

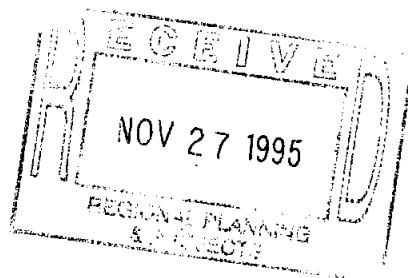
FLOOD PROTECTION PLAN

FINAL REPORT



**JOB NO. 67787
NOVEMBER, 1995**

RUST LICHLITER/JAMESON
Environment & Infrastructure
Consulting Engineers, Scientists and Planners
2929 Briarpark Drive, Suite 600 Houston, Texas 77042-3203



**CITY OF DONNA
FLOOD PROTECTION PLAN**

FINAL REPORT

Prepared By:

**Rust Lichliter/Jameson
2929 Briarpark, Suite 600
Houston, Texas 77042
Phone: (713) 785-9800
Fax: (713) 953-5044**

Project No.: 67787

November, 1995



Marta Juch
11/20/95

TABLE OF CONTENTS

<u>Section</u>	<u>Page</u>
1.0 INTRODUCTION	1-1
1.1 Background	1-1
1.2 Scope of Services	1-1
1.3 Related TWDB Studies	1-2
2.0 DATA COMPILATION	2-1
2.1 Planning Area	2-1
2.2 Existing Drainage System	2-1
A. Primary Drainage System	2-1
B. Secondary Drainage System	2-2
2.3 Historical Flooding	2-2
3.0 FLOODING ANALYSIS	3-1
3.1 Analysis of the Existing Drainage System	3-1
A. HEC-1 Model	3-1
B. HEC-2 Model	3-4
C. Storm Sewer Analysis	3-5
3.2 Results of Analyses	3-6
3.3 Extrapolation of Analysis to Future Development	3-9
4.0 RECOMMENDED FLOOD PROTECTION PLAN	4-1
5.0 IMPLEMENTATION PLAN	5-1
5.1 Phasing	5-1
A. Phase 1	5-1
B. Phase 2	5-1
C. Phase 3	5-1
5.2 Financing	5-4

TABLE OF CONTENTS - Continued

LIST OF TABLES

<u>Table Number</u>	<u>Title</u>	<u>Page</u>
2-1	Summary of Flooding Areas	2-3
3-1	Rainfall Depth for 24-hour Duration for the City of Donna	3-2
3-2	Hydrologic Parameters	3-3
3-3	Summary of the Causes of Potential Flooding	3-8
4-1	Recommended Flood Protection Plan Construction	
	Cost Estimate	4-2
5-1	5-Year Implementation Plan Construction Cost Estimate	5-2
5-2	10-Year Implementation Plan Construction Cost Estimate	5-3

LIST OF EXHIBITS

<u>Exhibit Number</u>	<u>Title</u>	<u>Following Section</u>
1	Planning Area	2.0
2	Primary Drainage Systems	2.0
3	Secondary Drainage System	2.0
4	Location of Historical Flooding	2.0
5a	Flood Profiles Channel A	3.0
5b	Flood Profiles Channel B	3.0
5c	Flood Profiles Channel C and Tributary	3.0
5d	Flood Profiles Channel I	3.0
5e	Flood Profiles Upper East Main Drain	3.0
6	Potential Flooded Areas Along Primary Drainage System	3.0
7	Projected Development Through 2005	3.0
8	Recommended Flood Protection Plan	4.0
9	5-year Implementation Plan	5.0
10	10-year Implementation Plan	5.0

TABLE OF CONTENTS - Continued

LIST OF APPENDICES

Appendix	
<u>Number</u>	<u>Title</u>
A	Existing Conditions HEC-1 Model
B	Existing Conditions HEC-2 Model

1.0 INTRODUCTION

1.1 Background

Localized flooding that hinders transportation and threatens residential and commercial structures has occurred frequently in the last ten years throughout the City of Donna and in Colonias within and near the City's extra-territorial jurisdiction (ETJ). The flooding has posed a potential health hazard by surcharging the sanitary sewer system in some areas and by interfering with pedestrian and vehicular traffic in critical areas near schools and residential communities. As the first step in reducing the flooding problem, the City of Donna, jointly with Hidalgo County, requested planning grant assistance from the Texas Water Development Board in September 1994. The grant assistance was targeted toward the development of a Flood Protection Plan (Plan) for the City and its ETJ. This Plan is the subject of this report and consists of the following elements:

- Identify the causes of flooding.
- Develop a plan for the orderly implementation of cost-effective solutions to the flooding problems.
- Eliminate flooding conditions, resulting flood damages, safety and access problems and health hazards.
- Develop a plan for the future anticipated growth in Donna and the surrounding area to insure properly controlled drainage.

1.2 Scope of Services

The City of Donna contracted with Rust Lichliter/Jameson (referred to in this report as the Engineer) in January of 1995 to perform a drainage study of the City and its ETJ and to develop a Flood Protection Plan for the area. The scope of engineering services summarized below was developed to identify the causes of flooding and recommend appropriate solutions to the flooding problems.

Task 1 Data Compilation

The Engineer met with staff at the City of Donna, Hidalgo County, the IBWC (Main Floodway system) and Donna Irrigation District No. 1 to identify areas of historical flooding and to compile sources of drainage information. Information on future drainage systems planned by the Texas Department of Transportation was also obtained. A map was developed to show the

existing watershed and drainage system as well as anticipated development for the next ten years.

Task 2 Flooding Analysis

The Engineer developed hydrologic and hydraulic models for the existing drainage system and developed hydraulic gradient profiles for the 5-, 10- and 100-year design frequencies for each primary drainage channel. Alternative methods of addressing the existing flooding areas and potential future problem areas were analyzed as to engineering feasibility, cost, benefits, and potential environmental impacts. The improvements recommended by the Engineer were prioritized into a 5-year and a 10-year capital improvement plan (CIP), and a 5-year implementation plan was proposed.

Task 3 Implementation Plan

The financial requirements associated with the recommended CIP were identified as were potential funding sources.

Task 4 Final Report and Deliverable

A draft report was prepared which describes the study results and the proposed solutions to the flooding problems. After receiving comments, a final report will be prepared and 25 copies will be submitted to the City.

1.3 Related TWDB Studies

No previous comprehensive flood protection studies have been done in the City of Donna or its ETJ.

Concurrent with the City of Donna study, two other cities near the planning area were identified by the Texas Water Development Board as participating in the Planning Grant program. The Cities of McAllen and Mission are developing Flood Protection Plans and were contacted in writing regarding the City of Donna study and requesting any pertinent information. However, neither city has the same watershed boundary with the City of Donna; therefore, no interaction in the planning activities that warranted further cooperation was identified.

2.0 DATA COMPIILATION

2.1 Planning Area

The planning area is shown on Exhibit 1 and encompasses the City of Donna, its ETJ, and surrounding drainage areas. The boundaries of the planning area are generally the International Boundary and Water Commission (IBWC) Main Floodway levee on the south, Midway Road on the east, FM 1423 on the west and Eleven Mile Road on the north. Business Route 83 (BR 83) and the Missouri Pacific Railroad traverse the City from west to east and generally form the north-south drainage divide. Based on the United States Geological Survey's *Donna, Texas Quadrangle 1:24000 7.5 minute series topographic map*, ground elevations in the planning area range from approximately 95 feet mean sea level (msl) at FM 1423 and BR 83, to approximately 70 feet msl at the southern limit and 75 feet msl at the northern limit of the planning area.

2.2 Existing Drainage System

The City of Donna's storm drainage system, like all urban storm drainage systems, consists of two separate and distinct elements, the primary system and the secondary system. The primary drainage system includes the major ditches, drainage channels, streams or rivers in the studied watershed. The secondary system includes open and closed conduits intended to convey runoff from frequent, low intensity storms to the primary system while causing relatively minor public inconvenience. The secondary system is supplemented in urban areas by a street system that conveys sheet flow runoff when the conduits of the secondary system have insufficient capacity during large storm events or are inoperable due to temporary blockages. At many locations the streets may be too flat to convey the excess flow from heavy rainfall events and the result is extended periods of street ponding. When both drainage systems and the local street system are properly designed, a high level of flood protection will be provided, even during significant storm events. The existing primary and secondary drainage systems in the City of Donna and surrounding areas are described below.

A. Primary Drainage System

The primary drainage system serving the City and its ETJ is a series of agriculture ditches originally designed to drain agriculture fields and to slow the rate of runoff. The planning area includes five watersheds designated by the Hidalgo County (Donna) Irrigation District No. 1 (Irrigation District) as Lateral A, B, C, I and the Upper East Main Drain. Construction plans for Lateral A, profiles of Lateral B, C and Upper East Main Drain and a map showing the layouts of the irrigation ditches were obtained from the Irrigation District. These plans and maps were used to help determine the limits of the watersheds for modeling purposes. No plans or profiles of Lateral I were available. In addition, three

field reconnaissance trips were made by the Engineer to identify local runoff patterns, collect and measure field information on the primary drainage channels, and identify the sizes and locations of the secondary drainage system.

Laterals A, B and C service the southern portion of Donna draining runoff from northwest to southeast to the Main Floodway. Lateral I and the Upper East Main Drain service the northern portion of the City, draining rainfall runoff north to County District Drain. These channels and their approximate drainage boundaries within and adjacent to the City are shown on Exhibit 2.

Many road crossings occur on each channel, with most involving one or more pipe or box culverts in the channel. Elevated irrigation ditches also crisscross the watershed and alter the natural drainage pattern. One or more culverts have been placed in the primary drainage channels where these irrigation ditches cross. Since the ditches were originally designed to drain runoff from agricultural land and convey the flow slowly to the Main Floodway or County District Drain, most of the road or irrigation canal crossings are undersized for urban drainage and significantly restrict the flows in the primary channels.

B. Secondary Drainage System

Within the City of Donna, the secondary drainage system consists of valley gutters along most streets, limited storm sewer systems, and roadside ditches. Detailed data on the existing storm sewer system is unavailable, and no detailed field surveys were obtained for this study. Although written requests for the storm sewer construction drawings were made through the City to three local engineering firms, no plans were made available for use in this study. Proposed construction drawings for a storm sewer system along Business 83 were obtained from the Texas Department of Transportation.

The alignments and sizes of the system pipes used for the storm sewer analysis were approximated using inlet and manhole locations collected during the Engineer's field reconnaissance. Sizes of critical outfalls and roadside ditches were also determined using field measurements. The approximation of the existing City storm sewer system used for this study is shown on Exhibit 3.

2.3 Historical Flooding

The City of Donna experiences frequent flooding of neighborhoods and streets as shown in Exhibit 4. A summary of the number of homes, businesses and public facilities identified by the City as affected by area flooding is shown on Table 1. From the locations of the flooded areas, the existing storm sewer and outfall channel systems apparently do not function efficiently. The flooding has resulted in structural damage to homes and business, loss of vehicular and pedestrian access to schools, businesses and homes, and sewage

back up in wastewater collection systems due to the flooding of manholes in existing streets.

