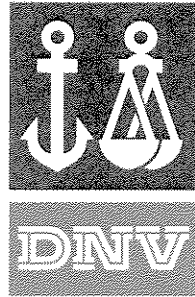


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# TECHNICAL REPORT

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## JOINT INDUSTRY PROJECT

### RELIABILITY OF CORRODED PIPES LABORATORY BURST TESTS

REPORT No. 96-3393

REVISION No. 02

DET NORSKE VERITAS



# TECHNICAL REPORT

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Date of first issue: 7 May 1997	Project No.: 25010049
Approved by: Tommy Bjørnsen <i>Tommy Bjørnsen</i> Head of Section	Organisational unit: Pipelines
Client: Joint Industry Project	Client ref.: See participation list

**Summary:**

This report is one of a serie of 4 reports in the JIP project "Reliability of Corroded Pipes", and describes the laboratory burst tests of pipes with simulated corrosion defects. This project is a continuation of the JIP project "Residual Strength of Dented and Corroded Pipes".

Twelve burst tests have been performed, of which 9 were with longitudinal corrosion defects and 3 with circumferential corrosion defects. The pipes were loaded with combined internal pressure and external loads, except for 2 tests with internal pressure only. The external loads considered were bending moment and axial compressive force.

The test specimen, test set-up execution of the tests and the main results are described in this report, while evaluation of the results are included in the DNV project report no. 96-3394 "Reliability of Corroded Pipes / Assessment of Capacity and Acceptance Criteria"

All tests were made from seamless pipe with 324 mm diameter and 10.3 mm wall thickness of X52 modified material. The defects were smooth corrosion made using spark erosion for the longitudinal corrosion and the circumferential corrosion was machined.

Report No.: 96-3393	Subject Group:	
Report title: Reliability of Corroded Pipes Laboratory Burst Tests		
Work carried out by: O. H. Bjørnøy, G. Sigurdsson, E. Cramer <i>Ola H. Bjornoy</i>		
Work verified by: Leif Collberg <i>Leif Collberg</i>		
Date of this revision: 16 Des. 1997	Rev. No.: 02	Number of pages: 65

**Indexing terms**

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Pipelines  
Laboratory tests  
Burst

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***Table of Revisions***

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**SUMMARY**

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## 1 SUMMARY

This report is one of a serie of 4 reports in the JIP project "Reliability of Corroded Pipes", and describes the laboratory burst tests of pipes with simulated corrosion defects. This project is a continuation of the JIP project "Residual Strength of Dented and Corroded Pipes".

Twelve burst tests have been performed, of which 9 were with longitudinal corrosion defects and 3 with circumferential corrosion defects. The pipes were loaded with combined internal pressure and external loads, except for 2 tests with internal pressure only. The external loads considered were bending moment and axial compressive force.

The test specimen, test set-up execution of the tests and the main results are described in this report, while evaluation of the results are included in the DNV project report no. 96-3394 "Reliability of Corroded Pipes / Assessment of Capacity and Acceptance Criteria".

All tests were made from seamless pipe with 324 mm diameter and 10.3 mm wall thickness of X52 modified material. The defects were smooth corrosion made using spark erosion for the longitudinal corrosion and the circumferential corrosion was machined.



## 2 INTRODUCTION

### 2.1 Motivation

A pipeline is a large financial assets for the pipeline operator and a safe operation of the pipeline is therefore of great concern. On the other hand, unnecessary repair and an over conservative operation of the pipeline may result in high costs and unexploded resource utilisation. As the pipelines are ageing and corrosion may develop, the economical consequences of reduced operation pressure, repairs, or replacements may become high. Available design equations for assessment of allowable operating pressures of degraded pipelines depending on the selected reliability level is therefore desirable.

When severe corrosion has been observed in a pipeline, the decision of necessary action to be carried out should be based on an overall assessment of the pipeline, where uncertainties associated with both the assessment of the degree of corrosion and the capacity evaluation should be considered. The cost of repair or replacement can be very high and should be avoided, or postponed in time, if this is possible within the safety requirements defined. Required actions should further also be initiated in order to maintain the integrity of the pipeline and to avoid an undesired risk exposure of the pipeline.

The objective of the work is to provide the participants with capacity formulas of corroded pipes. The work includes laboratory tests and a large number of finite element analyses of corroded pipes exposed to internal pressure, combined internal pressure and bending moment, and combined internal pressure and bending moment. Both longitudinal and circumferential corrosion are considered. The formulas will be calibrated using reliability methods. This will in a systematic manner include uncertainties in inspection results and variations in material properties, pressure and dimensions. The outcome of the project will be included in a manual for assessment of corroded pipes.

### 2.2 Background

The present Joint Industry Project "Reliability of Corroded Pipes" is a continuation of the project "Residual Strength of Corroded and Dented Pipes". The former project which was started in 1993 and concluded at the end of 1995, and the present project started shortly after.

The Phase I of the project was sponsored by Statoil, Phillips, Brasoil (Petrobras), Mineral Management Services (MMS), Norwegian Petroleum Directorate (NPD), The Research Council of Norway (NFR), and Det Norske Veritas (DNV).

The present project "Reliability of Corroded Pipes" is sponsored by Statoil, Amoco, Exxon, NPD and MMS.

The scope of work of the project has been modified in order to best utilise the funding. Especially has the work conducted by British Gas had an impact on our project as British Gas is undertaking a similar project. To avoid unnecessary overlapping of work the scope was changed, but some items were not overlapping. DNV have included combined load cases, circumferential corrosion, and a reliability calibration of the capacity and design equations that would be




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 INTRODUCTION
 

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established. British Gas, on the other hand, had already performed many tests and finite element analyses for internal pressure only, including interaction of separate pits and grooves, but they would not included a reliability calibration of the equations. A co-operation with British Gas has been discussed and an advantage would be that the equations would be based on a larger database including effects studied only by British Gas and effects studied only by DNV. The equations would include calibrated safety factors. Common capacity and design equations from British Gas and DNV would most probable receive greater acceptance in the marked, and hence, be a recognised equations.

After completion of both the British Gas and the DNV project, where both projects have made project specific guideline of corroded pipes, a unified guideline could be made.

### 2.3 Project Reports

The project concludes with 4 reports, given in the table below.

**Table 2-1 Overview of the project reports**

DNV report no.	Title / Subject
96-3392	Reliability of Corroded Pipes / Finite Element Analyses
96-3393	Reliability of Corroded Pipes / Laboratory Burst Tests (This document)
96-3394	Reliability of Corroded Pipes / Assessment of Capacity and Acceptance Criteria
97-3358	Reliability of Corroded Pipes / Project Guideline

### 2.4 Participants and Their Representatives

The following organisations participated in the project;

Participant	Representative	Telephone / Fax	
Minerals Management Service (MMS)	Wallace O. Adcox	telephone fax	(+1) 703 787 1354 (+1) 703 787 1010
Norwegian Petroleum Directorate (NPD)	Kjell A. Anfinsen	telephone fax	(+47) 51 87 62 26 (+47) 51 55 15 71
Den norske stats oljeselskap a.s.(Statoil)	Richard Verley	telephone fax	(+47) 73 58 41 85 (+47) 73 96 72 86
Amoco Norway Oil Company (Amoco)	Ole Jørgen Narvestad	telephone fax	(+47) 51 50 20 18 (+47) 51 50 22 18
Exxon Production Research Company (EPR)	Robert Appleby	telephone fax	(+1) 713 965 7193 (+1) 713 966 6423
Petrobras /CENPES/DIPREX	Adilson C. Benjamin	telephone fax	(+55) 21 598 6263 (+55) 21 598 6793




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 INTRODUCTION
 

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The SI units are used in the report. The conversion factors are between the SI units and the US units are;

**From US units to SI units**

length:	1 in (inch)	=	25.40 mm
Mass	1 lb (pound)	=	0.4536 kg
Force	1 lbf (pound force)	=	4.448 N
	1 kip	=	4.448 kN
Stress (Pressure)	1 psi (lbf/in <sup>2</sup> )	=	0.006895 MPa (N/mm <sup>2</sup> )
	1 ksi (1000 psi)	=	6.895 MPa

**From SI units to U. S units**

length:	1 mm	=	0.03937 in
Mass	1 kg	=	2.205 lb (pound)
Force	1 N	=	0.2248 lbf (pound force)
	1 kN	=	0.2248 kip
Stress (Pressure)	1 MPa	=	145.0 psi (lbf/in <sup>2</sup> )
	1 MPa	=	0.1450 ksi

$$1 \text{ ksi} = 1000 \text{ psi}$$

$$10 \text{ bar} = 1 \text{ MPa}$$



## GENERAL DESCRIPTION OF TESTS

### 3 GENERAL DESCRIPTION OF TESTS

#### 3.1 Overview of tests

A total of 12 tests has been carried out within the project. An overview of the tests are given in Table 3-1.

**Table 3-1 Overview of tests**

Test no.	Nom Dia (mm)	Nom thick (mm)	mat.	defect depth (d/t)	defect length	defect width	loading		
							int. press	/bending	/axial
1	324	10.3	X52	0.50	0.75 D	15 t	X		
2	324	10.3	X52	0.50	0.75 D	15 t	X	X	
3	324	10.3	X52	0.50	0.75 D	15 t	X	X	
4	324	10.3	X52	0.30	0.50 D	3 t	X	X	
5	324	10.3	X52	0.30	0.50 D	3 t	X		X
6	324	10.3	X52	0.30	0.50 D	3 t	X		X
7	324	10.3	X52	0.50	0.75 D	3 t	X		X
8	324	10.3	X52	0.50	0.75 D	3 t	X		
9	324	10.3	X52	0.70	0.75 D	3 t	X		X
10	324	10.3	X52	0.50	12 mm	circ.	X		X
11	324	10.3	X52	0.50	12 mm	circ.	X		X
12	324	10.3	X52	0.70	12 mm	circ.	X		X

The dimensions given in the table are nominal values. The actual values of diameter, wall thickness and corrosion defects were measured. The material curve was determined by coupon tests. All simulated longitudinal corrosion defects were smooth rectangular defects fabricated using spark erosion, while the circumferential corrosion defects were machined. Tests 1 through 9 were simulating longitudinal corrosion, while test 10 through 12 simulated girth weld corrosion. All defects were made at the outer surface in the parent material.

The test specimens were exposed to combined internal pressure and external forces until burst, except for 2 test specimens which were exposed to internal pressure only.

#### 3.2 Description of the test set-ups

The tests were exposed to different kind of loading which required different test set-ups;

- internal pressure only
- combined internal pressure and bending moment
- combined internal pressure and axial compressive force

The tests with internal pressure only requires virtually no special test set up, apart from the instrumentation and the water pump to increase the internal pressure until burst.



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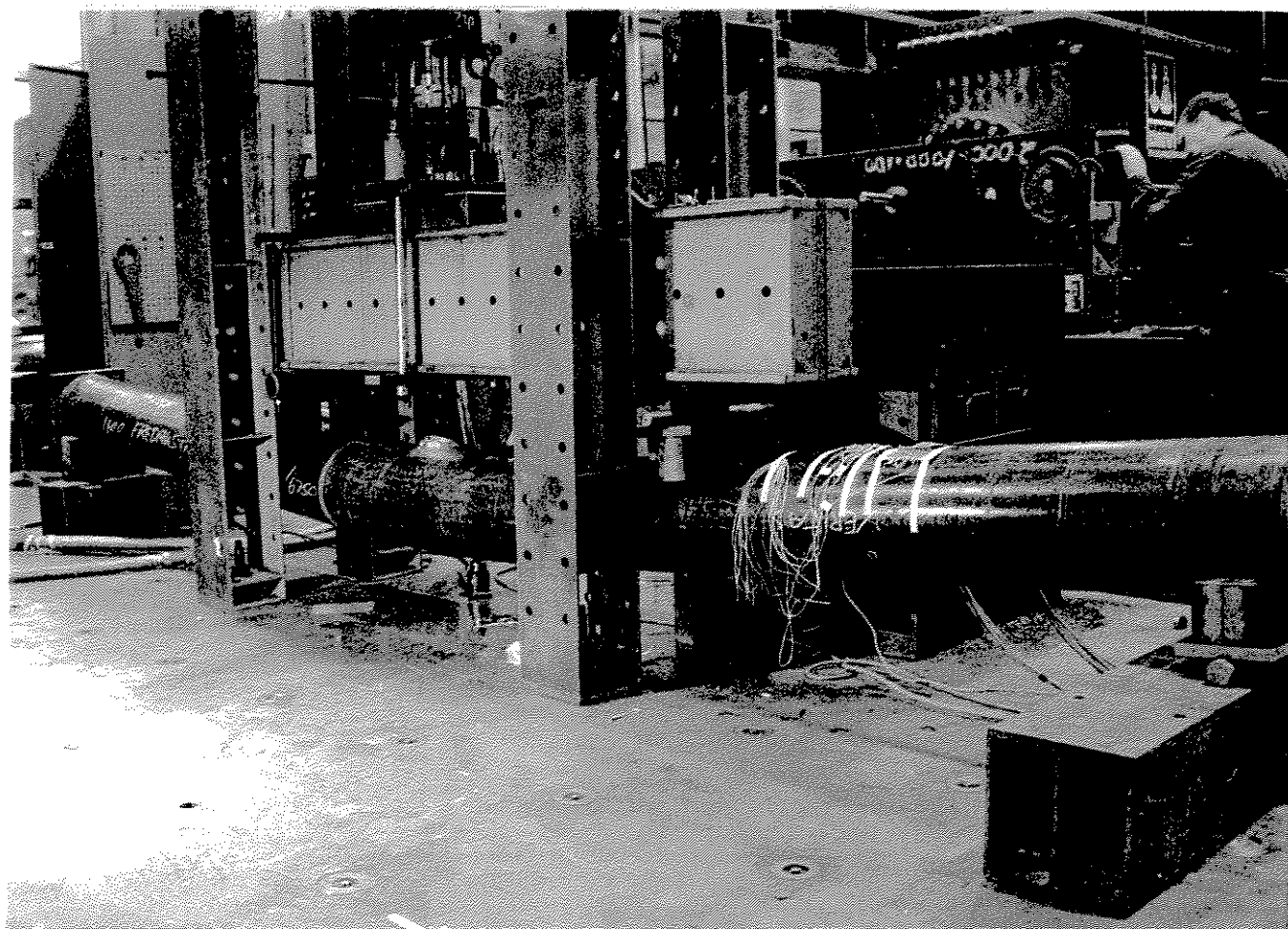
**GENERAL DESCRIPTION OF TESTS**

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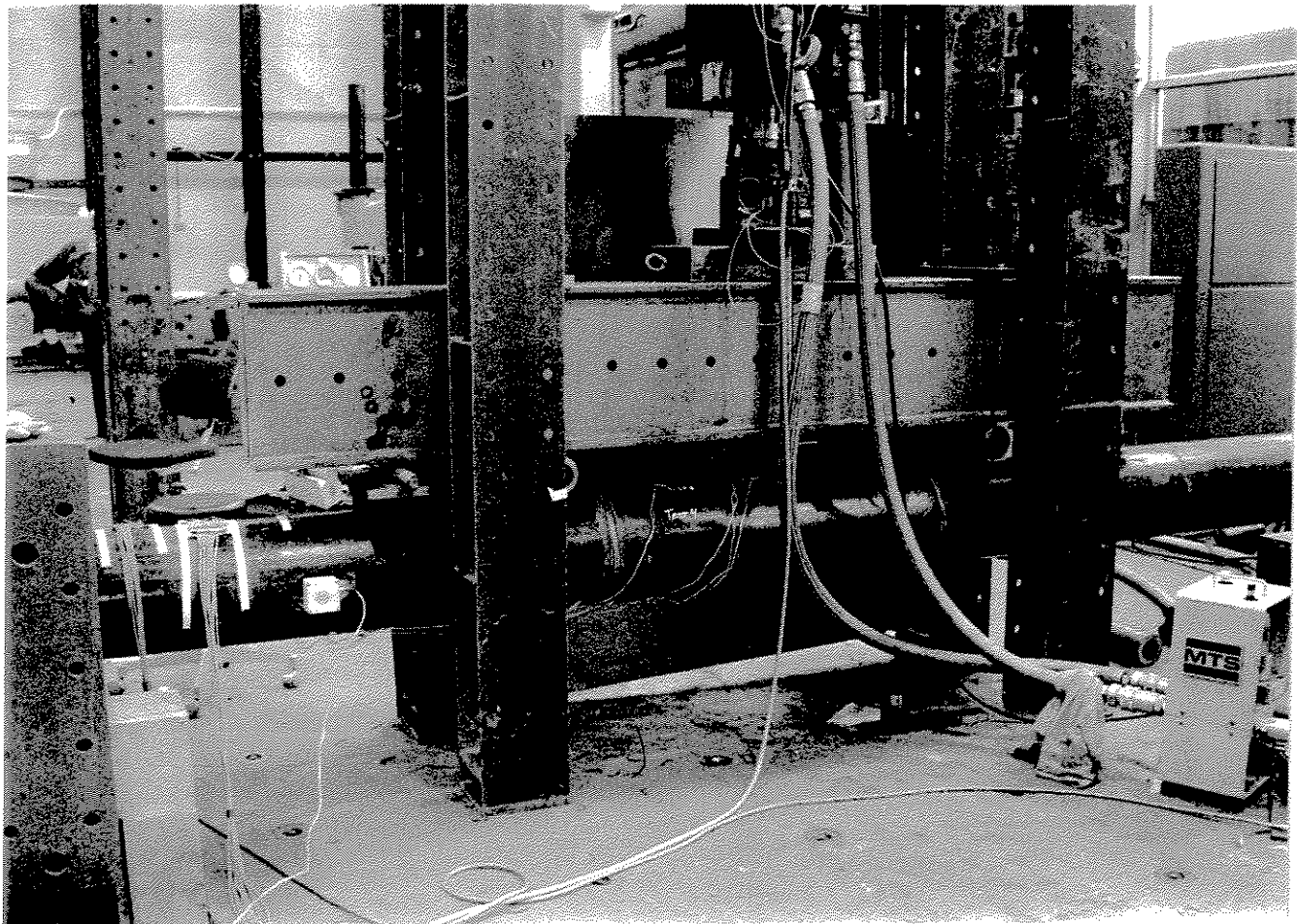
The tests with internal pressure and bending moment was performed in a 4-point-bending test rig. The test rig is shown in Figure 3-1 and Figure 3-2. A sketch of the test rig is also included in Appendix A. Rollers were used at the supports to in order to define and keep the distance between the supports constant. The distance between the rollers, which is the moment arm, varied from 1.27 to 1.43 meter for the three tests with bending moment. A servo controlled dynamic MTS 1000 kN actuator was used to apply the force. The specific test rig set-up made for this project had approximately 650 kNm moment capacity, and maximum 150 mm stroke.

The tests with combined internal pressure and axial compressive force was performed in a test frame as shown in Figure 3-3. A 10000 kN static jack was applied. The length of the test specimens were all 1000 mm, plus 2\*50 mm for the end-plates. The maximum stroke of the jack was slightly less than 100 mm.

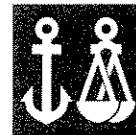
The water pump used in the burst tests had a capacity of 1000 bar. All tests were performed at room temperature at approximately 20°C



**Figure 3-1** Picture of the test rig for 4-point bending test (after completion).



**Figure 3-2** Picture of the test rig for 4-point bending test.



GENERAL DESCRIPTION OF TESTS

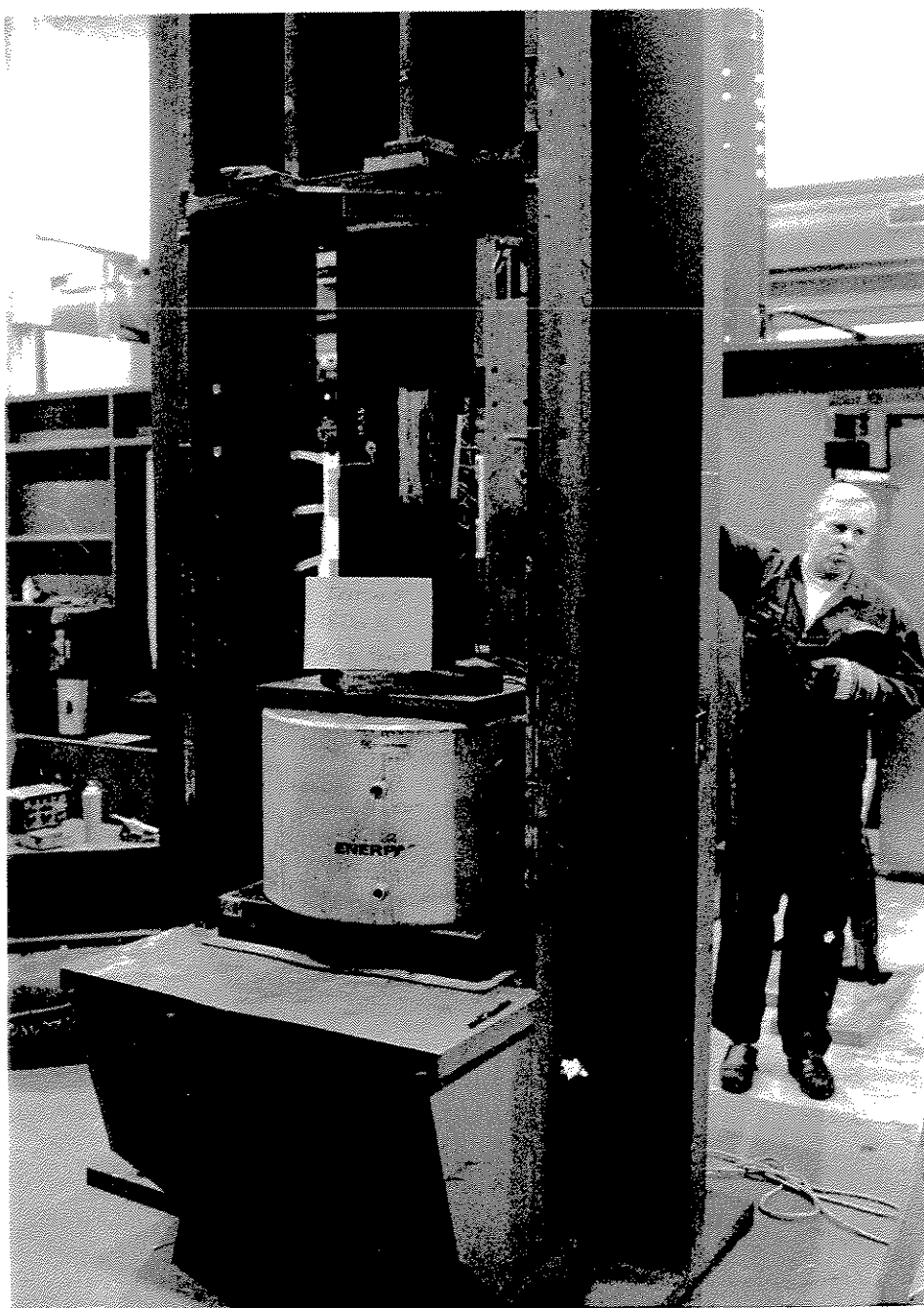


Figure 3-3 Picture of the test rig for axial compressive force





### 3.3 Instrumentation

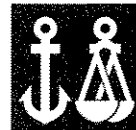
Each specimen was instrumented with strain gauges and pressure transducer in order to monitor the specimen during testing and for recording. The strain gauge instrumentation for each specimen are shown in Appendix A. Approximately 10 strain gauges were applied at each test. For the tests with combined loading the external loads were also monitored and recorded. In Figure 3-4 an example of the strain gauge instrumentation of a corrosion defect is shown.

For the specimens exposed to combined loads, some strain gauges were used for load and alignment control. All strain gauges were post yield cross gauges allowing for large strains from Tokyo Sokki Kenkyujo Co., LTD., type YFLA-2.

A 1000 bar pressure transducer was used, serie no. F02395. In order to minimise erroneous pressure fluctuations the pressure transducer was mounted directly to the end flange in a separate hole from the connection from the hose for the pump.

### 3.4 Manufacture of the test specimens

The simulated corrosion defects were spark eroded at the outer surface. The defect similar to test 1 to 3 is shown in Figure 3-4. The defects had a smooth surface and all edges were made with a small radius. The surfaces were also grinded slightly to get a smoother surface for ease thickness measurements and application of strain gauges. At each end of the test specimen a 50mm thick end-plate was welded to the pipe. For the tests exposed to bending moment thicker extension pipes of approximately 2 meters were welded to each end of the test specimen, and the end-plate were welded to the end of these extension pipes. The inlet for internal pressure and mounting of the pressure transducer were in the end flanges.



DNV

GENERAL DESCRIPTION OF TESTS



**Figure 3-4 Picture of a corrosion defect with strain gauge instrumentation**



## 4 DETAILED DESCRIPTION OF THE TESTS

### 4.1 General

Twelve test were performed. The 9 first test specimens were made from the same pipe, while the last 3 test specimens were made from another pipe, which was almost identical to the first one. The nominal parameters are the same for all 12 tests, apart for the simulated corrosion defects. For each test specimen the actual dimensions were measured and are described for each test in this report.

The following was the same for all tests;

<b>Pipe Diameter</b>	324 mm (nominal)	
<b>Pipe wall Thickness</b>	10.31 mm (nominal)	
<b>Pipe Grade</b>	X52	
<b>Type of Longitudinal Seam</b>	Seamless	
<b>Yield Strength (actual, eng.)</b>	380 MPa	(Average of 8 test coupons)
<b>Tensile Strength (actual, eng.)</b>	514 MPa	(Average of 8 test coupons)
<b>Year of Manufacture</b>	1996 / 1997	

The pipe diameter was measured at several locations, it was found to be closer to 325 than the nominal diameter of 324 mm, and was almost identical at all measured locations. The pipe wall thickness, however, varied far more, from minimum 10.25 mm to maximum 11.10 mm. The largest variation was in the circumferential direction, but large variations were also observed along the length of the pipe.

Some variables have been calculated based on measurements and constants, as for instance the axial stress is calculated based on the applied (measured) force and the diameter and thickness. For calculation of the cross section parameters the an outer diameter of 324 mm is used, and for the wall thickness the "average" thickness of 10.6 mm is used. This results in the following values for the cross section;

- Area<sub>pipe</sub> = 10437 mm<sup>2</sup>  $(D_o^2 - D_i^2) * \pi / 4$
- Area<sub>inner</sub> = 72012 mm<sup>2</sup>  $(D_i^2) * \pi / 4$
- Moment of Inertia (I) = 1.28 \* 10<sup>8</sup> mm<sup>4</sup>  $(D_o^4 - D_i^4) * \pi / 64$
- Section modulus W<sub>elastic</sub> = 791854 mm<sup>3</sup>  $I / (D_o / 2)$

D<sub>o</sub> ; Outer Diameter = 324 mm

D<sub>i</sub> ; Inner Diameter = 302.8 mm

In the following sub-sections each test is described. Sketches showing the test set-up, the corrosion defect, the instrumentation, the thickness measurements are included in Appendix A. Pictures of the test specimens after burst are included in the main section of the report. In Appendix B the material certificates are included, and in Appendix C listing of the recorded pressure, loads and strain gauges are given (Microsoft Excel spreadsheet)




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 DETAILED DESCRIPTION OF THE TESTS
 

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## 4.2 Test no. 1

### Loading

Internal pressure only.

### Corrosion defect parameters (nominal)

Corrosion defect depth	d	= 5.3 mm	(d/t = 0.5)
Corrosion defect length	L	= 245 mm	(L/D = 0.75)
Corrosion defect width	w	= 150 mm	(w = 15 t)
Length of test specimen	$L_{\text{specimen}}$	= 1500 mm	

### Instrumentation

In the corroded area 9 cross strain gauges were applied, and one strain gauge was applied away from the corroded area for load control and hoop strain measurement. Internal pressure and time for each scan were also recorded.

### Loading description

Internal pressure was applied until burst, and applied internal pressure versus time is shown in Figure 4-1.

### Results

The test failed at 232 bar. The test specimen after burst is shown in Figure 4-2.

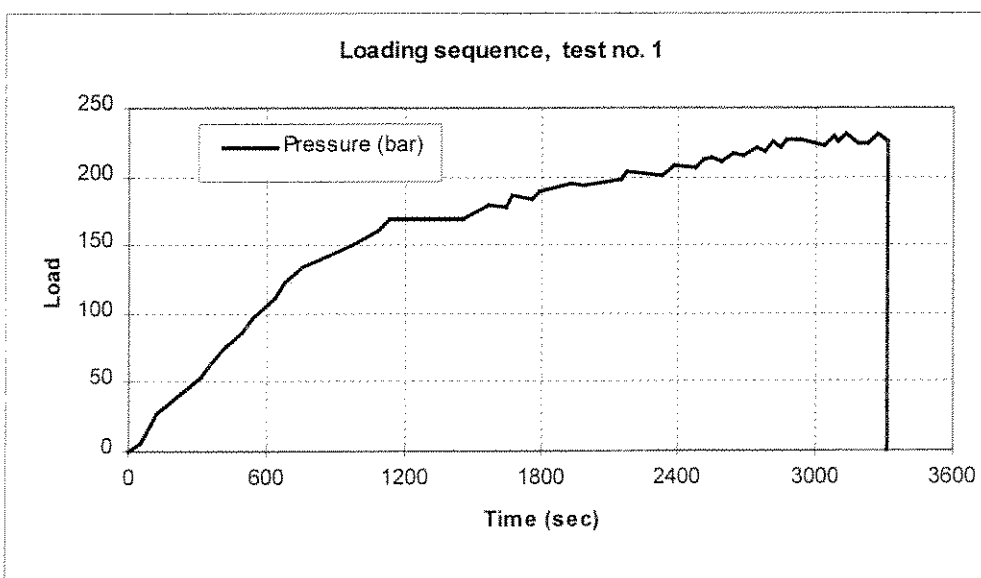


Figure 4-1 Applied pressure versus time for test no. 1



DETAILED DESCRIPTION OF THE TESTS

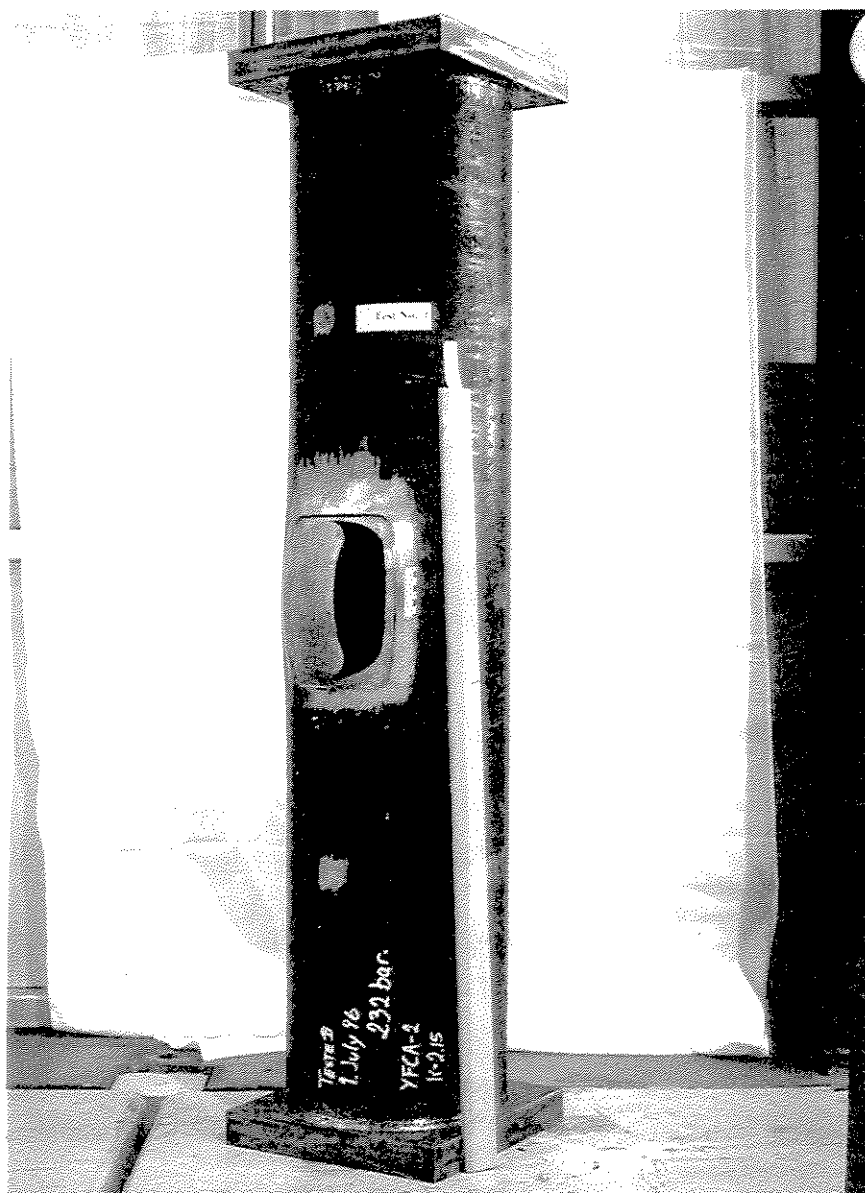


Figure 4-2 Picture of the test specimen no. 1 after the burst



DETAILED DESCRIPTION OF THE TESTS



Figure 4-3 Picture of the test specimen no. 1 after the burst



### 4.3 Test no. 2

#### Loading

Loaded with combined internal pressure and bending moment.

#### Corrosion defect parameters (nominal)

(Identical with specimen no. 1)

Corrosion defect depth	d	= 5.3 mm	(d/t = 0.5)
Corrosion defect length	L	= 245 mm	(L/D = 0.75)
Corrosion defect width	w	= 150 mm	(w = 15 t)
Length of test specimen	L <sub>specimen</sub>	= 1500 mm	

#### Instrumentation

In the corroded area 9 cross strain gauges were applied, and two single filament gauges were applied away from the corroded area for load control of the bending moment. The time, the actuator load and displacement were also recorded.

#### Loading description

The specimen was exposed to combined internal pressure and 4-point-bending moment. The corrosion defect was located at the compressive side of the bending moment.

An internal pressure of 165 bar was applied during the first 15 minutes. The loading is illustrated in Figure 4-4 to Figure 4-6. The internal pressure was then kept at 165 bar and bending moment was applied to the test specimen. The actuator was in displacement control, and for this test set-up the applied displacement results in a forced curvature of the pipe. At approximately 220 kNm bending moment more and more displacement was required in order to further increase the bending moment, which effect indicate excessive yielding of the pipe cross section. Further, the displacement was kept constant and the internal pressure was increased, which resulted in a drop in the bending moment at the constant displacement. In order to maintain the bending moment additional displacement was applied, but the pipe had softened significantly due to the internal pressure and the pipe could not carry much increased bending moment.



DETAILED DESCRIPTION OF THE TESTS

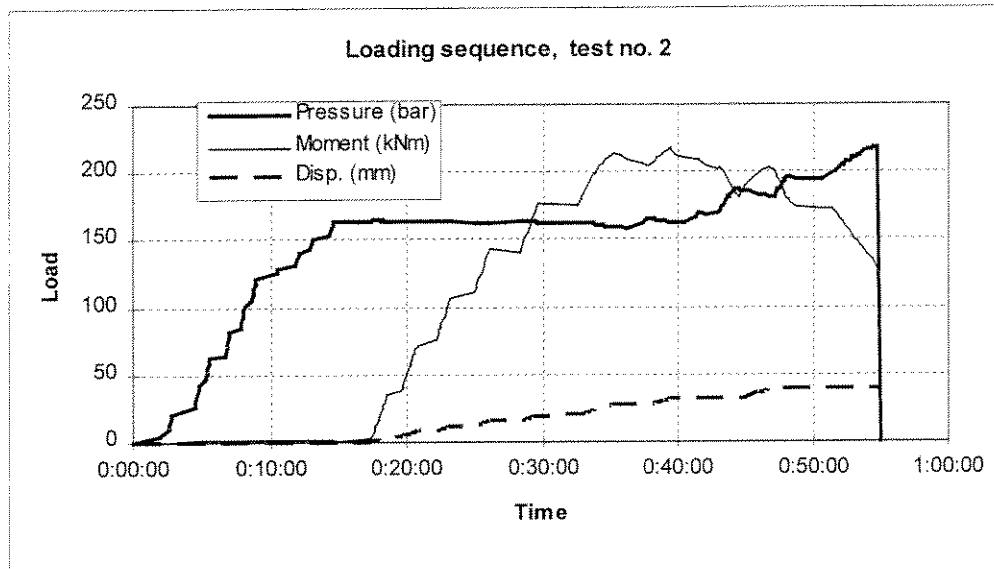


Figure 4-4 Loading sequence, test no. 2

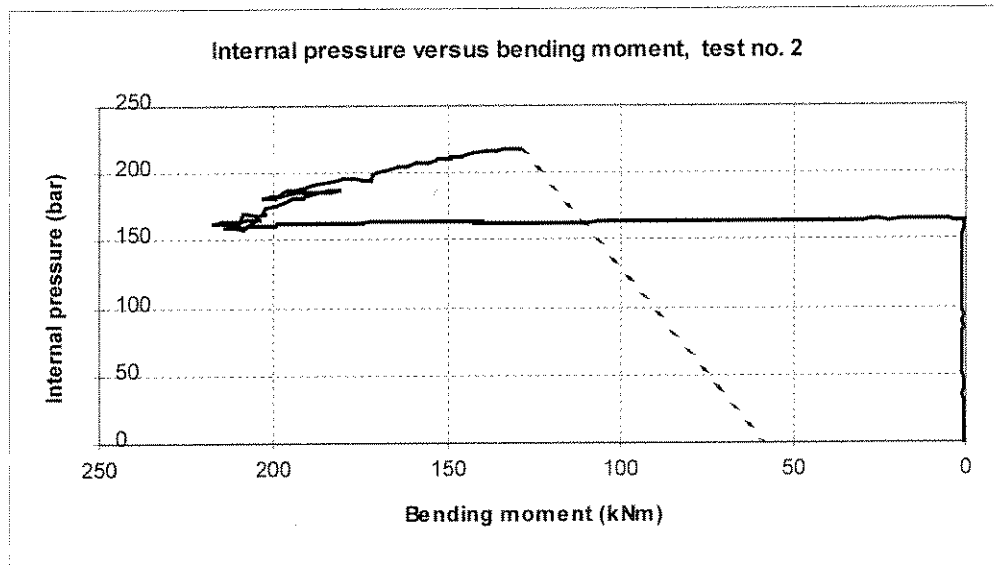
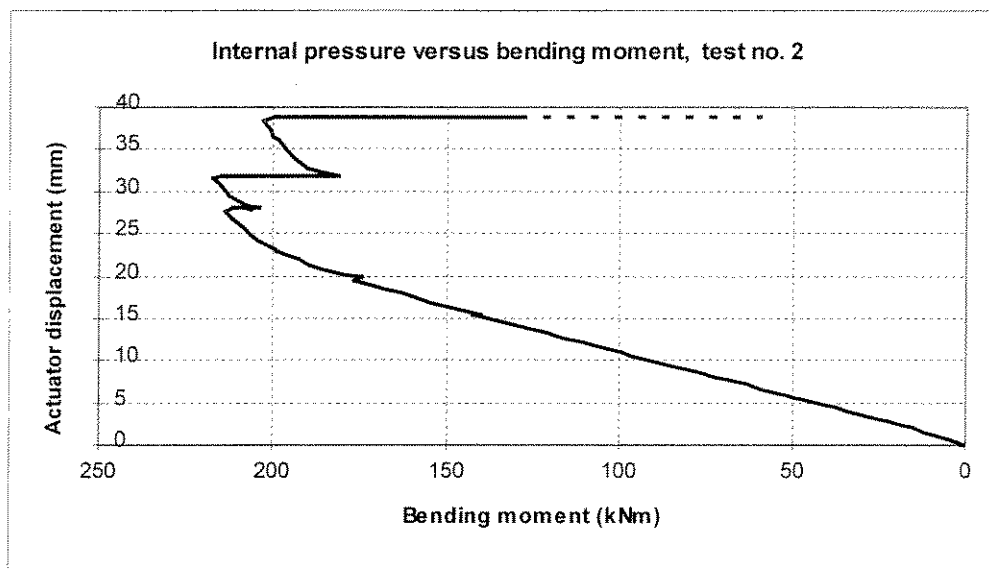


Figure 4-5 Internal pressure versus bending moment, test no. 2





## DETAILED DESCRIPTION OF THE TESTS



**Figure 4-6 Actuator displacement versus bending moment, test no. 2**

### Results

Excessive yielding was observed in the pipe, and it was not possible to maintain the maximum bending moment of approximately 220 kNm when the internal pressure was further increased. When the internal pressure was increased from 165 bar to rupture at 218.5 bar, the bending moment decreased from 220 kNm to 130 kNm.

The bending moment resulted in a radius of approximately 15-20 meter, where the 15 meter was estimated based on measurements of the test specimen after testing and the 20 meter was based on the applied displacement during the test.



DETAILED DESCRIPTION OF THE TESTS

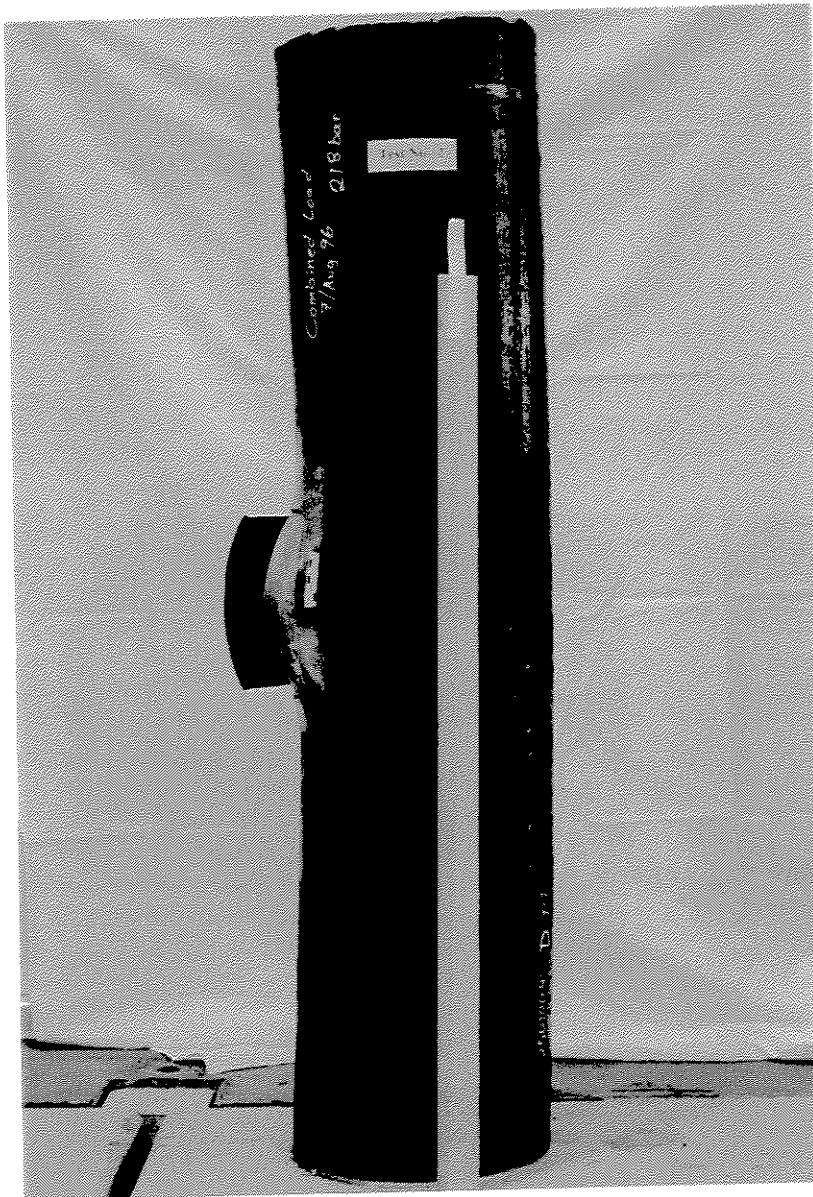


Figure 4-7 Picture of the test specimen no. 2 after the burst test



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DETAILED DESCRIPTION OF THE TESTS

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**Figure 4-8** Picture of the test specimen no. 2 after the burst test




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 DETAILED DESCRIPTION OF THE TESTS
 

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#### 4.4 Test no. 3

##### Loading

Loaded with combined internal pressure and bending moment (similar to test 2).

