

## TECHNICAL REPORT

## JOINT INDUSTRY PROJECT

RELIABILITY OF CORRODED PIPES
LABORATORY BURST TESTS

REPORT No. 96-3393

REVISION No. 02

DET NORSKE VERITAS

# TECHNICAL REPORT Date of first issue: 7 May 1997 Approved by: Tommy Bjørnsen Organisational unit: Pipelines Project No.: 25010049 Organisational unit: Pipelines Veritasveien 1,

N-1322 HØVIK, Norway Tel: +47 67 57 99 00 Fax: +47 67 57 74 74 http://www.dnv.no Org, No: NO 945 748 931 MVA

Summary:

Client:

Head of Section

Joint Industry Project

This report is one of a serie of 4 reports in the JIP project "Reliability of Corroded Pipes", and describes the laboratory burst tests of pipes with simulated corrosion defects. This project is a continuation of the JIP project "Residual Strength of Dented and Corroded Pipes".

Client ref.:

See participation list

Twelve burst tests have been performed, of which 9 were with longitudinal corrosion defects and 3 with circumferential corrosion defects. The pipes were loaded with combined internal pressure and external loads, except for 2 tests with internal pressure only. The external loads considered were bending moment and axial compressive force.

The test specimen, test set-up execution of the tests and the main results are described in this report, while evaluation of the results are included in the DNV project report no. 96-3394 "Reliability of Corroded Pipes / Assessment of Capacity and Acceptance Criteria"

All tests were made from seamless pipe with 324 mm diameter and 10.3 mm wall thickness of X52 modified material. The defects were smooth corrosion made using spark erosion for the longitudinal corrosion and the circumferential corrosion was machined.

Report No.: 96-3393	Subject G	roup:	Inde	xing terms		
Report title: Reliability of Corrode Laboratory Burst Test	•		Corrosion Pipelines Laboratory tests Burst			
Work carried out by: O. H. Bjørnøy, G. Sig		Cramer		No distribution without permission from the Client or responsible organisational unit		
Work verified by: Leif Collberg	ess		bours, and	Limited distribution within Det Norske Veritas		
Date of this revision: Rev 16 Des. 1997 02	No.: No. 6:	umber of pages: 5		Unrestricted distribution		

 Report No. 96-3393, rev. 02	心學
	W WICE

### Table of Revisions

TECHNICAL REPORT

Rev. No.	Description	Date
01	Draft for comment	7 May 1997
02	Final	16 Des. 1997



#### TECHNICAL REPORT

Table	of Co	ontents	Page
1	SUM	IMARY	1
2	INTE	RODUCTION	2
2.1	Moti	vation	2
2.2	Back	ground	2
2.3	Proje	ect Reports	3
2.4	Parti	cipants and Their Representatives	3
3	GEN	ERAL DESCRIPTION OF TESTS	5
3.1	Over	rview of tests	5
3.2	Desc	cription of the test set-ups	5
3.3	Instr	umentation	9
3.4	Man	ufacture of the test specimens	9
4	DET	AILED DESCRIPTION OF THE TESTS	11
4.1	Gene	eral	11
4.2	Test	no. 1	12
4.3	Test	no. 2	15
4.4	Test	no. 3	20
4.5	Test	no. 4	25
4.6	Test	no. 5	30
4.7	Test	no. 6	35
4.8	Test	no. 7	39
4.9	Test	no. 8	43
4.10	Test	no. 9	46
4.11	Test	no. 10	50
4.12	Test	no. 11	54
4.13	Test	no. 12	58
5	SUM	MARY OF TESTS AND TEST RESULTS	62
5.1	Over	rview of test results	62
6	MAT	TERIAL PROPERTIES	64
Appen	dix B	Description of the test rig, corrosion defects, thickness measurements and instrumentation  Material certificates and material test results  Listing of test results	

Report No.	96-3393,	rev.	02
------------	----------	------	----



SUMMARY

#### 1 SUMMARY

This report is one of a serie of 4 reports in the JIP project "Reliability of Corroded Pipes", and describes the laboratory burst tests of pipes with simulated corrosion defects. This project is a continuation of the JIP project "Residual Strength of Dented and Corroded Pipes".

Twelve burst tests have been performed, of which 9 were with longitudinal corrosion defects and 3 with circumferential corrosion defects. The pipes were loaded with combined internal pressure and external loads, except for 2 tests with internal pressure only. The external loads considered were bending moment and axial compressive force.

The test specimen, test set-up execution of the tests and the main results are described in this report, while evaluation of the results are included in the DNV project report no. 96-3394 "Reliability of Corroded Pipes / Assessment of Capacity and Acceptance Criteria".

All tests were made from seamless pipe with 324 mm diameter and 10.3 mm wall thickness of X52 modified material. The defects were smooth corrosion made using spark erosion for the longitudinal corrosion and the circumferential corrosion was machined.



INTRODUCTION

#### 2 INTRODUCTION

#### 2.1 Motivation

A pipeline is a large financial assets for the pipeline operator and a safe operation of the pipeline is therefore of great concern. On the other hand, unnecessary repair and an over conservative operation of the pipeline may result in high costs and unexploded resource utilisation. As the pipelines are ageing and corrosion may develop, the economical consequences of reduced operation pressure, repairs, or replacements may become high. Available design equations for assessment of allowable operating pressures of degraded pipelines depending on the selected reliability level is therefore desirable.

When severe corrosion has been observed in a pipeline, the decision of necessary action to be carried out should be based on an overall assessment of the pipeline, where uncertainties associated with both the assessment of the degree of corrosion and the capacity evaluation should be considered. The cost of repair or replacement can be very high and should be avoided, or postponed in time, if this is possible within the safety requirements defined. Required actions should further also be initiated in order to maintain the integrity of the pipeline and to avoid an undesired risk exposure of the pipeline.

The objective of the work is to provide the participants with capacity formulas of corroded pipes. The work includes laboratory tests and a large number of finite element analyses of corroded pipes exposed to internal pressure, combined internal pressure and bending moment, and combined internal pressure and bending moment. Both longitudinal and circumferential corrosion are considered. The formulas will be calibrated using reliability methods. This will in a systematic manner include uncertainties in inspection results and variations in material properties, pressure and dimensions. The outcome of the project will be included in a manual for assessment of corroded pipes.

#### 2.2 Background

The present Joint Industry Project "Reliability of Corroded Pipes" is a continuation of the project "Residual Strength of Corroded and Dented Pipes". The former project which was started in 1993 and concluded at the end of 1995, and the present project stared shortly after.

The Phase I of the project was sponsored by Statoil, Phillips, Brasoil (Petrobras), Mineral Management Services (MMS), Norwegian Petroleum Directorate (NPD), The Research Council of Norway (NFR), and Det Norske Veritas (DNV).

The present project "Reliability of Corroded Pipes" is sponsored by Statoil, Amoco, Exxon, NPD and MMS.

The scope of work of the project has been modified in order to best utilise the funding. Especially has the work conducted by British Gas had an impact on our project as British Gas is undertaking a similar project. To avoid unnecessary overlapping of work the scope was changed, but some items were not overlapping. DNV have included combined load cases, circumferential corrosion, and a reliability calibration of the capacity and design equations that would be



#### Introduction

established. British Gas, on the other hand, had already performed many tests and finite element analyses for internal pressure only, including interaction of separate pits and grooves, but they would not included a reliability calibration of the equations. A co-operation with British Gas has been discussed and an advantage would be that the equations would be based on a larger database including effects studied only by British Gas and effects studied only by DNV. The equations would include calibrated safety factors. Common capacity and design equations from British Gas and DNV would most probable receive greater acceptance in the marked, and hence, be a recognised equations.

After completion of both the British Gas and the DNV project, where both projects have made project specific guideline of corroded pipes, a unified guideline could be made.

#### 2.3 Project Reports

The project concludes with 4 reports, given in the table below.

Table 2-1 Overview of the project reports

DNV report no.	Title / Subject
96-3392	Reliability of Corroded Pipes / Finite Element Analyses
96-3393	Reliability of Corroded Pipes / Laboratory Burst Tests (This document)
96-3394	Reliability of Corroded Pipes / Assessment of Capacity and Acceptance Criteria
97-3358	Reliability of Corroded Pipes / Project Guideline

#### 2.4 Participants and Their Representatives

The following organisations participated in the project;

Participant	Representative	Telephone / l	Fax
Minerals Management Service (MMS)	Wallace O. Adcox	telephone	(+1) 703 787 1354
		fax	(+1) 703 787 1010
Norwegian Petroleum Directorate (NPD)	Kjell A. Anfinsen	telephone	(+47) 51 87 62 26
		fax	(+47) 51 55 15 71
Den norske stats oljeselskap a.s.(Statoil)	Richard Verley	telephone	(+47) 73 58 41 85
• . • • • • •		fax	(+47) 73 96 72 86
Amoco Norway Oil Company (Amoco)	Ole Jørgen Narvestad	telephone	(+47) 51 50 20 18
		fax	(+47) 51 50 22 18
Exxon Production Research Company (EPR)	Robert Appleby	telephone	(+1) 713 965 7193
		fax	(+1) 713 966 6423
Petrobras /CENPES/DIPREX	Adilson C. Benjamin	telephone	(+55) 21 598 6263
	v	fax	(+55) 21 598 6793



#### INTRODUCTION

The SI units are used in the report. The conversion factors are between the SI units and the US units are;:

#### From US units to SI units

length:	1 in (inch)	<del></del>	25.40 mm
Mass	1 lb (pound)	=	0.4536 kg
Force	1 lbf (pound force)		4.448 N
	1 kip	=	4.448 kN
Stress (Pressure)	1 psi (lbf/in2)	=	0.006895 MPa (N/mm2)
	1 ksi (1000 psi)	==	6.895 MPa

#### From SI units to U. S units

length:	l mm	Andrew Harpin	0.03937 in
Mass	1 kg		2.205 lb (pound)
Force	1 N	*	0.2248 lbf (pound force)
	I kN		0.2248 kip
Stress (Pressure)	1 MPa	=	145.0 psi (lbf/in2)
	1 MPa		0.1450 ksi

1 ksi = 1000 psi10 bar = 1 MPa



#### 3 GENERAL DESCRIPTION OF TESTS

#### 3.1 Overview of tests

A total of 12 tests has been carried out within the project. An overview of the tests are given in Table 3-1.

Table 3-1 Overview of tests

Test no.	Nom Dia	Nom thick	mat.	defect depth	defect length	defect width		loading	alavial
	(mm)	(mm)		(d/t)			ļ <u>.</u>	s / Denum	g/axiai
1	324	10.3	X52	0.50	0.75 D	15 t	X		
2	324	10.3	X52	0.50	0.75 D	15 t	X	X	
3	324	10.3	X52	0.50	0.75 D	15 t	X	X	
4	324	10.3	X52	0.30	0.50 D	3 t	X	X	
5	324	10.3	X52	0.30	0.50 D	3 t	X		X
6	324	10.3	X52	0.30	0.50 D	3 t	X		X
7	324	10.3	X52	0.50	0.75 D	3 t	X		X
8	324	10.3	X52	0.50	0.75 D	3 t	X		
9	324	10.3	X52	0.70	0.75 D	3 t	X	and the second	X
10	324	10.3	X52	0.50	12 mm	circ.	X		X
11	324	10.3	X52	0.50	12 mm	circ.	X		X
12	324	10.3	X52	0.70	12 mm	circ.	X		X

The dimensions given in the table are nominal values. The actual values of diameter, wall thickness and corrosion defects were measured. The material curve was determined by coupon tests. All simulated longitudinal corrosion defects were smooth rectangular defects fabricated using spark erosion, while the circumferential corrosion defects were machined. Tests 1 through 9 were simulating longitudinal corrosion, while test 10 through 12 simulated girth weld corrosion. All defects were made at the outer surface in the parent material.

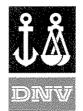
The test specimens were exposed to combined internal pressure and external forces until burst, except for 2 test specimens which were exposed to internal pressure only.

#### 3.2 Description of the test set-ups

The tests were exposed to different kind of loading which required different test set-ups;

- internal pressure only
- combined internal pressure and bending moment
- combined internal pressure and axial compressive force

The tests with internal pressure only requires virtually no special test set up, apart from the instrumentation and the water pump to increase the internal pressure until burst.



The tests with internal pressure and bending moment was performed in a 4-point-bending test rig. The test rig is shown in Figure 3-1 and Figure 3-2. A sketch of the test rig is also included in Appendix A. Rollers were used at the supports to in order to define and keep the distance between the supports constant. The distance between the rollers, which is the moment arm, varied from 1.27 to 1.43 meter for the three tests with bending moment. A servo controlled dynamic MTS 1000 kN actuator was used to apply the force. The specific test rig set-up made for this project had approximately 650 kNm moment capacity, and maximum 150 mm stroke.

The tests with combined internal pressure and axial compressive force was performed in a test frame as shown in Figure 3-3. A 10000 kN static jack was applied. The length of the test specimens were all 1000 mm, plus 2\*50 mm for the end-plates. The maximum stroke of the jack was slightly less than 100 mm.

The water pump used in the burst tests had a capacity of 1000 bar. All tests were performed at room temperature at approximately 20°C

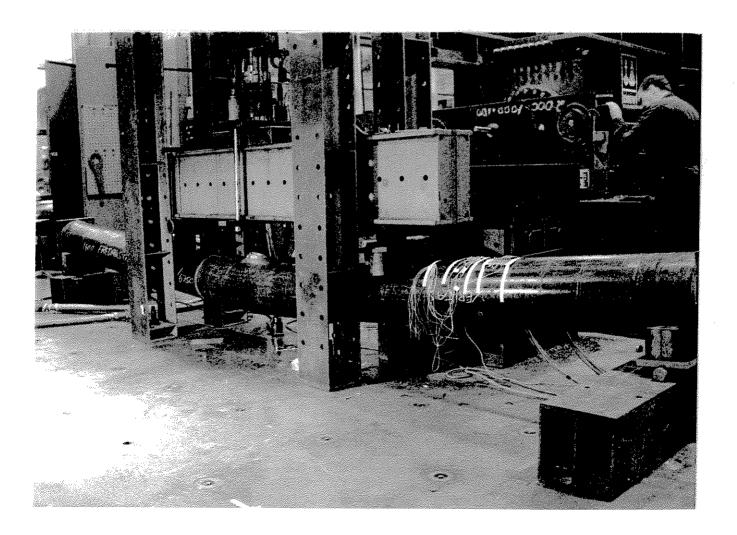


Figure 3-1 Picture of the test rig for 4-point bending test (after completion).



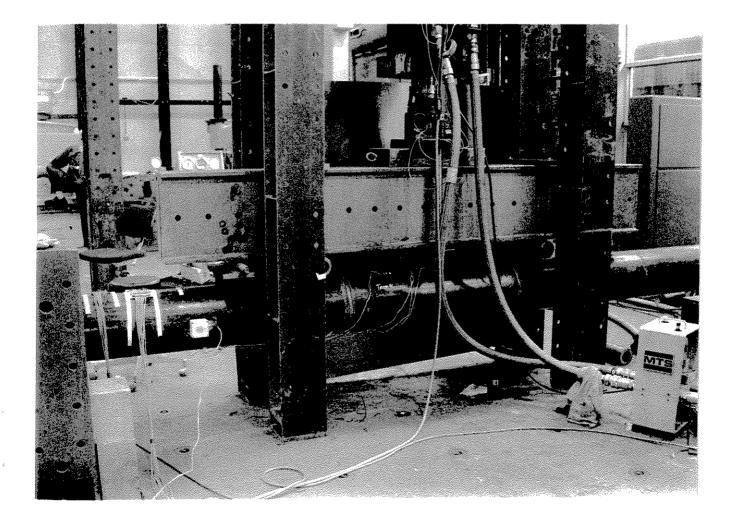


Figure 3-2 Picture of the test rig for 4-point bending test.





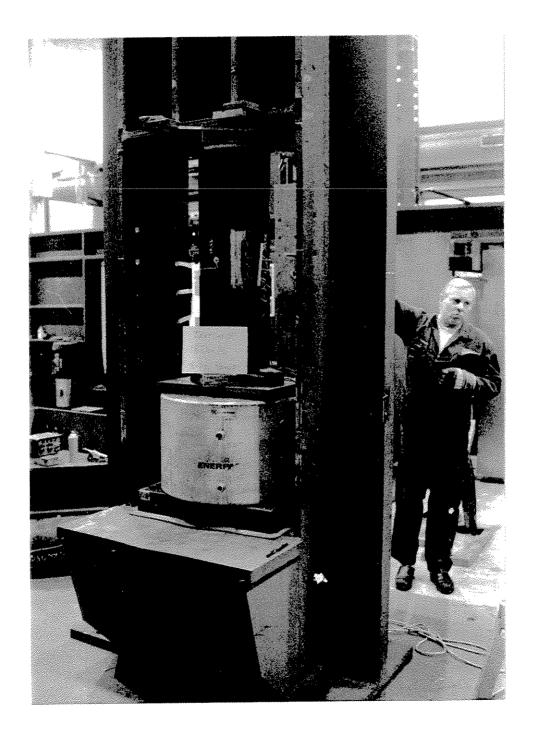


Figure 3-3 Picture of the test rig for axial compressive force



#### 3.3 Instrumentation

Each specimen was instrumented with strain gauges and pressure transducer in order to monitor the specimen during testing and for recording. The strain gauge instrumentation for each specimen are shown in Appendix A. Approximately 10 strain gauges were applied at each test. For the tests with combined loading the external loads were also monitored and recorded. In Figure 3-4 an example of the strain gauge instrumentation of a corrosion defect is shown.

For the specimens exposed to combined loads, some strain gauges were used for load and alignment control. All strain gauges were post yield cross gauges allowing for large strains from Tokyo Sokki Kenkyujo Co., LTD., type YFLA-2.

A 1000 bar pressure transducer was used, serie no. F02395. In order to minimise erroneous pressure fluctuations the pressure transducer was mounted directly to the end flange in a separate hole from the connection from the hose for the pump.

#### 3.4 Manufacture of the test specimens

The simulated corrosion defects were spark eroded at the outer surface. The defect similar to test 1 to 3 is shown in Figure 3-4. The defects had a smooth surface and all edges were made with a small radius. The surfaces were also grinded slightly to get a smoother surface for ease thickness measurements and application of strain gauges. At each end of the test specimen a 50mm thick end-plate was welded to the pipe. For the tests exposed to bending moment thicker extension pipes of approximately 2 meters were welded to each end of the test specimen, and the end-plate were welded to the end of these extension pipes. The inlet for internal pressure and mounting of the pressure transducer were in the end flanges.



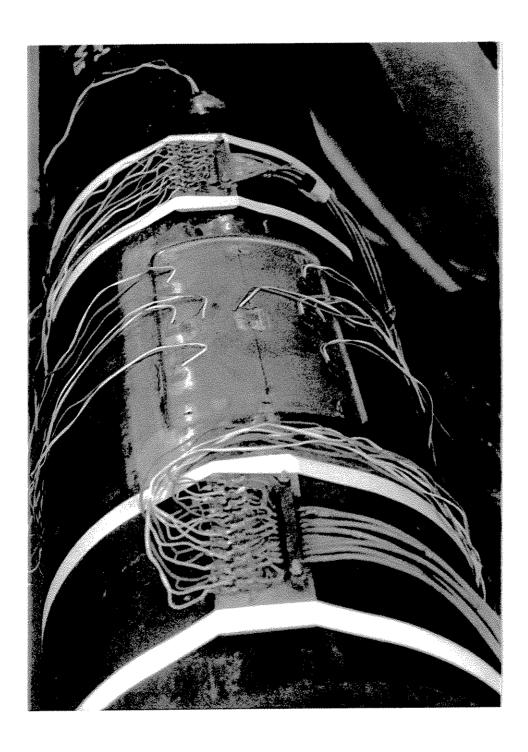


Figure 3-4 Picture of a corrosion defect with strain gauge instrumentation



#### DETAILED DESCRIPTION OF THE TESTS

#### 4.1 General

Twelve test were performed. The 9 first test specimens were made from the same pipe, while the last 3 test specimens were made from another pipe, which was almost identical to the first one. The nominal parameters are the same for all 12 tests, apart for the simulated corrosion defects. For each test specimen the actual dimensions were measured and are described for each test in this report.

The following was the same for all tests;

Pipe Diameter

324 mm (nominal)

Pipe wall Thickness

10.31 mm (nominal)

Pipe Grade

X52

Type of Longitudinal Seam

Seamless

Yield Strength (actual, eng.)

380 MPa

(Average of 8 test coupons)

Tensile Strength (actual, eng)

514 MPa

(Average of 8 test coupons)

Year of Manufacture

1996 / 1997

The pipe diameter was measured at several locations, it was found to be closer to 325 than the nominal diameter of 324 mm, and was almost identical at all measured locations. The pipe wall thickness, however, varied far more, from minimum 10.25 mm to maximum 11.10 mm. The largest variation was in the circumferential direction, but large variations were also observed along the length of the pipe.

Some variables have been calculated based on measurements and constants, as for instance the axial stress is calculated based on the applied (measured) force and the diameter and thickness. For calculation of the cross section parameters the an outer diameter of 324 mm is used, and for the wall thickness the "average" thickness of 10.6 mm is used. This results in the following values for the cross section;

Area pipe

 $= 10437 \text{ mm}^2$ 

 $(D_o^2 - D_i^2) * \pi/4$   $(D_i^2) * \pi/4$ 

• Area inner

 $= 72012 \text{ mm}^2$ 

• Moment of Inertia (I)

 $= 1.28*10^8 \text{mm}^4$ 

 $(D_0^4 - D_i^4) * \pi/64$ 

Section modulus W elastic

 $= 791854 \text{ mm}^3$ 

 $I/(D_c/2)$ 

 $D_{\circ}$ ; Outer Diameter = 324 mm

 $D_i$ ; Inner Diameter = 302.8 mm

In the following sub-sections each test is described. Sketches showing the test set-up, the corrosion defect, the instrumentation, the thickness measurements are included in Appendix A. Pictures of the test specimens after burst are included in the main section of the report. In Appendix B the material certificates are included, and in Appendix C listing of the recorded pressure, loads and strain gauges are given (Microsoft Excel spreadsheet)



#### 4.2 Test no. 1

#### Loading

Internal pressure only.

#### Corrosion defect parameters (nominal)

Corrosion defect depth	d	= 5.3  mm	(d/t = 0.5)
Corrosion defect length	L	= 245  mm	(L/D = 0.75)
Corrosion defect width	W	= 150  mm	(w = 15 t)
Length of test specimen	$L_{\text{specim}}$	$_{\rm en} = 1500 \; {\rm mm}$	n

#### Instrumentation

In the corroded area 9 cross strain gauges were applied, and one strain gauge was applied away from the corroded area for load control and hoop strain measurement. Internal pressure and time for each scan were also recorded.

#### Loading description

Internal pressure was applied until burst, and applied internal pressure versus time is shown in Figure 4-1.

#### Results

The test failed at 232 bar. The test specimen after burst is shown in Figure 4-2.

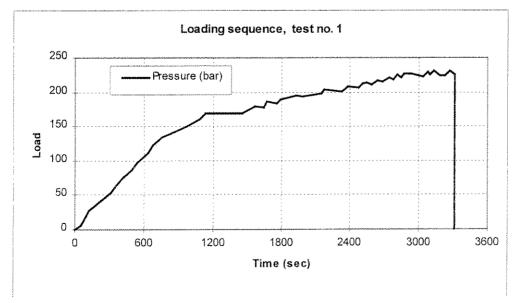


Figure 4-1 Applied pressure versus time for test no. 1



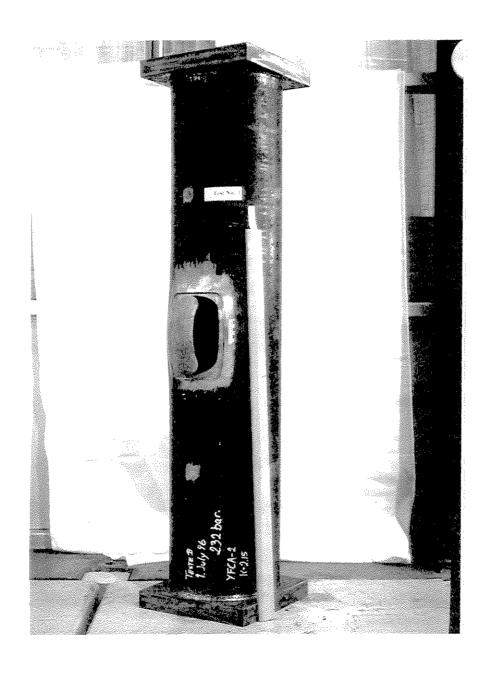


Figure 4-2 Picture of the test specimen no. 1 after the burst





Figure 4-3 Picture of the test specimen no. 1 after the burst



#### 4.3 Test no. 2

#### Loading

Loaded with combined internal pressure and bending moment.

#### Corrosion defect parameters (nominal)

#### Instrumentation

In the corroded area 9 cross strain gauges were applied, and two single filament gauges were applied away from the corroded area for load control of the bending moment. The time, the actuator load and displacement were also recorded.

#### Loading description

The specimen was exposed to combined internal pressure and 4-point-bending moment. The corrosion defect was located at the compressive side of the bending moment.

An internal pressure of 165 bar was applied during the first 15 minutes. The loading is illustrated in Figure 4-4 to Figure 4-6. The internal pressure was then kept at 165 bar and bending moment was applied to the test specimen. The actuator was in displacement control, and for this test set-up the applied displacement results in a forced curvature of the pipe. At approximately 220 kNm bending moment more and more displacement was required in order to further increase the bending moment, which effect indicate excessive yielding of the pipe cross section. Further, the displacement was kept constant and the internal pressure was increased, which resulted in a drop in the bending moment at the constant displacement. In order to maintain the bending moment additional displacement was applied, but the pipe had softened significantly due to the internal pressure and the pipe could not carry much increased bending moment.



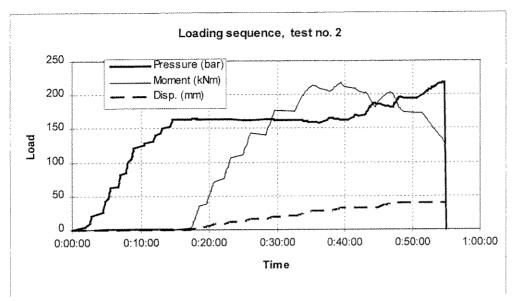


Figure 4-4 Loading sequence, test no. 2

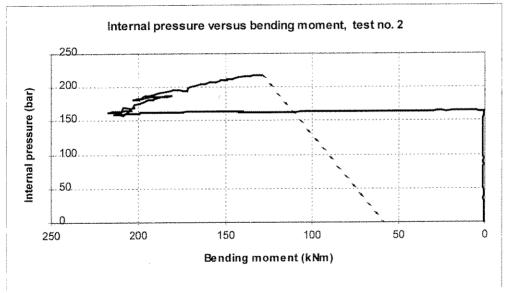


Figure 4-5 Internal pressure versus bending moment, test no. 2



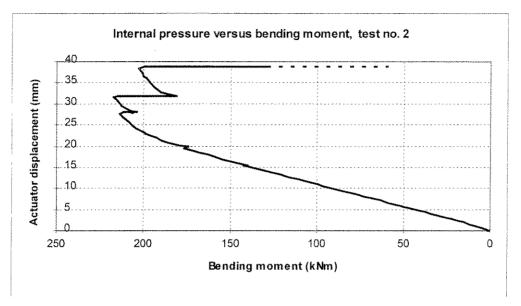


Figure 4-6 Actuator displacement versus bending moment, test no. 2

#### Results

Excessive yielding was observed in the pipe, and it was not possible to maintain the maximum bending moment of approximately 220 kNm when the internal pressure was further increased. When the internal pressure was increased from 165 bar to rupture at 218.5 bar, the bending moment decreased from 220 kNm to 130 kNm.

The bending moment resulted in a radius of approximately 15-20 meter, where the 15 meter was estimated based on measurements of the test specimen after testing and the 20 meter was based on the applied displacement during the test.



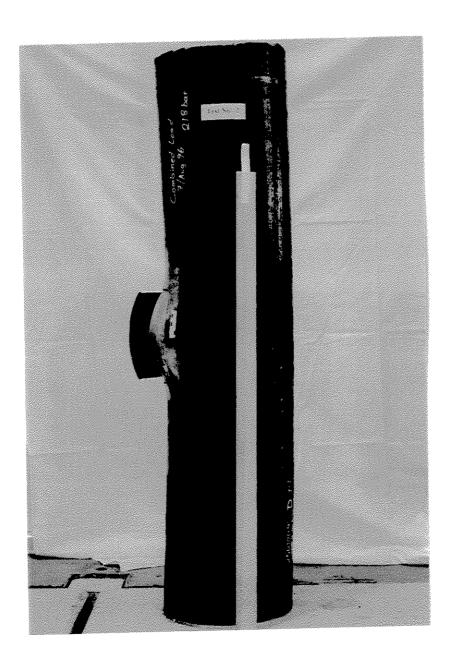


Figure 4-7 Picture of the test specimen no. 2 after the burst test





Figure 4-8 Picture of the test specimen no. 2 after the burst test



#### 4.4 Test no. 3

#### Loading

Loaded with combined internal pressure and bending moment (similar to test 2).

#### Corrosion defect parameters (nominal)

(Identical to specimen no 1 and 2)

Corrosion defect depth d = 5.3 mm (d/t = 0.5) Corrosion defect length L = 245 mm (L/D = 0.75) Corrosion defect width w = 150 mm (w = 15 t)

Length of test specimen Lspecimen = 1500 mm

#### Instrumentation

In the corroded area 9 cross strain gauges were applied, and two single filament gauges were applied away from the corroded area for load control of the bending moment. The time, rotation angle, the actuator load and displacement were also recorded.

#### Loading description

The specimen was exposed to combined internal pressure and 4-point-bending moment. The corrosion defect was located at the compressive side of the mending moment. In the previous test the MTS was in displacement control, but order to try to maintain the bending moment and hence allow the pipe to deflect the actuator was set in load (bending moment) control.

An internal pressure of 165 bar was applied during the first 12 minutes. The internal pressure was kept at 165 bar and bending moment was applied to the test specimen. Further, the bending moment was kept constant at 200 kNm, and the internal pressure was increased. The pipe was yielding extensively, which resulted in increased additional displacement in order to maintain the set bending moment of 200 kNm. An small increase in the bending moment up to 212.5 kNm was applied, and only marginal additional internal pressure was introduced before rupture.



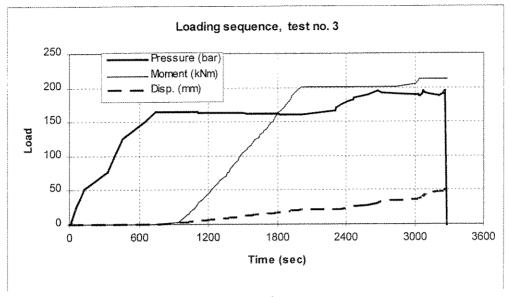


Figure 4-9 Loading sequence, test no.3

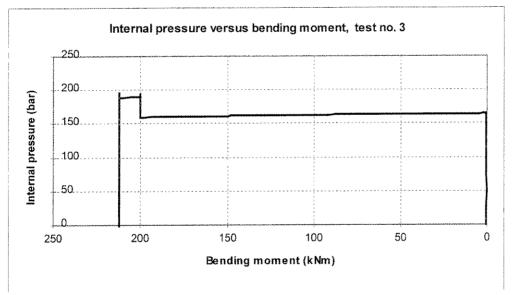


Figure 4-10 Internal pressure versus bending moment, test no. 3

#### Results

Excessive yielding was observed in the pipe before rupture in the corroded region. The test bursted at a bending moment of 212.5 kNm and an internal pressure of 195 bar.



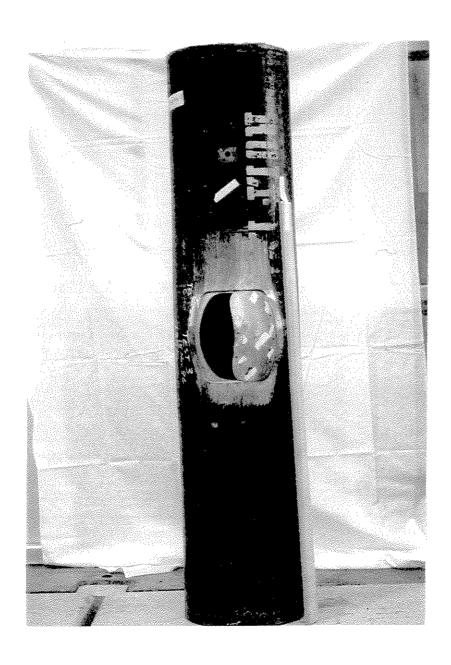


Figure 4-11 Picture of the test specimen no. 3 after the burst test



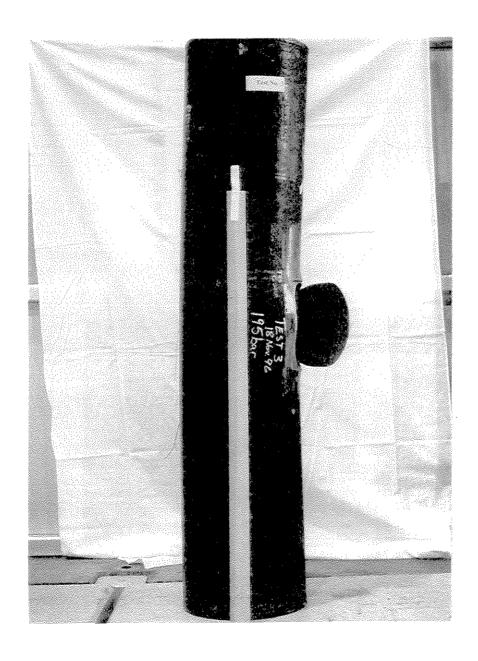


Figure 4-12 Picture of the test specimen no. 3 after the burst test





Figure 4-13 Picture of the test specimen no. 3 after the burst test



#### 4.5 Test no. 4

#### Loading

Test specimen no. 4 was loaded with combined internal pressure and bending moment.

#### Corrosion defect parameters (nominal)

#### Instrumentation

In the corroded area 3 cross strain gauges were applied, and two gauges were applied away from the corroded area for load control of the bending moment. The time, rotation angle, the actuator load and displacement were also recorded

#### Loading description

The specimen was exposed to combined internal pressure and 4-point-bending moment. The corrosion defect was located at the compressive side of the bending moment.

An internal pressure of 200 bar was applied during the first 15 minutes. The internal pressure was kept at 200 bar and bending was applied to the test specimen. When the moment exceeded 200 kNm the internal pressure started to drop due to excessive yielding of the pipe. The pipe had become soft and additional displacement was necessary in order to maintain the bending moment. Further, after excessive yielding the actuator reached the maximum stroke which resulted in that the tests changed from load (moment) controlled to displacement controlled. During the increase of internal pressure until burst at 290 bar the resulting bending moment decreased from 260 kNm to 73 kNm.

#### Results

Excessive yielding was observed in the pipe before rupture in the corroded region. The test bursted at a bending moment of 73 kNm and an internal pressure of 290 bar. During the loading the test specimen had also been exposed to an internal pressure of approximately 200 bar and 250 kNm.



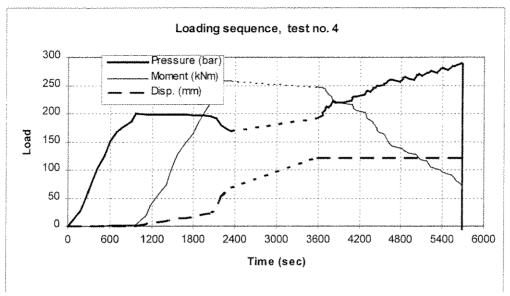


Figure 4-14 Loading sequence, test no.4

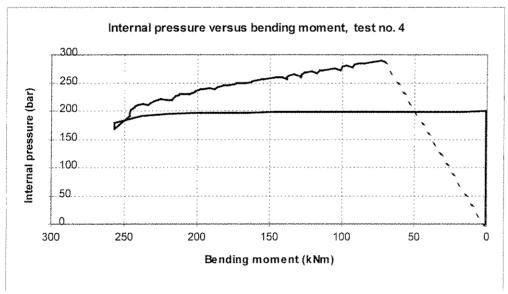


Figure 4-15 Internal pressure versus bending moment, test no. 4





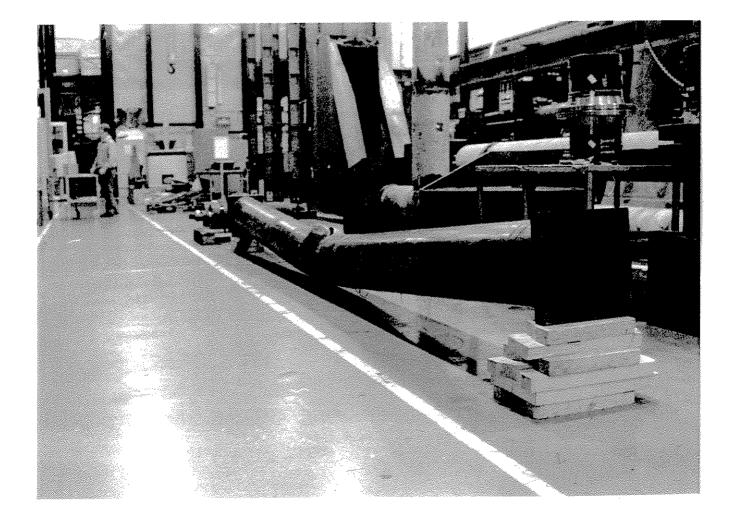


Figure 4-16 Picture of the test specimen no. 4 after the burst test







Figure 4-17 Picture of the test specimen no. 4 after the burst test

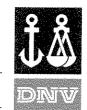




Figure 4-18 Picture of the test specimen no. 4 after the burst test



#### 4.6 Test no. 5

#### Loading

Test specimen no. 5 was loaded with combined internal pressure and axial compressive force.

#### Corrosion defect parameters (nominal)

(Identical with test no. 4)

Corrosion defect depth

 $d = 3.2 \text{ mm} \quad (d/t = 0.3)$ 

Corrosion defect length

L = 162 mm (L/D = 0.50)

Corrosion defect width

 $w = 32 \text{ mm} \quad (w = 3 \text{ t})$ 

Length of test specimen

 $L_{\text{specimen}} = 1000 \text{ mm}$ 

#### Instrumentation

In the corroded area 3 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded.

#### Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

The jack was operated with a manually controlled pump, and during the test the load and the displacement were monitored. With this set-up the operator could manually maintain the axial force by running the pump, or stop the pump and keep the displacement constant.

For test no.5 an internal pressure of 200 bar was first applied, and then the axial compressive load. At approximately 2500 kN external applied axial force the pipe was yielding excessively, and the internal pressure dropped. The internal pressure was again increased to 200 bar, and further axial compressive load was applied, resulting again in a drop in the internal pressure. Both the internal pressure and the jack displacement was increased, but the resulting axial force decreased, until burst occurred at 286 bar and with an axial compressive external force of 2563 kN.

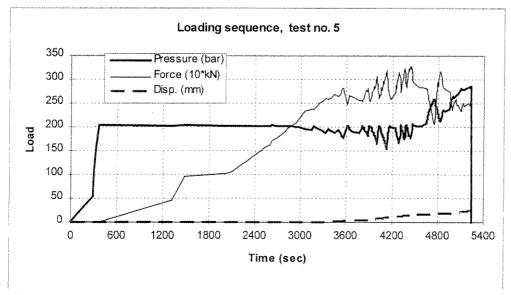


Figure 4-19 Loading sequence for test no. 5



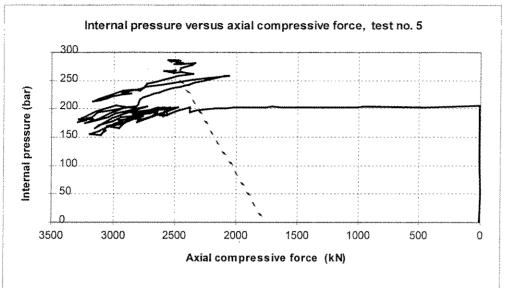


Figure 4-20 Internal pressure versus axial compressive force, test no. 5

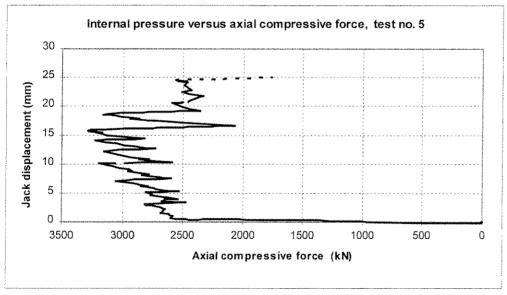


Figure 4-21 Jack displacement versus axial compressive force, test no. 5

#### Results

Excessive yielding was observed in the pipe before rupture in the corroded region occurred. The test bursted at an internal pressure of 286 bar, and with an axial compressive external force of 2563 kN. The end cap force due to the internal pressure was 2060 kN, resulting in a compressive pipe wall force of only 503 kN, equivalent to 48 MPa in axial compression.







Figure 4-22 Picture of the test specimen no. 5 in the test rig before the burst test





Figure 4-23 Picture of the test specimen no. 5 after the burst test







Figure 4-24 Picture of the test specimen no. 5 after the burst test

# JÅ Dinv

#### DETAILED DESCRIPTION OF THE TESTS

#### 4.7 Test no. 6

## Loading

Test 6 was loaded with combined internal pressure and axial compressive force.

## Corrosion defect parameters (nominal)

(Identical to test specimen no. 4 and 5)

Corrosion defect depth d = 3.2 mm (d/t = 0.3)Corrosion defect length L = 162 mm (L/D = 0.50)

Corrosion defect width  $w = 32 \text{ mm} \quad (w = 3 \text{ t})$ 

Length of test specimen  $L_{\text{specimen}} = 1000 \text{ mm}$ 

#### Instrumentation

In the corroded area 3 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded.

## Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

For test no.6 an internal pressure of 200 bar was first applied succeeded by axial compressive force. At approximately 2500 kN external axial force the pipe was yielding extensively, resulting in drop in the internal pressure. The internal pressure was maintained by pumping water simultaneously to the increase of the jack force to approximately 4300 kN. At this point the jack displacement was approximately 50 mm and the range of the displacement transducer was exceeded. The position of the transducer was changed, and due to safety reasons during this operation the test specimen was unloaded. The test specimen was reloaded to 200 bar, and further axial displacement/force was applied to the test. More excessive yielding was experienced, the pipe at the end supports started to deform, and in order to burst the pipe the internal pressure was increased when keeping the displacement constant allowing the axial compressive force to decrease.

