

Creep Behavior of a New Cast Austenitic Alloy

CF8C-Plus

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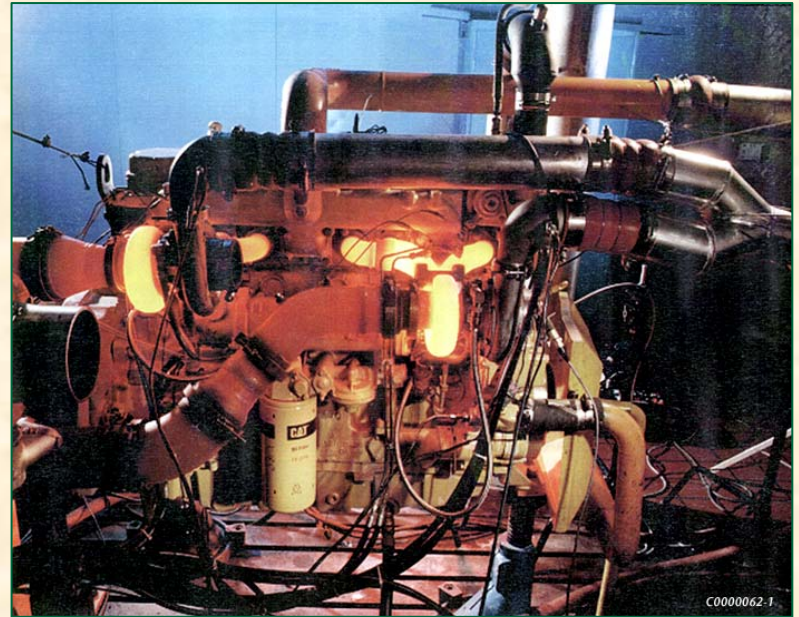
**ECCC Creep Conference
London, UK: September 12, 2005**

Outline

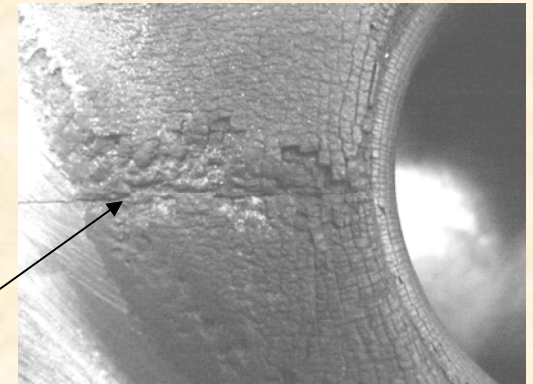
- **Development of CF8C-Plus**
 - **Materials Needs: Cost Effective Performance**
 - **Engineered Microstructure Approach**
 - **Casting Considerations**
- **Creep Behavior**
 - **CF8C vs. CF8C-Plus**
 - **Compared with Alloys of Interest**
- **Additional Mechanical Properties**
- **Current and Future Commercial Interest**
- **Additional Alloy Modifications**

Materials Needs

- **Increased Efficiency of Diesel Engines = Higher Exhaust Temperatures**
 - Load at Temperature: Creep
 - Start-up/Shut-down: Fatigue
 - Oxidation
- **CRADA between ORNL & CAT**
 - Unacceptable failure rate anticipated by CAT for SiMo Cast Iron applications
 - Evaluate New Cast Materials for Diesel Exhaust Manifolds, Turbo-charger housings, and turbine casings
 - Cast Stainless Alloy Development



*Turbo
Bridge
Failure*



Materials Needs: High Performance Low-Cost Alloy is needed to Replace SiMo Cast Iron

Some Candidate Alloy Compositions (wt%)

- SiMo Cast Iron: Fe-3.45C-4Si-0.6Mo-0.3Mn
- CF8C: Fe-19Cr-10Ni-0.07C-1.0Nb-0.7Mn-1Si
- CN-12: Fe-25Cr-13Ni-0.4C-1Mn-1.7Nb-0.3N-0.15S
- Ni-Resist: Fe-2Cr-35Ni-0.5Mn-5Si-1.9C
- Hitachi 20/20 – Fe-20Cr-20Ni-0.45C-2Nb-3W-1Mn-0.6Si-0.15S

Improving the properties of less expensive alloys without the costly addition of Ni offered the best opportunity

CF8C-Plus = Best Results

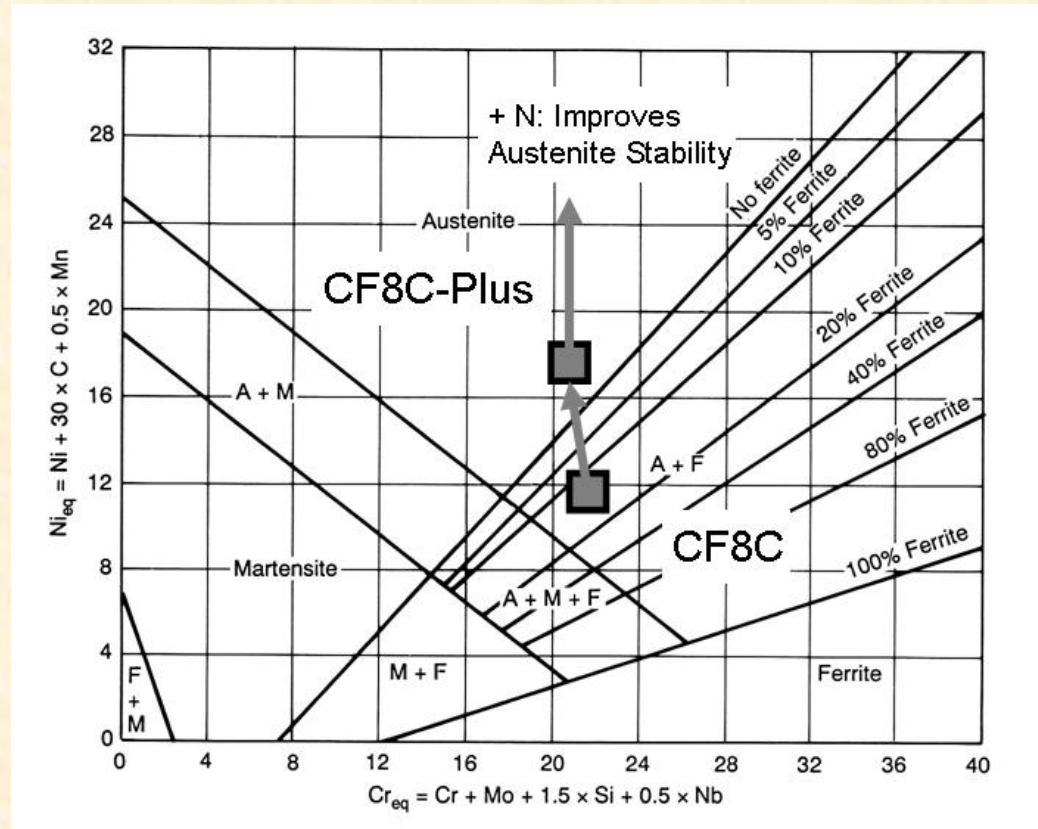
Nickel (LME), US\$/lb.