##### Corrosion defect parameters (nominal)

(Identical to specimen no 1 and 2)

Corrosion defect depth	d	= 5.3 mm	(d/t = 0.5)
Corrosion defect length	L	= 245 mm	(L/D = 0.75)
Corrosion defect width	w	= 150 mm	(w = 15 t)
Length of test specimen	Lspecimen	= 1500 mm	

##### Instrumentation

In the corroded area 9 cross strain gauges were applied, and two single filament gauges were applied away from the corroded area for load control of the bending moment. The time, rotation angle, the actuator load and displacement were also recorded.

##### Loading description

The specimen was exposed to combined internal pressure and 4-point-bending moment. The corrosion defect was located at the compressive side of the bending moment. In the previous test the MTS was in displacement control, but order to try to maintain the bending moment and hence allow the pipe to deflect the actuator was set in load (bending moment) control.

An internal pressure of 165 bar was applied during the first 12 minutes. The internal pressure was kept at 165 bar and bending moment was applied to the test specimen. Further, the bending moment was kept constant at 200 kNm, and the internal pressure was increased. The pipe was yielding extensively, which resulted in increased additional displacement in order to maintain the set bending moment of 200 kNm. A small increase in the bending moment up to 212.5 kNm was applied, and only marginal additional internal pressure was introduced before rupture.



DETAILED DESCRIPTION OF THE TESTS

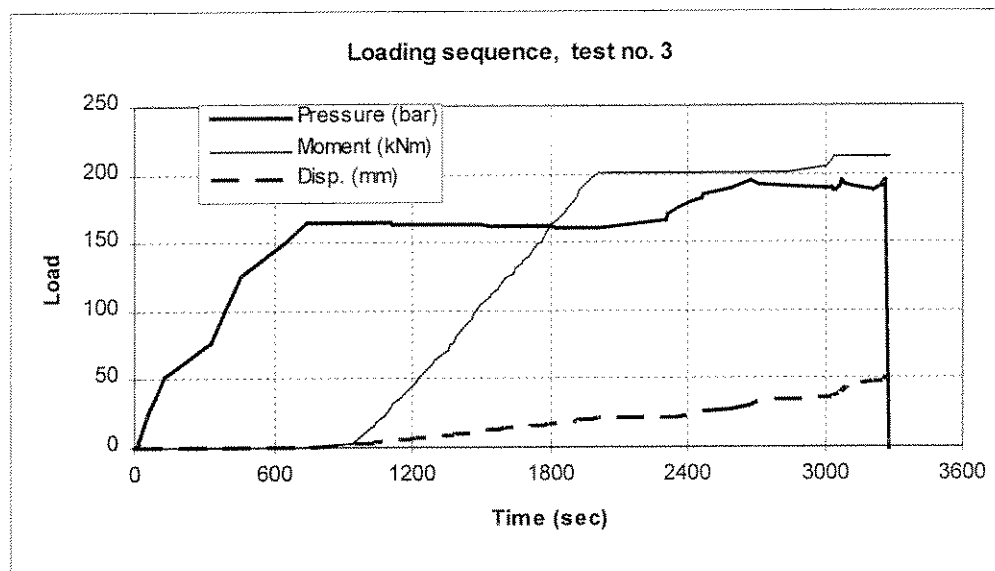


Figure 4-9 Loading sequence, test no.3

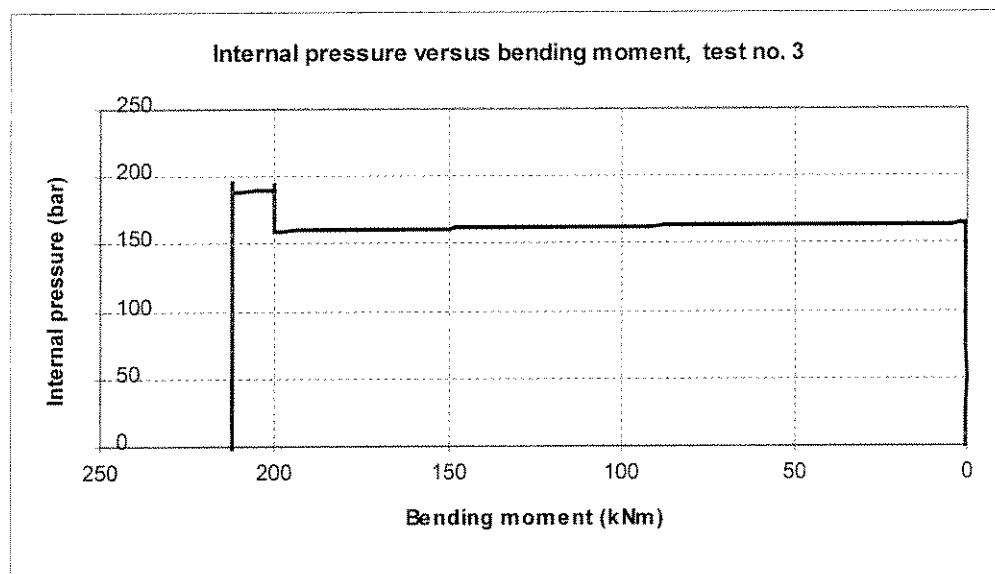


Figure 4-10 Internal pressure versus bending moment, test no. 3

**Results**

Excessive yielding was observed in the pipe before rupture in the corroded region. The test bursted at a bending moment of 212.5 kNm and an internal pressure of 195 bar.



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DETAILED DESCRIPTION OF THE TESTS

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**Figure 4-11** Picture of the test specimen no. 3 after the burst test

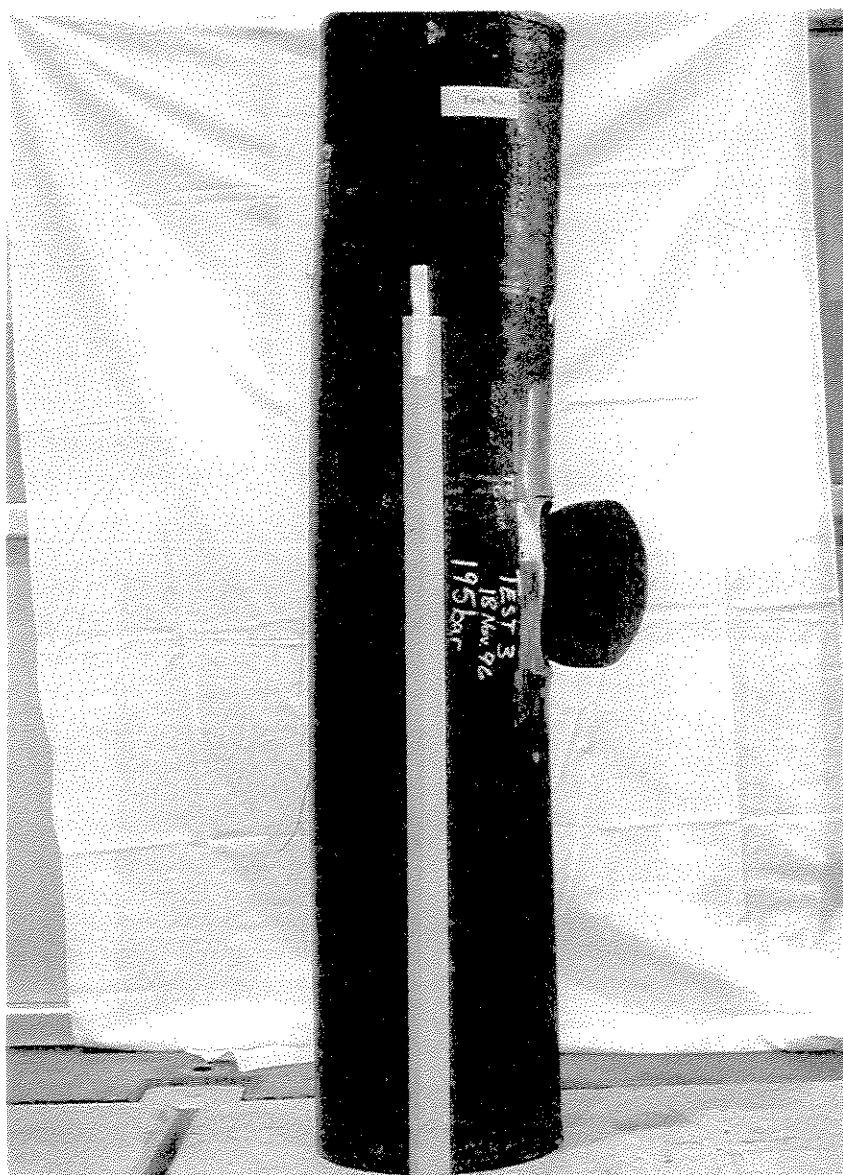


Figure 4-12 Picture of the test specimen no. 3 after the burst test



DETAILED DESCRIPTION OF THE TESTS



Figure 4-13 Picture of the test specimen no. 3 after the burst test





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**DETAILED DESCRIPTION OF THE TESTS**

---

## 4.5 Test no. 4

### Loading

Test specimen no. 4 was loaded with combined internal pressure and bending moment.

### Corrosion defect parameters (nominal)

Corrosion defect depth	$d = 3.2 \text{ mm}$ ( $d/t = 0.3$ )
Corrosion defect length	$L = 162 \text{ mm}$ ( $L/D = 0.50$ )
Corrosion defect width	$w = 32 \text{ mm}$ ( $w = 3 t$ )
Length of test specimen	$L_{\text{specimen}} = 1100 \text{ mm}$

### Instrumentation

In the corroded area 3 cross strain gauges were applied, and two gauges were applied away from the corroded area for load control of the bending moment. The time, rotation angle, the actuator load and displacement were also recorded

### Loading description

The specimen was exposed to combined internal pressure and 4-point-bending moment. The corrosion defect was located at the compressive side of the bending moment.

An internal pressure of 200 bar was applied during the first 15 minutes. The internal pressure was kept at 200 bar and bending was applied to the test specimen. When the moment exceeded 200 kNm the internal pressure started to drop due to excessive yielding of the pipe. The pipe had become soft and additional displacement was necessary in order to maintain the bending moment. Further, after excessive yielding the actuator reached the maximum stroke which resulted in that the tests changed from load (moment) controlled to displacement controlled. During the increase of internal pressure until burst at 290 bar the resulting bending moment decreased from 260 kNm to 73 kNm.

### Results

Excessive yielding was observed in the pipe before rupture in the corroded region. The test bursted at a bending moment of 73 kNm and an internal pressure of 290 bar. During the loading the test specimen had also been exposed to an internal pressure of approximately 200 bar and 250 kNm.



DETAILED DESCRIPTION OF THE TESTS

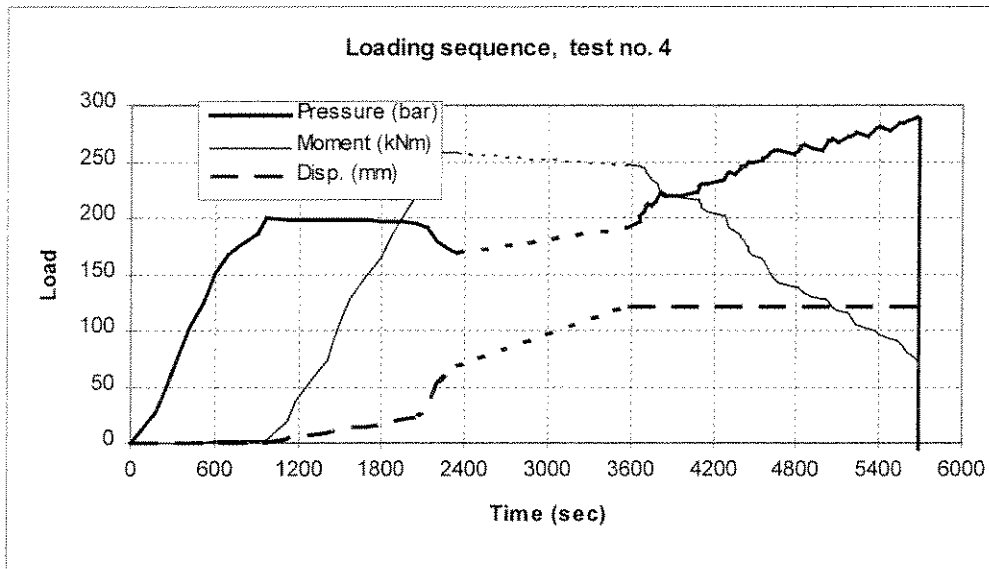


Figure 4-14 Loading sequence, test no.4

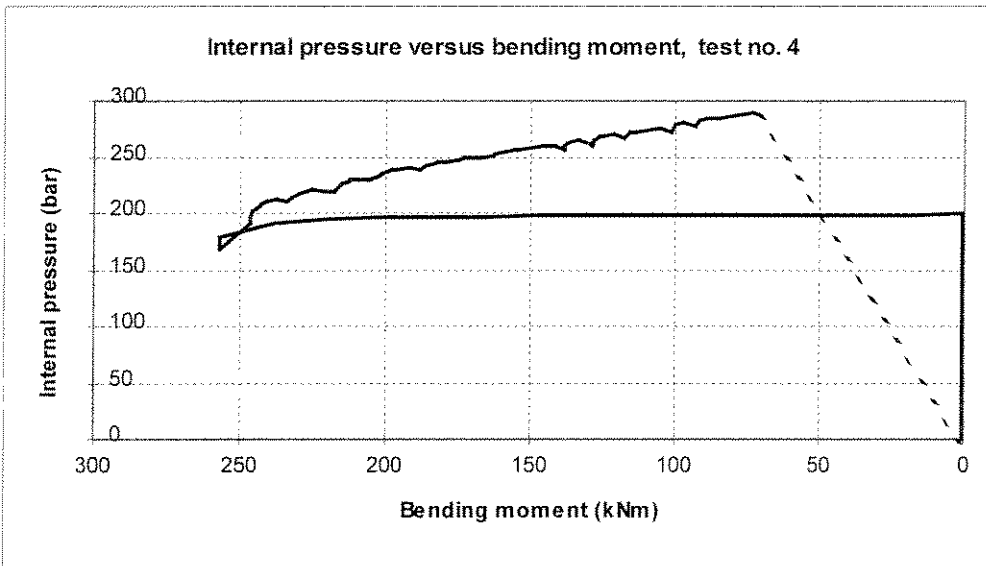
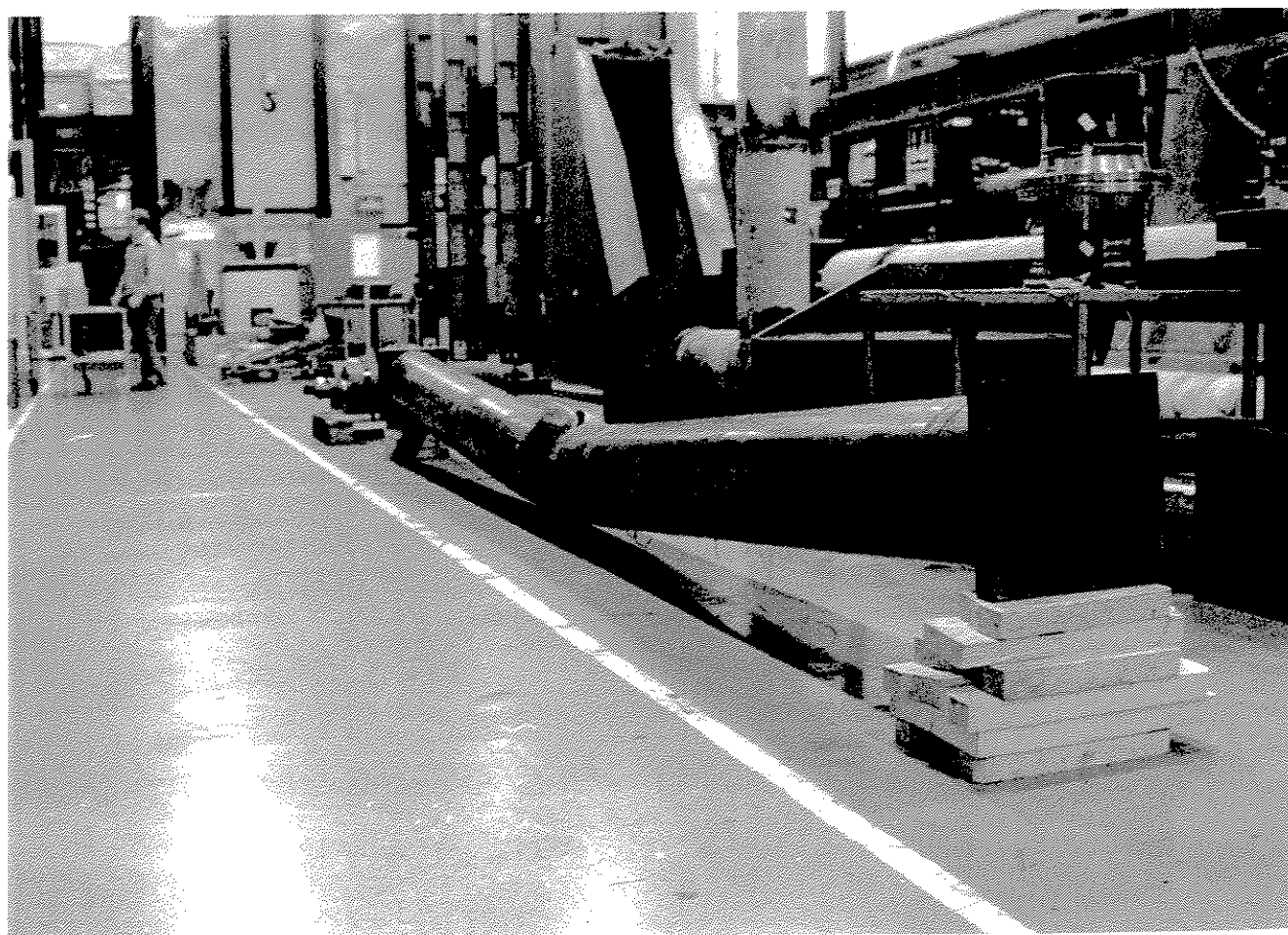


Figure 4-15 Internal pressure versus bending moment, test no. 4



**Figure 4-16** Picture of the test specimen no. 4 after the burst test



Figure 4-17 Picture of the test specimen no. 4 after the burst test



DETAILED DESCRIPTION OF THE TESTS



Figure 4-18 Picture of the test specimen no. 4 after the burst test




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 DETAILED DESCRIPTION OF THE TESTS
 

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## 4.6 Test no. 5

### Loading

Test specimen no. 5 was loaded with combined internal pressure and axial compressive force.

### Corrosion defect parameters (nominal)

(Identical with test no. 4)

Corrosion defect depth	$d = 3.2 \text{ mm}$ ( $d/t = 0.3$ )
Corrosion defect length	$L = 162 \text{ mm}$ ( $L/D = 0.50$ )
Corrosion defect width	$w = 32 \text{ mm}$ ( $w = 3 t$ )
Length of test specimen	$L_{\text{specimen}} = 1000 \text{ mm}$

### Instrumentation

In the corroded area 3 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded.

### Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

The jack was operated with a manually controlled pump, and during the test the load and the displacement were monitored. With this set-up the operator could manually maintain the axial force by running the pump, or stop the pump and keep the displacement constant.

For test no.5 an internal pressure of 200 bar was first applied, and then the axial compressive load. At approximately 2500 kN external applied axial force the pipe was yielding excessively, and the internal pressure dropped. The internal pressure was again increased to 200 bar, and further axial compressive load was applied, resulting again in a drop in the internal pressure. Both the internal pressure and the jack displacement was increased, but the resulting axial force decreased, until burst occurred at 286 bar and with an axial compressive external force of 2563 kN.

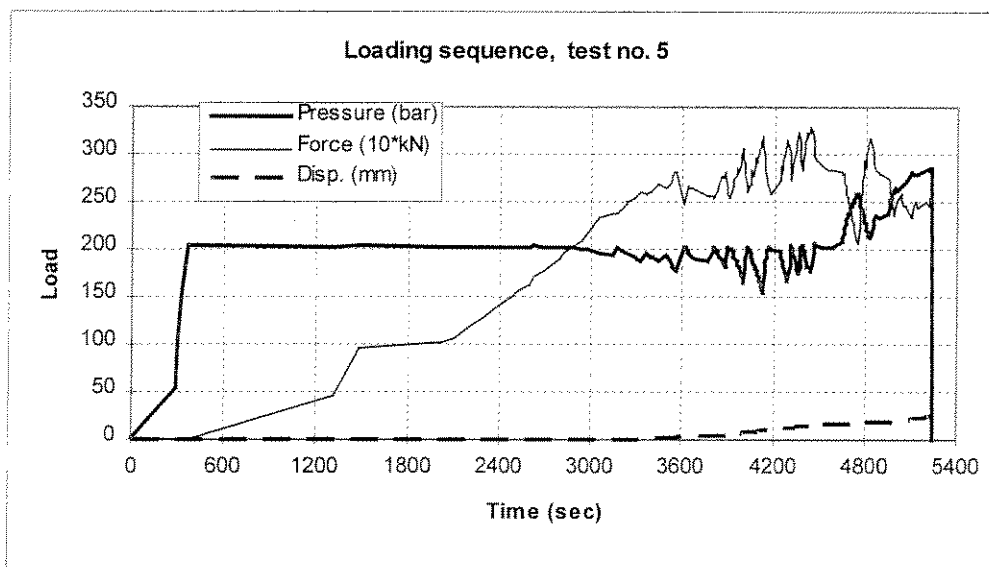


Figure 4-19 Loading sequence for test no. 5



DETAILED DESCRIPTION OF THE TESTS

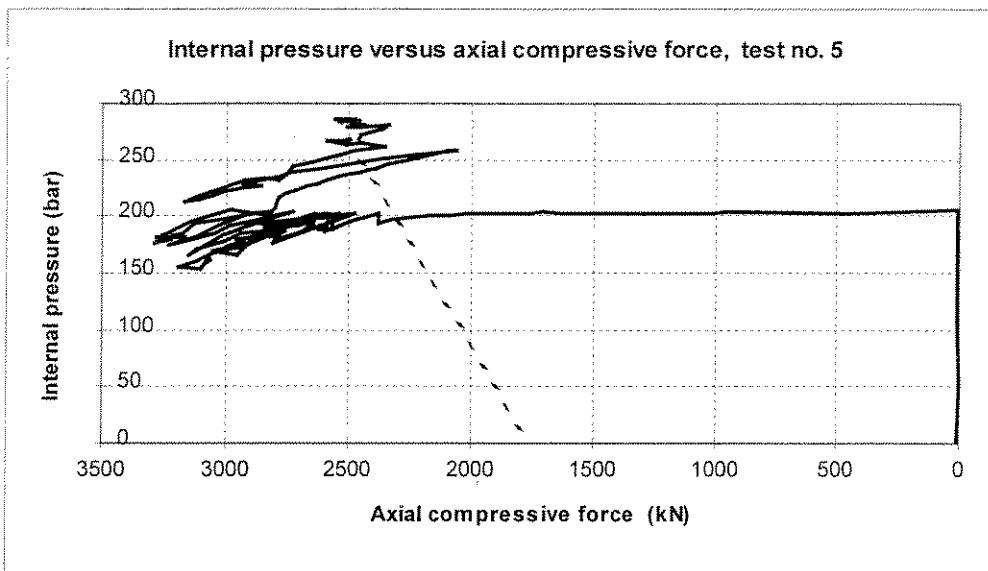


Figure 4-20 Internal pressure versus axial compressive force, test no. 5

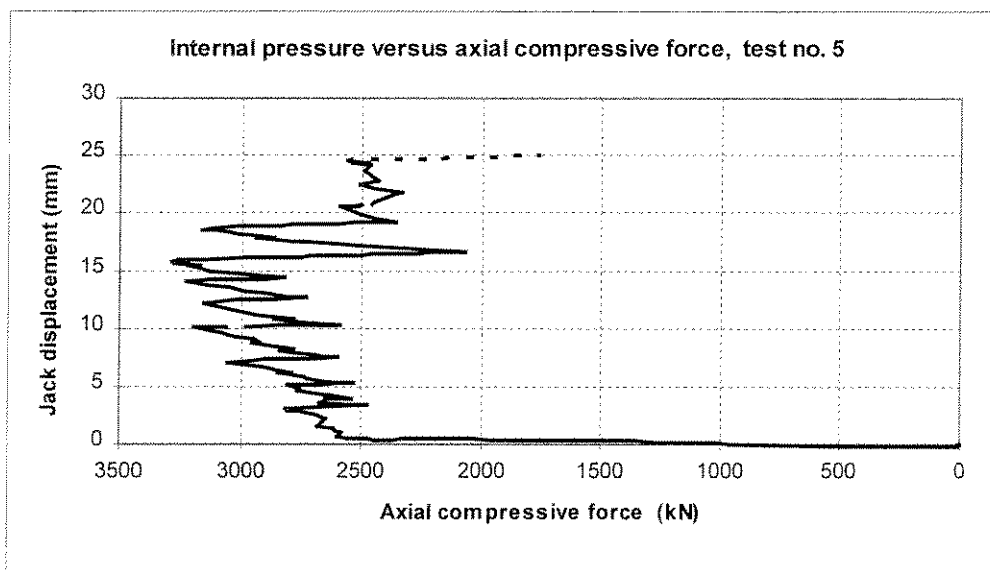


Figure 4-21 Jack displacement versus axial compressive force, test no. 5

**Results**

Excessive yielding was observed in the pipe before rupture in the corroded region occurred. The test bursted at an internal pressure of 286 bar, and with an axial compressive external force of 2563 kN. The end cap force due to the internal pressure was 2060 kN, resulting in a compressive pipe wall force of only 503 kN, equivalent to 48 MPa in axial compression.



DETAILED DESCRIPTION OF THE TESTS

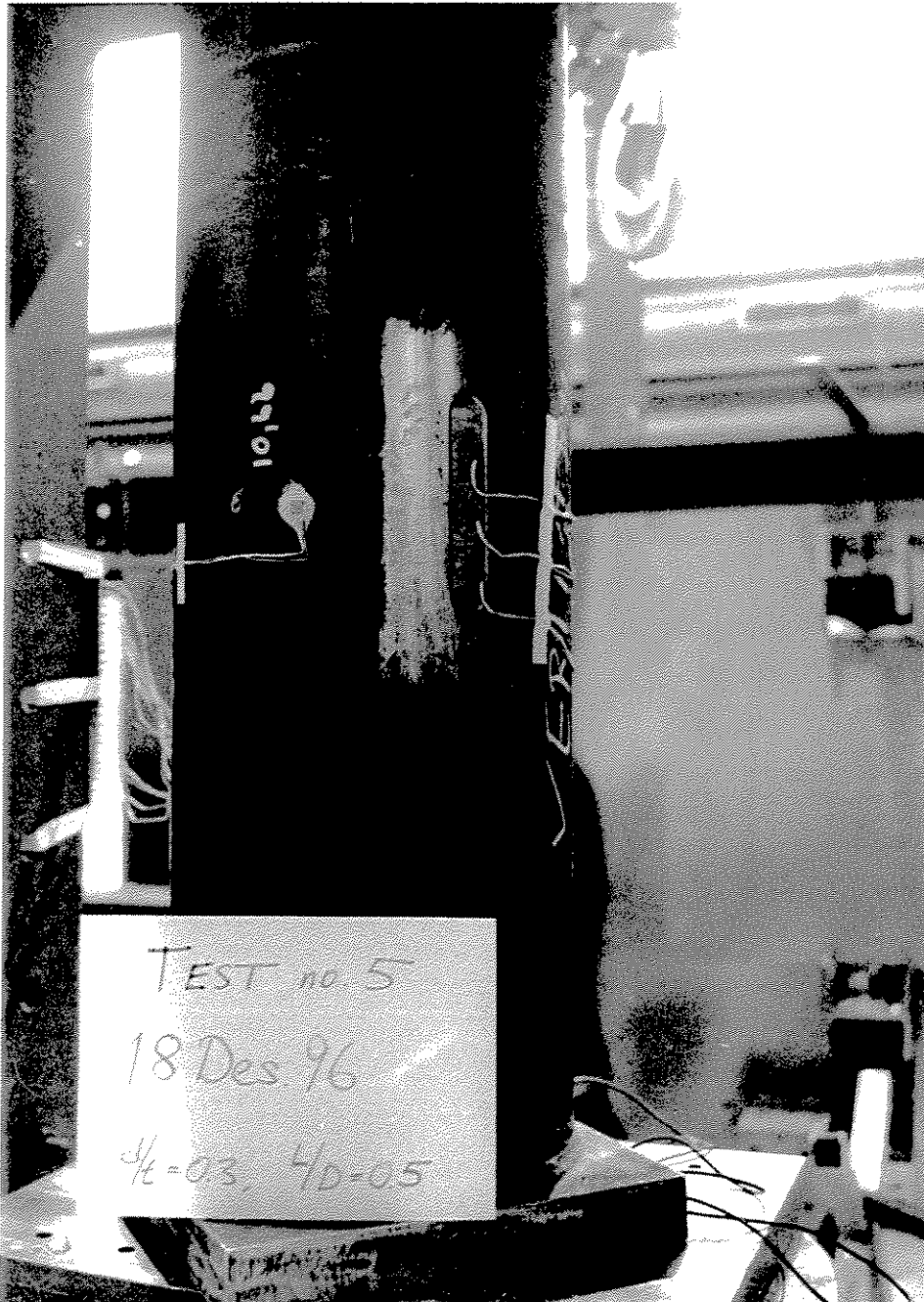


Figure 4-22 Picture of the test specimen no. 5 in the test rig before the burst test





DETAILED DESCRIPTION OF THE TESTS

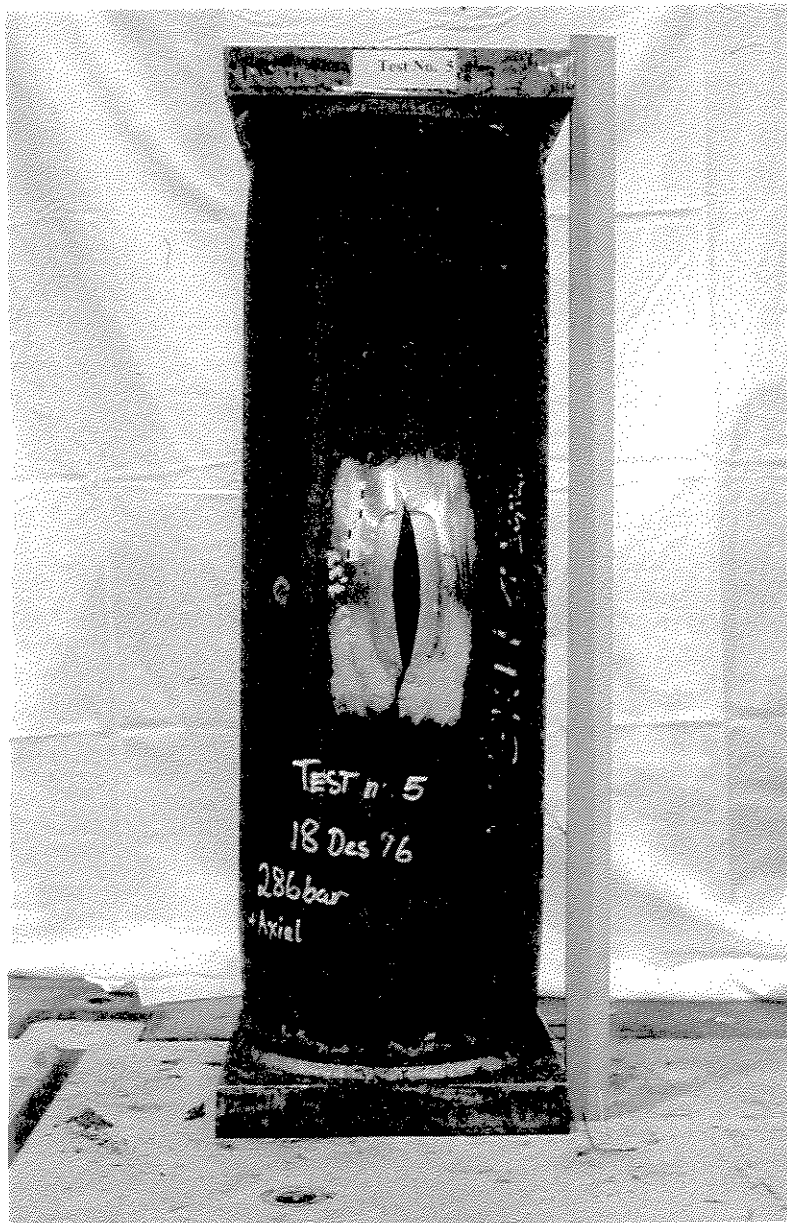


Figure 4-23 Picture of the test specimen no. 5 after the burst test



DETAILED DESCRIPTION OF THE TESTS



Figure 4-24 Picture of the test specimen no. 5 after the burst test




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 DETAILED DESCRIPTION OF THE TESTS
 

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## 4.7 Test no. 6

### Loading

Test 6 was loaded with combined internal pressure and axial compressive force.

### Corrosion defect parameters (nominal)

(Identical to test specimen no. 4 and 5)

Corrosion defect depth	$d = 3.2 \text{ mm}$ ( $d/t = 0.3$ )
Corrosion defect length	$L = 162 \text{ mm}$ ( $L/D = 0.50$ )
Corrosion defect width	$w = 32 \text{ mm}$ ( $w = 3 t$ )
Length of test specimen	$L_{\text{specimen}} = 1000 \text{ mm}$

### Instrumentation

In the corroded area 3 cross strain gauges were applied, and 4 gauges were applied in an uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded.

### Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

For test no.6 an internal pressure of 200 bar was first applied succeeded by axial compressive force. At approximately 2500 kN external axial force the pipe was yielding extensively, resulting in drop in the internal pressure. The internal pressure was maintained by pumping water simultaneously to the increase of the jack force to approximately 4300 kN. At this point the jack displacement was approximately 50 mm and the range of the displacement transducer was exceeded. The position of the transducer was changed, and due to safety reasons during this operation the test specimen was unloaded. The test specimen was reloaded to 200 bar, and further axial displacement/force was applied to the test. More excessive yielding was experienced, the pipe at the end supports started to deform, and in order to burst the pipe the internal pressure was increased when keeping the displacement constant allowing the axial compressive force to decrease.

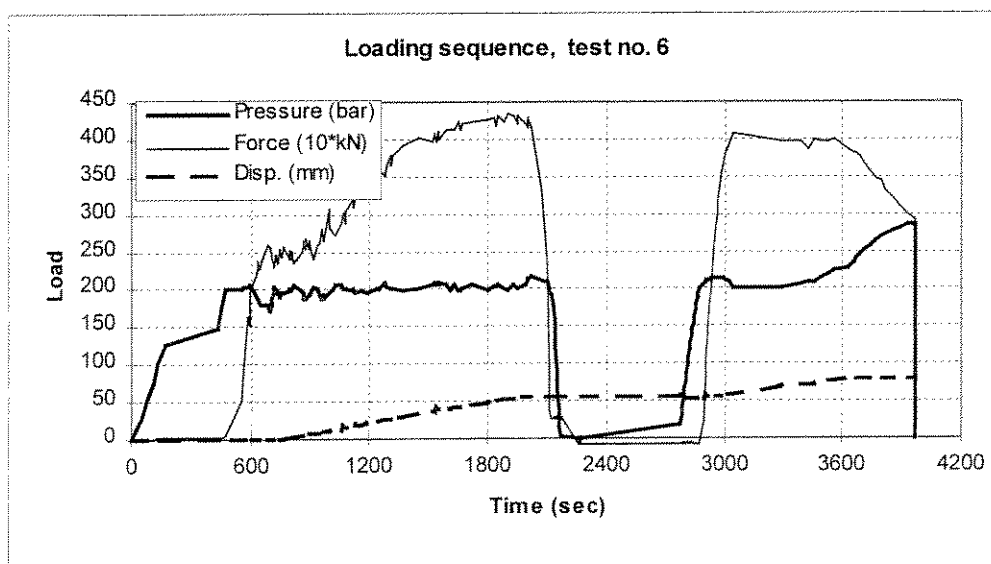


Figure 4-25 Loading sequence, test no. 6



DETAILED DESCRIPTION OF THE TESTS

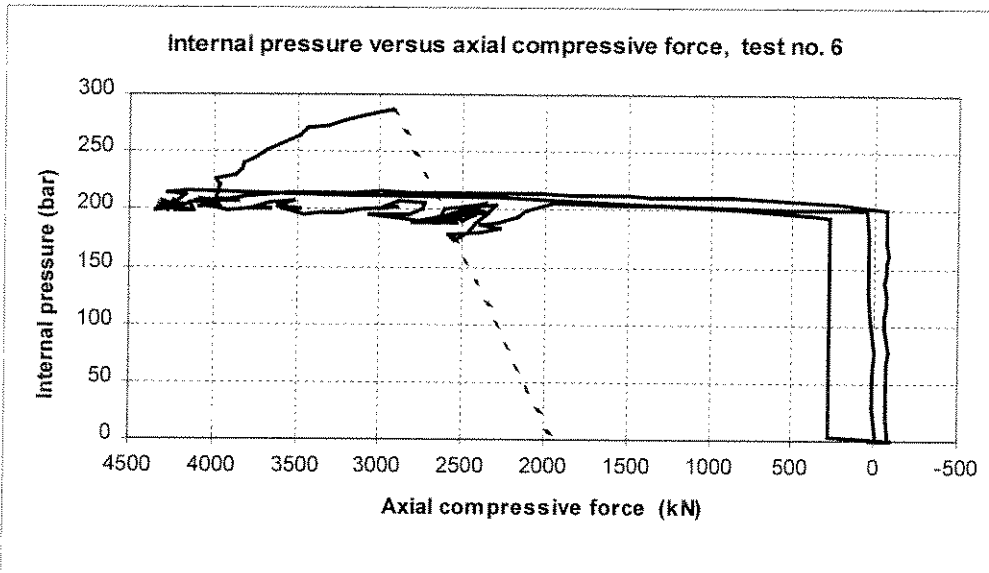


Figure 4-26 Internal pressure versus axial compressive force, test no. 6

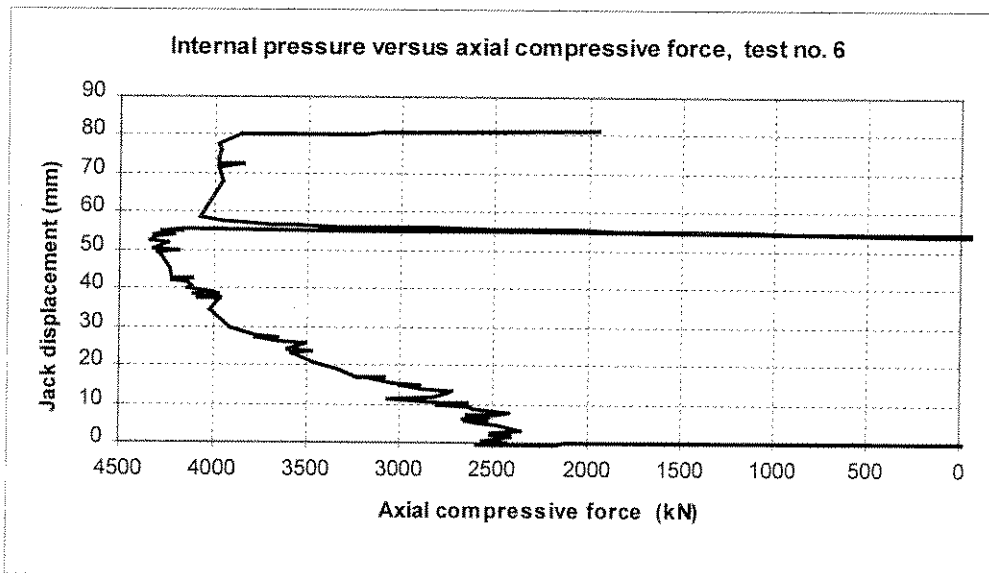


Figure 4-27 Jack displacement versus axial compressive force, test no. 6

**Results**

Excessive yielding was observed in the pipe before rupture in the corroded region. The test bursted at an internal pressure of 287 bar, and with an axial compressive external force of 2943 kN. The end-cap force due to the internal pressure was 2067 kN, resulting in a compressive pipe wall force of only 876 kN, equivalent to 84 MPa. The test specimen had during the test experienced 205 bar and 4323 kN.



DETAILED DESCRIPTION OF THE TESTS



Figure 4-28 Picture of the test specimen no. 6 after the burst test



DETAILED DESCRIPTION OF THE TESTS



Figure 4-29 Picture of the test specimen no. 6 after the burst test



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**DETAILED DESCRIPTION OF THE TESTS**

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## **4.8 Test no. 7**

### **Loading**

Test 7 was loaded with combined internal pressure and axial compressive force.

### **Corrosion defect parameters (nominal)**

Corrosion defect depth	$d = 5.3 \text{ mm}$ ( $d/t = 0.5$ )
Corrosion defect length	$L = 245 \text{ mm}$ ( $L/D = 0.75$ )
Corrosion defect width	$w = 32 \text{ mm}$ ( $w = 3 t$ )
Length of test specimen	$L_{\text{specimen}} = 1000 \text{ mm}$

The corrosion defect was longer and deeper compared to the test specimen no. 4, 5 and 6.

### **Instrumentation**

In the corroded area 3 cross strain gauges were used, and 4 gauges were applied in an uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded

### **Loading description**

The specimen was exposed to combined internal pressure and axial compressive force.