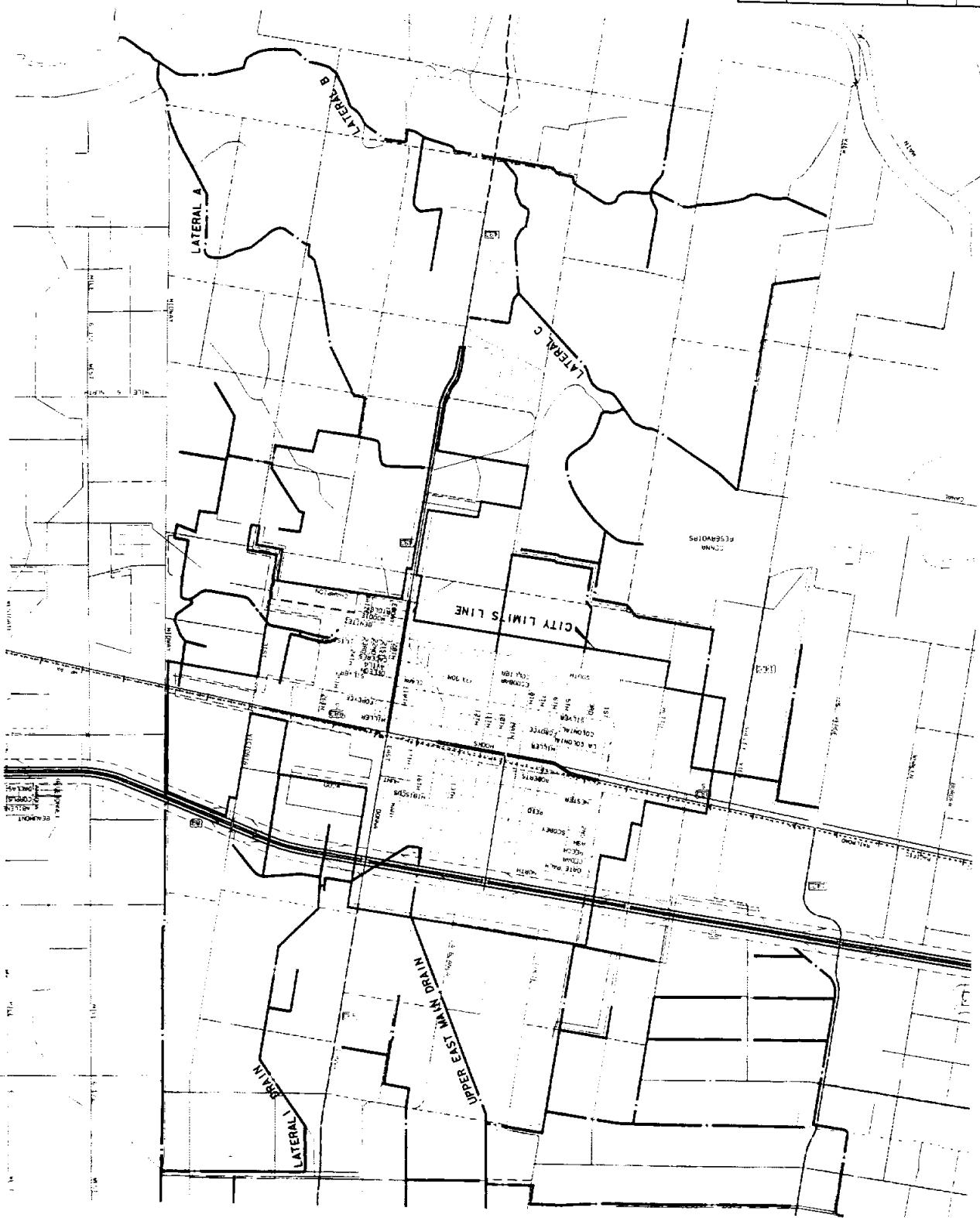
Besides the problem within the City, several Colonias in the City's ETJ have experienced flooding problems. These Colonias are also shown in Exhibit 4 and the affected homes are included in Table 2-1. Based on the estimated areas affected, approximately 445 homes, housing approximately 2000 residents, and several schools and public facilities are adversely affected by the flooding conditions.

**TABLE 2-1
SUMMARY OF FLOODING AREAS**

Area within City of Donna	Estimated Number of Homes Affected	Estimated Number of Businesses Affected	Estimated Number of Public Facilities Affected	Footnotes
(1) Roberts Avenue	12	1	0	
(2) North Main	20	3	2	(1)
(3) Scobey Avenue/School Area	10	0	0	
(4) U.S. 183 - S. 11th-13th	25	15	0	
(5) East Donna Boulevard	2	7	1	(2)
(6) South Avenue	14	2	3	(3)
(7) Silver Avenue/Fordyce/Mary	30	0	1	(4)
(8) Hooks Subdivision/East Donna	17	0	0	
Area Outside Donna				
(9) Colonia Nueva	200	0	0	
(10) Salinas Subdivision	25	0	0	
(11) Balli Estates	80	0	0	
(12) Valley View Estates	10	0	0	
Total	445	28	7	

- Footnotes:
- (1) La Sombra Apartments - Elderly Housing
Lenor Elementary School
 - (2) Todd Elementary School
 - (3) Donna Housing Authority, A.P. Solis Middle School
Ochoa Elementary School
 - (4) Stanike Elementary School

SCALE: 1" = 3000'



**CITY OF DONNA
FLOOD PROTECTION PLAN**

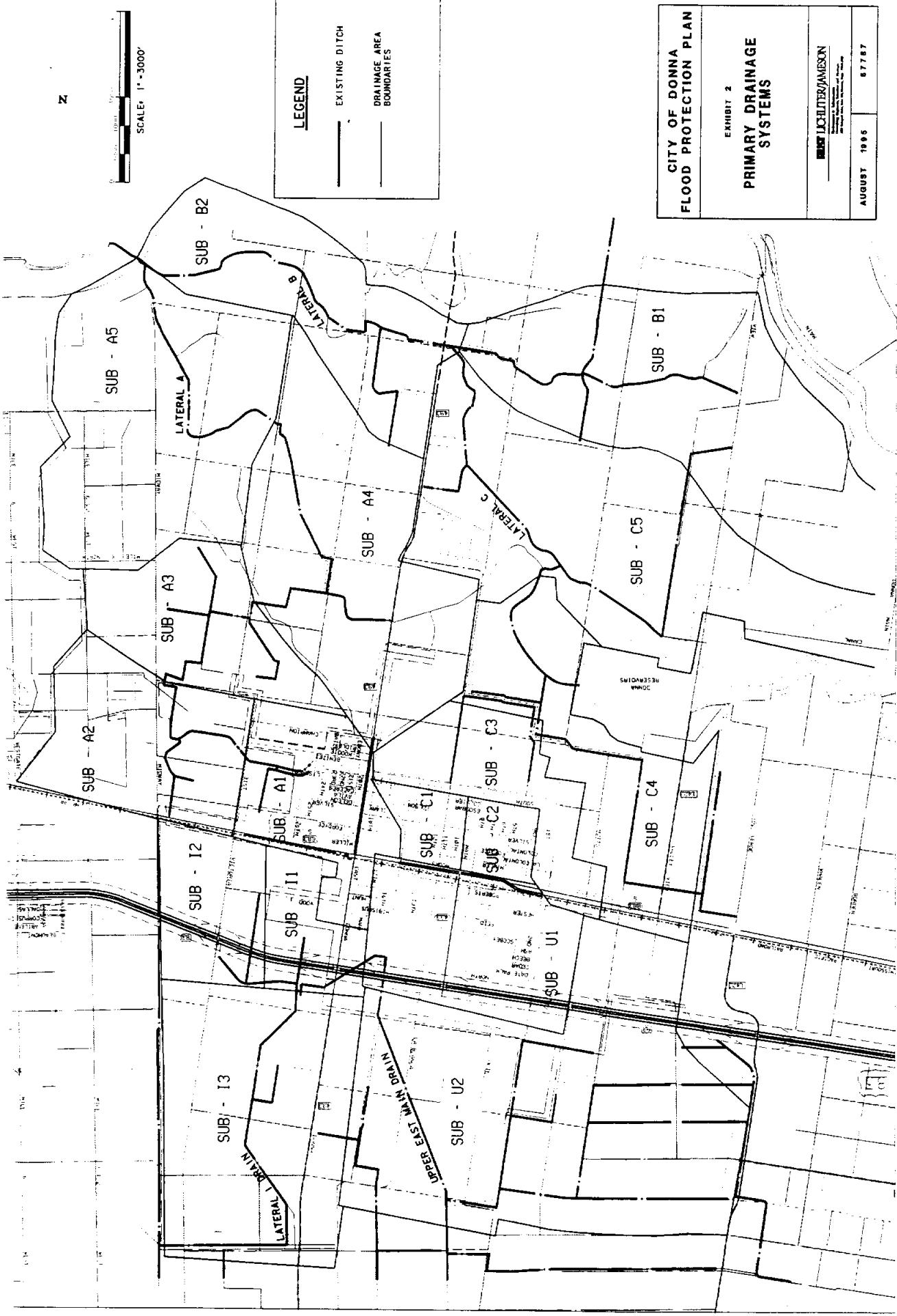
EXHIBIT 1

PLANNING AREA

MAP LIGHTER JAMESON

AUGUST 1995 67787

N





Z

SCALE 1" = 3000'

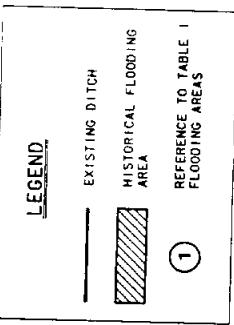


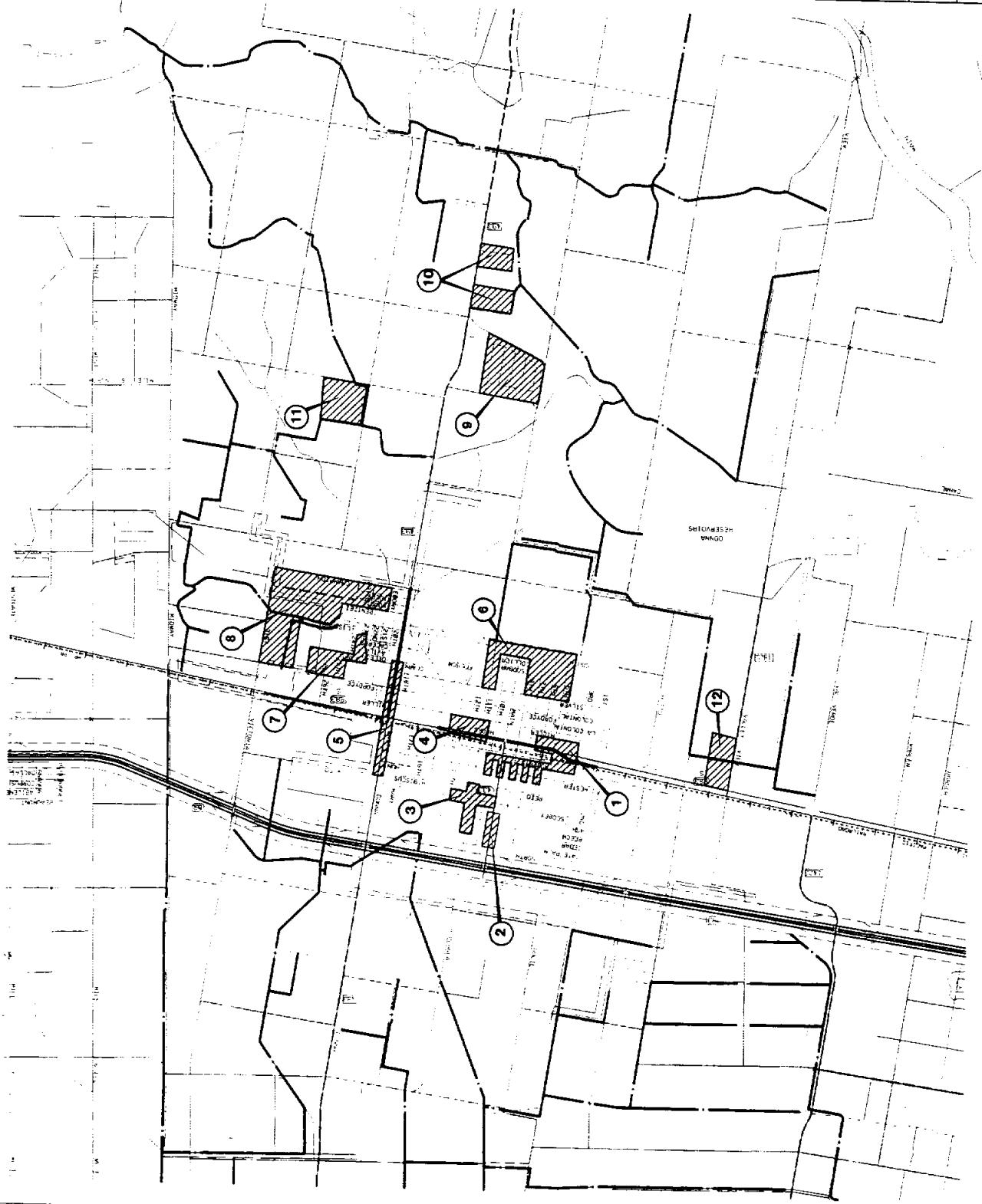
TABLE I SUMMARY OF FLOODING AREAS	
AREA WITHIN CITY OF DONNA	
(1) ROBERT'S AVENUE	(9) COLONIA NUEVA
(2) NORTH MAIN	(10) SALINAS SUBDIVISION
(3) SCOTT AVENUE/SCHOOL AREA	(11) BALLI ESTATES
(4) U.S. 183-S. 11TH-13TH	(12) VALLEY VIEW ESTATES
(5) EAST DONNA BOULEVARD	
(6) SOUTH AVENUE	
(7) SILVER AVENUE/FORDYCE/MARY	
(8) HOOKS' SUBDIVISION/EAST DONNA	
AREA OUTSIDE DONNA	
(9) COLONIA NUEVA	
(10) SALINAS SUBDIVISION	
(11) BALLI ESTATES	
(12) VALLEY VIEW ESTATES	

CITY OF DONNA
FLOOD PROTECTION PLAN

EXHIBIT 4
LOCATION OF HISTORICAL
FLOODING

LODGE TRAMMELSON

AUGUST 1995 67787



3.0 FLOODING ANALYSIS

Early field visits to the City and its ETJ identified that the extensive flooding and access problems that occur are probably the result of the very limited extent of the storm sewer system, undersized storm sewers, nearly flat grade in many streets, inadequate capacity in portions of the outfall channels and poorly designed drainage structures associated with these channels. Once the problem areas had been identified and the available data on the existing systems had been compiled, a methodology was developed to quantify the extent of the problem and develop a flood protection plan to reduce the flooding problem.