Engineered Microstructure Approach

- **Austenitic Alloy Design is based on achieving desired microstructure for High-Temperature Strength and Stability**
- **Additions made using ‘alloying rules’ developed using 30+ years of experience at ORNL**
 - **Reactant, Catalytic, Inhibitor, and Interference Effects**
- **Started with base CF8C composition (wrought equivalent = 347 stainless steel)**
- **Desired microstructure and properties were produced during the 1st year of development**
- **500 lb (1100kg) Commercial trials began during 2nd year**

Mn and N Additions can improve CF8C Austenite Stability

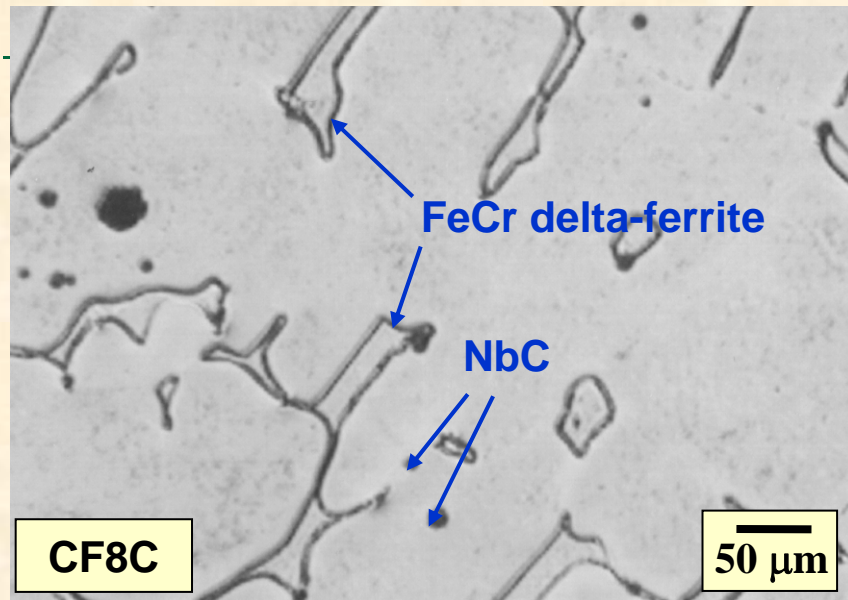


- Large Costly Additions of Ni are NOT needed for fully austenitic stainless steel
- **CF8C = 15% Delta Ferrite, CF8C-Plus = 0% Delta Ferrite**

Detrimental Phases can be avoided

CF8C

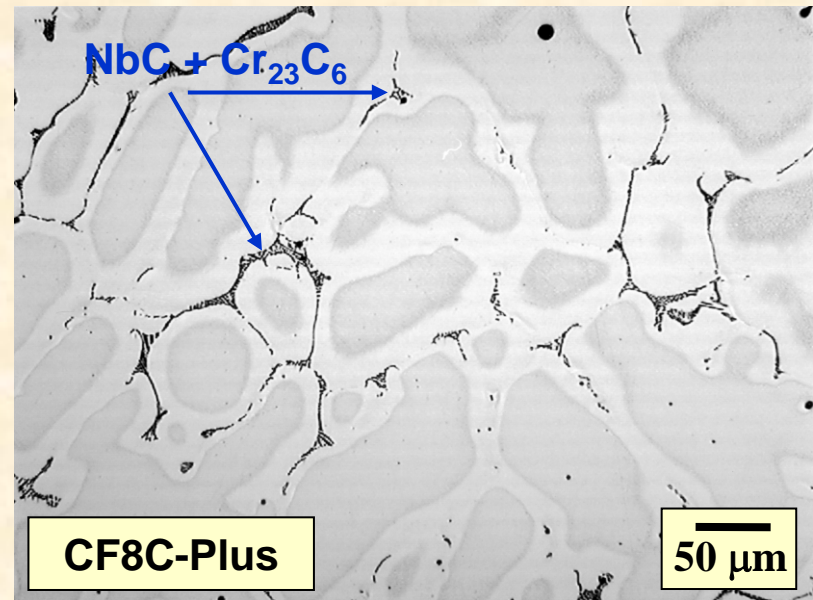
- Delta (δ) ferrite \rightarrow Aging \rightarrow Sigma (σ) Phase
 - Loss of Ductility & Toughness
 - Weakened Grain Boundaries



As-cast

CF8C-Plus

- No δ -ferrite
- Strong Grain Boundaries (mix of MC and M_{23}C_6 carbides)
- Fine stable MC carbide precipitate early during aging



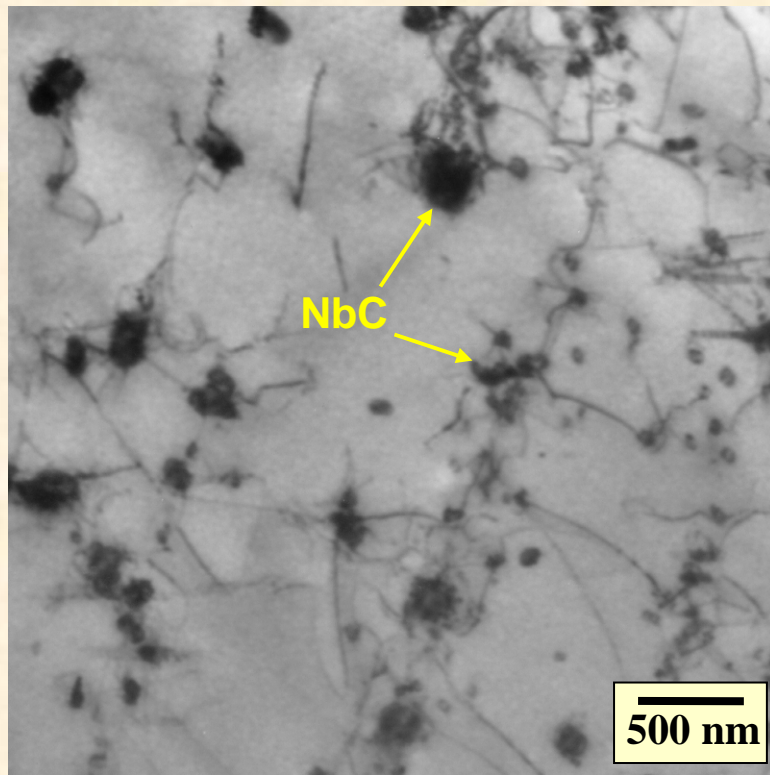
As-cast

(Optical metallography, polished and etched)

