City of Killeen

Water and Wastewater Master Plan

May 2007

Prepared for:

City of Killeen



KIL06188

Prepared by:



Freese and Nichols, Inc.

4055 International Plaza Suite 200 Fort Worth, TX 76109 817/735-7300



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1.0 EXECUTIVE SUMMARY

1.1 Introduction

Freese and Nichols, Inc. was retained in 2006 by the City of Killeen to prepare a Water and Wastewater Master Plan Update and development of a Capital Improvement Plan (CIP). The service area includes the City's existing city limits and extraterritorial jurisdiction (ETJ). To develop a plan to meet projected water demands and wastewater flows through 2031, computer models of the water and wastewater systems were developed. The City selected the H_2OMap Water and H_2O Map Sewer software packages for modeling Killeen's water and wastewater systems.

1.2 Population

The City of Killeen experienced a 23% growth in population between 1990 and 2000. Due to its proximity to major transportation corridors, recreational opportunities, abundant water supply, availability of developable land, and the Fort Hood economic engine, the City of Killeen is expected to see significant growth in the future. **Table 1.1** displays the historical growth that has occurred in Killeen since the 2000 Census, and **Table 1.2** displays the projected population growth that may occur through 2031. The 2006 population is included in **Table 1.2** as a baseline.

Year	Census Population	Percent Growth
1999	82,327	
2000	86,911	5.6%
2001	89,858	3.4%
2002	93,587	4.1%
2003	100,911	7.8%
2004	102,461	1.5%
2005	106,145	3.6%

Table 1.1Historical Growth

Year	Projected Population	Annual Growth Rate
2006	113,419	-
2011	137,992	4.0%
2016	163,891	3.5%
2031	256,576	3.0%

Table 1.2Projected Population Growth

The growth that may occur within the City of Killeen's water and wastewater utility service area over the next 25 years required Freese and Nichols to develop an updated plan to serve future utility system needs. This growth will require expansion and rehabilitation of current utility infrastructure operated and maintained by the City of Killeen.

1.3 Water Demands

Currently, the City of Killeen's potable water is supplied by Bell County Water Control and Improvement District #1 (BCWCID #1). The average day, maximum day, and peak hour water demands for the City of Killeen are listed in **Table 1.3**. The total maximum day water demand is expected to increase from 24.10 MGD in 2006 to 37.61 MGD in 2016.

		Avg. Day	Max. Day	Peak Hour
		Demand	Demand	Demand
Year	Population	(MGD)	(MGD)	(MGD)
2006	113,419	14.18	24.10	43.38
2011	137,992	17.94	30.50	54.89
2016	163,891	22.13	37.61	67.70
2031	256,576	35.92	61.07	109.92

Table 1.3

Projected Water Demands

1.4 Water Capital Improvement Plan

The proposed water Capital Improvement Plan (CIP) is divided into three-year bond packages and includes pumping, storage, and distribution system improvements necessary to continue providing quality water service under future water demands. One of the most crucial water utility system improvements to support future growth of the city is a new potable water supply point in the southern portion of the City. As the City continues growing, it will become increasingly difficult and more expensive to maintain adequate capacity in the south with the current water supply facilities. Therefore, a new south supply point is recommended to facilitate future growth. Other major water improvement projects include the following:

- Acquisition of selected West Bell Water Supply Corporation Infrastructure
- New Bundrant Elevated Tank Increase elevated storage capacity to 1.5 MG
- Distribution piping to extend service throughout expanding city limits
- Pump Station 3 Upgrades Increase in pumping capacity to 18.0 MGD
- South Delivery Point 5.0 MG ground storage tank, 7.0 MGD upper pressure plane pump station, 7.0 MGD lower pressure plane pump station
- Water system renewal program to prioritize replacement of debilitated and inadequate lines
- Future elevated storage in both the upper and lower planes in the far southern parts of the City

1.5 Wastewater Flows

Historically, all of the City of Killeen's wastewater flow has been treated by BCWCID #1 at the 38th Street Wastewater Treatment Plant (WWTP), which is located along South Nolan Creek in the northeastern portion of the City. In early 2007, the new South WWTP along Trimmier Creek became operational and started receiving flows from the City of Killeen. The new South WWTP and future wastewater collection system improvements will be critical to support the growth of the City and provide adequate long-term capacity within the existing wastewater

collection network. The total average day and peak wet weather wastewater flows for each planning period for the City of Killeen are displayed in **Table 1.4**.

Year	Population	Average Day Flow (MGD)	Peak Wet Weather Flow (MGD)
2006	113,419	11.91	47.64
2011	137,992	15.18	60.72
2016	163,891	18.85	75.39
2031	256,576	29.51	118.02

Table 1.4Projected Wastewater Flows

1.6 Wastewater Capital Improvement Plan

In order to support the future growth in the City of Killeen, the proposed wastewater CIP includes multiple sewer interceptors and several lift station improvements. In addition to development in the southern portion of the City, several upgrades to the existing wastewater collection system are recommended to support growth and sustain existing wastewater services. One of the major projects in the existing system is the need for an updated Inflow/Infiltration (I/I) Study, which will help pinpoint areas of the system that require rehabilitation to reduce overall flow to the BCWCID #1 WWTPs. This will preserve existing system capacity for future growth and reduce the costs of excessive wastewater treatment.

Other major wastewater improvement projects include the following:

- Rehabilitation of Lift Station #8
- Southern interceptor system to deliver flow to new South WWTP
- I/I Study to identify and solve excessive peak wet weather flows in older portions of the City
- Airport Lift Station Upgrades Expand to 2.0 MGD pumping capacity
- Collection system and lift stations to support development in the south

1.7 Recommended System Improvements

Based upon the evaluation of the City of Killeen's water and wastewater systems, Freese and Nichols developed a Capital Improvement Plan with cost estimates in three-year bond packages from 2007 through 2024. The water and wastewater systems were evaluated with projected populations through 2031, which resulted in improvements to meet the projected growth. A summary of the major system estimated CIP costs is displayed in **Table 1.5**.

The unit costs used to calculate CIP costs were escalated for each bond period to account for inflation. Summaries of the water and wastewater unit costs are included in **Appendices A** and **B**, respectively.

SYSTEM	2007-2009 CIP Costs	2010-2012 CIP Costs	2013-2015 CIP Costs	2016-2018 CIP Costs	2019-2021 CIP Costs	2022-2024 CIP Costs
Water	\$11,057,908	\$15,835,173	\$14,910,239	\$15,988,495	\$20,397,786	\$3,843,114
Wastewater	\$ 9,917,071	\$11,964,798	\$16,030,620	\$15,976,475	\$12,046,221	\$6,102,951
Total	\$20,974,978	\$27,799,971	\$30,940,859	\$31,964,970	\$32,444,007	\$9,946,065

Table 1.5CIP Summary Bond Projects

In addition to the CIP projects, projects based on regulatory and operational considerations include an I/I study, water and wastewater rehabilitation planning, and TCEQ required regulatory improvements. A summary of costs for these projects are listed in **Table 1.6**.

Table 1.6	Administrative, Regulatory, & Operational Project Costs
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SYSTEM	2007-2009	2010-2012	2013-2015	2016-2018	2019-2022
Water	\$155,000	\$1,680,000	\$1,680,000	TBD	TBD
Wastewater	\$260,000	\$3,188,000	\$0	TBD	TBD
Total	\$415,000	\$4,868,000	\$1,680,000	TBD	TBD

2.0 **POPULATION**

2.1 Historical and Existing Population

The City provided Freese and Nichols with the historical growth in the number of water accounts from 1999 through 2005 and historical population for the Census 2000 and October 2002. A correlation between the water accounts and population was established for the baseline population and used to help determine population. These factors included 2.9 people/connection for residential connections, 2 people/unit and 23 units/account for Class A3 (>4) multifamily connections, 2.2 people/unit for mobile homes connections. 2 people/unit and 2.3 units/account for Class A5 (<5) multifamily connections. Historical population and growth rates can be found in **Table 2.1**. In analyzing this data, it shows an annual average growth rate from 2000 to 2005 of 4.08%.

Year	Population	Percent Growth
1999	82,327	
2000	86,911	5.6%
2001	89,858	3.4%
2002	93,587	4.1%
2003	100,911	7.8%
2004	102,461	1.5%
2005	106,145	3.6%

Table 2.1Historical Population and Growth

2.2 Population and Commercial Growth Projections

The City of Killeen is geographically positioned to experience significant growth for at least the next 25 years. Several of the factors that will contribute to this growth are described below.

• Two major water reservoirs, Belton Lake and Stillhouse Hollow Lake, are less than 15 miles from Killeen and provide a major source of recreational activities to the area and a reliable water supply. • The City of Killeen is located approximately 50 miles southwest of Waco and 50 miles north of Austin. Three existing transportation corridors are located in or near the City of Killeen, IH 35, US 190, and SH 195.

These factors will provide a catalyst for the continued growth of Killeen and the surrounding areas. Since 2000, the City population has increased more than 30%, and the City currently provides utility services to approximately 113,419 people.

Projected population was determined based on historical growth rates, available land for development, future service areas, and establishing future growth rates through the year 2031. A summary of the projected population and growth rates is shown in **Table 2.2**.

Year	Projected Population	Annual Growth Rate
2006	113,419	-
2011	137,992	4.0%
2016	163,891	3.5%
2031	256,576	3.0%

 Table 2.2
 Projected Population and Annual Growth Rate

2.3 Population and Commercial Area Distribution

The future growth areas were based on development trends within and adjacent to the City, availability of land, topography and the certificate of convenience and necessity (CCN) boundaries of other entities. **Plate 1** shows the CCN boundaries of entities within Killeen's extraterritorial jurisdiction boundary (ETJ).



Population data for the year 2000 by census tract was obtained from the U.S. Census Bureau. This information along with recent development data was utilized to distribute population and commercial growth for the 2006, 2011, 2016, and 2031 planning periods as shown in **Plate 2** and **Table 2.3**. The City's current zoning categories were combined into four main categories: Single Family Residential, Multi-family Residential, Commercial and Industrial. Because the City does not have a future land use plan in the ETJ, it was necessary to make assumptions on future land use types based on information known on future developments and by comparing the breakdown of residential and commercial land use in other areas of the City. Freese and Nichols, Inc. [KIL06188]: H:\DELIVERABLES\DELIVERABLE_06-28-07_(Final_CIP_v3)\(Plate_2)-Census_Tract_and_Planning_Areas_Population_Projection_Map.mxd Printing Date: Tuesday, June 26, 2007



Census Tract within ETJ	2000 Population	2006 Population	2011 Population	2016 Population	2031 Population	Total Acres
0220	186	713	1.686	2.286	5.671	953
0220 EPA1	0	0	0	691	6,664	1,360
0221.01	5,059	5,059	5,059	5,059	5,059	545
0221.02	7,367	7,367	7,367	7,367	7,367	936
0221.03	4,745	6,070	6,070	6,070	6,070	654
0222	3,288	4,613	5,013	5,313	5,913	1,285
0223	4,624	7,383	8,583	9,083	10,083	2,139
0224.01	3,785	5,110	5,410	5,410	5,410	904
0224.02	9,847	14,658	17,658	20,158	24,658	3,889
0225	6,038	8,173	12,673	16,473	30,884	5,963
0226	4,668	4,668	4,668	4,668	4,668	556
0228.01	3,126	3,126	3,126	3,126	3,126	277
0229	4,454	4,454	4,454	4,454	4,454	553
0230	5,423	6,477	8,677	9,477	12,035	2,010
0231.02	13,638	23,559	29,259	35,180	50,297	7,819
0231.02 WPA1	4,620	0	0	500	0	272
0231.02 WPA2	3,706	0	0	700	0	369
0231.03	0	5,946	5,946	5,946	5,946	655
0231.04	0	3,706	3,706	3,706	3,706	424
0232	0	0	800	1,200	5,237	1,464
0233	0	0	2,000	4,000	15,429	1,552
0233 SPA1	0	0	2,500	5,987	11,301	2,451
0233 SPA2	0	0	500	2,900	5,662	4,240
0233 SPA3	0	0	500	900	14,594	2,696
0233 SPA4	0	0	0	500	6,698	3,356
0233 SPA5	0	0	0	400	3,307	2,362
0235	2,337	2,337	2,337	2,337	2,337	406
Total	86,911	113,419	137,992	163,891	256,576	50,090

Table 2.3City of Killeen Population By Census Tract and Time Period

3.0 WATER DEMANDS

3.1 Historical and Existing Water Demands

Historical water usage records from 1999 through 2005 were obtained from the City and evaluated to establish average day per capita usage rates and maximum day to average day peaking factors. This data is summarized in **Table 3.1**.

Year	Served Population	Avg. Day Water Usage (MGD)	Avg. Day Water Usage (gpcd)	Maximum Day Water Usage (MGD)	Max. Day to Avg. Day Ratio
1999	82,327	9.95	121	17.91	1.80
2000	86,911	10.56	121	18.26	1.73
2001	89,858	11.41	127	18.80	1.65
2002	93,587	12.09	129	19.84	1.64
2003	100,911	12.28	122	21.12	1.72
2004	102,461	10.86	106	16.75	1.54
2005	106,145	11.91	112	21.17	1.78
Average			120		1.69

Table 3.1Historical Water Usage Data

The City also provided information about consumption for large water users. **Table 3.2** shows the top 20 individual water users in the City.

	Customer	2005 Annual Consumption (1,000 gal)	2005 Average Day Usage (MGD)
1	Transit Mix Concrete	156,908	0.43
2	Ellison H. S.	154,708	0.42
3	Metroplex Hospital	151,861	0.42
4	Killeen I.S.D.	93,974	0.26
5	Zip Cleaners	65,367	0.18
6	Sheraton Plaza Hotel	65,029	0.18
7	Wells Laundromat	60,220	0.16
8	City of Killeen Parks Department	59,376	0.16
9	City of Killeen	57,240	0.16
10	Killeen I.S.D.	55,094	0.15
11	Killeen Ready Mix	54,840	0.15
12	Killeen I.S.D.	52,278	0.14
13	Sallie Mae Loan Service Center	52,069	0.14
14	City of Killeen	50,558	0.14
15	City of Killeen Regional Airport	48,823	0.13
16	Bell Haven Nursing Home	48,226	0.13
17	Wal-Mart Stores	48,208	0.13
18	La Quinta Inn #527	47,478	0.13
19	Killeen I.S.D.	47,092	0.13
20	Killeen Hilton	46,264	0.13
	TOTAL	1,415,613	3.88

 Table 3.2
 City of Killeen Top 20 Individual Water Users

It is important from a planning perspective that large users be identified to ensure adequate infrastructure exists to support the demands.

3.2 Projected Water Demands

Based on a review of the historical water usage data, it is recommended that an average day per capita rate of 125 gpcd be used to project 2006 average day demands and 130 gpcd for 2011 average day demands. Average day per capita rates of 135 gpcd and 140 gpcd are recommended for the 2016 and 2031 average day demands, respectively. The increase in demands over time is based on historical usage trends and the trend to use irrigation systems for the many new single family developments.

FNI recommends using an average day to maximum day peaking factor of 1.7 for projecting future maximum day demands. Historical maximum day to peak hour peaking factors were not available. The American Water Works Association (AWWA) recommends using a peaking value between 1.5 and 3.0; therefore, Freese and Nichols recommends using a maximum day to peak hour peaking factor of 1.8 based on the type of development in the City of Killeen.

A summary of the total projected demands for the 2011, 2016 and 2031 planning periods is shown in **Table 3.3**. Projected demands will be distributed based on population and commercial acreage throughout the City.

Year	Avg. Day Demand (MGD)	Max Day Demand (MGD)	Peak Hour Demand (MGD)
2006	14.18	24.10	43.38
2011	17.94	30.50	54.89
2016	22.13	37.61	67.70
2031	35.92	61.07	109.92

Table 3.3Projected Water Demands

Table 3.4Summary of Projected Water Demands by Pressure Plane

			2006				
Customer Base	Served Population	Avg Day Usage Rates	Avg Day Demand (MGD)	Max Day/ Avg Day Ratio	Max Day Demand (MGD)	Peak Hour/ Max Day Ratio	Peak Hour Demand (MGD)
Lower Pressure Plane	63,735	125 gpcd	7.97	1.70	13.54	1.80	24.38
Middle Pressure Plane	6,346	125 gpcd	0.79	1.70	1.35	1.80	2.43
Upper Pressure Plane	39,626	125 gpcd	4.95	1.70	8.42	1.80	15.16
Airport Pressure Plane	3,712	125 gpcd	0.46	1.70	0.79	1.80	1.42
Total City	113,419		14.18	-	24.10	-	43.38
	-		2011				
Customer Base	Served Population	Avg Day Usage Rates	Avg Day Demand (MGD)	Max Day/ Avg Day Ratio	Max Day Demand (MGD)	Peak Hour/ Max Day Ratio	Peak Hour Demand (MGD)
Lower Pressure Plane	74,183	130 gpcd	9.64	1.70	16.39	1.80	29.51
Middle Pressure Plane	6,896	130 gpcd	0.90	1.70	1.52	1.80	2.74
Upper Pressure Plane	51,541	130 gpcd	6.70	1.70	11.39	1.80	20.50
Airport Pressure Plane	5,372	130 gpcd	0.70	1.70	1.19	1.80	2.14
Total City	137,992		17.94	-	30.50	-	54.89
			2016				
Customer Base	Served Population	Avg Day Usage Rates	Avg Day Demand (MGD)	Max Day/ Avg Day Ratio	Max Day Demand (MGD)	Peak Hour/ Max Day Ratio	Peak Hour Demand (MGD)
Lower Pressure Plane	83,751	135 gpcd	11.31	1.70	19.22	1.80	34.60
Middle Pressure Plane	7,096	135 gpcd	0.96	1.70	1.63	1.80	2.93
Upper Pressure Plane	66,392	135 gpcd	8.96	1.70	15.24	1.80	27.43
Airport Pressure Plane	6,652	135 gpcd	0.90	1.70	1.53	1.80	2.75
Total City	163,891		22.13	-	37.61	-	67.70
2031							
Customer Base	Served Population	Avg Day Usage Rates	Avg Day Demand (MGD)	Max Day/ Avg Day Ratio	Max Day Demand (MGD)	Peak Hour/ Max Day Ratio	Peak Hour Demand (MGD)
Lower Pressure Plane	118,902	140 gpcd	16.65	1.70	28.30	1.80	50.94
Middle Pressure Plane	7,436	140 gpcd	1.04	1.70	1.77	1.80	3.19
Upper Pressure Plane	120,668	140 gpcd	16.89	1.70	28.72	1.80	51.69
Airport Pressure Plane	9,570	140 gpcd	1.34	1.70	2.28	1.80	4.10
Total City	256,576		35.92	-	61.07	-	109.92

4.0 EXISTING WATER SYSTEM

The City of Killeen does not currently operate any water treatment facilities. The City has contracts with BCWCID #1 that is the wholesale provider of water for the region. Water is purchased from BCWCID #1, which is delivered to the city at five different locations. **Plate 3** summarizes the orientation of the pressure planes and the location and capacities of the pumping and storage facilities. The operation of the system is explained in further detail in the following sections.

4.1 Existing Water Distribution System

A. Lower Pressure Plane

The Lower Pressure Plane (LPP) is comprised primarily of the North and East areas of the city as shown in **Plate 3**. Water is supplied to the system through Pump Stations 1, 2, 3 and 5. Pump Station 3 is largest pump station with a total capacity of 11.5 MGD. Pump Station 3 also supplies water to the Upper Pressure Plane (UPP) by delivering water into a ground storage tank located at Pump Station 4. Approximately 2 to 4 MGD is currently being transferred through an isolated 24-inch water line that goes through the Middle Pressure Plane (MPP). Pump Stations 1 and 2 are the original pump stations in the City and therefore the oldest. These pump stations are used occasionally during the peak summer time periods. Pump Station 5 supplies most of the area in the north portion of the City. **Table 4.1** summarizes the facilities in the LPP.



PLATE 3 CITY OF KILLEEN EXISTING WATER SYSTEM

<u>LEGEND</u>

- Existing Water Lines
- Existing Dist. Lines
- Existing Trans. Lines
- Existing Trans. Lines Greater than 16"
- Elevated Storage Tanks
- Ground Storage Tanks
- ☑ Pump Stations
- → Rail Roads



- Streams/Rivers
 Lakes
 Parcels
 Bell County Boundary
 Killeen City Limits
 Killeen ETJ
 Airport Pressure Plane
 Upper Pressure Plane
 Middle Pressure Plane
 - Lower Pressure Plane



Pumping Facility	Capacity (Firm Capacity)
Pump Station 1	
Pump 1	0.72 MGD
Pump 2	1.08 MGD
Pump 3	1.08 MGD
Total	2.88 MGD (2.16 MGD)
Pump Station 2	
Pump 1	1.73 MGD
Pump 2	1.73 MGD
Pump 3	1.73 MGD
Total	5.19 MGD (3.46 MGD)
Pump Station 3	
Pump 1	2.88 MGD
Pump 2	2.88 MGD
Pump 3	2.88 MGD
Pump 4	2.88 MGD
Total	11.52 MGD (8.64 MGD)
Pump Station 5	
Pump 1	2.65 MGD
Pump 2	2.65 MGD
Pump 3	2.65 MGD
Total	7.95 MGD (5.3 MGD)
Ground Storage Facility	
Pump Station 1 Ground Storage	0.25 MG
Tank	
Pump Station 2 Ground Storage	2.0 MG
Tank	
Pump Station 3 Ground Storage	10.0 MG
Tank	
Pump Station 5 Ground Storage	2.5 MG
Tank	
Total	14.75 MG
Elevated Storage Facility	
Rodeo Tank	1.0 MG
Park Street Tank	0.25 MG
Southeast Tank	2.5 MG
Bundrant Tank	0.25 MG
Total	4.0 MG

 Table 4.1
 Existing Lower Pressure Plane Facilities

B. Middle Pressure Plane

The Middle Pressure Plane (MPP) is bordered by the UPP and LPP. The MPP is located from Santa Rosa Dr. to South W.S. Young Dr. with the Central Texas Expressway on the south border and a combination of Terrace Dr. and Bryce Dr. making up the north border. The MPP was created from the LPP because the pressures provided by the LPP and the 8th Street EST were not adequate. The MPP is now served by the UPP. The 8th Street EST is inside the limits of the MPP but is not currently in service. The UPP supplies the MPP through a pressure reducing valve (PRV) located just south of Pump Station 4 on a 16-inch water line along Jasper Dr. Due to concerns of high pressures in the lower elevation areas in the MPP, a PRV was installed to keep pressures in the MPP in the 50 to 60 psi range. The MPP is supplied entirely by the 16-inch water line along Jasper Dr. from Pump Station 4, which branches off into a combination of a 10-inch and 12-inch water lines. The 24-inch water line that supplies water to Pump Station 4 passes through this pressure plane; however, it is isolated from service lines and other transmission lines in the MPP. Table 4.2 summarizes the facilities in located in the MPP.