3.1 Analysis of the Existing Drainage System

Computer models of the existing drainage systems were developed to analyze the flooding problems within the planning area. Two types of models were developed to quantify rainfall-runoff patterns in the regional area and to analyze the efficiency of the primary drainage system (i.e., drainage channels). These large-scale models were developed using the United States Army Corps of Engineers' HEC-1 hydrologic computer program and HEC-2 hydraulic computer program. These models are based on existing topographic, cross-section, profile and drainage area data from the City of Donna, Hidalgo County, the Irrigation District, and extensive field reconnaissance and are described below in Sections 3.1.A. and 3.1.B. A third type of model was used to evaluate the localized drainage patterns in the secondary drainage system (i.e., storm sewer system). This model was developed in-house by the Engineer and is described in Section 3.1.C. below.

A. HEC-1 Model

The HEC-1 program can simulate the precipitation-runoff process and compute flood hydrographs at desired locations in a watershed. The physical characteristics of the watershed are represented by an interconnected system of geographic and hydrologic components. The watershed boundaries are delineated, and the land area is divided into sub-watersheds based on the study objectives and hydrologic characteristics. After the rainfall-runoff process is simulated, runoff from the sub-watersheds is linked using channel routing. The basic hydrologic components of the model include land-surface runoff from each sub-watershed, channel and reservoir routing, and combining hydrographs at confluences.

No continuous long-term records of rainfall and resulting storm runoff were available in the study area. Therefore, rainfall values for the 5-, 10- and 100-year rainfalls were obtained from the National Weather Service's (NWS) Technical Paper No. 40 (TP-40) and Technical Memorandum NWS Hydro-35 ("Five- to 60-Minute Precipitation Frequency for the Eastern and Central United States) for use in the HEC-1 model. Table 3-1 shows the frequency and rainfall depth for a 24-hour duration according to previously mentioned documents.

TABLE 3-1
RAINFALL DEPTH FOR 24 HOUR DURATIONS FOR THE CITY OF DONNA

Frequency	Rainfall Depth (inches)
5- Year	6.0
10-Year	7.2
100-Year	11.0

The Soil Conservation Service (SCS) method was used for the HEC-1 hydrologic analysis. This method employs two parameters, the curve number (CN) and the lag. The CN for the various sub-basins was determined using the SCS Soil classification and the land use(s) within each sub-basin. The lag was calculated using the following formula:

$$Lag = \frac{I^{0.8}(S+1)^{0.7}}{1900Y^{0.5}}$$

where:
 S = (1000/CN)-10
 I = Hydraulic length in feet
 Y = Slope, in percent

The CN and lag values for each subarea (shown on Exhibit 2) are listed on Table 3-2.

TABLE 3-2
HYDROLOGIC PARAMETERS

Subarea	CN Value	Lag (hours)
A1	83.9	13.89
A1a	85.0	13.37
A1b	85.4	3.70
A1c	75.0	3.69
A2	76.1	7.33
A3	77.2	8.97
A4	78.3	8.45
A5	79.4	11.17
B1	86.0	14.87
B2	84.9	11.77
C1	85.0	1.59
C2	85.0	3.17
C3	75.0	8.80
C4	78.3	17.03
C5	85.5	18.68
U1	85.2	5.67
U2	76.7	14.43
I1	76.1	8.44
I2	76.1	6.25
I3	76.1	16.50

The SCS Dimensionless Unitgraph method in HEC-1 then determines how much of the rainfall actually becomes storm runoff. This method requires only the SCS lag, in hours, be entered to generate a unit hydrograph for the sub-basin.

The time to peak of the unitgraph is computed as:

$$T_{peak} = \frac{\Delta t}{2} + T_{lag}$$

in which:

- T_{peak} = the time to peak, in hours
 Δt = the computation time interval (also duration of unit excess), in hours
 T_{lag} = the watershed lag value, in hours

The peak flow rate of the unitgraph is computed by:

$$Q_{peak} = \frac{484 \text{ AREA}}{T_{peak}}$$

where:

- Q_{peak} = the peak flow rate of the unitgraph in cfs per inch
AREA = the watershed area in square miles
 T_{peak} = the calculated time to peak

Field reconnaissance showed Sub-basins A1-a, and A1-b drained to channel A through 18- and 30-inch outfall pipes, respectively. Channel C sub-basins C1 and C2 were also found to have restricted outfalls. These restrictions cause street ponding by limiting flow and creating storage areas upstream from the substandard outfall pipes. The HEC-1 model was adjusted to reflect this effective storage. The existing conditions HEC-1 model is included as Appendix A.

B. HEC-2 Model

The HEC-2 computer program has been developed for calculating water surface profiles for steady, gradually varied flow in natural or manmade channels. The program allows the effects of obstructions to flow, such as bridges, culverts, weirs, and buildings in the floodplain, to be modeled. Generally, the water surface profiles are calculated with the standard step method, which sequentially solves the one-dimensional energy equation between cross-sections. At some bridges, where more complex flow conditions exist, the program may use momentum and other hydraulic equations to determine changes in the water surface elevations.

HEC-2 has a variety of applications and many options for defining input and specifying output. This feature allows the Engineer to create models with several different channel or culvert improvement options.

The HEC-2 hydraulic models for the primary drainage channels in the planning area were developed using information from various sources. The topographic information for Lateral A was obtained from channel improvement plans provided by the Irrigation District. Profiles of Lateral B, Lateral C, and Upper East Main Drain were obtained from the Irrigation District and were augmented with field measured cross sections and elevations from the 1:24000 quad map. Dimensions and other required data for Lateral I were estimated from aerial photographs and the quad map since no profiles or plans for this ditch were available.

Timing of the peak flow was checked to establish the method for determining the starting water surface elevation in each channel. The peak flow in Lateral A, at the confluence with Lateral B, occurs approximately 12 hours before the peak in Lateral B. The peak flow in Lateral C, at its confluence with Lateral B, occurs approximately 11 hours after the peak in Lateral B. Since the early flow will be gone when the later flow arrives at the confluence, neither flow will affect the other. Therefore, the starting water surface elevation for each channel was calculated using the slope-area method. Similarly, the outfalls for both Lateral I and the Upper East Main Drain were estimated using the slope-area method. The existing conditions HEC-2 models are included as Appendix B.

C. Storm Sewer Analysis

A storm sewer conveys flow using the energy resulting from the difference in elevation of the upstream and downstream ends of the pipe. The Engineer developed an in-house program to simulate the pipe system. The analysis of the storm sewer system solves for the energy-loss in each pipe using Manning's formula for a pipe flowing full.

$$\text{Energy Loss} = Q^2 \left(\frac{n}{1.486 A R^{2/3}} \right)^2$$

where:

- | | | |
|----------|---|---|
| <i>n</i> | = | Manning's roughness coefficient |
| <i>Q</i> | = | the flow rate in cfs |
| <i>A</i> | = | cross-sectional area of the pipe in square feet |
| <i>R</i> | = | hydraulic radius |

The analysis simulates one conduit at a time, working methodically through the system top to bottom as though it were a basic gravity system. During this process, any parameters that will be used in the surcharge calculations are noted. When the first run is completed, the system is recalculated starting at the outfall, working back up the system to calculate the surcharge on each overloaded pipe and carrying any excess head along until the top of the system is reached, or until the pipes are no longer surcharged. The existing storm sewer system for the City of Donna was approximated from field observations as discussed previously and then analyzed using the in-house program.

3.2 Results of Analyses

Using the HEC-1 model described in Section 3.1.A. above, flows in each of the five primary channels were developed for the 5-, 10- and 100-year design frequencies. These flows were then input into the HEC-2 models for each channel as described in Section 3.1.B. and the design water surfaces were generated and are shown graphically in the hydraulic gradient profiles shown in Exhibits 5a through 5e. These profiles were then analyzed with the available topographic maps to identify areas potentially subjected to riverine flooding from the primary channel system under design storm conditions. Exhibit 6 shows the areas that have the greatest potential for flooding during each of the 5-year, 10-year and 100-year design storm events. Limitations imposed by the lack of detailed construction drawings or topographic surveys affect the accuracy of this exhibit; however, the map shows the general locations and severity of potential channel flooding.

According to residents, questioned during field visits by the Engineer, Channels A, B, and C have historic flooding and Channels I and Upper East Main Drain do not have historic flooding. According to the hydraulic modeling, all of the channels have the potential for out-of-bank riverine flooding as follows: Channel A has three areas of potential flooding between the following cross sections: 8000 - 10,000; 15,000 - 17,000 and 22,000 - 27,000. Channel B has two areas of potential flooding between cross sections 9000 - 11,000 and 12,000 - 12,750. Channel C has two areas of potential flooding at the mouth, near the Colonias next to channel and upstream of 16,000. The Upper East Main Drain has the potential 100-year flooding along the entire length of the channel and higher frequency flooding along the downstream half the channel. Modeling shows that Channel I has the potential for limited out-of-bank flooding at all three studied frequencies; however, the lack of reported historical flooding indicates that the modeling may be overpredicting the flooding potential due to the estimated data used to simulate the channel and overbank characteristics.

The analysis of the secondary drainage system as described in Section 3.1.C. identified localized areas that may flood during more frequent smaller storms as well as the design storms due to an undersized or inadequate storm sewer and roadside ditch systems. The analysis was based on field assumptions of the existing system layout, pipe slopes and sizes and is therefore limited in its accuracy. However, using the analysis and historical

flooding information shown on Exhibit 4, several areas were identified as flood prone and were considered during development of the Flood Protection Plan described in Section 4.0.

Table 3-3 summarizes the areas identified as either having experienced historical flooding or having the potential for future flooding based on the analyses. The table also identifies the possible cause of flooding for each location and the potential design frequency of flooding, if applicable. As in the analysis of the primary drainage system, detailed topographic information of the area (including the street system) was not available, so assumptions were made in determining the causes of historical flooding.

