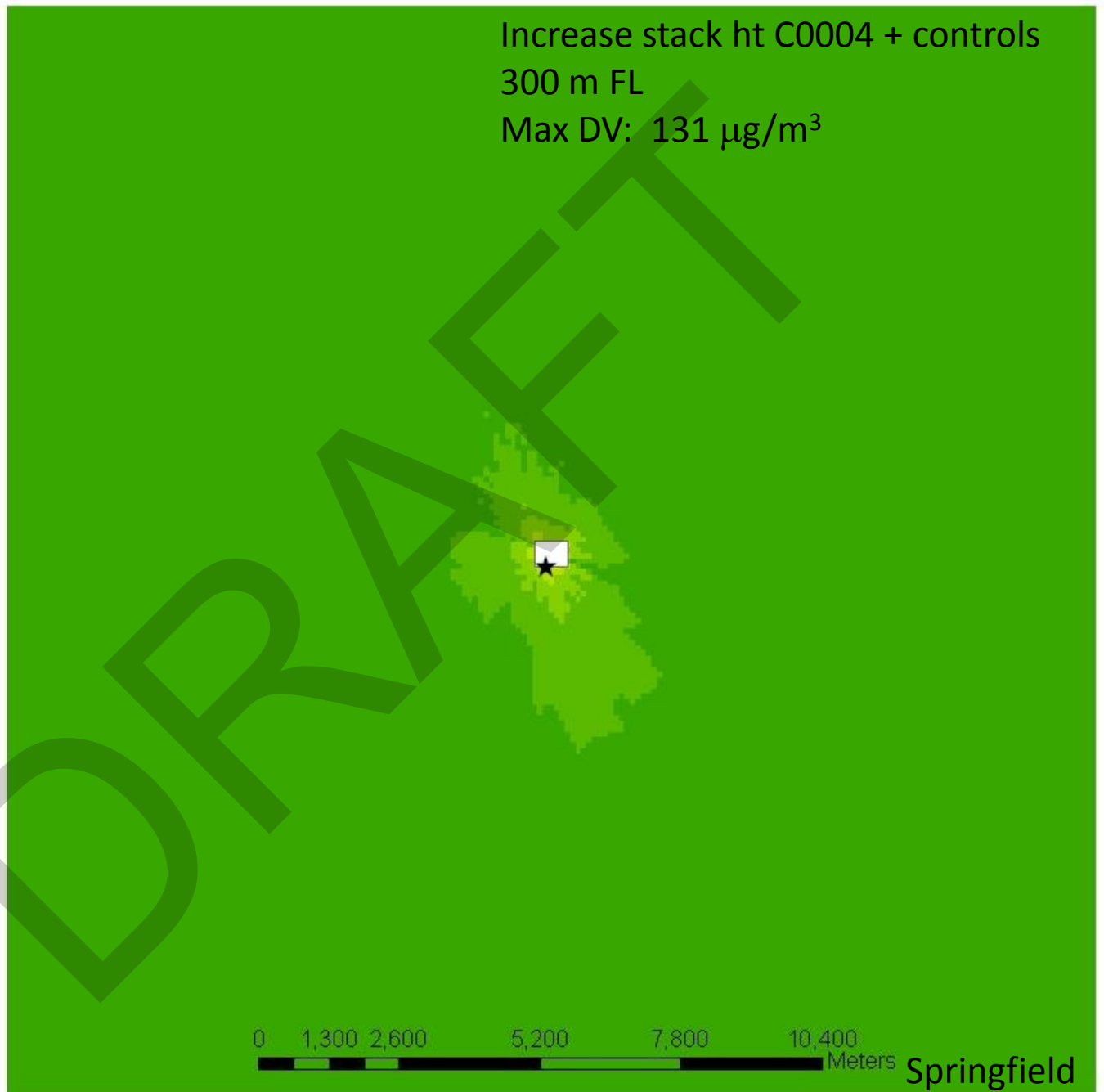
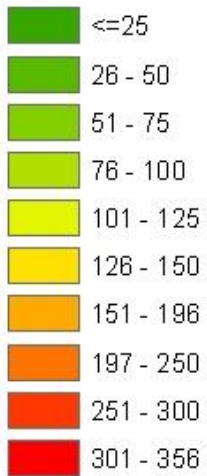
Increase stack ht C0004  
50 m FL  
Max DV: 356  $\mu\text{g}/\text{m}^3$

### Legend



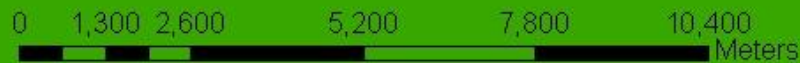
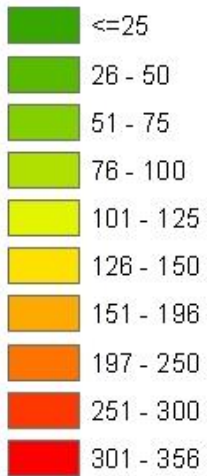
Increase stack ht C0004 + controls  
300 m FL  
Max DV: 131  $\mu\text{g}/\text{m}^3$

### Legend



Increase stack ht C0004 + controls  
50 m FL  
Max DV: 356  $\mu\text{g}/\text{m}^3$

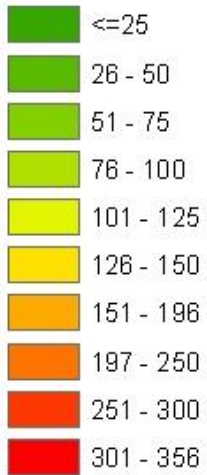
### Legend



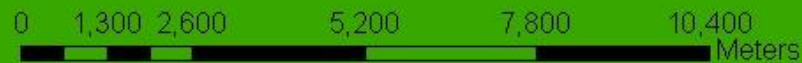
Springfield

Increase stack ht C0004 + additional controls  
300 m FL  
Max DV: 131  $\mu\text{g}/\text{m}^3$

**Legend**



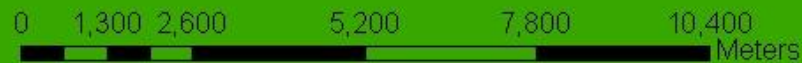
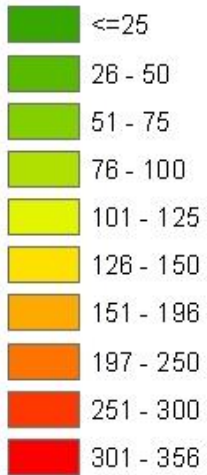
DRAFT



Springfield

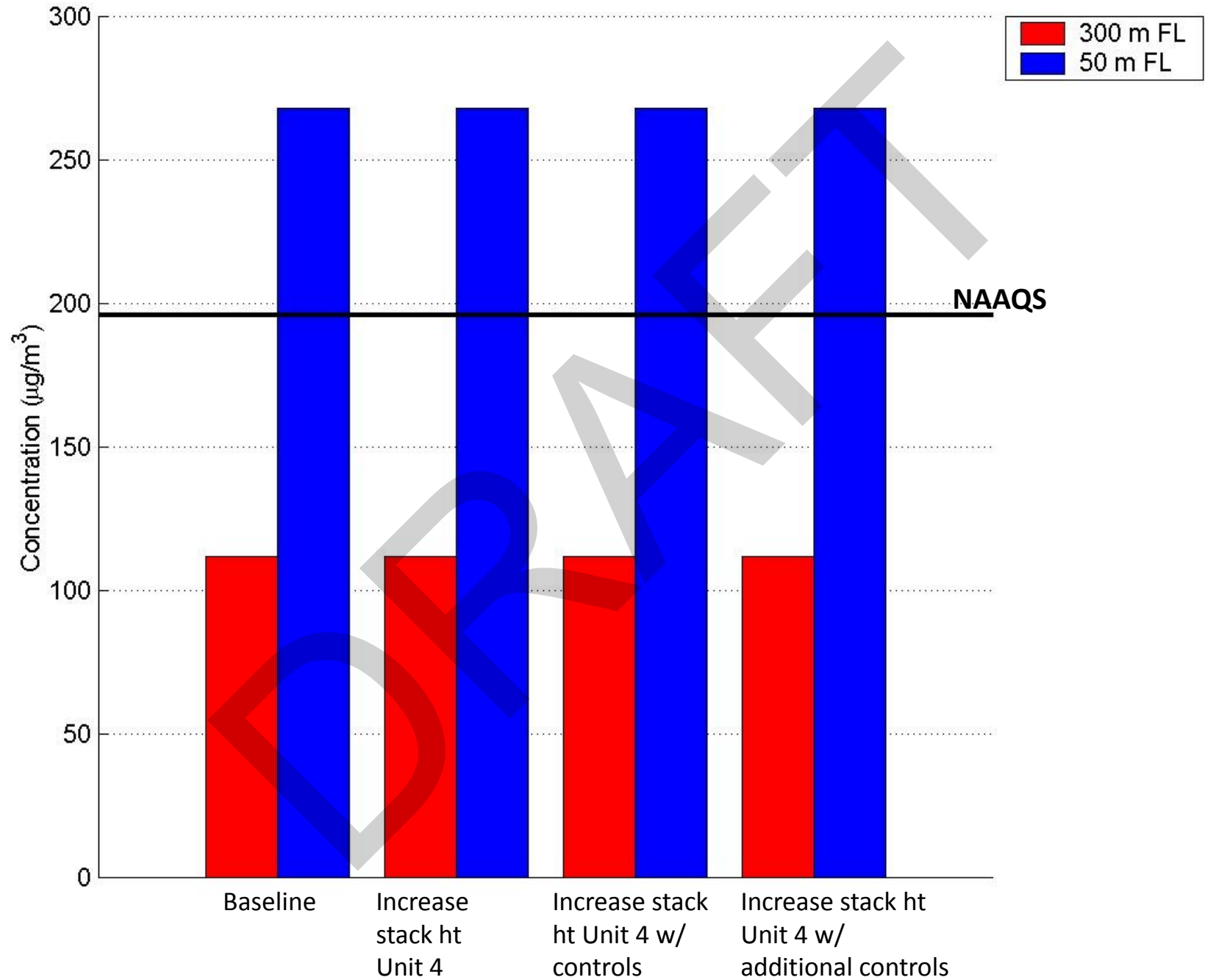
Increase stack ht C0004 + additional controls  
50 m FL  
Max DV: 356  $\mu\text{g}/\text{m}^3$

### Legend



Springfield

# Ethanol Plant (St. Louis): SO<sub>2</sub>



Base:  
300 m FL  
Max DV: 112  $\mu\text{g}/\text{m}^3$

**Legend**



St. Louis

Base  
50 m FL  
Max DV: 268  $\mu\text{g}/\text{m}^3$

**Legend**

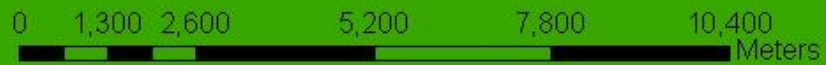
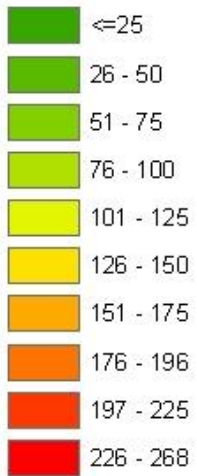


St. Louis



Increase stack ht C0004  
300 m FL  
Max DV: 112  $\mu\text{g}/\text{m}^3$

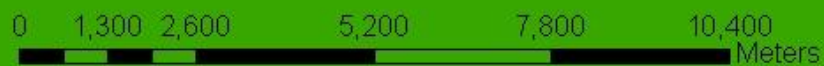
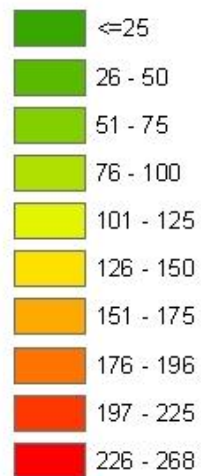
### Legend



St. Louis

Increase stack ht C0004  
50 m FL  
Max DV: 268  $\mu\text{g}/\text{m}^3$

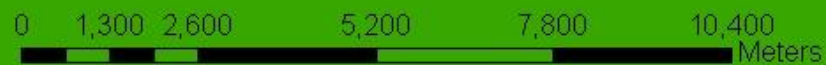
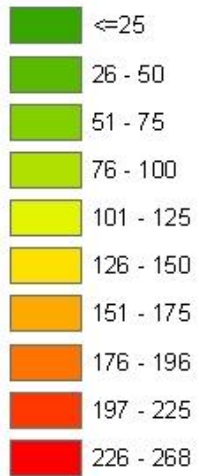
### Legend



St. Louis

Increase stack ht C0004 + controls  
300 m FL  
Max DV: 112  $\mu\text{g}/\text{m}^3$

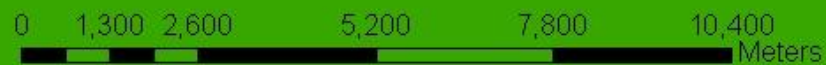
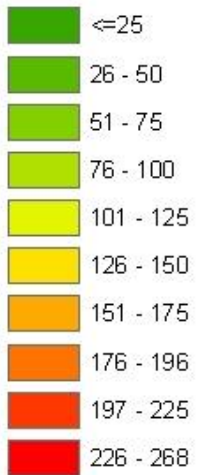
### Legend



St. Louis

Increase stack ht C0004 + controls  
50 m FL  
Max DV: 268  $\mu\text{g}/\text{m}^3$

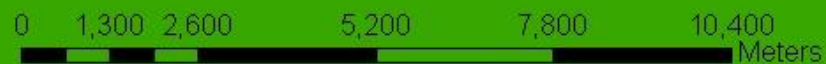
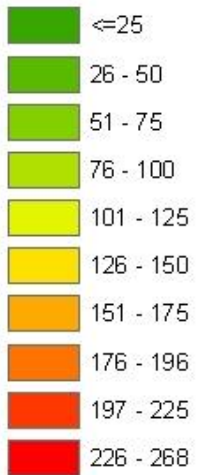
### Legend



St. Louis

Increase stack ht C0004 + additional controls  
300 m FL  
Max DV: 112  $\mu\text{g}/\text{m}^3$

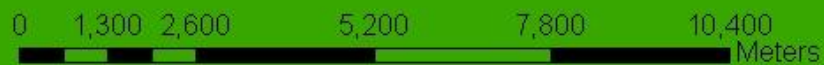
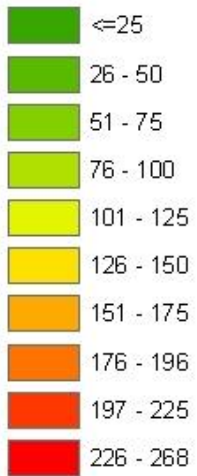
### Legend



St. Louis

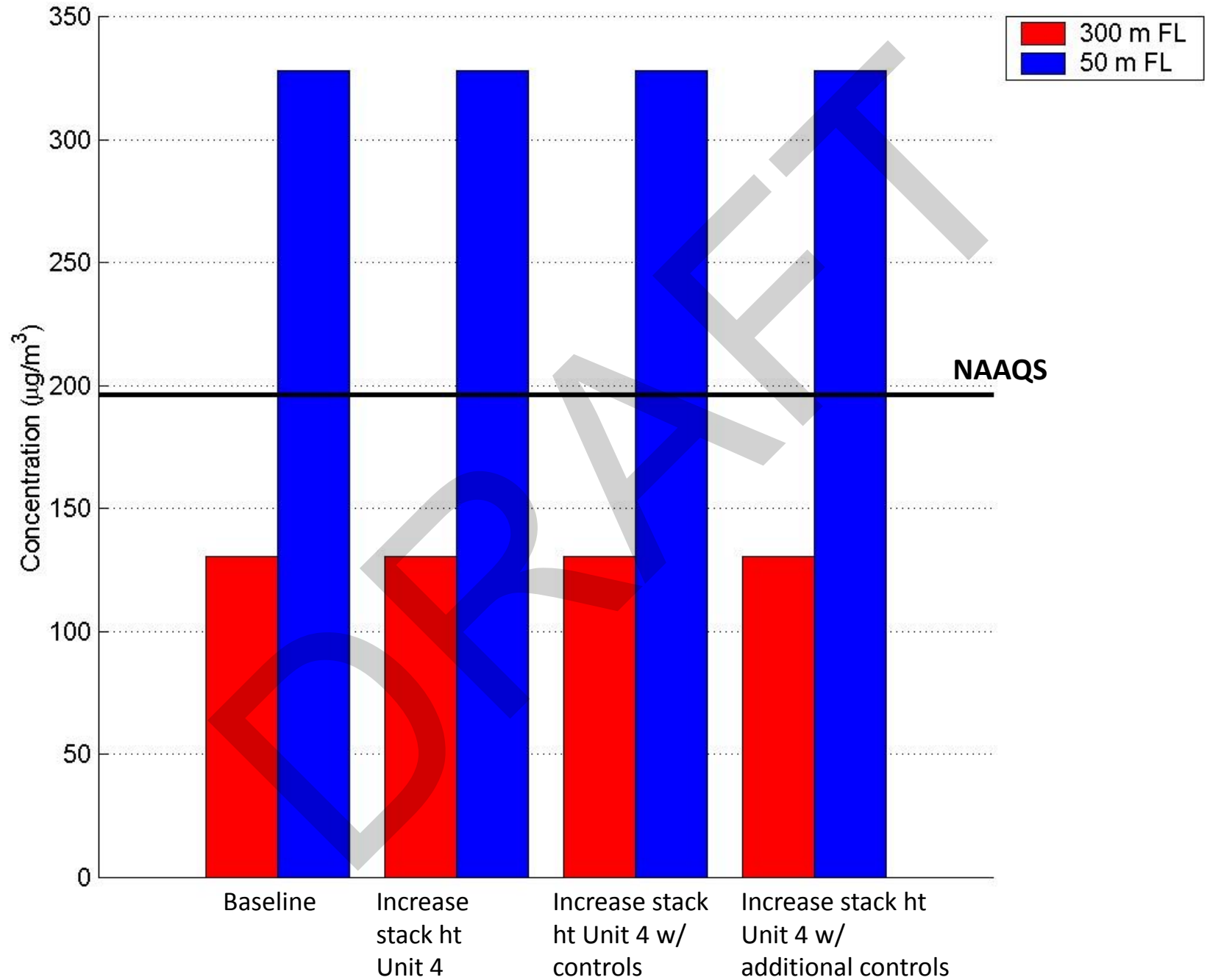
Increase stack ht C0004 + additional controls  
50 m FL  
Max DV: 268  $\mu\text{g}/\text{m}^3$

### Legend



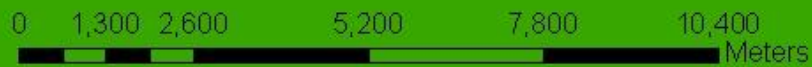
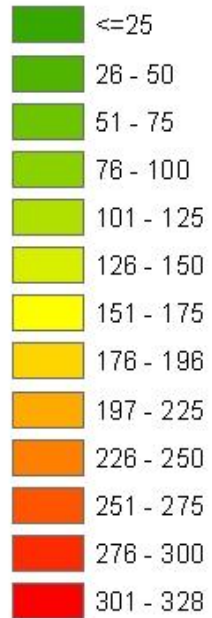
St. Louis

# Ethanol Plant (Waterloo): SO<sub>2</sub>



Base:  
300 m FL  
Max DV: 130  $\mu\text{g}/\text{m}^3$

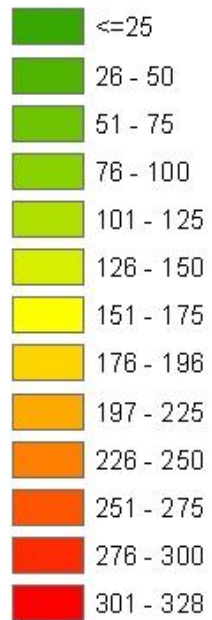
### Legend



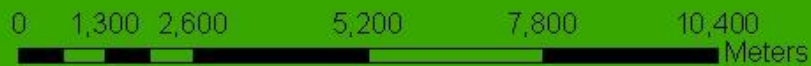
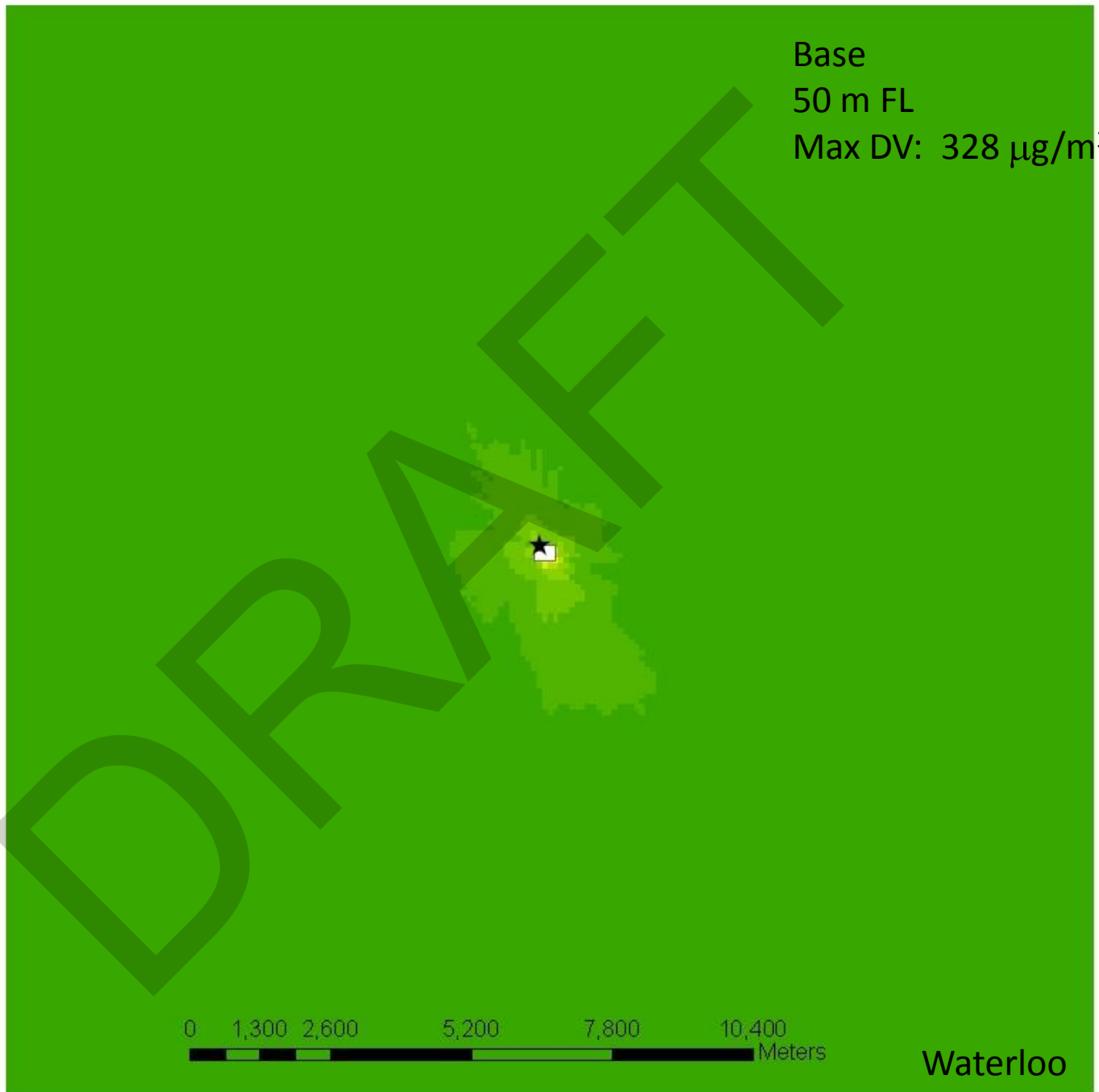
Waterloo



### Legend



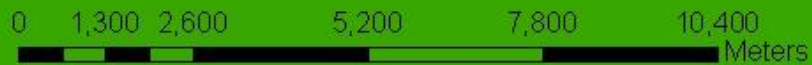
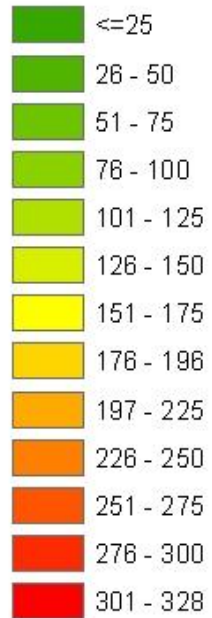
Base  
50 m FL  
Max DV: 328  $\mu\text{g}/\text{m}^3$



Waterloo

Increase stack ht C0004  
300 m FL  
Max DV: 130  $\mu\text{g}/\text{m}^3$

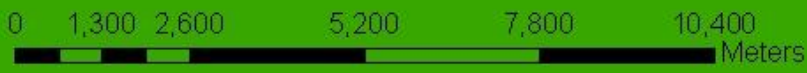
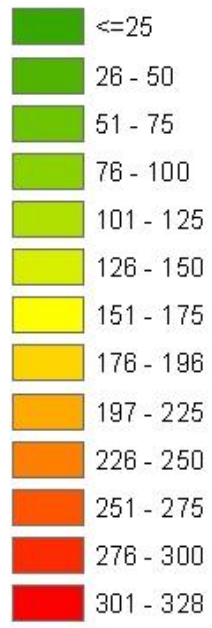
**Legend**



Waterloo

Increase stack ht C0004  
50 m FL  
Max DV: 328  $\mu\text{g}/\text{m}^3$

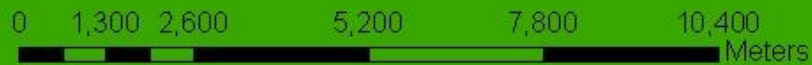
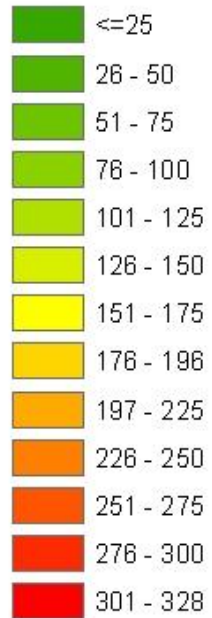
**Legend**



Waterloo

Increase stack ht C0004 + controls  
300 m FL  
Max DV: 130  $\mu\text{g}/\text{m}^3$

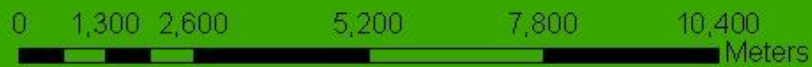
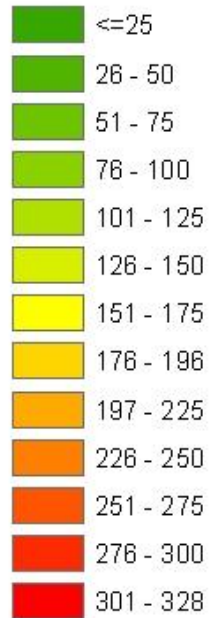
**Legend**



Waterloo

Increase stack ht C0004 + controls  
50 m FL  
Max DV: 328  $\mu\text{g}/\text{m}^3$

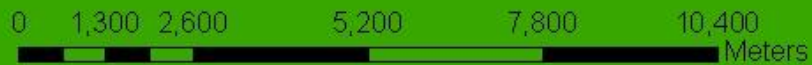
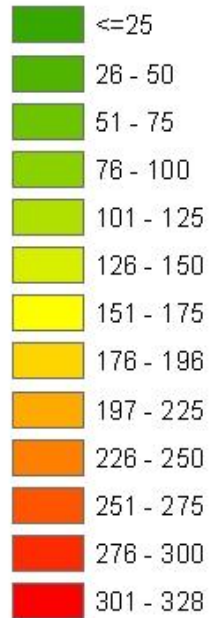
**Legend**



Waterloo

Increase stack ht C0004 + additional controls  
300 m FL  
Max DV: 130  $\mu\text{g}/\text{m}^3$

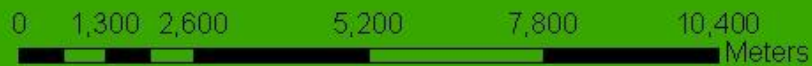
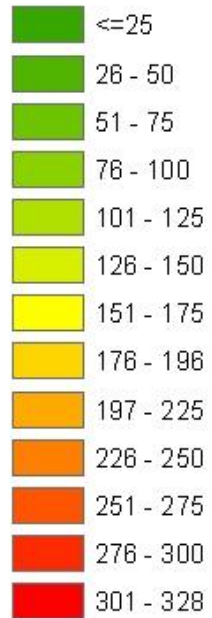
**Legend**



Waterloo

Increase stack ht C0004 + additional controls  
50 m FL  
Max DV: 328  $\mu\text{g}/\text{m}^3$

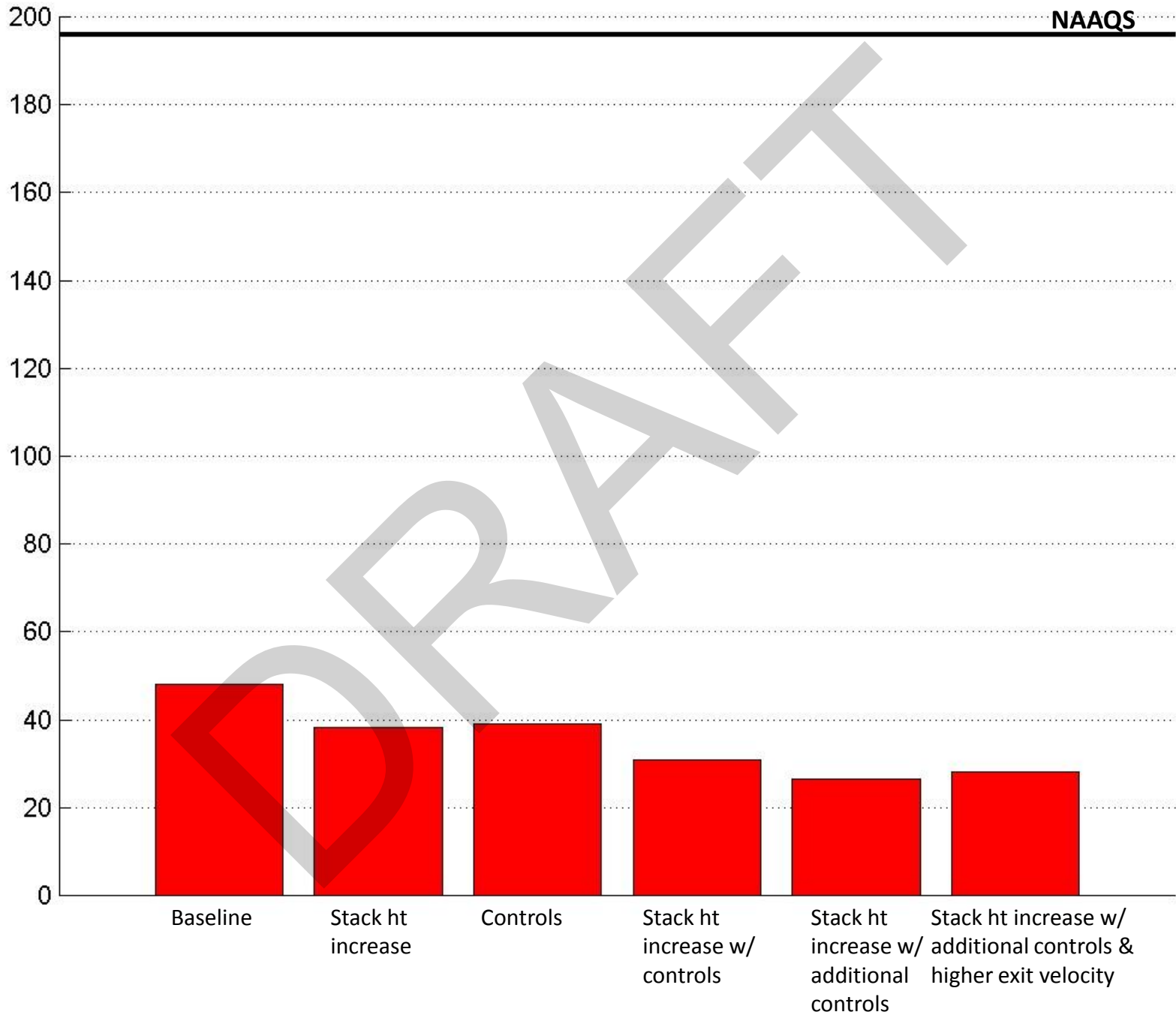
**Legend**



Waterloo

# Coal EGU (Springfield): SO<sub>2</sub>

NAAQS



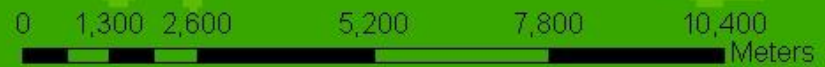
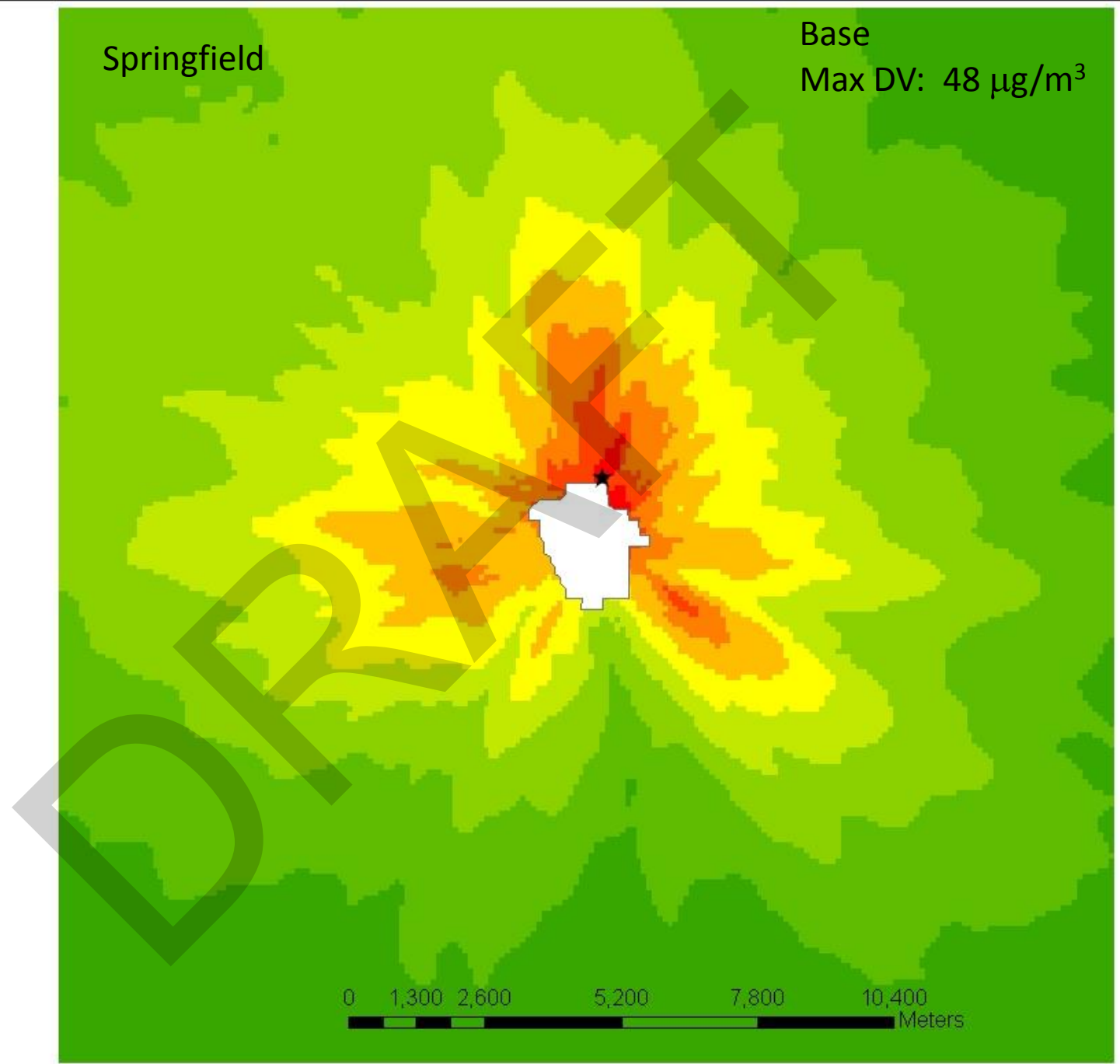
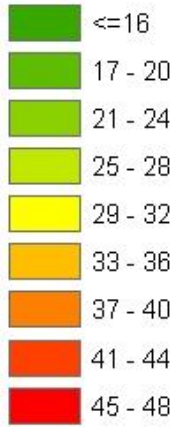