For test no.7 an internal pressure of 175 bar was applied, and succeeded by axial compressive load. At approximately 2500 kN axial force the pipe was yielding extensively and the internal pressure started to drop. The internal pressure was maintained simultaneously as the jack force was increased to approximately 3000 kN. The internal pressure was increased slightly while maintaining the axial force, until burst.

### **Results**

The specimen bursted at 186 bar and an axial force of 2998 kN.



DETAILED DESCRIPTION OF THE TESTS

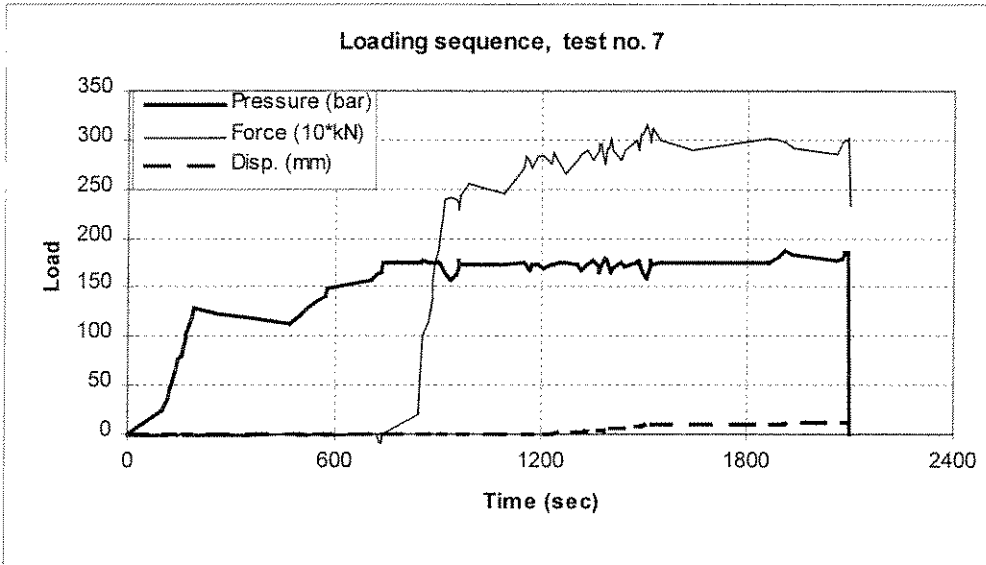


Figure 4-30 Loading sequence, test no. 7

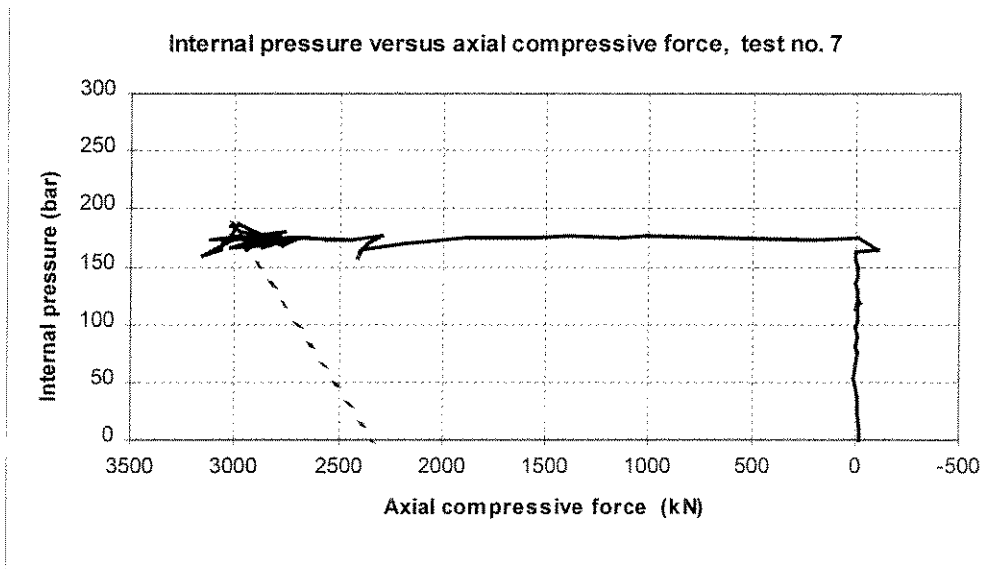


Figure 4-31 Internal pressure versus axial compressive force, test no. 7



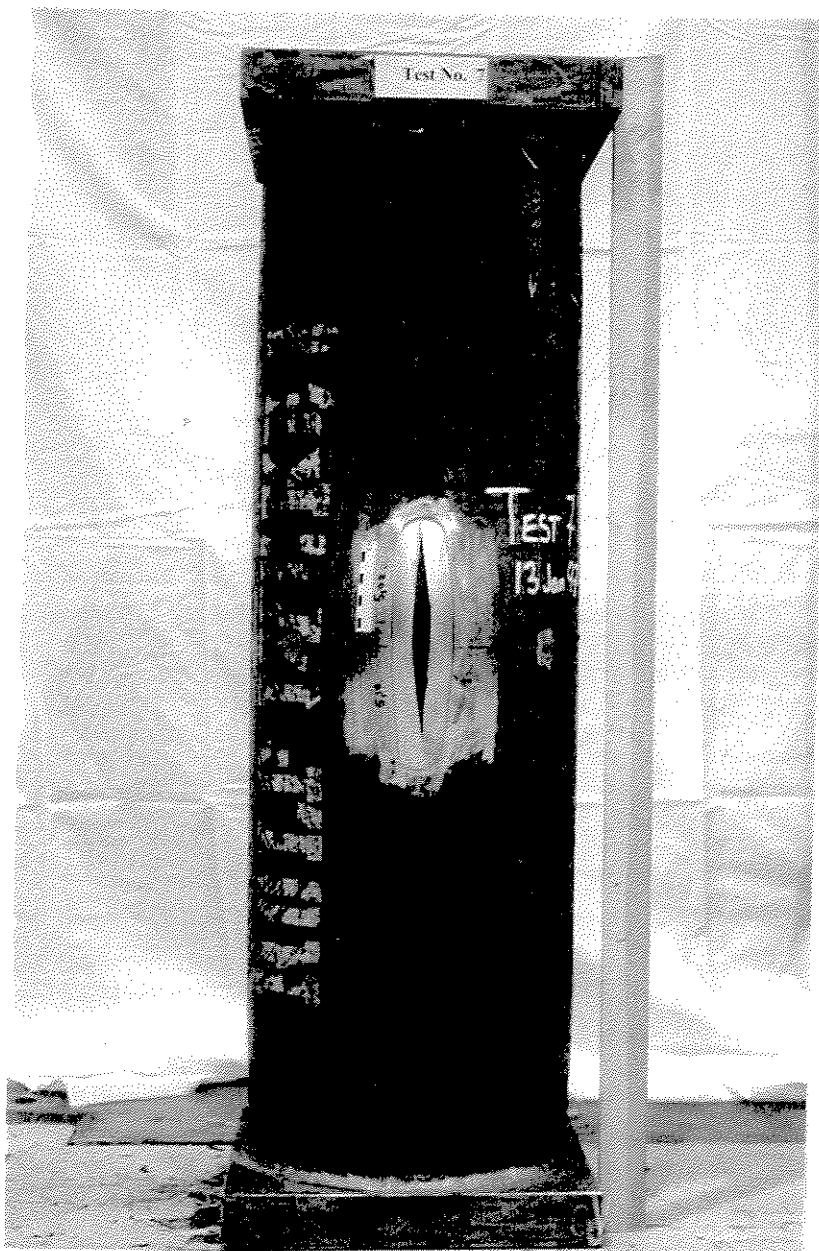


Figure 4-32 Picture of the test specimen no. 7 after the burst test



DETAILED DESCRIPTION OF THE TESTS

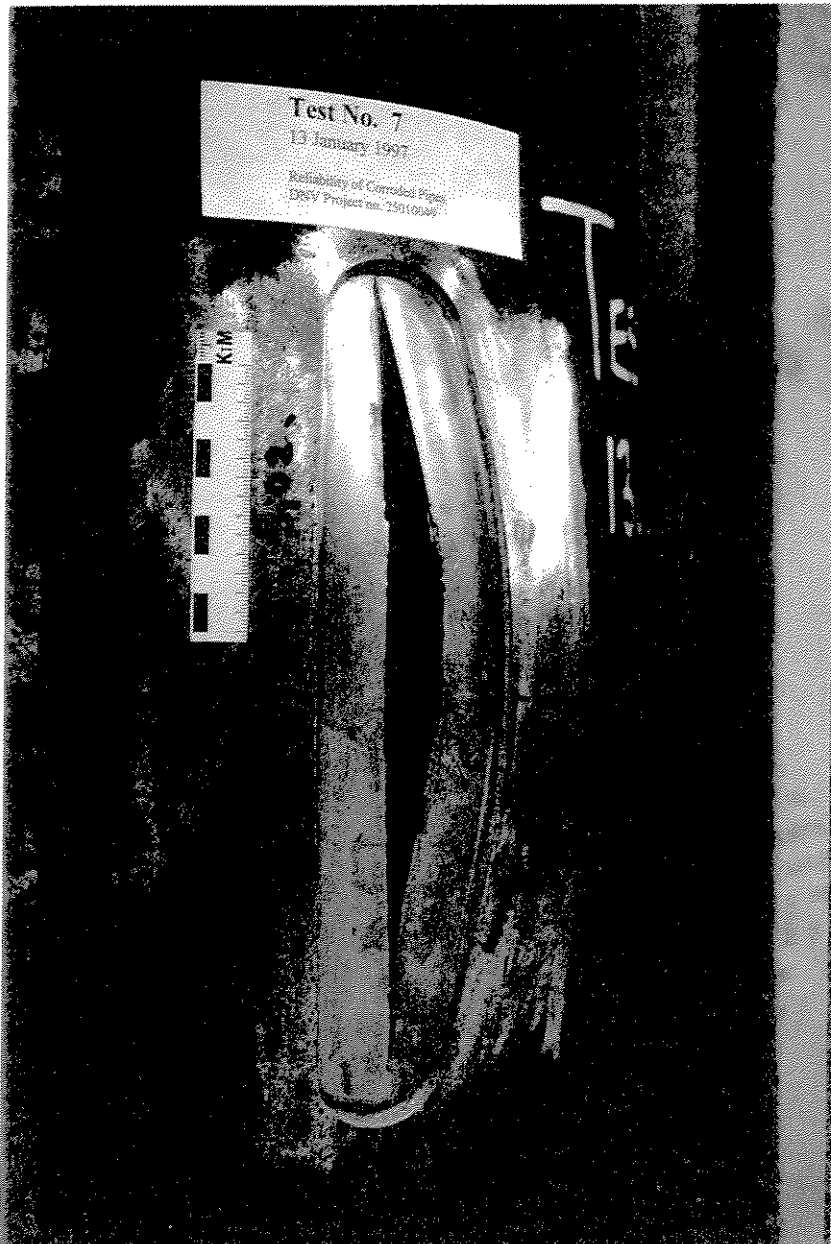


Figure 4-33 Picture of the test specimen no. 7 after the burst test




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 DETAILED DESCRIPTION OF THE TESTS
 

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#### 4.9 Test no. 8

##### Loading

Test no. 8 was loaded with internal pressure only.

##### Corrosion defect parameters (nominal)

(Identical to test specimen no. 7)

Corrosion defect depth	$d = 5.3 \text{ mm}$	$(d/t = 0.5)$
Corrosion defect length	$L = 245 \text{ mm}$	$(L/D = 0.75)$
Corrosion defect width	$w = 32 \text{ mm}$	$(w = 3 t)$
Length of test specimen	$L_{\text{specimen}} = 1000 \text{ mm}$	

##### Instrumentation

In the corroded area 3 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading.

##### Loading description

The specimen was exposed to internal pressure .

##### Results

The test specimen was loaded with internal pressure until burst at 220 bar.

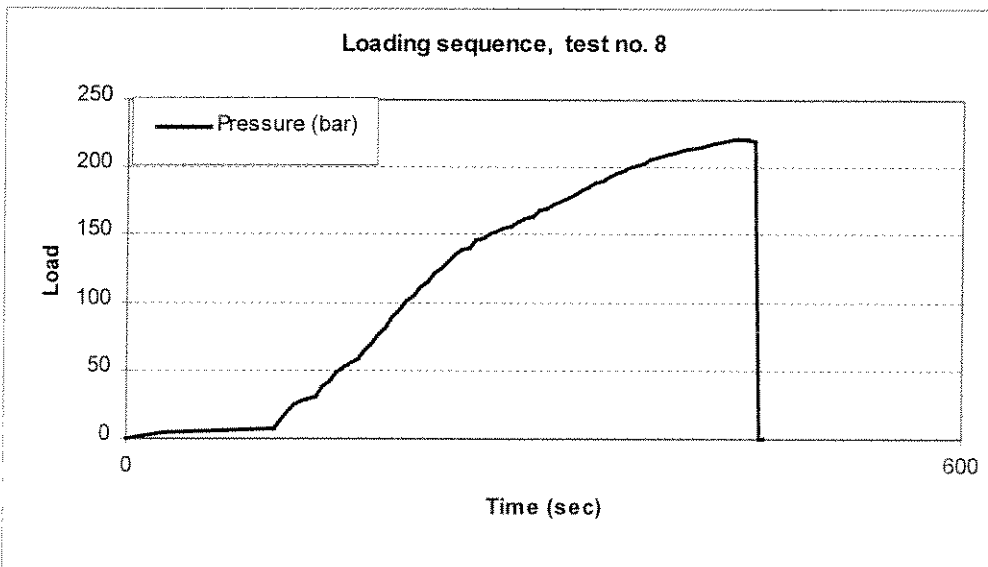


Figure 4-34 Loading of test no. 8, internal pressure only.



Figure 4-35 Picture of the test specimen no. 8 after the burst test



DETAILED DESCRIPTION OF THE TESTS

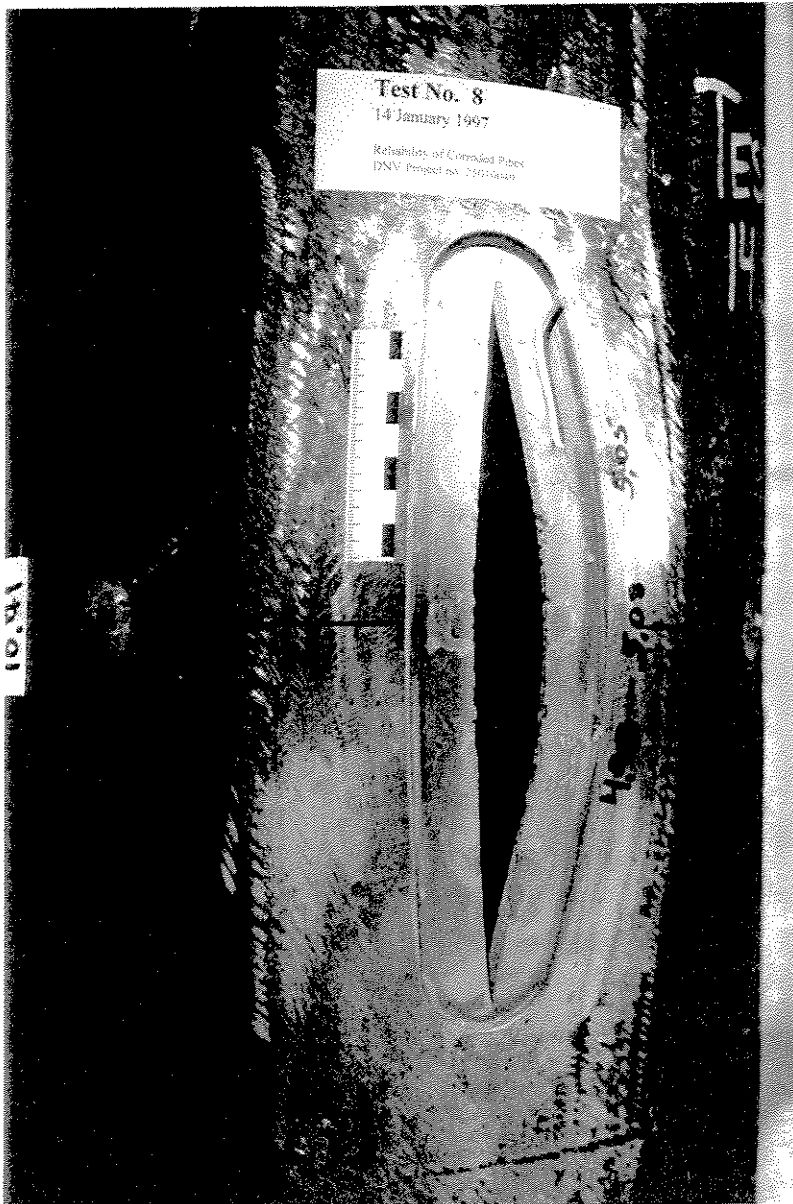


Figure 4-36 Picture of the test specimen no. 8 after the burst test



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**DETAILED DESCRIPTION OF THE TESTS**

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**4.10 Test no. 9****Loading**

Test 9 was loaded with combined internal pressure and axial compressive force.

**Corrosion defect parameters (nominal)**

Corrosion defect depth	$d = 7.5 \text{ mm}$ ( $d/t = 0.7$ )
Corrosion defect length	$L = 245 \text{ mm}$ ( $L/D = 0.75$ )
Corrosion defect width	$w = 32 \text{ mm}$ ( $w = 3 t$ )
Length of test specimen	$L_{\text{specimen}} = 1000 \text{ mm}$

**Instrumentation**

In the corroded area 3 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded

**Loading description**

The specimen was exposed to combined internal pressure and axial compressive force.

For test no.9 an internal pressure of 130 bar was applied, succeeded by axial compressive load was applied until burst. The internal pressure was 123 bar and the axial compressive force was 2070 kN at burst. The end-cap force due to the internal pressure was 886 kN, resulting in a compressive pipe wall force of only 1184 kN, equivalent to 113 MPa.

**Results**

The internal pressure was 123 bar and the axial compressive force was 2070 kN at burst.



DETAILED DESCRIPTION OF THE TESTS

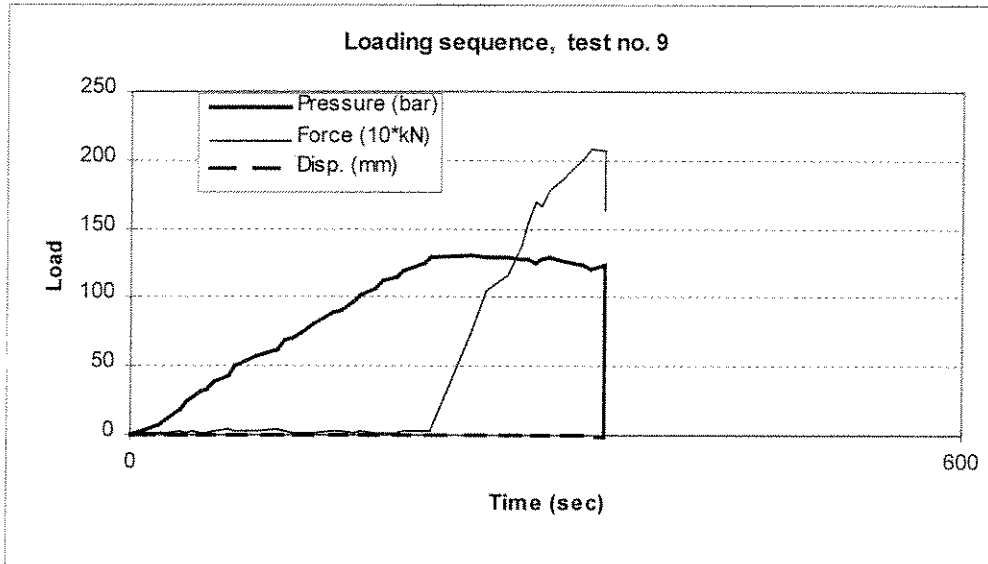


Figure 4-37 Loading sequence, test no. 9

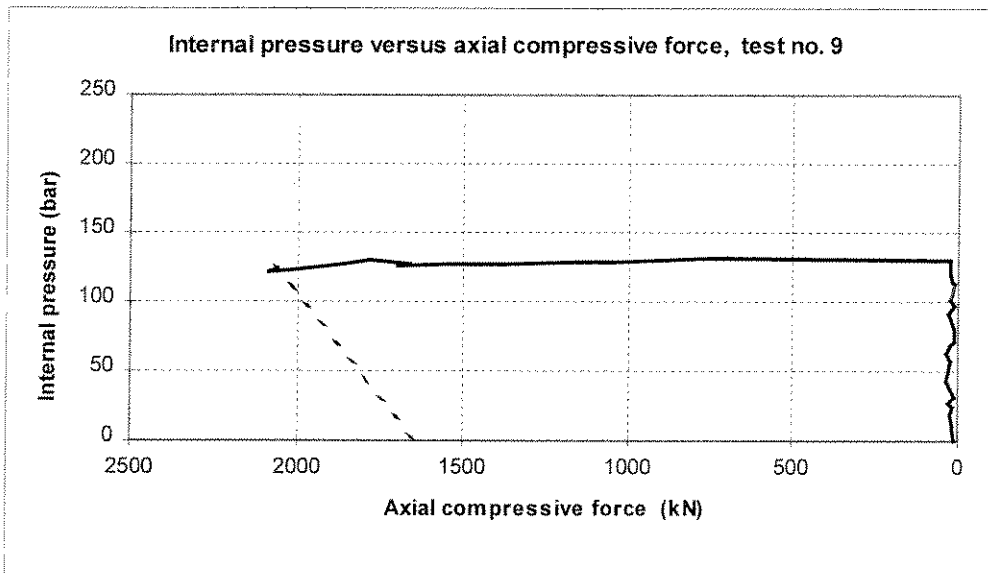


Figure 4-38 Internal pressure versus axial compressive force, test no. 9



DETAILED DESCRIPTION OF THE TESTS

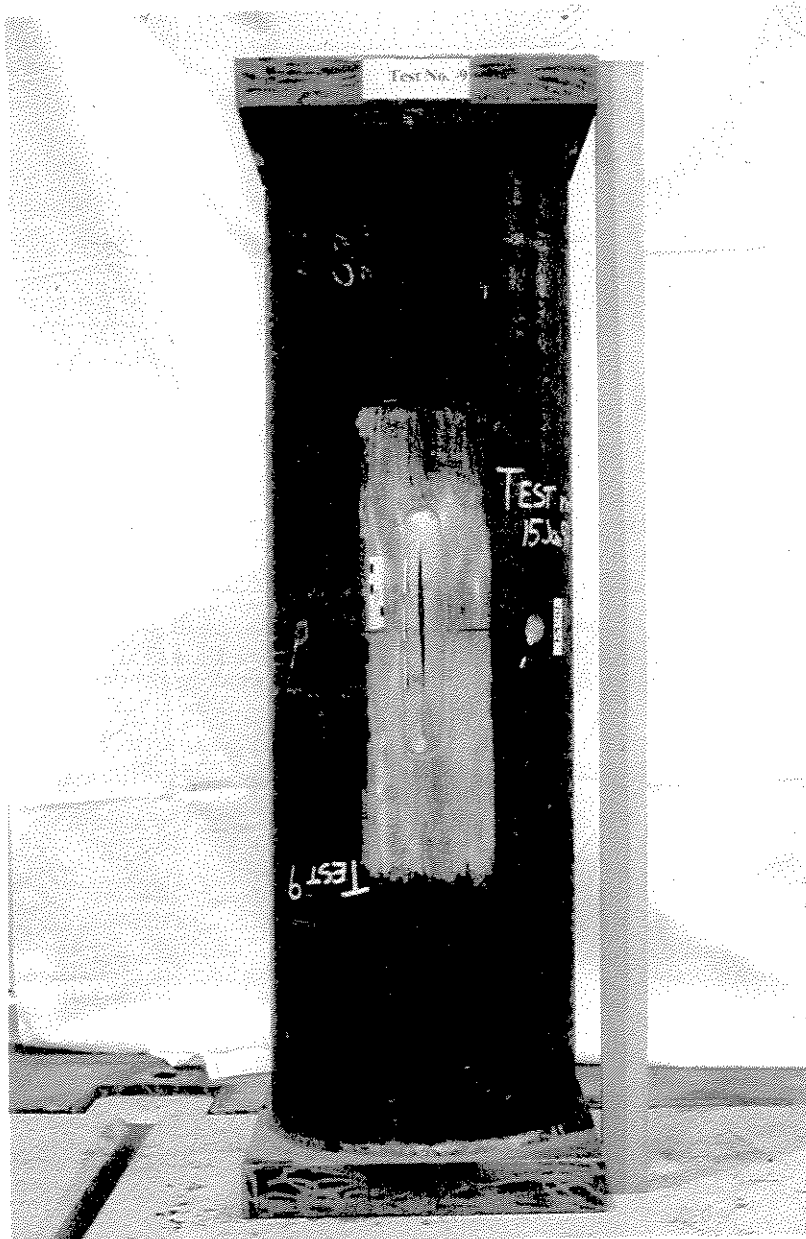


Figure 4-39 Picture of the test specimen no. 9 after the burst test





Figure 4-40 Picture of the test specimen no. 9 after the burst test



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**DETAILED DESCRIPTION OF THE TESTS**

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**4.11 Test no. 10****Loading**

Test 10 (and 11 and 12) were made with circumferential corrosion, and were loaded with combined internal pressure and axial compressive force.

**Corrosion defect parameters (nominal)**

Corrosion defect depth	$d = 5.3 \text{ mm}$ ( $d/t = 0.5$ )
Corrosion defect length	$L = 12 \text{ mm}$
Corrosion defect width	$w = \text{full circumference}$
Length of test specimen	$L_{\text{specimen}} = 1000 \text{ mm}$

A 12 mm wide ring groove was machined to 50% of the depth for the full circumference of the pipe at the outer surface to simulate girth weld corrosion. The groove was made in the parent material.

**Instrumentation**

In the corroded area (groove) 4 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded

**Loading description**

The specimen was exposed to combined internal pressure and axial compressive force.

Internal pressure was applied until burst and simultaneously an axial compressive force corresponding to the end cap force was applied. The resulting pipe wall force was close to zero. Burst occurred at 320 bar and an axial force of 2289 kN.

**Results**

Burst occurred at 320 bar and with an axial compressive force of 2289 kN. The rupture was in the longitudinal direction, even though the corrosion defect was in the circumferential direction.



DETAILED DESCRIPTION OF THE TESTS

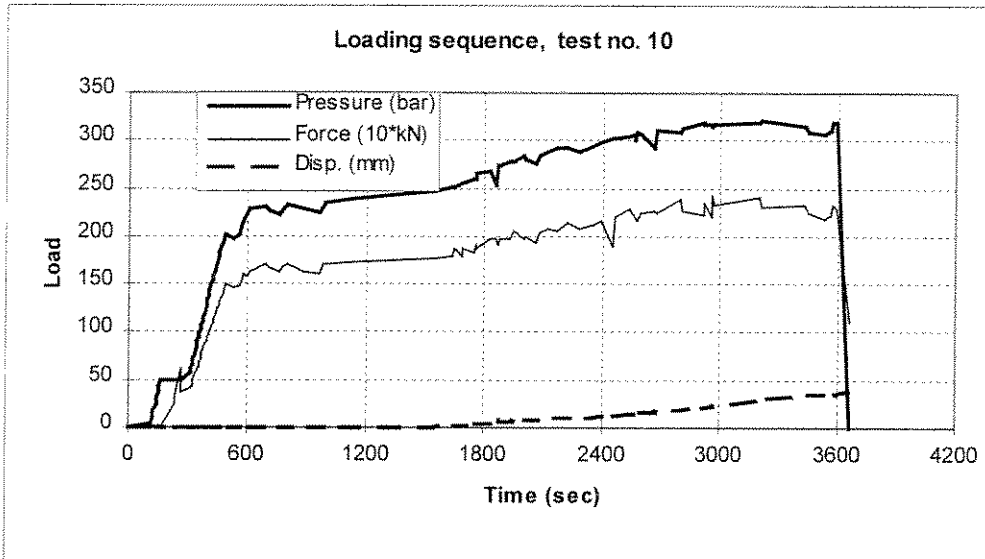


Figure 4-41 Loading sequence, test no. 10

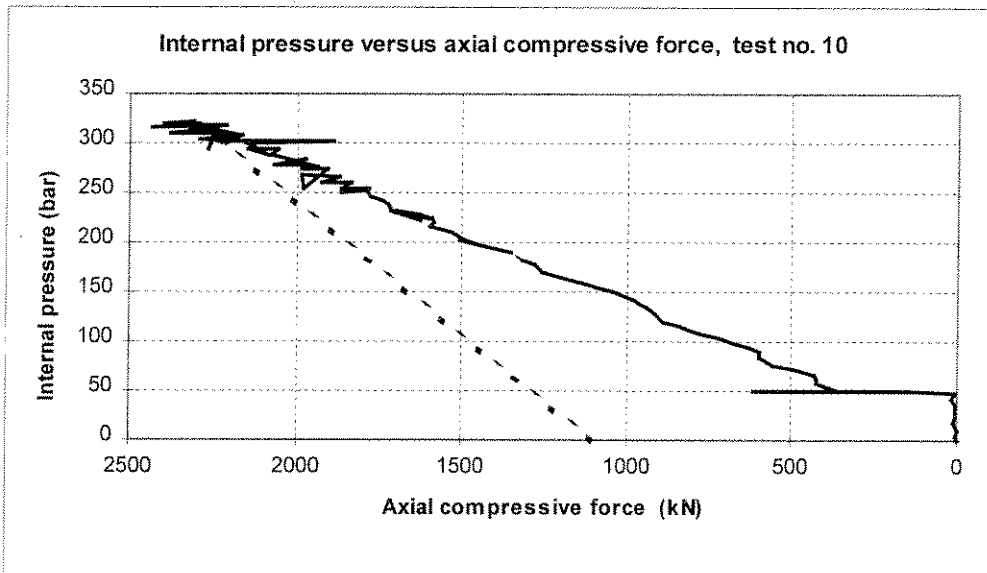


Figure 4-42 Internal pressure versus axial compressive force, test no. 10



Figure 4-43 Picture of the test specimen no. 10 after the burst test

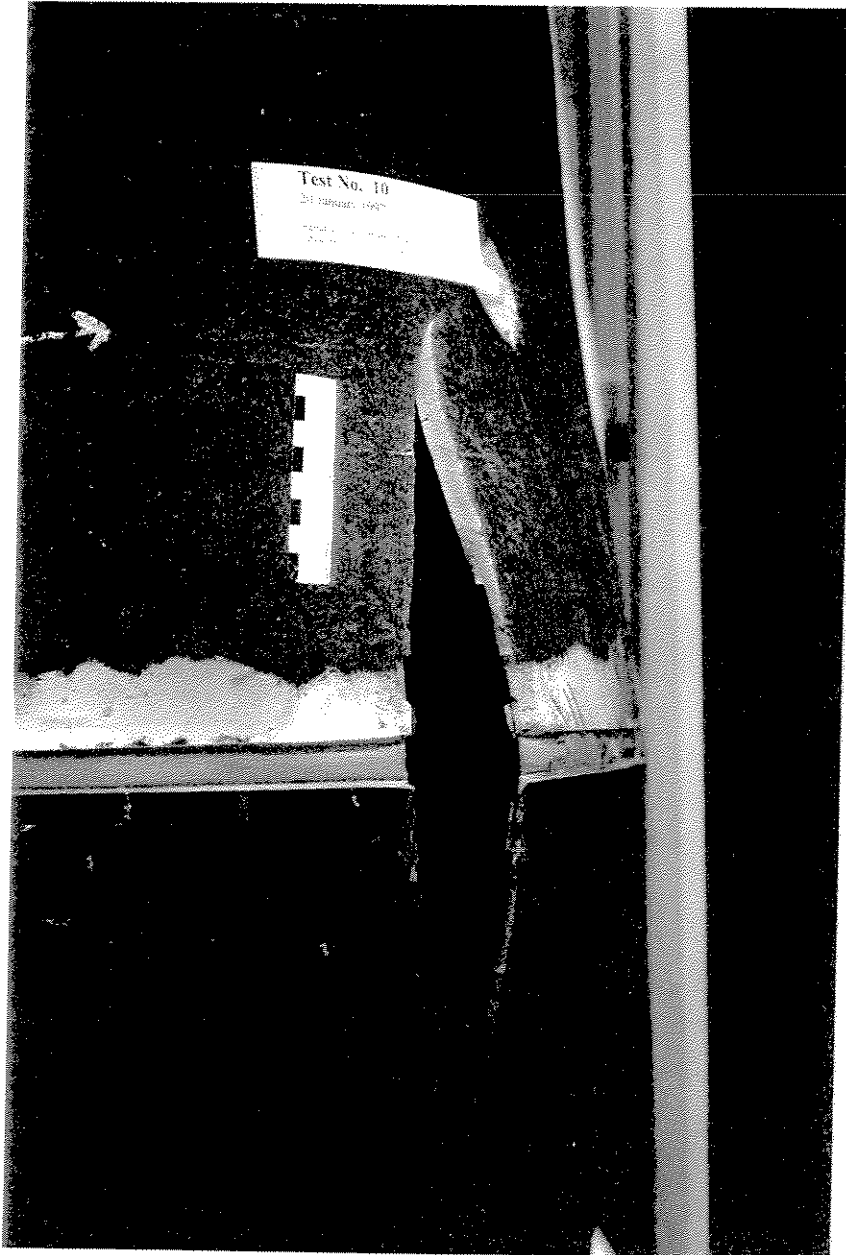


Figure 4-44 Picture of the test specimen no. 10 after the burst test



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**DETAILED DESCRIPTION OF THE TESTS**

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## 4.12 Test no. 11

### Loading

Test no. 11 was loaded with combined internal pressure and axial compressive force.

### Corrosion defect parameters (nominal)

(Identical with test specimen no. 10)

Corrosion defect depth  $d = 5.3 \text{ mm}$  ( $d/t = 0.5$ )

Corrosion defect length  $L = 12 \text{ mm}$

Corrosion defect width  $w = \text{full circumference}$

Length of test specimen  $L_{\text{specimen}} = 1000 \text{ mm}$

A 12 mm wide ring groove was machined to 50% of the depth for the full circumference of the pipe at the outer surface to simulate girth weld corrosion. The groove was made in the parent material.

### Instrumentation

In the corroded area (groove) 4 cross strain gauges were applied, and 4 gauges were applied in an uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded.

### Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

Internal pressure was applied simultaneously with an axial compressive force corresponding to the end cap force, hence the resulting pipe wall force was close to zero. The internal pressure was kept constant at 225 bar and only axial compressive force was applied up to 3800 kN. From this point additional internal pressure was applied and the axial force was tried maintained.

However, this required large displacements in the axial direction, and after 95 mm compression of the pipe the stroke limit of the jack was reached and the displacement was kept constant when further internal pressure was applied until burst. (The displacement transducer exceeded the measure range after 50 mm). This resulted in a drop in the axial load down to 2343kN when the pipe bursted at 335 bar.

### Results

Burst occurred at 335 bar and with an axial compressive force of 2345 kN. The rupture was in the longitudinal direction, even though the corrosion defect was in the circumferential direction.



DETAILED DESCRIPTION OF THE TESTS

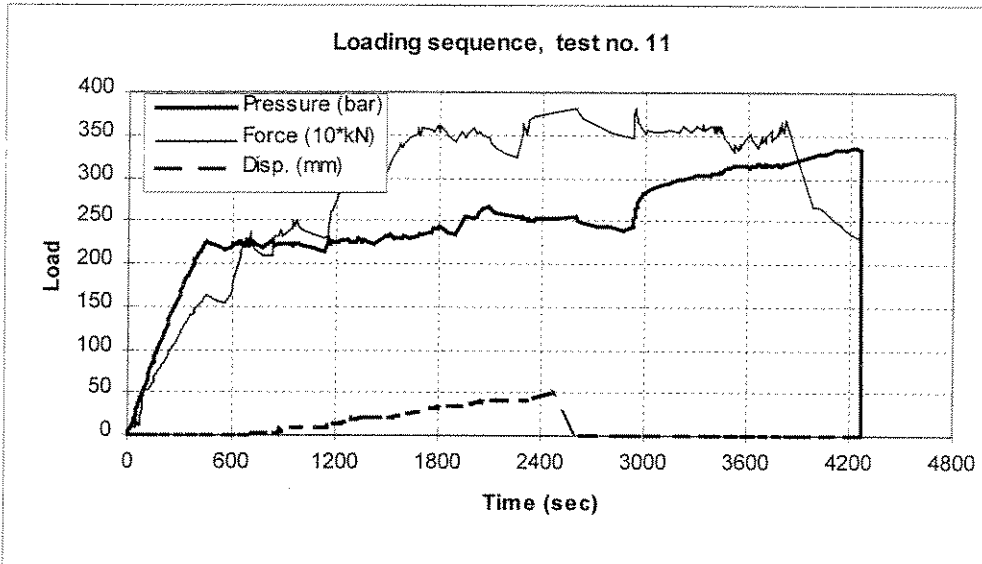


Figure 4-45 Loading sequence, test no. 11

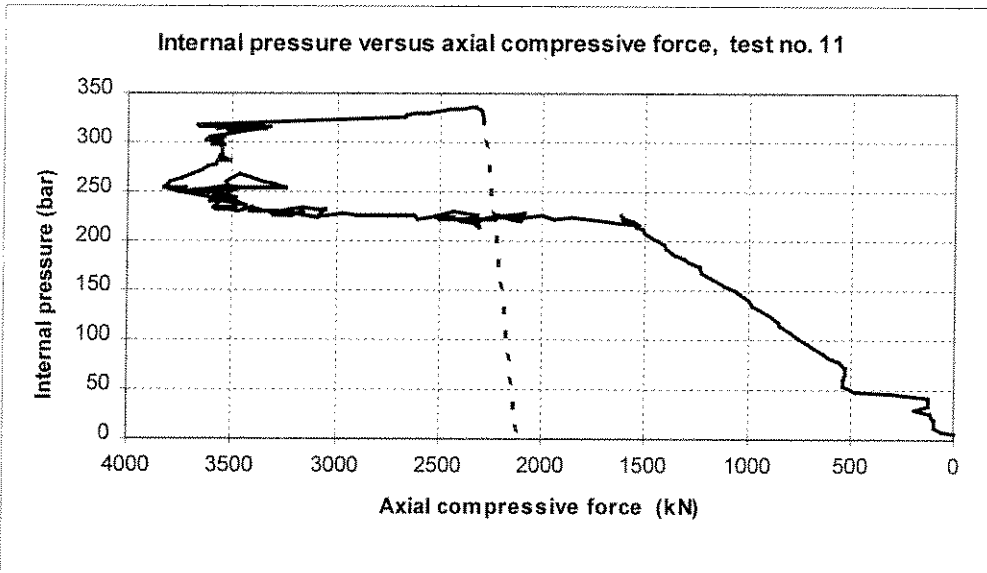
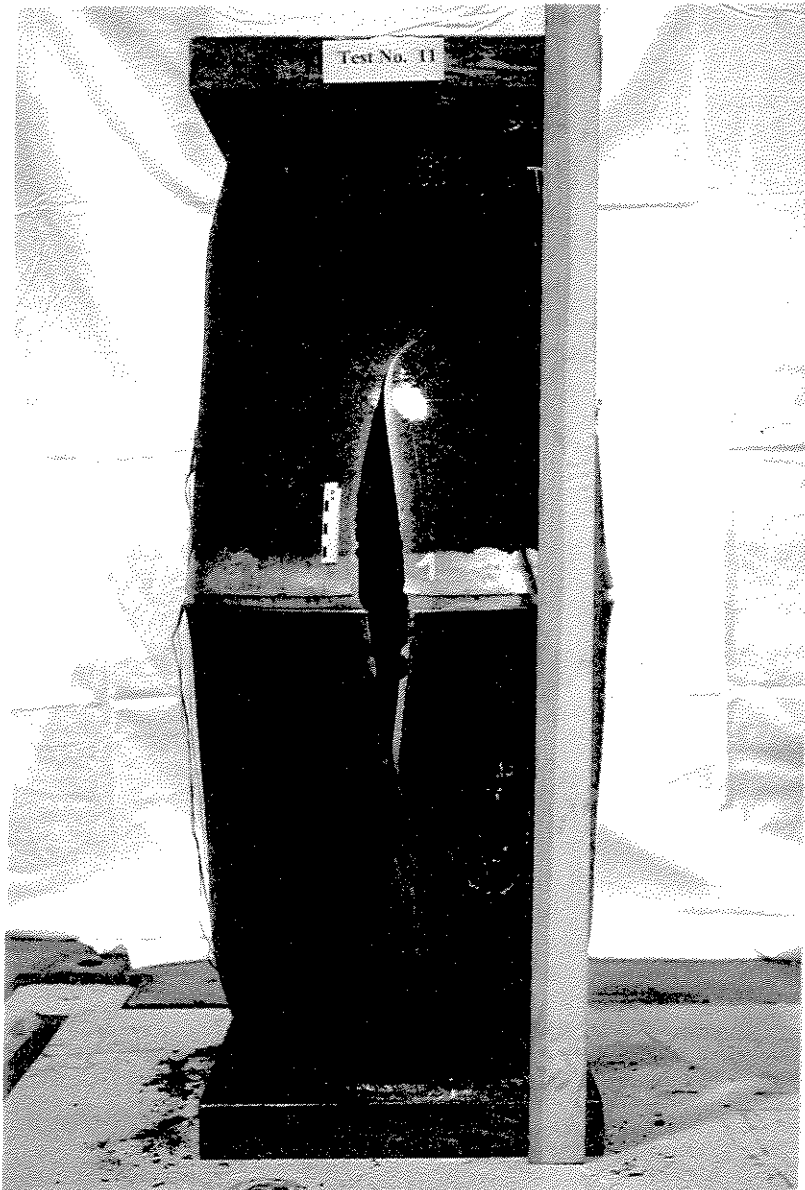
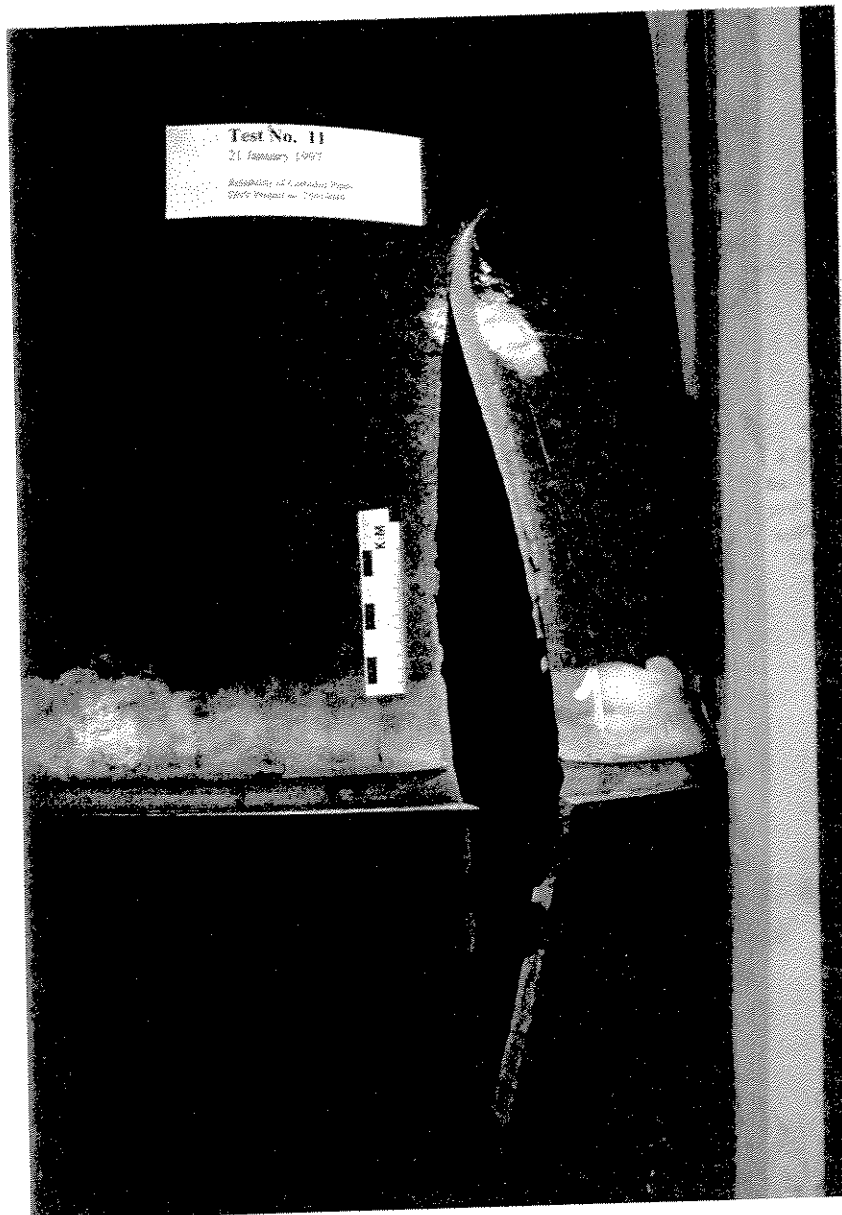
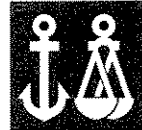


Figure 4-46 Internal pressure versus axial compressive force, test no. 11



**Figure 4-47** Picture of the test specimen no. 11 after the burst test





**Figure 4-48** Picture of the test specimen no. 11 after the burst test



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**DETAILED DESCRIPTION OF THE TESTS**

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**4.13 Test no. 12****Loading**

Test no. 12 was loaded with combined internal pressure and axial compressive force.