Table 4.2Existing Middle Pressure Plane Facilities

Pumping Facility	Capacity (Firm Capacity)
Pump Station 4	Transfer from UPP
Elevated Storage Facility	
8th Street Tank	Inactive

C. Upper Pressure Plane

The Upper Pressure Plane (UPP) is comprised of the southern and western most portions of the city. Water is supplied to the UPP through Pump Stations 4 and 6. The UPP also supplies water to a booster pump station facility that supplies the Airport Pressure Plane. The UPP has two 1.5 MG ground storage tanks south of Stan Schlueter Rd. that are located on a hill and therefore are able to operate as elevated storage for the UPP. **Table 4.3** summarizes the facilities located in the UPP.

Pumping Facility	Capacity (Firm Capacity)
Pump Station 4	
Pump 1	2.88 MGD
Pump 2	2.88 MGD
Pump 3	3.67 MGD
Pump 4	3.67 MGD
Total	13.10 MGD (9.43 MGD)*
Pump Station 6	
Pump 1	5.04 MGD
Pump 2	5.04 MGD
Pump 3	5.04 MGD
Total	15.12 MGD (10.08 MGD)
Ground Storage Facility	
Pump Station 4 Ground Storage Tank	1.5 MG
Pump Station 6 Ground Storage Tank	15.0 MG
Total	16.5 MG
Elevated Storage Facility	
McMillan Mountain Elevated Tank (1	
& 2)	3.0 MG

Table 4.3Upper Pressure Plane Existing Facilities

*Limited in pumping by supply from Pump Station 3 to approximately 3 MGD presently.

D. Airport Pressure Plane

The Airport Pressure Plane (APP) is the smallest of all of the pressure planes and is served by an in-line booster pump station that is supplied by the UPP. The Airport EST operates at an overflow of 1,164-feet, which is 39-feet higher than the UPP. **Table 4.4** summarizes the system facilities in the APP.

Table 4.4Airport Pressure Plane Existing Facilities

Pumping Facility	Capacity (Firm Capacity)
Pump Station 7	
Pump 1	1.51 MGD
Pump 2	1.51 MGD
Total	3.02 MGD (1.51 MGD)
Elevated Storage Facility	
Airport Tank	1.0 MG

4.2 Water System Field Testing and Model Calibration

The hydraulic model of the City of Killeen's water system was built using the H20Map modeling software. The model was created to comply with the Stage 2

Disinfectants/Disinfection Byproduct Rule (DBPR). The most stringent of these criteria is the requirement to model 50% of the total pipe length in the City's water system. This results in modeling all 10-inch and larger water lines, a majority of the 8-inch water lines and some key 6-inch water lines. This rule also requires the model to simulate the operation of the water system over a period of several days. **Plate 4** shows the water lines that are included in the hydraulic water model, along with the pressure testing locations.

The water model was constructed using the City's GIS water line shapefiles. After the water lines were imported into the software, the ground storage tanks, pumps and elevated tanks were added to the model using as-built drawings and pump curves from the City. Roughness coefficients were assigned to water lines using pipe age and material where available. The next steps in model development were to distribute water demands in the model and perform calibration of the model using Supervisory Control and Data Acquisition (SCADA) data and the pressure testing data collected during field testing performed in late May.

The distribution system was divided into two sections with each section being monitored by the pressure recorders for a one week period. The MPP and LPP were grouped together in the first week of field testing and the pressure recorder locations are shown in blue in **Plate 4**. The UPP and APP were grouped together in the second week and the pressure recorder locations are shown in red in **Plate 4**.

Figures 4.1 and **4.2** show the results of pressure testing conducted throughout the City from May 26 to June 9. **Figure 4.1** summarizes the LPP and MPP pressure recorder data. Pressure recorder 3 is not included, as it was placed at the discharge of





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Pump Station 6. Since Pump Station 6 serves the UPP, it was used to predict the discharge pressure during the second week of field testing. **Plate 4** summarizes the UPP and APP pressure recorder data. The data from the first week of pressure testing was used to predict the pressures for Pump Station 6.

Once field testing was completed, the demands for the system were distributed based on the City's existing GIS parcel shapefile data. Demands for each parcel were calculated based on Killeen's most recent land use map. These demands were distributed throughout the model using Thiessen polygons that assign each parcel's demand to a node in the water model. This method confirms a high degree of accuracy when performing model calibration.

The model was calibrated for two different dates, one for each field testing time period. The first calibration was performed to match the field results from May 30, 2006 and the second time period was calibrated to the field results recorded on June 5, 2006. The model was calibrated to be within 3 to 4 psi of the field observed pressures. As shown in **Plate 4**, the majority of the pressures are within 1 to 2 psi.

4.3 Water System Design Criteria

Freese and Nichols worked with the City of Killeen staff to establish design criteria for future water facilities. Criteria were developed for sizing water transmission lines, elevated storage tanks, ground storage tanks and pump stations for the water system.

A. Water Transmission Lines (8-inch and larger)

Water transmission lines shall be sized to maintain a minimum of 35 psi throughout the system during peak hour demand conditions. In addition, the transmission lines shall be designed for a maximum pipeline velocity of 7 feet/second and a maximum friction loss of 5 feet per 1,000 feet of pipeline length for 8-inch and larger water lines.

B. Elevated Storage Tanks

The design criteria used to size elevated storage tank capacity is the capacity to provide adequate storage for peak hour demands plus emergency storage for fire protection. The required capacity for the peak hour demands is calculated as the storage volume to allow a minimum of a 3-hour drain time using two-thirds of the tank volume during summer peak hour operating conditions. The required capacity for emergency fire protection storage is calculated as the volume of water needed to meet a 3,000 gpm fire for a 4-hour time period, which typically is met through the remaining one-third of the tank volume. In addition to these criteria, the City must also meet the TCEQ elevated storage capacity of 100 gallons per connection. The recommended design criteria to provide storage for peak hour demands plus fire protection is the most stringent criteria and therefore recommended for use in sizing future elevated storage facilities for the City of Killeen.

C. Ground Storage Tanks

The design criteria recommended to size ground storage tank capacity within each pressure plane is to provide adequate storage volume to meet eight hours of maximum day summer demand. In addition to these criteria, the City must also meet the TCEQ ground storage capacity requirement of 200 gallons per connection. The recommended criterion of eight hours of storage capacity is more conservative and was used to size the recommended ground storage capacity.

D. Pump Stations

The design criteria recommended for pump station capacity is providing a firm pumping capacity to meet 125% of the summer maximum day demands. The firm pumping capacity is defined as the total available pumping capacity with the largest pump out of service.

4.4 Existing Water System Analysis

The purpose of analyzing the existing system is to examine the distribution system, consisting of 8-inch and larger water lines and any smaller lines critical for system

looping, under four major operating conditions. These operating conditions are average day, maximum day, peak hour and maximum day with fire flow. The TCEQ required minimum pressure within a distribution system is 35 psi under peak hour demand conditions and 20 psi during maximum day fire flow scenario. Under recommended fire flow capacity of 1000 gpm, residual pressures throughout the system can be no lower than 20 psi. The water system is analyzed for additional criteria, including the headloss and velocities in the pipelines. Typically, headloss in water lines should not exceed 5 feet/1000 feet and velocities should not exceed 7 feet/second.

There are several specific areas in the distribution system that are not providing adequate fire protection capacities of at least 1,000 gpm. The majority are in the LPP and are caused by a lack of looping of smaller diameter lines or insufficient transmission capacity. The LPP has three major areas that are not able to provide adequate fire flows. The location of these areas and the reasons for the low available fire flow are:

- 1. The area west of the Rodeo EST along the border between the UPP and LPP boundaries delivers a maximum of 700 gpm. This condition is caused by the area having higher elevations and only being supplied by 6-inch water lines.
- The area immediately south of the Bundrant EST delivers a maximum of 900 gpm. This condition is caused by the insufficient capacity of the Bundrant EST.
- 3. The area along Schwald Rd. from Transit Dr. to Ridge Haven Dr. along the northern city limit line delivers a maximum of 600 gpm. This condition is caused by transmission capacity and the fact that a 6-inch water line is responsible for supplying the entire development along N. 60th St.

The UPP has two areas that experience low fire flow availability. First, the development along Yates Rd. is supplied water through a series of 6-inch and 3-inch water lines, which are able to supply only 400 gpm during fire flow conditions. The
second area is located in the development south of Old Copperas Cove Rd. and Pennington Ave. and delivers a fire flow of only 750 gpm at the TCEQ required minimum residual pressure of 20 psi due to high elevations in sections of the development. The problem areas are addressed in the capital improvement section of this report.

The next criteria analyzed for deficiencies were the headloss and velocities experienced in the pipes during all the operational conditions. There were no pipes 8-inch and larger in any of the operating conditions that experienced velocities in excess of 7 feet/second. However, there were a few pipes that measured in excess of 5 feet/1000 feet of headloss in the maximum day and peak hour conditions. Most of the excess headloss was experienced in short sections of the distribution system leading to and from pumping and storage facilities and ranged between 5 and 6 feet/1000 feet. It has been determined that these facilities are in an acceptable range of operating conditions and are not deficient.

Figure 4.3 summarizes the existing conditions used during the hydraulic model analysis. This figure is used during the analysis to determine if the elevated storage or pump station in a designated area is deficient by providing a tabular summary of the fill and drain rates for each elevated storage tank and the discharge flow and pressure of each pump station. The elevated storage tanks should fill in less than eight to 10 hours during the average day conditions and drain in no more than three hours during peak hours. **Figure 4.3** shows that the Rodeo, Southeast, and McMillan ESTs are taking longer than eight to 10 hours to fill. This may indicate insufficient transmission or pumping capacity. However, during peak hour demands, the elevated tanks do not drain faster than three hours, which indicates that there is sufficient elevated storage capacity. These deficiencies will be addressed by the future capital improvement plan.

Figure 4.3 Existing Modeled System Elevated and Storage Tank Analysis

A. Water Demands

	Average Day	Max Day	Peak Hour
Lower Pressure Plane	7.97 MGD	13.54 MGD	24.38 MGD
Middle Pressure Plane	0.79 MGD	1.35 MGD	2.43 MGD
Upper Pressure Plane	4.95 MGD	8.42 MGD	15.16 MGD
Airport Pressure Plane	0.46 MGD	0.79 MGD	1.42 MGD
TOTAL SYSTEM DEMAND	14.2 MGD	24.1 MGD	43.4 MGD

B. Existing System

Tank	Tank	Avg Day/	Avg Day/	Fill Time	Max Day	Max Day	Peak Hour	Peak Hour	Drain Time
Location	Vol.	Tank Refilling	Tank Refilling	Avg Day	Inflow	Current	Inflow	Current	at Pk Hr*
Lower Pressure Plane	(MG)	(MGD)	Status	(hr)	(MGD)	Status	(MGD)	Status	(hr)
Park St.	0.25	2.30	Filling	1.74	1.55	Filling	-0.56	Draining	7.13
Bundrant	0.25	1.01	Filling	3.96	0.31	Filling	-1.35	Draining	2.96
Rodeo	1.00	0.69	Filling	23.17	-0.31	Draining	-1.95	Draining	8.20
Southeast	2.50	2.53	Filling	15.78	0.51	Filling	-3.78	Draining	10.58
DELIVERY SOURCE		Inflow	Pressure		Inflow	Pressure	Inflow	Pressure	
DEELVERT SOURCE		(MGD)	(psi)		(MGD)	(psi)	(MGD)	(psi)	
Pump Station #1		1.3	70		1.4	65	1.5	58	
Pump Station #2		1.4	90		1.5	87	1.7	82	
Pump Station #3		9.8	80		10.1	77	10.5	73	
Pump Station #5		4.7	86		5.1	82	5.8	75	
Pump Station #4 Transfer		-4.0			-4.0		-4.0		
Total		13.2			14.1		15.6		
Tank	Tank	Avg Day/	Avg Day/	Fill Time	Max Day	Max Day	Peak Hour	Peak Hour	Drain Time
Tank Location	Tank Vol.	Avg Day/ Tank Refilling	Avg Day/ Tank Refilling	Fill Time Avg Day	Max Day Inflow	Max Day Current	Peak Hour Inflow	Peak Hour Current	Drain Time at Pk Hr*
Tank Location Upper Pressure Plane	Tank Vol. (MG)	Avg Day/ Tank Refilling (MGD)	Avg Day/ Tank Refilling Status	Fill Time Avg Day (hr)	Max Day Inflow (MGD)	Max Day Current Status	Peak Hour Inflow (MGD)	Peak Hour Current Status	Drain Time at Pk Hr* (hr)
Tank Location Upper Pressure Plane McMillan	Tank Vol. (MG) 3.00	Avg Day/ Tank Refilling (MGD) 3.27	Avg Day/ Tank Refilling Status Filling	Fill Time Avg Day (hr) 14.70	Max Day Inflow (MGD) 1.20	Max Day Current Status Filling	Peak Hour Inflow (MGD) -2.04	Peak Hour Current Status Draining	Drain Time at Pk Hr* (hr) 23.52
Tank Location Upper Pressure Plane McMillan Airport	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18	Avg Day/ Tank Refilling Status Filling Filling	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66	Max Day Current Status Filling Draining	Peak Hour Inflow (MGD) -2.04 -1.42	Peak Hour Current Status Draining Draining	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18	Avg Day/ Tank Refilling Status Filling Filling	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66	Max Day Current Status Filling Draining	Peak Hour Inflow (MGD) -2.04 -1.42	Peak Hour Current Status Draining Draining	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow	Avg Day/ Tank Refilling Status Filling Filling Pressure	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow	Max Day Current Status Filling Draining Pressure	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow	Peak Hour Current Status Draining Draining Pressure	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport DELIVERY SOURCE	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow (MGD)	Avg Day/ Tank Refilling Status Filling Filling Pressure (psi)	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow (MGD)	Max Day Current Status Filling Draining Pressure (psi)	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow (MGD)	Peak Hour Current Status Draining Draining Pressure (psi)	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport DELIVERY SOURCE Airport Pump Station	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow (MGD) 2.5	Avg Day/ Tank Refilling Status Filling Filling Pressure (psi) 61	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow (MGD) 0.0	Max Day Current Status Filling Draining Pressure (psi) 56	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow (MGD) 0.0	Peak Hour Current Status Draining Draining Pressure (psi) 55	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport DELIVERY SOURCE Airport Pump Station Pump Station #4	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow (MGD) 2.5 3.7	Avg Day/ Tank Refilling Status Filling Filling Pressure (psi) 61 95	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow (MGD) 0.0 3.9	Max Day Current Status Filling Draining Pressure (psi) 56 92	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow (MGD) 0.0 7.9	Peak Hour Current Status Draining Draining Pressure (psi) 55 91	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport DELIVERY SOURCE Airport Pump Station Pump Station #4 Pump Station #6	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow (MGD) 2.5 3.7 6.3	Avg Day/ Tank Refilling Status Filling Filling Pressure (psi) 61 95 123	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow (MGD) 0.0 3.9 8.2	Max Day Current Status Filling Draining Pressure (psi) 56 92 121	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow (MGD) 0.0 7.9 8.9	Peak Hour Current Status Draining Draining Pressure (psi) 55 91 121	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport DELIVERY SOURCE Airport Pump Station Pump Station #4 Pump Station #6 Total	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow (MGD) 2.5 3.7 6.3 12.5	Avg Day/ Tank Refilling Status Filling Filling Pressure (psi) 61 95 123	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow (MGD) 0.0 3.9 8.2 12.1	Max Day Current Status Filling Draining Pressure (psi) 56 92 121	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow (MGD) 0.0 7.9 8.9 16.9	Peak Hour Current Status Draining Draining Pressure (psi) 55 91 121	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport DELIVERY SOURCE Airport Pump Station Pump Station #4 Pump Station #6 Total	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow (MGD) 2.5 3.7 6.3 12.5	Avg Day/ Tank Refilling Status Filling Pressure (psi) 61 95 123	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow (MGD) 0.0 3.9 8.2 12.1	Max Day Current Status Filling Draining Pressure (psi) 56 92 121	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow (MGD) 0.0 7.9 8.9 16.9	Peak Hour Current Status Draining Draining Pressure (psi) 55 91 121	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport DELIVERY SOURCE Airport Pump Station Pump Station #4 Pump Station #6 Total Total Net Delivery	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow (MGD) 2.5 3.7 6.3 12.5 23.15	Avg Day/ Tank Refilling Status Filling Filling Pressure (psi) 61 95 123	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow (MGD) 0.0 3.9 8.2 12.1 30.20	Max Day Current Status Filling Draining Pressure (psi) 56 92 121	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow (MGD) 0.0 7.9 8.9 16.9 36.47	Peak Hour Current Status Draining Draining Pressure (psi) 55 91 121	Drain Time at Pk Hr* (hr) 23.52 11.27
Tank Location Upper Pressure Plane McMillan Airport DELIVERY SOURCE Airport Pump Station Pump Station #4 Pump Station #6 Total <u>Total Net Delivery</u> Maximum System Pressure	Tank Vol. (MG) 3.00 1.00	Avg Day/ Tank Refilling (MGD) 3.27 2.18 Inflow (MGD) 2.5 3.7 6.3 12.5 23.15	Avg Day/ Tank Refilling Status Filling Pressure (psi) 61 95 123 123	Fill Time Avg Day (hr) 14.70 7.34	Max Day Inflow (MGD) 1.20 -0.66 Inflow (MGD) 0.0 3.9 8.2 12.1 30.20	Max Day Current Status Filling Draining Pressure (psi) 56 92 121	Peak Hour Inflow (MGD) -2.04 -1.42 Inflow (MGD) 0.0 7.9 8.9 16.9 36.47	Peak Hour Current Status Draining Draining Pressure (psi) 55 91 121 121	Drain Time at Pk Hr* (hr) 23.52 11.27

* Drain Time @ Peak Hour is based on 2/3 of the tank volume

* Fill Time @ Average Day is based on 2/3 of the tank volume.

5.0 FUTURE WATER SYSTEM

5.1 Future Water Supply

The City of Killeen purchases water from BCWCID #1 and currently maintains six delivery points. As the City expands to the south, the existing and expanded pumping facilities will not be able to efficiently supply and support the development in the south. To adequately supply the southern development, an additional supply point will be needed along with an additional pumping facility. The 10-year Water Capital Improvement Map, **Plate 5**, identifies the new delivery point and pump station as Project 9. It has been estimated that the City of Killeen will need 40 MGD of supply from BCWCID #1 by the year 2016 and 62 MGD of supply by the year 2031.

5.2 Future Pressure Plane Delineation

The future City of Killeen distribution system will require some adjustments. Analysis of the future system with the proposed water system improvements have identified several areas where it is recommended that the existing pressure plane boundaries be altered to maintain the design criteria discussed in the preceding section. By the year 2013, the MPP should be consolidated into the UPP with the construction of the improvements identified in Project 16W. Also part of Project 16W is the expansion of the UPP to begin service to the customers east of the Rodeo EST. Due to the high ground elevation and proximity to the Rodeo EST, this area of the LPP experiences low pressures and fire flow during the existing and future 2016 maximum day with fire flow and peak hour demand scenarios. The next pressure plane alteration is the expansion of the APP to serve the development south of the W. Stan Schlueter Loop. This area also experiences lower than 35 psi pressures and low fire flow in the existing and future 2016 time period during maximum with fire flow and peak hour demand periods.

5.3 **Pumping and Elevated Storage Requirements**

The future pumping and elevated storage requirements have been analyzed for the 2011, 2016 and 2031 time periods. The following figures demonstrate the existing

system capacities and the required capacities to sustain the future growth as outlined in the capital improvement plan.

A. Elevated Storage

Figures 5.1 through **5.3** show the elevated storage for the LPP, the consolidated UPP and MPP, and the APP as compared to the elevated storage required to maintain adequate fire flow and the system's ability to supply water during peak demand periods.

B. Pumping Capacity

Figures 5.4 through **5.6** show the pumping capacity for the LPP, the consolidated UPP and MPP, and the APP as compared to the pumping capacity required to maintain adequate tank operation and meet demands during maximum day demand periods.

C. 2016 System Summary

Figure 5.7 summarizes the modeled water system results from the 2016 scenario. The CIP improvements modeled in the 2016 system demonstrate the impact on the elevated and pumping operation in the City. When compared to the existing system tank analysis in **Figure 4.3**, the added transmission and pumping capacity allow the elevated storage tanks to generally fill within the desired 8 to 10-hour timeframe during average day. The elevated tanks take longer than three hours to drain during peak hours. This demonstrates that there is adequate pumping capacity to fill the elevated tanks and adequate elevated storage to supply the system during peak hour and still maintain enough tank volume to provide fire flow protection.





Figure 5.1 Lower Pressure Plane Required Elevated Storage City of Killeen



Figure 5.2 Upper & Middle Pressure Plane Required Elevated Storage City of Killeen











Figure 5.5 Upper & Middle Pressure Plane Required Firm Pumping Capacity **City of Killeen**

^{*}Note: Required Firm Pumping Capacity is based on supplying 70% of peak hour demands.