Nano-scale Carbide Strengthening

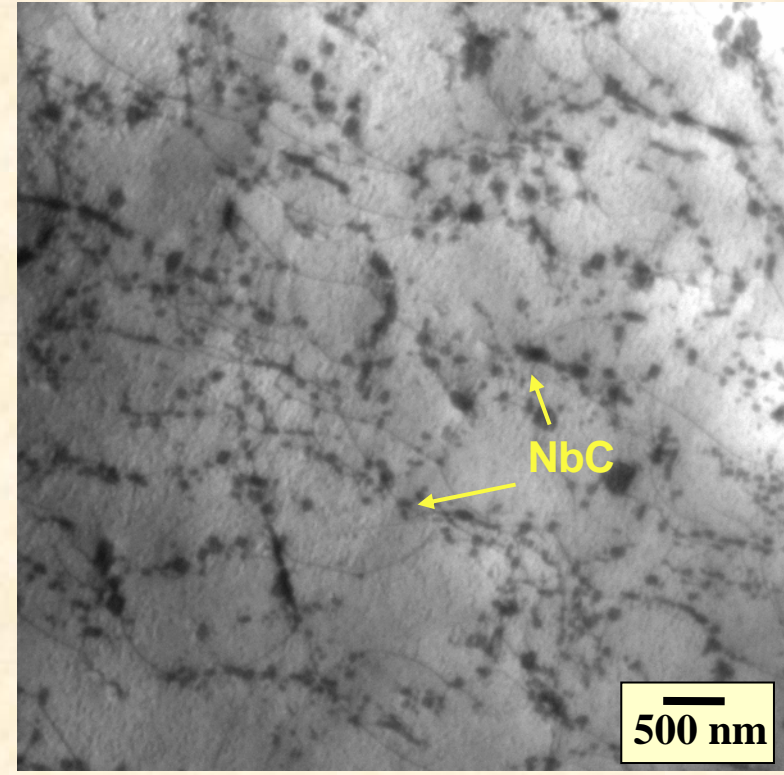
- CF8C-Plus Has “Super” Creep Resistance at 850°C Because Abundant, Stable Nano-Scale NbC Pin Dislocations

Commercial, Standard CF8C



Creep Tested **850°C/500 h**

CF8C-Plus



Creep Tested **850°C/23,000 h**

(TEM, as cast)

Additional Casting Considerations

- **Melt Fluidity:**
 - CF8C has Si to improve fluidity
 - CF8C-Plus has reduced Si, but Mn improves fluidity and shows as good or better melt fluidity compared to CF8C
- **Hot Tearing:**
 - CF8C is susceptible to hot tearing
 - No hot tears have been observed in any CF8C-Plus castings including components with cross sections ranging from 0.1” (2mm) to 9” (220mm) thick
- **Post-Casting Heat-Treatment**
 - CF8C is typically solution annealed after casting to homogenize structure
 - CF8C-Plus shows the best properties in the as-cast condition = process cost reduction
- **Machining**
 - Machining characteristics of CF8C-Plus are comparable to other austenitic alloys
- **Welding**
 - All weld trials have been successful on CF8C-Plus using commercially available weld fillers

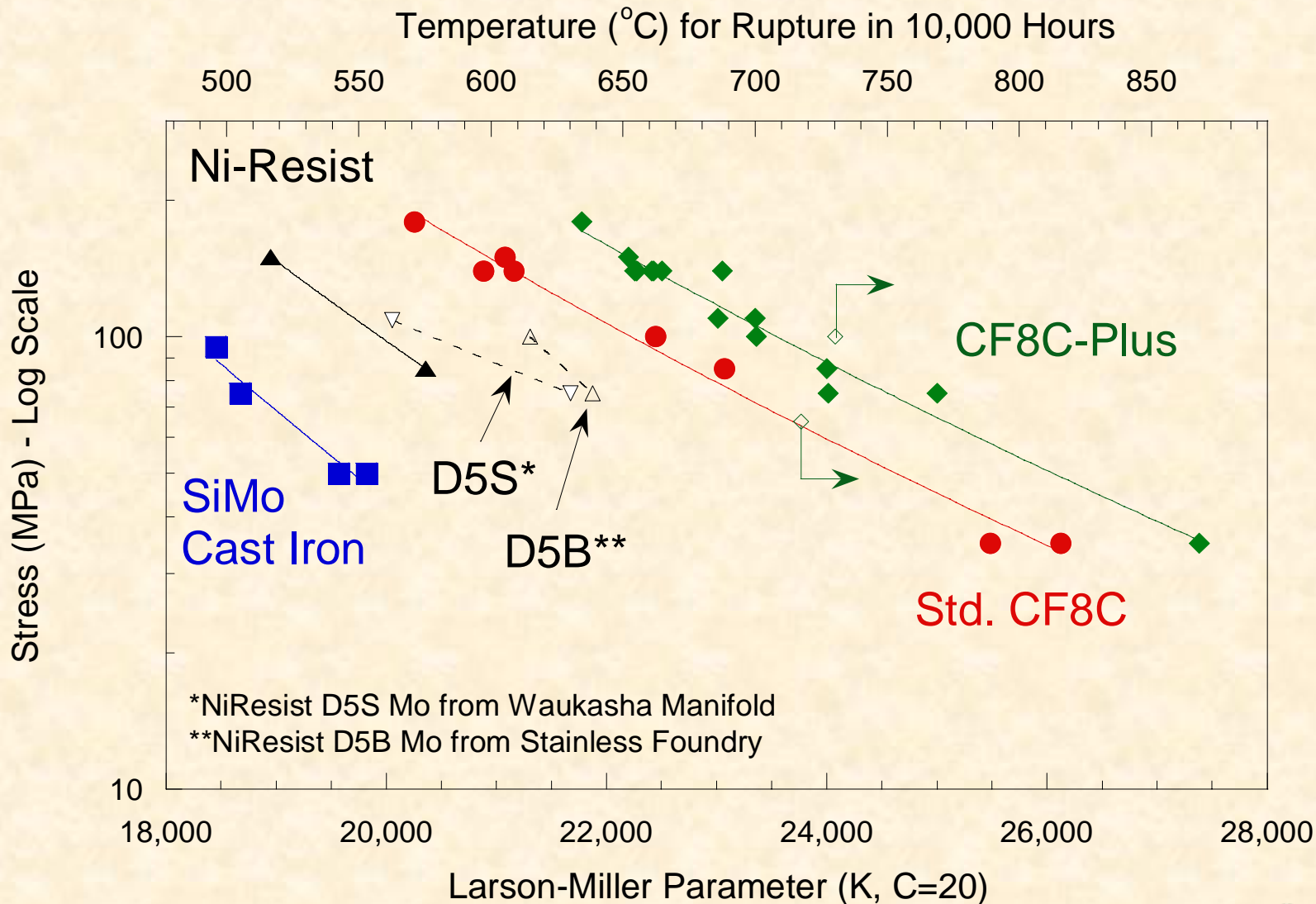
Typical Composition (wt%)