Springfield

Base

Max DV: 48  $\mu\text{g}/\text{m}^3$

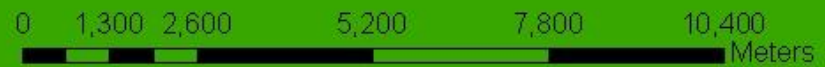
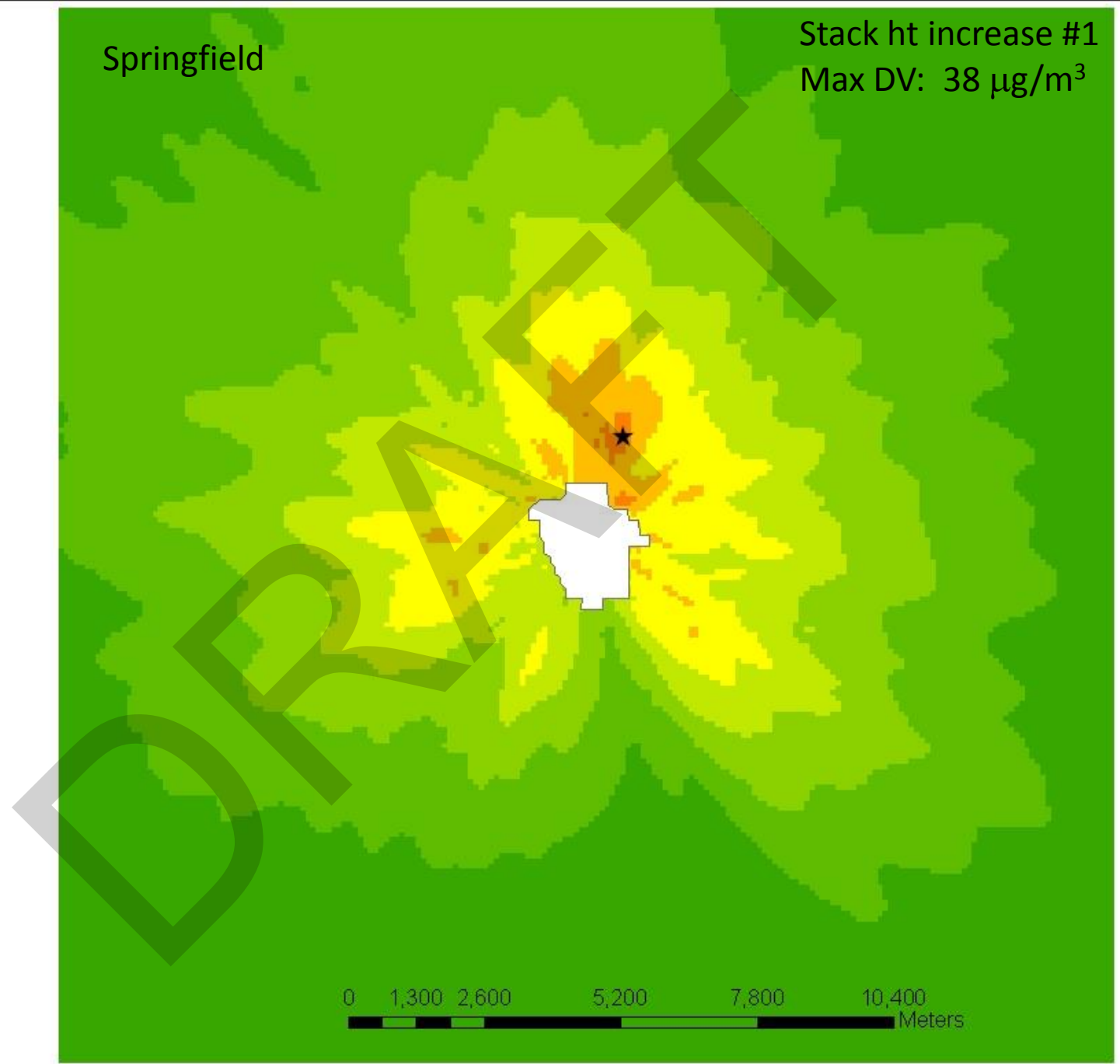
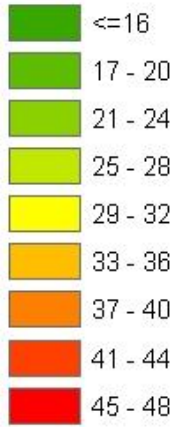
**Legend**



Springfield

Stack ht increase #1  
Max DV: 38  $\mu\text{g}/\text{m}^3$

**Legend**

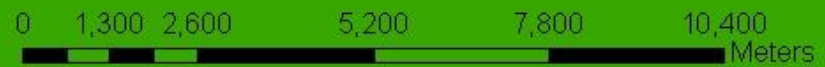
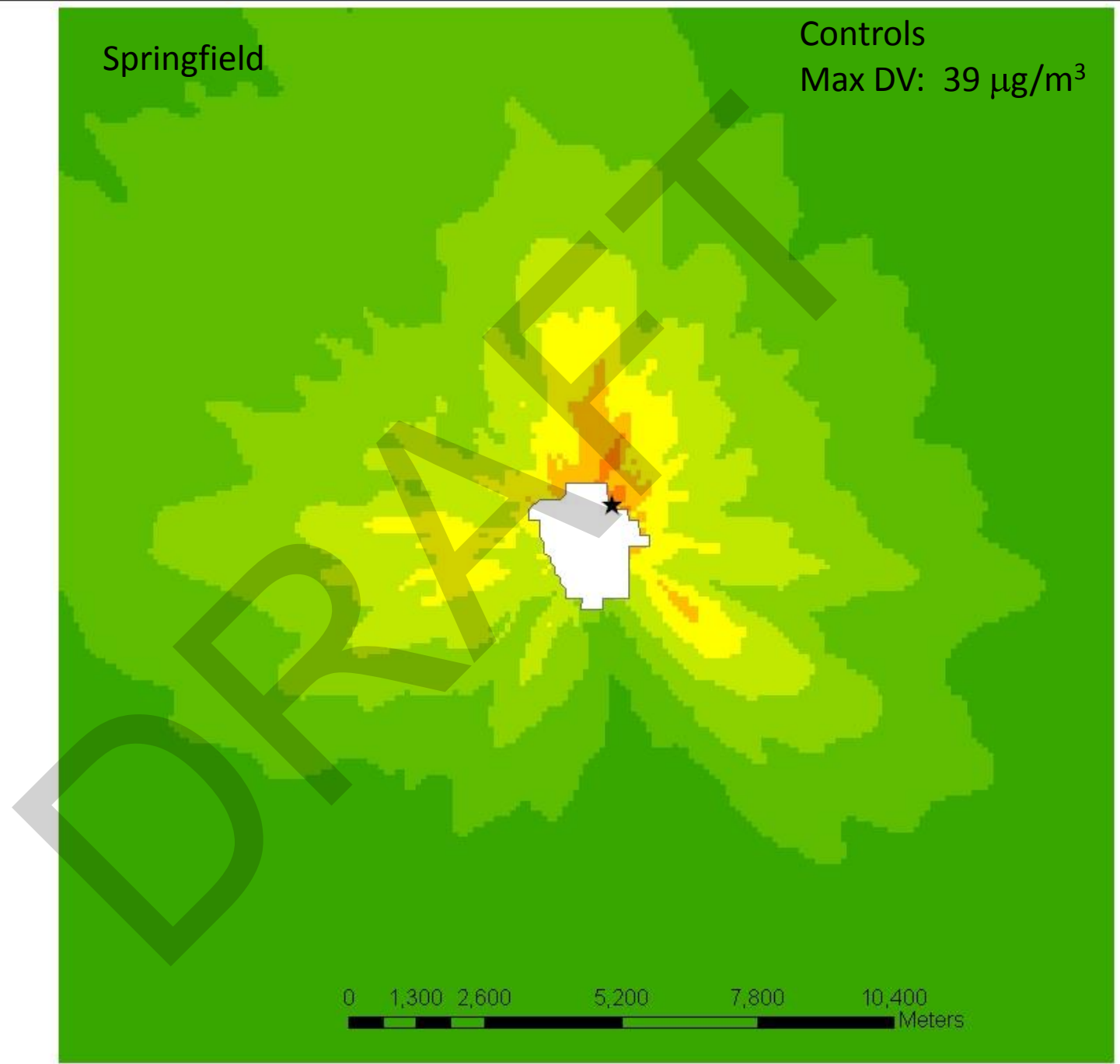
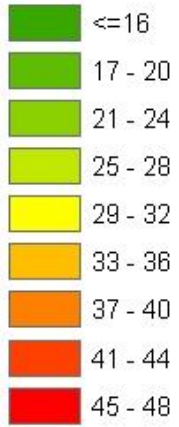


Springfield

Controls

Max DV: 39  $\mu\text{g}/\text{m}^3$

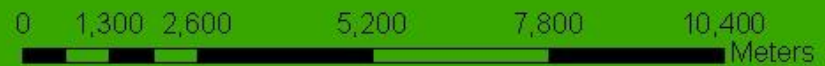
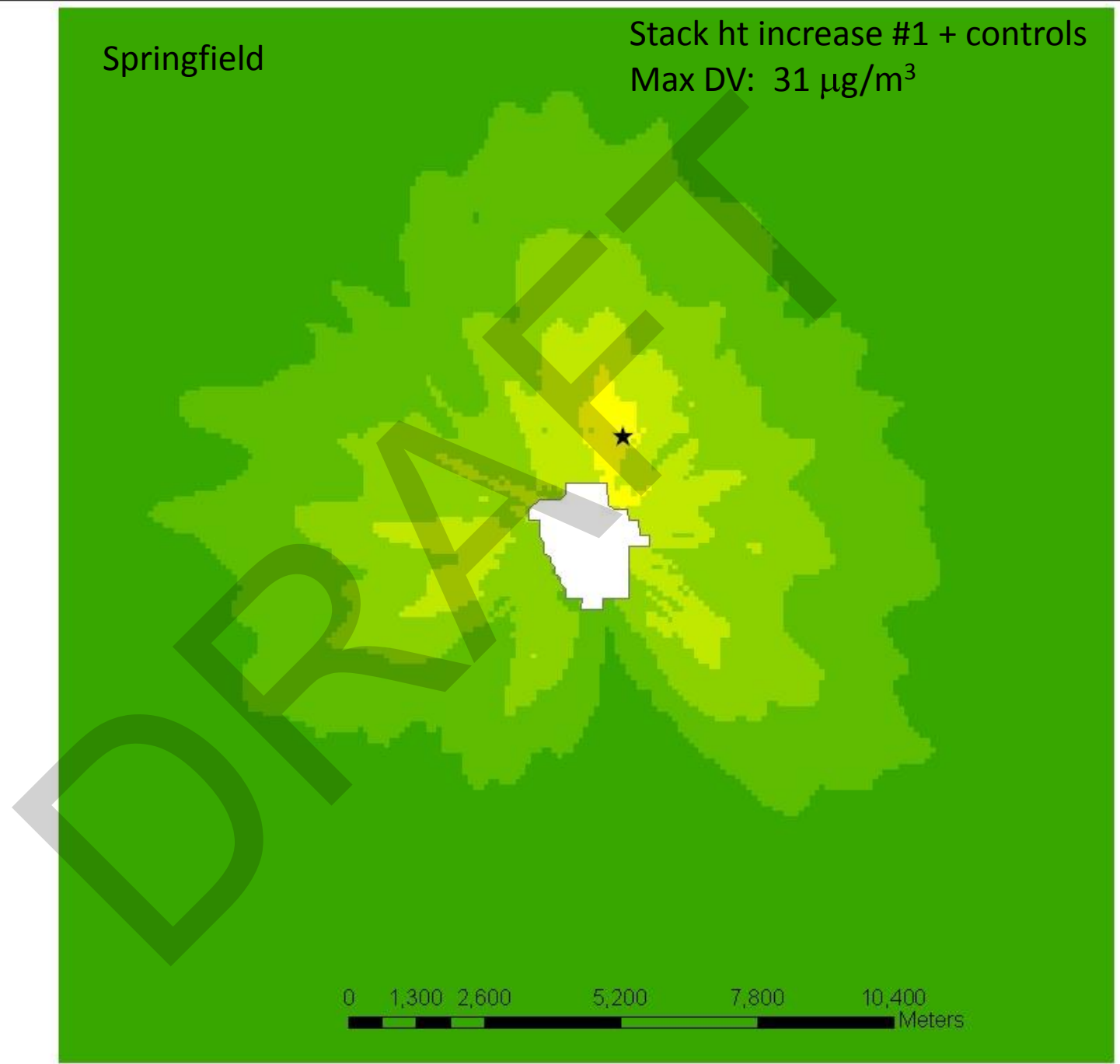
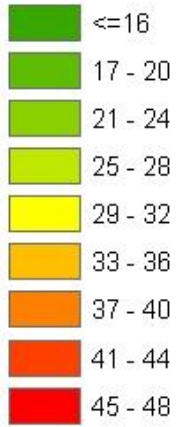
**Legend**



Springfield

Stack ht increase #1 + controls  
Max DV: 31  $\mu\text{g}/\text{m}^3$

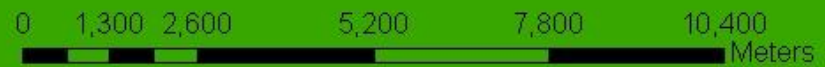
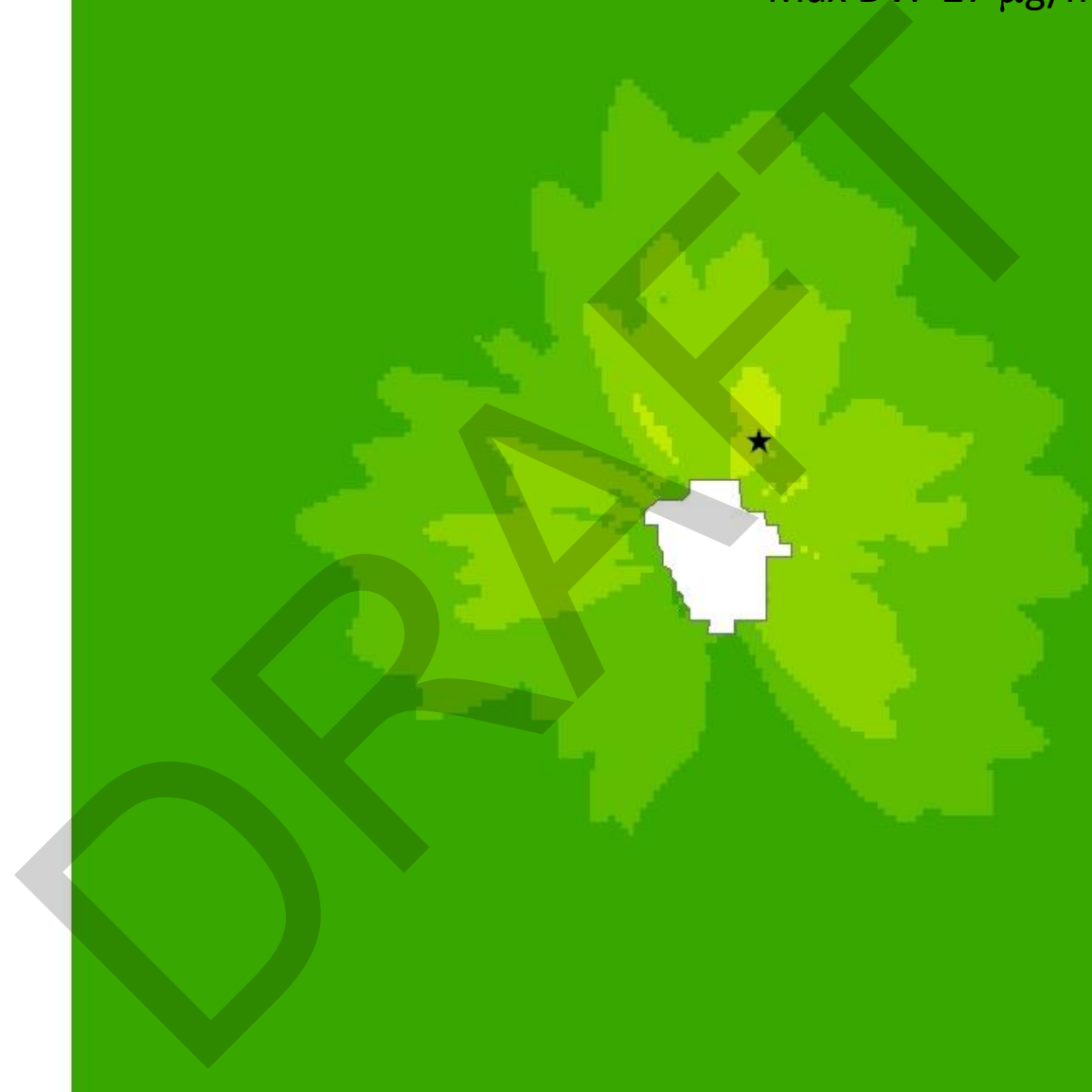
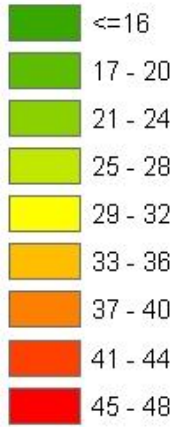
**Legend**



Springfield

Stack ht increase #2 + controls  
Max DV: 27  $\mu\text{g}/\text{m}^3$

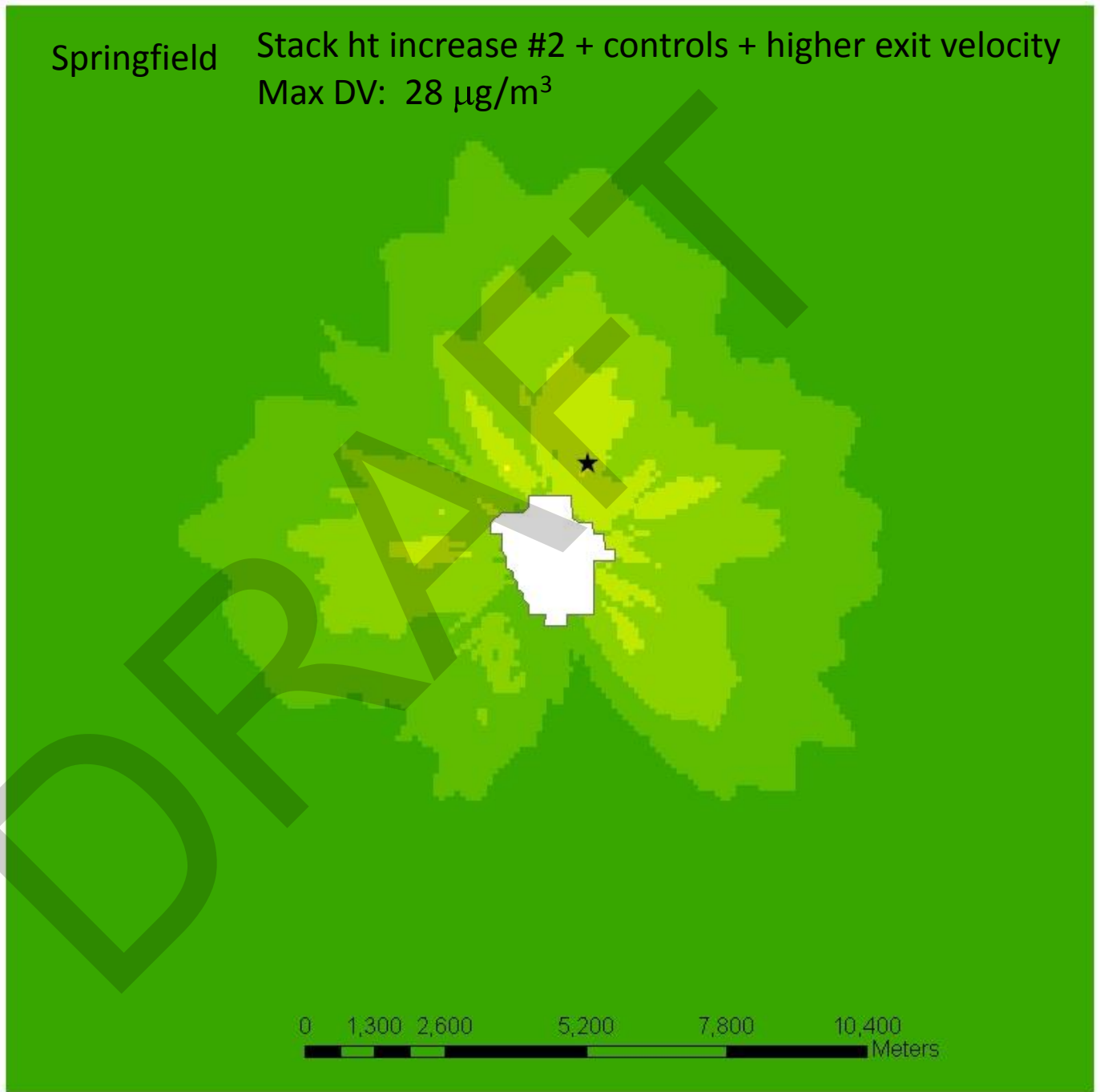
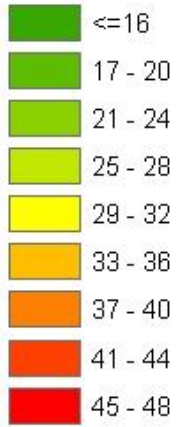
**Legend**



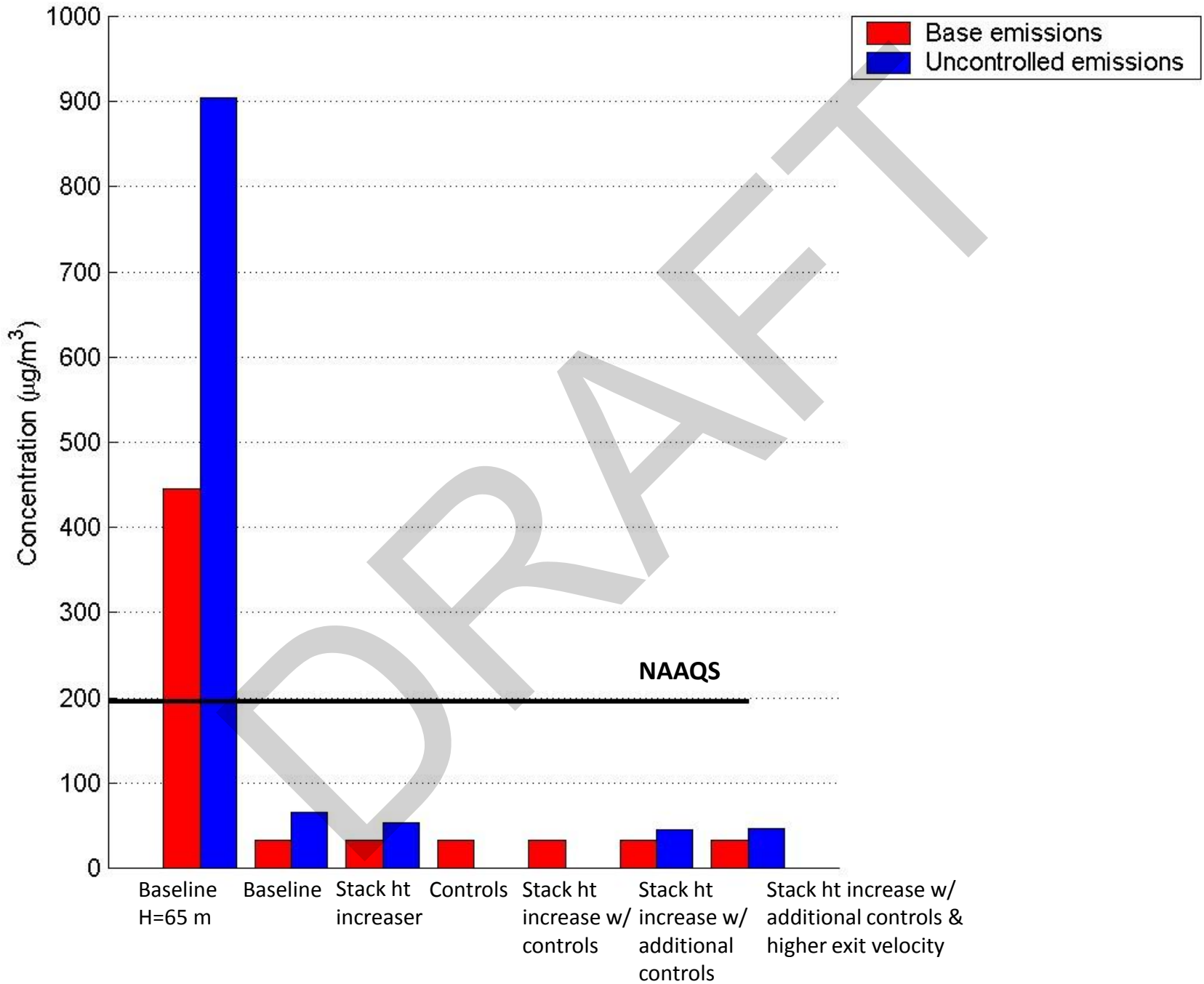
Springfield

Stack ht increase #2 + controls + higher exit velocity  
Max DV:  $28 \mu\text{g}/\text{m}^3$

**Legend**



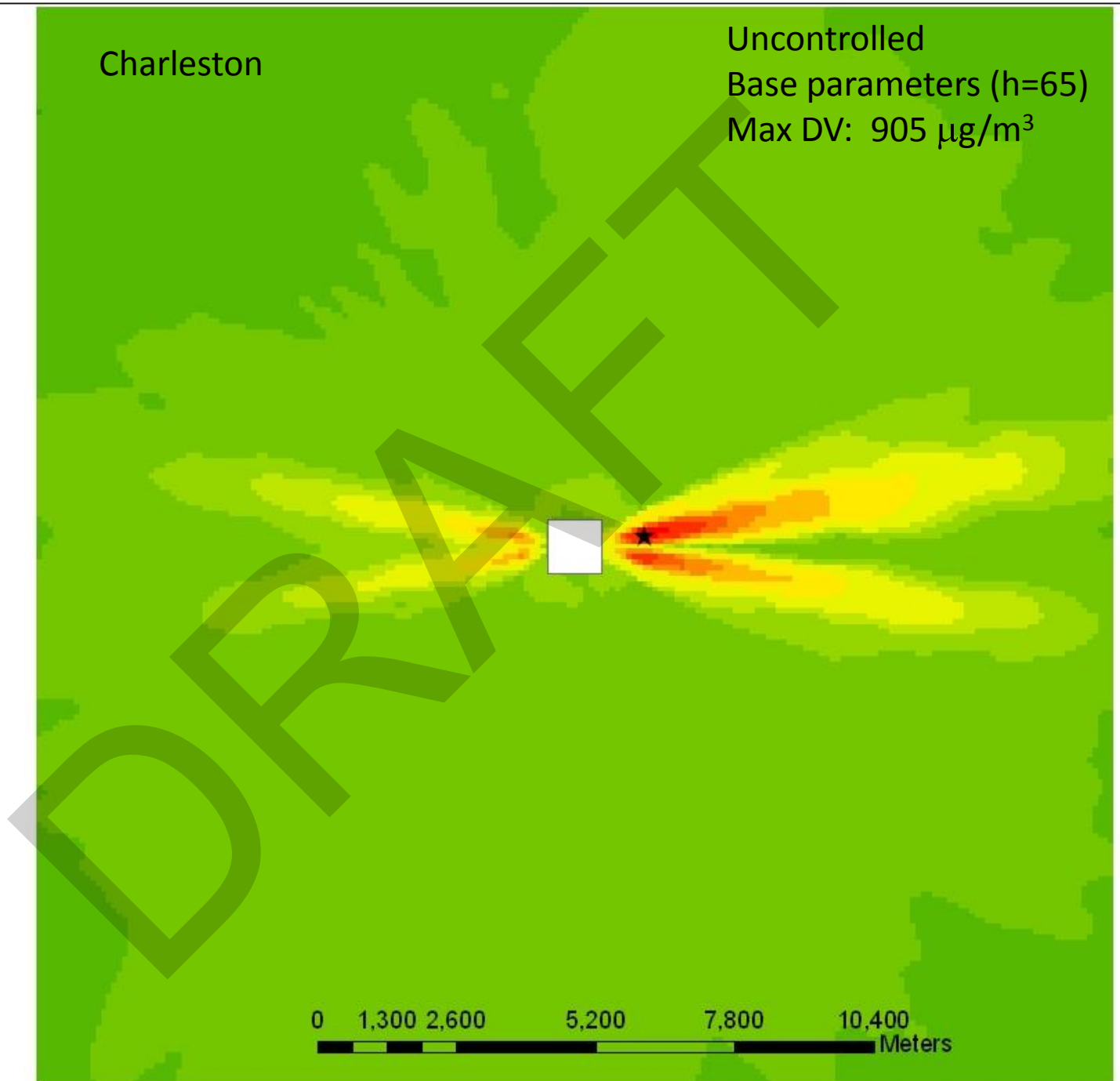
# Coal EGU (Charleston): SO<sub>2</sub>



Charleston

Uncontrolled  
Base parameters (h=65)  
Max DV: 905  $\mu\text{g}/\text{m}^3$

**Legend**



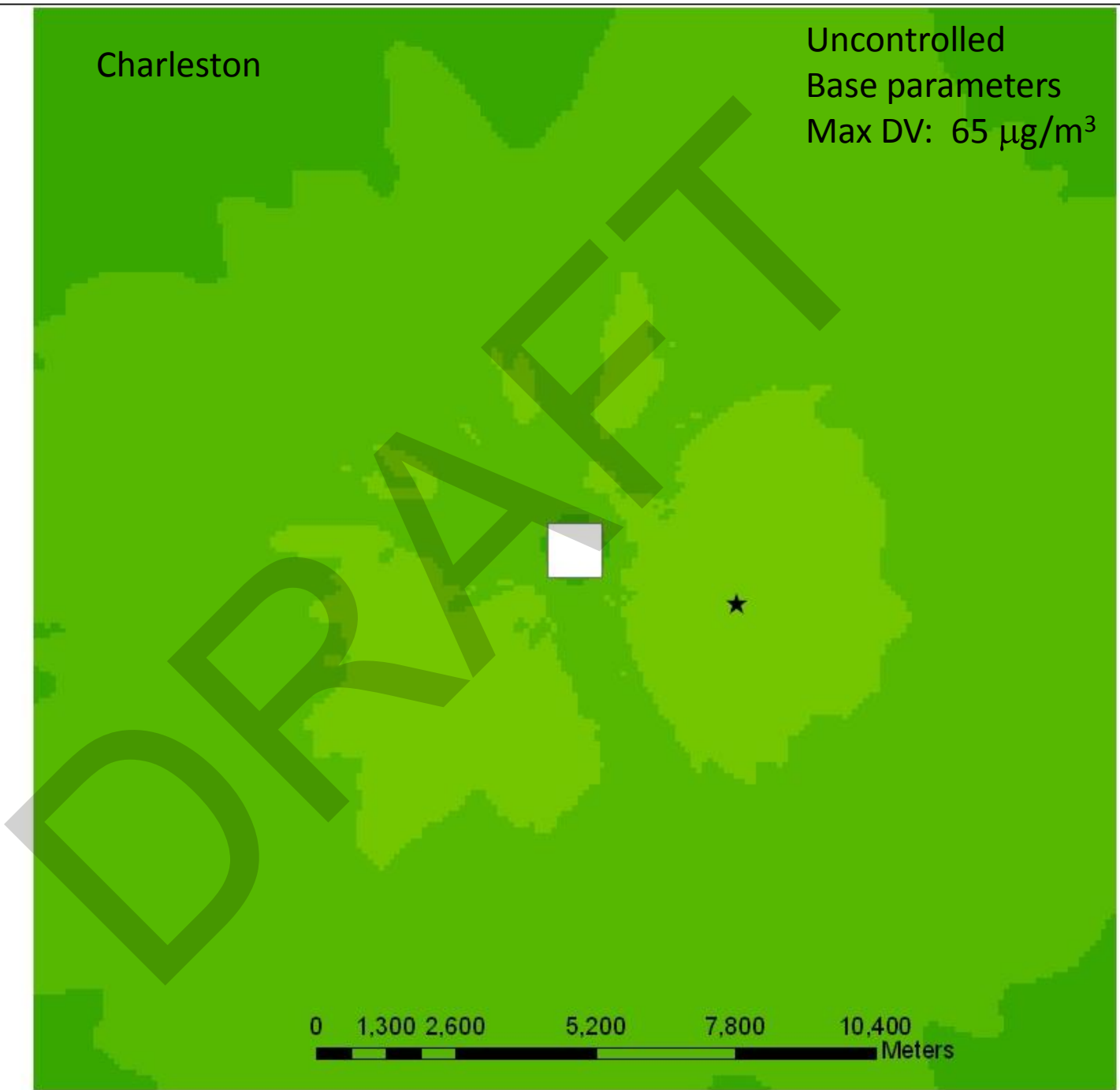
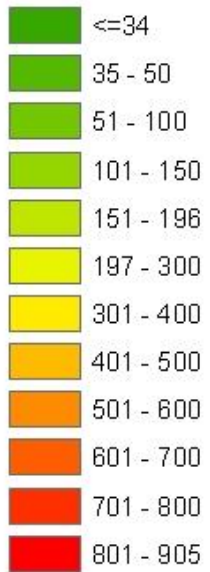
0 1,300 2,600 5,200 7,800 10,400  
Meters