Figure 5.7 2016 Modeled System Elevated and Storage Tank Analysis

A. Water Demands

	Average Day	Max Day	Peak Hour
Lower Pressure Plane	11.3 MGD	19.2 MGD	34.6 MGD
Middle Pressure Plane	1.0 MGD	1.6 MGD	2.9 MGD
Upper Pressure Plane	9.0 MGD	15.2 MGD	27.4 MGD
Airport Pressure Plane	0.9 MGD	1.5 MGD	2.7 MGD
TOTAL SYSTEM DEMAND	22.1 MGD	37.6 MGD	67.7 MGD

B. Existing System

Tank	Tank	Avg Day/	Avg Day/	Fill Time	Max Day	Max Day	Peak Hour	Peak Hour	Drain Time
Location	Vol.	Tank Refilling	Tank Refilling	Avg Day	Inflow	Current	Inflow	Current	at Pk Hr*
Lower Pressure Plane	(MG)	(MGD)	Status	(hr)	(MGD)	Status	(MGD)	Status	(hr)
Park St.	0.25	1.18	Filling	3.38	1.32	Filling	-1.85	Draining	2.16
Bundrant	1.50	4.18	Filling	5.74	4.49	Filling	-2.77	Draining	8.68
Rodeo	1.00	1.96	Filling	8.18	0.64	Filling	-1.52	Draining	10.56
Southeast	2.50	5.92	Filling	6.76	2.75	Filling	-3.29	Draining	12.16
DELIVERY SOURCE		Inflow (MGD)	Pressure (psi)		Inflow (MGD)	Pressure (psi)	Inflow (MGD)	Pressure (psi)	
Pump Station #1		0.0	65		1.7	64	0.0	50	
Pump Station #2		0.0	72		0.0	69	0.0	54	
Pump Station #3		17.8	88		18.6	85	19.7	80	
Pump Station #5		6.7	69		9.8	68	6.9	64	
Pump Station #7 - LPP		3.8	68		3.9	65	7.0	61	
PS #4 Transfer		-6.0			-6.0		-6.0		
Total		22.3			28.1		27.5		
	— 1			T .11 T .	N D	N D	D I II		D
Tank	Tank	Avg Day/	Avg Day/	Fill Time	Max Day	Max Day	Peak Hour	Peak Hour	Drain Time
Location	VOI.	Tank Refilling	Tank Refilling	Avg Day	Inflow	Current	Inflow	Current	at PK Hr*
Opper Pressure Plane	(MG)	(MGD)	Status	(nr)	(MGD)	Status	(MGD)	Status	(nr)
McMillan	3.00	5.07	Filling	9.47	-0.15	Draining	-11.20	Draining	4.29
Airport	1.00	1.63	Filling	9.82	-0.80	Draining	-1.48	Draining	10.84
Proposed UPP	1.50	1.85	Filling	8.65	1.13	Filling	-6.12	Draining	3.92
DELIVERY SOURCE		Inflow (MGD)	Pressure (psi)		Inflow (MGD)	Pressure (psi)	Inflow (MGD)	Pressure (psi)	
Airport Pump Station		3.0	59		1.5	57	1.5	55	
Pump Station #4		7.1	99		4.1	92	5.5	81	
Pump Station #6		10.0	128		7.9	122	11.8	113	
Pump Station #7 - UPP		7.0	123		6.9	120	8.7	106	
Total		27.2			20.4		27.6		
Total Net Delivery		46.45			46.97		53.63		
Maximum System Pressure			128		122		113		
Minimum System Pressure			43		40		36		

* Drain Time @ Peak Hour is based on 2/3 of the tank volume

* Fill Time @ Average Day is based on 2/3 of the tank volume.

6.0 WATER SYSTEM CAPITAL IMPROVEMENT PLAN

The capital improvement plan has six planning periods: 2007-2009, 2010-2012, 2013-2015, 2016-2018, and 2019-2021 and 2022-2031. The 2031 period was chosen because it coincides with the Texas Water Development Board (TWDB) Region G Water Plan. All of the proposed capital improvements for the water system are shown in **Plate 5**. Unit costs used to estimate projected costs of the water system improvements are in **Appendix A**. These costs are for the principal water facilities in the water system and do not include individual service connections or subdivision internal lines. The Water CIP cost estimate tables can be found in **Appendix A**.

Unit costs were based on reviewing bid tabs for several projects ranging in size. The 2007 time period costs were based on 2007 dollars and each subsequent planning period cost was adjusted for inflation. A complete cost table for each time period can be found in **Appendix A**. The costs include an allowance for engineering, surveying, geotechnical engineering and contingencies. The project costs include right-of-way acquisition for pump stations and tanks only. It is recommended that these improvements be constructed generally in the order listed; however, it is understood that development in certain areas of the City's service area may make it necessary to construct some future improvements sooner than anticipated.

Having utilized the hydraulic water model to analyze the water distribution systems capacity and transmission deficiencies in both the existing and future conditions, the improvements necessary to meet future growth were summarized into three-year phases. These phases identify the most pertinent projects necessary to meet the growing demands as they are currently projected. The following sections identify these projects and explain their purpose.

6.1 Water System Improvements from 2007 to 2009

A. Water Service Extension and Looping for Proposed Growth (Projects 1W & 3W)

Project 1W provides an extension of water service and looping to the west portion of the city nearest the airport along SH 201 and extends service to the West Bell County Water Supply Corporation (WBCWSC) service area along Stagecoach Road. Project 1W also connects a 12-inch water line along SH 195 to an existing 12-inch water line, which will provide service in the south portion of the UPP and provide fire flow to the area along Yates Rd. Project 3W extends service and provides looping for proposed development in the south portion of the LPP. Projects 1W and 3W are both either in the design phase or are under construction.

B. Increase Bundrant Elevated Storage Capacity to 1.5 MG (Project 2W)

The existing 0.25 MG Bundrant EST will be replaced with a 1.5 MG EST. This additional capacity is necessary to provide increased storage capacity and mandated fire flow protection for the growth being experienced in the northeast portion of the City in the LPP. Project 2W is also in the design/construction phase.

C. Pump Station 3 Pumping Capacity Expansion (Project 4W)

As the LPP continues to grow, the existing 10 MGD pumping capacity of the existing Pump Station 3 facility will need to be expanded to 18 MGD. This expansion will provide water to the Rodeo and Southeast ESTs and most of the south portion of the LPP. The expansion will also increase the ability to transfer additional water to Pump Station 4 and the UPP.

D. Downtown Condition Assessment Priority Renewal Plan (Project A)

Much of the infrastructure in the original downtown area of Killeen is aging and will require replacement. This proactive project will identify and prioritize projects that are most in need of replacement and critical to the distribution system.

6.2 Water System Improvements from 2010 to 2012

A. Increased Transmission Capacity to the Bundrant EST (Project 5W)

The increased capacity of the Bundrant EST creates a need for additional water lines to adequately supply water to and from the EST. Project 5W is an additional 16-inch water line north along N. 38th St. to increase the amount of water that can be supplied to the Bundrant EST from Pump Station 5. The 16/12-inch water line west along Poage St. and south along W.S. Young Ave. will increase the transmission capacity from the Bundrant Tank to the downtown area.

B. Water Service Extension and Looping in the LPP and UPP (Projects 6W&7W)

Project 6W extends a series of 12-inch and 16-inch water lines in the LPP to provide water service to a portion of the WBCWSC service area. The 16-inch water line connects to an existing 16-inch water line at Stagecoach Rd. and to the 16-inch identified in Project 3W, providing looping and service to additional areas. Project 7W serves in a similar capacity by looping water lines identified in Project 1W and providing service to currently undeveloped areas in the WBCWSC service area.

C. South Delivery Point and Increased Capacity to UPP (Projects 8W, 9W & 10W)

As the southernmost portions of the city continue to grow, expanding existing pumping facilities will not provide adequate transmission and fire flow to the far southern areas. The proposed location of the new South Delivery Point is at the intersection of Chaparral Rd. and East Trimmier Rd. The South Delivery Point is expected to need a 5 MG GST and an initial 7 MGD of pumping capacity for the UPP. Project 9W will be needed in conjunction with Projects 8W and 10W as it provides the necessary transmission capacity to the UPP. It has been projected that the area in the southern section of the UPP will develop before areas in the south section of the LPP. Therefore, the 30-inch water line from the South Pump Station will be isolated from the LPP distribution system and be tied directly into the UPP distribution system. Project 8W will extend a 30-inch and 24-inch water line from the isolated 30-inch water line, which will make a looped system upon connecting to the 24-inch water line in Project 7W, and Project 10W will extend a 20-inch water line to the existing 12-inch water line along SH 195.

D. Downtown Rehabilitation (Project B)

Upon completion of Project A, the Condition Assessment Renewal Plan, several projects will be identified for replacement. This project involves renewing the most critical water lines for the 2010 time period.

6.3 Water System Improvements from 2013 to 2015

A. New Pump Station and Ground Storage Tank Serving the Northeast LPP (Project 11W)

Project 11W includes the building of a new 4 MGD Quarry Road Pump Station and 2 MG Storage Tank connected to an existing 12-inch water line through a 16inch water line. These additions to the LPP will be used to serve the expanding area in the north and allow more growth to the east.

B. Airport Pressure Plane Looping and PRV (Project 12W)

As the area near the airport grows, additional transmission capacity will be necessary to meet the increased demand. The 12-inch water line along the eastern border of the Airport Pressure Plane (APP) will provide a redundant supply of water for fire flow. The PRV connecting the UPP and the APP will allow additional supply into the APP without expanding the Airport Pump Station.

C. UPP Service Extension and Increased Elevated Storage Capacity (Project 13W)

Project 13W includes 12-inch water lines looping in undeveloped areas in the southern section of the UPP. A 20-inch water line will connect to Project 10W and supply a proposed 1.5 MG EST with an overflow of 1,125-feet. This EST will provide pressure and future fire flow demand.

D. 16-Inch Water Line along 38th Street (Project 14W)

Project 14W identifies the need for a 16-inch water line from Pump Station 3 north to the Bundrant EST along S. 38th St. that will create a redundant supply for the Bundrant EST. This 16-inch line also increases the ability of Pump Station 3 to transfer water further north if Pump Station 5 experienced problems.

E. LPP Pump Station and Transmission Lines (Project 15W)

In the 2013 time period, the southern portion of the LPP is projected to grow. Because of this growth and the addition of the South Delivery Point in Project 15W, an additional pumping facility will be necessary to serve the new growth in this area. A 7 MGD pump station will be necessary to supply water to the southern LPP area. Also as a part of Project 15W, a 20-inch water line will connect to the 16-inch water line along East Trimmier Rd., and a 16-inch water line will connect to the existing 16-inch water line bordering the Southeast city limit line. To transmit this water to the system, Project 15W will provide looping along the UPP and LPP border by connecting to the 16-inch water line proposed in Project 3W.

F. Downtown Rehabilitation (Project C)

Upon completion of Project A, the Condition Assessment Renewal Plan, several projects will have been identified for replacement. These projects will renew the most critical water lines for the 2013 time period and improve fire flow availability.

6.4 Water System Improvements from 2016 to 2018

A. Pressure Plane Modifications (Project 16W)

The existing MPP runs along the north portion of US 190 and is primarily fed from Pump Station 4 in the UPP through a PRV and has been identified to be consolidated into the UPP. To achieve this, several 8-inch lines will have to be tied into the system to ensure adequate pressure will be available to the new UPP area. An 8-inch water line along Trimmier Rd. and Marigold will be connected into the new UPP area. The area to the west of the Rodeo EST also experiences lower pressures during maximum and peak hour demand conditions. It is also recommended that this area be brought into the UPP.

B. Increased Transmission Capacity & Looping in UPP (Projects 19W & 20W) Project 19W parallels an existing 12-inch water line along SH 195 and connects to the 20-inch/16-inch water line identified in Project 1W. This line will allow additional supply to the southern portions of the City from Pump Station 4. Project 20W extends water service to the southern most section of the UPP along SH 195 and loops the easterly border of the UPP. These lines are identified and sized to meet the transmission and fire flow capacity for the area.

C. Increased Transmission Capacity & Looping in LPP (Projects 18W, 21W & 25W)

Projects 18W and 21W provide looping and service to the northeast section of the LPP and to future developments. Project 25W provides looping in the southeast

section of the city and provides service to future developments. All lines are sized to meet fire flow demands.

D. Extend Water Service and Looping (Project 22W)

Project 22W will provide water service to the areas growing in the northeast section of the City and will loop the existing system by connecting to the existing 12-inch water line on N. Roy Reynolds Dr. and the proposed 16-inch water line on Rancier Ave.

E. Water Service Extension in LPP (Projects 17W & 23W)

The 16-inch line in Project 23W will create a loop to serve future development areas and connect to Project 25W and Project 17W. The future EST will be supplied water from the South Delivery Point Pump Station through the proposed 16-inch water line in Project 17W, which then runs north connecting to Project 3W with a 12-inch water line.

F. Increased Airport Pressure Plane Boundary and Pumping Capacity (Project 24W)

The area south of W. Stan Schlueter Loop experiences pressures lower than 35 psi under peak hour demands and low fire flow availability in the existing and future 2016 time periods under maximum day demand conditions. It is recommended that the development served by the water line along Judson Ave. be moved into the APP. As the APP continues to grow, additional pumping capacity will be necessary to meet the maximum day demands. The Airport Pump Station should be expanded to 3.0 MGD.

The next pressure plane alteration is the expansion of the APP to serve the development south of the W. Stan Schlueter Loop. This area would experience pressures lower than 35 psi in the future 2016 time period during maximum and peak hour demand periods without alteration.

6.5 Water System Improvements from 2019 to 2021

A. Water Service Extension in the LPP and Elevated Storage (Projects 27W & 29W)

Project 29W provides water service to future development areas in the south portion of the LPP. A 16-inch line connects to Project 23W and will supply the 1.0 MG EST required to serve adequate fire flow and peak hour demand conditions in Project 27W. The line has been sized to meet adequate fire flow and transmission capacities required to serve the area.

B. Increased Transmission Capacity in LPP (Project 28W)

Project 28W is a 16-inch water line that will parallel an existing 8-inch water line along W. Veterans Memorial Blvd. to increase the transmission capacity of Pump Station 3 to the northeastern section of the City.

C. Water Service Extension and Looping for the UPP (Projects 26W & 31W)

Project 26W will provide service for future development by creating a loop connecting a 12-inch water line from Project 20W to a 12-inch water line in Project 13W and running south along SH 195 incorporating the area southeast of SH 195 around FM 2484. Project 31W would extend service west of SH 195 connecting the 1.5 MG GST in Project 13W to the 12-inch water line in Project 26W with a 16-inch water line.

D. Additional South Delivery Point Storage and Pumping Capacity (Project 30W)

The continued growth in the UPP and limited pumping from the north section of the UPP will require the South Delivery Point Pump Station to be expanded by 7 MGD. In order to supply this system properly during peak time periods, the additional pumping capacity will require an additional 5 MG ground storage tank.

6.6 Water System Improvements from 2022 to 2024

A. Water Service Extension and Looping in the LPP (Projects 32W & 33W)

Project 32W will provide a 12-inch loop to the easternmost section of the south LPP area. This line has also been sized to meet the fire flow requirements and provide the needed transmission capacity into this area. The northeast corner of

the LPP will need to be supplied by Project 33W which is a 12-inch water line along FM 439. These water lines will be necessary to sustain pressure and fire flows in the future developing areas.

7.0 WASTEWATER FLOWS

7.1 Historical and Existing Wastewater Flows

As part of the analysis, Freese and Nichols reviewed the historical cumulative monthly wastewater flows from 2000 to 2005. From the data, a gross monthly average daily flow was calculated for each year in MGD and per capita. The data from 2000-2005 is summarized in **Table 7.1**.

Year	Population	Monthly Avg. Daily Flow (MGD)	Monthly Avg. Daily Flow (gpcd)
2000	86,911	9.42	108
2001	89,858	11.78	131
2002	93,587	11.20	120
2003	100,911	10.62	105
2004	102,461	13.60	133
2005	106,145	12.77	120
Average		11.99	122

Table 7.1Historical Wastewater Flows

Historical wastewater records from the City and BCWCID #1 were reviewed to help determine historical average day wastewater flows and wet weather peaking factors. During the data analysis, it was determined that the City's per capita flow is significantly affected by the rate of inflow and infiltration (I/I). Typically, wastewater collection systems see a return of 65% to 80% of a service area's water usage. Historical meter data for the City's water and wastewater systems indicate a high rate of wastewater flow as compared to the City's water usage and are displayed in **Table 7.2**. This is a direct result of excessive inflow and infiltration leading to a strong recommendation for the City to conduct a detailed inflow/infiltration study to identify solutions to eliminate these excess flows that rob the collection system of capacity and results in excessive treatment costs.

	Monthly			
	Total	Rainfall Total	Wastewater/Water	
Month	(gallons)	(inches)	Flow Percentage	
Water December 2005	291,251,411	0.2	860/	
Sewer December 2005	250,318,737	0.2	8070	
Water November 2005	348,326,589	1.2	800/	
Sewer November 2005	309,533,226	1.2	89%	
Water October 2005	406,714,552	0.0	780/	
Sewer October 2005	319,066,289	0.9	7870	
Water September 2005	431,607,308	1 9	70%	
Sewer September 2005	300,346,764	1.0	70%	
Water August 2005	396,836,764	77	1160/	
Sewer August 2005	458,473,506	1.1	110%	
Water July 2005	487,510,748	4	770/	
Sewer July 2005	377,183,613	4	/ / %0	
Water June 2005	452,512,004	0.5	770/	
Sewer June 2005	350,549,520	0.3	/ / %0	
Water May 2005	401,018,312	2.0	0.80/	
Sewer May 2005	391,131,285	5.8	98%	
Water April 2005	343,142,304	0.66	1120/	
Sewer April 2005	384,056,483	0.88	112%	
Water March 2005	313,633,932	2.2	1780/	
Sewer March 2005	557,001,190	5.5	1/8%	
Water February 2005	252,149,540	27	2020/	
Sewer February 2005	508,864,863	5.7	20270	
Water January 2005	291,182,720	1 55	1520/	
Sewer January 2005	444,228,965	4.33	133%	

Table 7.2Comparison of Wastewater Flow to Water Usage

7.2 **Projected Wastewater Flows**

The projected wastewater loads for the 2006 and future periods were calculated using the projected populations, flow monitoring data from the testing period, and other historical meter data. From the historical data in **Table 7.1**, we can conclude that the per capita flow is trending up over time. Due to the historical data identifying I/I issues, an analysis of the flow during the testing period was conducted to determine an accurate per capita flow. It was determined that the per capita flow for 2006 is 105 gpcd and that the average peaking factor for a 5-year/6-hour design-storm for the City of Killeen is approximately 4.0. Freese and Nichols recommends that the per capita flow for all subsequent time periods increase as indicated in **Table 7.3**. The factors used for calculating the future wastewater loads are summarized in **Table 7.3**. Table

7.4 summarizes the projected wastewater flows by major wastewater basin for the 2006, 2011, 2016 and 2031 planning periods.

Year	Average Day per capita (gpcd)	Average Day Flow (MGD)	Peak Wet Weather Factor	Peak Wet Weather Flow (MGD)
2006	105	11.91	4.00	47.64
2011	110	15.18	4.00	60.72
2016	115	18.85	4.00	75.39
2031	115	29.51	4.00	118.02

Table 7.3Projected Wastewater Flows

Table 7.4Summary of Projected Wastewater Flows by Major Wastewater Basin

		20	06		
Major Basin	Served Population	Avg Day Flow Rates	Avg Day Flow (MGD)	Wet Weather Peaking Factor	Peak Wet Weather Flow (MGD)
South Nolan	35,877	105 gpcd	3.77	4.00	15.07
Central	30,955	105 gpcd	3.25	4.00	13.00
Long Branch	22,621	105 gpcd	2.38	4.00	9.50
WWTP	11,140	105 gpcd	1.17	4.00	4.68
SH 195	2,126	105 gpcd	0.22	4.00	0.89
Trimmier Creek	10,700	105 gpcd	1.12	4.00	4.49
Total City	113,419		11.91	-	47.64
		20	11		
Major Basin	Served Population	Avg Day Flow Rates	Avg Day Flow (MGD)	Wet Weather Peaking Factor	Peak Wet Weather Flow (MGD)
South Nolan	40,985	110 gpcd	4.51	4.00	18.03
Central	36,732	110 gpcd	4.04	4.00	16.16
Long Branch	24,867	110 gpcd	2.74	4.00	10.94
WWTP	11,192	110 gpcd	1.23	4.00	4.92
SH 195	6,664	110 gpcd	0.73	4.00	2.93
Trimmier Creek	17,552	110 gpcd	1.93	4.00	7.72
Total City	137,992		15.18	-	60.72
		20	16		
Major Basin	Served Population	Avg Day Flow Rates	Avg Day Flow (MGD)	Wet Weather Peaking Factor	Peak Wet Weather Flow (MGD)
South Nolan	45,125	115 gpcd	5.19	4.00	20.76
Central	40,327	115 gpcd	4.64	4.00	18.55
Long Branch	26,562	115 gpcd	3.05	4.00	12.22
WWTP	11,235	115 gpcd	1.29	4.00	5.17
SH 195	14,133	115 gpcd	1.63	4.00	6.50
Trimmier Creek	26,509	115 gpcd	3.05	4.00	12.19
Total City	163,891		18.85	-	75.39
		20	31		
Major Basin	Served Population	Avg Day Flow Rates	Avg Day Flow (MGD)	Wet Weather Peaking Factor	Peak Wet Weather Flow (MGD)
South Nolan	56,732	115 gpcd	6.52	4.00	26.10
Central	51,595	115 gpcd	5.93	4.00	23.73
Long Branch	42,228	115 gpcd	4.86	4.00	19.43
WWTP	11,320	115 gpcd	1.30	4.00	5.21
SH 195	26,849	115 gpcd	3.09	4.00	12.35
Trimmier Creek	67,851	115 gpcd	7.80	4.00	31.21
Total City	256,576		29.51	-	118.02

8.0 EXISTING WASTEWATER SYSTEM

8.1 Existing Wastewater Collection System

The existing collection system currently conveys wastewater to the BCWCID #1 South Nolan and Trimmier Creek WWTPs. The South Nolan WWTP total treatment capacity is 21 MGD, with 15 MGD of treatment capacity at Plant #1 and 6 MGD of treatment capacity at Plant #2. The Trimmier Creek WWTP was constructed with an initial treatment capacity of 6 MGD. The City of Killeen's service area is divided into six sub-basins: Central, Long Branch, South Nolan, Trimmier, WWTP, and SH 195. Most portions of the Central, Long Branch, WWTP, and South Nolan Subbasins gravity flow to the South Nolan WWTP. The Trimmier and SH 195 subbasins' natural flow lines are away from South Nolan WWTP and are being redirected to the Trimmier Creek WWTP, eliminating some of the existing lift stations. Where possible, it is desirable to construct gravity wastewater lines and avoid lift stations to avoid the additional energy and operations and maintenance costs associated with lift stations.

8.2 Wastewater Model Development

The model of the City of Killeen's wastewater system includes 10-inch and larger wastewater gravity lines, key 8-inch wastewater gravity lines and force mains for all major lift stations. **Plate 6** shows the wastewater lines that are included in the wastewater model. The wastewater model was constructed using the City's Geographical Information System (GIS) Spatial Data Engine (SDE) database to include wastewater lines and manhole shapefiles. Invert elevations for major interceptors were added using as-built drawings. If as-builts of the pipe inverts were not available, inverts were back calculated either from known inverts using TCEQ minimum slope requirements or by straight line interpolation if an upstream and downstream invert was available. The budget did not include the cost to field verify inlet elevations. Wet wells and pumps at lift stations were added to the model using as-built drawings and pump curves from the City.