	Cr	Ni	Fe	Mn	Mo	Nb	C	Si	Other
CF8C	19.0	10.0	Bal.	<1	0.3	0.80	0.07	1.0	
CF8C-Plus	19.0	12.5	Bal.	4.0	0.3	0.80	0.10	0.5	0.25N
SiMo			Bal.	0.3	0.6		3.45	4.0	
Ni-Resist	2.0	35.0	Bal.	0.5			1.90	5.0	

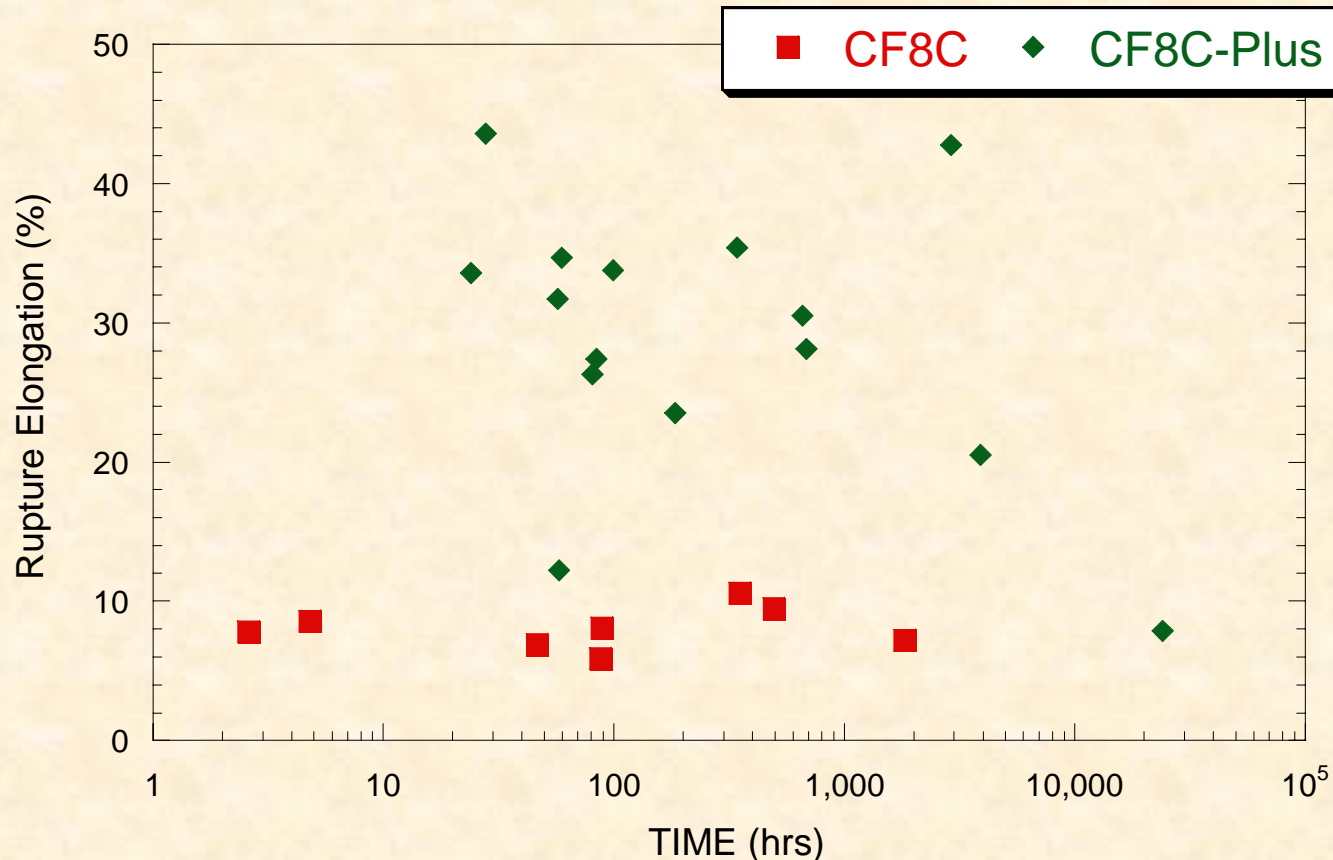
SiMo Cast Iron = Current Alloy of Choice for Diesel Applications

NiResist = Austenitic Iron used in some applications in place of cast iron (good casting properties – many variants)

CF8C-Plus has much greater creep strength compared to current materials and shows large improvements compared to CF8C



CF8C-Plus has improved creep strength & ductility compared to CF8C



Creep-Rupture Ductility for CF8C and CF8C-Plus tested at 650 to 850C and 35 to 180 MPa

Reasons for Creep Strength Improvement

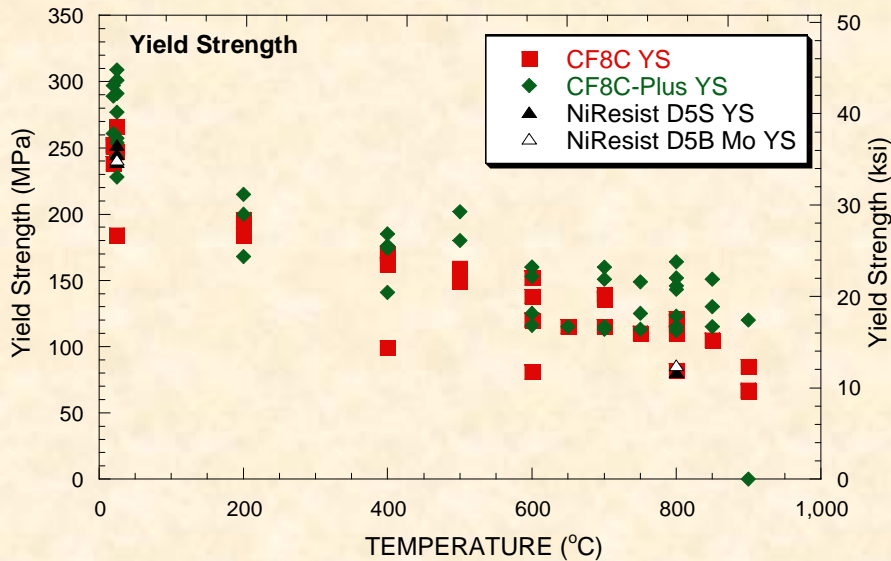
- **Fully Austenitic Structure**
- **Elimination of Deleterious Phases (sigma)**
- **N Solid Solution Strengthening**
- **Synergistic Effect of Mn and N**
 - Mn improves the solubility of N in austenite
 - Mn and N alter MC carbide precipitate structure
 - **Stacking Fault – Partial Dislocation precipitation mechanism (Silcock and Tunstall)**
 - **Rejection of Mn and N at NbC interface**
 - **Solidification differences between CF8C and CF8C-Plus**

