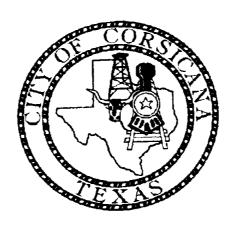
CITY OF CORSICANA FLOOD PROTECTION PLANNING STUDY



MAY 2 9 2001
MAY S MANAGEMENT

The City of Corsicana Navarro County, Texas and the Texas Water Development Board

May 2001





PLANNERS • SURVEYORS

4000 FOSSIL CREEK BOULEVARD FORT WORTH, TEXAS 76137 (817) 847-1422 METRO (817) 429-9975 FAX (817) 232-9784

May 11, 2001 AVO 18175

Connie Standridge, PE. City of Corsicana 200 N. 12th Street Corsicana, Texas 75110

Flood Protection Planning Study for the City of Corsicana, Texas Re:

Dear Ms. Standridge:

Transmitted herewith is one (1) unbound and five (5) bound copies of the Final Report entitled Flood Protection Planning Study for the City of Corsicana, Texas.

This final report includes a discussion of study procedures, alternative methods of reducing flood damages, results of technical analyses, and recommended plans to help alleviate flood damages in the study area. Final submittal of detailed Post Oak Creek drainage area delineation, 100-Year Flood plain Maps, and Flood Profiles are presented in Appendix D, which supplement this report.

It has been a privilege and a challenge for our firm to prepare this report and begin developing a storm water management plan for the City. Halff Associates is especially appreciative of the cooperation of the Corsicana residents and landowners as well as the members of the city staff, city council, and Texas Water Development Board who have assisted in the development of this study.



Gilbert Ward, TWDB

Sincerely,

HALFF ASSOCIATES, INC.

Michael A. Moya, P.E.

Project Manager

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Project Engineer

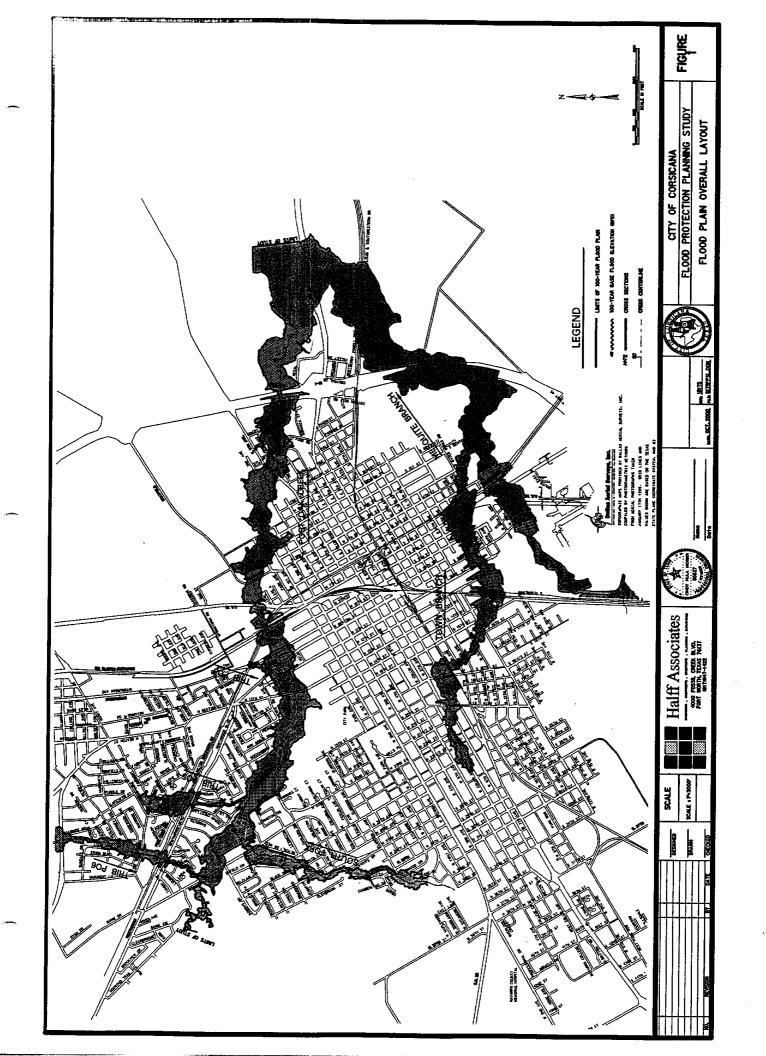


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ACKNOWLEDGEMENTS

Halff Associates, Inc. wishes to acknowledge the valuable assistance of the various organizations and individuals who have assisted in the preparation of the Flood Protection Planning Study for the City of Corsicana, Texas. We wish to express our gratitude to all those listed below who have contributed their time and effort to this study.

Texas Water Development Board, including Gilbert Ward, have provided invaluable assistance and advice throughout this study, in addition to the Flood Protection Grant provided to accomplish this study.

City of Corsicana Staff, including Mrs. Connie Standridge, P.E., City Engineer, Mr. Truitt Gilbreath, City Manager, Ms. Carole Mitchell, Mr. Ricky Jennings, and Mr. Frank Nerthling have provided invaluable assistance and advice throughout this study. The citizens of Corsicana have also provided a tremendous amount of flood data, information on problems, and valuable suggestions on the solutions.

The employees of Halff Associates who have worked most closely with the project include: Mr. Michael A. Moya, P.E., Ms. Cindy Mosier, P.E., Ms. Nancy Sieminski, Ms. Emilia Salcido, P.E., Mr. Troy Lynn Lovell, P.E., Ms. Ronda Visintainer, P.E., Mr. Michael Anderson, E.I.T, and Mr. Brian Agbulos. Halff Associates deeply appreciates the dedicated efforts of all the groups and individuals who have helped in the performance of this study.

GLOSSARY OF TERMS

- BASE FLOOD. The flood having a one percent chance of being equalled or exceeded in any given year, the 100-year flood. Note, for this study the <u>base flood</u> is based on a future fully urbanized watershed and existing channels and bridges with floodway encroachments in-place to account for potential upstream losses in valley storage. The FEMA base flood is based on existing land use and existing channels/bridges.
- <u>DISCHARGE</u>. As applied to a stream, the rate of flow, or volume of water flowing in a given stream at a given place and within a given period of time, usually quoted in cubic feet per second (cfs) or gallons per minute (gpm).
- <u>DRAINAGE AREA</u>. The area contributing to a lake, stream, sewer, or drain. Also called catchment area, watershed, and river basin.
- <u>FLOOD</u>. An overflow of land not normally covered by water and that is used or usable by man. Floods have two essential characteristics: The inundation of land is temporary; and the land is adjacent to and inundated by overflow from a river or stream or an ocean, lake, or other body of standing water.

Normally, a "flood" is considered as any temporary rise is a streamflow or stage, but not the ponding of surface water, that results in significant adverse effects in the vicinity. Adverse effects may include damages from overflow of land areas, temporary backwater effects in sewers and local drainage channels, creation of unsanitary conditions or other unfavorable situations by deposition of materials in stream channels during flood recessions, and rise of ground water coincident with increased streamflow.

- FLOOD FREQUENCY. A means of expressing the probability of flood occurrences as determined from a statistical analysis of representative streamflow, rainfall and runoff records. A 10-year frequency flood would have an average frequency of occurrence in the order of once in 10 years (a 10 percent chance of being equaled or exceeded in any given year). A 50-year frequency flood would have an average frequency of occurrence in the order of once in 50 years (a 2 percent chance of being equaled or exceeded in any given year). A 100-year frequency flood would have an average frequency of occurrence in the order of once in 100 years (a 1 percent chance of being equaled or exceeded in any given year). A 500-year frequency flood would have an average frequency of occurrence in the order of once in 500 years (a 0.2 percent chance of being equaled or exceeded in any given year).
- <u>FLOOD PEAK</u>. The maximum instantaneous discharge of a flood at a given location. It usually occurs at or near the time of the flood crest.
- <u>FLOOD PLAIN</u>. The relatively flat area or low lands adjoining the channel of a river, stream or watercourse or ocean, lake or other body of standing water, which has been or may be covered by flood water.
- <u>FLOOD PROFILE</u>. A graph showing the relationship of water surface elevation to location, the latter generally expressed as distance above the mouth for a stream of water flowing in an open channel. It is generally drawn to show surface elevation for the peak of a specific flood, but may be prepared for conditions at a given time or stage.
- <u>FLOODWAY</u>. The channel of a river or other watercourse and the adjacent land areas that must be reserved in order to discharge the base flood without cumulatively increasing the water surface elevation more than a designated height.

GLOSSARY OF TERMS (Continued)

- FULLY URBANIZED CONDITIONS. In the context of a drainage study, the watershed or drainage area of a stream is considered to be completely developed, i.e. all land is assumed to be functioning in it's ultimate use. Other descriptions include: Fully Developed, 100 Per Cent Urbanized, Ultimate Development or Land Use, and Maximum Development.
- ONE HUNDRED YEAR FLOOD. A flood having an average frequency of occurrence in the order of once in 100 years, at a designated location, although the flood may occur in any year and possibly in successive years. It would have a 1 percent chance of being equaled or exceeded in any year. In the past, this flood has been referred to as the Intermediate Regional Flood.

WATERSHED. The area contained within a divide above a specified point on a stream.

<u>VALLEY STORAGE</u>. The term used to describe a channel and flood plain's capacity to store some portion of the runoff volume as a flood wave moves downstream.

EXECUTIVE SUMMARY

In August 1999, the City of Corsicana contracted Halff Associates, Inc. to prepare a Flood Protection Planning Study for Post Oak Creek, South Fork Creek, Tributary PO-3, Tributary PO-5, Tributary PO-6, Mesquite Branch and Town Branch. In this study, Halff Associates developed detailed hydrologic (HMS) and hydraulic (HEC-RAS) computer models of the Post Oak watershed. This report was prepared to assist the City of Corsicana to plan and coordinate for future upstream development, flood plain reclamation, and help minimize existing potential flood damages.

Flood information that was developed for this study includes:

- 5-, 10-, 25-, 50-, 100-, and 500-year frequency storms
- Future, fully urbanized watershed conditions 100-year "base flood" elevations were delineated onto city topographic maps to show the extent of the 100-year flood plain limits.
- Conceptual improvements, such as improved channels and bridges were analyzed for reduction of potential flood and erosion damages. Estimates of probable cost were then prepared for each improvement plan.

Findings

Table A-1 is a summary of the study findings. Within the City of Corsicana project limits, approximately 955 acres of the Post Oak watershed is inundated by the future, fully urbanized 100-year flood plain. An estimated 409 homes are within those flood plain limits. This future 100-year "base flood" would overtop 60 of the existing 71 bridges or culverts within the study area.

TABLE A-1 Summary of Study Findings

Stream	Total Length In Study (miles)	Acres in the 100-Yr Flood Phin* (acres)	Number of Structures in the 190-Yr Flood Plain *	Number of Bridges Overtopped by 100-Yr Flood *	Total Extinated Cost for Channel and Bridge Improvements Analyzed
Post Oak Creek	5.4	450	154	10 - 514	
South Fork Creek	1.4	44	27	10 of 14	\$8,683,700
Tributary PO-3	0.3	2	6	6 of 6	\$2,548,900
Tributary PO-5	0.7	24	43	2 of 3	
Tributary PO-6	1.0	28	31	7 of 7 9 of 9	\$1,250,200
Mesquite Branch	4.1	287	8	Ĭ.	\$1,444,900
Town Branch	<u>2.4</u>	<u>120</u>	140	6 of 9 <u>20 of 23</u>	- \$6,542,100
TOTAL					
	15.3	955	409	60 of 71	\$20,469,800

 ¹⁰⁰⁻Year Flood Plain determined with existing channels and bridges/culverts and flood descharges based on future fully urbanized land use conditions and on existing channels/bridges.

Recommendations

Based on the results of this study, Halff Associates recommends the following:

Initial Flood Damage Reduction Plans:

• Tributary PO-6 channel and bridge improvements
Estimated Cost = \$1,444,900
Benefit to Cost ratio = 4.0

• Tributary PO-5 channel and bridge improvements
Estimated Cost = \$1,250,200

Benefit to Cost ratio = 1.4

Total Estimated Cost of Initial Recommended Improvements = \$2,695,100

Other Recommended Improvement Plans Include:

• South Fork Tributary channel and bridge improvements with Detention Ponds
Estimated Cost = \$2,548,900
Benefit to Cost ratio = 0.5

• Post Oak Creek Reach 4 (Oaklawn Drive to Dobbins Road) - channel and bridge improvements Estimated Cost = \$980.800

Benefit to Cost ratio = 0.5

Post Oak Creek Structure Purchase in conjunction with Reach 4 improvements

Purchase structures inundated by 5-year Flood Plain

Estimated Cost = \$96,650

Benefit to Cost ratio = 6.1

Or Purchase structures inundated by 10-year Flood Plain

Estimated Cost = \$230,500

Benefit to Cost ratio = 2.9

Or Purchase structures inundated by 100-year Flood Plain

Estimated Cost = \$1,852,000

Benefit to Cost ratio = 0.5

Town Branch Reach 1 (Chicago & Rock Island Railroad to S. Beaton Street) - channel and bridge improvements

Estimated Cost = \$1,415,200

Benefit to Cost ratio = 0.4

Town Branch Reach 2 (S. 12th Street to S. 16th Street) - channel and bridge improvements Estimated Cost = \$1,213,700 Benefit to Cost ratio = 0.4

Town Branch structure purchase in conjunction with Reaches 1 and 2 improvements

Purchase structures inundated by 5-year Flood Plain

Estimated Cost = \$678,600

Benefit to Cost ratio = 2.7

Or Purchase structures inundated by 10-year Flood Plain

Estimated Cost = \$1,030,900

Benefit to Cost ratio = 2.1

Purchase structures inundated by 100-year Flood Plain

Estimated Cost = \$2,594,740

Benefit to Cost ratio = 0.9

Other Recommendations:

- The City of Corsicana consider adopting flood plain management policies similar to the North Central Texas Council of Governments Flood plain Management Policies described in Chapter III.
- All stream crossings be included in a city-wide inspection and rating program for replacing undersized or dangerous bridges/culverts.
- All hazardous flood prone stream crossings should be marked with an active or passive flood warning system.
- The City formally adopt the flood levels shown in this report for its flood plain management program.
- The City periodically update the hydraulic models as channel conditions are modified.

I. INTRODUCTION

A. GENERAL

The City of Corsicana, Texas is a rapidly developing community that is concerned about the increasing threat of flooding and associated damages due to increased urbanization in the Post Oak watershed. Post Oak Creek, South Fork of Post Oak Creek, Town Branch, and Mesquite Branch are the major drainage waterways that flow through the City. These creeks were formed by centuries of flood water erosion and their flood plains include an abundance of scenic and environmental resources. Corsicana's future population growth and associated development will require careful planning and management in order to minimize flood damages and to ensure the maximum possible preservation of the Post Oak drainage corridors.

B. PURPOSE OF REPORT

The purpose of the City of Corsicana Flood Protection Planning Study is to provide a comprehensive, updated flood control-flood plain management master plan for Post Oak Creek, South Fork of Post Oak Creek, Post Oak Tributary-3, Post Oak Tributary-5, Post Oak Tributary-6, Mesquite Branch, and Town Branch within the Corsicana City Limits. This study addresses existing flooding/erosion problems within the city and provides planning alternatives and design concepts to help alleviate potential flood damages. The information presented in this report will provide the City with the necessary updated drainage information to coordinate future development and help minimize existing potential flood damages along Corsicana's major stream corridors.

This report provides a summary of the procedures used to analyze the existing flood problems and the results and recommendations that were derived from the analyses. Additional information (i.e. field survey notes, photographs, and work maps) and computer files used in the production of this report are available from Halff Associates, Inc. and from the City of Corsicana.

Specific objectives of the Flood Protection Planning Study are:

- 1. Compile pertinent existing engineering data and newly developed information into a comprehensive report with an <u>up-to-date</u>, <u>fully developed watershed</u>, <u>100-year flood plain delineation</u> of the study area.
- 2. Formulate <u>conceptual plans</u> and analyze the effects of <u>proposed improvements</u> to reduce the flooding potential along the streams. Consideration of improving channel flow characteristics and enlarging bridges or culverts is included. Prepare predesign estimates of probable cost for the various channel/bridge improvement plans.
- 3. Formulate <u>conceptual plans</u> and analyze the effects of <u>non-structural solutions</u> to reduce the flooding potential along the streams. Determine the number of properties to be acquired and removed from flood prone areas. Prepare estimates of probable costs.
- 4. Based on the analysis of various alternative plans to reduce flooding, make <u>recommendations</u> to the City. These recommendations are presented in Chapter V, with accompanying engineering data to guide the City in a planned program of needed improvements.
- 5. Coordinate all phases of the study, from data gathering to final design recommendations, with the City Engineering Staff.

In addition to the basic objectives listed above, Halff Associates always attempts to fulfill the following criteria in the planning of any proposed improvements:

- 1. Acquire community acceptance through neighborhood enhancement.
- 2. Preserve, to the extent possible, the flood plain's natural environmental resources.
- 3. Minimize relocation or alteration of residential and business properties and disruption of services to citizens.
- 4. Formulate and recommend practical, flexible, and affordable alternative plans to solve flooding problems.

C. COMMUNITY DESCRIPTION

The City of Corsicana is the county seat of Navarro County and is located in north central Texas. According to 1998-1999 Texas Almanac (Reference 1) the estimated population of the City of Corsicana is 24,042. Existing development in Corsicana consists primarily of single family residential neighborhoods with commercial development throughout the city.

The City of Corsicana lies within the Blackland Prairie subdivision of the Coastal Plains physiographic province. The topography is gently rolling to almost level with narrow streams being well incised. Elevations vary from approximately 320 to 500 feet above the National Geodetic Vertical Datum of 1929 (NGVD). The soils in the area generally consist of sandy, silty clay soils with loamy surface layers and clays subsoils. Native vegetation consists of bunch and short grasses with scattered overstory trees (Reference 2).

The climate of the study area is humid subtropical with hot summers. Summers are hot, and winters are short and mild. Extremes of temperature and precipitation are of relatively short duration. The mean annual precipitation is about 37 inches. Record temperature extremes range from a maximum of 113°F to a minimum of -7°F (Reference 2).

Post Oak Creek and Mesquite Branch are the major drainage collectors for the City of Corsicana. However, many smaller tributaries such as South Fork of Post Oak Creek and Town Branch also traverse through the City providing drainageways for existing and future development. Generally, storm water from the northern portion of the City drains to Post Oak Creek. Storm water from the southern portion of the city generally drains to Mesquite Branch. These two major creeks flow in an easterly direction joining downstream at the east side of the City.

D. PRINCIPAL FLOOD PROBLEMS

Most of the flood producing storms that occur in the Corsicana area are experienced in the spring and fall. Many of the higher floods that have occurred are a result of prolonged or successive storms that produce heavy rainfall. However, intense localized thunderstorms are common throughout the year and flash flooding may occur at any time.

The City of Corsicana has a history of flood problems and damages within the Post Oak Creek drainage basin. Urbanization of the watershed and reclamation within the flood plain have resulted in increased flood flows and flood elevations. Many of the city's flood damages or related problems are caused by inadequate capacities of the existing channels and bridges. Existing development, subject to overbank flooding, is primarily residential but also includes some commercial property especially along the major creeks. An estimated 409 homes are within the limits of the future fully urbanized 100-year flood plain, which covers approximately 955 acres within the Corsicana study area.

Major flooding events have occurred in Corsicana in April 1957, May 1968, October 1974, November 1974, July 1982, May 1989, and March 1990. There are no stream gauging records and no adequate high-water marks to estimate flows for the Streams for any of these periods. However, following the May 1989 flood, the City of Corsicana conducted a detail survey of flooded structures throughout the City. Approximately 308 structures reported flooding. About 174 of these structures reported damages totaling about \$2.7 million. Damages were not tallied for the remaining 134 flood inundated structures. See Chapter IV for descriptions of potential flooding problems along each creek.

II. STUDY PROCEDURES

A. HYDROLOGIC STUDIES

1. General

Hydrologic analyses were conducted by Halff Associates for the Post Oak Creek, South Fork of Post Oak Creek, Post Oak Tributary-3, Post Oak Tributary-5, Post Oak Tributary-6, Mesquite Branch, and Town Branch Watershed basins (hereon referenced as Post Oak Watershed) using the Corps of Engineers hydrologic computer program HEC-HMS Version 2.0 (Reference 3). Halff Associates' hydrologic analysis for this study was prepared using existing (2000) and future, fully-urbanized watershed conditions. Flood events of a magnitude which are expected to be equaled or exceeded once on the average of any 5-, 10-, 25-, 50-, 100-, and 500-years have been selected as having special significance for this study. These events have a 20, 10, 4, 2, 1, and 0.2 percent chance, respectively, of being equaled or exceeded during any one year. Tables of peak flood discharges can be found in Chapter IV. Although the recurrence interval represents the long term, average period between floods of a specific magnitude, rare floods could occur at short intervals or even within the same year. The risk of experiencing a rare flood increases when periods greater than one year are considered. For example, the risk of having a flood which equals or exceeds the 100-year flood (one percent chance of annual occurrence) in any 50-year period is about 40 percent (4 in 10), and for any 90-year period, the risk increases to about 60 percent (6 in 10).

The Post Oak drainage watershed was sub-divided into approximately 30 sub-watershed basins. Watershed characteristics such as drainage area, watercourse length, location of centroid, basin slope, land use, soil type, and channel/flood plain storage were determined for each sub-watershed basin. The hydrologic procedure used in the preparation of this report includes the development of synthetic unit hydrographs at each of these sub-basin locations. Derived runoff hydrographs were then combined and routed through existing channels. The program HMS (Reference 3) was used to compute storm runoff based on Soil Conservation Service (SCS) curve numbers, derived from land use and hydrologic soil type. The Snyder's unit hydrograph method and the Modified Puls routing method were used to determine peak flood discharges for a given frequency rainfall.

2. <u>Land Use</u>

As communities such as Corsicana develop, farms and pastures are replaced with residential, commercial, and industrial land uses. Halff Associates used the City of Corsicana Existing Land Use Map (Reference 4) and aerial photographs flown by

Dallas Aerial Surveys, Inc. in January 1999 to determine existing land use conditions. Land use classifications in the City of Corsicana were verified and adjusted based on field observations. Existing land use trends and information provided by the City of Corsicana was compiled to predict future land use and growth patterns within the watershed.

3. <u>Impervious Coverage</u>

Percent impervious is a function of land use of the drainage area. Residential impervious cover typically reflects the housing market by allowing greater building and pavement coverage as land prices increase. The assumed impervious coverage for land uses found in the Post Oak watershed study area can be found in Table II-1.

Percent impervious values were derived by Halff Associates using Corps of Engineers and Soil Conservation Service (SCS) publications and using drainage design manuals from various Texas cities. Halff Associates has also derived impervious coverage values for Dallas-Fort Worth Metroplex residential areas using detailed measurements of developed areas, as shown in Halff Associates' 1980 study for the City of University Park (Reference 5).

TABLE II-1 Characteristic Imperviousness for Land Use found in the Post Oak Watershed

Land Use Classification:	Characteristic		
	Enperviousness :		
Moderate Density Residential (R-20 maximum)	40%		
High Density Residential (R-15, R-10, RD)	55%		
Commercial / Industrial	85%		
Mixed Urban/Commercial	60%		
Industrial with Open Space	55%		
Schools / Public and Semipublic	30%		
Parks / Golf Courses / Cemeteries / Open Space	5%		
Crops / Pasture	5%		
Impervious Areas Pavement, Water)	100%		

4. Soil Types

Hydrologic soil types are divided into four groups (A, B, C, and D). Group A soils have the highest infiltration rates and the lowest runoff potential of the four soil types. Group B soils have moderate infiltration rates. Group C soils have slow infiltration rates. Group D soils have the slowest infiltration rates and the highest runoff potential. Group A soils are usually well drained and consist of sand or gravel. Group D soils, on the other hand, are often clayey, have a high water table, or consist of bedrock or other nearly impervious material. Hydrologic Soil Types for the Post Oak watershed basin were estimated from the Soil Conservation Service Navarro County, Texas Soil Survey (Reference 6).

The antecedent moisture condition (AMC) defines the soil moisture condition prior to a storm. The Soil Conservation Service has defined three levels of antecedent moisture conditions (Reference 7) listed below. AMC II soil conditions were assumed for this study.

AMC-I Dry soils and low runoff potential AMC-II Average soil moisture conditions

AMC-III Saturated soil condition from antecedent rains

5. Loss Rates

The SCS Curve Number Method is a technique, developed by the Soil Conservation Service (SCS), for classifying land use and soil type using a single parameter called the Curve Number (CN). The curve number is dependent on the land use, impervious coverage, soil classification, and antecedent runoff conditions. Table II-2 is a list of composite CN's for land uses, with AMC-II hydrologic soil types, representative of the study area.

Halff Associates computed SCS Curve Number's using a weighted average percent imperviousness for individual soil types and land use within each sub-watershed basin. The composite CN's shown in Table II-2 were computed using the percent impervious values from Table II-1.

The *initial abstraction (IA)* was computed for AMC-II (average) soil conditions using the following equation (Reference 3):

IA = 0.2 * (1000 - 10 * CN) / CN

TABLE II-2
Composite SCS Curve Numbers for the Land Use found in the Post Oak Watershed

Land Use Classification	Composite SCS Curve Number for each Hydrologic Soil Type						
	Soil A	Soil B	Soil C	Soil D			
Moderate Density Residential	61.4	74.6	82.4	86.0			
High Density Residential7	69.8	79.7	85.6	88.3			
Commercial / Industrial	86.6	89.9	91.9	92.8			
Mixed Urban/Commercial	72.6	81.4	86.6	89.0			
Industrial with Open Space	69.8	79.7	85.6	88.3			
Schools / Public and Semipublic	55.8	71.2	80.3	84.5			
Parks / Golf Courses / Cemeteries / Open Space	41.8	62.7	75.1	80.8			
Crops / Pasture	41.8	62.7	75.1	80.8			

Composite Curve Numbers were computed using the average percentage of impervious area shown on Table II-1. These curve numbers were computed assuming all impervious areas have a curve number of 95. Pervious areas are considered equivalent to open space in good hydrologic soil conditions (CN for soil A = 39, soil B = 61, soil C = 74, and soil D = 80).

6. Snyder's Unit Hydrograph

Time of Concentration is the time required for runoff to travel from the most distant part, hydraulically, of the storm area to the watershed outlet. Times of Concentration were determined by dividing the total stream and overland flow length by the average velocity. Average velocities were determined from an SCS chart (Reference 7) utilizing basin slope and type of cover.

Halff Associates computed lag times using the following equation (Reference 9):

Tp = 0.6 * Time of Concentration

Snyder's Unit Hydrograph Lag Times (Tp) were also determined from watercourse length, basin slope, from regional relationships, developed by the Corps of Engineers, of sub-basin geometry and percent urbanization (Reference 2). These regional relationships are a function of watercourse length, location of centroid, basin slope, percent urbanization, and soil type. Typically, these values were in the same range as the SCS method, therefore, the SCS method was utilized.

Snyder's Peaking Coefficient (Cp) was determined from information developed specifically for the Dallas-Fort Worth Metroplex by the U.S. Army Corps of Engineers Fort Worth District (Reference 8).