TABLE 3-3
SUMMARY OF THE CAUSES OF POTENTIAL FLOODING

Area within City of Donna	Frequency of Potential Flooding	Cause of Potential Flooding
(1) Roberts Avenue	A	Inadequate Storm Sewers
(2) North Main	A	Inadequate Storm Sewers
(3) Scobey Avenue/School Area	A	Inadequate Storm Sewers
(4) U.S. 183 - S. 11th-13th	A	Inadequate Storm Sewers
(5) East Donna Boulevard	A	Inadequate Storm Sewers
(6) South Avenue	A	Inadequate Storm Sewers and Outfall to Channel
(7) Silver Avenue/Fordyce/Mary	A	Inadequate Storm Sewers and Outfall to Channel
(8) Hooks Subdivision/East Donna	A	Inadequate Storm Sewers and Outfall to Channel
Area Outside Donna		
(9) Colonia Nueva	B	Low Lying Sheet Flow Flooding
(10) Salinas Subdivision	B	Low Lying Sheet Flow and Riverine Flooding
(11) Balli Estates	A	Low Lying Sheet Flow and Riverine Flooding
(12) Valley View Estates	A	Restricted Outfall Channel with Constrictions
Primary Drainage Systems		
(13) Channel A: 8000-10,000	B	Small Pipe Crossing
(14) Channel A: 15,000-17,000	A	Low Lying Sheet Flow and Riverine Flooding
(15) Channel A: 22,000-27,000	A	Low Lying Area
(16) Channel B: 9000-11,000	A	Small Pipe Crossing
(17) Channel B: 12,000-12,750	A	Small Pipe Crossing and Confluence w/Channel C
(18) Channel C: at Mouth	A	Small Pipe Crossing on Channel B and Confluence w/Channel B
(19) Channel C at Colonias	B	Low Lying Sheet Flow and Riverine Flooding
(20) Channel C: 16,000-20,000	A	Small Pipe Crossing
(21) Channel UEMD	B	Small Pipe Crossing

Note: (A)Frequency Less Than 5-years
 (B)Frequency Between 5-years and 10-years
 (C)Frequency Between 10-years and 100-years
 (D)Frequency Greater Than 100-years

3.3 Extrapolation of Analysis to Future Development

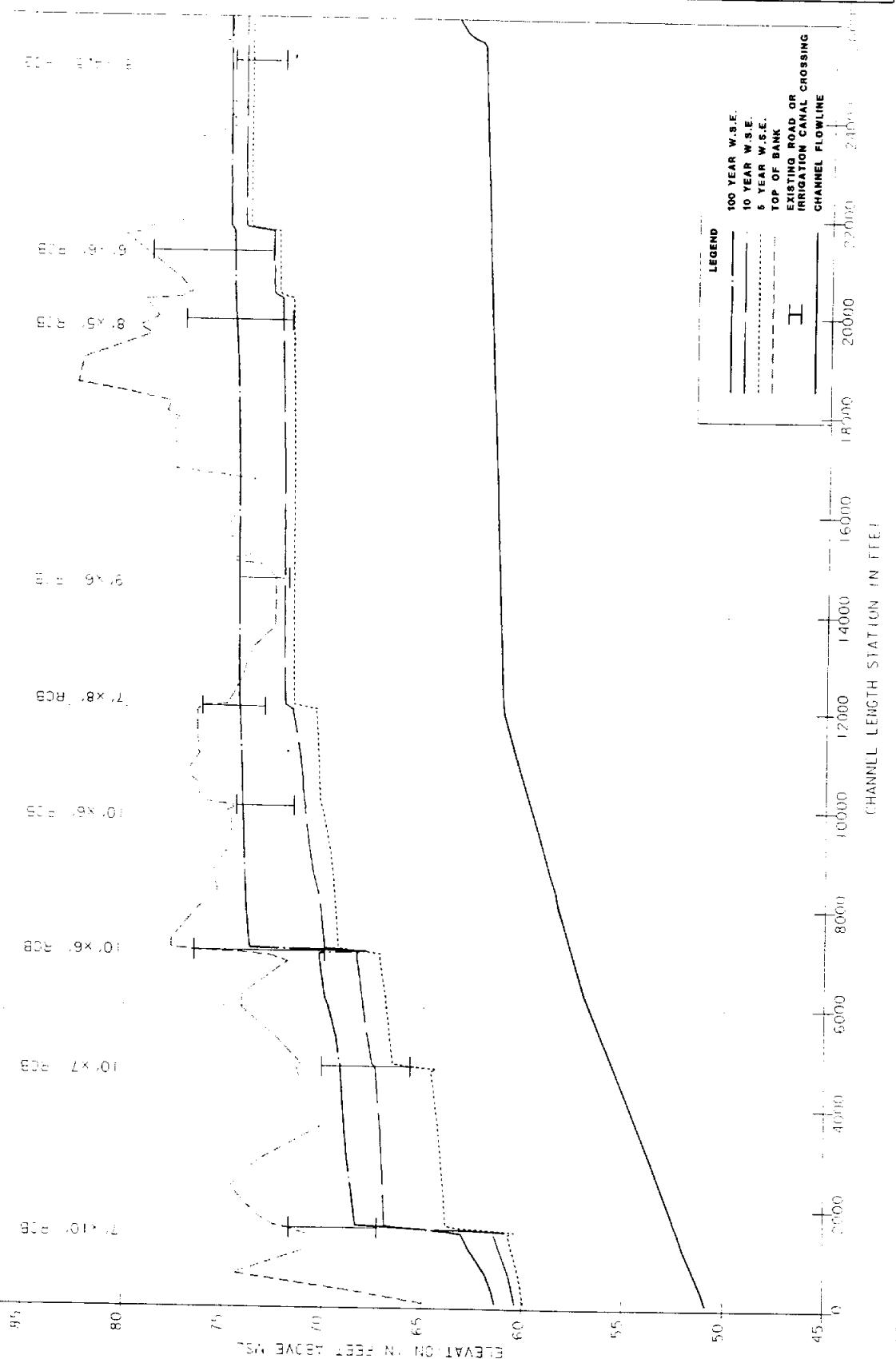
In fulfillment of the TWDB planning grant requirements, a projection was developed which used current development trends and proposed future commercial plans to estimate new development that is likely to occur in the next ten years. The Engineer estimated the most probable locations and types of future development within the City and its ETJ as shown on Exhibit 7.

The projected development is limited to areas near current developed subdivisions or along the major roadways. This projection could change dramatically depending upon the construction of an international bridge and adjacent industrial complex or other development scenarios not considered as part of the scope of this study. A more detailed land planning study has been proposed by the City and can be used in the future to modify the projections used in this report.

The areas identified in Exhibit 7 were considered during development of the Flood Protection Plan described below. The improvements have been sized to accommodate limited future development in the areas indicated; however, land plans for these areas should be required to perform adequate analysis of the drainage system serving the targeted area in order to anticipate and prevent future flooding problems.