Once the census tract populations were determined, each of the six sub-basins in the study area was intersected with the census tracts to determine the 2006 through 2031 population estimates by sub-basin. A summary of flows by sub-basin is displayed in **Table 7.4** "Summary of Projected Wastewater Flows by Major Wastewater Basin." For all planning periods, the sub-basin populations were distributed to each manhole using Thiessen-polygons to determine a population that contributes flow to each manhole. The populations by census tract are displayed in **Plate 2**. After distributing the wastewater loads, dry weather and wet weather calibrations of the model were performed based upon flow monitoring from May through June 2006.



8.3 Wastewater System Field Testing

The wastewater field testing was conducted from May 4, 2006 through June 1, 2006. During this time, three temporary flow meters were installed by Freese and Nichols to record the flow generated by the City of Killeen and record the effect that any rain events had on the system. These three flow meters were placed on critical collection mains. Additional flow data was obtained from meters owned by the City of Killeen and BCWCID #1. These meters helped determine the total flow at the WWTP and the amount of flow contributed to the system by Fort Hood. BCWCID #1 has four meters that record incoming flow from Fort Hood and one meter that records all flow coming from Fort Hood and the City of Killeen. During the monitoring period, a significant rainfall event was recorded which allowed for a discrete calculation of Rainfall Dependent Inflow/Infiltration (RDII) for the City. **Appendix D** contains the wastewater field testing information.

8.4 Dry Weather Model Calibration

The primary components of the wastewater flows in sanitary sewers during dry weather periods are domestic wastewater, industrial wastewater, and groundwater infiltration. Loads that originate from ground water infiltration (GWI) typically enter the sewer system through defective pipes or connections and/or through manhole walls. Other dry weather loads can include water from public fountain drains, pools, cooling water discharges, and other intermittent industrial/commercial discharges. For this study, there are no specific inflows known, and GWI was assumed to be present within the gross gpcd assigned to each manhole. Based on the available data, all flows were distributed on a per capita basis for domestic wastewater flows. The principal sources of domestic sanitary sewer loads are residential areas and commercial developments.

In order to determine a dry weather calibration time period, the metered flow data was analyzed to determine an average hourly flow for a period of 24 hours for each of the three meter locations. For each of the metered locations, the dry weather calibration time period selected was May 27, 2006. Using each meter's dry weather flow data and the population distribution by sewer sub-basins, an estimated gross gpcd was calculated for each sub-basin. Based on the gpcd and the distributed population within each sub-basin, flows were generated and assigned to each manhole within the sub-basin.

In order to represent the flows entering the system over time, a dry weather pattern was developed for each sub-basin based on the flow meter data. The pattern was calculated by using the measured hourly flow divided by the average daily flow for the calibration time period. Each manhole was then assigned a pattern. At this point, the model was run and compared to the measured dry weather event data. Manning's roughness coefficient was adjusted for various pipes until the model was calibrated for the dry weather event of May 27, 2006. A map of the flow meters observed and modeled flows can be seen in **Plate 7**. The results show a close correlation between the dry weather model flows and those measured in the field for actual conditions. Additional information on the dry weather calibration is contained in **Appendix D**.

8.5 Wet Weather Model Calibration

The primary components of wet weather flows are the same as dry weather flows plus the flows that can be linked to rainfall dependent infiltration and inflows (RDII). When determining wet weather loads, one must consider the hydrologic analysis of excess precipitation and the associated runoff. In order to calibrate the model to a specific rainfall event, recorded flow meter data during a rain event and the model simulation of that event were compared. When analyzing the data for wet weather events it was determined that one significant storm event of 2.5-inches was recorded during the testing period. The event recorded peak wet weather flows less than anticipated due to extremely dry antecedent soil conditions, which lowers the expected RDII. The field data was adjusted to represent more typical weather and saturated soil conditions.



For each sub-basin, the dry weather flow event was subtracted from the recorded flow from each storm by each hourly time step to determine the amount of RDII for that storm event for a 24-hour time period. In other words, the difference between the two curves by time step provides the amount of RDII volume generated by that storm event for each sub-basin. For each hourly time step within the storm, the RDII was then divided by the average hourly RDII. The value derived from this calculation produces a 24-hour wet weather RDII pattern for the storm for each sub-basin.

An RDII per diameter-inch of linear foot of pipe was calculated for each sub-basin. To calculate the amount of RDII per diameter-inch of linear foot of pipe the total volume of RDII per sub-basin for each storm was divided by the diameter-inch of linear foot of pipe. The estimated RDII per diameter-inch of pipe was then added to the model. Each sub-basin was then assigned a wet weather pattern. The model was run and the results were compared to the flow meter data collected at each site. In order to calibrate the model, minor adjustments were made to the wet weather patterns. In **Plate 8**, a snapshot of the wet weather calibration model shows the observed versus modeled flows for each flow meter for that rain event. Additional information on the wet weather calibration is contained in **Appendix D**.

8.6 Wastewater System Design Criteria

A. Sewer Trunk Lines (Interceptors)

The design criteria for sewer trunk lines or interceptors is based on the TCEQ requirements that meet peak wet weather design flows with no overflows while maintaining a minimum of 2-feet/second cleaning velocity and a maximum of 8-feet/second velocity.

B. Lift Station Pumping Capacity

The design criteria for lift station pumping shall be to provide firm pumping capacity to meet 125% of the peak wet weather design flows. The firm pumping capacity is defined as the total available pumping capacity with the largest pump out of service.



Freese and Nichols, Inc. [KIL06188]: H:DELIVERABLES\DELIVERABLE_06-28-07_(Final_CIP_v3)\(Plate_8)-Wet_Weather_Calibration_Map.

C. Lift Station Wet Well Capacity

The design criteria for lift station wet wells are to provide adequate volumes to limit pump cycling to once every 10 minutes. Based on this criterion, the required operating volume for each pump can be calculated as:

$$V = \frac{t * Q}{4}$$

where,

t = Maximum pump cycling time (10 minutes)

Q = Lead pump discharge rate (gpm)

V = Required wet well volume between pump start and stop elevation

D. Force Mains

The design criteria recommended for force mains is to meet the required pumping capacity of the lift station at a velocity less than 8-feet per second and a maximum discharge pressure of 100 psi and to allow a minimum of 2-feet per second scouring velocity during a single pump operation.

8.7 Existing Wastewater System Analysis

In order to evaluate the existing wastewater collection system, Freese and Nichols staff met with City staff and operations personnel. They were able to identify areas of concern and potential problem areas based on existing conditions and future development. In addition, Freese and Nichols staff investigated various portions of the system during field testing and analyzed historical and current flow monitoring records. The culmination of the analysis was the use of the model to determine the vulnerabilities of the system under varying load conditions to include analysis of the system under the influence of a design storm event, which would produce peak wet weather loads. Based on these factors, areas of concern were identified for the existing system:

• The northern and central portions of the City experience higher than normal rates of Inflow and Infiltration (I/I) resulting in significant overloading of existing lines during peak wet weather conditions.

- The City needs to continue constructing improvements in the southern portion of the collection system to transfer additional flows to the Trimmier Creek WWTP in order to reduce the costs associated with pumping and to free up capacity in the interceptors going to the existing South Nolan WWTP.
- Lift Station 8 needs to be rehabilitated or replaced.
- Lift Station 7 needs to be rehabilitated or replaced.
- The collection mains that flow into Lift Stations 1 and 6 experience significant surcharging.

9.0 FUTURE WASTEWATER SYSTEM

9.1 Design Storm Conditions

In order to determine the appropriate pipe capacity for future wastewater loads the appropriate per capita load must be combined with the effect of a 5-year/6-hour storm on the City of Killeen's collection system. The RDII was calculated for both flow monitoring rain events and plotted on a graph. By using the two wet weather points, a trend line was plotted to show the volume of expected RDII that would occur for a 5-year/6-hour design storm (as shown in Figure 9.1). From this data, the estimated RDII was calculated for the City and distributed within each sub-basin. By using the existing wet weather flow data, an hourly interpolation of the design storm wet weather flow was developed. The loads in each of the sub-basins were then assigned a 24-hour wet weather pattern for the design storm. When the model was run with the design storm conditions, all gravity mains were analyzed to determine which pipes were surcharged. Surcharged pipes were defined by taking the modeled flow and dividing by the available pipe capacity during free flow conditions. If this ratio was 1.0 or greater, it was considered surcharged. Manholes were also identified as potential Sanitary Sewer Overflows (SSOs) if the manholes had an unfilled depth of less than 2-feet from the rim elevation. Based on the modeling and the analysis, portions of the wastewater collection system were identified for future CIP projects and sized in order to carry future flows.



Figure 9.1 Design Storm RDII Graph
10.0 WASTEWATER SYSTEM CAPITAL IMPROVEMENT PLAN

The capital improvement plan has six planning periods: 2007-2009, 2010-2012, 2013-2015, 2016-2018, 2019-2021 and 2022-2031. All of the proposed capital improvements for the wastewater system are shown in **Plate 9**. Unit costs used to estimate projected costs of the wastewater system improvements are in **Appendix B**. These costs are for the principal wastewater collection facilities in the wastewater system and do not include individual service connections or subdivision internal lines. The estimated costs for the wastewater CIP by project can be found in **Appendix B**, Wastewater Capital Improvement Cost Estimates.

Unit costs were based on reviewing bid tabs for several projects ranging in size. These costs include an allowance for engineering, surveying, geotechnical engineering and contingencies. The project costs only include right-of-way acquisition for lift stations and not for wastewater lines. It is recommended that these improvements be constructed generally in the order listed; however, it is understood that development in certain areas of the City and its service areas may make it necessary to construct some future improvements sooner than anticipated. Additional information on the wastewater collection system and its improvements are in **Appendix B**.



10.1 Wastewater System Improvements from 2007 to 2009

A. Lift Station Upgrade to Support Growth in Long Branch Sub-basin (Project 1S)

The area near Roy Reynolds Drive is experiencing growth, which will require an upgrade to Lift Station 8. The projected population through 2016 is over 17,000 people, which will contribute an estimated peak flow of 4.86 MGD to the subbasin supported by Lift Station 8. The estimated peak wet weather flow of 4.86 MGD is based on a system that has aged sufficiently such that the amount of rainfall dependent inflow and infiltration (RDII) will match the existing peaking factor of 3.9 for that area of the City. Since the majority of the population growth that will occur in the sub-basin will require construction of a new collection system, the estimated rainfall dependent inflow and infiltration (RDII) can be significantly reduced for the first 10 years. It is estimated that through 2016 an estimated peak wet weather flow of 4.0 MGD can be expected. Based on this, it is recommended that the Lift Station #8 Rehabilitation Project install three pumps with a duty point of 1,400 gpm pumps at 80-feet total dynamic head (TDH). This recommendation is only to support the anticipated growth and aging of the system through 2016. Beyond 2016, as the population and the age of the system increases, additional capacity will be required.

B. Collection Interceptor to Support Growth (Projects 2S, 3S)

In order to support growth in the southern portion of the City's service area, a major collection interceptor is needed from Featherline Rd. to just east of East Trimmier Rd. This interceptor network will provide the backbone for the collection system required to service a majority of the growth that will occur for the next 10 years. The interceptor network will carry flow into an existing interceptor that is served by the new BCWCID #1 Trimmier Creek WWTP just south of the City. Future developments, which will be supported by the interceptor, include a new school and police station in the vicinity of Chaparral Rd. and Featherline Rd.

C. Collection System to Support Growth in SH 195 Sub-basin (Projects 4S, 5S) In order to support growth in the SH 195 Sub-basin, a series of gravity mains, lift stations and force mains need to be constructed. When constructed, flow will initially be lifted by force main to a Central Sub-basin gravity main and treatment will occur at the existing BCWCID #1 Nolan Creek WWTP. In the future the flows from these supported areas will be redirected through Project 2S to the Trimmier Creek WWTP. In addition to the new growth that these projects will support, they will also allow the decommissioning of Lift Station 11A, which will reduce the amount of pumping that occurs in the system.

D. Reduction of Inflow and Infiltration in the City (Project A)

When evaluating a wastewater collection system, the amount of inflow and infiltration (I/I) entering the system can play a critical role in the assessment and sizing of pipes, lift stations, and required WWTP capacities. I/I simply defined are flows that enter a wastewater collection system that do not originate from a paying customer. Based on the flow monitoring data, it was determined that an excessive I/I rate for the City of Killeen is occurring. Typically, the wastewater system of a City collects about 65% to 80% of the City's water demand. Based on flow meter recordings, the City of Killeen has experienced significant I/I during rain events. Flow monitoring conducted during the study indicates that portions of Long Branch, WWTP, Central and South Nolan Sub-basins merit further study. In order to determine which specific areas in the sub-basins require rehab and/or expansion, the City of Killeen needs to conduct an I/I Study.

10.2 Wastewater System Improvements from 2010 to 2012

A. Collection System for New Service Areas and Interconnectivity (Projects 6S, 9S)

These projects will provide dual functions for the overall collection system in Killeen. First, it will allow the flow from Projects 4S and 5S to be redirected to the Trimmier Creek WWTP, which will free up treatment capacity at the existing Nolan Creek WWTP and flow capacity in numerous gravity mains needed to support growth in other areas of the City. Secondly, it will also provide service

for new customers along Stagecoach Rd. from West Trimmier Rd. to East Trimmier Rd.

B. Collection System to Support Growth in South (Projects 7S, 10S, 12S, 13S) Growth along the SH 195 Corridor will need to be serviced. In order to support residential and commercial development along the upper portions of North Reese Creek subcatchement, additional collection mains will need to be constructed north of Reese Creek Road (Project 7S). The construction of these collection mains will gravity flow into Lift Station 20 (Project 4S). In order to support growth in and around the southwestern portion of South Nolan Creek Sub-basin, Lift Station 23 will need to be expanded to a 2.0 MGD firm capacity (Project 12S). Another key portion of the collection system in the South is the construction of gravity mains, a lift station, and force main system to support development expected to occur along the southern portion of the SH 195 corridor (Projects 10S & 13S). This project will collect flows from new customers and which will be lifted eastward to Project 3S where it will gravity flow to the Trimmier Creek WWTP.

C. CMOM/SSO Program (Project B)

The EPA Capacity Management Operations and Maintenance (CMOM) program is not official legislation at this time; however, the EPA has expressed to the state governments that the CMOM program will happen at some point in the future. The Texas Commission on Environmental Quality (TCEQ), which is responsible for wastewater system compliance, is currently inviting municipalities to be a part of the Sanitary Sewer Overflow Initiative (SSOI) Program. For now, the criteria being used to select entities for participation in the CMOM/SSOI Program include: large systems, large systems with problems, and medium systems with problems. When systems volunteers for the program, they are asked to develop and implement programs that include the following:

- Reduce/ Eliminate overflows
- Tracking Sanitary Sewer Overflows (SSOs)
- Categorizing SSOs by cause

- SSO Response Plan (Sanitary Sewer Evaluation Studies, capacity analysis, CIP, CMOM audit)
- Backup power requirements for lift stations
- Effluent treatment standards raised for BNR

Freese and Nichols recommends that the City of Killeen take proactive steps to meet impending CMOM standards by executing Project B. Project B will allow the City to get ahead of the pending legislation and develop the programs necessary to meet CMOM standards over a longer time period, instead of being forced to meet those standards based upon future legislation, or worse, through an Administrative Order.

D. Reduction of I/I to Free up Treatment and Collection Capacity (Projects 8S & C)

In order to free up treatment and collection capacity to support future growth and to reduce the amount of flow treated at the Nolan Creek WWTP, the study area identified in Project A will require several future projects. Based on existing information, Project A will need to be conducted in order to reduce I/I flows and reduce the likelihood of an administrative order or fines due to sanitary sewer overflows. Since Project A will provide a more in-depth look at the study area, the results from the study may reduce, eliminate, or identify more specific projects for execution.

E. Lift Station Upgrade in Central Sub-basin (Project 11S)

Lift Station 7 collects flows in the far eastern portion of the Central Sub-basin and pumps the flow to a gravity main to be treated in the existing Nolan Creek WWTP. In order to ensure dependable service in its service area, Lift Station 7 will need to have extensive rehabilitation performed, or a new lift station will need to be constructed to replace it.

10.3 Wastewater System Improvements from 2013 to 2015

A. New Collection System to Support Growth in Long Branch (Projects 14S & 15S)

Future growth along Hay Branch in Long Branch Sub-basin will require a collection system and lift station (Project 14S). The new Hay Branch Lift Station will also receive flows from a new lift station and gravity system located to the northeast along a tributary of South Nolan Creek near FM 439. The FM 439 Lift Station will support growth that will occur north of and along FM 439. Flows from these lift station will be treated at the Nolan Creek WWTP

- B. Collection System to Support Growth South of the City (Projects 16S & 17S) As developments occur in the south, new collections systems will have to be constructed to support and convey flows to the Trimmier Creek WWTP. Project 16S and 17S consist of gravity mains and the new Upper Rock Creek Lift Station to support expected development along portions of Rock Creek and immediately south of Chaparral Rd.
- C. Interceptor to Support Growth in the Central Sub-basin (Project 18S)

The Central Sub-basin will require additional interceptor capacity in order to support the future flow projections. The existing interceptor will have to be upsized to a 21-inch/24-inch/36-inch pipe starting just west of Gateway Drive to the new Lift Station 2. Depending on the results of the I/I study in Project A, this project may be subject to a reduction in scope or the project may shift focus to other collection pipes that feed into it.

D. Collection System to Support Growth in South Nolan Sub-basin (Project 19S)

The western portion of South Nolan Sub-basin will require two separate gravity mains, the new Lift Station 25, and an 8-inch force main in order to support commercial and residential growth. Lift Station 25 will be located west of Clear Creek Rd. Flows that are pumped from both lift stations will be transported through the existing collection system in South Nolan Sub-basin and will be treated by the Nolan Creek WWTP.

10.4 Wastewater System Improvements from 2016 to 2018

A. Collection System to Support Growth in the South (Projects 20S, 21S, 22S, 24S)

In order to support growth south of Chaparral Rd. multiple lift stations and the supporting gravity collection systems will need to be constructed. Four lift stations aligned in a series will collect flows from their own gravity network and the preceding lift station and pump the flow from the west to the east, where it will ultimately be lifted to the Trimmier Creek WWTP. All four lift stations will be located along tributaries that feed the Lampasas River/Stillhouse Hollow Lake. The flows will be collected and pumped from the Live Oak Cemetery Lift Station (Project 24S), to the Lower Rock Creek Lift Station (Project 22S), to the Onion Creek Lift Station (Project 21S), and the Little Trimmier Creek Lift Station (Project 20S). The Trimmier Creek Lift Station will then lift the flows to the Trimmier Creek WWTP.

B. New Gravity Main in the North (Project 23S)

With expansion and growth, a new 8-inch gravity main will be constructed to convey flow to the Hay Branch Lift Station.

10.5 Wastewater System Improvements from 2019 to 2021

A. Addition of a Parallel Major Interceptor to Trimmier Creek WWTP (Project 25S)

In order to convey the additional flow as the City grows, a 30-inch parallel interceptor will be required from just east of East Trimmier Rd. to the Trimmier Creek WWTP.

B. Development of SH 195 Corridor (Projects 26S, 27S, 28S)

As the SH 195 corridor continues to develop, additional areas will require utility service. In order to support this growth two new lift stations and their subcatchement systems will be required. The new Lampasas Lift Station will collect flows from two collection mains, a 10-inch/12-inch gravity main and an 8-inch/10-inch/12-inch gravity main located along a Lampasas River tributary. The Lampasas Lift Station will then pump the flows to the South SH 195 Lift Station. The South SH 195 Lift Station also collects flows from a new 10-inch/12-inch gravity main just west of SH 195 and a second 10-inch/12-inch gravity main along the southern portion of Reese Creek. The South SH 195 Lift Station will

pump the flows it collects along a new 10-inch force main to the North SH 195 Lift Station constructed in Project 13S.

C. Rehabilitation of Lift Station 1(Project 29S)

Lift Station 1 will require rehabilitation in order to effectively convey flows to the Nolan Creek WWTP. Based upon the age of the lift station, it is expected that the pumping units at the lift station will require replacing.

10.6 Wastewater System Improvements from 2022 to 2024

A. New Collection System to support Growth in the South (Project 30S)

In order to accommodate additional growth south of Stillhouse Hollow Lake, SH 2484 Lift Station will need to be constructed along with an 8-inch force main to convey the flow collected from a 12-inch gravity main north of the Little Trimmier Creek Lift Station.

B. New Collection System to support Growth in the North (Project 31S)

As the City grows further to the East towards Shaw Branch a new gravity main will be installed to support the expansion along with the construction of the Shaw Branch Lift Station to lift flow west through an 8-inch force main to a 12-inch gravity main connected to the FM 439 Lift Station.

11.0 Summary Capital Improvement Costs and Bond Program

Currently the City of Killeen funds its Capital Improvement Program through (threeyear) bond packages. In order to assist the City with developing its bond program, Freese and Nichols evaluated projects based on projected needs and put together six, three-year bond packages that will allow for the construction of the projects identified by this report. The bond packages are laid out for the following time periods:

2007-2009 2010-2012 2013-2015 2016-2018 2019-2021 2022-2024

Each of the bond packages lists the most important projects for each time period first. **Table 11.1** summarizes the costs for each bond-package, showing the water and wastewater projects separately and the combined cumulative costs for both programs. The costs shown have been adjusted to provide an estimated cost escalation associated with projected inflation.