7. Rainfall

Point rainfall depths for the Post Oak watershed were taken from the National Weather Service Publication *Technical Paper No. 40* (Reference 10) and from the National Oceanic and Atmospheric Administration (NOAA) Technical Memorandum *Hydro-35* (Reference 11). The National Weather Service has developed a relationship to convert point rainfall depths to aerial average rainfall based on the size of the drainage area and the duration of the storm. However, because of the small drainage basin studied, aerial reduction of point rainfall depths was not necessary for this study.

Table II-3 are the point rainfall depths used for this study for the 5-, 10-, 25-, 50-, 100-, and 500-year flood frequencies.

TABLE II-3
* Rainfall Depth / Duration for the Corsicana Study Area

Return Period (years)	2.040 1.040 1.040	Pom Ra	iriali Depihs	(inches) fi	or Corsicar	na Study Ar	ea This is a second	e L
	δ-jnin.	E Stink	4 6 0-mm	2-hour	3-hom	6-hour	12 hour	24-hou
5-Year	0.58	1.25	2.44	3.17	3.42	4.13	4.89	5.64
10-уеаг	0.64	1.38	2.77	3.67	4.08	4.87	5.82	
25-Year	0.74	1.58	3.25	4.34	4.76	5.75		6.76
50-Year	0.81	1.74	3.63	4.84	 	t	6.80	7.84
100-Year	0.88	1.89	 		5.36	6.52	7.72	8.94
500-Year		- -	4.00	5.34	5.88	7.29	8.70	9.97
——— <u> </u>	1.2 from Technical Pape	2.3	4.6	6.5	7.1	9.0	10.8	12.4

8. Flood Routing

The Modified Puls routing method was utilized for this study by establishing storage-outflow relationships from steady-flow water surface profiles determined from HEC-RAS hydraulic analyses. Storage-outflow relationships were determined for existing (2000) channel/flood plain conditions.

B. HYDRAULIC ANALYSES

1. General

Flood profiles for Post Oak Creek, South Fork of Post Oak Creek, Post Oak Tributary-3, Post Oak Tributary-5, Post Oak Tributary-6, Mesquite Branch, and Town Branch were developed using the Corps of Engineer's backwater computer program HEC-RAS Version 2.2(Reference 12).

2. Existing Channel and Bridge Conditions

Cross-sections used in the HEC-RAS computer models were located at close intervals above and below bridges and culverts in order to compute the significant effective flow and backwater effects of these structures. Synthetic cross-sections were taken from two-foot contour interval mapping compiled from January 1999 aerial photographs, prepared by Dallas Aerial Surveys, Inc. The mapping was supplemented with data from previous Corps' studies, as-built bridge and roadway plans, and field surveyed cross sections provided by the City of Corsicana taken in March and April 2000. All elevations are measured from National Geodetic Vertical Datum of 1929 (NGVD). A list of vertical control benchmarks is provided in Appendix B.

Channel roughness factors (Manning's "n") were assigned on the basis of field inspections of flood plain areas and from previous studies by the Corps of Engineers. For study purposes, it was assumed that no clogging would occur and that all bridge structures would stand intact. Significant changes in this premise, imposed by differing conditions of a future flood, could alter the estimated flood elevations and flood limits shown on the profiles and flood plain maps that supplement this report.

The location of cross-sections and the results of this analysis are displayed in Appendix D on the flood plain maps and flood profiles that supplement this report. Appendix E contains the HEC-RAS summary printout for the existing channel condition hydraulic runs with the future fully developed 5-, 10-, 25-, 50-, 100-, and 500-year flood results. Appendices D and E were not published with this report but are available from the City of Corsicana or from Halff Associates, Inc. Computer disks containing copies of all hydrologic and hydraulic computer models used in the preparation of this report were also provided to the City of Corsicana.

3. <u>Improved Channel and Bridge Conditions</u>

Halff Associates modified the existing channel conditions HEC-RAS hydraulic computer models to analyze conceptual design alternatives of proposed channel and

bridge improvements. The basic design objective was to reduce potential flood heights and damages while minimizing the destruction of waters of the U.S. and to provide the City Engineering Staff with conceptual channel/bridge designs for future development and roadway improvements. Descriptions and sketches of these proposed designs are provided in Chapter IV. The resulting improved flowlines and water surface elevations are displayed on the flood profiles that supplement this report. Note, there are some reaches of the streams where no improvements are recommended, and the existing channel should remain in its natural state, unless a specific plan is formulated. Summary HEC-RAS computer printouts for the proposed recommendations may be found in Appendix E.

C. FLOOD PLAIN DELINEATION

The City's current flood regulatory maps are the FEMA Flood Insurance Rate Maps effective date August 1981 (Reference 13). The National Flood Insurance Program uses the 100-year flood (existing conditions) as the "base flood" for insurance and mapping purposes. Since floods greater than the 100-year flood may occur, citizens should bear in mind that if the level of protection is for a 100-year flood, it is possible for flood levels to exceed this limit.

For this study, the "Base Flood" 100-year flood plain limits and flood profiles were prepared for existing channel and bridge conditions with future, fully urbanized flood discharges. For this study, this condition is referred to as Baseline Conditions. Flood plain maps and flood profiles are presented in Appendix D which supplements this report. The delineation of the future fully urbanized 100-year flood plain for Post Oak Creek, South Fork of Post Oak Creek, Post Oak Tributary-3, Post Oak Tributary-5, Post Oak Tributary-6, Mesquite Branch, and Town Branch provides the City of Corsicana with one of the basic tools of flood plain management. This data will be instrumental in the performance of many flood plain management functions, some of which are listed below.

- 1. Formulation of flood plain management alternatives;
- 2. Outlining of flood-hazard areas;
- 3. Planning for parks and recreation in flood-prone areas;
- 4. Compliance with requirements of federal flood insurance programs;
- 5. Establishment of safe finished-floor elevations;
- 6. Planning of subdivisions to provide room for the passage of floodwater;
- 7. Design of roads, bridges, and utilities; and
- 8. Designation of easements or land to be purchased and used for open space.

Included in this study are computer data disks containing copies of all hydrologic and hydraulic computer models used in the production of this report. These baseline computer models will enable City Engineering staff to predict flood levels for flows based on existing and/or future land use conditions. The city will also have the ability to periodically update

and modify the models prepared for this study to predict anticipated changes in land use and/or watershed characteristics.

D. DESIGN CRITERIA FOR IMPROVEMENTS

For each creek in the study, channel and/or bridge conceptual design HEC-RAS computer models were developed. Possible flood control improvements include enlarged grass-lined or rock-lined channels, bridge/culvert modifications and replacements, erosion control features, drop structures, and detention ponds. The proposed improvements have been designed to best achieve the following criteria:

- 1. Where practical, contain the future fully-urbanized 100-year flood discharge within the proposed channel;
- 2. Maintain non-erosive or non-damaging velocities (approximately 6 fps for grass-lined channels and about 8 to 10 fps for natural rock-lined channels);
- 3. Minimize rises in flood elevation due to new roadway alignments and flood plain reclamation;
- 4. Minimize the amount of additional R.O.W. to be acquired;
- 5. Minimize or avoid major utility relocations;
- 6. Minimize environmental damage where possible.

E. DESIGN CONSTRAINTS

In addition to the basic design criteria listed above, the following items were also considered in the conceptual design phase of this study:

- 1. Restricted Right-of-Way Based on subdivision plans and plat maps, drainage easements along the creeks and tributaries are limited or non-existent in many reaches. Where drainage easements do exist, they are often too narrow for significant channel improvements. These narrow corridors restrict the viable alternatives considerably, and in some places, rule out a grass-lined trapezoidal channel.
- 2. <u>Steep Existing Channel Slope</u> Portions of the existing channel slopes are relatively steep and create high, erosive velocities in the natural channel.
- 3. <u>Inadequate Road Crossings</u> Many existing bridges and culverts are generally undersized in comparison with future fully urbanized 100-year flood flows. When

existing culverts are relatively low with respect to the channel, higher head losses are common at road crossings. These low culverts are also prone to catch debris and dam up flood waters. From a design perspective, some of the existing streets, driveways, and sidewalks in the vicinity of some road crossings are often too low, when compared to 100-year flood elevations, and must be rebuilt or adjusted if larger drainage structures are to be installed.

- 4. Natural Beauty of Streams The existing environment along most of the streams is generally of a high quality with many large trees, considerable landscaping, and much natural beauty. It is difficult to design flood control improvements that will not destroy or significantly alter these attributes. Also, the potential loss of trees located immediately adjacent to the creek bank is often unavoidable due to continual channel erosion and subsequent damage to the tree's root system.
- 5. Preservation of Waters of the U.S. Proposed improvements shall adhere to the requirements of The U.S. Army Corps of Engineers Section 404 permits. Projects impacting more than 1/10 acre of waters of the U.S. shall require formal notification of the U.S. Army Corps of Engineers. An Individual Permit will be required for channel projects impacting greater than ½ acre or 300 linear feet of perennial and intermittent stream beds.
- 6. <u>Existing Water and Sewer Lines</u> These and other utilities dictate the design channel flowline elevations and alignment in some reaches.
- 7. Houses and business are extremely close to the channel banks in some locations.

F. ECONOMIC ANALYSIS

1. Purpose - The principal purpose for an economic analysis is to identify and quantify the extent of flood problems and, on a comparable basis, evaluate solutions to reduce flood losses. Estimates of flood damages and benefits presented in this report reflect 2000 prices with future fully urbanized development. Corps of Engineer's procedures were generally used for this economic analysis.

The computer program HEC-Flood Damage Analysis with Risk (Reference 21) was used in the economic analyses as described below.

2. <u>Inventory of Structures</u> - The economic analysis study area included all properties lying within the 500-year flood plain limits for Post Oak Creek, South Fork of Post Oak Creek, Post Oak Tributary-3, Post Oak Tributary-5, Post Oak Tributary-6, Mesquite Branch, and Town Branch. Topographic maps, compiled from aerial photography flown January 1999, served as base maps to identify the flood-prone properties. Finished floor elevations for all structures within the future 100-year

flood limits were estimated from the topographic maps assuming one (1) foot above the estimated ground elevation.

Information provided by the City of Corsicana was utilized to inventory the flood plain lands along Post Oak Creek and its tributaries in order to identify the current types and level of flood plain development. This included enumeration of the types and numbers of structures within the 500-year flood plain limits.

3. Evaluation of Flood Damages - The water surface profile elevations for 1-, 2-, 5-, 10-, 25-, 50-, 100-, and 500-year flood events, based on existing (2000) channel and bridge conditions with future fully developed watersheds, were used to evaluate flood damages. These flood profiles aided in delineating the flood plain limits and in determining the relationship of damageable properties to both elevation and frequency of flood occurrence.

The current market values of the structures identified were estimated through the assistance of the City of Corsicana. Existing damageable properties were classified into the major damage categories shown in Table II-4. Estimates were made on the value of flood plain investment (structure and contents) for each of the damage categories. Note, the value of existing residential contents was estimated to be 50 percent of the value of the structure.

TABLE II-4
MAJOR DAMAGES CATEGORIES

Damage Categories	Activity Description
Residential Multi-Family Commercial Church School	Single-Family Residential Apartments, Townhomes, Duplexes Commercial, Office, and Industrial Church, Civic School

4. <u>Estimated Project Costs</u> - For each of the alternatives considered, a preliminary estimate of implementation (construction) costs was prepared. These costs were based on preliminary quantities and estimated unit prices from recent bids. No geotechnical borings were obtained for the study, and no detailed grading plans, utility relocation investigations, or right-of-way computations were prepared. Preliminary estimates of probable cost for each alternative are shown in Appendix C and are summarized in Chapter IV, of this report.

5. Benefit-Cost Comparisons - Benefit-cost calculations were made only for those areas that had significant existing flood damages. Average annual benefits were computed by subtracting the proposed (improved) channel conditions average annual damages, from the existing channel conditions average annual damages. Annual damages and benefits for specific reaches of the study area are contained in Chapter IV. Note that the primary benefit, to be derived from a proposed plan of improvement, is a reduction in flood damages. Social, environmental, and other intangible benefits are not quantified in monetary terms and were not considered in this benefit-cost analysis.

The average annual costs and benefits were calculated for a 50-year period of analysis. Benefit and cost accruals were made comparable by conversion to an equivalent annual basis using an interest rate of 7.75 percent (Assumed Average Current Federal Discount Rate). The normal measure of economic feasibility, as used in Federal projects, is a benefit-cost ratio being greater than or equal to 1.0. See Chapter IV for proposed alternative details and the overall benefit-cost ratio of alternatives considered.

III. METHODS OF REDUCING FLOOD DAMAGES

A. INTRODUCTION

A number of alternative measures can be used, either separately or collectively, to reduce the threat of flooding. The alternatives can be grouped into four broad categories: (1) No Action; (2) Non-Structural Measures; (3) Structural Measures; and (4) Relief Measures. This chapter discusses the alternatives to flood reduction and their applicability to the Post Oak Creek drainage basin within the Corsicana city limits.

B. NO ACTION

Taking no action is a non-structural measure that must always be considered. Taking no action towards the flooding problems identified would mean that the City of Corsicana would rely on its current flood plain zoning and subdivision ordinances to regulate all future development along the creeks, and on its Flood Insurance Program regulations to manage future and existing development in the 100-year flood plain and floodway fringe. The interest and significant effort undertaken in the production of this study indicates that the City of Corsicana desires to initiate some action towards alleviating existing and future flooding problems in the study area.

No action constitutes rejection of most mitigation methods of flood plain management. The flood plain would be defined based on existing land use discharges. FEMA regulations would be used to govern the reclamation of flood plain land. The flood plain would be developed or preserved on a piecemeal basis with no consistency or continuity. For example, one owner may preserve his entire flood plain, while the upstream owner may channelize and fill to the floodway limits. This could result in higher discharges downstream and could increase channel velocities and flood elevations through the property of the downstream owner. The development of a predictable flood plain elevation could not be achieved with any certainty. Therefore, each development would have to be handled on an individual basis. This would create considerably more work for the Corsicana city staff, whereas, each flood plain development would be evaluated on an individual basis.

C. NON-STRUCTURAL MEASURES

Non-structural methods are the management techniques and/or legislative safeguards intended to decrease flooding and reduce flood damage to individual structures or to land in or around a community. Structures can be protected by elevating in place or by regulating or acquiring specific areas of land in fee or easement. Non-structural measures considered for this study are discussed below:

1. Land Use Zoning and Subdivision Regulations

One means of preventing flood damage is to keep industrial, commercial, and residential structures from being built within the flood plain. Flood plain zoning restricts flood plain utilization to uses that can sustain floods without endangering life or valuable property. Regulatory ordinances are intended to secure the maximum benefits and productivity of flood-prone land by allowing flood plains to convey the design flood; promoting the public's health, safety and general welfare; and minimizing potential flood losses.

Non-structural measures such as land use zoning and subdivision regulations allow a community to regulate development within the flood plain. As participants in the National Flood Insurance Program, the City of Corsicana has adopted regulations that equal or exceed the minimal FEMA requirements of controlling the existing 100-year flood plain.

2. Construction Regulations

Construction regulations constitute an important means of preventing flood damage in a developing watershed. Some cities have building codes that contain general flood-protection provisions whereby the building inspector tries to route all building-permit applications in flood-prone areas through the City Engineer. The City Engineer should then carefully review each application to determine if the proposed building may be flooded and ensure that all buildings adjacent to a flood-hazard area are built with a ground elevation that is at least 1-foot above, and a finished floor elevation that is at least 2-feet above the fully urbanized 100-year flood elevation. The City should require that all finished floor elevations be specified on the final plat of each new subdivision to help ensure all new structures are built above 100-year flood plain elevations.

To limit erosion and downstream sediment, construction projects should be phased to limit the land area that is bare at any one time, and vegetation should be left undisturbed wherever possible. Other practices, such as proper placement of hay bales and silt fences, should also be required. Graded areas should be replanted as soon as possible, and mulches should be used during periods that are not suitable for

replanting.

3. Municipal Purchase or Private Donation of Land for Public Use

The municipal purchase or private donation of flood plain land is the most secure way for a city to control flood-prone areas. A flood plain could be used as dedicated open spaces, recreational areas, lakes, streets, or wildlife refuges. Greenbelt parks are an example of municipally owned land that serves as a drainage course and a popular recreational area. Municipal parks can often improve the quality of urban life and enhance property values.

The City may acquire land in the flood plain by three avenues: (1) dedication to municipal ownership on the final plat of a new subdivision; (2) purchase; or (3) gift. The land should be permanently reserved for flood conveyance, open spaces, and/or recreation.

4. <u>Informing the Public</u>

A study of flood-related deaths in the Dallas area indicates that most deaths occur at undersized bridges that are either overtopped or washed out by floodwaters (Reference 14). Using the hydrologic and hydraulic methods discussed in Chapter II, the frequency of flooding and the depth of water overtopping each roadway can be calculated. Computed future 100-year flood depths at existing roadway crossings in the Corsicana study area are presented in Chapter IV and are illustrated in the flood profiles that supplement this report.

An alternative to improving dangerous bridges and culverts is to install flood warning signs, barricades, or other systems to inform and alert motorists of hazardous crossings. The City should consider the need for a flood warning sign at all crossings that are overtopped by water during the 100-year and more frequent floods.

Flood warning systems can be passive or active. A passive system would be a warning sign, such as "BEWARE OF HIGH WATER", which would notify people using the bridge that flooding may occur. A gage with easy-to-read depth markings, measured in feet, should show motorists the height of water over the roadway. Guardrails can be installed to prevent vehicles from being washed off a dangerous road crossing, and can be used to identify the edge of the road surface where it may be obscured by floodwater.

Passive warning systems are feasible on lightly traveled residential streets where the motorists are familiar with the area, and are used at crossings with minor flooding. Installation of a passive warning system would be relatively inexpensive. Features

include warning signs, staff gages, and guardrails.

Active warning systems use a sensing device which monitor the water level in the channel and alerts motorists before the water is actually flowing over the roadway. The active system could be an automatic unfolding warning sign with flashing lights and sirens, or a relayed signal that would alert city workers to barricade the crossings. An active system could also be used to alert local residents of rising floodwaters and to evacuate prior to the flood. Active warning systems are necessary on heavily traveled thoroughfares or at crossings which are extremely hazardous.

The National Weather Service uses radar to locate severe and turbulent weather. The Weather Service declares a flash-flood watch when potentially severe storms are likely. A flash-flood warning is issued when a severe storm has developed and flooding is imminent. The warning is sent to weather wire services, counties and municipalities in the area, and to local Civil Defense authorities. Flood-prediction and early-warning systems usually give populated areas time to prepare flood defenses, evacuate flood-hazard areas, and close dangerous stream crossings.

A Corsicana flood-warning system could be used to alert city officials to barricade flood-prone streets along Post Oak Creek, South Fork of Post Oak Creek, Post Oak Tributary-3, Post Oak Tributary-5, Post Oak Tributary-6, Mesquite Branch, and Town Branch that become treacherous when overtopped. This system would not reduce or prevent property inundation or flood damages; however, it would increase public safety.

Many developed areas are flood prone, even if floods have not occurred within the memory of local residents. Flood-hazard maps delineating flood-prone areas, such as those included with this report, have been prepared by the Federal Emergency Management Agency (Reference 13) and by the U.S. Army Corps of Engineers (Reference 2). Dissemination of such flood-hazard information helps landowners to understand the need for compliance with flood plain zoning regulations. It also gives residents in dangerous flood-prone areas evidence of the need to consider relocating their families and businesses.

This report, by accurately updating and delineating the flood-prone areas, pinpoints dangerous flood-prone stream crossings, makes residents aware of local flood hazards, and helps the city and the public evaluate proposed plans to minimize existing and future flood problems.

5. Watershed Management

The reduction of runoff in a watershed lowers peak discharges and flood stages.

Soil conservation and the maintenance of vegetative ground cover retain water on the soil's surface, allowing infiltration into the soil. Urban development increases the percentage of impervious surfaces in an area, which generally increases the runoff potential. The preservation of trees, the maintenance of lawns, and the discharge of roof drains into vegetated areas all increase the infiltration of storm water into soils in developed areas.

Bare soils are easily eroded, resulting in transportation of sediment through water courses. The flood-carrying capacity of creeks and the storage capacity of flood-control reservoirs are greatly reduced by deposits of this sediment. To limit erosion, vegetation should be left undisturbed wherever possible. Graded areas should be replanted as soon as possible, and mulches should be used during periods that are not suitable for replanting. Some potential erosion problems along Post Oak Creek, South Fork of Post Oak Creek, Post Oak Tributary-3, Post Oak Tributary-5, Post Oak Tributary-6, Mesquite Branch, and Town Branch are discussed in Chapter IV.

6. Debris Removal

The accumulation of trees, brush, sediment, and other debris at bridges, culverts, pipe crossings, or other obstructions has several dangerous consequences. Obstructions to flow could cause higher flood stage elevations upstream of the crossing. In addition, masses of debris can break loose as flood flows increase, producing a destructive wall of water and debris that surges downstream. The force of water on the upstream side of a bridge plugged by debris may exceed the structural capacity of the bridge, causing it to fail. Prevention of debris obstructions can reduce flood damage and potential hazards.

The City should designate a maintenance division responsible for creek-debris removal. This department could inspect bridges quarterly, or upon request, and remove debris from bridge openings. It is not always economically practical for the city to take responsibility for debris removal on private property especially in Corsicana where a significant portion of the flood plain land is privately owned. The removal of debris is an essential flood-reduction technique, the use of which should be continued and increased.

Creeks should be inspected periodically to identify, cut, and remove dead trees or trees whose root systems have been undermined by erosion. An inspection program of this type should be aimed at the prevention of stream obstructions before they occur. Erosion-prevention measures should be instituted in areas where significant trees would be in danger of being uprooted by floodwaters. The inspection program should also identify areas in which siltation and debris could significantly decrease the flood-carrying capacity of the stream channel or the waterway under a bridge

7. Raising of Finished Floor Elevations

Another non-structural measure is the physical raising of structures affected by flooding. Such a measure requires the placement of the structure on a raised pier foundation, adjusting utilities and site aesthetics, and flood proofing utility connections. The types of structures ideally suited for raising are residential and light commercial structures with pier and beam foundations. Slab-on-grade structures are not normally feasible to raise. Federal studies (Reference 15) show that raising of structures is generally not cost-effective if the buildings are above the 10-year flood level. Within the study area, the majority of damages to structures appears to occur above a 10-year flood, therefore, this alternative would probably not be cost effective.

8. Greenbelt Alternatives

Generally, greenbelt/park alternatives are based on the results of an Environmental Inventory. Greenbelt alternatives can be developed as individual projects, or combined with several other alternatives. Greenbelt plans can be integrated with other flood plain management options. Some alternatives that could be considered include:

- o Establishment of Low Maintenance Greenbelts,
- o Hike and Bike Trails,
- o Equestrian Trails,
- o Active Recreation in Broad Flood Plain Areas.

D. STRUCTURAL MEASURES

Structural measures are actions taken to alter sections of a watercourse within a watershed to prevent flood losses. Structural measures include dams, levees, diversion, dikes, channels, pump stations, and pipe systems. The structural measures considered for this study are discussed below and in Chapter IV.

1. <u>Channel Improvements</u>

Channelization is the widening, deepening, and/or straightening of a stream to improve its conveyance. Channel side slopes may be grass-lined when the slopes are relatively flat (usually 3:1 or flatter), or gabion-lined when the slopes are steep. Channelization is unnecessary wherever an adequate natural drainage-way is available for flood conveyance. Maintenance is a requirement associated with channelization. Deposits of sediment may lead to vegetative growth, causing a reduction in flow capacity. Therefore, sediment should be periodically removed.

Grass-lined channels must be mowed periodically to maintain conveyance. Concrete-lined channels may also need to be cleaned periodically. Channel improvements were considered in conjunction with alternative flood improvements along each of the creeks in the study area. Specific channel improvement plans are discussed in Chapter IV in sections relating to the individual streams.

2. Bridge and Culvert Improvements

An analysis of existing bridges and culverts for replacement or removal should consider both upstream and downstream effects. Undersized bridges and culverts constrict the flow of flood waters and raise backwater elevations. This temporary storage may be beneficial in lowering downstream flood peaks but can endanger upstream property or make the road crossing dangerous. The replacement or removal of these bridges and culverts would reduce backwater flooding, but could increase downstream flood levels. Halff Associates recommends that the City of Corsicana implement a city-wide bridge rating program as outlined in Chapter V, Section F. Bridges should be rated according to the following criteria: structural safety; flood depths and velocities; hydraulic efficiency; and traffic. Alternatives for improving the flooded bridges and culverts along Post Oak Creek, South Fork of Post Oak Creek, Post Oak Tributary-3, Post Oak Tributary-5, Post Oak Tributary-6, Mesquite Branch, and Town Branch are presented in Chapter IV.

3. Storm water Detention Basins

A detention basin is a reservoir with an outlet device that is designed to release storm water at a slower rate than it's free flow rate in the stream. Detention basins have an emergency overflow that is utilized when the capacity of the outlet and the storage in the pond are exceeded. The outlet may act either by gravity or by pumping.

An on-site detention policy could help the City of Corsicana reduce the impact of urbanization on undeveloped portions of a watershed. Such a policy would require developers to provide temporary storage of storm water within their development or subdivision. This structural alternative proposes to require all future developments to construct on-site detention basins to prevent an increase of runoff beyond existing conditions. A thorough understanding of a detention basin is necessary in order to adopt a detention basin policy. The basic objective of such a detention policy would be to minimize the increase in peak discharges and runoff volumes resulting from increased impervious cover due to development.

As an example, this policy could require that small to medium sized detention basins would be constructed by the developer at the time of paving and drainage construction, and that the basins be designed to contain the 100-year frequency

flood and/or provide storm water discharges that are no greater than predevelopment conditions. The ownership and maintenance of the basins would be decided on a case by case basis during the planning and zoning stage of the development.

A variation of the on-site detention policy would be the retention of storm water by homeowners using underground cisterns on their lots. The water could be used by homeowners for irrigation of their lawns and gardens. Previous studies of the feasibility of this measure (Reference 16) have shown that the cost of a cistern retention system is too large to be offset by the reduced water use costs, and would require the city to offer incentives to cover the disparity.

Some of the factors that need to be addressed in connection with detention basins include: design criteria, ownership, safety, health, aesthetics, operation and maintenance, and legal issues. Brief discussion of these factors are listed below:

a. <u>Design</u> - The design frequency often depends on the capacity of the stream or storm sewer below the basin. The pond is presumed to detain enough storm water to reduce the outflow rate to the capacity of the outlet channel or pipe.

The design of dams, spillways, and structures is described in engineering literature and need not be repeated here. A commonly used reference is the <u>Design of Small Dams</u>, a publication of the U. S. Bureau of Reclamation (Reference 17).

- b. Ownership Ownership of the facility by a municipality or public agency is highly preferable. Detention basins are designed based on certain design criteria and zoning coverage that apply at the time of design changes and revisions may be desirable if the conditions change. These changes are more easily accomplished if the basin is publicly owned. Furthermore, accessibility for maintenance and sediment removal is minimized.
- c. <u>Safety</u> Safety of small detention basins is usually improved by fencing. Inlet structures should be screened to prevent a person from being swept into a storm sewer.

Detention basins may also breed mosquitoes that are a health hazard. Standard preventive measures are available for their control. Odors may also become a nuisance in retention ponds. Aeration by a fountain may reduce these problems.