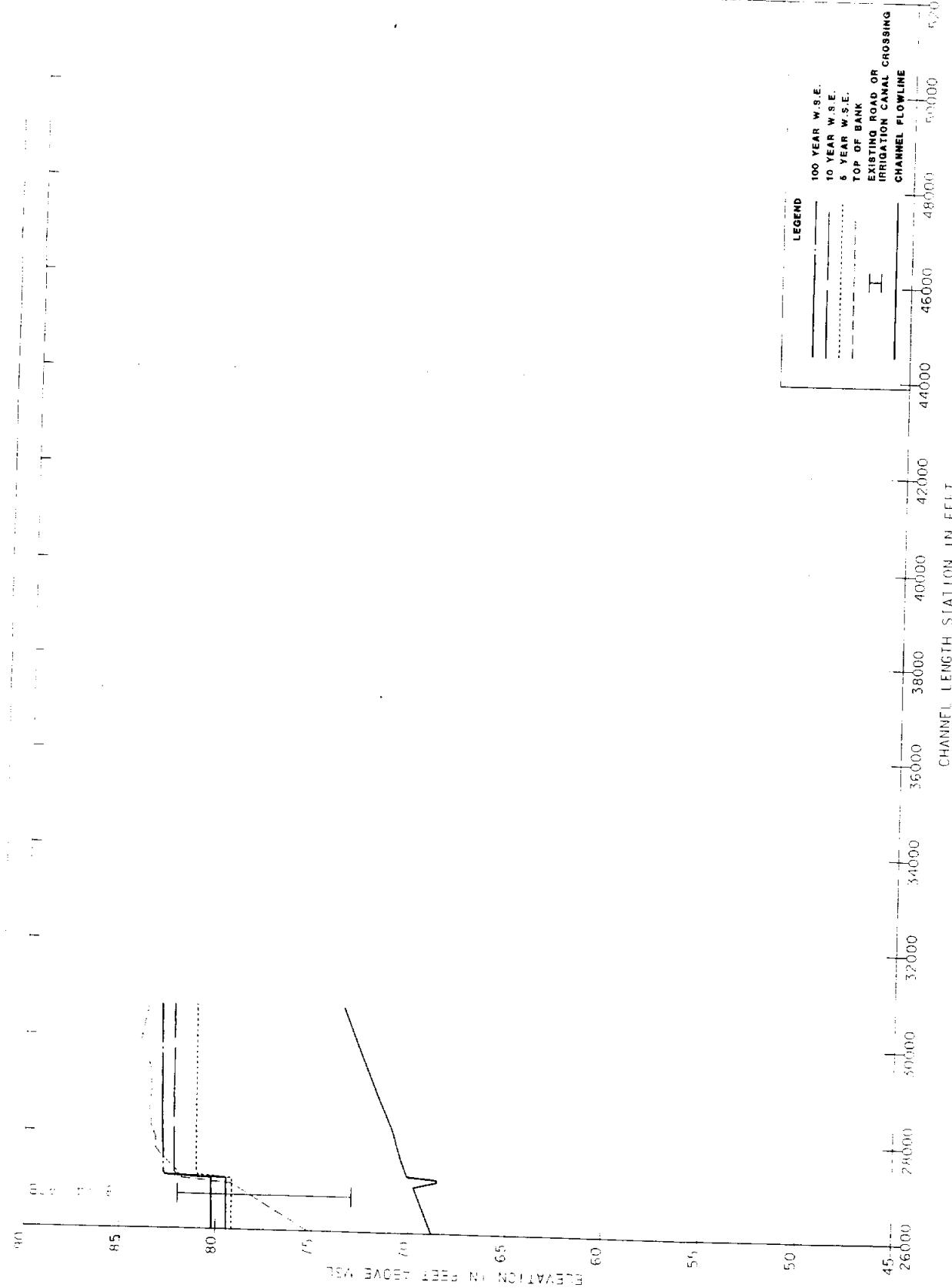
CITY OF DONNA FLOOD PROTECTION PLAN
EXHIBIT 5a - FLOOD PROFILES
CHANNEL A

AUGUST 1996 37787



FLOOD PROTECTION PLAN
CITY OF DONNA

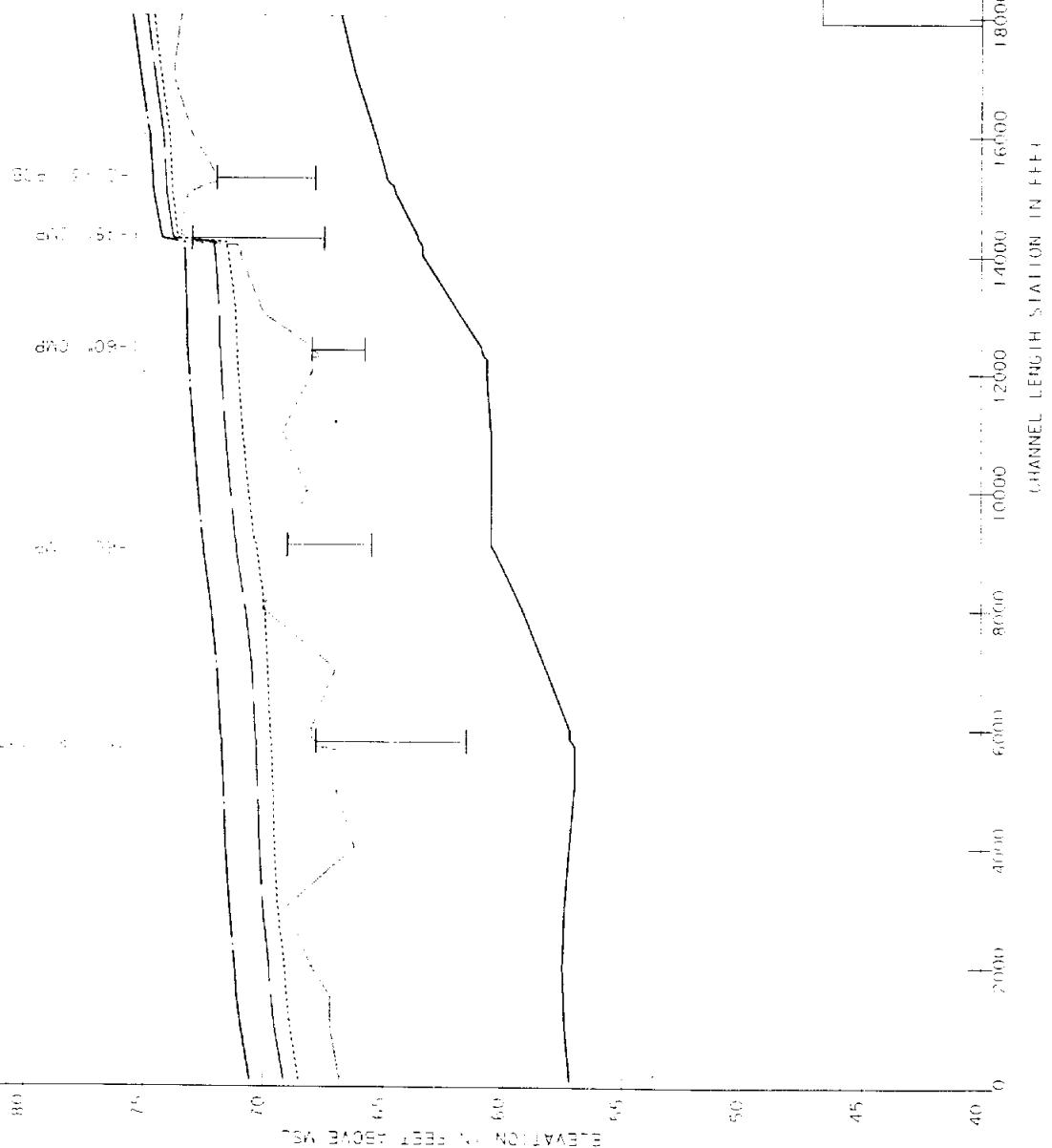
EXHIBIT 5a - FLOOD PROFILES



AUGUST 1995 67787
CITY OF DONNA FLOOD PROTECTION PLAN
FLOOD PROTECTION PLAN

CHANNEL B

EXHIBIT 5B - FLOOD PROFILES

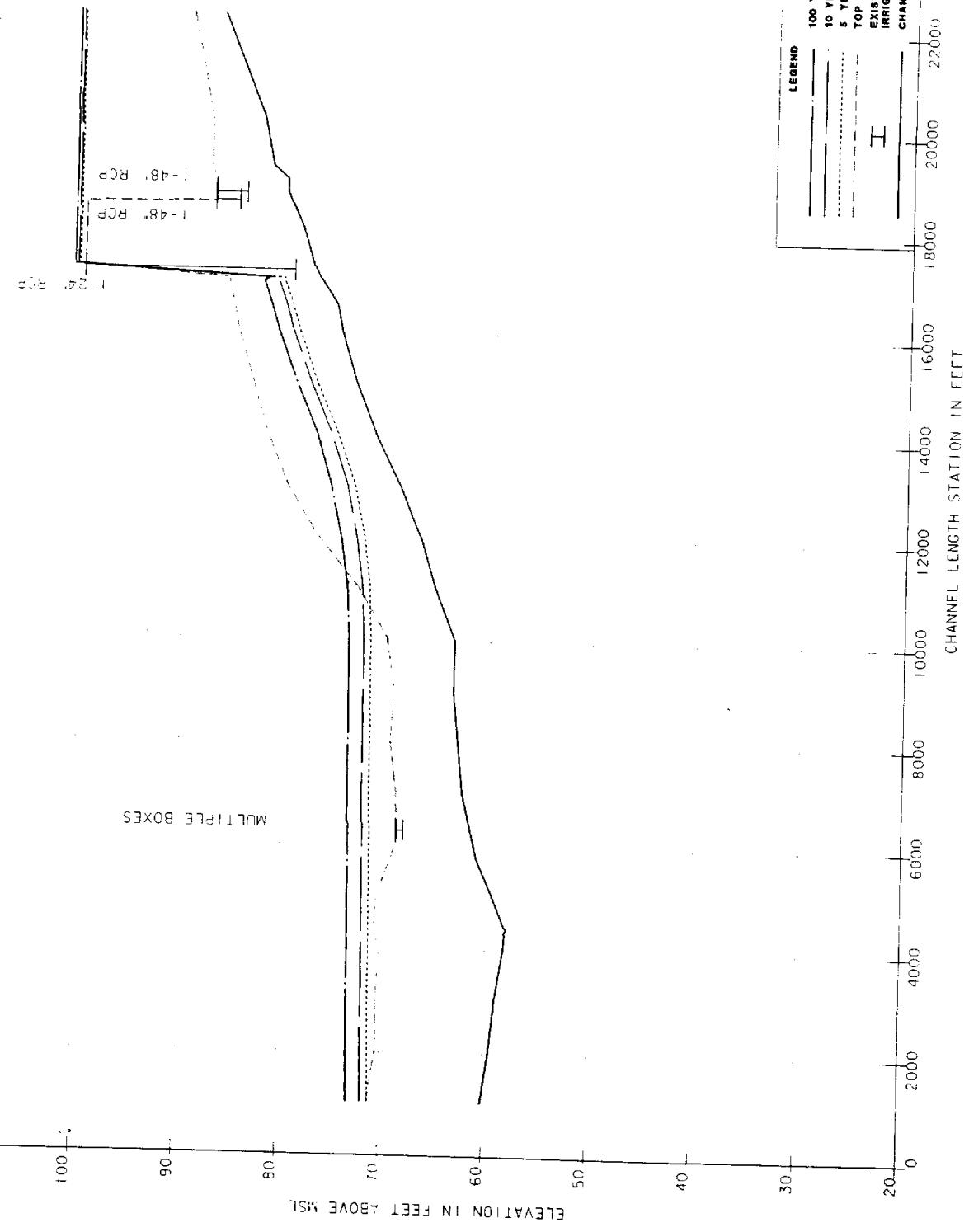


CHANNEL C

EXHIBIT 5c - FLOOD PROFILES

CITY OF DONNA FLOOD PROTECTION PLAN

אוקטובר 1981 2022



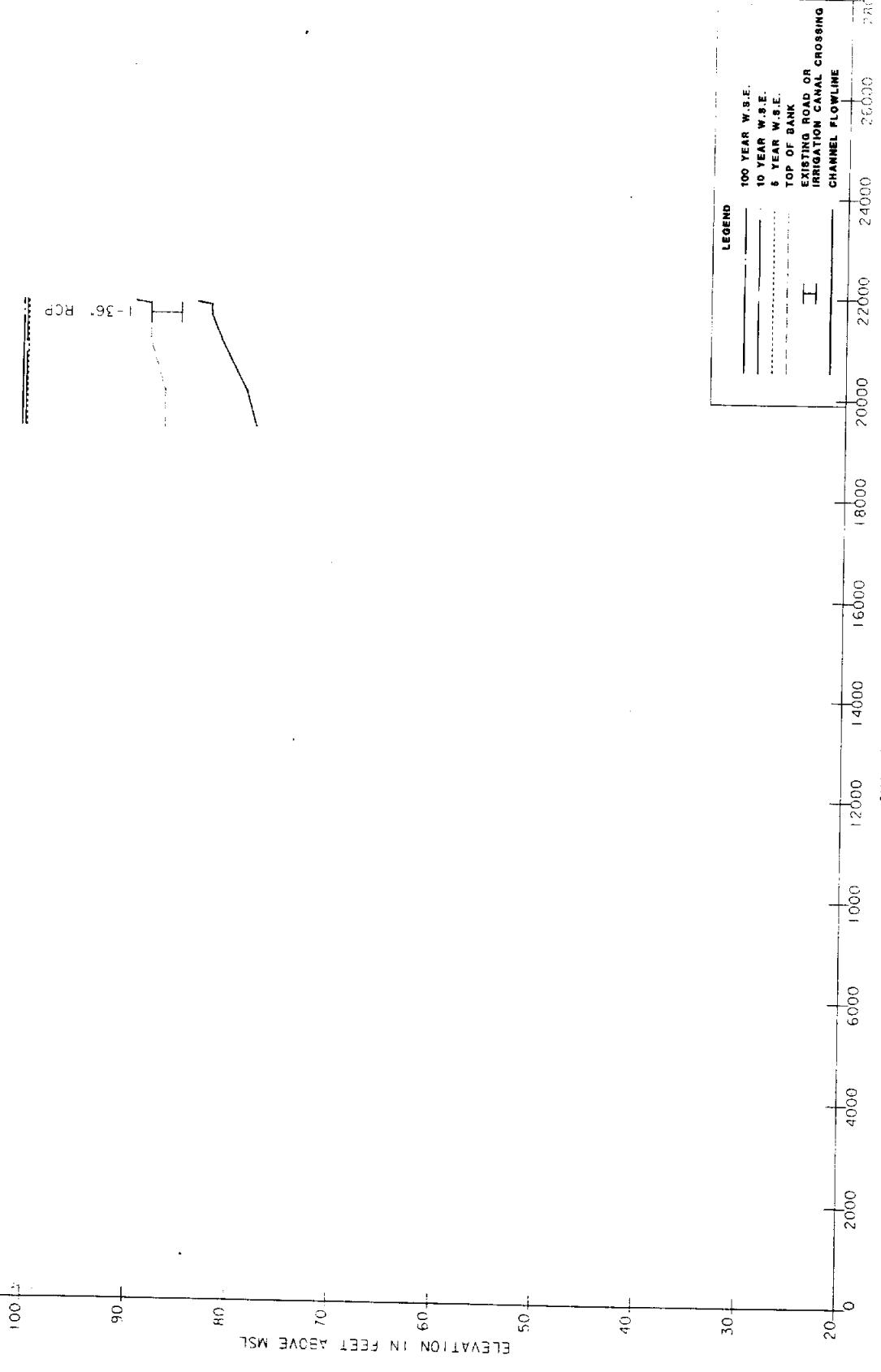
FLOOD PROTECTION PLAN

CITY OF DONNA
MUD HIGHWAY MILEAGE

FLOOD PROTECTION PLAN

EXHIBIT 5C - FLOOD PROFILES

TRIBUTARY TO CHANNEL C



CITY OF DONNA FLOOD PROTECTION PLAN	
EXHIBIT 5d - FLOOD PROFILES	
CHANNEL I	CHANNEL FLOWLINE
100 YEAR W.S.E.	24000
10 YEAR W.S.E.	22000
5 YEAR W.S.E.	20000
TOP OF BANK	18000
EXISTING ROAD OR IRRIGATION CANAL CROSSING	16000
CHANNEL FLOWLINE	14000
	12000
	10000
	8000
	6000
	4000
	2000
	0