Table 11.1 Summary of Capital Improvement Costs and Bond Program

	WATER		2007	7	SANI	TARY SEWER		
	WATER		Cumulative		GAN	TART SEWER	Cumulative	Combined
Project	Description	Cost	Cost	Project	Description	Cost	Cost	Cumulative
1W	12/16/20" along Reese Creek Rd.	\$2,931,506	\$2,931,506	1S	Lift Station #8	\$1,086,200	\$1,086,200	\$4,017,706
2W	1.5 MG Bundrant EST Expansion	\$2,352,000	\$5,283,506	2S	Trimmier Creek 21/27/36" Gravity Main	\$2,850,052	\$3,936,252	\$9,219,758
3W	12/16" Southeast Loop	\$2,414,402	\$7,697,908	3S	Trimmier Creek 21" Gravity Main	\$1,076,923	\$5,013,176	\$12,711,083
4W	Pump Station 3 Upgrade	\$3,360,000	\$11,057,908	4S	LS 20 and 14" FM & SH 195 12/18" GM	\$3,254,435	\$8,267,610	\$19,325,518
			\$11,057,908	5S	LS #22, 6" FM, 12"	\$1,649,460	\$9,917,071	\$20,974,978
TOTAL		\$11,057,908		TOTAL		\$9,917,071	. , ,	\$20,974,978
	WATER	1 · · ·	2010)	SANI	TARY SEWER		. , ,
			Cumulative				Cumulative	Combined
Project	Description	Cost	Cost	Project	Description	Cost	Cost	Cumulative
5W	12/16" along N. Young Drive	\$861,638	\$861,638	6S	Stagecoach 18" GM & 14" FM, 8/10"	\$2,053,237	\$2,053,237	\$2,914,875
6W	12/16" Onion Road Water Line	\$1,770,828	\$2,632,466	7S	SH195 12/15" GM	\$914,445	\$2,967,682	\$5,600,148
7W	12/24" Trimmier Road Water Line	\$2,108,091	\$4,740,557	8S	Long Branch 15/18/24" GM	\$2,055,044	\$5,022,726	\$9,763,283
8W	24/30" along Chaparral Road	\$2,339,904	\$7,080,461	9S	Trimmier Creek 10/12" GM	\$1,447,729	\$6,470,455	\$13,550,916
9W	5 MG GST, 7 MGD PS, 30" Line	\$7,604,248	\$14,684,709	10S	16" FM Along Chaparral Rd.	\$1,046,514	\$7,516,969	\$22,201,678
10W	20" Line along Chaparral Rd	\$1,150,464	\$15,835,173	11S	Lift Station 7 Rehab	\$651,840	\$8,168,809	\$24,003,982
			\$15,835,173	12S	Expand Lift Station #23	\$779,520	\$8,948,329	\$24,783,502
			\$15,835,173	13S	LS & 14"FM 12/10"GM-Chaparal Rd	\$3,016,469	\$11,964,798	\$27,799,971
TOTAL		\$15,835,173		TOTAL		\$11,964,798		\$27,799,971
	WATER	n	2013	3	SANI	FARY SEWER	Comparing	C ombined
Project	Description	Cost	Cumulative	Project	Description	Cost	Cumulative	Cumulative
11W	4 MGD PS 16" along FM 439	\$4,646,006	\$4,646,006	149	New I S #18_16" FM_10/12/15" GM	\$4 377 626	\$4 377 626	\$9,023,632
12\//	12" Airport/ Lipper PP	\$1 429 716	\$6,075,723	159	New Lift Station 10" FM 12" GM	\$2,618,368	\$6,995,994	\$13,071,717
13\//	12/20" & 1.5 GST W of Chap. Rd	\$2 981 477	\$9,057,200	165	Future Planning Area 10/15" GM	\$1 702 973	\$8,698,967	\$17,756,167
14W	16" Water Line along 38th Street	\$1 470 927	\$10 528 127	175	New 2 MGD LS 10" FM 10/12" GM	\$2 611 385	\$11 310 352	\$21,838,479
15W	16/20/24"& 7.0 MGD PS Lower PP	\$4 382 112	\$14 910 239	185	Central Basin 21/24/36" GM	\$2 884 144	\$14 194 496	\$29,104,735
		• .,• • _, · · =	\$14,910,239	195	N Clear Creek LS25 8"FM&12"	\$1,836,124	\$16.030.620	\$30,940,859
			• //			· //	• • • • • • • • • •	
TOTAL		\$14,910,239		TOTAL		\$16,030,620		\$30,940,859
TOTAL	WATER	\$14,910,239	2016	TOTAL	SANI	\$16,030,620		\$30,940,859
TOTAL	WATER	\$14,910,239	2016 Cumulative	TOTAL	SANI	\$16,030,620 TARY SEWER	Cumulative	\$30,940,859 Combined
TOTAL Project	WATER Description	\$14,910,239 Cost	2016 Cumulative Cost	TOTAL Project	SANI Description	\$16,030,620 FARY SEWER Cost	Cumulative Cost	\$30,940,859 Combined Cumulative
TOTAL Project 16W	WATER Description Pressure Plane Modifications	\$14,910,239 Cost \$806,400	2016 Cumulative Cost \$806,400	TOTAL Project 20S	SANI Description New LS, 18"FM 12/15/18" GM	\$16,030,620 TARY SEWER Cost \$6,114,966	Cumulative Cost \$6,114,966	\$30,940,859 Combined Cumulative \$6,921,366
TOTAL Project 16W 17W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS	\$14,910,239 Cost \$806,400 \$1,131,043	2016 Cumulative Cost \$806,400 \$1,937,443	TOTAL Project 20S 21S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214	Cumulative Cost \$6,114,966 \$9,338,180	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623
Project 16W 17W 18W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173	TOTAL Project 20S 21S 22S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725
TOTAL Project 16W 17W 18W 19W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St.	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763	TOTAL Project 20S 21S 22S 23S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981
Project 16W 17W 18W 19W 20W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243	Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718
Project 16W 17W 18W 19W 20W 21W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863	Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338
Project 16W 17W 18W 19W 20W 21W 22W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075	Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550
TOTAL Project 16W 17W 18W 19W 20W 21W 22W 23W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916	Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391
TOTAL Project 16W 17W 18W 19W 20W 21W 22W 23W 24W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156	Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495	Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195	\$16,030,620 TARY SEWER \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Along FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495	Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195	\$16,030,620 TARY SEWER \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Along FM 439 12" Along To FM 439 12/16" SW part of Lower PP WATER	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2019 Cumulative	Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195	\$16,030,620 TARY SEWER \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 Combined
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Along FM 439 12/16" SW part of Lower PP WATER Description	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495 Cost	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2019 Cumulative Cost	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI Description	\$16,030,620 TARY SEWER \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 Combined Cumulative
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Along FM 439 12"/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495 Cost \$3,473,971	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2019 Cumulative Cost \$3,473,971	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project 25S	SANI Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI Description Trimmier Creek 30" Gravity Main	\$16,030,620 TARY SEWER \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 Combined Cumulative \$5,853,075
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Along FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495 Cost \$3,473,971 \$2,483,960	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2019 Cumulative Cost \$3,473,971 \$5,957,931	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project 25S 26S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI Description Trimmier Creek 30" Gravity Main New LS, 10" FM & 12" GM by 2484	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970\$31,964,970 \$31,964,970\$31,964,970 \$31,965,965
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$1,5988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2019 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project 25S 26S 27S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475\$15,976,475 \$15,976,475 \$15,976,475\$15,976,475 \$15,976,475 \$15,976,475\$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$16,976,476\$16,976,476,476\$16,976,476\$16,976,476\$16,976,476	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$1,5988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project 25S 26S 27S 28S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, 8/10/12" near SH195 10/12" West of SH 195	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475\$15,976,475 \$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$16,	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$32,773,679
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W 30W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop 5.0 MG GST & 7.0 MGD PS Expan.	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1672,339 \$15,988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773 \$6,289,920	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618 \$18,213,538	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project 26S 27S 28S 29S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, 8 10/12" near SH195 10/12" West of SH 195 Lift Station #1 Rehab.	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000 \$1,196,160	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475\$15,976,475 \$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$30,259,759
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W 30W 31W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop 5.0 MG GST & 7.0 MGD PS Expan. 16" West of 195 in Upper PP	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$1,5988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773 \$6,289,920 \$2,184,248	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618 \$18,213,538 \$20,397,786	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project 26S 27S 28S 29S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, 8/10/12" near SH195 10/12" West of SH 195 Lift Station #1 Rehab.	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000 \$1,196,160	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475\$15,976,475 \$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$33,259,759 \$32,2444,007
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W 30W 31W TOTAL	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop 5.0 MG GST & 7.0 MGD PS Expan. 16" West of 195 in Upper PP	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773 \$6,289,920 \$2,184,248 \$20,397,786	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2019 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618 \$18,213,538 \$20,397,786	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project 26S 27S 28S 29S TOTAL	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, 8/10/12" near SH195 10/12" West of SH 195 Lift Station #1 Rehab.	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000 \$1,196,160 \$12,046,221	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$33,259,759 \$32,444,007 \$32,444,007 \$32,444,007
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W 30W 31W TOTAL	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop 5.0 MG GST & 7.0 MGD PS Expan. 16" West of 195 in Upper PP	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773 \$6,289,920 \$2,184,248 \$20,397,786	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2015 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618 \$18,213,538 \$20,397,786	TOTAL Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI" Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, 8/10/12" near SH195 10/12" West of SH 195 Lift Station #1 Rehab.	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000 \$1,196,160 \$12,046,221 TARY SEWER	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475}	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$32,2444,007 \$32,444,007
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W 30W 31W TOTAL	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop 5.0 MG GST & 7.0 MGD PS Expan. 16" West of 195 in Upper PP WATER	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773 \$6,289,920 \$2,184,248 \$20,397,786	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2015 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618 \$18,213,538 \$20,397,786 2022 Cumulative	TOTAL Project 20S 21S 22S 23S 24S TOTAL Project 26S 27S 28S 29S TOTAL	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI" Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 8"FM, 8/10/12" near SH195 10/12" West of SH 195 Lift Station #1 Rehab.	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000 \$1,196,160 \$12,046,221 TARY SEWER	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475\$15,976,475 \$15,976,475 \$15,976,475\$15,976,475 \$15,976,475 \$15,976,475\$15,976,475 \$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475 \$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,976,475\$15,	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$32,244,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$33,2444,007 \$32,2444,007 \$32,2444,007 \$32,2444,007 \$33,2447 \$33,2447 \$33,2447 \$33,247 \$34,347 \$35,247
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W 30W 31W TOTAL Project 28W 29W 30W 31W TOTAL	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop 5.0 MG GST & 7.0 MGD PS Expan. 16" West of 195 in Upper PP WATER Description	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$1,5988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773 \$6,289,920 \$2,184,248 \$20,397,786 Cost	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2019 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618 \$18,213,538 \$20,397,786 2022 Cumulative Cost	TOTAL Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI" Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 8"FM, 8/10/12" near SH195 10/12" West of SH 195 Lift Station #1 Rehab. SANI" Description	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000 \$1,196,160 \$12,046,221 TARY SEWER Cost Cost	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475\$15,	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$32,2773,679 \$30,259,759 \$32,444,007 \$32,444,0
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W 30W 31W TOTAL Project 32W 29W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop 5.0 MG GST & 7.0 MGD PS Expan. 16" West of 195 in Upper PP WATER Description 12" Water Line in SE Lower PP 42" Water Line in SE Lower PP	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,912,620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773 \$6,289,920 \$2,184,248 \$20,397,786 Cost \$3,401,691 \$4,40,691 \$4,40,691	2016 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2019 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618 \$18,213,538 \$20,397,786 2022 Cumulative Cost \$3,401,691	TOTAL Project 20S 21S 22S 23S 24S	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI" Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 8"FM, 8/10/12" near SH195 10/12" West of SH 195 Lift Station #1 Rehab. SANI" Description New LS, 8" FM, 12" Gravity Main	\$16,030,620 TARY SEWER Cost \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER Cost \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000 \$1,196,160 \$1,20,046,221 TARY SEWER Cost \$2,705,276 \$2,705,276	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$15,976,475 \$12,046,221 \$12,046,221 \$12,046,221 \$12,046,221 \$12,046,221 \$12,046,221 \$12,046,221 \$12,046,221 \$12,046,221	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$32,244,007 \$32,2444,007 \$32,444,0
Project 16W 17W 18W 19W 20W 21W 22W 23W 24W 25W TOTAL Project 26W 27W 28W 29W 30W 31W TOTAL Project 32W 32W 32W	WATER Description Pressure Plane Modifications 12/16" at Chaparral & Bell PS 12" along NE City Limits 20" along 195 and Fort Hood St. 12" South of Chaparral Road 12" along FM 439 12" along FM 439 12" Railroad To FM 439 12/16/20" East Stagecoach Road Airport PS Expans. & PP Mods 12/16" SW part of Lower PP WATER Description 12" by FM 2484 1.0 MG EST in Lower PP & PRV's 16" Vet. Mem. Blvd to Railroad 12/16" South Lower PP Loop 5.0 MG GST & 7.0 MGD PS Expan. 16" West of 195 in Upper PP WATER Description 12" Water Line in SE Lower PP 12" Water Line in NW Lower PP	\$14,910,239 Cost \$806,400 \$1,131,043 \$864,730 \$1,821,590 \$1,320,480 \$1,31,2620 \$1,372,213 \$4,468,840 \$618,240 \$1,672,339 \$15,988,495 Cost \$3,473,971 \$2,483,960 \$1,181,914 \$4,783,773 \$6,289,920 \$2,184,248 \$20,397,786 Cost \$3,401,691 \$441,423 \$0,215,115,115,115,115,115,115,115,115,115	2014 Cumulative Cost \$806,400 \$1,937,443 \$2,802,173 \$4,623,763 \$5,944,243 \$7,856,863 \$9,229,075 \$13,697,916 \$14,316,156 \$15,988,495 2015 Cumulative Cost \$3,473,971 \$5,957,931 \$7,139,845 \$11,923,618 \$11,923,618 \$11,923,618 \$12,037,786 2022 Cumulative Cost \$3,401,691 \$3,843,114	Project 20S 21S 22S 23S 24S TOTAL Project 25S 26S 27S 28S 29S TOTAL	Description New LS, 18"FM 12/15/18" GM New LS and 14" FM, 10/12" GM New LS, 12"FM & 12/15" GM 8" GM North of Railroad New LS 10" FM & 12" West of 195 SANI" Description Trimmier Creek 30" Gravity Main New LS, 10" FM, & 12" GM by 2484 New LS, 10" FM, & 12" GM by 2484 New LS, 8"FM, 8/10/12" near SH195 10/12" West of SH 195 Lift Station #1 Rehab. SANI" Description New LS, 8" FM, 12" Gravity Main New LS, 8" FM, 12" Gravity Main New LS, 8" FM, 10/12" Gravity Main	\$16,030,620 TARY SEWER \$6,114,966 \$3,223,214 \$3,346,372 \$418,666 \$2,873,257 \$15,976,475 TARY SEWER \$2,379,103 \$3,071,159 \$4,373,798 \$1,026,000 \$1,196,160 \$1,2,046,221 TARY SEWER \$2,705,276 \$3,397,675 \$2,705,276 \$3,397,675	Cumulative Cost \$6,114,966 \$9,338,180 \$12,684,552 \$13,103,218 \$15,976,475 \$12,046,221	\$30,940,859 Combined Cumulative \$6,921,366 \$11,275,623 \$15,486,725 \$17,726,981 \$21,920,718 \$23,833,338 \$25,205,550 \$29,674,391 \$30,292,631 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$31,964,970 \$32,2444,007 \$32,2447 \$32,2447 \$32,2467 \$32,24

Appendix A

Water Capital Improvement Plan Cost Estimate

TABLE A.1

WATER UNIT COSTS

2019

\$323

\$287

\$251

\$216

\$180

\$149

\$132

\$105

\$99

\$79

\$66 \$53

\$719

\$647

\$599

\$575

\$479

\$455

\$407

\$383

\$359

\$311

\$240

2022

\$343

\$305

\$267

\$229

\$191

\$158

\$140

\$112

\$105

\$84 \$70

\$56

\$763

\$687

\$636

\$610

\$509

\$483

\$432

\$407

\$381

\$331

\$254

 ${\rm Continuous}\;{\rm Compounding}{=}\; {Present}\; Value\; {}^{*}\; e^{rn}$

	Years (n)	3								ROUNDED TO) NEAREST I	OOLLAR
	Rate (r)	2.00%			Cost per Di	ameter-inch					Cost per L	inear Foot
SELECT ITEM		Diameter	2007	2010	2013	2016	2109	2022	2007	2010	2013	2016
54" WL & Appurtenances		54	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$254	\$270	\$287	\$305
48" WL & Appurtenances		48	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$226	\$240	\$255	\$271
42" WL & Appurtenances		42	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$198	\$210	\$223	\$237
36" WL & Appurtenances		36	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$170	\$180	\$191	\$203
30" WL & Appurtenances		30	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$141	\$150	\$159	\$169
24" WL & Appurtenances		24	\$4.89	\$5.19	\$5.51	\$5.85	\$6.22	\$6.60	\$117	\$125	\$132	\$141
20" WL & Appurtenances		20	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$104	\$110	\$117	\$124
16" WL & Appurtenances		16	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$83	\$88	\$93	\$99
15" WL & Appurtenances		15	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$78	\$83	\$88	\$93
12" WL & Appurtenances		12	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$62	\$66	\$70	\$74
10" WL & Appurtenances		10	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$52	\$55	\$58	\$62
8" WL & Appurtenances		8	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$41	\$44	\$47	\$50
60" Boring and Casing		60	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$565	\$600	\$637	\$677
54" Boring and Casing		54	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$509	\$540	\$574	\$609
50" Boring and Casing		50	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$471	\$500	\$531	\$564
48" Boring and Casing		48	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$452	\$480	\$510	\$541
40" Boring and Casing		40	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$377	\$400	\$425	\$451
36" Boring and Casing		38	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$358	\$380	\$404	\$429
34" Boring and Casing		34	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$320	\$340	\$361	\$383
32" Boring and Casing		32	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$301	\$320	\$340	\$361
30" Boring and Casing		30	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$283	\$300	\$319	\$338
26" Boring and Casing		26	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$245	\$260	\$276	\$293
20" Boring and Casing		20	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$188	\$200	\$212	\$226

${\rm Continuous}\; {\rm Compounding}{=}\; {\rm Present}\; {\rm Value}\; {*}\; {\rm e}^{{\rm rn}}$

ROUNDED TO NEAREST TEN THOUSAND DOLLARS Years (n) 3 Rate (r) 1.67% Lump Sum Cost 2007 2010 2013 2016 2109 2022 2013 2022 2007 2010 2016 2019 \$1,100,000 \$1,160,000 Pump Station - New 4 MGD \$1,000,000 \$1,050,000 \$1,220,000 \$1,280,000 Pump Station - New 7 MGD \$1,700,000 \$1,790,000 \$1,880,000 \$1,980,000 \$2,080,000 \$2,190,000 Pump Station - Expans 1 MGD \$360,000 \$325,000 \$340,000 \$380,000 \$400,000 \$420,000 Pump Station - Expans 7 MGD \$1,840,000 \$2,030,000 \$1,750,000 \$1,930,000 \$2,130,000 \$2,240,000 Pump Station - Expans 8 MGD \$2,500,000 \$2,630,000 \$2,770,000 \$2,910,000 \$3,060,000 \$3,220,000

1.5MG Ground Tank				\$900,000	\$950,000	\$1,000,000	\$1,050,000	\$1,100,000	\$1,160,000
2.0 MG Ground Tank				\$1,000,000	\$1,050,000	\$1,100,000	\$1,160,000	\$1,220,000	\$1,280,000
5.0 MG Ground Tank				\$2,090,000	\$2,200,000	\$2,310,000	\$2,430,000	\$2,550,000	\$2,680,000
1.0 MG Elevated Tank				\$1,500,000	\$1,580,000	\$1,660,000	\$1,750,000	\$1,840,000	\$1,930,000
1.5 MG Elevated Tank				\$1,750,000	\$1,840,000	\$1,930,000	\$2,030,000	\$2,130,000	\$2,240,000
Pressure Reducing Valve				\$13,000	\$14,000	\$15,000	\$16,000	\$17,000	\$18,000
System Improvements - Upper & Lower PP							\$600,000		
System Improvements - Airport PP							\$100,000		
42" Water Supply Allowance with Bell WSC					\$0				
ROW for Facility (per Acre)				\$11,000	\$12,000	\$13,000	\$14,000	\$15,000	\$16,000
Pavement Repair				\$35	\$35	\$35	\$35	\$35	\$35

		Table A.2 City of Killeen	2007 2000			
	Wat	er System Improvements Year Opinions Of Probable Projec	t Cost			
Project Number	Project Description	Construction Items	Quantity	Units	Unit Price	Costs
1W	12/16/20" along Reese Creek Rd. 20" WL along Stagecoach Rd from SH 201 to W. Trimmier Rd; 16" water line along Reese Creek Rd from Bunny Trail to Highway 195 and 12" WL runs southwest along Highway 195 to existing 12" WL.	12" WL & Appurtenances 16" WL & Appurtenances 20" WL & Appurtenances 30" Boring and Casing Pavement Repair Engin	7,280 11,180 6,420 400 600	LF LF LF LF LF Total Co eying & C To	\$62 \$83 \$104 \$283 \$35 Subtotal gency @ 20% nstruction Cost Geotech @ 12% tal Project Cost	\$451,360 \$927,940 \$667,680 \$113,200 \$21,000 \$2,181,180 \$436,236 \$2,617,416 \$314,090 \$2,931,506
2W	1.5 MG Bundrant EST Expansion Replace Existing 0.25 MG tank with 1.5 MG elevated storage tank.	1.5 MG Elevated Tank Engin	1 eering, Surve	LS Contin Total Co eying & C To	\$1,750,000 Subtotal gency @ 20% nstruction Cost Geotech @ 12% tal Project Cost	\$1,750,000 \$1,750,000 \$350,000 \$2,100,000 \$252,000 \$2,352,000
3W	12/16'' Southeast Loop 16" WL running east from intersection of Featherline Rd and Chaparral Rd to E. Trimmier Rd and north of the intersection about 3000 feet; 12" WL running north along E. Trimmier Rd to existing 12" WL; 12" WL running east about 8000 feet.	12" WL & Appurtenances 16" WL & Appurtenances 20" Boring and Casing Pavement Repair Engin	11,990 12,150 200 200 eering, Surve	LF LF LF LF Contin Total Co eying & C To	\$62 \$83 \$188 \$35 Subtotal agency @ 20% nstruction Cost Geotech @ 12% tal Project Cost	\$743,380 \$1,008,450 \$37,600 \$1,796,430 \$359,286 \$2,155,716 \$258,686 \$2,414,402
4W	Pump Station 3 Upgrade Pump Station 3 expansion from 10 MGD to 18 MGD.	Pump Station - Expans 8 MGI	D 1	LS Contin Total Co cying & C To	\$2,500,000 Subtotal gency @ 20% nstruction Cost Geotech @ 12% tal Project Cost	\$2,500,000 \$2,500,000 \$3,000,000 \$360,000 \$3,360,000
C N	CITY OF KILLEEN WATER SYSTEM COSTS 2007					\$11,057,908