Detention basins can often be made into multi-purpose projects that are both

useful and aesthetically pleasing. In a park setting, the basins can contain athletic facilities that will not be damaged by infrequent flooding. A retention basin that holds water can be an attractive park feature.

d. Operation and Maintenance - Operation and maintenance of detention basins may include pump operation and maintenance, trash clean up, water treatment, and sediment removal. Operation and maintenance requires that the basin have access for the type of equipment to be used, such as trucks for trash removal, front-end loaders or draglines for sediment removal, etc. Over the years a substantial amount of sediment can accumulate and reduce the flood control effectiveness of the basin. Removal of silt or a designed sediment allowance volume is important.

The cost of acquiring and operating detention basins should be weighed against the cost of providing adequate stream corridors. While the first cost of detention basins may seem to be extremely favorable if the developer is made to pay total cost, the long term operation and maintenance cost should be included in any analysis.

e. <u>Legal</u> - Legally one cloud on the horizon is that the EPA (Environmental Protection Agency) could require some treatment of urban run-off. If this occurs, then detention basins could conceivably retain the storm water long enough to provide the required treatment. A study, "Results of the Nationwide Urban Runoff Program" by U.S.E.P.A., December 1983, reported, "Detention basins are capable of providing very effective removal of pollutants in urban runoff" (Reference 18).

Detention basins may be advantageous to a landowner in meeting his legal requirements not to increase the flow of water onto the landowner below him.

The other legal problems are those involving safety, health, and nuisances which have already been discussed. Municipal laws of the state involved should be followed.

4. Regional Storm water Detention Basins

A relatively large regional storm water detention basin could be located and sized to retain a specified volume of storm water so that the peak of the runoff would be reduced.

Such regional basins will be large enough to require the city to construct and maintain the facilities. Basins could be incorporated into a community or regional

park site and function as a major recreational amenity to the park. The same design consideration and other issues that were previously described for on-site detention basins apply to regional detention basins as well.

5. Selective Reclamation

This alternative would include selective reclamation for development of the flood plain based on fully-developed conditions. This alternative would allow property owners to reclaim a portion of their flood plain land, while preserving the environmentally sensitive areas. Under this alternative, the future tax base of the city could increase as the land is reclaimed and added to the tax rolls.

6. Reclamation with Compensating Conveyance

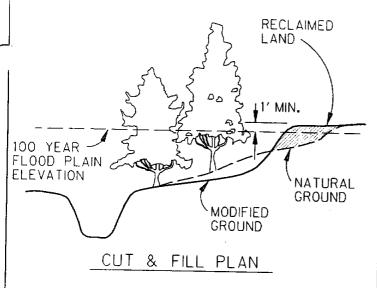
This alternative allows reclamation of a portion of the flood plain fringe by providing additional conveyance in the remaining flood plain. Reclamation would hopefully be limited to broad non-wooded flood plain land or in areas with minimal environmental assets. Possible methods of reclaiming flood plain fringe land, as shown in Figure III-1, are listed below:

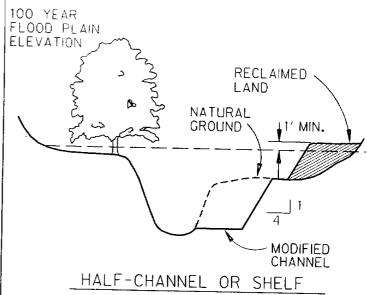
- Cut and fill which provides equal or greater flood conveyance for the area which was reclaimed,
 - Half channel or shelf,
 - Reduce roughness coefficient of stream by providing greater maintenance, i.e., <u>selective clearing</u>, remove heavy underbrush, monthly mowing,
 - · Overflow swales.

E. RELIEF MEASURES

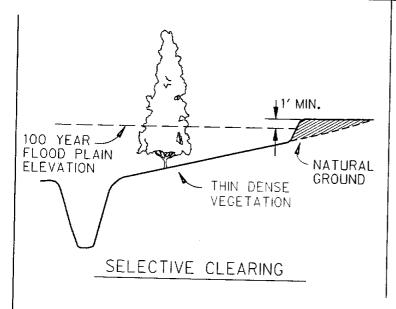
1. Public Disaster Action

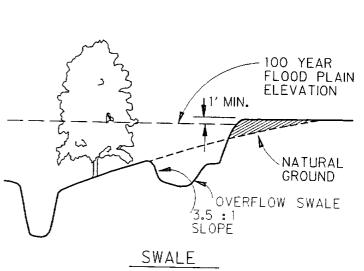
The City of Corsicana has procedures to be followed when flooding is anticipated at specific locations. City officials monitor areas that are likely to flood, and when flooding becomes imminent, personnel are dispatched to the areas to warn the residents, and to barricade dangerous roads. The potential need for public disaster action in the Corsicana study area could be greatly reduced by improvements recommended in Chapter IV.





- 1. RECLAMATION SHOULD MINIMIZE THE DESTRUCTION OF WOODED AREAS. 2. RECLAMATION SHOULD NOT SIGNIFICANTLY RAISE WATER SURFACE ELEVATION OR VFI OCITY.
- 3. FILL SLOPES SHOULD NOT BE STEEPER THAN 4 TO 1.
- 4. FILL AREAS SHOULD BE A MINIMUM OF ONE FOOT ABOVE THE 100-YEAR FLOOD ELEVATION.





- 1. PRESERVE SIGNIFICANT VEGETATION
- 2. THIN THE DENSE VEGETATION TO LOWER FLOOD ELEVATION THROUGH RECLAIMED SEGMENT. PRESERVE ALL TREES OF SIX INCHES OR GREATER DIAMETER.
- 3. OVERFLOW SWALE MAY BE EXCAVATED TO PROVIDE EQUAL CONVEYANCE PROVIDED IT IS NOT CONSTRUCTED IN WOODED AREAS.

HALFF ASSOC., INC.

FIGURE III-1
FLOOD DAMAGE
MITIGATION METHODS

2. Flood Insurance

Flood insurance helps to alleviate the cost to individuals of flood damages after flooding has occurred. However, flood insurance does not prevent damaging floods, which remain burdensome to insurance institutions, property owners, and local and Federal Governments. Purchase of more flood insurance for property owners in the study area will offer some relief from expensive flood damages. This alternative may be advantageous in areas too infrequently flooded to justify any other flood damage mitigation measure. The City of Corsicana is a participant in the National Flood Insurance Program (NFIP). Currently, there are 84 policies in force. As a condition to property owners purchasing flood insurance offered by the NFIP, participating communities have agreed to adopt and administer local flood plain management measures aimed at protecting lives and new construction from future flooding. The Federal Emergency Management Agency (FEMA), as part of this program, published Flood Insurance Rate Maps (FIRM) as part of the Corsicana Flood Insurance Study (Reference 13). In communities where a flood map has been published, Section 102 of the Flood Disaster Protection Act of 1973, as amended, requires the purchase of flood insurance as a condition of Federal or Federally-related financial assistance for acquisition or construction of buildings in special flood hazard areas, as shown on the FIRMs. The act also requires local Governments to furnish the following:

- · Copies of land use and control measures,
- · Maps identifying jurisdictional limits and flood plain areas,
- · Estimates of buildings and populations in flood plains,
- A local depository where flood-insurance and flood-hazard maps will be available for public inspection, and
- A summary of the community's history of flooding.

Communities currently participating in the NFIP that enforce more restrictive measures than the minimum criteria can reduce flood insurance rates for citizens within their jurisdiction by applying for the "Community Rating System" (CRS).

F. NORTH CENTRAL TEXAS COUNCIL OF GOVERNMENTS FLOOD PLAIN MANAGEMENT POLICIES

The North Central Texas Council of Governments (NCTCOG) has developed a program of cooperative watershed management policies for effective storm water management and stream corridor planning at the local government level. Eight broad policies have been developed in other NCTCOG watersheds such as Rowlett Creek (Reference 19), which addressed flood plain delineation and management, greenbelt planning, and design standards.

The City of Corsicana should consider adopting some or all of these policies, with modifications to reflect the results of this study. The City staff should determine if the policies should be adopted as presented or modified prior to presentation to the City Council for consideration.

The eight North Central Texas Council of Government policies and supporting justification as developed are presented as follows.

Policy No. 1

BFE: 100-Year Flood Plain - Fully Developed Watershed Land Use. The base flood elevation (BFE) and flood plain used for design and planning should be evaluated upon total storm water discharge quantities that will, through future urbanization, be generated from a fully developed watershed.

Basing flood plain maps and discharge quantities on fully developed land use conditions is required to assure that buildings, bridges, and reclaimed flood plain areas are safe and can adequately accommodate anticipated hydrologic changes created by a maturing watershed. Developing a storm water discharge computer model for fully developed watershed conditions will help identify needed capital improvements or other special conditions that warrant preventative actions.

Policy No. 2*

Allow No Rise in Base Flood Elevation. Reclamation of the flood plain should be permitted only if it can be demonstrated that there will be no rise in the base flood elevation.

The FEMA "floodway" concept contained in the National Flood Insurance Program allows up to a one foot rise in flood elevations assuming current development conditions only. Reclamation which allows a rise in flood elevation could predictably create adverse impacts either upstream or downstream. Therefore, it is strongly recommended that no rise in base flood elevation be allowed. Note, if the No Rise policy is adopted, coordination with TxDOT is recommended when evaluating bridge improvements.

Policy No. 3

Velocity Controls. Velocity controls should be established which specify maximum allowable flow rates for specific channel, bed and bank treatments.

Uncontrolled flow velocities which are excessive could cause damage to the channel, bank, water body and the downstream reservoir. Erosion could also cause severe damage to structures (e.g. bridges) or even cause channel modifications which result in additional downstream flooding.

Policy No. 4

Minimize Alteration or Channelization of Post Oak Creek and its Major Tributaries (except where required for safety and public welfare). The drainage-way of the creek and its major tributaries should be left in a natural state to control erosive velocities, prevent excessive downstream discharges and preserve the natural effect of the stream.

Historic efforts in managing storm flow consisted of simple routing of storm water through gutters and channels with the simple objective of removing the storm water as quickly as possible. It has long been recognized that simply bypassing storm flows really shifts the location of the problem and very often aggravates the problem by compounding downstream flows. The end result is often an increase in total flow, peak flow rate and stream velocity.

A more effective approach to storm water management for Post Oak Creek, Mesquite Creek, and Tributaries is to maintain as nearly as possible the natural runoff flow characteristics.

Policy No. 5

<u>Seek Public Ownership of Remaining Flood</u> Plain. Any flood plain remaining after final reclamation should be deeded or dedicated to the city to prevent further encroachment and assure proper drainage maintenance.

As reclamation proceeds, the remaining flood plain land provides critical drainage during major storm events. In a functional sense, the flood plain remaining after reclamation has evolved into the classical definition of a floodway. In other words, the flood plain will have been reduced to the channel and adjacent land area required to provide passage of the base flood.

Policy No. 6

Buffer Zones. Where practical, the City of Corsicana should require parallel streets, greenbelts, etc. along the stream corridor to assure access and to create buffer zones between the flood plain and development.

A buffer zone should function as a clear transition between natural areas which may be subject to flooding and areas of other land uses. Buffer zones should visually define the flood plain and be available to provide additional water conveyance during major storm events

Policy No. 7

Linear Park. Cooperation in development of a contiguous linear park along the Post Oak Creek stream corridor should be actively pursued.

The use of the natural stream corridor for drainage requirements can be combined with other valuable non-competing uses such as public recreation. By combining these uses with drainage and flood protection requirements, the community can maximize the total beneficial use of the flood plain and adjacent areas.

Policy No. 8

Pursue Discussion of Specific Development Standards. Further evaluation and discussion of specific development standards such as detention policies and minimum floor slab elevations should be jointly pursued to insure adequate water quality protection and flood water control.

Several specific flood plain management rules and requirements have been identified as needing further attention. For example, Halff Associates has recommended requiring finished floor elevations be at least a minimum of two feet above the "base flood" elevation. Local implementation of Policy No. 3 will result in development standards which specify maximum flow velocities. Also, Corsicana will need to establish minimum requirements for acceptable drainage easements. Drainage easements will require sufficient room for access of necessary maintenance equipment and/or sufficient suitable land to construct and maintain existing and future walking and bicycling paths.

IV. STUDY RESULTS

A. GENERAL

Halff Associates updated the previous Corps of Engineers' hydrologic data in the Post Oak watershed basin, to develop the drainage area map illustrated on Figure IV-1. (A detailed map is provided in Appendix D.) This detailed drainage area map includes approximately 30 sub-basins.

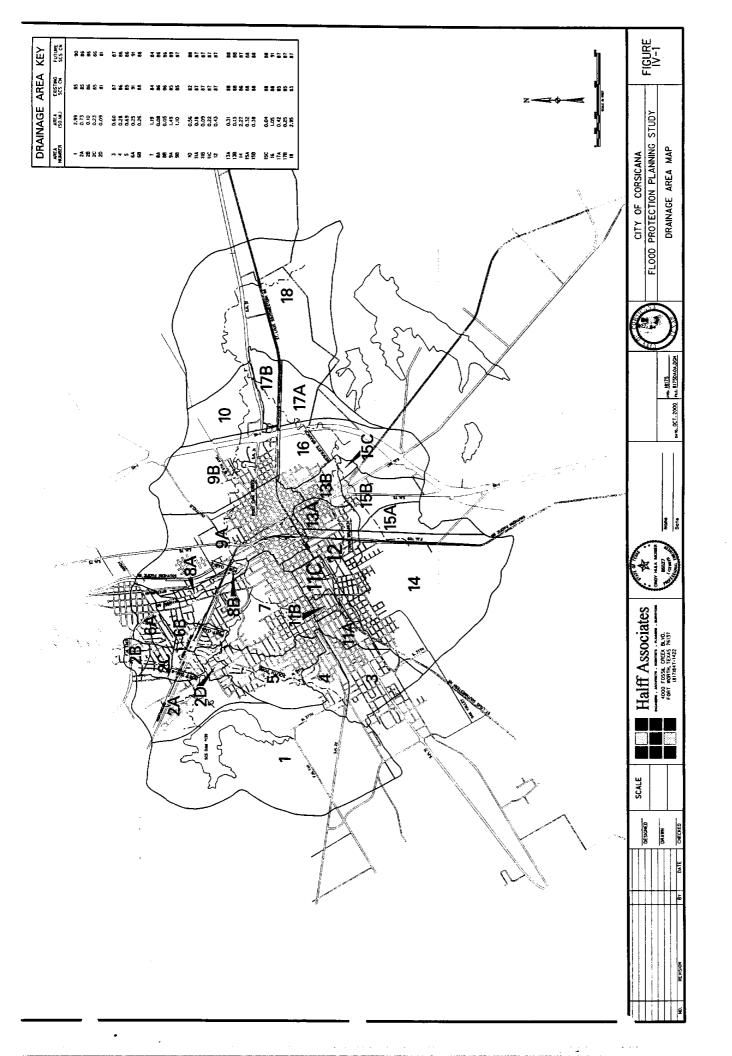
Table IV-1 is a list of computed drainage areas and estimated SCS Curve Numbers (for existing and ultimate land use conditions) for each sub-watershed basin in the study area.

This study includes flood information for the following land use and flood plain conditions:

- o Flood discharges based on <u>existing land use</u> conditions and <u>existing channels and bridges</u>. Note, this data could be very useful if the city of Corsicana decides to submit a city-wide update of the current FEMA Flood Insurance Rate Maps.
- o Flood discharges based on <u>future land use</u> conditions (fully urbanized watershed) and <u>existing channels and bridges</u>. For this study, this condition is referred to as Baseline Conditions.
- o <u>100-Year flood plain delineation and flood profiles</u> for existing channels and bridges with flood discharges based on future land use conditions (fully urbanized watershed). (See Appendix D)
- O <u>Selective channel and bridge improvements</u> and accompanying flood profiles with flood discharges based on future land use conditions (fully urbanized watershed) and existing channels/.

TABLE IV-1
Post Oak Watershed
Drainage Areas and Estimated SCS Curve Numbers

, AREÁ NO.	ARÉA (sq. mi.)	EXISTING	UEFIMATE
1		SCS CN = 1	∰. scscn : E
	2.99	85	90
2A	0.73	85	86
2B	0.10	86	86
2C	0.23	85	86
2D	0.09	81	81
3	0.60	87	87
4	0.28	86	86
5	0.69	85	86
6A	0.25	91	91
6B	0.26	88	88
7	1.19	84	84
8A	0.08	86	86
8B	0.05	86	86
9A	1.49	85	89
9B	1.10	85	87
10	0.56	82	88
11A	0.18	87	87
11B · · · ·	0.09	87	87
11C	0.22	87	87
12	0.43	87	87
13 A	0.31	88	88
13B	0.13	88	88
14	2.27	86	87
15A	0.32	88	88
15B	0.38	88	88
15C	0.04	88	88
16	1.05	88	91
17A	0.42	85	87
17B	0.25	85	87
18	2.95	83	87
••	4.73	0.5	8/



B. POST OAK CREEK

1. Description of Watershed

Post Oak Creek originates a few miles west of Corsicana, and flows north to Soil Conservation Dam 139. It then flows in an easterly direction through the northern portion of the City. It then flows southerly until it reaches its confluence with Chambers Creek about seven miles east of the City.

Existing land uses in the Post Oak Creek watershed study area consist of approximately 70% crops and pasture; 15% residential; 10% business/commercial/industrial areas; 3% parks and open space; and scattered public/semi-public areas (i.e. schools, churches, etc.). Future development will consist of approximately 50% residential; 40% business/commercial/industrial; and scattered parks, public/semi-public areas.

2. Hydrologic Study Results

Halff Associates prepared detailed HMS hydrologic computer models of the watershed to analyze existing land use conditions and projected ultimate land use conditions. Ultimate land use conditions were analyzed with channel flood routing data based on existing channels and bridges. Peak flood discharges calculated for this study include the 5-, 10-, 25-, 50-, 100-, and 500-year flood frequencies. Tables IV-2 and IV-3 contain peak flood discharge information at key locations along Post Oak Creek within the study area. Existing peak flood discharges based on existing land use and existing channel/bridge conditions are presented in Table IV-2. Future peak discharge information based on future land use and existing channel/bridge conditions are presented in Table IV-3.

TABLE IV-3 FUTURE PEAK FLOOD DISCHARGES (cfs) (With Existing Channels and Bridges) Post Oak Creek

	1.0			omputed P	eak Discharg	e (cfs)	
Location The Control of the Control	Area (m)	5-VR	IO-YR	25-YR	50 YR	100-YR	500-YI
Just Downstream Dam Site 139	2.99	70	70	80	80	110	480
At Bowie Drive	3.72	1100	1300	1600	1800	2000	2400
At Confluence w/ PO-6	4.05	1500	1800	2000	2400	2500	3300
At Confluence w/ South Fork	5.71	2800	3400	4000	4600	5100	6200
At Confluence w/ PO-5	6.22	3300	3900	4700	5300	5900	7100
At N Beaton Street	7.41	3600	4300	5200	6000	6700	8100
At Confluence w/ PO-3	7.54	3700	4400	5400	6100	6800	8300
At N Burnert Street	9.03	5000	5800	6700	7600	8500	10400
At Interstate 45	10.13	5000	6000	6900	7700	8600	10400
At Confluence w/ Mesquite Creek	16.78	8000	9600	11100	12600	14500	18700

Discharges were rounded to the nearest 100.

A comparison of existing conditions 100-year peak flood discharges computed for this study and the peak discharges published in the 1991 COE Post Oak Creek Reconnaissance Report (Reference 2) and the 1981 Corsicana Flood Insurance Rate Study (Reference 13) are presented in Table IV-4. The difference between existing development discharges and FEMA published discharges can be attributed to increased urbanization and level of detail. A comparison of future conditions 100year peak flood discharges computed for this study and the peak discharges published in the 1978 COE Detailed Project Report (Reference 21) are presented in Table IV-5. The difference between future development discharges and the COE published discharges can be attributed to level of detail such as detailed routing throughout model for this study. Differences between existing discharges and ultimate discharges is attributed to urbanization of the watershed as outlined above.

^{2.} Peak discharges are based on future land use watershed with existing channels and culverts.

COMPARISON OF EXISTING CONDITIONS COMPUTED PEAK FLOOD DISCHARGES Post Oak Creek TABLE IV-4

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	ALIENTA ALIENT	400	2000	2500	0009	0069	7800	8000	0066	0066	18000	
	WASSI	ı	1600	1	5400	1	7600	1		1	15200	
H (O)		610	1700		5500	,	0008	,	1	9200	ı	
	TILLING.	08	1700	2300	4900	2600	6400	0099	8000	8000	13900	
		ı	1450	1	4800	1	0099		1	1	13400]
(GB) (CONTR		170	1500	1	4900	•	0069	1	-	7900	ı	
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		1	ŀ	ı	I	1	ı	1	ı	1	I	
	12 (3)	95	1300	1	4300	-	2900		1	0089	ı	
		08	1300	1800	3800	4400	2000	5100	9300	9209	10700	
	SW COLUMN	ŀ	1100	1	3500	1	4550	1	ı	t	0006	
		06	1100	1	3600	ı	4800		1	5100	1	
	11,23	70	1100	1500	3200	3700	4100	4200	5400	2200	9100	
	10.00	ı	t	ł	ı	,			:	1	t	
E	*(C0) #35 \$80 (C)	06	006	1	3000	-	3800	ı	ı	3900	ı	
		0/	006	1200	2700	3100	3400	3450	4400	4600	7600	
		2.99	3.72	4.05	5.71	6.22	7.41	7.54	9.03	10.13	16.78] -
ing the state of t		Just Downstream Dam Site 139	At Bowie Drive	At Confluence w/ PO-6	At Confluence w/ South Fork	At Confluence w/ PO-5	At N Beaton Street	At Confluence w/ PO-3	At N Burnert Street	At Interstate 45	At Confluence w/ Mesquite Creek	

Discharges were rounded to the nearest 100.

2. Peak discharges are based on an existing land use watershed with existing channels and culverts.

3. Corps Discharge from 1991 COE Reconnaissance Report

4. FEMA Flood Insurance Study for the Town of Corsicana, Tx, Effective Date 1981.

COMPARISON OF FUTURE CONDITIONS COMPUTED PEAK FLOOD DISCHARGES Post Oak Creek TABLE IV-5

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						;; };	¥.33.	S)		A TOTAL SERVICE	7.10	10.4-10.5	TO THE REAL PROPERTY.
			3						T.HIV		Courted	LIE BILL	Corps
Just Downstream Dam Site 139	2.99	70	85	07	85	80	96	80	06	110	06	480	-
1	3.72	1100	1000	1300	1200	1600	1400	1800	1600	2000	1800	2400	
At Confluence w/ PO-6	4.05	1500	ı	1800	ŀ	2000	ı	2400	ı	2500	ı	3300	1
*	5.71	2800	3200	3400	3800	4000	4500	4600	\$100	5100	5700	9700	1
At Confluence w/ PO-5	6.22	3300	ı	3900	ı	4700	1	5300	ı	2900	1	7100	1
	7.41	3600	3900	4300	4800	\$200	2900	0009	0069	9029	7900	8100	
At Confluence w/ PO-3	7.54	3700	,	4400	ı	2400		9019	ŀ	0089	ı	8300	1
†	9.03	2000		2800	1	0029	1	7600		8500		10400	
╁	10.13	2000	3800	0009	4900	0069	9069	7700	7500	0098	8700	10400	1
/#	16.78	8000	7200	0096	9300	11100	11700	12600	13700	14500	15600	18700	ı
1	1 Discharges more and the the	001											

Discharges were rounded to the nearest 100.
 Peak discharges are based on an existing land use watershed with existing channels and culverts.

3. Corps Discharge from 1978 COE Detailed Project Report.

3. Hydraulic Study Results

Post Oak Creek is approximately 5.4 miles in stream length through the City of Corsicana study area. The average channel slope through the study area is about 0.20%. The channel is well defined with depths ranging from about 5 feet to 18 feet. The entire length of stream through the study area consists of a natural earthen channel. Portions of existing flood plains are generally undeveloped while certain areas consist of residential and commercial developments. The Post Oak Creek future fully urbanized 100-year flood plain delineation prepared for this report includes approximately 450 acres of land within the Corsicana City limits. One hundred and fifty-four structures are located within this 100-year flood plain delineation. Seventy-eight of these structures have estimated finish floors below the 100-year flood plain as indicated in Table IV-6. The expected annual damage for these structures is \$74,400.

TABLE IV-6
BASELINE CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES
Post Oak Creek

Flood Even	Stricture in the	t Zones	Expected Damages for
	Contribution per i	Total for Event	Event :
5-yr	8	8	\$66,000
10-уг	8	16	\$147,000
25-уг	26	42	\$332,000
50-yr	18	60	\$614,000
100-уг	18	78	\$880,000
500-yr	44	122	\$1,900,000

There are fourteen bridges along Post Oak Creek. Pertinent data for each bridge can be found in Table IV-7. The computed future 100-year flood overtops the existing roadway at ten of the fourteen bridge locations along Post Oak Creek. Graphical representation of these and other potential flooding areas along Post Oak Creek are presented on the flood plain maps and flood profiles that supplement this report. (See Appendix D.)

Existing channel velocities are generally non-erosive, less than 6.0 feet per second. Channel velocities greater than 8 feet per second were computed at bridge crossings at Burnert Road (stream stations 264+43 to 267+74) and at Chatfield Road (stream stations 285+95 to 287+29). Although erosion continues to occur along Post Oak

Creek, there were no identified instances of high potential loss of private property or areas classified as severe erosion problems.

TABLE IV-7 BRIDGE DATA Post Oak Creek

Identification	Upstream Channel X-Section	Upstream Flowline (1)	Low Cliord 7(1)	Min Top of Road (t)	Q ₁₀₆ (cfs) (2)	100-Yr WSEL (3)	Description
IH-45 North Bound Frontage Road	209+40	360.09	375.3	381.3	8600	378.82	Concrete Bridge with 2 Piers
IH-45 South Bound Frontage Road	210+25	362.55	376.8	383.44	8600	380.52	Concrete Bridge with 2 Piers
E. 5th Avenue	240+95	381.22	382	387.17	8600	382.91	Concrete Bridge with 2 Piers
Burnert Street	268+00	372.97	379.97	381.26	8500	388.07	5-84" RCP
N. 3 rd Street	286+62	376.5	388.88	394.33	8500	391.33	Concrete Bridge with 1 Pier
N. 7th Street	295+80	380.8	392.7	395.7	6800	395.06	Concrete Bridge with 3 Piers
Southern Pacific RR	303+50	385.9	394.08	398.08	6800	396.50	Concrete Bridge with 3 Piers
N. 10 th Street	313+79	384.7	390.53	393.53	6800	397.26	Concrete Bridge with 2 Piers
Beaton Street	31 6+9 9	384.7	396.65	402.32	6700	398.26	Concrete Bridge with 2 Piers
N. Main Street	322+69	386.4	394.2	397.2	6700	399.13	Concrete Bridge with 2 Piers
N. 13 th Street	330+49	389	399.07	402.07	6700	401.28	Concrete Bridge with 2 Piers
Oaklawn Drive	350+99	388.53	396.53	397.61	5900	403.28	1-20'x8' CBC
Dobbins Road	393+04	396.2	405.2	407.16	2500	410.92	1-12'x9' CBC
Bowie Drive	409+29	403.11	407.11	410.9	2000	412.61	4-48" RCP

Approximate Elevations (NGVD).