AUGUST 1996 67787

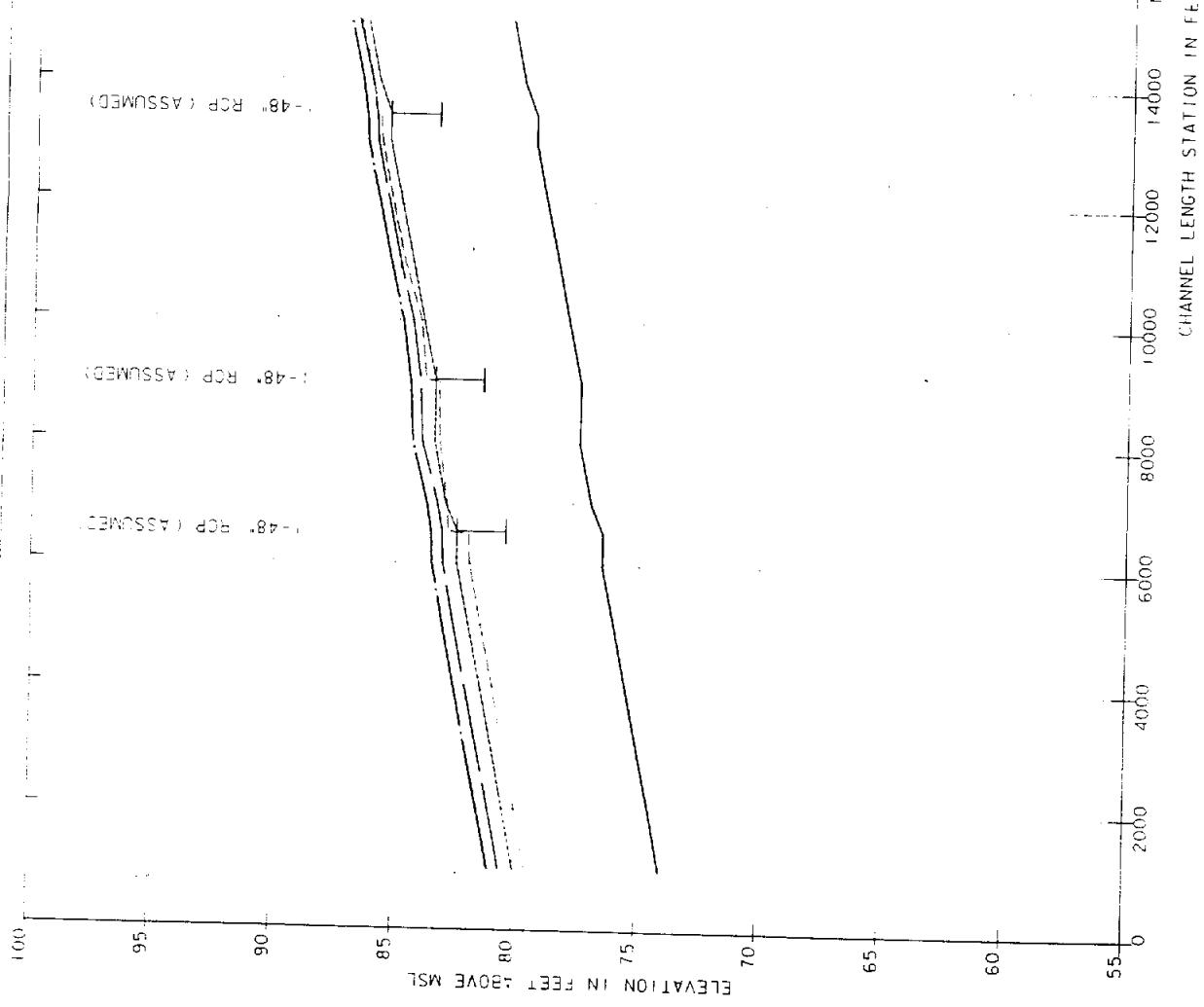
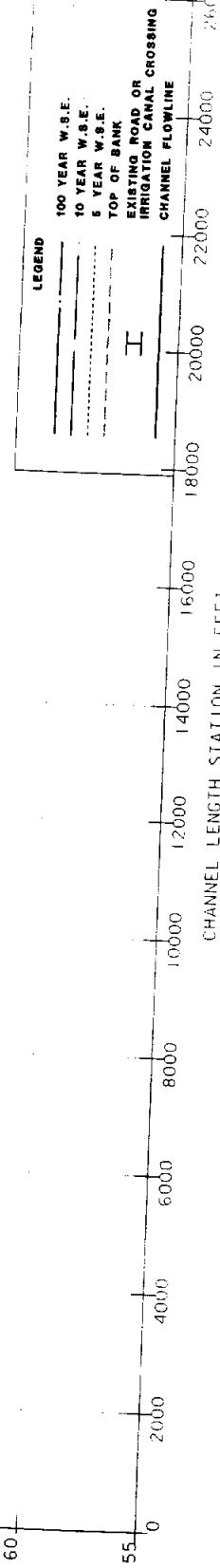
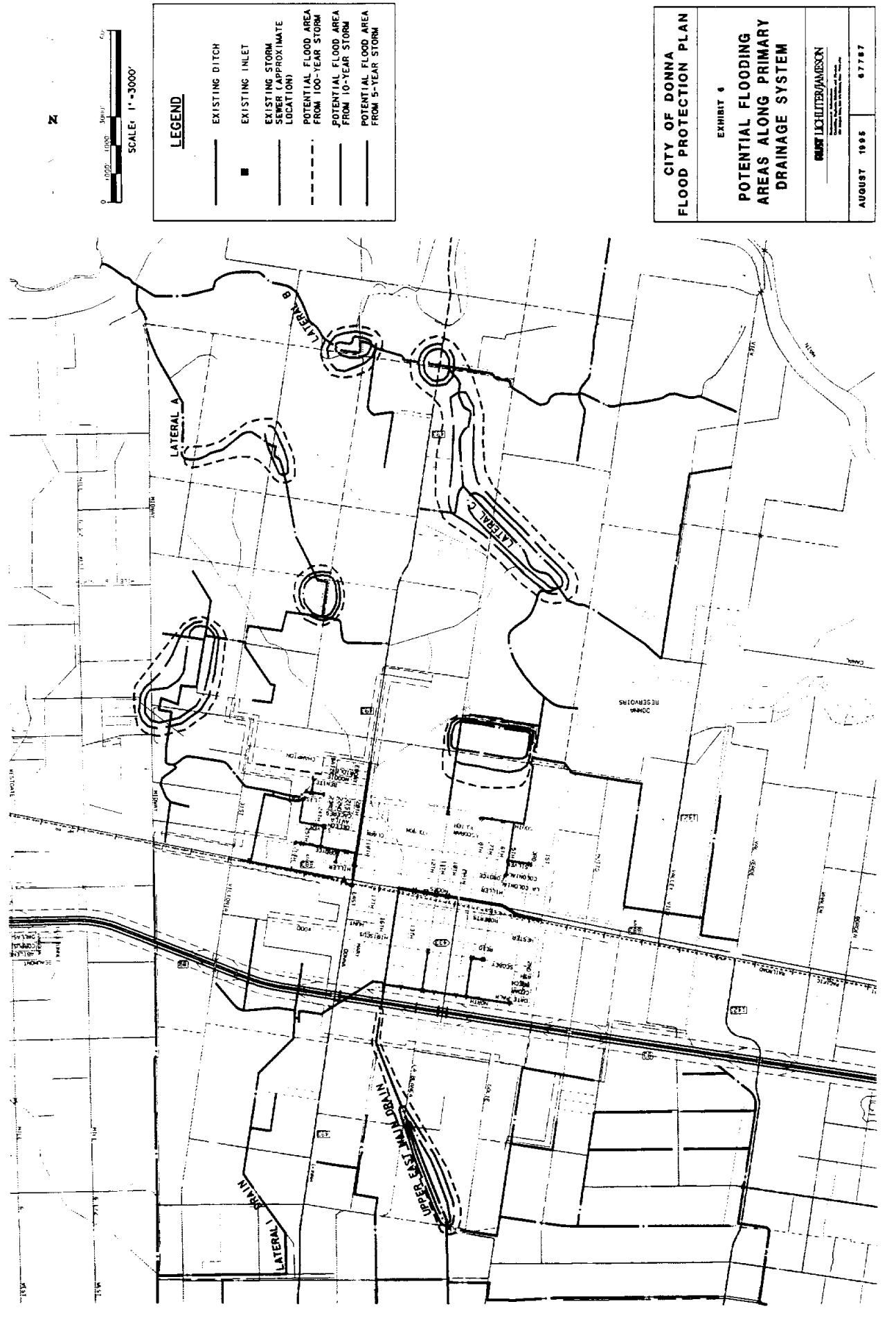


EXHIBIT 5e - FLOOD PROFILES	
CITY OF DONNA FLOOD PROTECTION PLAN	
UPPER EAST MAIN DRAIN	
AUGUST 1986	67787
BENSON, LUCILLE/MESON	





SCALE: 1" = 3000'
0 1000 2000 3000 4000 5000

LEGEND

EXISTING DITCH

PROJECTED AREAS OF
FUTURE DEVELOPMENT

CITY OF DONNA
FLOOD PROTECTION PLAN

EXHIBIT 7
PROJECTED DEVELOPMENT
THROUGH 2005

BEST LIGHTER JAMISON

AUGUST 1985 67767



4.0 RECOMMENDED FLOOD PROTECTION PLAN

Using the results of analysis discussed in Section 3.0 above, the Engineer developed a Flood Protection Plan that mitigates the 5-, 10- and 100-year design flood along the primary drainage channels in areas of existing or projected future development. The plan also eliminates or reduces the flooding within the City caused by the inadequate existing storm sewer system. Typically, severe storm events will still surcharge the storm sewer system and cause flow to pond or be conveyed in the street system; however, the improved storm sewer system will provide conveyance that will significantly decrease the time and depth of ponding and should decrease or eliminate inconvenience to vehicular or pedestrian traffic. Additional surveying of the local topography and the existing storm sewer/street system must be done before the preparation of construction drawings for any element of the proposed plan in order to supplement the limited data used in this study.

The Flood Protection Plan is shown on Exhibit 8 and is composed of elements that add or replace thousands of linear feet of storm sewer pipe, add or expand the placement of inlet/lead systems, involve several thousand feet of open-cut roadway and driveway culverts, include nearly a thousand feet of bore-and-jack crossings, and proposes over three miles of channel clearing, clean-out and/or improvements. Table 4-1 lists the components of the Plan and shows cost estimates for construction activities involved with each component. The estimated cost for the recommended Flood Protection Plan for the City of Donna is \$4,250,000 (does not include utility adjustments or other soft costs).

Channel improvements are recommended for many reaches of ditches in both the primary and secondary drainage systems. Most of the improvements are along roadside ditches or existing primary channels, with one new bypass ditch proposed southeast of the City. This new ditch is necessary to relieve flooding conditions along Lateral A which threaten the development in low-lying areas. Costs for right-of-way acquisition are included in Table 4-1. For existing channel improvements, only the cost for the additional easement is included in construction estimates.

Channel clearing shown on the plan consists of cleaning out debris and silt which has accumulated in the channel, clearing one bank of all vegetation except groundcover, and digging out the bottom with a backhoe. Many of the primary channels have sufficient storage capacity even with the heavy growth of vegetation; however, the flowline of the channel, culverts and storm sewer outfalls cannot be maintained without having at least one side cleared and accessible to maintenance crews and machinery.

The Engineer assumed bore-and-jack or tunneling construction techniques for the proposed irrigation ditch crossings along the primary channels so that the use of the irrigation ditches is not interrupted. For the wider irrigation ditch crossings with embankments, portions of the pipe culvert construction can be open-cut with the about 50

feet requiring tunneling directly under the conveyance portion of the ditch. All other culvert installations are assumed to be applicable to the less expensive open-cut construction techniques. The costs for installing driveway and street culverts given in Table 4-1 include pavement replacement.

TABLE 4-1
RECOMMENDED FLOOD PROTECTION PLAN
CONSTRUCTION COST ESTIMATE

ITEM	DESCRIPTION	UNIT	QTY	CONSTRUCTION COST	
				UNIT COST	TOTAL
1	18-Inch R.C.P. Storm Sewer w/M.H.	LF	5800	\$30.00	\$174,000
2	24-Inch R.C.P. Storm Sewer w/M.H.	LF	8200	\$40.00	\$328,000
3	30-Inch R.C.P. Storm Sewer w/M.H.	LF	4200	\$50.00	\$210,000
4	36-Inch R.C.P. Storm Sewer w/M.H.	LF	3500	\$60.00	\$210,000
5	48-Inch R.C.P. Storm Sewer w/M.H.	LF	6000	\$80.00	\$480,000
6	60-Inch R.C.P. Storm Sewer w/M.H.	LF	2000	\$100.00	\$200,000
7	Inlet with 18-Inch R.C.P. Lead	EA	76	\$1,800.00	\$136,800
8	72-Inch Open Cut Culvert	LF	150	\$90.00	\$13,500
9	60-Inch Open Cut Culvert	LF	950	\$80.00	\$76,000
10	48-Inch Open Cut Culvert	LF	160	\$70.00	\$11,200
11	36-Inch Open Cut Culvert	LF	100	\$60.00	\$6,000
12	72-Inch Bore & Jack Crossing	LF	100	\$250.00	\$25,000
13	60-Inch Bore & Jack Crossing	LF	860	\$200.00	\$172,000
14	48-Inch Bore & Jack Crossing	LF	360	\$150.00	\$54,000
15	36-Inch Bore & Jack Crossing	LF	50	\$100.00	\$5,000
16	Channel Debris & Silt Clean out	LF	21000	\$30.00	\$630,000
17	Channel Cross-Section Improvement	LF	14200	\$40.00	\$568,000
18	New Channel	CY	25000	\$3.00	\$75,000
Sub-Total Estimated Construction Costs					<hr/> \$3,374,500
Right-of-Way Costs					<hr/> \$75,000
Sub-Total Construction w/ROW Costs					<hr/> \$3,449,500
Contingencies (10%)					<hr/> \$344,950
Sub-Total					<hr/> \$3,794,450
Engineering, Surveying, Const. Adm. (12%)					<hr/> \$455,334
TOTAL					<hr/> \$4,249,784
ROUND TO					<hr/> \$4,250,000

5.0 IMPLEMENTATION PLAN

5.1 Phasing

The Flood Protection Plan recommended in Section 3.0 was divided into three phases for implementation. The third phase is the Recommended Flood Protection Plan discussed in the previous section and shown on Exhibit 8. Phase 1 and Phase 2 are the 5-year and 10-year implementation plans. The meaning of "5-year" and "10-year" in this context refers to construction work over the next 5- or 10-year period and does not have the same meaning as in the earlier discussion of design storm frequency.