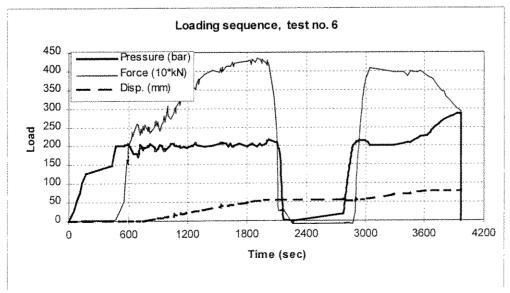


Figure 4-25 Loading sequence, test no. 6





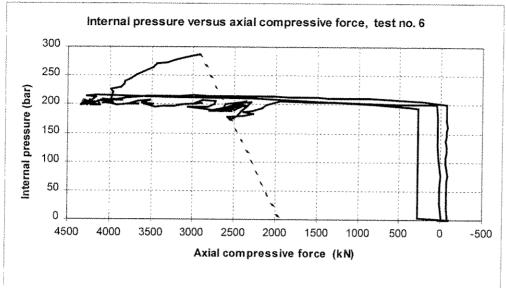


Figure 4-26 Internal pressure versus axial compressive force, test no. 6

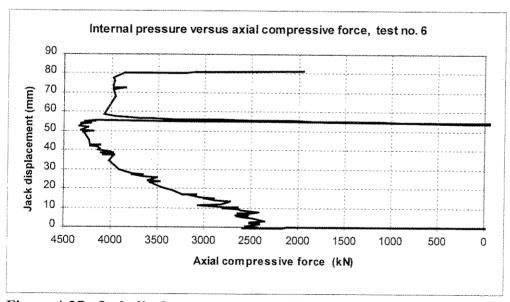


Figure 4-27 Jack displacement versus axial compressive force, test no. 6

#### Results

Excessive yielding was observed in the pipe before rupture in the corroded region. The test bursted at an internal pressure of 287 bar, and with an axial compressive external force of 2943 kN. The end-cap force due to the internal pressure was 2067 kN, resulting in a compressive pipe wall force of only 876 kN, equivalent to 84 MPa. The test specimen had during the test experienced 205 bar and 4323 kN.





Figure 4-28 Picture of the test specimen no. 6 after the burst test





Figure 4-29 Picture of the test specimen no. 6 after the burst test



#### 4.8 Test no. 7

## Loading

Test 7 was loaded with combined internal pressure and axial compressive force.

#### Corrosion defect parameters (nominal)

The corrosion defect was longer and deeper compared to the test specimen no. 4, 5 and 6.

#### Instrumentation

In the corroded area 3 cross strain gauges were used, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded

## Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

For test no.7 an internal pressure of 175 bar was applied, and succeeded by axial compressive load. At approximately 2500 kN axial force the pipe was yielding extensively and the internal pressure started to dropped. The internal pressure was maintained simultaneously as the jack force was increased to approximately 3000 kN. The internal pressure was increased slightly while maintaining the axial force, until burst.

#### Results

The specimen bursted at 186 bar and an axial force of 2998 kN.



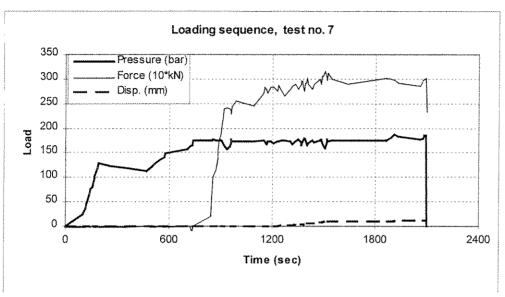


Figure 4-30 Loading sequence, test no. 7

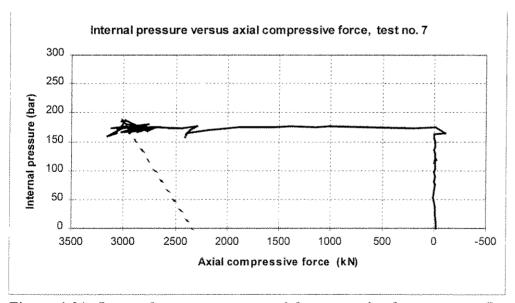


Figure 4-31 Internal pressure versus axial compressive force, test no. 7



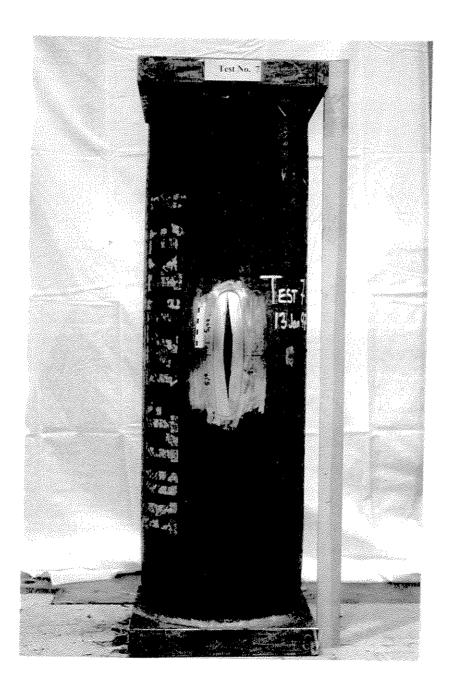


Figure 4-32 Picture of the test specimen no. 7 after the burst test





Figure 4-33 Picture of the test specimen no. 7 after the burst test



#### 4.9 Test no. 8

## Loading

Test no. 8 was loaded with internal pressure only.

## Corrosion defect parameters (nominal)

(Identical to test specimen no. 7)

Corrosion defect depth  $d = 5.3 \text{ mm} \quad (d/t = 0.5)$ Corrosion defect length L = 245 mm (L/D = 0.75)

Corrosion defect width  $w = 32 \text{ mm} \quad (w = 3 \text{ t})$ 

 $L_{\text{specimen}} = 1000 \text{ mm}$ Length of test specimen

#### Instrumentation

In the corroded area 3 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading.

## Loading description

The specimen was exposed to internal pressure.

#### Results

The test specimen was loaded with internal pressure until burst at 220 bar.

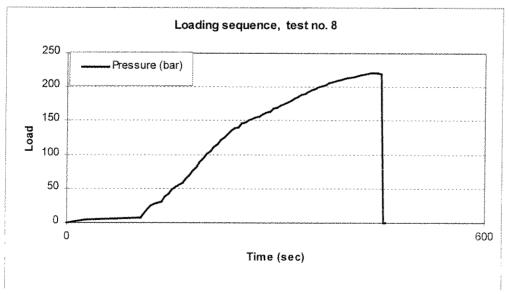
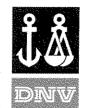


Figure 4-34 Loading of test no. 8, internal pressure only.



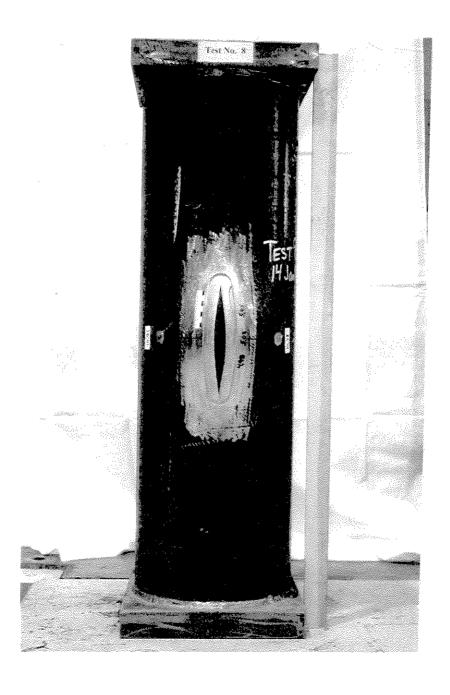


Figure 4-35 Picture of the test specimen no. 8 after the burst test





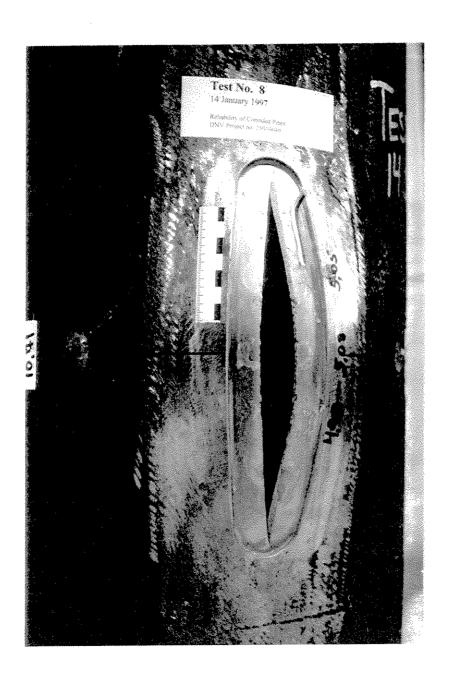


Figure 4-36 Picture of the test specimen no. 8 after the burst test



## 4.10 Test no. 9

## Loading

Test 9 was loaded with combined internal pressure and axial compressive force.

## **Corrosion defect parameters (nominal)**

#### Instrumentation

In the corroded area 3 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded

## Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

For test no.9 an internal pressure of 130 bar was applied, succeeded by axial compressive load was applied until burst. The internal pressure was 123 bar and the axial compressive force was 2070 kN at burst. The end-cap force due to the internal pressure was 886 kN, resulting in a compressive pipe wall force of only 1184 kN, equivalent to 113 MPa.

#### Results

The internal pressure was 123 bar and the axial compressive force was 2070 kN at burst.



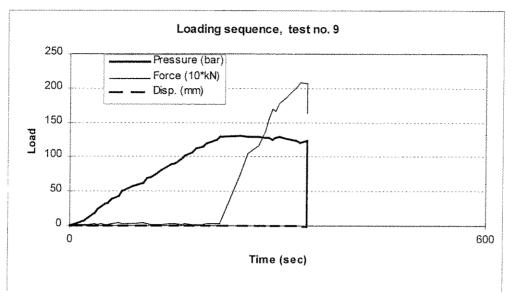


Figure 4-37 Loading sequence, test no. 9

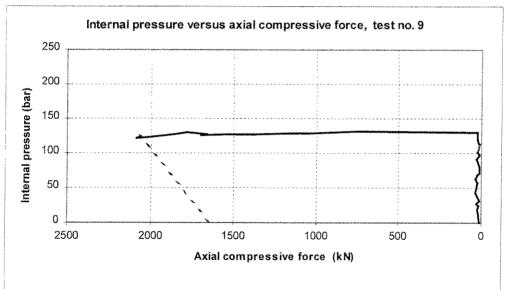


Figure 4-38 Internal pressure versus axial compressive force, test no. 9







Figure 4-39 Picture of the test specimen no. 9 after the burst test



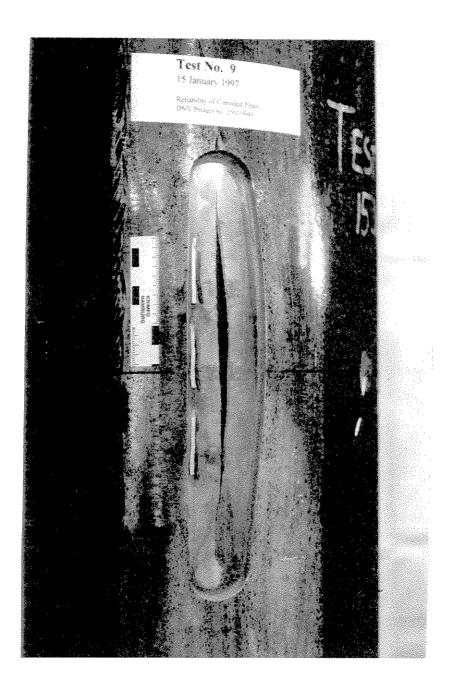


Figure 4-40 Picture of the test specimen no. 9 after the burst test



## 4.11 Test no. 10

#### Loading

Test 10 (and 11 and 12) were made with circumferential corrosion, and were loaded with combined internal pressure and axial compressive force.

## Corrosion defect parameters (nominal)

Corrosion defect depth

 $d = 5.3 \text{ mm} \quad (d/t = 0.5)$ 

Corrosion defect length

L = 12 mm

Corrosion defect width

w = full circumference

Length of test specimen

 $L_{\text{specimen}} = 1000 \text{ mm}$ 

A 12 mm wide ring groove was machined to 50% of the depth for the full circumference of the pipe at the outer surface to simulate girth weld corrosion. The groove was made in the parent material.

#### Instrumentation

In the corroded area (groove) 4 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded

## Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

Internal pressure was applied until burst and simultaneously an axial compressive force corresponding to the end cap force was applied. The resulting pipe wall force was close to zero. Burst occurred at 320 bar and an axial force of 2289 kN.

#### Results

Burst occurred at 320 bar and with an axial compressive force of 2289 kN. The rupture was in the longitudinal direction, even though the corrosion defect was in the circumferential direction.



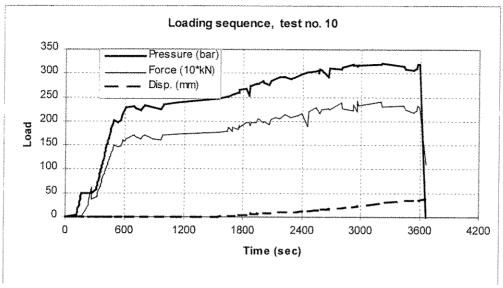


Figure 4-41 Loading sequence, test no. 10

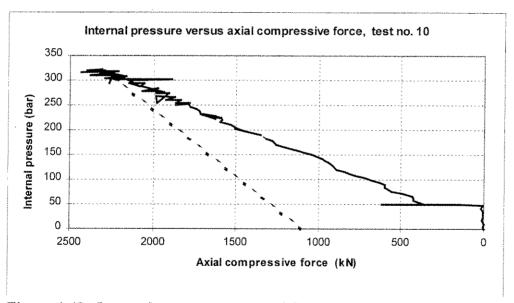


Figure 4-42 Internal pressure versus axial compressive force, test no. 10





Figure 4-43 Picture of the test specimen no. 10 after the burst test





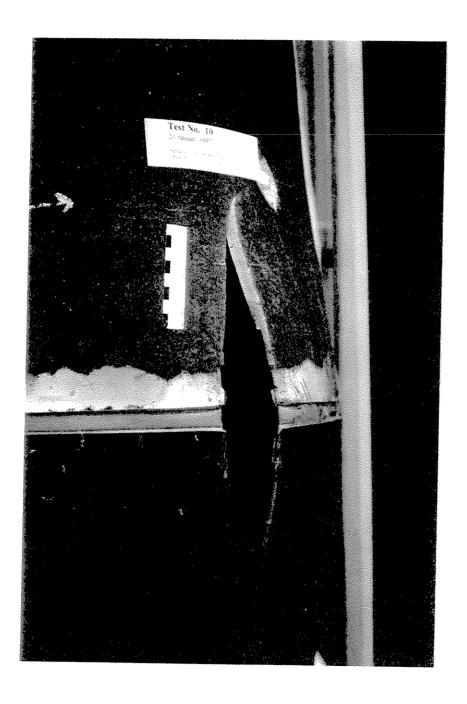


Figure 4-44 Picture of the test specimen no. 10 after the burst test



#### 4.12 Test no. 11

## Loading

Test no. 11 was loaded with combined internal pressure and axial compressive force.

## Corrosion defect parameters (nominal)

(Identical with test specimen no. 10)

Corrosion defect depth  $d = 5.3 \text{ mm} \quad (d/t = 0.5)$ 

Corrosion defect length L = 12 mm

Corrosion defect width w = full circumference

Length of test specimen  $L_{\text{specimen}} = 1000 \text{ mm}$ 

A 12 mm wide ring groove was machined to 50% of the depth for the full circumference of the pipe at the outer surface to simulate girth weld corrosion. The groove was made in the parent material.

#### Instrumentation

In the corroded area (groove) 4 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded.

#### Loading description

The specimen was exposed to combined internal pressure and axial compressive force.

Internal pressure was applied simultaneously with an axial compressive force corresponding to the end cap force, hence the resulting pipe wall force was close to zero. The internal pressure was kept constant at 225 bar and only axial compressive force was applied up to 3800 kN. From this point additional internal pressure was applied and the axial force was tried maintained. However, this required large displacements in the axial direction, and after 95 mm compression of the pipe the stroke limit of the jack was reached and the displacement was kept constant when further internal pressure was applied until burst. (The displacement transducer exceeded the measure range after 50 mm). This resulted in a drop in the axial load down to 2343kN when the pipe bursted at 335 bar.

#### Results

Burst occurred at 335 bar and with an axial compressive force of 2345 kN. The rupture was in the longitudinal direction, even though the corrosion defect was in the circumferential direction.



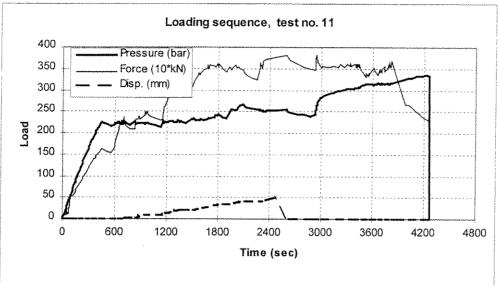


Figure 4-45 Loading sequence, test no. 11

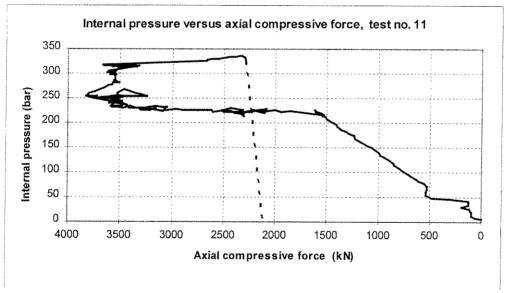


Figure 4-46 Internal pressure versus axial compressive force, test no. 11





Figure 4-47 Picture of the test specimen no. 11 after the burst test





Figure 4-48 Picture of the test specimen no. 11 after the burst test



#### 4.13 Test no. 12

## Loading

Test no. 12 was loaded with combined internal pressure and axial compressive force.

## **Corrosion defect parameters (nominal)**

Corrosion defect depth

 $d = 7.5 \text{ mm} \quad (d/t = 0.7)$ 

Corrosion defect length

L = 12 mm

Corrosion defect width

w = full circumference

Length of test specimen  $L_{\text{specimen}} = 1000 \text{ mm}$ 

A 12 mm wide ring groove was machined to 70% of the depth for the full circumference of the pipe at the outer surface to simulate girth weld corrosion. The groove was made in the parent material.

## Instrumentation

In the corroded area (groove) 4 cross strain gauges were applied, and 4 gauges were applied in a uncorroded region to monitor the loading. The time and the jack load and displacement were also recorded.

Unfortunately, the recorded data were lost and only the data from the final part of the test were recovered based on the test log and (security) paper printout from the datalogger, which is the results of most interest.

#### Loading

The specimen was exposed to combined internal pressure and axial compressive force.

Internal pressure was applied simultaneously with an axial compressive force corresponding to the end cap force was applied. The resulting pipe wall force was close to zero. The internal pressure was kept constant at 250 bar and axial compressive force was applied up to 3250 kN. From this point additional internal pressure was applied and the axial force was tried maintained, but at further increase in the internal pressure the displacement was kept constant. This resulted in a drop in the axial load down to 2380 kN when the pipe bursted at 321 bar.

#### Results

The test specimen bursted at 321 bar with an axial compressive force of 2399 kN. The rupture was in the bottom of the groove with a length of 70 mm.



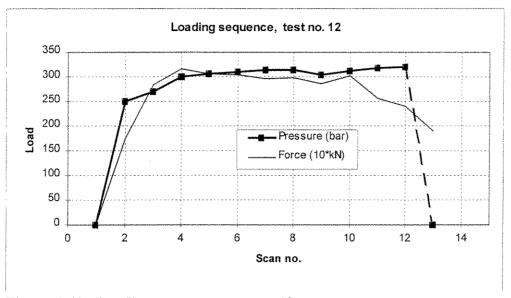


Figure 4-49 Loading sequence, test no. 12

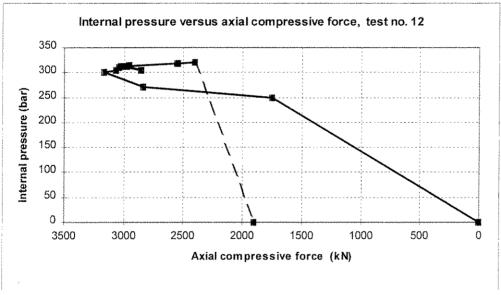


Figure 4-50 Internal pressure versus axial compressive force, test no. 12





Figure 4-51 Picture of the test specimen no. 12 after the burst test



SUMMARY OF TESTS AND TEST RESULTS

## 5 SUMMARY OF TESTS AND TEST RESULTS

#### 5.1 Overview of test results

In Table 5-1 and Table 5-2 the main results from the tests are included. In Table 5-2 the loads are given in bot forces and stresses.

Table 5-1 Overview of test results

Test no.	Nom Dia (mm)	Nom thick (mm)	Mat	defect depth (d/t)	defect length L/D	defect width w/t	Loading	Date of test	Burst (press) (force/mom.)
	324	10.3	X52	0.50	0.75	15	internal press	1 July 1996	232 bar 0
2	324	10.3	X52	0.50	0.75	15	internal press and bending moment	7 Aug. 1996	219 bar 129 kNm
3	324	10.3	X52	0.50	0.75	15	internal press and bending moment	18 Oct. 1996	195 bar 212 kNm
4	324	10.3	X52	0.30	0.50	3	internal press and bending moment	20 Nov. 1996	290 bar 73 kNm
5	324	10.3	X52	0.30	0.50	3	internal pressure and axial comp. force	18 Des. 1996	286 bar -2563 kN
6	324	10.3	X52	0.30	0.50	3	internal pressure and axial comp. force	7 Jan. 1997	287 bar -2943 kN
7	324	10.3	X52	0.50	0.75	3	internal pressure and axial comp. force	13 Jan. 1997	186 bar -2998 kN
8	324	10.3	X52	0.50	0.75	3	internal pressure	14 Jan. 1997	220 bar 0
9	324	10.3	X52	0.70	0.75	3	internal pressure and axial comp. force	15 Jan. 1997	123 bar -2070 kN
10	324	10,3	X52	0.50	12 mm	full circ.	internal pressure and axial comp. force	20 Jan, 1997	320 bar -2289 kN
11	324	10.3	X52	0.50	12 mm	full circ.	internal pressure and axial comp. force	21 Jan. 1997	335 bar -2343 kN
12	324	10.3	X52	0.70	12 mm	full circ.	internal pressure and axial comp, force	22 Jan. 1997	321 bar -2399 kN

The forces given in the table are external applied axial compressive forces measured in the jack. See Table 5-2 for more details of the loads.

For the tests with bending moment the corrosion defect was located on the side of the pipe with compressive axial stresses due to the moment.



## SUMMARY OF TESTS AND TEST RESULTS

DINV

Table 5-2 Overview of test results

Test	defect	defect	defect	Loading	Burst 1) (press.)	Pipe wall forc	es and stresses 2)
no.	depth (d/t)	length L/D	width w/t		(force/mom.)	press. / force	pipe wall stresses
1	0.50	0.75	15	internal press	232 bar 0	232 bar 1668 kN	331MPa (hoop) 160 MPa (long.)
2	0.50	0.75	15	internal press and bending moment	219 bar 129 kNm	219 bar not given	312 MPa (hoop) -12 MPa (long.)
3	0.50	0.75	15	internal press and bending moment	195 bar 212 kNm	195 bar not given	278 MPa (hoop) -134 MPa (long.)
4	0.30	0.50	3	internal press and bending moment	290 bar 73 kNm	290 bar not given	412 MPa (hoop) 109 MPa (long.)
5	0.30	0.50	3	internal pressure and axial comp. force	286 bar -2563 kN	286 bar -503 kN	409 MPa (hoop) -48 MPa (long.)
6	0.30	0.50	3	internal pressure and axial comp. force	287 bar -2943 kN	287 bar -876 kN	410 MPa (hoop) - 84 MPa (long.)
7	0.50	0.75	3	internal pressure and axial comp. force	186 bar -3000 kN	186 bar -1659 kN	265 MPa (hoop) -159 MPa (long.)
8	0.50	0.75	3	internal pressure	220 bar 0	220 bar 1586 kN	314 MPa (hoop) 152 MPa (long.)
9	0.70	0.75	3	internal pressure and axial comp. force	123 bar -2070 kN	123 bar 1184 kN	176 MPa (hoop) -113 MPa (long.)
10	0.50	12 mm	full circ.	internal pressure and axial comp. force	320 bar -2289 kN	320 bar 10 kN	456 MPa (hoop) 1 MPa (long.)
11	0.50	12 mm	full circ.	internal pressure and axial comp. force	335 bar -2343 kN	335 bar 84 kN	479 MPa (hoop) 8 MPa (long.)
12	0.70	12 mm	full circ.	internal pressure and axial comp. force	321 bar -2399 kN	321 bar -94 kN	458 MPa (hoop) -9 MPa (long.)

Nominal diameter: 324 mm. Nominal wall thickness: 10.3 mm.

- 1) The forces given in this column are external applied forces.
- 2) The forces given in these columns are pipe wall forces and stresses. The force is calculated as the force on the end-cap due to the internal pressure minus the applied external force on the jack.

For tests exposed to bending moment, the pipe wall stress is given on the compressive side where the defect was located. The pipe wall forces are not given for the cases with bending moment.

The calculation of the stress is based on uncorroded and undeformed cross section. The average measured wall thickness of 10.6 mm is used (nominal 10.3mm).



MATERIAL PROPERTIES

#### 6 MATERIAL PROPERTIES

The test specimens were manufactured from 2 tubes of seamless X52 modified material. A copy of the material certificates are included Appendix A. The test specimens 1 to 9 were made from one single tube, while the test specimens 10 to 12 were made from another tube. Tensile tests were conducted on four specimens machined from each tube to provide the required material parameters. The tensile test specimens were machined such that two had their axis in the longitudinal direction and two had their axis in the circumferential direction from each tube.

The tensile test specimens were manufactured with a diameter of 6 mm, and the length of each specimen was 50 mm. A 25 mm extensometer was fitted to each specimen.

The behaviour of specimens under tensile force showed a very good degree of consistency.

Plots of the axial tension as function of elongation are included in Appendix B.

The material average engineering properties were determined to be;

• Yield strength:

380 MPa

• Tensile strength:

514 MPa

Based on the plots included in Appendix B the "average" material curve is calculated as shown in Figure 6-1. Both the engineering and the true stress-strain material curve are given.

The material showed a yielding plateau at 380 MPa.

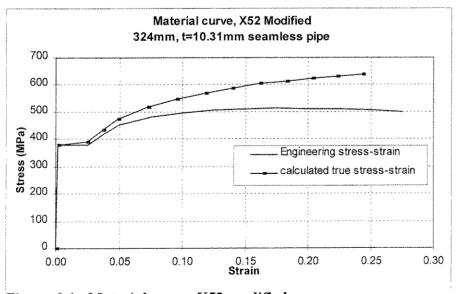


Figure 6-1 Material curve, X52 modified



#### MATERIAL PROPERTIES

The corresponding numbers are given in Table 6-1.

Table 6-1 Material data

Engineering st	ress-strain	Calculated true stress-strain		
strain	stress (MPa)	strain	stress (MPa)	
0	0.0	0.000	0.0	
0.0018	380.0	0.002	380.7	
0.025	380.0	0.025	389.5	
0.038	419.3	0.037	435.0	
0.050	450.9	0.049	473.4	
0.075	482.4	0.072	518.6	
0.100	496.0	0.095	545.6	
0.125	505.0	0.118	568.1	
0.150	509.5	0.140	585.9	
0.175	514.0	0.161	603.9	
0.200	511.7	0.182	614.1	
0.225	509.5	0.203	624.1	
0.250	505.0	0.223	631.2	
0.275	500.5	0.243	638.1	

The true stress-strain curve is calculated from the engineering stress-strain curve;

$$\begin{split} \epsilon_{true} &= ln(1 + \epsilon_{eng}) \\ \sigma_{true} &= \sigma_{eng}(1 + \epsilon_{eng}). \end{split}$$

# **APPENDIX**

#### $\mathbf{A}$

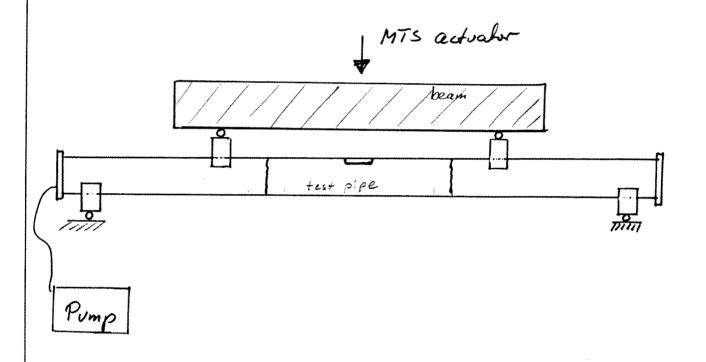
DESCRIPTION OF THE TEST RIG, CORROSION DEFECTS, THICKNESS MEASUREMENTS AND INSTRUMENTATION

- 000 -



roject title:				Project No.		
Client/Subject:	PREPARED Date:		Sign.:	Doc. No.:		
	VERIFIED	Date:	Sign.:	Rev.:	Page:	

Test set-up for combined internel pressure and 4-point bending moment. (not to scale)



Project title:	111	<b>&gt;</b>		Project N	
Project tide:  Reliability of Corre	PREPARED	Date:	Sign.:	Doc. No.:	10049
DNV Test 1,2 and 3	VERIFIED	Date:	Sìgn.:	Rev.:	Page:
Spark eroded defect for	- test lect:	$d = \sim$ $L = 29$	5.3 m	,m. ( n (	$\frac{1}{4/2} = 0.5$ $\frac{4}{10} = 0.75$ $\frac{4}{10} = 0.75$
+~10.5 mm	:1 150mm				



Project title: Reliability of Cor	Project No.: 25010049				
Client/Subject:	PREPARED	Date:	Sign.:	Doc. No.:	
Test no. 4 to 9.	VERIFIED	Date:	Sign.:	Rev.:	Page:

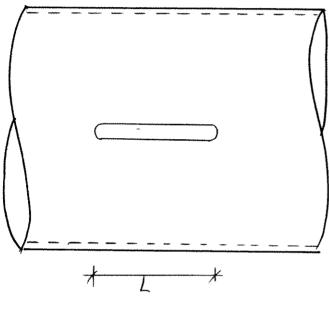
Spark eroded defects.

D = 324 mm defect : d - various

t ~10.5mm

: L - various

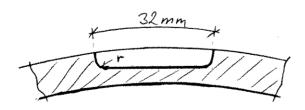
: W = 32 mm



# W=32mm

	<u> </u>	j
t=105	V///kr	Id
ر پايان ز	11/11/11/11/11/11/11/11/11/11/11	1

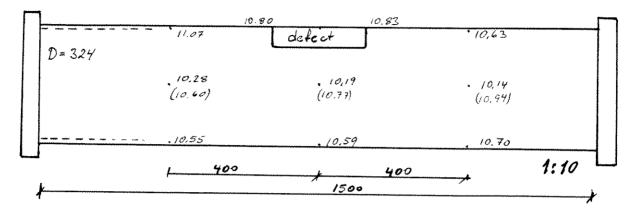
Test no	. L	d mm	r mm
4	162	3,2	3
5	162	3.2	3
6	162	3.2	3
7	245	5.3	3
8	245	5.3	3
9	245	7.5	3



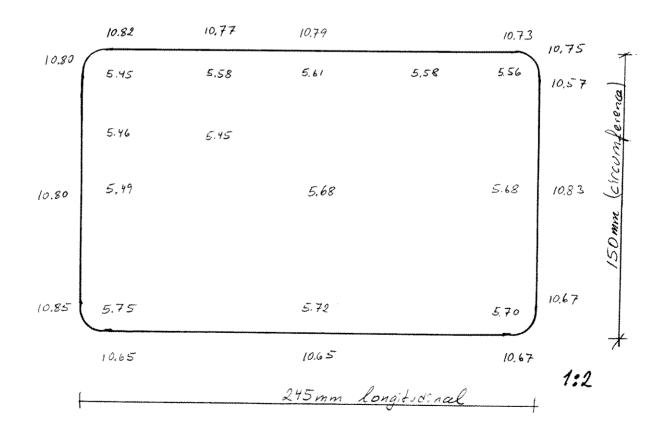


Project title:	Reliability.	of Corroded	Pipes		Project N	No.: 010049
Client/Subject:		PREPARED	Date: 1997	Sign.: OHB	Doc. No.	
Test	L no. 1	VERIFIED	Date:	Sign.:	Rev.:	Page:

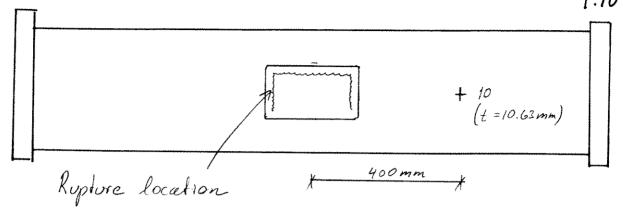
# Thickness measurements (mm)

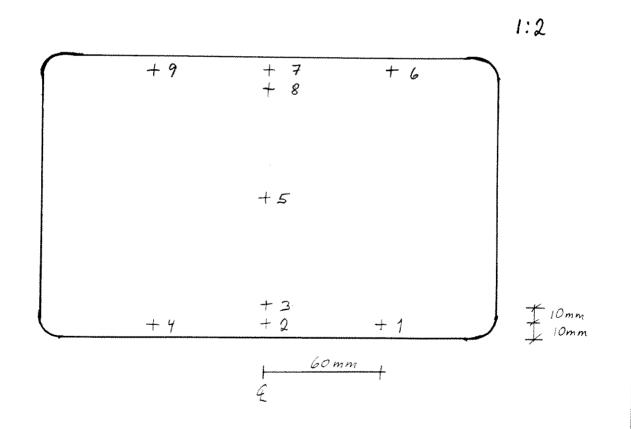


# Thickness measurements of the corrosion defect (mm)



Client/Subject:  PREPARED  Date: Sign.: Doc. No.:  Verified  Date: Sign.: Page:  Strain gauge location and numbering	우유	Project tide: Reliability of	f Corroded	Pipe:	<u> </u>	Project 1	No.: 010049
	小心	Client/Subject:		Date:	Sign.:	Doc. No	
Strain gauge location and numbering	DNV	Test no. 1.	VERIFIED	Date:	Sign.:	Rev.:	Page:
	St	rain gauge locatro	on and nu	n berr	- <u> </u>		

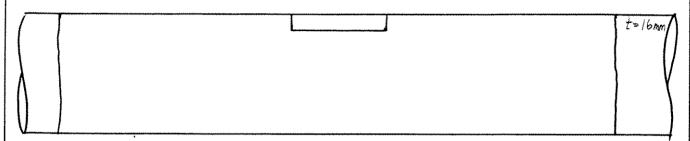




ĴÅ
DNV

ľ	Project title: Reliability of C	.orroded	P:pes		Project No.	: 10049
	Client/Subject: V	PREPARED	Date:	Sign.:	Doc. No.:	
	Test no. 2	VERIFIED	Date:	Sign.:	Rev.:	Page:

1:10



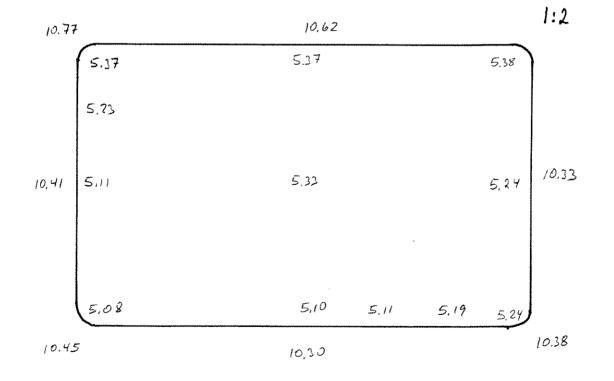
# Thickness measurements of the corrospon defect (mm)

10,56	10.42	10.36		10.41	10.43	1:2
10.30	5,33	5,53	5,33	5,46	5.38	10,61
10.60	5.24	6,40	5.26	5.29	5,24	10.55
						10,53
10.56	5,36	5.48	5.50	5,36	5.27	10.82
	10.67	10.85		10.70	10.78	

<b>4 8</b>	Project title: Re	loabiloty q	f Corrodec	Pipe	.5		710049
	Client/Subject:	V	PREPARED	Date.		Doc. No.:	
DNV	Test	no. 2	VERIFIED	Date:	Sign.:	Rev.:	Page:
Str	aln Gauge	e location	and humb	ering			1:10
	(	10 (11) (e filaments (L) 450					
	<del>}-</del>	750	<del></del>	Rupdure	locat	lon	
						1	: 2
		+1	+3	+4			
			+5			The second secon	
		+6	+ 8 + 7	+ 9	7		10 mm
			+ 60	mm			,

Project No.: 25010049	es	Pop	1 Corroded	Project title: Reliability of
Doc. No.:	Sign.:	Date:	PREPARED	Client/Subject:
Rev.: Page:	Sign.:	Date:	VERIFIED	Test no.3
		Date:		Test no.3

10.40 | t=16 | t

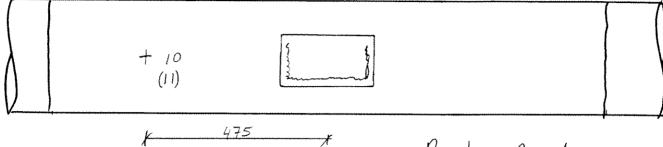


22	Project title:				Project No.:
ÅÅ	Client/Subject:	PREPARED	Date:	Sign.:	Doc. No.;
DNV	Test no.3	VERIFIED	Date:	Sign.:	Rev.:

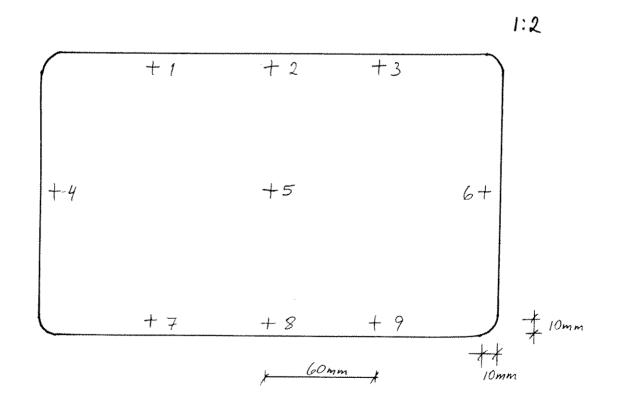
Strain gauge location and numbering

1:10

Page:



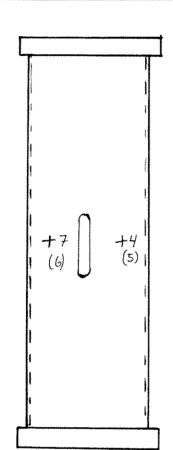
Rupture location



2 8	Project tide:  Reliability of Co	proded	Pipes		Project No.: 250100 4 9	***************************************
	Client/Subject:	PREPARED	Date:	Sign.:	Doc. No.:	•
DINV	Test no. 4	VERIFIED	Date:	Sign.:	Rev.: Page:	
THE PARTY OF THE P	c	defect			1:10	
/ t=16	1 + 10,65				t=16	\
V	2 + 10.66					ļ
	300		1100	····		
	10.75 10.71		1:2			
10,54 7.	7.59 7.53 34 7.29 7.38 7.41	7,30) 10	),42			
	7.45 7.46		-			
- Article and Arti	10.45 10.46					
	10	_				
	+3 +4 +5					
	x 45 x 45	-				

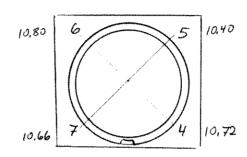
2 2	Projec
小例	Client
	_

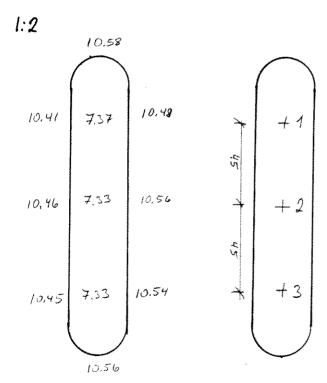
Project title: Relability of	Corrodec	& Pope	£	Project No.	10049
Client/Subject:	PREPARED	Date:	Sign.:	Doc. No.:	
Test no. 5	VERIFIED	Date:	Sign.:	Rev.:	Page:

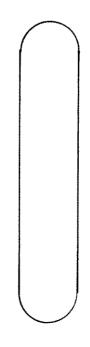


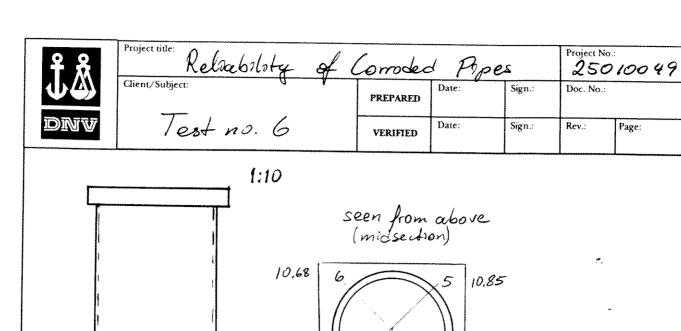
1:10

seen from above (midsection)

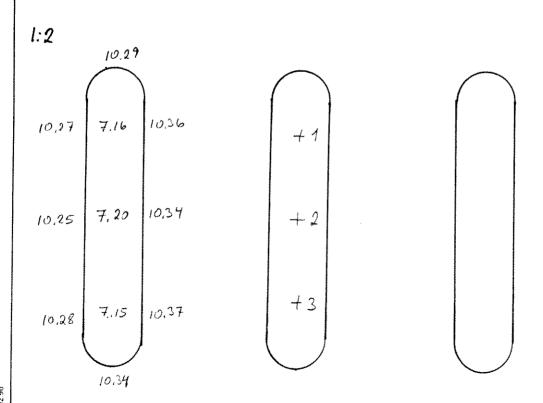








10.29



<b>4 8</b>	Projec	Reliab	ilsty o	4 Com	ded P	nes		Project N	010049
中国	Client	/Subject:	V		PREPARED	Date:	Sign.:	Doc. No.	
VINIC		Test	no.	7	VERIFIED	Date:	Sign.:	Rev.:	Page:
				:10					
		Andrew Angeles			Seen	from a section)	bose		
	and the same of th	- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1-			(mid	section)		ź.	
	AND THE PROPERTY OF THE PROPER	-		10,59	6		10,52		
	· · · · · · · · · · · · · · · · · · ·					$\langle \rangle$			•
	   +7   (G)	+4 (5)					/		
	(G) 	$\left  \left  \left  \left  \left  \left  \left  \left  \left  \left  \right  \right  \right  \right  \right  \right  \right  \right $		10.60	, 7×		10.37		
		-							
	! !								
Г			T						
\$	10.26	)							
1:2	4,86	)	ł						
			:						
10,58	5,02	10.34	_	+ 1					
			45	The state of the s		P			
	4,98	10.46		+2					
10.40	7,75	10.40	54	7.2					
			×1	MARKATA CALLANDA CAL			Mark Control of the C		
10,43	5,18	10.48	4	+3					
						West of the last o			
(	5.01					(	J		

DET NORSKE VERITAS

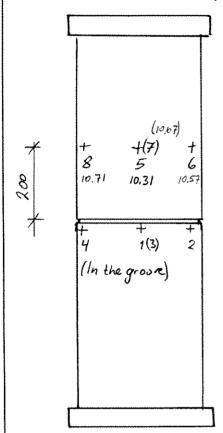
<b>2</b> 8	Project	Reliab	ilsty of	Corre	oded Py	oes		Project No.	10049
中创	Client/	Subject:	0 1		PREPARED	Date:	Sign.:	Doc. No.:	
DWV		Test	no. 8		VERIFIED	Date:	Sign.:	Rev.:	Page:
			] 1:10						
					Seen	from a section)	bore		
	· 	į.			(mid	section)		*	
	**************************************			11.0	8 6		10.68		
		$\cap  \   ]$				$\langle \rangle$			
**************************************	   +7   (G)	+4 (5)			,   7		10.38		
	<i>(G)</i> 	$\left  \left  \left  \frac{(5)}{3} \right  \right $		10.7	1 7	5 9	10.38		
	-	#:							
		i i							
	***	<b>1</b>							
		i i	<b>T</b>						
	10.40	)							
1:2	4.96	)							
10.73	5.05	10.33		+1					
			24	***************************************					
				+2					
10,57	5,08	10,38	<b>5</b>	•					
10.52	4.98	10.31		+3					
. +			CANADIA AND AND AND AND AND AND AND AND AND AN				***************************************		
i			77 - 77			W. Andrews	**************************************		
(	5,14,	)	(						

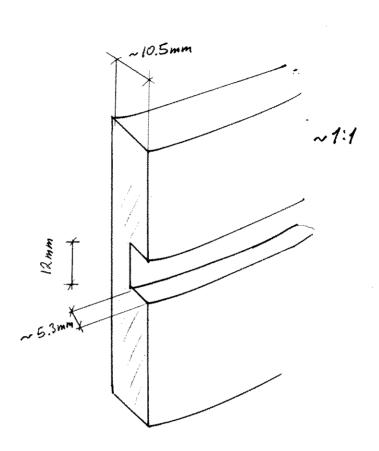
<b>4 8</b>	Project	Reliabi	laty of	Com	ded Py	nes		Project N	io.: D10049
心學	Client/	Subject:	V /		PREPARED	Date:	Sign.:	Doc. No.	
VIND	athinds the street section of the se	Test	no.	9	VERIFIED	Date:	Sign.:	Rev.:	Page:
			l:						
			-		Seen	from a section)	bore		
*					(mid	section)			2
The second secon		- Harris - H		10.86	6	<b>X</b>	10.30		_
Administration of the Control of the		$\cap$				$\langle \rangle$			
Y THE PROPERTY OF THE PROPERTY	+ 7 (G)	+4		10.89	7		1 10,64		
middeliji i programa	(G)			10,67		7			
· · · · · · · · · · · · · · · · · · ·		#							
		-							
na.	!								
			<b>T</b>						
\$	1051		<b></b>						
1:2 (	3,02	)	(						
1057	3.//	10.52	And a part of the	+ 1					
10.57	2.06	10/2	S#	***************************************					
***************************************									
10.62	3,16	10.40	24	+2					
			5						
10,65	2,18	10.33	4	+3					
			Personalisassissississississississississississis				***************************************		
up and the state of the state o			Management of the Control of the Con	The state of the s			V		
	3,70	<b>)</b>							



Project title: Relia	bility of	Corroded Po	pes		Project N	No.: 010049
Client/Subject:	4 1	PREPARED	Date:	Sign.:	Doc. No	.:
Test 1	10. 10	VERIFIED	Date:	Sign.:	Rev.:	Page:

1:10





# measured thechness

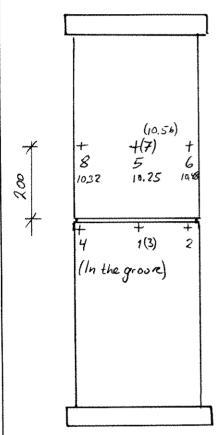
Gange	groose	Pipe
1	5.22	10.34
	5,5 <b>5</b>	10.50
	5.30	10.38
	5.55	10.49
Z	5.66	10.52
	5.95	10.81
	5.70	10.41
	5.70	10.77
3	5.75	10.67
	5.67	10.78
	5.60	10.80
	5.75	10.70
4	5.59	10.71
	5.67	10.78
	5.22	10.35
	5.21	10,51

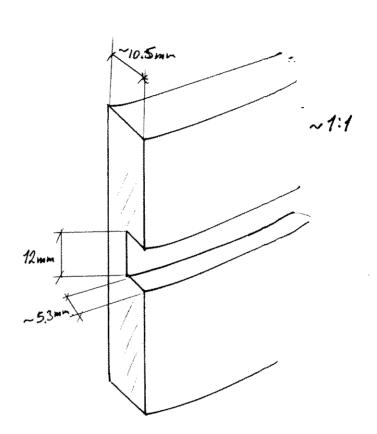
Rupture location close to steam gauge 2.