**Corrosion defect parameters (nominal)**

Corrosion defect depth	$d = 7.5 \text{ mm}$ ( $d/t = 0.7$ )
Corrosion defect length	$L = 12 \text{ mm}$
Corrosion defect width	$w = \text{full circumference}$
Length of test specimen	$L_{\text{specimen}} = 1000 \text{ mm}$

A 12 mm wide ring groove was machined to 70% of the depth for the full circumference of the pipe at the outer surface to simulate girth weld corrosion. The groove was made in the parent material.

**Instrumentation**

In the corroded area (groove) 4 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded.

Unfortunately, the recorded data were lost and only the data from the final part of the test were recovered based on the test log and (security) paper printout from the datalogger, which is the results of most interest.

**Loading**

The specimen was exposed to combined internal pressure and axial compressive force.

Internal pressure was applied simultaneously with an axial compressive force corresponding to the end cap force was applied. The resulting pipe wall force was close to zero. The internal pressure was kept constant at 250 bar and axial compressive force was applied up to 3250 kN. From this point additional internal pressure was applied and the axial force was tried maintained, but at further increase in the internal pressure the displacement was kept constant. This resulted in a drop in the axial load down to 2380 kN when the pipe bursted at 321 bar.

**Results**

The test specimen bursted at 321 bar with an axial compressive force of 2399 kN. The rupture was in the bottom of the groove with a length of 70 mm.



DETAILED DESCRIPTION OF THE TESTS

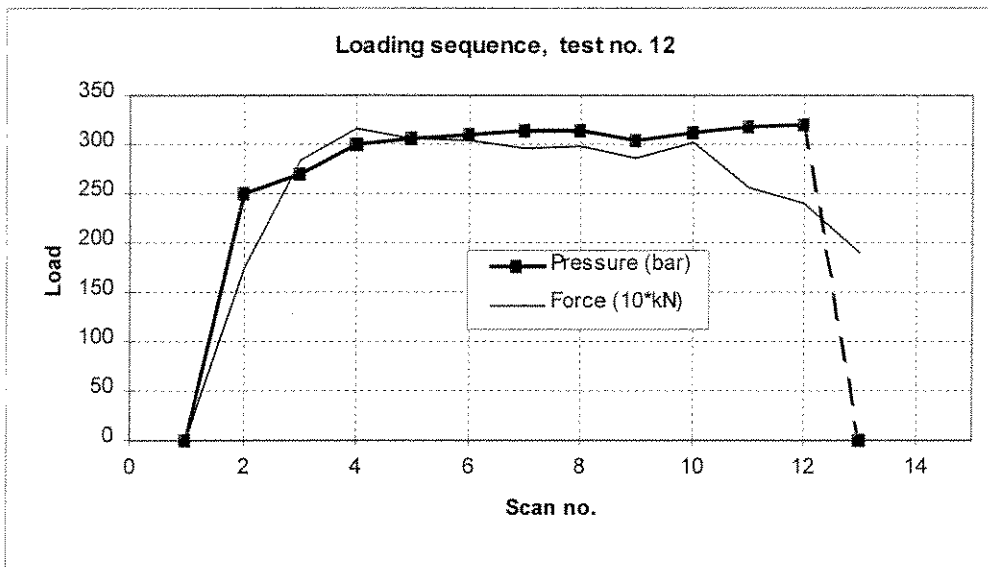


Figure 4-49 Loading sequence, test no. 12

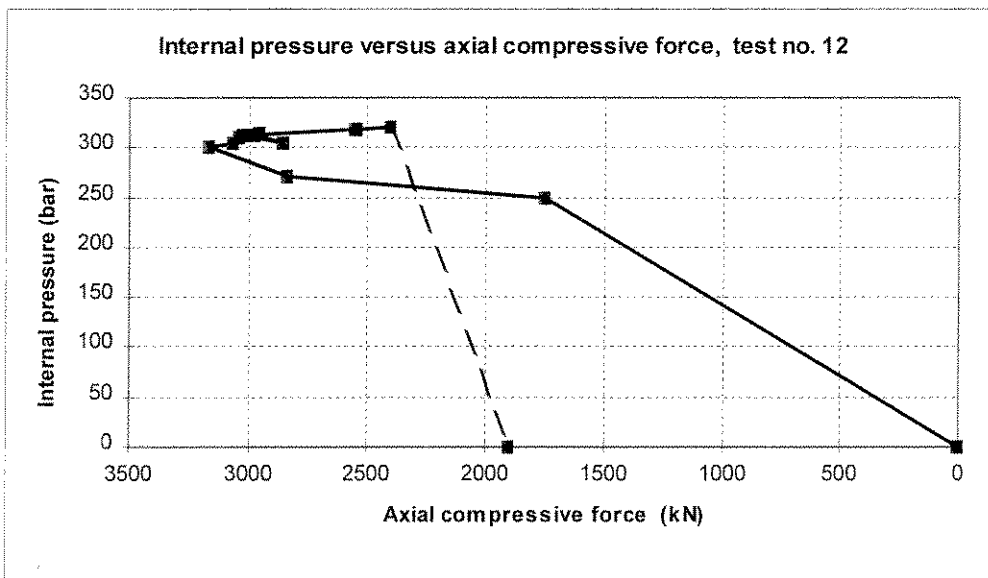


Figure 4-50 Internal pressure versus axial compressive force, test no. 12



DETAILED DESCRIPTION OF THE TESTS

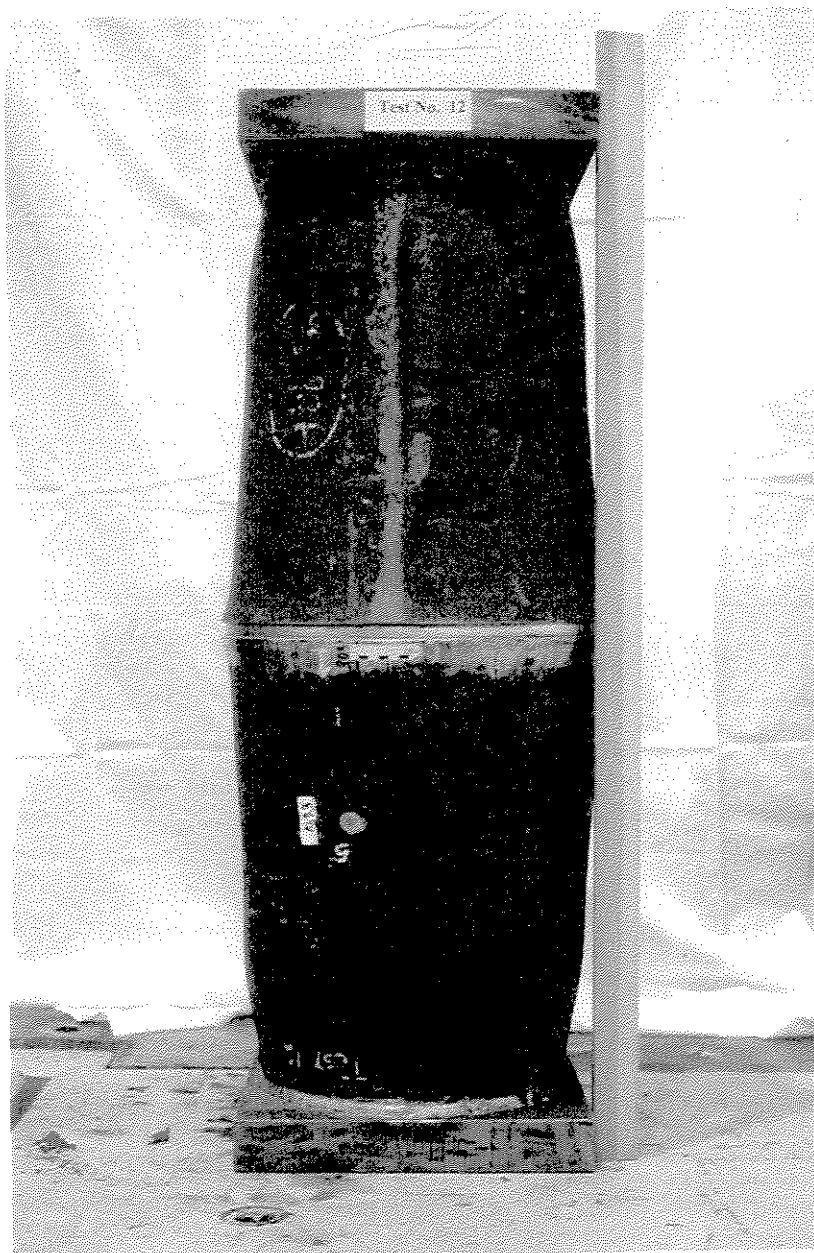


Figure 4-51 Picture of the test specimen no. 12 after the burst test



## SUMMARY OF TESTS AND TEST RESULTS

## 5 SUMMARY OF TESTS AND TEST RESULTS

### 5.1 Overview of test results

In Table 5-1 and Table 5-2 the main results from the tests are included. In Table 5-2 the loads are given in bot forces and stresses.

**Table 5-1 Overview of test results**

Test no.	Nom Dia (mm)	Nom thick (mm)	Mat	defect depth (d/t)	defect length L/D	defect width w/t	Loading	Date of test	Burst (press) (force/mom.)
1	324	10.3	X52	0.50	0.75	15	internal press	1 July 1996	232 bar 0
2	324	10.3	X52	0.50	0.75	15	internal press and bending moment	7 Aug. 1996	219 bar 129 kNm
3	324	10.3	X52	0.50	0.75	15	internal press and bending moment	18 Oct. 1996	195 bar 212 kNm
4	324	10.3	X52	0.30	0.50	3	internal press and bending moment	20 Nov. 1996	290 bar 73 kNm
5	324	10.3	X52	0.30	0.50	3	internal pressure and axial comp. force	18 Des. 1996	286 bar -2563 kN
6	324	10.3	X52	0.30	0.50	3	internal pressure and axial comp. force	7 Jan. 1997	287 bar -2943 kN
7	324	10.3	X52	0.50	0.75	3	internal pressure and axial comp. force	13 Jan. 1997	186 bar -2998 kN
8	324	10.3	X52	0.50	0.75	3	internal pressure	14 Jan. 1997	220 bar 0
9	324	10.3	X52	0.70	0.75	3	internal pressure and axial comp. force	15 Jan. 1997	123 bar -2070 kN
10	324	10.3	X52	0.50	12 mm	full circ.	internal pressure and axial comp. force	20 Jan. 1997	320 bar -2289 kN
11	324	10.3	X52	0.50	12 mm	full circ.	internal pressure and axial comp. force	21 Jan. 1997	335 bar -2343 kN
12	324	10.3	X52	0.70	12 mm	full circ.	internal pressure and axial comp. force	22 Jan. 1997	321 bar -2399 kN

The forces given in the table are external applied axial compressive forces measured in the jack. See Table 5-2 for more details of the loads.

For the tests with bending moment the corrosion defect was located on the side of the pipe with compressive axial stresses due to the moment.



## SUMMARY OF TESTS AND TEST RESULTS

**Table 5-2 Overview of test results**

Test no.	defect depth (d/t)	defect length L/D	defect width w/t	Loading	Burst 1) (press.) (force/mom.)	Pipe wall forces and stresses 2)	
						press. / force	pipe wall stresses
1	0.50	0.75	15	internal press	232 bar 0	232 bar 1668 kN	331MPa (hoop) 160 MPa (long.)
2	0.50	0.75	15	internal press and bending moment	219 bar 129 kNm	219 bar not given	312 MPa (hoop) -12 MPa (long.)
3	0.50	0.75	15	internal press and bending moment	195 bar 212 kNm	195 bar not given	278 MPa (hoop) -134 MPa (long.)
4	0.30	0.50	3	internal press and bending moment	290 bar 73 kNm	290 bar not given	412 MPa (hoop) 109 MPa (long.)
5	0.30	0.50	3	internal pressure and axial comp. force	286 bar -2563 kN	286 bar -503 kN	409 MPa (hoop) -48 MPa (long.)
6	0.30	0.50	3	internal pressure and axial comp. force	287 bar -2943 kN	287 bar -876 kN	410 MPa (hoop) - 84 MPa (long.)
7	0.50	0.75	3	internal pressure and axial comp. force	186 bar -3000 kN	186 bar -1659 kN	265 MPa (hoop) -159 MPa (long.)
8	0.50	0.75	3	internal pressure	220 bar 0	220 bar 1586 kN	314 MPa (hoop) 152 MPa (long.)
9	0.70	0.75	3	internal pressure and axial comp. force	123 bar -2070 kN	123 bar 1184 kN	176 MPa (hoop) -113 MPa (long.)
10	0.50	12 mm	full circ.	internal pressure and axial comp. force	320 bar -2289 kN	320 bar 10 kN	456 MPa (hoop) 1 MPa (long.)
11	0.50	12 mm	full circ.	internal pressure and axial comp. force	335 bar -2343 kN	335 bar 84 kN	479 MPa (hoop) 8 MPa (long.)
12	0.70	12 mm	full circ.	internal pressure and axial comp. force	321 bar -2399 kN	321 bar -94 kN	458 MPa (hoop) -9 MPa (long.)

Nominal diameter: 324 mm.

Nominal wall thickness: 10.3 mm.

- 1) The forces given in this column are external applied forces.
- 2) The forces given in these columns are pipe wall forces and stresses. The force is calculated as the force on the end-cap due to the internal pressure minus the applied external force on the jack.  
For tests exposed to bending moment, the pipe wall stress is given on the compressive side where the defect was located. The pipe wall forces are not given for the cases with bending moment.

The calculation of the stress is based on uncorroded and undeformed cross section. The average measured wall thickness of 10.6 mm is used (nominal 10.3mm).



## 6 MATERIAL PROPERTIES

The test specimens were manufactured from 2 tubes of seamless X52 modified material. A copy of the material certificates are included Appendix A. The test specimens 1 to 9 were made from one single tube, while the test specimens 10 to 12 were made from another tube. Tensile tests were conducted on four specimens machined from each tube to provide the required material parameters. The tensile test specimens were machined such that two had their axis in the longitudinal direction and two had their axis in the circumferential direction from each tube.

The tensile test specimens were manufactured with a diameter of 6 mm, and the length of each specimen was 50 mm. A 25 mm extensometer was fitted to each specimen.

The behaviour of specimens under tensile force showed a very good degree of consistency.

Plots of the axial tension as function of elongation are included in Appendix B.

The material average engineering properties were determined to be;

- Yield strength : 380 MPa
- Tensile strength: 514 MPa

Based on the plots included in Appendix B the “average” material curve is calculated as shown in Figure 6-1. Both the engineering and the true stress-strain material curve are given.

The material showed a yielding plateau at 380 MPa.

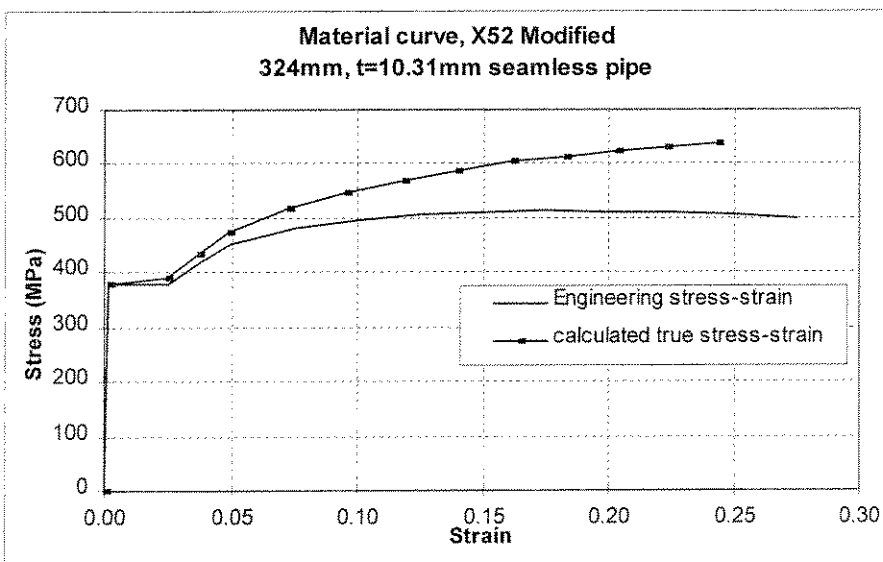


Figure 6-1 Material curve, X52 modified



## MATERIAL PROPERTIES

The corresponding numbers are given in Table 6-1.

**Table 6-1 Material data**

Engineering stress-strain		Calculated true stress-strain	
strain	stress (MPa)	strain	stress (MPa)
0	0.0	0.000	0.0
0.0018	380.0	0.002	380.7
0.025	380.0	0.025	389.5
0.038	419.3	0.037	435.0
0.050	450.9	0.049	473.4
0.075	482.4	0.072	518.6
0.100	496.0	0.095	545.6
0.125	505.0	0.118	568.1
0.150	509.5	0.140	585.9
0.175	514.0	0.161	603.9
0.200	511.7	0.182	614.1
0.225	509.5	0.203	624.1
0.250	505.0	0.223	631.2
0.275	500.5	0.243	638.1

The true stress-strain curve is calculated from the engineering stress-strain curve;

$$\epsilon_{\text{true}} = \ln(1 + \epsilon_{\text{eng}})$$

$$\sigma_{\text{true}} = \sigma_{\text{eng}}(1 + \epsilon_{\text{eng}})$$

- o0o -



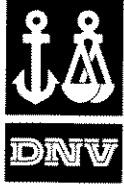
## **APPENDIX**

---

### **A**

### **DESCRIPTION OF THE TEST RIG, CORROSION DEFECTS, THICKNESS MEASUREMENTS AND INSTRUMENTATION**

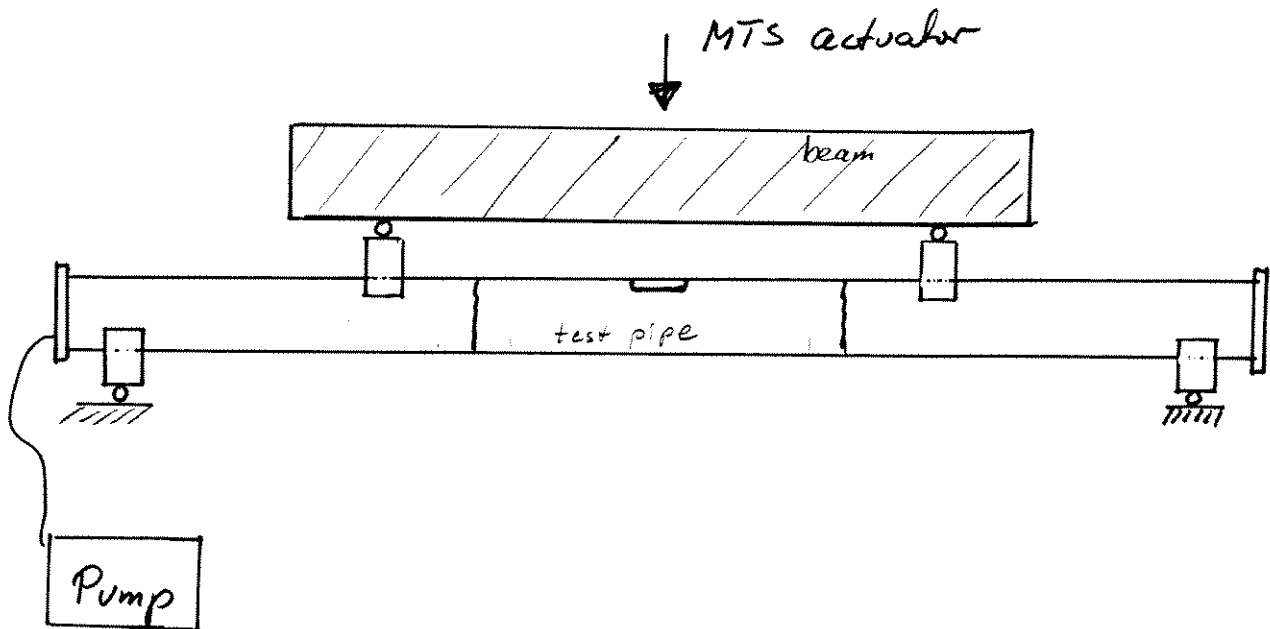
- 000 -



Project title:		Project No.:			
Client/Subject:	PREPARED	Date:	Sign.:	Doc. No.:	
	VERIFIED	Date:	Sign.:	Rev.:	Page:

Test set-up for combined internal pressure and 4-point bending moment.

(not to scale)





Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>			
Client/Subject: <i>Test 1, 2 and 3</i>	PREPARED	Date:	Sign.:	Doc. No.:	
	VERIFIED	Date:	Sign.:	Rev.:	Page:

Spark eroded defect for test no. 1, 2 and 3.

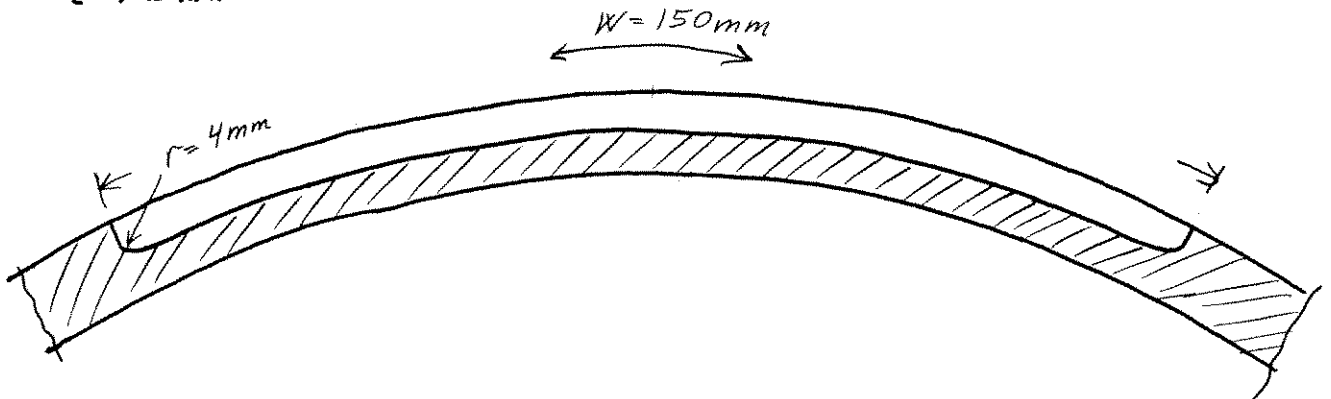
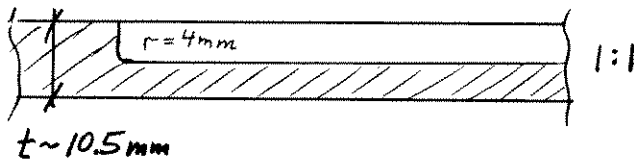
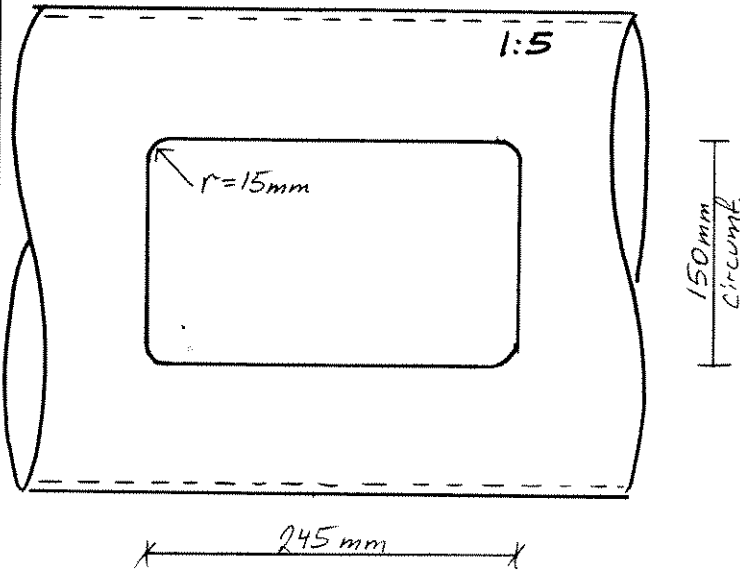
Dia = 324 mm

$t = \sim 10.5 \text{ mm}$

defect :  $d = \sim 5.3 \text{ mm}$  ( $d/t \sim 0.5$ )

$L = 245 \text{ mm}$  ( $L/D = 0.75$ )

$W = 150 \text{ mm}$  ( $W/t \sim 15$ )





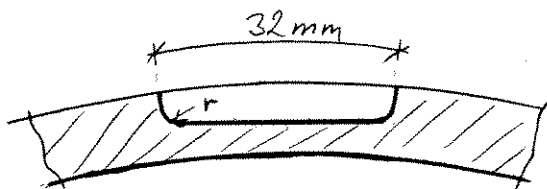
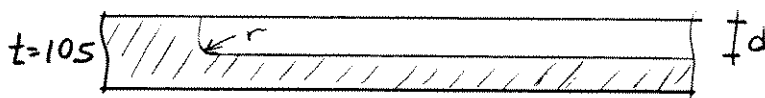
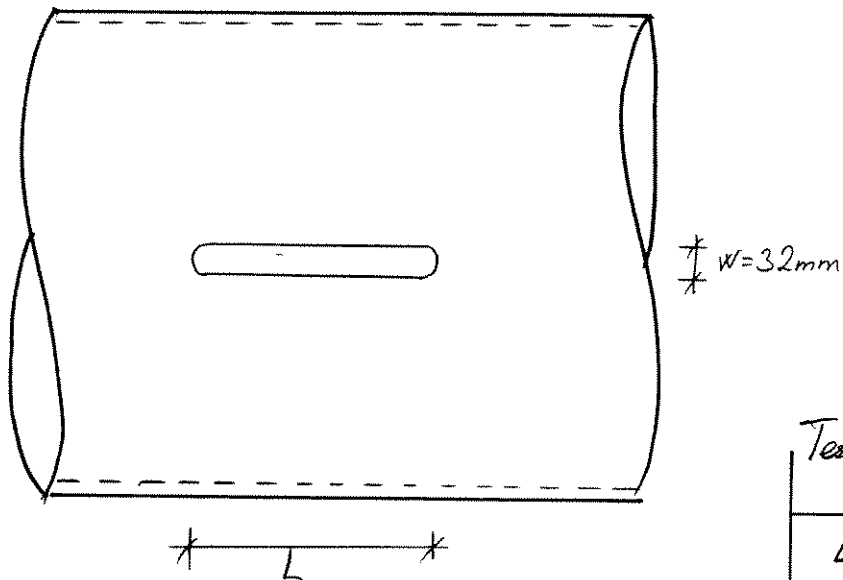
Project title: <i>Reliability of Corroded pipes</i>		Project No.: <i>25010049</i>	
Client/Subject:  <i>Test no. 4 to 9.</i>	PREPARED	Date:	Sign.:
	VERIFIED	Date:	Sign.:
		Doc. No.:	Rev.:
			Page:

Spark eroded defects.

$D = 324\text{ mm}$  defect :  $d$  - various

$t \sim 10.5\text{ mm}$  :  $L$  - various

:  $w = 32\text{ mm}$

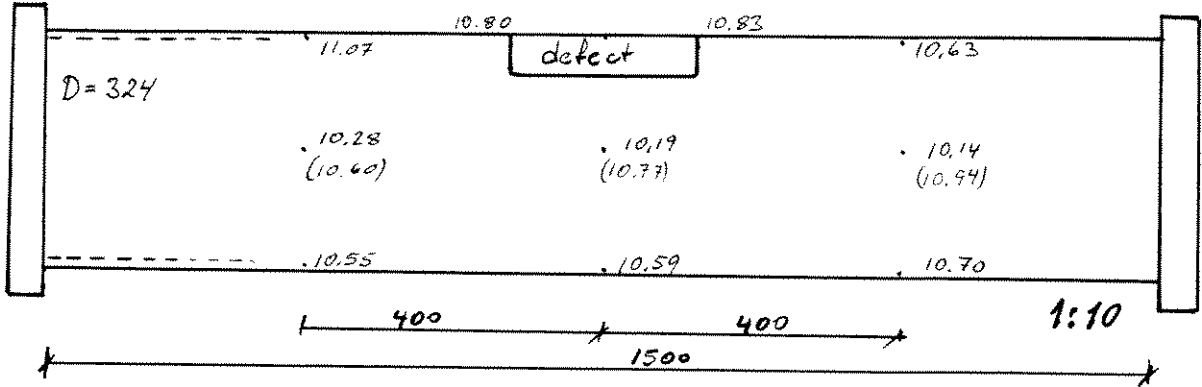


Test no.	L mm	d mm	r mm
4	162	3.2	3
5	162	3.2	3
6	162	3.2	3
7	245	5.3	3
8	245	5.3	3
9	245	7.5	3

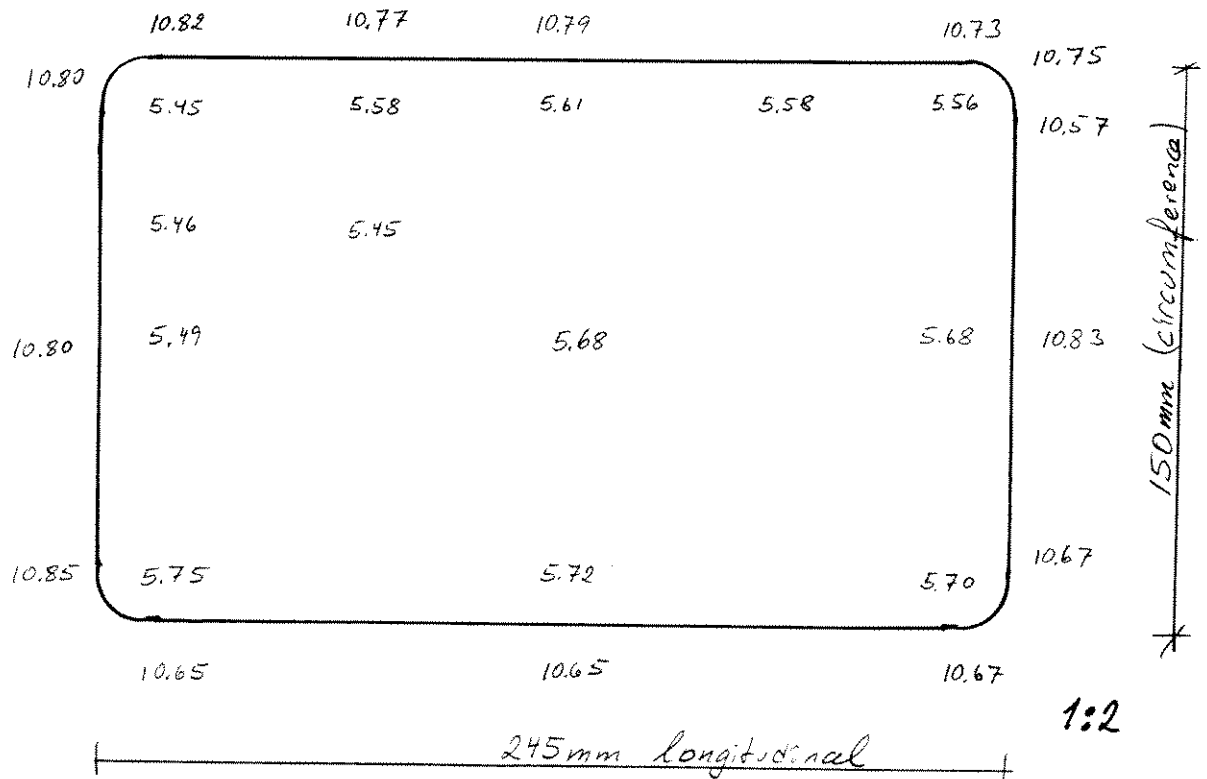


Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>	
Client/Subject: <i>Test no. 1</i>	PREPARED	Date: <i>1997</i>	Sign.: <i>OHB</i>
	VERIFIED	Date:	Sign.: Rev.: Page:

*Thickness measurements (mm)*



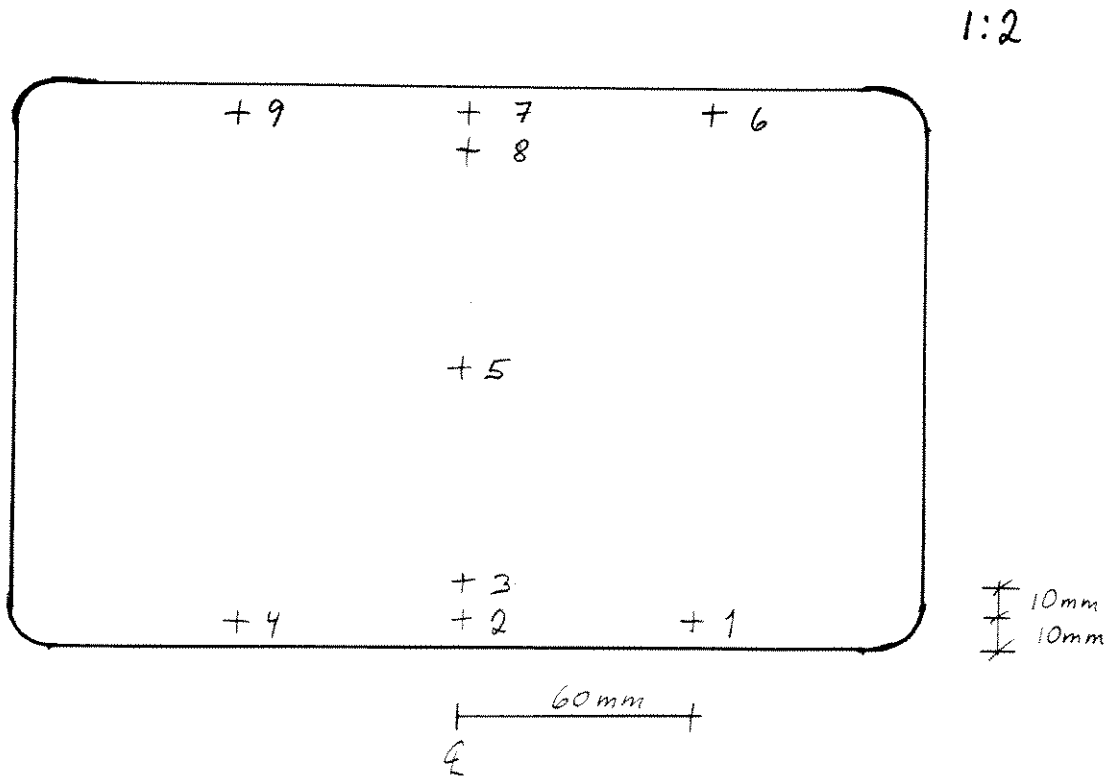
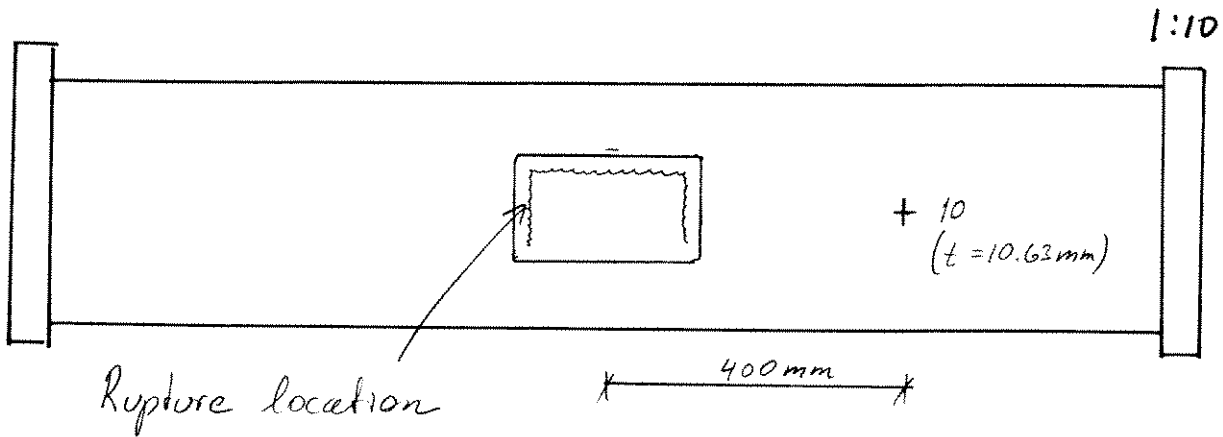
*Thickness measurements of the corrosion defect (mm)*





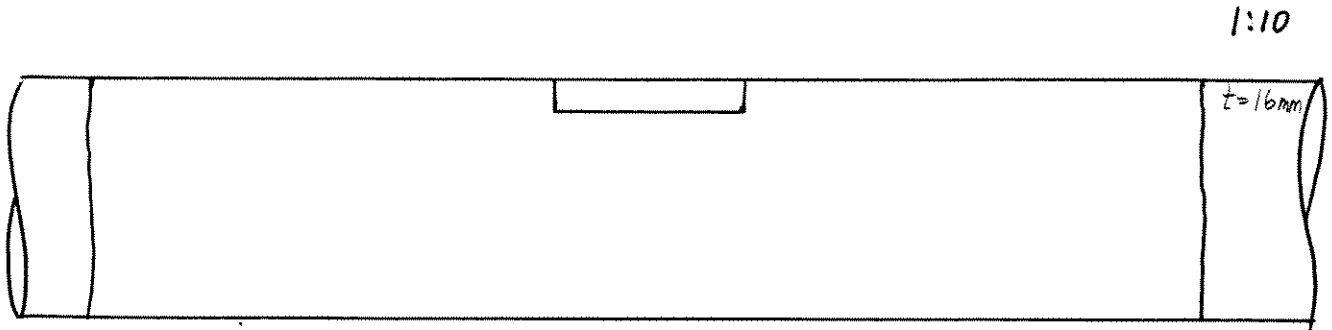
Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>		
Client/Subject:  <i>Test no. 1.</i>	PREPARED	Date:	Sign.:	Doc. No.:
	VERIFIED	Date:	Sign.:	Rev.:

*Strain gauge location and numbering*

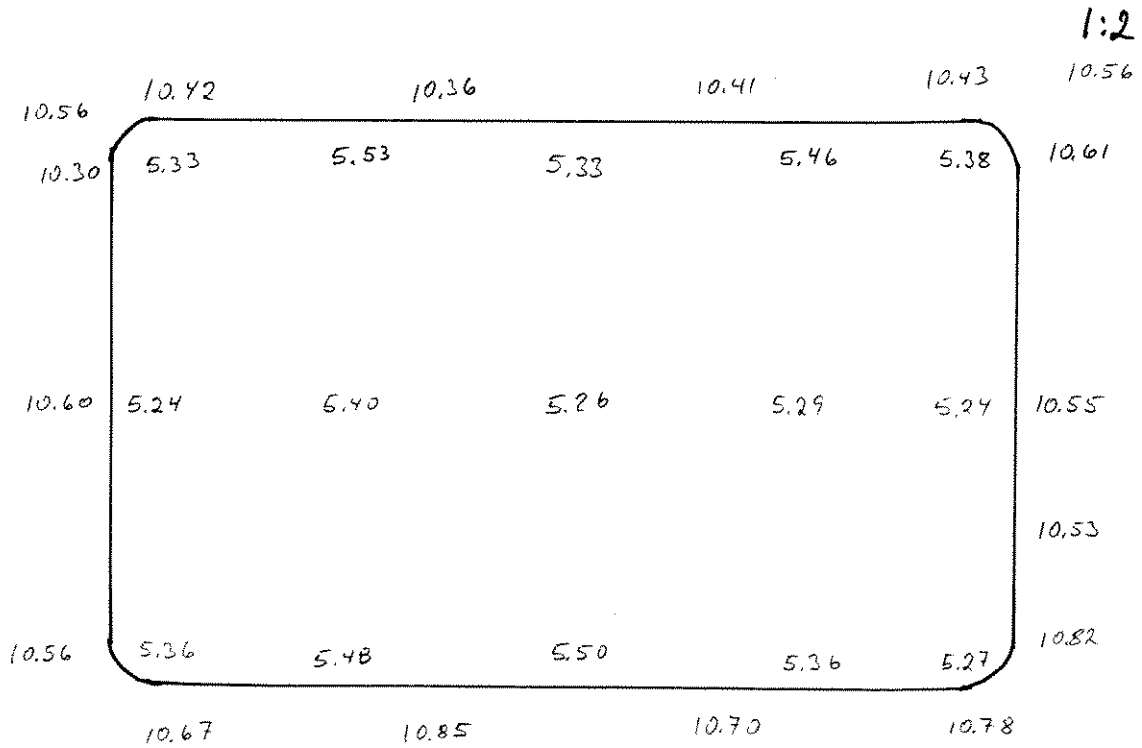




Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>			
Client/Subject:  <i>Test no. 2</i>	PREPARED	Date:	Sign.:	Doc. No.:	
	VERIFIED	Date:	Sign.:	Rev.:	Page:



*Thickness measurements of the corrosion defect (mm)*





DNV

Project title: Reliability of Corroded Pipes

Project No.: 25010049

Client/Subject: Test no. 2

PREPARED Date: Sign.:

Doc. No.:

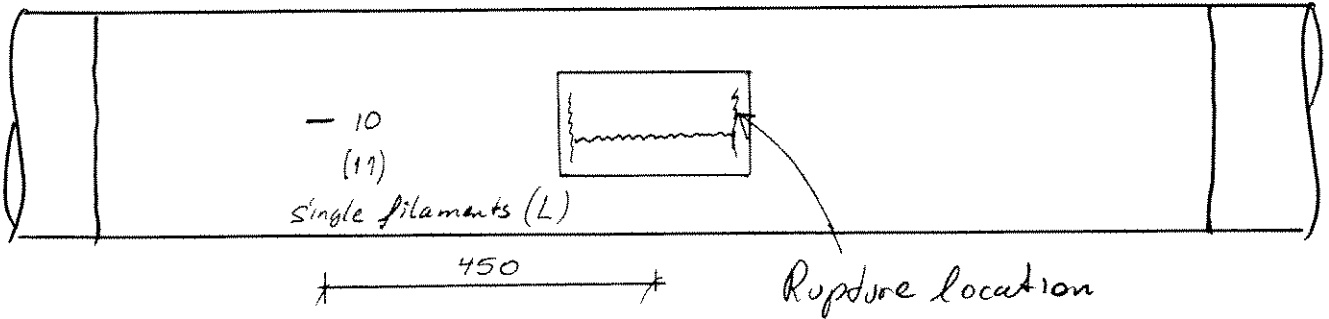
VERIFIED Date: Sign.:

Rev.:

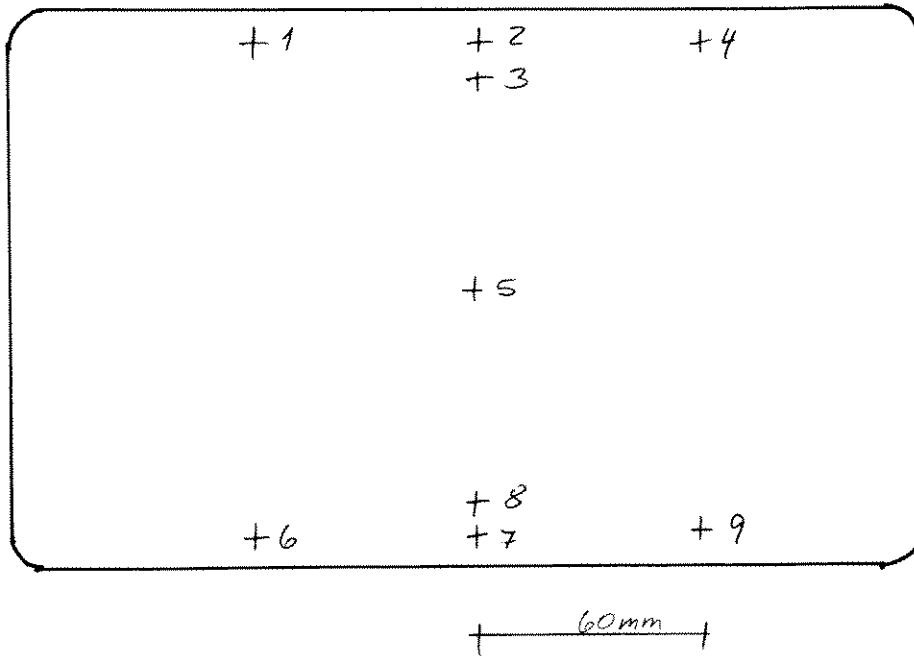
Page:

### Strain gauge location and numbering

1:10



1:2



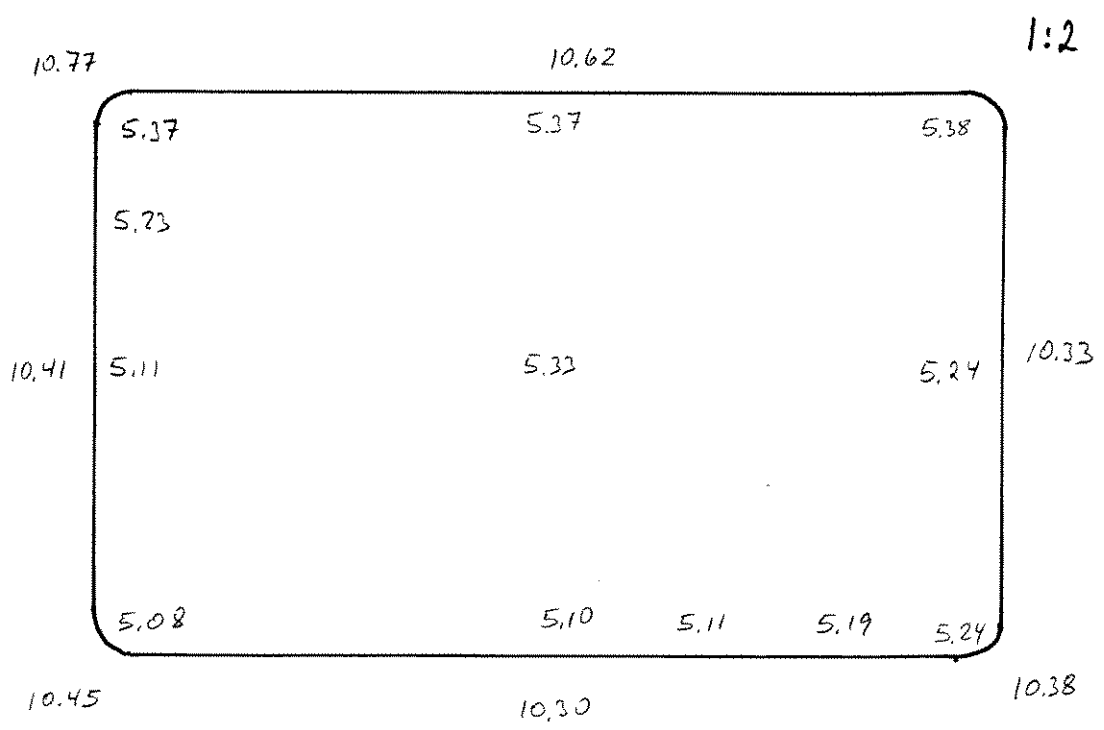
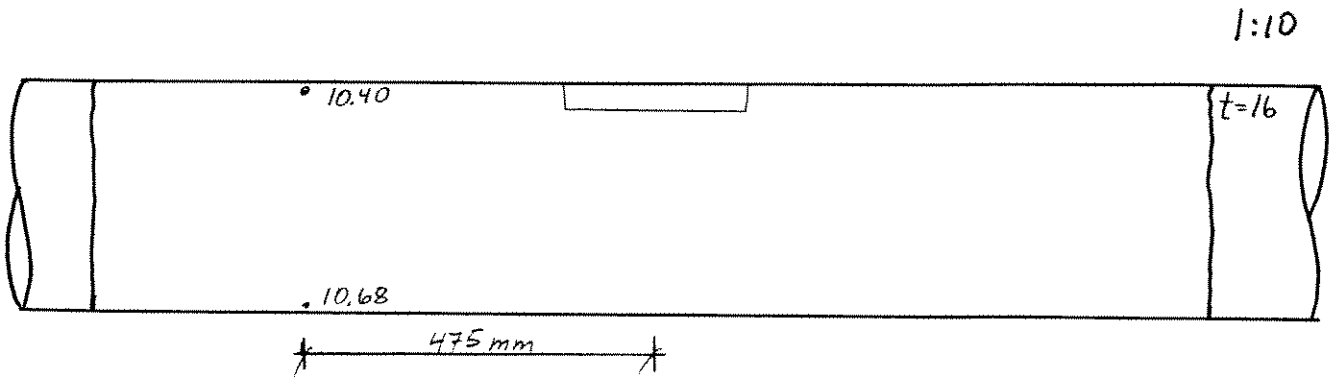
10mm  
10mm





Project title: Reliability of Corroded Pipes Project No.: 25010049

Client/Subject: Test no. 3  
PREPARED Date: Sign.: Doc. No.:  
VERIFIED Date: Sign.: Rev.: Page:



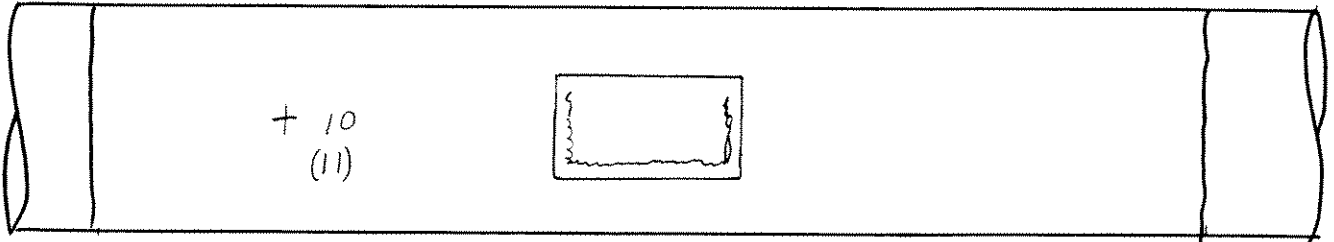
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Project title:		Project No.:		
Client/Subject: <i>Test no.3</i>	PREPARED	Date:	Sign.:	Doc. No.:
	VERIFIED	Date:	Sign.:	Rev.:

*Strain gauge location and numbering*

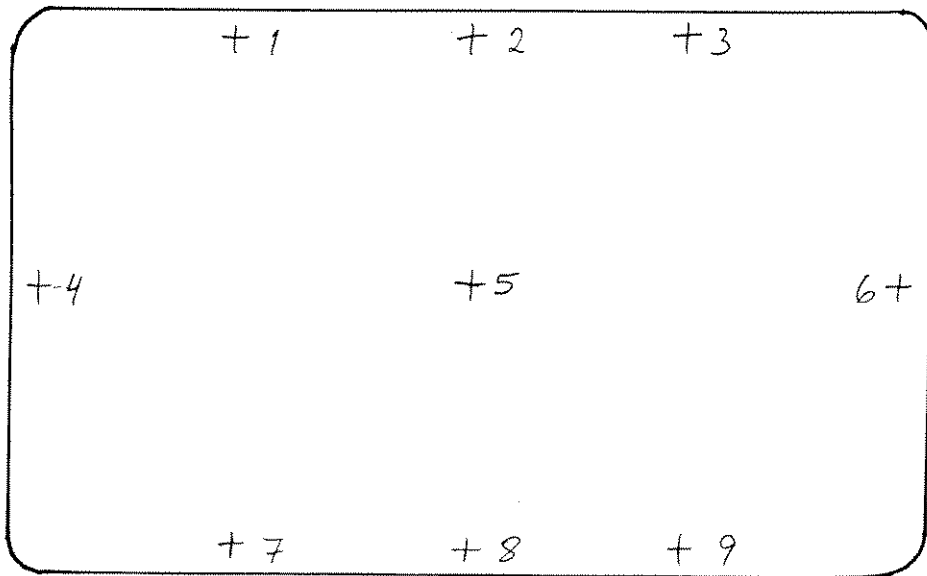
*1:10*



*475*

*Rupture location*

*1:2*

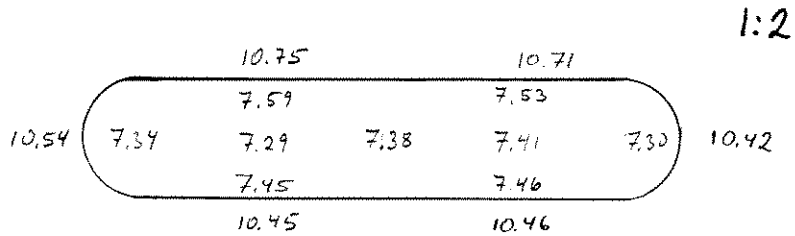
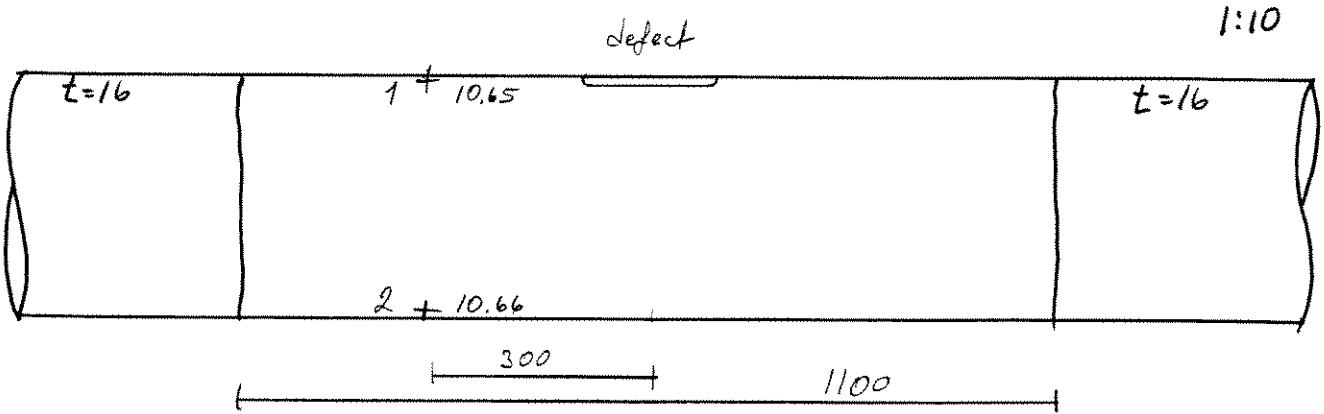


*60mm*

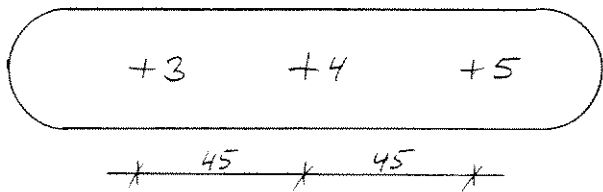
*10mm*  
*10mm*



Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>	
Client/Subject: <i>Test no. 4</i>	PREPARED	Date:	Sign.:
	VERIFIED	Date:	Sign.:
		Doc. No.:	Rev.:
			Page:

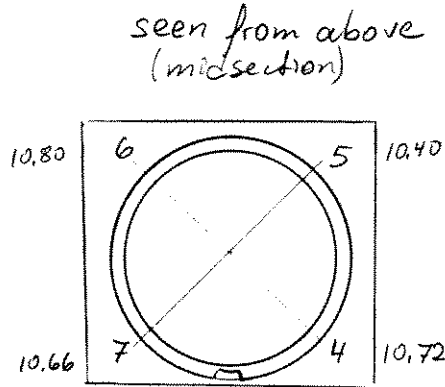
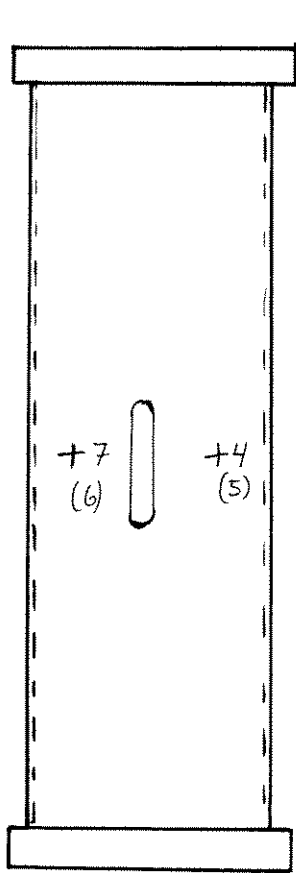


	10.75		10.71	
	7.57		7.53	
10.54	7.34	7.29	7.38	7.41
	7.45		7.46	
	10.45		10.46	

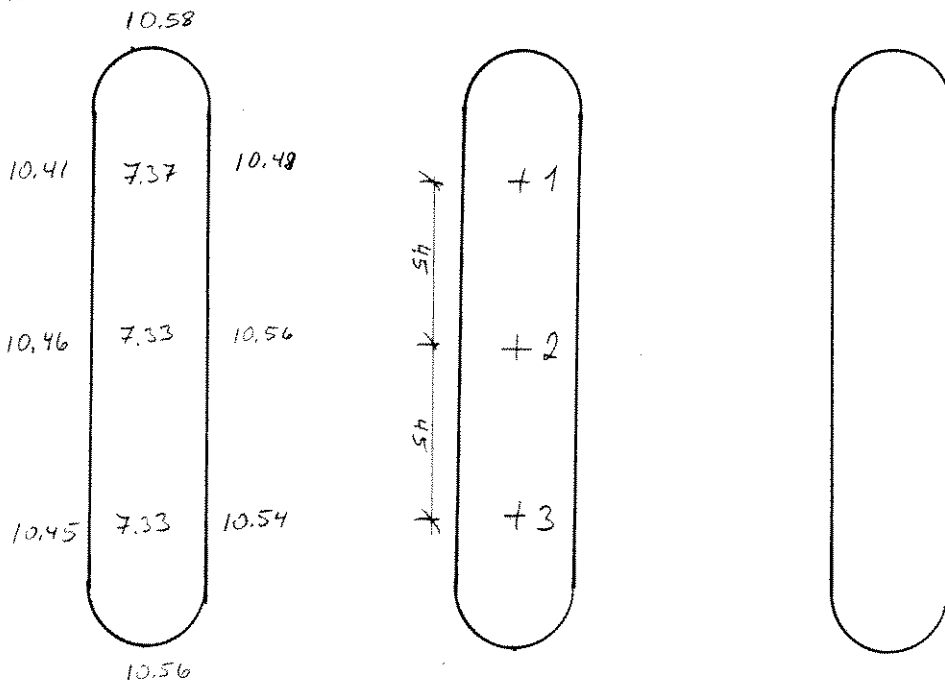




Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>	
Client/Subject:  <i>Test no. 5</i>	PREPARED	Date:	Sign.:
	VERIFIED	Date:	Sign.:
		Doc. No.:	Rev.:
			Page:

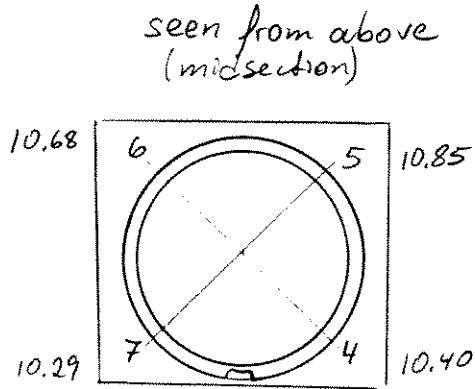
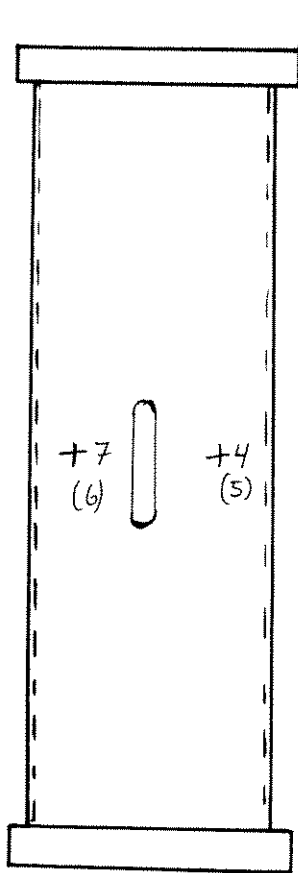


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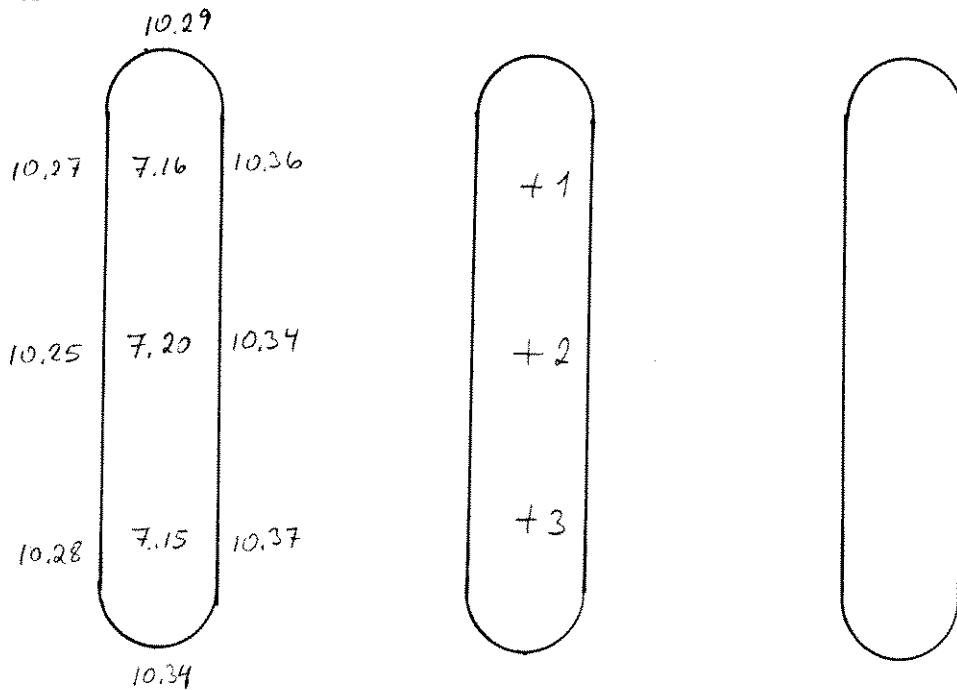




Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>		
Client/Subject: <i>Test no. 6</i>	PREPARED	Date:	Sign.:	Doc. No.:
	VERIFIED	Date:	Sign.:	Rev.:

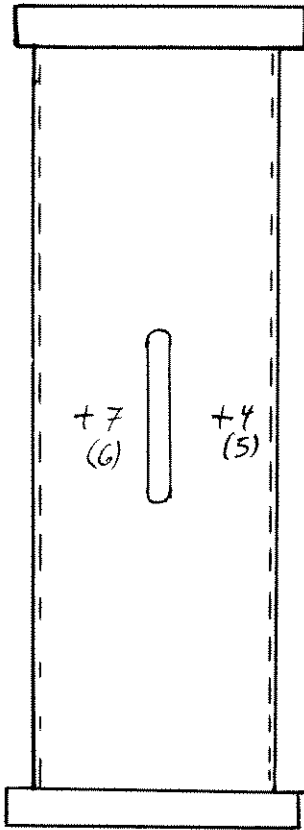


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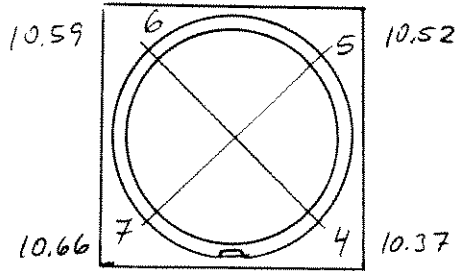


Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>	
Client/Subject: <i>Test no. 7</i>	PREPARED	Date:	Sign.:
	VERIFIED	Date:	Sign.:
		Rev.:	Page:

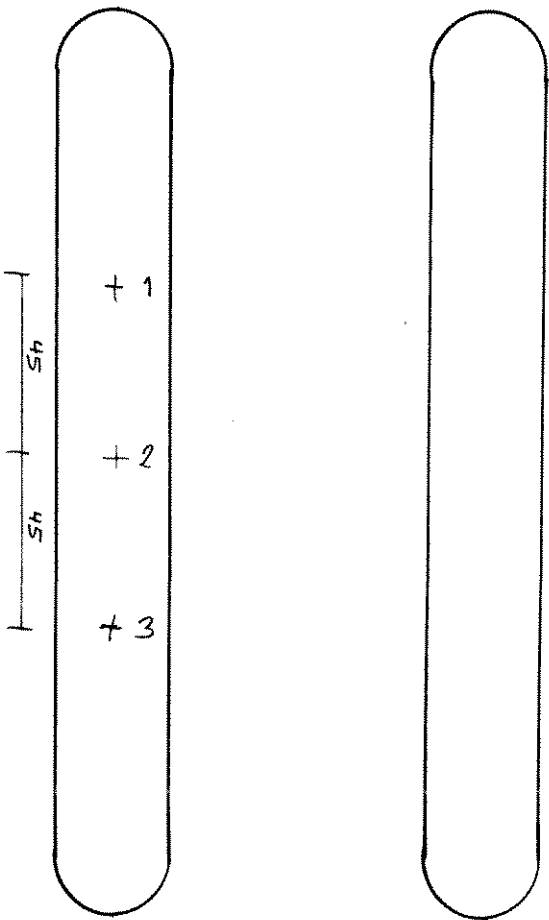
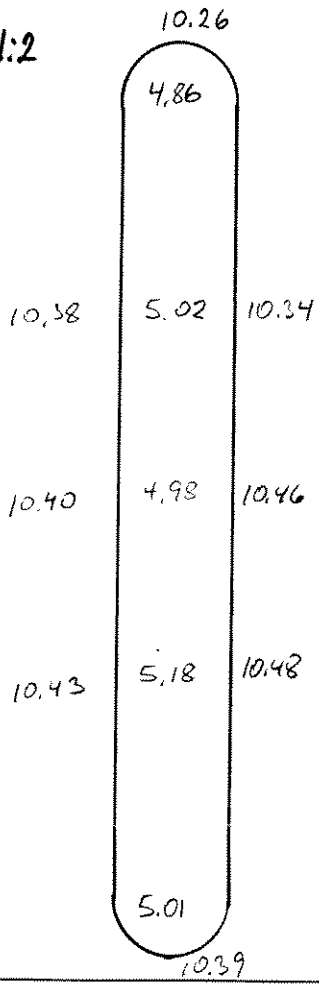


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(midsection)*



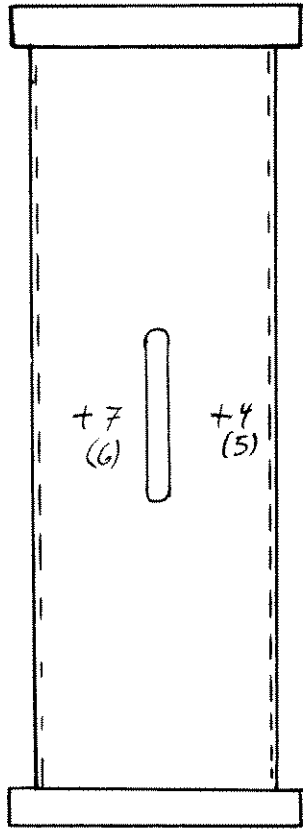
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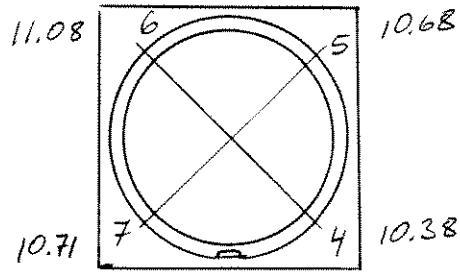


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Client/Subject:  <i>Test no. 8</i>	PREPARED	Date:	Sign.:
	VERIFIED	Date:	Sign.:
		Rev.:	Page:

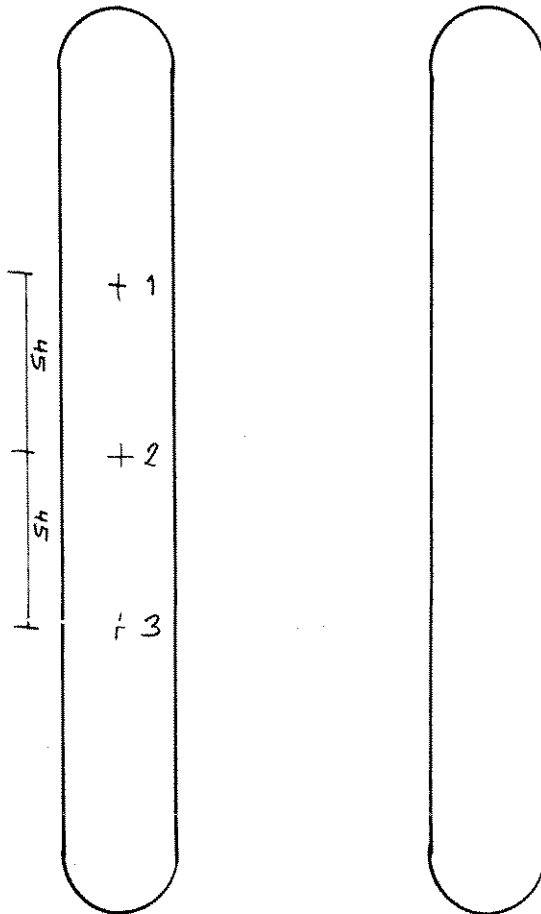
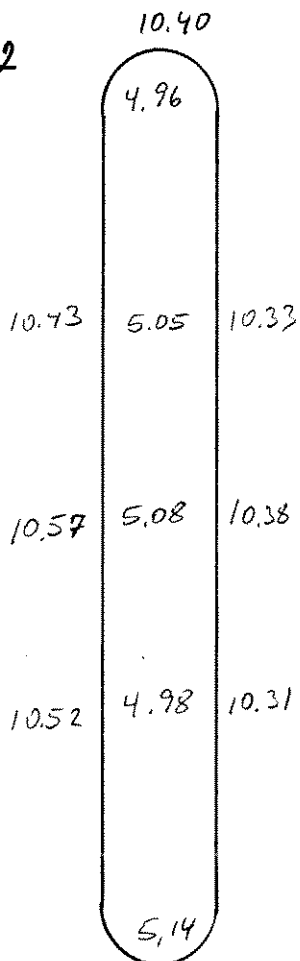


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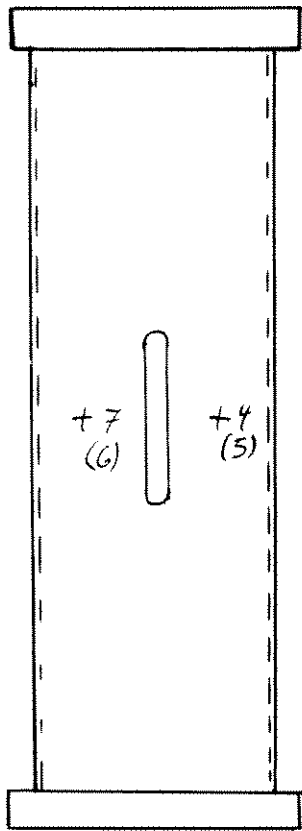


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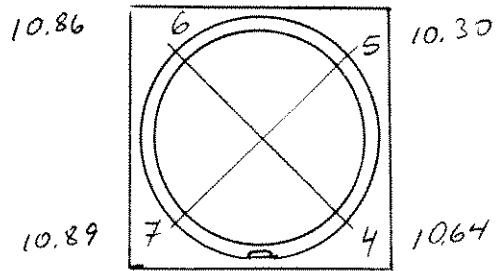


Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>	
Client/Subject:  <i>Test no. 9</i>	PREPARED	Date:	Sign.:
	VERIFIED	Date:	Sign.:
		Rev.:	Page:

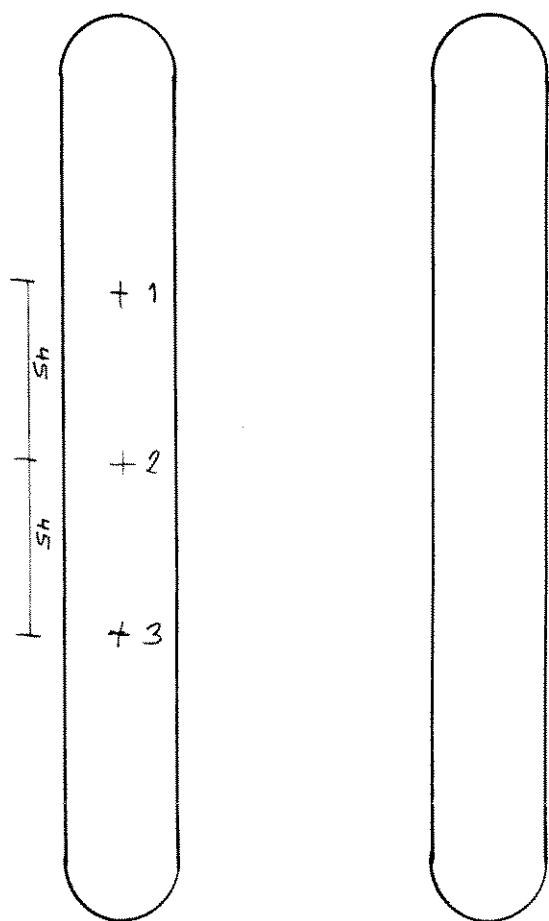
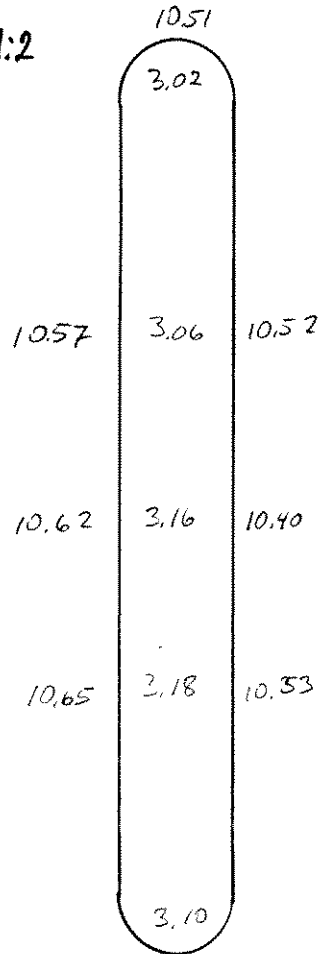


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*seen from above  
(midsection)*



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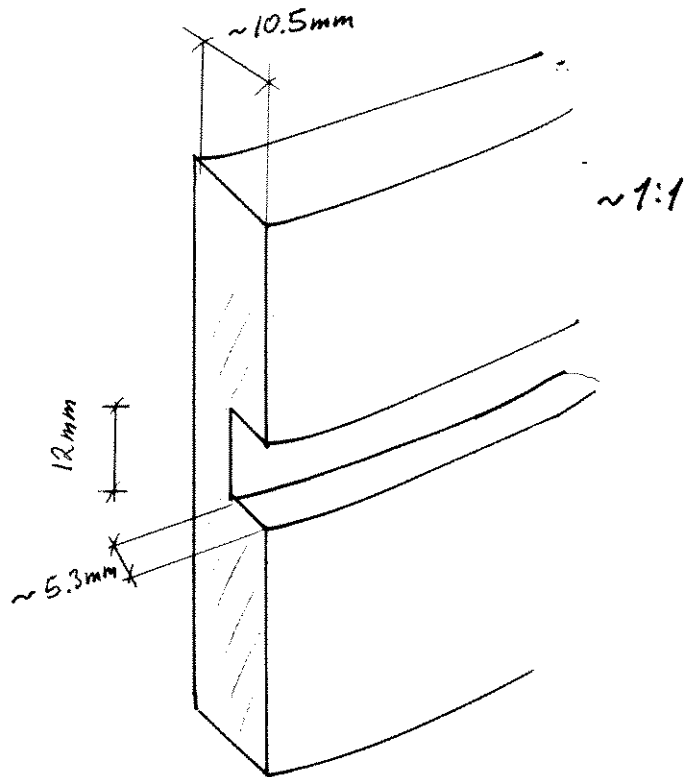
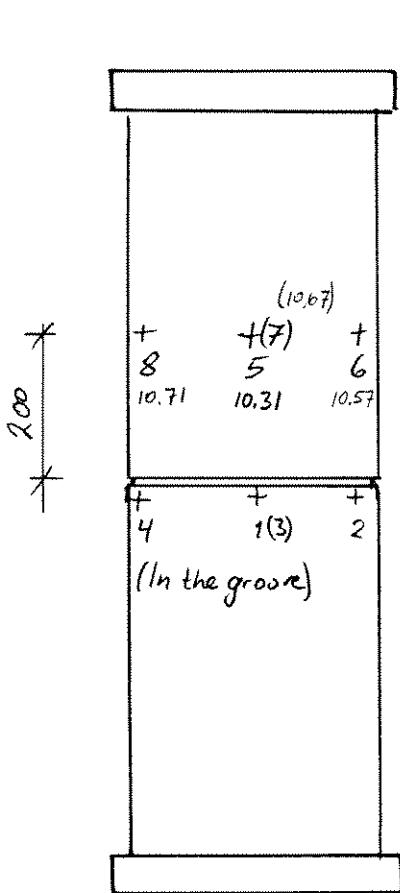


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Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>		
Client/Subject:  <i>Test no. 10</i>	PREPARED	Date:	Sign.:	Doc. No.:
	VERIFIED	Date:	Sign.:	Rev.: Page:



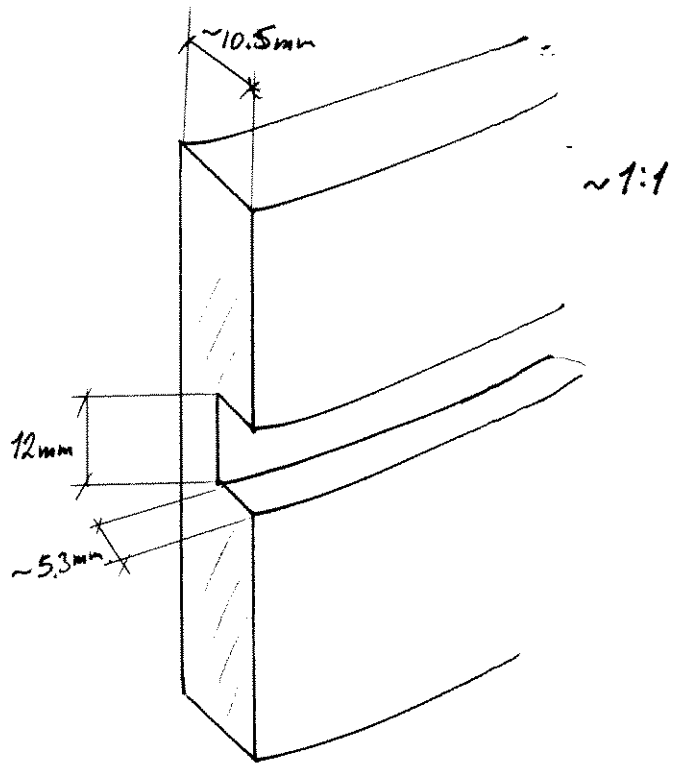
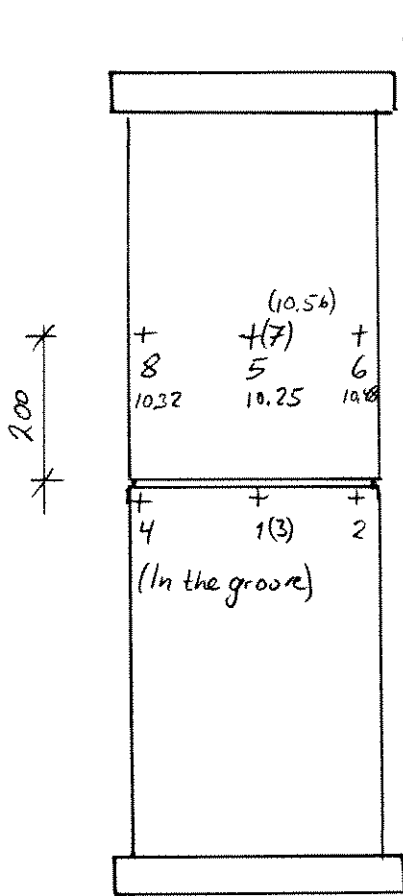
*measured thickness*

<i>Gauge</i>	<i>groove</i>	<i>pipe</i>
<i>1</i>	<i>5.22</i>	<i>10.34</i>
	<i>5.55</i>	<i>10.50</i>
	<i>5.30</i>	<i>10.38</i>
	<i>5.55</i>	<i>10.49</i>
<i>2</i>	<i>5.66</i>	<i>10.52</i>
	<i>5.95</i>	<i>10.81</i>
	<i>5.70</i>	<i>10.41</i>
	<i>5.70</i>	<i>10.77</i>
<i>3</i>	<i>5.75</i>	<i>10.67</i>
	<i>5.67</i>	<i>10.78</i>
	<i>5.60</i>	<i>10.80</i>
	<i>5.75</i>	<i>10.70</i>
<i>4</i>	<i>5.59</i>	<i>10.71</i>
	<i>5.67</i>	<i>10.78</i>
	<i>5.22</i>	<i>10.35</i>
	<i>5.21</i>	<i>10.51</i>

*Rupture location close to strain gauge 2.*



Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>	
Client/Subject:  <i>Test no. 11</i>	PREPARED	Date:	Sign.:
	VERIFIED	Date:	Sign.:
		Rev.:	Page:



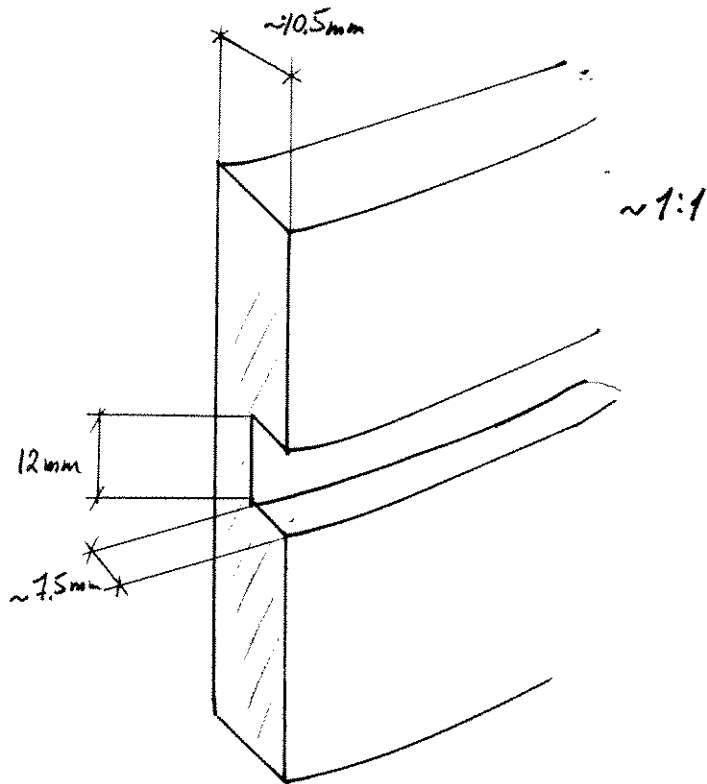
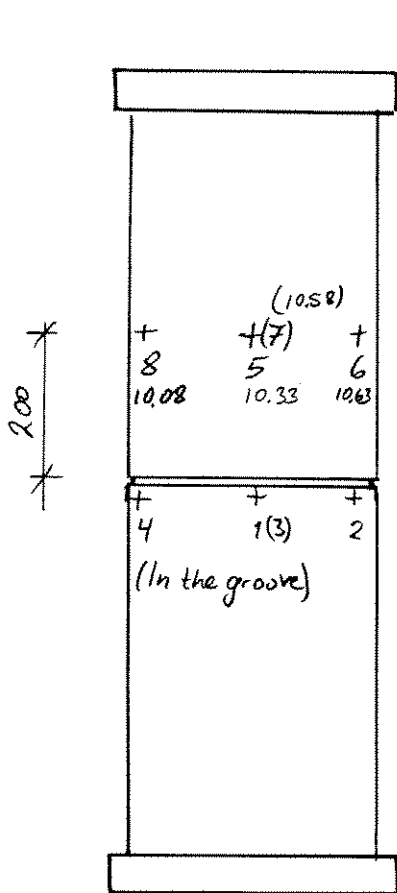
*Thickness measurements*