A. Phase 1

The Phase 1 Implementation Plan consists of the critical improvements that will be most cost effective in reducing flooding in the City of Donna. The Phase 1 improvements are presented on Exhibit 9 and have been structured so that they can be constructed within a 5-year time frame with financing as discussed below. The estimated costs of these improvements are \$1,350,000 as summarized on Table 5-1. Some improvements are outside the City or its ETJ and are required to increase the conveyance of the primary drainage system serving the City. All elements of Phase 1 are compatible with the recommended Flood Protection Plan.

B. Phase 2

The Phase 2 Implementation Plan is the second tier of improvements recommended upon completion of Phase 1 when additional drainage funds become available. Using the financing assumption discussed below in Section 5.2, these improvements should be able to be fully constructed in 10-years. The Phase 1 and Phase 2 improvements are presented on Exhibit 10. The estimated costs of the Phase 2 improvements are an additional \$1,450,000. The total project which includes Phase 1 and Phase 2 is summarized on Table 5-2. All elements of Phase 2 follow the Phase 1 improvements and are compatible with the remainder of the Flood Protection Plan.

C. Phase 3

The Phase 3 Implementation Plan is the third tier of improvements which completes the Flood Protection Plan. The additional estimated costs of the Phase 3 improvements are \$1,450,000, bringing the total cost of the Plan to \$4,250,000 as shown in Table 4-1.

TABLE 5-1
5-YEAR IMPLEMENTATION PLAN
CONSTRUCTION COST ESTIMATE

ITEM DESCRIPTION	UNIT	QTY	CONSTRUCTION COST	
			UNIT COST	TOTAL
1 18-Inch R.C.P. Storm Sewer w/M.H.	LF	2400	\$30.00	\$72,000
2 24-Inch R.C.P. Storm Sewer w/M.H.	LF	3200	\$40.00	\$128,000
3 30-Inch R.C.P. Storm Sewer w/M.H.	LF	1500	\$50.00	\$75,000
4 36-Inch R.C.P. Storm Sewer w/M.H.	LF	1400	\$60.00	\$84,000
5 48-Inch R.C.P. Storm Sewer w/M.H.	LF	900	\$80.00	\$72,000
6 60-Inch R.C.P. Storm Sewer w/M.H.	LF	2000	\$100.00	\$200,000
7 Inlet with 18-Inch R.C.P. Lead	EA	33	\$1,800.00	\$59,400
8 72-Inch Open Cut Culvert	LF	0	\$90.00	\$0
9 60-Inch Open Cut Culvert	LF	610	\$80.00	\$48,800
10 48-Inch Open Cut Culvert	LF	0	\$70.00	\$0
11 36-Inch Open Cut Culvert	LF	100	\$60.00	\$6,000
12 72-Inch Bore & Jack Crossing	LF	0	\$250.00	\$0
13 60-Inch Bore & Jack Crossing	LF	250	\$200.00	\$50,000
14 48-Inch Bore & Jack Crossing	LF	0	\$150.00	\$0
15 36-Inch Bore & Jack Crossing	LF	50	\$100.00	\$5,000
16 Channel Debris & Silt Cleanout	LF	5000	\$30.00	\$150,000
17 Channel Cross-Section Improvement	LF	3000	\$40.00	\$120,000
18 New Channel	CY	0	\$3.00	\$0
Sub-Total Estimated Construction Costs				\$1,070,200
Right-of-Way Costs				\$25,000
Sub-Total Construction w/R.O.W. Costs				\$1,095,200
Contingencies (10%)				\$109,520
Sub-Total				\$1,204,720
Engineering, Surveying, Const. Adm. (12%)				\$144,566
TOTAL				\$1,349,286

Rust Lichliter/Jameson 10/10/2019 \$1,349,286

TABLE 5-2
10-YEAR IMPLEMENTATION PLAN
CONSTRUCTION COST ESTIMATE
(inclusive of the 5-Year Plan)

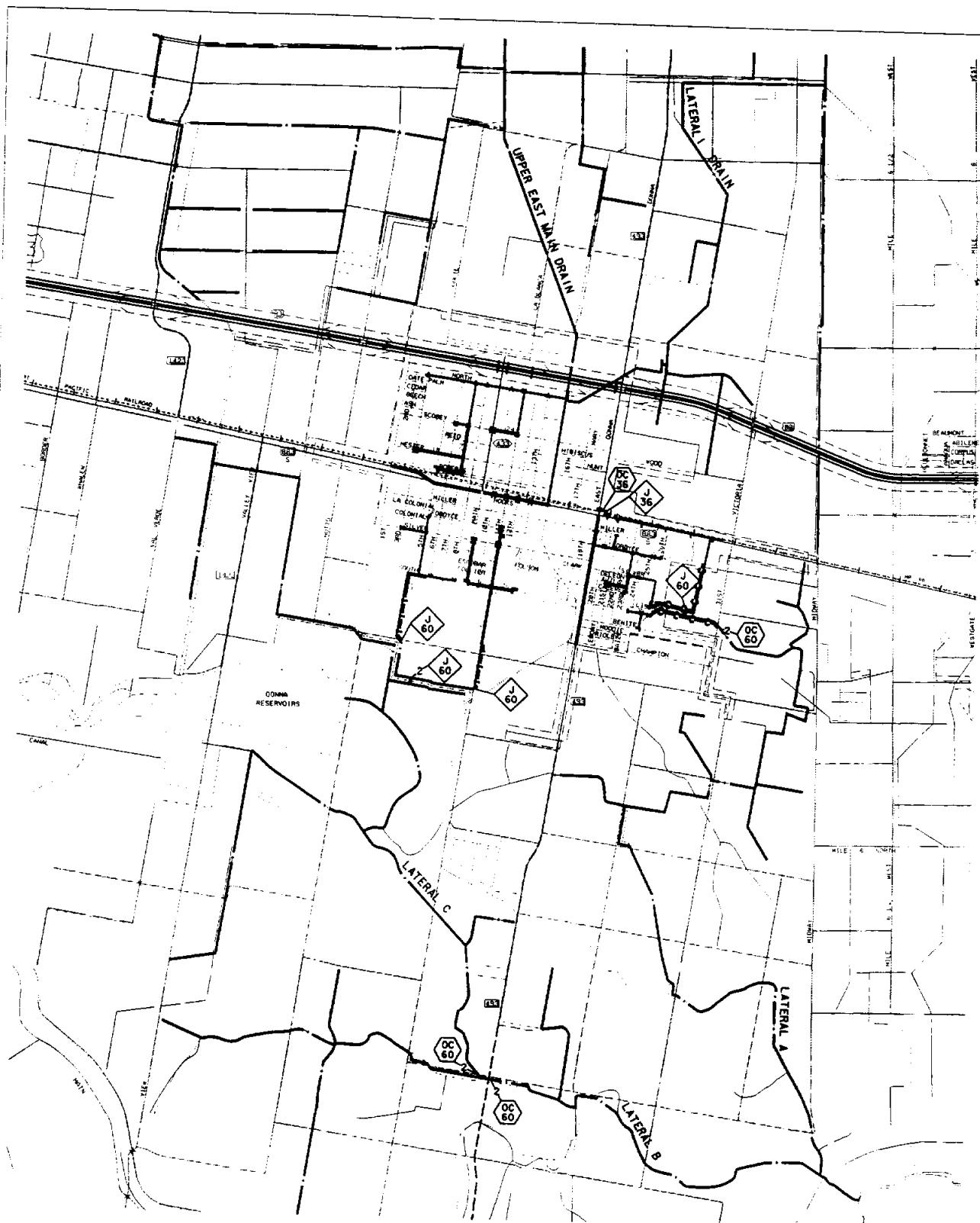
ITEM DESCRIPTION	UNIT	QTY	CONSTRUCTION COST	
			UNIT COST	TOTAL
1 18-Inch R.C.P. Storm Sewer w/M.H.	LF	4000	\$30.00	\$120,000
2 24-Inch R.C.P. Storm Sewer w/M.H.	LF	8200	\$40.00	\$328,000
3 30-Inch R.C.P. Storm Sewer w/M.H.	LF	3000	\$50.00	\$150,000
4 36-Inch R.C.P. Storm Sewer w/M.H.	LF	3600	\$60.00	\$216,000
5 48-Inch R.C.P. Storm Sewer w/M.H.	LF	6000	\$80.00	\$480,000
6 60-Inch R.C.P. Storm Sewer w/M.H.	LF	2000	\$100.00	\$200,000
7 Inlet with 18-Inch R.C.P. Lead	EA	64	\$1,800.00	\$115,200
8 72-Inch Open Cut Culvert	LF	150	\$90.00	\$13,500
9 60-Inch Open Cut Culvert	LF	610	\$80.00	\$48,800
10 48-Inch Open Cut Culvert	LF	50	\$70.00	\$3,500
11 36-Inch Open Cut Culvert	LF	100	\$60.00	\$6,000
12 72-Inch Bore & Jack Crossing	LF	100	\$250.00	\$25,000
13 60-Inch Bore & Jack Crossing	LF	400	\$200.00	\$80,000
14 48-Inch Bore & Jack Crossing	LF	150	\$150.00	\$22,500
15 36-Inch Bore & Jack Crossing	LF	50	\$100.00	\$5,000
16 Channel Debris & Silt Cleanout	LF	0	\$30.00	\$0
17 Channel Cross-Section Improvement	LF	9000	\$40.00	\$360,000
18 New Channel	CY	25000	\$3.00	\$75,000
Sub-Total Estimated Construction Costs				<hr/> \$2,248,500
Right-of-Way Costs				<hr/> \$25,000
Sub-Total Construction w/R.O.W. Costs				<hr/> \$2,273,500
Contingencies (10%)				<hr/> \$227,350
Sub-Total				<hr/> \$2,500,850
Engineering, Surveying, Const. Adm. (12%)				<hr/> \$300,102
TOTAL				<hr/> \$2,800,952

ROUND TO \$2,800,952

5.2 Financing

The total estimated cost of the Flood Protection Plan is \$4,200,000. The majority of these costs will be borne by the City. The cost of some future facilities may be paid by developers in cases where portions of the plan are not constructed and drainage capacity is not available.

Commitments are in place for most of the funding for the 5-year plan. The City has \$500,000 allocated to the project from certificates of obligation to be issued this year. In addition, Urban County Funds of \$535,000 per year for the next four years will be provided. Hidalgo County will provide about \$500,000 in "in kind" services to the plan. Their service will be in channel improvement, channel clearing and desnagging, and the construction of certain culverts. For the "in kind" work on urban culverts, the City would provide the materials and the County would perform the work with their equipment and personnel. It is anticipated that the remainder of the 10-year plan (\$1,450,000) and the ultimate recommended Flood Protection Plan (\$1,450,000) will be funded with future bond issues or any available State grants or loans.