CF8C-Plus shows improved Mechanical Properties compared to CF8C for:

- **Yield Strength at Temperature**
- **Tensile Strength at Temperature**
- **Tensile Ductility at Temperature**
- **Low Cycle Fatigue Resistance at 650 to 850C**
- **Thermal-Mechanical Fatigue**

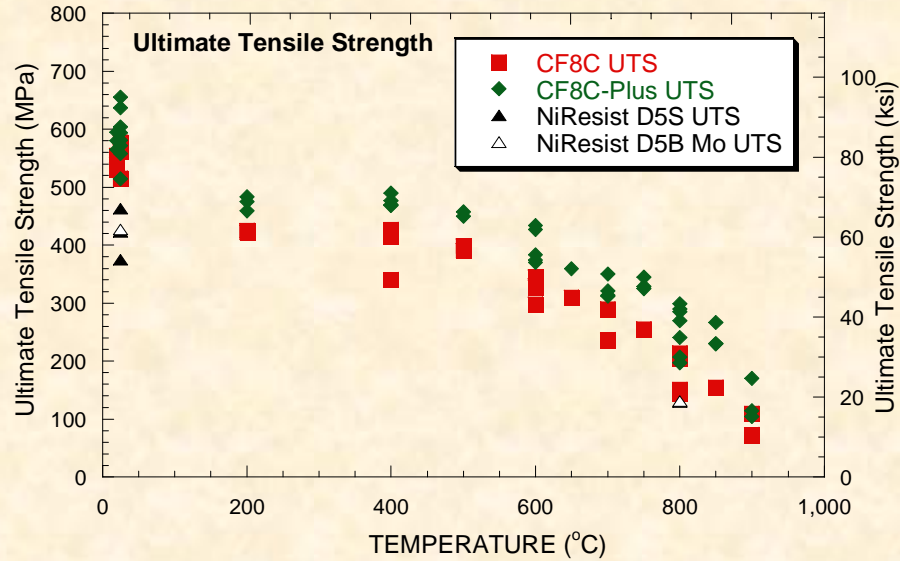
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400 800 1200 1600