*Gauge groove pipe*

1	4.93	10.12
	5.14	10.27
	5.12	10.14
2	5.35	10.47
	5.66	10.22
	5.92	10.66
	5.67	10.57
3	5.31	10.41
	5.64	10.56
	5.82	10.57
	6.01	10.48
4	6.06	10.55
	5.87	10.30
	5.68	10.48
	5.37	10.60
	5.15	10.22



Project title: <i>Reliability of Corroded Pipes</i>		Project No.: <i>25010049</i>	
Client/Subject: <i>Test no. 12</i>	PREPARED	Date:	Sign.:
	VERIFIED	Date:	Sign.:
		Doc. No.:	Rev.:
			Page:



Measured thickness

Gauge groove pipe

1	2.89	10.51
	3.14	10.59
2	2.87	10.40
	2.94	10.53
	2.98	10.52
	3.56	10.93
	3.26	10.58
3	3.49	10.48
	3.44	10.50
	3.76	10.51
	3.60	10.48
4	3.07	10.30
	2.88	10.07
	3.26	10.48
	2.95	10.52
	3.03	10.46

## **APPENDIX**

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### **B**

## **MATERIAL CERTIFICATES AND MATERIAL TEST RESULTS**

- o0o -

Spørsmål 8002



DET NORSKE VERITAS  
Research laboratories

DATA SHEET

Form No. 20.2008a

Project No. 7756  
18/6-96  
Date : ..... Sign : *[Signature]*

Shredd	Flyegrensene		Shreddfasthet		Føllingskval Kontraksjon				
	KN	N/mm <sup>2</sup>	KN	N/mm <sup>2</sup>	As	o2o			
L 1	5.96	27.90	11.65	416	14.3	513	41.1	37.0	76.3
L 2	5.98	28.09	12.30	438	14.45	514	41.6	38.7	74.9
T 1	5.96	27.80	11.05	396	14.4	516	40.2	34.0	72.9
T 2	6.00	28.27	11.25	398	14.5	513	41.3	37.7	75.0

TEST SPECIMENS  
1-9

1756 18/6 - 96 088

10V = 50kN

10.25V

PRV

10V = 6.25 mm

0.5V

d = 5.98 A = 28.09 mm<sup>2</sup>

C. loop gauge = 2.5 mm

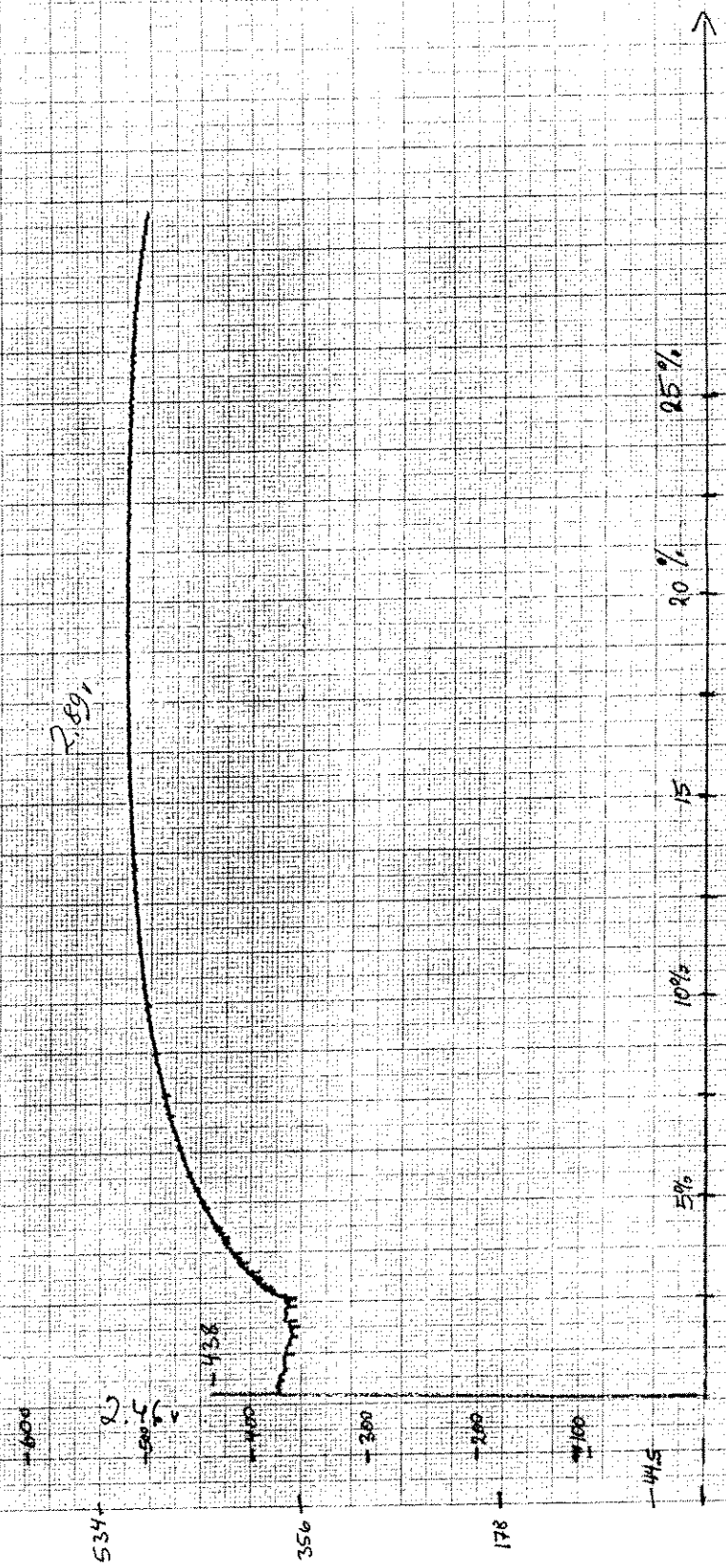
10V = 6.25 mm disp =  $\frac{6.25}{2.5} = 0.25$  tegangan 25%

1V = 2.5% = 1

10V = 50kN  $\Rightarrow$  10V =  $\frac{50kN}{28.09} = 1780 \text{ MPa} \Rightarrow$  1V = 178 MPa  $\Rightarrow$  4cm

$$\epsilon_{\text{teori}} = \ln(1 + \epsilon)$$

$$\sigma_{\text{teori}} = \sigma(1 + \epsilon)$$

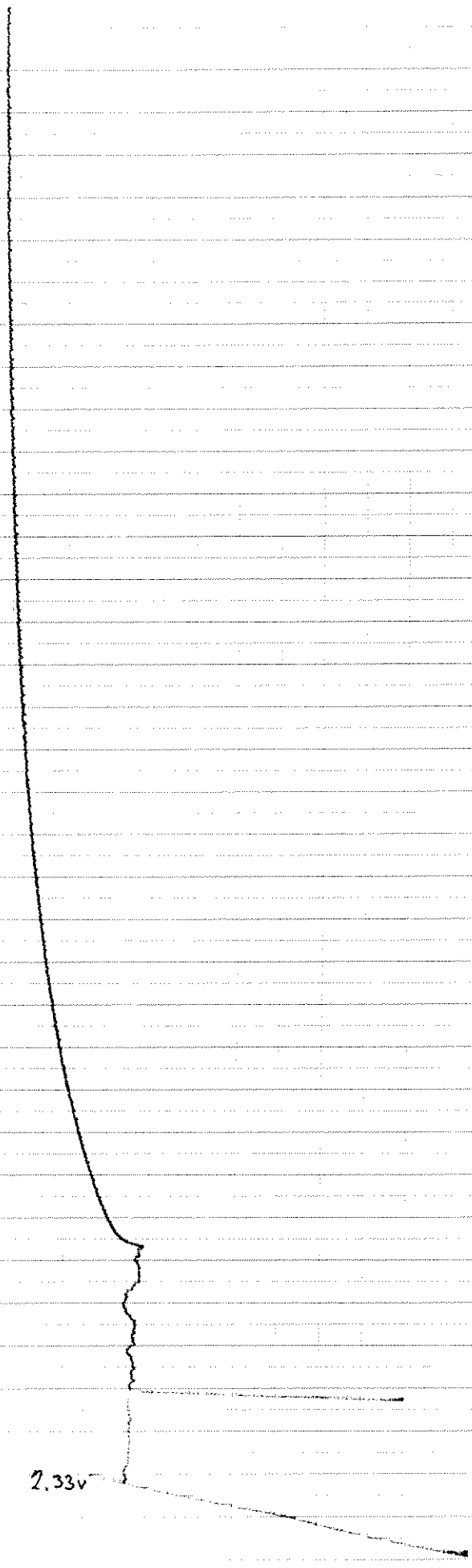


PRV L2

$10V = 50k\Omega$   
 $10V = 6.25mm$   
 $V = 3700sek$   
 $\gamma = 0.8mm/min$   
 $10V = 10k\Omega$   
 $0.25V$   
 $0.2\%$   
 $1.2V$

2.86V

2.33V



Prime 11

10V = 50mV  
10V = 6.25V

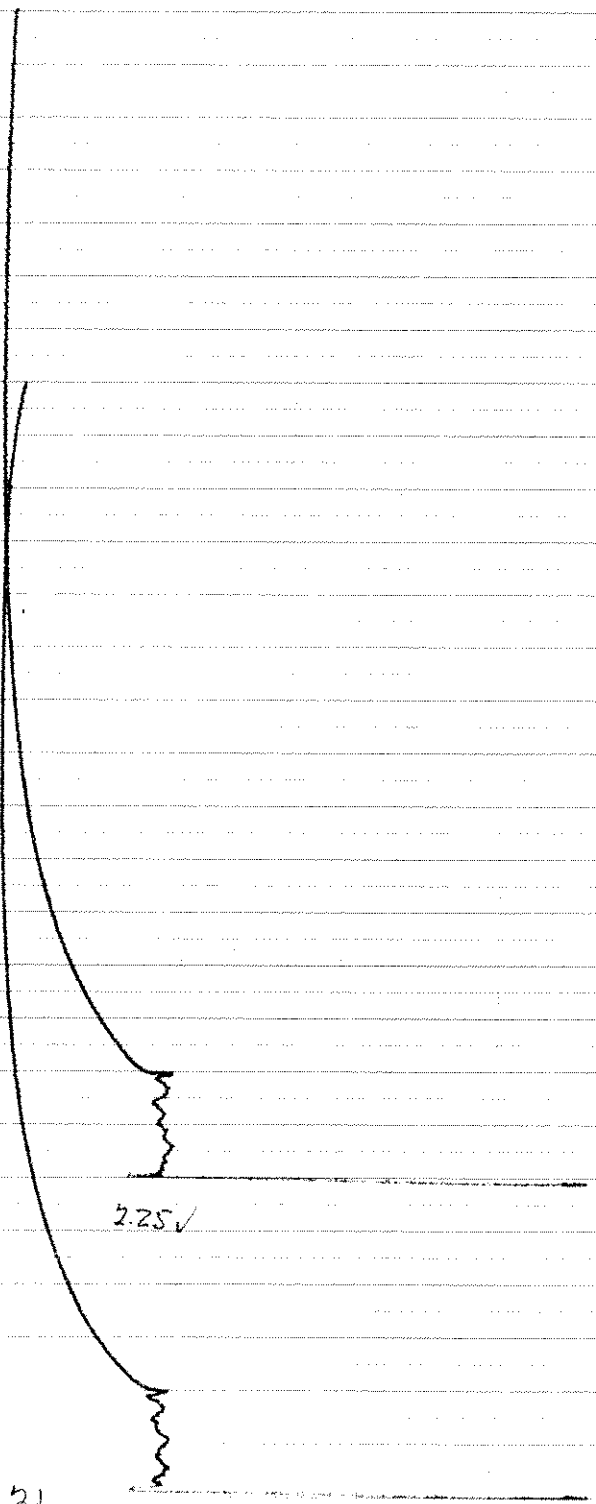
2.90V

2.88V

2.25V

2.21

Base T1







FAKSEDEL/PACKING LIST

OSLO LAGERP: Avd. BRYNE

11510  
DET NORSKE VERITAS INDUSTRY A/S  
VERITASUN. 1  
P.B.300  
1322 HØVIK

Lev. adresse:  
VERITASUN. 1  
HØVIK

S./P.: 1

Deres best.nr./Your P.O No. Deres ref./Your Ref. Vår ref./Our Ref. Vårt ordre nr./Our Order No.  
O.H.BJØRNØY F.H. Martinussen / R 11236 / 01

Merking/Marking Best. dato/Date of Order  
96-05-07

Bet.beting/Payment Terms Lev.beting/Delivery Terms Lev.måte/Delivery Lev.dato/Date of Delivery  
NETTO PR. 30 DAGER FOB BRYNE SNRST.MULIG 96-05-07

Pos./ Vare/ Antall/ Enh/ Levert/ Rest/  
Item Article Quantity Unit Delivered Rest

SERTIFIKAT EN 10204/DIN 50049-3.1.B

1 014545AT 323.8\*10.31MM PIPE SP S.40 X52 MOD 12.00 M 13.32  
79.73 kg

Ch.nr: 93226  
DELES I TO FOR TRANSPORT.  
VERITAS ØNSKER AT RØRET ANK. PÅ EN SLIK MÅTE AT  
OPPRINNELIG ORIENTERING MELLOM DE TO DELENE  
KAN BESTEMMES.

2 014548AT 323.8\*15.88MM PIPE SP X52 MOD 6.00 M 6m  
120.62 kg

Ch.nr: 93227  
KAPPES I FIX LGD 6M.

**CERTIFICATES  
ENCLOSE**

*13.32  
1785 kg*

Porto : ..... Kollit : 2 RØR ..... Uttak : G.V. ..... Lev dato : .....

Etter forfall beregnes 1.0 % rente pr. mnd. I.h.t. panteloven forbeholder vi oss eiendomsretten til de leverte varer inntil kjøpesummen er helt betalt. Aksept ansees ikke som betaling før den er innfridd i sin helhet. 1.0% pr month is added for late payment. Title to goods belongs to Rolf Lycke AS until payment has been received in full. Mottatt: .....



**DET NORSKE VERITAS**

Certificate No.:  
VER 52995048-06

**INSPECTION CERTIFICATE OF MATERIALS**

- DNV certificate acc. to Classification Rules.  
 3.1C acc. to ISO 10474/EN 10204

Product	SEAMLESS LINE PIPE, 12-3/4 inx0.406 in (323.9 mmx10.30 mm)	Total mass	(761.780 M) 60.647 Ton.
Manufacturer	TUBOS DE ACERO DE MEXICO, S.A.	Manufacturer's order No.	003830-03
Purchaser	ROLF LYCKE A/S	Purchaser's order No.	23005

Destination/Supplementary information  
NORWAY / Manufacturer's Certificate N° 95003439

**MATERIAL SPECIFICATION**

Material standard and grade	API Spec 5L (April 1, 1995), Grade X52	Any additional requirements	As per Rolf Lycke A/S, PO 23005
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**SPECIFIED MECHANICAL PROPERTIES**


TENSILE PROPERTIES					CHARPY V-NOTCH IMPACT PROPERTIES				
Specimen type/ dimensions	Yield point R <sub>eH</sub> or R <sub>p0.2</sub> N/mm <sup>2</sup>	Tensile strength R <sub>m</sub> N/mm <sup>2</sup>	Elongation A <sub>5</sub> %	Reduction of area Z %	Orientation L or T	Test temp. °C	Width of test piece mm	Energy, J, min.	
								Single	Average
	360	490 - 620	22		T	-50	10	28	36

Remarks

**SPECIFIED CHEMICAL COMPOSITION**

Element	C, %	Mn, %	Si, %	P, %	S, %	Mo, %	Cr, %	V, %	Nb, %	Ni, %	Cu, %	CA, %	CE, %
Specific value(s)	0.14	1.35	0.40	0.015	0.005	0.080	0.20	0.060	0.040	0.20	0.200	0.004	0.41

Remarks V + Nb + Ti, 0.07% Max., V + Nb, 0.06% Max., Cu + 6Sn, 0.32% Max.

<p>Marking:</p> <p style="text-align: center;">N</p> <p>The stamping is placed: between 5 to 15 cm from pipe end</p>	<p>The materials are tested and inspected in the <b>Normalized</b> condition, and are found to be in accordance with the above specification. (For test results, see overleaf)</p> <p>If applicable state drawing number and approval date</p> <div style="text-align: center;">  <p>Veracruz, Mexico Place</p> <p>1995.10.27 Date</p> <p><i>[Signature]</i> R. O. TINOCO Inspector</p> </div>
--	---

It is agreed that save as provided below Det Norske Veritas, its subsidiaries, bodies, officers, directors, employees and agents shall have no liability for any loss, damage or expense allegedly caused directly or indirectly by their mistake or negligence, breach of warranty, or any other act, omission or error by them, including gross negligence or willful misconduct by any such person with the exception of gross negligence or willful misconduct by the governing bodies or senior executive officers of Det Norske Veritas. This applies regardless of whether the loss, damage or expense was affected anyone with whom Det Norske Veritas has a contract or a third party who has acted or relied on decisions made or information given by or on behalf of Det Norske Veritas. \* However, if any person uses the services of Det Norske Veritas or its subsidiaries or relies on any decision made or information given by or on behalf of them and in consequence suffers a loss, damage or expense proved to be due to their negligence, omission or default, then Det Norske Veritas will pay by way of compensation to such person a sum representing his proved loss. \* In the event Det Norske Veritas or its subsidiaries may be held liable in accordance with the sections above, the amount of compensation shall under no circumstances exceed the amount of the fee, if any, charged for that particular service, decision, advice or information. \* Under no circumstances whatsoever shall the individual or individuals who have personally caused the loss, damage or expense be held liable. \* In the event that any provision in this section shall be invalid under the law of any jurisdiction, the validity of the remaining provisions shall not in any way be affected.

TEST RESULTS

MECHANICAL PROPERTIES

TENSILE TESTS						CHARPY V-NOTCH IMPACT TESTS							
Cast. No.	Test No.	Yield point	Tensile strength	Elongation	Reduction	Orientation	Width of test piece	Test temp	Energy, J, min.				
		$R_{eH}$ or $R_{p0.2}$	$R_m$	$A_5$	$Z$				1	2	3	Ave.	
		N/mm <sup>2</sup>	N/mm <sup>2</sup>	%	%	L or T	mm	°C					
93226	01	375.60	513.88	46		T	10	-50	70	73	69	71	
93226	02	401.10	528.59	46		T	10	-50	69	69	75	71	

Remarks

CHEMICAL COMPOSITION

Cast. No.	C, %	Mn, %	Si, %	P, %	S, %	Mo, %	Cr, %	V, %	Nb, %	Ni, %	Cu, %	CA, %	CE, %
93226	0.139	1.16	0.28	0.007	0.004	0.030	0.05	0.034	0.00	0.06	0.123	.0022	0.36
93226	0.138	1.14	0.25	0.007	0.004	0.029	0.06	0.034	0.00	0.06	0.121	.0022	0.36

Remarks Product Chemical Analysis

Process  
Seamless pipe

Heat treatment (state temperatures)  
Normalized: 880 C

Non-destructive testing  
Ultrasonic SR4 - 5% Notch & MPI

ADDITIONAL INSPECTION

Type and extent of inspection

Review of Chemical Analysis and Data Sheets, Mechanical Properties, Review of Dimensional Control Sheets and Hydrostatic Test Records, Ultrasonic & Electromag. Inspection Records, DNV Marking and Issue of Insp. Certificate.



# TUBOS DE ACERO DE MEXICO, S.A.

PURCHASER ROLF LYCKE A.S.		MILL TEST CERTIFICATE		INSPECTOR		DATE		No	
TYPE OF PIPE SEAMLESS		SALES CONFIRMATION 003830 / 03		MR. RAFAEL TINOCO		24/10/95		95003439	
LINE PIPE		DIMENSIONS 12 3/4 INCH X 0.406 INCH		NOMINAL WEIGHT 53.52 LB/FT		STEEL GRADE K52		ENDS NORMAL BEVEL	
SPECIFICATION OR STANDARD API 5L		SPECIFIC LENGTH OR R. 26.20 / 45.90 FT		SURFACE ***		HYDROSTATIC TEST P. 2810 PSI		5 SEC	

HEAT NUMBER 93226	LONGITUDINAL STRENGTH YIELD NW/MM2	490.00 620.00	22.0	28.000	36.000	22.00 ( )
	TENSILE NW/MM2	513.88 528.59	46 46	73.000 69.000	71.000 71.000	80.11 HRB 82.00 HRB

M E C H A N I C A L P R O P E R T I E S A N D T E S T  
 XELONGATION IN 2 INCH FLATTENING WIDE THICKNESS IMPACT CHАРPY TRANSVERSE  
 TENSILE SAMPLE IN DIV IDUAL AVERAGE SHEAR HARDNESS  
 MM. MM. JOULE AREA HRC (HRB)

**100% ULTRASONIC INSPECTION**  
**SATISFACTORY**

**SR4-5% notch**

**100% MAGNETIC PARTICLE INSPECTION**  
**SATISFACTORY**

**on Pipe ends**

INSPECTION SATISFACTORY: SR-4 - EMI - VPI - MPI

**\*\*\* VARNISHED**  
 MILL: ON-458 E CARBON STEEL VERNER VERACRUZ VER  
 APDO POSTAL 402 TEL(781) 81-11-88 FAX(781) 164-5  
 P.02073 81-252-88  
 ORIGINAL PAGE 1 OF 4 ENG. SARA GARCIA PAJARES  
 QUALITY CERTIFICATION NAME AND SIGNATURE

THIS IS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREIN WERE MANUFACTURED, SAMPLED, TESTED, AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.



# TUBOS DE ACERO DE MEXICO, S.A.

PURCHASER		MILL TEST CERTIFICATE		INSPECTOR		DATE		No.	
ROLF LYCKE A.S.		SALES CONFIRMATION		MR. RAFAEL TINOCO		24/10/95		95003439	
TYPE OF PIPE		DIMENSIONS		NOMINAL WEIGHT		STEEL GRADE		ENDS	
LINE PIPE SEAMLESS		12 3/4 INCH X 0.406 INCH		53.52 LB/FT		K52		NORMAL BEVEL	
SPECIFICATION OR STANDARD		SPECIFIC LENGTH OR R.		SURFACE		HYDROSTATIC TEST P			
API 5L		26.20 / 45.90 FT		***		2810 PSI		5 SEC	
HEAT NUMBER		MICRO-STRUCTURE		METHALLOGRAPHIC EVALUATION		HARDNESS VICKER HV			
GRAIN SIZE				LEVEL INCLUSIONS					
MINIMUM		A		B		C		D	
MAXIMUM									
93226									
93226									

**100% ULTRASONIC INSPECTION SATISFACTORY**

**SR4-5% notch**

**100% MAGNETIC PARTICLE INSPECTION SATISFACTORY**

**on Pipe ends**

\*\*\* VARNISHED

MILL  
 KM 433 8 CAMER MEX-VER  
 VERACRUZ, VER  
 ADDO. POSTAL 402  
 TELEX 18643  
 FAX(52) 91-02-88

QUANTITY 57 LENGTHS

ORIGINAL PAGE 2 OF 4

ENG SARA GARCIA PAJARES

QUALITY CERTIFICATION NAME AND SIGNATURE

THIS IS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREIN WERE MANUFACTURED, SAMPLED, TESTED, AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.



# TUBOS DE ACERO DE MEXICO, S.A.

PURCHASER		MILL TEST CERTIFICATE	
ROLF LYCKE A.S.		SALES CONFIRMATION	
TYPE OF PIPE		INSPECTOR	
SEAMLESS		MR. RAFAEL TINOCO	
DIMENSIONS		DATE	
12 3/4 INCH X 0.406 INCH		24/10/95	
SPECIFICATION OR STANDARD		ENDS	
API 5L		NORMAL BEVEL	
APRIL 1, 1995.		HYDROSTATIC TEST P.	
SPECIFIC LENGTH OR R.		2810 PSI	
26.20 / 45.90 FT		5 SEC	
NOMINAL WEIGHT		STEEL GRADE	
53.52 LB/FT		K52	

## PRODUCT CHEMICAL ANALYSIS

HEAT NUMBER	C	MN	SI	P	S	MO	CR	V	NB	NI	CU	SN	AL	TI	B	AS	CA	C.E.
MINIMUM	0.140	1.35	0.40	0.015	0.005	0.080	0.20	0.060	0.040	0.20	0.200	0.015						
MAXIMUM	0.139	1.16	0.26	0.007	0.004	0.030	0.05	0.034	0.000	0.06	0.123	0.006	0.020	0.000	0.000	0.004	0.0022	0.36
	93226	0.138	1.14	0.007	0.004	0.029	0.06	0.034	0.000	0.06	0.121	0.006	0.017	0.000	0.000	0.004	0.0022	0.36

0.0040 0.41

**100% ULTRASONIC INSPECTION**  
**SATISFACTORY**

**SR4-5% notch**

**100% MAGNETIC PARTICLE INSPECTION**  
**SATISFACTORY**

**on Pipe ends**

\*\*\* VARNISHED

MILL	QUANTITY
KM 433 S CARR MEX-VER	57 LENGTHS
VERACRUZ, VER	
APDO POSTAL 202	
TEL 51 1543	
FAX(23) 51-92-88	

ORIGINAL PAGE 3 OF 4

ENG. SARA GARCIA PAJARES

QUALITY CERTIFICATION NAME AND SIGNATURE

THIS IS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREIN WERE MANUFACTURED, SAMPLED, TESTED, AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.



# TUBOS DE ACERO DE MEXICO, S.A.

PURCHASER		MILL TEST CERTIFICATE	
ROLF LYCKE A.S.		SALES CONFIRMATION	
TYPE OF PIPE		INSPECTOR	
003830 / 03		DATE	
MR. RAFAEL TINOCO		24/10/95	
DIMENSIONS		No.	
12 3/4 INCH X 0.406 INCH		95003439	
SEAMLESS		ENDS	
NOMINAL WEIGHT		STEEL GRADE	
53.52 LB/FT		K52	
SPECIFIC LENGTH OR R.		SURFACE	
26.20 / 45.90 FT		NORMAL BEVEL	
APRIL 1, 1995.		HYDROSTATIC TEST P.	
***		2810 PSI	
		5 SEC	

## HEAT CHEMICAL ANALYSIS

HEAT NUMBER	C	MN	SI	P	S	MO	CR	V	NB	NI	CU	SN	AL	TI	B	AS	CA	N	C.E.	
MINIMUM	%	%	%	%	%	%	%	%	%	%	%	%	%	%	%	%	%	%	%	%
MAXIMUM	0.140	1.35	0.40	0.015	0.005	0.080	0.20	0.060	0.040	0.20	0.200	0.015								
	93226	0.120	1.16	0.007	0.003	0.029	0.06	0.037	0.000	0.06	0.120	0.007	0.022	0.000	0.0000	0.004	0.0020	0.0058	0.35	

**100% ULTRASONIC INSPECTION**  
**SATISFACTORY**

**SR4-5% notch**

THIS CERTIFICATE CANCELS AND SUBSTITUTES THE ONE SENT ON 03/10/95 WITH No. 95003439.

**100% MAGNETIC PARTICLE INSPECTION**  
**SATISFACTORY**

NOTES: CERTIFICATE ACC. TO EN 10204/DIN 50049 3.1.C/DIN 50049 3.1.B /ASTM A106 B 94/ASTM A333 GRADE 6 94. HARDNESS ACCORDING TO NACE MR-01-75 1995. IMPACT TEST: SPECIMEN SIZE 10 X 7.50 MM. TEMPERATURE -50. HEAT TREATMENT: NORMALIZED (TEMPERATURE = 880 C). GRAIN SIZE ACC. TO ASTM E112-85. TAMSA REF: 2571. INSPECTION COMPANY: D.N.V. **on Pipe ends**

\*\*\* VARNISHED

ORIGINAL PAGE 4 OF 4  
ENG. SARA GARCIA PAJARES

MILL	QUANTITY	LENGTHS
EN 433 S. CARR MELVER	57	
ARCO PISA 403		
TEL (39) 051 1100		
TELEX 15843		
FAX (39) 051 02 88		

THIS IS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREIN WERE MANUFACTURED, SAMPLED, TESTED, AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.

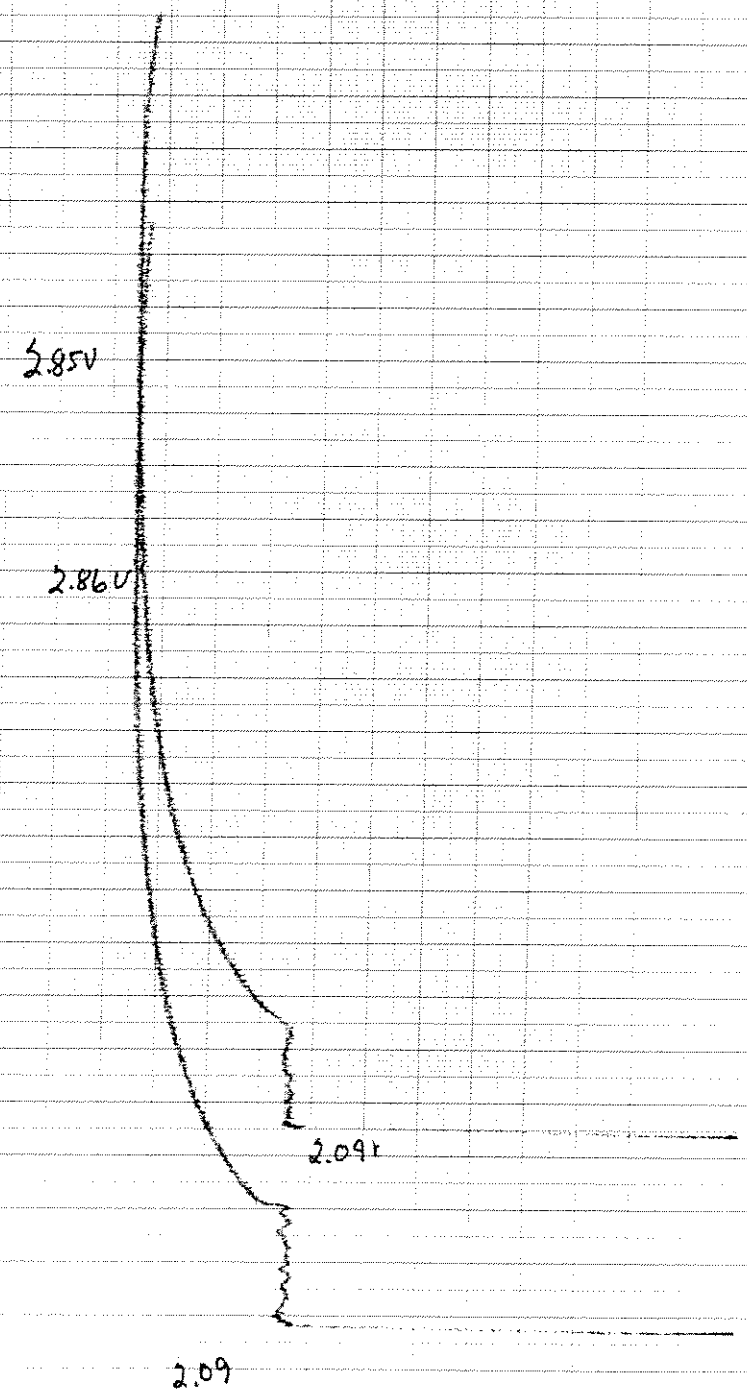
QUALITY CERTIFICATION NAME AND SIGNATURE





10V = 50kΩ ↓ 0.5V  
10V = 6.25mm → 0.5V

Circ. com



Prave T I

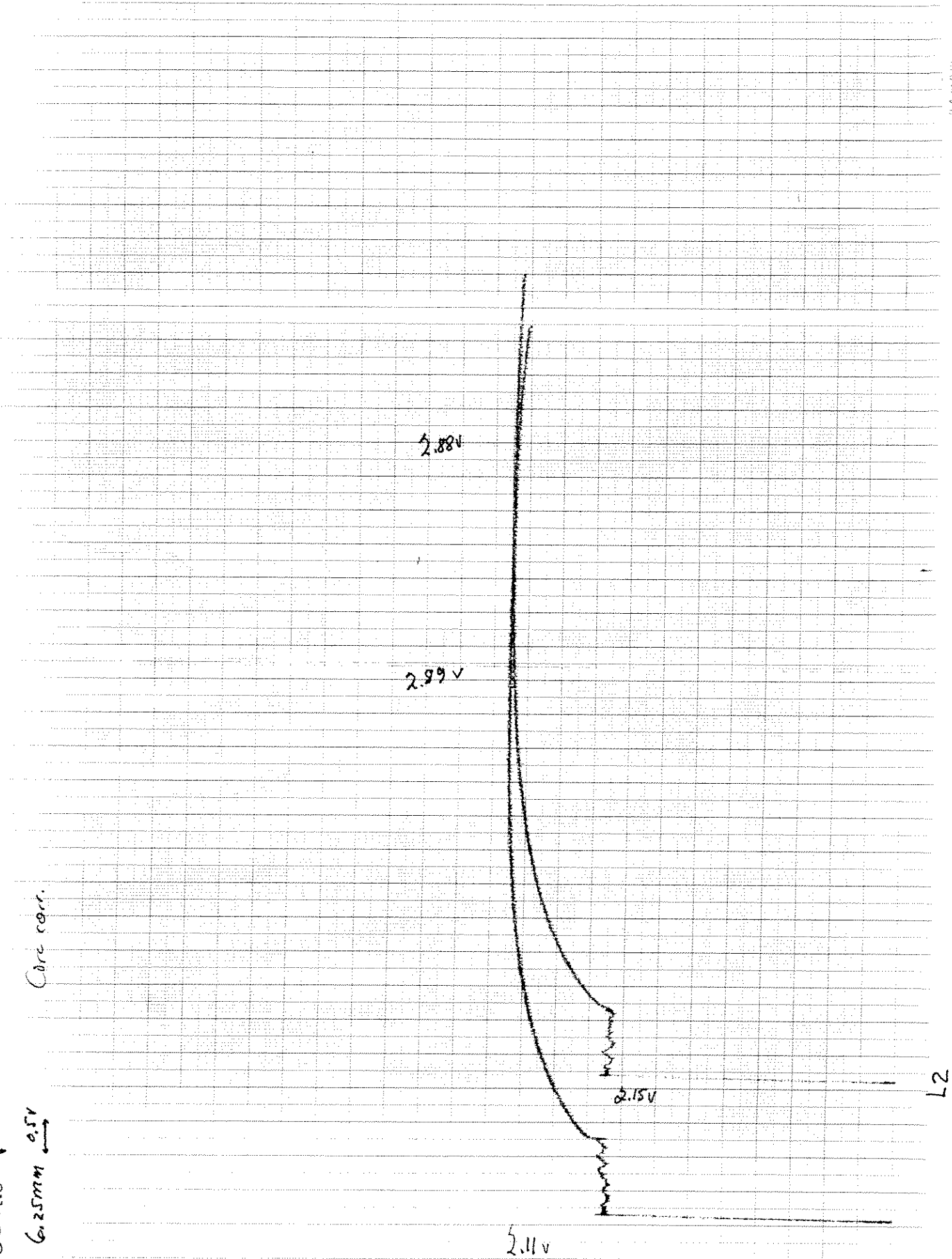
10V = 50kΩ

0.25V

10V = 6.25mm

0.5V

Core cart.



Probe L1

L2



### PAKKSEDEL/PACKING LIST

*For test specimen  
no. 10, 11 and 12*

LAGERP: Avd. OSLO

11510  
 DET NORSKE VERITAS INDUSTRY A/S  
 VERITASUN. 1  
 P.B. 300  
 1322 HØVIK

Lev. adresse:  
 3 STK FREDRIKSTAD MONTERING AS  
 INDUSTRIUN. 5-11  
 FREDRIKSTAD

S./P.: 1

Deres best.nr./Your P.O No. 6750      Deres ref./Your Ref. O.H.BJØRNØY      Vår ref./Our Ref. Thorbjørn Hoel / BMR      Vårt ordre nr./Our Order No. 169369 / 01

Marking/Marking 3 STK MRK: J. SÆTER      Best. dato/Date of Order 96-12-13

Bet.beting/Payment Terms NETTO PR. 30 DAGER      Lev.beting/Delivery Terms FOB OSLO      Lev.måte/Delivery      Lev.dato/Date of Delivery 96-12-13

Pr. / Vare / It./Article	Antall/ Quantity	Enh/ Unit	Levert/ Delivered	Rest/ Rest
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#### SERTIFIKAT EN 10204/3.1.B

1 014545A 323.8*10.31MM PIPE SP S.40 X52 MOD Ch.nr: <u>93226</u> 3 * 1 METER	3.00	m	<u>3,00</u> 29.73 kg	
2 014545A 323.8*10.31MM PIPE SP S.40 X52 MOD Ch.nr: <u>93226</u> 1 * 0.5 METER	0.50	m	<u>0,50</u> 29.73 kg	
3 281 KAPP	4.00	STK	<u>4</u>	

3 \* 1 METER SENDES FREDRIKSTAD MONTERING  
 0.5 METER SENDES VERITAS, HØVIK.  
 RØRENE TIL F.M. MERKES "J. SÆTER"  
 RØRET TIL DNU MERKES "O. BJØRNØY"  
 FRAKT TIL FREDRIKSTAD FORUTBETALES.  
 KOPI AV SERT. TIL BEGGE.

*3 stk in Fr. montering Thomsen A 10/12 - 96  
 1 stk in Veritas. Bil 10/12 - 96*

Porto : ..... Kollit : 4/108 ..... Uttak : DC/V ..... Lev dato : .....

Etter forfall beregnes 1.0 % rente pr. mnd. i.h.t. panteloven forbeholder vi oss eiendomsretten til ds leverte varer inntil kjøpenummer er helt betalt. Aksept ansees ikke som betaling før den er innfridd i sin helhet.

1.0 % per month is added for late payment. Title to goods belongs to ROLF LYCKE AS until payment.

10/11/12



DET NORSKE VERITAS

Certificate No.:  
VER 82895048-08

INSPECTION CERTIFICATE OF MATERIALS

- DNV certificate acc. to Classification Rules.
- 3.1C acc. to ISO 10474/EN 10204

Product <b>SEAMLESS LINE PIPE, 12-3/4 in x 0.406 in (323.9 mm x 10.30 mm)</b>	Total mass <b>(781.780 M) 80.647 Ton.</b>
Manufacturer <b>TUBOS DE ACERO DE MEXICO, S.A.</b>	Manufacturer's order No. <b>003830-03</b>
Purchaser <b>ROLF LYCKE A/S</b>	Purchaser's order No. <b>23008</b>

Destination/Supplementary information  
**NORWAY / Manufacturer's Certificate N° 99003439**

Material standard and grade <b>API Spec 5L (April 1, 1995), Grade X52</b>	Any additional requirements <b>As per Rolf Lycke A/S, PO 23006</b>
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SPECIFIED MECHANICAL PROPERTIES

TENSILE PROPERTIES					CHARPY V-NOTCH IMPACT PROPERTIES				
Specimen type/ dimensions	Yield point R <sub>0.2</sub> or R <sub>p0.2</sub>	Tensile strength R <sub>m</sub>	Elongation A <sub>5</sub>	Reduction of area Z	Orien- tation L or T	Test temp. °C	Width of test piece mm	Energy, J, min.	
	N/mm <sup>2</sup>	N/mm <sup>2</sup>	%	%				Single	Average
	360	490 - 620	22		T	-50	10	28	38

Remarks

SPECIFIED CHEMICAL COMPOSITION

Element	C, %	Mn, %	Si, %	P, %	S, %	Mo, %	Cr, %	V, %	Nb, %	Ni, %	Cu, %	CA, %	CE, %
Specific value(s)	0.14	1.38	0.40	0.015	0.005	0.080	0.20	0.060	0.040	0.20	0.200	0.004	0.41

Remarks V + Nb + Ti, 0.07% Max., V + Nb, 0.06% Max., Cu + 6Sn, 0.32% Max.

<p>Marking:</p> <p style="text-align: center; font-size: 2em;">N</p> <p>The stamping is placed: between 8 to 15 cm from pipe end</p>	<p>The materials are tested and inspected in the and are found to be in accordance with the above specification. (For test results, see overleaf)</p> <p style="text-align: right;">Normalized condition.</p> <p>If applicable state drawing number and approval date</p> <div style="text-align: right; margin-top: 20px;">   <b>R. O. TINOCO</b>              Inspector         </div> <div style="text-align: center; margin-top: 20px;">   <b>Veracruz, Mexico</b>              Place         </div> <div style="text-align: center; margin-top: 20px;"> <b>1995.10.27</b>              Date         </div>
--	---

I hereby agree that none be provided below Det Norske Veritas, its subsidiaries, bodies, officers, directors, employees and agents shall have no liability for any loss, damage or expense allegedly caused directly or indirectly by their mistake or negligence, breach of warranty, or any other act, omission or error by them, including gross negligence or willful misconduct by any such person with the exception of gross negligence or willful misconduct by the governing bodies or senior executive officers of Det Norske Veritas. This applies regardless of whether the loss, damage or expense has affected anyone with whom Det Norske Veritas has a contract or a third party who has relied or acted on decisions made or information given by or on behalf of Det Norske Veritas. However, if any person uses the services of Det Norske Veritas or its subsidiaries or relies on any decision made or information given by or on behalf of them and in consequence suffers a loss, damage or expense proved to be due to their negligence, omission or default, then Det Norske Veritas will pay by way of compensation to such person a sum representing the proved loss. In the event Det Norske Veritas or its subsidiaries may be held liable in accordance with the sentence above, the amount of compensation shall under no circumstances exceed the liability of the loss, if any, alleged for that particular service, omission, advice or information. Under no circumstances whatsoever shall the individual or individuals who have personally caused the loss, damage or expense be held liable. In the event that any provision in this section shall be invalid under the law of any jurisdiction, the validity of the remaining provisions shall not in any way be affected.