0.0	
4 %	

Project title: Reliability &	A Corroded Py	pes		Project N	o.: 10049
Client/Subject:	PREPARED	Date:	Sign.:	Doc. No.	•
Test no. 11	VERIFIED	Date:	Sign.:	Rev.:	Page:

1:10





## Thekness measurements

Coange	grosve	- Pipe
1	4.93	10.12
	5,14	10.27
	5.12	10,14
	5.35	10.47
2	5.66	10.22
	5.92	10.66
	5.67	10.57
	5.31	10.41
3	5.64	10.56
	5.82	10.57
	6.01	10.48
	6.06	10.55
4	5.87	10.30
	5.68	10.48
	5,37	10.60
	JE 15	10 22



Project title:

Reliability of Coroded Pipes

Client/Subject:

PREPARED

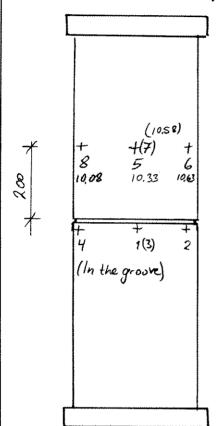
Date:

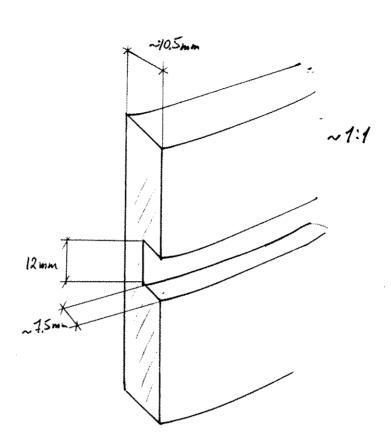
Sign.:

Doc. No.:

Page:

1:10





Measured thockness

Gauge	groome	pipe
l	2.89	10,51
	3,14	10.59
	2.87	10.40
	2.94	10.53
2	2.98	10.52
	3.56	10.93
	3,26	10.58
	3.49	10.48
3	3,44	10.50
	3.76	10,51
	3.60	10.48
	-3.04	10,30
4	2.88	10.07
	3.26	10,48
	2.95	10.52
	303	10.46

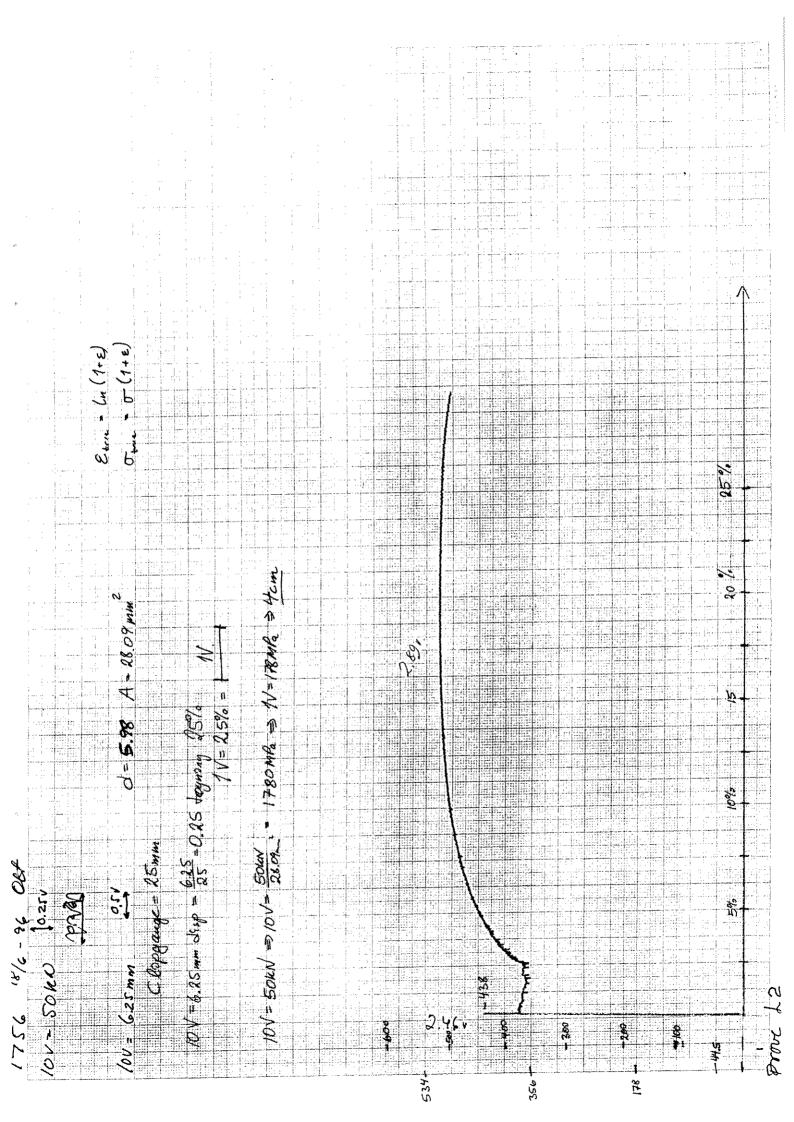
## **APPENDIX**

MATERIAL CERTIFICATES AND MATERIAL TEST RESULTS

- 000 -

Project No. 156

Date: 16 - 9 Sign: M. Forlangula Kontrakezon Form No. 20.200a 76.3 Es 74.9 30 75,0 729 Ar As 34.0 37.0 37.7 38.7 Tylegrender | Shulckfasther |
| 0.2 grender | Shulckfasther |
| KN N/mme KN N/mme LO30 M. |
| WN N/mme KN N/mme LO30 M. | 40,2 41.3 Harvay 8002 513 516 <u>マラ</u> ナ・ナー DATA SHEET 396 398 11.05 11.25 27.50 28.27 27.90 28.09 5,96 DET NORSKE VERITAS 6.00 85'5 2.3 Research laboratories 2



): 0.8 mm/min V= 3700524 0,23 100 = 50 KD 2.33v 101 = 6.25 mm

117

		The state of the s
	·	
	•	
		· · · · · · · · · · · · · · · · · · ·
ši		
*		
	the state of the s	
	2,200	
• •		
	2.880	/
	**************************************	
Z.		· · · · · · · · · · · · · · · · · · ·
		The state of the s
\$		225/
3		-
<i>)</i>		
2 6		
6,23		
3	30	the state of the s
3		<u> </u>
SOKL)	3	2.2/
9 (%)	<i>√</i> .	
	Ou = 6.25°	
· · ·	30	
`	7	

Tet., 51 48 27 00 - Jelefax, 01 40 05 04 Reg.No.: 947 539 191 - V.A.T.: 279 826 38





### PAKKSEDDEL/PACKING LIST

OSLO

LAGERP: Avd. BRYNE

11510 DET NORSKE VERITAS INDUSTRY A/S

UERITASUN, 1

\_\_\_\_\_\_

P.B.300 1322 HØVIK Lev. adresse: UERITASUN. 1 HØVIK

Deres best.nr./Your P.O No. Deres ref./Your Ref. Vår ref./Dur Ref. Vårt ordre nr./Our Order No. O.H.BJØRNØY F.H. Martinussen / R 11236 / 01

S./P.: 1

|Merking/Marking

Best. dato/Date of Order

96-05-07

Bet.beting/Payment Terms Lev.beting/Delivery Terms Lev.mate/Delivery Lev.dato/Date of Delivery NETTO PR. 30 DAGER FOB BRYNE SNRST.MULIG 96-05-07 \_\_\_\_\_

Pos./ Vare/ Item Article Antall/ Enh/ Levert/ Rest/ Quantity Unit Delivered Rest

SERTIFIKAT EN 10204/DIN 50049-3.1.B

1 014545AT

323.8\*10.31MM PIPE SP S.40 X52 MOD 12.00 M

Ch.nr: 93226

DELES I TO FOR TRANSPORT.

VERITAS ØNSKER AT RØRET ANK. PÅ EN SLIK MÅTE AT

OPPRINNELIG ORIENTERING MELLOM DE TO DELENE

KAN BESTEMMES.

2 014548AT .

has been received in full.

323.8\*15.88MM PIPE SP X52 MOD

5.00 M

KAPPES I FIX LGD 6M.

CERTIFICATES ENCLOSE

Porto: Kolli: DRØR Uttak : CA	Lev dato :
Etter forfall beregnes 1.0 % rente pr. mnd. I.h.t. panteloven forbeholder vi oss eiendomms inntil kjøpesummen er helt betalt. Aksept ansees ikke som betaling før den er innfridd i	sin helhet.
1.0% pr month is added for late payment. Title to goods belongs to Rolf Lycke AS until pay has been received in full.	yment Mottatt:



## **DET NORSKE VERITAS**

Certificate No.: VER 52995048-06

### **INSPECTION CERTIFICATE OF MATERIALS**

			1	TANK!	certificate		lanaldinati	on Distor					
DNV			1		acc, to IS				•				
Product SI	EAMLES	S LINE	E PIPE, 12						· · · · · · · · · · · · · · · · · · ·	1	otal mass	***	
										(	761.780	M) 60.64	7 Ton.
Manufacturer TI	JBOS D	E ACEI	RO DE ME	EXICO, S	S.A.			***************************************		M	anufacture	er's order i	<b>√o</b> .
	•		**************************************								03830-03		
Purchaser Ri	OLF LYO	CKE A/	S							1	urchaser's 3005	order No.	
Destination/Supple	-												
NORWAY / Ma	nufactu	rer's C	ertificate	N° 9500:	3439								
					(Argent)		( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	(C)					
Material standard	•					1	y addition	•					
API Spec 5L (A	ipni 1, 1	1995), C	Grade X52			A	per Ro	olf Lyci	(e A/S, PC	23005			
				SPECII	FIED ME	CHANIC	AL PRO	OPERT	ES				
		TENSI	LE PROPE	RTIES				Ç	HARPY V-N	отсн ім	PACT PR	OPERTIE	S
Specimen type/ dimensions	Yield R <sub>aH</sub> c	point or R <sub>p0,2</sub>	Tensile str R <sub>m</sub>	ength	Elongation A <sub>s</sub>	Reduction Orientation			1	Width of est piece	Energy, J, min.		min.
·-	N/n	nm²	N/mm	*	%	×	\$	LorT	<b>°</b> C	mm	Sing	e /	\verage
	31	50	490 - 6	20	22			T	-50	10	28		36
Remarks					······································								*
				SPECII	FIED CH	FMICAL	COMP	OSITIO				······································	***************************************
Element	C, %	Mn, 7	6 Si, %	P, %	s, %	Mo, %	Cr, %	T		Ni, %	Cu, %	CA, %	CE, %
Specific value(s)	0.14	1.35	0.40	0.015	0.005	0.080	0.20	0.06	0 0.040	0.20	0.200	0.004	0.41
Remarks V + Nt	+ Ti, O.	07% M	ax., V + N	b, 0.06%	6 Max., (	cu + 6Sr	ı, 0.32%	Max.		1	<u> </u>	1	<u></u>
Marki	ıg:		The materia and are four					pecificati	Norma on. (For test		ee overleal	conditio	n,
√N	,		If applicable	state dra	wing numb	er and ap	proval da	te .		1	>		
The stamping	k planed	***************************************	ſ					Ą	1 4		<u> </u>		
between 5 to	•	- 1	Va	racruz, I	Verico		400	5.10.27	-	1	,		
pipe (	end		₹ 🗗	Place				5. 10.21 Date	_	-/	R. O. TIN	осо	***************************************

it is agreed that some as provided believe Det Norsian Vertica, its subsidiaries, bodies, officers, directors, exceptings and agents that have no lability for any loss, dermage or expense allegadly exceed directly in historiative for interesting their solution or present that it is not considered by their solution or present that it is not considered by the present provided in the control of present that it is not control or information of better vertical. This applies regardless of whether this true, thousage or expenses the attention around anyther solution that their provided in their provided or decisions and/or or information given by or on behalf of Det Norsian Vertica. This expenses the attention of their solutions around or information given by or on behalf of their party who has been added to their and in exchangement of their solutions. There is a subsidiaries or their provided to their solutions or debut, if has Det Montain Vertica to the solution endors a laboration or debut, if has Det Montain Vertica by the vertical or debut, and are expenses the solution of the solution in this soulies shall not be several under the law of any judiciality of the restairing provisions shall not in any way be allected.

						(2.11.7):				* ****	VI	ER 529	5048	-06
						****	PROPER	TIEC						
		TE	NSILE T	FSTS	mircin.	WICAL	PROPER	IIES					······································	
Cast. No.	Test	<del></del>	point	Tenslie si	trenoth	Elong-	Reduction			1	TCH IMP			******
	No.	ReH	or R <sub>p0,2</sub>	R	- 1	ation A <sub>5</sub>	of area Z	Orien- tation	Width of test piece	Test		Energy,	J, min. 	T
93226	01		mm² 5.60	N/mn 513.8		46	<u>*</u>	LorT	mm	*C	1	2	3	1
93226	02	401	1.10	528.5		46	The state of the s	T	10	-50 -50	70 69	73 69	69 75	POPULATION OF THE PROPERTY OF
marks		Mn, %		P, %	SHEMICA S, % 0.004	Mo, %		N V, %	Nb, %	Ni, %	Cu, %	G CA,	% C	Ε,
Cast. No. 93226 93226	C, % 0.139 0.138	1.16 1.14	0.26 0.25	0.007	0.004	0.030 0.029	0.05 0.06	0.034 0.034	0.00	0.06 0.06	0.123 0.121	.002	2 (	
93226 93226	0.139 0.138	1.14	0.25	1		į			1 1	0.06	0.123	.002	2 (	
93226 93226 Produces miless pipe	0.139 0.138	1.14	0.25	1		0.029		0.034	0.00	0.06	0.123	.002	2 (	
93226	0.139 0.138	1.14	0.25	0.007	0.004	Heat Nor	0.06	0.034 (state term) 880 C	0.00	0.06	0.123	.002	2 (	).3(
93226 93226 Produces smiless pipe	0.139 0.138 ct Chemic	1.14	0.25	0.007	0.004	Heat Nor	0.06	0.034 (state term) 880 C	0.00	0.06	0.123	.002	2 (	

Hydrostatic Test Records, Ultrasonic & Electromag, Inspection Records, DNV Marking and Issue of Insp. Certificate. DET NORSKE VERITAS CLASSIFICATION AS , VERITASVEIEN 1, N-1322 HOVIK, NORWAY, TEL. INT: +47 67 57 99 00, TELEFAX: +47 67 57 99 11 Form No.: 38.01aSI Issue: September 93 Page 2 of 2

(	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
,	

MIII TEST CEDITEICATE	NFIRMATION THE INSPECTOR OF	WD DACAE! TTMOOD	NOMINAL WEIGHT STAFF CO. S. 7 - 24/10/90	X 0.406 INCH 53 52 18/FT NE2		26.20 / 45.90 FT *** SUKFACE HYDROSTATIC TEST P.	C A L P R O P E R T I E S A N D T E S T HICKNESS IMPACT CHARPY TRANSVERSE SHEAR HARDNES TENSILE SAMPLE I N D I V I D U A L AVERAGE SHEAR HPC (H	28.000 35.000	38.10 10.80 /0.000 /3.000 69.000 /1.000 100 80.11 HRB 38.00 11.00 69.000 69.000 75.000 71.000 100 82.00 HRB	100% ULTRABORIC INSPECTION 8 A F I S F A C T O R I	
				12 3/4 INCH		APRIL 1, 1995.	LONGITUDINAL STRENGTH *ELONGATION FL YIELD TENSILE IN 2 INCH NW/MM2 NW/MM2	490.00 ZZ.0 620.00	513.88 46 528.59 46		
	PURCHASER	CKE A.S.	TYPE OF PIPE	SEAMLESS	SPECIFICATION OR STANDARD	APRI	ONGITUDINAL STRE YIELD TEN NW/MM2 N	360.00 4	375.60 5 401.10 55		
		ROLF LYCKE A.S.	TYPE	LINE PIPE	SPECIFICATION	API 5L	HEAT L NUMBER	MAXIMUM	93226 93226	ork a manufacture of the control of	***************************************

100 % MAGNETIC PARTÍCLE INSPECTION SATISFACTORY

on Pipe ends

. MPI

. VPI

INSPECTION SATISFACTORY: SR-4 - EMI

THISISTO CERTIFY THAT THE PRODUCTS DESCRIBED HEREINWERE MANUFACTURED, SAMPLED, TESTED, AND FOR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS. OUALITY CERTIFICATION NAME AND SIGNATURE

SARA GARCIA PAJARES

1 유

ORIGINAL PAGE

57 цематия

QUANTITY

KW 433 E CARP MEN-VER VFRACAUL, VER APOG POSYAL 402 TELEX 18443 FAX(21) 81-02-88

PLUS LETRA

\*\*\* VARNISHED

i		
1		
1	-	

			····~										ì		
	Z NO.	24/10/05	NOMINAL WEIGHT STEEL GRADE FINS FINS	ODKA! PC	2	2810 PSI 5 SEC				CLTRASONIC INSPECTION SATISFACTORY	SR4-5%notch	MAGNETIC PARTICLE INSPECTION SATISFACTORY	on Pipe ends	The second secon	~
	ECTOR /	M COO		£23	Ø.		N O	0		OLTER S A	SR4	MAGNE	00		
	INSPECTOR	MR. RAFAEL TINOCO	VAL WEIGH	B/FI	2	*	E V A L U A T I O N LEVEL INCLUSIONS	ပ		100%		100%		11	
CERTIFICATE		£	IIWON ,	53.52 LB/FT	ENGTH OF	.90 FF 06:	E V A L	<b>&amp;</b>			į	1	\	- malle	
	1			INCH	SPECIFIC LENGTH OR R	26.20 / 45.90 FT	J I C	¥						KILLER	YYY
MILL	CONFIRMATION	003830 / 03	SNC	0.406 IN		<u></u>	GRAPHIC	**************************************						1	7/
	SALES	003	DIMENSIONS	×			I A L L O EUCTURE	***************************************							
				12 3/4 INCH		995.	MICRO-STRUCTURE	**************************************						•	
					a	APRIL 1, 1995.									·
	PURCHASER	· ·	3.	SEAMLESS	STANDAR	*	, <b>2</b> ,,				7		•		
	PUR	ROLF LYCKE A.S.	TYPE OF PIPE	ᇤ	TION OR		GRAIN	20	10						
}		ROLF	1	LINE PIPE	SPECIFICATION OR STANDARD	API 5L	HEAT NUMBER	MINIMUM	93226 93226					** VARNISHED	
	1				S				<u> </u>					土	

ENG SARA GARCIA PAJARES SAMPLED, TESTED, AND FOR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION AME AND SIGNATURE REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS.

2 OF

ORIGINAL PAGE

57 цематив

OUANTITY

KM 433 CARR MEX-VER VERACRUZ VER AFDO POSTAL 407 TRL(28) 9-11 00 TRLK 15843 FAX(28) 81-02-EE

PLUS ULTRA

Í		-
1		
•	-	

		<del>.,,</del>								<i></i>
	No.	05.0			HYDROSTATIC TEST P.	5 SEC	and the first control of the f			
	DATE	24/10/95		IORMAL BEVEL	MDROST	2810 PSI		٠ س	0.41	0.36
	<b>Q</b>	77	1	<u>S</u>		8		AS CA C.E.	0.0040 0.41	0.0022 0.0022
	<b>7</b>	116	NOMINAL WEIGHT STEEL GRADE		ACE.	The state of the s		AS*		93226 0.139 1.16 0.26 0.007 0.004 0.030 0.05 0.034 0.000 0.06 0.123 0.006 0.020 0.000 0.000 0.004 0.0022 0.36 93226 0.138 1.14 0.25 0.007 0.004 0.029 0.06 0.000 0.000 0.06 0.121 0.006 0.017 0.000 0.0000 0.004 0.0022 0.36
1	INSPECTOR	9	ISTE	(52	SURFACE			∞*		0.000 0.000
	NSPEC	ONIL	(FIGHT		ルタス ・2 ス ・3 イ カチ ルチ	***	SIS	¥. ∀*		0.000
<u> </u>		MR. RAFAEL TINOCO	IINALV	53.52 LB/FT	OR R.		ANALYSIS	4*		0.020
MILL TEST CERTIFICATE		₹	NON	53.52	SPECIFIC LENGTH OR R.	90 FI	AN	Σ×	0.015	0.006
CFB	Z			<b>-</b>	JEIC LE	26.20 / 45.90 FT	A L	3×	0.200	0.123
TEST	SALES CONFIRMATION	က		INCH	SPEC	26.20	CHEMICAL	Z*	0 0.20	0.00
	ONFIR	003830 / 03	ONS	X 0.406 INCH			CHE	<b>2</b> *	0 0.04	4 0.00
2	ALES (	0038	OSN	×			<u>,                                    </u>	>*	0.06	5 0.03
	တ		DIMENS	INCH			PRODUCT	ర∺	0 0.20	0.06
						5.	P R O	₽*	90.09	0.03
				12 3/4		APRIL 1, 1995.		U) de	0.00	0.00
	ं ते कर्ते			SS	RD.	APRIL		<b>₽</b> *	0.015	0.007
	PURCHASER			SEAMLESS	TANDA	_		IS. New	0.40	0.25
	PURC	E A.S.	F PIP	σ,	OR S			٤×	0 1.35	9 1.16 8 1.14
	-	ROLF LYCKE A.S.	TYPE OF PIPE	JJE	ATION	5		<b>∪ ≯</b> €	i 0.14	0.13
>		ROLF		LINE PIPE	SPECIFICATION OR STANDARD	API 5L	,	HEAT	MAXIMUM 0.140 1.35 0.40 0.015 0.005 0.080 0.20 0.060 0.040 0.20 0.200 0.015	93226 93226

100% ULTRASOMIC INSPECTION SATISFACTORY 1

SR4-5%notch

100%

MAGNETIC PARTICLE INSPECTION SATISFACTORY

on Pipe ends

\*\*\* VARNISHED

QUANTITY

57 ценатив

3 OF ORIGINAL PAGE

DUALITY CERTIFICATION NAME AND SIGNATURE SARA GARCIA PAJARES

THIS IS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREINWERE MANUFACTURED. SAMPLED, TESTED, AND FOR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEET STHE REQUIREMENTS IN ALL RESPECTS.



PURCHASER	MILL TEST CERTIFICATE INSPECTOR CAS DATE NO NO TO THE TOTAL OF THE TOT	003830 / 03 MR RAFAFI TIMOTO 24,19,05		INCH X 0.406 INCH 53.52 LB/FT X52 NORMAI RE-	SURFACE	. 26.20 / 45.90 FT ***		MO CR V NB NI CU SN AL TI B AS CA N C.E.	MAXIMUN 0.140 1.35 0.40 0.015 0.005 0.080 0.20 0.060 0.040 0.20 0.200 0.015	93226 0.120 1.16 0.26 0.007 0.003 0.029 0.06 0.037 0.000 0.06 0.120 0.007 0.022 0.000 n mm n mm n mm n mm n mm
EES 12 3/4  LESS 12 3/4  DARD  APRIL 1, 1995.  K  X  X  X  X  X  X  X  X  X  X  X  X	MILL SALES CONFIRM	003830 / 03	DIMENSIONS			8	-	%×.	0.20 0.060 0.040	729 0.06 0.037 0.000
	FR				DARD	APRIL 1, 1995.		σ.× Ω.*κ	40 0.015 0.005 0.	26 0.007 0.003 0.

100%

# ULTRASONIC INSPECTION SATISFACTORY

SR4-5%notch

THIS CERTIFICATE CANCELS AND SUBSTITUTES THE ONE SENT ON 03/10/95 WITH No. 95003439.

100%

MAGNETIC PARTICLE INSPECTION SATISFACTORY

1.B /ASTM A106 B 94/ASTM A333 GRADE 6 94. HARDNESS ACCORDING TO 4. TEMPERATURE - 90 %. HEAT TREATMENT: NORMALIZED (TEMPERATURE = NOTES: CERTIFICATE ACC.
NACE MR-01-75 199
880 C). GRAIN SI
\*\*\* VARNISHED

SARA GARCIA PAJARES

ORIGINAL PAGE

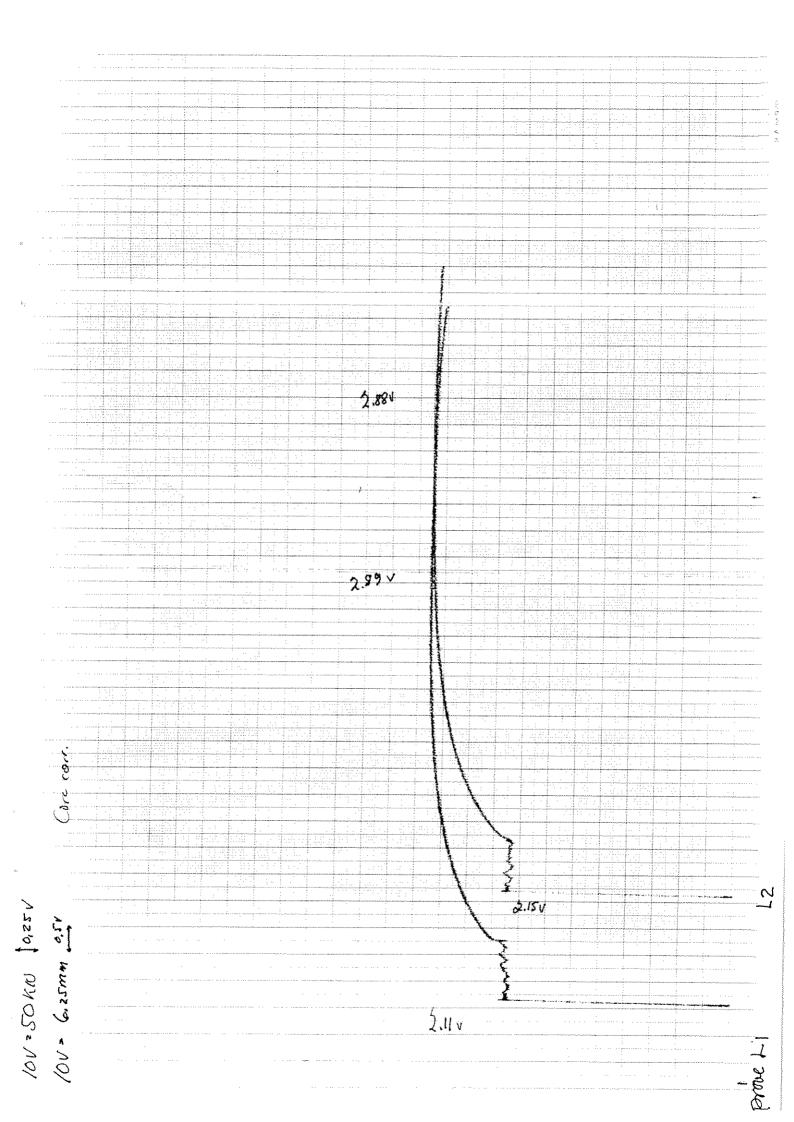
DUANTITY

TLUS ULTRA

on Pipe ends

THISIS TO CERTIFY THAT THE PRODUCTS DESCRIBED HEREIN WERE MANUFACTURED. SAMPLED, TESTED, AND JOR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE REQUIREMENTS IN ALL RESPECTS. DUALITY CERTIFICATION NAME AND SIGNATURE

250 100 49 Form No. 20.200a Project No. 150/7 40-30 Fortuniste A. Kontroksjon 41.5 38,3 2.81 75,8 41.3 37.7 285.7 Date: 24/1-92 Sign: CH For 3 ror Circ. corrosion 3 37.0 2.81 75,5 35,7 2.81 75.5 *``*} 46.7 N/mm. 11.52 | 511 14.80 513 5/3 Flykegrunde Strekkfasthet 115 24.41 14.30 5 DATA SHEET 10.55 373 28.09 10.75 383 KN Nmm 375 376 DU 750 764.01 27.36 10.45 27.90 ひ くくら 28.27 DET NORSKE VERITAS 5,96 5.98 5,96 Laboratory Department Shuth 21.41



# ROBBINGKE

## a Milato Ilor

Jitegi, 14-89 gili 227 g sz. 20 t Telléjak 22 87 03 29

215	\$4 p	
250	4.0	

				PAKKSEDDEL.	PACKING LIST	Fan Lead	OHT NORSKE VEN CENTERED COMP
DE. VEI	510	1	OSLO INDUSTRY	' A/S	Lev. adresse 3 STK FREDRI INDUSTRIVN. FREDRIKSTAD	KSTAD MONTERI 5-11	specimen.  11 and 12  NG AS
Deres b 6750	est.nr./Your		Deres ref./You O.H.BJØRN		Vár ref./Our Ref. Thorbjørn Hoel	Vart ordra  / BMR 16936	
	Marking < MRK:J.	SÆTER				Best, dato	∕Date of Order -13
Bet.bet NETT(	ing/Payment T D PR. 30	DAGER	Lev.beting/De FOB OSLO	livary Terms	Lau.máta/Delivary	Lev.dato/Do 96-12-	sta of Delivery -13
Pr /	Uara/ Articla	and the made and they after the time.	anie dans inim dans meie dien Adle beier dan	golff sein deir der der sem gest son gust aufb "	Antall/ Enh/ Quantity Unit		Rest/ Rest
2	014545A 323.8-1 Ch.nri 9	0.31MM P 3226 3 * 1 ME 0.31MM P 3226	TER	40 X52 MOD	3.00 ft Lok.: X-1-8. 0.50 M Lok.: X-1-8.	<u>0,50</u> 79/73 kg	
	) \$ F	REFERENCE TO SERVICE T	R SENDES IL F.M. MI IL F.M. MI _ DNU MERI _ FREDRIKS SERT. TIL	VERITAS, HEERKES "J. 8 KES "O. BJE STAD FORUTE BEGGE.	SETER" Brnøy"	14/19-8	l ,



### **DET NORSKE VERITAS**

Certificate No.: VER 52995045-06

### INSPECTION CERTIFICATE OF MATERIALS

				] DNV	certificate a	oc. to Cita	ssifica	tion Rul					
DIMA					20C, to 180								
Product ge/	AMLES:	B LINE	PIPE, 12-	3/4 inx	0.406 in (3	323.9 m:	mx10	), <b>3</b> 0 mi	m)		Total frame (761.780	M) 60.64	t7 Ton.
Manufacturer TU	BOS DE	ACER	O DE ME	aco. s	J.A.						Menufacture	r's order	No.
											003630-0		
Purchager RO	LF LYC	KE A/S	3								Purchaseri 23005	i order Nó	·
Destination/Supplies NORWAY / Main	•			<b>P 95</b> 00	3439								
		ş.,	My di	hO.								ia d	
Meterial standard s	-	***					·		puinements	50 500	\F		
APi Spec SL (A	pril 1, 1	995), C	Brade X5Z			<b>A8</b>	per	Mart L	/GKO PV6,	, PO 2300	<b>19</b>		
			· · · · · · · · · · · · · · · · · · ·	SPECI	FIED ME	CHANIC	AL P	ROPE	RTIES			······	***************************************
		TENSI	E PROPER	TIES					CHARPY	V-NOTCH	IMPACT P	OPERTI	EŞ
Specimen type/ dimensions	Yield R <sub>ex</sub> o	point r R <sub>pó.2</sub>	Tensile str R <sub>in</sub>	ingth	Elongation A <sub>a</sub>	Redux of as	<b>88</b>	Orlen- tation	Tost temp.	Width test pla	**	Energy, J	, min.
	No	en²	N/mm	. !	*	N		Ler	•¢	m	Sin	<b>*</b>	Averege
	30	<b>SO</b>	490 - 8	20	22			τ	-50	10	2	•	36
Remarks	1				•	. ! _		<u> </u>	<u> </u>			<u> </u>	
	• • • • • • • • • • • • • • • • • • • •	<b>-</b> · ·	,	SPEC	IFIED CH	EMICAL	COI	APOSI	ΠΟN				
Element	C, %	Mn, 5	6 Si. %	P, %	8, %	Mo, %	Cr.	% V	, % Nb	, % Ní,	% Cu, %	CA, 9	CE, %
Specific value(s)	0.14	1.35	0.40	0.015	0.005	0.080	0,:	20 O	.060 0.1	040 0.3	0.200	0.004	0,41
Remarks V+NE	+ TI, O.	07% M	iex., V + N	b, 0.06	% Max., (	:u + 68r	i, 0.3	2% Ma	x.	- ' -			
Martin	d:	_			sted and ine	,		e specif		rmailzed r test recui	is, see overis	sondi)	ion,
N	/		If applicable	white dr	ewing numb	er and ap	prove	ciete			>	·	
								4	13:6	Z.			
The stamping between 8 to	•	1					_			一个			
pipe (			Ve	racruz, Piac	Mexico •		1	995.10 Dale	).27		R.O.TI	_	
It is agreed that serve as pri- frest installs or negligenes, poverting bedens of service author or resided on deciding given by as an behalf of than installed in the province than the province that any provintion the overall that any provintion	braach of was unsepting office studie or infos u and in acros ." Yi the stant untilitator april	mety, or may nee of Dat No realizate green aparense malle I Dat Hornes In, Konidant.	ather sal, certania projet Vertige, This by or set install of ore at team, abrough Vertige or by sub- maride or by sub-	e or over by opplies sope the Morses or oppores of pres rey les, "Under	trurre, leakuling gre cilings of subgitage variose. "Historicas provinci in insi dene i be inne Egipu at a la nine(Historica)	oan hagilgarea Ito luss, sterne I, if they person to trub rugbyn Lusardarea wit aladonaraw shu	er wilke i pe ar wa week lin rest, april i line seat dene inel	njetornkej i grave inst gj : Survices al ssian ar ggja (sha jibina, vicani ar jugi	y any mich period festell anysine will I Del Norder Vall of, hop (but him the Etheunt of so industrial and how	on with the energy Privations Class No. Hast or his and old your Vertical with properties of an area is personnelly assur-	r majorine plingwily Gon at proce hogiga when Vertes has a se majorine service wy by way of manage under the encomment	severed street, nee as with m street or a tru y decision succession to our meastern to our state assessed	county the 'ma i party who 'ma is at information it prover a sur- e hillent of the

DET NORSKE VERITAS CLASSIFICATION AS , VERITASVEIEN 1, N-1922 HØVIK, NORWAY, TBL. INT: +47 67 57 89 00, TBLBFAX; +47 67 57 99 11 Form No.: 36.01eSI lesue: September 93

Certificate No.; VER 57995045-06

		TENSILE 1	ESTS				CHARP	Y V-NO1	CHIM	PACT T	EBT3	
Cast, No.	Test No.	Yield point Red of Rpt.3	1	Elong- ation A	Reduction of area	Orien- tation	Width of test place	Test temp			, J, min.	<u> </u>
20220		Mineri*	Nma*	<b>^</b> *	*	LOT	mm	<b>-c</b> ∫	1	2	3	Av
93226 93226	01 02	375.60 401.10	513.88 528.59	48 46		T	10 10	-60 -60	70 69	73 69	69 75	7.
			!			***************************************						
		•			İ							
							1		:			
						i	*		ļ	: !		
						!	***************************************					
				;	o margan and an and an			. !	]		!	
				1	**	1		1				
i	İ		1	- 1	i	1		,	į	-	- 1	

	····			Ç	HEMIC/	L COMP	OBITIO	N					
Cest. No.	C. %	Mn, %	31, %	P, %	8, %	Mo, %	Cr. %	V, %	Nb, %	NI, %	Cu, %	CA, %	CE. Y
9322 <b>6</b> 93226	0.139	1.16 1.14	0.26 0.25	0.007	0.004 0.004	0.030 0.029	0.05 0.08	0.034 0.034	0.00 0.00	0.06 0.08	0.123 0.121	.0022 .0022	0.36
	To company a service of the company								<b>83</b> 5	A	,		

Remarks Product Chemical Analysis

Process Seamless pipe

Heat freelment (state temperatures)

Normalized: 880 C

Non-destructive testing Ultrasonic SR4 - 5% Notch & MPI

Type and extent of inspection

Review of Chemical Analysis and Data Sheets, Mechanical Properties, Review of Dimensional Control Sheets and Hydrostatic Test Records, Ultrasonic & Electromag. Inspection Records, DNV Marking and Issue of insp. Certificate.