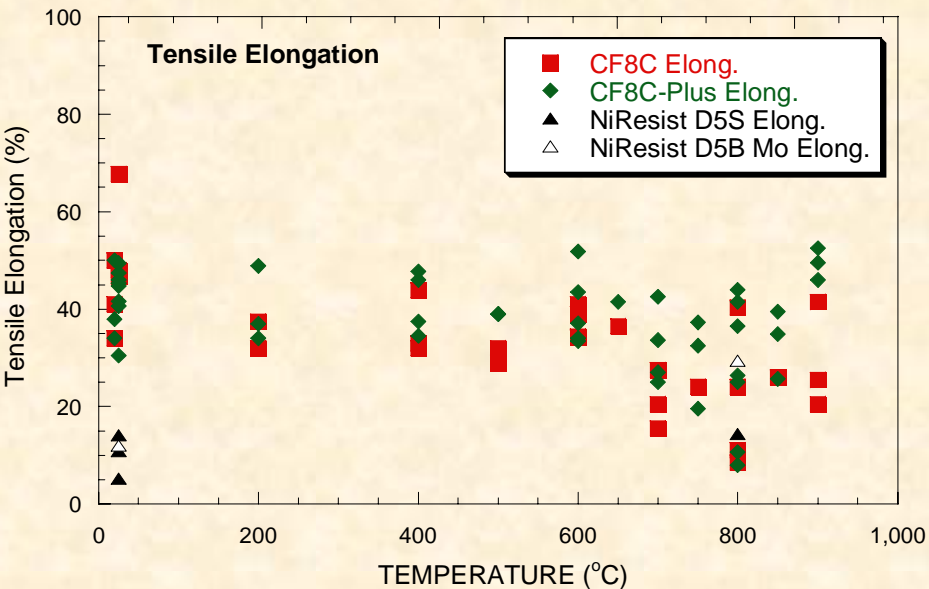
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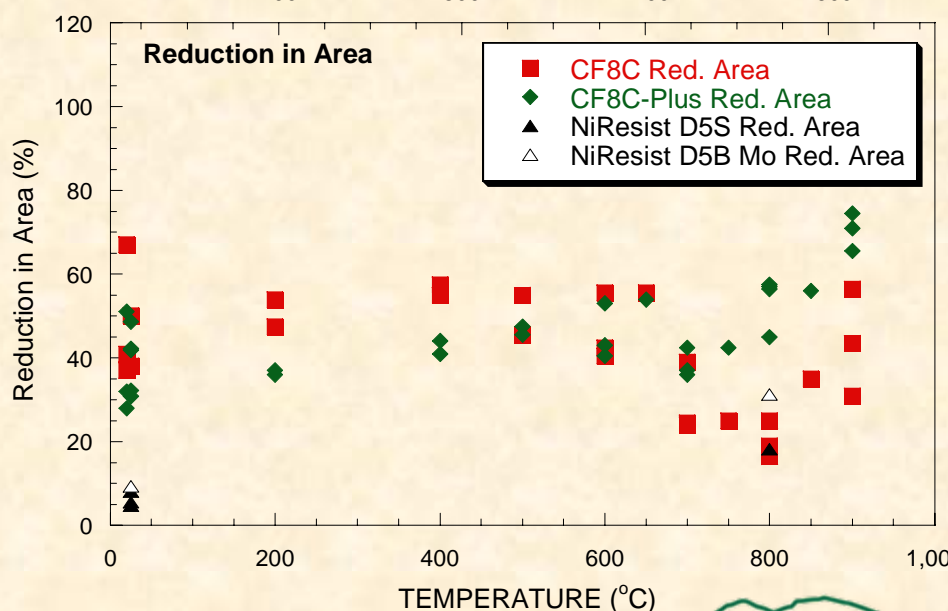
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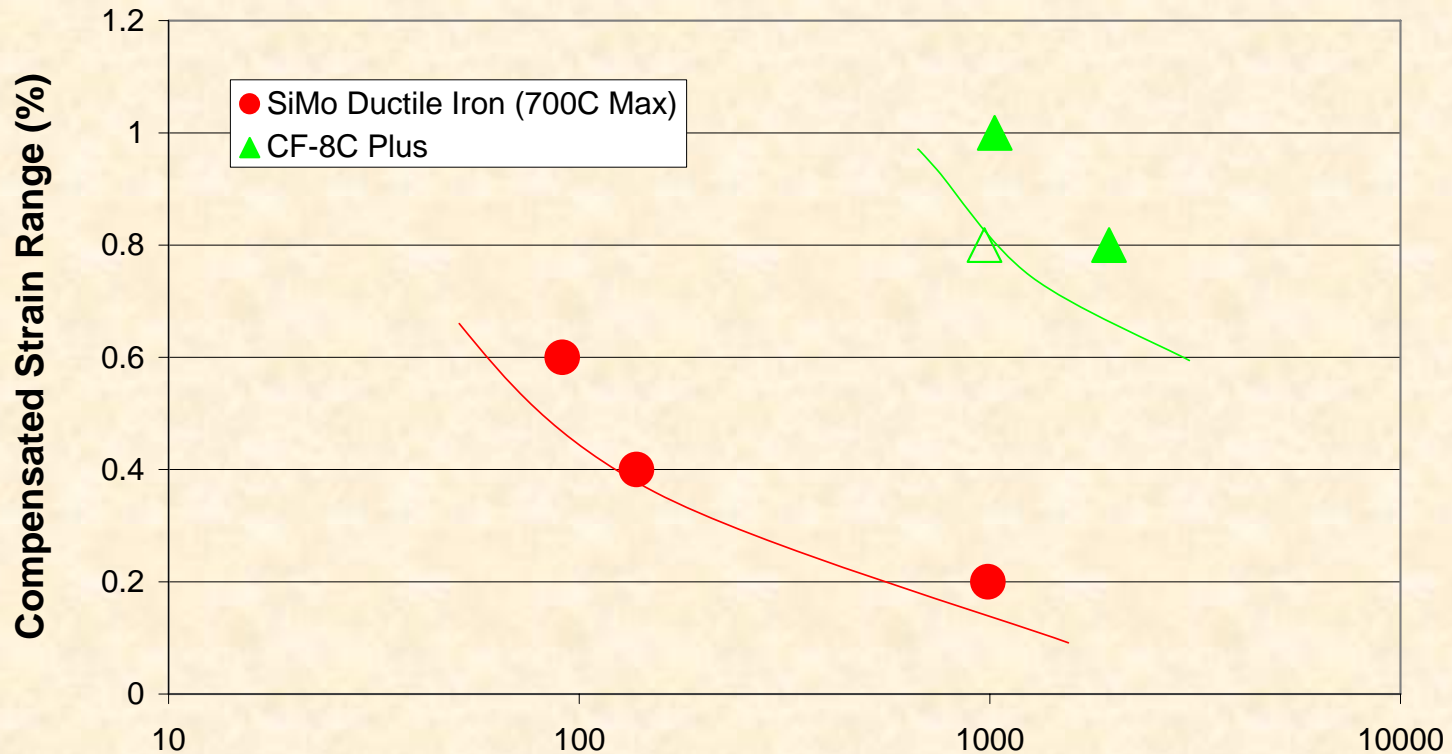
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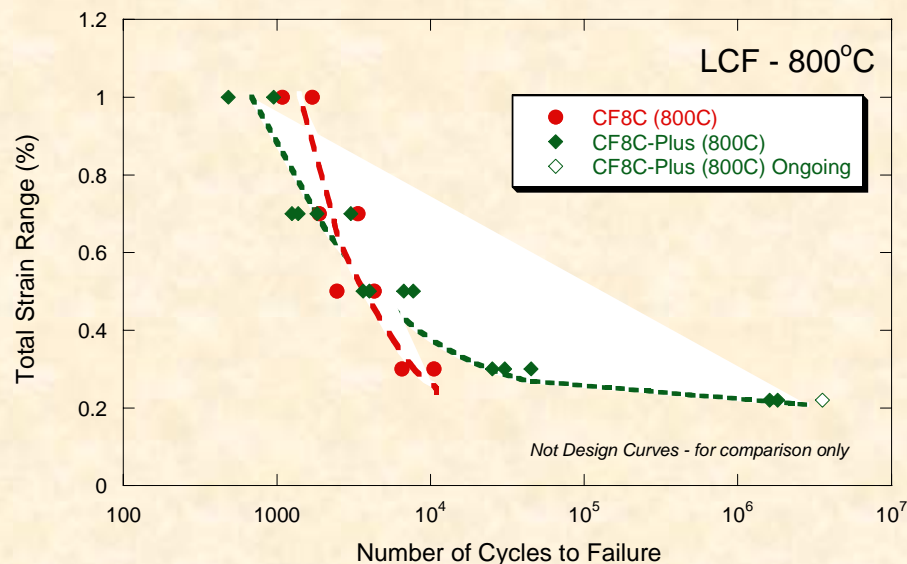
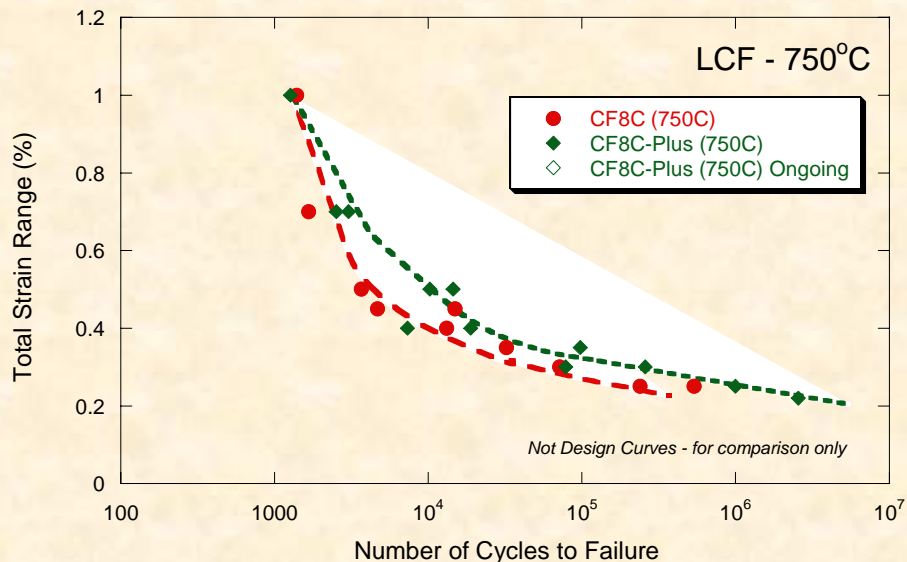
CF8C-Plus show a dramatic improvement over SiMo Cast Iron in Thermal Mechanical Fatigue (TMF)