Charleston

Uncontrolled  
Base parameters  
Max DV: 65  $\mu\text{g}/\text{m}^3$

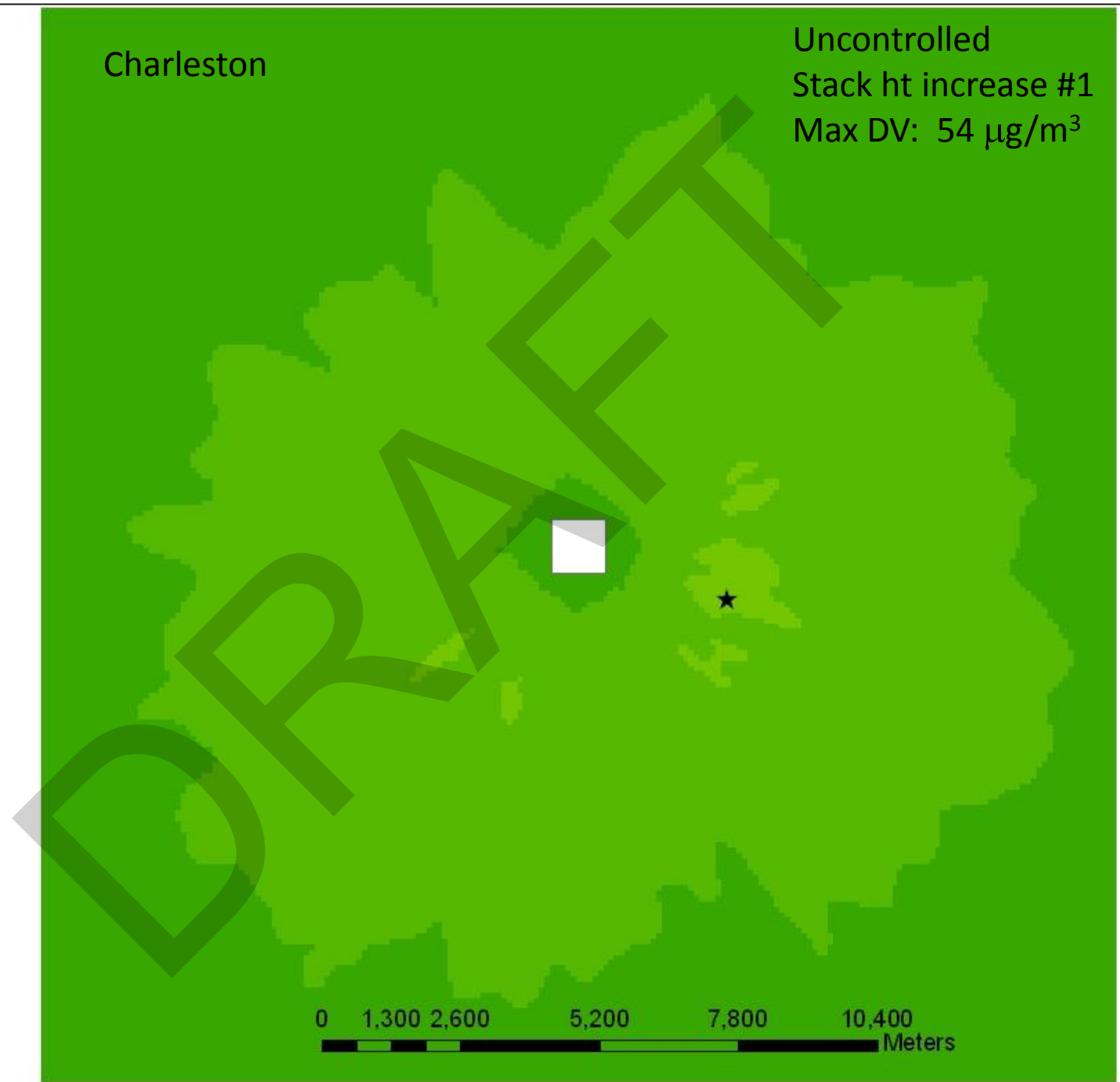
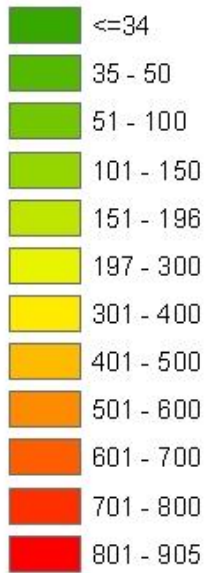
**Legend**



Charleston

Uncontrolled  
Stack ht increase #1  
Max DV: 54  $\mu\text{g}/\text{m}^3$

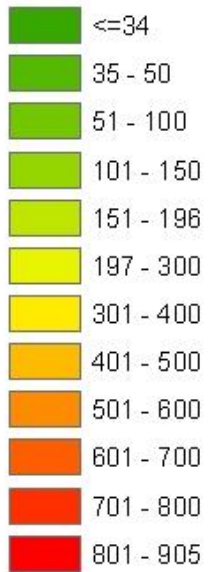
**Legend**



Charleston

Uncontrolled  
Stack ht increase #2  
Max DV: 45  $\mu\text{g}/\text{m}^3$

**Legend**



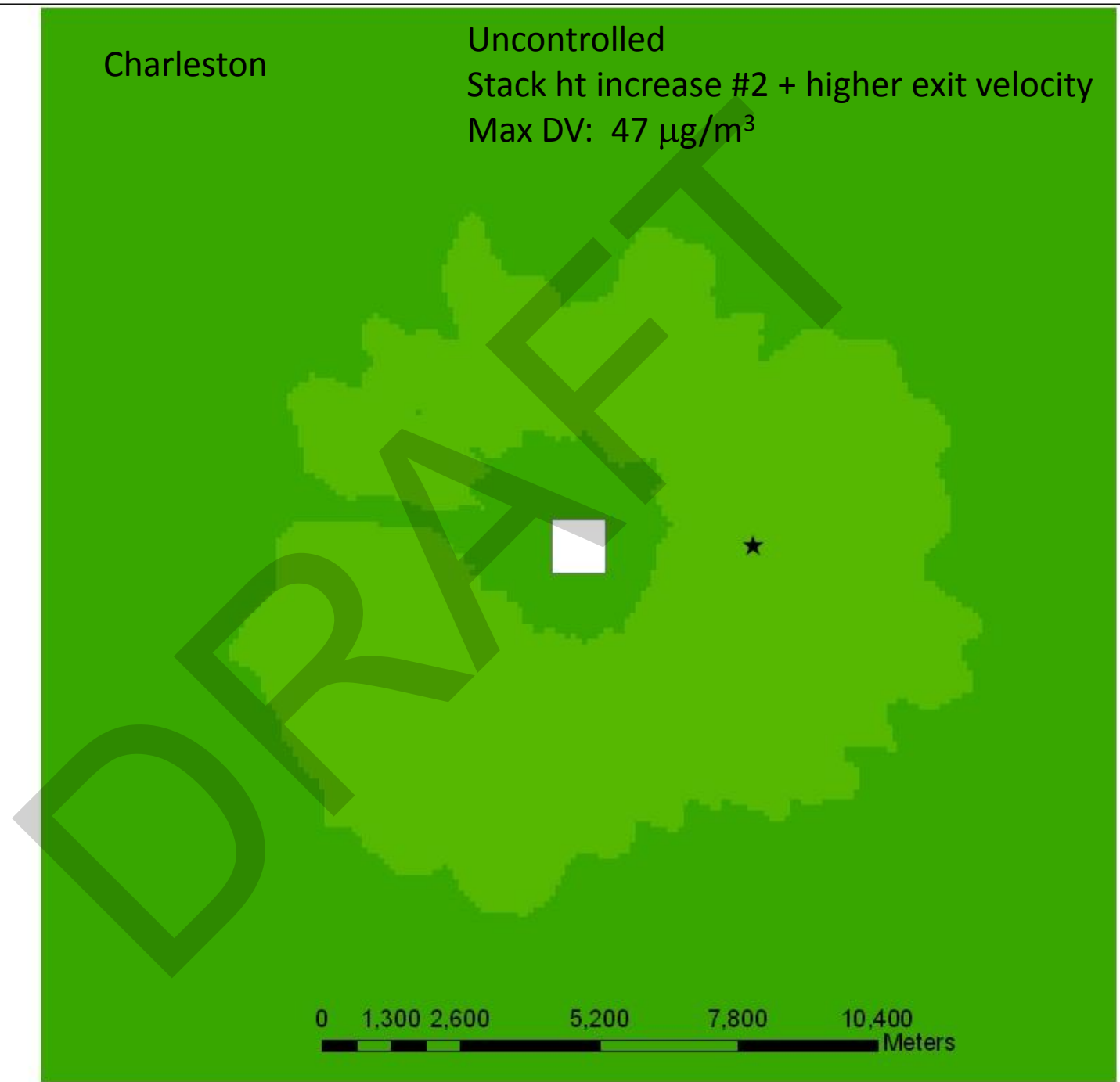
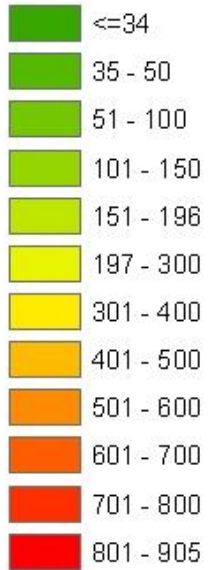
Charleston

Uncontrolled

Stack ht increase #2 + higher exit velocity

Max DV:  $47 \mu\text{g}/\text{m}^3$

**Legend**



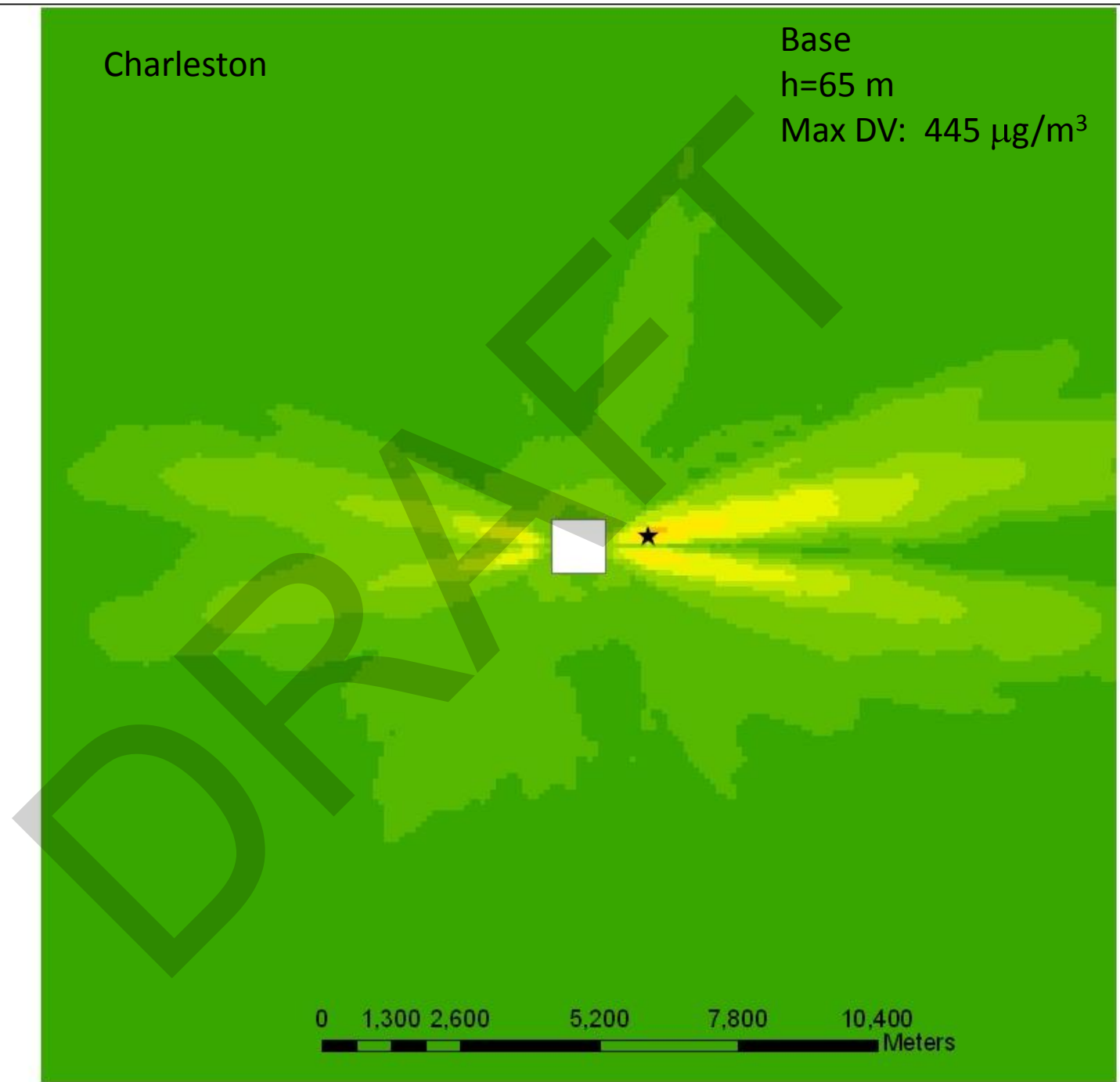
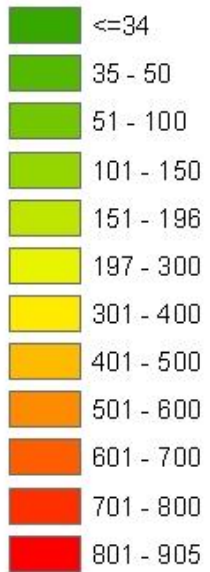
Charleston

Base

$h=65\text{ m}$

Max DV:  $445\ \mu\text{g}/\text{m}^3$

**Legend**

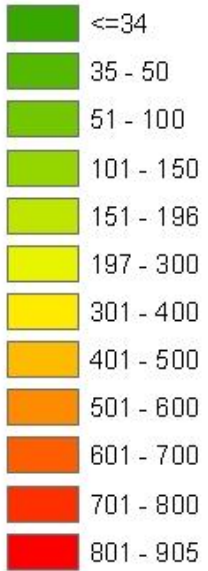


Charleston

Base

Max DV: 33  $\mu\text{g}/\text{m}^3$

**Legend**



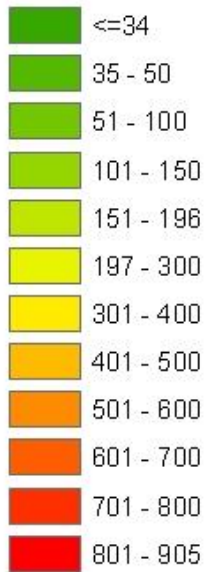
DRAFT



Charleston

Stack ht increase #1  
Max DV: 33  $\mu\text{g}/\text{m}^3$

**Legend**



DRAFT

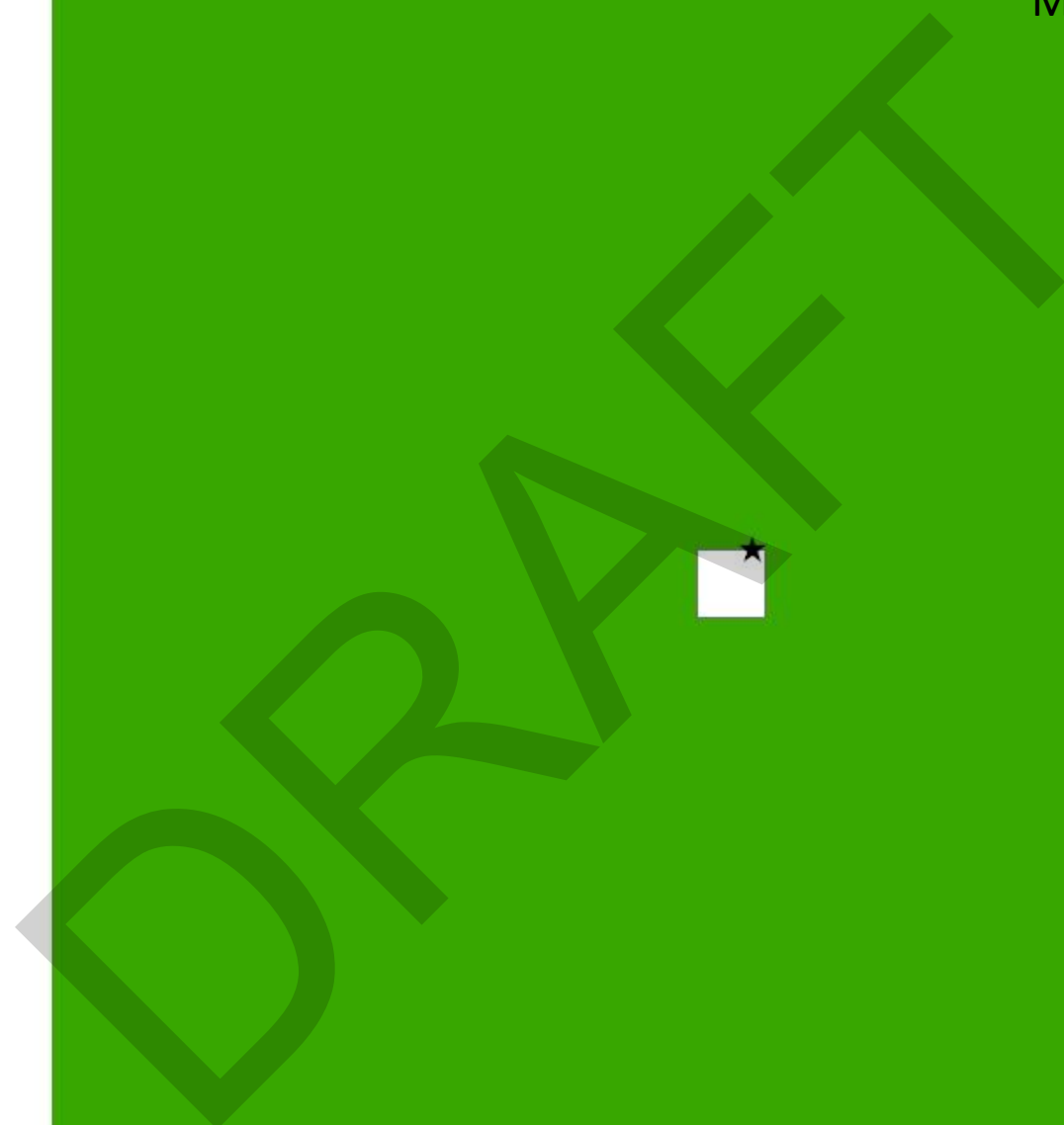
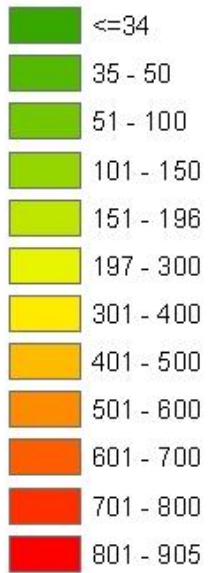


Charleston

Controls

Max DV: 33  $\mu\text{g}/\text{m}^3$

**Legend**

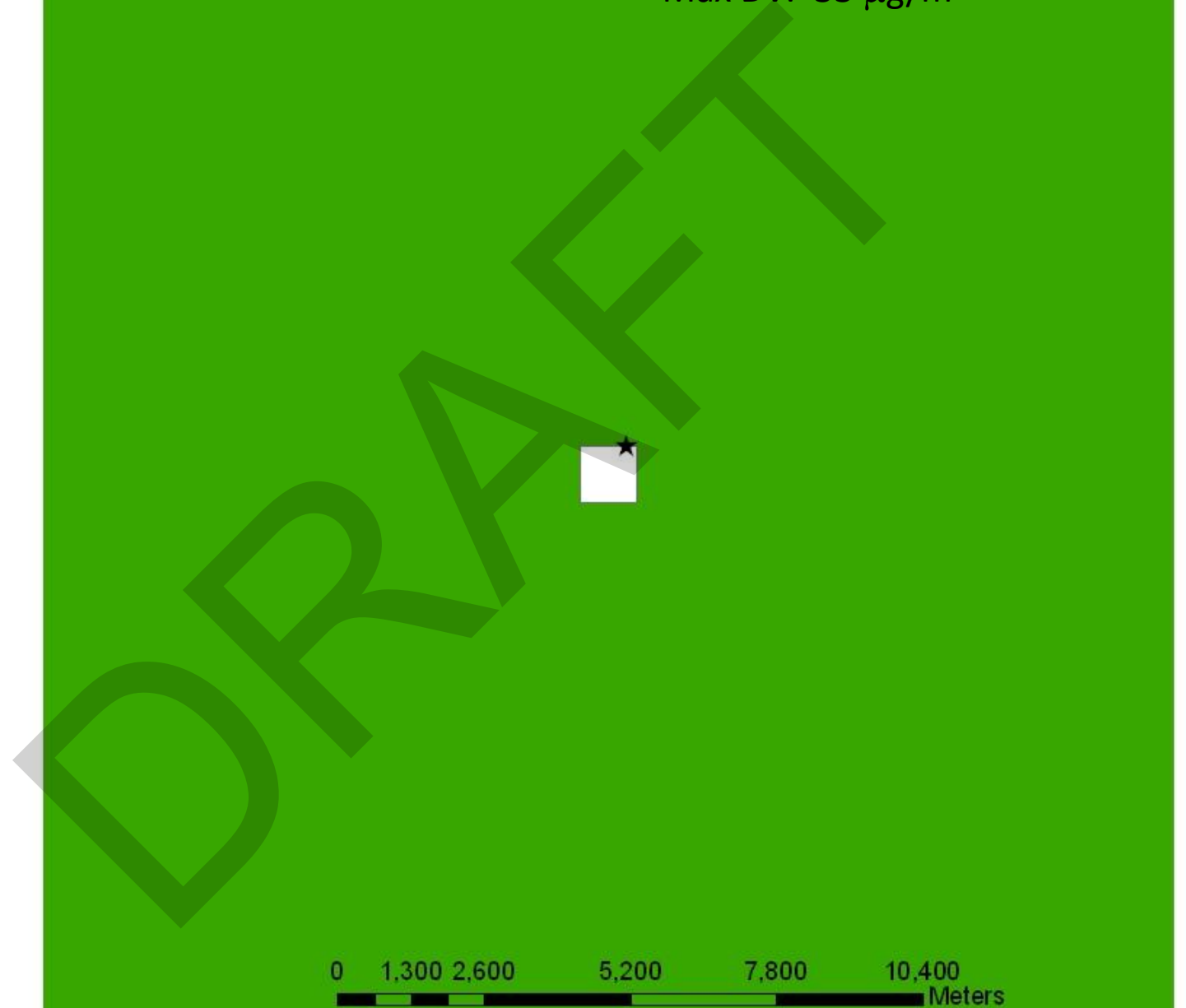
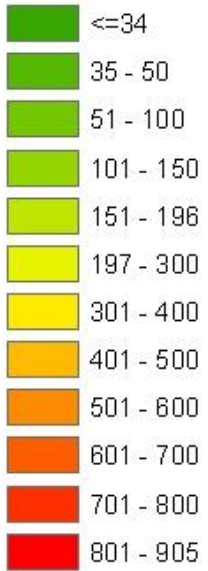




Charleston

Stack ht increase #1 + controls  
Max DV: 33  $\mu\text{g}/\text{m}^3$

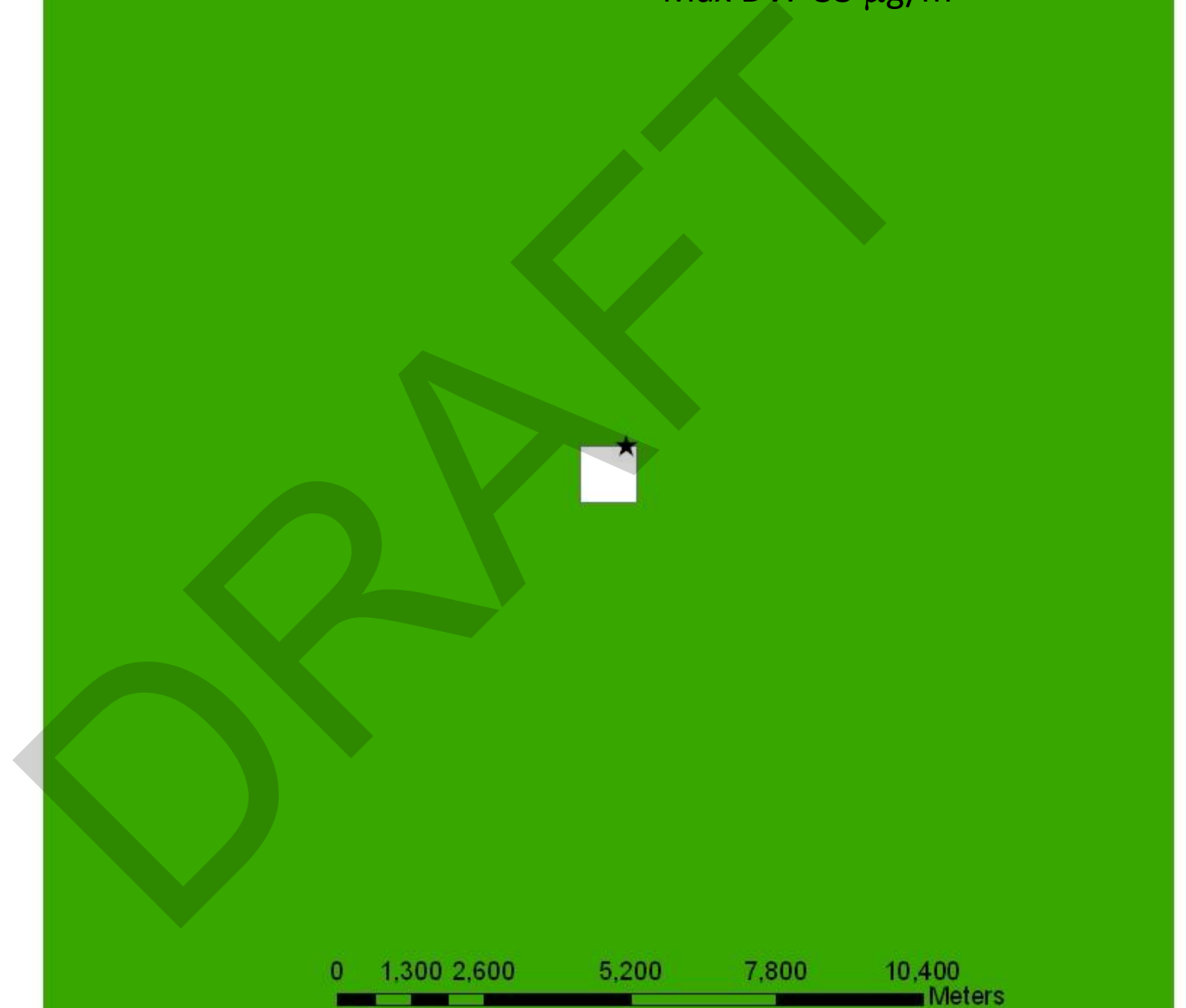
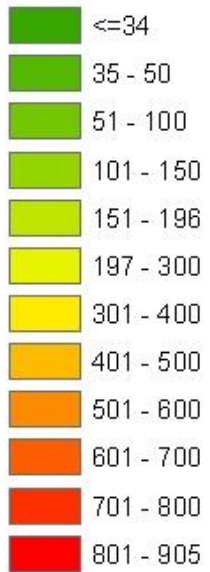
**Legend**



Charleston

Stack ht increase #2 + controls  
Max DV: 33  $\mu\text{g}/\text{m}^3$

**Legend**

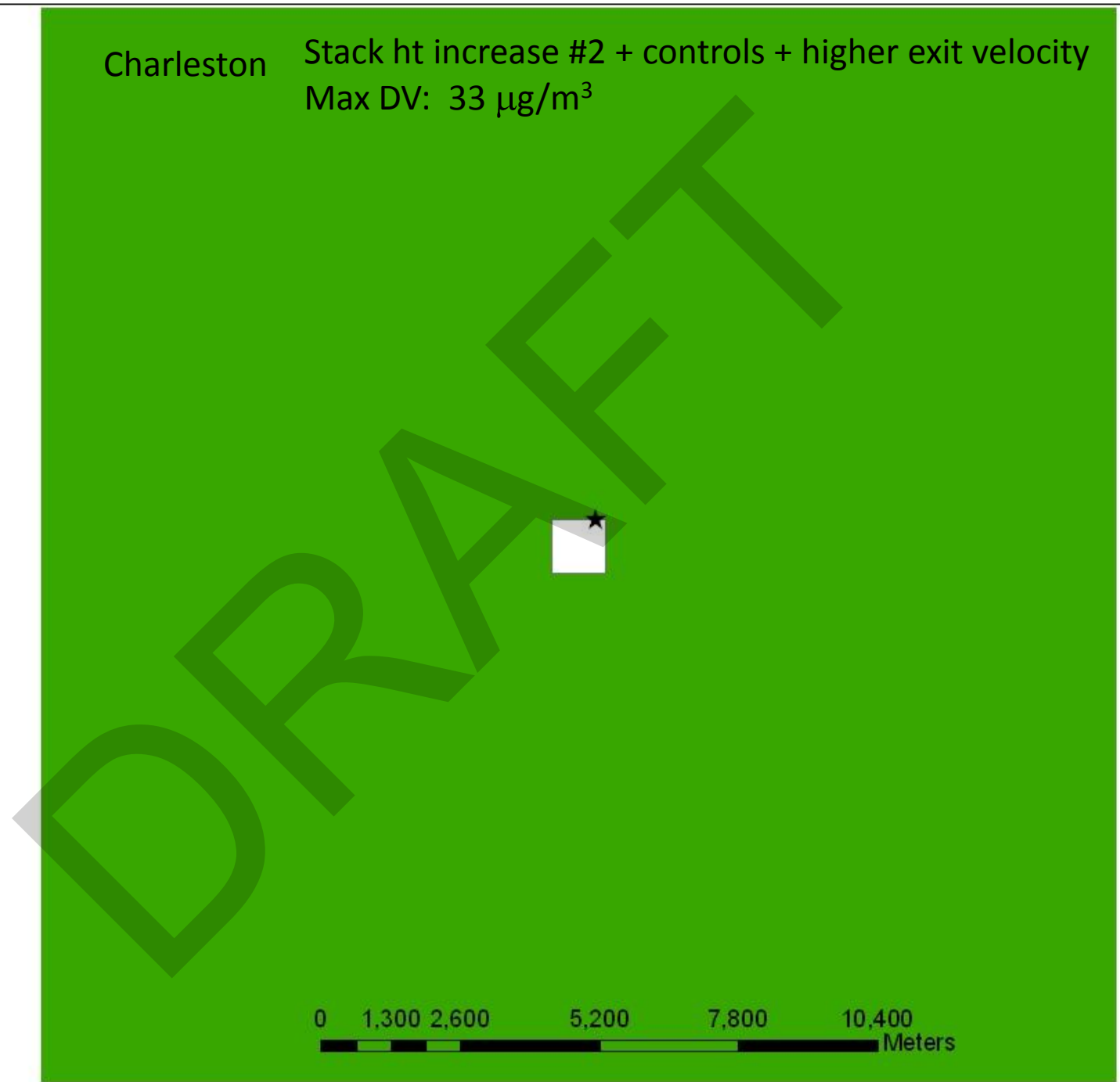
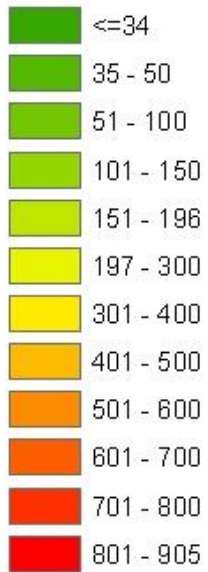


Charleston

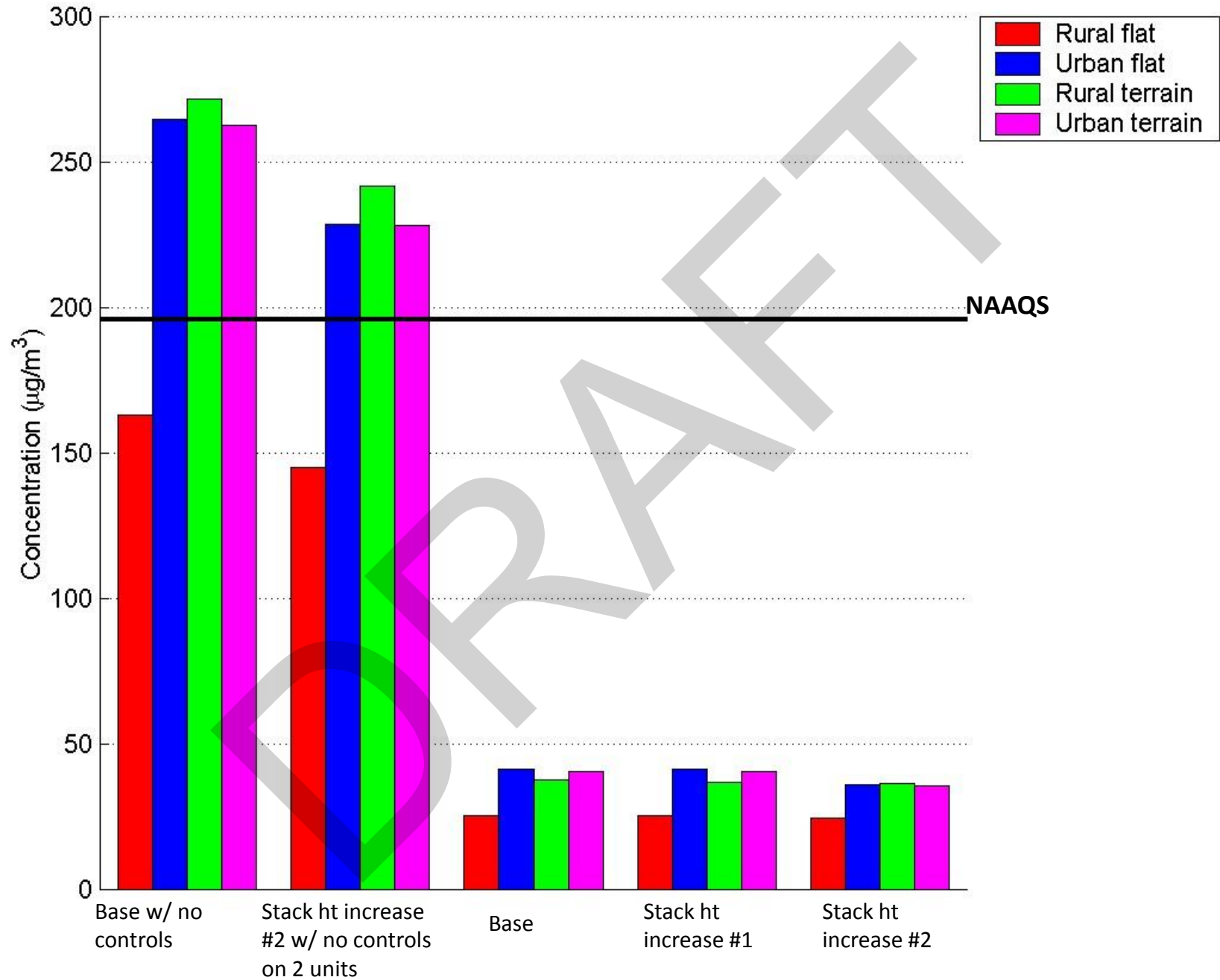
Stack ht increase #2 + controls + higher exit velocity