¹⁰⁰⁻Year Discharge based on future development with existing channels and bridges/culverts (Baseline Conditions).

100-Year flood elevation based on existing channels and culverts.

4. **Improvements**

Halff Associates utilized the existing channel condition Post Oak Creek HEC-RAS hydraulic computer model to prepare conceptual bridge and channel designs for future roadway improvements and erosion protection. The following is a brief description of the proposed conceptual improvements for Post Oak Creek:

Reach 1 - Downstream of N. Burnert Street to W. 7th Street (stream stations 249+40 to

- Five 12'x7' concrete box culverts at N. Burnert Street.
- 3700 LF 50' bottom width 3:1 grass-lined channel from 1800' downstream of N. Burnert Street to E. Chatfield Road (stream stations 249+40 to 286+45).
- Bridge expansion at Chatfield Road.
- 875 LF 50' shelf channel between E. Chatfield Road and W. 7th Street (stream stations 286+79 to 295+53). Figure III-1 illustrates a typical proposed "shelf" channel.

Estimated Probable Cost: \$3,592,400 **Average Annual Cost:** \$284,400 Estimated Annual Benefit: \$5,600 Benefit/Cost Ratio: 0.02

The estimated probable cost of these proposed conceptual improvements for Reach 1 is \$3,592,400. Proposed improvements through Reach 1, from N. Burnert Street to W. 7th Street, will remove two (2) structures from the 100-year flood plain delineation as shown in Table IV-8. Reach 1 proposed conceptual solutions reduce the expected annual damages by about \$5,600.

TABLE IV-8 IMPROVED CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES REACH 1 (N. BURNERT STREET TO W. 7TH STREET) Post Oak Creek

	图 新知识 建氯	recinción hacaz	ine	Service .
Hood Even	Printper Lyen: without the Limprovements	Total per Event with Improvements		Expected Damage (or Event
5-yr	8	7	1	\$56,000
10-yr	16	14	2	\$130,000
25-уг	42	40	2	\$311,000
50-ут	60	58	2	\$576,000
100-ут	78	76	2	\$838,000
500-уг	122	116	6	\$1,807,000

Reach 2 - Downstream of N. Beaton Street to Upstream of N. 13th Street (stream stations 314+92 to 334+24)

- 840 LF 50' shelf channel from N. Beaton Street to just upstream of N. Main Street (stream stations 314+92 to 323+35). Figure III-1 illustrates a typical proposed "shelf" channel.
- Bridge expansion/ Raise N. Main St.
- 640 LF 100' shelf channel from just upstream of N. Main Street to N. 13th Street (stream stations 323+35 to 329+76). Figure III-1 illustrates a typical proposed "shelf" channel.
- Purchase 4 structures between N. Main Street and N. 13th Street in order to construct above 640 LF of improvements.
- 450 LF 50' shelf channel from N. 13th Street to just upstream of N. 13th Street (stream stations 329+76 to 334+24). Figure III-1 illustrates a typical proposed "shelf" channel.

Estimated Probable Cost: \$3,417,300 **Average Annual Cost:** \$271,600 Estimated Annual Benefit: \$14,000 Benefit/Cost Ratio: 0.05

The estimated probable cost of these proposed conceptual improvements for Reach 2 is \$3,417,300. Fourteen (14) structures are removed from the 100-year flood plain delineation as indicated in Table IV-9 by the proposed improvements through Reach 2, from N. Beaton Street to N. 13th Street. Reach 2 proposed conceptual solutions reduce the expected annual damage by \$14,000.

TABLE IV-9 IMPROVED CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES REACH 2 (N. BEATON STREET TO N. 13TH STREET) Post Oak Creek

	Asset Street	tructures in Pood Za	ne -	
Flood Event	Tural per Event without Improvements			Expected Damage For Event:
5-yr	8	5	3	\$ 54,000
10-уг	16	13	3	\$125,000
25-yr	42	29	13	\$271,000
50-yr	60	47	13	\$503,000
100-уг	78	64	14	\$726,.000
500-yr	122	116	6	\$1,634,000

Reach 3 - N. 13th Street to 1690' upstream of Oaklawn Drive (stream stations

3375 LF 30' bottom width 3:1 grass-lined channel from just upstream of N. 13th Street to 1690' upstream of Oaklawn Drive (stream stations 334+24 to

Estimated Probable Cost: \$756,200 **Average Annual Cost:** \$60,100 Estimated Annual Benefit: \$2,700 Benefit/Cost Ratio: 0.05

The estimated probable cost of these proposed conceptual improvements for Reach 3 is \$756,200. The proposed improvements through Reach 3, from N. 13th Street to upstream of Oaklawn Drive remove seven (7) structures from the 100-year flood plain delineation as illustrated in Table IV-10. The expected annual damage is reduced by \$2,700 by the Reach 3 proposed conceptual solutions.

TABLE IV-10 IMPROVED CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES REACH 3 (N. 13TH STREET TO OAKLAWN DRIVE) Post Oak Creek

	See See Control of the Control of th	tructures in Flood Z	one .	
Flood Event	Total per Event: withou: Improvements	For with		Expected Damages for Event
5-yr	8	8	0	\$66,000
10-yr	16	16	0	\$147,000
25-уг	42	40	2	\$296,000
50-уг	60	55	5	\$527,000
100-yr	78	71	7	\$756.000
500-yr	122	107	15	\$1,635,000

Reach 4 - 1690' upstream of Oaklawn Drive to Dobbins Road (stream stations 368+00 to392+85)

- 2485 LF 30' bottom width 3:1 grass-lined channel from just 1690' upstream of Oaklawn Drive to Dobbins Road (stream stations 368+00 to 392+85).
- Three 12'x9' concrete box culverts at Dobbins Road.

Estimated Probable Cost: \$980,800 **Average Annual Cost:** \$77,900 Estimated Annual Benefit: \$38,400

Benefit/Cost Ratio:

0.5

The estimated probable cost of these proposed conceptual improvements for Reach 4 is \$980,800. Nineteen (19) structures are removed from the 100-year flood plain delineation by the proposed improvements through Reach 4, from Oaklawn Drive to Dobbins Road, as shown in Table IV-11. The Reach 4 proposed conceptual solutions reduce the expected annual damage by \$38,400.

TABLE IV-11 IMPROVED CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES REACH 4 (OAKLAWN DRIVE TO DOBBINS ROAD) Post Oak Creek

		tructures in Mood Z	one.	
Rlood Event	Total per Event withour Improvements		Total takes out of a Flood Zone per	Expected Damages for Event
5-yr	8	6	2	\$22,000
10-yr	16	11	5	\$22,000
25-yr	42	34	8	\$170,000
50-yr	60	46	14	\$296,000
100-yr	78	59	19	\$420,000
00-yr	122	83	39	\$1,084,000

The total estimated probable cost of all (Reaches 1-4) proposed conceptual improvements for Post Oak Creek is \$8,683,700. The estimated annual cost for all (Reaches 1-4) improvements is \$690,100. The resulting improved flowlines and water surface elevations are displayed on the flood profiles that supplement this report (See Appendix D). HEC-RAS summary printouts for the proposed recommendations may be found in Appendix E.

The aforementioned estimates for removal of structures were determined by each individual reach investigated independently. Therefore, overlap exists among the number of structures removed (i.e. the improvements from N. 13th Street to upstream of Oaklawn Drive improve conditions upstream and remove structures that are also removed by the improvements from upstream of Oaklawn Drive to Dobbins Road). However, more structures are removed by the combined effect of implementing all improvements (Reaches 1-4). In this case, the sum of structures removed by the implementation of all improvements (Reaches 1-4) is less than the sum of that of the individual improvements by reach due to the overlap. With all improvements in place (Reaches 1-4), thirty-nine (39) structures are removed from the 100-year flood plain delineation as illustrated in Table IV-12. aforementioned estimates of reduction of expected annual damage determined for

each improvement were also investigated independently. When all the improvements (Reaches 1-4) are implemented, their combined effect lowers the water surface elevation more than their individual effect. Therefore, with all improvements (Reaches 1-4) in place, the reduction in expected annual damages is greater than the sum of that of the individual improvements by reach. With all improvements (Reaches 1-4) in place, the proposed conceptual solutions reduce the expected annual damage by \$61,400. The benefit to cost ratio is 0.09.

TABLE IV-12
IMPROVED CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES
ALL IMPROVEMENTS (REACHES 1-4)

Post Oak Creek

		structures in Flood Zo	ne	
Flood Event	Total per Event Without Improvements	Total per Event with Emprovements	Total laker our of Flood Zone per Teen	Expected Damages for Event
5-ут	8	0	8	\$0
10-уг	16	3	13	\$2,000
25-уг	42	15	27	\$59,000
50-yr	60	31	29	\$158,000
100-ут	78	39	39	\$205,000
500-yr	122	62	60	\$564000

C. SOUTH FORK OF POST OAK CREEK

1. Description of Watershed

The South Fork of Post Oak Creek watershed study area lies in the west side of Corsicana. South Fork originates north of State Highway 31 and flows northerly until it reaches its confluence with Post Oak Creek where the total drainage area is approximately 1.57 square miles (1,004 acres).

Existing land uses in the South Fork of Post Oak Creek watershed study area consist of approximately 70% residential; 20% crops and pasture; 5% business/commercial/industrial areas; and scattered parks, public/semi-public areas (i.e. schools, churches, etc.). Future development will consist of approximately 90% residential; 5% business/commercial/industrial; and scattered parks, public/semi-public areas.

2. Hydrologic Study Results

Halff Associates prepared detailed HMS hydrologic computer models of the watershed to analyze existing and projected ultimate land use conditions. Ultimate land use conditions were analyzed with channel flood routing data based on existing channels and bridges. Peak flood discharges calculated for this study include the 5-, 10-, 25-, 50-, 100-, and 500-year flood frequencies. Tables IV-13 and IV-14 contain peak flood discharge information at key locations along South Fork. Existing peak flood discharges based on existing land use and existing channel/bridge conditions are presented in Table IV-13. Future peak discharge information based on future land use and existing channel/bridge conditions are presented in Table IV-14.

TABLE IV-13
EXISTING CONDITIONS PEAK FLOOD DISCHARGES (cfs)
South Fork Creek

A Commence of the Commence of	A PART	\$ 5 KR	(C) II	125915	50.551	100 Yes	9500 YR
At Pond just upstream 29th Street	(sm): 3						4.4
	.88	1220	1450	1735	1970	2200	2650
At Confluence w/ Post Oak Creek	1.57	1530	1830	2190	2500	2790	3390

TABLE IV-14 FUTURE PEAK FLOOD DISCHARGES (cfs) (With Existing Channels and Bridges) South Fork Creek

		puted Peak					
Little (in the little of the l		955YR	e HOYRK	2255YII 2555YII	242 VR 2	ongevie	500-Y
t Confluence w/ Post Oak Creek	.88	1220	1450	1740	1970	2200	2650
t Chicago Rock Island RR Discharges were rounded to the nearest 1	1.57	1540	1850	2210	2510	2800	3400

3. Hydraulic Study Results

South Fork of Post Oak Creek is approximately 1.6 miles in stream length through the City of Corsicana of which 1.4 miles was studied. The average channel slope through the study area is about 0.5%. The channel is well defined with depths ranging from 3 feet to 12 feet. The entire length of stream through the study area consists of an earthen channel with some concrete occurring at bridges. An existing 3 acre pond is located upstream of N. 29th Street.

The South Fork of Post Oak Creek future fully urbanized 100-year flood plain delineation prepared for this report includes approximately 44 acres of land within the Corsicana City limits. Twenty-seven structures are located within this 100-year flood plain delineation. Sixteen of these structures have estimated finish floors below the 100-year flood plain as indicated in Table IV-15. The South Fork expected annual damages for these structures is \$104,900.

TABLE IV-15
BASELINE CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES
South Fork Creek

Plood bye	Strictures	in Flood Zone	: Expected Damages to
	Contribution per	Total for Events.	Event Services
5-ут	5	5	\$159,000
10-yr	6	11	\$346,000
25-yr	2	13	\$539,000
50-yr	2	15	\$692,000
100-yr	1	16	\$826,000
500-yr	6	22	\$1,150,000

In the City of Corsicana, there are six bridges along South Fork of Post Oak Creek. Pertinent data for each bridge can be found in Table IV-16. The computed future 100-year flood will overtop the existing roadway at all six of these bridge locations. Graphical representation of these and other potential flooding areas along South Fork of Post Oak Creek are presented on the flood plain maps and flood profiles that supplement this report. (See Appendix D.)

TABLE IV-16 BRIDGE DATA South Fork Creek

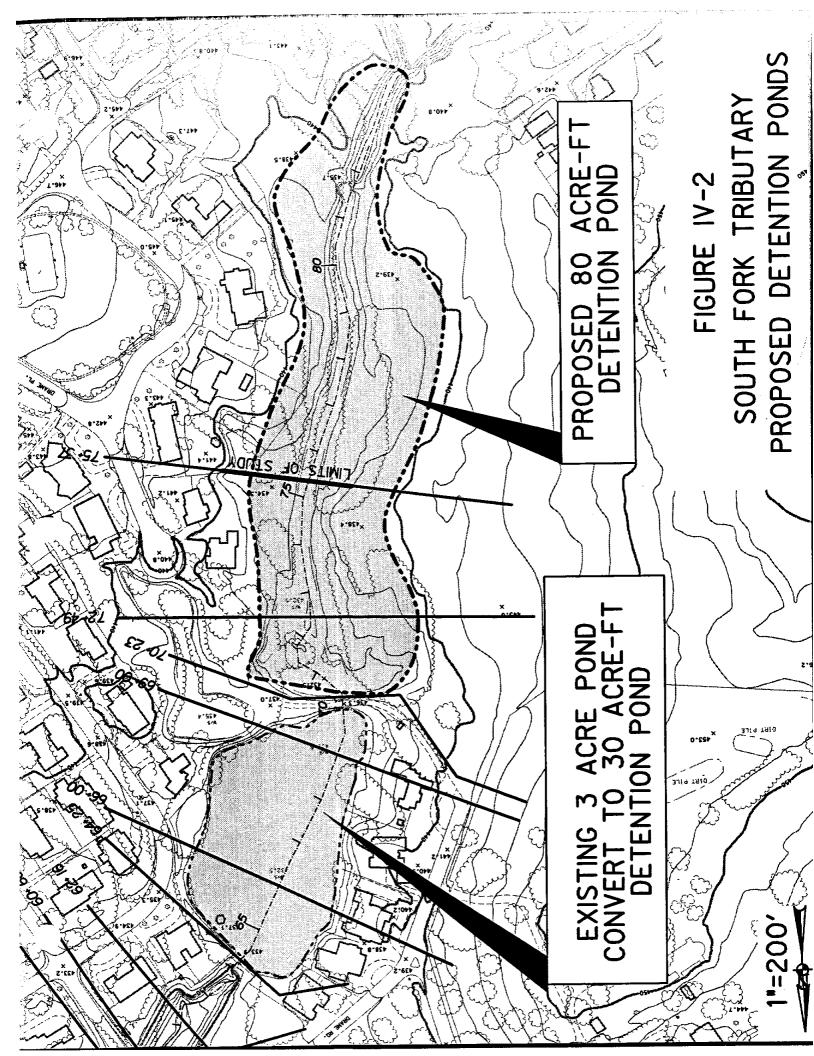
Bridge Identification	Upstream Channel X-Section	Epstream. Flowline. (1)	Law Chord (1)	Min.Top of Road (1)	Q ₁₆₀ (cfs) (2)	100 Yr WSEL (3)	Description
Mimosa Drive	2+25	397.81	402.31	404.04	2800	409.06	3-7'x4.5' CBC
Fairfax Drive	5+57	399.68	404.18	404.94	2800	409.48	3-7'x4.5' CBC
N. Bowie Drive	10+20	403.62	408.15	409.49	2800	413.70	1-20'x4.5' CBC
Paloma Street	20+60	405.15	413.15	414.16	2800	417.95	1-20'x8' CBC
N. 26th Street	33+50	407.70	416.70	419.62	2200	421.37	3-10'x9' Ellipse Culvert
N. 29th Street	60+50	420.60	428.60	430.25	2200	430.90	5-96" CMP

Approximate Elevations (NGVD).

100-Year Discharge based on future development with existing channels and bidges/culverts (Baseline Conditions).

100-Year flood elevation based on existing channels and culverts.

South Fork of Post Oak Creek existing channel velocities are generally non-erosive, less than 6.0 feet per second. Channel velocities greater than 8 feet per second were computed downstream of N. Bowie Drive (stream stations 6+50 to 10+04). Two homes are close to the channel banks in this high velocity area.



4. Improvements

Halff Associates utilized the existing channel condition South Fork HEC-RAS hydraulic computer model to prepare conceptual bridge and channel designs for future roadway improvements and erosion control. See Chapter V for guidance on erosion control. The following is a brief description of the proposed conceptual improvements for the South Fork of Post Oak Creek:

- Five 10'x6' concrete box culverts at Bowie Drive.
- 1000 LF 10' bottom width 3:1 grass-lined channel from Bowie Drive to Paloma Street (stream stations 10+36 to 20+41).
- Three- 10'x8' concrete box culverts at Paloma Street.
- 1255 LF 20' bottom width 3:1 grass-lined channel from Paloma Street to N. 26th Street (stream stations 20+41 to 33+34).
- Turn existing 3 acre pond upstream N. 29th Street into 3 acre x 10' detention pond.
- Add 8 acre x 10' detention pond upstream existing pond. Figure IV-2 illustrates proposed detention ponds.

Estimated Probable Cost: \$2,548,900 Average Annual Cost: \$202,600 Estimated Annual Benefit: \$104,900 Benefit/Cost Ratio: 0.5

The estimated probable cost of these proposed conceptual improvements is \$2,548,900. The resulting improved flowlines and water surface elevations are displayed on the flood profiles that supplement this report (See Appendix D). HECRAS summary printouts for the proposed recommendations may be found in Appendix E. The proposed improvements remove sixteen (16) structures from the 100-year flood plain delineation as illustrated in Table IV-17. The proposed conceptual solutions reduce the expected annual damage by \$104,900.

TABLE IV-17
IMPROVED CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES
South Fork Creek

	2 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	bructures in Flood Zo	ne troud k	
Flood Event	Fotal per Event Without Improvements	Total per Event with Improvements	Fotal taken out of Flood Zone per I Event	Expected Damages for Events
5-yr	5	0	5	\$0
10-yr	11	0	11	\$0
25-уг	13	0	13	\$0
50-yr	15	0	15	\$ 0
100-yr	16	0	16	\$ 0
500-ут	22	0	22	\$0

D. TRIBUTARY PO-3

1. <u>Description of Watershed</u>

Tributary PO-3 (Post Oak 3) is located in the north-central quadrant of the City of Corsicana. Tributary PO-3 originates just downstream of Chicago Rock Island Railroad and flows in southerly until it reaches its confluence with Post Oak Creek. The total drainage area of the Tributary PO-3 watershed is 0.13 square miles (89 acres).

The Tributary PO-3 watershed is approaching its maximum projected development stage in 2000. Existing land uses in the Tributary PO-3 watershed consist of approximately 60% residential, 20% business/commercial/industrial areas; 15% crops and pasture; and scattered public/semi-public areas (i.e. schools, churches etc.). Future development will consist of approximately 75% residential, 20% business/commercial/industrial areas; and scattered public/semi-public areas.

2. Hydrologic Study Results

Halff Associates prepared detailed HMS hydrologic computer models of the watershed to analyze existing land use and projected ultimate land use conditions. All hydrologic analyses were prepared with flood routing data based on existing channels and bridges. Peak flood discharges calculated for this study include the 5-, 10-, 25-, 50-, 100-, and 500-year flood frequencies. Existing peak flood discharges based on existing land use and existing channel/bridge conditions are presented in Table IV-18. Future peak discharge information based on future land use and

IV-19

existing channel/bridge conditions are presented in Table IV-19.

TABLE IV-18 EXISTING CONDITIONS PEAK FLOOD DISCHARGES (cfs) Tributary PO-3

10.70	de la la					
	10.00	10-YR	25- VR	50-YR9	100 YR	500-V
0.08	160	190	220	250	280	350
0.13	220	250	300	350	400	500
	0.08	0.08 160	(sm) 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	(sm) 2 11 220 220 220 220 220 23 24 25 27 26 27 27 27 27 27 27 27 27 27 27 27 27 27	(sm) 1.0 190 220 250	0.08 160 190 220 250 280

^{2.} Peak discharges are based on an existing landuse watershed with existing channels and culverts.

TABLE IV-19 FUTURE PEAK FLOOD DISCHARGES (cfs) **Tributary PO-3**

Selection of the select				omputed Pe			
		L/SVR	10-YR	25-YR	305718	\$100 YR	500-Y
	(m)						
At Chicago Rock Island RR	0.08	160	_ 190	220			
			150	220	250	280	350
t Confluence w/ Post Oak Creek			1				
- Communice w/ Post Oak Creek	0.13	220	250	300	350	400	500
						.50	300

^{2.} Peak discharges are based on future land use watershed with existing channels and culverts.

3. **Hydraulic Study Results**

Tributary PO-3 is approximately 0.3 miles in stream length through the City of Corsicana study area. The entire length of stream through the study area consists of a natural earthen channel. The average channel slope through the study area is about 0.70%. The channel is well defined with depths ranging from about 3 feet to 10 feet.

The Tributary PO-3 future fully urbanized 100-year flood plain delineation prepared for this report includes approximately 2 acres of land within the Corsicana City limits. There are six known structures within this 100-year flood plain delineation. None of which have estimated finish floors below the 100-year flood plain.

There are 3 bridge/culverts along Tributary PO-3 within the City of Corsicana study limits. The computed future 100-year flood will overtop the existing roadway at two of these three culvert locations. Pertinent data for each bridge can be found in Table IV-20. Graphical representation of these and other potential flooding areas along Tributary PO-3 are presented on the flood plain maps and flood profiles that supplement this report (see Appendix D). Channel velocities along Tributary PO-3 are generally non-erosive, less than 6.0 feet per second. Although erosion continues to occur along Tributary PO-3, there were no identified instances of high potential loss of private property or areas classified as severe erosion problems.

TABLE IV-20 BRIDGE DATA **Tributary PO-3**

Bridge Literation	Opencam Chimnel X-Section	Upsiceam se Mowline(f)	Chord.	Mm Top; of Road (i) L	Q ₁₀ . (da)(a)	100-Yr WSEL (5)	Description :
Avenue F	9+35	392.15	397.15	396.65	400	397.88	1-60" CMP
10th Street	13+73	396.93	399.93	400.11	280	400.65	3-36" RCP
Burlington Northern RR	15+08	397.45	405.45	405.55	280	401.90	2-96" CMP

Approximate Elevations (NGVD).

¹⁰⁰⁻Year Discharge based on future development with existing channels and bridges/culverts (Baseline Conditions). 2 100-Year flood elevation based on existing channels and culverts.

4. <u>Improvements</u>

Halff Associates did not prepare hydraulic computer models of conceptual bridge and channel designs along Tributary PO-3 since there are no known structures with estimated finish floors below the 100-year flood plain delineation for the area studied.

E. TRIBUTARY PO-5

1. Description of Watershed

The Tributary PO-5 (Post Oak 5) watershed lies in the northwest to north-central side of Corsicana. Tributary PO-5 flows southerly until it reaches its confluence with Post Oak Creek. The total drainage area of the Tributary PO-5 watershed is 0.51 square miles (328 acres).

The lower portion of the Tributary PO-5 watershed is predominantly single family residential while the upper watershed consists of predominantly residential and commercial development. The Tributary PO-5 watershed is approaching its maximum projected development stage in 2000. Existing land uses in the Tributary PO-5 watershed consist of approximately 50% residential; 45% business/commercial/industrial areas; and scattered parks, public/semi-public areas (i.e. schools, churches, etc.). The projected future development is similar to existing landuse conditions.

2. Hydrologic Study Results

Halff Associates prepared detailed HMS hydrologic computer models of the watershed to analyze existing land use and projected ultimate land use conditions. All hydrologic analyses were prepared with flood routing data based on existing channels and bridges. Peak flood discharges were calculated for the 5-, 10-, 25-, 50-, 100-, and 500-year flood frequencies. Existing peak flood discharges based on existing land use and existing channel/bridge conditions are presented in Table IV-21. Future peak discharge information based on future land use and existing channel/bridge conditions are presented in Table IV-22.

TABLE IV-21 **EXISTING CONDITIONS PEAK FLOOD DISCHARGES (cfs) Tributary PO-5**

The second secon	Compa	ted Peak Disc	harge (cfs)				
Location). Area (8m):	5-VR	10-YR	25-YR	50 YR	100-YR	500 YI
At Forest Lane	0.25	510	590	690	770	050	4,316
At Confluence w/ Post Oak Creek	0.51	760	870			850	1030
Discharges were rounded to the nearest 10.			870	1020	1140	1250	1500

Peak discharges are based on an existing land use watershed with existing channels and culverts.

TABLE IV-22 **EXISTING CONDITIONS PEAK FLOOD DISCHARGES (cfs) Tributary PO-5**

Location 22	3,000			Computed P	cak Dischar	हर (दक्कि)	9
	A. B. (1987)	SYR,	IO YR	25 VR	50-YR:	100:YR	500-YR
At Forest Lane	0.25	510	500		1.01		
At Confluence w/ Post Oak Creek			590	690	770	850	1030
Tost Oak Creek	0.51	760	870	1020	1140	1250	1500

^{2.} Peak discharges are based on future land use watershed with existing channels and culverts.

3. **Hydraulic Study Results**

Tributary PO-5 is approximately 0.7 miles in stream length from the confluence with Post Oak Creek to the study limits. The average channel slope of Tributary PO-5 is about 0.8%. The entire length of stream consists of a natural earthen channel with depths ranging from 3-feet to 14-feet. Residential development has occurred along the majority of the stream corridor.

The Tributary PO-5 future fully urbanized 100-year flood plain delineation prepared for this report includes approximately 24 acres of land within the Corsicana City limits. There are forty-three known structures within this 100-year flood plain delineation. Thirty-two of these structures have estimated finish floors below the 100-year flood plain as indicated in Table IV-23. The expected annual damage for these structures is \$135,800.

There are seven bridges/culverts along Tributary PO-5. The computed future 100year flood will overtop the existing roadway at all of these culvert locations.

Pertinent data for each road crossing can be found in Table IV-24. Graphical representation of these and other flood prone areas along Tributary PO-5 are presented on the flood plain maps and flood profiles that supplement this report (see

TABLE IV-23 BASELINE CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES **Tributary PO-5**

Flood Event	Structures	n Flood Zone	Expected Damages for
5	Contribution per Event	Fotal for Event	Byent
5-уг	11	11	\$171,000
10-yr	6	17	\$345,000
25-yr	4	21	\$481,000
50-ут	9	30	\$785,000
100-уг	2	32	\$831,000
500-уг	3	35	\$957,000

TABLE IV-24 **BRIDGE DATA Tributary PO-5**

Bridge Identification	Upstream Channel X-Section	Upstream. Flowline (1)	Low Chord (1)	Min Top of Road (1)	Q ₁₀₀ (cts) (2)	100-Yr WSEL-(3)	Description
Royal Street	8+95	400.42	405.42	407.67	1250	410.17	2-60" RCP
Northwood Blvd	18+60	407.96	412.96	414.54	850	415.24	2-60" RCP
Chicago RR	21+10	412.17	422.17	424.7	850	423.69	1-120" CMP
Madison Drive	23+50	412.72	416.72	419.49	850	423.69	3-48" RCP
Mamie Ave/Dobbins	28+10	418.82	422.82	424.22	850		
Fish Tank Road	33+10	419.30	422.80			425.20	2-8'x4' CBC
			722.80	422.97	850	425.68	4-42" CMP
Forrest Lane	37+70	425.45	427.45	428.85	850	429.63	2-108" RCP

Approximate Elevations (NGVD).