DET NORSKE VERITAS CLASSIFICATION AS , VERITASVERN 1, N-1322 HEVIK, NORWAY, TEL INT: +47 67 57 90 ID, TELEFAX: +47 67 57 90 11 Form No.: 38,01mSi Imaue; September 93 Page 2 of 2 Ordrenr: 169369 PONO: 6750 ITEMNO: 1

10/11/12 HYDROSTATIC TEST R THIS ID CERTEY HAT HE PRODUCTS DESCRIBED HERPWINERE MAMERICHTS G. SAMPLED, TESTED, MID FOR INCRECIED OF ACCORDANCE WHILE SPECIFICATION REFERENCED AND MÉETS THE RECUIREMENTS IN ALL RESPECTS. 95003439 5 SEC 25.00 HEB HARDNE SS 100% OLTHABORIC INSPECTION 100 % MAGNETIC PARTICLE INSPECTION 圣 23.00 CRIMIL BEYE SATISFACTORY 2810 PSI SR4-5%notsh on Pipe ends SEA REA MEXICO, S.A. 88 77.88 71.88 35.000 SURFACE 55.000 75.000 INSPECTOR NOMINAL WENGHT 69.69 28.000 MR. RAFAEL 53.52 LB/FI SPECIFIC LENGTH OR R DE ACERO DE 200.69 69.60 CPRITEICATE 26.20 / 45.90 FT HKIT LY CERTIFICATION NAME AND FLATTENING NIDE THICKNESS
TENSILE SAMPLE
NN. M. 88 8:1 SALES CONFIRMATION 38.13 3 X 0.406 DIMENSIONS 2 RECHAIN RELONGATION IN 2 INCH TUBOS 三 **2**2.0 68 ORIGINAL Page · YPI 12 3/4 APRIL 1, 1995, 430.08 620.08 LONGITUDINAL STRENGTH YIELD TENSILE NA/PRE NA/PRE 513.88 528.59 3 SPECIFICATION OR STANDAND SEAM ESS INSPECTION SATISFACTORY: SR.4 PURCHÁSER TYPE OF PIPE CIMETET ROLF LYCKE A.S. LINE PIPE \* VARNISHED MAXIMA API NEW TEAT 43226 93226

4

200/100 M

+++ R.L. LAGER OSLO

ROLF LYCKE A.S

29869T TS 472885

TT:80

\$6.77.02

10/11/12

		23		STP	5 SEC			***************************************	-			CTIMED
	DATE	24/10/95 95003439 EADS	KORWA, BEVEL	HYDROSTATIC TEST P	0 PSI			INSPECTION ACTORI	otch	INSPECTION TORY	spu	STREET HE REINWESTE, MANUEL CORDANCE WITH THE SPEEC IN ALL RESPECTS.
MIL TEST CHRITICALE		STEER GRADE!	2	× X	HARE	0	Providence and in the common space of the comm	ULTRABONIC IN	SR4-5%noteh	MAGNETIC PARTICLE INSPECTION SATISFACTORY	on Pipe ends	THIS IS TO CERTIFY THAT THE PRODUCTS DESCRIPCIONE REINWERE MANAFACTISFED. SAMPLED, TESTED, AND FOR HISTEGTED BA ACCORDANCE WITH THE SPECIFICATION REPERENCEDAND MEETS THERE OA REMEATS WALL RESPECTS.
に iviに入 Aff	INSPECTOR	I NOMINAL WEIGHT			E V A L U A T 1 0 N LEYEL INCLUSIONS	ပ		100% 001	0,	100% MA		بتبت ا
TEST CERTIFICATE				SPECIFIC LENGTH OR R.	PHICEVA	A 88		i	i	\		ENG SARA GARCIA PAJMES  OMMITY CE ETTE CATION NAME AND SHON SHOWE
	SALES CONFIRMATION	DINENSIONS			OGRAP			-			•	4
		MIG.	12 3/4 INCH	<b>.</b>	H E T H A L L							ORIGINAL 2 OF
•	PURCHASER A S			STANDARD	1			(*				амитт 57 сияти
The same of the sa	ROLF LYCKE A	TYPE OF PIPE	LINE PIPE	SPECIFICATION OR STANDARD	HEAT GRAIN NUMBER SIZE	MINIHOM B MAXIMUN	93226 10				(Abbit Curb	# # # # # # # # # # # # # # # # # # #

	<b>3</b>	95003439	FZ 0x		HYCHOSTATIC TEST P	5 SEC	A MARKET CO. A. C.				1	NO.	***	NO.		THISHETO CERTET THAT THE PRODUCTS DESCAIBED HEREIN WERE MANAFACTURED, SAMPLEG, TESTED, WID TOR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION REFERENCED AND MEETS THE RECURRINGING MAIL MESPECTS.
	PATE	24/10/95	E	ORIM, BEYEL	HYTHOSTA	2810 PSI	A AND STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET,	C.E.	0.41	0.36		ACTORY	SR4-5%notch	MAGNETIC PARTICLE INSPECTION SATISFACTORY	sp	THISHE TO CE ATA'Y TOAT THE PRODUCTS GESCUIDED HEREIN WER SANTLEO, TESTED, AND FOR HISPECTED IN ACCORDANCE WITH T REFERENCED AND MEETS THE REGUIR DIGHTS IN ALL BESPECTS.
4		77	B	8		8	<b>*</b>	5	0.0040 0.41	0.0022	i		% E%	MTCL. FAC	9	UCTS DESC CTED IN AC JARESKEITS
DE ACERO DE MEXICO, S.A.		76	LGRADE		**			Z*		9.0		SATIBE SATIBE	<u>ا</u> ا	T IS	ipe	THE PROD JOR HISPE STHE REG
$\frac{9}{2}$	STANT.	*	(5+6	8	SURFACE		-	<b>20.4</b> +		90 90 90 90 90	;	₹ <b>4</b> <b>1</b> 00	<b>SR4</b>	GNET SA	on Pipe ends	ATEC, PRO
X W	INSPECTOR	-	1. 1	1			S	<b>=</b> *		0.000 0.0000 0.004 0.0022 0.36 0.000 0.0000 0.004 0.0022 0.36	****	200 % DOI	0,		ō	HALEO, TE
2	Ä	FAEL	AL WE	I/FT	α,	***	. Y S ]	₹*		020 0. 017 0.		5 %		100%	- ///	
D E		MR. RAFAEL	THOMINAL WEIGHT	53.52 LB/FI	THOS	Ħ	ANALY	Br	015	000 000 0.0				100		MAE'S
0	CERTIFICATE		* · ·	<u>ස</u>	CLENC	45.99	ŀ	3∗	200 0.	123 0	1					IA PA
圧め	SI			=	SPECIFICLENGINGRA	26.20 / 45.90 FT	CHEMICAL	Z×	0.060 0.040 0.20 0.200 0.015	0.034 0.000 0.06 0.123 0.006 0.020 0.034 0.000 0.06 0.121 0.006 0.017						SARA GARCIA PAJARES STYCERI IFICATION NAME AND SIGNATURE
AC	ALES CONFIRMATION	8		jumi)	3	92	E	型,,	040	0000						A SE
Ш	NOS S	003830	NSIONS	X 0.406			1	>*	060 0.	034 O.						ENG.
	SALE	8	DIMENS				UCT	ర్*		0.05 U. 0.06 O.						5
TUBOS		_	מ	E		;	PRODUC	₽**	0.005 0.080 0.20	0.030 0						
	***************************************			3/4		1995.	٩	v) ec	005 0.	0.004 0.						PAGE
<b></b>	4			12		11. 1,	i	C.M	0.015 0.	007 0.		: , 4360	r			57 цисти
	SER	the second	19	SEAMLESS	CARD.	APRIL		IS*	.40 0.	0.26 0.007						5.
	PURCHASER	A.S.	à be	SE SE	OR STANDARD			₹~	1.35 0	1.16 0						QUANTIL
	đ	XOC	TYPE OF PIP	<u>u</u>	O SO			O#	0.140 1.35 0.40	0.139						and the second
	3	ROLF LYCKE	2	LINE PIPE	4	API SE		AT SEE	AXIMM	93226 93226						
~					SPEC			# <b>E</b>	Ž	RR						A VARMIS

10/11/12

DE ACERO DE MEXICO, S.A.	CRITEICATE WSPECTOR COMP. DATE NO.		TELL CHARDE	OR B. SURFACE MYDROSTATIC	Y S I S	N. W.	00 0.015 0.0040 0.0090 0.41	0.037 0.000 0.06 0.120 0.007 0.022 0.000 0.0000 0.004 0.0020 0.0058 0.35	100% DETERMENT INSPECTION SATISFACTION	SR4-5%notch	100% BATISFACTION SATISFACTION SATISFACTION	.B /ASTH A106 B 99/ASTH A333 GRADE 6 94. HARDNESS ACCORDING TO TEMPERATURE -90 2. HEAT TREATMENT: NORMALIZED (TEMPERATURE = INSPECTION CONCANY: D.N.Y. ON PIPE ends	A PAJARES THSISTOCENTEY HALTHE PRODUCTS DESCRIBED HEN ENTHERS BANK HACKNED, SANCE OF TESTED, AND FOR INSPECIED IN ACCORDANCE WITH THE SPECIFICATION NAME AND SIGNATURE.
	NILL TEST CE	003830 / 03	INCH X 0.406 INCH		TCHEMICAL	N N N N N N N N N N N N N N N N N N N	0 0.20 0.060 0.040 0.20 0.200 0.015	,			100%	I. C/DIN 50049 3.1. IZE 10 x 7 50 M. IMISA REF. 281.	4 OF 4 ENG. SARA GARCIA PAÍARES
TUBOS	PURCHASER	ROLF LYCKE A.S.	12 3/4	SPECIFICATION OR STANDARD API 5L API 1. 1995.	V A H	HEAT C IN SI P S HO NUMBER X X X X X X X X X X X X X X X X X X X	MAXIMUM 0.140 1.35 0.40 0.015 0.005 0.080 0.20	93226		THIS CERTIFICATE CANCES AND SINGIFFICE		MOTES: CERTIFICATE ACC. TO "EN 10204/DIN 50049 3 NACE NR-01-75 1995. INPACT TEST:SPECINEN S. B80 C). GRAIN SIZE ACC. TO ASTN E112-85. *** VARNISHED	FILE OF CONTROL OF CON

## **APPENDIX**

LISTING OF TEST RESULTS

Printout of the Excel spreadsheet results for the tests are given. The content of each column are described in the table.

Column	Test no.1	Test nos. 2-4	Test nos. 5-12
A	time	time	time
В	internal press (bar)	internal press (bar)	internal press (bar)
С		actuator force (kN)	jack force (kN)
D		actuator disp. (mm)	jack disp. (mm)
Е		angle (deg) for test 3 and 4	
F	test time (sec)	test time (sec)	test time (sec)
G		bending moment (kNm)	(jack force/10)
H	σ axial, int. press	σ axial, int. press	σ axial, int. press
I		σ axial, moment	σ axial, jack force
J	σ axial, total	σ axial, total	σ <sub>axial, total</sub>
K	σ <sub>hoop</sub>	σ <sub>hoop</sub>	σ <sub>hoop</sub>
L	•	-	
M	strain gauge 1	strain gauge 1	strain gauge !
N	strain gauge 1	strain gauge 1	strain gauge 1
O	strain gauge 2	strain gauge 2	strain gauge 2
P	etc to no. of gauges	etc to no. of gauges	etc to no. of gauges

Column A-E and M and the following letters contains measured values.

Column F-L contains calculated values

All stresses ( $\sigma$ ) are in MPa, and strain in microstrain  $\mu$ s (10<sup>-6</sup>). Examples; 2500  $\mu$ s = 0.25% strain, 85000  $\mu$ s = 8.5% strain

## Calculation of:

 $\sigma_{\text{axial, int. press}} = \text{internal pressure * (Area}_{\text{inner}} / \text{Area}_{\text{pipe}})$ 

 $\sigma_{\text{axial, moment}} = \text{bending moment} / W_{\text{elastic}}$ 

 $\sigma_{axial, jack force} = axial force / Area_{pipe}$ 

 $\sigma_{axial, total}$  = sum of the above axial stresses

 $\sigma_{\text{hoop}}$  = internal pressure \* (Di / 2\*t)

where the following values are used for the cross section;

• Area pipe =  $10437 \text{ mm}^2$   $(D_o^2 - D_i^2) * \pi/4$ 

• Area  $_{inner}$  = 72012 mm<sup>2</sup>  $(D_i^2)*\pi/4$ 

• Moment of Inertia (I) =  $1.28*10^8 \text{mm}^4$   $(D_0^4 - D_1^4)*\pi/64$ 

• Section modulus W <sub>elastic</sub> =  $791854 \text{ mm}^3$  I / (D<sub>o</sub>/2)

 $D_{o}$ ; Outer Diameter = 324 mm

 $D_i$ ; Inner Diameter = 302.8 mm

( wall thickness t = 10.6 mm)

The calculations are based on the undeformed cross-section.

- 000 -

Г		1 68 8 2	382 453 578	72% 72% 78%	842 842	797	928	944	2 8	955	984	124	858	2	3.5	8 8	43	2 5	Ci.	22	92	3.55 5.05 5.05 5.05 5.05 5.05 5.05 5.05	27.7	25.5
	thoop																							
	Gauge 10 lang.	4 6 6 5	47 103 133	152 198	237	357	800	2004 8034 8035	503	533	568	609	654	695	714	731	727	736	745	730	746	760	740	753
	_	97 513 515	1201 1427 1638 1829	3747 3889 3044	7252 7096 7096	9827	7374	9851	988	f732 f732	9470 9030	3220 3860	20		50	00	0	<u> </u>	0	00		00	• **	¢ ¢
	thoop										,					os um		<b>.</b>	m	m e.	-	en er	. 10	
	රිෂයසුණ 9 මාල	· ** ** ***	242 270 270	* * *	\$ <del>4</del> 5	4 4	888	4 56 5	18 E	· 100 12	-36	45.55	7.7	104	-101	001	-100	\$1 65 \$1 65	807	200	, 90 g	97.6	6	8 6 8 6
		45 45 45 45 45 45 45 45 45 45 45 45 45 4	1049 1243 1424 1588	1670 1702 4316	0516 5152 2625	9347	6773	6733	1780	1156	3140	6400 1930	00	00	00	¢ ¢	٥	9 0	o e	30	. a .	00	c	ငင
	dop <sub>ii</sub>										_			± 0	101	e es	g s	0.35	· 12:1	சுழ	· ·	· ·	4	9 V)
	Gauge និ Kng	- 60 47	168 223 257 257	888	4 % 8	9.5	ş ş ş	50.00	25.5	138	-149	-163	1897	180	7.7	7.69	25.9	9 69	263	2.76	-192	18. L	-180	168
		.2 524 524	1219 1446 1689 1689	4194 8510 18053	24158 28512 39789	19368	22460 52460 53840	72789	52224	9270	50283	50155	50139 50103	50068	92009	08661	9948	19921	19901	9800	89768	9/48	0296	19664 19599
	7 Peop		178 212 243 273																					
	Gauge 7 long	-	+ 0 0 0	en verubi	rv i	úú.	ያ 49 <b>1</b> 9	* * *	£ 5	00	E. C.	5.5	55	- e-		¥ 52	φ:	2 2	₩.	5 55	£.	25	200	13. 10.
	<u> </u>	100 100 524 1935	1224 1455 1670 1865	3835 6258 15857	20183 24471 32653	14809	14839	14805	1475B	14700	14648	14598	14582	14542	14517	14495	14481	14461	14448	14382	14384	14305	14330	14309
	5 hoop		270 270 270														134			N 60				8 5
	Gauge 5 long.																. ,	•		<b>y</b>				
	p.	88 451 905	1076 1285 1483 1663	1914 2892 11101	18053 21198 27510	33906	43287	21867	20962	20605	20303	20323	20287	20134	20022	19936	19895	19828	19791	19671	19655	19629 19629	18616	19500
	£ though	0 14 78 163	181 215 279	2 2 2 7 :	4 62 52 27 8 27 8	737	\$ 50 20 20 20 20 20 20 20 20 20 20 20 20 20	8.4	57 53	က်ဆိ	-91	4 43	128	\$ 8	6.00	÷ 9	44.6	3 5	on c	3 25	80 8	စ္က ကို	S.,	4 5
	Gauge S long																							
	уч	85. 449 719	1096 1315 1524 1712	1979	18702 22531 29962	35540	49400	57903 62710	73100	80631	53451 52964	52266 52106	52025 51888	51739	51485	51326	\$1203	51059	50970	50554	50516	50304	50230	50175 50072
		t \$ 7 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4	166 136 224 249	290 323 467	333 383 202	1.58 1.18	223	354	542	368	163 144	135	124	20 24	i F, G	 	34.	şş	op z	, Q	8 5	5 <del>1.</del>	<u>4</u> 0	¢3 }~
	Gauge 4 long																							
	dooq	79 79 82	978 1169 1349 1512	2009	20873 20873 27822	34073	47340	48354	61939	74961	78336 86604	88657 92180	100480 102720	67402	61203	59382	58721	57511	57071	55752	55482	54665	54396	53816
	m	20 83 160	188 224 257 288	338 405 447	543 543	215	385	421	500	526	543	533 518	4 2 4	795	323	629	660	413	472	328	302	920	500	762 041
	Gauge																Ċ			. ,				
	увор	. 9. 4. 08	1069 1277 1476 1655	1907	2076/	33437	43256	51396	66578	74112	56474	5470	53487	51191	50815	50018	49738	49429	49389	49.196	49194	49175	49139	49154
		- 4 52 8	215 215 250 280	320	5599 668	652	582	372	1003	275	533	638	747	902	854	210	017	063	093	100	074	062	630	S 55
	microstrain Gauge 2 Iong																							
	gauges in hoop	8 4 8	953 953 1052	757 158 157 157	1943	3213	3985	4628 5004	5845	6924	7022	5752	5039	4699	4649	4631	46203	4611	4606	4572	45698	4551	4543	4530
	rein gas †	- 5 5 5	79 T T T T T T T T T T T T T T T T T T T	5 2 2 5 5 2 2 5 5 2 5 5	1446 613	320 278 165	143	8 2	156	102	725	579	8 2	117	137	132	4 4	153	15,	£	8 4	12	139	£ <del>‡</del>
	All strein Gauge 1 king.																							
	Axiał (MPałtoop (MPa) Axiał hoop	03 77 388 767	124.3 138.6 138.6	155.0 155.0	215.4	242.4 240.8 255.4	254 1	263.0	277.7	281.9	296.8	302.7	302 1	315.2	316 1	321.2	375.5	324 1	324.8	327.8	322.9	320.9	319.9	322.9
	Pattoop																						w r	- 0
	Axial (N Axial	0 0 2 2	43.7 52.2 60.0 67.1	5 2 2 2	##E	116	128	127	133	£ 53	25. 25.	5.5	145	6.41 6.42	152	155	3	156	158	158	159	8	154	90
	8																							
,		+ 1- 47 + 1	43.7 52.2 57.1	က္တာလ •	225	- m =	~ 6	9 -	<del>-</del> 00	2.0	0 4	325	~ @	a 0	. a	CV.	<b>T</b> 50	10	നെത	158.3	0.4	9	10 h	
	Ax_press	0.00	# 22 P. C. }	ද නී නි නි	\$ \$ E	11,	22	95	¥ 5	£ £	£ 5 ;	<u> </u>	5.4	140	152	200	155.4	156.6	86	- £	159.4	155.0	1546	156.0
	nerd (k																							
	96 Mor	55 55 5 37 57 55 0	<u> </u>	31.82	E 52 48	8 42 33	45	8 E	X X	Z &	333	18:	0 45 1	37	7.9	4	7.5	50.5	8 5	26	8 8 8	8	500	
Do de	Test tin	e- en :	त्र <b>च च भ</b> 7 ध	3 63 ~ ≪	. o. Đ		å å	<u> </u>	<del>~</del> ~	22	ឧឧ	<b>.</b>	3 63	88	27	82	28	8,8	2 G	330	85	. <b>5</b> .	2 2	16
	pa.																							
. Liste	meastu Disp. (																							
3	esured ce (KX)																							
,	nessured massured measured Pressure (Force (RR) Disp. (mm) (bar) RM	0487	25 4 5 5 5 6 4 5 6 7 6 9	5 44 44 85 5 46 66 76	0 0 0 °	~ ဟု က အေဆး က်	177.9 185.9	+ 0 ·	क क क	<b>寸 </b>	** ec. c	* 00 F	r isi i	N ds N of	10 to	Ch t	n N	0.0	4 5	an .	2310	No. 1	o us	; - ; ; go, e
Cate S		** % <b>16</b> 6	· 在四次的	: 6 5 5	( <u>16</u> <u>16</u>	15 171	5 86	<u>స్</u>	တို့ မြို	o č	283	17.5	4 62 6	215	22.	22.5	22,52	8	3 2	225	23.2	22	88	22.5
SM-0.4	measured Time	43900 43655 44020 44212	44373 44373 44393 44439	44877 44774	44885	45033 45354 45469	45540 45572	45654	45834	46074 46074	46283	46409	46.685	46585	46679	46714	46774	46805	46941	46082	47035	47088	47170	47212
4																							,	

				0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8
		¥		6-613201  6-6132	96.09
H		Mada		ఆడ్డిక్క్షిక్టిళ్ళిన్ని మంద్రమైద్దన్ని ద్వర్ధిక్షిక్షిత్రి ప్రవాగాలు చేసిన అద్ది కు.మీదు మంద్రమైద్దన్ని మంద్రమే	
Y Y		Ξ		- C - B B B B B B B B B B B B B B B B B	şş
AF		5	g. G.	医支柱性 医乳球状 医甲状腺 医甲状腺素 医乳腺性 医克朗斯氏氏征 网络阿朗斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯	147
AE		8	Dr.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2635
VO.			hoop	2	
AC		Сякирь Э	<del>G</del> uş	1	015
A.B			dooy		33
ΨΨ		Gauge 8	g, g,		98
~			poor	112 2 2 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	360
ŗ		Gauge 7	grad	中 · · · · · · · · · · · · · · · · · · ·	924
×			toop to	1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1	39933
*		Gassge 6	Buoj	4 元 元 元 元 元 元 元 元 元 元 元 元 元 元 元 元 元 元 元	265
<del> </del>		ĕ		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	39870
H		Gauge 5	doug	4 C C C C C C C C C C C C C C C C C C C	,4 <b>6</b> ).
<u>.</u>		Gas	e e	8   8   164	36680
		4	dod	- 7 日	43
Н		Garge	Brig	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	19425
H		*	ng cort	。 日本本本本文学 化二甲基丙基 化二甲基丙基 化二甲基 化二甲基 化二甲基 化二甲基 化二甲基 化二甲基 化二甲基 化二甲	103
Ĥ		Gauge	long.	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	1362
		81	Padp		-\$0.7
°	nierovetrain	Oauge 2	Series S	1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1	848
z	9	e enyma	hoop		23
×	A Paragraph	Gauge 1	Busq	· 中国企业的企业的企业的企业企业企业企业企业企业企业企业企业企业企业企业企业企业企业	-
				77 Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	*
×		memory A void (AfPa Heore (MPa)	dooq	2	
<u>-</u>		Avord Offine	Axin	中では、18 日に、18 日本の日に、18 日本の日に、	
		Margarett A.	EX-routhold	6 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Ì
Ħ		C Decree (AS)	press	0 C C C T E C M M M M M M M M M M M M M M M M M M	8 2 2
0		army (* 439) Morrott (k N.)	e v		*
Marione Control		Siene		0.000.000 0.000.0000.0000.0000.0000.00	NO 22:38
d handang n		,			
D E F F F F F F F F F F F F F F F F F F		arod arod immi		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.6
Combined internal po		MTS-action MCS-activates measured measured	Marie (vers)	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	9 92 9
Combi	To the second se	NTIS od meann		8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	163.5
H		n bonnesc bo	Sec.	### ### ### ### ### ### ### ### ### ##	1
1 15	2	cassis			12
<u></u>					

7	10 16	15.64	10.88	32.55	2 5	0 2	2 2	52.45	12.73	13.22	13 73	2 2	3 3	. 4	5.55	28.02	5. 4.	16.73	50.5	7 :	200	2	16.93	69.69	19.77	P 1	8 5	8	S	13 13 13 13 13 13 13 13 13 13 13 13 13 1	Si i	i i	6.53	2, 24	8 8	88	26 63	27.37	27.60	S 1	2 6	27.07	27.96	# 1 F. 1	<b>2</b> 5	8	8 3	8.8	<u>Z</u>	31.81	3.87	33	31.85	3 8	31.00	X 1	3 53	34.89	33.88	3 33	£ 55	32.56	8 8 8 8	8 8 8 8	34.113	80.00	5 K	36 32	£ 8	92 98 98 98
A.H.	599E I6-	-96.94	99,3133	101 7645	104 104	106.639	-10 682 -110 682	133.295	115 402	-121 264	138 413	30.9163	-133419	143 714	-540,426	145 3595	148 9325	152 7955	\$530.554	10.665	105 506	168.454	372.458	477 034	474.746	179.465	2199191	86 6863	3.89.904	-(92.9785	196335	1992703	199,480	264.061	206 7665	208.9943	3313.497	-213 3845	13,9995	2H1.497	168 1633	283 1333	204,1325	-207 493	-219.23	212615	.216.788	257,4355	\$17.5695	210 21	209.405	202 493	-204 919	302.987	202 2735	199,8425	194 4085	193 363	\$ U.S 061	18447	181 5385	183,8265	186,4005	193,2645	196 196	198.77	203 0 58	203 2745	199 954	197 5545
AG				,														•												1					.,	,		7	*:		•	,			`,				<i>.</i>		•				,				•				*					-7		
AF	8,33	£83	906	946	0.10	15.6	286	990	64.64	1052	Z:	= 3	÷ 3	7000	562	1230	13.7	1289	1366	623	2	(36)	1428	1961	1443	200	X.+	1517	150	154	9230	9	1683	146	163	1398	383	1376	3336	333	1111	1329	1325	245	381	13.59	1357	1376	1321	300	9 5	104	1252	1384	1283	1384	977	1365	1263	12.53	1233	1245	1260	1384	1285	1282	1282	1283	1923	252
AE T	-63	<u>1</u>	193	302	213	308	138	.256	2.7	293	ř.	341	6	102	98	383	<b>\$1</b> 9	423	£3:	9	7 5	563	919	983	513	2.5	Ş	CKS	600	619	90	r į	(9)	643	E E	736	764	38.	386	181	555	.233	.726	330	86	S.	-83.7	7 C	70%	797	895	352	236	7 84	310	, S	626	609	58 58	615	498	204	-549	27.5	4694	9690	5.53	679	699	693
ΨD	41800	423.70	423.49	63.67	43.730	02.027	43930	43,983	44060	44300	44636	45040	45,770	46160	9252	47670	47835	47965	48150	48680	49,450	49720	90206	\$49510	\$2530	52830	23030	\$2K70	53336	43,890	25.5	22.52	32440	64780	\$77.40	38770	38 109	61280	63630	62678	63.506	6-6200	64466	53634	90,540	638-405	69630	20,200	71290	71640	72120	77,840	13730	76550	74800	75950	20000	80,636	S1130	26.78	\$90.68	89720	900,65	92600	95486	98333	190605	103405	105200	106400 107298
AC	- [848	(1)-40	*1998	3051	7100	100	13.59	-2386	.1428	12517	* : %	\$74°	(364)	3050	3118	23.372	-3448	.3502	-3563	970%	1963	-4034	-4203	-4395	4789	-48.00	216	67.69	\$135.	-5322	0000	-5745	-28.59	86.09	6699	000	-7509	6162.	-804	0.74	-8631	3878.	-8855	2006	3605	19220	0.4904	0.19820	41139	41330	02430	-11560	11030	1596	12006	37708	42240	.\$2880	13920	135.40	43760	-13840	-13930	1630	.34940	65530	.16976	01993	43,703.0	47300
AB	37770	34090	38250	38450	38610	26010	39880	39920	40008	46210	00300	40370	41570	93050	43940	44663	44230	449.70	46540	4520	432%	02.199	46.783)	47440	49300	0.565	40400	06968	\$0060	0.90	51773	05636	CALC	13480	05595	55550	DE894	57780	28030	28930	59670	60540	09869	61340	61.760	64150	02459	65960	66339	0.699	67280	82173	68579	69470	69370	79520	73486	74170	76850	77330	77450	77350	77370	77960	28230	17660	76670	76940	75350	75450
AA	.466	479	27.5	139	59	(89)	268	586	953	-1020	i a	2021	198	1.46.9	1307	.0753	¥383·	288	1963	9	1617	3272	2408	25.50	2778	CHRZ	(L34	297	3940	3300	868	3533	3043	3615	3845	4084	2664	4637	6113	206	4921	1963	3635	<u> </u>	1576	.4972	4174	.3380	1808	262	2505	149.	1443	2369	.2361	23.60	.7259	.2231	2	1942	1838	9185	1898 1461	1749	197	0.870	688	9881	4881	3776
ž	68889	36386	50620	(C920)	\$1170	\$1440	50.50	\$3006	533.80	53420	0885	34460	11460	\$40863	58419	58540	58736	58935	\$9150	90863	00000	63350	62129	63010	65800	06969	65840	65960	66489	67320	68790	0.069	10340	75270	77360	73950	75820	77270	77690	79190	80340	31260	81620	82200	84190	86306	341740	\$9250	89866	90300	91260	90816	93860	93836	94136	95450	98188	100200	101299	H05700	1983500	199300	150000	157699	0		•	- 60	D	0 0
۸	4755	8981	5681	. 1945	5661	-3087	.7246	.1362	-2304	73357	1692	580	-28/H	2074	3.8	.3183	3252	-3301	3358	-3489	1000	-3764	3900	-4055	-4380	44.65	7466	4562	1495-	588	-3086	9874	97.50	-5K04	-6122	47.40	6989	-7364	-2486	200	-8036	-8130	-8154	#57.8°	**************************************	9176	-9456	-9505	3888	-9485	-9473	1881	\$696	9896.	8996	E060	9875	94.66	97.86	-8686	-8333	3,100	-8276	9878	(S)(S)	136.	.1755	20.00	-2525	7479
×	39236	39610	39790	40000	40210	66430	41770	41830	41900	42130	42490	02020	43470	4630	46690	46820	47020	47196	47419	440000	49/100	49.560	\$0230	\$10M0	53560	13852	(276)	\$3900	\$4330	55939	3833	06290	00000	88659	0F865	61670	62630	63790	64170	65360	66486	67356	67960	096289	30,806	72120	73370	73620	\$20.00	43180	41860	9627	41400	40730	46760	(K)(K)	0507	40510	60400	90,00	46190	46330	40/40	39950	19820	39700	39610	39500	39420	39380
*	G.	-313	256-	.394	Ç	423	646	46.5	669	.764	-844	780	.3083	1178	.1398	1434	1499	.1538	.1563	1808	OLEG.	.1932	2005	.22E3	2535	1034	3634	.2677	.27%	.2954	315	332.0	3863	373	-4036	-6335	47.	5025	5118	285	263	.3699	.5758	385	-6333	-6784	.T.	7407	-4363	4367	-4123	-4122	-410? -404<	-4082	-4080i	850 F	4028	3400	400.	0.940	386	-3888	3880	-3882	3877	1873	.3870	3866	-3862	3862
>	40060	45433	40610	40810	41010	41710	42390	42340	42420	42630	43980	4540X	54731	44576	46246	46330	96490	46630	46820	47020	28750	48550	49190	49870	00815	0.010	61480	37.53	\$2560	23280	54080	24830	20000	26980	58228	D9-5-65	61280	62600	63040	6450	65434	66339	666570	67230	65769	21330	72760	74160	74710	75130	76020	76540	18550	78300	78730	02562	83760	\$4490i)	86070	91460	94000	94540	44610	97850	002300	604500	167100	110300	112500	112390
2	1495	E897	·H653	.1736	1768	1824	2002	0602	-2135	-2225	734	143	2698	.2844	3182	.3229	-0316	3373	-3442	1966	186	3986	-4389	.4611	4919	4003	1000	.5112	\$625	98	6 ta 6	9617	9674	6854	-7334	-7812	.8473	8888	93.58	1803	1966	-10160	-19250	10430	-15140	.11870	J1330	08821-	-13620	-13150	-13340	-13460	13.550	-13910	13950	99178	-14740	4 4906	-15050	15650	11920	16006	05083-	04994	17276	98136	38769	39636	99163	.18526
-	34846	37150	37318	37490	37678	37860	39030	39000	39150	39340	DV 964	0000	40739	96137	43350	43460	43636	43.768	43940	44430	1505	45670	46330	47030	49340	49430	10,440	476.40	59000	\$0,500	21216	05616	CTORO	53739	\$4730	55760	47140	58220	24570	29966	96909	61159	62160	62776	64,195	66030	02120	98888	68670	69040	99669	70,566	71740	72800	02054	74600	2682	863.66	81400	E66680	65368	89840	90,600	92366	94790	97036	9886	191008	\$62500	103400
s	- <del>(</del> )	Š.	625	100	85	989	.K12	-831	-84.2	-923	*	-1062	. 1192	4326.	-1439	4430	-1527	1561		1766	1833	6881	-3003	-2324	.2401	1985	0.874	-2536	-2636	.2771	- 13 Ib	3110	3303	3474	-3730	-4005	-4372	467	500	505	-5122	-5934	-5390	0.00	2982	-6380	9299-	2569-	.7963	2008	-7239	\$308	.7592	-7614	.7640	9314	\$1.65	-8262	-3365	48764	.8348	-9614	1919.	-9439	9286	-10330	10696	13136	-1540	.11570 .11570
u u	19130	19120	19130	19420	19110	19%60	18066	17980	17970	17979	17990	18650	18078	18070	17520	17480	13480	17500	12530	17660	136(8)	17730	17730	1730	16780	07.04	E 53	06290	1678)	16830	169720	104/0	10000	16960	16930	16800	16520	16320	162.70	156.00	15150	15150	15340	14380	6E\$1	15280	15270	15250	15030	14800	*	16650	14620	14460	18465	4560	14630	14600	14540	1260	11720	11620	15280	11570	91530	20511	11480	11478	33460	11550
o	Z.	2	137	139	139	3.5	123	123	125	123	2	2 2	200	161	157	158	¥	193	ž į	136	Ē	E23	621	183	ž:	. e	. 22	177	323	200	97	1	3 %	252	37.7	28%	323	Ħ P	2 5	Z F	383	388	382	392	467	00 T	\$ \$	42+	416	42	000	453	24.0	0; <b>*</b>	42	939	\$ \$#	40]	397	162	163	9	2 5	2	£ i	F 5	Ç.	Ç	94	\$ \$
a	£	340	1360	6363	1369	1359	1331	1353	1354	1339	*	5 P	1321	252	1382	1643	16.53	1662	699	7897	6691	1704	1714	1712	924	2,72	1021	57.	17.18	133	667	5 5	135	1769	138	1838	1883	\$16	2761	1943	1961	1953	562	E263	876	0661	F661	986	19.79	1939	1945	25-51	1943	909	1927	1632	1833	1938	1927	6963	6881	888	S (38)	1632	906	1984	86	1913	1903	1962
٥	004	397	394	393	588	383	-436	.436	.435	-433	Ş	ŞŞ	2	433	Ş	-372	-362	<b>%</b>	S.	640	11.	-332	#ZE-	-326	64.	1 02	5	352	685	- 25	7.5	188°	111	43	337	-297	-244	215	907-	12	Ę	-363	S. :	7 C	173	3.	<b>8</b> 8	Ş	6	ź 4	4	ų:	2, 2	28	92.	Ļ r	7 #	27	33	3	12	69	0 0	36	8 :	5. S	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	2	103	185
ź	39140	33490	39700	39386	40135	60360	42670	41725	45890	42030	45390	428.00	<b>43590</b>	44.50	463.50	46485	46670	46830	\$70.50	01674	48650	49030	49700	\$0579	12980	230800 43.5 H)	1158	53310	\$3750	2466	223.00	66369	0000	580.20	59220	56450	62070	63280	6,46,43	65470	66030	066990	67380	6.7970	69799	21690	73000	74240	74830	14710	76089	76629	78390	78678	78840	80030	\$3660	846.90	85260	90546	92836	03.556	94196	06656	98580	000000	000001	305343	10699K	1679X0
×	Ç :	7.60	-976	-107	1001	7	.1283	-1310	.1340	.1410	4644	. F636	0021	1838	7997	3688	-215	.2198	2743	748	1.445	38.3%	-3756	1962	3245	11003	3119	3383	-3513	3630	2016	\$100	8869	\$055	-4803	.5304	\$308	5833	1660	791.9	484	1669	6654	16.5	27.79	7807	-8166 -8166	.850¢	18640	6326	2847	-8923	5113	-9269	-9296	3432	386	-9982	50105	-19560	36190	00100	.35346	10190	180320	2020	16230	30(0)	16270	(6256
×	62	137	233.3	233.1	233.2	233.9	233.7	233.7	232.5	232.7	232.2	7,47	234.8	232.0	234 D	234.1	234.0	233.8	234.8	# E26	233.4	233.4	233.5	7.27.2	132.1	272	202	23 8.3	2332	131 4		230.5	13014	230.0	229.5	238.2	778.1	137.4	226.7	276.4	231.2	235.7	135.6	234.7	334.2	233.2	232.5	231.5	234.5	231.5	244.2	241.2	7417	244.4	2435	1 1 1 1	258.1	3.59.8	4 F	2633	2.66.5	286.3	367.8	3656	263.4	261.6	350.8	235.4	259.8	764.2
F	80 e	8.4	.12.8	15.5 g	80 80 7	23.3	\$ 1.77	-308	545	8 ·	Ç	* 69.Y	6.79	48.2	643	\$ 02.	263	5030	10 a a a a a a a a a a a a a a a a a a a	# # # # # # # # # # # # # # # # # # #	989	4 005	-107.7		5886	1 212	* 6Z1.	-123.8	-127.9	33.8	5.0%.0	2005	143.6	146.6	-539.2	153.7	-3%6	2,003	7607	1587	.1493	545.	¥,	# C	1553	-1383	5 1917	5 5	- F56 6	983	47.4	\$ \$74.	28.1. 588.3.	.1382	.135.9	1361	-170.8	1914	* F	-1837	\$ (703)	9 (31)	(113)	,H6 §	-120.6	138	-127.9	-133.4	+22.0	-119.2
	-316.6	-3224	-625.4	128.5	331.5	- E	4303	-3452	-147.9	433	185	\$ 89F	433.6	1807	177.4	978811	88	0.64	6464	106.7	203.3	411.7	\$17.8	.223 6	1207	1 575	.232 6	-135.8	-239.8	243.7	1 632		3.54.8	.257.7	168.1	261.9	1 692	2697	6 2.75	.1640	6.092	133	257.8	3797	268.5	.271.8	273.8	377.5	-268.5	265.5	263.9	-262.	2355	1,46	255.5	202.4	245.5	-242.2	2410	-233 6	129.3	2323	340.7	2641	8 (45.	2 657	-223 9	-256.7	252.5	-247.5
Ŧ	D3-	112 6	113.6	132.7	132	113.5	1124	112.4	1123	113	25	200	312.0	1121	313.0	83	9130	5.5	113.1	223	113.7	117.7	132.6	312.4	112	127.	15.1.2	332.0	131.9	2	0 2	2 2	7.0	Ξ	110.9	1153	136.2	8 501	106	109	111.7	113.8	2	25	183.2	112.7	523	*	111.8	\$ P.	116	*	116.3 116.3	1.8.1	9643	97.0	E .	138	202	(29.7	128.7	128.6	133	8	277.	9 %	126.0	125.3	125.9	128.7
0	97.3	07.6	£ 6%	1613	104.3	198	110.7	113.4	16.4	1313	ž	133.4	137.7	42.7	\$0.0	4.5.4	140.0	253		1633	165.7	92	(22)	130		1 2 2	84.2	186.7	*	0 161	0004	5 0%1	363.8	204.1	2087	9'602	233.5	7560	238.5	200 5	3,095 6	205	704.7	210.2	2126	2153	236.8	2350	212.6	2002	2113-0	5. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15.	7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	202 9	262.3	× × ×	135.	8   61	æ =	4	181	2	9861	193.3	1961	8 8	201	£ 502	8,661	1983
Ŀ	0.27.09	60-22-53	00 22.58	(80,135.93	99-23-09	(0.23.13	99.24.99	96.25.94	00:33:00	60-25-19	96.25.29	200.25.46	06.25.54	30,28.04	94-87-90	00 28:33	00.28:41	06.23.46	00 28.51	00 30 H	00.29-16	99:29:33	00.29.3d	00:29:41	98.2.3	06 32.54	06-31-96	80:33.65	80,33,85	00.33.25	80.13.84	97.17.00	S0 14 D0	09-34-19	00-34,25	09:34:40	003800	00:35:35	02:33.60	28.75.00	00.37,22	90.37:42	25.25.00	00.38-27	99-38:42	00 30-07	19.39.13 10.19.13	80:39:32	00.39.52	90 48:27 10:41 22	96 41 27	180:45.33	00 42 50 00 42 50	00 43 97	23-63-63	22.4.00	(95.43.42	00,43.47	00.45.52	00.44 12	10,44,32	05 44 42	25 74 90	00 45 13	00.45.37	2 94 00 2 94 00	00 46:22	10 46-43	00.47.97	06.47.22
o o		9,61	10.9	7	7	Ē	12.7	12.5	F 72	2.5	: :	i J	545	\$ 53	15.6	0.91	\$ 9E	9	200	- 0	187	5.81	2	5.64	# # \$2.5	70.4	\$ 92	50.2	13.4	2	7 0	23.2	2	24.2	24.9	23.3	¥ 1	4.74	26.2	280	27.9	28.0	20 T	28.8	ž	30.6	# K		×	* >	3.5	6 2 3	× ×	31.9	32.5	* *	20.00	*	- 4 - 2	31.0	5.5	2 2	32.6	33.0	34.8	 - - - - - - - -	1.7%	38.3	94 9 96 9	388
٥	200	1386	1385	. 142.3	145.6	6.0	1548	985	162.8	9 69 6	22.	186	592.6	38	*	503	85	2137	5.03	258.4	231.8	3226	241.2	367.6	1000	2.25	3176	.363 3	9 ₹92 €	76/9	216	279.0	383	283	5303	2.82	8 :62	202	306.8	2924	C 882	286	200	7567	197	301.0	363.2	GGE	2973	25.62	7923	2362	282.9	,283.8	623	275.2	271.9	2683	363.0	258.0	253.9	1000	3,68.5	10°	4.77.	2 20	281	-284.3	4	-274.5
H H	7 (9)	163.2	363.2	1633	E(9)	1831	162.9	162.9	162 8	162.9	929	162.3	1623	162.4	163.8	163.9	æ !	1637	5 6 9 1	7 292	99	363.4	163.2	5.53	3 5	162.5	162.5	162.3	362.3	162.2	441.6	3614	191	9810	160.7	155.8	. 55	7.6.1	6 85 3	2.88.2	6438	0.59	3 3	1643	1640	163.3	8 2 91 9 2 91	1621	162.1	182	5.89	688	569.2	1141	2733	2 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	188	1813	6 5 8 4 9	1823	86.6	\$ 3 3 3	3	S. 5.2	****	7 (C)	1826	978	6 8 8	186.5
T ¥	15.65.29	15.05-30	15.05.35	15-05-40	15.05 45	35.53	15-07-36	15,67 41	15.07.46	15-07-56	2002	15 (8:23	15.68-33	15.0%.41	15.10.53	15-13:08	* :	55.53.23	52 11 25	18 51 68	15.11.53	15-11-58	15 (2 5)	15-12-18	251287	15.15.52	15:15:17	15.35 42	15,15,52	19.16.92	15,16,33	15.16.23	15-16.37	15:16 47	15-12-93	2172150	15-17-07	15-13-0	25.18.19	15-18-49	15:19.59	55-29:19	2.2.2	13.73.04	15.23.19	15:28:39	15-21-54	15,23.69	15-23-29	15-23-54	35.24.04	15.24.509	13.7433 15.25.34	15.25.66	0.32.0	25.26.09	15-26.19	15 26.24	15 26 29	15-76-49	66.33,00	15.27.29	1527.34	(3.27.45)	15 200 34	0.88.0	65 38 51	17.29.24	15 29 44	12 20 20 12 20 20
																											_																																											189