Max DV:  $33 \mu\text{g}/\text{m}^3$

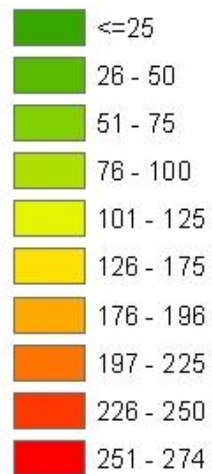
**Legend**



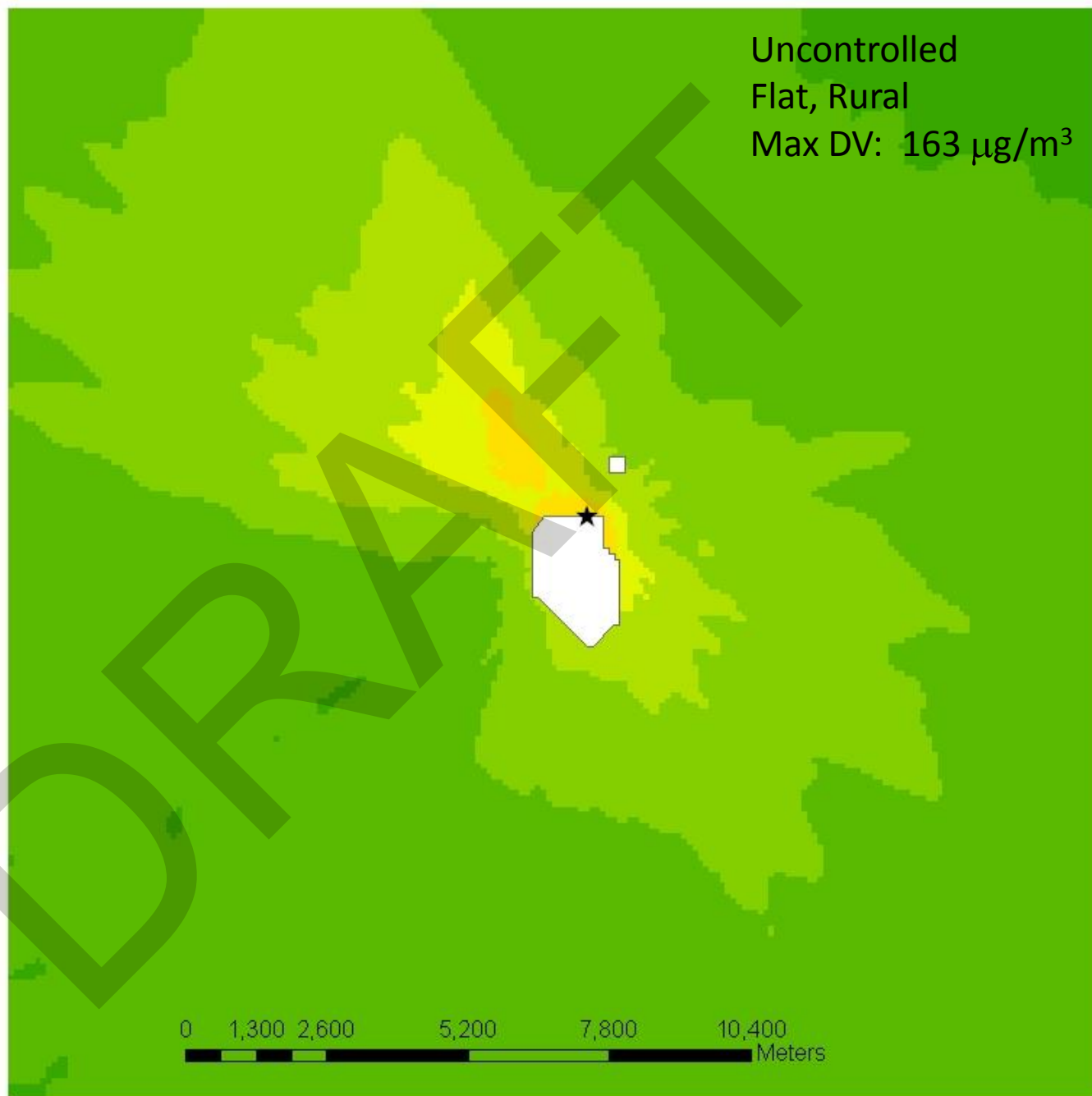
# Refinery: SO<sub>2</sub>



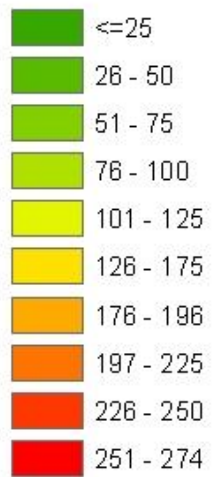
### Legend



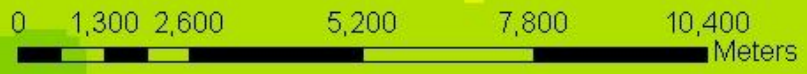
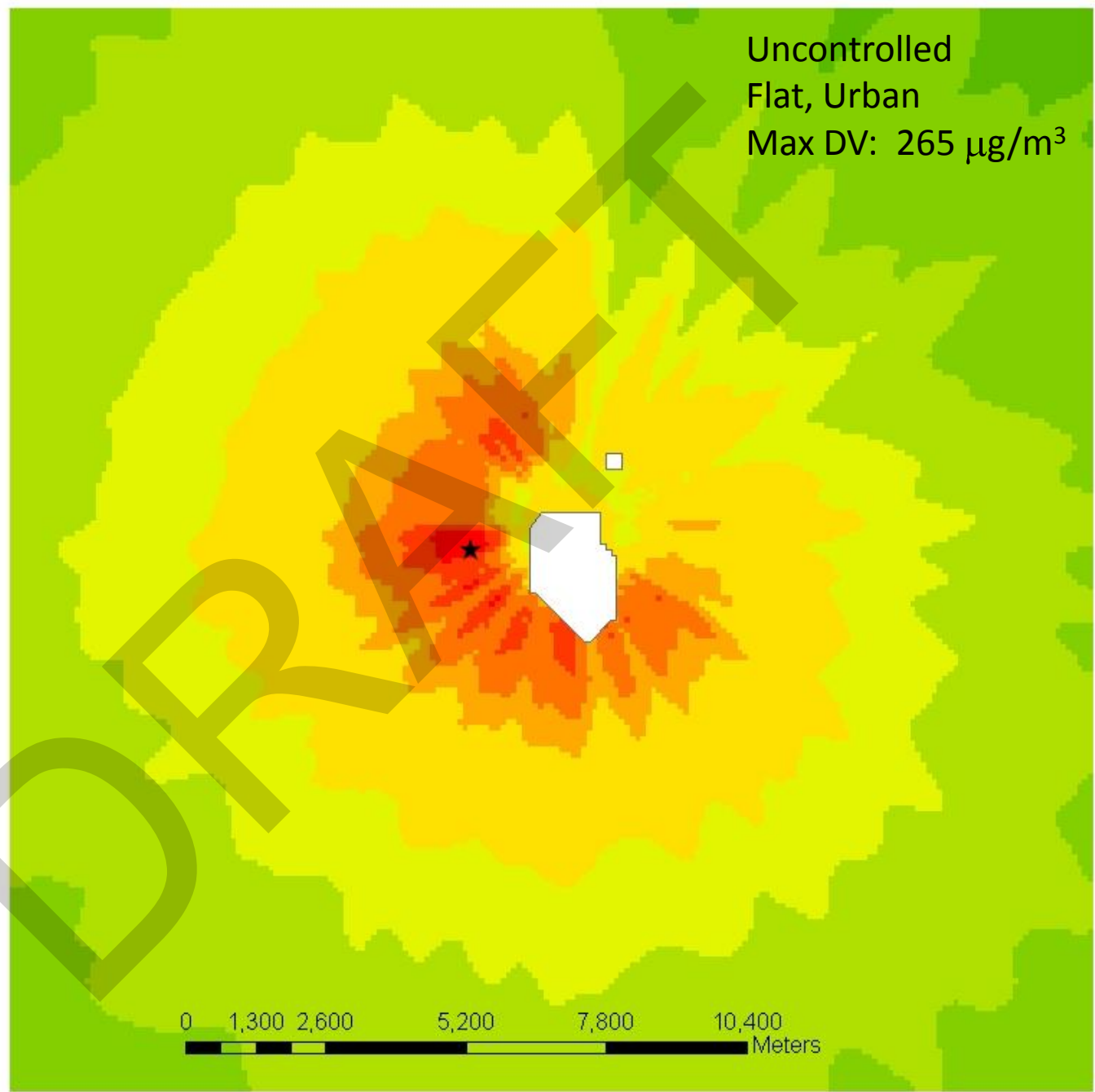
Uncontrolled  
Flat, Rural  
Max DV: 163  $\mu\text{g}/\text{m}^3$



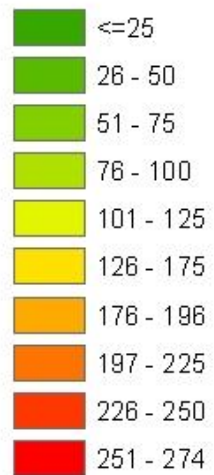
**Legend**



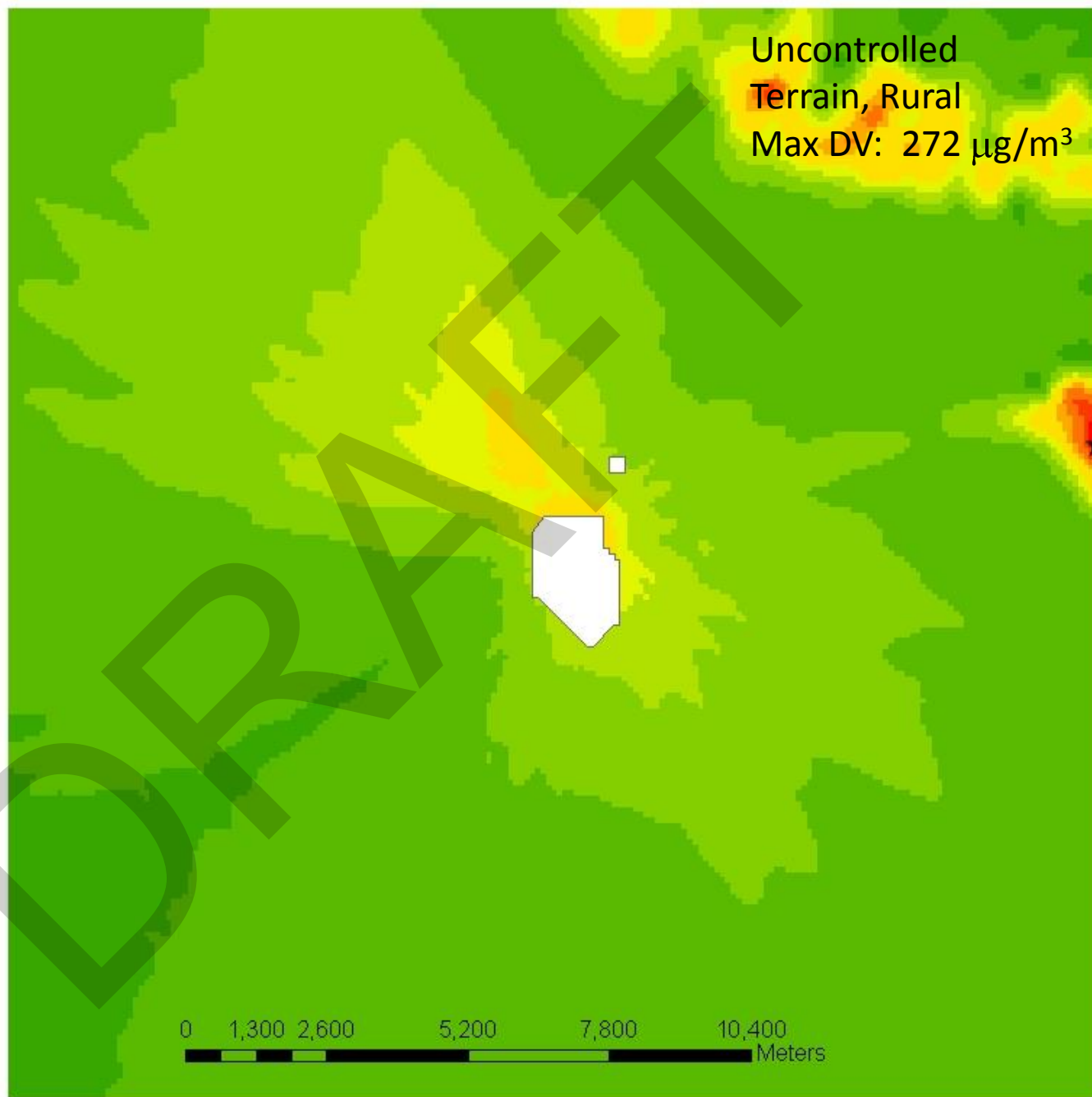
Uncontrolled  
Flat, Urban  
Max DV: 265 µg/m<sup>3</sup>



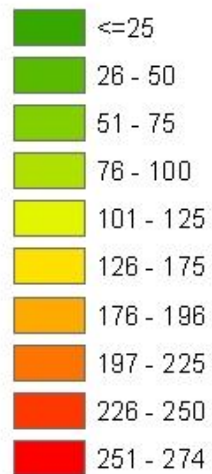
### Legend



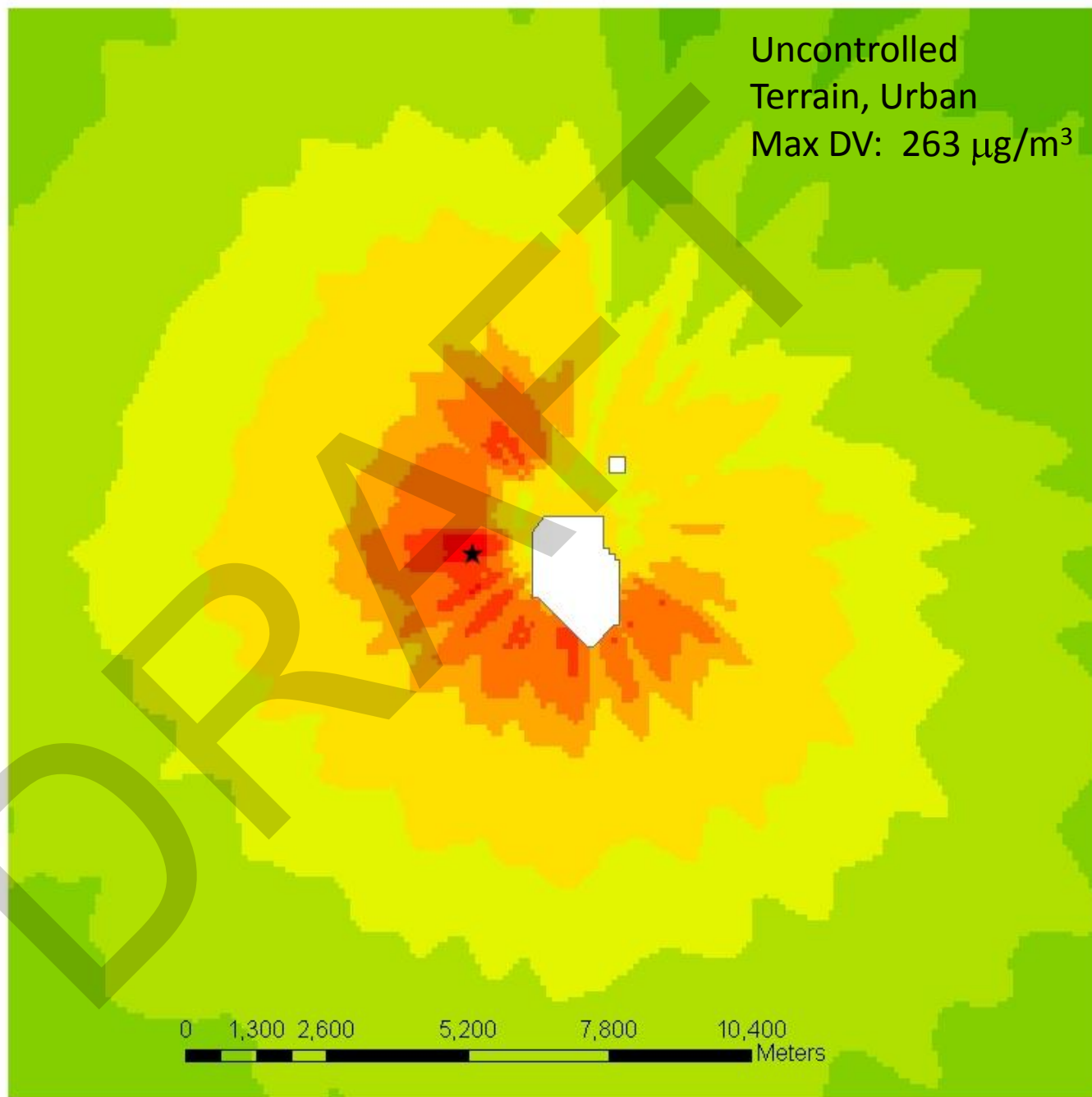
Uncontrolled  
Terrain, Rural  
Max DV: 272  $\mu\text{g}/\text{m}^3$



### Legend

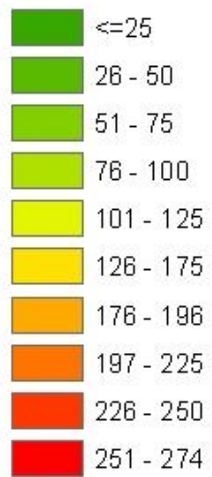


Uncontrolled  
Terrain, Urban  
Max DV: 263  $\mu\text{g}/\text{m}^3$

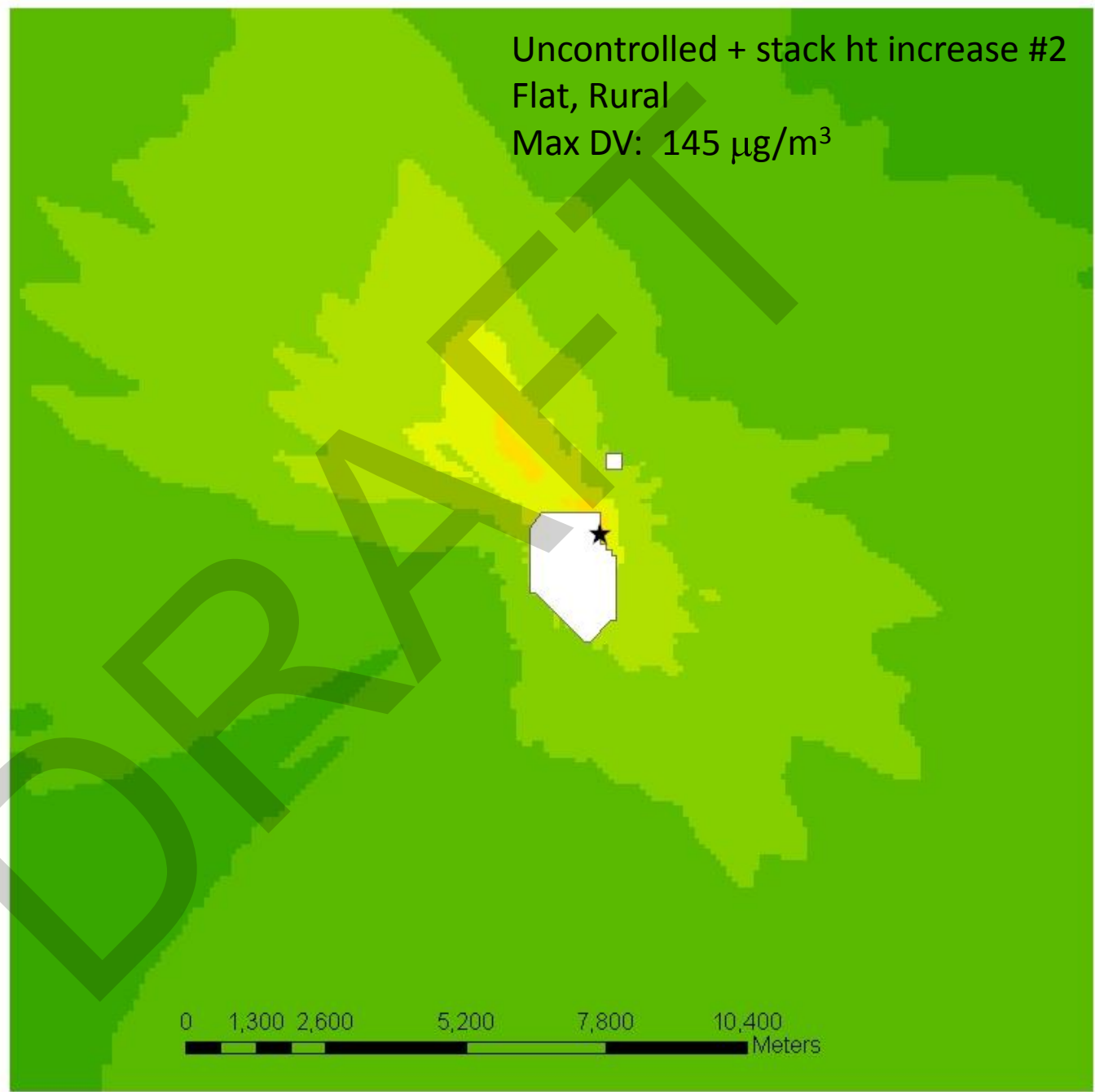




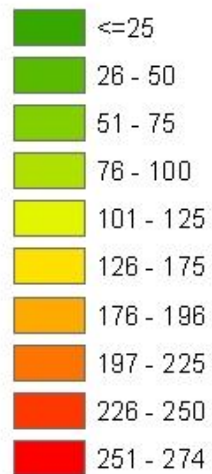
**Legend**



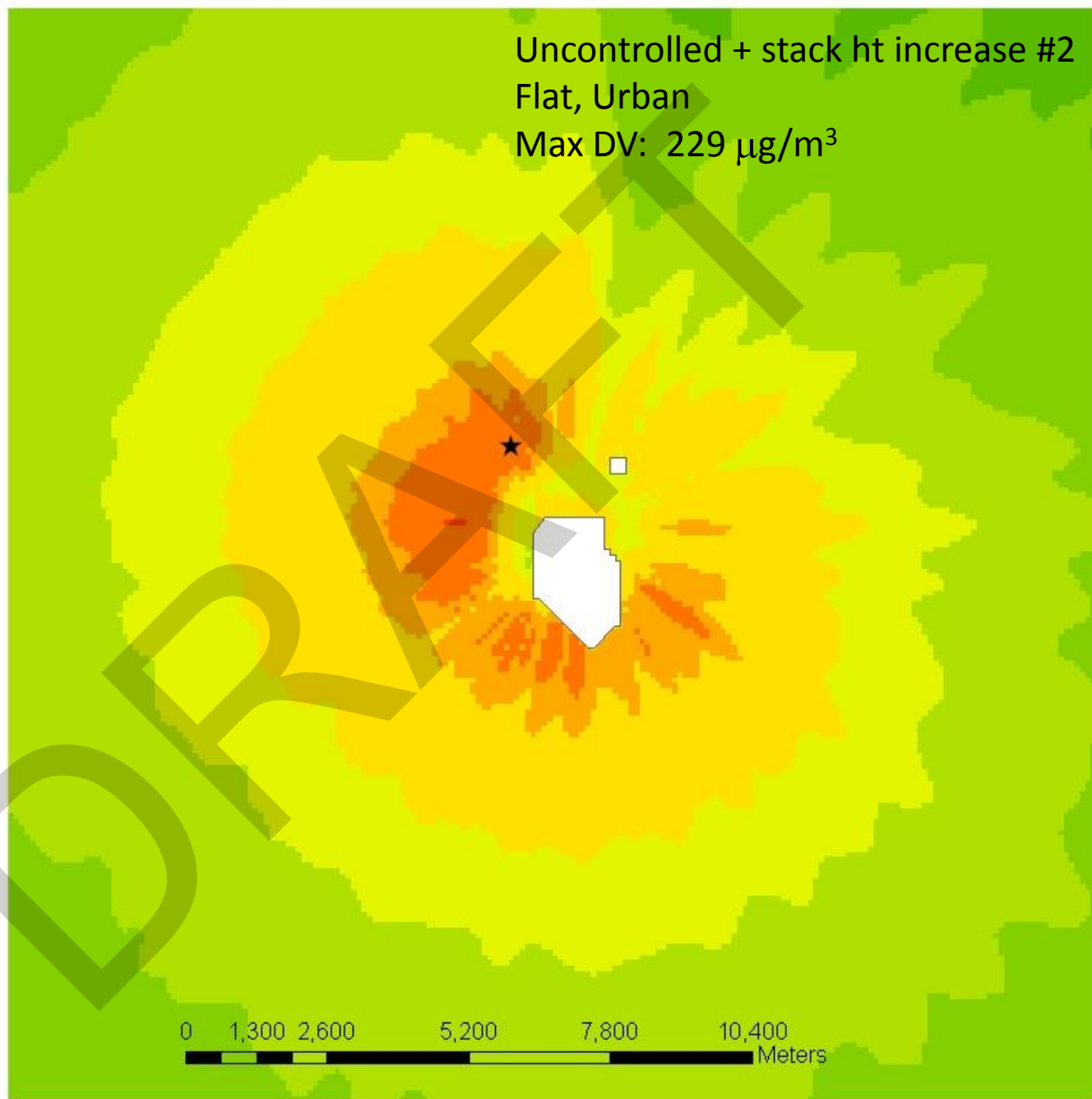
Uncontrolled + stack ht increase #2  
Flat, Rural  
Max DV: 145 µg/m<sup>3</sup>



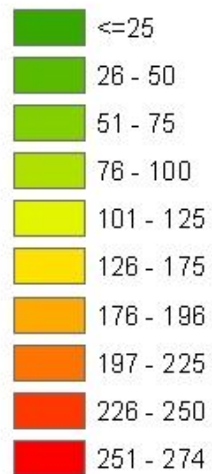
### Legend



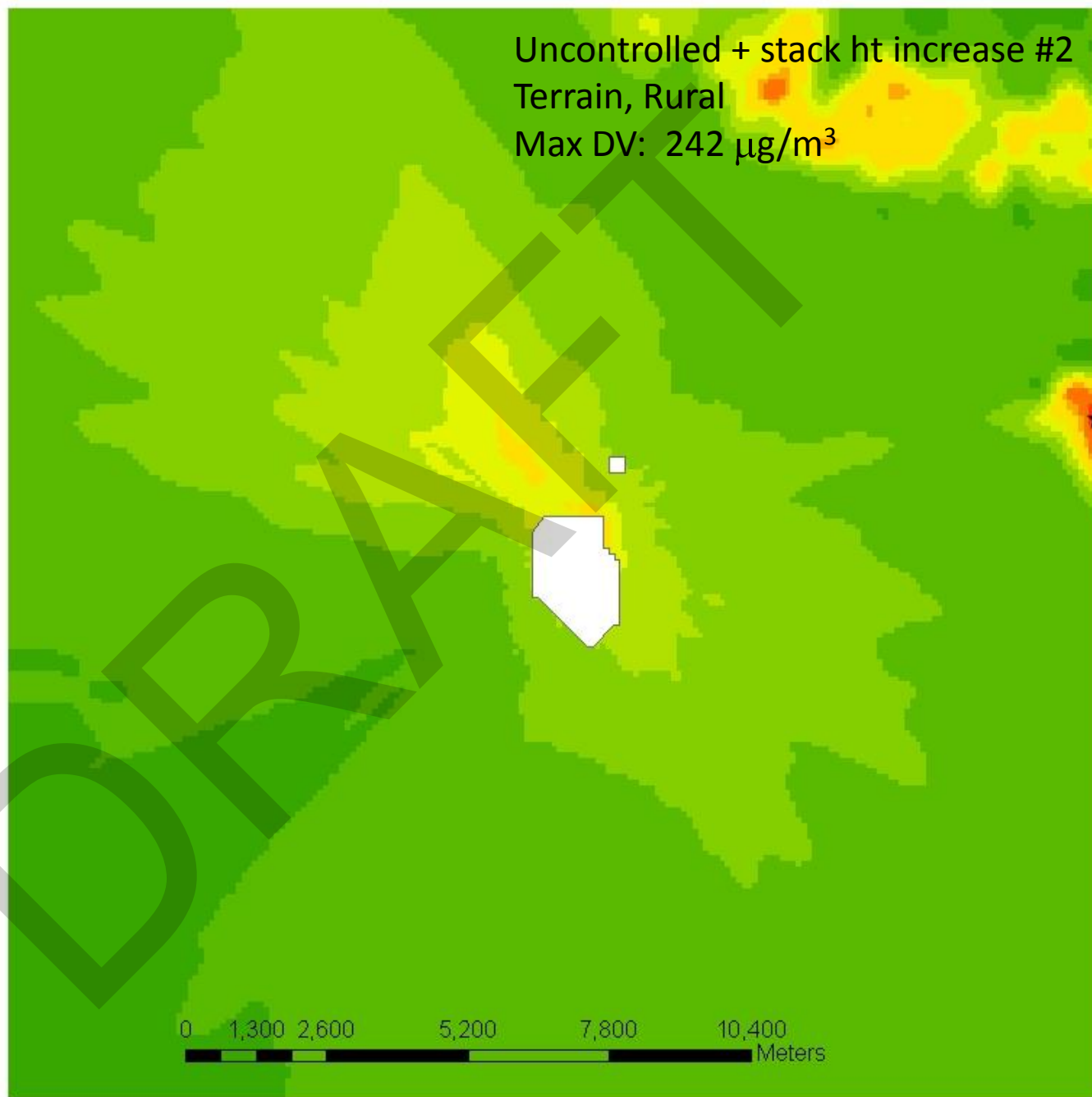
Uncontrolled + stack ht increase #2  
Flat, Urban  
Max DV: 229  $\mu\text{g}/\text{m}^3$



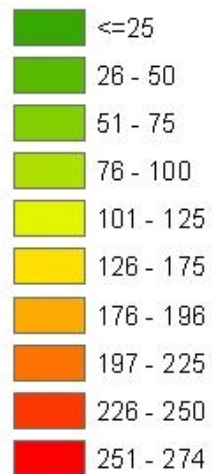
### Legend



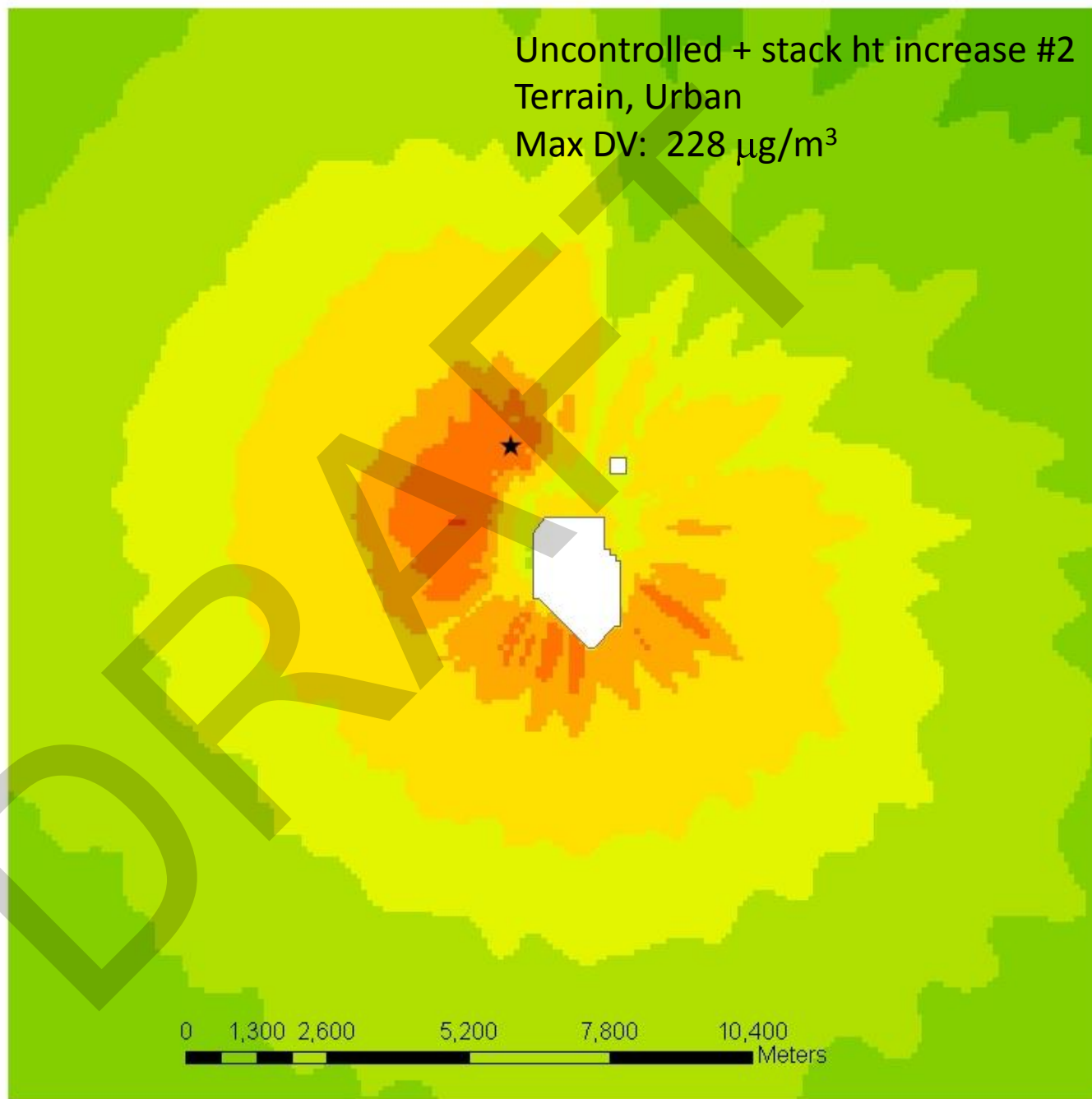
Uncontrolled + stack ht increase #2  
Terrain, Rural  
Max DV: 242  $\mu\text{g}/\text{m}^3$



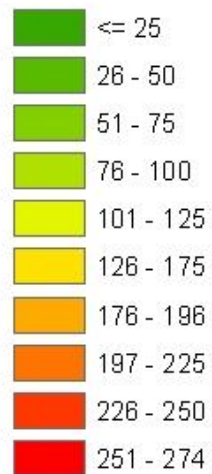
### Legend



Uncontrolled + stack ht increase #2  
Terrain, Urban  
Max DV: 228  $\mu\text{g}/\text{m}^3$



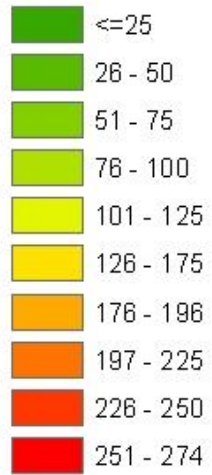
### Legend



Base  
Flat, Rural  
Max DV: 25  $\mu\text{g}/\text{m}^3$



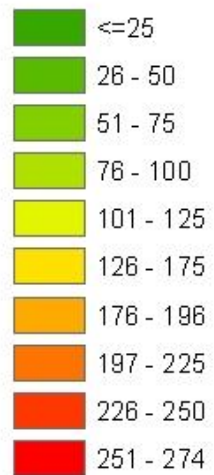
### Legend



Base  
Flat, Urban  
Max DV:  $41 \mu\text{g}/\text{m}^3$



### Legend



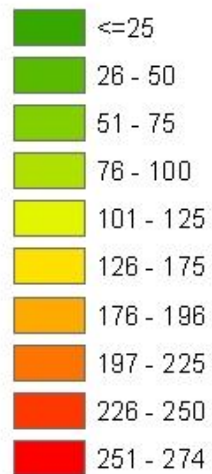
Base  
Terrain, Rural  
Max DV:  $38 \mu\text{g}/\text{m}^3$

0 1,300 2,600 5,200 7,800 10,400 Meters

A horizontal scale bar with tick marks at 0, 1,300, 2,600, 5,200, 7,800, and 10,400 meters. The bar is black with white tick marks.