10/11/12

Certificate No.:  
VER 52895045-06

MECHANICAL PROPERTIES												
TENSILE TESTS						CHARPY V-NOTCH IMPACT TESTS						
Cast. No.	Test No.	Yield point	Tensile strength	Elongation	Reduction	Orientation	Width of test piece	Test temp	Energy, J, min.			
		R <sub>eH</sub> or R <sub>p0.2</sub>	R <sub>m</sub>	A <sub>5</sub>	Z				1	2	3	Avg.
		N/mm <sup>2</sup>	N/mm <sup>2</sup>	%	%	L or T	mm	°C				
93226	01	375.60	513.88	48		T	10	-60	70	73	69	71
	02	401.10	526.59	46		T	10	-60	69	69	78	71

Remarks

CHEMICAL COMPOSITION													
Cast. No.	C, %	Mn, %	Si, %	P, %	S, %	Mo, %	Cr, %	V, %	Nb, %	Ni, %	Cu, %	CA, %	CE, %
93226	0.139	1.16	0.26	0.007	0.004	0.030	0.05	0.034	0.00	0.06	0.123	.0022	0.36
93226	0.138	1.14	0.25	0.007	0.004	0.029	0.06	0.034	0.00	0.06	0.121	.0022	0.36

Remarks: Product Chemical Analysis

Process: Seamless pipe  
Heat treatment (state temperatures): Normalized: 880 C

Non-destructive testing: Ultrasonic SR4 - 5% Notch & MPI

**ADDITIONAL NOTES**

Type and extent of inspection:  
Review of Chemical Analysis and Data Sheets, Mechanical Properties, Review of Dimensional Control Sheets and Hydrostatic Test Records, Ultrasonic & Electromag. Inspection Records, DNV Marking and Issue of Insp. Certificate.

10/11/12

TUBOS DE ACERO DE MEXICO, S.A.

PURCHASER		MILL TEST CERTIFICATE		INSPECTOR		DATE		No.	
ROLF LYCKE A.S.		003830 / 03		MR. RAFAEL LIMCO		24/10/95		95003439	
TYPE OF PIPE		DIMENSIONS		NOMINAL WEIGHT		STEEL GRADE		ENDS	
LINE PIPE SEAMLESS		12 3/4 INCH X 0.406 INCH		53.52 LB/FT		X52		NORMAL BEVEL	
SPECIFICATION OR STANDARD		SPECIFIC LENGTH OR R		SURFACE		HYDROSTATIC TEST R		5 SEC	
API 5L		APRIL 1, 1995.		26.20 / 45.90 FT		***		2810 PSI	
HEAT NUMBER		LONGITUDINAL STRENGTH TENSILE		MECHANICAL PROPERTIES AND TEST		IMPACT CHART		HARDNESS	
93226		490.00 620.00		RELONGATION IN 2 INCH		TENSILE SAMPLE INDIVIDUAL		SHEAR AREA	
93226		360.00 401.70		46 46		MM. MM.		HRC (HRB)	
MINIMUM		22.0		28.000		35.000		22.00 ( )	
MAXIMUM		375.60 401.70		38.10 10.80 70.000 69.000		71.000 71.000		80.11 HRB 82.00 HRB	

INSPECTION SATISFACTORY: SR-4 · ENI · VPI · MPI

100% ULTRASONIC INSPECTION  
SATISFACTORY

SR4-5% notch

100% MAGNETIC PARTICLE INSPECTION  
SATISFACTORY

on Pipe ends

INSPECTION SATISFACTORY: SR-4 · ENI · VPI · MPI

WARRANTY

WE OILS CARBON MEXICO  
VERMONTA, VER  
LIDIO SOLAR, S  
TEL: 01 244 3  
FAX: 01 244 3

QUANTITY 57 UNITS

ORIGINAL PAGE 1 OF 4

ENG. SARA GARCIA PAJARES

DATE OF CERTIFICATION NAME AND SIGNATURE

THIS IS TO CERTIFY THAT THE PRODUCT DESCRIBED HEREIN WERE MANUFACTURED OR SAMPLED, TESTED, AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.

DCR 07188



10/11/12



# TUBOS DE ACERO DE MEXICO, S.A.

PURCHASER		MILL TEST CERTIFICATE		DATE		NO.			
ROLF LYCKE A.S.		SALES CONFIRMATION		INSPECTOR		24/10/95		95003439	
TYPE OF PIPE		DIMENSIONS		NOMINAL WEIGHT		STEEL GRADE		ENDS	
SEAMLESS		12 3/4 INCH X 0.406 INCH		53.52 LB/FT		K52		NORMAL LEVEL	
SPECIFICATION OR STANDARD		SPECIFIC LENGTH OR R.		SURFACE		HYDROSTATIC TEST P.		HYDROSTATIC TEST P.	
API 5L		26.20 / 45.90 FT		***				2810 PSI	
APRIL 1, 1995.								5 SEC	

HEAT NUMBER

GRAIN SIZE

MINIMUM 8

MAXIMUM 10

93226

93226

HEAT METALLOGRAPHIC EVALUATION LEVEL INCLUSIONS

HARDNESS VICKER HV

A	B	C	D
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100% ULTRASONIC INSPECTION SATISFACTORY

SR4-5% notch

100% MAGNETIC PARTICLE INSPECTION SATISFACTORY

on Pipe ends

VARNISHED

QUANTITY	57 LENGTH
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ORIGINAL PAGE 2 OF 4

ENG. SARA GARCIA PALMES

THIS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREIN WERE MANUFACTURED, SAMPLED, TESTED AND / OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.

DECA 777 84 8

10/11/12



# TUBOS DE ACERO DE MEXICO, S.A.

PURCHASER		MILL TEST CERTIFICATE	
ROLF LYCKE A.S.		SALES CONFIRMATION	
TYPE OF PIPE		INSPECTOR	
SEAMLESS		DATE	
DIMENSIONS		No.	
12 3/4 INCH	X 0.406 INCH	MR. RAFAEL TIMCO	24/10/95
SPECIFICATION OR STANDARD		STEEL GRADE	
API 5L		K52	
APRIL 1, 1995.		HYDROSTATIC TEST P.	
SPECIFIC LENGTH OR R.		SURFACE	
26.20 / 45.90 FT		2810 PSI	
***		5 SEC	

## PRODUCT CHEMICAL ANALYSIS

HEAT NUMBER	C	MN	SI	P	S	MO	CR	V	NB	NI	CU	SN	AL	TI	B	AS	CA	C.E.	
MINIMUM	0.139	0.16	0.007	0.004	0.030	0.05	0.034	0.000	0.000	0.06	0.123	0.006	0.020	0.000	0.000	0.004	0.0022	0.36	
MAXIMUM	0.138	0.25	0.007	0.004	0.029	0.06	0.034	0.000	0.000	0.06	0.121	0.006	0.017	0.000	0.000	0.004	0.0022	0.36	
	0.140	1.35	0.40	0.015	0.005	0.080	0.20	0.060	0.040	0.20	0.200	0.015						0.0040	0.41

**100% ULTRASONIC INSPECTION**  
**SATISFACTORY**

**SR4-5% notch**

**100% MAGNETIC PARTICLE INSPECTION**  
**SATISFACTORY**

**on Pipe ends**

VARNISHED

ORIGINAL PAGE 3 OF 4

QUANTITY 57 LENGTH

ENG. SARA GARCIA PAJARES

QUALITY CERTIFICATION NAME AND SIGNATURE

THIS IS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREIN WERE MANUFACTURED, SAMPLED, TESTED, AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.

PLUZ 05/27/94

00CA 17/84A



10/11/12

# TUBOS DE ACERO DE MEXICO, S.A.



## MILL TEST CERTIFICATE

PURCHASER ROLF LYCKE A.S.		SALES CONFIRMATION 003830 / 03		INSPECTOR MR. RAFAEL TIMOCO		DATE 24/10/95		No. 95003439	
TYPE OF PIPE LINE PIPE		DIMENSIONS 12 3/4 INCH X 0.406 INCH		NOMINAL WEIGHT 53.52 LB/FT		STEEL GRADE K52		ENDS NORMAL BEVEL	
SPECIFICATION OR STANDARD API 5L		APRIL 1, 1995.		SPECIFIC LENGTH OR R. 26.20 / 45.90 FT		SURFACE SURFACE		HYDROSTATIC TEST 2810 PSI 5 SEC	

### HEAT CHEMICAL ANALYSIS

HEAT NUMBER	C	MN	SI	P	S	MO	CR	V	NB	NI	CU	SN	AL	TI	B	AS	CA	N	C.E.
93226	0.140	1.35	0.40	0.015	0.005	0.080	0.20	0.060	0.040	0.20	0.200	0.015							
MAXIMUM	0.140	1.35	0.40	0.015	0.005	0.080	0.20	0.060	0.040	0.20	0.200	0.015							
	0.120	1.16	0.26	0.007	0.003	0.029	0.06	0.037	0.000	0.120	0.007	0.022	0.000	0.000	0.004	0.0020	0.0058	0.35	

100% **ULTRASONIC INSPECTION**  
**SATISFACTORY**

**SR4-5% notch**

100% **MAGNETIC PARTICLE INSPECTION**  
**SATISFACTORY**

THIS CERTIFICATE CANCELS AND SUBSTITUTES THE ONE SENT ON 03/10/95 WITH No. 95003439.

NOTES: CERTIFICATE ACC. TO "EN 10204/DIN 50049 3.1.C/DIN 50049 3.1.B /ASTM A106 B 99/ASTM A333 GRADE 6 94. HARDNESS ACCORDING TO  
 PAGE MR-01-75 1995. IMPACT TEST: SPECIMEN SIZE 10 X 7.50 IN. TEMPERATURE -50 °C. HEAT TREATMENT: NORMALIZED (TEMPERATURE =  
 880 C). GRAIN SIZE ACC. TO ASTM E112-85. TAMSA REF: 29. I. INSPECTION COMPANY: D.N.V. **on Pipe ends**  
 VARNISHED

ORIGINAL PAGE 4 OF 4  
ENG. SARA GARCIA PALARES

NO. 0023, CASE NUMBER	57
VENUE, CITY AND POSTAL AND TELEPHONE NUMBER	LENNING
DATE	

THIS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREIN WERE MANUFACTURED, SAMPLED, TESTED, AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.

QUALITY CERTIFICATION NAME AND SIGNATURE

DNV 172 84 0

**APPENDIX**

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**C**

**LISTING OF TEST RESULTS**

Printout of the Excel spreadsheet results for the tests are given. The content of each column are described in the table.

Column	Test no.1	Test nos. 2-4	Test nos. 5-12
A	time	time	time
B	internal press (bar)	internal press (bar)	internal press (bar)
C		actuator force (kN)	jack force (kN)
D		actuator disp. (mm)	jack disp. (mm)
E		angle (deg) for test 3 and 4	
F	test time (sec)	test time (sec)	test time (sec)
G		bending moment (kNm)	(jack force/10)
H	$\sigma_{\text{axial, int. press}}$	$\sigma_{\text{axial, int. press}}$	$\sigma_{\text{axial, int. press}}$
I		$\sigma_{\text{axial, moment}}$	$\sigma_{\text{axial, jack force}}$
J	$\sigma_{\text{axial, total}}$	$\sigma_{\text{axial, total}}$	$\sigma_{\text{axial, total}}$
K	$\sigma_{\text{hoop}}$	$\sigma_{\text{hoop}}$	$\sigma_{\text{hoop}}$
L	-	-	-
M	strain gauge 1	strain gauge 1	strain gauge 1
N	strain gauge 1	strain gauge 1	strain gauge 1
O	strain gauge 2	strain gauge 2	strain gauge 2
P	etc... to no. of gauges	etc... to no. of gauges	etc... to no. of gauges

Column A-E and M and the following letters contains measured values.

Column F-L contains calculated values

All stresses ( $\sigma$ ) are in MPa, and strain in microstrain  $\mu\epsilon$  ( $10^{-6}$ ).

Examples; 2500  $\mu\epsilon$  = 0.25% strain, 85000  $\mu\epsilon$  = 8.5% strain

Calculation of;

$$\sigma_{\text{axial, int. press}} = \text{internal pressure} * (\text{Area}_{\text{inner}} / \text{Area}_{\text{pipe}})$$

$$\sigma_{\text{axial, moment}} = \text{bending moment} / W_{\text{elastic}}$$

$$\sigma_{\text{axial, jack force}} = \text{axial force} / \text{Area}_{\text{pipe}}$$

$$\sigma_{\text{axial, total}} = \text{sum of the above axial stresses}$$

$$\sigma_{\text{hoop}} = \text{internal pressure} * (D_i / 2*t)$$

where the following values are used for the cross section;

- Area<sub>pipe</sub> = 10437 mm<sup>2</sup>  $(D_o^2 - D_i^2) * \pi / 4$
- Area<sub>inner</sub> = 72012 mm<sup>2</sup>  $(D_i^2) * \pi / 4$
- Moment of Inertia (I) = 1.28 \* 10<sup>8</sup> mm<sup>4</sup>  $(D_o^4 - D_i^4) * \pi / 64$
- Section modulus W<sub>elastic</sub> = 791854 mm<sup>3</sup>  $I / (D_o / 2)$

D<sub>o</sub> ; Outer Diameter = 324 mm

D<sub>i</sub> ; Inner Diameter = 302.8 mm

( wall thickness t = 10.6 mm)

The calculations are based on the undeformed cross-section.

- o0o -



Y	X	W	V	U	T	S	R	Q	P	O	N	M	L	K	J	I	H	G	F	E	D	C	B	A	AI																																																																															
0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF	AG	AH	AI	
1	15495520	15495521	15495522	15495523	15495524	15495525	15495526	15495527	15495528	15495529	15495530	15495531	15495532	15495533	15495534	15495535	15495536	15495537	15495538	15495539	15495540	15495541	15495542	15495543	15495544	15495545	15495546	15495547	15495548	15495549	15495550	15495551	15495552	15495553	15495554	
2	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	
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	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF	AG	AH	AI			
169	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50	15,30,50





text 3

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF	AG	AH
81	49329	188.9	-320	28.1	9.825	2857	200.3	130.3	252.9	-122.6	269.8																67	18011	-100	27268	-439	1428	1219	869
82	49329	194.6	-320	30.9	0.867	2877	200.2	134.3	-252.9	-118.5	277.9																14	18019	-114	24227	-411	1453	1211	921
83	49329	192.5	-320	33.3	1.073	2707	200.3	132.8	-252.9	-120.1	274.9																9	18035	-122	24713	-432	1442	1169	929
84	49329	190.3	-320	34.5	1.182	2827	200.2	131.3	-252.9	-121.6	271.8																4	17998	-149	24160	-458	1434	1138	928
85	49329	189.4	-320	36.1	1.202	3007	200.5	130.7	-259.6	-129.9	270.5																6	17988	-163	24960	-495	1438	1133	977
86	49329	189.9	-320	36.7	1.228	3026	210.2	130.3	-295.5	-136.2	269.9																7	17958	-152	24658	-507	1448	1167	972
87	49329	189.4	-340	37.3	1.251	3039	212.3	130.0	-295.2	-136.2	269.1																7	17958	-152	24658	-507	1448	1167	972
88	49329	189.4	-340	37.9	1.273	3047	212.5	129.7	-298.4	-136.7	269.5																7	17958	-152	24658	-507	1448	1167	972
89	49329	189.4	-340	38.6	1.308	3057	212.4	131.9	-298.3	-136.4	273.9																7	17958	-152	24658	-507	1448	1167	972
90	49329	189.4	-340	40.5	1.353	3067	212.5	134.1	-298.4	-136.5	274.8																7	17958	-152	24658	-507	1448	1167	972
91	49329	189.4	-340	42.9	1.411	3067	212.5	137.5	-298.4	-136.5	274.8																7	17958	-152	24658	-507	1448	1167	972
92	49329	189.4	-340	45.1	1.477	3067	212.5	139.2	-298.4	-136.5	274.8																7	17958	-152	24658	-507	1448	1167	972
93	49329	189.4	-340	47.0	1.551	3077	212.5	139.2	-298.4	-136.6	274.8																20	17958	-152	24658	-507	1448	1167	972
94	49329	189.4	-340	47.4	1.625	3267	212.4	133.6	-298.2	-137.1	271.8																9	17937	-133	24038	-594	1486	1132	963
95	49329	190.3	-340	47.4	1.726	3267	212.4	133.6	-298.2	-137.1	271.8																9	17937	-133	24038	-594	1486	1132	963
96	49329	193.6	-340	47.7	1.726	3267	212.4	133.6	-298.2	-137.1	271.8																2	17969	-133	23699	-611	1478	1146	962
97	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																3	17902	-134	23337	-610	1489	1150	967
98	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																3	17902	-134	23337	-610	1489	1150	967
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9	1.795	3087	212.4	134.5	-298.3	-133.8	278.4																5	17922	-135	23934	-592	1523	1178	969
99	49329	194.9	-340	48.9																														



	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF						
76	50237	258.9	-193	121.2	4.54	4769	142	176.7	-176.0	-0.3	365.8	-21238	27456	26270	4508	-24922	0	-25412	146900	-24113	126070																	
77	50302	259.1	-188	121.2	4.54	4780	139	176.7	-174.7	4.6	371.0	-21237	27590	26335	4625	-24922	0	-25463	150020	-24185	130020																	
78	50401	259.8	-188	121.2	4.54	4809	138	176.8	-173.9	6.9	374.2	-21340	27633	26385	4665	-24975	0	-25508	150930	-24191	130640																	
79	50441	260.4	-186	121.2	4.54	4829	136	181.8	-172.2	9.5	376.2	-21346	27896	26385	4725	-25023	0	-25544	151740	-24229	131430																	
80	50457	261.6	-181	121.2	4.54	4845	133	182.6	-168.5	14.1	377.9	-21599	27890	26446	4841	-25122	0	-25613	165480	-24326	132780																	
81	50506	261.2	-178	121.2	4.55	4914	130	180.2	-163.8	16.5	373.1	-21596	27898	26512	4865	-25265	0	-25706	0	-25720	0	-24443	0															
82	50598	265.2	-175	121.2	4.55	4984	129	175.5	-162.5	17.0	371.6	-21534	27928	26527	4899	-25213	0	-25739	0	-25739	0	-24449	0															
83	50621	267.8	-172	121.2	4.55	5009	128	182.3	-162.1	20.2	377.4	-21393	27970	26544	5041	-25215	0	-25988	0	-26004	0	-24649	0															
84	50641	267.8	-172	121.2	4.55	5034	126	184.8	-160.1	25.5	382.5	-21301	28085	26598	5168	-25302	0	-26286	0	-26286	0	-24649	0															
85	50646	268.3	-170	121.2	4.55	5034	125	185.1	-159.1	27.0	383.3	-21304	28130	26619	5208	-25335	0	-26386	0	-26386	0	-24649	0															
86	50651	268.6	-165	121.2	4.55	5049	121	186.0	-153.3	32.7	385.1	-21329	28255	26681	5377	-25451	0	-26598	0	-26598	0	-24649	0															
87	50671	271.1	-157	121.2	4.56	5099	118	183.9	-148.6	35.2	380.9	-21349	28388	26752	5522	-25561	0	-26808	0	-26808	0	-24720	0															
88	50776	271.1	-157	121.2	4.56	5179	114	187.1	-146.1	40.9	387.3	-21357	28538	26805	5663	-25660	0	-27028	0	-27028	0	-24720	0															
89	50816	274.5	-149	121.2	4.57	5294	109	189.4	-138.3	51.1	392.1	-21365	28668	26854	5781	-25713	0	-27288	0	-27288	0	-24720	0															
90	50841	278.3	-143	121.2	4.57	5329	105	190.6	-132.8	57.8	394.6	-21402	29142	27052	6095	-25825	0	-27591	0	-27591	0	-24843	0															
91	50826	272.6	-138	121.2	4.58	5314	102	188.1	-128.2	58.9	396.4	-21425	29345	27127	6377	-25951	0	-27898	0	-27898	0	-24962	0															
92	50896	278.5	-136	121.2	4.58	5314	100	192.2	-126.3	65.8	397.8	-21425	29497	27175	6733	-25951	0	-28148	0	-28148	0	-25010	0															
93	50906	280.4	-132	121.2	4.58	5384	97	193.5	-122.5	71.0	400.5	-21432	29718	27249	6778	-25986	0	-28208	213250	-25094	0																	
94	50928	276.5	-127	121.2	4.59	5484	93	193.8	-117.9	72.9	395.0	-21463	29947	27326	7244	-25986	0	-28376	169530	-25094	0																	
95	50938	281.8	-125	121.2	4.59	5574	92	194.4	-115.9	78.0	402.5	-21467	30178	27424	7651	-25986	0	-28512	174950	-25094	0																	
96	50956	283.4	-122	121.2	4.59	5644	89	195.8	-112.8	82.7	404.1	-21468	30273	27545	7652	-25986	0	-28512	174950	-25094	0																	
97	50967	285.9	-116	121.2	4.60	5915	85	195.7	-107.5	95.2	400.2	-21446	30793	27845	8071	-25986	0	-28512	174950	-25094	0																	
98	50977	286.6	-111	121.2	4.61	6095	77	196.8	-101.7	101.7	411.5	-21449	31480	27726	8033	-25986	0	-28512	174950	-25094	0																	
99	50977	286.3	-103	121.2	4.61	6095	77	196.8	-97.2	101.7	411.8	-21439	31596	27739	8007	-25986	0	-28512	168000	-20837	0																	
100	60381	289.6	-100	121.2	4.61	6095	73	198.8	-92.6	109.3	412.8	-21360	31883	27819	8309	-25986	0	-28512	168000	-20837	0																	
101	60386	288.5	-97	121.2	4.62	6584	71	198.1	-88.8	109.3	412.8	-21317	31985	27849	8564	-25986	0	-28512	168000	-20837	0																	
102	60394	288.5	-95.5	-2	121.2	5.48	6694	1	-3.8	-1.4	-7.8	-18907	28733	27253	7932	-6489	0	-7303	58410	0																		

11:35:11 Progeve 961205a

Test time Force (10\*MAX\_gross (MAX\_force (Maxial (MPa) Hoop (MPa)

All strain gauges in microstrain

Time	Test Date	S Pipe 18 12 96 Time	disp mm	measured force (kN)	measured disp (mm)	ax-force	hoop	hoop	hoop	Gauge 3												Gauge 4												Gauge 5												Gauge 6												Gauge 7												Gauge 8												Gauge 9												Gauge 10																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										
										0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819	820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840	841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861	862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882	883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903	904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924	925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945	946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966	967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987	988	989	990

A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE
5	50474	150	2650	5.34	3629	250.5	137.7	249.6	-119.9	285.1	282.5	81522	-16526	84728	-14738	73029	-48116	1623	-785	18846	-634	13520	-11330	15107	-10326					
6	50475	150	2640	5.46	3829	257.4	136.5	256.2	-119.7	282.5	282.5	81577	-16594	84878	-14822	73029	-48116	1623	-785	18846	-634	13520	-11330	15107	-10326					
7	50484	155	2727	5.51	3934	272	134.7	278.8	-128.6	278.8	278.8	81598	-16638	85012	-14964	73056	-48116	1674	-848	17098	-776	14097	-11904	15276	-10312					
8	50489	155	2730	5.61	3939	273	135.9	262.2	-129.4	275.1	281	81599	-16681	85131	-15067	73056	-48116	1674	-848	17098	-776	14097	-11904	15276	-10312					
9	50504	185	2793	6.07	3954	270.3	128.7	267.6	-138.9	266.5	266.5	81543	-16683	85288	-15215	73022	-48116	1949	-1166	17159	-2206	14844	-12679	15396	-10369					
10	50509	185	2796	6.13	3965	294.5	128.0	272.6	-144.6	265.0	265.0	81512	-16661	85328	-15242	73022	-48116	1949	-1166	17159	-2206	14844	-12679	15396	-10369					
11	50514	185	2799	6.24	3964	278.8	128.4	267.1	-140.7	261.7	261.7	81490	-16670	85330	-15278	73022	-48116	1949	-1166	17159	-2206	14844	-12679	15396	-10369					
12	50518	181	2841	6.37	3969	294.1	125.0	272.2	-147.3	258.7	258.7	81475	-16682	85335	-15261	73022	-48116	2044	-1411	17245	-5155	15371	-13112	15428	-10461					
13	50523	174	2910	6.70	3879	251.8	120.7	275.6	-158.9	249.8	249.8	81424	-16731	85458	-15509	73024	-48116	2244	-1637	17329	-10503	16044	-13457	15628	-10568					
14	50538	173	2987	6.82	3924	298.7	116.6	266.2	-156.6	247.5	247.5	81436	-16721	85466	-15537	73024	-48116	2244	-1637	17329	-10503	16044	-13457	15628	-10568					
15	50545	168	3057	6.79	3894	305.7	116.2	292.5	-176.7	240.5	240.5	81339	-16738	85511	-15647	73024	-48116	2760	-2648	17367	-13701	17011	-13880	15932	-10681					
16	50559	178	3066	7.30	4039	289.8	123.0	277.7	-164.6	254.7	254.7	81327	-16661	85671	-15675	73022	-48116	3055	-2893	17619	-13907	17570	-13761	16111	-10677					
17	50564	189	3107	7.37	4014	277.7	123.1	266.1	-135.0	271.4	271.4	81528	-16566	85666	-15667	73022	-48116	3055	-2893	17619	-13907	17570	-13761	16111	-10677					
18	50569	198	3100	7.48	4019	268.8	130.7	257.5	-109.9	282.9	282.9	81679	-16541	85713	-15664	73024	-48116	3596	-3360	17801	-14555	17703	-13831	15964	-10674					
19	50584	188	3050	7.73	4024	260.2	135.6	249.3	-120.9	288.9	288.9	81911	-16503	85657	-15697	73022	-48116	3643	-3366	18172	-14333	17883	-13922	16111	-10716					
20	50589	188	3050	7.89	4034	265.7	137.3	278.6	-122.6	278.6	278.6	81911	-16503	85657	-15697	73022	-48116	3643	-3366	18172	-14333	17883	-13922	16111	-10716					
21	50594	194	3100	7.92	4044	269	134.3	268.6	-123.6	273.6	273.6	81904	-16586	85670	-15698	73022	-48116	4534	-3892	18172	-14333	17883	-13922	16111	-10716					
22	50599	188	3050	8.08	4054	264.2	131.7	273.3	-140.6	272.7	272.7	81850	-16680	85693	-15698	73022	-48116	4534	-3892	18172	-14333	17883	-13922	16111	-10716					
23	50604	188	3050	8.24	4064	278	128.5	268.5	-136.0	265.9	265.9	81737	-16672	85691	-15717	73024	-48116	4594	-3892	18172	-14333	17883	-13922	16111	-10716					
24	50609	181	2940	8.38	4064	278	128.5	268.5	-136.0	265.9	265.9	81737	-16672	85691	-15717	73024	-48116	4594	-3892	18172	-14333	17883	-13922	16111	-10716					
25	50614	181	2940	8.57	4079	266.7	124.1	283.3	-165.3	256.6	256.6	81684	-16693	85698	-15710	73024	-48116	7061	-7463	18386	-14673	18216	-14860	16633	-11417					
26	50619	178	2970	8.67	4084	262.6	122.0	280.3	-168.4	243.5	243.5	81646	-16693	85698	-15710	73024	-48116	7061	-7463	18386	-14673	18216	-14860	16633	-11417					
27	50624	178	2970	8.87	4084	262.6	122.0	280.3	-168.4	243.5	243.5	81646	-16693	85698	-15710	73024	-48116	7061	-7463	18386	-14673	18216	-14860	16633	-11417					
28	50629	178	2970	9.03	4094	266.1	119.9	283.7	-183.9	246.1	246.1	81568	-16693	85698	-15710	73024	-48116	8413	-8465	18465	-14860	18216	-14860	16633	-11417					
29	50634	178	2970	9.21	4084	266.1	119.9	283.7	-183.9	246.1	246.1	81568	-16693	85698	-15710	73024	-48116	8413	-8465	18465	-14860	18216	-14860	16633	-11417					
30	50639	185	3020	9.36	4084	302.2	117.2	289.5	-171.4	238.2	238.2	81644	-16693	85698	-15710	73024	-48116	8413	-8465	18465	-14860	18216	-14860	16633	-11417					
31	50644	185	3020	9.55	4134	309.3	115.1	294.4	-182.5	233.7	233.7	81628	-16673	85740	-15823	73022	-48116	8957	-8957	18594	-15079	18594	-15079	16719	-10669					
32	50649	185	3020	9.69	4134	309.3	115.1	294.4	-182.5	233.7	233.7	81628	-16673	85740	-15823	73022	-48116	8957	-8957	18594	-15079	18594	-15079	16719	-10669					
33	50654	169	3120	9.69	4114	312	117.0	298.9	-187.9	238.4	238.4	81413	-16718	85740	-15823	73022	-48116	10764	-10967	18594	-15079	18594	-15079	16719	-10669					
34	50659	169	3120	10.04	4134	316.5	117.0	298.9	-187.9	238.4	238.4	81413	-16718	85740	-15823	73022	-48116	10764	-10967	18594	-15079	18594	-15079	16719	-10669					
35	50664	153	3150	10.08	4120	310	116.6	287.0	-181.2	219.0	219.0	81270	-16688	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
36	50669	153	3150	10.23	4134	310	116.6	287.0	-181.2	219.0	219.0	81270	-16688	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
37	50674	149	3060	10.09	4134	308	116.6	285.1	-184.5	219.0	219.0	81404	-16688	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
38	50679	149	3060	10.22	4146	284.3	128.8	287.3	-183.4	286.8	286.8	81576	-16640	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
39	50684	148	2840	10.37	4164	275.9	128.1	286.3	-183.5	282.8	282.8	81644	-16640	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
40	50689	139	2750	10.30	4164	275.9	128.1	286.3	-183.5	282.8	282.8	81644	-16640	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
41	50694	139	2750	10.46	4179	264.4	130.0	283.3	-183.4	282.8	282.8	81892	-16641	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
42	50699	139	2750	10.36	4179	264.4	130.0	283.3	-183.4	282.8	282.8	81892	-16641	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
43	50704	139	2750	10.49	4244	266.1	131.9	274.7	-180.4	277.1	277.1	82106	-16653	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
44	50709	139	2750	10.72	4244	266.1	131.9	274.7	-180.4	277.1	277.1	82106	-16653	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
45	50714	139	2750	10.82	4244	266.1	131.9	274.7	-180.4	277.1	277.1	82106	-16653	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
46	50719	139	2750	11.01	4254	266.3	132.3	274.3	-185.0	267.7	267.7	82106	-16653	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
47	50724	139	2750	11.19	4254	266.3	132.3	274.3	-185.0	267.7	267.7	82106	-16653	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
48	50729	139	2750	11.37	4254	266.3	132.3	274.3	-185.0	267.7	267.7	82106	-16653	85802	-15853	73024	-48116	11959	-12159	18594	-15079	18594	-15079	16719	-10669					
49	50734	139	2750	11.57	4260	300.0	127.1	2																						





63	44372	191.0	2768.0	10.5	972	278.8	131.8	-264.2	-133.4	-1791.3	87324	-17802	16624	-13674	17585	-15908	17677	-15079	16627	-11463	Z
64	44382	195.0	3068.0	11.5	992	306.8	134.5	-295.0	-159.4	-18855	87926	-17928	19401	-14361	18506	-16762	19051	-15970	19223	-14155	Y
65	44397	195.0	2826.0	11.9	897	282.6	134.5	-270.8	-136.2	-18955	88287	-17928	19401	-14361	18506	-16762	19051	-15970	19223	-14155	X
66	44417	201.2	2747.0	12.8	1027	274.7	138.8	-261.2	-124.4	-18955	90269	-17928	19401	-14361	18506	-16762	19051	-15970	19223	-14155	W
67	44427	206.3	2726.0	13.2	1027	272.6	142.3	-261.2	-118.8	-19532	90274	-18562	22032	-15402	20011	-17933	20465	-16220	21347	-16125	V
68	44452	207.0	2885.0	14.1	1052	288.5	142.8	-276.4	-133.6	-19532	94250	-19549	20960	-18941	20558	-18304	21004	-16446	21956	-16564	U
69	44467	201.4	3008.0	14.8	1067	300.8	139.0	-288.2	-149.2	-19888	94680	-19888	22908	-15769	20558	-18304	21004	-16446	21956	-16564	T
70	44472	201.6	2699.0	15.0	1072	269.9	139.3	-277.7	-138.4	-20769	94680	-20769	26095	-17482	22606	-19914	23010	-17586	23949	-18340	S
71	44477	200.6	3051.0	15.2	1072	305.1	139.3	-277.7	-138.4	-20769	94680	-20769	26095	-17482	22606	-19914	23010	-17586	23949	-18340	R
72	44512	198.1	3197.0	16.8	1117	319.7	138.4	-292.3	-153.9	-23055	97000	-23055	29465	-19482	24946	-21809	23472	-17853	24437	-18748	Q
73	44517	200.0	3085.0	16.9	1117	308.5	138.4	-292.3	-153.9	-23055	97000	-23055	29465	-19482	24946	-21809	23472	-17853	24437	-18748	P
74	44522	197.2	3235.0	17.2	1122	323.5	136.1	-310.0	-173.8	-25274	104560	-25274	30184	-19932	25473	-22229	25639	-19351	27007	-20847	O
75	44582	197.6	3347.0	18.9	1157	334.7	136.5	-320.7	-184.2	-26111	104560	-26111	30184	-19932	25473	-22229	25639	-19351	27007	-20847	N
76	44582	195.6	3467.0	20.4	1182	346.7	135.5	-320.7	-184.2	-26111	104560	-26111	30184	-19932	25473	-22229	25639	-19351	27007	-20847	M
77	44632	200.2	3580.0	23.3	1232	358.0	135.5	-331.2	-196.3	-27938	1133280	-27938	33691	-26173	29337	-25230	29633	-21952	31279	-24894	L
78	44637	200.2	3483.0	23.5	1232	348.3	138.1	-344.0	-205.8	-29620	0	-29620	40101	-26414	32926	-27939	33115	-24465	35636	-20955	K
79	44647	201.7	3609.0	24.1	1247	360.9	138.1	-344.0	-205.8	-29620	0	-29620	40101	-26414	32926	-27939	33115	-24465	35636	-20955	J
80	44677	208.0	3515.0	25.6	1277	351.5	143.5	-336.8	-193.3	-34756	126450	-34756	40938	-29884	33329	-28140	33399	-24616	35661	-21135	I
81	44687	204.9	3694.0	26.2	1287	366.4	141.4	-351.1	-209.7	-36781	130950	-36781	43259	-29428	35795	-29969	35901	-25349	38619	-29044	H
82	44702	200.2	3783.0	27.2	1302	378.3	141.4	-351.1	-209.7	-36781	130950	-36781	43259	-29428	35795	-29969	35901	-25349	38619	-29044	G
83	44707	200.7	3666.0	27.4	1307	366.6	138.5	-351.3	-212.8	-38708	0	-38708	45764	-30146	37727	-31481	37504	-27642	40628	-30478	F
84	44712	200.4	3780.0	27.6	1312	378.0	137.8	-362.2	-223.9	-39182	0	-39182	46008	-30321	37937	-31655	37831	-27954	41163	-30828	E
85	44762	199.2	3912.0	30.1	1374	391.2	137.4	-374.8	-237.4	-46153	0	-46153	49481	-32624	40604	-33672	40405	-29845	44361	-32945	D
86	44852	201.7	4019.0	34.4	1452	401.9	139.2	-385.0	-245.9	-46732	0	-46732	56009	-38517	45158	-40305	44647	-33028	50066	-36647	C
87	44922	207.0	3968.0	37.5	1522	396.8	142.8	-396.2	-237.4	-48613	0	-48613	60182	-39228	48437	-39334	47731	-35226	54330	-39654	B
88	44927	208.5	4086.0	37.8	1527	408.6	143.4	-396.2	-237.4	-48613	0	-48613	60182	-39228	48437	-39334	47731	-35226	54330	-39654	A
89	44942	207.6	4104.0	38.8	1547	410.4	143.4	-396.2	-237.4	-48613	0	-48613	60182	-39228	48437	-39334	47731	-35226	54330	-39654	
90	44952	207.9	4003.0	38.9	1552	400.3	143.4	-396.2	-237.4	-48613	0	-48613	60182	-39228	48437	-39334	47731	-35226	54330	-39654	
91	44982	201.7	4003.0	38.9	1552	400.3	143.4	-396.2	-237.4	-48613	0	-48613	60182	-39228	48437	-39334	47731	-35226	54330	-39654	
92	44982	205.3	4137.0	40.1	1592	413.7	141.7	-396.4	-254.7	-49488	0	-49488	64277	-41657	51001	-41172	50162	-37083	57826	-40135	
93	45007	198.8	4121.0	40.6	1607	412.1	137.7	-394.8	-257.1	-50068	0	-50068	65220	-42190	51220	-41361	50337	-37161	58156	-41130	
94	45032	205.2	4139.0	41.5	1632	413.9	141.6	-396.6	-255.0	-49488	0	-49488	64277	-41657	51001	-41172	50162	-37083	57826	-40135	
95	45052	199.2	4225.0	42.3	1652	422.5	137.4	-404.8	-257.4	-50068	0	-50068	65220	-42190	51220	-41361	50337	-37161	58156	-41130	
96	45062	199.2	4212.0	42.6	1662	421.2	137.4	-404.8	-257.4	-50068	0	-50068	65220	-42190	51220	-41361	50337	-37161	58156	-41130	
97	45067	201.0	4222.0	42.8	1667	422.2	138.7	-404.5	-265.6	-50068	0	-50068	65220	-42190	51220	-41361	50337	-37161	58156	-41130	
98	45122	206.6	4232.0	45.0	1722	423.2	142.7	-405.5	-262.8	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
99	45197	198.1	4274.0	48.2	1797	427.4	136.7	-405.5	-272.8	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
100	45227	203.6	4299.0	49.4	1827	429.9	140.5	-411.9	-271.4	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
101	45242	204.5	4184.0	50.1	1842	418.4	141.1	-401.8	-269.7	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
102	45252	205.4	4323.0	50.5	1852	432.3	141.7	-414.2	-275.5	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
103	45277	199.9	4240.0	51.7	1877	424.0	137.3	-406.2	-268.3	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
104	45302	199.0	4341.0	52.6	1902	434.1	137.3	-406.2	-268.3	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
105	45327	206.6	4307.0	53.4	1927	430.7	142.5	-412.7	-279.1	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
106	45347	201.5	4211.0	53.9	1947	421.1	139.0	-403.5	-264.4	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
107	45352	205.4	4323.0	54.1	1952	432.3	141.7	-414.2	-275.5	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
108	45367	206.0	4220.0	54.9	1987	422.0	143.1	-414.3	-276.0	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
109	45397	212.3	4187.0	54.9	1987	418.7	146.5	-399.3	-262.2	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
110	45402	213.9	4277.0	55.0	2002	427.7	146.5	-399.3	-262.2	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
111	45417	216.7	4159.0	55.3	2017	415.9	145.5	-398.5	-249.0	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
112	45472	213.0	3324.0	55.3	2072	332.4	147.0	-318.5	-171.5	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
113	45502	210.3	3313.0	55.2	2102	331.3	145.1	-321.6	-165.6	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
114	45507	200.2	335.0	54.7	2107	335.0	138.1	-360.0	98.1	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
115	45512	198.1	377.0	54.7	2107	377.0	138.1	-360.0	98.1	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
116	45517	194.1	276.0	54.3	2112	276.0	133.3	-361.1	99.2	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
117	45532	178.0	272.0	54.3	2112	272.0	133.3	-361.1	99.2	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
118	45537	154.8	279.0	54.3	2132	279.0	123.5	-26.4	107.5	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
119	45542	120.5	272.0	54.3	2140	272.0	106.8	-26.1	90.4	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
120	45547	89.5	282.0	54.3	2140	282.0	83.1	-26.1	97.1	-52628	0	-52628	71840	-46374	56690	-45159	55443	-40894	67102	-46214	
121	45552	63																			