Ę	N S	12	, s	2 8	6 2	100	30.00	8 8	20 20 20 20 20 20 20 20 20 20 20 20 20 2	2 50	2 5	26.00	74 17	2 6	2 2	- S	92.55	9 5	22	22, 52	38.78	36.76	38.81	ž.	38.80	7.	2, 25	52	× 50	38.78	97.68
ž.	154.48	£ 92 203	7 Pu 88	200 200	189,736	Mark Co.	000000	2014	24 3404	75 Tallet	\$ 2145	FO 2414	2 900	60.00	164.99	3 040 5	0.83	1 19 2303	153 87	54013	2 7955	49.792	49.43	323 94	787.	3 6715	8 7m1 8	36.452	34 0625	131,6315	277.623
46										1							: -	4 7		-		~	7	7	-	. 2	. 13		- 12	.13	Ψ.
- ST	1242	1334	236	1016	200	5000	(303	151	222	555	3.7.5	E	691.	8	2	3	5	263	1361	1146	1135	1124	22	21.25	1308	1194	ross	8201	20.25	1961	10,63
AE	ž.	565	595	5	8	285	169	10	199	25	<u> </u>	864	125	3.58	343	1369	301	3.60	577	-203	禁	951	90 -	*F7	£6;	(8)	-36	٠	æ	<i>8</i> °.	22
AD.	108200	96166	F3 (WK)	1154000	135581	118700	1 FORDS	£22000	177900	0	÷	Ð	0	O		0	ø	¢	0	0	53	С	0	6	Þ	¢	Ç	₽	Ġ	٥	С
34	.17438	17560	17860	-38146	38280	18420	0.18440	18670	18830	-1896C	-19630	(806)	19220	05300	.19370	(9520	16568	06263	86861	-20010	250.50	20166	-70190	36233	-20310	.76330	.20360	.76349	.20290	06107	19983
48	06554	06562	35679	74180	73930	72220	26230	6,803.0	03659	63860	02909	63820	64096	64310	63993	67940	62470	57330	3630	\$2930	\$2780	\$2430	52426	27460	52350	52360	\$2830	17880	52880	52850	527(4)
A.A.	·1686	4655	-3633	2693	+1634	4Z91	-1620	1682	1376	-1838	-1839	. 6827	1819	-1812	1307	82.63	1879	988	3818	1383	£.	·1386	- 1788	362	+1783	1387	1762	-1366	1768	-1177	-1786
Z	c	6	G	Ġ.	6	Û	0	6	B	v	۵	127	w	0	₽	₽	0	0	¢	D	O1	e	٥	Ð	D	Đ	0	æ	0	٥	0
ŀ	.74)	-1136	1383	2189	.7144	-70186	-7033	1869	5009-	-6806	-6772	63.69	6359-	-6687	5999	-6630	-6628	6839	-6761	67.73	6348	-6783	ψ., ψ.,	-6467	46199	4272	9699-	4684	-66.77	-6647	-66.29
×	38350	38330	39290	39250	39230	39246	39200	39166	39986	38764	386 20	38658	38620	38610	38600	38580	38560	38630	38500	38.480	38460	38430	38470	38390	38360	38350	38300	38270	38240	38210	38(%)
3	3828	3836	3835	3843	-3844	3842	3838	.3836	3834	-3837	.3838	1838	3835	-3832	.3829	3826	.3874	3818	3812	800	1804	3400	60.5	19.00	3794	378	-3789	13284	3779	3772	3766
>	106960	(K) (6)(1)	77120	75550	75060	746402	74230	23558	21970	69730	69350	96769	68330	69380	09869	69060	6901/0	68870	68320	08989	(1804)	58490	58430	08339	68256	68210	68060	67940	6-86d	67780	63696
þ	:14720	2	62661-	-13879	.13830	13.380	.13740	-13680	13.5180	-13330	-13300	-13280	13270	-13269	-13260	05253	13259	-13260	-53239	9776	+3230	13266	9776	-102.0	13,40	-13240	13230	-13319	.13200	8	-13180
۲	302 00	30796	50864Ki	H 2500	133KHG	H4700	116300	188330	120300	126000	137796	211396	8	0	0	\$	0	۵.	0:	Ş	-	0 0	9 0	2 :	≏ •	<b>a</b>	Ş.	e .	c :	o ∢	> 0
s	43.738	-13830	12080	-12330	12500	.F2840	-12429	112300	41970	31260	- F430	1908	133	-11270	.11210	11040	10920	30596	. 378	7676	-9030	9383	9000		9557	1976	700	1976	-9249	0.70	1959
~	200	6673	123	13/40	11570	23	086	11526	81836	1450	(143)	11430	2430	13430	15436	11420	11420	22	1413	13.60	W. 1	15,400	11400	17.400	11400	400	(1.45)K3	7. FEE	E1410	13470	2
9	Ξ.	×. ;	η:	51	2	<b>S</b> :	12	ę.	# ·	ξ:	g :	Ģ	ę ;		şi i	6	602	ę.	254	7 2	9 5	9 5		ì	: :	2 8	100		į.	2 12	2.0
•	1 1	0.60	200	žek.	8	2	836	1884	583	1892	Z i	200	× 1	2.00%	50%	6364	23.62	ED STATE	10000	1000	S S S	2 2 3	LANG	FOOD	1001	1607	1007	7,07	1900	1943	14.67
0	603	5 5	7	#5 :	Ş :	7	.45	2	¥.	9 3	2 3	Ė	2 5	707	£ 5		2 4	Ž	701	7 7	191	18.	1	101	9	ê	į	7 1	E 2	153	5
z	110600	000000	11200	Office of the	05120	1413(0)	=	φ:	ρ	9 4	5 6	5 5	> 0		<b>\$</b> =	= <	= <	o 4	2 0		2 2			- 5		2 0		· «	5 ×2	, =	: =
¥	17622	00201	00404	CFT OF	0650	Obrigin.	2866	*85¢	0.00	2000	6000	You	200	9106	66040	0000	0000	0.00	****	28.487	6438	8238	8	1988	8474	4437	3444	15447	.X448	8449	
¥	2690	373.3	775.4		1877	100	17.0	2.00	\$ 50.0 \$	1 2 2 2	386	200	780	4000	* 0.07 * 0.1 1	704 1	70.5	707 4	8862	299.7	307.5	3619	303 %	304.9	308.9	3,91%	a box	150.6	317	312.1	0
r USU	* 111.	> 0F	3		909	7.0			6.53	6 28	4 35	1	ř,		9.44	6.24	6.89	5	20%	-48.3	6.23	42.9	-38.4	-35.6	43.9	-263	-22.6	665	* **	-12.5	-74 €
	-242.2	£ 2.5.5	2313	2301	3556	236.2	2 6.64	270.3	A 7.44.	2130	.245.0	1000	.717.2	Conc	3671	107	100	6.963	55.	0.663	5 88 5	1887	(8)	-182.9	-180,7	475.	372.3	1693	166	163	-746
¥ 884	130.4	132.0	133.5	5343	1367	147	234.0	771	134.6	18.8	28	339.7	V 64 )	7.46.2	141	9.00	6 23 6	143.7	146.3	1 54 8	145.7	145.9	146.8	1473	8:42.8	0.683	149.3	55	9	156.8	6.2
	8 76.	988	33	6 681	7 58	78.7	128.3		123	123	1702	1898	0891	16.59	6194	1619	25.55	6 58 7	3.45	132.8	1493	F (48.3	146.6	1.44.8	143.6	138.8	136.4	7.7	1316	1293	366
100	00 47 33	96 47 42	25, 52, 53	C3 C3-000	68 68	06.48.67	100 48-14	00.48.47	66.59.43	96.51.27	50.51.37	58,145	50 51.52	50-31.57	\$3.53	00.52,12	77, 52, 53	00,52.40	89.53.48	00 52 53	96,53,68	06 53 43	90 53 28	90.53.38	00:53,43	00 34 93	00.54 18	00.54.2%	8K 25 0X3	199,54:48	50.54.58
a **	388	38.8	38.8	38.8	38.	38.5	88	26	**	98 88 8	3,8 %	3,8,8	38 86	***	38.8	38.8	38.8	8.8%	38.8	3 × 8	38 ×	38.8	0K 0K 0K	20 F1	38.8	38.8	38 8	38.8	3.8%	38.8	38.8
372.8	368.2	263.0	.258.4	8 9 5 2 .	2523	987	2471	4.243.	146	2463	1382	.2353	.235.6	-335 0	.229.3	1336.5	7 222.	-2380	*517	.213.7	8 802	209.6	2000	0.000	1 002	1961	8 06 1	\$ £81 ·	- 1×4 I	8 ±81 :-	.82.6
B 8 8 8 1	189 6	191	1933	1.00	98.2	6 561	6.89	0.561	194.4	1983	2003	203.7	202.4	263.2	3394.5	288.2	- 12	2083	109.3	205.8		777	5 5	213.5	214.2	245.9	216.9	2176	238.2	238.5	63
15 30 04	15 30 GW	02.00.00	13,30,39	15,30,34	57 56 53	15.36.64	15 36:54	15.53.24	45,33 (9	12.34.06	35.34,14	15 34 24	15 34 29	15.34.34	15,34,44	82 M. 63	15.35.04	13.55.41	1535.25	15,35,39	15.35.45	15.35 20	\$ X X	13.36 IN	(5.36.29	ES 36 46	15:36.55	15.37.05	15 37 15	15,37,23	15,37,33
<b>₽</b>	2,0	Ξ	2	17.3	=	17.5	13.8	117	1,1	179	186	£	18.2	183	3	18	188	18.7	8	<u></u>	<u>*</u> ]	ē		22	1	195	É	ž	198	=	2001

96 W

₽ E		<u>ş</u> .		ž~ į	3 %	22	478	621	770	ŝ	¥	340	924	\$20	8	392	981	90.00	683	2 2	845	634	2 60	910	96.5	794	7887	£	757	2	ž 2	715	è	682	17. 8 1. 8	98	8 8	638	8 9 8 31	908	88	36	2 89 85	988	8. S.	82.5	8 8	800	įě	7.95 12.25
H	<u>.</u>	yaay		ma	, Ç	<b>\$</b> 8	118	154	187	9 50	27.5	<b>X</b>	2	364	8 8	121	Ç.	8	916	F 3	280	513	979	986	732	40	86.	324	£ £	<b>\$</b>	5 8	200 Mar	5	2 kg	£ 5	10	£ 58	200	§ \$8	Ę. s	2 2	88	S (S	8 9	5 & 5 &	<b>3</b> 8 :	7.6	1368	3 33	\$ 55 \$
H	Gauge 11	grad																																																
AF		ෂ්ඨය		= 8	:₩	2,5	4	6.21	£ §	8	8	96	266	296	8 8	5005	101	5.01	10,26	5 5	\$403	2003	2003	1066	1071	1078	5 50	1086	1108	1115	1128	1138	44 :	11.5	1159	8	1179	1180	1196	1197	1205	123	1220	1227	1236	1248	128	1372	980	138A
¥.	(); #ds	_		0 4	φ	8 8	B	120	156	Ę 8	282	280	226	92	158	146	S 1	ā	\$ 8	88	R	4 5	8,	ş	B F	86	2 4	46	173	188	ŞŖ	¥ %	18	311	334	88	ķķ	387	35	451	25	8/8	500	609	98	572	542	513	98	\$ £
H	estines)	Buck																																																
AD		decu																																														29696 27085		
SA.	6 <b>ఇ</b> డ్చూల	g nov		* 8	. <b>3</b> K	26 T	8	926	9 6	\$ #F	8	Ŗ,	17	227	9.69	-272	87.5°	-279	2,	8	286	\$ \$ \$	Ř	8	<b>€</b> 89	200	Ş	88	445	345	936	-326	388	-382	<b>8</b>	988	186 186 186 186 186 186 186 186 186 186	375	345	8 6 6 6	-307	Ř	-285	278	, 8,	246	8 8	\$ \$	\$ P	È &
8				1180	158	578 1043	1603	2228	33581	32916	23557	23041	23131	23114	22969	22979	DESC.	22896	22889	22833	00922	22778	22751	22711	22516	22597	22457	22445	22406	0,523	22193	2220	2132	2112	747	1819	444	1417	340	308	336	8 2	8	1380	100	143	0830	19716	7795	7812
Н	ec	форм																													2 # 1																	E >	57	8 2
	ියාලිශ	Rong																																																
2		poop		e G	92 5	8 9	\$	213	27/72	4184	4405	# 44 2 (2)	451.1	4559	4567	200	600	4617	4624	4600	4695	47394	477.25	48053	48328	48516	48342	9000	48894	50081	5170	51783	52360	53075	53603	54468	250:00	55372	56511	57441	56012	56847	59470	60840	61906	63012	96646	70552	58422	50844
_	Sauge 7			£ 12	≈ 3	4 5 4 5	224	X 5	2 2	268	533	25	424		908	8 8	3 7	173		2.	<b>£</b> :	€ 65	Š	183	-247	297	\$	28.5	27	ų,	£.	\$ 80 80 80 80 80 80 80 80 80 80 80 80 80 8	98	-1119	1239	1288	-65	81.6	622	-1786 -1883	-1978	4 5 4 5 4 5	5365	25.5	37.50	3124	3514	3885	71.5	è 88
Н	ి	₿waş																																														19540		- 1
Ã		фац																																																- 1
≩	Gauge 8	Buog		7 7	€ 8	\$ \$	2	4.5	, ES	-52	\$ F	2,5	-233	245	Ŕ	157	\$ 89. \$ 87.	-274	7 8	2887	80, 8	9 7	321	356	28.7	365	100	3775	38%	40.55	9090	4236	4.466	4520	4663	4729	4928	-5116	5234	\$390	5474	98	5706	6	9229	6537	6734	7053	1327	7528
A				ñ	<b>8</b> 8	\$ 8	8	1208	17789	88	8562	3	5442	2 2	84.56	8416	2 <del>2</del>	8418	2 2	8432	8423	8431	8438	84.38	8444	8453 2463	8463	3484 3484	8498	8488 8484 8484	8496	6503	8508 8512	8514	9258 8520	8520 8525	925	85.48	8552	9560	B562	9260	8562	8591	8581	6582	8418	8867	8668	9810
Н	io s	форм																																														526		- 1
Н	Gauge	king.																																																- 1
<b> -</b> -		hoop																																														19292		
80	Garage 4	<b>Ç</b> ı	•	ė w	R &	333	465	8 8	52	-2228	23.52 23.85 23.85	2238	-2346	2476	6987	3880	-2714	-2774	288	2803	3116	3151	-3249	3377	3404	2 X X	3718	386	3903	4104	6775	88	4579	4660	2 5	688	-5108	-5316	5637	2198	5713	2800	6036	6319	6515	6869	-7094	7.86	7871	2811
Н	්	gund																																														58142		- 1
H		tyoot t																																																- 1
a	Gauge 3	D puri		- ,,	., .	, <del>85</del>	₹ 5	4 35	æ	2 8	2 8	28	8 6	4 4	2 1	8 89	8	<b>8</b> 2	3 13	8 :	2 "	ı ko	' '	ò eò	÷	ž Ķ	Š,	3 \$	\$ £	ř	\$ 5	<b>1</b>	è gi	96 S	Ę.	124	-1318	1477	1526	.1713	1738	.1946	3056	2310	-2406	2885	-3189	11 to 1	4981	99-
		doou	-	Ę:	151	10(3	\$ 5 5 5 5 5	7724	25506	37769	\$ \$ \$ \$	40446	40594	40967	41103	41476	41594	41780	6220	42361	9065	43224	43628	44198	44338	65185	<b>4</b> 5514	46037	46318	47419	47817	48228	49395	49616	50349	50925	51517	52360	52945	53798	54717	92038	55577	56797	57752	26262	61991	70526	76897	98926
Н	88n 12	£																																														585		- 1
Ă	microstram Gange 2	gus																																																
ž	Auges in	book		***	- 65	i es	4 6	1	306	308	326	3285	328	33.14	3330	36.	3361	3374	3403	343	38.8	3469	808	3634	3541	3668	3622	3687	3708	3758	3772	3818	3904	3921	3978	4020	406S	4127	41963	4235	42496	42856	42976	4304E	43362	38678	33454	23506	2082	209.30
¥	All strein g Gauge 1	ig.	2	æ ;	7 28	99	9 9	24.0	943	1594	1332	127	12,46	1178	¥ :	68.5	1052	2 %	28	937	38	200	2 2	678	98	232	477	387	18 8 18 8 18 8 18 8 18 8 18 8 18 8 18 8	12	163	8 5	្ត ទុ	132	181	8	6 ts	Ş	125 \$25	-579	-623 -623	-566	25.00	-1158	1248	1561	1610	90 c	916	926
Н	ইউ	ğ																																																
H	(*d		c	· 60, 6	2 0	ep :	T ()	en:	- :	φ. <b>c</b>	3 <b>6</b> 0	nà r	n en	so.	<b>*</b> -	- 84			0	e0: 1~	· <b>I</b> S	un ·			00		<b>⊢</b>	מו	* ~		en to	ec ic	. ~ .	• ~			m 6-			۰.										
×	M) daah	poor		- 47 P	· 165	73	3 3	6,1	274	8 K	₹	Ž.	23.5	334	2 2	Ř	×.	3 8	2	n g	333	233	ž	233	2 23	233	3 3	232	2 2	232	តីតី	2 2	8	ŠŠ	ää	Š	200	230.	200	200	Š	200	222	22	2282	2	244.0	248.1	18	263.7
	ern < 25m Movem 1978, jorges (Ax. monyan Axiisi (NPa Hoop (MPa)	Axial	ģ	5.0	17.4	36.2	3 %	863	103.0	1104	1074	# F	1 68	83.4		68.0	88	2 10	53.4	£ £	8	£ 5	5 F	17.6	କୁ ଫ ଫୁଫ	ne +	<del>7</del> 4	-513	139	88	F 17	- 38 - 73 - 73	\$ 5	\$ 60 60 60 60 60 60 60 60 60 60 60 60 60 6	ģ. ģ.	8	78.2	8	3 7	98.2	080	1102	2 5	8 5	100	142.7	8 8	1326	23	125.6
	SUMBURA	ак-тютел Ах	Ş	\$ 0.5	* 65 P Q	ģ (	ş iç	ę,	ရာ မ ထုံးရ	သု ကု ကု ကု	sp.	e e	2 60	88	# # # #	£.	40 0 40 0	6.89	88.6	222	69	40.0	* 60 60 60 60 60 60 60 60 60 60 60 60 60 6	098	8 6 6 6 8 6	10.7	18.5 5.4 5.4																					252.9		- 1
H	88 (Ax_n	8 8x-st	0	~ <b>•</b>	. 9	¥6.5																																									ę ĸ		3 KS	
≆ हिं	Ma Bress	ax-press		*** (*	, F.	88	18	98	523	2.5																					111.9																	8 8	128	127
0 83	eom ~4 25m Mannent (E)	and Same	C)	0.0		es e	` ಪ	Ö	8	2 4	100	\$ 4 \$ 4	18.7	7.87	31.2	35.7	as c € 5	<b>.</b>	47.2	8 8	608	6 6	2	28.5	812	87.7	2 K	97.9	100.0	109.2	115.4	118.8	1276	134.9	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	142.5	502	155.9	162.8	188.7 7 88.7	17.8	175.1	184.1	197.9	1983	2003	2003	2003	2003	2003
+		Si.	(3	ž č	2 2	£ 5	362	45.8	3 45	2 8	8	1007	2.5	1203	1117	1148	7551	1187	1217	282	282	2	88	282	37.5	427	£ 5	463	437	537	283	578 607	1637	67.7	707	747	321	77.7	100	557	967	877	3.5	£ 50	2967	90%	31.7	2357	(2)	187
H	,																																																	
w l	a MTS-acquator measured measured (Disp. (mm) angle	tî de	8	රිජි	900	86	( E)	9	9 5																						0.244												0.435					0.589		1
a 200.00	MTS-actuator measured m Disp. (mm) at	ಜ	0	000	Ģ	é é	ģ	e -	9 9	4 45	23	· ·	do m	(f) s	4.42	\$3.5	en ec	83	60 c	5 K	₹. i	# ¢	6 40 0 45	es 6	† r~ 3: 65	£ 5	9	112	± = 0	000	Ç.	13.2	0 7	4	15.1	633	18.0	5 6 6 19 19	175	5.4	18.0	100 100 100 100 100 100 100 100 100 100	19.2	9 8	2 8	o 4 % %	313	223	***	ĝ
H	ectus MC uned me (RCN) Die	94.6	۳	2 4	**	0 4	÷	<u>پ</u>		4	e)	ŖĶ	8	89 S	ę S	iş i	φ <b>%</b>	ę	£ i	ŝ	Ę,	5 8	113	130	3 8	140 140	ž.	157	16.7	175 180	382	30.50	X 5	536	52.23 52.33	822	. OF	9 10	2	2 %	378	2 20	98	5 5	72	88	8	8 58 58 58 58 58	8	3
3 Comb	MTS-actual d measured : ( Force (KN) [	2	g	er co	ette i	so e		۲	37 E	e un	<b>.</b>	× 6	I P#	e .	^ E7:	C2 4	ns 100	69:																																
87 e3	Pressure	(Spar)	ea ea	Cr ve	8	, i	100	X.	5 5	100	3		164	184	163.1	79.	3 3	1633	163 C 53	163	163	163,	1637	199	163	163.	162.6	162.	162 6	1631	162.2	162 1	161 8	181	161	165 £	181.5	161.0 6.10 8.10	5612	161	1609	38.8	160.5	1602	158.9	200 SE C C C C	203	179 1	162.0	109.0
<b>▼</b> ,	sorred e		\$189 <b>\$</b>	46338	46982	47052 47265	47311	47374	47664	47856	47866	47826	47308	47276	4BC(36	490,688	4877.0	48106	48138	46.78	48206	48246	48276	48286 64286	48308	45346	48378	48306	68416	48456 48456	48405	\$55.78 \$55.78	48556	48596	49626 19626	48638	19676	48696 45716	18726	\$5745 18766	18796	9875	9838	86.76	× 100	9228	9536	49276	32.65	0000
हैं हैं हैं हैं																																																		1
								_	-	44													اسة		لسد			-1-	1.1			لت		11.	لتد	1	171	1	. ا	1"	"ات	1	1,	10	rr	-1'	ורו	17	~l*	1

F 306 F

A.F.	00 00 00 00	92.	828	328	23	912	236	913	200	986	365	960	298	ŝ	986	<b>X</b> X	-765
	1219	1211	1169	1138	1633	183	1164	1156	1152	168	1155	1132	1145	1150	1182	1178	1301
۲	92			ES						1505					50.55	233	-381
ĄĘ	~ *			456						544					-	585	
¥€.	ľ		•											,		_	,
QΨ	ľ			8 24160			•	•								2803	69 1 SHE
AC	130			8 148													
¥.B	1901	1801	180.2	17988	1795	1795	1785	1786	1786	1795	1795	15831	2 1780	200	3 17902	17922	14930
ΑA	.8	ž	-		_					×	~	•				-	122
	Ĩ	•	•	44305	•	Ť	7	•	•	•	•	Ť	•	Ī	·	42797	3668
Y	543	-874	.769	<b>₹</b>	412	£12	-612	.e911	ŧ,	.758	-784	808	-621	929	928i	-813	202
×	32103	38672	42807	44505	45235	45374	45553	45788	46363	49283	51575	53160	54473	54842	55824	57589	31231
3	- XX	8968	-8732	-10433	-10901	-11148	:1403	-11620	-11874	-12991	-14148	-15243	-16221	1650	-16965	17871	-5647
^	8608	9306	6178	86.68	9044	5042	6043	6036	9CD9	6040	6053	804	6015	8008	9009	8008	\$182
a	-385	-81	88	æ	=	¥	~	01-	40	c.	Ф	33	Ç	Œ	භ	Ś	307
L-	30344	36721	40911	42582	43293	43422	43587	43805	44389	47197	48385	45469	44814	44867	45374	45361	24561
တ	-8671	-9335	-10148	10884	-11375	-11634	-11903	-12140	-12517	13586	-14835	-15679	-17050	17220	-17442	-18346	-7866
~	35516	29598	28845	28499	28263	28289	28358	28401	28514	28910	28116	279(16	27862	27527	27709	27828	26236
	-7286	-8438	-5875	-5710	-5659	-5656	-5663	5648	9636	2887	-5536	3321	-5503	2069	5499	-5480	-5552
d	04840	18920	38160	o	Þ	۵	0	O	0	ø	c	o	o	ø	ø	ф	39620
0	10051	12191	_	14733	15229	5441	15678	15928	16372	77.70	8011	16620	5862	5684	5683	15713	11939 1
_	1998	9664		19516	19294 · 1		•			19344	•	•	ľ	8068	8068	8931	6514
	Γ	-		220										_	•	•	-
_																	
_	86	40	6	877.8	5.0	89	5.1	8.5	2.9	80.00	wi.	4.5	85	1.8	8.5	60	-17
ľ																_	~
	9 -122.6	_		9 -1216			,			14 -1337			34 -1388	_		5.33	33 -269
-	ľ	3 252.8	•	,						·		2 288.4		·	•	.288.	.268
×				2 1313													
٥	ľ			2002													212.5
4	2587	8	7202	2827	3007			3047	3067	3077	3088			3247	3257	328	22.77
Į,	928.0	0.957	073	152	302	1 226	10	1 273	308	38	1.509	6	1 706	1 728	1 742	1 795	2 413
a	78.4	900	2	3	98	18	37.3	37.8	88	40.5	6.04	455.1	47.0	47.4	47.7	200	628
0	-320	-320	330	88	37.8	939	3,	340	380	2,40	O.S.	340	340	989	3.60	OF C	340
-	188.9	TOFE	6.0	06	83	188 9	\$ 883	188.0	181	188.2	192.6	88	188.0	1903	9 833	0.00	7.5
\ \	90508	96%57	9099	49746	40078	458945	45956	49966	9000	45896	50007	900035	50126	80.08	80176	50%86	96508
L	+	T	T	Ta	152	12	E	*	¢2	g	F	S	52	Į,	ŀ	95	Į.

928.5

<u>.</u>																												••••																										
AF			53	hoop																																																		
AE			Gauge 13	<b>Buo</b> l																																																		
AD				3 0 0 0																																																		
AC			Gange 9	Buos																																																		
AB				hoop																																																		
₩			Gauge 8																																																			
2			5	gnot .																																																		
H			}~ #\	doou																																																		
À			Sauge 7	theop																																																		
×				hoop																																																		
Ж			Gauge 6	joug.																																																		
>				doou		35.2	695	1028	1691	9	1914	15732	19150	24491	26186	26922	27390	28270	29276	33,855	34354	39115	52157	71421	72285	85551	85551	86145	86424	85525	87417	87677	88230	89630	90083	90718	91250	91610	93045	93883	95437	96068	97750	99668	101150	101670	104810	105769	106900	110910	111310	116870	117640	124680
n			Gauge 5	forg		c 18	80	159	259	341	455 5.5.1	- P	9 6	707	4	150	465	648	-829	1314	-1787	-2859	6889	15876	16293	-21535	21531	21572	-21600	21624	21752	-21781	21837	21987	22067	22113	22157	22188	-22337	-22419	-22526	52573	22708	22878	-22977	-23011	-23175	-23217	-23270	-23470	-23486	-23708	23740	-24005
H				hoop to		372	735	1087	1783	1989	1847	17698	22249	27962	28743	29521	31181	32269	33635	36815	39307	44329	56305	72575	73751	92020	92705	92625	92918	93130	93390	94248	84848 95540	96210	96703	97403	98028	98443	00140	01080	02910	03960	05690	03080	09810	10460	14360	15560	17020	22180	22710	129910	30950	40750
S			Gauge 4					\$5 28,									580																																			24975 1		
Н			Gau	iong.		289	541	103	384	583	424	587	916	436	560	825	253	108																																	က်င	, Ċ	00	9 69
æ			m	poop				25 25 26 26								-161 24 -201 24																																			35	2 2	27	
			Oande 3	long.																																																-24643		
4				doca																																																4098		
0		crostrain	Gauge 2	Buo	,	2 %	7.0	\$ 8	173	209	245	261	279	490	597	705	923	1631	1341	1363	147	4691	1431	1468	1489	24415	24442	24482	24512	24584	24643	24676	24811	24877	24937	24995	25031	25102	25172	25243	25317	25347	25428	25527	25575	25534	25696	25730	25833	25902	25913	26030	26047	26201
z		All strein gauges in motostrain		hoap		- 82	256	379	629	763	6940	947	1013	1053	1078	1129	1155	1180	1203	1244	1260	1283	1,283 1026	9946	14535	23253	23327	23414	23478	23621	23719	23786	24047	24158	24253	24378	24453	24585	24697	24832	24991	25050	25340	25429	25557	25733	25904	25996	26268	28453	26483	26915	25868	27305
¥		strein gai				~ E	88	32 39	164	90°	232	253	287	193	S	. 193-	-287	-384	74.5	64	-731	930	-14161	14811	-15171	20181	20178	20197	20209	20246	.20281	20284	20353	20365	20423	20429	20444	20474	20505	20534	20560	20573	20652	20669	20702	20760	20813	20638	20917	20961	20967	21067	21072	21177
7		Ą	હੌ	§not																																																		
×			(MPa)		4	37.7	73.6	108 4 144 4	5 62	150	50.2	65.4	85.8	84.3	83.5	82.8 82.8	82.5	82.2	914	1 2	80.5	20.5	55.0	46.3	41.4	74.2	67.4	958	87.2	02.0	613	95.9	9.4	80.0	17.6	23.3	26 ts	23.5 23.5 23.5 23.5 23.5 23.5 23.5 24.5 25.5 25.5 25.5 25.5 25.5 25.5 25	327.5	34.6 34.6	39.7	‡ <del>‡</del>	60.6	95.0	49.0 7.48	51.0	53.0	ж Ж. Я	55.6	88.3	50 th	365.6	0.88.0 5.8.5	20.6
Н			Mumunt (MAx_press (Ax_momerAxia) (MPathoop (MPa)	toot	,			53.3 1.2 1.2								20.4																		-127.9 3										ω.	n e	: m	ĸ.	E		<b>,</b>	as un	4 (	C 1X	6
Ľ,			nerAxis! (i	en Axial			e :	5 W	£.	. 40		2 12	2 2			F2										o r	٠.	rds .	m c		m	10. 4													9 62					•		9	e u	40
1000			(Ax, mon	ax-momen Axial	,	7 4	Ψ,	₹ <del>†</del>	Ţ	ς.	7	7				7			209.2											300				-279.5								2483											\$ E	-183
<b>±</b>	961108a		sex_press	ex-press		2	32.0	8.28 4.88	96	\$ £	120.0	128																						1510													170	170				1788		1
<b>8</b>	rogver	asm≃1,47m	firenent (k)	r Z	•				-		-	-	- 2	37	98	8.28	11	Z :	£ 92	184	202	277	257	257	257	745	246	244	242	238	234	232	228	223	2,5	215	213	203	206	202	198	197	188	186	28.2	179	575	17.	167	163	159	155	# 50 # 20	146
1 55	16 D8.35 Progver.	*0	Test tene A	às.	4	` <u>F</u>	286	418	518	800 880	780	803	1125	1182	1287	1456	1514	1569	1784	1959	1943	7474	2196	228	2344	35/6	3664	3694	3704	3719	3749	3774	3804	3840	4069	4084	4094	4109	4149	4274	4289	4294	4344	4379	4383	4414	4435	4454	4474	4550	4554	4559	4535	4639
3					8	88	500	5 5 9 9	0.02	26 SS SS SS SS SS SS SS SS SS SS SS SS SS	0.03	0.03	5 E	0.05	000	0 1	2Z 0	92 ; G c	0.35	0 46	0.46	0 y	2.2	2.32	236	4 4	4.43	4.43	43	4.43	4.44	4.64	4.45	A 4	4.46	4.45	46	446	447	4 47	4.48	4 4	4 48	69.49	্ কুক কুক	49	8 8	9 50	4.51	25	4 4 52	4 52	2 5 23 5 23 7	4.53
l alie		actuator	ured mea (mm)angi	Day.	c c	0.0	000	00	00	50	0.0	000	3 K	4.7	es es	4 60	11.5	23	165	183	203	202	25 cm	62.9	26 v	21.1	23.3		2 2	24 4	23.1	2,7	21.1	121.1	22	21.1	2.5	21.1	£ .		23.1		7			21.2	es e	V (V				121.2		
Oressure	11-20-1996Time.	charaft 18-	measured measured measured myasured Pressure (Force (kN)Dap (mm)angle	Sam.	5	· <del>-</del>	₹ ₹	; <del>".</del>	<b>,</b> ,	<del>, ,</del>	4	<b>+</b> •				125																																				211 12	·	
o questo	11-20-	MTS-a	ed measu. siffotosi	Z,	e	; <b>ч</b>	us o	·	0	n ec	N	ec •				2 ES	no 1	e v	r ene	æ	* .	D TO	- un-	4	an c	2 +	. 63	en •	- ~	·								_	m c													e e		
S4	Date		Pressur	(pg)				401								188				198	8	10.	178	173	158	197	203	204		311	27	218	220	219				230	ž ž			238.8			544 S			249	249	251	354	256	257	259
Fest	ISM-01 TRAE		Theakured	ಲ ಆ	4,0813	54783	54877	55930	55127	55294	55392	55515	55737	55794	555015	56068	56126	25.161 R6C788	56408	55471	56561	56733	56808	56833	56956	58266	\$8276	58306	58321	58331	58361	58401	58416	58452	58883	58595	58731	56721	58761	58886	58901	58906 58921	58956	56933	59011	59026	58047	59056	5,00,86	59152	59196	50201	50227	59251
Œ		-	0 4	r- 20 0	9 5	2	2	Þ	9	-   92	ø.	2	32	7	\$ 1	92	2	e la	R	5	2]:	ŀ	35	99	*	2	9	=[:	7		2	ŀ	\$	9 5	ž	25	3 <b>[</b> 3	33	9 F	88	8	9 8	23	2 3	99	99	٤١٤	69	2	=	۲,	7.5	<u>'</u>  *	77

ĄĘ				••••												-										_		****		7
AE .																														
ov.																														
AC A																														
AB A																														
AA																														-
4																														
~ 																														
^ 																														
W.	9070	130200	0640	1430	3280	7640	0690	o	o	0	c	0	0	c	0	0	0	6	E)	0	0	C	0	0	0	0	o	ය	0	٥
П								4443	4449	4519	4545	4634	4720	4773	4843	4962	5010	4992	5004	4815	2171	1563	2965	0785	0786	10837	0835	02,30	-20876	٥
Ш		50020 -2					e,	O E	0	c)	o Ç	¢	c)	0	e Ci	o,	c,												168400 -2	
S	ľ	•	•	•	•	•	5706	5730	5739	5908	6004	6386	2856	2628	2559	2497	2268													
R	0	0 -2	ç.	0	e e	0	0	e e	G Ç	Č.	o o	0	0 -2	0	D.	6	0 -7	0	e,	Ð -5	- -5	0	6	ç	ç	e e	Ç;	O Ci	0	ů
Ш	4922	4956	4958	4975	5023	5122	6205	5213	5215	5302	5335	-25451	5541	5560	5513	2425	0591	3223	9281	9246	9673	9637	9613	8882	9528	9480	9472	9429	19429	6489
L	ľ	4587 -2	Ċ	4665 -2	·							5357 -2														8933 -1			5864	
Γ				5354	9385																			7545	7837	7726	7739	7818	27849	7253
																													31985	
L																													-21317	١
	-2	Ċ.	~	Ç	Ċ,	ι'n	Ġ	Ċ,	Ġ	7	ťγ	7	~	Ŋ	ťγ	ť	Ġ	r,	ΕŅ	ιγ	r și	ι'n	• •	.,	17	* 7	175	1,7	• •	1
Ĺ	369.8	865.8	3710	574.2	376.2	877.9	173 t	371.6	377.4	382.5	383.3	385.1	380,6	387.3	389.5	392.1	394 €	389.4	397.8	60.5	395.0	402.5	404 7	407.1	409.3	4115	411.8	413.6	412.1	-7.8
L	.03		46				16.5					32.7															101 7	107.2	1093	-5.2
F	179.0	175.1	1747	173.9	172.2	168.5	163.8	162.5	182.1	159.2	158.1	-153.3	1486	146.1	143.5	1383	132.8	128.2	1253	122.5	-112.9	115.9	112.8	107.5	-102.6	87.8	.97.2	-92.6	-88 &	-1 4
Ļ	787	1787	179.2	189.8	1818 -1	182.6	160.2	179.5	но	184.8		0	183.9		es.	189.4	190 6				æ	-	195.5	1966	197.7	198.8	198 9	1939.8	663	.3.8
1	142	138	138	38	3.96	133	136	129				E.			114	109	105	192	100	26	63	35	88	85	8,1	77	1.1	2	7.5	-
	4665	4780	4809	4819	4829	4845	4954	4984	5003	5030	5034	5043	5099	5164	5179	5204	5223	5314	5374	5394	5464	5524	5544	5575	5605	5635	5638	5669	5684	5689
3	4.5¢	26.4	4 54	4 54	4 54	5.54	8,55	523	55	4.55	4 55	4 55	4.56	55	4 58	4.57	4.57	4.58	4.58	4.58	4 59	59	4.59	4 60	4 61	4.61	197	4.61	4.62	5.48
	121.2	121.2	121.2	121.2	121.2	1212	121.2	121.2	1212	121.2	121.2	1212	1212	121.2	121.2	121.2	121.2	1212	1212	121.2	121.2	121.2	121.2	121 2	121 2	121.2	121.2	1212	1212	121.2
										172					523		.143				127		-122	-116	-111	10.5	.105	100	-87	-2
	6.852	£ 66	259.8	962.0	763.4	264.6	261.2	280.2	2842	82.93	768.3	369.6	366.5	2711	172.7	274 5	278.3	272.6	278.5	280.4	276 \$	281 8	283.4	285.0	286.5	288.1	2883	289.6	288.5	-5.5
	9277 2		3421 2							59641 2			_	_	59791 2	_					60076		,,,		30217	50247	30294	50281	30206	90304
Ľ	82	[2 [2	,	· · · ·	25 25	83	Į,	2	98	τ.	8	83	,	_	§ 8	53	2	\$8 \$8	·	971	_	56	98	101	102	8	100	9	9	107

	WE.	Gauge 10																																											*******			******	
	GA .	_																																															
L		Gauge 9																																															
	28 - T	Gau																																															
		nc																																															
ľ		Gauge 8			e 4	• h	Da e	on ec		<b>v</b> (	v ~	~ .	es es	. en	c> 60		••	v m	, ni	١.	- ~		<b>.</b> .									_																	
ļ	1			0																																													.12921 -12955
,		Zanik 7		docu	707	573	834	818	104	1040	1989	1068	1088	1100	1115	143	1159	1200	1223	1251	1327	1349	1341	1293	1356	1346	1329	1307	1302	1348	1413	2588	6275	8558	8932	9658	11330	11754	12123	12931	13032	13113	13579	13752	13982	14260	14417	14742	14944
ļ	١	Ŭ		ž Boo	೧೧ ಕ್ಷ	161	237	194	8	ec a	\$ <del>1</del>	-134	£ \$	-207	255	-282	9.40 9.50	343	-386	### 008 008	4 4	448	469	485	535	583	21.0	-302	703	457	1.5¢	696	888	-709	-711	761	722	978	1233	2569	2712	2740	-4090	996	-5250	688	10121	10609	10894
		Gauge 6			SO 808	595	967	1121	155	154	8 2	1168	1179	1184	1392	1197	1203	1207	1202	1198	18	1179	1166	1139	36	1162	1178	1219	1203	1260	1238	1207	1233	1168	1155	1127	1521	1883	2250	4024	4218	4318	5965	6977	9375	1680	2156	2786	13119
		Ü		2																																													-621
F		49	3	\$ \$																																													16715
-		Gauge 5	4	Ě																																													
ļ			e d	Ž									PDS.																																				744
ø		Gลบ <i>รู</i> ค 4	hoon																																													1574	1617
[			500	•	123	236	338	352	ξ. <u>a</u>	å gi	-152	236	-282	-347	189	.592	ò	-929	1987	1534	1886	-2245	3283	-4065	-4918	-6691	-6921	7.949	-8549	9844	-10162	-10702	-12429	-12733	-13025	-13163	13529	-13700	-13834	-14017	14015	-14030	.14220	14446	-14548	-14637	-14/25	.14718	-14747
		Gauge 3		ć	2 2	1608	24845	26836	28144	28883	29063	29561	29857	30233	31163	31872	33217	34002	34850	37240	38805	40295	44199	46503	50339	55286	55804	57955 58480	59425	64200	65312	66221	71908	72396	72888	73119	75597	75863	76441	76528	76563 78848	77061	77481	77843	77962	78095	78242	78606	79227
-		ő	gody	,									382				-844																				13032												14650
-		£ 8	pour	· :	851	1567	0047	2126	1001	177	344	180	869	782	324	118	555																							,		-			,	83352 -1-	- 1	'	` '
		All strein gauges in microstrain. Gauge 1 Gauge 2	poop										145																																				
≥		ganges F	ond	•																																									,				-16465
≆		All sfrem Gauge 1	8004		, E	283	2236	2861	3044	3163	3183	3235	3268	3356	3394	3456	3556	3611	3774	3923	4114	4318	4946	5286	5668	6171	6226	6507	65964	70428	71508	72556	77097	77377	77551	77633	79534	79692	79956	7997	29987 80084	80393	80649	80755	80778	80780	80802	81013	81460
-		_																																															
¥		оор (МРа	doob	,	77.1	351.8	292.9	288.5	280.8	289.1	289.1	288.9	289.1	289.5	290.1	289.7	289.7	289.7	288.2	288.2	286.9	283.9	2811	278.2	283.9	280.5	2803	2715	267.4	280.2	2728	276.9	267.5	262.0	255 5	252 1	287.2	2837	273.2	2701	281.2	288.7	283.2	2747	2714	259.5	268.5	283.7	286.5
-		Force (10"KAX_press (Mx_force (Maxiel (MPa)+toop (MPa)		6	36.9	107.7	140.9	964	48.9	37.5	29.5	18.1	~ r	4. 14.	0	0 97	29.6	54.7	4 4. 5 4.	-55.2	Ø 6	28.4	-87.1	945	6. 89. 8. 89. 8. 89.	-101 4	1041	3136	-120 0	111.9	118 9	128 1	128 6	1355	145.4	-984	1060	1190	122.0	1207	1100	104.6	115.2	126.6	1340	-136.2	136.4	1187	104.5
H		orce (Maxi	roe Axial	**	Ó	ရေး ရ ရေး	60	430	-61 G	102.1	10.2	121.5	129.9																																	258.8			
	Sa	ess (MX_f	ss ax-force	1.7	87.3	en 0	11.5																																							125.4			1
Ξ.	. 961205a	O*KAx_pr	ax-press	**	~	. କ କ																																											
O	i. 1135 11 Progver																																													280.5			
L	7. 13. 13.	Fast line			286	32.5	367	1308	2019	2100	2225	2284	2350	2475	2520	2623	2688	2738	2823	2875	7934	3007	3054	3137	3207	3227	3235	3292	3325	3392	3400	3487	3512	3535	3546	9609E	3624	3639	3664	3659	3804	3809	3834	3844	3849	3879	3864	3894	3908
ü																																																	
٥	é è	measured Disp (mm) mss			-0.02	0.00	600-	g ငုံင	6.31	0.15	0 22	0.24	0.27	0.33	80 c	238	5 38	0.47	0 43	0.43	0.48 0.45	0.44	0.44	24.0	0.42	0.43	0.52	0.54	0.62	1 23	85	2 22	2 23	. SE . CI	2.87	333	346	372	3.92	4 4 20 5	10.4	3.5	4 4 32 5	4.54	30 E	5 to	513	8 73 e	5.26
o	3 Fige 18 12 96 Time	Sured mea e (KN) Disp msn		dsp 12.0	4 6	0.0	90	448 E	913.0	0 990	207.0	268.0	1356.0 1416.0	902 D	557.0	17120	7550	328.0	354.0	0220	73.0	1500	326.0	3950 1840	24400	4730	.0.4.0.	388.0	5010	28082	316.0	2853.0	194.5 38.0	0.59	2806.0	800	2555.0	530	26510	5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2566.0	25.55 5.05 5.05 5.05 5.05 5.05 5.05 5.05	2647.0	2706 0	2750.0	20	2767.0	200	36.0
Н		reessured measured in Pressure (bf. prox (kbt) D (bar) kM in		E																																										181 281			- 1
8		ed measu. Pressu. (bar)		9																																													
¥	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Time									487	£ 5	48851					_			4953																									50429			
Ц		4 10 10 1-	ော	E	=1=	[2]	21:	2 2	El	2 2		22 8	12	S.	4	₹	2	F	E	<u> </u>	118	[8]	5	g	ş	ŀ	13	4	9 4	-	£ 5	8	\$ 6	3	25.	8	ŝ	88	9	62	3	2 2	Ŕ	67	8	70	7 2	Ľ	7