		Table A.3 City of Killeen				
	Wate	er System Improvements Yea	r 2010-2012			
Project		Opinions Of Probable Project	et Cost		Unit	
Number	Project Description	Construction Items	Quantity	Units	Price	Costs
5W	12/16" along N. Young Drive	12" WL & Appurtenances	1,850	LF	\$66	\$122,100
	12" WL along N. Young Dr from	16" WL & Appurtenances	5,500	LF	\$88	\$484,000
	Duncan Ave to Poage Ave, 16" WL	Pavement Repair	1,000	LF	\$35 Subtotal	\$35,000
	along Poage Ave to Tucker Dr and			Conting	gency @ 20%	\$128.220
	along Tucker Dr to Lake Rd; 16" WL			Total Cor	nstruction Cost	\$769,320
	along Lake Rd from Tucker Dr to N.	Engir	neering, Surve	eying & G	eotech @ 12%	\$92,318
	38th St, along N. 38th St to Muir Dr			Tot	al Project Cost	\$861,638
6W	12/16" Opion Bood Water Line	12" WI & Appurtenances	6 390	IF	\$66	\$421 740
0 **	12" WL running south from the	16" WL & Appurtenances	10,180	LF	\$88	\$895,840
	intersection of Onion Rd and Rio				Subtotal	\$1,317,580
	Grande Ct to Stagecoach Rd; 16" WL			Conting	gency @ 20%	\$263,516
	running east along Stagecoach Rd from	E	: G	Total Cor	istruction Cost	\$1,581,096
	Featherline Rd to Cunningham Rd and	Engir	ieering, Surve	eying & G	al Project Cost	\$189,732
	south from Stagecoach Rd and			100	ai i lojeet cost	φ1,770,020
	Featherline to proposed 16" WL.					
7W	12/24" Trimmier Road Water Line	12" WL & Appurtenances	15,220	LF	\$66	\$1,004,520
	12" WL along Stagecoach Rd from	24" WL & Appurtenances	4,400	LF	\$125 \$25	\$550,000
	WS Young Dr. to W. Trimmier Rd and	Pavement Repair	400	LF	\$35 Subtotal	\$14,000
	along W. Trimmier to Atlas Ave; 24"			Contine	3u0101a1	\$313 704
	WL along W. Trimmier Rd from			Total Cor	struction Cost	\$1.882.224
	Stagecoach Rd to S. Kelley Ln and 12"	Engir	eotech @ 12%	\$225,867		
	WL running west from S. Kelley Ln to			Tot	al Project Cost	\$2,108,091
	11wy 195.		- -		* * * *	#0 00 7 00
8W	24/30" along Chaparral Road	24" WL & Appurtenances	6,580	LF	\$125	\$822,500
	24" WL along Trimmier Rd from	30" WL & Appurtenances	5,110		\$150	\$766,500 \$152,000
	chaparral to S. Kelley Ln; 30" WL	50 Bornig and Casing	400	LI	Subtotal	\$152,000
	to Easthorling Rd			Conting	gency @ 20%	\$348.200
	to realiferine Ru.			Total Cor	nstruction Cost	\$2,089,200
		Engir	neering, Surve	eying & G	eotech @ 12%	\$250,704
				Tot	al Project Cost	\$2,339,904
9W	5 MG GST, 7 MGD PS, 30" Line	30" WL & Appurtenances	10.800	LF	\$150	\$1.620.000
	7 MGD Pump Station and 5 MG	Pump Station - New 7 MGD	1	LS	\$1,790,000	\$1,790,000
	Ground Storage Tank; 30" WL along	5.0 MG Ground Tank	1	LS	\$2,200,000	\$2,200,000
	Chaparral Rd from Featherline Rd to	Pavement Repair	200	LF	\$35	\$7,000
	Bell Pump Station, serving the Lower	WL Supply Allowance	0	LS	\$0	\$0
	Pressure Plane (at E. Trimmier Rd);			Contin	Subtotal	\$5,617,000
	Allowance for 42" Bell Co. South			Total Cor	struction Cost	\$1,125,400
	Water Supply Line.	Engir	neering. Surve	eving & G	eotech @ 12%	\$808.848
		6	8,	Facility R	OW (5 Acres)	\$55,000
				Tot	al Project Cost	\$7,604,248
10W						
10W	20 Line along Unaparral Kd Runs from 195 east to Trimmier along	20" WL & Appurtenances	7 100	LF	\$110	\$781.000
	Chaparral Road	30" Boring and Casing	250	LS	\$300	\$75.000
	Chapartai Roud.				Subtotal	\$856,000
				Conting	gency @ 20%	\$171,200
				Total Cor	nstruction Cost	\$1,027,200
		Engir	neering, Surve	eying & G	eotech @ 12%	\$123,264
				Tot	ai Project Cost	\$1,150,464
	CITY OF KILLEEN					
	WATER SYSTEM COSTS 2010					\$15,835,173

		Table A.4								
	Wa	City of Killeen ater System Improvements Year	r 2013-2015							
		Opinions Of Probable Project	et Cost							
Project Number	Project Description	Construction Items	Quantity	Units	Unit Price	Costs				
11000			Quantity	ento						
11W	4 MGD PS 16" along FM 439	Pump Station - New 4 MGD	1		\$1,100,000	\$1,100,000				
	4 MGD pump station and a 2.0 MG	2.0 MG Ground Tank 16" WI & Appurtenances	13 000		\$1,100,000 \$93	\$1,100,000 \$1,209,000				
	Boad 16" WL running south and then	30" Boring and Casing	15,000	LF	\$319	\$47.850				
	west from the pump station.	6			Subtotal	\$3,456,850				
	west from the pump station.			Contin	igency @ 20%	\$691,370				
		Ensin	aanina Cumu	Total Co	Instruction Cost	\$4,148,220				
		Engin	eering, Surve	eying & C	tal Project Cost	\$497,780 \$4,646,006				
				10	tur i roject cost	\$4,040,000				
12W	12" Airport/Upper PP	12" WI & Appurtenances	14 391	IF	\$70	\$1 007 377				
12.00	12" WL along Reese Creek Rd from	Pavement Repair	400	LF	\$35	\$14,000				
	S. Hwy 201 east for about 4000 feet;	20" Boring and Casing	200	LF	\$212	\$42,400				
	12" WL running north from Reese				Subtotal	\$1,063,777				
	Creek Rd to Stan Schlueter Loop and			Contin	igency @ 20%	\$212,755				
	connects to existing 8" WL at Golden	Engin	ooring Surv	Total Co	Soctoch @ 12%	\$1,276,532				
	Gate Dr	Engin	cornig, Surv	Tor	tal Project Cost	\$1.429.716				
					j	+ - , · - , , · - •				
13W	12/20'' & 1.5 GST W of Chap. Rd	20" WL & Appurtenances	6,028	LF	\$117	\$705,311				
	20" WL west from S. Hwy 195 then	12" WL & Appurtenances	6,800	LF	\$70	\$476,000				
	south to proposed 1.5 MG GST. 12"	20" Boring and Casing	150	LF	\$212	\$31,800				
	WL running along S. Hwy 195 from	Pavement Repair	150	LF	\$35	\$5,250				
	Chaparral Rd.	1.5MG Ground Tank	1	LS	\$1,000,000 Subtotal	\$2,218,361				
				Contin	igency @ 20%	\$443,672				
				Total Co	nstruction Cost	\$2,662,033				
		Engin	eering, Surve	eying & C	Jeotech @ 12%	\$319,444				
				10	tai i lojeet Cost	\$2,901,477				
14W	16" Water Line along 38th Street	16" WL & Appurtenances	8,630	LF	\$88	\$759,440				
	16" WL from Pump Station 3 along	30" Boring and Casing	1,000	LF	\$300	\$300,000				
	Water St to N. 38th St and runs north	Pavement Repair	1,000	LF	\$35 Subtotal	\$35,000				
	along N. 38th St to Lake Rd.			Contin	igency @ 20%	\$1,094,440				
				Total Co	nstruction Cost	\$1,313,328				
		Engin	eering, Surve	eying & C	Geotech @ 12%	\$157,599				
				To	tal Project Cost	\$1,470,927				
15W	16/20/24"& 7.0 MCD PS I ower PD	16" WL & Annurtenances	7.500	LF	\$93	\$697 500				
10 11	7 MGD PS with 24" WL running	24" WL & Appurtenances	1,750	LF	\$132	\$231,000				
	south to proposed 16" WL. 24" WL	20" WL & Appurtenances	3,500	LF	\$117	\$409,500				
	east approximately 1,500'. 20" WL	40" Boring and Casing	100		\$425 \$1,880,000	\$42,500 \$1,880,000				
	north along E. Trimmier to proposed	Tump Station - New / MOD	1	LS	\$1,880,000 Subtotal	\$3,260,500				
	12" WL. 16" WL east along			Contin	igency @ 20%	\$652,100				
	Chaparral to existing 16"WL.	E	ooring Com	Total Co	nstruction Cost	\$3,912,600				
		Engin	cering, Surve	Jynng & C Tor	tal Project Cost	\$4,382,112				
					~	·				
CITY OF KILLEEN										
	WATER SYSTEM COSTS 2013					\$14,910,239				

	Wa	Table A.5 City of Killeen ter System Improvements Y	ear 2016-2018			
		Opinions Of Probable Pro	ject Cost			
Project					Unit	
Number	Project Description	Construction Items	Quantity	Units	Price	Costs
16W	Pressure Plane Modifications	12" WL & Appurtenances	1	EA	\$600,000	\$600,000
	Upper and Lower Pressure Plane			Contine	Subtotal	\$600,000
	System Improvements.			Total Cor	sency @ 20%	\$120,000
		En	gineering, Surv	eving & G	eotech @ 12%	\$86,400
			.g	Tota	al Project Cost	\$806,400
17W	12/16" at Chaparral & Bell PS	12" WL & Appurtenances	4,250	LF	\$70	\$297,500
	16" WL west from proposed Bell PS	16" WL & Appurtenances	5,850	LF	\$93	\$544,050
	along Chaparral Rd then a 12" WL				Subtotal	\$841,550
	north along Chaparral Rd to proposed			Conting Total Car	gency @ 20%	\$168,310
	16" WL.	En	gineering Surv	eving & G	eotech @ 12%	\$1,009,800
			gineering, bui v	Tota	al Project Cost	\$1,131,043
					5	
18W	12" along NE City Limits	12" WL & Appurtenances	7,980	LF	\$70	\$558,600
	12" WL runs along Schwald Rd from	20 ^a Boring and Casing	400	LF	\$212 Subtotal	\$84,800
	Polk St about 3,000' east and			Conting	ency @ 20%	\$128 680
	continues south to E. Rancier Rd.		struction Cost	\$772,080		
		En	eotech @ 12%	\$92,650		
				Tota	al Project Cost	\$864,730
19W	20" along 105 and Fort Hood St	20" WL & Appurtenances	10.350	LF	\$117	\$1,210,950
17 11	20" WL north from intersection of	34" Boring and Casing	400	LF	\$361	\$144,400
	Stagecoach Rd and S. Hwy 195 to	6 6			Subtotal	\$1,355,350
	existing 20" WL on Stan Schlueter			Conting	gency @ 20%	\$271,070
	Rd.	E	struction Cost	\$1,626,420		
		En	gineering, Surv	eying & G	al Project Cost	\$195,170
				104	ai i loject Cost	\$1,821,390
20W	12" South of Chaparral Road	12" WL & Appurtenances	13,430	LF	\$70	\$940,100
	12" WL from the intersection of	20" Boring and Casing	200	LF	\$212	\$42,400
	Chaparral Rd and Trimmier Rd to S.			Contine	Subtotal	\$982,500 \$196,500
	Hwy 195 north of FM 2484.			Total Cor	struction Cost	\$1,179,000
		En	gineering, Surv	eying & G	eotech @ 12%	\$141,480
				Tota	al Project Cost	\$1,320,480
21W	1011 - L FNA 420	12" WIL & Appurton appage	10 724	IE	\$70	\$1 380 680
21 W	12" along FM 439	20" Boring and Casing	200	LF	\$212	\$1,380,080
	hack to proposed 12" WI 12" WI	20 Boring and Cusing	200	LI	Subtotal	\$1,423,080
	running east to Bell PS			Conting	gency @ 20%	\$284,616
	running cast to ben 15.	_		Total Con	struction Cost	\$1,707,696
		En	gineering, Surv	eying & G	eotech @ 12%	\$204,924
				Tota	a Project Cost	\$1,912,620
22W	12" Railroad To FM 439	12" WL & Appurtenances	12,768	LF	\$70	\$893,792
	12" WL running about 5,000' east	20" Boring and Casing	600	LF	\$212	\$127,200
	along Atchison Topeka & Santa Fe			C i	Subtotal	\$1,020,992
	Railroad from N. Roy Reynolds Dr,			Conting Total Cor	gency @ 20%	\$204,198
	continues north to E. Rancier Ave.	En	gineering Surv	Total Construction Cost urveying & Geotech @ 12%		\$147.023
			6	Tota	\$1,372,213	
					2	

		Table A.5 City of Killeen				
	Wa	ter System Improvements Year 2 Opinions Of Probable Project (016-2018 Cost			
Project <u>Number</u> 23W	Project Description 12/16/20'' East Stagecoach Road 20'' WL south from E. Trimmier Rd & Chaparral Rd. 16'' WL west approximately 12,500' then north about 5000' and 12'' WL west about 3500' with 16'' WL running east connecting to proposed 16''.	Construction Items 16" WL & Appurtenances 20" WL & Appurtenances 12" WL & Appurtenances 30" Boring and Casing Enginee	Quantity 24,830 5,420 3,630 400 ering, Surve	Units LF LF LF LF Contin Total Con eying & C Tot	Unit Price \$93 \$117 \$70 \$319 Subtotal gency @ 20% nstruction Cost Geotech @ 12% cal Project Cost	Costs \$2,309,190 \$634,140 \$254,100 \$127,600 \$3,325,030 \$665,006 \$3,990,036 \$478,804 \$4,468,840
24W	Airport PS Expans. & PP Mods Airport and Upper Pressure Plane Svstem Improvements.	Pump Station - Expans 1 MGD System Improvements Enginee	1 1 ering, Surve	LS EA Contin Total Con eying & C Tot	\$360,000 \$100,000 Subtotal gency @ 20% nstruction Cost Geotech @ 12% al Project Cost	\$360,000 \$100,000 \$460,000 \$92,000 \$552,000 \$66,240 \$618,240
25W	12/16" WL south from existing 16" WL at Chaparral Road, then west	12" WL & Appurtenances 16" WL & Appurtenances 20" Boring and Casing Engined	14,800 1,100 500	LF LF LF Contin Total Con eying & C Tot	\$70 \$93 \$212 Subtotal gency @ 20% nstruction Cost Geotech @ 12% al Project Cost	\$1,036,000 \$102,300 \$1,244,300 \$248,860 \$1,493,160 \$179,179 \$1,672,339
	CITY OF KILLEEN WATER SYSTEM COSTS 2016					\$15,988,495

	W	Table A.6 City of Killeen	Voor 2010 2022	,		
	W	Opinions Of Probable Pr	oject Cost	2		
Project					Unit	
Number	Project Description	Construction Items	Quantity	Units	Price	Costs
26W	12" by FM 2484 12" WL running about 5000' southwest along State Hwy 195 from the intersection with FM 440: 12"	12" WL & Appurtenances 20" Boring and Casing	31,200 500	LF LF Contin	\$79 \$240 Subtotal gency @ 20%	\$2,464,800 \$120,000 \$2,584,800 \$516,960
	water line runs east from the intersection at FM 440 about 3000' then south about 5000' then east across FM 2484 then north	Enį	nstruction Cost Geotech @ 12% tal Project Cost	\$3,101,760 \$372,211 \$3,473,971		
27W	1.0 MG EST in Lower PP & PRV's 1.0 MG EST in the Southwest area of the Lower Pressure Plane.	1.0 MG Elevated Tank Eng	1 gineering, Surve	EA Contin Total Co eying & C Facility To	\$1,840,000 Subtotal gency @ 20% nstruction Cost Geotech @ 12% ROW (1 Acre) tal Project Cost	\$1,840,000 \$1,840,000 \$368,000 \$2,208,000 \$264,960 \$11,000 \$2,483,960
28W	16'' Vet. Mem. Blvd to Railroad 16" WL along E. Veterans Memorial Blvd from east of Rio Blvd to N. Roy Reynolds Dr and north along N. Roy Reynolds Dr to the Railroad.	16" WL & Appurtenances 30" Boring and Casing Pavement Repair Eng	7,600 100 1,300 gineering, Surve	LF LF LF Contin Total Co eying & C To	\$105 \$359 \$35 Subtotal gency @ 20% nstruction Cost Geotech @ 12% tal Project Cost	\$798,000 \$35,900 \$45,500 \$879,400 \$175,880 \$1,055,280 \$126,634 \$1,181,914
29W	12/16'' South Lower PP Loop 16" WL connects into proposed 16" WL south of Rock Creek stream and runs south; 12" WL continues south then east past the Onion Creek stream; 16" WL continues north from the 12" WL.; install PRVs to connect southern Lower Plane Loop	12" WL & Appurtenances 16" WL & Appurtenances Pressure Reducing Valve 20" Boring and Casing Eng	21,400 16,331 2 500 gineering, Surve	LF LF EA LF Contin Total Co eying & C To	\$79 \$105 \$17,000 \$240 Subtotal gency @ 20% nstruction Cost Geotech @ 12% tal Project Cost	\$1,690,600 \$1,714,755 \$34,000 \$120,000 \$3,559,355 \$711,871 \$4,271,226 \$512,547 \$4,783,773
30W	5.0 MG GST & 7.0 MGD PS New 5 MG Ground Storage Tank and 7.0 MGD Upper Pressure Plane Pump Station Expansion	5.0 MG Ground Tank Pump Station - Expans 7 M Eng	GD 1 gineering, Surve	LS LS Contin Total Co eying & C To	\$2,550,000 \$2,130,000 Subtotal gency @ 20% nstruction Cost Geotech @ 12% tal Project Cost	\$2,550,000 \$2,130,000 \$4,680,000 \$936,000 \$5,616,000 \$673,920 \$6,289,920
31W	16" West of 195 in Upper PP 16" WL loop to connect proposed 12" and 20" WL in the far southwest corner of the City.	16" WL & Appurtenances 30" Boring and Casing Eng	12,059 1,000 gineering, Surve	LF LF Contin Total Co eying & C To	\$105 \$359 Subtotal gency @ 20% nstruction Cost Geotech @ 12% tal Project Cost	\$1,266,185 \$359,000 \$1,625,185 \$325,037 \$1,950,221 \$234,027 \$2,184,248
	CITY OF KILLEEN WATER SYSTEM COSTS 2019					\$20,397,786

Table A.7 City of Killeen Water System Improvements Year 2022-2024 Opinions Of Probable Project Cost											
Project <u>Number</u>	Project Description	Construction Items	Quantity	Units	Unit Price	Costs					
32W	12'' Water Line in SE Lower PP 12" WL loop in the south east corner of the lower pressure plane connecting the proposed 12" WL in 2019 and proposed 12" WL in 2016 with a pressure reducing valve at the north east corner connecting to the proposed 12" WL in 2016.	12" WL & Appurtenances 20" Boring and Casing Pressure Reducing Valve Engi	28,405 500 1 neering, Surve	LF LF EA Conting Total Cor eying & G Tot	\$84 \$254 \$18,000 Subtotal gency @ 20% nstruction Cost ieotech @ 12% al Project Cost	\$2,386,020 \$127,000 \$18,000 \$2,531,020 \$506,204 \$3,037,224 \$364,467 \$3,401,691					
33W	12" Water Line in NW Lower PP 12" WL looping in the northwest corner of the lower pressure plane connecting the 2 MG storage tank to the proposed 16" WL along FM 439.	12" WL & Appurtenances Engi	3,910 neering, Surve	LF Conting Total Con eying & G Tot	\$84 Subtotal gency @ 20% istruction Cost deotech @ 12% al Project Cost	\$328,440 \$328,440 \$65,688 \$394,128 \$47,295 \$441,423					
	CITY OF KILLEEN WATER SYSTEM COSTS 2022					\$3,843,114					