¹⁰⁰⁻Year Discharge based on future development with existing channels and bridges/culverts (Baseline Conditions). 100-Year flood elevation based on existing channels and culverts

Existing channel velocities for Tributary PO-5 are generally non-erosive, less than 6 feet per second. Channel velocities greater than 8 feet per second were computed near the existing culvert crossing at Chicago Railroad (stream station 21+10). Three homes are close to the channel banks in generally non-erosive areas, however, proximity to the banks could warrant erosion protection.

4. Improvements

Halff Associates utilized the existing channel condition Tributary PO-5 hydraulic computer model to prepare conceptual bridge and channel designs for future roadway improvements and erosion protection. See Chapter V for guidance on erosion control. The following is a brief description of the proposed conceptual improvements for Tributary PO-5:

- Three 12'x6' concrete box culverts at Royal Lane.
- Three 9'x5' concrete box culverts at Northwood Boulevard.
- Two 10'x9' concrete box culverts at Chicago Rock Island Railroad (the downstream effect of opening the railroad were not determined).
- Two 9'x6' concrete box culverts at Madison Drive.
- 900 LF 10' bottom width 3:1 grass-lined channel from Madison Drive to Fish Tank Road (stream stations 23+85 to 32+90).
- Two 10'x7' concrete box culverts at Dobbins Road.
- Three 9'x5' concrete box culverts at Fish Tank Road.

Estimated Probable Cost: \$1,250,200 Average Annual Cost: \$99,400 Estimated Annual Benefit: \$134,800 Benefit/Cost Ratio: 1.4

The estimated probable cost of these proposed conceptual improvements is \$1,250,200. The resulting improved flowlines and water surface elevations are displayed on the flood profiles that supplement this report (See Appendix D). HEC-RAS summary printouts for the proposed recommendations may be found in Appendix E. The proposed improvements remove thirty-one (31) structures from the 100-year flood plain delineation as illustrated in Table IV-25. The proposed conceptual solutions reduce the expected annual damage by \$134,800.

TABLE IV-25
IMPROVED CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES
Tributary PO-5

	/fl / c / S	tructures in Flood Zo	ine .	
Flood Event	Total per Event : without Improvements	Total per Event with Improvements		Expected Damages for Event
5-ут	11	0	11	\$0
10-ут	17	0	17	\$0
25-уг	21	0	21	\$0
50-yr	30	1	29	\$500
100-yr	32	1	31	\$12,.000
500-уг	35	3	32	\$50,000

F. TRIBUTARY PO-6

1. Description of Watershed

The Tributary PO-6 (Post Oak 6) watershed lies in the northwest side of Corsicana. Tributary PO-6 flows southerly until it reaches its confluence with Post Oak Creek. The total drainage area of the Tributary PO-6 watershed is 0.42 square miles (276 acres).

The northwestern portion of the Tributary PO-6 watershed is generally undeveloped at this time; however, the remainder of the watershed consists predominantly of single family residential units. Existing land uses in the Tributary PO-6 watershed consist of approximately 75% residential; 20% crops and pasture; 4% parks and open space; and scattered public/semi-public areas (i.e. schools, churches, etc.). Projected future development will consist of approximately 97% residential landuse; 2% parks and open space; and scattered public/semi-public areas.

2. Hydrologic Study Results

Halff Associates prepared detailed HMS hydrologic computer models of the watershed to analyze existing land use and projected ultimate land use conditions. All hydrologic analyses were prepared with flood routing data based on existing channels and bridges. Peak flood discharges were calculated for the 5-, 10-, 25-, 50-, 100-, and 500-year flood frequencies. Existing peak flood discharges based on existing land use and existing channel/bridge conditions are presented in Table IV-26. Future peak discharge information based on future land use and existing

channel\bridge conditions are presented in Table IV-27.

TABLE IV-26 EXISTING CONDITIONS PEAK FLOOD DISCHARGES (cfs) Tributary PO-6

	Compute	ed Peak Disch	arge (cfs)		A.		
Location	Area (am)	5 YR	10 YR	25-YR	(50-YR)	100-YR	500-YR
Just upstream of Lakewood Ave	0.1	205	240	285	320	360	440
At Chicago Rock Island RR	.27	395	470	550	620	690	840
At Confluence w/ Post Oak Creek	0.33	450	530	630	720	800	960

^{1.} Discharges were rounded to the nearest 100.

TABLE IV-27 EXISTING CONDITIONS PEAK FLOOD DISCHARGES (cfs) Tributary PO-6

	40 5 4 6 4	Computed Peak Discharge (cfs),						
Location	Areas (Sin)	S-YR (10-YR	25 YR	50-YR	100 YR	500 YR	
Just upstream of Lakewood Ave	0.1	205	240	285	320	360	440	
At Chicago Rock Island RR	.27	400	470	550	620	690	840	
At Confluence w/ Post Oak Creek	0.33	460	540	640	720	800	970	

^{1.} Discharges were rounded to the nearest 100.

3. Hydraulic Study Results

Tributary PO-6 is approximately 1.0 miles in stream length from the confluence with Post Oak Creek to the study limits. The average channel slope of Tributary PO-6 is about 0.9%. The entire length of stream consists of a natural earthen channel with depths ranging from 2-feet to 10-feet. Residential development has occurred along the majority of the stream corridor.

^{2.} Peak discharges are based on an existing land use watershed with existing channels and culverts.

^{2.} Peak discharges are based on future land use watershed with existing chamels and culverts.

The Tributary PO-6 future fully urbanized 100-year flood plain delineation prepared for this report includes approximately 28 acres of land within the Corsicana City limits. There are thirty-one known structures within this 100-year flood plain delineation. Eighteen of these structures have estimated finish floors below the 100-year flood plain as indicated in Table IV-28. The expected annual damage for these structures is \$468,000

There are nine bridges/culverts along Tributary PO-6. The computed future 100-year flood will overtop the existing roadway at all of these culvert locations. Pertinent data for each road crossing can be found in Table IV-29. Graphical representation of these and other flood prone areas along Tributary PO-6 are presented on the flood plain maps and flood profiles that supplement this report (see Appendix D). Existing channel velocities for Tributary PO-6 are generally non-erosive, less than 6 feet per second. Four homes are close to the channel banks in generally non-erosive areas, however, proximity to the banks could warrant erosion protection.

TABLE IV-28
BASELINE CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES
Tributary PO-6

Flood Event	. Structures u	Structures in Flood Zone					
	Contribution per . Event	Total for Event	Event				
5-yr	16	16	\$509,000				
10-yr	0	16	\$525,000				
25-уг	0	16	\$542,000				
50-ут	1	17 .	\$562,000				
100-уг	1 .	18	\$581,000				
500-yr	5	23	\$671,000				

TABLE IV-29 BRIDGE DATA Tributary PO-6

Bridge Identification	Upstream Channel X-Section	Upstream Flowline (1)	Low Chord	Min Top of Road	Q ₁₀₀ (CB) (2)	100-Yr WSEL (5)	Description
Mimosa Drive	10+65	408.65	413.65	415.83	800	416.96	2-60" RCP
Northwood Blvd	14+75	411.90	416.90	419.73	800	420.84	1-60" RCP
Chicago RR	16+80	414.10	424.10	432.73	690	423.91	1-120" CMP
Fish Tank Road	22+75	420.53	424.53	425.65	690	426.97	2-48" RCP
Edgewood Street	24+50	424.62	427.62	429.63	690	431.55	3-36" RCP
McKinney Street	27+55	427.11	430.11	431.88	690	433.21	3-36" CMP
Louis Street	31+55	429.26	432.26	434.03	360	434.83	3-36" CMP
Lakewood Avenue	34+75	431.21	434.21	436.29	360	436.89	2-36" CMP
FM 3383	50+25	444.0	448.0	448.5	360	448.86	1-4'x4' CBC

Approximate Elevations (NGVD). 1 2 3

¹⁰⁰⁻Year Discharge based on future development with existing channels and bridges/culverts (Baseline Conditions). 100-Year flood elevation based on existing channels and culverts.

4. Improvements

Halff Associates utilized the existing channel condition Tributary PO-6 hydraulic computer model to prepare conceptual bridge and channel designs for future roadway improvements and erosion protection. See Chapter V for guidance on erosion control. The following is a brief description of the proposed conceptual improvements for Tributary PO-6:

- Four 10'x5' concrete box culverts at Fish Tank Road.
- 1500 LF 20' bottom width 3:1 grass-lined channel from Fish Tank Road to upstream of Lakewood Avenue (stream stations 22+94 to 38+00).
- Four 10'x5' concrete box culverts at Edgewood Street.
- Purchase structure at Edgewood in order to construct above 1500 LF of improvements.
- Four 10'x4' concrete box culverts at McKinney Street.
- Three 8'x4' concrete box culverts at Louis Avenue.
- Three 8'x4' concrete box culverts at Lakewood Avenue.
- FM 3383 culverts require upgrade and channel or storm drain system to alleviate flood damages to homes.

Estimated Probable Cost: \$1,444,900 Average Annual Cost: \$114,800 Estimated Annual Benefit: \$460,400 Benefit/Cost Ratio: 4.0

The estimated probable cost of these proposed conceptual improvements is \$1,444,900. The resulting improved flowlines and water surface elevations are displayed on the flood profiles that supplement this report (See Appendix D). HEC-RAS summary printouts for the proposed recommendations may be found in Appendix E. The proposed improvements remove ten structures from the 100-year flood plain delineation as illustrated in Table IV-30. The proposed conceptual solutions reduce the expected annual damage by \$460,400.

TABLE IV-30
IMPROVED CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES
Tributary PO-6

		Structures in Flood Zo	ne	
Flood Event	Total per Event without Improvements	Total per Event. with a limprovements	Total taken out of Flood Zone pers. Event	Expected Damages for Event
5-yr	16	1	15	\$13,000
10-ут	16	1	15	\$19,000
25-yr	16	1	15	\$26,000
50-yr	17	2	15	\$44,000
100-уг	18	8	10	\$104,000
500-уг	23	8	15	\$154,000

G. MESQUITE BRANCH

1. Description of Watershed

Mesquite Branch originates southwest of the city limits of Corsicana. It then flows in a northeasterly direction through the southern portion of the City until it reaches its confluence with Post Oak Creek. The total drainage area of the Mesquite Branch watershed is 4.73 square miles (3026 acres).

The Mesquite Branch watershed is generally undeveloped at this time. Existing land uses in the Mesquite Branch watershed consist of approximately 55% crops and pasture; 30% business/commercial/industrial areas; 8% residential; 2% parks and open space; and scattered public/semi-public areas (i.e. schools, churches, etc.). Projected future development will consist of approximately 45% residential; 45% business/commercial/industrial areas; 5% parks and open space; and scattered public/semi-public areas (i.e. schools, churches, etc.).

2. Hydrologic Study Results

Halff Associates prepared detailed HMS hydrologic computer models of the watershed to analyze existing land use and projected ultimate land use conditions. All hydrologic analyses were prepared with flood routing data based on existing channels and bridges. Peak flood discharges were calculated for the 5-, 10-, 25-, 50-, 100-, and 500-year flood frequencies. Existing peak flood discharges based on

existing land use and existing channel/bridge conditions are presented in Table IV-31. Future peak discharge information based on future land use and existing channel\bridge conditions are presented in Table IV-32.

TABLE IV-31
EXISTING CONDITIONS PEAK FLOOD DISCHARGES (cfs)

<u>Mesquite Branch</u>

Area (sm)	5-YR	10-YR	25-YR	SECTION SE		
(sm) :-					100-YR	500-YR
7.7						48.515
2.27	2300	2750	3300	3800	4250	5150
2.59	2500	3000	3550	4000	4450	5350
2.97	2800	3350	4000	4500	4950	6000
2.97	2400	2900	3550	4100	4550	5400
4.37	3450	4100	5050	5750	6400	7700
5.42	3650	4400	5300	6100	7100	9000
5.84	3750	4500	5300	6200	7250	9150
5.84	3200	3700	4350	4900	5900	8000
6.09	3200	3700	4350	4900	5900	8000
	2.59 2.97 2.97 4.37 5.42 5.84 5.84	2.59 2500 2.97 2800 2.97 2400 4.37 3450 5.42 3650 5.84 3750 5.84 3200	2.59 2500 3000 2.97 2800 3350 2.97 2400 2900 4.37 3450 4100 5.42 3650 4400 5.84 3750 4500 5.84 3200 3700	2.59 2500 3000 3550 2.97 2800 3350 4000 2.97 2400 2900 3550 4.37 3450 4100 5050 5.42 3650 4400 5300 5.84 3750 4500 5300 5.84 3200 3700 4350	2.59 2500 3000 3550 4000 2.97 2800 3350 4000 4500 2.97 2400 2900 3550 4100 4.37 3450 4100 5050 5750 5.42 3650 4400 5300 6100 5.84 3750 4500 5300 6200 5.84 3200 3700 4350 4900	2.59 2500 3000 3550 4000 4450 2.97 2800 3350 4000 4500 4950 2.97 2400 2900 3550 4100 4550 4.37 3450 4100 5050 5750 6400 5.42 3650 4400 5300 6100 7100 5.84 3750 4500 5300 6200 7250 5.84 3200 3700 4350 4900 5900

^{1.} Discharges were rounded to the nearest 50.

^{2.} Peak discharges are based on an existing land use watershed with existing channels and culverts.

TABLE IV-32 FUTURE CONDITIONS PEAK FLOOD DISCHARGES (cfs) Mesquite Branch

Killippe 18 and Spiel Spiel		1.1	Co	mputed Pea	k Discharge	(cfs)	1.0
Location	Arta	5-YR	10-YR	25-YR	50-YR	100-YR	500-YR
	(sm)						
At Southern Pacific RR	2.27	2450	3950	3500	4000	4500	5400
At River Station 185+45	2.59	2650	3150	3700	4150	4650	5600
Just Upstream of Chicago Rock Island RR	2.97	2950	3500	4150	4650	5150	6250
Just Downstream of Chicago Rock Island RR	2.97	2550	3000	3700	4200	4700	5550
At Confluence with Town Branch	4.37	3600	4250	5200	5950	6600	7900
At Interstate 45	5.42	3750	4450	5350	6250	7250	9100
Just Upstream of St. Louis & Southwestern RR	5.84	3950	4650	5600	6450	7500	9550
Just Downstream of St. Louis & Southwestern RR	5.84	3300	3850	4500	5150	6200	8400
At Confluence w/ Post Oak Creek	6.09	3300	3850	4500	5150	6200	8400

^{1.} Discharges were rounded to the nearest 50.

3. Hydraulic Study Results

Mesquite Branch is approximately 4.1 miles in stream length from the confluence with Post Oak Creek to the study limits. The average channel slope of Mesquite Branch is about 0.2%. The entire length of stream consists of a natural earthen channel with depths ranging from 4-feet to 14-feet.

The Mesquite Branch future fully urbanized 100-year flood plain delineation prepared for this report includes approximately 287 acres of land within the Corsicana City limits. There are eight structures within this 100-year flood plain delineation. Three of these structures have estimated finish floors below the 100-year flood plain as indicated in Table IV-33. The expected annual damage for these structures is \$28,000.

There are nine bridges/culverts along Mesquite Branch. The computed future 100-year flood will overtop the existing roadway at six of these nine culvert locations. Pertinent data for each road crossing can be found in Table IV-34. Graphical representation of these and other flood prone areas along Mesquite Branch are presented on the flood plain maps and flood profiles that supplement this report (see Appendix D).

^{2.} Peak discharges are based on future land use watershed with existing channels and culverts.

Existing channel velocities for Mesquite Branch are generally non-erosive, less than 6 feet per second. Channel velocities greater than 8 feet per second were computed at bridge crossings at Chicago and Rock Island Railroad (stream stations 152+33 to 153+97). Although erosion continues to occur along Mesquite Branch, there were no identified instances of high potential loss of private property or areas classified as severe erosion problems.

TABLE IV-33
BASELINE CONDITIONS SINGLE OCCURRENCE FLOOD LOSSES

<u>Mesquite Branch</u>

Flood Event	Structures	n Flood Zone	Expected Damages for
	Contribution per Event	Total for Event	Event
5-yr	3	3	\$44,000
10-yr	0	3	\$52,000
25-yr	0	3	\$60,000
50-уг	0	3	\$64,000
100-yr	0	3	\$68,000
500-уг	2	5	\$79,000

TABLE IV-34 **BRIDGE DATA** Mesquite Branch

Bridge Identification	Upstream Channel X-Section	Upstream Flowline (1)	Low Chord (1)	Min Top of Road	Q ₁₀₀ (cfs) (2)	100-Yr WSEL (5)	Description
Powell Pike	45+15	358.7	367.64	369.64	6200	371.83	Steel Bridge
St. Louis & Southwestern RR	45+95	361	372.34	375.35	6200	375.88	Wood Bridge with 6 Piers
SE0010 Road	84+10	368.1	373.1	374.63	7250	378.48	6-9'x5' CBC
IH-45 North Bound Frontage Road	103+65	370.1	381.24	387.24	7250	382.22	Concrete Bridge with 1 Pier
IH-45 South Bound Frontage Road	104+35	381.24	381.24	387.24	7250	382.53	Concrete Bridge
Chicago Rock Island RR	153+ 9 0	386.1	397.5	400	4700	396.14	Wood Bridge with 5 Piers
Hwy 287	157+80	386.1	394.1	396.8	5150	399.06	4-8'x8' CBC
Hwy 75/Business 45	163+65	388.7	394.7	395.8	5150	399.39	7-6'x6' CBC
Southern Pacific RR	217+05	402.77	416.02	419.02	4500	415.43	Wood Bridge with 5 Piers
FM 709	217+95	403	411	412.18	4500	416.62	2-8'x8' CBC

Approximate Elevations (NGVD).

4. **Improvements**

Halff Associates did not prepare hydraulic computer models of conceptual bridge and channel designs along Mesquite Branch because it is neither practical nor cost effective for the City to implement a major construction alternative at this time considering there are only three structures with estimated finish floors below the 100-year flood plain. However, non-structural measures such as construction regulation and purchasing structures should be considered.

¹⁰⁰⁻Year Discharge based on future development with existing channels and bridges/culverts (Baseline Conditions).

¹⁰⁰⁻Year flood elevation based on existing channels and culverts.

H. TOWN BRANCH

1. <u>Description of Watershed</u>

The Town Branch watershed lies in the south-central quadrant of the City of Corsicana. Town Branch easterly until it reaches its confluence with Mesquite Branch. The total drainage area of the Town Branch watershed is 1.36 square miles (870 acres).

The Town Branch watershed is approaching its maximum projected development stage in 2000. Existing land uses in the Town Branch watershed consist of approximately 70% residential; 20% business/commercial/industrial areas; 5% parks and open space; and scattered public/semi-public areas (i.e. schools, churches, etc.). The projected future development is similar to existing landuse conditions.

2. Hydrologic Study Results

Halff Associates prepared detailed HMS hydrologic computer models of the watershed to analyze existing land use and projected ultimate land use conditions. All hydrologic analyses were prepared with flood routing data based on existing channels and bridges. Peak flood discharges were calculated for the 5-, 10-, 25-, 50-, 100-, and 500-year flood frequencies. Existing peak flood discharges based on existing land use and existing channel/bridge conditions are presented in Table IV-35. Future peak discharge information based on future land use and existing channel/bridge conditions are presented in Table IV-36.

TABLE IV-35
EXISTING CONDITIONS PEAK FLOOD DISCHARGES (cfs)

<u>Town Branch</u>

Tarangan pang 1988	13.44			Computed P	ealt Dischar	ge (cfs)	
Lication 22 constant in the co		S VR	3 4 K	25 YR	50-VR	100 YR.	500AYR
		100			4.5		1000
At N 24th Street	0.18	460	530	620	700	770	970
At W 6th Avenue	0.27	510	590	690	780	860	1050
At St. Louis & Southwestern RR	0.49	840	970	1140	1320	1500	1820
At Southern Pacific RR	0.92	1190	1380	1650	1890	2110	2510
At Confluence w/ Mesquite Creek	1.36	1230	1460	1760	2010	2250	2690

^{1.} Discharges were rounded to the nearest 10.

^{2.} Peak discharges are based on an existing land use watershed with existing channels and culverts.

TABLE IV-36
FUTURE CONDITIONS PEAK FLOOD DISCHARGES (cfs)
Town Branch

10000000000000000000000000000000000000	250.6			Computed P	eak Dischar	ge (cls)	
Location .	Ares	5-YR	: 10-YR	25-YR	50-YR	100 YR	500-YR
大學學 化乙烷酸	(sin)						
At N 24th Street	0.18	460	530	620	700	770	970
At W 6th Avenue	0.27	510	590	690	780	860	1050
At St. Louis & Southwestern RR	0.49	840	970	1140	1320	1500	1820
At Southern Pacific RR	0.92	1190	1380	1650	1890	2110	2510
At Confluence w/ Mesquite Creek	1.36	1230	1460	1760	2010	2250	2690

^{1.} Discharges were rounded to the nearest 10.

3. Hydraulic Study Results

Town Branch is approximately 2.4 miles in stream length from the confluence with Mesquite Branch to the study limits. The average channel slope of Town Branch is about 0.5%. The stream consists of natural earthen channel for approximately 9200 linear feet from downstream to W. 7th Avenue. Upstream of W. 7th Avenue, the stream consists of approximately 200 linear feet of 10 foot bottom width concrete pilot channel with grass-lined slopes. The stream then transitions back to natural earthen channel for approximately 700 linear feet to W. 6th Avenue. Upstream of W. 6th Avenue, the stream consists of 200 linear feet of a 5 foot bottom width concrete channel. The stream then transitions to natural earthen channel for the remaining length of stream. The stream has depths ranging from 3-feet to 11-feet.

The Town Branch future fully urbanized 100-year flood plain delineation prepared for this report includes approximately 120 acres of land within the Corsicana City limits. There are one hundred and forty known structures within this 100-year flood plain delineation. Seventy-five of these structures have estimated finish floors below the 100-year flood plain as indicated in Table IV-37. The expected annual damage for these structures is \$194,500.

There are twenty-three bridges/culverts along Town Branch. The computed future 100-year flood will overtop the existing roadway at twenty of these twenty-three culvert locations. Pertinent data for each road crossing can be found in Table IV-38. Graphical representation of these and other flood prone areas along Town Branch are presented on the flood plain maps and flood profiles that supplement this report

^{2.} Peak discharges are based on future land use watershed with existing channels and culverts.

(see Appendix D).

Existing channel velocities are generally non-erosive, less than 6.0 feet per second. Channel velocities greater than 8 feet per second were computed at several bridge/culvert crossings. Six homes are close to the channel banks in generally non-erosive areas, however, proximity to the banks could warrant erosion protection.

TABLE IV-37
BASELINE CONDITIONS SINGLE OCCURRENC FLOOD LOSSES

<u>Town Branch</u>

Flood Event	Structures i	Structures in Flood Zone					
	Contribution per Event	Total for Event	Event				
5-yr	24	24	\$211,000				
10-yr	10	34	\$354,000				
25-yr	11	45	\$679,000				
50-yr	14	59	\$1,032,000				
100-уг	16	75	\$1,290,000				
500-yr	31	106	\$2,066,000				

TABLE IV-38 BRIDGE DATA Town Branch

Bridge Identification	Upstre am Chann el X- Section	Upstream Flowline (1)	Low Chord	Min Top of Road (1)	O ₁₀₀ - (cfs) (2)	100-Yr WSEL (3)	Description
S. 5th Street	20+75	388.2/387.1	202 2/202 1	# 1 = 4 T			Transfer Communication (Communication)
Chicago Doch John J.D.			392.2/392.1	392.32	1840	394.47	2-48" RCP & 2-60" RCP
Chicago Rock Island RR	26+50	389.5	399.5	406.22	1840	402.27	2-120" CMP
S. 7th Street	31+10	391.38	398.48	400.15	2110	402.38	2-10'x7.1' CBC
9th Street/Brewer	38+15	394.25	401.25	401.7	2110	402.66	2-84" RCP
S. Beaton Street	45+20	394.5	401.5	401.51	2110	403.68	3-84" RCP
11th Street/Main	49+04	397.2	403.7	404	2110	405.71	2-78" CMP
S. 12th Street	53+02	398.5	404.5	405.65	2110	409.03	2-72" CMP
Old City Iron Works #1	54+60	399	408	408.24	2110	409.76	1-108" CMP
Old City Iron Works #2	58+52	401.02	410.02	410.6	2110	412.60	1-8'x9' Ellipse Culvert
Southern Pacific RR	59+77	402	411.49	415.49	2110	414.09	Wood Bridge with 2 Piers
S. 15th Street	65+42	404.5	410.5	411.51	2110	414.79	2-10'x6' CBC
W. 13th	71+75	406.4	411.4	414.14	1500	415.56	2-10'x5' CBC
W. 11th Avenue	77+62	410.47	414.97	415.73	1500	418.10	2-10'x4.5' CBC
W. 10 th Avenue	82+57	411.3	417.5	418.53	1500	420.23	2-9'x6.2' Ellipse Culvert
W. 9th Avenue	86+02	413.69	419.19	420.55	1500	421.37	2-9'x5' CBC
St. Louis RR	89+52	415.52	415.52	427.94	1500	428.62	3-6'x5' CBC
W. 7th Avenue	93+42	418.57	423.57	424.33	1500	428.61	1-10.5'x5' CBC
W. 6th Avenue	104+05	427.19	430.19	430	860	433.67	1-10'x5' & 1-7'x5' ARCH BOX DS
Just Upstream of W. 6th Avenue	105+83	427.3	431.3	432	860	433.93	& 2-36" RCP US
Collins Avenue	113+20	433.1	437.1	437.58	770	439.41	1-10'x3' & 1-10'x5' CBC DS &
Just Upstream of Collins at Old 23 rd Street	114+62	433.53	437.53	437.58	770	439.58	1-13'x4' CBC US 2-48" RCP
231/2 Street	117+55	437.76	440.76	441.15	770	442.92	2-36" RCP
24th Street	121+90	441.95	444.95	447.24	770	447.90	1-5.5'x3 Ellipse Culvert

Approximate Elevations (NGVD).

100-Year Discharge based on future development with existing channels and bridges/culverts (Baseline Conditions).

100-Year flood elevation based on existing channels and culverts.

4. Improvements

Halff Associates utilized the existing channel condition Town Branch hydraulic computer model to prepare conceptual bridge and channel designs for future roadway improvements and erosion protection. See Chapter V for guidance on erosion control. The following is a brief description of the proposed conceptual improvements for Town Branch:

Reach 1 - Chicago & Rock Island Railroad to S. Beaton Street (stream stations 26+82 to 45+04)

- 1820 LF 40' bottom width 3:1 grass lined channel from Chicago & Rock Island Railroad to S. Beaton Street (stream stations 26+82 to 45+04).
- Four 10' corrugated metal pipes at Chicago Rock Island Railroad (the downstream effects of opening railroad were not determined).
- Purchase 1 large and several small structures upstream S. 7th Street in order to construct above 1820 LF of improvements.
- Four 11'x8' concrete box culverts at S. 7th Street.
- Four 11'x7' concrete box culverts at S. 9th Street.