DRAFT

### Legend

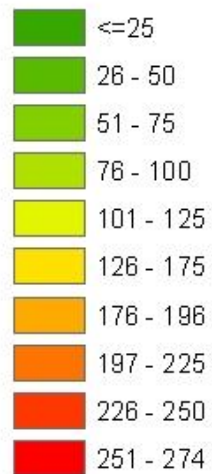


Base  
Terrain, Urban  
Max DV:  $41 \mu\text{g}/\text{m}^3$





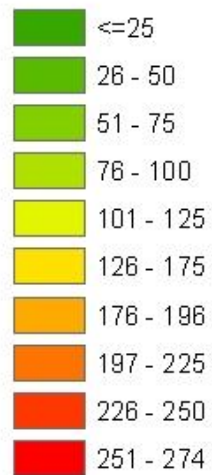
### Legend



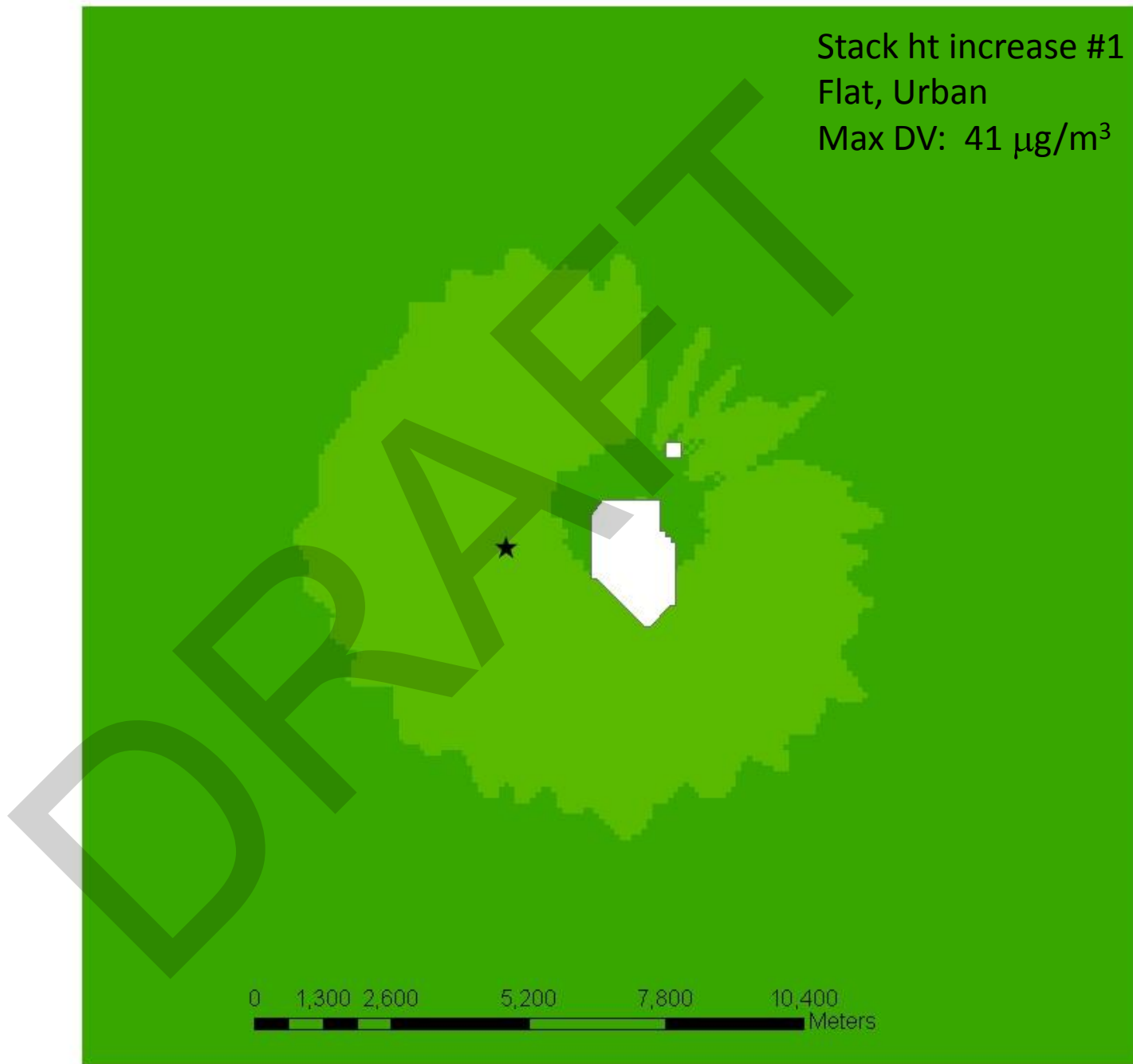
Stack ht increase #1  
Flat, Rural  
Max DV: 25  $\mu\text{g}/\text{m}^3$



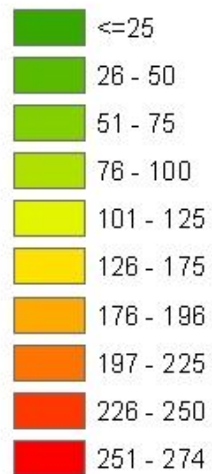
### Legend



Stack ht increase #1  
Flat, Urban  
Max DV: 41  $\mu\text{g}/\text{m}^3$



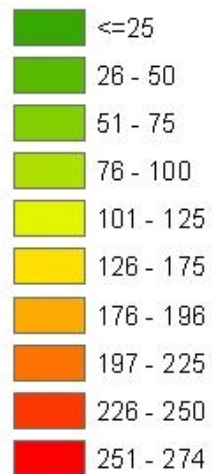
### Legend



Stack ht increase #1  
Terrain, Rural  
Max DV:  $37 \mu\text{g}/\text{m}^3$



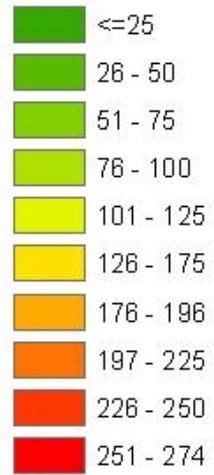
### Legend



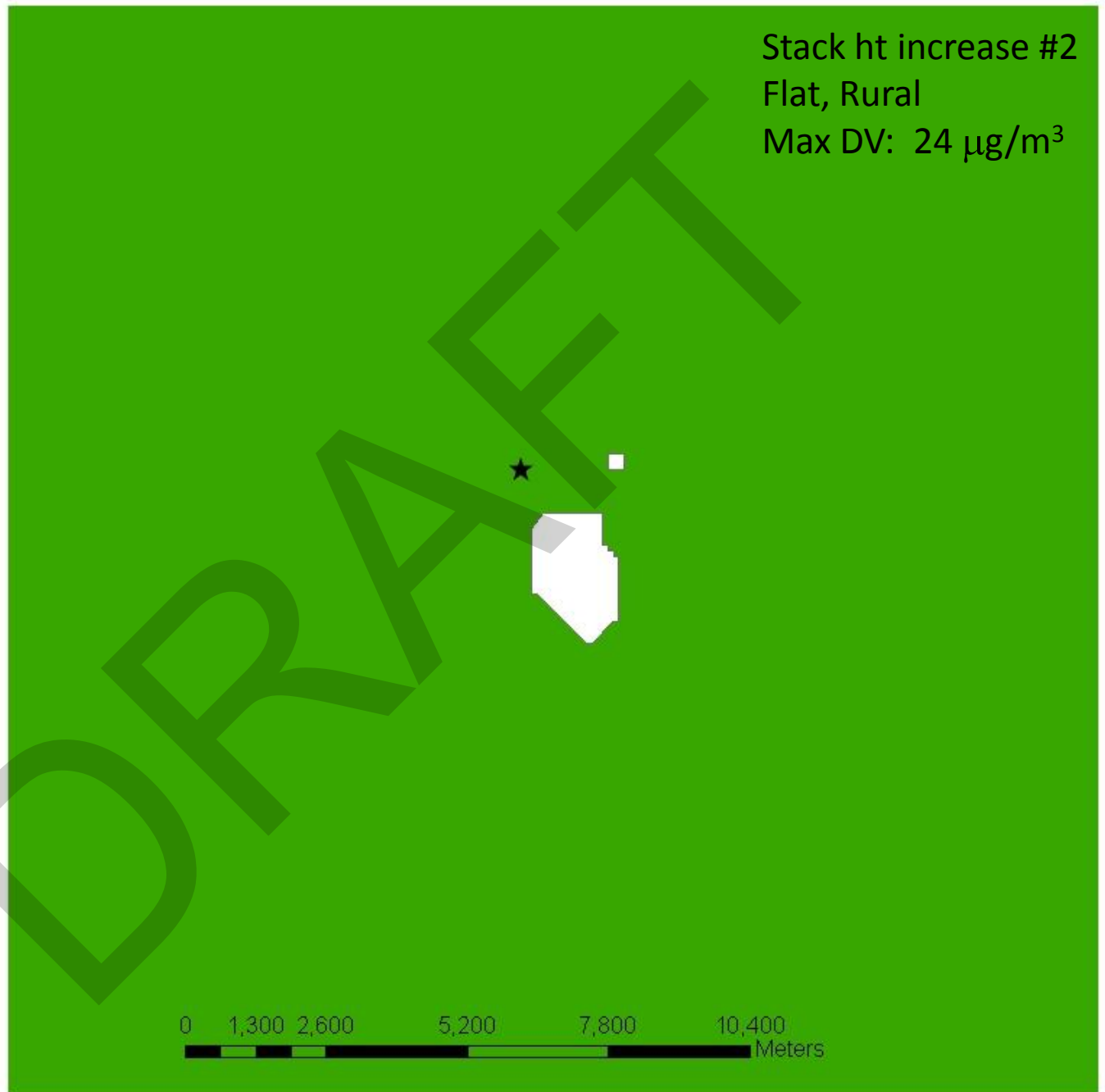
Stack ht increase #1  
Terrain, Urban  
Max DV: 41  $\mu\text{g}/\text{m}^3$



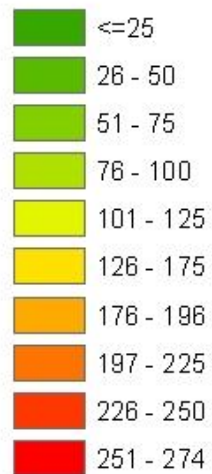
### Legend



Stack ht increase #2  
Flat, Rural  
Max DV: 24  $\mu\text{g}/\text{m}^3$



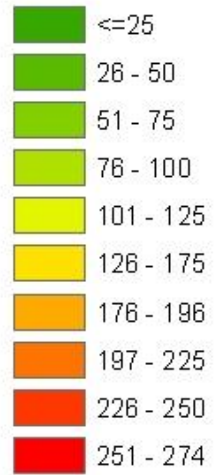
### Legend



Stack ht increase #2  
Flat, Urban  
Max DV:  $36 \mu\text{g}/\text{m}^3$



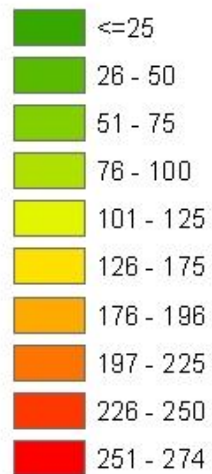
### Legend



Stack ht increase #2  
Terrain, Rural  
Max DV:  $36 \mu\text{g}/\text{m}^3$



### Legend

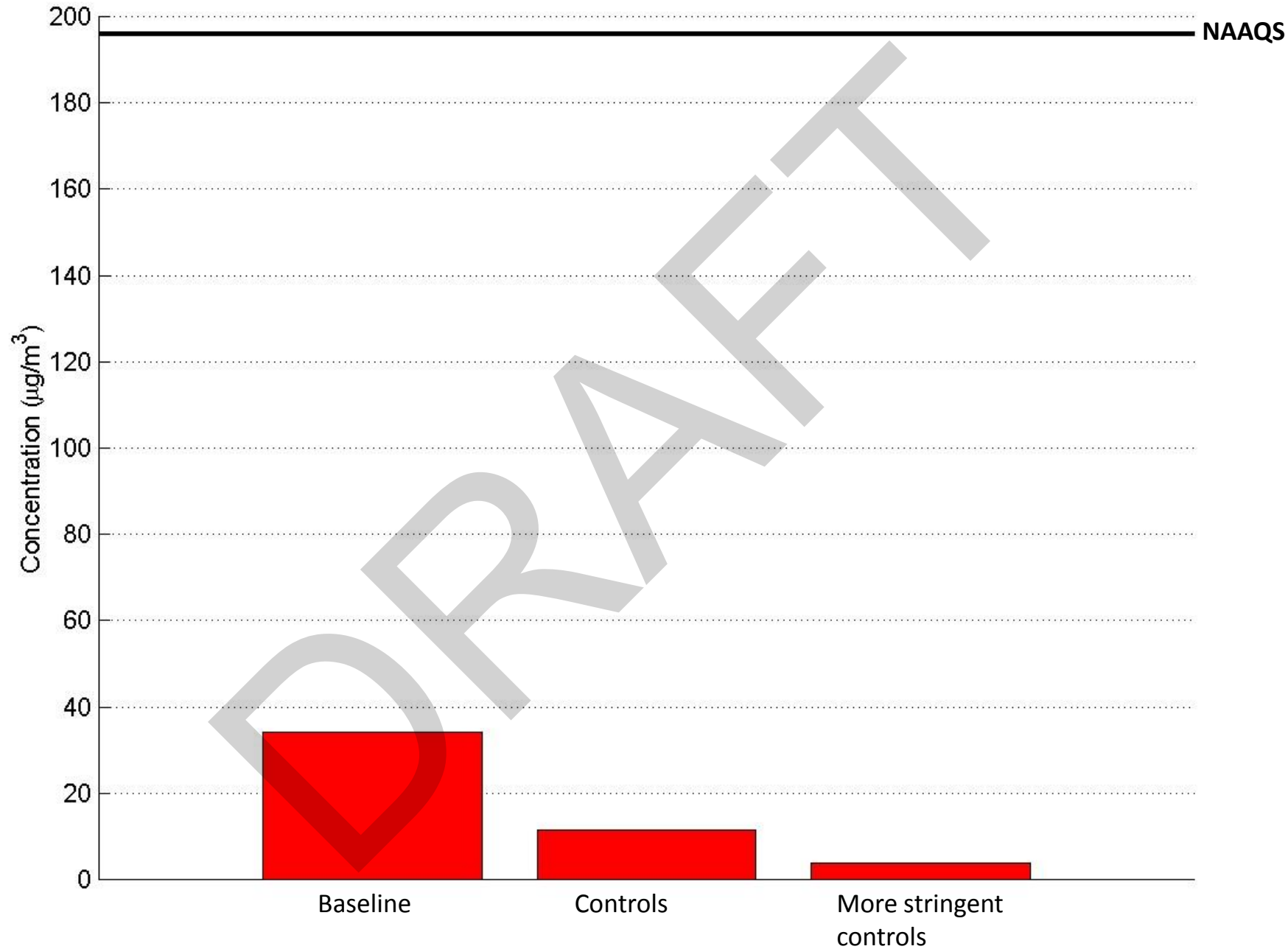


Stack ht increase #2  
Terrain, Urban  
Max DV:  $35 \mu\text{g}/\text{m}^3$



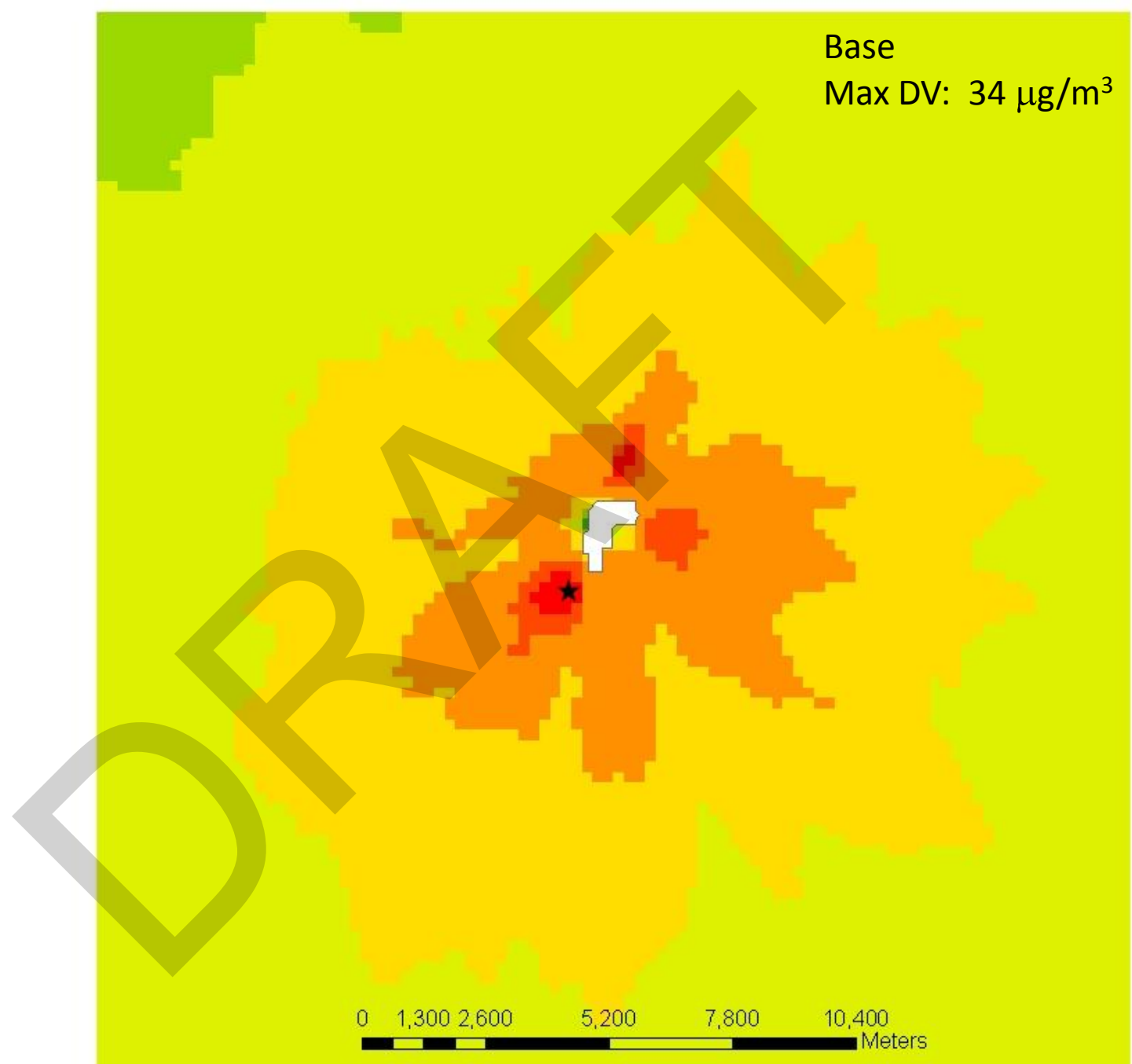
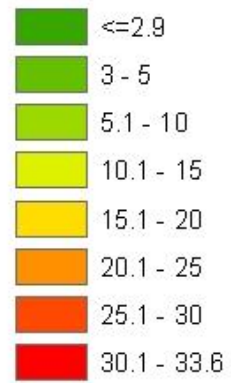


# Cement Kiln: SO<sub>2</sub>



Base  
Max DV: 34  $\mu\text{g}/\text{m}^3$

### Legend

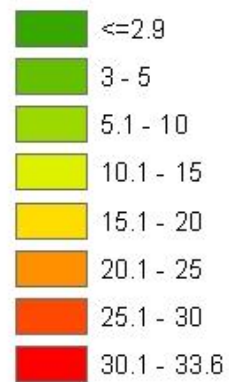


0 1,300 2,600 5,200 7,800 10,400  
Meters

Controls

Max DV: 11  $\mu\text{g}/\text{m}^3$

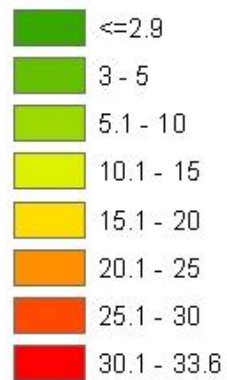
### Legend



0 1,300 2,600 5,200 7,800 10,400 Meters

More stringent controls  
Max DV: 4  $\mu\text{g}/\text{m}^3$

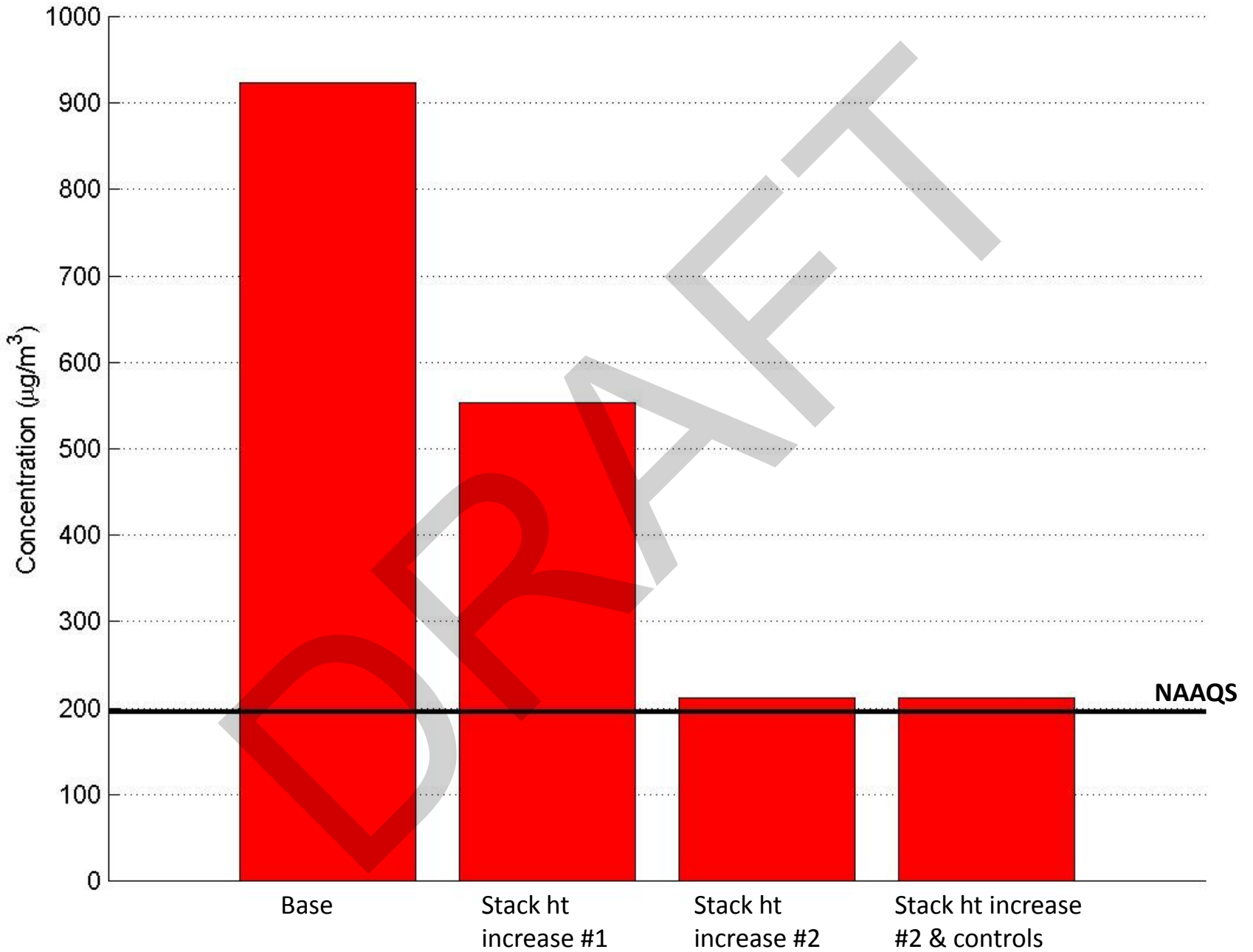
### Legend



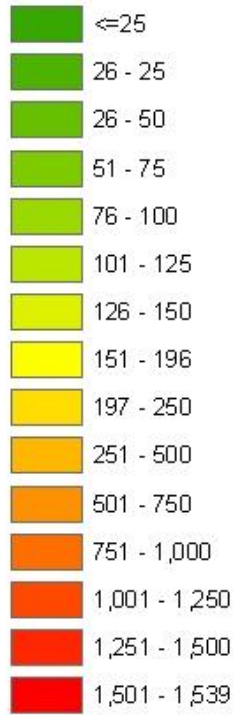
0 1,300 2,600 5,200 7,800 10,400  
Meters



# Pulp & paper: SO<sub>2</sub>

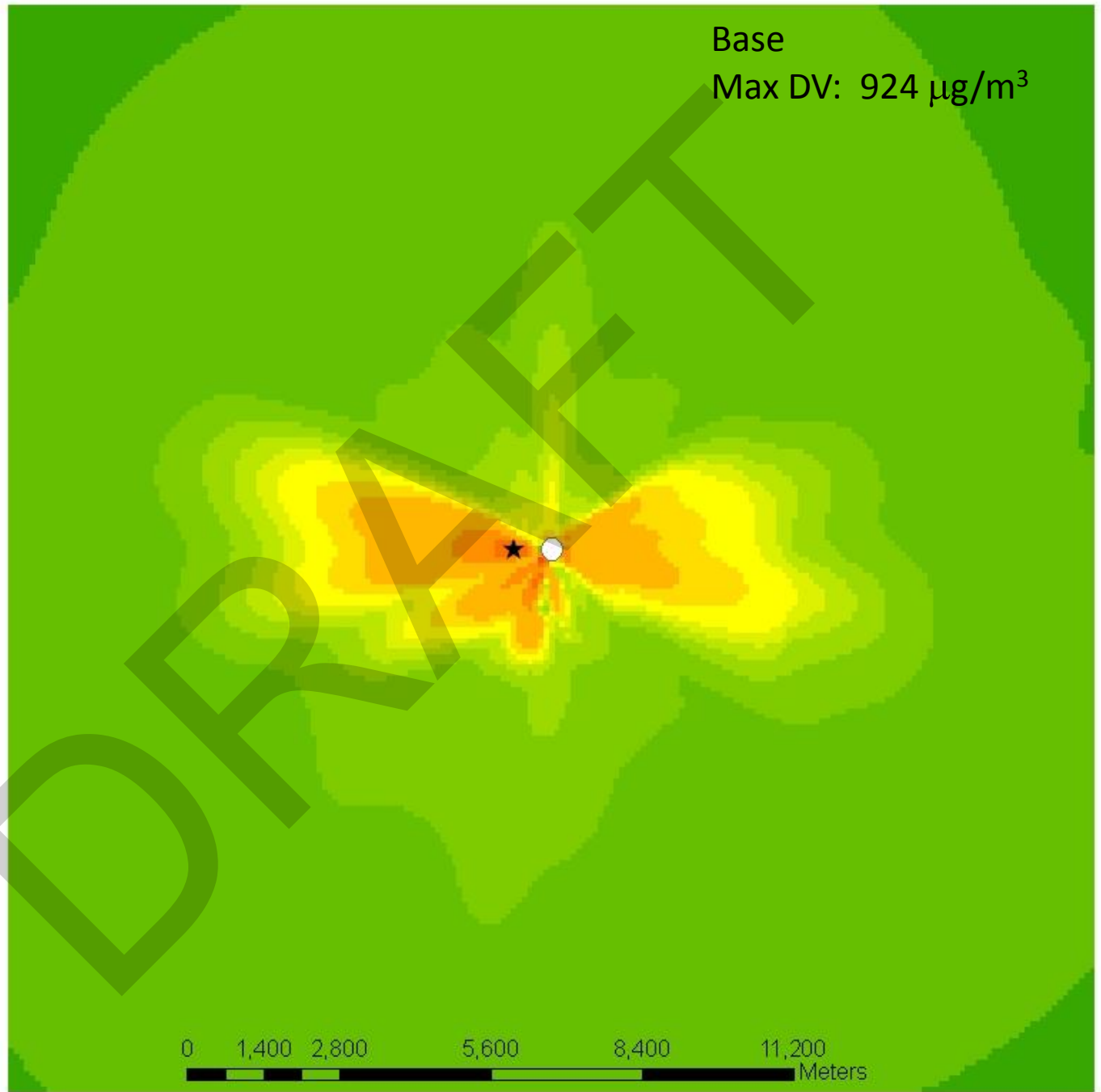


# Legend



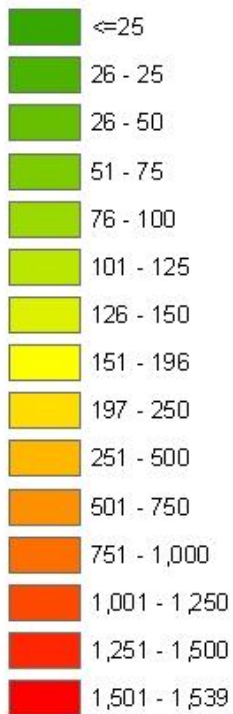
Base

Max DV: 924  $\mu\text{g}/\text{m}^3$

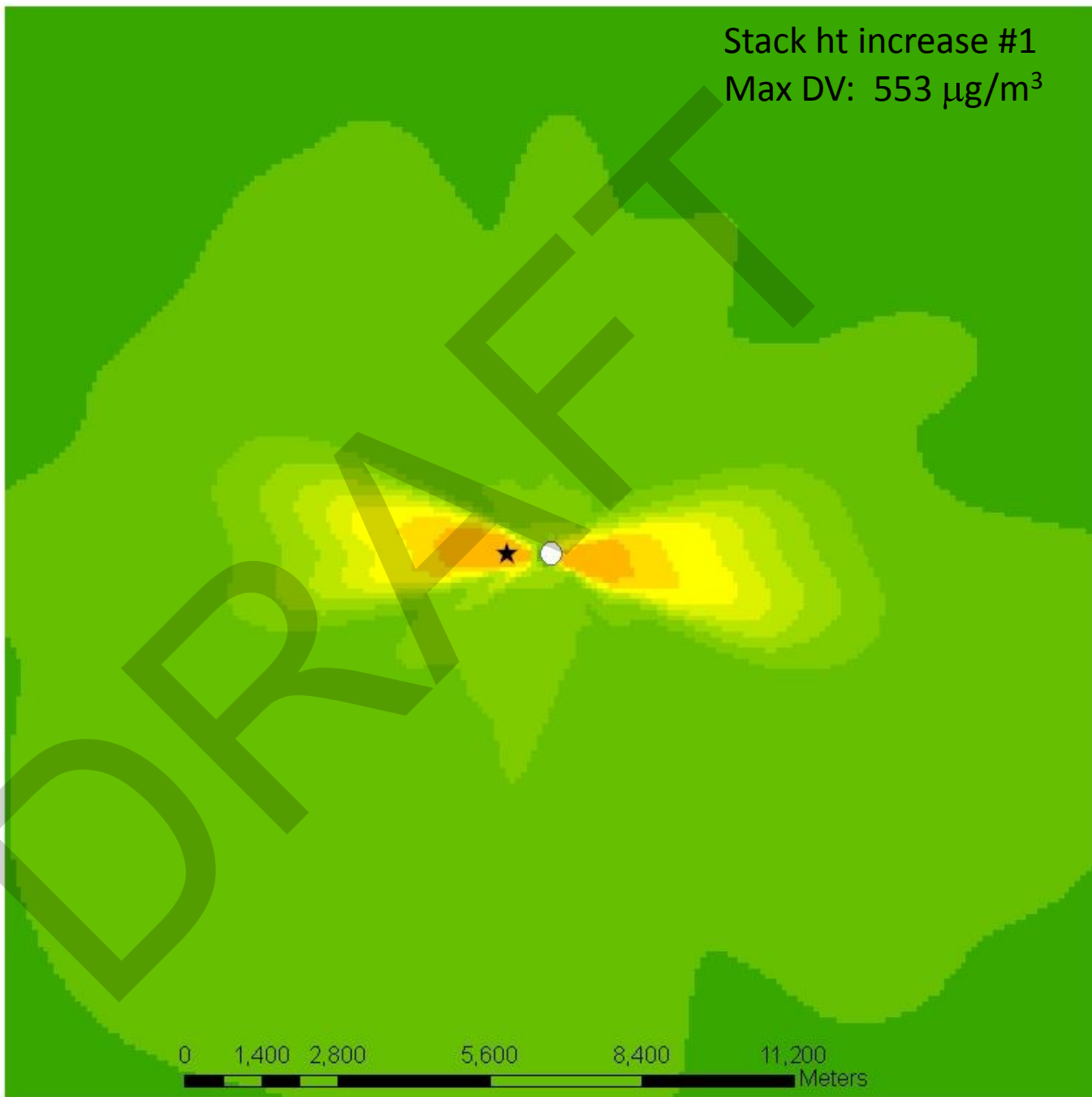


0 1,400 2,800 5,600 8,400 11,200 Meters

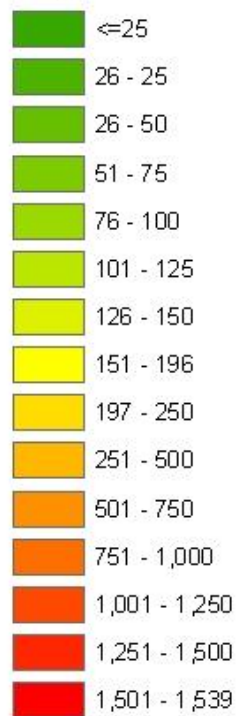
### Legend



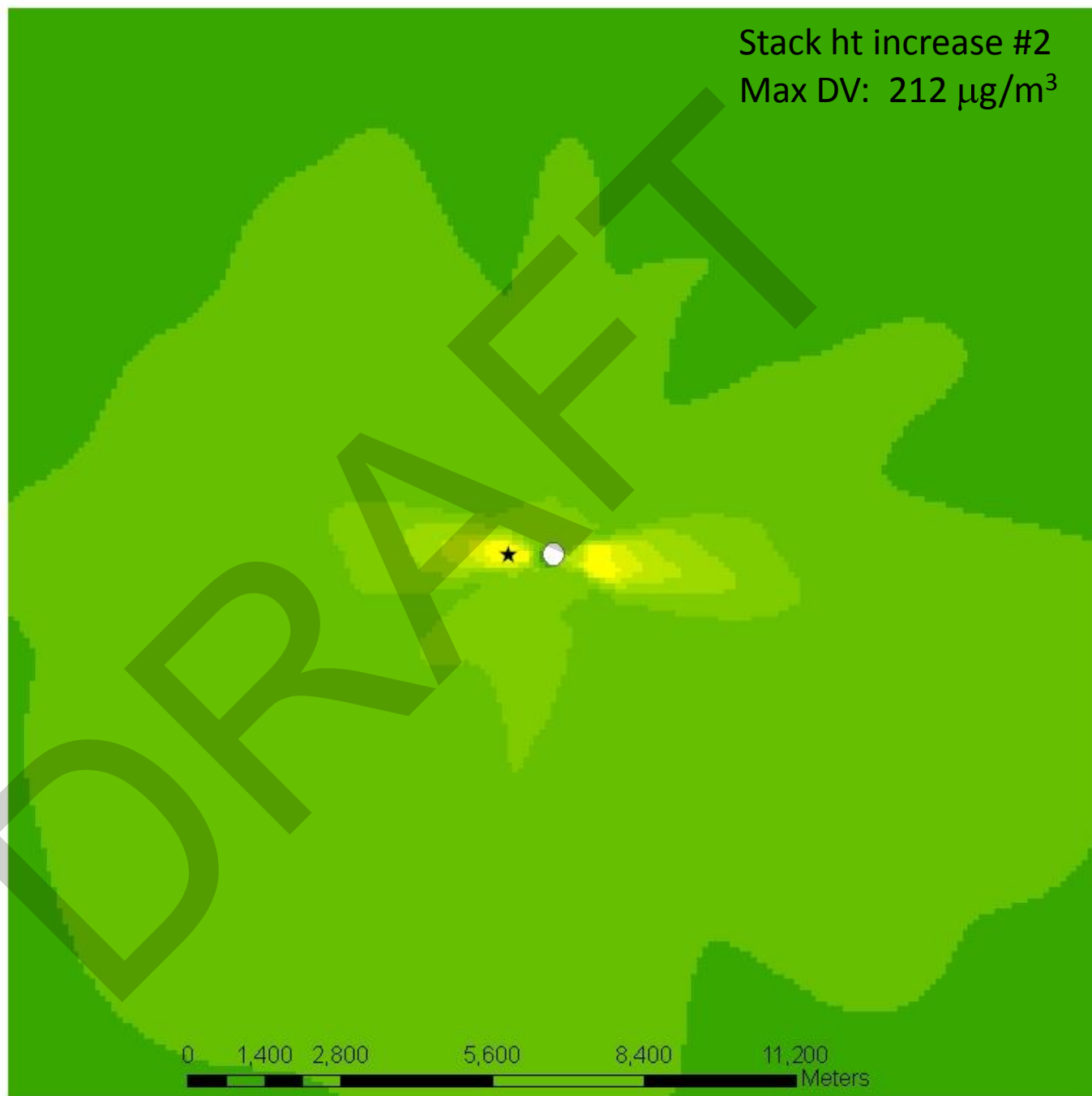
Stack ht increase #1  
Max DV: 553  $\mu\text{g}/\text{m}^3$