AE	Γ		***	••••							_						••••							_		_									_																											•							*****	
AD	-																																																																					
AC																																																																						
AB	1																																																																					
-																																																																						
AA		17.8	212	272	381	1300	45	13461	553	598	1681	689	1567	8548	1667	716	836	845	1033	*	213	5/2	34411	1461	573	6659	744	**	918	2087	060	5092	67.0	5005	5115	131	5162	9178	5253	250	100	470	K 5	3830	270	6770	1428	34.85	1637	16785	9888	308	480	1471	17487	528	566	707	1/8/3	18774	58451	18457	18531	1582	673	5749	93.6	3875	2800	16918
2			·		ľ	ľ								•			•			•									·		·																			20380 - 1						•						,								23725 -18
_	ľ																																																	15925 20																				17251 23
×	ľ								Ċ	•		Ċ																•		•	·		·																							•		•						•		,		, ,		· 1
*																																																																						22 20655
>																																																																						2 -18782
ŀ																																																																						24172
_																																		ľ															•				·													Ċ				17454
ø	1623	1642	1674	1731	1949	1969	1989	2041	2244	2321	2800	2790	3055	3367	3588	3820	4136	4534	4744	5184	9889	6781	1050	7610	20.	9005	9517	10262	10764	11959	12294	12387	12832	13497	13842	14051	14355	14521	14726	22.10	15525	10520	YOU'LL	10001	17180	17587	18087	18508	18777	19036	19310	20022	20320	20460	20706	21013	21227	21433	24500	32376	22542	22586	22639	22744	22848	23026	23284	19952	23799	23815
ľ	.14816	14904	14984	15047	.15168	15167	-15213	-15289	.15394	15422	-15506	15524	-15451	-15454	15448	15474	15578	136/4	-15/33	-15798	13849	4080)	90861 ·	-15973	16031	1566/	-16107	-16145	-16169	.16238	-16215	16200	.16143	-16095	-16073	-16073	.16094	-16110	16223	19380	79291	466.47	10000	00001	16879	16961	16998	-17073	-17237	17400	47974	18002	-18207	-18234	-18275	-18353	18450	-18636	10044	19411	18552	-19566	19623	18711	19813	19907	-19983	20130	20227	20234
a	79329	79425	79505	79558	79635	79627	79638	79657	79684	79682	79690	79659	79802	80081	80424	80878	00119	81183	81218	81243	81230	61224	8	81155	8113	81084	81(960	81025	80888	80938	80897	80838	81140	81411	81541	81707	82049	82164	82308	00.70	97479	67479	00000	92876	82585	82960	83517	84320	84648	84856	80008	85525	85708	85846	86278	86941	67480	87772	00000	88841	89012	89058	89124	89231	88337	89552	90133	97.513	91479	91526
ŀ	.14738	.14852	-14964	15057	15215	.15212	-15278	-35351	.15509	.15537	-15647	15689	-15675	-15657	19684	15697	-15803	13803	-1595-8	.16033	16105	16217	97791	16249	16321	16384	15408	.16460	-16488	-16574	-16565	.16553	-18525	.16497	-16476	-18467	16462	-15459	16554	1004	20001-	1695	10001	47480	-17255	.47375	17385	17424	-17549	-17882	10007	-18291	-18519	18566	.18815	-18679	18741	-18907	10000	19710	-19873	.19897	-19950	-20058	.20174	.20296	-20374	-213328 -20584	-20613	-20520
0	84738	84879	85012	85131	85288	85288	85330	85375	85458	85466	85511	85522	85871	85830	86173	86517	86590	SC / 28	5000	85858	86384	96.923	\$0808	86698	20.00	86916	86908	86910	86903	86913	86892	86935	67143	87377	87488	87593	87795	87825	87912	0/8/6	08600	0000	60.00	800.01	A8324	88737	89150	89645	69820	85362	90709	90686	90950	83 127	91523	92053	92451	972584	82.420	97478	94310	94390	94460	94619	94750	95020	95573	9640	96740	967.90
Į	-16526	-16594	-16638	-16663	.15683	.16651	-16670	16692	-16731	-16724	16738	.16718	16661	96591	16541	.16503	-16536	16565	1828/	16890	//92/	1552.2	12082	16593	-1507F	.16993	16654	-16673	-16679	-16713	16886	.16669	-16615	-16540	-16483	16470	-16441	-16421	-16504	7000	70001	18883	3000	10001	15894	.16936	-16942	17000	-17153	-17294	19719	-17894	-18093	18132	.18181	-18277	18388	-16555	70005	-19387	19536	19559	-19603	.19710	-19814	19910	-19991	20021	-20253	20262
Z	81528	81577	81598	81589	81543	81512	61490	81475	81424	81396	81339	81285	81397	81528	81679	81874	81813	81888	81836	81839	637/4	61/32	0 000	61545	6,536	81578	81542	81505	81473	81410	81370	81404	81588	81775	81844	81911	82062	62071	82123	92135	901.70	0,443	20120	92028	82068	82361	82789	83457	83736	83800	64056	94528	84706	84845	85274	85836	80434	75999	97367	87827	88017	88085	88143	88264	88369	88570	89132	90350	90476	90520
*	285.1	282 5	2788	275.1	266.5	265.0	261.7	258.7	249 8	5 242	240.5	236.4	254.7	271.4	282.9	288.9	284.2	5/88	2762	2727	5 0 2	7.567	500.5	252 5	242	242.5	2382	233.7	229 8	221.5	2190	229.0	249 8	266.8	274.9	282 2	287.8	285.2	282 7	211.1	6 7 5 7	783.1	262.0	262.6	237.1	260.5	279.8	290.8	285 5	279.9	6017	2564	249 1	258.2	274.2	289.7	6 162	5 7 5	275.8	284.8	2610	259.0	258.0	255 4	252 8	267.0	1 8/2	290 4	288.2	287.4
Ļ	111.9	119.7	126.6	129.4	138.9	144.6	140.7	147.3	158.9	156.6	176.7	168.9	154 0	135.0	120.9	109.7	5 1	9 77	925	0 P	0.98.0	193.0	2000	1584	363.9	1 1 2 4	577.3	182.5	487.9	199.1	1912	184.5	164.8	143.4	1315	123 5	114.3	0.0	124.2	140.0	0.65	7.56.7	166.4	. E	5 6 6	162.7	139.2	1215	-131.0	142.4	156.0	1785	1831	1748	158.0	-138.8	9 67 1	0.784	158.6	176.7	182.5	-178.5	-189.8	185.4	192.8	-186.2	8 40	-140.7	136.7	133.4
F	ľ																																																																			2810		-
F																																																																				140.3		1
Ĺ	ı																																																																			293.3		
9																																																		4329																		1474 2		
	3	6.3	6	m	ger)	es		m	i,	6.2	E,	e	4	· ·	~	4 ,	æ '	ď	~ •	4	a .	, -			٠.	*	*	Ψ.	4	4	<b>√</b> 2′	•	₹	4	Ą.	4	4	w.	• '	. 1	. •	. •	. •	. •	4	च	4	4	*	•	. ~	- 47	*	ď	*	* '	. •	. •	. ~	4	₹	•\$	*	4.	∢ .	. •	. •	. 4	4	
Ľ	34	46	T-	75	2.0	13	24	37	70	82	60	20	9	75 :	£ :	90 c	200	P :	26	8	€ (	i s	š	S 5	5 6	17	200	28 1	as Ge	*	82	60	14	22	23	38	*	30	C7 1	7.	, e	5 5	27	70	18	5	525	659	7.6	es r	98	2 20	99	52	2	28	a e	D 4	9 67	28	45	48	.57	.65	77	26	22	16.13	: 5:	13
٥																																																																						
0	£	œ	c.	40		\$	. ~	1 28410	cm:	ė	•	\$	ins i	o ,	٠.	m c	- ·	. oc		ot. :	٠.	rs e		sc 4	•	ю.			~	_	~	m	rt.	nó:	ı.	erin.	e e		on e	٠.				- ن	, 0	. 4	2864.0	10	ch:	o •		y art	4	urs	0	nc 1	n e	7 (		. 47	~	F*)	(n		KY F	~ n	n 40		1 m	
8	198	Ī						181		4 573		•	•		. ,					130		22.										4 160					201				•				9 166					98								467										203		
٨	50474	,	50,484			,			80828	\$0834	5054	\$054£	3025	2026	5036	5037	2008	9000	3026	200					_						72.4																			50879																		2005		
	75	32	1	<u>2</u>	į.	8	<b>*</b>	12	83	84	82	86	<u>``</u>	8	8	8	s [	×[	1	\$	<u> </u>	\$   2	Ì			5	1	165	2	\$	ŝ.	108	9	8	109	<u>=</u> [	Ξ	=	= ;	1	= ==	Ę	15	1	120	12	12	123	12		1	Ę	128	23	5	2	2	115	ľ	137	138	138	146	=[	4	-	I.	4	E	

Γ	Т			-										-					_			_													••••																			
3 45	J																																																					
3																																																						
	. 1																																																					
av	4																																																					
Ý	1	5 4F	922	939	<b>*</b> 26	383	999	986	120	552	15 S	283	283	320	349	*	503	536	583	\$29	208	128	500	27.7	202	908	942	028	151	102	25.00 27.00 27.00	r vo	98	123	***	250	988	342	280	38.4	152	537	25.5	173	544	316	212	e %	5 Z	203	<b>50</b>	534	30 S	0
Ĺ	1					24185 -18993 24315 -19024																																								Ť								
<u>}</u>	]					-17371 24																																																
ľ	1					21316 -17																																													•			50 .25978
Å	1					18942 21																																													•			•
2	ľ					24939 -18																																			Ċ				Ċ	•		•	Ċ					Ì,
L	J					-17574 24																																																
ľ	_					24437 -17																																																·
8						20497 24																																																
L	1					93910 - 20																																						ľ	0	0	5	0 25	0	0	0.0	200	0 133	0 -13
L	J					-20886 93																																							463	333	343	376	402	381	308	16150	243	287
Ĺ	]					38630 -20																															2.28	6	9 0	0 25	-17	71.	0 - 10	0 .46	0 .16	9, 0	200	94.	91- 0	91- 0	0 -19	 	0 -16	014
ľ	J					20505 98											·					·									•					•	707	874	245 069	202	843	535	963	290	608	28724	20234	283	23682	340	223	23177	172	23156
L	1					92500 -20																																					156900 -27		0 '28	0	200	0 2	0 -23	ee :	96	9 5		D -23
H		8	96	E 3	56.5	i Ci	S	83	8. 3	<b>3</b> 5	8 36	26	97	88	8 5	105	38	108	400	130	110	444	111	112	112	112	112	112	E \$	13.5	114	114	116	135	116	117	119	2 2	2.5	126	135	143	156	154										
-	ı,	~	93.9	80 %	v c	3234	\$ 12	3311	100	2 4 5	4	17.5	350.8	53.4	ch e	96.1	58.3	57.8	53.2	on 0	th or un	4 4 4	37.2	23.5	53.9	70.7	හ. න	5.5	- 6	10.2	24 ¥	608	a: 15	225	50.5	9.40	59.4	F 4	3715	374.9	377.B	3733	381.6	384.2	18.1	395.3	9 12 R	. 2	400 5	404 4	7 27	607.5	38.5	9.0
×						1000																																										18.1 39					Ī	
	l					2562																																									236.1		m	<i>a</i> ) ,		237.5		
Ľ	1					156.2																																														1968		
Ĺ						267.4																																										•	•				•	
L						4669 2																																																
4	7	*	•		•		•	•	•			•	*	•	•	. •	•	•	•	•			•	•	•	•	•	•			•	•	7			•	•			•	• •	., 4.		•,			, .		91		.,		4,1	
L	6.14		16.15	£0 α	n c	16.25	6.28	6.31	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5,38	6 42	6.45	5.47	ବ କଥ	200	6.63	6.65	୫ ୫୫	6.81	9 :	12.6		7.52	7.84	7.88	50.0	e> e • • •	n u	3 4 4 5 3 4 4 5 3 4 4 5	8 76	8.82	888	8.93	0.50	8 80	20.00	80 CG G	51.5	19 20	9.25	600	- 22	0.63	0.82	66.0	787	2.00	2.45	2.75	88	4.35	24.34	4.54	5 11
Ĺ		r)		o r		2674.0																		~		cr i	0.0				_	2				~	n c				~ ~											2485 0 2		1
ا	l					226.4 26.																						215 B 34						2368 27			60 E	> e-	. 4	5	vr c	3 0	267.2 25	0	ı~ :	2,000	- 40	~	<b></b>	do v	· (c	285 3 248	()	0.4 175
8						51219 25																																														51774 28		608
Ľ	_					155					<b></b>		163			167		169	ه 12	6 5	· ·	174	175	176	177	78	6 G		182	163		581	196	188		8		18	5.	195	200		198	200	S I	202		205	206		602	51	\$ \$	512

March   Manages in microstrain   Catage 3   Catage 4   Catage 5   Catage 6   Catage 7
Part   Cange
House   Hous
465         61         41         41         42         43         42         42         42         43         42         42         42         43         42         42         42         42         42         42         43         42         42         42         42         43         42
62         487         51         44         6         7         2         2         3         3         7           115         514         94         875         113         289         56         285         78         7         44         411         465         113         3         7         113         465         113         465         114         414         465         113         3         7         114         465         115         464         111         465         115         464         111         465         115         464         111         465         113         3         115         464         111         465         115         464         111         465         113         3         114         465         115         464         114         465         114         465         114         465         114         465         114         465         114         465         114         465         114         465         114         465         114         465         114         465         114         465         464         114         465         464         464         414         46
115   914   94   875   113   289   58   295   778   313   775   715
13         125         153         165         160         40         40         41         111         465         118         40         41
258         175         175         169         226         777         144         569         145         569         145         569         146         157         146         157         148         77         144         275         164         177         144         276         168         171         144         276         164         171         164         170         245         187         171         186         186         187         278         187         171         186         187         278         187         171         186         187         278         187         278         187         278         187         278         187         278         187         278         187         278         188         187         278         188         188         187         278         188         188         187         278         188         188         187         188
218         219         211         2024         284         274         717         144         756         169         192         237         181           467         1606         1625         336         447         173         169         193         233         231           467         3641         236         436         436         436         169         122         232         231           457         3641         3680         436
446         6161         389         2043         388         847         173         880         132         383         847         173         880         132         223         132         138         140         142         132         228         469         122         132         238         469         122         112         23         23         469         222         112         23         138         140         46         132         140         26         136         136         140         22         112         23         144         23         26         46         142         136         142         144
466         192.7         386         19389         481         917.2         208         1029         22         11.55         27.8           467         3249         386         1939         786         10.6         12.0         1261         28         132         2.9           457         3864         386         10.6         120         1261         28         138         2.9           2.3         38428         -346         380         10.6         127         128         -34         138         149         39           2.8         38428         -460         3829         146         120         126         132         36         136         140         30         136         1440         40         136         144         1440         40         136         144         144         1440         40         136         144         144         1440         40         148         148         147         144         146         146         137         144         146         146         137         144         146         146         137         148         149         149         146         146         137
467         356.9         357.1         105         156.1         249         139         144         139         139         139         139         144         139         139         139         144         139         139         144         139         139         144         139         139         1
47         360.0         -68         390.0         37         1 (49.4         1.20         1 (32)         2.89         13.32         2.89           28         36.0         36.0         37.1         1 (40.4         1.57         1.98         1.98         1.98         1.39         1.33         2.89           28         36.2         4.0         36.0         3.0         2.0         1.25         3.0         4.0         1.30
194         326.2         336         1184         -135         -136
2.9.         3845-8         -600         3928         136         1230         -226         164         164         164         164         164         164         164         164         164         164         164         164         165         -266         408         -126         130         -266         -266         -266         -266         -2
266         40895         1022         38649         -126         1301         464         1357         469         489         37           2961         42326         -1426         4023         -126         1373         -421         148         -149         439           2961         42326         -1426         40231         -126         1373         -421         148         -74         1499         -37           4548         52087         -402         1373         -421         -681         1544         -199         -300           -5786         52087         -627         1484         -74         1444         -744         1499         -300           -5786         52487         -627         -744         -744         48936         -128         -741         -449         -449           -5786         52487         -627         -747         1471         -886         -139         -131         -449         -449         -300         -1474         -1476         -149         -449         -300         -1476         -4576         -1479         -144         -149         -449         -449         -144         -144         -144         -144
304         4225         146         128         427         1446         146         173         611         1489         74         428         461         158         461         1489         74         468         461         158         74         469         304         469
666         4336         -1426         40237         -402         1373         -611         1381         -619         1564         -1856           2561         4536         -1426         40237         -402         1373         -173         144         -774         1499         -300           -556         52007         -373         464         334         460         1381         -744         1439         -300           -578         52007         -373         464         3         -600         1291         -173         1444         -786         1394         -410           -578         5200         -5324         -6007         -4872         1254         -791         1441         -788         -336         -484           -570         -586         -596         -517         1421         -791         -449         -307           -631         -570         -670         -487         -586         -570         -487         -570         -449         -570           -632         -586         -570         -487         -570         -487         -570         -449         -470         -449         -470           -794
2551         48714         2269         48318         1496         1373         737         1436         774         1499         308           -5562         55337         -3753         46401         25696         1313         -729         1446         -766         1384         -437           -5662         5337         -4371         -4562         1781         -773         1444         -766         1384         -449           -6786         5438         -6787         -4767         1241         -769         138         -449           -6786         5437         -4767         1254         -971         -479         -489         138         -449           -6788         5565         -5672         1259         -410         -439         -439         -449         -4
4548         52087         -3753         46401         -2696         1315         -723         1446         -744         1434         -327           -5862         53837         -4643         -3804         1281         -773         1444         -786         1384         -410           -5786         5431         -4643         -3804         1254         -791         1444         -889         1384         -410           -6786         55265         -5602         -4997         1254         -791         1441         -889         1338         -449           -794         5734         -6525         51374         -4872         1254         -791         1441         -889         1338         -449           -794         5734         -6272         1254         -791         1441         -889         1338         -449         -410           -8048         5629         5672         -626         1364         -791         1444         -879         1479         -679           -8056         5849         -677         1424         -791         1448         -879         1479         -679           -8068         5849         -677         1
5562         5393         4563         1593         129         172         144         178         144         178         144         178         144         178         144         178         144         400         1885         449         446         450         189         189         449         450         189         189         449         450         188         449         450         189         189         449         450         188         449         450         188         558         449         4872         1254         -891         144         -893         189         449 <t< td=""></t<>
-5702         -5703         -5704 <th< td=""></th<>
-5788 5245 - 4714 48936 - 3904 1291 - 813 1421 - 906 1385 - 449   -5788 5255 - 5685 5 3904 1294 - 391 1414 - 839 1338 - 449   -5788 5265 - 5685 5 31374 - 4872 1254 - 347 1414 - 839 1318 - 617   -7974 5734 - 6373 53649 - 6272 1259 - 910 1437 - 675 1318 - 617   -8048 57774 - 6373 53649 - 6278 1264 - 900 1448 - 885 1303 - 683   -8046 57774 - 6373 53649 - 6278 1264 - 900 1448 - 885 1303 - 673   -8056 59457 - 6470 54576 - 6427 1317 - 855 1479 - 842 1343 - 670   -8056 60850 - 6839 60855 - 6781 1477 - 765 1544811 1376 - 646   -8056 60850 - 7732 5899 - 7710 1454 - 791 152 - 604 1353 - 711   -8056 6087 - 7712 6087 - 7742 1424 - 7761 - 626 126   -8056 6087 - 7712 - 6805 - 10103 - 8073 - 1429 - 827 1414 - 706   -8056 6087 - 10103 - 8073 - 9168 - 13103 - 8073 - 1429 - 825 1293 - 814   -8056 6087 - 10103 - 8073 - 9168 - 13103 - 8073 - 1429 - 825 1293 - 814   -8057 6087 - 10103 - 8073 - 9168 - 13103 - 8073 - 1429 - 825 1293 - 814   -8057 7759 - 1274 - 8759 - 13103 - 8073 - 1429 - 825 1293 - 814   -8058 77759 - 1274 - 13103 - 8074 - 1631 1380 - 1128 - 1180 - 1284 1  -8059 77759 - 1274 - 1325 - 8090 - 1482 - 1429 - 825 1326 - 3029 - 1475 - 1276 - 806   -8059 - 13103 - 8070 - 1482 - 1429 - 825 1326 - 3029 - 1475 - 1276 - 806   -8059 - 13103 - 8070 - 1482 - 825 1408 - 1311 - 827 1418 - 827 1
-678         5565         -5682         -4997         -436         754         1414         838         1338         -449           -678         5565         -5685         51374         -5202         1254         -797         1421         -875         1324         -617           -708         56247         -5665         51374         -5202         1254         -900         1448         -865         1303         -613           -8048         56774         -6870         54576         -6427         137         -855         1478         -869         -677         -717         -869         -814         -842         1303         -659           -8056         -6829         -6876         -6427         137         -856         147         -765         147         -765         -842         -710         -765         -766         -780         -840         -850         -870         -870         -866         -866         -1701         1472         -827         -827         -827         -842         -870         -870         -870         -870         -870         -870         -870         -870         -870         -870         -870         -870         -870 <t< td=""></t<>
6788         55869         -5434         50817         4872         1254         -678         5289         -678         5387         -678         5784         -678         5784         -678         3124         -522         1259         -143         -829         1318         -617         -715         -818
-7068         66247         -6655         51374         -5202         1259         -940         1437         -829         1318         617         -175         -804         -944         -149         -829         1318         617         -175         -804         -804         51774         -675         5364         -6627         1250         -944         -148         -829         1317         -715         -804         -804         -805
-7874         5734         -6321         -5172         -6173         1250         -944         1409         -6330         1271         -775           -8048         5574         -6373         53649         -6276         1264         -900         1448         -885         1303         -683           -8166         54457         -6470         5476         1264         -900         1448         -885         1303         -683           -8266         55672         -6586         1387         -865         1447         -811         1373         -696           -8266         6270         -7714         60188         -7701         1454         -761         -827         1414         -776           -973         63900         -7714         60188         -7701         1452         -864         1507         -646           -10043         6475         -868         -1701         1442         -767         -827         1414         -775           -10043         6470         -1704         -776         -470         -874         -874         -775           -10043         -1704         -776         -470         -874         -476         -476
816         57774         6373         5364         6276         125         904         1448         885         1479         6470         6476         64
8166         54457         -6470         -5279         -1524         -910         -1438         -6859         -6470         -
-8765         5647         -6475
-8366 62102 - 6859 55572 - 6566 1366 - 814 1514 - 811 1376 - 659
-8226         60850         -6839         56855         -6781         1417         -756         1546         -730         1407         -646           -9737         62002         -7714         60187         -7101         1454         -761         1527         1414         -766           -9737         62002         -7714         60187         -7101         1454         -761         1527         1414         -766           -10143         64750         -8068         61309         -8207         1472         -824         1650         -933         1306         -814           -11039         66547         -8746         63286         -10120         1422         -824         1650         -925         1275         -838           -11080         68477         -8746         68591         -10120         1422         -846         9183         -869         1737         -1189         -711         -872         1489         -711         -872         1489         -711         -711         -872         1473         -711         -872         -872         -873         -873         -873         -873         -873         -873         -873         -873         -873
9966         62102         7732         58198         -7101         1454         797         1557         -827         1434         -776           -9737         684750         -7742         58198         -7101         1454         -797         1557         -827         1414         -776           -10043         66124         -8718         63266         -8053         -1429         -834         6508         -925         1775         -894         1353         -711           -11009         66124         -8718         63260         -9188         1448         -787         7018         -892         1287         -795           -15010         6657         -1497         -2456         69591         -1402         -846         9193         -956         1287         -890         -150         -894         1353         -171         -140 </td
-773 63900 -7714 60168 -7724 1434 -761 1522 -804 1353 -714 1709 66547 -8066 61309 -8207 1472 1434 -761 1522 -804 1353 1366 -814 1009 66547 -8786 -9053 1429 -831 6506 -925 1275 -838 1409 66547 -8786 -9053 1429 -8787 10120 1492 -846 9193 -955 1287 -1287 1409 66547 -9786 -9654 -10120 1492 -846 9193 -955 1297 -980 1500 -951 1728 17759 -1274 77384 -13911 1596 -623 13264 -1971 1423 1423 1420 1436 1436 1436 1436 1436 1436 1436 1436
-11009 666124 - 8719 63286 - 9053 1429 - 831 6506 - 925 1275 - 838 - 11098 66647 - 8718 63286 - 9053 1429 - 831 6508 - 925 1275 - 838 - 11929 66473 - 9345 695691 - 10102 1428
-11099         66547         -8784         63903         -9168         1448         -787         7018         -892         1287         -795           -15002         76547         -19456         68591         -10120         1492         -846         9859         1287         -795           -15012         75692         -1917         1492         -661         1287         -1631         1380         -1917         1423         -1980           -15012         7666         -1917         160         -661         1287         -1631         1423         -189           -15541         7784         -13941         1659         -662         1326         -1917         1423         -180           -15442         7784         -13941         1659         -662         1326         -1917         1423         -180           -15441         7785         -1244         7784         -1659         -661         -677         -686         1475         -1475         -1476           -1735         6873         -16601         1618         -675         -14673         -10210         1475         -1478         -1478         -1478           -1734         6873
11980         68473         -9456         68581         -10120         1492         -846         9193         -353         1293         -880           -15013         75587         -11872         7498         -13103         1560         -661         12874         -1631         1380         -1128           -15302         7553         -1274         7739         -1274         7739         -1274         1423         -1180           -15941         7876         -1316         78604         -14331         1627         -656         1346         -2400         1432         -1180           -17135         86730         -1569         80090         -14822         -656         1346         -3029         1475         -1776           -17135         86730         -1561         8654         -16801         1687         -677         1493         -1720         1462         -1769           -17289         86573         -16801         1687         -675         -1749         -1721         1666         -534         -1749         -1749           -17289         86732         -16801         1687         -1754         -1171         1666         -534         -1463
15012         75587         -1972         17020         1492         -646         1584         -1593         -1693         -1693         -1693         -1693         -1693         -1793         -1793         -1793         -1793         -1793         -1793         -1793         -1793         -1794         -1757         -1793         -1794         -1757         -1757         -1757         -1758         -1750         -1757         -1753         -1753         -1754         -1757         -1758         -1753         -1
-1502 7657 - 12315 78105 - 13103 1560 - 561 1328
15922         15873         15873         15874         1423         1486         1601         -677         13066         -1917         1423         -1180           -15946         7755         -1274         7284         -2400         1436         -1180           -15941         7876         -1274         7384         -2400         1436         -1180           -15942         1756         80030         -1482         1681         -677         -656         1349         -117         167         -1180           -17135         86953         -1587         86582         -16801         1688         -63         -1418
15666         77759         12744         77384         13911         1596         623         13264         2400         1436         -1180           -16541         7778         1367         1345         -3029         1475         -1180           -16226         800306         -13431         1627         -356         13495         -3029         1475         -1276           -17135         85730         -15816         85435         -16881         1618         -615         14673         -10210         1664         -4783           -17249         86572         -16801         1535         -657         14794         -1121         1656         -5449           -17249         86502         -16906         1535         -657         1478         -1272         1469         -5499           -17249         86203         -17094         1494         -688         14803         -1309         1749         -4459           -17240         86704         -1651         85557         -16936         1472         -1276         14809         -1276         -1489         -1276         -1489         -1480         -1480         -1480         -1480         -1480         -1480
15941         78768         13116         78564         -14331         1625         13496         -1475         1475         -1456         1475         -1475         1476         -1475         1476         -1475         1475         1475         -177         1475
-16225 60306 -13659 60090 -1433 1 1027 -1359 -1323 1 475 -1275 -1394 1 475 -1275 -1413 1 68534 -1433 1 1027 -1365 60090 -13659 60090 -13659 60090 -13659 60090 -13651 68587 -16861 1 1618 -615 1 4673 -10210 1 4654 -4763 -17259 68154 -1414 68582 -16861 1 1618 -615 1 4778 -11210 1 6156 -5449 -17224 68203 -16325 -16368 1482 -632 14784 -17127 1 6165 -5449 -17224 68203 -16325 -17084 1482 -632 14803 -13029 1 17327 1 6169 -1732
17135         88730         15516         85435         -16801         1618         -615         14673         -10210         1654         -4763           -17139         86933         -15877         85557         -16801         1595         -675         14794         -11121         1656         -5849           -17249         86124         -16146         85582         -16864         1462         -632         14786         -1272         1656         -5849           -17249         86124         -16146         85582         -16968         1462         -632         14786         1727         1666         -6309         -1704         17127         1666         -6309         -1704         -1726         1636         -1742         -1712         1666         -5849         -1740         -1726         1636         -1740
-17193 65953 -15977 65557 -16801 1595 -637 14754 -11121 1656 -5549 -17259 68124 -16146 65552 -16936 1535 -637 14754 -11121 1656 -5549 -17249 68124 -16146 65552 -16936 1482 -632 14806 -17276 14631 -16551 68189 -17284 1480 -17275 14806 -17276 1490 -17275 14906 -17276 14909 -17275 14909 14752 14909 14752 14909 14752 14753 -16654 68039 -17266 1501 -1183 1539 1599 14909 14752 14753 14909 14754 14757 14754 14754 14754 14754 14754 14756 14754 14756 14754 14756 14754 14755 14754 14757 1475
-17299 86124 16146 85582 -10804 1395 -557 14798 -17211 1055 -5549 -17289 86124 -16146 85582 -10805 1482 -632 14806 -12726 1663 -5459 -17289 86124 -16146 85582 -17084 1482 -632 14806 -12726 1663 -7459 -17289 86432 -16525 85685 -17084 1482 -632 14806 -12726 1663 -7459 -17289 86432 -16525 85685 -17084 1482 -632 14806 -12726 1663 -7459 -17289 17727 87333 -16684 86039 -17286 1561 -11827 15299 17323 3892 -14917 -17327 87333 -16684 86039 -17286 1561 -11883 15299 14017 6124 -12925 17529 87752 -16777 88124 -17189 87752 -17229 1603 -12251 15599 15693 -14017 6124 -12925 17597 8775 -17540 17597 8775 8775 8775 8775 8775 8775 8775
17242         86124         16146         85582         -16936         1535         675         47291         1839         6899           -17242         86203         -1694         1482         -632         1486         -12212         1839         -6999           -17289         86432         -1651         86895         -17084         148         -688         1790         -4459           -17278         87064         -16651         85878         -17180         1482         -683         1790         -4459           -17327         87762         -16651         86878         -17246         1483         1539         -1407         6124         -189           -17327         87762         -1674         86170         -17246         1501         -1407         6124         -1295           -17328         87762         -1674         8652         -1729         1603         -1401         612         -1295           -1737         8914         -1749         8776         -1726         1603         -1401         618         -1302           -1767         892         -1749         4176         -1235         1603         -1401         618         -1302
17242         68203         -16192         85572         -16986         1482         -632         14806         -12726         1663         -7459           -17289         8623         -16325         85686         -17084         1494         -688         14809         1790         -4450           -17276         87064         -16651         85878         -17084         1456         1182         1509         1790         4450           -17292         87763         -16757         86770         -17265         1501         -11883         15299         -1490         1790         -4450           -17592         87762         -1677         8670         -17264         16544         -12355         15595         -14017         6124         -1292           -17592         87762         -16774         86522         -17229         1663         -1674         -1292         -1467         6124         -1292           -17592         87754         1759         1766         1754         1754         1753         1769         1769         1769         1769         1769         1769         1769         1769         1769         1769         1769         1769         1769
-1728 86432 -16325 85695 -17084 1494 -888 14883 -13089 1730 -1432 -17278 87064 16551 85878 -17180 1456 -11327 15109 -13639 1733 -1491 -17327 87762 -16757 86170 -17266 1501 -11883 15595 -14017 6124 12825 -17392 87762 -16757 86170 -17266 1501 -11883 15595 -14017 6124 12825 -17572 87975 -17749 8652 -17229 1603 -12418 15591 -14018 6618 -13027 -17577 89124 -17495 87757 -17530 1603 -12418 15591 16504 14675 12823 13804 -17683 89450 -17401 87757 -17574 12812 -13504 16724 15022 -14188 -17827 89962 -17694 87757 -17574 12812 -13504 16724 15022 14678 -17683 99662 -17684 87757 -17574 12812 -13504 16724 16025 -17684 90083 -17682 87731 -17514 14677 -17457 17487 17487 17484 16752 14675
17276         87064         -16551         85878         -17180         1456         -1830         3173         -11291           -17327         87333         -16664         86039         -17266         1501         -1183         1529         -1832         3892         -11892           -17302         87762         -16757         86170         -17264         152         1529         -1407         6124         -12825           -17302         87976         -1677         86752         -1729         1603         -12418         15691         -14018         6618         -1325           -1757         88914         -1749         87159         -17289         4178         -1264         1650         -14617         6618         -13027           -17637         89450         -1740         8715         -1750         784         -1750         1603         -14018         6618         -1302           -17817         8956         -1763         1757         1757         1757         1756         -1392         1603         -14018         6618         -1302           -1782         8956         -1783         8724         1875         -1757         1784         -1584
-1732 87333 16864 86039 -17126 1192 1529 1539 3892 11992 11992 17399 87762 -16757 86170 -17246 1544 -12355 15595 14017 6124 -12925 17599 87762 -16778 86170 -17246 1544 -12355 15595 14017 6124 -12925 17597 8775 -17248 8759 1603 -17248 15699 14057 12593 13927 17577 88124 -17185 87759 17590 7844 -13251 15504 14677 12593 13924 17698 17690 87750 17574 17812 17597 87750 17574 17812 17577 17594 87750 17574 17812 17504 17597
-17327 8733 -16664 66039 -17265 1501 -11883 15299 -13823 3892 -11892 -17309 87762 -16757 86170 -17249 1554 15595 15691 14018 6618 -13027 -17292 87975 -17729 1603 -12418 15691 14018 6618 -13027 -17593 89450 -17401 87157 -17530 7644 -13392 16798 15021 15022 -14318 -13027 -17593 89450 -17401 87157 -17530 7644 -13392 16798 15021 15022 -14318 -17817 89785 -17830 87150 -17574 17812 13804 17644 16752 -17545 14673 -13400 17198 -15435 16285 -14588 -14675 17604 90083 -17862 87231 -17751 14472 -17457 174675 1746
-17309 87762 -16757 86170 -17246 1544 -12355 15595 -14017 6124 -12925 -17229 16717 6124 -12925 15595 -14017 6124 -12925 15727 87757 89124 -17185 87159 -17486 4176 -12551 16504 -14657 12593 -13927 -176757 89124 -17185 87159 -17486 4176 -13251 16504 -14657 12593 -13964 -17681 89450 -17401 87157 -17530 7844 -13382 16798 -15021 15022 -14318 -17827 89962 -17639 87150 -17574 12812 -13580 17188 -15524 16724 14875 -17694 87159 -17545 14472 -17467 1
-17292 87975 -19749 805552 -17249 1603 -12418 15893 14011 1124 -12825 -17292 87975 -17293 805552 -17293 1603 -122418 15891 14018 6618 -13027 -17593 89450 -17401 87157 -17530 7644 -13392 16798 15021 15022 -14318 -13027 -17593 89450 -17640 87157 -17530 7644 -13392 16798 15021 15022 -14318 -17693 89952 -17693 87750 -17575 14673 -13400 17198 -15435 15285 -14588 -17545 14673 -13400 17198 -15435 16272 -14318 -17694 80083 -17692 -17545 14673 -13400 17198 -15544 16724 -14575 -17604 80083 -17652 -17545 14673 -13400 17198 -15544 16724 -14575 -17604 80083 -17682 87231 -17751 14472 -17457
-17292 81975 -19749 86552 -17229 1603 -12418 15691 -14018 6618 -13027 -17577 819124 -17195 81759 -17486 4178 -17251 16504 -14657 15283 -13964 -17693 89450 -17401 87757 -17550 7844 -13592 16798 -15021 15022 -14318 -17817 89786 -17674 12817 17824 16725 -17584 87757 -17574 12812 -13504 16724 16725 -14586 47673 -17545 14872 -14673 1788 -15624 16724 14675 -17694 80603 -17682 87231 -17511 14472 -17457 17467 17467
-17577 89124 -17195 87159 -17466 4176 -12251 16504 -14647 17593 13964 -17678 89124 -17195 87159 -17530 7644 -13251 16504 15021 15022 -14318 -13027 -17683 89450 -17401 87157 -17530 7644 -13392 16798 15021 15022 -14318 -17817 89785 -17639 87150 -17574 12812 -13360 17694 15642 17645 16285 -14688 -17645 17694 87152 -17545 14673 -13400 17168 -15544 16722 -14675 -17604 90083 -17682 87231 -17511 14472 -13457 17564 15544 16753 -14746
-17577 89124 -17195 87759 -17486 4176 -13251 16504 -14657 12593 -13964 -17693 89450 -17401 87757 -17530 7844 -13392 16798 -15021 15022 -14318 -17817 89785 -17893 87759 -17575 17575 17574 16775 -13504 17084 -15435 16285 -14588 -14589 -17827 89962 -17894 87752 -17545 14673 -13480 17188 15544 16724 -14675 -17804 87083 -17868 87231 -17511 14972 -17457
-17693 89450 -17401 87157 -17530 7844 -13392 16798 15021 15022 -14318 -17817 89786 -17630 87750 -17574 12812 -13504 17084 -15435 15285 -14588 -17827 89962 -17639 87750 -17545 14673 -13400 17188 -15544 16752 -14675 -17604 80083 -17682 87331 -17511 14472 -17457
-1789 89450 -11401 6715/ -17530 7644 -13382 16788 15021 15022 -14318 -17817 89765 -17630 87150 -17574 12812 -13564 17084 -15435 16285 -14588 -17827 89962 -17894 87152 -17545 14673 -13480 17188 -15544 16724 -14675 -77804 90083 -17682 87231 -17511 14872 -13457 17765 -15554 16898 -14116
-17817 89785 -17630 87150 -17574 12812 -13504 17084 -15435 (6285 -14588 -14588 89952 -17884 87152 -17545 14673 -17480 1718 -15544 18724 14675 -17804 90083 -17682 87231 -17511 14872 -17457 17764 17687 87231 -17511 14872 -17457
. 17827 89962 - 17894 8725 - 17545 16675 - 13844 17894 15444 16724 - 14675 - 17786 - 16544 16774 - 14675 - 17786 - 17584 16773 - 13480 17788 - 15544 16774 - 14675 - 17788 - 15544 16774 - 14675 - 17887 - 17888 - 178
-17827 89962 -17894 87162 -17545 14673 -13480 17198 -15544 16724 -14675 -17804 90083 -17682 87231 -17511 14972 -13457 17265 -15554 18898 -14716
-17604 17682 87231 -17511 14972 17265 16564 16896 14176
-17884 90083 -17682 87231 -17511 14972 -13457 17065 -16554 1889e -14716
DISM - 00001 - 00711 (Chair - 2011 )