Estimated Probable Cost: \$1,415,200 Average Annual Cost: \$112,500 Estimated Annual Benefit: \$46,100 Benefit/Cost Ratio: 0.4

The estimated probable cost of these proposed conceptual improvements for Reach 1 is \$1,415,200. Proposed improvements through Reach 1, from Chicago & Rock Island Railroad to S. Beaton Street, will remove eleven (11) structures from the 100-year flood plain delineation as shown in Table IV-39. Reach 1 proposed conceptual solution reduce the expected annual damages by about \$46,100.

TABLE IV-39 IMPROVED CONDITIONS SINGLE OCCURRENC FLOOD LOSSES REACH 1 (CHICAGO & ROCK ISLAND RAILROAD TO S. BEATON STREET) Town Branch

		Structures in Flood Zone						
Flood Event	Total per Event without Improvements	Total per Event with Improvements	Total taken out of Flood Zone per Event	Expected Damages for Event				
5-yr	24	20	4	\$ 150,000				
10-уг	34	27	7	\$274,000				
25-уг	45	36	9	\$560,000				
50-yr	59	49	10	\$858,000				
100-yr	75	64	11	\$1,055,000				
500-уг	106	84	22	\$1,454,000				

Reach 2 - S. 12th Street to S. 16th Street (stream stations 54+40 to 71+98)

- 1760 LF 40' bottom width 3:1 grass lined channel from just upstream of S. 12th Street to S. 16th Street (stream stations 54+40 to 71+98).
- Five 12'x7' concrete box culverts at S. 15th Street.
- Purchase 3 structures by S. 15th Street in order to construct above 1760 LF of improvements.
- Four 10'x5' concrete box culverts at S. 16th Street.

Estimated Probable Cost: \$1,213,700
Average Annual Cost: \$96,500
Estimated Annual Benefit: \$36,300
Benefit/Cost Ratio: 0.4

The estimated probable cost of these proposed conceptual improvements for Reach 2 is \$1,213,700. Twenty (20) structures are removed from the 100-year flood plain delineates as indicated in Table IV-40 by the proposed improvements through Reach 2, from S. 12th Street to S. 16th Street. The Reach-2 proposed conceptual solutions reduce the expected annual damage by \$36,300.

TABLE IV-40 IMPROVED CONDITIONS SINGLE OCCURRENC FLOOD LOSSES REACH 2 (S. 12TH STREET TO S. 16TH STREET) Town Branch

	S S	Structures in Flood Zone				
Flood Event	Total per Event without Improvements	Total per Event with Emprovements		Expected Damages for Event		
5-yr	24	15	9	\$163,000		
10-уг	34	23	11	\$294,000		
25-yr	45	29	16	\$594,000		
50-yr	59	40	19	\$924,000		
100-ут	75	55	20	\$1,163,000		
500-уг	106	73	33	\$1,886,000		

Reach 3 - S. 16th Street to W. 7th Avenue (stream stations 71+98 to 91+85)

- 1990 LF 20' bottom width 3:1 grass lined channel from S. 16th Street to W. 7th Avenue (stream stations 71+98 to 91+85).
- Five 11'x5' concrete box culverts at W. 11th Avenue.
- Four 12'x7' concrete box culverts at W. 10th Avenue.
- Four 10'x6' concrete box culverts at W. 9th Avenue.
- Four 10'x6' concrete box culverts at St. Louis & Southwestern Railroad (the downstream effects of opening railroad were not determined).
- Four 10'x6' concrete box culverts at W. 7th Avenue.
- Purchase 3 structures between S. 16th Street and W. 11th Avenue in order to construct above 1990 LF of improvements.
- Purchase structure on top culvert at W. 7th Avenue.

Estimated Probable Cost: \$2,139,000 Average Annual Cost: \$170,000 Estimated Annual Benefit: \$35,300 Benefit/Cost Ratio: 0.2

The estimated probable cost of these proposed conceptual improvements for Reach 3 is \$2,139,000. The proposed improvements through Reach 3, from S. 16^{th} Street to W. 7^{th} Avenue, remove eighteen (18) structures form the 100-year flood plain delineation as illustrated in Table IV-41. The expected annual damages is reduced by \$35,300.

TABLE IV-41 IMPROVED CONDITIONS SINGLE OCCURRENC FLOOD LOSSES REACH 3 (S. 16TH STREET TO W. 7TH AVENUE) Town Branch

	S. C. Service S				
Flood Event	Total per Event without Improvements	Total per Event with Improvements	Total taken out of Flood Zone per Event	Expected Damages for Event	
5-yr	24	24	0	\$220,000	
10-yr	34	30	4	\$292,000	
25-yr	45	38	7	\$401,000	
50-ут	59	47	12	\$525,000	
100-yr	75	57	18	\$683,000	
500-ут	106	86	20	\$1,348,000	

Reach 4 - Upstream of W. 6th Avenue to end of Study Limits (stream stations 106+00 to 128+07)

- Three 10'x4' concrete box culverts at W. 6th Avenue.
- 550 LF 10' bottom width 3:1 grass lined channel from upstream of W. 6th Avenue to Collins Avenue (stream stations 106+00 to 111+50).
- Three 12'x4' concrete box culverts at Collins Avenue.
- 1335 LF 10' bottom width 3:1 grass lined channel from Collins Avenue to end of study limits (stream stations 114+72 to 128+07).
- Three 8'x4' concrete box culverts at N. 23 ½ Street.
- Three 7'x4' concrete box culverts at N. 24th Street.
- Purchase 1 structure at 24th Street in order to construct above 1335 LF of improvements.

Estimated Probable Cost: \$1,774,200
Average Annual Cost: \$141,000
Estimated Annual Benefit: \$26,600
Benefit/Cost Ratio: 0.2

The estimated probable cost of these proposed conceptual improvements for Reach 4 is \$1,774,200. Thirteen (13) structures are removed from the 100-year flood plain delineation by the proposed improvements through Reach 4, from upstream of W. 6th Avenue to the end of study limits, as shown in Table IV-42. Reach 4 proposed conceptual solutions reduce the expected annual damages by \$26,600.

TABLE IV-42 IMPROVED CONDITIONS SINGLE OCCURRENC FLOOD LOSSES REACH 4 (UPSTREAM OF W. 6^{TH} AVENUE TO END OF STUDY LIMITS) <u>Town Branch</u>

Flood Event	** *** *** *** *** *** *** *** *** ***	Structures in Flood Zone					
	Total per Event without improvements	Total per Event. with Improvements	Total taken out of Flood Zone per Event	Expected Damages for Event			
5-yr	24	17	7	\$177,000			
10-уг	34	26	8	\$300,000			
25-yr	45	37	8	\$609,000			
50-yr	59	49	10	\$948,000			
100-уг	75	62	13	\$1,188,000			
500-уг	106	94	12	\$1,911,000			

The total estimated probable cost of all (Reaches 1-4) proposed conceptual improvements for Town Branch is \$6,542,100. The estimated annual cost for all (Reaches 1-4) improvements is \$519,900. The resulting improved flowlines and water surface elevations are displayed on the flood profiles that supplement this report (See Appendix D). HEC-RAS summary printouts for the proposed recommendations may be found in Appendix E.

The aforementioned estimates for removal of structures were determined by each individual reach investigated independently. Therefore, overlap exists among the number of structures removed (i.e. the improvements from S. 12th Street to S. 16th Street improve conditions upstream and remove structures that are also removed by the improvements from S. 16th Street to W. 7th Avenue). However, more structures are removed by the combined effect of implementing all improvements (Reaches 1-4). In this case, the sum of structures removed by the implementation of all improvements (Reaches 1-4) is greater than the sum of that of the individual improvements by reach. With all improvements (Reaches 1-4) in place, sixtythree structures are removed from the 100-year flood plain delineation as illustrated in Table IV-43. When all improvements (Reaches 1-4) are implemented, their combined effect lowers the water surface elevation more than their individual effect. Therefore, with all improvements in place (Reaches 1-4), the reduction in expected annual damages is greater than the sum of that of the individual improvements by reach. With all improvements in place (Reaches 1-4), the proposed conceptual solutions reduce the expected annual damage by \$147,300. The benefit to cost ration is 0.3.

TABLE IV-43
IMPROVED CONDITIONS SINGLE OCCURRENC FLOOD LOSSES
ALL IMPROVEMENTS (REACHES 1-4)

<u>Town Branch</u>

1205	S	Structures in Flood Zone					
Flood Event	Total per Event without Improvements	out. with Fig.		Expected Damages for Event			
5-ут	24	4	20	\$73,000			
10-ут	34	4	30	\$96,000			
25-уг	45	5	40	\$121,000			
50-yr	59	9	50	\$157,000			
100-уг	75	12	63	\$200,000			
500-уг	106	22	84	\$309,000			

I. SUMMARY OF REPORT FINDINGS

Table IV-44 is a summary of conclusions defined by this study. Within the City of Corsicana project limits, approximately 955 acres of the Post Oak watershed is inundated by the future fully urbanized 100-year flood plain. An estimated 409 structures are within the future 100-year flood plain limits. And the future 100-year flood will overtop 19 of the existing 22 stream crossings within the study area. Table IV-45 is a summary of the expected annual damages for existing and improved conditions. A summary of benefit/cost ratios is illustrated in Table IV-46.

TABLE IV-44 SUMMARY OF 100-YEAR FLOOD PLAIN ANALYSES

Sfream	Total Length in Study (miles)	Acres in the 5100-Yr Flood Plain* (acres)	Number of Structures in the 100-Yr Flood Plain."	Number of Bridges Overtopped by 100-Yr Flood *	Total Estimated Cost for Channel and Bridge Improvements Analyzed
Post Oak Creek	5.4	450	154	10 of 14	\$8,683,700
South Fork Creek	1.4	44	27	6 of 6	\$2,548,900
Tributary PO-3	0.3	2	6	2 of 3	-
Tributary PO-5	0.7	24	43	7 of 7	\$1,250,200
Tributary PO-6	1.0	28	31	9 of 9	\$1,444,900
Mesquite Branch	4.1	287	8	6 of 9	-
Town Branch	<u>2.4</u>	<u>120</u>	<u>140</u>	20 of 23	<u>\$6,542,100</u>
TOTAL	15.3	955	409	60 of 71	\$20,469,800

 ¹⁰⁰⁻Year Flood Plain determined with existing channels and bridges/culverts and flood dicharges based on future fully urbanized land use conditions and on existing channels/bridges.

TABLE IV-45 SUMMARY OF EXPECTED ANNUAL DAMAGES

Stream 1	Expected Anottal Damage without Improvements	Expected Annual Company Compan	Benefits/ Damage Reduced
Post Oak Creek - Reach 1	\$74,400	\$68,800	\$5600
Post Oak Creek - Reach 2	\$74,400	\$60,400	\$14,000
Post Oak Creek - Reach 3	\$74,400	\$71,200	\$2,700
Post Oak Creek - Reach 4	\$74,400	\$36,000	\$38,400
Post Oak Creek- (Reaches 1-4)	\$74,400	\$13,000	\$61,400
South Fork Tributary	\$104,900	\$0	\$104,900
Post Oak Tributary - 3	\$ 10	-	-
Post Oak Tributary - 5	\$135,800	\$1,000	\$134,800
Post Oak Tributary - 6	\$468,000	\$7,600	\$460,400
Mesquite Branch	\$28,000		-
Town Branch - Reach 1	\$194,500	\$148,400	\$46,100
Town Branch - Reach 2	\$194,500	\$158,200	36,300
Town Branch - Reach 3	\$194,500	\$159,200	\$35,300
Town Branch - Reach 4	\$194,500	\$167,900	\$26,600
Town Branch – (Reaches 1-4)	\$194,500	\$47,200	\$147,300

TABLE IV-46 SUMMARY OF CONCEPTUAL SOLUTIONS BENEFIT/COST RATIOS

Stream	Estimated Cost	Average Annual Cost (1)	Benefits (7)	Benefit/Cost
Post Oak Creek - Reach 1	\$3,592,400	\$284,400	\$5,600 (2 of 78 struct)	0.02
Post Oak Creek - Reach 2	\$3,417,300	\$271,600	\$14,000 (14 of 78 struct)	0.05
Post Oak Creek - Reach 3	\$756,200	\$60,100	\$2,700 (7 of 78 struct)	0.05
Post Oak Creek - Reach 4	\$980,800	\$77,900	\$38,400 (19 of 78 struct)	0.5
Post Oak Creek – (Reaches 1-4)	\$8,683,700	\$690,100	\$61,800 (39 of 74 struct)	0.09
South Fork Tributary	\$2,548,900	\$202,600	\$104,900 (16 of 16 struct)	0.5
Post Oak Tributary - 3			+	
Post Oak Tributary - 5	\$1,250,200	\$99,400	\$134,800 (31 of 32 struct)	1.4
Post Oak Tributary - 6	\$1,444,900	\$114,800	\$460,400 (10 of 18 struct)	4.0
Town Branch - Reach 1	\$1,415,200	\$112,500	\$46,100 (11 of 75 struct)	0.4
Town Branch - Reach 2	\$1,213,700	\$ 96,500	\$36,300 (20 of 75 struct)	0.4
Town Branch - Reach 3	\$2,139,000	\$170,000	\$35,300 (18 of 75 struct)	0.2
Town Branch - Reach 4	\$1,774,200	\$141,000	\$26,600 (13 of 75 struct)	0.2
Town Branch - (Reaches 1-4)	\$6,542,000	\$519,900	\$147,300 (63 of 75 struct)	0.3
Mesquite Branch	-			

⁽¹⁾Capital Recovery Factor based on 7.75% and 50 year.
⁽²⁾ Reduction of Average Annual Damages/ (Structures removed from 100-year flood plain)

V. RECOMMENDATIONS

A. INTRODUCTION

The recommended improvement plans that follow have been formulated and prioritized to reduce the potential flooding of buildings, bridges and culverts; minimize the impact on the natural flood plain environment; and provide practical and affordable solutions to render the most benefits for each tax-dollar expended.

B. RECOMMENDED IMPROVEMENTS

Halff Associates recommends the City investigate improvements described in Chapter IV for Post Oak Creek, Tributaries PO-3, Tributary PO-5, Tributary PO-6, Mesquite Branch and Town Branch. Halff Associates recommends the City implement the following improvements in the following order of priority:

- Structural improvements for Tributary PO-6 and Tributary PO-5 based on benefit/cost ratio as indicated on Table V-1.
- Structural improvements for South Fork Tributary including detention ponds. Although these improvements have a relatively low benefit to cost ratio as shown on Table V-1, the improvements remove 16 of 16 structures from the 100-year flood plain, and is, therefore, a feasible alternative.
- Structural improvements for Reach 4 of Post Oak Creek. These Reach 4 improvements benefit to cost ratio is relatively low as indicated in Table V-1, but the improvements remove 19 of 78 structures from the 100-year flood plain. The City could then consider purchasing the structures remaining in the 5-year to 100-year flood plain after the implementation of Reach 4 improvements as shown in Table V-2. Purchasing structures in the Post Oak Creek flood plain with no structural improvements should also be considered as shown on Table V-2.
- Structural improvements for Reaches 1 and 2 of Town Branch. These two reaches have relatively low benefit to cost ratios as shown on Table V-1, however, Reach 1 improvements remove 11 of 75 structures and Reach 2 improvements remove 20 of 75 structures. The City could then consider purchasing the structures remaining in the 5-year to 100-year flood plain after the implementation of Reaches 1 and 2 improvements as shown in Table V-2. Purchasing structures in the Town Branch flood plain with no structural improvements should also be considered.
- Purchasing the three structures inundated by the 100-year storm for Mesquite Branch is also cost effective as indicated on Table V-2.

TABLE V-1 Summary of Conceptual Improvements Structural Solutions

Stream	Estimated Cost	Average Annual Cost (1)	Benefits (2)	- Bencfit/Cost Ratio
Post Oak Creek - Reach 1	\$3,592,400	\$284,400	\$5,600 (2 of 78 struct)	0.02
Post Oak Creek - Reach 2	\$3,417,300	\$271,600	\$14,000 (14 of 78 struct)	0.05
Post Oak Creek - Reach 3	\$756,200	\$60,100	\$2,700 (7 of 78 struct)	0.05
Post Oak Creek - Reach 4	\$980,800	\$77,900	\$38,400 (19 of 78 struct)	0.5
Post Oak Creek – (Reaches 1-4)	\$8,683,700	\$690,100	\$61,800 (39 of 74 struct)	0.09
South Fork Tributary	\$2,548,900	\$202,600	\$104,900 (16 of 16 struct)	0.5
Post Oak Tributary - 3	-	-	-	
Post Oak Tributary - 5	\$1,250,200	\$99,400	\$134,800 (31 of 32 struct)	1.4
Post Oak Tributary – 6	\$1,444,900	\$114,800	\$460,400 (10 of 18 struct)	4.0
Town Branch - Reach 1	\$1,415,200	\$112,500	\$46,100 (11 of 75 struct)	0.4
Town Branch - Reach 2	\$1,213,700	\$96,500	\$36,300 (20 of 75 struct)	0.4
Town Branch - Reach 3	\$2,139,000	\$170,000	\$35,300 (18 of 75 struct)	0.2
Town Branch - Reach 4	\$1,774,200	\$141,000	\$26,600 (13 of 75 struct)	0.2
Town Branch – (Reaches 1-4)	\$6,542,000	\$519,900	\$147,300 (63 of 75 struct)	0.3
Mesquite Branch		***	_	

⁽¹⁾ Capital Recovery Factor based on 7.75% and 50 year.
(2) Reduction of Average Annual Damages / (Structures removed from 100-year flood plain)

TABLE V-2
Summary of Conceptual Improvements
Non-Structural Solutions

Stream	Estimated Cost	Average Annual Cost (1)	Benefits (2)	Benefit/Cost Ratio
Purchase Structures with FF below 5-year PO	\$ 246,970	\$19,600	\$27,000	1.4
Purchase Structures with FF below 10-year PO	\$581,100	\$46,200	\$38,600	0.8
Purchase Structures with FF below 5-year PO after Reach 4 improvements implemented	\$96,650	\$7,900	\$48,400	6.1
Purchase Structures with FF below 10-year PO after Reach 4 improvements implemented	\$230,500	\$18,300	\$53,300	2.9
Purchase Structures with FF below 100-year PO after Reach 4 improvements implemented	\$1,852,000	\$147,200	\$71,800	0.5
Purchase Structures with FF below 10-year PO-5	\$1,552,000	\$123,000	\$123,000	1.0
Purchase Structures with FF below 5-year PO-6	\$1,627,000	\$129,000	\$466,000	3.6
Purchase Structures with FF below 500-year PO-6	\$2,622,000	\$208,000	\$468,000	2.3
Purchase Structures with FF below 5-year Sfork	\$1,208,000	\$96,000	\$41,000	0.4
Purchase Structures with FF below 500-year Sfork	\$4,324,000	\$344,000	\$105,000	0.3
Purchase Structures with FF below 5-year TB	\$1,383,000	\$110,000	\$134,000	1.2
Purchase Structures with FF below 10-year TB	\$2,274,000	\$180,000	\$166,000	0.9
Purchase Structures with FF below 5-year TB after Reaches 1 & 2 improvements implemented	\$678,600	\$53,900	\$148,000	2.7
Purchase Structures with FF below 10-year TB after Reaches 1 & 2 improvements implemented	\$1,030,900	\$81,900	\$175,000	2.1
Purchase Structures with FF below 100-year TB after Reaches 1 & 2 improvements implemented	\$2,594,740	\$206,200	\$180,600	0.9
Purchase Structures with FF below 100-year MB	\$199,000	\$16,000	\$28,000	1.8

⁽¹⁾ Capital Recovery Factor based on 7.75% and 50 year.

C. EROSION CONTROL RECOMMENDATIONS

A visual reconnaissance of Post Oak Creek, South Fork of Post Oak Creek, Tributaries PO-3, Tributary PO-5, Tributary PO-6, Mesquite Branch and Town Branch revealed some areas of channel erosion. Some erosion problems identified in the study area are described in Chapter IV. Estimated costs for erosion control measures can vary depending upon site-

⁽²⁾ Reduction of Average Annual Damages.

specific conditions such as soil type, channel side slope, and the condition of existing structures.

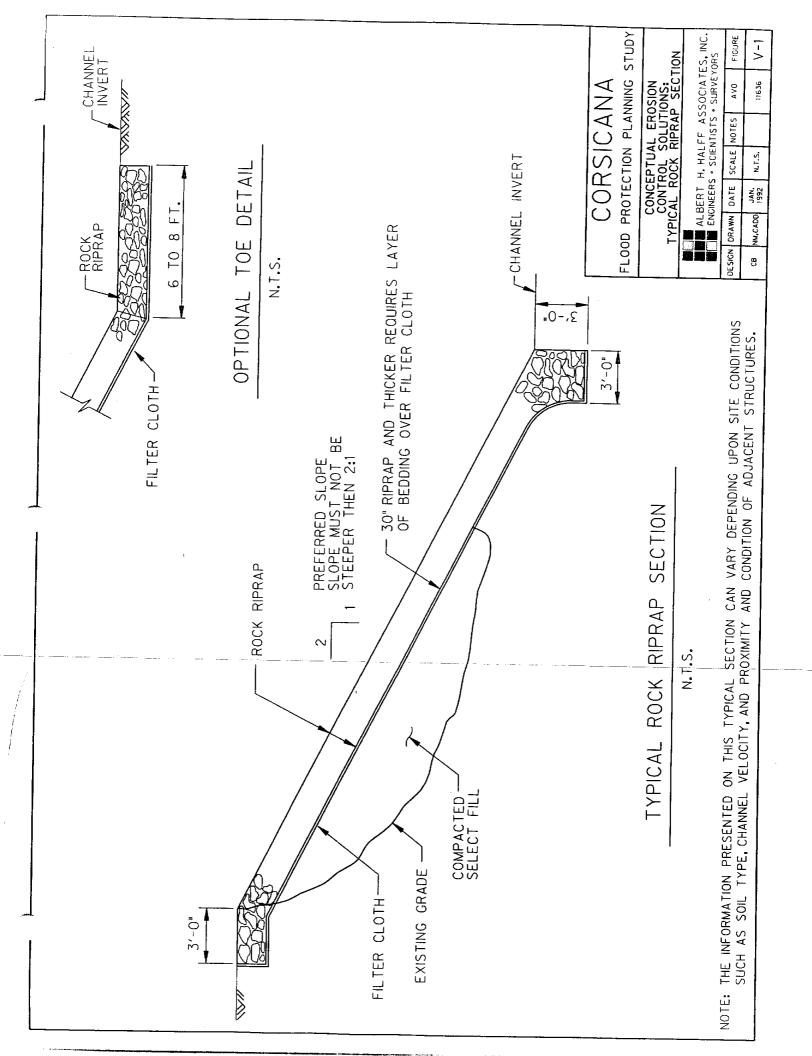
Erosion is a natural on-going process. As urbanization occurs in the Post Oak watershed, storm water runoff characteristics will change and subsequent erosion potential will increase. Halff Associates recommends the city perform a detailed annual inspection of all structures that are being undermined by flood waters to verify their structural integrity. During this time the City should also identify erosion damaged channel banks and trees where appropriate erosion protection (i.e. rock riprap or gabions) could prevent future erosion problems. Trees with root systems that have been severely weakened by erosion and subsequent chance of survival is slight, need to be removed.

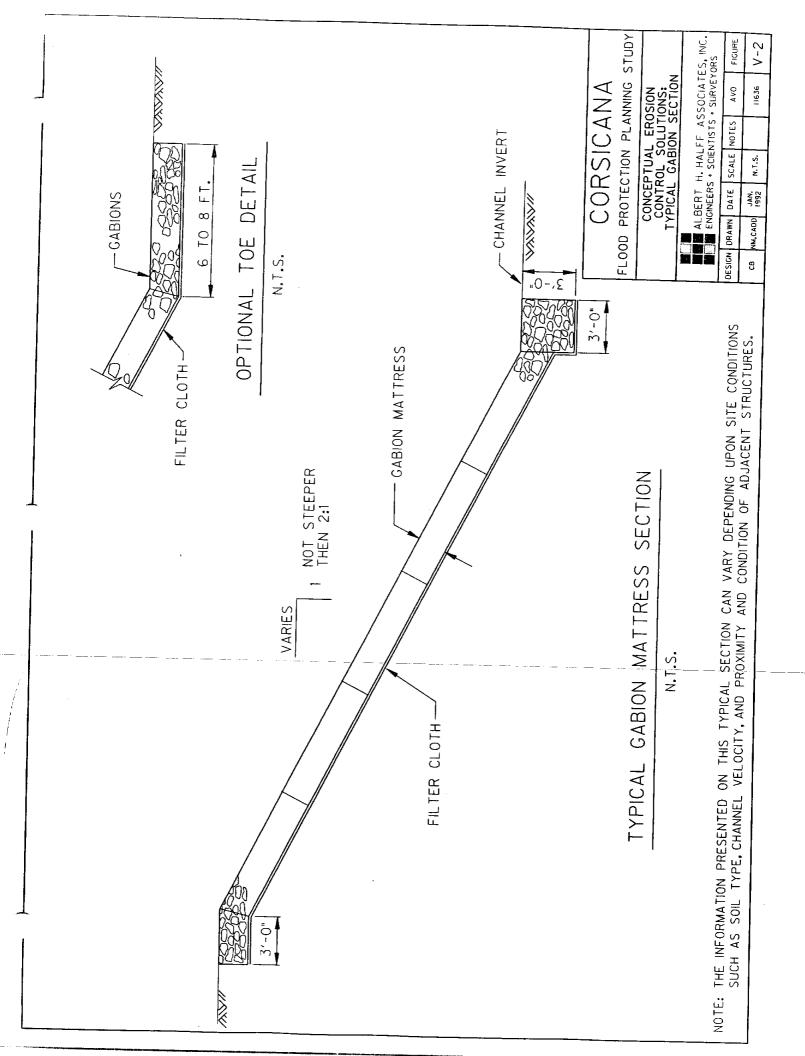
Table V-3 provides some general guidelines of required rock riprap and gabion thickness and estimated cost per linear feet for a range of channel velocities. City staff could use this information to help plan and budget future erosion remediation measures on a case by case basis.

TABLE V-3
Estimates of Probable Costs of Construction for Rock Riprap and Gabions
Channel Lining for Erosion Control

Channel Velocity (fps)	Rock Riprap Thickness	Gabion Thickness		Side Slo 5-ft and 10	Channel for Both Sides 2:1 opes for -ft Heights Fill Not Included)		
		5' Ht. Rock		10' Ht. Rock	5' Ht. Gabion	10' Ht. Gabion	
8	12"	9"	120	180	210	290	
10	18"	12"	150	230	250	340	
12	24"	12"	200	300	250	340	
14	30"	18"	310	375	330	420	
16	30"	18"	310	375	330	420	

Illustrations of typical sections for rock riprap and gabion erosion control measures are provided in Figures V-1 and V-2.