### Legend

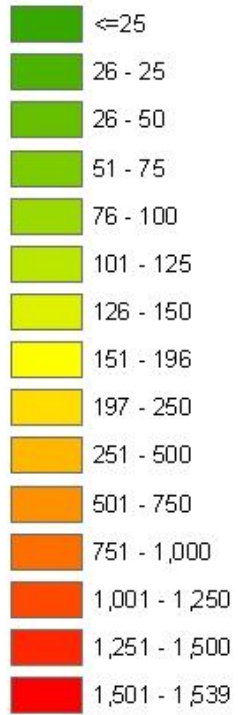


Stack ht increase #2  
Max DV: 212  $\mu\text{g}/\text{m}^3$

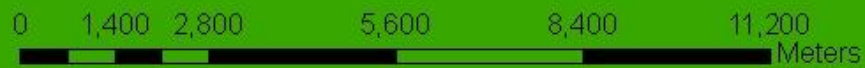
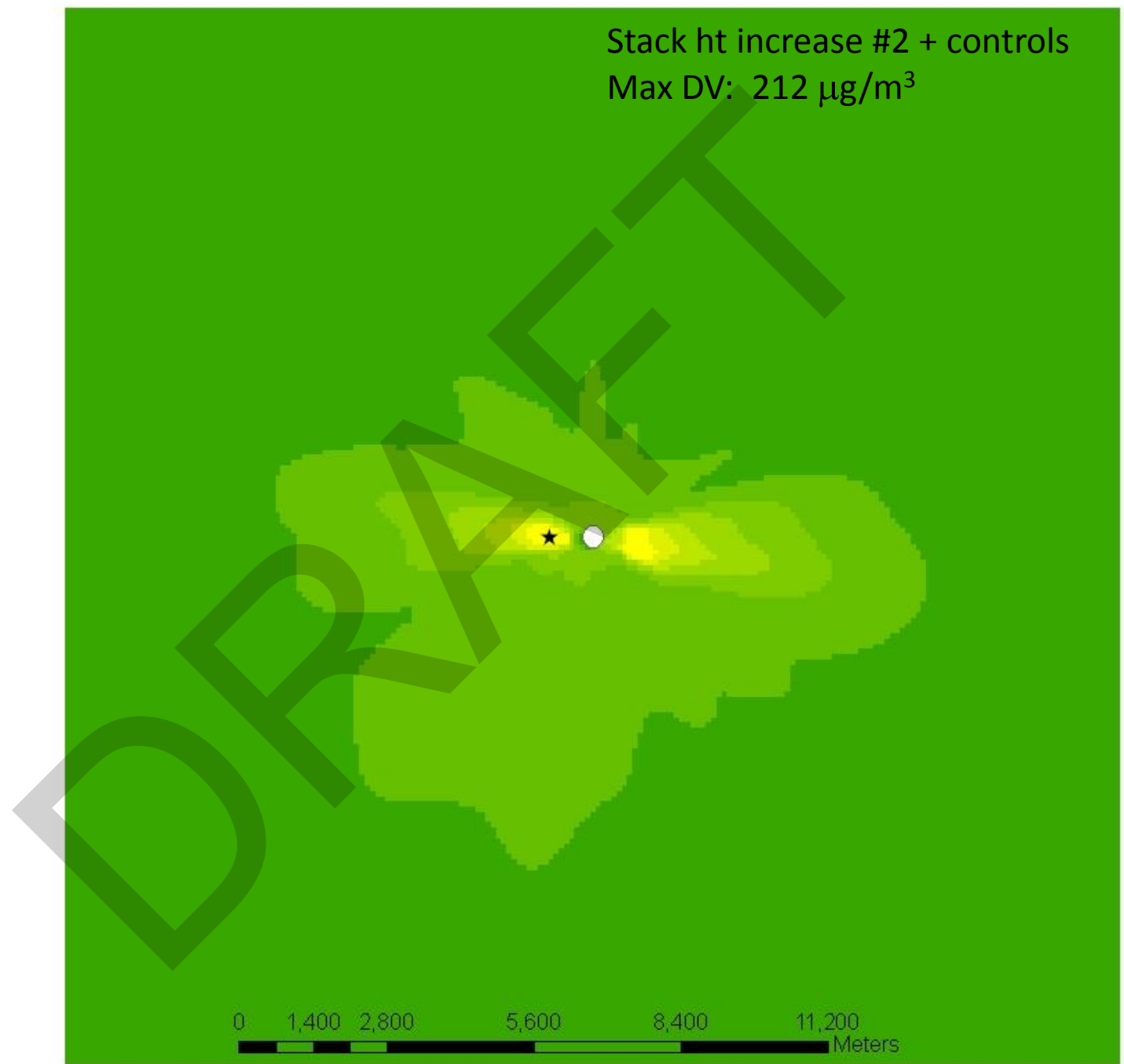




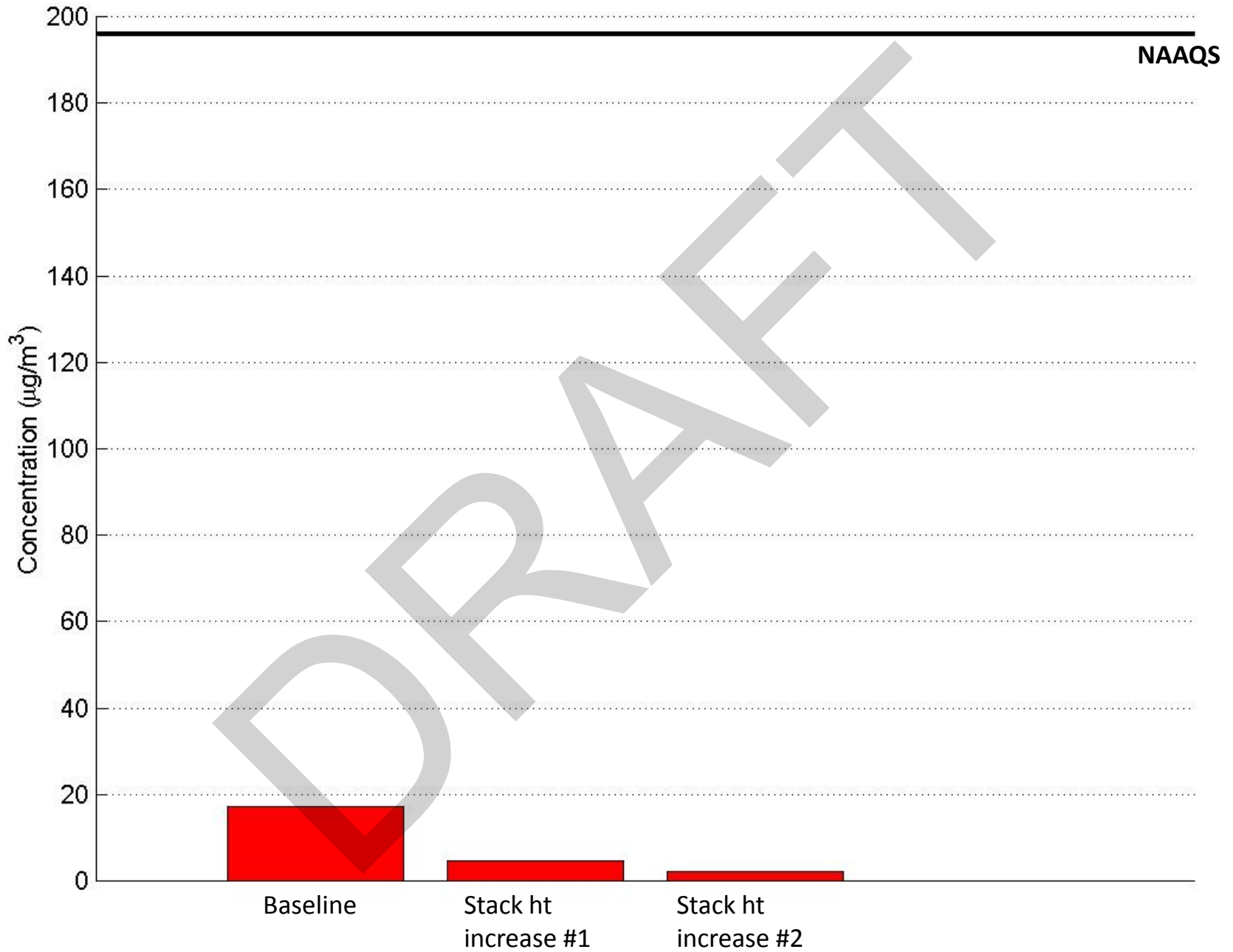
# Legend



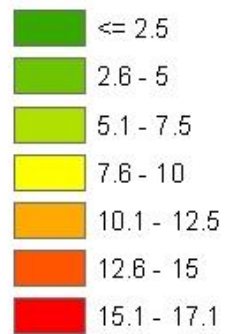
Stack ht increase #2 + controls  
Max DV: 212  $\mu\text{g}/\text{m}^3$



# Landfill Gas Turbine: SO<sub>2</sub>



### Legend



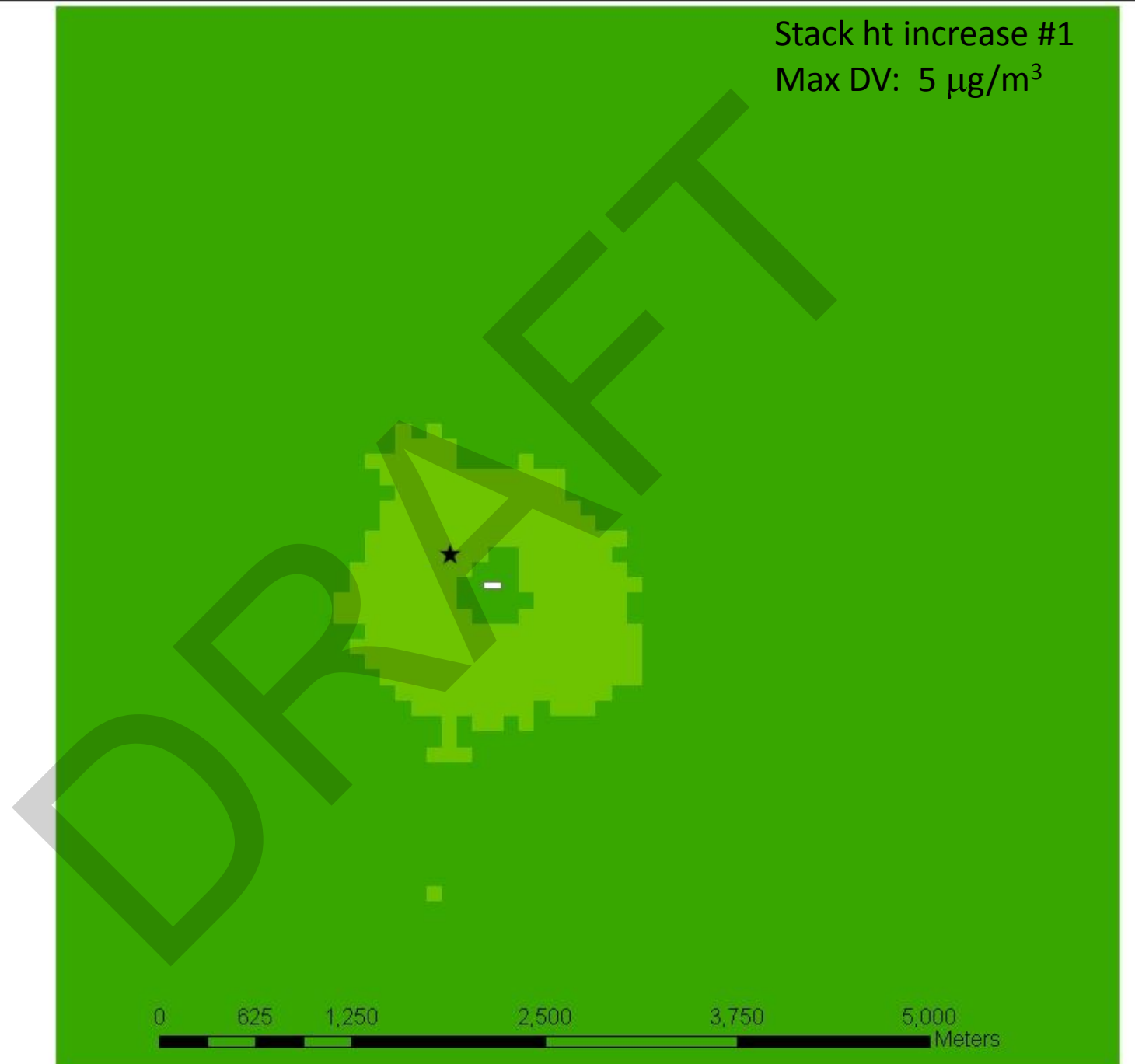
Base  
Max DV: 17  $\mu\text{g}/\text{m}^3$

0 625 1,250 2,500 3,750 5,000 Meters

A horizontal scale bar with alternating black and white segments, corresponding to the numerical values above it.

Stack ht increase #1  
Max DV: 5  $\mu\text{g}/\text{m}^3$

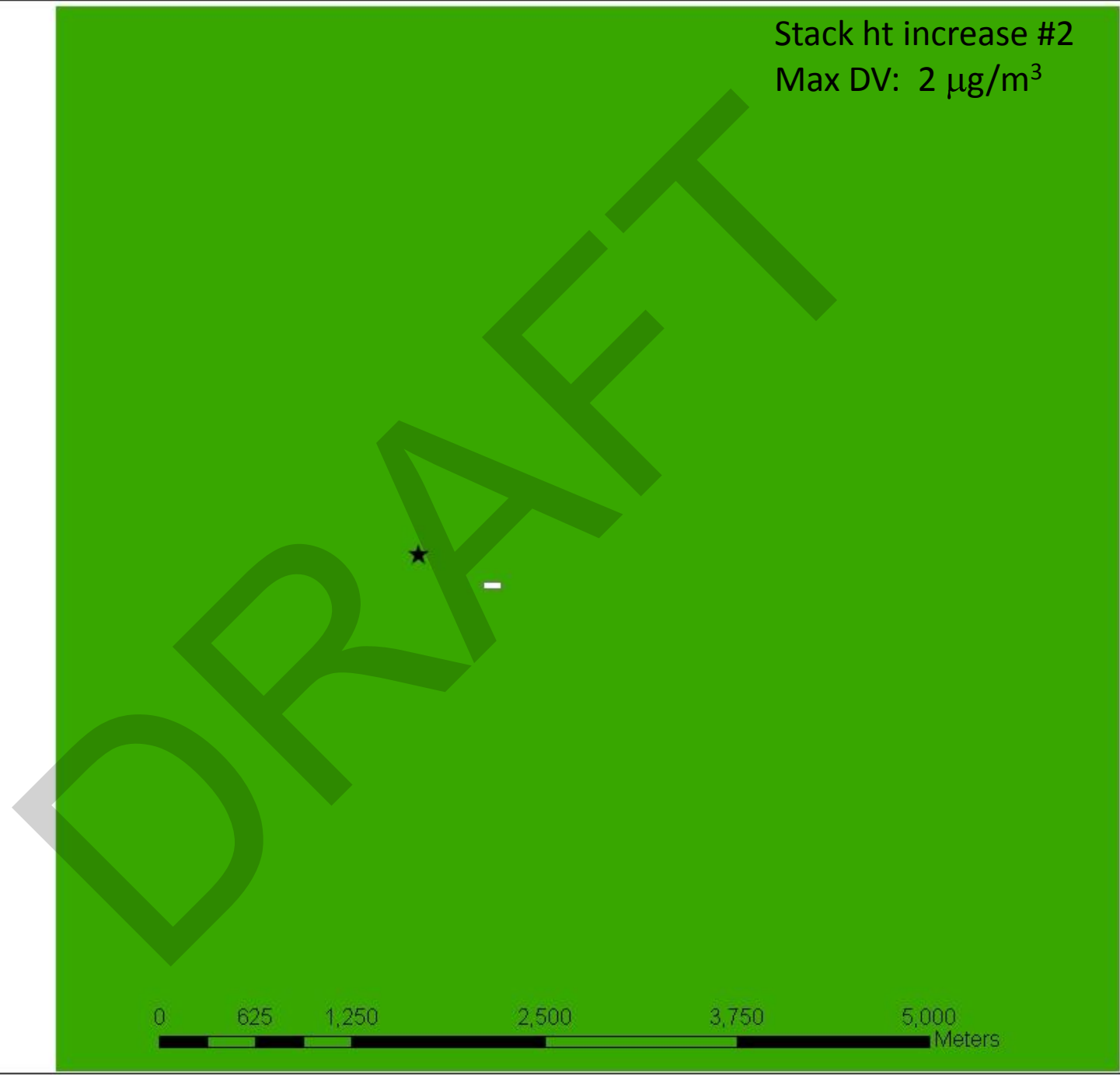
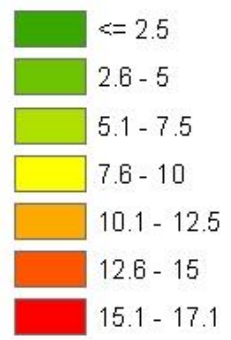
### Legend



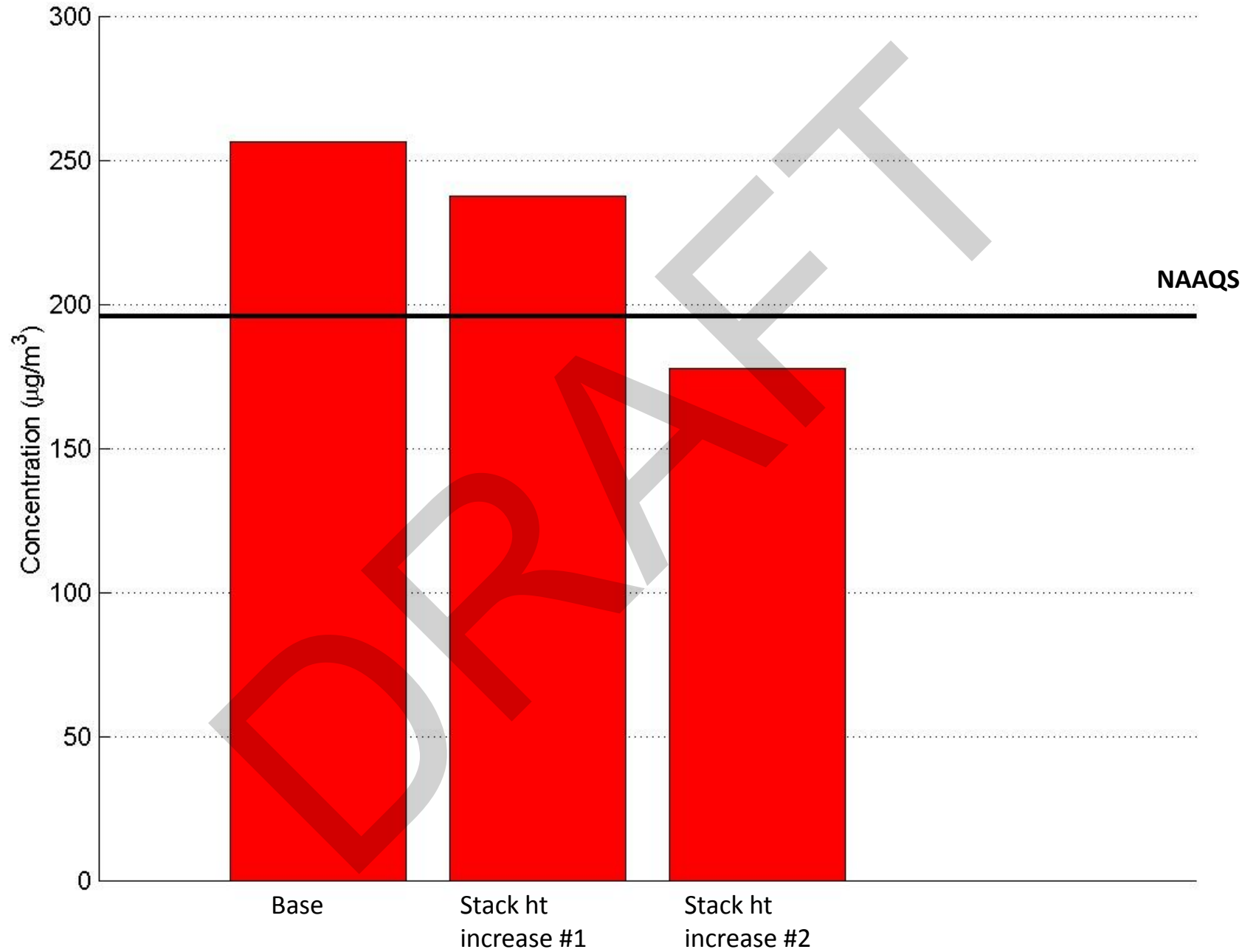
0 625 1,250 2,500 3,750 5,000 Meters

Stack ht increase #2  
Max DV: 2  $\mu\text{g}/\text{m}^3$

**Legend**

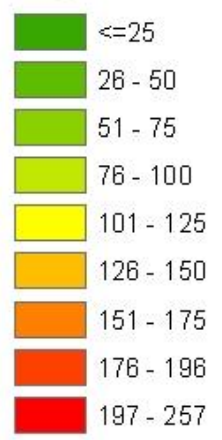


# Fuel Oil Turbine: SO<sub>2</sub>



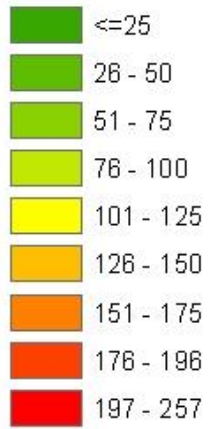
Baseline  
Max DV: 257  $\mu\text{g}/\text{m}^3$

**Legend**



Stack ht increase #1  
Max DV: 238  $\mu\text{g}/\text{m}^3$

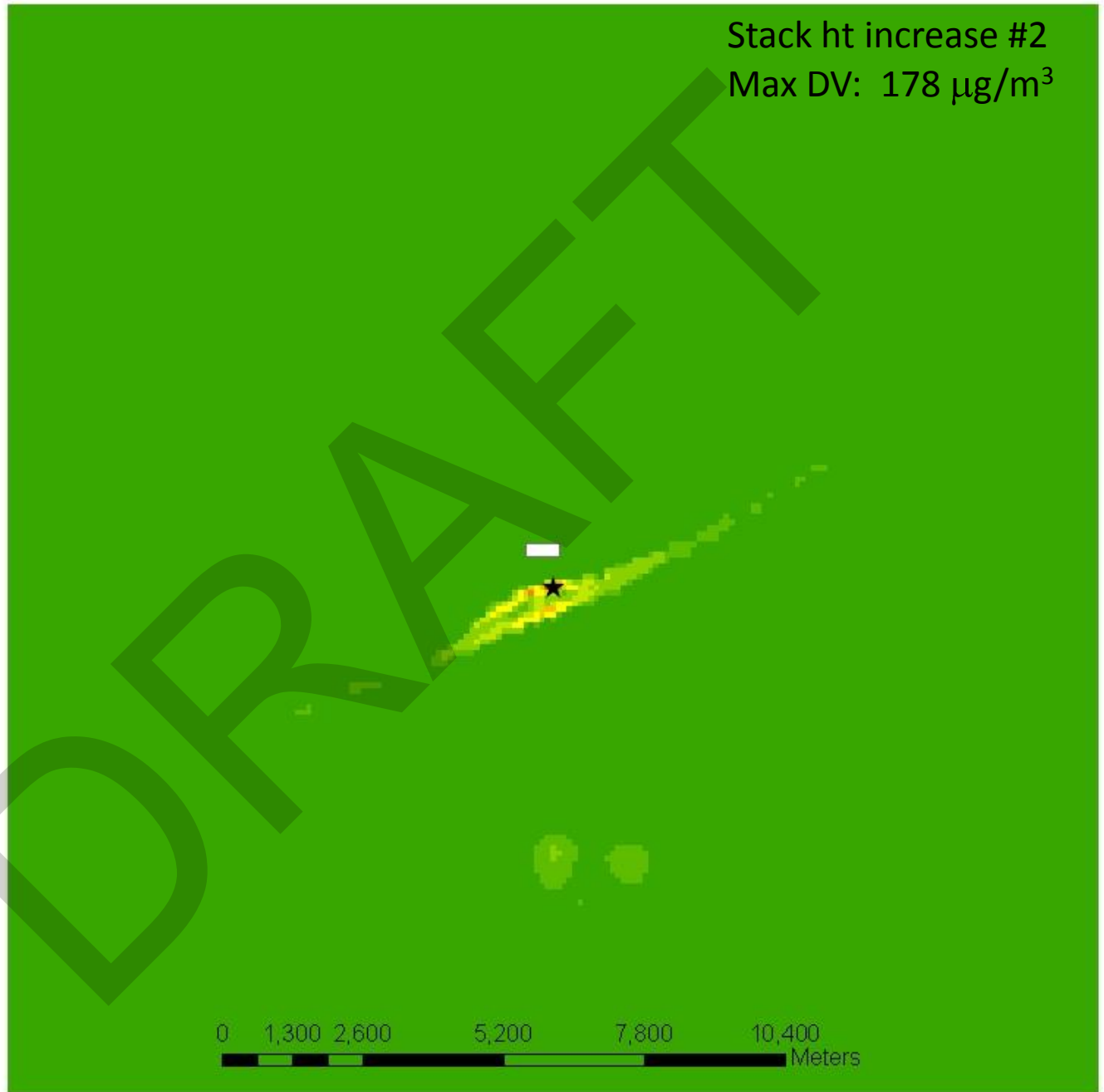
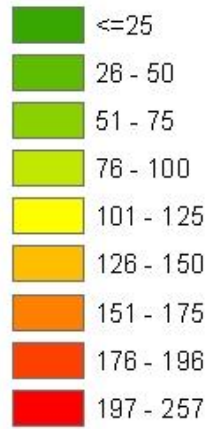
**Legend**