Appendix B

Wastewater Capital Improvement Plan Cost Estimate

TABLE B.1

WASTEWATER UNIT COSTS

		D		'n										
Continuous C	ompounding=	Present	Value ^ e											
	Years (n)	3			~ ~					ROUNDED TO) NEAREST I	JOLLAR		
	Rate (r)	2.00%			Cost per Di	ameter-inch				1	Cost per L	inear Foot		
SELECT ITEM		Diameter	2007	2010	2013	2016	2109	2022	2007	2010	2013	2016	2019	2022
548.0 to 0			* 4 = 1	\$5.00	\$5.01	07.54	\$7.00	\$5.25	* 254	#25 0	#207	\$205	* 222	\$2.42
54" Sanitary Sewer		54	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$254	\$270	\$287	\$305	\$323	\$343
48" Sanitary Sewer		48	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$226	\$240	\$255	\$271	\$287	\$305
42" Sanitary Sewer		42	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$198	\$210	\$223	\$237	\$251	\$267
36" Sanitary Sewer		36	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$170	\$180	\$191	\$203	\$216	\$229
33" Sanitary Sewer		33	\$4.71	\$5.00	\$5.31	\$5.64	\$5.99	\$6.36	\$155	\$165	\$175	\$186	\$198	\$210
30" Sanitary Sewer		30	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$155	\$165	\$175	\$186	\$198	\$210
27" Sanitary Sewer		27	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$140	\$149	\$158	\$167	\$178	\$189
24" Sanitary Sewer		24	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$124	\$132	\$140	\$149	\$158	\$168
21" Sanitary Sewer		21	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$109	\$116	\$123	\$130	\$138	\$147
18" Sanitary Sewer		18	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$93	\$99	\$105	\$112	\$119	\$126
15" Sanitary Sewer		15	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$78	\$83	\$88	\$93	\$99	\$105
12" Sanitary Sewer		12	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$62	\$66	\$70	\$74	\$79	\$84
10" Sanitary Sewer		10	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$52	\$55	\$58	\$62	\$66	\$70
8" Sanitary Sewer		8	\$5.18	\$5.50	\$5.84	\$6.20	\$6.59	\$6.99	\$41	\$44	\$47	\$50	\$53	\$56
60" Doring and Cooing		60	¢0.42	\$10.00	\$10.62	¢11.00	¢11.09	¢10.70	\$565	\$600	\$627	\$ <i>677</i>	\$710	\$762
54" Devine and Casing		60 54	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$565	\$600	\$037	\$677	\$/19	\$703
54 Boring and Casing		54	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$509	\$540	\$574	\$609	\$647	\$087
50 Boring and Casing		50	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$471	\$500	\$551	\$564	\$399	\$030
48 Boring and Casing		48	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$432	\$480	\$310	\$341	\$373	\$010
40 [°] Boring and Casing		40	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$377	\$400	\$425	\$451	\$479	\$309
36 Boring and Casing		38	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$358	\$380	\$404	\$429	\$455	\$483
34 Boring and Casing		34	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$320	\$340	\$301	\$383	\$407	\$432
32 Boring and Casing		32	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$301	\$320	\$340	\$301	\$383 \$250	\$407
30" Boring and Casing		30	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$283	\$300	\$319	\$338 \$202	\$339	\$381
26 Boring and Casing		20	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$245	\$260	\$276	\$293	\$311	\$331
20 Boring and Casing		20	\$9.42	\$10.00	\$10.62	\$11.28	\$11.98	\$12.72	\$188	\$200	\$212	\$226	\$240	\$254
20" Dance Main		20	¢£ 10	\$5.50	\$5.04	\$6.20	\$6.50	\$6.00	¢155	¢165	¢175	¢196	¢100	\$210
30 Force Main		20	\$5.18	\$5.50	\$3.84 \$5.84	\$6.20	\$6.59	\$0.99 \$6.00	\$133	\$105	\$1/3	\$180	\$198	\$210
26 Force Main		20	\$J.10 \$5.19	\$5.50	\$3.04 \$5.94	\$6.20	\$6.59	\$6.00	\$145	\$1.34	\$104	\$174	\$104 \$171	\$190
26 Force Main		20	\$5.18	\$5.50	\$3.84 \$5.94	\$6.20	\$0.39	\$0.99 \$6.00	\$133	\$143	\$132	\$101	\$1/1	\$162
24 Force Main		24	\$5.18	\$5.50	\$3.84 \$5.94	\$6.20	\$0.39	\$0.99 \$6.00	\$124	\$132	\$140	\$149	\$138	\$108
22 Force Main		22	\$5.18	\$5.50	\$3.84 \$5.94	\$6.20	\$0.39	\$0.99 \$6.00	\$114	\$121	\$128	\$130	\$145	\$134
20 Force Main		20	\$5.18	\$5.50	\$3.84 \$5.94	\$6.20	\$0.39	\$0.99 \$6.00	\$104	\$110	\$117	\$124	\$152	\$140
18 Force Main		16	\$5.18	\$5.50	\$3.84 \$5.94	\$6.20	\$0.39	\$0.99 \$6.00	\$93	\$99	\$105	\$112	\$119	\$120
16 Force Main		10	\$5.18	\$5.50	\$3.84 \$5.94	\$6.20	\$0.39	\$0.99 \$6.00	\$83 \$72	\$86 \$77	\$95	\$99	\$105	\$112 ¢09
14 Force Main		14	\$J.10 \$5.19	\$5.50	\$3.04 \$5.94	\$6.20	\$6.59	\$6.00	\$73	\$77 \$66	\$02 \$70	\$07 \$74	\$92	\$90 \$94
12 Force Main		12	\$5.18	\$5.50	\$3.84 \$5.94	\$6.20	\$0.39	\$0.99 \$6.00	\$62	\$00 \$55	\$70	\$74	\$/9	\$84 \$70
10 Force Main		10	\$5.18	\$5.50	\$3.84 \$5.94	\$6.20	\$0.39	\$0.99 \$6.00	\$32	\$33	\$38 \$47	\$62	\$00	\$70
6" Force Main		6	\$5.18	\$5.50	\$3.84 \$5.84	\$6.20	\$6.59	\$6.99 \$6.00	\$41	\$33	\$47 \$35	\$30	\$35	\$30
		0	\$3.10	\$3.30	\$J.04	\$0.20	\$0.39	\$0.99	\$51	\$35	\$33	\$37	\$40	\$42
48" Diameter Manhole									\$3 500	\$3 500	\$3 500	\$3 700 00	\$3 700	\$3 700
60" Diameter Manhole				+					\$5,000	\$5,000	\$5,000	\$5,700.00	\$5 300	\$5,700
72" Diameter Manhole				+					\$6 500	\$6 500	\$6 500	\$6,900.00	\$6,900	\$6,900
T-Block				+					\$6 500	\$6 500	\$6 500	\$6,900.00	\$6,900	\$6,900
1 DIOCK				1	1	I			φ0,500	ψ0,500	φ0,500	φ0,700.00	ψ0,700	φ0,700

Years (n)	3								ROUNDED IC	J NEAREST I	EN THOUSA	IND DOLLAR	6
Rate (r)	1.67%									Lump Su	ım Cost		
		2007	2010	2013	2016	2109	2022	2007	2010	2013	2016	2019	2022
Lift Station - New 1 MGD								\$550,000	\$580,000	\$610,000	\$640,000	\$670,000	\$700,000
Lift Station - New 1.5 MGD								\$600,000	\$630,000	\$660,000	\$690,000	\$730,000	\$770,000
Lift Station - New 2 MGD								\$700,000	\$740,000	\$780,000	\$820,000	\$860,000	\$900,000
Lift Station - New 2.5 MGD								\$750,000	\$790,000	\$830,000	\$870,000	\$910,000	\$960,000
Lift Station - New 4 MGD								\$800,000	\$840,000	\$880,000	\$930,000	\$980,000	\$1,030,000
Lift Station - New 5 MGD								\$1,100,000	\$1,160,000	\$1,220,000	\$1,280,000	\$1,350,000	\$1,420,000
Lift Station - New 7 MGD								\$2,000,000	\$2,100,000	\$2,210,000	\$2,320,000	\$2,440,000	\$2,570,000
Lift Station - Mod pipes, elec, site								\$150,000	\$160,000	\$170,000	\$180,000	\$190,000	\$200,000
Lift Station - Expans 1 MGD								\$325,000	\$340,000	\$360,000	\$380,000	\$400,000	\$420,000
Lift Station - Expans 2 MGD								\$400,000	\$420,000	\$440,000	\$460,000	\$480,000	\$500,000
Lift Station - Expans 7 MGD								\$1,750,000	\$1,840,000	\$1,930,000	\$2,030,000	\$2,130,000	\$2,240,000
Lift Station - Expans 8 MGD								\$2,500,000	\$2,630,000	\$2,770,000	\$2,910,000	\$3,060,000	\$3,220,000
Lift Station - Rehab #7									\$325,000				
Lift Station - Rehab #1												\$700,000	
ROW for Facility (per Acre)								\$11,000	\$12,000	\$13,000	\$14,000	\$15,000	\$16,000
Change FM to GM								\$150,000	\$160,000	\$170,000	\$180,000	\$190,000	\$200,000
Pavement Renair								\$35	\$35	\$35	\$35	\$35	\$35

Pavement Repair					\$35	\$35	\$35	\$35	\$35	\$35
Sewer System I/I Rehab						\$2,000,000				
CMOM & SSO Program Development						\$500,000				

		Table B.2				
	Wast	ewater System Improve	ements - 2007-2009			
		Opinions Of Probable	Project Cost			
Project Number	Project Description	Construction Iten	ns Quantity	Units	Unit Price	Costs
15	Lift Station #8 Lift Station # 8 located off the Atchison Topeka & Santa Fe Railroad in the Long	Lift Station - New 4 M	GD I	Contin	Subtotal gency @ 20%	\$800,000 \$800,000 \$160,000
	Branch Sub-Basin near North Rov		T Engineering, Survey	fotal Con /ing & G Facility I	eotech @ 12% ROW (1 Acre)	\$960,000 \$115,200 \$11,000
				Tota	al Project Cost	\$1,086,200
25	Trimmier Creek 21/27/36'' Gravity A 21" gravity main flows eastward from Featherline Rd. into a 27" interceptor until East Trimmier Rd. where it becomes a 36" interceptor which flows into the existing 30" major	21" Sanitary Sewer27" Sanitary Sewer36" Sanitary Sewer60" Diameter Manhole72" Diameter Manhole	7,418 3,956 3,213 19 18	LF LF LF EA EA	\$109 \$140 \$170 \$5,000 \$6,500 Subtotal gency @ 20%	\$808,508 \$553,840 \$546,227 \$95,000 \$117,000 \$2,120,575 \$424,115
			T Engineering, Survey	fotal Con /ing & G Tota	astruction Cost eotech @ 12% al Project Cost	\$2,544,689 \$305,363 \$2,850,052
3S	Trimmier Creek 21'' Gravity Main 21" gravity main flows east from the south end of Featherline Rd. into a 27" interceptor.	21" Sanitary Sewer 60" Diameter Manhole	6,488 16 7	LF EA Conting Fotal Con	\$109 \$5,000 Subtotal gency @ 20% istruction Cost	\$707,225 \$80,000 \$787,225 \$157,445 \$944,670
			Engineering, Survey	ing & G/ Tota	eotech @ 12% al Project Cost	\$132,254 \$1,076,923
4S	LS 20 and 14" FM & SH 195 12/18" 12" gravity main conveys flow south from decommissioned LS #11A to new LS #20; 18" gravity main flows south from Reese Creek Rd. to the new LS. LS #20 lifts flow through a 14" force main along Stagecoach to W Trimmier Rd.	Lift Station - New 5 Me 12" Sanitary Sewer 18" Sanitary Sewer 48" Diameter Manhole 60" Diameter Manhole 14" Force Main T-Block	GD 1 6,820 1,304 17 3 9,315 1	LS LF EA EA LF EA	\$1,100,000 \$62 \$93 \$3,500 \$5,000 \$73 \$6,500 Subtotal	\$1,100,000 \$422,809 \$121,281 \$59,500 \$15,000 \$679,995 \$6,500 \$2,405,085
			T Engineering, Survey F	Conting Fotal Con ving & G Facility R Tota	gency @ 20% astruction Cost eotech @ 12% OW (2 Acres) al Project Cost	\$481,017 \$2,886,102 \$346,332 \$22,000 \$3,254,435
58	LS #22, 6" FM, 12" 12" collection main flows south to new LS #22 off of Reese Creek Rd. which lifts flow through a 6" force main along Reese Creek Rd. to an 18" collection main	Lift Station - New 2 Me 6" Force Main 12" Sanitary Sewer 48" Diameter Manhole T-Block	GD 1 3,498 5,728 14 1 T Engineering, Survey	LS LF EA EA Contin, Total Con ving & G Facility I Tota	\$700,000 \$31 \$62 \$3,500 \$6,500 Subtotal gency @ 20% istruction Cost eotech @ 12% ROW (1 Acre) al Project Cost	\$700,000 \$108,447 \$355,145 \$49,000 \$6,500 \$1,219,093 \$243,819 \$1,462,911 \$175,549 \$11,000 \$1,649,460
C 1	CITY OF KILLEEN WASTEWATER SYSTEM COSTS 2007					\$9,917,071

	Waste	Table B.3 City of Kille ewater System Improve Opinions Of Probable	en ements - 2 Project (2010-2012			
		Opinions Of 1 Tobable	Toject				
Project						Unit	
Number	Project Description	Construction Iter	ns	Quantity	Units	Price	Costs
6S	Stagecoach 18" GM & 14" FM, 8/10"	8" Sanitary Sewer		3,565	LF	\$44	\$156,860
	An 8/10" GM conveys flows north and	10" Sanitary Sewer		2,519	LF	\$55	\$138,518
	west across W Trimmier Rd; 14" FM	18" Sanitary Sewer		6,199	LF	\$99	\$613,652
	extended along Stagecoach Rd. to an 18"	14" Force Main		4,301	LF	\$77	\$331,177
	interceptor continuing along Stagecoach	Change FM to GM		1 15		\$160,000	\$160,000
	Rd. then south along Featherline Rd. to	48" Diameter Manhole	;	15	EA EA	\$3,500 \$5,000	\$52,500 \$75,000
	21" GM.; existing 10" FM is converted	00 Diameter Mannole	,	15	LA	\$5,000 Subtotal	\$1,527,706
	to gravity flow along Kelley Lane				Conting	gency @ 20%	\$305,541
				[Fotal Con	struction Cost	\$1,833,247
			Engineer	ing, Surve	ying & G	eotech @ 12%	\$219,990
					Tota	al Project Cost	\$2,053,237
							**
7 S	SH195 12/15" GM	12" Sanitary Sewer		6,012	LF	\$66 #92	\$396,805
	12/15" gravity main flowing south to 18"	15" Sanitary Sewer		2,531		\$83	\$210,085
	collection main at Reese Creek Rd.	48 Diameter Mannole	;	21	EA	\$3,500 Subtotal	\$73,500
					Contine	gency @ 20%	\$136.078
				-	Fotal Con	struction Cost	\$816.469
			Engineer	ing, Survey	ying & G	eotech @ 12%	\$97,976
			e		Tota	al Project Cost	\$914,445
8S	Long Branch 15/18/24'' GM	15" Sanitary Sewer		3,758	LF	\$83	\$311,931
	New 15/18/24" GM conveying flow	18" Sanitary Sewer		8,287	LF	\$99	\$820,403
	south from Persimmons Dr to Lake Inks	24" Sanitary Sewer		1,672		\$132	\$220,717
	Ave south past RR to existing 36"	60" Diameter Manhole	;	30	EA EA	\$5,000 \$6,500	\$150,000
	interceptor; New 15" gravity main to	72 Diameter Mannole	,	4	LA	Subtotal	\$1 529 051
	convey flow near Hooten St west to Lake				Contin	gency @ 20%	\$305.810
	Inks Ave			-	Fotal Con	struction Cost	\$1,834,861
			Engineer	ring, Surve	ying & G	eotech @ 12%	\$220,183
					Tota	al Project Cost	\$2,055,044
20		10" 9		0.062	LE	¢ E E	¢442.292
98	Trimmier Creek 10/12'' GM	10" Sanitary Sewer		8,062		\$33 \$66	\$443,383
	A new 10/12 gravity main flows south	12 Saintary Sewer 48" Diameter Manhole		7,555		\$3 500	\$497,297 \$136 500
	15" collection main	40 Diameter Mannole	, ,	57	LA	Subtotal	\$1.077.179
					Conting	gency @ 20%	\$215,436
				5	Fotal Con	struction Cost	\$1,292,615
			Engineer	ring, Surve	ying & G	eotech @ 12%	\$155,114
					Tota	al Project Cost	\$1,447,729
100		16 Erma Main		0 775	IE	¢00	¢770 156
105	16" FM Along Chaparral Rd.	T Plock		8,775		\$88 \$6 500	\$/72,156
	New 16 FM to replace existing FM will	I-DIOCK		1	EA	\$0,500 Subtotal	\$778 656
	Rd to 21" intercentor just west of				Conting	gency @ 20%	\$155,731
	Featherline Rd			5	Fotal Con	struction Cost	\$934,387
	Peathernite Ru.		Engineer	ing, Surve	ying & G	eotech @ 12%	\$112,126
			-		Tota	al Project Cost	\$1,046,514
110	T #P4 64+ 4* 7 70 1 1	Lift Station M. 1.	o alas .'	4 1	IC	\$160.000	¢1.00.000
115	Lift Station / Kenab Lift Station 7 Rebab located off E	Lift Station - Not pipe	es, eiec, si	. I 1		\$100,000 \$325,000	\$100,000 \$225.000
	Veteran Memorial Blvd, on the edge of	Ent Station - Kenal #/		1	LO	Subtotal	\$485,000
	the Central Sub-Basin and the Long				Contine	gency @ 20%	\$97.000
	Branch Sub-Basin				Fotal Con	struction Cost	\$582,000
			Engineer	ring, Surve	ying & G	eotech @ 12%	\$69,840
					Tota	al Project Cost	\$651,840

		Table B.3				
	Wast	City of Killeen ewater System Improvements - 2	2010-2012			
		Opinions Of Probable Project	Cost			
Project <u>Number</u> 12S	Project Description Expand Lift Station #23 Expand Lift Station #23 off Reese Creek Rd. in the South Nolan Creek Sub-Basin	Construction Items Lift Station - Expans 2 MGD Lift Station - Mod pipes, elec, si	Quantity 1 it 1	Units LS LS Conting Fotal Con	Unit Price \$420,000 \$160,000 Subtotal gency @ 20% astruction Cost	 Costs \$420,000 \$160,000 \$580,000 \$116,000 \$696,000
		Engineer	ring, Survey	ying & G Tota	eotech @ 12% al Project Cost	\$83,520 \$779,520
138	LS & 14"FM 12/10"GM-Chaparal Rd 10/12" gravity main flows north along SH 195 to the new North SH 195 LS; 14" FM from new LS lifts flow along Chaparral Rd. to LS #24	Lift Station - New 2.5 MGD 14" Force Main 10" Sanitary Sewer 12" Sanitary Sewer 48" Diameter Manhole Engineer	1 7,989 8,116 4,185 31 ring, Survey	LS LF LF EA Conting Total Con ying & G Facility I	\$790,000 \$77 \$55 \$66 \$3,500 Subtotal gency @ 20% istruction Cost eotech @ 12% ROW (1 Acre)	 \$790,000 \$615,157 \$446,355 \$276,200 \$108,500 \$2,236,212 \$447,242 \$2,683,455 \$322,015 \$11,000
				Tota	ll Project Cost	\$3,016,469
c N	CITY OF KILLEEN WASTEWATER SYSTEM COSTS 2010					\$11,964,798

	Wast	Table B.4 City of Killeen ewater System Improvement Opinions Of Probable Proje	s - 2013-2015 ect Cost			
Project <u>Number</u>	Project Description	Construction Items	Quantity	Units	Unit Price	 Costs
148	New LS #18, 16" FM, 10/12/15" GM Two 10/12" gravity main convey flow along and to the east of Hay Branch to a 15" gravity main. The flow will be collected at the new LS #18 and lifted through a 16" FM to an existing 36" interceptor near Twin Creek Dr	Lift Station - New 2 MGD 16" Force Main T-Block 10" Sanitary Sewer 12" Sanitary Sewer 15" Sanitary Sewer 48" Diameter Manhole 60" Diameter Manhole Engin	1 14,574 1 5,530 8,234 920 34 2 	LS LF EA LF LF EA EA Contin Total Cor ying & G Facility]	\$780,000 \$93 \$6,500 \$58 \$70 \$88 \$3,500 \$5,000 Subtotal gency @ 20% nstruction Cost deotech @ 12% ROW (1 Acre) al Project Cost	 \$780,000 \$1,355,377 \$6,500 \$320,760 \$576,380 \$80,960 \$119,000 \$10,000 \$3,248,978 \$649,796 \$3,898,773 \$467,853 \$11,000 \$4,377,626
158	New Lift Station, 10'' FM, 12'' GM A new 10/12" gravity main will convey flows south to the new FM 439 LS. The LS will convey flow west through a 10" FM to a 12" interceptor.	Lift Station - New 1 MGD 10" Force Main 10" Sanitary Sewer 12" Sanitary Sewer 48" Diameter Manhole T-Block Engin	1 8,172 5,988 5,725 29 1 	LS LF LF EA EA Contin Total Cor ying & G Facility	\$610,000 \$58 \$58 \$70 \$3,500 \$6,500 Subtotal gency @ 20% nstruction Cost feotech @ 12% ROW (1 Acre) al Project Cost	\$610,000 \$473,970 \$347,307 \$400,729 \$101,500 \$6,500 \$1,940,006 \$388,001 \$2,328,007 \$2,79,361 \$11,000 \$2,618,368
165	Future Planning Area 10/15'' GM 10" gravity main flows east to a 15" interceptor just west of Chaparral Rd. and will carry flow east to the 36" major interceptor at East Trimmier Rd.	10" Sanitary Sewer 15" Sanitary Sewer 48" Diameter Manhole 60" Diameter Manhole Engin	6,562 8,244 16 21 neering, Surve	LF LF EA EA Contin Total Cor ying & G Tot	\$58 \$88 \$3,500 \$5,000 Subtotal gency @ 20% nstruction Cost eotech @ 12% al Project Cost	 \$380,590 \$725,503 \$56,000 \$105,000 \$1,267,093 \$253,419 \$1,520,512 \$182,461 \$1,702,973
178	New 2 MGD LS, 10" FM, 10/12" GM 10/12" gravity main flows south along Rock Creek to the new Upper Rock Creek LS. The LS will lift flows through a 10" FM north and east to the 15" interceptor at Chaparral Rd.	Lift Station - New 1 MGD 10" Sanitary Sewer 12" Sanitary Sewer 48" Diameter Manhole 10" Force Main T-Block Engin	1 6,764 4,371 28 9,000 1	LS LF EA LF EA Contin Total Cor ying & G Facility 1 Tot	\$610,000 \$58 \$70 \$3,500 \$58 \$6,500 Subtotal gency @ 20% astruction Cost beotech @ 12% ROW (1 Acre) al Project Cost	 \$610,000 \$392,329 \$305,981 \$98,000 \$522,000 \$6,500 \$1,934,810 \$386,962 \$2,321,772 \$278,613 \$11,000 \$2,611,385

	Table B.4 City of Killeen Wastewater System Improvements - 2013-2015 Oninions Of Probable Project Cost							
Project <u>Number</u>	Project Description	Construction Items	Quantity	Units	Unit Price	Costs		
185	Central Basin 21/24/36'' GM 21/24/27" gravity main flows east from Walmart Blvd. across Hwy 190 to a 36" interceptor flowing into LS #2.	21" Sanitary Sewer24" Sanitary Sewer27" Sanitary Sewer36" Sanitary Sewer72" Diameter ManholeEngir	1,190 9,078 875 2,070 30	LF LF LF EA Conting Total Con ying & Go Tota	\$123 \$140 \$158 \$191 \$6,500 Subtotal gency @ 20% struction Cost eotech @ 12% dl Project Cost	\$146,401 \$1,270,920 \$138,250 \$395,370 \$195,000 \$2,145,941 \$429,188 \$2,575,129 \$309,015 \$2,884,144		
195	N Clear Creek LS25 8"FM&12" 12" gravity main flows west to LS #25. The 8" force main lifts flow from the LS to an existing 10" gravity main.	Lift Station - New 1 MGD 8" Force Main 12" Sanitary Sewer 48" Diameter Manhole T-Block Engir	1 8,692 4,207 11 1 neering, Surve	LS LF EA EA Total Con ying & Go Facility F Tota	\$610,000 \$47 \$70 \$3,500 \$6,500 Subtotal gency @ 20% struction Cost eotech @ 12% ROW (1 Acre) Il Project Cost	\$610,000 \$408,510 \$294,469 \$38,500 \$1,357,979 \$271,596 \$1,629,575 \$195,549 \$11,000 \$1,836,124		