test 6

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	
125	45662	0.1	-88.0	54.4		2262	-5.8	0.4	6.4	8.5	0.1			0	226530	122120	-36819	0	-27458	71895	-45805	55114	-43778	53695	-39710	65674	-45273
126	45667	0.6	22.0	54.3		2267	2.2	0.4	-2.1	-1.7	0.8			0	-28629	122090	-36817	0	-27457	71896	-45803	55115	-43778	53694	-39711	65674	-45273
127	45672	0.7	-86.0	54.3		2272	-8.6	0.5	8.2	8.7	1.0			0	-28525	122070	-36816	0	-27453	71895	-45804	55114	-43777	53695	-39711	65673	-45273
128	46177	18.4	69.0	54.3		2777	-6.9	12.7	6.6	26.3	26.3			0	-28291	118140	0	0	-27006	71964	-45770	55202	-43749	53805	-39673	65962	-45241
129	46182	30.6	-74.0	54.2		2782	-7.4	21.1	6.1	28.2	43.7			0	-28278	118130	0	0	-26994	72093	-45747	55289	-43733	53911	-39654	66060	-45229
130	46187	43.0	-74.0	54.2		2787	-7.4	29.7	7.1	36.8	61.4			0	-28266	118110	0	0	-26962	72181	-45727	55367	-43719	54002	-39624	66137	-45205
131	46192	55.4	-74.0	54.2		2792	-7.2	38.2	6.9	45.1	79.1			0	-28254	118100	0	0	-26951	72261	-45708	55443	-43703	54095	-39603	66213	-45191
132	46197	66.8	-66.0	54.2		2797	-6.6	46.1	6.3	52.4	95.4			0	-28243	118090	0	0	-26948	72345	-45689	55519	-43691	54180	-39584	66296	-45177
133	46202	77.3	-82.0	54.2		2802	-8.2	53.3	7.9	61.2	110.4			0	-28232	118080	0	0	-26947	72427	-45673	55592	-43684	54264	-39566	66359	-45163
134	46207	87.8	-74.0	54.2		2807	-7.4	60.6	7.1	67.7	125.4			0	-28221	118070	0	0	-26943	72501	-45659	55658	-43678	54342	-39548	66435	-45148
135	46212	97.8	-61.0	54.2		2812	-6.1	67.5	5.8	73.3	139.7			0	-28209	118060	0	0	-26937	72579	-45642	55728	-43665	54428	-39530	66500	-45137
136	46217	108.1	-63.0	54.2		2817	-6.3	74.6	6.0	80.6	154.4			0	-28198	118040	0	0	-26934	72654	-45629	55795	-43654	54505	-39515	66574	-45124
137	46222	117.6	-74.0	54.2		2822	-7.4	81.3	7.1	88.4	168.3			0	-28188	118030	0	0	-26934	72726	-45614	55859	-43643	54582	-39500	66642	-45111
138	46227	127.6	-69.0	54.2		2827	-6.9	88.0	6.6	94.7	182.3			0	-28178	118020	0	0	-26933	72798	-45601	55925	-43633	54658	-39485	66711	-45099
139	46232	136.5	-57.0	54.2		2832	-5.7	94.2	5.5	99.6	195.0			0	-28168	118010	0	0	-26932	72868	-45587	55992	-43624	54732	-39471	66779	-45088
140	46237	145.0	-65.0	54.1		2837	-6.5	100.0	6.4	106.3	207.1			0	-28157	118000	0	0	-26932	72932	-45576	56055	-43614	54809	-39456	66840	-45077
141	46242	154.4	-67.0	54.1		2842	-6.7	106.5	6.4	113.0	220.5			0	-28147	117990	0	0	-26932	73003	-45562	56117	-43604	54893	-39443	66900	-45066
142	46247	162.0	-78.0	54.1		2847	-7.6	111.8	7.3	119.1	231.4			0	-28137	117980	0	0	-26932	73065	-45550	56174	-43595	54945	-39431	66965	-45056
143	46252	171.4	-70.0	54.1		2852	-7.1	123.8	6.8	125.0	244.8			0	-28126	117970	0	0	-26932	73130	-45539	56237	-43587	55017	-39417	67029	-45045
144	46257	179.5	-71.0	54.1		2857	-7.1	128.8	6.8	130.7	256.4			0	-28116	117960	0	0	-26932	73192	-45527	56291	-43578	55079	-39408	67094	-45036
145	46262	187.0	-70.0	54.1		2862	-7.0	129.0	6.7	135.7	267.1			0	-28105	117940	0	0	-26932	73257	-45515	56345	-43569	55152	-39391	67149	-45028
146	46267	194.5	-73.0	54.1		2867	-7.3	134.2	7.0	141.2	277.8			0	-28098	117930	0	0	-26932	73310	-45505	56399	-43560	55208	-39381	67198	-45021
147	46272	200.7	-73.0	54.1		2872	-7.3	138.5	7.0	145.5	286.7			0	-28088	117920	0	0	-26932	73366	-45497	56454	-43552	55263	-39371	67247	-45008
148	46277	206.3	-72.5	54.2		2877	-7.3	138.5	7.0	145.5	286.7			0	-28079	117910	0	0	-26932	73420	-45489	56509	-43544	55319	-39364	67297	-45001
149	46282	210.0	-85.0	54.2		2882	-8.5	142.3	-21.6	150.8	294.7			0	-28069	117900	0	0	-26932	73475	-45481	56564	-43536	55374	-39357	67343	-45000
150	46287	213.7	-85.0	54.2		2887	-8.5	144.9	-21.6	150.8	294.7			0	-28060	117890	0	0	-26932	73529	-45473	56619	-43528	55429	-39350	67390	-45000
151	46292	216.6	-123.0	54.8		2892	-11.2	145.3	-107.6	154.4	300.8			0	-28052	117880	0	0	-26932	73583	-45465	56674	-43520	55484	-39343	67437	-45000
152	46297	219.9	-143.0	55.0		2897	-12.3	145.3	-107.6	154.4	300.8			0	-28043	117870	0	0	-26932	73637	-45457	56729	-43512	55539	-39336	67484	-45000
153	46302	213.1	-183.0	55.2		2902	-14.3	146.2	-143.0	157.9	302.7			0	-28034	117860	0	0	-26932	73691	-45449	56784	-43504	55594	-39329	67531	-45000
154	46307	216.3	-203.0	55.4		2907	-14.3	146.2	-143.0	157.9	302.7			0	-28025	117850	0	0	-26932	73745	-45441	56839	-43496	55649	-39322	67582	-45000
155	46312	219.9	-203.0	55.4		2912	-14.3	146.2	-143.0	157.9	302.7			0	-28016	117840	0	0	-26932	73799	-45433	56894	-43488	55704	-39315	67633	-45000
156	46317	213.1	-183.0	55.2		2917	-14.3	146.2	-143.0	157.9	302.7			0	-28007	117830	0	0	-26932	73853	-45425	56949	-43480	55759	-39308	67684	-45000
157	46322	216.3	-203.0	55.4		2922	-14.3	146.2	-143.0	157.9	302.7			0	-28000	117820	0	0	-26932	73907	-45417	57004	-43472	55814	-39301	67735	-45000
158	46327	219.9	-203.0	55.4		2927	-14.3	146.2	-143.0	157.9	302.7			0	-27991	117810	0	0	-26932	73961	-45409	57059	-43464	55869	-39294	67786	-45000
159	46332	213.1	-183.0	55.2		2932	-14.3	146.2	-143.0	157.9	302.7			0	-27982	117800	0	0	-26932	74015	-45401	57114	-43456	55924	-39287	67837	-45000
160	46337	216.3	-203.0	55.4		2937	-14.3	146.2	-143.0	157.9	302.7			0	-27973	117790	0	0	-26932	74069	-45393	57169	-43448	55979	-39280	67888	-45000
161	46342	219.9	-203.0	55.4		2942	-14.3	146.2	-143.0	157.9	302.7			0	-27964	117780	0	0	-26932	74123	-45385	57224	-43440	56034	-39273	67939	-45000
162	46347	213.1	-183.0	55.2		2947	-14.3	146.2	-143.0	157.9	302.7			0	-27955	117770	0	0	-26932	74177	-45377	57279	-43432	56089	-39266	67990	-45000
163	46352	216.3	-203.0	55.4		2952	-14.3	146.2	-143.0	157.9	302.7			0	-27946	117760	0	0	-26932	74231	-45369	57334	-43424	56144	-39259	68041	-45000
164	46357	219.9	-203.0	55.4		2957	-14.3	146.2	-143.0	157.9	302.7			0	-27937	117750	0	0	-26932	74285	-45361	57389	-43416	56199	-39252	68092	-45000
165	46362	213.1	-183.0	55.2		2962	-14.3	146.2	-143.0	157.9	302.7			0	-27928	117740	0	0	-26932	74339	-45353	57444	-43408	56254	-39245	68143	-45000
166	46367	216.3	-203.0	55.4		2967	-14.3	146.2	-143.0	157.9	302.7			0	-27919	117730	0	0	-26932	74393	-45345	57499	-43400	56309	-39238	68194	-45000
167	46372	219.9	-203.0	55.4		2972	-14.3	146.2	-143.0	157.9	302.7			0	-27910	117720	0	0	-26932	74447	-45337	57554	-43392	56364	-39231	68245	-45000
168	46377	207.4	-381.0	67.9		3282	-38.3	139.3	-300.8	157.9	299.2			0	-28245	117650	0	0	-26932	75034	-47348	57563	-45482	56563	-41443	69837	-46872
169	46382	208.1	-386.0	72.7		3287	-38.3	139.3	-300.8	157.9	299.2			0	-28236	117640	0	0	-26932	75088	-47340	57618	-45474	56618	-41436	69888	-46865
170	46387	207.4	-381.0	71.6		3292	-38.3	139.3	-300.8	157.9	299.2			0	-28227	117630	0	0	-26932	75142	-47332	57673	-45466	56673	-41429	69939	-46858
171	46392	210.6	-381.0	57.1		3297	-38.3	140.2	-300.8	157.9	299.2			0	-28218	117620	0	0	-26932	75196	-47324	57728	-45458	56728	-41422	69990	-46851
172	46397	213.7	-381.0	57.1		3302	-38.3	140.2	-300.8	157.9	299.2			0	-28209	117610	0	0	-26932	75250	-47316	57783	-45450	56783	-41415	70041	-46844
173	46402	216.3	-381.0	57.1		3307	-38.3	140.2	-300.8	157.9	299.2			0	-28200	117600	0	0	-26932	75304	-47308	57838	-45442	56838	-41408		

12.43.47 Progver: 981205a			All strain gauges in microstrain																																							
A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z																	
1	Test	7 Pipe																									Gauge 1		Gauge 2		Gauge 3		Gauge 4		Gauge 5		Gauge 6		Gauge 7			
2	ISM.01	Date:	01-13-1997/Time:																								hoop		hoop		hoop		hoop		hoop		hoop		hoop			
3	measured	measured	measured																								long.		long.		long.		long.		long.		long.		long.		long.	
4	Time	Pressure (Force (KN) Disp. (mm))	Time	Force (MPa) Hoop (MPa)	ax.press	ax.force	Axial	hoop																																		
5	Time	(bar)	(mm)	(MPa)					hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop	hoop																
6	Time	(bar)	(mm)	(MPa)					9	10	8	8	9	8	10	10	8	10	8	10	8	9	9	9	8	8																
7	Time	(bar)	(mm)	(MPa)					9	10	8	8	9	8	10	10	8	10	8	10	8	9	9	9	8	8																
1																																										
2	45836	0.0	-17.0	0.0	-1.7	0.0	0.0	1.6	1.6	0.0	286	32	285	34	44	44	15	15	15	15	26	26	60	20	48	18																
3	45876	9.4	-18.0	0.0	-1.8	6.5	13.4	8.2	8.2	13.4	615	54	601	55	82	82	24	24	24	24	48	48	124	36	107	34																
4	45936	23.5	-15.0	0.0	-1.5	16.2	17.7	1.4	1.4	17.7	74	620	74	1129	57	140	35	218	35	218	46	46	204	56	171	52																
5	45951	36.7	-15.0	0.0	-1.5	25.3	26.8	2.4	2.4	26.8	115	1125	115	1682	44	183	44	263	44	263	92	92	265	71	220	64																
6	45966	47.1	-5.0	0.0	0.5	35.3	33.0	0.5	0.5	33.0	167	215	167	215	1682	13	207	50	322	103	302	79	250	71																		
7	45981	52.6	-5.0	0.0	0.5	36.3	35.8	-0.5	-0.5	35.8	1990	279	1990	279	2150	14	1957	50	322	103	302	79	250	71																		
8	45996	66.0	-5.0	0.0	-0.5	45.5	46.0	0.5	0.5	46.0	2689	378	2689	378	3135	-44	2893	-55	257	397	126	373	97	309	87																	
9	45978	66.0	-5.0	0.0	-0.5	45.5	46.0	0.5	0.5	46.0	2689	378	2689	378	3135	-44	2893	-55	257	397	126	373	97	309	87																	
10	45991	81.1	-3.0	0.0	1.5	52.4	51.8	1.5	1.5	51.8	3527	476	3527	476	4385	-82	4009	-156	288	69	450	142	425	109	351																	
11	45966	90.0	-13.0	0.0	-1.3	62.1	63.3	0.2	0.2	63.3	4148	540	4148	540	5318	-71	4935	-223	307	73	482	151	456	117	375																	
12	46001	97.8	-1.0	0.0	0.1	67.5	67.6	0.1	0.1	67.6	687	1094	687	1094	879	-39	10406	-209	375	59	532	165	502	128	409																	
13	46006	103.0	-14.0	0.0	1.1	71.1	72.4	1.1	1.1	72.4	9182	687	9182	687	1094	-5	13781	-72	412	112	697	214	661	167	508																	
14	46021	118.1	-12.0	0.0	0.8	81.5	82.6	0.8	0.8	82.6	18762	637	18762	637	18799	-163	16731	-83	413	155	763	234	721	183	519																	
15	46026	128.5	-12.0	0.0	0.8	88.7	89.8	1.1	1.1	89.8	18762	637	18762	637	18799	-163	16731	-83	413	155	763	234	721	183	519																	
16	46066	123.3	-12.0	0.0	-1.2	85.1	86.2	1.1	1.1	86.2	22315	512	22315	512	22216	-339	19695	-203	298	178	178	669	169	432	225																	
17	46186	117.8	-19.0	0.0	-0.9	81.3	83.1	1.8	1.8	83.1	22172	500	22172	500	19555	-350	19555	-203	298	178	178	669	169	432	225																	
18	46306	112.5	-7.0	0.0	0.7	77.6	78.3	0.7	0.7	78.3	22020	487	22020	487	21923	-361	19408	-214	271	184	677	208	638	161	402																	
19	46331	120.3	-13.0	0.0	-1.3	83.0	84.2	1.2	1.2	84.2	22169	502	22169	502	22111	-346	19596	-196	722	221	221	882	172	445	230																	
20	46356	128.7	-16.0	0.0	-1.6	88.8	90.3	1.5	1.5	90.3	22426	520	22426	520	22373	-330	19621	-182	343	194	787	234	724	183	445																	
21	46376	134.9	-6.0	0.0	0.6	93.1	93.7	0.6	0.6	93.7	23537	519	23537	519	23743	-398	20956	-191	348	214	800	244	756	191	502																	
22	46406	140.7	-16.0	0.0	-1.6	92.8	92.8	1.5	1.5	92.8	29839	578	29839	578	31745	-501	27588	-260	319	296	296	256	796	200	472																	
23	46411	149.0	-16.0	0.0	-1.6	107.8	108.4	1.5	1.5	108.4	31957	662	31957	662	34707	-607	30415	-239	336	336	885	269	839	211	488																	
24	46541	156.3	-6.0	0.0	0.6	107.8	114.0	0.5	0.5	114.0	37880	559	37880	559	41940	-866	37949	-322	388	937	283	890	229	474	396																	
25	46556	162.1	-11.0	0.0	-1.1	114.0	116.9	1.0	1.0	116.9	42974	433	42974	433	47262	-984	43173	-377	287	308	967	292	917	229	474																	
26	46576	174.3	-9.0	0.0	0.9	120.3	123.2	0.9	0.9	123.2	48213	303	48213	303	52635	-1091	49057	-447	287	471	990	298	944	233	465																	
27	46676	174.0	199.0	0.0	63.7	121.2	80.2	-61.0	80.2	251.0	66406	-886	66406	-886	72169	-2120	65210	-1249	467	57	1148	-234	1037	174	542																	
28	46686	175.7	637.0	0.0	101.5	122.3	114.2	-109.4	114.2	250.0	68347	-871	68347	-871	74147	-2306	66633	-1274	483	-129	1148	-287	1099	39	596																	
29	46691	177.3	1015.0	-0.1	114.2	120.7	109.4	-109.4	113	250.0	69400	-1091	69400	-1091	75249	-2545	67744	-1317	547	-291	1163	-406	1122	-18	614																	
30	46706	175.0	1386.0	-0.1	138.6	121.3	-132.8	-11.5	11.5	251.1	81752	-3072	81752	-3072	83857	-3928	73971	-1909	648	-129	1175	-488	1141	-61	638																	
31	46716	175.8	1386.0	-0.1	149.4	121.0	-149.4	-28.4	250.5	242.0	88953	-4598	88953	-4598	88660	-4883	78642	-2185	650	-892	1187	-869	1099	-274	865																	
32	46721	175.4	1559.0	-0.1	165.9	120.7	-165.9	-45.1	250.0	249.4	97520	-6533	97520	-6533	92961	-6324	79372	-2150	634	-1003	1174	-940	1028	-305	897																	
33	46726	175.0	1731.0	-0.1	181.0	120.5	-181.0	-60.5	249.4	248.4	100830	-7367	100830	-7367	95400	-6957	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
34	46736	174.6	1889.0	-0.1	208.1	118.1	-208.1	-97.8	248.4	248.4	103470	-7681	103470	-7681	98740	-7232	84194	-1907	815	-1236	1252	-917	1058	-283	977																	
35	46741	172.0	2081.0	-0.1	218.8	116.9	-218.8	-109.4	245.7	245.7	108770	-8019	108770	-8019	105670	-7614	90501	-416	870	-1235	1285	-891	1082	-268	995																	
36	46746	169.4	2367.0	-0.2	236.7	113.2	-236.7	-115.6	242.0	242.0	115100	-8587	115100	-8587	112440	-8201	90909	-437	1020	-1579	1286	-952	1077	-312	992																	
37	46756	164.0	2367.0	-0.2	228.7	113.2	-228.7	-115.6	234.5	234.5	141700	-8019	141700	-8019	135060	-7700	79723	-566	3551	-1579	1286	-952	1077	-312	992																	
38	46771	157.2	2413.0	-0.3	241.3	120.0	-241.3	-118.1	248.4	248.4	141700	-8019	141700	-8019	135060	-7700	79723	-566	3551	-1579	1286	-952	1077	-312	992																	
39	46786	162.4	2402.0	-0.3	240.2	116.6	-240.2	-109.4	248.4	248.4	151100	-8587	151100	-8587	144100	-8135	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
40	46791	169.0	2352.0	-0.3	235.2	119.1	-235.2	-115.6	248.4	248.4	161100	-9175	161100	-9175	153560	-8019	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
41	46796	176.4	2291.0	-0.3	229.1	121.7	-229.1	-114.0	247.8	247.8	171100	-9175	171100	-9175	153560	-8019	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
42	46801	172.4	2434.0	-0.3	243.4	119.4	-243.4	-126.2	247.8	247.8	181100	-9175	181100	-9175	153560	-8019	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
43	46821	173.0	2563.0	-0.4	256.3	120.0	-256.3	-114.5	247.8	247.8	191100	-9175	191100	-9175	153560	-8019	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
44	46826	173.9	2474.0	-0.4	247.4	120.2	-247.4	-140.8	247.8	247.8	201100	-9175	201100	-9175	153560	-8019	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
45	46866	174.2	2427.0	-0.4	242.7	120.2	-242.7	-140.8	247.8	247.8	211100	-9175	211100	-9175	153560	-8019	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
46	46891	172.6	2829.0	-0.4	282.9	119.1	-282.9	-150.5	247.8	247.8	221100	-9175	221100	-9175	153560	-8019	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
47	47001	167.3	2776.0	-0.3	277.6	115.4	-277.6	-150.5	247.8	247.8	231100	-9175	231100	-9175	153560	-8019	80885	-1897	751	-1228	1210	-941	1028	-300	943																	
48	47006	173.5	2718.0	-0.3	271.8	119.7	-271.8	-15																																		

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z
63	47086	174.5	2758.0	1.4		1250	275.8	120.4	-254.3	-143.9	249.2			0	-532.1	-484.0	6240.1	232	1737.9	-14785	1237	-14855	1033	-810	7647	-413
64	47106	174.9	2651.0	1.5		1270	265.1	120.7	-254.0	-133.3	249.8			0	-4693	-4893	6195.1	-289	17626	-14724	1247	-14874	1039	-610	7647	-413
65	47141	172.4	2803.0	1.6		1305	280.3	119.0	-268.6	-149.6	246.2			0	-5272	-5084	61380	-377	17746	-14860	1246	-15133	1047	-820	8288	-359
66	47151	167.0	2864.0	1.8		1315	286.4	115.2	-274.4	-152.2	238.5			0	-5275	-5054	61278	-391	17795	-14905	1239	-14905	1025	-850	10522	-411
67	47171	173.5	2893.0	2.0		1335	289.3	119.7	-277.2	-157.5	247.8			0	-5244	-5054	62019	-390	18409	-15231	13435	-15794	1125	-851	14698	-397
68	47186	171.4	2786.0	3.7		1350	278.6	122.4	-266.9	-144.5	253.4			0	-5327	-5054	60881	-520	19007	-15537	18564	-17100	1213	-835	14698	-397
69	47201	177.8	2884.0	4.2		1365	288.4	118.5	-277.3	-158.7	245.4			0	-5390	-5060	60613	-513	19307	-15771	19033	-17367	1277	-1770	15836	-455
70	47206	164.5	2947.0	4.6		1370	294.7	113.5	-282.4	-168.9	235.0			0	-5404	-5067	60595	-523	19460	-15983	19033	-17367	1277	-1770	15836	-455
71	47211	170.4	2957.0	4.7		1375	295.7	117.6	-263.3	-165.7	243.4			0	-5411	-5067	60534	-525	19534	-16003	19079	-17419	1422	-3784	16018	-540
72	47216	174.3	2828.0	4.9		1380	282.9	120.3	-271.1	-150.8	249.0			0	-5416	-5067	60551	-528	19658	-16033	19137	-17350	1422	-3784	16018	-540
73	47221	179.5	2760.0	5.0		1385	276	123.8	-264.4	-140.6	256.4			0	-5414	-5057	60627	-526	19734	-16015	19193	-17301	1943	-5128	16111	-509
74	47226	176.2	2919.0	5.3		1390	291.9	121.6	-279.7	-158.1	251.7			0	-5412	-5057	60611	-525	19809	-16164	19235	-17369	2893	-7479	16340	-528
75	47231	170.8	2919.0	5.6		1395	291.9	117.8	-278.7	-161.8	244.0			0	-5439	-5066	60491	-527	20046	-16326	19406	-17406	4366	-9894	16428	-699
76	47236	165.9	3025.0	5.9		1400	302.5	114.5	-289.8	-175.4	237.0			0	-5461	-5063	60467	-531	20159	-16464	19240	-17440	8820	-11785	16515	-1186
77	47241	169.7	2887.0	6.0		1405	288.7	116.4	-276.6	-160.2	241.0			0	-5470	-5065	60442	-533	20226	-16467	19269	-17392	8621	-12573	16562	-1475
78	47246	175.4	2796.0	6.3		1430	279.6	121.0	-267.9	-146.9	250.5			0	-5487	-5068	60330	-538	20400	-16528	19362	-17394	11926	-13433	16710	-2179
79	47281	171.5	2902.0	6.6		1445	290.2	118.3	-278.0	-159.7	245.0			0	-5482	-5068	60268	-540	20542	-16679	19406	-17434	13336	-13847	16818	-2903
80	47311	175.7	3007.0	8.2		1475	300.7	121.2	-288.1	-169.9	251.0			0	-5500	-5074	60153	-545	21517	-17346	19873	-17649	15942	-14592	17495	-8526
81	47316	177.3	2887.0	8.3		1480	288.7	122.3	-276.6	-154.3	253.2			0	-5501	-5059	60136	-544	21670	-17408	19873	-17669	16100	-14666	17579	-10119
82	47326	171.4	3084.0	8.6		1490	306.4	116.3	-293.6	-175.3	244.8			0	-5509	-5063	60100	-544	21855	-17613	20067	-17826	16266	-14875	17684	-11095
83	47331	164.8	3067.0	8.9		1495	306.7	113.7	-293.9	-180.2	235.4			0	-5511	-5071	60084	-544	22036	-17807	20123	-17943	16367	-14893	17741	-11794
84	47341	159.9	3152.0	9.2		1505	315.2	109.6	-302.0	-192.4	227.0			0	-5515	-5075	60053	-545	22211	-17995	20159	-18050	16444	-15102	17801	-12368
85	47351	170.7	3027.0	9.4		1515	302.7	117.8	-280.0	-172.2	243.8			0	-5517	-5075	60018	-546	22410	-18050	20295	-18067	16578	-15109	17941	-12567
86	47356	176.7	2970.0	9.4		1520	297	121.9	-284.6	-162.6	252.4			0	-5518	-5069	60001	-546	22510	-18051	20389	-18065	16663	-15109	18029	-12567
87	47361	172.4	3120.0	9.6		1525	312	119.0	-288.9	-180.0	246.2			0	-5521	-5065	59987	-546	22712	-18234	20491	-18198	16768	-15293	18162	-12964
88	47381	175.2	3007.0	10.3		1545	300.7	120.9	-288.1	-167.2	250.2			0	-5538	-5072	59935	-547	23544	-18770	20666	-18445	17234	-15528	18769	-13814
89	47476	174.1	2894.0	10.4		1640	289.4	120.1	-277.3	-157.2	248.7			0	-5565	-5071	59869	-547	23623	-18782	20833	-18453	17290	-15528	18786	-13814
90	47701	176.0	3018.0	10.4		1665	301.8	121.4	-289.2	-167.7	251.4			0	-5575	-5070	59236	-549	23666	-18819	20872	-18489	17331	-15563	18842	-13713
91	47726	181.4	3001.0	10.7		1690	300.1	125.2	-287.5	-162.4	259.1			0	-5587	-5053	59202	-546	24213	-19171	21238	-18679	17627	-15760	19251	-14161
92	47746	187.2	2984.0	11.0		1810	298.4	129.2	-285.9	-156.7	267.4			0	-5587	-5053	59202	-546	24213	-19171	21238	-18679	17627	-15760	19251	-14161
93	47766	182.1	2922.0	11.1		1930	292.2	125.6	-280.0	-154.3	260.1			0	-5587	-5053	59202	-546	24213	-19171	21238	-18679	17627	-15760	19251	-14161
94	47896	177.0	2850.0	11.1		2060	285	122.1	-274.0	-151.9	252.8			0	-5599	-5144	58893	-545	25061	-19630	21695	-18932	18108	-16040	20020	-14827
95	47811	180.0	2978.0	11.1		2075	297.8	124.2	-285.3	-161.1	257.1			0	-5599	-5144	58893	-545	25061	-19630	21695	-18932	18108	-16040	20020	-14827
96	47916	182.6	3001.0	11.2		2080	300.1	125.1	-287.5	-161.4	261.1			0	-5599	-5136	58871	-545	25107	-19678	21709	-18957	18165	-16052	20036	-14886
97	47921	184.4	3006.0	11.2		2085	300.6	127.2	-288.0	-160.8	263.4			0	-5599	-5122	58869	-542	25213	-19848	21789	-19010	18190	-16117	20157	-14860
98	47926	185.5	2988.0	11.3		2090	298.8	126.0	-287.2	-159.3	265.0			0	-5599	-5122	58869	-542	25417	-19872	21875	-19074	18305	-16185	20340	-15126
99	47831	184.6	3017.0	11.3		2085	301.7	127.4	-289.1	-161.7	263.7			0	-5364	-5096	58859	-526	25556	-19973	21939	-19124	18371	-16238	20464	-15269
100	47935	0.0	2329.0	11.2		2100	232.9	0.0	-223.1	-223.1	0.0			0	-3746	0	0	-479	21338	-19862	20516	-19126	16981	-16205	16516	-15630

		12.40.36 Proqver. 961205a																								
		jp.																								
		8 Pipe																								
		01.14.1997/Ime.																								
		SM-01 Date:																								
A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	
1	Test	All strain gauges in microstrain																								
2	SM-01	Force (MPa) Axial																								
3	Date:	hoop long hoop long hoop long hoop long hoop long hoop long hoop long hoop long hoop long hoop long hoop long hoop long hoop long																								
4	measured measured measured measured measured	ax-press ax-force Axial hoop																								
5	measured measured measured measured measured	ax-press ax-force Axial hoop																								
6	Time	Pressure (Force (kN) Disp. (mm)																								
7	(bar)	kN mm																								
8																										
9																										
10																										
11	45653																									
12	45678																									
13	45758																									
14	45763																									
15	45768																									
16	45773																									
17	45778																									
18	45788																									
19	45793																									
20	45798																									
21	45803																									
22	45808																									
23	45818																									
24	45823																									
25	45828																									
26	45833																									
27	45838																									
28	45843																									
29	45848																									
30	45853																									
31	45858																									
32	45863																									
33	45868																									
34	45873																									
35	45878																									
36	45883																									
37	45888																									
38	45893																									
39	45898																									
40	45903																									
41	45908																									
42	45913																									
43	45918																									
44	45923																									
45	45928																									
46	45933																									
47	45938																									
48	45943																									
49	45948																									
50	45953																									
51	45958																									
52	45963																									
53	45968																									
54	45973																									
55	45978																									
56	45983																									
57	45988																									
58	46003																									
59	46008																									
60	46013																									
61	46023																									
62	46028																									

test 8

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z
63	46038	208.5				385	0	143.9	0.0	143.9	297.8								495	815	1139	340	1201	278	241	798
64	46043	210.6				390	0	145.3	0.0	145.3	300.8								519	835	1146	342	1210	277	279	819
65	46053	213.0				400	0	147.0	0.0	147.0	304.2								614	898	1155	343	1220	276	417	879
66	46063	215.5				410	0	148.7	0.0	148.7	307.8								699	948	1161	343	1229	276	516	932
67	46073	217.9				420	0	150.3	0.0	150.3	311.2								693	1003	1168	342	1237	274	559	946
68	46088	220.1				435	0	151.9	0.0	151.9	314.4								1354	1102	1172	341	1243	271	656	992
69	46093	220.4				440	0	152.1	0.0	152.1	314.8								1692	1128	1170	339	1244	269	669	1003
70	46098	220.3				445	0	152.0	0.0	152.0	314.7								1984	1172	1169	338	1242	268	688	1017
71	46103	219.8				450	0	151.7	0.0	151.7	313.9								2201	1197	1160	334	1234	265	683	1033
72	46108	-0.5				455	0	-0.3	0.0	-0.3	-0.7								-4075	529	-98	51	-120	58	-4641	222
73	46110	0.5				457	0	0.3	0.0	0.3	0.7								-4078	530	98	53	-120	59	-4634	223



08:21:51 Property: 981205a

1 Test Date: 01-20-1997 Time: 10  
2 ISM-01  
3  
4  
5 measured Pressure (kN) measured Disp. (mm)  
6 Time (bar) kN mm  
7  
8  
9

All strain gauges in microstrain  
Gauge 1 long hoop hoop hoop  
Gauge 2 long hoop hoop hoop  
Gauge 3 long hoop hoop hoop  
Gauge 4 long hoop hoop hoop  
Gauge 5 long hoop hoop hoop  
Gauge 6 long hoop hoop hoop  
Gauge 7 long hoop hoop hoop  
Gauge 8 long hoop hoop hoop

Force (10\*Max\_press) Ax\_force (Maxial) Hoop (MPa)

ax-press: ax-force Axial hoop

Table with columns labeled A through RB and rows 1 through 67. Each cell contains numerical data representing test results for various gauges and force measurements.

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB
65	35729	234.4	1715.0	-0.5	175.5	990	171.5	161.7	-164.3	-2.6	334.8		1896	31699	58278	19402	6364	6563	2239	28462	675	1642	-3.4	1714	-146	1535	-1880	18487
66	35699	228.7	1743.0	-0.4	167.3	1000	172.3	164.7	-165.1	0.4	340.9		1012	31550	58271	27547	10966	16240	2994	26962	-757	1862	-4.3	1802	-460	1633	-2528	19997
67	35699	248.8	1742.0	0.0	155.5	1130	172.3	164.7	-165.1	-0.6	346.8		1012	31550	58271	27547	10966	16240	2994	26962	-757	1862	-4.3	1802	-460	1633	-2528	19997
68	35699	248.8	1742.0	0.0	155.5	1130	172.3	164.7	-165.1	0.4	346.8		1012	31550	58271	27547	10966	16240	2994	26962	-757	1862	-4.3	1802	-460	1633	-2528	19997
69	35699	248.8	1742.0	0.0	155.5	1130	172.3	164.7	-165.1	-0.1	352.6		1012	31550	58271	27547	10966	16240	2994	26962	-757	1862	-4.3	1802	-460	1633	-2528	19997
70	35699	248.8	1742.0	0.0	155.5	1130	172.3	164.7	-165.1	0.4	346.8		1012	31550	58271	27547	10966	16240	2994	26962	-757	1862	-4.3	1802	-460	1633	-2528	19997
71	36394	246.9	1778.0	0.8	154.5	177.9	170.4	-170.5	-1.0	2.4	359.2		-1234	41532	7225	37440	8985	34594	329	43562	-6872	27033	-4534	26549	-3940	23148	-10768	33872
72	36394	251.5	1786.0	1.7	164.0	164.0	178.6	-171.1	-0.1	2.4	359.2		-1234	41532	7225	37440	8985	34594	329	43562	-6872	27033	-4534	26549	-3940	23148	-10768	33872
73	36394	250.3	1864.0	1.8	164.5	186.4	172.7	-178.6	-0.8	-5.9	357.5		-1390	41780	7194	37894	8446	34718	181	43680	-7025	27247	-4737	26418	-4109	23414	-10850	33974
74	36394	250.3	1864.0	1.8	164.5	186.4	172.7	-178.6	-0.8	4.8	361.5		-1378	43220	7054	38314	8501	35742	186	44489	-7537	28361	-5093	26386	-4673	24645	-11014	34756
75	36429	254.5	1783.0	0.2	173.3	169.4	175.9	-178.6	-2.7	364.2		-1393	43431	7114	39546	8476	35913	124	44618	-7641	28529	-5181	26545	-4778	24787	-11098	34834	
76	36429	255.0	1864.0	2.3	174.5	163.9	179.1	-178.2	-2.9	370.8		-1547	43735	7098	42484	8520	38337	53	46476	-8592	30563	-5863	28365	-5615	26169	-11598	34936	
77	36494	260.2	1839.0	3.0	175.5	192.5	183.4	-179.8	-1.8	378.6		-1611	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
78	36494	265.8	1875.0	3.3	176.0	185.4	184.5	-180.1	-1.6	379.6		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
79	36594	267.4	1984.0	4.4	182.5	198.4	184.5	-183.0	-1.6	381.9		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
80	36594	253.4	1978.0	5.1	186.5	197.8	184.5	-183.0	-1.6	381.9		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
81	36804	273.2	1910.0	5.0	187.5	198.6	185.4	-186.8	-1.7	401.7		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
82	36814	273.2	1986.0	5.3	193.0	198.6	185.4	-186.8	-1.7	401.7		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
83	36869	278.2	2068.0	6.6	196.6	206.8	189.9	-185.8	-1.8	411.1		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
84	36869	278.2	2068.0	6.6	196.6	206.8	189.9	-185.8	-1.8	411.1		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
85	36749	285.0	1972.0	7.4	201.0	201.0	193.0	-192.8	-1.9	418.9		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
86	36749	285.0	1972.0	7.4	201.0	201.0	193.0	-192.8	-1.9	418.9		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
87	36799	275.3	1939.0	7.6	208.0	202.8	195.5	-195.4	-2.0	421.9		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
88	36819	283.4	2028.0	7.6	212.0	207.3	196.6	-196.6	-2.0	421.9		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
89	36819	283.4	2028.0	7.6	212.0	207.3	196.6	-196.6	-2.0	421.9		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
90	36914	293.1	2058.0	8.4	217.5	205.6	202.4	-197.2	-2.1	431.3		-1611	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
91	36859	293.3	2147.0	10.3	222.0	214.7	202.4	-205.7	-2.3	431.3		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
92	37024	288.8	2088.0	11.1	235.5	212.7	203.8	-203.8	-2.0	427.6		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
93	37084	295.4	2156.0	11.8	239.5	215.6	208.8	-208.8	-2.0	427.6		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
94	37134	299.5	2156.0	11.8	245.5	219.7	208.9	-210.5	-2.1	432.3		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
95	37194	302.0	2197.0	13.0	246.0	219.7	208.9	-210.5	-2.1	432.3		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
96	37199	305.7	2288.0	14.4	253.0	228.8	210.4	-219.2	-2.2	437.6		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
97	37299	305.0	2288.0	14.4	253.0	228.8	210.4	-219.2	-2.2	437.6		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
98	37299	306.4	2201.0	15.0	256.5	221.1	207.5	-211.8	-2.1	440.1		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
99	37399	308.1	2211.0	15.0	266.5	221.1	207.5	-211.8	-2.1	440.1		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
100	37399	308.1	2211.0	15.0	266.5	221.1	207.5	-211.8	-2.1	440.1		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
101	37359	309.9	2251.0	15.5	259.0	225.1	211.6	-217.7	-3.9	438.3		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
102	37409	293.1	2265.0	17.1	267.0	226.5	202.2	-217.0	-4.8	444.2		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
103	37414	311.0	2248.0	17.1	272.0	228.1	213.6	-215.4	-4.8	444.2		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
104	37539	309.1	2381.0	19.3	280.0	238.1	213.6	-215.4	-4.8	444.2		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
105	37544	319.8	2271.0	18.4	280.5	227.1	219.5	-217.6	-7.1	454.5		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
106	37654	319.2	2371.0	21.5	293.5	221.7	219.5	-224.0	-5.1	453.2		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
107	37694	317.3	2338.0	21.6	293.0	233.8	219.9	-224.0	-5.1	453.2		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
108	37694	317.3	2213.0	22.4	295.5	221.3	219.9	-224.0	-5.1	453.2		-1700	47463	7093	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
109	37699	315.8	2432.0	22.5	296.0	243.2	217.8	-223.0	-15.3	453.8		-1596	43947	7098	43210	8448	39076	78	46997	-8864	31114	-6129	29059	-5938	26896	-11830	37004	
110	37709	317.7	2320.0	22.7	297.0	232.0	219.2	-222.9	-9.3	459.1		-1700	47463	7093	43210	8448												





66	34037	224.0	185.9	154.6	-178.1	-23.8	319.9	-393.7	8904	1640	1708	529	3586	847	1634	-523	1401	-23	1761
67	34047	223.0	184.2	153.9	-186.1	-36.2	318.5	-7835	16660	1633	1746	-619	3577	838	1627	-640	1408	-184	1784
68	34057	225.0	191.0	155.5	-181.3	-32.2	321.9	-7523	16271	1521	1815	-681	3729	868	1621	711	1408	-286	1843
69	34062	223.9	208.1	154.9	-189.4	-44.9	319.8	-7805	17568	1483	1883	-778	3880	916	1600	1000	1367	-354	1864
70	34072	224.5	214.0	154.9	-205.0	-50.1	320.7	-8415	19501	1458	1858	-851	3880	963	1589	720	1360	-457	1918
71	34077	223.5	220.1	154.2	-210.9	-56.7	319.2	-8890	19520	1335	1933	-936	4256	1002	1556	-1002	1338	-457	1918
72	34082	221.3	228.0	152.7	-218.7	-64.0	316.1	-9897	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
73	34092	221.3	228.0	152.7	-218.7	-64.0	316.1	-10265	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
74	34102	226.8	221.9	156.5	-212.8	-60.2	316.7	-10735	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
75	34112	221.7	225.0	153.8	-215.2	-60.2	316.7	-11076	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
76	34122	222.6	235.0	153.8	-225.8	-72.2	317.9	-11342	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
77	34132	222.9	239.4	154.3	-219.8	-66.4	318.4	-11342	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
78	34142	222.9	243.0	154.3	-223.1	-72.2	317.9	-11342	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
79	34152	222.5	245.4	153.5	-206.4	-52.9	317.8	-11328	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
80	34162	221.8	246.0	151.1	-200.2	-43.0	325.2	-11285	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
81	34172	221.7	246.0	151.1	-200.2	-43.0	325.2	-11581	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
82	34182	222.5	252.9	155.2	-216.4	-61.2	321.4	-11826	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
83	34192	225.0	258.0	155.2	-222.2	-70.3	314.5	-12270	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
84	34202	223.5	262.0	154.2	-222.3	-68.1	319.2	-12270	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
85	34212	223.5	262.0	154.2	-222.3	-68.1	319.2	-12424	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
86	34222	223.5	262.0	154.2	-222.3	-68.1	319.2	-12675	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
87	34232	221.9	268.0	153.1	-223.5	-70.4	316.9	-13640	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
88	34242	223.9	273.0	153.1	-223.5	-70.4	316.9	-13970	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
89	34252	221.9	278.0	152.7	-229.1	-86.5	316.1	-14247	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
90	34262	221.3	285.0	152.7	-232.5	-78.1	319.8	-14643	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
91	34272	221.3	285.0	152.7	-232.5	-78.1	319.8	-15044	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
92	34282	223.9	292.0	152.5	-223.3	-60.1	319.1	-15044	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
93	34292	223.9	292.0	152.5	-223.3	-60.1	319.1	-15498	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
94	34302	221.9	298.0	153.1	-229.8	-75.7	316.9	-15711	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
95	34312	221.9	298.0	153.1	-229.8	-75.7	316.9	-16016	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
96	34322	221.3	305.0	152.7	-231.5	-86.5	317.1	-16241	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
97	34332	221.3	305.0	152.7	-231.5	-86.5	317.1	-16416	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
98	34342	223.9	312.0	154.3	-241.1	-86.7	319.5	-16824	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
99	34352	223.9	312.0	154.3	-241.1	-86.7	319.5	-17189	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
100	34362	225.0	318.0	154.5	-234.3	-60.1	319.1	-17644	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
101	34372	225.0	318.0	154.5	-234.3	-60.1	319.1	-18019	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
102	34382	225.0	318.0	154.5	-234.3	-60.1	319.1	-18474	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
103	34392	226.9	326.0	156.6	-277.5	-120.9	324.1	-19254	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
104	34402	226.9	326.0	156.6	-277.5	-120.9	324.1	-19644	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
105	34412	227.9	332.0	156.6	-280.2	-134.4	323.1	-20099	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
106	34422	227.9	332.0	156.6	-280.2	-134.4	323.1	-20554	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
107	34432	225.9	335.0	155.9	-303.0	-144.9	327.2	-21009	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
108	34442	225.9	335.0	155.9	-303.0	-144.9	327.2	-21464	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
109	34452	228.0	342.0	156.5	-308.3	-151.8	323.9	-21919	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
110	34462	228.0	342.0	156.5	-308.3	-151.8	323.9	-22374	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
111	34472	227.3	344.0	156.2	-316.8	-160.4	324.7	-22829	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
112	34482	227.3	344.0	156.2	-316.8	-160.4	324.7	-23284	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
113	34492	227.3	344.0	156.2	-316.8	-160.4	324.7	-23739	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
114	34502	225.5	347.0	155.6	-286.4	-142.4	318.9	-24194	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
115	34512	225.5	347.0	155.6	-286.4	-142.4	318.9	-24649	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
116	34522	231.9	354.0	160.0	-292.6	-132.6	331.2	-25104	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
117	34532	231.9	354.0	160.0	-292.6	-132.6	331.2	-25559	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
118	34542	232.5	361.0	161.9	-302.9	-141.0	335.1	-26014	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
119	34552	232.5	361.0	161.9	-302.9	-141.0	335.1	-26469	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
120	34562	230.7	362.0	160.3	-313.8	-154.4	329.5	-26924	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
121	34572	230.7	362.0	160.3	-313.8	-154.4	329.5	-27379	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
122	34582	233.0	367.0	159.0	-326.9	-167.9	328.2	-27834	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
123	34592	233.0	367.0	159.0	-326.9	-167.9	328.2	-28289	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
124	34602	230.6	371.0	158.2	-332.9	-173.6	329.7	-28744	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
125	34612	232.5	375.0	160.2	-342.9	-182.7	331.5	-29199	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
126	34622	232.5	375.0	160.2	-342.9	-182.7	331.5	-29654	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
127	34632	230.8	376.0	157.6	-331.8	-165.4	328.2	-30109	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
128	34642	230.8	376.0	157.6	-331.8	-165.4	328.2	-30564	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
129	34652	234.9	382.0	161.8	-343.8	-177.7	331.5	-31019	19551	71	1955	-1038	5367	1015	1552	-906	1304	-478	1943
130	34662	234.9	382.0	161.8	-343.8	-177.7	331.5	-31474	19551										

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	
1	measured	measured	measured	measured	All strain gauges in microstrain																								
2	Time	Pressure (Force)	(kN)	Disp. (mm)	Gauge 1																								
3		(bar)	(kN)	(mm)	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.	hoop	long.
4					Gauge 2																								
5					Gauge 3																								
6					Gauge 4																								
7					Gauge 5																								
8					Gauge 6																								
9					Gauge 7																								
10					Gauge 8																								
11					hoop																								
12					ax-press																								
13					ax-force																								
14					Axial																								
15					hoop																								
16					Time /scan Force (10 <sup>4</sup> Max_press ( Ax-force (Max)axial (MPa Hoop (MPa)																								
17					ax-press																								
18					ax-force																								
19					Axial																								
20					hoop																								
21					ax-press																								
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