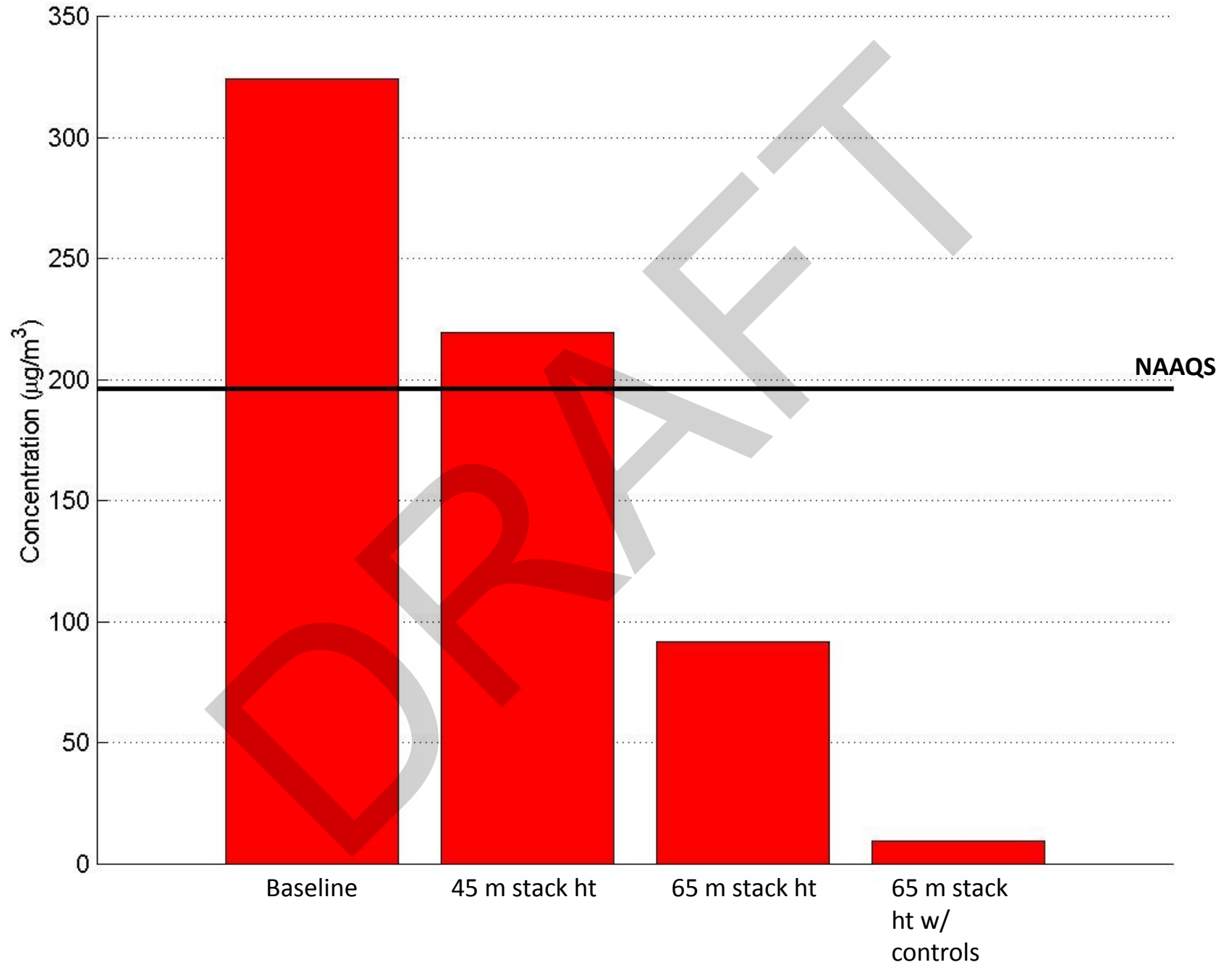


Stack ht increase #2  
Max DV: 178  $\mu\text{g}/\text{m}^3$

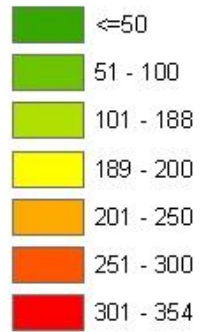
**Legend**



# Flare: SO<sub>2</sub>

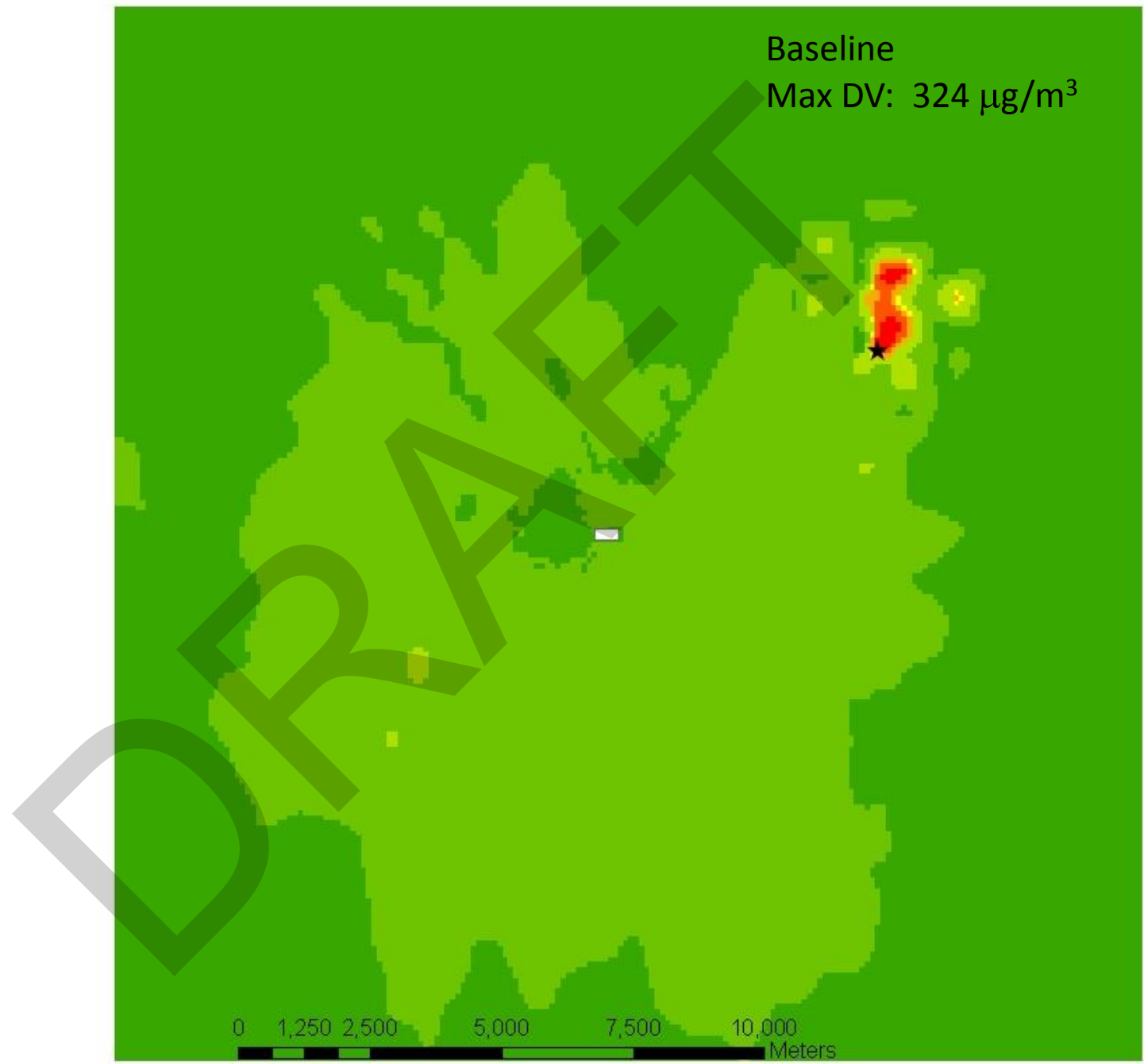


### Legend



Baseline

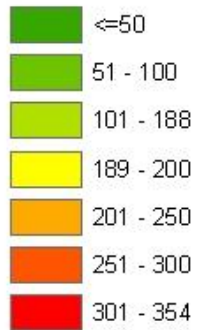
Max DV: 324 µg/m<sup>3</sup>



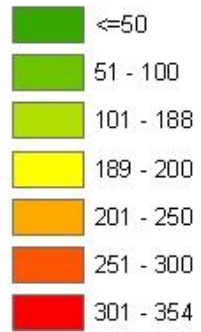
0 1,250 2,500 5,000 7,500 10,000 Meters

Stack ht increase to 45  
Max DV: 219  $\mu\text{g}/\text{m}^3$

### Legend



### Legend

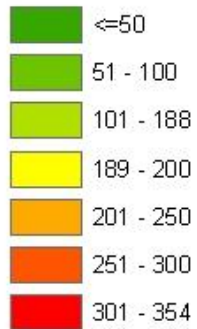


Stack ht increase to 65  
Max DV: 92  $\mu\text{g}/\text{m}^3$

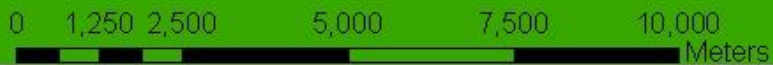


Stack ht increase to 65 + controls  
Max DV: 9  $\mu\text{g}/\text{m}^3$

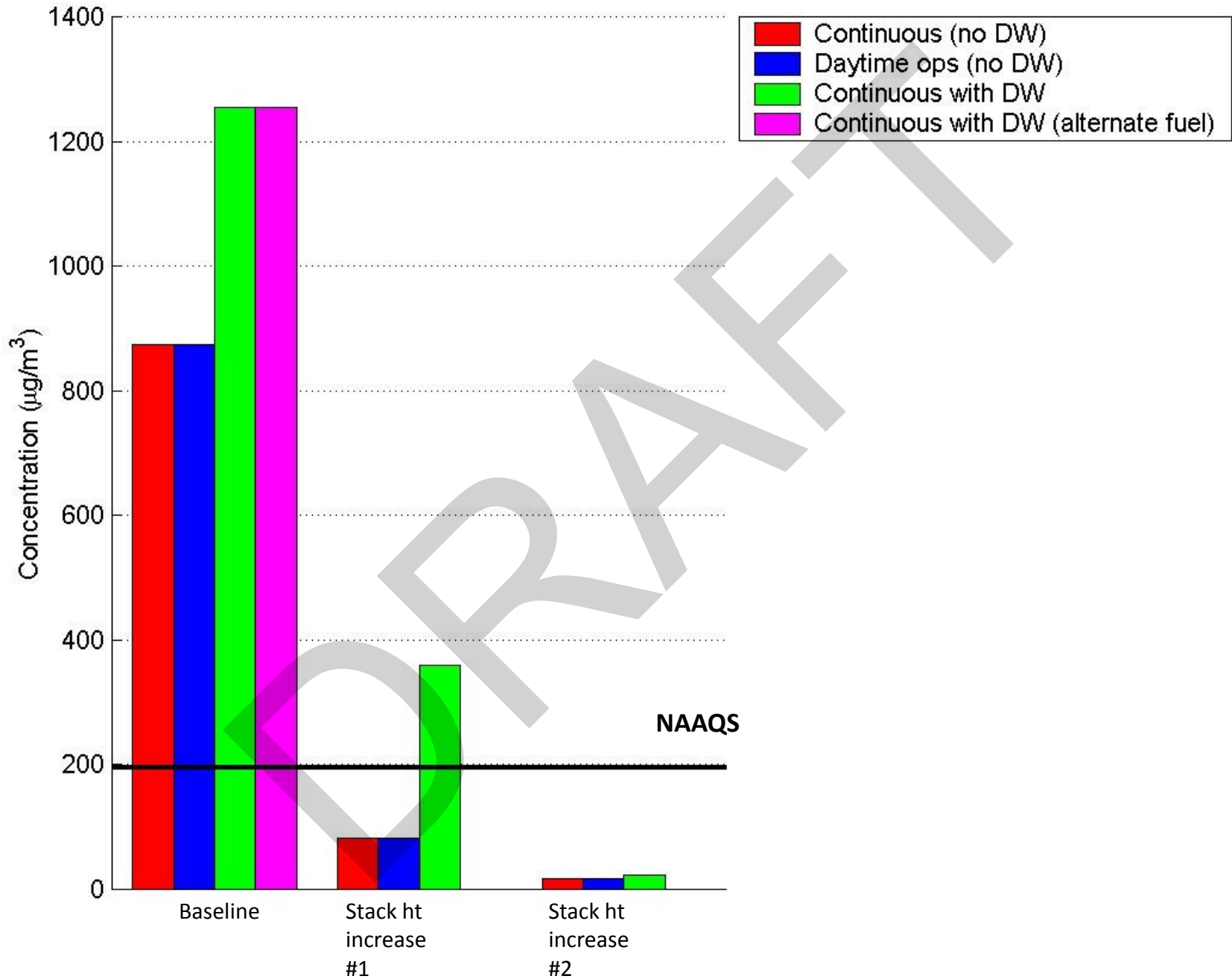
**Legend**



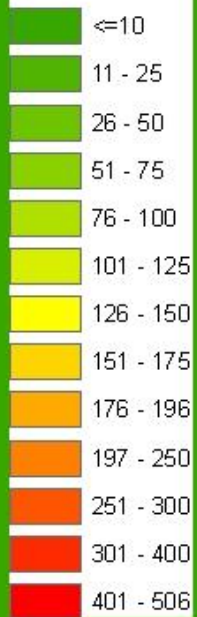
DRAFT



# Asphalt Plant (Alva): SO<sub>2</sub>



**Legend**

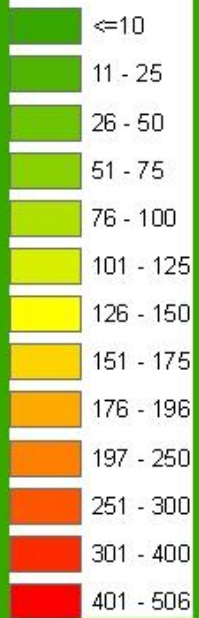


Base  
Continuous operations  
No downwash  
Max DV: 874  $\mu\text{g}/\text{m}^3$





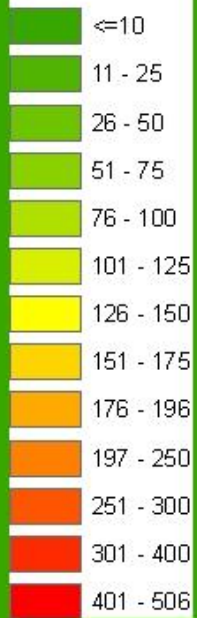
### Legend



Base  
Daytime operations  
No downwash  
Max DV:  $874 \mu\text{g}/\text{m}^3$



### Legend

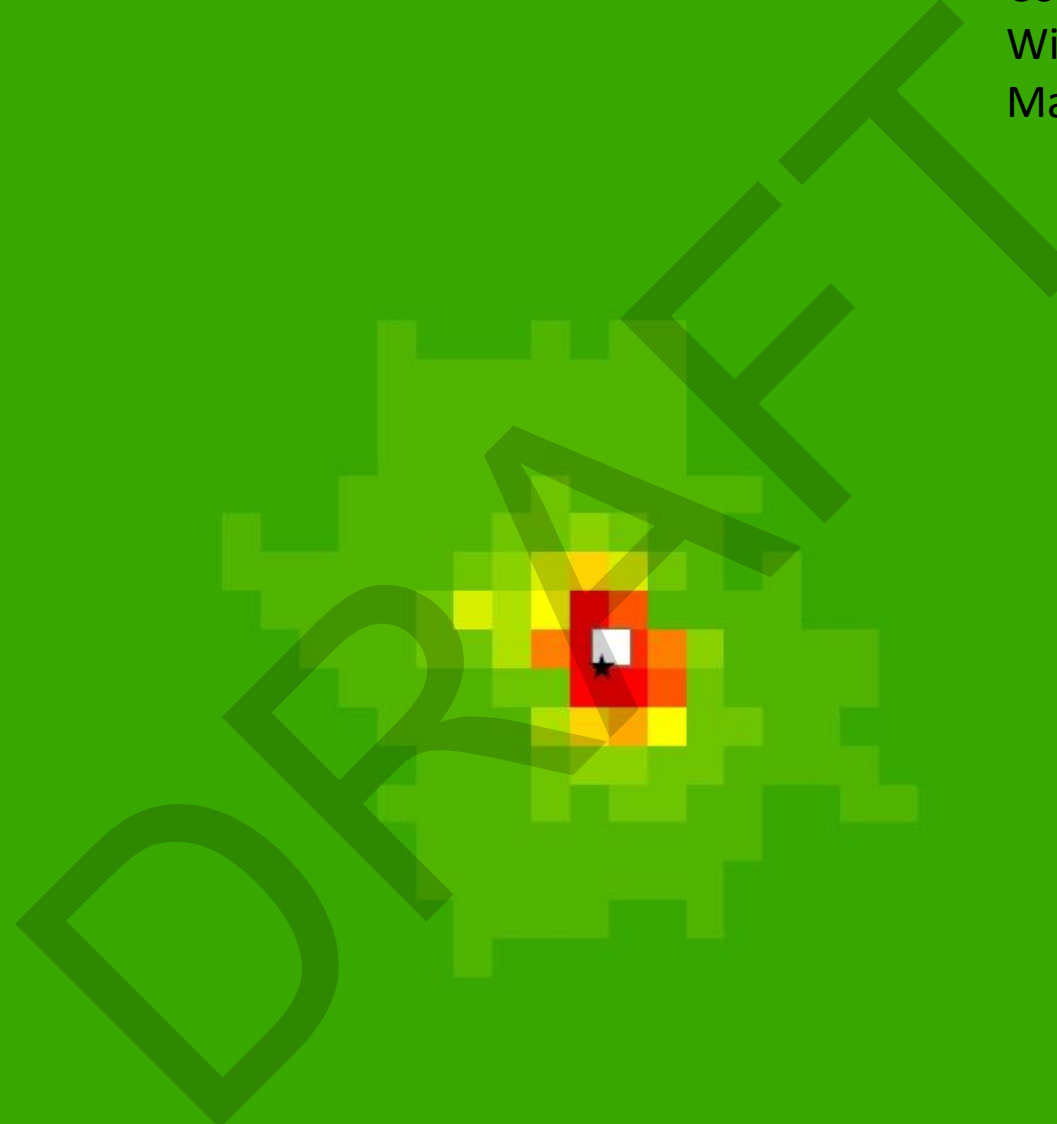


Base

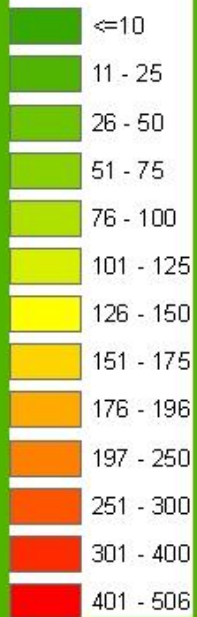
Continuous operations

With downwash

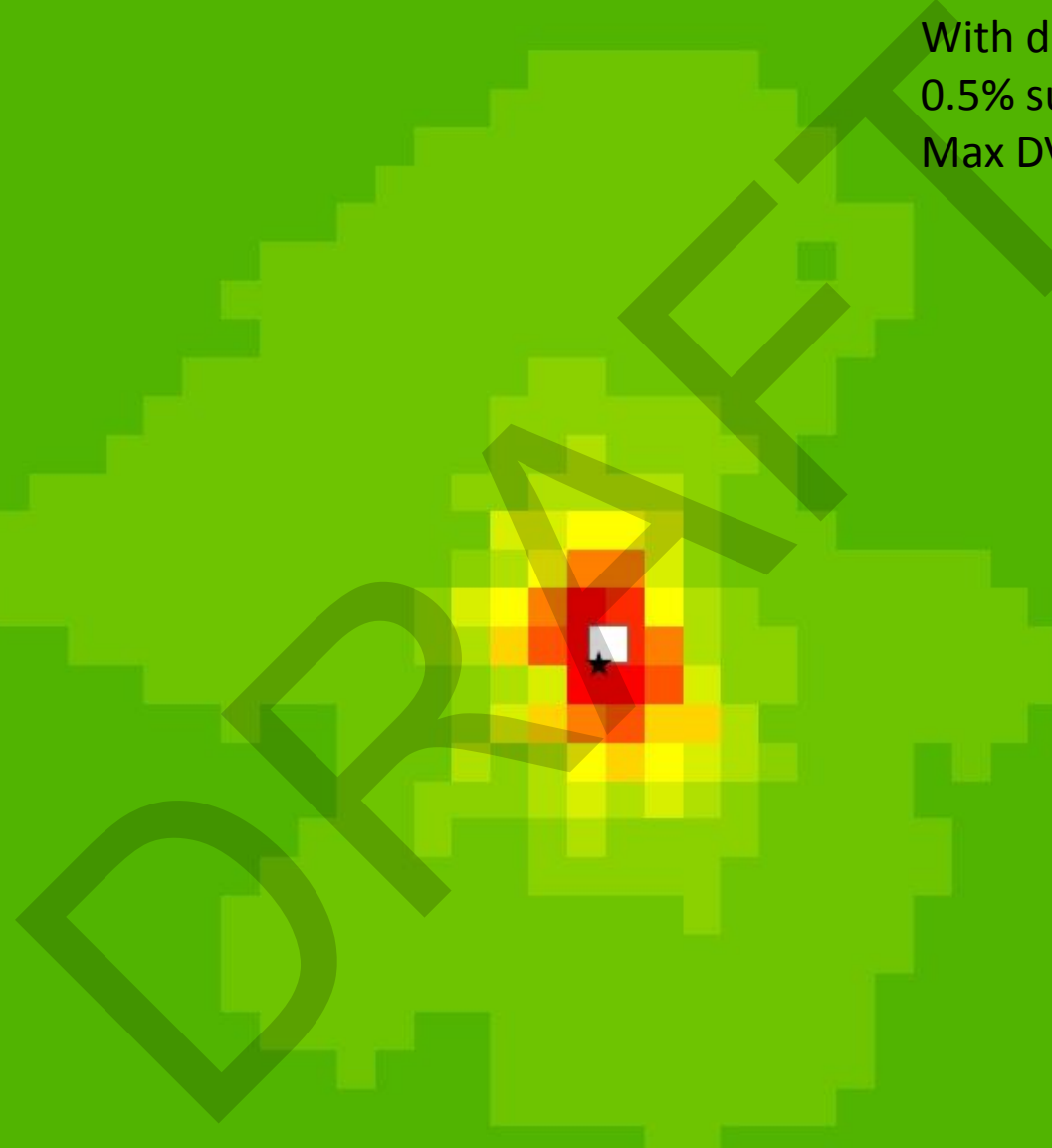
Max DV: 1254  $\mu\text{g}/\text{m}^3$



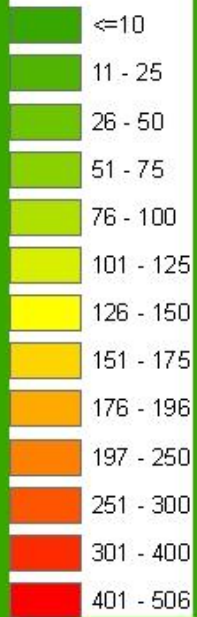
**Legend**



Base  
Continuous operations  
With downwash  
0.5% sulfur content fuel oil  
Max DV: 1255  $\mu\text{g}/\text{m}^3$



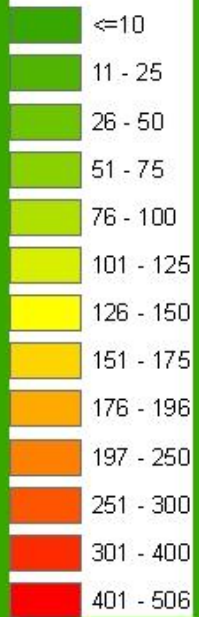
**Legend**



Stack ht increase #1  
Continuous operations  
No downwash  
Max DV: 82  $\mu\text{g}/\text{m}^3$



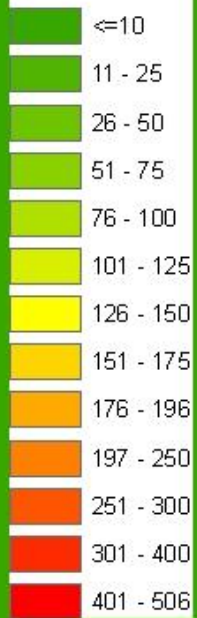
### Legend



Stack ht increase #1  
Daytime operations  
No downwash  
Max DV: 82  $\mu\text{g}/\text{m}^3$



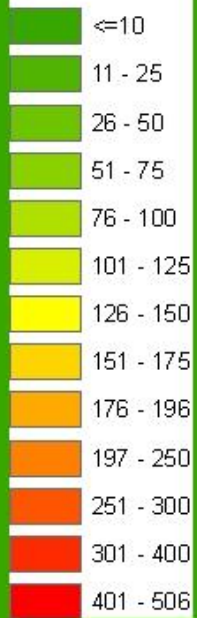
### Legend



Stack ht increase #1  
Continuous operations  
With downwash  
Max DV: 359  $\mu\text{g}/\text{m}^3$



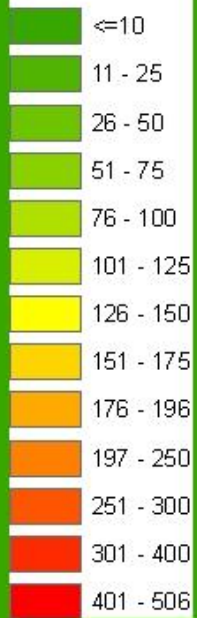
### Legend



Stack ht increase #2  
Continuous operations  
No downwash  
Max DV:  $17 \mu\text{g}/\text{m}^3$



### Legend



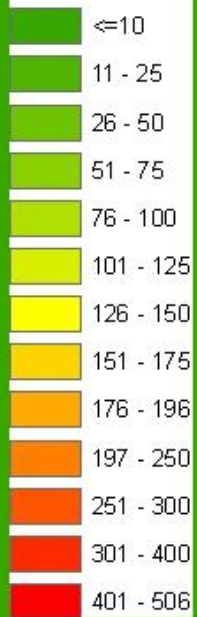
Stack ht increase #2  
Daytime operations  
No downwash  
Max DV:  $17 \mu\text{g}/\text{m}^3$

DRRAFT





**Legend**

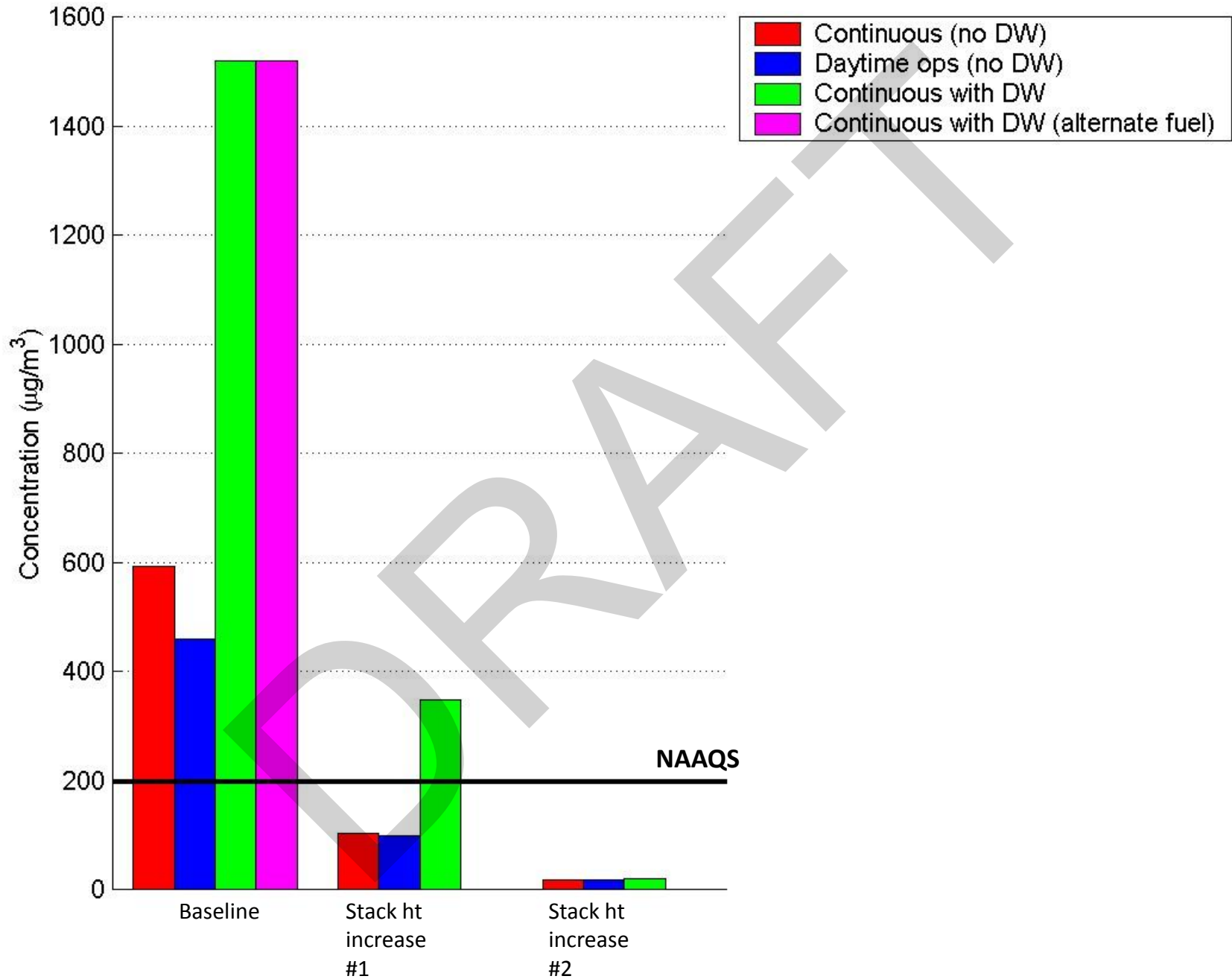


Stack ht increase #2  
Continuous operations  
With downwash  
Max DV: 23  $\mu\text{g}/\text{m}^3$

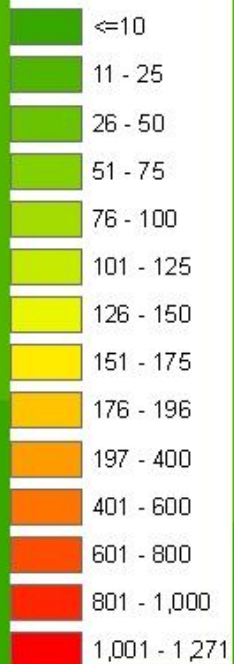
DRRAFT



# Asphalt Plant (Boise): SO<sub>2</sub>



### Legend



Base

Continuous operations

No downwash

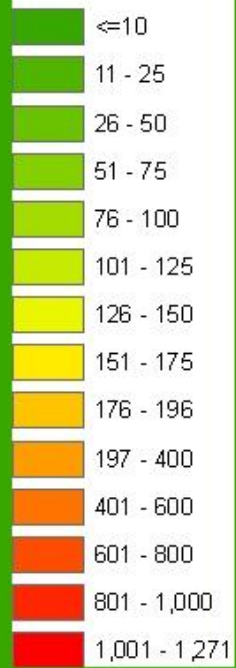
Max DV: 592  $\mu\text{g}/\text{m}^3$

DRAFT



Boise

# Legend

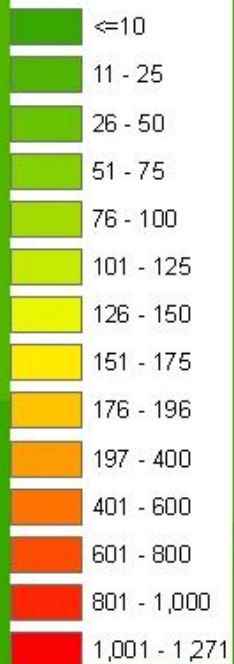


Base  
Daytime operations  
No downwash  
Max DV: 460  $\mu\text{g}/\text{m}^3$



Boise

### Legend



Base

Continuous operations

With downwash

Max DV:  $1520 \mu\text{g}/\text{m}^3$

DRIFT

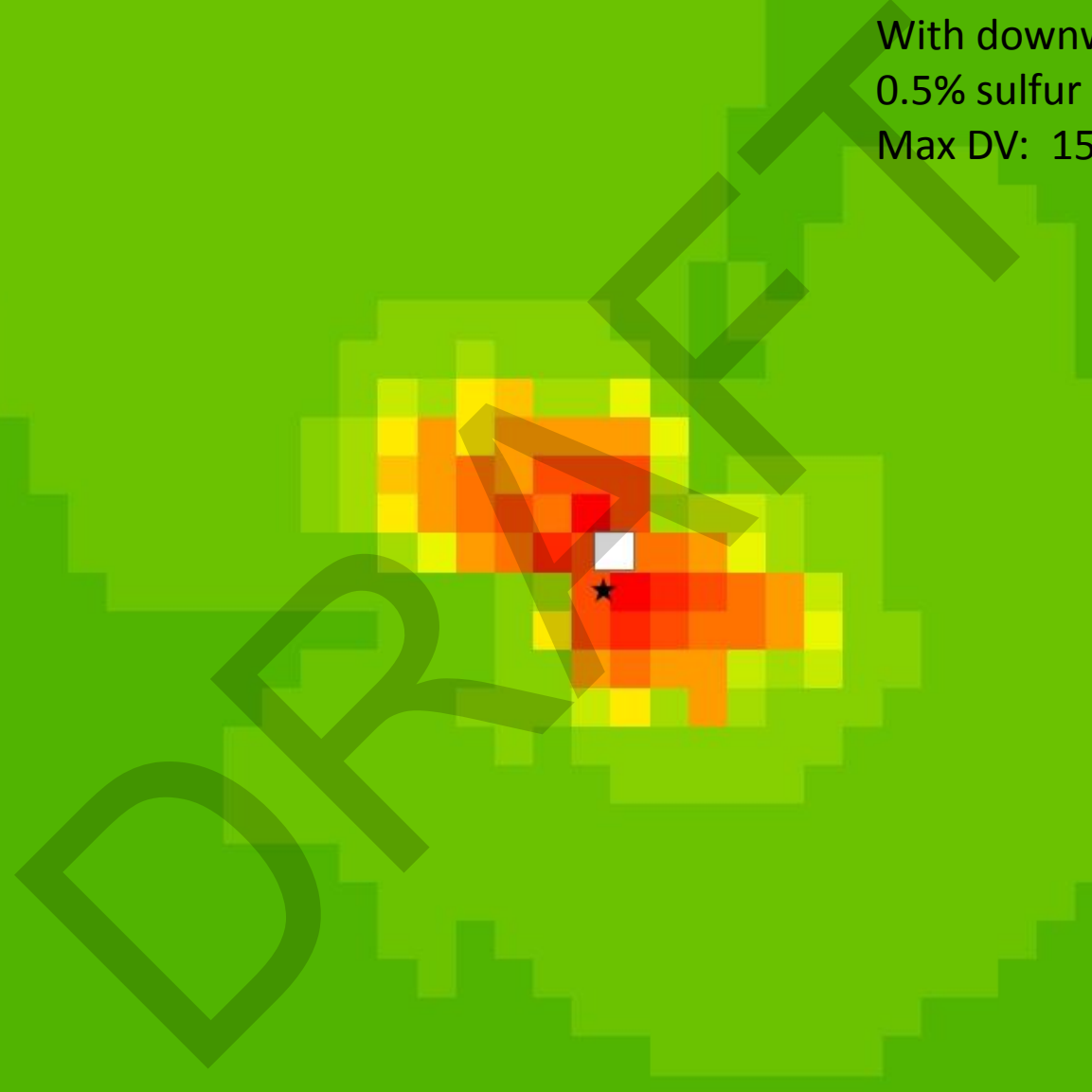


Boise

### Legend

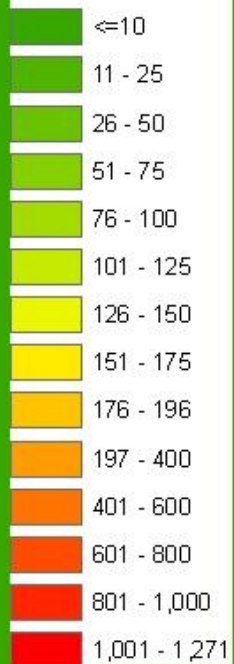


Base  
Continuous operations  
With downwash  
0.5% sulfur content fuel oil  
Max DV: 1520  $\mu\text{g}/\text{m}^3$



Boise

### Legend

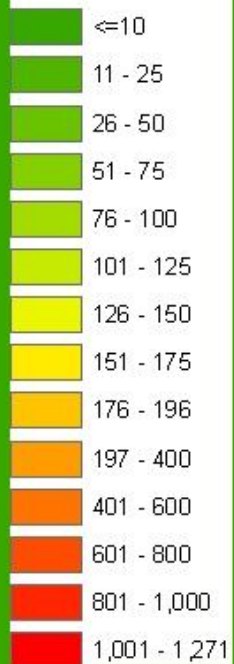


Stack ht increase #1  
Continuous operations  
No downwash  
Max DV: 102  $\mu\text{g}/\text{m}^3$



Boise

### Legend



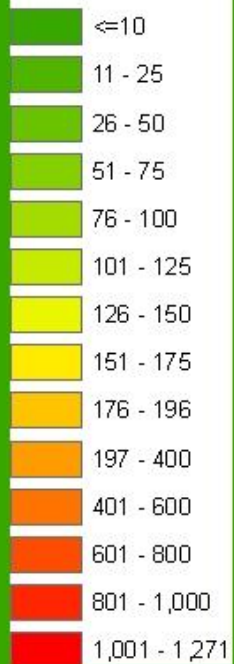
Stack ht increase #1  
Daytime operations  
No downwash  
Max DV:  $98 \mu\text{g}/\text{m}^3$



Boise



### Legend

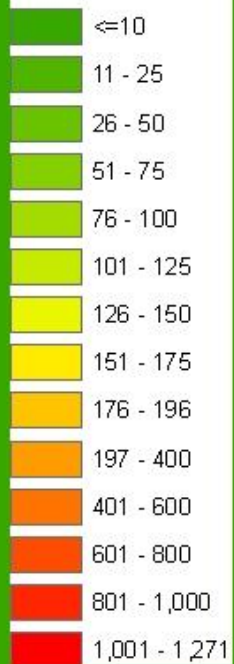


Stack ht increase #1  
Continuous operations  
With downwash  
Max DV: 347  $\mu\text{g}/\text{m}^3$



Boise

### Legend



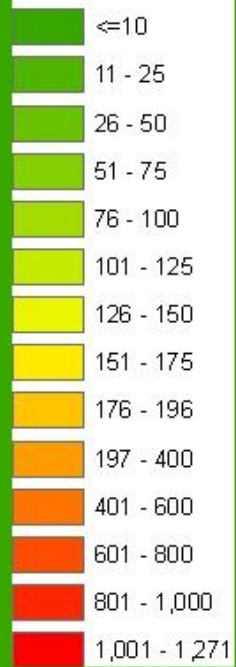
Stack ht increase #2  
Continuous operations  
No downwash  
Max DV: 17  $\mu\text{g}/\text{m}^3$

DRAGNET



Boise

### Legend



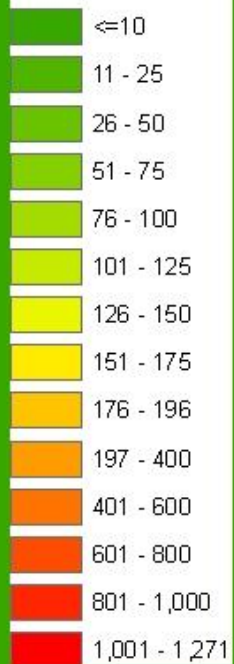
Stack ht increase #2  
Daytime operations  
No downwash  
Max DV: 17  $\mu\text{g}/\text{m}^3$