D. GENERAL WATERSHED RECOMMENDATIONS

- 1. To minimize land erosion and the subsequent sediment loading and siltation in the streams, the City should consider requiring large construction projects to be phased to limit the land area that is bare at any one time. Vegetation should be left undisturbed wherever possible. Graded areas should be replanted as soon as possible, and mulches should be used during periods that are not suitable for replanting. Hay bales and/or silt fences should be properly located and included in general construction plans and specifications.
- 2. Halff Associates recommends that the City of Corsicana inspect all channels periodically to identify potential stream obstructions before they occur. Fallen trees or trees whose root systems have been weakened by erosion need to be identified and removed. Periodic inspections should identify City controlled floodway areas in which siltation has decreased the flood-carrying capacity of the stream and culverts. The City should also consider removing existing fences which impede channel flows.
- 3. Natural vegetation should be preserved, where possible, in the channel and 20-feet beyond the top of the banks.
- 4. City flood plain zoning maps should be revised to correspond to the revised 100-year flood delineation at the appropriate time.
- 5. Stream crossings that are hazardous during floods with a return period of 100 years or less, should be marked with an active or passive flood warning system. Passive warning systems are feasible on lightly traveled streets where motorists are familiar with the area and at crossings with minor flooding. Active flood warning systems are necessary on heavily traveled thoroughfares. Guardrails should be installed at hazardous crossings where a vehicle may be washed off the road surface. Guardrails are also useful in indicating the edge of the trafficable road surface to pedestrians and motorists, where floodwaters may mask the location of the road surface. Tables IV-7, IV-16, IV-20, IV-24, IV-29, IV-34, and IV-38 provide pertinent information for each bridge/culvert in the Corsicana study area.
- 6. The City should continue with its present policy of monitoring new development and requiring developers to submit a detailed drainage study of existing (pre-development) and post-development conditions with corresponding hydrologic and/or hydraulic computer models. Halff Associates also recommends the City require an analysis for a full range of flood frequency events (minimum of 2-, 5-, 10-, 25-, 50-, and 100-year flood events), this is especially important in the development of an effective detention pond design.

E. BRIDGE AND CULVERT RATING PROGRAM

Halff Associates recommends that all bridges and culverts in the City of Corsicana be inspected and reviewed on a regular basis. The Texas Highway Department prioritizes bridge replacement based on a ranking number calculated for each crossing. The City of Corsicana should consider adopting a bridge and culvert rating program similar to the THD ranking system with consideration of flood safety criteria. Note, the costs for any increase in structure required to meet stricter requirements than that of TxDOT are expected to be borne by the entity requiring the stricter criteria. Coordination with TxDOT is recommended in the early planning process.

The following criterion could be used in conjunction with the THD bridge rating system for a city-wide evaluation of bridges and culverts:

Criterion 1	If the bridge or culvert is not structurally safe, it should be replaced.
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<u>Criterion 2</u> If a bridge is historically significant or aesthetically pleasing, it should be saved.

<u>Criterion 3</u> If a crossing is not adequate for the traffic that it must carry, it should be replaced.

Criterion 4 If flood depths or water velocities over a roadway are dangerous, and a warning system is impractical, the structure should be replaced.

Criterion 5 If a bridge or culvert constitutes an obstruction that causes upstream flooding, and if bridge replacement is less costly than right-of-way purchase of the flood-prone property, the structure should be replaced.

<u>Criterion 6</u> If a bridge need not be replaced on the basis of Criteria 1 through 5, and it met the design standards that were in force at the time of its construction, it should be retained.

<u>Criterion 7</u> If a culvert or bridge does not permit passage of the 100-year flood without overtopping, the City should consider replacing the structure.

F. CALIBRATION DATA FOR COMPUTER MODELS

In order to verify the hydrologic and hydraulic data generated by this report, Halff Associates recommends the City of Corsicana install staff gages at major flood prone bridges and install non-recording rain gauges in the watershed. These gages could be monitored by volunteers or city personnel during heavy rainfall and runoff periods. Installation of these gages will help establish long-term rainfall and runoff records for the City of Corsicana.

If funding permits, Halff Associates recommends that the City of Corsicana and the U.S.G.S. expand their stream and rainfall gaging program in the Post Oak Creek Watershed. Installation of automated recorders could provide the City with an active warning system for flood plain management. At the same time, the U.S.G.S. would be providing

hydrologists with the basic data they need to address the requirements for urban water quantity and quality problems.

G. UPDATING HYDROLOGIC AND HYDRAULIC COMPUTER MODELS

Included in this report are the computer data diskettes containing the hydrologic and hydraulic computer models used in the production of this report. These baseline models will enable the Corsicana City Engineering staff to predict effects of anticipated changes in land use and/or watershed characteristics upon flood levels using an IBM or compatible Personal Computer. Halff Associates recommends that the City of Corsicana require developers to provide updated "as-built" HEC-RAS hydraulic computer models as channel and/or flood plain conditions are modified. The HMS hydrologic computer model used in this report should be applicable for a fully developed watershed, provided development occurs as predicted by the future land use maps of the cities within the watershed.

H. FLOOD PLAIN MANAGEMENT POLICIES

Halff Associates recommends that the City of Corsicana consider adopting flood plain management policies similar to the North Central Texas Council of Governments Flood plain Management Policies described in Chapter III. This would allow the City the ability to regulate: allowable rises in water surface due to development; limitation of velocity increases for erosion control, and preservation of existing/natural flood plain land.

It is further recommended that the City of Corsicana formally adopt the flood levels shown in this report for its flood plain management program. The City has been provided with hydrologic and hydraulic computer models of the entire watershed.

APPENDIX A

References

APPENDIX A

REFERENCES

- 1. 1998-1999 Texas Almanac, The Dallas Morning News, Dallas, Texas.
- 2. <u>Post Oak Creek, Corsican, Texas, Reconnaissance Report,</u> U.S. Army Corps of Engineers, Fort Worth District, Fort Worth, Texas, October 1991.
- 3. <u>HEC Hydrologic Modeling System (HMS) Version 2.0</u>, U.S. Army Corps of Engineers, Hydrologic Engineering Center, Davis, California, March 1990.
- 4. Existing Land Use Map for City of Corsicana, Texas, Kindle Stone & Associates, Inc., Longview Texas, 1984.
- 5. Master Drainage Study, City of University Park, Prepared by Halff Associates, Inc., 1980.
- 6. <u>Soil Survey of Navarro County, Texas</u>, United State Department of Agriculture Soil Conservation Service, December 1974.
- 7. SCS National Engineering Handbook, Section 4, Hydrology, United States Department of Agriculture Soil Conservation Service, 1969.
- 8. NUDALLAS Documentation and Supporting Appendices, U.S. Army Corps of Engineers, Fort Worth, Texas, September 1986.
- 9. <u>Hydrology and Hydraulic of Flood Plain Studies for the City of Dallas</u>, prepared by Halff Associates, January 1976.
- 10. <u>Technical Paper No. 40, Rainfall Frequency Atlas of the United States</u>, National Weather Service, May 1961.
- 11. <u>Technical Memorandum HYDRO-35</u>, National Oceanic and Atmospheric Administration, June 1977.
- 12. <u>HEC-RAS River Analysis System Version 2.2</u>, U.S. Army Corps of Engineers, Hydrologic Engineering Center, Davis, California, September 1998.
- Flood Insurance Study, Town of Corsicana, Texas, Navarro Counties, prepared for the Federal Emergency Management Agency by the U.S. Army Corps of Engineers, Fort Worth District, Fort Worth, Texas, August 17, 1981.
- 14. Flood-Loss Prevention in Bachman Branch Basin, Dallas, Texas, Prepared by Halff Associates, Inc., June 15, 1969.

APPENDIX A (Continued)

REFERENCES

- 15. Physical and Economic Feasibility of Non-Structural Flood Plain Management Measures, U.S. Army Corps of Engineers, Hydrologic Engineering Center, March 1978.
- 16. Aquifer Recharge Utilizing Playa Lake Water and Filter Underdrains, Phase IV, Lloyd V. Urban, B.J. Claborn, R.H. Ramsey, Texas Tech University, Water Resources Center, January 1988.
- 17. <u>Design of Small Dams</u>, United States Department of the Interior, Bureau of Reclamation, 1973.
- 18. Results of the Nationwide Urban Runoff Program, United States Environmental Protection Agency, Water Planning Division WH-554, December 1983.
- 19. Rowlett Creek Interjurisdictional Watershed Management Program, North Central Texas Council of Governments, Flood plain Management Policies for the Cities of Allen, Dallas, Garland, McKinney, Plano, and Richardson, Texas, January 1985.
- 20. <u>Detailed Project Report for Flood Control, Post Oak Creek, Corsicana, Texas</u>, U.S. Army Corps of Engineers, Fort Worth District, Fort Worth, Texas, June 1978.
- 21. <u>HEC Flood Damage Analysis with Risk (FDA) Version 1.2</u>, U.S. Army Corps of Engineers, Hydrologic Engineering Center, Davis, California, March 2000.

APPENDIX B

Vertical Control Benchmarks

APPENDIX C

Preliminary Estimates of Probable Costs

CITY OF CORSICANA FLOOD PROTECTION PLANNING STUDY

Proposed Channel Improvements for Post Oak Creek Reach 1 - Downstream of N. Burnert Street to W. 7th Street (stream stations 249+40 to 295+53) STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Eventuation (4575 L.5)	22500			
2	Unclassified Channel Excavation (4575 LF)	86500	CY	\$15.00	\$1,297,500
	Seed and Fertilize Earthen Channel	65000	SY	\$2.00	\$130,000
3	Five - 12'x7' CBCs at N. Burnert St.	225	CY	\$500.00	\$112,500
4	Remove & Dispose exist 5-84" at N. Burnert St.	1	LS	\$5,000.00	\$5,000
5	Sawcut for Removal of Asphalt or Concrete	200	LF	\$2.50	\$500
6	Remove & Dispose exist. Bridge at Chatfield	5000	SF	\$10.00	\$50,000
7	Bridge at Chatfield (250' span)	12500	SF	\$50.00	\$625,000
8	24" Rock RipRap Channel Transitions	745	CY	\$100.00	\$74,500
9	Asphalt Pavement Repair	550	SY	\$50.00	\$27,500
10	Clearing and Grubbing	1	LS	\$15,000.00	
11	Mobilization	1	LS	\$20,000.00	\$15,000 \$20,000
12	Utility Adjustment	1	LS	\$200,000.00	\$20,000
	SUBTOTAL			\$200,000.00	\$200,000
			,		\$2,557,500
	20% Contingency				
					\$511,500
	SUBTOTAL (Construction)				\$3,069,000
	459/ Engineering Committee 2.0				
	15% Engineering, Surveying, & Construction Man.	agement			\$460,350
	TOTAL			_	\$3,529,400

This cost estimate does not include cost of right of way/easement aquisition

This statement was prepared utilizing standard cost estimate practices. It is understood and agreed that this is an estimate only, and the Engineer shall not be liable to owner or to a third party for any failure to accurately estimate the cost of the project, or any part therof.

Proposed Channel Improvements for Post Oak Creek Reach 2 - Downstream of N. Beaton Street to Upstream of N. 13th Street (stream stations 314+92 to 334+24) STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Excavation (1930 LF)	66500	CY	£45.00	0007.500
2	Seed and Fertilize Earthen Channel	23050	SY	\$15.00	\$997,500
3	Sawcut for Removal of Asphalt or Concrete	300	LF	\$2.00	\$46,100
4	Remove & Dispose exist. Bridge at Main Street	7500	SF	\$2.50	\$750
5	Bridge at Main Street (250' span)	12500	SF	\$10.00	\$75,000
6	Purch 4 Structs bt Main & 13th	12300	LS	\$50.00	\$625,000
7	Other costs associated with structure purchase	1		\$260,000	\$260,000
8	24" Rock RipRap Channel Transitions	1120	LS	\$130,000	\$130,000
9	Clearing and Grubbing	1120	CY	\$100.00	\$112,000
10	Mobilization	1	LS	\$5,000.00	\$5,000
11	Utility Adjustment	1	LS	\$25,000.00	\$25,000
,,	ounty / tojusurion	1	LS	\$200,000	\$200,000
	SUBTOTAL				\$2,476,350
	20% Contingency				\$405.270
	SUBTOTAL (construction)			-	\$495,270 \$2,971,600
					ΨΔ,311,000
	15% Engineering, Surveying, & Construction Man	agement			\$445,740
	TOTAL			_	\$3,417,300

This cost estimate does not include cost of right of way/easement aquisition

Proposed Channel Improvements for Post Oak Creek Reach 3 - N. 13th Street to 1690' upstream of Oaklawn Drive (stream stations 334+24 to 368+00)

STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Excavation (3375 LF)				
2	Seed and Fertilize Earthen Channel	23000	CY	\$15.00	\$345,000
3	24" Rock RipRap Channel Transitions	43500	SY	\$2.00	\$87,000
4	Clearing and Grubbing	5 6 0	CY	\$100.00	\$56,000
5	Mobilization	1	LS	\$5,000.00	\$5,000
6	Utility Adjustment	1	LS	\$5,000.00	\$5,000
Ū	Junty Adjustitient	1	LS	\$50,000.00	\$50,000
	SUBTOTAL				
	,				\$548,000
	20% Contingency				
	SUBTOTAL (construction)				\$109,600
	, , , , , , , , , , , , , , , , , , , ,				\$657,600
	15% Engineering, Surveying, & Construction Mai	2000			
	TOTAL	iayement		_	\$98,640
					\$756,200

This cost estimate does not include cost of right of way/easement aquisition

\$64,000

\$90,000

\$5,000

\$27,500

\$37,500

\$5,000

\$10,000

\$15,000

\$250

CITY OF CORSICANA FLOOD PROTECTION PLANNING STUDY

Proposed Channel Improvements for Post Oak Creek Reach 4 - 1690' Upstream Oaklawn Drive to Dobbins Road (stream stations 368+00 to 392+85) STATEMENT OF PROBABLE COST

Item No. Description Quantity Unit Price Amount Unclassified Channel Excavation (2485 LF) 1 26100 Seed and Fertilize Earthen Channel CY 2 \$15.00 \$391,500 32000 SY 3 Three - 12'x9' CBC's at Dobbins \$2.00 180 4 Remove & Dispose exist 12x9 CBC at Dobbins CY \$500.00 1 Sawcut for Removal of Asphalt or Concrete 5 L\$ \$5,000.00 100 LF 6 Asphalt Pavement Repair \$2.50 550 7 SY 24" Rock RipRap Channel Transitions \$50.00 375 CY 8 Clearing and Grubbing \$100.00 1 LS 9 Mobilization \$5,000.00 1 LS 10 Landscape Repair \$10,000.00 1,500 LF 11 **Utility Adjustment** \$10.00 1 LS \$65,000 \$65,000

20% Contingency	\$710,750
SUBTOTAL (construction)	\$142,150
,	\$852,900
15% Engineering, Surveying, & Construction Management TOTAL	\$127,935 ···
	\$980,800

This cost estimate does not include cost of right of way/easement aquisition

SUBTOTAL

Proposed Channel Improvements for South Fork Tributary

STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Excavation (2255 LF)	8500	CY	\$ 15.00	\$127,500
2	Seed and Fertilize Earthen Channel	22000	SY	\$2.00	\$44,000
3	Five - 10'x6' CBC's at Bowie	200	CY	\$500.00	\$100,000
4	Three - 10'x8' CBC's at Paloma	155	CY	\$500.00	\$77,500
5	Remove & Dispose exist. 20x4.5 at Bowle	1	LS	\$5,000.00	\$5,000
6	Remove & Dispose exist. 20x8 at Paloma	1	LS	\$5,000.00	\$5,000
7	Sawcut for Removal of Asphalt	200	LF	\$2.50	\$500
8	Asphalt Pavement Rapair	1,100	SY	\$50.00	\$55,000
9	Excavate Exist. Pond for Detention	25000	CY	\$10.00	\$250,000
10	Excavate Prop 80 ac-ft Dentention Pond	90000	CY	\$10.00	\$900,000
11	Proposed outlet structures for Det. Ponds	1	LS	\$60,000.00	\$60,000
12	Seeding for Proposed Detention Ponds	65000	SY	\$1.50	\$97,500
13	24" Rock RipRap Channel Transitions	350	CY	\$100.00	\$35,000
14	Clearing and Grubbing	1	LS	\$10,000.00	\$10,000
15	Mobilization	1	LS	\$25,000.00	\$25,000
16	Landscape Repair	3,000	LF	\$10.00	\$30,000
17	Utility Adjustment	1	LS	\$25,000.00	\$25,000
	SUBTOTAL				\$1,847,000
	20% Contingency				\$369,400
	SUBTOTAL (construction)		•	•	\$2,216,400
	15% Engineering, Surveying, & Construction	Management			\$332,460
	TOTAL	•		•	\$2,548,900

This cost estimate does not include cost of right of way/easement acquisition

Proposed Channel Improvements for Tributary PO-5

STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
4	Understand Channel Expenses (000 LE)	2600	CY	\$15.00	\$39,000
1	Unclassified Channel Excavation (900 LF)	5700	SY	\$15.00 \$2.00	\$39,000 \$11,400
2	Seed and Fertilize Earthen Channel	160	CY	\$500.00	\$80,000
3	Three - 12'x6' CBC's at Royal Lane	140	CY	\$500.00 \$500.00	\$70,000
4	Three - 9'x5' CBC's at Northwood				
5	Two - 10'x9' CBC's at RR	130	CY	\$500.00	\$65,000 \$60,000
6	Two - 9'x6' CBC's at Madison	120	CY	\$500.00	\$60,000 \$60,000
7	Two - 10'x7' CBC's at Dobbins	120	CY	\$500.00	\$60,000
8	Three - 9'x5' CBC's at Fish Tank	140	CY	\$500.00	\$70,000
9	Remove & Dispose exist. 2-60" at Royal	1	LS	\$5,000.00	\$5,000 \$5,000
10	Remove & Dispose exist. 2-60" at Northwood	1	LS	\$5,000.00	\$5,000 \$5,000
11	Remove & Dispose exist. 1-10' CMP at RR	1	LS	\$5,000.00	\$5,000
12	Remove & Dispose exist. 3-48" at Madison	1	LS	\$5,000.00	\$5,000
13	Remove & Dispose exist. 2-8x4 at Dobbins	1	LS	\$5,000.00	\$5,000
14	Remove & Dispose exist. 4-42" at Fish Tank	1	LS	\$5,000.00	\$5,000
15	Reconstruct Railroad	150	LF	\$200.00	\$30,000
16	Sawcut for Removal of Asphalt	600	LF	\$2.50	\$1,500
17	Asphalt Pavement Repair	3500	SY	\$50.00	\$175,000
18	24" Rock RipRap Channel Transitions	850	CY	\$100.00	\$85,000
19	Clearing and Grubbing	1	LS	\$1,000.00	\$1,000
20	Mobilization	1	LS	\$10,000.00	\$10,000
21	Landscape Repair	1,800	LF	\$10.00	\$18,000
22	Utility Adjustment	1	LS	\$100,000.00	\$100,000
	SUBTOTAL				\$905,900
	20% Contingency				\$181,180
	SUBTOTAL (construction)				\$1,087,100
	15% Engineering, Surveying, & Construction M	lanagement			\$163,065
	TOTAL	•			\$1,250,200

This cost estimate does not include cost of right of way/easement acquisition

Proposed Channel Improvements for Tributary PO-6

STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Excavation (1500 LF)	2900	CY	\$15.00	\$43,500
2	Seed and Fertilize Earthen Channel	11500	SY	\$2.00	\$23,000
3	Four - 10'x5' CBC's at Fish Tank	150	CY	\$500.00	\$75,000
4	Four - 10'x5' CBC's at Edgewood	150	CY	\$500.00	\$75,000
5	Four - 10'x5' CBC's at McKinney	150	CY	\$500.00	\$75,000
6	Three - 8'x4' CBC's at Louis	140	CY	\$500.00	\$70,000
7	Three - 8'x4' CBC's at Lakewood	140	CY	\$500.00	\$70,000
8	Three - 8'x4' CBC's at FM 3383	140	CY	\$500.00	\$70,000
9	Remove & Dispose exist. 2-48" at Fish Tank	1	LS	\$5,000.00	\$5,000
10	Remove & Dispose exist. 3-36" at Edgewood	1	LS	\$5,000.00	\$5,000
11	Remove & Dispose exist. 3-36" at McKinney	1	LS	\$5,000.00	\$5,000
12	Remove & Dispose exist. 3-36" at Louis	1	LS	\$5,000.00	\$5,000
13	Remove & Dispose exist. 2-36" at Lakewood	1	LS	\$5,000.00	\$5,000
14	Remove & Dispose exist. 1-4x4 at FM 3383	1	LS	\$5,000.00	\$5,000
15	Sawcut for Removal of Asphalt	600	LF	\$2.50	\$1,500
16	Asphalt Pavement Repair	3500	SY	\$50.00	\$175,000
17	24" Rock RipRap Channel Transitions	800	CY	\$100.00	\$80,000
18	Clearing and Grubbing	1	LS	\$2,000.00	\$2,000
19	Mobilization	1	LS	\$10,000.00	\$10,000
20	Landscape Repair	3,000	LF	\$10.00	\$30,000
21	Purchase 620 Edgewood	1	LS	\$78,000.00	\$78,000
22	Other costs associated with structure purchase	1	LS	\$39,000.00	\$39,000
23	Utility Adjustment	1	LS	\$100,000.00	\$100,000
	SUBTOTAL	···			\$1,047,000
	20% Contingency				\$209,400
	SUBTOTAL (construction)			•	\$1,256,400
	15% Engineering, Surveying, & Construction Mar	nagement			\$188,460
	TOTAL			•	\$1,444,900

This cost estimate does not include cost of right of way/easement acquisition

Proposed Channel Improvements for Town Branch Reach 1 - Chicago & Rock Islan Railroad to S. Beaton Street (stream station 26+82 to 45+04) STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Excavation (1820 LF)	12000	0.4	A 4	
2	Seed and Fertilize Earthen Channel	13000	CY	\$15.00	\$195,000
3	Two - 10' CMP at Chicago RR (salvage ex. 2)	19000	SY	\$2.00	\$38,000
4	Four - 11'x8' CBC's at 7th	130	LF	\$500.00	\$65,000
5	Four - 11'x7' CBC's at 9th	260	CY	\$500.00	\$130,000
6		250	CY	\$500.00	\$125,000
7	Remove & Dispose exist. 2-10x7's at 7th	1	LS	\$5,000.00	\$5,000
. 8	Remove & Dispose exist. 2-74" 's at 9th	1	LS	\$5,000.00	\$5,000
	Reconstruct Chicago RR	150	LF	\$200.00	\$30,000
9	Sawcut for Removal of Asphalt	200	LF	\$2.50	\$500
10	Asphalt Pavement Repair	1100	SY	\$50.00	\$55,000
11	24" Rock RipRap Channel Transitions	700	CY	\$100.00	\$70,000
12	Clearing and Grubbing	1	LS	\$2,000.00	\$2,000
13	Mobilization	1	LS	\$10,000.00	\$10,000
14	Purchase Structures US of 7th	1	LS	\$130,000.00	\$130,000
- 15	Other costs associated with structure purchase	1	LS	\$65,000.00	\$65,000
16	Utility Adjustment	1	LS	\$100,000.00	\$100,000
	SUBTOTAL				\$1,025,500
	20% Contingency				\$205,100
	SUBTOTAL (Construction)				\$1,230,600
	15% Engineering, Surveying, & Construction Man TOTAL	agement			\$184,590 \$1,415,200

This cost estimate does not include cost of right of way/easement acquisition

Proposed Channel Improvements for Town Branch Reach 2 - S. 12th Street to S. 16th Street (stream stations 54+40 to 71+98) STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Excavation (1760 LF)	19500	CY	\$15.00	\$292,500
2	Seed and Fertilize Earthen Channel	20000	SY	\$2.00	\$40,000
3	Five - 12'x7' CBC's at 15th	225	CY	\$500.00	\$112,500
4	Two - 10'x5' CBC's at 16th (Salvage exist. 2)	110	CY	\$500.00	\$55,000
5	Remove & Dispose exist. 2-10x6 at 15th	1	LS	\$5,000.00	\$5,000
6	Sawcut for Removal of Asphalt	200	LF	\$2.50	\$500
7	Asphalt Pavement Repair	1100	SY	\$50.00	\$55,000
8	24" Rock RipRap Channel Transitions	550	CY	\$100.00	\$55,000
9	Clearing and Grubbing	1	LS	\$2,000.00	\$2,000
10	Mobilization	1	LS	\$10,000.00	\$10,000
11	Landscape Repair	700	LF	\$10.00	\$7,000
12	Purchase 3 Structures by 15th	1	LS	\$97,000.00	\$97,000
13	Other costs associated with structure purchase	1	LS	\$48,000.00	\$48,000
14	Utility Adjustment	1	LS	\$100,000.00	\$100,000
	SUBTOTAL				\$879,500
	20% Contingency				\$175,900
	SUBTOTAL (Construction)				\$1,055,400
	15% Engineering, Surveying, & Construction Ma	nagement			\$158,310
	TOTAL				\$1,213,700

This cost estimate does not include cost of right of way/easement acquisition

Proposed Channel Improvements for Town Branch Reach 3 - S. 16th Street to W. 7th Avenue (stream stations 71+98 to 91+85) STATEMENT OF PROBABLE COST

Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Excavation (1990 LF)	10000	CY	\$15.00	\$150,000
2	Seed and Fertilize Earthen Channel	16500	SY	\$2.00	\$33,000
3	Five - 11'x5' CBC's at 11th	200	CY	\$500.00	\$100,000
4	Four - 12'x7' CBC's at 10th	190	CY	\$500.00	\$95,000
5	Four - 10'x6' CBC's at 9th	170	CY	\$500.00	\$85,000
6	Four - 10'x6' CBC's at St. Louis RR	170	CY	\$500.00	\$85,000
7	Four - 10'x6' CBC's at 7th 240 If	800	CY	\$500.00	\$400,000
8	Remove & Dispose exist. 2-10x4.5 at 11th	1	LS	\$5,000.00	\$5,000
9	Remove & Dispose exist. 2-9x6 at 10th	1	LS	\$5,000.00	\$5,000
10	Remove & Dispose exist. 2-9x5.5 at 9th	1	LS	\$5,000.00	\$5,000
11	Remove & Dispose exist. 3-6x5 at RR	1	LS	\$5,000.00	\$5,000
12	Remove & Dispose exist. 1-10.5x5 at 7th	1	LS	\$5,000.00	\$5,000
13	Reconstruct St. Louis RR	200	LF	\$200.00	\$40,000
14	Sawcut for Removal of Asphalt	400	LF	\$2.50	\$1,000
15	Asphalt Pavement Repair	2500	SY	\$50.00	\$125,000
16	24" Rock RipRap Channel Transitions	1100	CY	\$100.00	\$110,000
17	Clearing and Grubbing	1	LS	\$3,000.00	\$3,000
18	Mobilization	1	LS	\$15,000.00	\$15,000
19	Landscape Repair	3,500	LF	\$10.00	\$35,000
20	Purchase 4 Structures between 16th & 11th	1	LS	\$35,000.00	\$35,000
21	Other costs associated with structure purchase	1	LS	\$18,000.00	\$18,000
22	Purchase Structure on culvert at 7th Avenue	1	LS	\$30,000.00	\$30,000
23	Other costs associated with structure purchase	1	LS	\$15,000.00	\$15,000
24	Utility Adjustment	1	LS	\$150,000.00	\$150,000
	SUBTOTAL				\$1,550,000
	20% Contingency			•	\$310,000
	SUBTOTAL (Construction)				\$1,860,000
	15% Engineering, Surveying, & Construction Ma	nagement			\$279,000
	TOTAL				\$2,139,000