*	11466	4155	14833	6125	16564	17595	16340	8748	20399	0489	20858	22647	4034	26955	7135	-27718	3044	9657	0478	0521	30028	0.000	1500	200	30780	2011	5135	41.12	1320	1811	2312	2372	2490	3657	2587	45684	5817	3044	5214	2286	7453	46472	46467	5585	46789	050	45693	1371	45205	45213	45235	45281	45291	292	45300	(295
	]	,	•	21347 -1	,	'	24420 -1		,	-		29363 .2				36479 -2			40628 3		44764		54330		55576			57836 .4·								66190 -45									58518 -46				_			m w	n m		66072 -45	
	15079	•		`				• • •											•	•																40526 66										_	_	-	_	_						İ
ľ	7677				21004 -16																																											36 -39797				3.000.00 3.000.00 3.000.00				ı
3	ľ																							•	74 48593			72 50162				51451				55029							55841				5 55748		-,	7 55362		5 54596 54596	,		41	
L	ľ	,	'	,	58 -18304		31 .20067																													_											3 -44185				43775		1 2		٠	
L				- •	9 20558				•	•																		51001								56255		56570					57069								56404	.,				55189
-	ľ																																			-46238						47021	47012	47774	-47139	47034	-46083	-45812	45682	45690	75777	45773	45790	-45807	45818	-43823
S																																				72694						, ,	74299	74890	74843	74756	74001	73739	73611	73519	73059	72785	72549	72330	72132	C961./
æ	'	,	•	'	18941								-27367	-30983	-31297	22043	24000	35475	17863	.35780	-37081	-33710	-32539	-32461	-31911	-31790	-31665	-30887	-30681	-30461	-30311	-30232	-30204	-28744	-28529	-28423	-28367	28248	-28056	-27994	-27985	-27884	27851	277796	-27665	-27812	-27513	-27472	-27451	27457	-27471	-27487	-27500	-27511	27520	57637
٥	87324	87926	88287	90274	91520	96480	97000	97500	102110	102720	103570	113280	0	0	00	<b>&gt;</b> <	> c	o c	, c	. 0	٥	0	0	0	0	0	0	0	0	0	0	0	<b>o</b> c	0	0	0	0	00	) Q	0	0	0 (	<b>-</b>	0 0	0	0	0	0 (	<b>&gt;</b> (	<b>&gt;</b> <	> 0	0	O	00	00	>
d.	-17913	-18655	18906	-19932	-20420	-22541	-22795	-23035	-25058	-25274	-25631	-27938	-29820	-33684	34750	36784	37565	38708	38994	-39182	-42151	-45626	-46753	-46773	46312	-33939	-39438	-38280	-38068	-37853	-37735	-37687	37500	-37330	37272	-37247	-37230	-3/195	-37130	-37090	-37083	-37039	-37027	-37011	-36959	-36939	-36933	-36929	-2007	36010	36903	36902	36897	-36892	-36888 -36884	-2000
0	90483	92189	92732	95380	99640	101570	102160	102660	107070	107650	108350	113660	118000	12/4/0	120430	135970	138050	141060	141940	142460	152640	0	c	0	0	0	0	0	0	0	<b>a</b> :	00	<b>o</b> c	128800	126560	126020	125760	125290	124620	124550	124510	124200	124120	123970	123430	123210	123140	123080	22040	22900	22860	122800	122750	22700	122660	25010
2	-179671-	-18452	-18657	18526	-20928	-21752	-21972	-22167	-23910	-24113	-24417	-26409	-281/4	17717	32670	-34358	-34630	34655	-34592	-34474	-33271	-32027	-31082	-31004	-30747	-30686	-30598	-30196	-30088	-29928	-29801	20771	28549					-29101		-29008			-28916				28589		28488	28511			•		-28585 1	1
	88405	89727	80269	69/76	94250	06686	99610	09866	04000	104560	105210	10180	018011	<b>&gt;</b> 0	<b>5</b> C	o c	· c	0	0	0	٥	0	0	0	o	Ο:	0	<b>C</b> :	0	0 1	0 (	<b>5</b> C	0	: Ф	0	0 (	<b>&gt;</b> 0	) C	0	0	0 0	5 c	ם כ		0	0	0 1	, o c	, ,		, 0	0	00	) c	, ,	, manual
 									•		- ,																																													
×	272.8	278.5	2600	7 7 7 7 7	295.7	287.7	288.4	286 5	282.9	7.667	701 /	20707	205.0	202.0	788 1	297.1	292.7	285.9	286.7	286.2	284.5	288.1	295.7	297.8	295.7	296.5	296.9	293.2	285.1	283.7	284.5	287.1	195.4	282.9	290.8	292.1	185.4 185.4	284.2	295.1	87.8	286.4	204.2	305.5	309.5	304.2	300.4	285.9	277.2	255.7	221.1	172.1	27.8	90.3	55.7 74.6	န် ရေ	
- -	133.4	158.4	700	4 4 4 4 4 4 4 4	133.6	149.2	138.4	153.9	109.0	10/10	200	7.601-	205.0	105.0	908	193.3	208.7	224.3	212.8	223.9	37.4	245.9	37.4								67.4	•					0.47				,						58.1	- 1			-	-		15.1	24.2	
- 0	265.2	200																																													0 g					-27.0	en en	י מסיכ מסיכ	. v . v . v	
- {					142.8																									5- 0.14.			142.7 -4														138.3 135.3					61.8				
																																																				28.2		. +-		
╛					1052 28																																																	28.		
	,,,	, 0	, ,	- 4	Į.	2	2 5	2 5	- *		: =		. 2	12	12	12	12	133	13	13	£ ;	4	ភ្ជ មុ	ũ,	≙ ម៉	Ŭ.	ū f	5 £	2 4	5 4	26.0	200	17	17	96. 5	ě č	ģ	190	6	<u> </u>	i ĝi	196	200	Ŕ	207	27.2	. F.	217	213	213	234	2147	215	216	216	
<u> </u>	יט ל	s es	o co	· CV	<b>V</b> ····	œ,	۵ ،	v ox	o		ı on	***	· 100	ĸ	-	ന	2	2	**	en ·	···· v	e <b>r</b> 1.	n 4	י מ	n 11		· •	- u	* 12*	. ~			-	<b>.</b>								_	_													
الم	5 +	-	12	Ę,	14		e i	·	·	·	·		23.3				- '	27.2																													. un	54.3	54.3	54.3	54.3	5. 4. 2. 5. 4. 5.	2.40	54.4	54.4	
2768.0					2885.0				3085.0			3457.0				3515.0																				4323.0														279.0		282.0	277.0	281.0	281.0	
191	194.0	185.0	201.2	206.3	207.0	201.4	2001.8	1981	200 0	197.2	197.8	195.6	200.2	200.2	201.7	208.0	204.9	200.2	200.7	700.4	7 600	207.0	2000	207.0	207.6	207 9	205.3	199.6	205.2	199.2	199.2	201.0	206.8	198.1	202.0	205.4	199.9	199.0	206.6	200 2	206.0	212.3	213.9	7.67	240.3	2002	196.1	194.1	179.0	154.8	120.5	88.0 83.7	39.0	47.2	3.9	
44377	14392	44397	44417	44427	44452	44467	444/2	44512	44517	44522	44557	44582	44632	44637	44647	44677	44687	44702	44707	71/55	44.02	44933	44927	44943	44947	44952	44992	45007	45032	45052	45062	45067	45122	45197	45647	45252	45277	45302	45327	45352	45387	45397	45402	40417	40472	45507	45512	45517	45532	45537	45542	46552	45557	45562	45587	
189	2	92	92	67	88	69	₹.	<u> </u>	2	7.4	32	92	77	78	٤	8	<u>.</u>	82	3	\$ 5	8 %		E	2	ŝ	8	6	18	2	95	96	6	8	6	<u> </u>	102	103	2	2 2	þ	108	109	=		4 6	=	<u>‡</u>	116	=	<u>=]</u> :	÷	121	122	173	124	

	45.030	01704	457.73	45273	19269	32,22	45.19.1	-45177	45163	45149	45137	-45124	-45111	45099	-45089	-45077	-45066	45055	-45045	-45036	45025	45016	-4500g	42074	45515	-45641	45767	45823	45581	78004	6/704-	46633	46613	46685	46772	46811	46833	775087	47130	-47126	-47090	47122	47173	47773	47575	-47598	-47683	47858	48038	48250	A CAD / US	48807	48834	49165	49308	49378	48384
}	£5.07.4	0000	9/000	65873	70000	66137	66213	66286	66359	66435	66500	68574	66842	66711	66773	66840	66300	66965	67029	67084	67149	67156	6/24/	67333	67640	67728	67822	67866	198/0	50075	77799	58460 68460	68538	68619	68727	68773	68803	68909	69216	69266	69258	69285	95559	69637	70532	70637	70901	71379	71856	72419	735,48	73939	74505	75045	75549	75791	75779
ļ	30740	20744	11.760	38/11	3000	30824	39603	39584	39566	39548	39530	39515	39500	39485	39471	-39456	-39443	39431	39417	39406	38383	39381	2500	-33443	33333	00000	40070	40124	#0000a	40030	40720	40132	40928	41015	-41159	41243	41331	41494	41504	41499	-41458	41492	41433	41552	11759	-41768	41835	42030	42254	42528	42088	43240	13477	-43691	3873	3951	43959
N	5080F	50000	20004	50000	53044	54002	54095	54180	54264	54352	54428	54505	54582	54658								20700						22706			Secure						56495					56715		57001					0.000		. ,		52253 ~			63835 63860	
L	4377R	43778	01.01	43740	25757	43719	43703	43691	43678	43656	43655	43645	43833	-43623	43614	43604	43593	43585		4356/		40040						44494			44566			44856			45288			-45735			45758						40419			_	47433 6	_			47885 6
=	55114		27.77	•	5528G	,	_			_		•						·		1 18700		50400		Season a		10000		20133		56939		57084					57584 L				57875		580414			58720 -4		•	50000			,	ĺ		83146 .4		
-	45805	45803	45.80.4	45770	45747	45727	45708	45689	45673	45659	45642	45629	-45614	45601	45587	45576	45562	10000	42238		46505			45785		650039		46.153		46428				46855 (			47348					47579					47968 5			-48533 B		**	48937 6				49251 6
S	Ľ	71896				72181	•		•	ś		72654				72932			10100		72240			7.8850						74187		74415 -4		74564 -4			75034	·									76826 .4								30476 -4		806864
R	27458	27457	7453	7008	.6994	26962		, -	26948	, -		-26914						•	-,			Ċ	26780 7	,	_		-c0032 /		26851 7			26872 7		26879 7			26873 7		•			•		1	F~		26497 7		. ,-		26049 78				26.326 80		26324 80
a	0	0		2 0	0	0	0	0	0	ς <sub>γ</sub>	ς·	0	ς · ·	nyi i Dir	O (	, r	) r	, ,	) (	) f		, ,	. 0		10	10	9 0	4 G	0	0	ō,	0	0	0	00	ņ o c	0	0	ě,	o i	, i	, ,	. 0	0 .28	0 .2	o o	D 0	2 6	, ,	. 0	0	0 -28	0 .28	e c	9 c	3 0	0 -26
	-36819	6817	-35815	2 0	0	0	0	Φ.	0 1	0 1	<b>o</b> :	<b>D</b> (	0 (	<b>_</b>	<b>.</b>	<b>&gt;</b> c	<b>&gt;</b> c	> c	> c	<b>.</b> c	· c	0	0	0			<b>,</b> c	. 0	0	0	0	0	0	0 1	00	<b>&gt;</b> 0	00	0	0	0 6	<b></b>		0	0	0	<b>D</b> 6	<b>၁</b> c	· c	. 0	0	0	0	0	0 0	<b>5</b> C	, 0	0
H	122120 -3				18130	118110	3100	18090	18080	18070	13050	18040	118030	070	18010	200	117980	025	11796D	17950	17940	17940	980	117880	117870	17870	17850	17840	17830	117810	790	117790	17780	17770	17740	710	17690	17650	330	17220	150	17120	17080	17060	17020	17000	17000	17000	17000	16940	16880	320	16740	16660	116610	310	310
	ľ	**	4	28291 118		_		-28243 118		28221 118		26199 11		•			-28137 117	·		•	28098 117	•	28069 117	•	-28143 117	_		4	4				•		.26253 11/ .36253 117	•	•	•		28128 117	- +	28092 117	•	4-	~ ,	_	r- 4	•	-	-	***	- ·					
	32- 0	0 -28	0 -26	0 -2	0 -28	0 -28	0 -26	0 0	o c	iş e	5 6	S 6	27.0	9 6	2 6	2 6	2 6		. 0	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 -28	0 4	2 6	9 60	0 -28	0 -28;	0 -28	2, 62	2,50	0 782	0 -28073	0 -280	27951	275	0 -27757	0 -275	0 -27261	0 -27169	9-78-6	0 -27063	0 -27206	0 -27242	0 -27186	0 -27176	0 -271
Σ																																																									
	0.1	6.0	1.0	6.3	43.7	61.4	79.1	95.4	10.4	4.02	53.7	4 4 6	82.3	195.0	207.1	220.5	231.4	244.8	44	267.1	7.8	7.86.7	4.7	299.9	300.8	25	2.7	302.9	305.2	5.2	rō.	ιņ	5.	a	17		80	1.7	4 0	40	1 2	ښا ا	7	BD 6	9 1	· -	· •	6	4	Ø,	53	eç e	×ς α	<sub>တု</sub> ဇ	ာတ	တ	1
<u>~</u>				3.3				52.4		~ e	າ ແ				•																		306.1						288.4						326.9								8,585,8 0,460,8	•		•	2 -1.1
-,	4	`· Ti	2	6 11	1 28	× ×	o	200	9	- a	. a	5 8 5 8	. 6	i Ki	2 2	4	3 116	~	00	۲-	٥																1 -235.8													3 -151.	7 -142	7.021-	1,000	96.	94.1	-82.5	3 -187.
-		<b>4</b>	80	.7	-	the .	7.	- e	- r	- ur	) (C	o 100	- 6		9 60	2 40	8		හ	0												6 -286.3		. n	10		4 -379.1										-359.1			-333				-287		,	
Σ	φ ·							9		_		. 2		25	•	7 106			1 123													3 48.6		148	147		143.4											173.4		•		101.7	,	18.	197	197.5	-0.6
2								p of			·			15					.7																												374.8		358.5	347.9	343.1	321.00	3467	300	284.3	292.3	194.8
_	977	526	227	277	278	278	27.07.0	280	280	281	781	282	282	283,	283	284	284	285	285	286	2867	287	289	2907	2907	291	2917	2922	293	2947	7957	2962	2972	2962	2882	3007	3022	3047	3387	3422	3452	3487	3527	3630	3657	3672	3692	3712	3737	3767	3797	3857	3892	3932	3962	3967	3872
4																																																									***************************************
١	4.4	X i	. 55	54.3	10 I	24.2	2 2	54.2	2.2	54.2	54.2	54.2	54.2	54.2	54.1	54.1	54.3	50			54.1		54.2		Λ. αs			55		n u	8 5		3,50	8	38	57.1	57.8	10 C	71.8	72.5	72.7	74.3	7.52	80.1	80.1	80.1	80.1	80.2	80.2	80.3	90.4	90.6	80.5	80.5	80.5	80.5 6.5	91.0
	o c	77	9	0.89	1	2 5		•	•			.74.0	-69.0	-57.0	-65.0	-67.0	-78.0	-70.0	-710	-70.0	73.0	-73.0	225.0	0.000	1123.0	1367.0	1493.0	1832.0	2030.0	2903.0	2000	31610	3331.0	3560.0	3691.0	3813.0	3957.0	30830	3981.0	3856.0	3985.0	3976.0	3085.0	3866.0	3825.0	3815.0	3748.0	3672.0	3585.0	34780	3318.0	3210.0	3107.0	3000.0	2943.0	2923.0	
	* 4 5 C	010	2.0	18.4	808	4. 4. 5. 8.	8 8	77.3	82,78	97,8	108.1	117.8	127.6	136.5	145.0	154.4	162.0	17.4	179.5	187.0	94.3	2007	206.3	0.012	210.6		211.9	212.3	243.7	244.0	214.0	214.3	215.0	214.8	213.1	210.8	207.8	204.3	207.4	208.1	209.5	214.7	228.0	228.9	234.3	240.2	246.0	251.3	257.2	7203.7	2724	277.1	281.9	284.9	286.8	286.3	
1000	45867	43007	430(2	46177	75.07	40107	46197	46202	46207	46212	46217	48222	46227	46232	46237	46242	46247	48252	46257	46262	45257	7/796	18700	40204	40307	46312	46317	46322	4000A	46347	48983	46367	46372	46382	46392	46407	46422	48682	46787	46822	46852	46887	40927	47032	47057	47072	47092	4/112	47.137	47197	47222	47257	47292	47332	47362	47273	4.0.0
ţ	100		3	178		1	132	133	132	135	136	137	138	139	140	141	<u> </u>	÷	4	<u>\$</u>	<u> </u>		-	2	2		122	2		2 4	¥.	158	<u> </u>	160	161	162	163	15	166	167	<b>2</b>	198	1	172	173	174	47	<u></u>	, f		180	181	182	183	48	£ 18	5,00

П				ac o	2	3	9	7.1	87	2 2	113	122	129	2 4	235	228	219	230	263	310	340	396	473	529	567	700	142	י מי	4. c.	268	423	782	-883	-872	777	-804	-719	505	678	-626	-587	-487	434	263	
2			long.									_					R. I			. 5:	ort:	·	<b>.</b>	0	۸.,	~. *e	r ms	<b>45</b> -1	ത ദ	o ne	co i	າທ	: t~	en e	· 16	s ex	ø	en (	ಖ	ট যুৱ	- ©	8	Q 1	ପ୍ରିଲି	
>		Gauge 7	۵	ស្ន	5 5	5 5	220	250	308	8 5	608	440	457	80.4	462	432	402	44	50.5	47.	48	25. 1	464	48	3	4 5	<b>3</b>	60	8 83	22	79	5 85 4 85	80	8 8	n o	ŝŝ	\$	<u>\$</u> \$	2 5	3 4	55	190	219	3569	
Н		, Gar	hoop	<b>60</b> 5	2.8	2 19		5	37	4 30	- 60	04	4.7	200	9 89 -4 0	89	6	C# 6	0 6	. 8	-	3 5	3 8	7	42	44	38	<u>ښ</u>	မှာ မေရ	25	8	2 7 2 7 3 7	505	8	20 E	312	172	386	0 G	989		954	989	-830	
×			long.	,	.4.0	,	, ,	, -		<del>~</del> +	- 1	; <sub>4</sub> 2.	÷	<del>***</del> *		-	÷.			. 2	R	evi e	<i>1</i> ~	1 (/)	2	-		•	, ,	,	₹ '	i, i	s ep	eş i		7 57	ų.	~, ·	Υ '	7 47	~~	Ž.	Ψ.	7 7	
H		φ	٥	6	3 5	707	265	302	373	425 456	203	550	280	9 6	707	699	638	582	758	296	833	830	944	888	988	1037	1099	1122	1441	1161	1158	1099	1028	1026	1058	1077	90	1039	10/3	5 6	1098	1093	998	1016	
≥		<b>Самде 6</b>	doay																																										
>				on a	27 9	7 4	92.	103	126	142	38.	82	191	214	207	218	208	22	234	256	269	283	282	6	34	8 8	287	406	488	, %	-697	- 77	9	-94	an e	9 6	98	800	20.00	101	. 60 . 60	104	108	.40340	3
Ц			long	ο,	n e	y co	. 0	C4	<u>-</u>	9 9	1 2	: D:	8	<u>~</u> 9	2 =	. o	11	on i	<u>≒</u> ⊱	3.2	35	<u> </u>	~ G	37	5,7	ထွေးရ	5 60	63	22	4 80	91	2 20	7.	10	N 10	98	84	747	80	- F	- 9	22	92	1213	
⊃		Gauge 5	μοσφ	4 (	D C	2 5	. 82	32	38	4. 4.	r ir	, W	60	% i	2 72		8	i. i	~ 2	S ico	č	òri è	ði ði	5	Ç	2 :	÷ ;=	Ţ	4- ±		<b>.</b>		===	12	<u> </u>	7 2	12	\$ £	7 5	2 5	1 22	12	₩.	12	1
Н		Ö	ž	ecr :	2 3	1 %	. <del>1</del>	20	61	69	2 &	88	E)G	112	5 5 5	184	178	138 138 138	194	298	327	388	430	526	582	282	129	-291	412	-570	-603	-725	1003	1228	1236	1579	3787	9919	1060	3643	3667	4201	4486	14601	43.1%
٢			long.																																				·				,		
		4		0.	4 6	140	283	207	257	288	3 5	36.	375	412	20,413	298	271	8	343	319	336	322	308	280	231	345	483	547	594	630	636	946	634	751	60 6	1020	3551	11457	12623	1530	15290	16152	1667	17145	3
		Gauge 4	hoop	m	<b>47</b> 1	n &	. 45	· ra	ហ	e c	າແ	o oo	රා	OI :	m c	, es	4	go i	N F	- ¢	ජා	O !	h- 1:	- 52	2	** 5	n et	2	Ξ;	<b>- 9</b>	22	œ y	2 0	25	2	2 2	. g	37	₩ ;	2 ¥		. 16	82	126	-
ď			Ď.		e i	n u	३ चरें		ιņ	ů.	7 6	3, 2,	-50	-1	φ <u>ξ</u>	2	-21	-13	£. 5	-26	-23	57	ė, į	ķ	Ŕ	δ,	12	8	4	n e	-174-	6 5	7 77	-186	<u></u>	5 4 4	Ϋ́	ų,	Ċγεć	d d	∮ <del>₹</del>			7 7	1
Н		e	long	¢h.	မ္တာ	5 6	9 8	22	133	60	2 2	5 7	90	78.1		555	408	598	321	989	415	948	173	023	288	037	033	744	683	250	92	971	372	885	<b>4</b>	503 809	723	1157	8 5	747	679	503	836	63443	40
σ		Gauge 3	dooy		01 (	Ď :	- 40	i ç	58	\$ £	9 3	2 8	ő	137	167	196	197	195	1 10	27.6	å	37.	4 4	2 4	62	93	90	67	80 6	7 2	2	5 5	5 50	8	8 8	3 8	6.	80	67	à à	; 6¢	. 89	8	63	3
H		O	£	60	35	4 .	3 5	14	-44	95	Çä	Ç 49	-39	ιņ	.163	350	381	346	-330	504	-607	-866	-984	1209	1420	1657	2308	2545	2743	3275	3467	3928	6324	-6957	7232	-7614	7788	-5660	-5613	-55599 6558	-5529	5384	-5230	-5032	4000
g.			fong.										_																														0	0 (	_
0		Cauge 2	Ω.	œ	538	620	1683	2150	3135	4385	5518	8735	10894	14615	18795	22076	21923	22111	22337	31745	3470	4194(	4726	5919	6069	6956	7414	7524	7641	70643	8101	8385	9286	9540	9874	105670	13086	15651	15814	15968	16418	,			
Н		All strein gauges in microstrain Gauge 1 Gauge 2	hoop	0	<b>у</b> р ;	<b>4</b> 5	2 5	, p	80	476	ဍ	2 2	26	1.	24	<u> </u>	87	05	g ;	מ ת	92	59	සු	3 2	۳.	23	3.4	. <del>5</del>	177	2 5	35	225	333	2967	22	97.9	32	547	536	8000	9 29	55	145	-5384	8
z		ges t	long.	4		- ;	2 6	1 77	ř	र्च	5 G	න් ඊ	õ	7	ić i	n võ	4	ű	úr) u	ត រេ	o ob	ťΩ	47.0	n +-	-	ch .	no no	. 9	5.	4 2	Ç.	S,	ę ę	-73	₽,	žó gá	φ	şç	ζή i	gi, g	įνή	į	ψ	ùγù	Ų
Н		th gau	₫	ග	294	615	567	066	669	527	148	5 5	182	822	782	172	020	189	426	933/	1957	980	2974	25.13	3557	3977	3406	8	0549	1641	9609	1752	7520	0830	3470	108770	1470	0	0	0 0	<b>5</b> C	, co	0	00	2
æ		All strein Gauge 1 fong.	hoop			•			. 2	ტ.	4.	0 1	. 55	ŭ	₩ ;	3 6	23	22	23	N X	က်နဲ	ë	4.	er ry	60	à	2 2	<b>3</b>	F~ +	<u>-</u> Γ	. F	ec é	රා ජා	, 5	2	5 5	. 4								
		(R)		0	<b>*</b> 27*	ır.	er (*	3 v~	. 62	4	oo i	o r		2	s,	, (r	. ~	60	ao i	~ c	9 00	, ci	wn e	<b>.</b>	ڊيب	0	o, c	, ***	uņ -	0 1	برا با	c) i	N K	0	₹.	o r	4 5	4	00	s c	<u> </u>	نس <u>ا</u> خ	-	80	
×		op (MF	<u>Q.</u>	0.0	13.4	33	92.4	3 2	8 8	108.4	115.8	128	147	168	183	5 8	160	171	83	192	212	223	8	249	248	251	253.2	251	250.5	250.0	245	242	234.2	232	241	252.0	247.1	248.4	248	246.5	247	247.7	240	247	747
F		(МРаНоор (МРа)	hoon	Ø	7.5	<u></u>	100 C	) (C	0	0	2.5	m K	7 7	9.2	80 (	N 4	83	4.2	0.3	~ ¢	0.44 0.63	4	es e	4 <del>-</del>	- 0	0.2	25.1	iri	4,	£. 6	7.0	8.28	2.5	1.8	7.60	60 c	126.2	114.5	8.04	0.5	150.5	4 4	100	144.4	50.0
h			Axial	_	Ψ,	-	N N	ર્ગ સે	5.4∓	ດິນ	ŭ,	υά	· 1	άÖ	ão e	in in	, r.	œ	on i	en c	. 0	2	Σ:	5 5	: 0	Φ	21 1-		Ġ	4 4	, w	ų;													7
$\vdash$		ve (₩		9	1.7	₹	4. 0	n ir	9 0	5	0.3	~ 6	- e	7	<u>.</u>	t	0.7	<u>c</u>	r.	Q 4	i di	0.6	0.5	0.6	19.1	-61.0	97.3	132.8	-148.4	165.9	199.4	-209.6	228.7	230.1	226.3	219.5	245.6	234.5	261.0	271.1	266.0	271.1	-272.1	264.1	275.7
-		Ax_fo	ax-force															_																											
F	205a	press	ax-press	0.0	6.5	16.2	25.3	3,50	3.5	52.4	8	62.1	3 7	8	88.7	50	77.6	83.0	88.8	88.5	102.8	107.8	111.8	114	20.02	121	122.3	121	121	120	118	116	113	112	116	121.7	139	120	120	119	115.4	2 <del>C</del>	116.0	119	119.4
L	961205a	O**	з-хе	۳-	80	un -	ın ı	n, ur	i vo	60	6	ed 4	- <del>-</del> -	2	2	cri o	D P-	m	ω,	φ t	0,40	9 0	-0.5	- 0	n 01	£	101.5	4 60	6	173.1	n 16	218.8	238.7	2.0	236.2	E .	256.3	244.7	272.4	50 0	277.6	5 G	28.	275.6	7.7
5	p. 12:43:47 Progver.	rce (16		4	Ť	4	<del>ب</del> د	j c	φ	4	Ģ	₩ <b>&lt;</b>	7 "	7	7	Ψ, «	<del>,</del> 9	7	7	Q *	7 7	- ф	Ÿ	÷.,	, Ç	6	ģ;	33.	Ü	17	50.5	2.1	230	24.	23	22	25.	1 %	27	8 5	27	282	1	27	25
H	.47 Pr	å. K		0	<b>\$</b>	50	115	128	140	145	155	160	5 5	185	190	380	470	495	520	540	575	705	720	730	840	850	855	088	885	068	902	910	920	950	955	098	985 985	1090	1150	155	1165	3 8	1205	1231	1235
4	Jip. 12:43	Test time Force (10°Mx_press (Ax_force (Mxial																																											
		<b>7</b> P				0	0		5 0		۵	0 4	<b>5</b> C	0	0	00	o c		0	٥	<b>3</b> C	. O	0	O E		, C)	***	<b>-</b>	· •	***		_	ČĮ E	2.0	m	600	2 3	, Q	4	4	en e	5.5		0.7	6.0
۵	76.	measured measured measured Pressure (Force (kN) (Jisp. (mm) Man.		õ	ő	ő	c i	ci ŝ	oi di	ó	C	O E	si c	o	Ö	O 6	) C	o	¢	0	0 0	) O	0	0 (	<i>3</i> C	: (3)	Ģ.	ş Ç	φ,	<b>•</b>	<b>~</b> ~	ې	۽ ٻ	~ 무	ٻ	÷.	4 5	۳	Y	٠ ب	₹ 5	7 %	, ~		1
-	7 Pipe 997 ime	ed mek kN) Dist		O.	0	50	5.0	တ တို့ မ	o in	-16.0	-3.0	-13.0	2 5	-12.0	2.0	0.5	2007	0.0	-16.0	φ :	0 E	0.0	5.0	-111.0	) (2) (3) (4)	637.0	1015.0	1386.0	1559.0	31.0	1889.0 2081.0	2188.0	2387.0	20.00	2362.0	2291.0	34.0	47.0	2724.0	2829.0	76.0	2718.0	40.04	2756.0	2877.0
U	7 Pipe 01-13-19977 ime	measun Force (A			****	Ť	ς.		1	4"	•	<i>2,</i>	. *	• •	7	٠, ١	ī ·	7	77		, *		•	4																					ı
-		ured n		00	5	23.5	36.7	47.1	0 K	75.9	81.1	90.0	20.00	1,00	128.5	123.3	11 / K	120.3	128.7	134.9	140.7	158.3	162.1	165.2	174.0	175.7	177.3	175.0	175.4	175.0	174.6	169.4	164.0	162.4	169.0	176.4	172.4	173.9	174.2	172.6	167.3	173.5	168.1	173.5	173.0
[	Test	meass Press																						ഗ	p e								ф·	- G	· •	įΣ.		T 60	i α	Ţ.	¥ 1	io G	8 <u>m</u>	: 12	Σ
4	10.	mesaured measured measured measured Time Pressure (Force (kN) Disp. (mm Anar)		45836	45876	45936	45951	45956	45078	45981	45991	45996	46001	45021	46026	46096	46188	46331	46356	46376	46406	46541	46558	4656	46576 45676	4668	46691	46705	46721	46726	46736	46746	46756	46786	46791	46796	46801	46926	4638	46994	47001	47006	4704	47067	470%
-	Test SM				1~	[6]	41	ر داري	٠١٠	- [±0	6.	o l	: 1:	315	4	χη.	0 1	38	ಜಿ	sl	<u> </u>	2 2	Ä	22	36	: E	2	ş  :	42	21	<b>3</b> 4	48	<b>1</b>	5 2	20	ह्य	212	2 2	55	8	57	28	8 8	<u>تا</u> 3	62
L	[7]	[4] <sub>0</sub> [ <sub>0</sub> ]	ا ا	خلتا	Γ.	<u> </u>	لـــا		1	1		1	1	<u>"L"</u>	Ľ	Ш	1	1	1	Ш	`_!*	10	12	Ш			Ш	-1.		لــا		1			1.	<u> </u>	1.				1.		-	لـــــ	

Z	-413	-359	5	4	-397	-371	-455	-540	-550	508	994-	-528	-689	.1186	.1475	2179	2903	9226	10119	-11095	-11794	12368	-12527	.12567	-12864	-13614	-13651	.13713	-14161	14618	14877	14880	14886	0.00	15033	-15126	15269	15630
, ,	7647	8538	8926	10522	14699	15532	15836	15935	16018	16111	16195	16340	16428	16515	16562	16710	16818	17495	17579	17684	17741	17801	17941	18029	18162	18709	18786	18842	19251	19801	20020	20038	20098	20157	202.48	20340	20464	18518
×	-810	-760	-827	-850	-851	-935	.1770	-2971	-3784	-5128	-5731	-7479	-9894	-11785	-12573	-13433	13847	14592	-14666	-14875	14993	.15102	-15109	15109	.15253	-15528	15528	15563	-15760	15959	15040	16052	16067	16117	16149	16185	16238	36205
W	1033	1039	1047	1025	1125	1213	1277	1332	1422	1704	1943	2693	4366	6820	8621	11926	13336	15942	16100	16266	16367	16444	16578	16663	16786	17234	17290	17331	17627	17992	18108	18105	18128	18190	182.48	18305	18371	16981
^	-14855	14874	-15133	-15316	-15794	.17100	-17387	-17453	-17419	-17350	-17301	17369	-17406	-17440	-17392	-17354	17434	-17649	-17669	-17826	-17943	-18050	-18067	-18065	18198	-18445	-18453	18489	-18679	-18882	-18932	.18937	.18957	19010	19037	-19074	-19124	-19126
P	1237	1248	1247	1239	13435	18564	19033	19036	19079	19137	19193	19235	19230	19246	19269	19362	19406	19873	19973	20067	20123	20159	20285	20389	20491	20866	20933	20972	21238	21593	21695	21687	21709	21769	21823	21875	21939	20516
T	-14785	-14724	14860	-14905	-15231	-15537	-15771	-15983	-16003	-16033	-16015	-16164	-16326	.16464	-16467	-16528	16679	-17348	-17408	-17613	-17807	-17995	18050	-18051	-18234	-18770	-18782	-16819	-19171	19476	-19630	-19653	-19678	19748	19804	-19872	-19973	-19962
s	17579	17626	17746	17795	18409	19007	19307	19460	19534	19658	19734	19909	20046	20159	20228	20400	20542	21517	21670	21855	22036	22211	22410	22510	22712	23544	23623	23666	24213	24806	25061	25079	25107	25213	25313	25417	25558	21338
œ	-232	-288	-377	-391	-390	-520	-518	-523	-525	-528	-526	525	-527	-531	-533	-538	-540	-545	.544	-544	-544	-545	-546	-546	-546	-548	-547	-549	-548	-533	-545	-545	-545	-545	-542	-536	-526	-479
ø	62401	81951	61380	61278	62019	60691	60613	60595	60572	60551	60527	60511	60491	60467	60442	60330	60268	60153	60136	60100	60084	60053	60018	60001	59987	59935	59689	59236	59202	59182	59119	58883	58877	58871	58869	58865	58859	٥
Д	-4840	-4683	-5064	-5063	-5054	-5054	-2060	-5067	-5067	-5067	-5057	-5043	-5056	-5063	-5065	-5068	-5068	-5063	-5059	-5063	-5071	-5075	-5074	-5069	-5065	-5072	-5071	-5070	-5053	-5133	-5180	-5144	-5141	-5136	-5122	-5100	-5096	-3746
0	0	٥	0	0	0	0	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0	0	165090	164240	163810	162810	150530	135930	135820	192030	162940	172810	173640	173190	164280	190520	176760	0
z	-5321	-5275	-5272	-5275	-5244	-5327	-5390	-5404	5411	-5416	-5414	-5412	-5439	-5461	-5470	-5487	-5482	-5500	-5501	-5509	-5511	-5515	-5517	-5518	-5521	-5538	-5565	-5575	-5587	-5430	-5414	-5399	-5397	-5399	-5399	-5382	-5364	٥
×	0	0	0	0	0	0	0	0	0	0	0	0	0	٥	0	٥	٥	0	0	0	0	0	o	0	0	0	0	0	٥	165870	156160	146490	146250	146130	145820	145550	145710	0
7																																						
×	249.2	249.8	246.2	238.5	247.8	253.4	245.4	235.0	243.4	249.0	256.4	251.7	244.0	237.0	241.0	250.5	245.0	251.0	253.2	244.8	235.4	227.0	243.8	252.4	246.2	250.2	248.7	251.4	259.1	267.4	260.1	252.8	257.1	261.1	263.4	265.0	263.7	0.0
5	-1439	-133.3	-149.6	-159.2	-157.5	-144.5	-158.7	-168.9	-165.7	-150.8	-140.6	-158.1	-161.8	-175.4	-160.2	-146.9	-159.7	-166.9	-154.3	-175.3	-180.2	-192.4	-172.2	-162.6	-180.0	-167.2	-157.2	-167.7	-162.4	-156.7	-154.3	-151.9	-161.1	-161.4	-160.8	-159.3	-161.7	-223.1
-	.264.3	-254.0	-268.6	-274.4	-277.2	-266.9	-277.3	-282.4	-283.3	-271.1	-264.4	-279.7	-278.7	-289.8	-276.6	-267.9	-278.0	-288.1	-276.6	-293.6	-293.9	-302.0	-290.0	-284.6	-298.9	-288.1	-277.3	-289.2	-287.5	-285.9	-280.0	-274.0	-285.3	-287.5	-288.0	-287.2	-289.1	-223.1
x	120.4	120.7	1190	115.2	119.7	122.4	118.5	113.5	117.6	120.3	123.8	121.6	117.8	114.5	116.4	121.0	118.3	121.2	122.3	138.3	113.7	109.6	117.8	121.9	119.0	120.9	120.1	121.4	125.2	129.2	125.6	122.1	124.2	126.1	127.2	128.0	127.4	0.0
9	275.8	265.1	280.3	286.4	289.3	278.6	289.4	294.7	295.7	282.9	276	291.9	281.9	302.5	288.7	279.6	290.2	300.7	286.7	306.4	306.7	315.2	302.7	297	312	300.7	289.4	301.8	300.1	298.4	292.2	286	297.8	300.1	300.6	299.8	301.7	232.9
ir.	1250	1270	1305	1315	1335	1350	1365	1370	1375	1380	1385	1390	1385	1400	1405	1430	1445	1475	1480	1490	1495	1505	1515	1520	1525	1545	1640	1865	1890	1910	1930	2060	2075	2080	2085	2090	2085	2100
ш																																						
۵	4.	m.	<u>ක</u>	£.	2.9	63	4.	4.6	4.7	9.	20	5.3	5.8	en en	0.9	63	9.6	8.2	ලා සර	83	6	9.3	Q.	3.6	9	10.3	0.	10.4	10.7	11.0	**	14.4	£.	11,2	11.2	£.	113	11.2
u د	2758.0	2651.0	2803.0	2864.0	2893.0	2786.0	2884.0	2947.0	2957.0	2829.0	2760.0	2919.0	2919.0	3025.0	2887.0	2796.0	2902.0	3007.0	2887.0	3064.0	3067.0	3152.0	3027.0	2970.0	3120.0	3007.0	2894.0	3018.0	30010	2984.0	2922.0	2860.0	2978.0	3001.0	3006.0	2998.0	3017.0	2329.0
8	174.5	174.9	172.4	167.0	173.5	177.4	171.8	164.5	170.4	174.3	179.5	176.2	170.8	165.9	168.7	175.4	171.5	1757	177.3	1714	164.8	158.9	170.7	178.7	172.4	175.2	1/4	5 P.C.	4 .	187.2	182 1	177.0	180.0	182.8	184.4	185.5	184.6	0.0
4	47086	47.10	47141	4/151	47171	47186	47201	47206	47211	47216	47231	47226	47231	47236	4724	47266	47281	47311	47316	47326	47331	47341	4/351	4/358	47361	47381	4/4/0	47703	4/726	47746	47766	47896	47911	47916	47921	47926	¥7931	47936
-	3	3	6	99	Ġ	8	ŝ	2	٦	7.	2	7	7.5	2	F	<b>*</b>	7.	ဓ္ဓ	<u>-</u>	83	83	8	2	9	8	80	2	<b>3</b>	5 4	95	8	8	8	8	6	8	8	100

5. 12:40:36 Progver. 961205a										
(Ax_force (		All strein gauges in microstrain Gauge 1	icrostrain Gauge 2	Gauge 3	Gauge 4	გ 4	Gauge 5	Gauge හි	Gauge 7	
ax-press ax-torce Axial	hoop	hoop long. hoop	long	ol qoad	long. haap	long	hoop long.	hoop	long. hoop	long.
0	0.0	0			-	1	-			
0.0		eo ?			on (	44	53			
0.5		3 7			2 2					
0.0	7 28.4	568 45	682 100	2009	2 8	82 18	131	35 115	28 71	0 +
0		52			56					
٥		60			90					
0		65			65					
> 0		0 5			,,					
2 0		òö			826 60					
0		105			5					
0		112			112					
0		120			120					
0		129			128					
φ.		138			34					
<b>.</b>		140			136					
<b>5</b> C		797			99					
۰ <b>د</b>		5 £			19.					
, 0		193			210					
0		198			211					
0		240			214					
0		252			203					
0 6		273			167					
0 0		317			108					
> c		243 158			4 4					
: 0	.0 200.8	2 40			-55					•
0		29			-24					
o		7			44					
φ.		16			-37					
Φ 6		26			-29					
<b>.</b>		88 2			န် န					
<b>5</b> 6		3 6			66.					
		2 6			- 14.					•
· C		Ę			785					,
. 0		54			386					
0		φ			47.1					
. 0		135			- 54			,		
· c		200			345			•		
) E		600			Crack C					
		60.			933			•		
0.0		8,			-828			,		-
0.0		63			-1017			•		
0.0		96			-1105			Ì		_
0.0		251			-1207		•			
0		484	•		-1300		•	•		_
3 0.0		538	•		-1398		`	•		
8 0.0		510	•	0 0	-1508		-	•		
3 0.0		536		-	4770		•	•		
		7		>	-1729					