DRAFT



Boise

### Legend



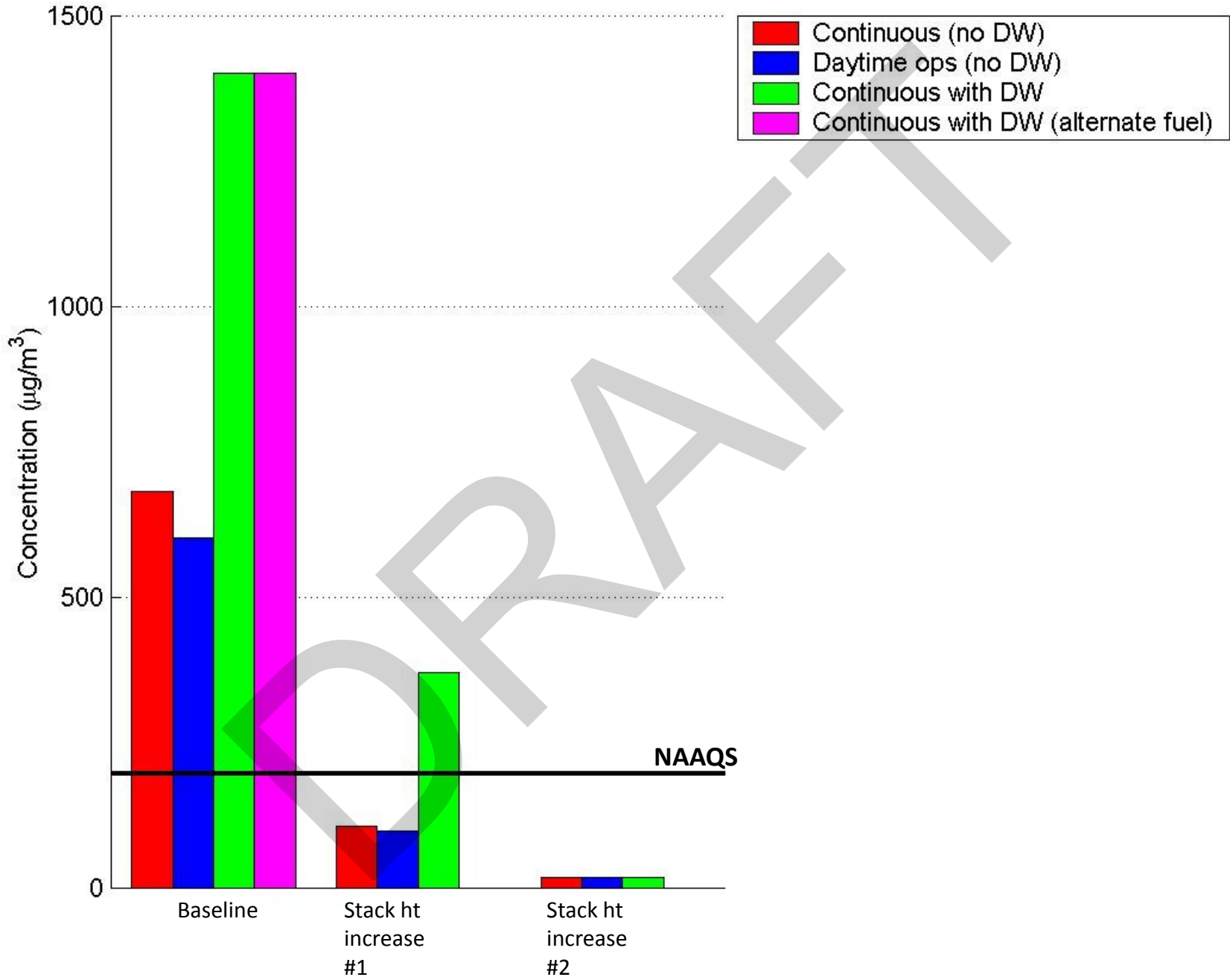
Stack ht increase #2  
Continuous operations  
With downwash  
Max DV:  $19 \mu\text{g}/\text{m}^3$

DRAFT

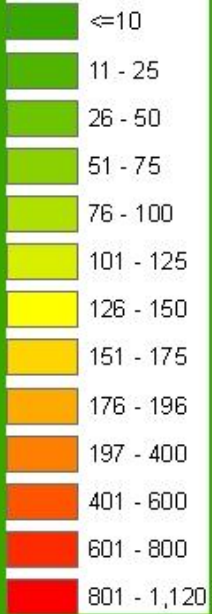


Boise

# Asphalt Plant (Empire Abo): SO<sub>2</sub>



**Legend**



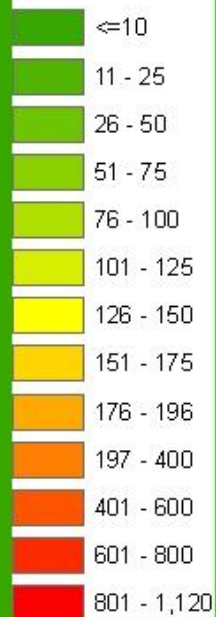
Base  
Continuous operations  
No downwash  
Max DV: 681  $\mu\text{g}/\text{m}^3$

DRAFT



Empire Abo

### Legend



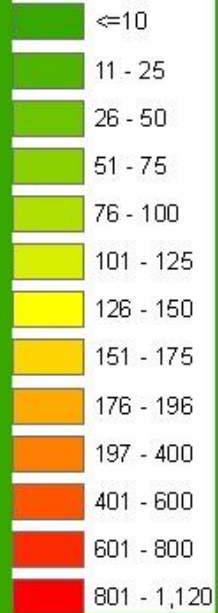
Base  
Daytime operations  
No downwash  
Max DV: 602  $\mu\text{g}/\text{m}^3$

DRAFT



Empire Abo

### Legend



Base  
Continuous operations  
With downwash  
Max DV: 1401  $\mu\text{g}/\text{m}^3$

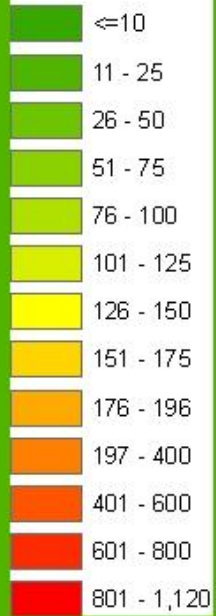
DRYFET



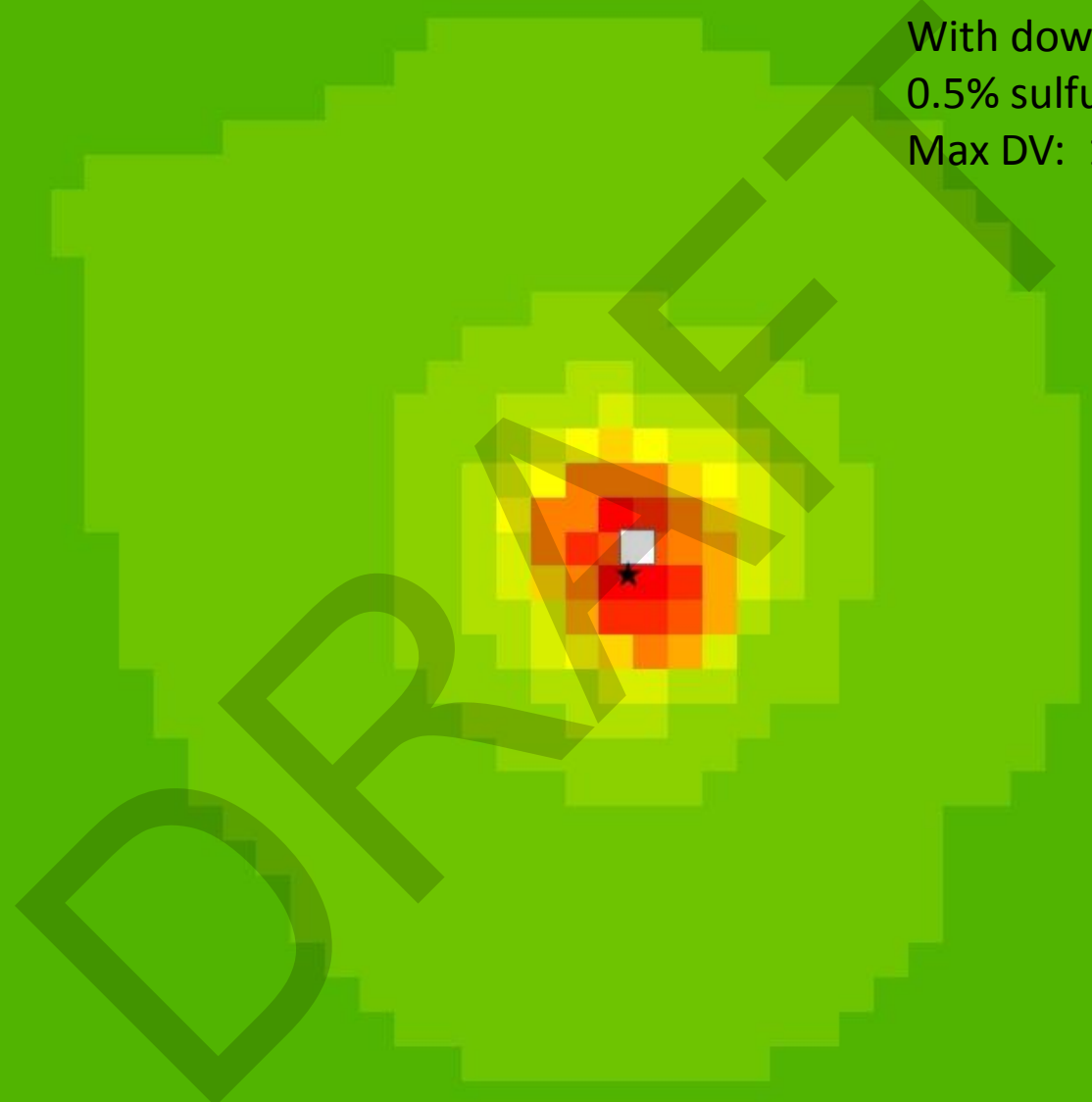
Empire Abo



### Legend

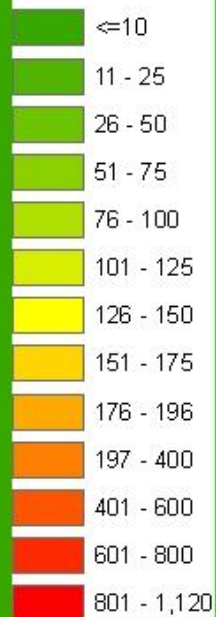


Base  
Continuous operations  
With downwash  
0.5% sulfur content fuel oil  
Max DV:  $1401 \mu\text{g}/\text{m}^3$



Empire Abo

**Legend**

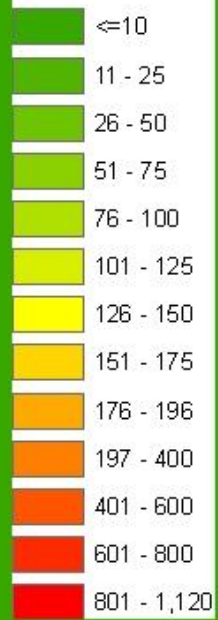


Stack ht increase #1  
Continuous operations  
No downwash  
Max DV: 106  $\mu\text{g}/\text{m}^3$

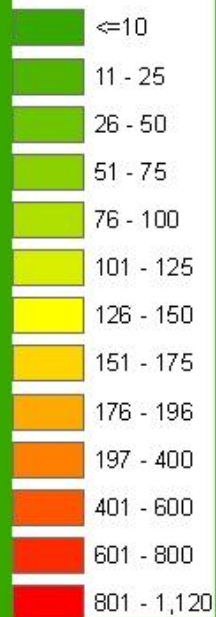


Stack ht increase #1  
Daytime operations  
No downwash  
Max DV: 99  $\mu\text{g}/\text{m}^3$

**Legend**



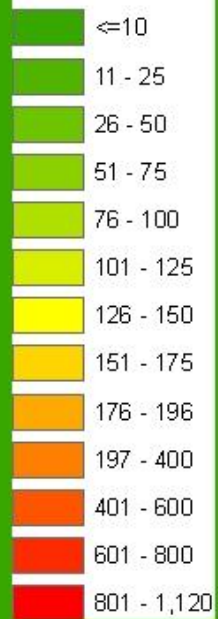
**Legend**



Stack ht increase #1  
Continuous operations  
With downwash  
Max DV: 371  $\mu\text{g}/\text{m}^3$



### Legend

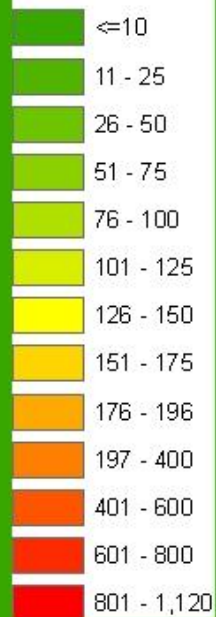


Stack ht increase #2  
Continuous operations  
No downwash  
Max DV: 18  $\mu\text{g}/\text{m}^3$

DRAFT



### Legend



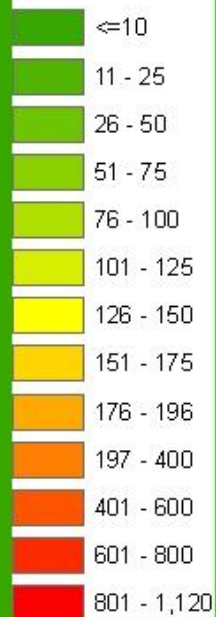
Stack ht increase #2  
Daytime operations  
No downwash  
Max DV: 18  $\mu\text{g}/\text{m}^3$

DRAFT



Empire Abo

### Legend

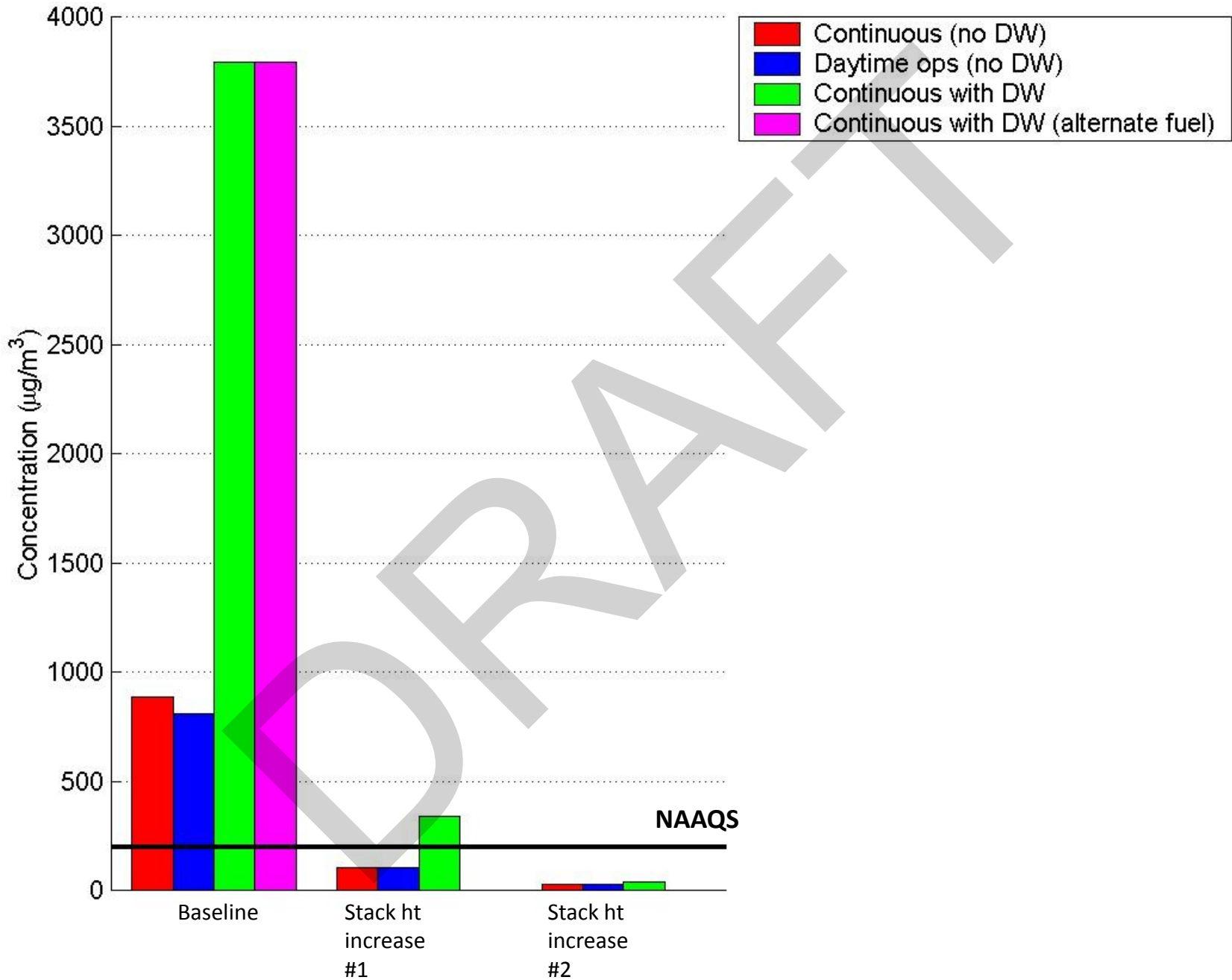


Stack ht increase #2  
Continuous operations  
With downwash  
Max DV: 18  $\mu\text{g}/\text{m}^3$

DRAFT

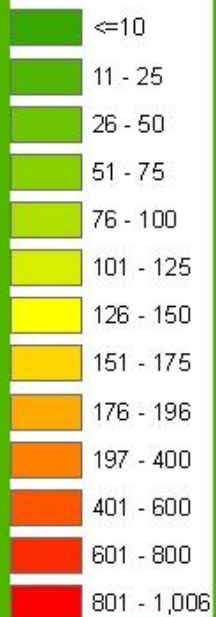


# Asphalt Plant (San Juan): SO<sub>2</sub>





**Legend**



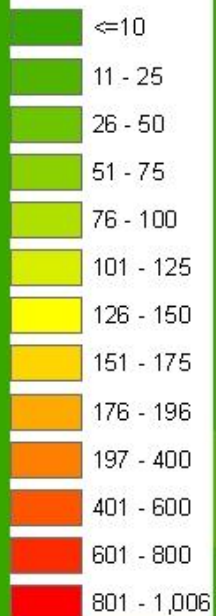
Base  
Continuous operations  
No downwash  
Max DV: 886  $\mu\text{g}/\text{m}^3$

DRAFT



San Juan

### Legend



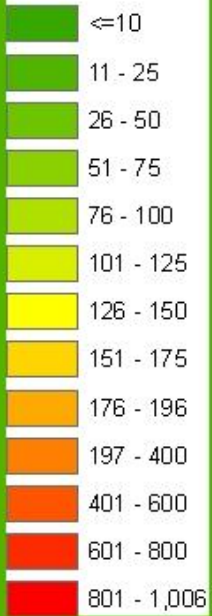
Base  
Daytime operations  
No downwash  
Max DV: 810  $\mu\text{g}/\text{m}^3$

DRAFT



San Juan

### Legend

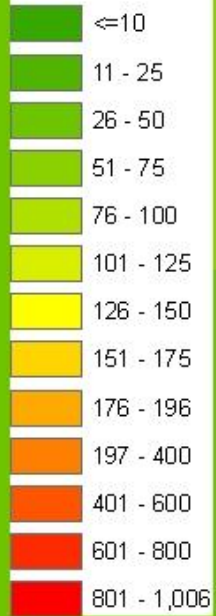


Base  
Continuous operations  
With downwash  
Max DV: 3790  $\mu\text{g}/\text{m}^3$

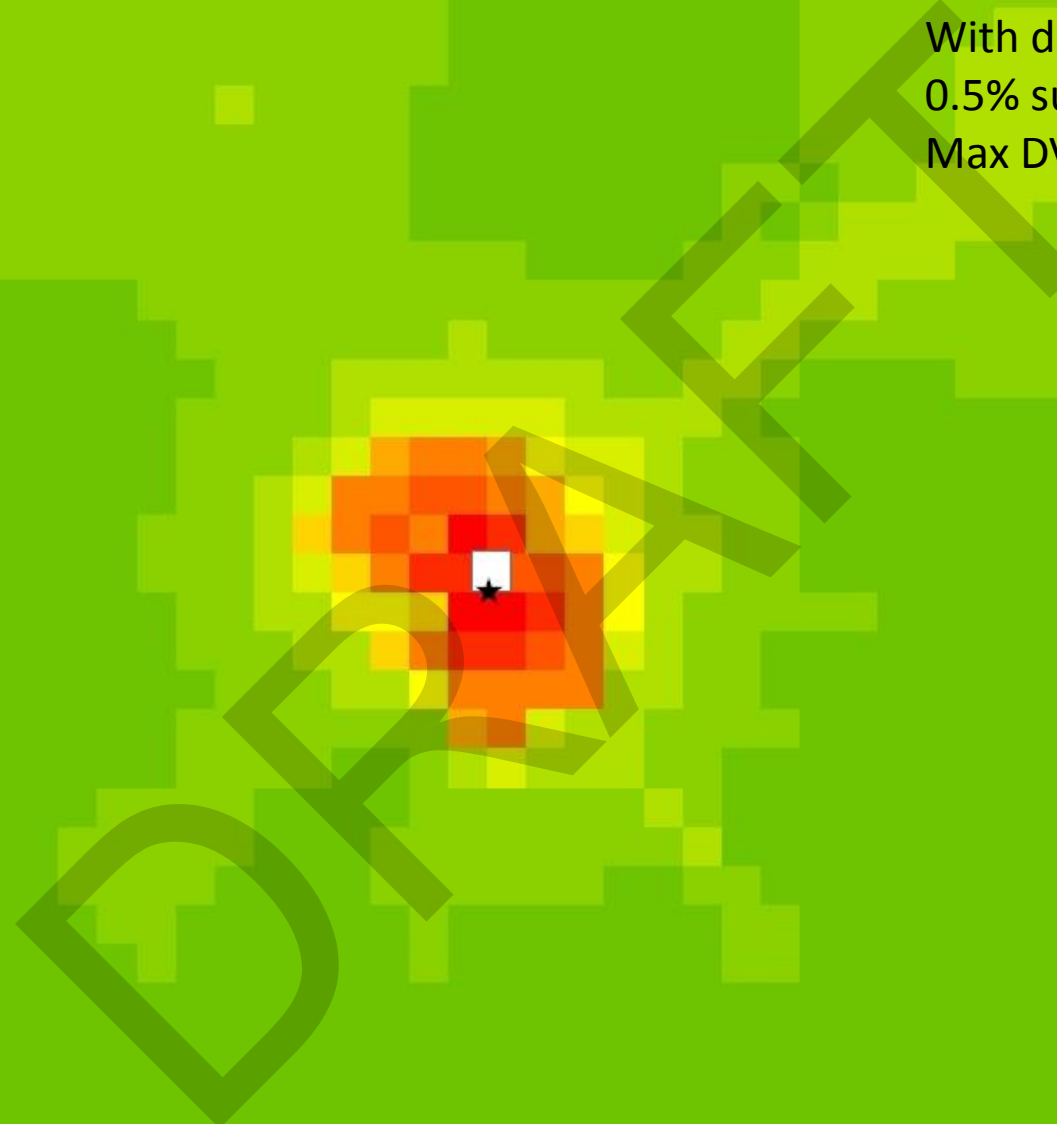


San Juan

### Legend

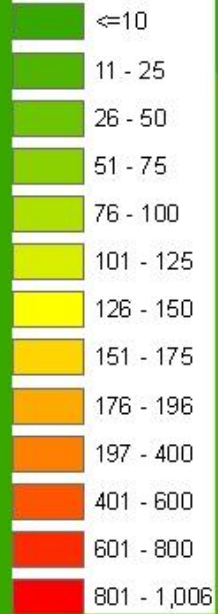


Base  
Continuous operations  
With downwash  
0.5% sulfur content fuel oil  
Max DV: 3790  $\mu\text{g}/\text{m}^3$



San Juan

**Legend**



Stack ht increase #1  
Continuous operations  
No downwash  
Max DV: 103 µg/m<sup>3</sup>

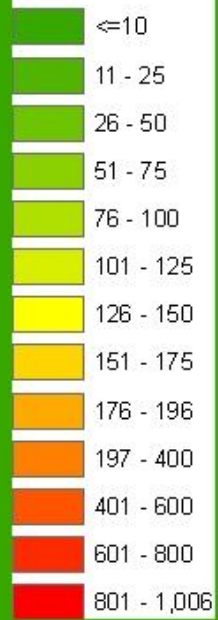
DRRAFT



San Juan

Stack ht increase #1  
Daytime operations  
No downwash  
Max DV: 103  $\mu\text{g}/\text{m}^3$

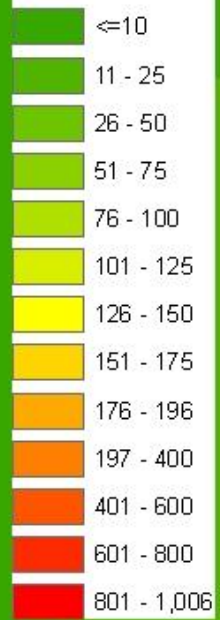
**Legend**



San Juan

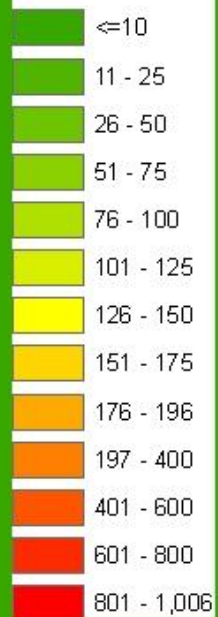
Stack ht increase #1  
Continuous operations  
With downwash  
Max DV: 341  $\mu\text{g}/\text{m}^3$

**Legend**



San Juan

### Legend



Stack ht increase #2  
Continuous operations  
No downwash  
Max DV: 29  $\mu\text{g}/\text{m}^3$



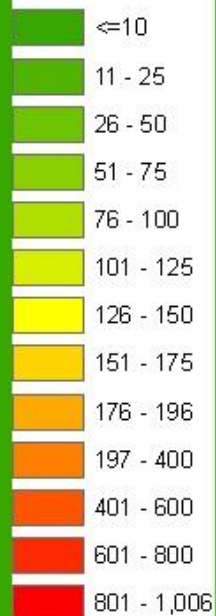
DRAFT



San Juan



### Legend



Stack ht increase #2  
Daytime operations  
No downwash  
Max DV: 29  $\mu\text{g}/\text{m}^3$

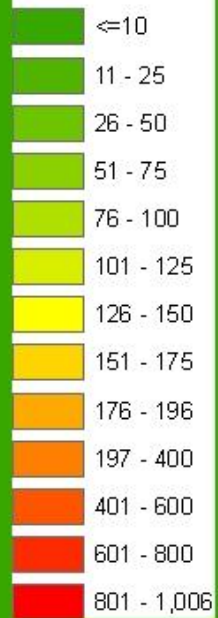


DRAFT



San Juan

**Legend**

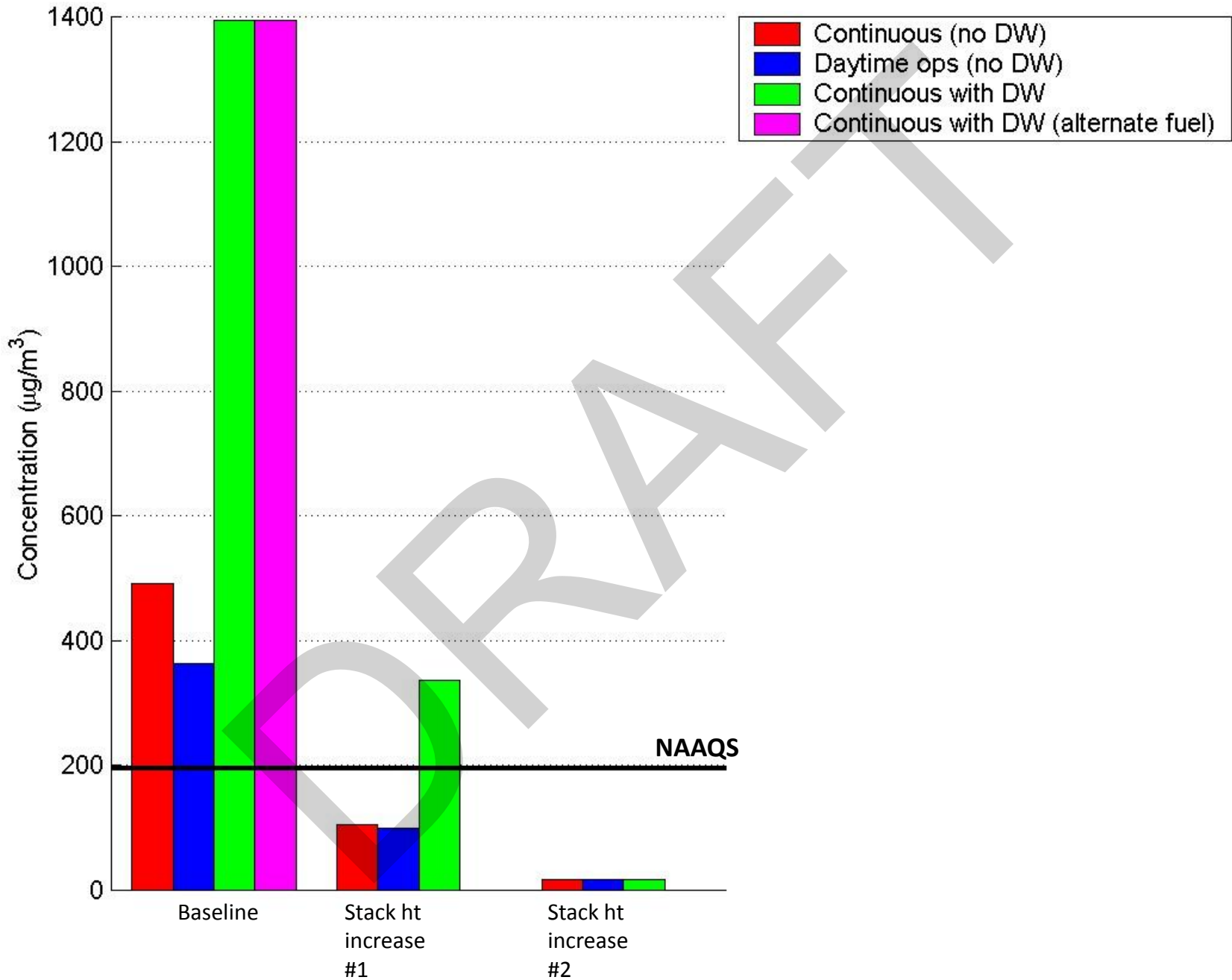


Stack ht increase #2  
Continuous operations  
With downwash  
Max DV: 37  $\mu\text{g}/\text{m}^3$

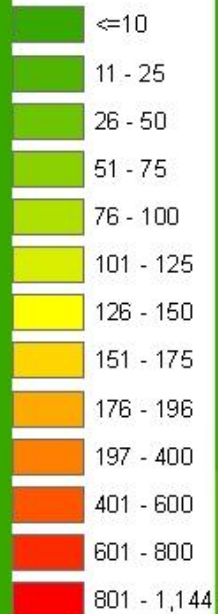


San Juan

# Asphalt Plant (Val Verde): SO<sub>2</sub>



### Legend



Base

Continuous operations

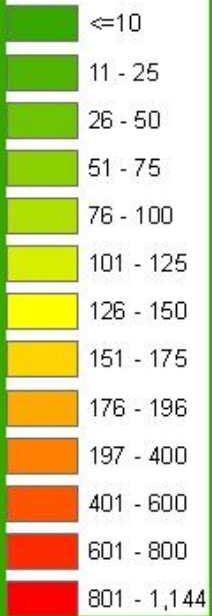
No downwash

Max DV: 492  $\mu\text{g}/\text{m}^3$

0 275 550 1,100 1,650 2,200 Meters

Val Verde

### Legend

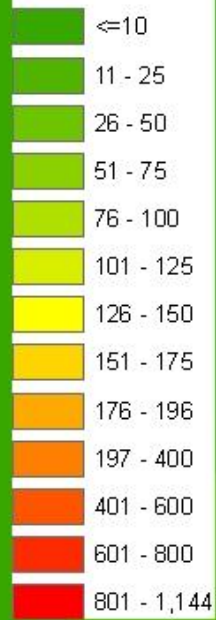


Base  
Daytime operations  
No downwash  
Max DV: 364 µg/m<sup>3</sup>



Val Verde

**Legend**



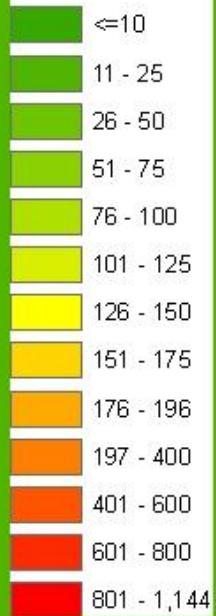
Base  
Continuous operations  
With downwash  
Max DV: 1394 µg/m<sup>3</sup>

DRIFT



Val Verde

### Legend

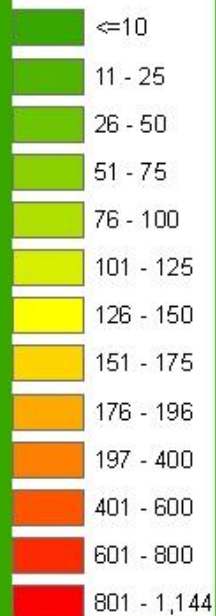


Base  
Continuous operations  
With downwash  
0.5% sulfur content fuel oil  
Max DV: 1394  $\mu\text{g}/\text{m}^3$



Val Verde

### Legend



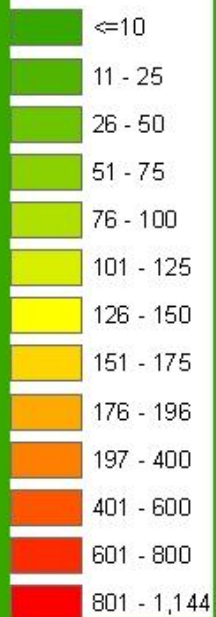
Stack ht increase #1  
Continuous operations  
No downwash  
Max DV: 106  $\mu\text{g}/\text{m}^3$



Val Verde



### Legend



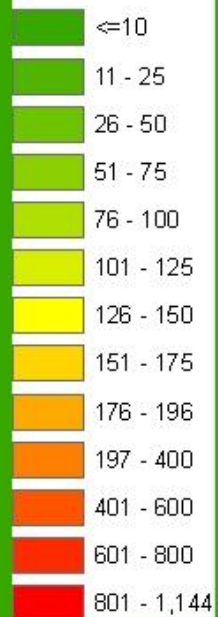
Stack ht increase #1  
Daytime operations  
No downwash  
Max DV: 100  $\mu\text{g}/\text{m}^3$

DRAFT



Val Verde

### Legend

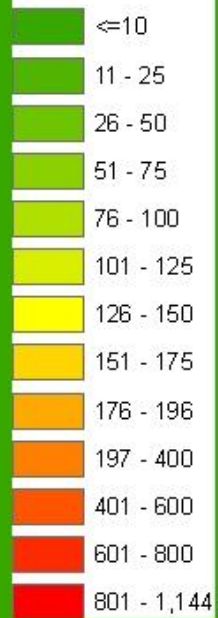


Stack ht increase #1  
Continuous operations  
With downwash  
Max DV: 337  $\mu\text{g}/\text{m}^3$



Val Verde

### Legend



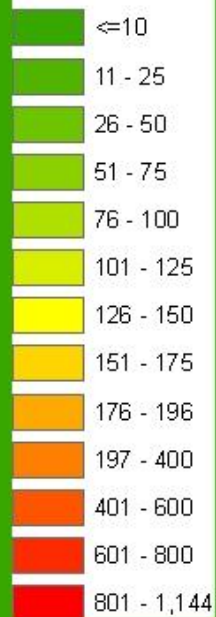
Stack ht increase #2  
Continuous operations  
No downwash  
Max DV: 18  $\mu\text{g}/\text{m}^3$

DRAFT



Val Verde

### Legend



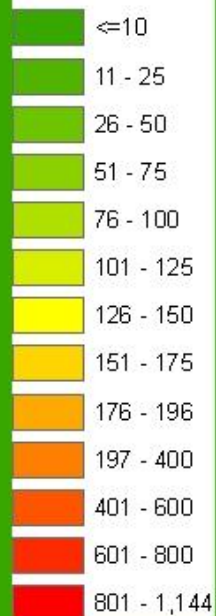
Stack ht increase #2  
Daytime operations  
No downwash  
Max DV: 18  $\mu\text{g}/\text{m}^3$

DRAFT



Val Verde

### Legend



Stack ht increase #2  
Continuous operations  
With downwash  
Max DV: 18  $\mu\text{g}/\text{m}^3$

DRAFT



Val Verde