TMF Tests at 300 - 760C, 50C/min, Out of Phase, Air



Nf (Open symbol indicates failure outside extensometers)

CF8C-Plus shows improved Low-Cycle Fatigue (LCF) Resistance over CF8C

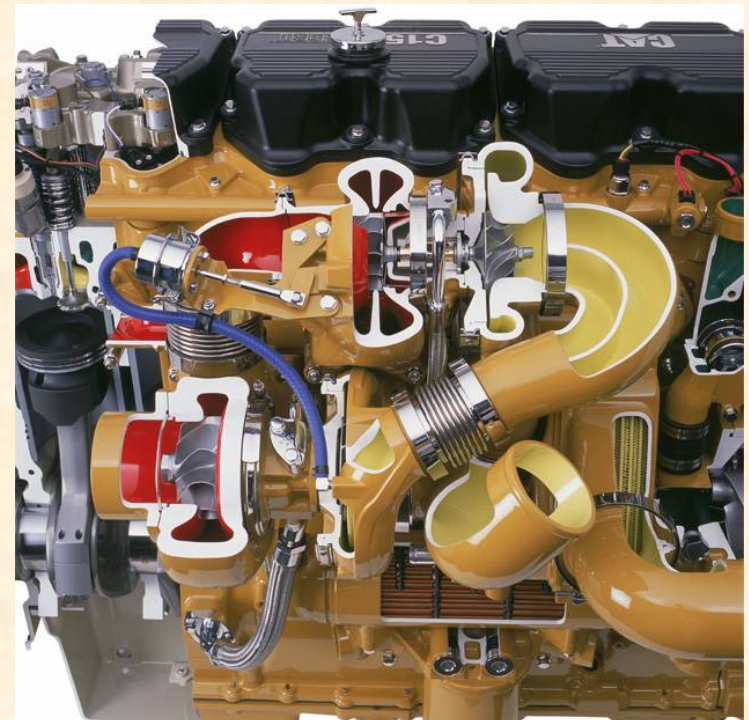
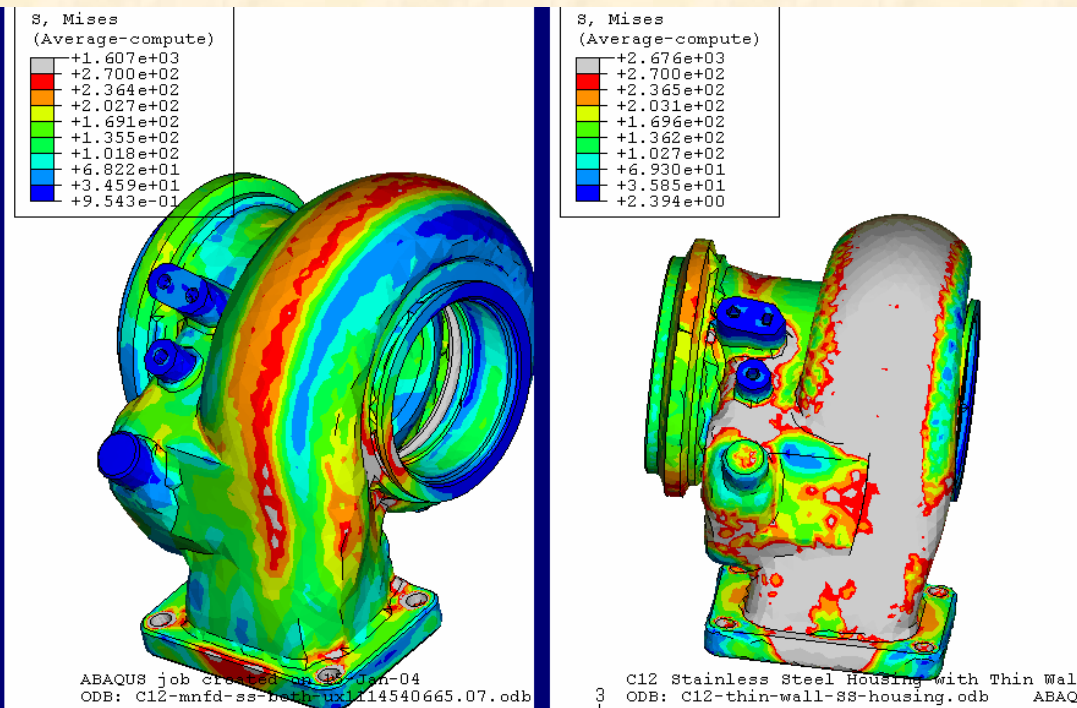


Low Cycle Fatigue (LCF) test results at 750 and 800C show CF8C-Plus approaches endurance limit at higher strain ranges

Slow strain rate and creep-fatigue studies ongoing

Commercial Interest Within CAT: Redesign and Replacement of SiMo Cast Iron

- Potential for use in turbocharger housings and exhaust manifolds **across the board** as emissions requirements lead to increased exhaust temperatures.