CITY OF KILLEEN WASTEWATER SYSTEM COSTS 2013

\$16,030,620

		Table B.5				
	Wast	City of Killee ewater System Improven	n nents - 2016-2018			
		Opinions Of Probable P	roject Cost			
Project					Unit	
Number	Project Description	Construction Items	s Quantity	Units	Price	Costs
20S	New LS, 18''FM 12/15/18'' GM	Lift Station - New 5 MG	D 1	LS	\$1,280,000	\$1,280,000
	12/15/18" gravity main flows south	12" Sanitary Sewer	3,907	LF	\$74	\$289,085
	along Little Trimmier Creek to the new	15" Sanitary Sewer	6,917		\$93	\$643,304
	Little Trimmier Creek LS. The LS will	18" Sanitary Sewer	3,010		\$112 \$3.700	\$404,947
	convey flow north an 18" force main to	60" Diameter Manhole	26	FA	\$5,700	\$137,000
	the Trimmier Creek WWTP.	18" Force Main	15 486	LE	\$112	\$1 734 421
		T-Block	10,100	EA	\$6,900	\$6,900
					Subtotal	\$4,533,457
				Contin	ngency @ 20%	\$906,691
				Total Co	nstruction Cost	\$5,440,148
		E	Engineering, Surve	ying & C	Beotech @ 12%	\$652,818
				Facility F	ROW (2 Acres)	\$22,000
				Tot	al Project Cost	\$6,114,966
215	Now I S and 14" FM 10/12" CM	Lift Station - New 2 MG	ו ח	15	\$820.000	\$820,000
215	10/12" gravity main flows south along	12" Sanitary Sewer	8 846	LS	\$74	\$654 589
	Onion Creek the new Onion Creek I S	10" Sanitary Sewer	2.947	LF	\$62	\$182.742
	The LS will then lift flows east through a	48" Diameter Manhole	29	EA	\$3,700	\$107,300
	14" force main to the Little Trimmier	14" Force Main	7,109	LF	\$87	\$618,509
	Creek LS	T-Block	1	EA	\$6,900	\$6,900
					Subtotal	\$2,390,040
				Contir	ngency @ 20%	\$478,008
		T		Total Co	nstruction Cost	\$2,868,048
		E	Engineering, Surve	Fooility	POW (1 A cro)	\$344,100
				Tacinty	al Project Cost	\$3 223 214
				100	an i lojeet cost	ψ5,225,214
22S	New LS, 12''FM & 12/15'' GM	Lift Station - New 2 MG	D 1	LS	\$820,000	\$820,000
	12/15" gravity main will collect flows	12" Sanitary Sewer	6,938	LF	\$74	\$513,408
	along the southern portions of Rock	15" Sanitary Sewer	8,224	LF	\$93	\$764,799
	Creek into the new Lower Rock Creek	12" Force Main	2,735	LF	\$74	\$202,368
	LS. The LS will convey flows to the	T-Block	1	EA	\$6,900	\$6,900
	east through a 12" force main to the	48" Diameter Manhole	17	EA	\$3,700	\$62,900
	Onion Creek LS.	60 Diameter Mannole	21	EA	\$5,300 Subtotal	\$111,300
				Contir	Jogeney @ 20%	\$496 335
				Total Co	nstruction Cost	\$2,978,011
		Е	Engineering, Surve	ving & C	Beotech @ 12%	\$357,361
			0 0,	Facility	ROW (1 Acre)	\$11,000
				Tot	al Project Cost	\$3,346,372
23S	8" GM North of Railroad	8" Sanitary Sewer	5,268	LF	\$50	\$263,408
	8" gravity main flows east to LS #18.	48" Diameter Manhole	13	EA	\$3,700	\$48,100
				Contin	Subtotal	\$311,508
				Conun Total Co	netruction Cost	\$02,502
		F	Engineering Surve	ving & C	Geotech @ 12%	\$44 857
		L	ingineering, buive	Tot	al Project Cost	\$418,666

		Table R 5				
		City of Killeen				
	Wast	ewater System Improvements	- 2016-2018			
		Opinions Of Probable Projec	t Cost			
Project			0	TT T .	Unit	
Number	Project Description	Construction Items	Quantity	Units	Price	Costs
248	New I S 10" FM & 12" West of 195	Lift Station - New 1.5 MGD	1	LS	\$730,000	\$730,000
245	New 12" gravity main which will convey	12" Sanitary Sewer	8.628	LF	\$74	\$638.505
	flow to the new Live Oak Cemetery LS.	8" Force Main	11,385	LF	\$50	\$569,250
	The LS will convey flow east through a	T-Block	1	EA	\$6,900	\$6,900
	8" force main to the Lower Rock Creek	48" Diameter Manhole	50	EA	\$3,700	\$185,000
	LS.				Subtotal	\$2,129,655
				Conting	gency @ 20%	\$425,931
		Engine	oring Survo	Total Con	struction Cost	\$2,555,586 \$206,670
		Englie	ering, Surve	Facility F	OW (1 Acre)	\$11,000
				Tota	al Project Cost	\$2,873,257
				100	a i lojeet cost	φ2,075,257
_						
	CITY OF KILLEEN					¢15.057.455
	WASTEWATER SYSTEM COSTS 2016					\$15,976,475

	Waste	Table B.6 City of Killeen ewater System Improvemen Oninions Of Probable Proj	nts - 2019-2021 ject Cost			
Project Number	Project Description	Construction Items	Quantity	Units	Unit Price	Costs
258	Trimmier Creek 30'' Gravity Main 30" interceptor parallels existing 30" interceptor from east of E. Trimmier Rd to the Trimmier Creek WWTP.	30" Sanitary Sewer 72" Diameter Manhole Eng	9,261 23 ineering, Survey	LF EA Contin Total Cor ving & G	\$175 \$6,500 Subtotal gency @ 20% istruction Cost eotech @ 12%	\$1,620,666 \$149,500 \$1,770,166 \$354,033 \$2,124,200 \$254,904 \$2,370,103
268	New LS, 10" FM, & 12" GM by 2484 10/12" gravity main flows south paralleling SH195 to the new South SH 195 LS. From the LS flows will be lifted north through a 10" force main along SH195 to the North SH 195 LS.	Lift Station - New 1 MGD 10" Force Main T-Block 10" Sanitary Sewer 12" Sanitary Sewer 48" Diameter Manhole Eng	1 11,379 1 1,691 9,827 25 ineering, Survey	LS LF EA LF EA Contin Fotal Cor ying & G Facility I Tota	\$640,000 \$62 \$6,900 \$62 \$74 \$3,700 Subtotal gency @ 20% istruction Cost eotech @ 12% ROW (1 Acre) al Project Cost	\$640,000 \$705,514 \$6,900 \$104,811 \$727,180 \$92,500 \$2,276,904 \$455,381 \$2,732,285 \$327,874 \$11,000 \$3,071,159
278	New LS, 8"FM, 8/10/12" near SH195 8/10/12" gravity main flows southwest to the new Lampasas LS; another 10/12" interceptor flows southeast to the new LS which will lift flow north across SH195 through a 8" force main to South SH 195 LS	Lift Station - New 1 MGD 8" Force Main 8" Sanitary Sewer 10" Sanitary Sewer 12" Sanitary Sewer 48" Diameter Manhole T-Block Eng	1 9,683 6,813 9,709 11,889 71 1 1 ineering, Survey	LS LF LF LF EA EA Contin Fotal Corving & G Facility I Tota	\$670,000 \$50 \$50 \$62 \$74 \$3,700 \$6,900 Subtotal gency @ 20% istruction Cost eotech @ 12% ROW (1 Acre) al Project Cost	\$670,000 \$484,150 \$340,630 \$601,986 \$879,764 \$262,700 \$6,900 \$3,246,130 \$649,226 \$3,895,356 \$467,443 \$11,000 \$4,373,798
288	10/12'' West of SH 195 10/12" gravity main flows south to the South SH 195 LS	12" Sanitary Sewer10" Sanitary Sewer48" Diameter ManholeEng	5,212 5,316 13 ineering, Survey	LF LF EA Contin, Total Con ving & G Tota	\$74 \$62 \$3,700 Subtotal gency @ 20% istruction Cost eotech @ 12% al Project Cost	\$385,673 \$329,620 \$48,100 \$763,393 \$152,679 \$916,072 \$109,929 \$1,026,000
298	Lift Station #1 Rehab. Lift Station #1 Rehab in the South Nolan Creek Sub-Basin.	Lift Station - Mod pipes, ele Lift Station - Rehab #1 Eng	ec, sit 1 1 ineering, Survey	LS LS Contin Fotal Cor ving & G Tota	\$190,000 \$700,000 Subtotal gency @ 20% astruction Cost eotech @ 12% al Project Cost	\$190,000 \$700,000 \$890,000 \$178,000 \$1,068,000 \$128,160 \$1,196,160
	CITY OF KILLEEN WASTEWATER SYSTEM COSTS 2019					\$12,046,221

	Table B.7 City of Killeen Wastewater System Improvements - 2022-2024 Opinions Of Probable Project Cost							
Project <u>Number</u>	Project Description	Construction Items	Quantity	Units	Unit Price	Costs		
305	New LS, 8'' FM, 12'' Gravity Main 12" collection main flows east to the new SH 2484 LS and will then be lifted through a 8" force main to the Little Trimmier Creek LS	8" Force Main 12" Sanitary Sewer T-Block Lift Station - New 2 MGD 48" Diameter Manhole Engi	8,947 8,280 1 1 21 neering, Surve	LF LF EA LS EA Continy Total Con ying & G Facility I Tota	\$50 \$74 \$6,900 \$860,000 \$3,700 Subtotal gency @ 20% istruction Cost eotech @ 12% ROW (1 Acre) al Project Cost	\$447,350 \$612,720 \$6,900 \$860,000 \$77,700 \$2,004,670 \$400,934 \$2,405,604 \$288,672 \$11,000 \$2,705,276		
318	New LS, 8" FM, 10/12" Gravity Main 10/12" gravity main flows southeast to the new Shaw Branch LS which will lift flow west through an 8" force main to a new 12" gravity main that will carry flow to the FM 439 LS	Lift Station - New 1 MGD 8" Force Main 12" Sanitary Sewer 10" Sanitary Sewer 48" Diameter Manhole Engi	1 6,624 13,455 5,571 48 neering, Surve	LS LF LF EA Continy Total Con ying & G Facility I Tota	\$670,000 \$50 \$74 \$62 \$3,700 Subtotal gency @ 20% istruction Cost eotech @ 12% ROW (1 Acre) al Project Cost	\$670,000 \$331,200 \$995,670 \$345,377 \$177,600 \$2,519,847 \$503,969 \$3,023,817 \$362,858 \$11,000 \$3,397,675		
()	CITY OF KILLEEN WASTEWATER SYSTEM COSTS 2022					\$6,102,951		

Appendix C Water Background Information



Week 1 - Pressure Recorder #1 Middle Pressure Plane Trimmier Road at Jasper



Week 1 - Pressure Recorder #2 Middle Pressure Plane Carmen Street at Dimple







----- Minimum ----- Average ----- Maximum
Week 1 - Pressure Recorder #5 Lower Pressure Plane Illinois Avenue between Grey Fox and Amber Road



Week 1 - Pressure Recorder #6 Lower Pressure Plane Telluride Drive between Teal Drive and Chantz Drive





Week 1 - Pressure Recorder #7 Lower Pressure Plane Rosewood Drive between Lightning Rock and Cinnamon Stone Week 1 - Pressure Recorder #8 Lower Pressure Plane Westcliff Road between Cedarview Drive ad Kingwood Drive



Week 1 - Pressure Recorder #9 Lower Pressure Plane Gray at Avenue D Drive





Week 1 - Pressure Recorder #10 Lower Pressure Plane Discharge side of Pump Station #3



South Clear Creek Road between Reese Creek Road and Tiffany Circle B Week 2 - Pressure Recorder #1 **Airport Pressure Plane**



Week 2 - Pressure Recorder #2 Airport Pressure Plane Golden Gate Drive east of Confederation



Week 2 - Pressure Recorder #3 Airport Pressure Plane Discharge side of Airport Pump Station



Week 2 - Pressure Recorder #4 Upper Pressure Plane Mustang Drive at Windfield Drive



Week 2 - Pressure Recorder #5 Upper Pressure Plane Clairidge Avenue at Carpet Lane



South of Turtle Creek Drive between Pebble Drive and Florence Road Week 2 - Pressure Recorder #6 **Upper Pressure Plane**



Week 2 - Pressure Recorder #7 Upper Pressure Plane WS Young between Riley and Stagecoach





- Maximum

- Average

Date

Week 2 - Pressure Recorder #8 Upper Pressure Plane lana Estacado west of Bunny Lan Week 2 - Pressure Recorder #9 Upper Pressure Plane State Highway 195 south of Omar Drive



Week 2 - Pressure Recorder #10 Upper Pressure Plane Goodhue Drive at Cascade Drive



Appendix D Wastewater Background Information

KILLEEN DURING F	I RAINFALL DATA LOW MONITORING
Date	Precipitation (inches)
5/1/2006	0.00
5/2/2006	0.00
5/3/2006	0.00
5/4/2006	0.00
5/5/2006	0.00
5/6/2006	2.50
5/7/2006	0.00
5/8/2006	0.00
5/9/2006	0.00
5/10/2006	0.00
5/11/2006	0.00
5/12/2006	0.00
5/13/2006	0.00
5/14/2006	0.20
5/15/2006	0.00
5/16/2006	0.00
5/17/2006	0.00
5/18/2006	0.00
5/19/2006	0.00
5/20/2006	0.00
5/21/2006	0.00
5/22/2006	0.00
5/23/2006	0.00
5/24/2006	0.00
5/25/2006	0.00
5/26/2006	0.00
5/27/2006	0.00
5/28/2006	0.00
5/29/2006	0.00
5/30/2006	0.00
5/31/2006	0.00
TOTAL	2.70

City of Killeen Wastewater Metering Station #1 (42" line) 106 N. WS Young Dr.



Depth (in) - Velocity (fps)





Depth (in) - Velocity (fps)

City of Killeen Wastewater Metering Station #3 (21.25" line) Maude St. at Lynn Ave.



Depth (in) - Velocity (fps)

		2006			2011			2016			2031	
			Peak Wet									
		Avg Day	Weather									
Census Tract		Flow	Flow									
in Subbasin	Population	(MGD)	(MGD)									
0221.01	2,074	0.22	0.87	2,074	0.23	0.91	2,074	0.24	0.95	2,074	0.24	0.95
0222	830	0.09	0.35	902	0.10	0.40	926	0.11	0.44	1,064	0.12	0.49
0223	1,107	0.12	0.47	1,287	0.14	0.57	1,362	0.16	0.63	1,512	0.17	0.70
0224.01	409	0.04	0.17	433	0.05	0.19	433	0.05	0.20	433	0.05	0.20
0225	1,153	0.12	0.48	1,162	0.13	0.51	1,341	0.15	0.62	1,445	0.17	0.66
0226	840	0.09	0.35	840	0.09	0.37	840	0.10	0.39	840	0.10	0.39
0229	4,231	0.44	1.78	4,231	0.47	1.86	4,231	0.49	1.95	4,231	0.49	1.95
0230	907	0.10	0.38	1,215	0.13	0.53	1,327	0.15	0.61	1,517	0.17	0.70
0231.02	15,313	1.61	6.43	19,668	2.16	8.65	23,308	2.68	10.72	30,794	3.54	14.17
0231.03	3,805	0.40	1.60	3,805	0.42	1.67	3,805	0.44	1.75	3,805	0.44	1.75
0231.04	3,706	0.39	1.56	3,706	0.41	1.63	3,706	0.43	1.70	3,706	0.43	1.70
0232	0	0.00	0.00	160	0.02	0.07	240	0.03	0.11	547	0.06	0.25
TOTAL	34,377	3.61	14.44	39,485	4.34	17.37	43,625	5.02	20.07	51,970	5.98	23.91

City of Killeen South Nolan Creek Subbasin Flows

_		200	9			201	1			201	9			203	1	
				Peak Wet												
		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather
Census Tract		Flow	Flow	Flow												
in Subbasin	Population	(MGD)	(MGD)	(MGD)												
0223	3,291	0.35	0.54	1.47	3,825	0.42	0.65	1.79	4,048	0.47	0.72	1.98	4,494	0.52	0.80	2.20
0224.01	4,344	0.46	0.71	1.94	4,599	0.51	0.78	2.16	4,599	0.53	0.82	2.25	4,599	0.53	0.82	2.25
0224.02	3,958	0.42	0.64	1.77	4,768	0.52	0.81	2.24	5,578	0.64	0.99	2.73	6,118	0.70	1.09	3.00
0225	7,032	0.74	1.14	3.15	8,871	0.98	1.51	4.16	10,213	1.17	1.82	5.01	12,205	1.40	2.18	5.98
0230	4,599	0.48	0.75	2.06	6,161	0.68	1.05	2.89	6,729	0.77	1.20	3.30	7,692	0.88	1.37	3.77
0231.02	2,591	0.27	0.42	1.16	3,328	0.37	0.57	1.56	3,944	0.45	0.70	1.93	5,211	0.60	0.93	2.55
0231.03	2,141	0.22	0.35	0.96	2,141	0.24	0.36	1.00	2,141	0.25	0.38	1.05	2,141	0.25	0.38	1.05
0233	0	0.00	0.00	0.00	40	0.00	0.01	0.02	76	0.01	0.01	0.04	136	0.02	0.02	0.07
TOTAL	27,955	2.94	4.55	12.51	33,732	3.71	5.75	15.82	37,327	4.29	6.65	18.30	42,595	4.90	7.59	20.88

City of Killeen Central Subbasin Flows

		200	9			201	1			201	9			203	1	
				Peak Wet												
		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather
Census Tract		Flow	Flow	Flow												
in Subbasin	Population	(MGD)	(MGD)	(MGD)												
0220	713	0.07	0.12	0.32	2,186	0.24	0.37	1.02	2,786	0.32	0.50	1.37	6,671	0.77	1.18	3.24
0221.01	2,024	0.21	0.33	0.91	2,024	0.22	0.35	0.95	2,024	0.23	0.36	0.99	2,024	0.23	0.36	0.99
0221.02	7,367	0.77	1.20	3.30	7,367	0.81	1.26	3.45	7,367	0.85	1.31	3.62	7,367	0.85	1.31	3.62
0221.03	6,070	0.64	0.99	2.72	6,070	0.67	1.03	2.85	6,070	0.70	1.08	2.98	6,070	0.70	1.08	2.98
0222	3,137	0.33	0.51	1.40	3,409	0.37	0.58	1.60	3,613	0.42	0.64	1.77	4,021	0.46	0.72	1.98
0223	2,953	0.31	0.48	1.32	3,433	0.38	0.59	1.61	3,633	0.42	0.65	1.78	4,033	0.46	0.72	1.98
0224.01	358	0.04	0.06	0.16	379	0.04	0.06	0.18	379	0.04	0.07	0.19	379	0.04	0.07	0.19
AE1	0	0.00	0.00	0.00	0	0.00	0.00	0.00	691	0.07	0.11	0.31	6,664	0.77	1.19	3.27
TOTAL	22,621	2.38	3.68	10.12	24,867	2.74	4.24	11.66	26,562	3.05	4.73	13.02	37,228	4.28	6.63	18.25
)								

City of Killeen Long Branch Subbasin Flows

		200	9			201				2016	6			2031		
				Peak Wet												
		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather
Census Tract		Flow	Flow	Flow												
in Subbasin	Population	(MGD)	(MGD)	(MGD)												
0221.01	961	0.10	0.16	0.43	961	0.11	0.16	0.45	961	0.11	0.17	0.47	961	0.11	0.17	0.47
0222	646	0.07	0.11	0.29	702	0.08	0.12	0.33	744	0.09	0.13	0.36	828	0.10	0.15	0.41
0226	3,847	0.40	0.63	1.72	3,847	0.42	0.66	1.80	3,847	0.44	0.69	1.89	3,847	0.44	0.69	1.89
0228.01	3,126	0.33	0.51	1.40	3,122	0.34	0.53	1.46	3,123	0.36	0.56	1.53	3,124	0.36	0.56	1.53
0229	223	0.02	0.04	0.10	223	0.02	0.04	0.10	223	0.03	0.04	0.11	223	0.03	0.04	0.11
0235	2,337	0.25	0.38	1.05	2,337	0.26	0.40	1.10	2,337	0.27	0.42	1.15	2,337	0.27	0.42	1.15
TOTAL	11,140	1.17	1.81	4.99	11,192	1.23	1.91	5.25	11,235	1.29	2.00	5.51	11,320	1.30	2.02	5.55

City of Killeen WWTP Subbasin Flows

	Peak Wet Weather Flow	(MGD)	0.80	2.57	1.07	3.27	10.71
1	Peak Day Flow	(MGD)	0.29	2.03	66.0	1.19	3.89
203	Avg Day Flow	(MGD)	0.19	1.31	0.25	0.77	2.51
		Population	1,625	11,370	2,190	6,664	21,849
	Peak Wet Weather Flow	(MGD)	0.70	4.22	0.47	1.83	7.21
6	Peak Day Flow	(MGD)	0.25	1.53	0.17	0.66	2.62
201	Avg Day Flow	(MGD)	0.16	66.0	0.11	0.43	1.69
		Population	1,422	8,606	960	3,724	14,712
	Peak Wet Weather Flow	(MGD)	0.61	3.41	0.30	0.92	5.23
1	Peak Day Flow	(MGD)	0.22	1.24	0.11	0.33	1.90
201	Avg Day Flow	(MGD)	0.14	08'0	20.0	0.22	1.23
		Population	1,302	7,262	640	1,960	11,164
	Peak Wet Weather Flow	(MGD)	0.43	2.53	00.00	0.00	2.97
9	Peak Day Flow	(MGD)	0.16	0.92	00'0	0.00	1.08
200	Avg Day Flow	(MGD)	0.10	0.59	0.00	0.00	0.70
		Population	972	5,654	0	0	6,626
	Census Tract	in Subbasin	0230	0231.02	0232	0233	TOTAL

City of Killeen SH 195 Subbasin Flows

		200	9			201	1			201	9			203		
				Peak Wet												
		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather		Avg Day	Peak Day	Weather
Census Tract		Flow	Flow	Flow												
in Subbasin	Population	(MGD)	(MGD)	(MGD)												
0224.02	10,700	1.12	1.74	4.79	12,890	1.42	2.20	6.04	15,080	1.73	2.69	7.39	16,540	1.90	2.95	8.11
0225	0	0.00	0.00	0.00	2,661	0.29	0.45	1.25	4,942	0.57	0.88	2.42	14,760	1.70	2.63	7.24
AS1	0	0.00	0.00	0.00	1,500	0.17	0.26	0.70	3,687	0.42	0.66	1.81	10,290	1.18	1.83	5.04
AS2	0	0.00	0.00	0.00	500	0.06	0.09	0.23	1,300	0.15	0.23	0.64	5,662	0.65	1.01	2.78
AS3	0	0.00	0.00	0.00	0	0.00	0.00	0.00	1,500	0.17	0.27	0.74	11,872	1.37	2.12	5.82
AS4	0	0.00	0.00	0.00	0	0.00	0.00	0.00	0	0.00	0.00	0.00	722	0.08	0.13	0.35
AS5	0	0.00	0.00	0.00	0	0.00	0.00	0.00	0	0.00	0.00	0.00	4,698	0.54	0.84	2.30
AS6	0	0.00	0.00	0.00	0	0.00	0.00	0.00	0	0.00	0.00	0.00	3,307	0.38	0.59	1.62
TOTAL	10,700	1.12	1.74	4.79	17,552	1.93	2.99	8.23	26,509	3.05	4.73	12.99	67,851	7.80	12.09	33.26

City of Killeen Trimmier Creek Subbasin Flows