7	007	O N	819	976	5 6	70.	200	685	000+	LOCAL TOTAL	1017	1033	20.0	223
_ >	244	4	279	417	E 46	2 6	200	656	000	200	200	6.00	4844	4634
	27.0	0 17	211	278	27.0	0.00	714	271	380	202	202	264		2 0
×	1204													120
×	ĺ													. `.
>														
ß	l													66
<b>}</b>	816	2 6	000	898	876	400	200	1102	1128	100	7/11	1197	529	230
s	496	3 0	3	614	899	203	700	1354	1692	1004	100	2201	-4075	-4078
œ	.2060	1000	2.7	-2388	-2588	3356	200	4098	6637	7326	1000	3547	C	0
ď	G	o	•	O	0	· c	)	0	O		>	0	O	0
<u>a</u>	-1917	6000	2007	-2165	-1284	200	2	707	156	27.0	77	-316	-1504	-1479
_	٥		>	0	0	c		>	٥	c	>	0	0	0
_	503	240	7	695	537	266	1	0	110	100	3	306	0	0
z 	0	c	>	0	0	c	, (	5	0	c		0	0	0
ž														
<u></u>		. ~		0		•		-	~			•		
¥	3.797.8	3005	3	304.2	307.8	3112		9	314.6	314 7		313.5	Q	0
L.	143.9	465.2	2	147.0	148.7	150.3	1 4	0	152.1	150 0	1	151.7	6	0.3
-	0.0	C	5	0.0	0.0	00	6	> >	00	c	) i	0.0	0.0	00
Ξ.	143.9	145.3	9	147.0	148.7	150.3	ų ų	0.10	152.1	152.0		151.7	-03	0.3
9	0	С	٠.	0	0	0	•	>	٥	С	, ,	>	0	0
	385	390		400	410	420	307	200	440	445		200	455	457
ш														
2														
<b>-</b>														
-	208.5	210.6		213.0	215.5	217.9	228.4		220.4	220.3	340.0	0.5	c) E:	0.5
													46108	Ì
_	_			_	65 46							_		

age 18

T	***************************************		c	> *4*	u's	ė ;	- 63	0	17	21	ν α.	5	37	45	\$	9 5	146	178	209	243	308	341	380	6000	2 5	9	268	422	576	707	926	1151	1357	391	1399
]		guol																														,	•	•	·
	Gauge 7	Ç.	۲,	a Ç	27	<b>4</b> 0	9	79	8	\$ 5	130	147	158	167	101	159	4 6	2	83	8	2,42	0	63	တို ငို	9 69	89	ô	-23	e,	n s	140	28.0	140	138	128
	œ œ	doou	*7	- 5	20	34	ž 7 <del>.</del>	83	55	99	2 E	55	0.5	4	23	g #	3 4	23	63	172	: 8	83	8	<u> </u>	2 %	8	1.1	4.1	φ. (	p q	5 60	27	63	8	75
		buo			-					_			-	*	** 1		- 🕶		***		- +-	•	C4	ñ≩ r	ų <del>tii</del>	-				•			7	7	•
	Gauge 6		υģ	4	88	117	2 5	185	192	238	è 8	337	369	399	420	455	223	541	573	603	554	680	707	742	813	828	834	841	948	840	844	2	780	771	753
	Sau	hoop	e,	1 2	ø	- a	e 5	9	-25	<b>*</b> 5	D 00	2	6	4	2 9	2 8		: 52	155	163	ာ ဗွ	. E	8	go y	2 2	E	35	2	₽ :	₹ <u>©</u>	o go	90	5	65	S
		long.		•	***	., .	, 4	4,	4,	ω.	J 1~		ω.	~ :	;	2 5	2 2		#*	* ;	≚ Ç	#	¥# :	¥ ¥	\$ <del>}</del>	સ્	Ñ	33	4 5	ή¥ς	) (m)	ěξ	쓝	õņ	č
	ಕು ಕು		ď	5	72	128	122	202	208	257	318	368	405	439	462	4 25 A	574	58	631	663	721	748	778	916	88	606	910	917	922	638	965	995	1027	1057	1437
	Gauge 5	hoop	-	- 10	7	<b>v</b>	- 0	60	4	0 (	o ~	- Ko		+- (	ഗ	e e	5 6	; र	60	۰ د	4 (4	en:	ea :	7 00	- 00	cı	σz	<b>.</b>	0 6	o co	000	: EV	7	_	,
		long.	`,			* <u>*</u> *	- 42	23	Ň	٠ آ	ń in	4	ún	ép i	~ 6	36 E	2 00	8	255	290	3 88	8	4	Ö i	) 1	8	ő	25	i, i	n æ	1,00	-145	-173	-2031	300
	4	ē	4	7	32	57	3 62	94	64	120	, <u>r</u>	174	186	193	88 5	13/	153	128	139	88 8	5 8	35	ro i	<u> </u>	88	145	8	172	207	2 6	483	070	1537	778	000
	Gauge 4	doou																														•	,	•	C
		න්	J.	* \$5	25	<b>₹</b> £	25.5	61	63	7 2	8 8	133	178	232	65	21.2	4 65	38	30	<u>.</u>	-283	420	-583	48,	2145	-2645	-2755	-3067	-3169	3486	-3853	-4085	-4108	-3840	CFSC
	e	long	50	326	661	370	28	378	112	202	245	293	383	227	342	224	383	503	218	33225	335	34.	374	928	5.00	450	390	980	30	380	0	0	0	0	c
	Gauge 3	фооц		.,	•											2 5	24	37.	29.	80 6	3 24	47	23	2 5	6.06	50	106	100	41.0	132					
			ı,	4	25	4 4	3 2	59	90	2 :	2 80	85	9	8 9	1 9	- 6	30,	900	-653	853 853	-1171	-1331	-1517	2637	-3577	-4374	4518	-5039	-5234	8172	-7052	-8362	-9239	-9757	10.480
	c 8	long	2	. 65	533	9 7	234	481	1517	<u>.</u>	£ 7	33	78	88	7 8	2 43	2 8	98	89	2 4	2 8	88	32	- 4 - 6	8 8	90	70	6 5	<u></u>	<b>,</b>	, 0	0	0	0	
	crostrain Gauge 2	hoop	77	ຕັ	ùń i	go 4	- 53	4	15	20 6	27.	47	76	124	280	238	272	309	344	39412	495	552	626	4 8 4 0	1074	1201	1245	1303	1355						
	o mic		eq	, <del>2</del>	<del>6</del> 0	S 45	38	45	46	83	62 5	45	5	8 (	27	108	-258	.313	385	653 653 653	8 4	-991	1176	1452	3091	3927	-4082	4678	4920	6223	7249	-8748	-9877	10512	4100
	əbneb	long	7.7	- on	9	a a	2 0	Σ.	<u>.</u>	= <	> [~	=	ထ္ဆ	9 9	N:	- <u>c</u>	·	1.5	4	e c	9 00	មា	2									0	٥		
	All strein gauges in microstrain Gauge 1 Gauge 2	hoop	ç	8, 8	23	8 £	124	149	152	28	28.5	469	720	1149	1358	2017	25.15	2826	3087	35645	4475	4991	5641	2697	9655	10958	11359	11910	12392	15011					
	∢ 0	£																																	
	,a)			· m	₩.	m (*	) (C)	60	6	<del>-</del> -	e ex	en.	_		0	o 40	ນຄ	භ	ю	4 4	r un	90	an e	า๕	) (T)	es es	<del>-</del>	***	3 F	~ 4	. 62		63	7	
	oop (ME	hoop	Ç	11.3	15.4	27.3	38	44	48	g ရ	8 6	82	68	97	101	2 4	126	30	138	145.4	9	163	1,0	2, 2	187	184	184	182.4	182.0	82	185.3	181	176	172	476
	MPaHo	\$	<del>.</del>	3.8	8	G 4	18.0	20.2	9	7 9	5 20	37.6	39.4	7.0	9.9	2.22	60	88	85.8	67.8	 	7.6	න ( න	7 C	- 60	1.0	22.55	E 5	ا ا ا	0 0	31.2	6.0	138.1	16.4	5.5
	MAxial (	Axia																																	
	force (		77	.16	¥0 :	(A) 17	Ċ,	-	9	chi c ebi n	3 60	ξį	ဂို	ch 4	7. 4		. 5	ကို	-	Ú 4	, <del>, ,</del>	5	Ċi c	<b>う</b> ひ 4. R		-100.0	-111.4	131.6	36.00	-159.0	-170.7	-178.4	-193.3	-199.8	198.2
ū	5\$ (Ax.	ax-press ax-force	q	un:	4.5	13.23 F. 6.23	80	21.4	3.7	27.3	5 4	39.7	43.1	47.2	20 C	55.3	-	67.9	8.0	70.2	- e-	9.1	82.4	و در 10 م	90.5	9.0	68.9	500	B 75	5 60	89.5	87.5	85.1	63.4	,
961205a	Ax_pre	ax-pres	7		•			2	N	~ 0	i es	ñ	4	**	<b>₹</b> 14	ra in	60	60	Ø 1	F 1	, p.	ř~	ego (	io ec	i dis	æ	œ	eo t	x) ë	9 40	i ác	œ	æφ.	CO :	œ
	e (10*k		-	***	÷.	ζ; τ. 4. α	ှက	1.2	1.7	2.0	i ei	2.2	3.8	2.6	<u>د</u> دن ح	- 63	2.4	3.2	2	6 6 6	Ţ	1.6	2.6	7 K	75.5	104.4	136.3	137.4	24.5	168	178.2	186.2	201.7	208.5	20%
2. 12:20:30 Progver.	Test time Force (10"4x_press (Ax_force (Naxial (MPaHoop (MPa)		c	, Q	25	e e	i in	S.	52	0 5	3 25	8	105	5.0	ភ ក	130	145	တ္ထ	Q	165	. g	9	ر و و و	5 m <sup>2</sup> .	£	55	270	280	200	295	300	9	325	င္က :	Ć,
lip. 12:20:	est tim			17	.,		•	٠.,	•	,		-	=	÷ ÷	, ·	-2 \$2	. 42.	***	#	~ ~	. 🚎	<del>***</del>	ě. (	46	i cu	22	2	ř.	S 6	iñi	ř	'n	₩.	èğ i	5
	-																																		
	ъ €		n	. (3)	0.1	a c	rα	0	a :	o 6	3 0	0	0	0 6	<b>5</b> 6	. 0		5	0	00	: 0	_	0 (	o c	ניה)	60	en -	നെ	ng ne	. 4	10	ø,	P 1	į i	α
ne. The	sasure sp. (mr		Ĉ	Ö	0	5 6	i	o	C .	0 0	Ö	0	Ö	a c	<u>ت</u> د	0	Ö	Ö	0	0 0	įφ	0	Ö	s c	Ģ	Ģ	Q.	ထုံးဖ		ģ	Ą	φ <sup>'</sup>	Q.		Ç
9 Pipe 01-15-1997⊓me	ired mer		0 0		16.0	24.0	30.0	12.0	17.0	27.0	37.0	22.0	38.0	26.0	13.0	300	24.0	32.0	12.0	25.0	110	16.0	26.0	28.0	755.0	1044.0	1163.0	1374.0	1243.0	1660.0	1782.0	1862.0	2017.0	2085.0	2070.0
01-15	measured measured measured Pressure (Force (kN) Disp. (mm) (bar) kN mm		•	·																															
اللة يبد	ssured ssure (1		9	7.9	10.8	18.1	27.3	31.0	33.6	200	49.6	57.6	62.4	4.69	2 4 2	90.2	88.0	91.2	97.0	101.8	112.4	1147	119.4	29.0	131	129.0	28.9	27.7	125.4	127.7	129.7	126.8	123.4	120.9	7333
Test Date:			90	(S)	54	4 6 4 6	96	68	94	20 C	4	623	44	D 4	ž 4	2 B	*	68)	669	54	6	46429	<u></u>	e e	¥6	194	60	46519	# 0 0 0 0 1 1	8	46539	46549	994	0.00 Q2	16579
Test: ISM-01	measured Time		46239	46259	46284	46279	46284	46289	46294	46299	46314	46329	46344	48349	48384	46369	46384	46389	463	46404	48419	464	46434	46454	46484	48434	46509	46519	40024	46534	465	465	46564	46569	465
-121		en 5	2 =	7,5	₽.	4 15	9	F	<b>2</b>	2]5	ī	22	R	7 7	Q g	2 2	82	53	90	6	33	ĕ	£ 1	3	38	38	ş	7	1	4	55	46	47	<del>2</del>	4

AB			hanp																																										5 19172			
AA		Сянде в	leng.																																										1766			
2			hoop																																										5 1467			
>		Gauge 7	long.																																										9, 5			
×			фоор																																										1647			
3		Gauge 6	-bud		٣	7	₽ ;	\$ 52	45	83	68	2 :	6.78	39	28	5 5	32.	38	23	2 6	2 83	24	16	m	o si	e ÷	Ŧ.	3 13	-53	27	86 A	G.	-62	.72	80	g 5	f E	90	.107	113	123	110	126	-380	.361	360		360
>			hoop		٢	83	24	28 5	172	209	246	279	30,43	339	342	300	430	454	493	573	614	647	684	725	7962	827	852	948	116	1007	1096	1128	1181	1274	1305	1355	44	1419	1450	1496	1568	1613	1662	1585	1553	1556		1600
		ē 5	kng. h		٣	Ø	<del>2</del> ;	2.24	. 4 6	* \$	64	22	4 8	8	4.	-102	-95	06-	-123	384	-157	-171	-200	-238	-283	-585	-292	-334	-347	-351	-379	416	439	4 4 6	499	415.	-563	-573	-581	-596	612	-621	-644	5,569	563 563	-575		-586
-					**	¥	66	133	248	300	352	398	397	383	375	424	475	51.	** ;	3/5	677	712	745	774	840	874	900	1010	1042	1075	1138	1189	1230	1356	1387	1445	1533	1503	1537	1590	1671	1715	1750	22994	23543	23663		24146
s		4	toou roop		0	45	23 5	340	307	373	434	492	302	-52	128	787	.133	38	178	23.5	183	-188	-263	-361	4 4	-461	108	454	-467	452	-513	543	585	ģ 9 209	-631	623	-685	-717	-714	-717	76.	.759	-765	1566	1646	1612		1862
F			p long.		٣	35	£ 5	131	243	286	343	390	400	402	397	454	864	534	268	673	302	742	777	812	882	916	95	1056	1087	1123	1218	1250	1282	1412	1443	1501	1593	1563	1599	155	1726	1770	1810	3452	3630	3675		3925
0		9	hoop		7	39	ដដ	324	284	357	412	471	433	333	302	328	376	419	430	469	510	530	536	528	550	564	200	980	673	704	740	748	752	825	831	889	913	862	885	915	953	1001	1043	3335	3581	3643		3912
F			pud																																										1212			
Ê			фооц																																									•	3088			•
٥		Ail strein gauges in microstrain Gauge 1 Gauge 2	long.																																										27743 3			
z		ı gauges ir	thoop																																										1527 275 172 277			
Σ-		All streil Gauge	long.				•	~ ~	ı m	ı eō	4	ur u	u 4	-	-	.,	•		,	, -1	ŗ	,	ة نه	ņi č	Αų	e.	n e	, iù	*	e, i	ग्रं च्	Š.	ų, i	, Ą	κģ	φř		.7	1.	· 0	, ed	1.	ė,	in è	2 60	17		12.
Ľ		Pa)			٥	0	<u>د</u> د		, wo	7	e¢ i	o +		7	<b>4</b> 7 (4	, ~	2	₩.	e	5 <b>6</b> 0	4	en	-	n, n	, -	0	D 1		2	Pr. *	ę so	60		- h.	ss.	no r	. ~	803			. ~	5	an I	~ ~	<b>v</b>			4
¥		a Hoop (MPa)		dooq																																									318.1			
ſ		Maxial (MP		Axiat		2.3											2.3													4. t. E. a															7 ? ?			
-		Ax_force (		ax-force																												-107.7				-129.5			142.7			-152.5	156.2	158.0	156.0	-169.9		-163.0
I	961205a	) ssaud xt		ax-press	0.0	2.9	φ <del>ς</del>	17.2	21.5	25.5	29 4	33.8	34.4	34.6	34.0	36.9	42.8	46.1	4 6 6	58.4	62.0	64.9	67.7	74.2	77.3	80.2	20 00	91.8	85	984	106.5	109.6	112.4	123.0	125.9	134.1	139.4	136.1	139.6	148.6	151.5	154.8	157.9	158.7	153.7	157.0		160.5
Ö		arce (10*W		-	0.2	6.5	٥.	- 60	9.0	8.0	60.1	0 5 5:5	23.9	33.2	81.8	42.2	42.3	5	4 3 4 4 7	60.1	59.8	62.9	67.1	77.9	4.	84.3	59.1	*	96.1	98.2	108.8	112.4	177.5	128.1	131.5	135.2	150.9	145.3	148.9	159.6	158.2	159.2	163	165.8	162.8	167.9		170.1
£	09.21.51 Progver	Test time Force (10"PAx_press ( Ax_force (NAxial (MPa Ho			0	115	5 5	140	145	150	155	0 00	230	235	28 28 28 28	310	315	320	330	340	345	350	355	35.50	370	375	350	395	6	405	420	425	430	450	455	455 470	680	520	580	288	585	585	605	710	780	780		195
3		in in																																														
٥	10 10	asured 5. (mm)	_		0.0	0.0	0 0	000	0,0	0.0	0.0	o o	000	0.0	ф ф	Ģ	Ģ.	Ç, c	ģ ç	ę o	0.1	0.1	o c		ó	-0.1	ŞÇ	Q.	Ę,	۵ ¢	Ģ	φ.	n q	Ş	φ. 1.	- c	40.2	0.2	다 야 ?	, ¢	-0.2	-0.2	5.0	ခု ရ ဂ မ	9 6	8.0	,	ç, c
2	Jip 01-20-1997Time:	measured measured measured Pressure (Morce (kN) Disp. (mm)	ELIW.		2.0	0.0	0 <b>5</b>	3 0	5.0	8.6	18.0	1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	239.0	332.0	3810	422.0	423.0	9.00	555.0	601.0	596.0	629.0	671.0	779.0	814.0	843.0	914.0	940.0	961.0	982.0	0.88.0	1124.0	256.0	281.0	315.0	406.0	509.0	453.0	489.0	596.0	582.0	582.0	1630.0	658.0	1628.0	679.0		9.10/
83		ured mea. ture (bForc	Z		0.0								80.00			87.8					89.9																								222.3			
-	Pipe 11 Date:	Sured	(bar)		1739	4854	4864	5878	4884	4889	4894	4088	1969	\$974	5669	5049	5054	8600	3069	5079	5084	5088																							35499			
¥	1 Test: 2 ISM-01	5 measured Time	J.	o 6 €		लं है	, 2 - - - -	े हें च	ě	با چ			. % . %	,		·····		5 F		i se	<b></b> ,	35				32				43 35															29			

m	8487	1666	5145	1874	3872	3974	4893	6434	6838	7004	800000	1393	1591	500	0604	7050	63.45	8410	18584	17700	53888	36620	59295	59480	51846	55753	86054	73480	73505	73847	75297	81200	81553	26770	09956	08100	03450	03880	04790	32430	24500	58050	86160	66280	66920	171430	76810	
1																																														42996		
1	1					23414 -1																																									0	
Z	i																																													-41088 15	3285	
<u>}</u>	l																																															
ļ	1																																													200 250490	1	
3	1																																													67 .38200		
>	1																																													33 76687		
5																																_	_	.2548	72357	2775	2851	-2868	0 -2887	0 -3387	-333	-250	248	247	247	0 -24733	0 -243	
+	28482	35032	41232	42301	43562	43680	44489	44518	46997	47227	51358	53806	54145	54958	59197																							_			_							
U	2238	7004	1063	870	329	181	8 3	124	2 8	=	110	326	476	444	822	802	340	344	1383	1884	2237	2532	2970	6262	3371	3954	4009	4706	5073	5109	5315	609	6146	7168	7204	7961	8276	8290	8438	9547	9548	9712	9712	870	9688	9677	9991	
	5562	6000	15240	33686	34594	34718	35742	35913	30076	39385	44545	47464	47877	48800	53598	54998	29392	60171	80700	64187	69483	74060	78635	78877	82698	89259	89801	98290	102040	102590	105680	122200	124060	Φ.	00	o c	9 00	0	a	0	0	0	0	-	2 6	. 0	٥	
·	7000	7	0367	8905	8585	8446	8501	8476	0700	8523	8767	9010	9117	9108	9449	9455	9925	9931	n de de	10254	10703	10963	11315	11337	11648	12103	12147	12700	12956	12982	13126	13682	13735	14410	14437	14503	15048	15048	15151	16743	0	0	0	0 0	, 0	1 0	٥	
	40000	ואאחל	27547	34243	37440	37694	39314	39546	47454	43510	48723	51579	51984	52892	57618	58882	63279	64046	64224	67083	73544	77744	82215	82363	86195	92900	93430	101970	106540	107320	108220	0	0	Ö	0 (	<b>5</b> C	o c	0	0	0	o	D	ο :	0	> 0	, 0	٥	
ŀ	2	205	8271	7710	7225	7095	7134	7114	2007	7081	7286	7584	7689	7686	8144	8176	8770	8801	1799	0000	0.867	10232	10751	10771	11189	11825	11880	12624	12953	12998	13067	13942	14037	15807	16248	<b>=</b> 0	o c	0	0	0	O	0	0	0	<b>&gt;</b> C	ם נ	٥	
	× ×	31868	36150	37403	41532	41780	43220	43431	46375	47463	52994	56087	56536	57533	62858	64393	69212	70097	70216	14645	71011	85811	91031	91287	95800	103250	103840	113310	117980	118710	119330	0 677	0	0	0 0	<b>5</b> 6	2 6			0	0	0	0	0 (	<b>&gt;</b> <	> 0	0	
	1					1390																											4990	5832	5858	5504	7408	7285	7551	8960	8590	5379	5333	5268	5255	5300	5275	
					•	·																																										
	_	85.08	6.0	80.8	0.25.0	357.5	53.5	54.2	20.8	71.8	81.0	6.19	200	90.2	97.4	98.2	07.1	39.1	93.2	S .		0.0	79 W	0710	2. T. S.	13.1	32.3	135.6	137.6	129 6	140.1	449.6	44.2	441.5	448.3	454.5 1 54.5	553.2	4 00 F	53.8	456.5	159.1	448.6	442.1	438.6	644.9	454.B	14.	
	×	2.8	9.0	9.0		1 60	4.8	2.7 3	2.9	en e		1 P			89	5.8	7.7	1.1	4.2		0.0	D 4	e e	9 6				80		4.3	9 (				4.0	,			) <del>+</del>			5.4	-2.0	7.5	4- T	4.0	106.7	
		٠ د		on 4	0 =	178.6	3.8	3.6	3.2	***	S -	•			22	5.1	8.9	1.7	5.8	٠. د	19 I	N. F	2.0	- a	o 4					1.8	7.7	- P	3 4	28.1	17.6	12.4	0.0				221.0	222.1	15.6	208.2	13.1	223.1	106.2	
	-	•	7 -165.1																																						·	·	•	·		, ,	-0.6	
	Ŧ					172.7					183.4			188.5			-	_																													- 1	
	O																																														50 110.8	
	lå.	056	1130	1330	1545	1640	1585	1690	1745	1755	1750	2001	300	187	1936	35	199	201	206	208	212	237	222	128	252	877	240	253	256	256	257	259	2 2	280	2805	291	29.	286	ž è	32.6	32	35	34	35	326	35	3660	
	ш																																											_	-	<b></b>		
	٩	ç	ģ	0.0	æ :	~ *	2.5	23	3.0	3.2	80 a	4 (	2.0	n u	) F	, 4C	7	1.6	7.6	7.6											15.1									78.5			8.	34.8	34.8	34.5	38.3	
	S	1715.0	1723.0	1742.0	1778.0	1786.0	1783.0	1864.0	1839.0	1925.0	1875.0	1984.0	19/8/6	10867	10000	2068 0	1972.0	2001.0	1939.0	2028.0	2073.0	2058.0	2147.0	2088.0	2127.0	2156.0	1891.0	2288.0	22010	2211.0	2168.0	2251.0	2265.0	23810	2271.0	2217.0	2338.0	2213.0	2432.0	2320.0	2307.0	2318.0	2250.0	2173.0	2224.0	2328.0	1108.0	
	B	234.4	238.7	242.8	246.9	251.5	256.5	255.0	259.6	260.2	265.8	267.4	253.4	273.2	2.617	0.18	285.0	279.4	275.3	283.4	287.8	293.1	293.3	288.8	285.4	288.2	302.0	305.1	305.0	300.8	308.1	306.9	293.1	300.5	313.9	318.2	317.3	317.3	en r	317.7	321.4	314.1	309.5	307.1	311.5	3183	319.6	
	-	35729	35869	36069	36284	36379	30.50* 76.474	36429	36484	38494	36489	36584	36599	30504	20014	26684	36734	36749	36799	36819	36859	36914	36859	37024	37094	37134	37194	37380	17200	37304	37309	37329	37409	37839	37544	37654	37659	37894	37689	37709	37056	22476	38194	38269	38304	38309	38334	
	L	88	69	92	F	72	<u> </u>	<b> </b>	76	E	۳.	٤	2	<u>=</u>	<b>3</b> [8	3 3	ľ	3 2	22	88	2	8	91	25	8	8	8	£	î ê	8	8	101	<u> </u>	3 [3	103	<b>8</b>	107	108	ŝ	₽]:	=[:	[	<u> </u>	115	<b>‡</b>	E	118	

П					31	7.6	26	8 9	167	5	217	270	283	296	344	388	430	472	250	581	624	20 1	22.0	797	837	200	864	00.4	946	128	165	3 %	280	320	383	432	404 F03	53	558	1592	634	1671	1701	1685	1540	1657	1682	1715
A8			hoop																																													
¥,¥		Gauge 8	ģ		ඟ ආ	17	23	* *	3 ₹	47	er e	3 45	8	80 8	8 0	, g	77	æ ;	<b>3</b> 3	( 35	103	<u>.</u>	7 4	Ξ	12	3 5	÷	£ :	<b>*</b> *	, <del>1</del>	7	<b>*</b> *	15	₹. 15. 4.	- P	*** :	£ 4	9 42	\$	9	2 -	: 1	\$	= :	- 4-	: 🚅	7	2
H		ő	Buog		3 33	88	73	- i	128	146	166	207	225	263	2 2	374	406	439	47.7	537	576	612	687	726	760	(3) R3&	869	903	938	1008	1041	1105	1135	1168	1226	1258	17.84	1339	1359	1387	1407	1447	1453	1426	1384	1397	1417	1411
			peop		<b>-</b> 0"		_	m d	m h		₩.	x -e	· os	P~ L	o =	. 4	9	ø.	ry a	, <del>-</del> 4	8	ey s	<b>9</b> 63	e con	w :	⊃ g	9	go :	D 15	2 SE	4.1	<u> </u>	e e	œ 5	3 ==	2	£ 5	3 25	69	92 :	8 : 8 :	: 13	œ	5 5	5 5 5	18	2	60
<b>&gt;</b>		Gauge 7	long.		- C	, <del>;</del>	÷	= 1	4 %	. es	el) e	5 vě	4		યું વ	9	ņ	Ġ.	rý r	, 4	κů	wp s	ဂု <b>ဖ</b> ု	sκó	αĢ i	~ 1	- ec	<u>-</u>	en e	, up	2 9	7 7	2	<u> </u>	4 51	÷	7 7	. *	Ť	Ψ.;	ž š	ı Ç	ř.	स ह	Ş	jėņ	-342	Ÿ
×					8 4	70	88	80 5	352	174	198	243	560	287	380	420	451	486	526	280	634	98	748	790	823	820	931	966	1001	107	106	1169	1197	1228	1281	1315	1306	1343	1347	1366	1394	1503	1569	1575	1535	1552	1584	1632
П			фооц		<b>⊢</b> σ	- <u>6</u> -	æ	œ:	5 5	: \$	æ :	8. 28 82. 48	50	27	25	0.00	43	36	\$ 60 C	25.4	9	<b>3</b>	4.8	28	50	50 g	5 55	899	888	3 5	169	\$ 60 60 60 60 60 60 60 60 60 60 60 60 60 6	503	105	322	335	787	302	792	209	4 4	4	795	776	764	198	824	883
3		Gauge 6	long.																																													
7		_			8 8	8	83	<u>\$</u>	123	168	190	238	258	299	929	424	460	501	564	6.11	658	697	783	828	871	912	993	1035	1076	1160	1201	1238	1314	1354	1435	1481	1516	1592	1634	1698	1779	1901	3034	3312	3404	3392	3425	3483
Н		so	ноор		ф «	s Ž	60	24	82 ES	3 8	7.	£ 8	: 8	en f	27.	န် ဆို	35	5	8	3 85	4	.67	E 8	3 5	66-	ΞŞ	2 5	7.	145	13.0	180	-198	210	-230	7,52	-289	20.	5 E	338	406	459	362	-358	332	331	377	413	-806
٦		Санде 5	iong.					_							<b>-</b> .			~	<b>.</b>	~ -		Ni	~ ~	u m	100	ec e		vo.	r- +	~ 60	<b>80</b> -	eo vr	· ω	en 1	ກຍວ	. 69	ın ı	- 2	ł <del>*</del>	8	O t	- ø	op.	<b>6</b> 2 +	ey u	o 00	- 40	e e
-			hoop		5. A. A. A. A. A. A. A. A. A. A. A. A. A.	8 8	122	120	2000	24.	273	33.8	365	378	390	2 40	53	587	925	10.	74	73	80.8	25	978	101	5 5	114	118	7 6	130	£ 5	142	146	153	157	180 180	167	170	172	174	170	184	166	ž ž	2 40	184	167
H		4	ğ		89	3 5	<b>1</b> 4	174	208	278	313	346	415	8 :	406	48.	533	587	633	908	74.	777	818 854	888	5	28.5	1027	1057	1087	138	1157	1183	1245	1263	1303	1319	1347	1,400	1426	1477	1528	1748	1801	2016	2087	2032	2000	1885
S		Gauge 4	long.		\$ C	<b>,</b>	ıg.	₹	C4 4	- 0	19	<b>T</b> 4	2 (9	58 (	0,1	0 E	- 01	98	eo s	H =	. 86	<b>*</b>	ee 5	2 00	*	2 5	2 ==	8	2 2	3 %	22	3 30	. 49	9	2 80	25	Z :	ς <del>(</del> ξ	22	90	33	- 55	88	27	8 5	¥ 22	16	60
œ			hoop																																													
o		Gauge 3			4 :	6 6	124	154	185	248	274	310	378	89 ;	8	<u>ب</u> ج	60	63	94	S K	3 %	78	do é	2 40	9	32	3 %	5	63	23 6	53	65 K	5 5	8	5 6	88	8	¥ 50	=======================================	8	1 8	2 %	11	88	38	5 \$2	ę,	-176
H		Gaug	long		<b>3</b> 9	8 8	22	54	<b>%</b> ;	U 85	282	7. 52	3 8	63	6	2 33	26.	946	069	2 3	5 5	<del>-</del>	5 25	2 89	7	555	33.5	775	116	66	230	287	3 5	382	416	492	528	958 874	640	673	704	778	812	799	785	758	785	814
۵			hoop																																													1
0	.5	nge 2	à		57	123	157	196	235	316	349	380	477	S.	238	-570	4	-356	-383	404	516	-574	623	200	-695	-739	77.		-840	-923	-969	986	979	-987	886-	-1016	.817	, 50 P	737	-739	-703	20 4	999	-523	55	, 600 1000	2.	-75
Н	micros	An suem gouges in marchine. Gauge 1 Gauge 2	Song.		84.8	5 E	131	162	194	222	298	333	398	383	399	436	544	595	640	2000	758	800	847	233	984	1024	108	150	192	232	1308	1349	1431	1464	1498	1567	1596	1632	1693	1721	1745	1,65	1885	2507	2604	2557	2729	4033
z	2000	e spine	doou																																													
æ	cients	allen y	lang		53	8 7	148	180	217	582	323	327	428	. 82	m	¥	5 65	7	ğ	÷ ;	ú Xí		** 8	÷ α	i ež	ing (	io e	i eo	òn :	£ 47	, <del>(</del>	e -	* **	-23	F 7	, <del>8</del> 9	₹ 1	di Si	, g	.70	5.	222	5.6	-1002	98	188	-10163	-1061
Н	4	€ී	b																																													
7		(8°C	ī		7	· 64	,	9	τρι	<b>.</b> .	3 TO	٠,	<del>4</del> (C	,		e	<b>⊃ ¢</b> ≎	(E)	es.	t		173	eş e	D -	- 45		<b>-</b> €	. I~		တ္ေထ	i ed	<u>-</u> د	- ec	0	N.	- e0	4.	<u>م</u> د	vs	4	<b>60</b>	- 0		3.2	2.7	on ur	A SE	3.5
¥		(MPA)		роер	7	<u>6</u> €					48.6																															5	32.	318	34	3, 50	5 E	3.1
Н		H EGN			3.5	d d v k	4	4.4	0.6	2 4	# ## 86	13.9	10.1	0.4	.12.3	14.1	i ni	93 T,	Ď.3	en e	4 6	6	Δ, 4D,	<u>.</u> .	9.0	0.3	Ó.	i m	£	- c	6.5	0.1	÷ **	0.3	G 0	e en	ő	G C	90	6.0	0.3	<	8.0	0.3	2.4	es e	-10.2	-16.5
		(14) via	(Manager)	Axia 8	2	** "	· 17	6	60 (	<b>.</b>	11.7	60 1	~ "	2 0	5.5	we s	- 0	6	3.6	ر د ب	0 5	100	2.2	о 10 т	t wi	ιο (2)	on o	5 40i	8.0	ا دن د	-110.8	4 .	- Di	20	er o	9 =	5.1	9:4	n en	1 (2)	7.9	~ c	5 50	-153.4	4.6	89 Y	-152.5	70.4
-		åv frans	<b>1</b>	ax-press ax-force																																												
x		7 23004	) ecost	3ress	3.7	4. a	10.7	13.3	15.7	4 6	23.5	£ 5	30.7	31.9	33.2	37.3	4 7 4 4	60	53.3	57.1	200	66.8	70.7	4. 6	6.19	85.8	4.60	86.5	8.66	103.3	110.0	113.4	10.4	123.2	128.2	132.3	135.0	137.6	143.2	146.1	148.2	150.8	156.1	153	151.5	149.2	152.3	153.5
H		Tast time. Erons (40% to wees / to fore fill till (MPs Hote	) 2	3.0	0.2	5.6	4 7	6.0	2.0	ئ ئن د	12.2	85 6	64 Y	, Q1	3.5	53.7	2 5		6.5	9	53.3	70.6	75.4	28.5	5 45 5 45 5 45 5 45	39.3	80 G	2 66 66 68	02.3	65.9	15.65 6.63	19.4	22.2	28.2	30.9	40.0	41.0	43.6	47.3	51.5	54.4	2 20 2	62.7	80,1	88.9	53.2	69.6	77.8
g		7 8400	300																																												- 40	9
<b>.</b>		et times	e de la companya de l		Þ	\$ . K	1 6	38	04	2. £	. B	G ;	200	3 15	80	60	ē <del>I</del>	. 2	131	140	34. 1	\$	17	£ 5	£ 55	216	226	2.45	28	38	387	55	2 3	8	Ř	# 55 4 55	38	37	9 65	, <del>\$</del>	4	2 7	4 40	47	ភ	15 B	n un	8
		ŕ	<u>.</u>																																													
#		_ 1	-			0.0	3 6			<b>.</b>	2 0	c	0 (	9 0	***				_	_	· ·		evi.	ni e	N N	F4	٠, ١	i e	į Cų	cy c	ńα	N	es e	i tri	e .	e e	63	e 9	e e	9 22	7	**	च ५०	1 107	3.5	50 F	e 2.	98
Q		measured measured measured	osp. (mm								0.0																																		4	، پ	4 4	7
<u> </u>		m pain	3 E		2.0	0.88 0.08 0.08	07.0	93.0	102.0	115.0	193.0	128.0	122.0	292.0	475.0	537.0	533.0	531.0	559.0	601.0	631.0	706.0	754.0	762.0	849.0	883.0	938.0	7.00E	1023.0	1059.0	1156.0	1194.0	1222.0	1282.0	1309.0	1495.0	1410.0	1436.0	14/5.0	1515.0	1544.0	1562.0	1607.0	1601.0	1559.0	1532.0	1624.0	1778.0
٥		1 meas	W.								36.0																																					- 1
8		หะลรมกร	Fressure (bar)		uri	- (	7 4	2 00	- 22	82 5	7 B	37	7 7																																			
~		med			33421	33437	00440	33457	33462	33467	33477	33482	33487	33497	33502	33512	33522	335.49	33552	33552	33567	33587	33597	33607	33677	33637	33647	33657	33677	33687	33767	33717	33727	33747	33757	33767	33787	33797	33867	33827	33637	33847	33862	33897	33932	33877	34012	34027
L		4 3 .	<u></u>	m m	el=	~	-T:	1 10	4	ΞĪ	20 00	ह्य	z.l:	23 25	75	12	92	; [×	29	8	75	33.52	8	38	36	89																					\$ 5	
L									11			ئــــ				<u></u>									_	-						4	-							_								

8	1761	1784	1843	1864	1897	1943	2002	2001	2036	2048	2028	2004	2071	2043	2072	2089	2912	6943	12847	17591	20978	21015	21008	21092	22080	22944	24599	27366	27806	31681	32318	33424	35608	36391	36599	37184	37301	37340	37440	37529	37718	38372	39628	40255	41073	42675	44444	44767	45416	47930	49089	49207	A SANCE
AA /	-23	-164	-286	-354	424	7	-472	53.5	673	-607	-581	-570	-930	-853	-658	-702	Ç 07	2780	-8576	-9546	11435	11460	11465	11481	17621	12641	13820	15318	15613	18221	18678	19450	20888	21419	21581	21752	-22015	-22035	22042	-22075	-22200	22681	-23502	24077	24445	~25514	26696	26874	-27324	28683	29592	-29621	10167-
1																																																				49455	_
7	1																																																			-30148	1
<u>\</u>	ı																																												_							48377	
×																																																				-33218	
*	L																																																			52354 -3	ı
^																																																					
7	1																																																			50 -31427	
ŀ	1																																																			52 97250	1
1	1																																																			4 .37432	-
ŀ	1																																																			91504	.1
	35.	3 5	- 430	314	120	233	-1048	-2240	-4219	-6121	-6139	-6233	-6190	-0/51	-9548	-10066	-10408	-11984	-12239	-12692	-13143	-13135	-13141	-13078	-13174	-13487	-14557	-16010	-16345	-17986	-20963	-22401	23553	-26281	-26545	-27033	-27541	-27570	-27582	-27501	-27747	28088	-30585	-31502	-31892	-35175	-38280	-38575	-39776	-43689	45821	45749	-4598
•	4727	2116	4714	7296	15828	19335	29354	30771	32769	33717	34667	34685	34748	35366	36453	36713	36760	37799	38474	39363	40647	40204	40686	40768	40956	41286	43415	46222	46860	49912	55120	57638	59730	54564	65131	66012	67232	67341	67374	67566	67847	68294	73153	75060	77566	83210	91061	91854	95390	107960	109560	115680	116380
-	281	202	, s	-478	-2105	2761	4889	-5458	-6373	7174	-7173	7117	.7129	7825	-8846	-9114	.9283	10211	.11153	.11789	-12527	12523	-12518	-12456	-12563	-12961	-14454	-16255	.16863	18629	-22031	-23663	-24960	27908	-28179	-28734	29065	-29288	.29291	-29197	-29456	29813	-32413	.33357	-33/61	.37125	-40286	40576	-41733	-45409	45744	-47037	47214
-		4080	24271	27568	33501	35520	39764	41745	42489	42114	43058	43051	43105	43350	43788	43917	44051	45724	46315	47118	48270	48315	48296	48377	48569	48882	50949	54021	54749	58265	64419	67420	69927	75896	76454	77553	78382	79185	79226	79425	79762	80314	86278	88646	89669	98980	108920	109920	114160	130160	132130	138690	140510
-	2,1,0	707	7528	-7805	-8415	-8800	.10265	-10636	-11075	-11312	-11328	11328	-11285	11581	-12270	-12424	-12657	13550	.14247	-14643	-15064	-15048	.15048	14988	-15074	-15387	15/11	-17824	-18155	-19819	.22836	-24306	-25482	-2710/ -28180	-28400	-28908	-29198	-29424	.29426	-29370	-29575	29894	-32178	-33009	-33382	-36205	-38742	-38962	-39828	-42276	42484	φ (	0
ļ	_																																																				
		3.9.5	318.5	312.3	320.7	319.2	316.1	316.7	317.9	4.00	317.8	312.9	325.2	321.4	319.2	316.9	316.9	318.1	319.8	319.5	319.1	315.7	306.8	322.1	327.7	320.4	377.5	322.4	322.9	324.1	323.1	320.9	322.7	327.2	323.4	324.7	324.8	322.1	318.9	331.2	335.1	331.9	329.4	329.2	329.4	329.7	331.5	331.7	334.4	339.4	3461	347.9	347.6
		ica e	32.2	ńα	50.1	-56.7	64.0	٠.	-72.2	۰.	-52.9	503						4.85																		-154.0				132.6		-148.3	• ~	60		-173.6		<b>-</b> a	1823	4	~ 0	-170.7	s
	-	1.8.1	36.1	* 50	0.50	6.01	-216.7 -215.6	13.2	25.8	80 6	06.4 4.00	5.50	00.2	16.4	22.3	29.8	23.5	31.00 4.00	32.5	41.1	34.3	50.0	24.5	2 2	33.1	43.9													296.4	292.6	302.9	308.6	0.00	326.9	321.3	332.9	337.8	342.9	343.8	342.3	339.5	338.8	345.4
							152.7 -2										_	י א	5.65																						161.9	•		•	1.59.1	559.2	180.1	160.2	161.5	163.9	167.2	168.1	167.9
	_	·	۸.			220.1 15			235.7 1								•	- 1																							316.1				335.3	. 4 4.	52.6	57.9	358.8	357.3	354.3	353.6	\$60.5
				36 200			671 23																																													1796 1	
	4	න	i Ca	ati d	à i	æ	kt5 ti	6 60	1	P 1	~ ~	· P··	80	æ) (	no ex	2 60	60	co c	an o	a G	Ç,	≆ :	≥ ;		***	-	¥ ¥		: <del>}.</del> :	***	¥ ¥		<u></u>	** *		***	₩.	, y						-			. ~	Ψ	<del>4</del> -	•	•		
	<u></u>	~		•	n eo		e e	n un	o da	2	47 V	n un	sc.	ආ	5G ¥		*	٠.	<del>ব</del> ্ ০	n un	**	e.	ej t	d E	***	£.	on, ∈	e e	i ci	ιĄ	6.4	o au	69	ලද	3.0	4	1.	xo sc	1.9	o. c	. 0	.2	9.6	3.4	23.6	- F-	7.7	en -	28.0	. 2	£.	32.6	2.9
	اء	Ģ		ğ	Ş	•	o c	Se	ö	₽.	<u>.</u> .			<u>.</u>	- ~	ri mi	4	<u>ب</u>	acia ⇔	s es																									00	0 6		ο:	 	9	<b>6</b>	00	0
	اد	1859.0	1942.0	2001.0	21400	2201.0	2282.0	2225 II	2357.0				2089.0			2398.0					2445.0					2546.0						3102.1	л.	_ ,	3354	3 3244.0	3312.	3202.0		m. i	3161.0	4 3221.0	7 3273.0 8 3337.0		· ·	N α	3526	N	3485.			7 3612 6 3536.	1
	8	224.0	223.0	225.4	223.9	223.5	221.3	221.7	222.6	222.9	225.4	219.1	227.7	225.0	220.2	221.0	221.9	222.0	221.3	223.7	223.4	221.0	217.9	224.8	229.4	224.3	222.5	226.7	226.1	226.9		224.7			226.6		.,	227.7		231.9			230.7			233.			234.5			240.7	
	₩	34037	34047	34057	34062	34077	3,4092	74107	34122	34127	34137	34197	34252	34297	34262	34297	34307	34362	34372	24302	34407	34427	34482	34552	34577	34582	34587	34602	34632	34857	34687	34717	34732	34752	34757	34777	34782	34787	34842	34912	34937	34942	34952	34992	34997	35012	35092	35097	35102	35177	35187	35212	35222
		89	69	2	<u> </u>	2	2	e s	1	F	9	3 2	82	83	3	2 2	87	88	<b>S</b>	3 2	25	3	\$	8 8	3 5	98	88	8 5	102	Ę	2	9 8	6	108	103	ξ	112	2 3	1115	<b>£</b>		119	2 2	122	123	2 2	126	127	128	130	[2]	212	

lest 11

Г	Τ								ć	5	- E		9	8	8	30	: 9	, c	? C	0	· c
AB						peco					112380	1129	118700	1331	(722)	2000	2031	2460			
A.A.				Garson 8		loon	•		c	>	42867	42841	-44487	-48470	-57791	5,59.11	-60575	50727	-61463	-61253	-6.14
1 2					•				c	2	กรองก	97430	01710	12800	42870	54020	62870	56130	84700	89760	86920
-	-			,		hone			<	>			•	4	•			*	•		-
À				Garne 7	i i	tono:	¢.						Ċ		ľ	Ċ	163	.431	428	42765	.42862
×						pood	-		•	>	95360	95830	99540	109440	138340	0				0	0
3				Gaune 5	1				c	,	42320	42448	43605	46658	55437	58735	61258	61638	66890	67670	67979
-				Gat		long.			-	r	•	•	Ċ	•	,	•	•	•	•	,	•
>						COOD			c			•		•	•	•	·	,	••	3 222960	.,
þ				Gaude 5		tond.	,		_	,	-64711	44842	48412	-50386	-60283	.63605	-68022	-66345	70895	-71713	-72155
Ļ				U					c	,	0	٥	o	0	0	0	0	0	0	0	٥
-				4		hoop			c	,	0	0	0	0	0	0	0	0	0	0	0
S				Gauge 4	,	long.	•		_		_		_	_	_	_	_	_	_	_	_
ď						0000			_		_	~	Ū		_	~	Ĭ	_	_	Ĭ	_
o				Gauge 3	,				c		¢	C	0	Ç	0	O	0	0	a	a	0
H				Ça		Pool			0		710	10640	640	620	440	300	10090	110050	09650	09860	09430
۵						hoop			0		•	4	•		•						•
0			ostrain	Gauge 2		long.			_		-113	-113	-1140	-113	-112	-111	-112	-1123	-1099	-1075	-1385
z			Alf strein gauges in microstrain	0					0		0	0	٥	0	0	0	0	0	٥	o	D
H			in gauge	_		doou			0		0	0	0	Ģ	0	0	0	0	0	0	0
Œ			Alf stre	Gauge		Guo															
د																					
*					ip (MPa)		ra.		0.0	357.1	386.2	428.2	435.9	442.2	449.2	447.3	434.5	445.8	455.3	457.8	0.0
_		salts			MPa Hoo		hoop		0.0	80	-85.3	9.96	83.1	47.7	65.9	68.9	-63.)	-74.5	24.5	-8.7	-182.3
		Test results			(MAxial (		Axial														1
-					vx_force		ex-force		0.0	167.7	271.8	303	-293.7	-291.0	282 9	285.0	-273.5	289.8	244 4	.229.9	-182.3
±					y) ssakt		ax-press a		0.0	172.5	186.6	206.9	210.6	213.6	217.0	218.1	209.9	215.3	220.0	221.1	0.0
H					Time /scan Force (10*x4x_press ( Ax_force (MAxial (MPa Hoop		÷x.		0.0	175.0	283.7	316.7	306.5	303.7	295.3	297.5	285.5	302.5	255.1	239.9	190.3
9					an Force.				٥	7.	0 23										
4					Time /sca				1.5	12.	es	4.0	ŝ	80	7.0	8.0	9.0	10.0	11.0	12.0	13.0
=					,																-
H				ned	mm)																
٥				measured measured measured measured	Pressure (Force (kN) Disp. (mm)	TITLE T			4	c	2	~	ır.	h., .	· ·	c.	ς.	co.	-	an a	3
ပ				зеаѕигес	orce (kN	z			_	1750	2837	3167	3065	3037	2823	297	285	3025	2551	2399	1903
8				sured n	g) einss				¢	250	270.4	288.8	305.2	303.6	0 1	313.2	304.2	3/2	318.8	320.5	
H				red mea	Pre-	(PART)			**	Ç.	೯	4	so e	r i	~ 1	<b>a</b> C	on :	ę.	<del>-</del> :	2 9	2
*		,		เกอสรแห	5 Time	_,	_		,,									4	<sub>Y</sub> .		
Ц	-12	m	*	¥D	ø	^	<u>"l</u>	<u>* </u> =	F	72	끄	*	ا2	£ '	ÈĽ	اءُ	2	2	N .	*	