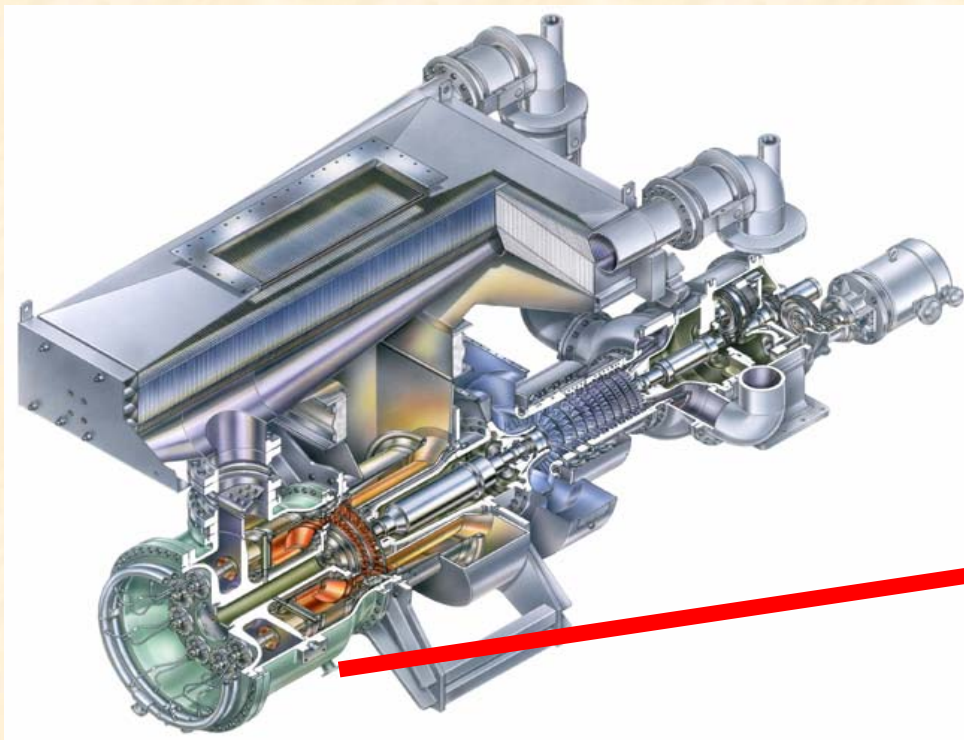
***Prototype Parts Being Produced**

Commercial Applications – Direct Replacement of NiResist for Natural Gas Reciprocating Engines at Reduced Cost (*Cost of CF8C-Plus = 80% of NiResist*)



80 lb (180kg) static sand-cast **CF8C-Plus** exhaust component cast by Stainless Foundry and Engineering, Inc.

Solar Turbines Mercury 50 gas turbine application: CF8C Upgrade



Solar Turbines 4.6 MW
Mercury 50 recuperated low
NO_x gas turbine engine

6,700 lb (14,800 kg) CF8C-
Plus end-cover cast by
MetalTek

Centrifugally cast CF8C-Plus steel tubes for a global petrochemical company technology application

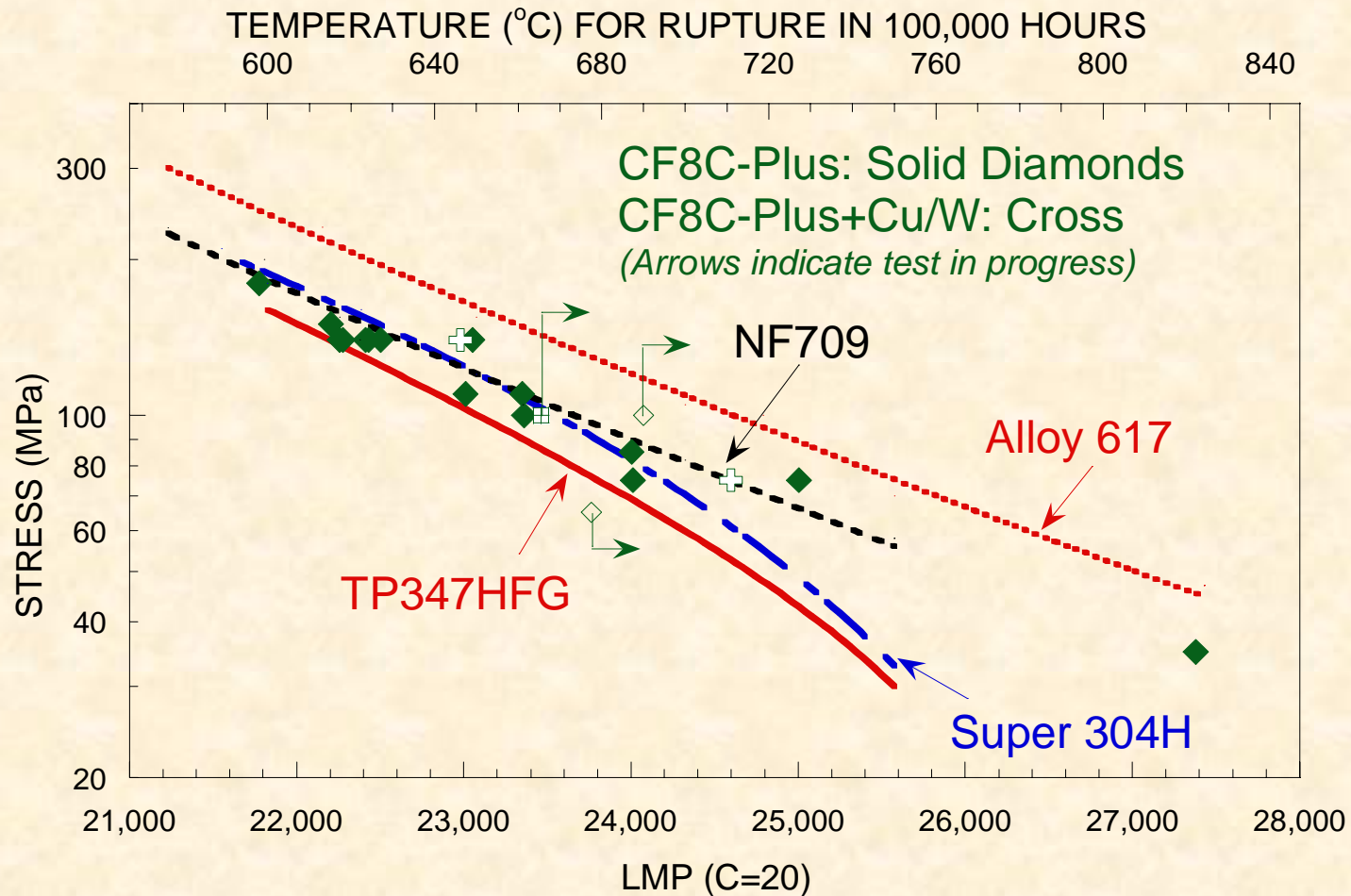


21,000 lbs (46,000kg) of Thin Wall Tubing Produced by MetalTek

Commercialization Summary

- **Good high temperature strength, castability, and cost are driving applications of CF8C-Plus inside and outside of Caterpillar**
- **Trial licensees: MetalTek International, Wollaston Alloys, and Stainless Foundry & Engineering**
- **Over 30,000 lb of CF8C-Plus steel have been melted to date**
 - **Static and centrifugal castings**
 - **No Casting Defects or difficulties encountered**
 - **Casting sizes/weights range from 0.5 to 7,000 lbs with thin and thick walls**
- **Additional Alloy Modifications are being examined to:**
 - **Maximize Creep Strength: Cu and W**
 - **Improve corrosion resistance in steam/water vapor**
- **Potential for High-Temperature Plant applications such as USC turbine casings**

Creep strength of CF8C-Plus compared to wrought austenitics and Ni-based alloys



Creep Strength and potential for further alloy modifications at low cost is driving additional interest including high-temperature plant applications