This cost estimate does not include cost of right of way/easement acquisition

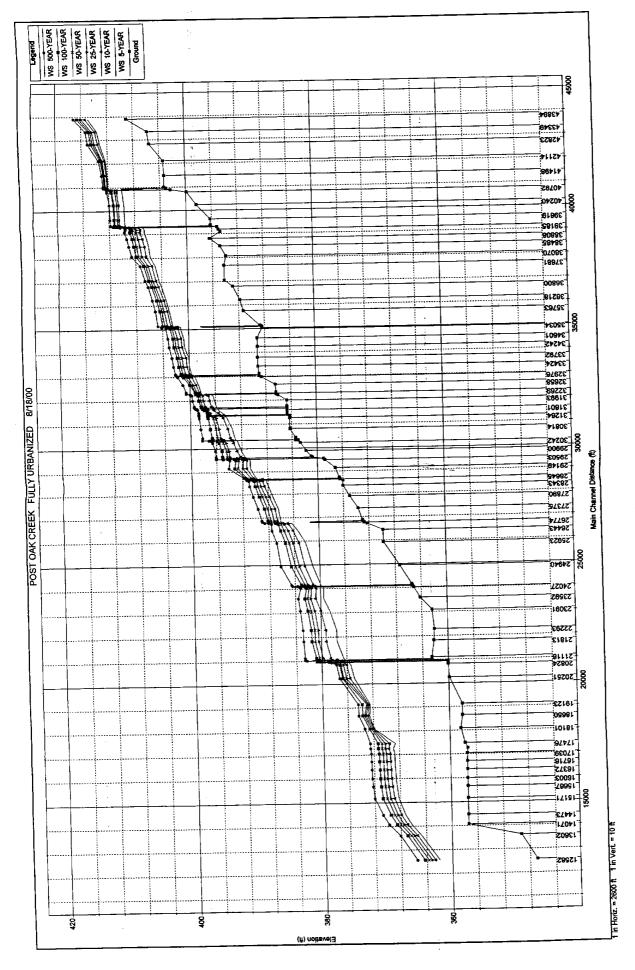
Proposed Channel Improvements for Town Branch Reach 4 - W. 6th Avenue to Study Limits (stream stations 106+00 to 128+07) STATEMENT OF PROBABLE COST

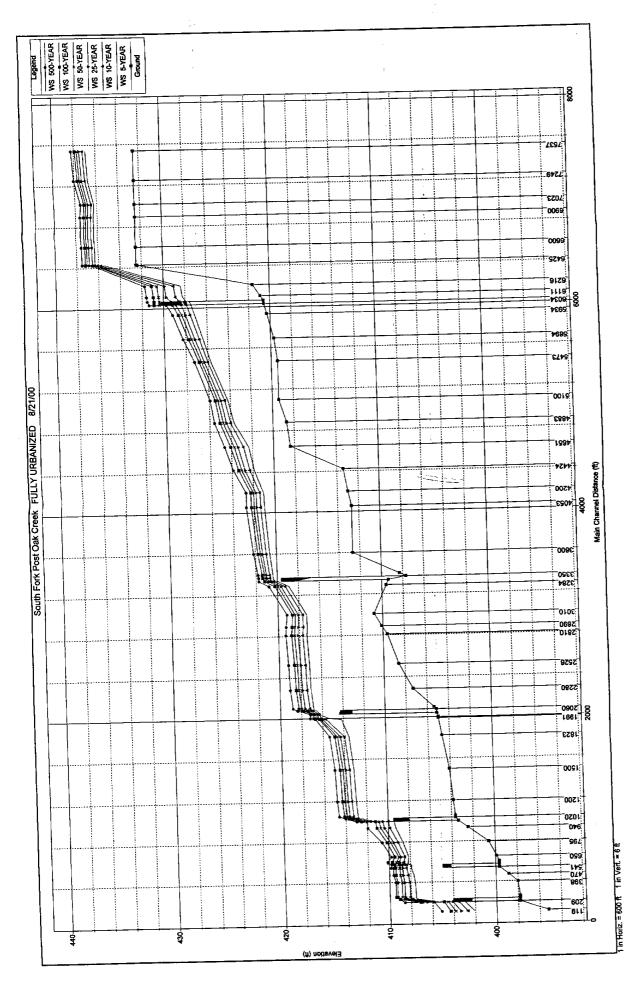
Item No.	Description	Quantity	Unit	Price	Amount
1	Unclassified Channel Excavation (1335 LF)	7000	CY	\$15.00	\$105,000
2	Seed and Fertilize Earthen Channel	8600	SY	\$2.00	\$17,200
3	Three - 10'x4' CBC's at 6th 220 lf	500	ÇY	\$500.00	\$250,000
4	Three - 12'x4' CBC's at Collins 282 If	650	CY	\$500.00	\$325,000
5	Three - 8'x4' CBC's at 23 1/2 St	140	CY	\$500.00	\$70,000
6	Three - 7'x4' CBC's at 24th St	110	CY	\$500.00	\$55,000
7	Remove & Dispose Ex 2-36",10x5arch, 2-48" @6th	1	LS	\$10,000.00	\$10,000
8	Remove & Dispose exist. 1-12x4 & 2-48" at Collins	1	LS	\$10,000.00	\$10,000
9	Remove & Dispose exist. 2-36" RCP's at 23 1/2 St	1	LS	\$5,000.00	\$5,000
10	Remove & Dispose exist. 1-5.5x3 at 24th St.	1	LS	\$5,000.00	\$5,000
11	Sawcut for Removal of Asphalt	600	LF	\$2.50	\$1,500
12	Asphalt Pavement Repair	3500	SY	\$50.00	\$175,000
13	24" Rock RipRap Channel Transitions	900	CY	\$100.00	\$90,000
14	Clearing and Grubbing	1	LS	\$2,000.00	\$2,000
15	Mobilization	1	LS	\$15,000.00	\$15,000
16	Landscape Repair	2,500	LF	\$10.00	\$25,000
17	Purchase 1Structures by 24th	1	LS	\$10,000.00	\$10,000
18	Other costs associated with structure purchase	1	LS	\$5,000.00	\$5,000
19	Utility Adjustment	1	LS	\$110,000.00	\$110,000
	SUBTOTAL				\$1,285,700
	20% Contingency				\$257,140
	SUBTOTAL (Construction)				\$1,542,800
	15% Engineering, Surveying, & Construction Manag	ement			\$231,420 \$1,774,200

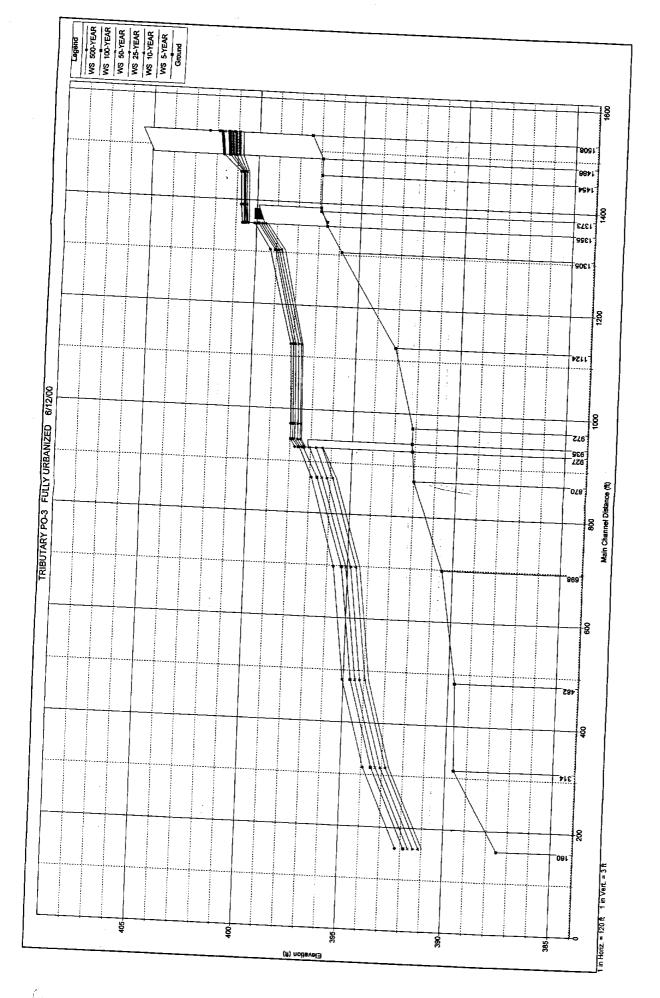
This cost estimate does not include cost of right of way/easement acquisition

APPENDIX D

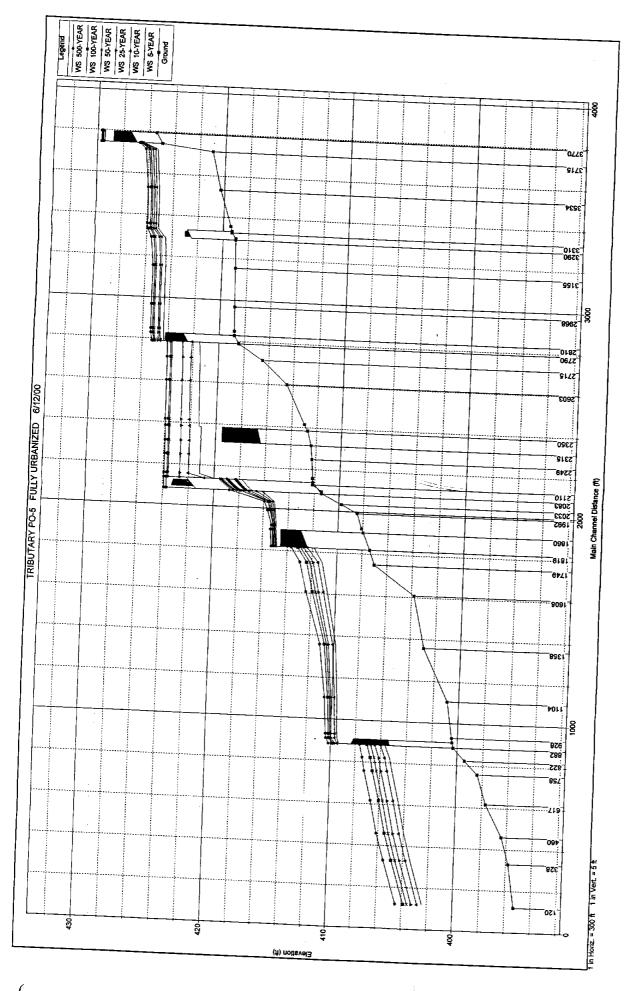
Drainage Area Map, 100-Year Flood Plain Maps and Flood Profiles (24" x 36" maps are bound separate of this report) BASELINE CONDITIONS
(Existing Channel and Bridge/Culverts with Future Peak Discharges)





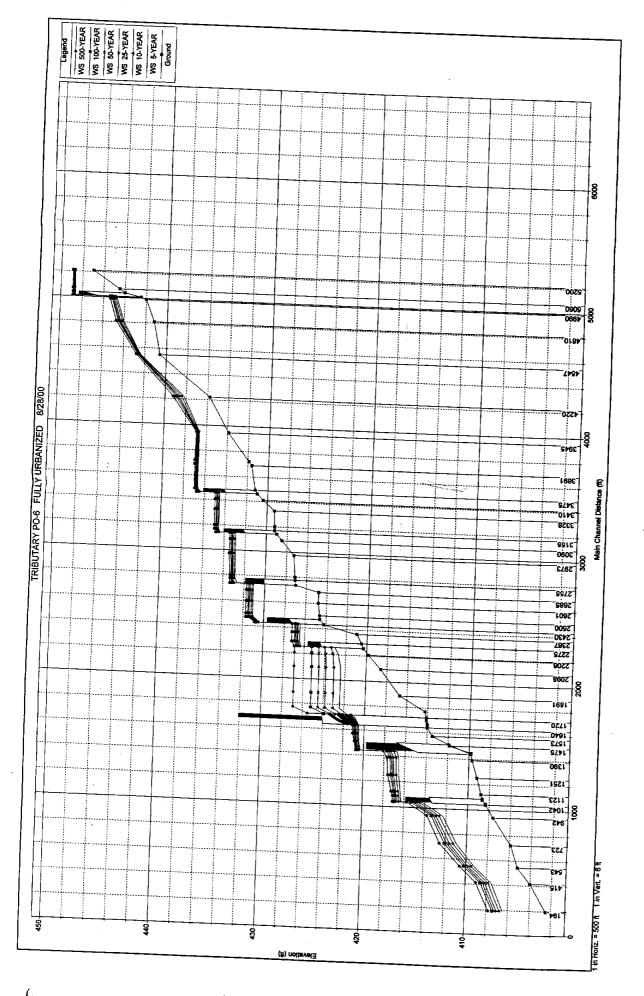


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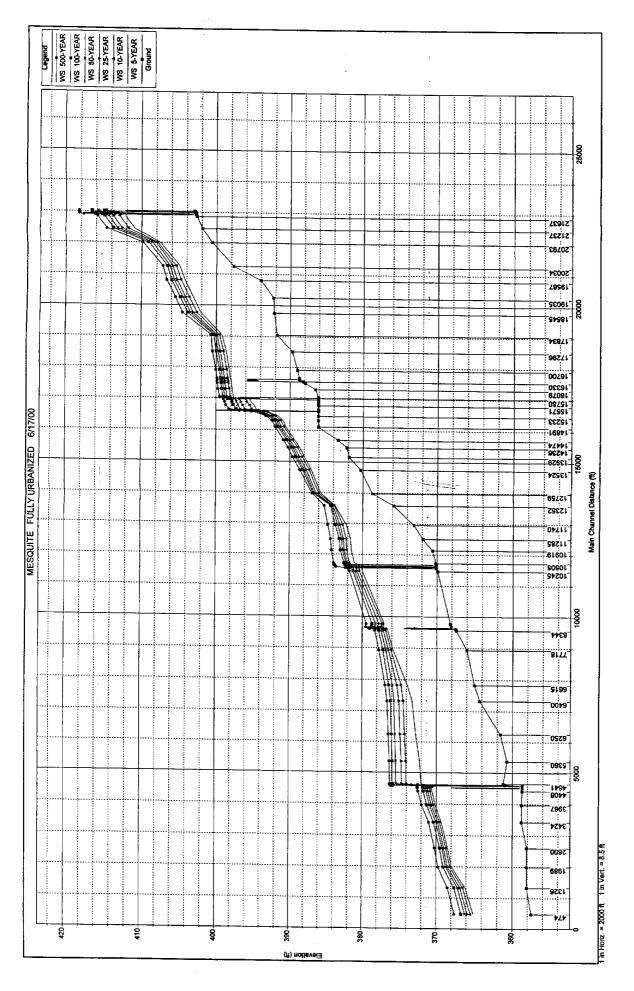


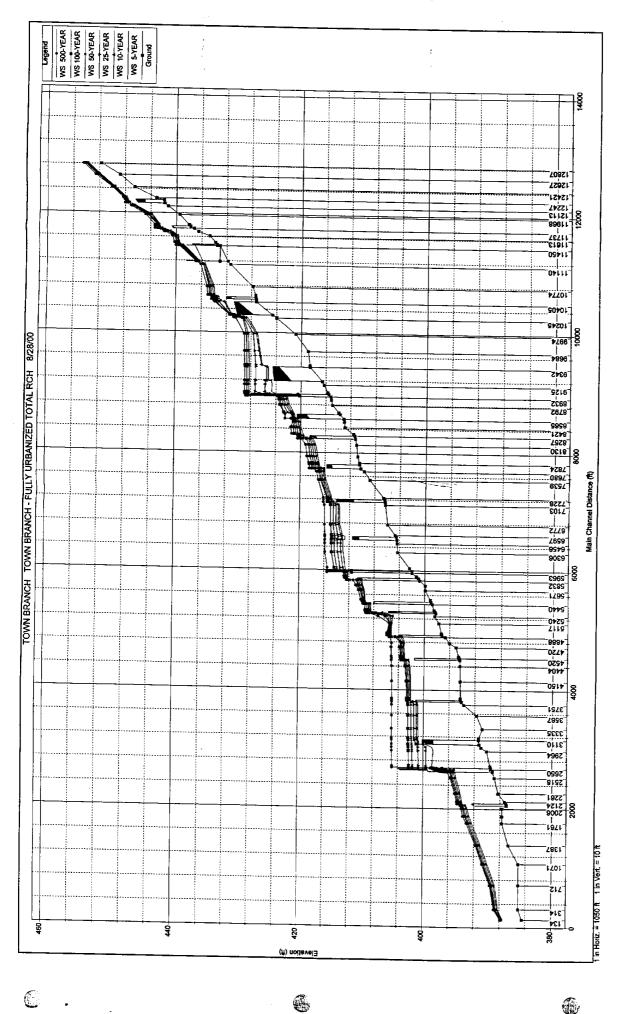
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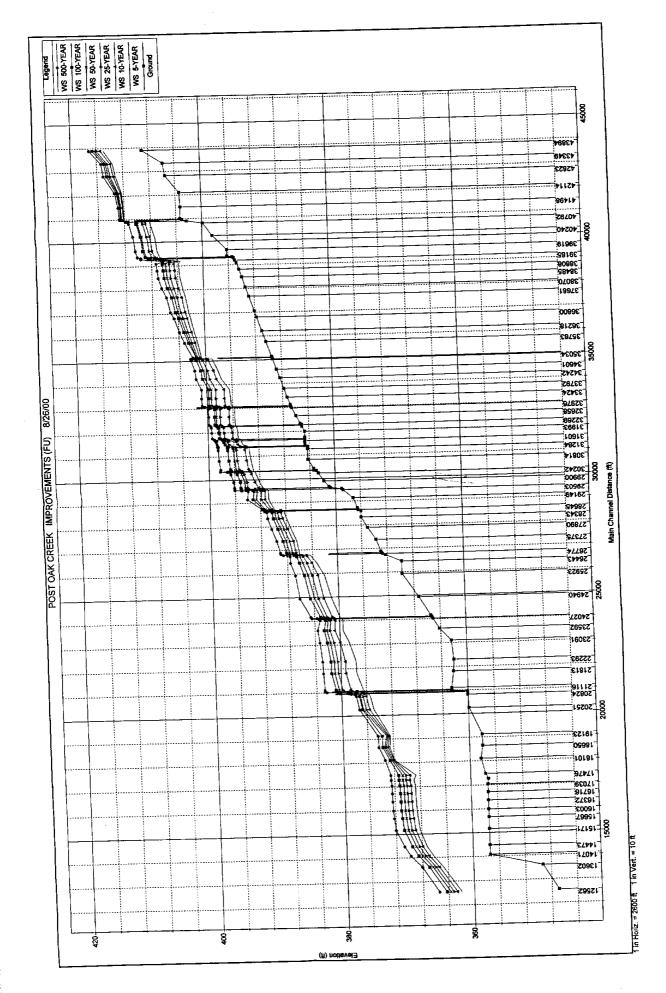
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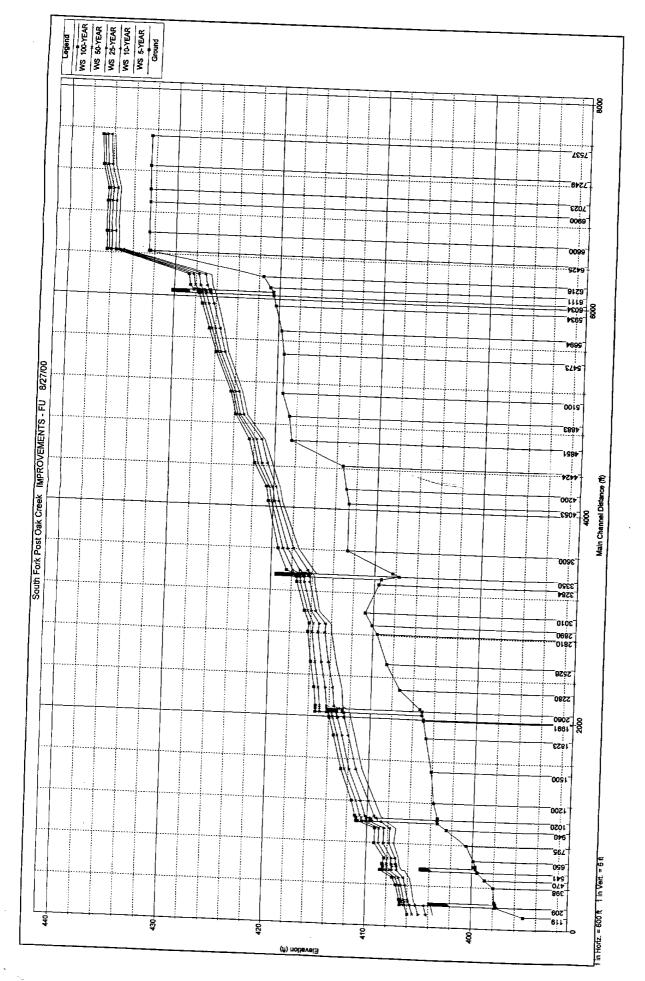


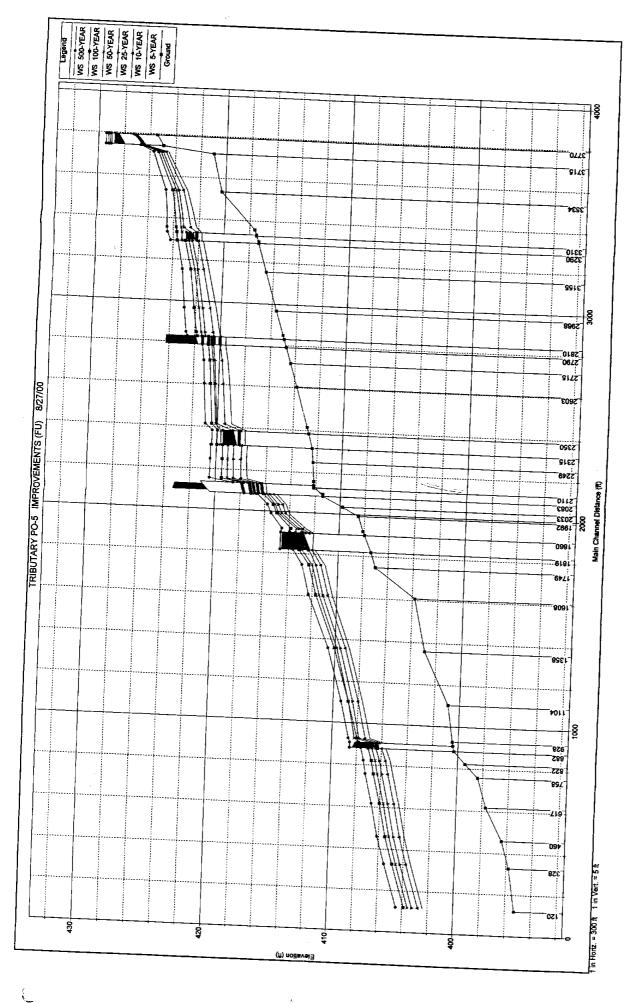




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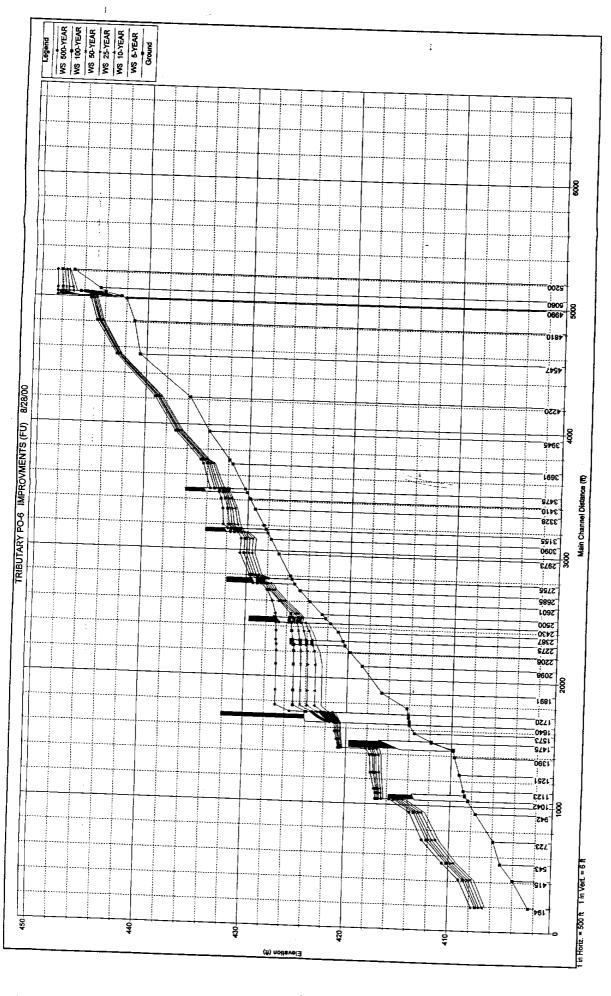




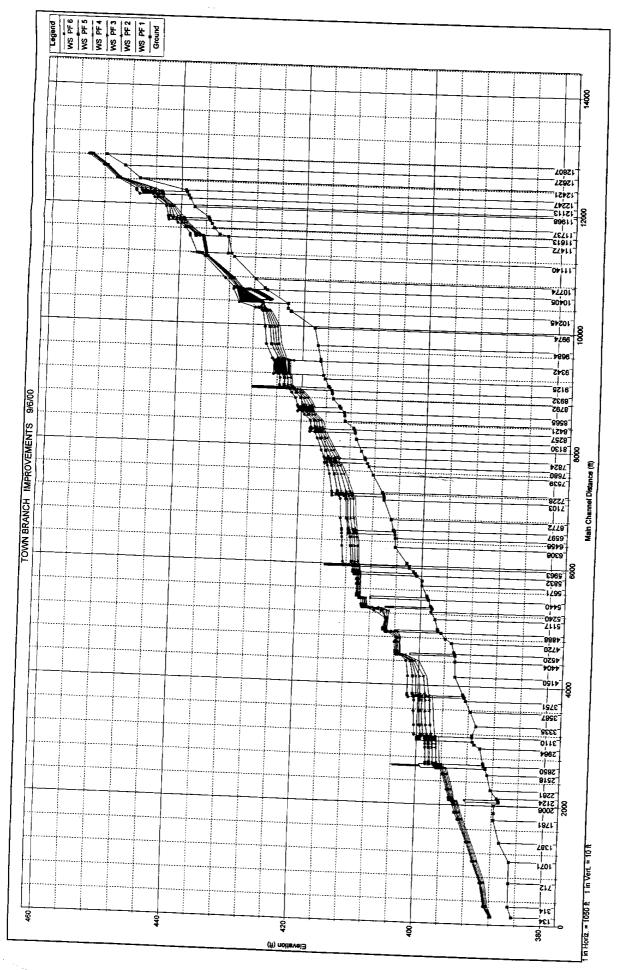
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APPENDIX E

Computer Summaries of Hydrologic and Hydraulic Models (printed in a separate volume or on computer disk)