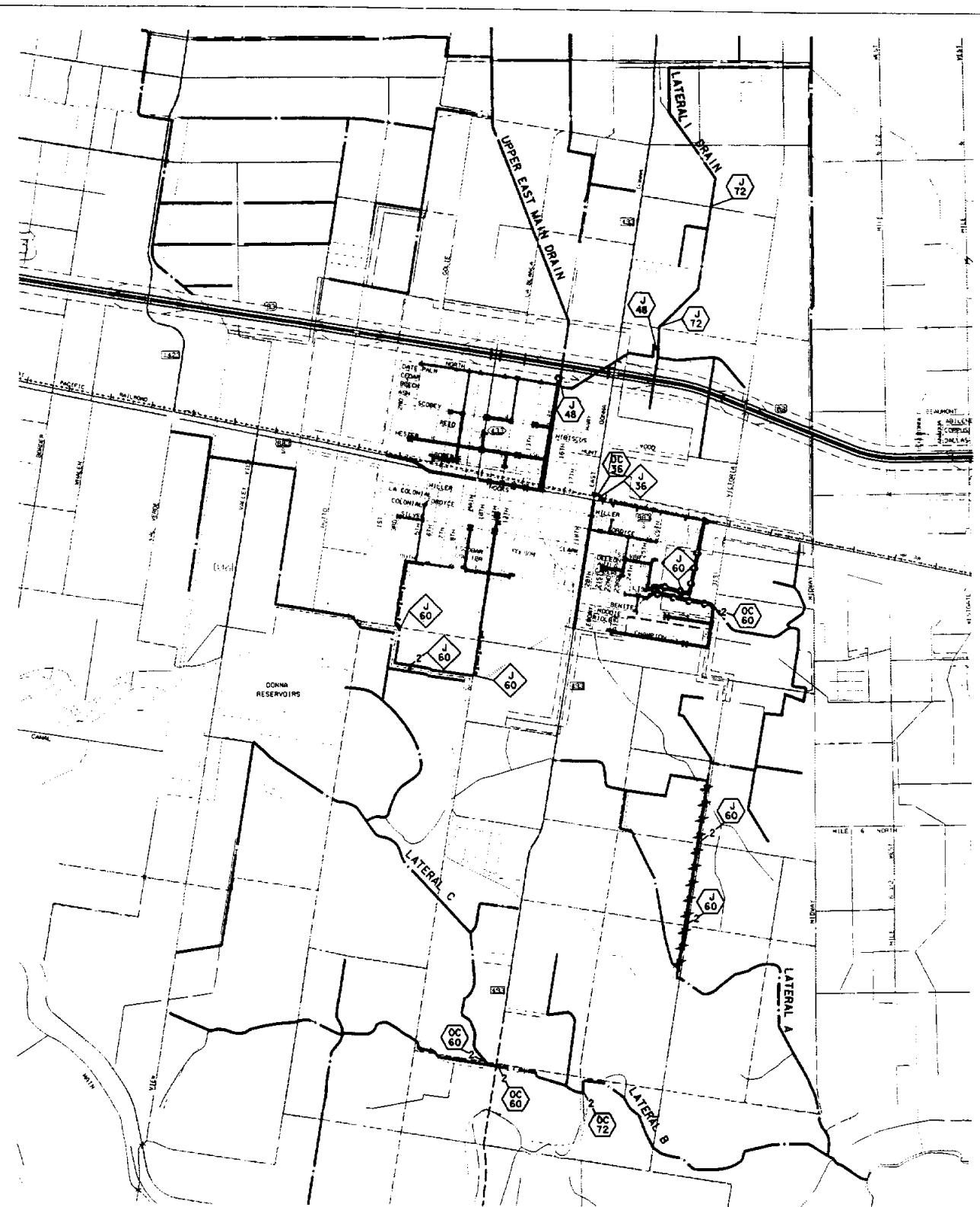
CITY OF DONNA
FLOOD PROTECTION PL/

EXHIBIT 6

5-YEAR
IMPLEMENTATION PLAN

MR. LUCILLE JAMESON

AUGUST 1985 67775



LEGEND

EXISTING

EXISTING DITCH

EXISTING INLET

EXISTING STORM
SEWER (APPROXIMATE
LOCATION)

PROPOSED

STORM SEWER

INLET W/ 18" LEAD

OPEN CUT TWO
60° R.C.P.

BORE & JACK
60° R.C.P.

CHANNEL CLEAN OUT

CHANNEL
IMPROVEMENT

NEW DITCH

SCALE 1" = 3000'

0 1000 1500 2000 2500 3000 3500 4000 4500 5000 5500 6000 6500 7000 7500 8000 8500 9000 9500 10000

CITY OF DONNA FLOOD PROTECTION PLAN	
EXHIBIT 10	
10-YEAR IMPLEMENTATION PLAN	
LOCHMILLER/JAMISON	
AUGUST 1995	67767

APPENDIX A

Existing Conditions HEC-1 Model

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 08/08/95 TIME 07:55:44 *

* * U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
* *

X	X	XXXXXX	XXXX	X
X	X	X	X	X
X	X	X	X	XX
XXXXXX	XXXX	X	XXXX	X
X	X	X	X	X
X	X	X	X	X
X	X	XXXXXX	XXXX	XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*DIAGRAM

1 ID CITY OF DONNA FLOOD STUDY RUST JOB NO. 67787
 2 ID DESIGN FREQUENCY MODEL 24 -HOUR AREAS A, B AND C
 3 ID FILENAME: DONNA_S.HC1 CSG 07/21/95
 4 IT 20 01JAN95 0000 500
 5 IO 5 0 0
 6 JP 3

* Divide original Sub-A1 into three subareas

*

7 KK Ala
 8 KO 21
 9 KM SUBAREA A1 - NORTHWEST PORTION DRAINED BY EXISTING STORM SEWER SYSTEM
 10 BA .61
 11 LS 0 BS
 12 UD 13.37

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR , 25 YEAR AND 100 YEAR EVENTS FROM TP-40

	* DURATION=		5MIN	15 MIN	1HR	2HR	3HR	6HR	12HR	24HR
13 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
14 KP	2									
15 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
16 KP	3									
17 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0

*

18 KK Ala>A1
 19 KO 21
 20 KM ROUTE SUB_A1A TO COMBINING POINT A1
 21 KM 18" PIPE OUTFALL - MODELED AS DETENTION RESERVOIR
 22 RS 1 -1
 23 SA 0 25 50 100 150 200 300 390
 24 SE 77 78 79 80 81 82 83 83.1
 25 SQ 0 17 20 21 23 25 26 30

*

26 KK Alb
 27 KO 21
 28 KM SUBAREA A1 - CENTRAL PORTION DRAINING TO 24" RCP
 29 BA .27
 30 LS 0 85.4
 31 UD 3.7

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR , 25 YEAR AND 100 YEAR EVENTS FROM TP-40

	* DURATION=		5MIN	15 MIN	1HR	2HR	3HR	6HR	12HR	24HR
32 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
33 KP	2									
34 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
35 KP	3									
36 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0

*

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

37 KK A1b>A1
 38 KM ROUTE SUB_A1b TO COMBINING POINT A1
 39 KO 21
 40 KM MODELED AS DETENTION RESERVOIR
 41 RS 1 -1
 42 SA 10 25 50 100 150 173
 43 SE 79 80 81 82 83 83.1
 44 SQ 0 33 39 47 55 65
 *

45 KK A1c
 46 KO 21
 47 KM SUBAREA A1 - SOUTH PORTION DRAINING TO 30" RCP
 48 BA .13
 49 LS 0 75
 50 UD 3.69

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR, 25 YEAR AND 100 YEAR EVENTS FROM TP-40

	DURATION=	5MIN	15 MIN	1HR	2HR	3HR	6HR	12HR	24HR
51 PH	20	0		2.7	3.4	3.7	4.4	5.1	6.0
52 KP	2								
53 PH	10	0		3.2	4.0	4.3	5.1	6.2	7.2
54 KP	3								
55 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5
	*								11.0

56 KK A1c>A1
 57 KO 21
 58 KM ROUTE SUB_A1c TO COMBINING POINT A1
 59 KM MODELED AS DETENTION RESERVOIR
 60 RS 1 -1
 61 SV 0 3 5 7 9 10 1879
 62 SQ 0 10 20 30 40 50 2000
 *

63 KK A1
 64 KO 21
 65 KM COMBINE THREE SUBAREAS AT A1
 66 HC 3
 *
 * BEGIN LATERAL "A"
 *

67 KK A1>A2
 68 KM ROUTE SUB_A1 FROM COMBINING POINT A1 TO A2
 69 KM HEC2 CROSS SECTIONS 30250 - 25060
 70 RS 5 -1
 71 SV 0 1.24 1.98 2.65 3.29 3.92 1084.74
 72 SQ 0 10 20 30 40 50 2000

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

73 KK SUB_A2
 74 KM SUBAREA A2
 75 BA 1.27
 76 LS 0 76.1
 77 UD 7.33

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR , 25 YEAR AND 100 YEAR EVENTS FROM TP40

	* DURATION=		5MIN	15MIN	1HR	2HR	3HR	6HR	12HR	24HR
78 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
79 KP	2									
80 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
81 KP	3									
82 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0

83 KK A2
 84 KM COMBINE SUB_A2 HYDROGRAPH WITH ROUTED HYDROGRAPH
 85 HC 2

86 KK A2>A3
 87 KM ROUTE TOTAL FLOW FROM COMBINING POINT A2 TO A3
 88 KM HEC2 CROSS SECTIONS 25060-19370
 89 RS 11 -1
 90 SV 0 3 5 7 9 10 1879
 91 SQ 0 10 20 30 40 50 2000

92 KK SUB_A3
 93 KM SUBAREA A3
 94 BA 1.06
 95 LS 0 77.2
 96 UD 8.97

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR , 25 YEAR AND 100 YEAR EVENTS FROM TP40

	* DURATION=		5MIN	15MIN	1HR	2HR	3HR	6HR	12HR	24HR
97 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
98 KP	2									
99 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
100 KP	3									
101 PH	1	0			4.5	5.7	6.3	7.7	9.5	11.0
	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0

102 KK A3
 103 KM COMBINE SUB_A3 HYDROGRAPH WITH ROUTED HYDROGRAPH
 104 HC 2

105 KK A3>A4
 106 KM ROUTE TOTAL FLOW FROM COMBINING POINT A3 TO A4
 107 KM HEC2 CROSS SECTIONS 19370-9980
 108 RS 10
 109 SV 0 5 7 10 12 13 3130
 110 SQ 0 10 20 30 40 50 2000

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

111 KK SUB_A4
 112 KM SUBAREA A4
 113 BA 2.43
 114 LS 0 78.3
 115 UD 8.45

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR , 25 YEAR AND 100 YEAR EVENTS FROM TP40

* DURATION= SMIN 15MIN 1HR 2HR 3HR 6HR 12HR 24HR

	PH	20	0	2.7	3.4	3.7	4.4	5.1	6.0
117	KP	2							
118	PH	10	0	3.2	4.0	4.3	5.1	6.2	7.2
119	KP	3							
120	*	1	0	4.5	5.7	6.3	7.7	9.5	11.0
	PH	1	0	.87	1.5	4.3	5.7	6.3	7.7
121	KK	A4							
122	KM	COMBINE SUB_A4 HYDROGRAPH WITH ROUTED HYDROGRAPH							
123	HC	2							
124	KK	A4>A5							
125	KM	ROUTE TOTAL FLOW FROM COMBINING POINT A4 TO A5							
126	KM	HEC2 CROSS SECTIONS 9980-100							
127	RS	6							
128	SV	0 5 6 7 8 9 1224							
129	SQ	0 10 20 30 40 50 2000							
130	KK	SUB_A5							
131	KM	SUBAREA A5							
132	BA	2.54							
133	LS	0 79.4							
134	UD	11.17							
	PH	20	0	2.7	3.4	3.7	4.4	5.1	6.0
136	KP	2							
137	PH	10	0	3.2	4.0	4.3	5.1	6.2	7.2
138	KP	3							
139	*	1	0	4.5	5.7	6.3	7.7	9.5	11.0
	PH	1	0	.87	1.5	4.3	5.7	6.3	7.7
140	KK	A5							
141	KM	COMBINE SUB_A5 HYDROGRAPH WITH ROUTED HYDROGRAPH UPSTREAM OF MOUTH							
142	KM	FOR THE TOTAL "A" HYDROGRAPH							
143	KO	21							
144	HC	2							
	*								
	* BEGIN LATERAL "B"								
145	KK	SUB_B1							
146	KM	SUBAREA B1							
147	KO	21							
148	BA	2.95							
149	LS	0 86							
150	UD	14.87							

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

151 PH 20 0 2.7 3.4 3.7 4.4 5.1 6.0
 152 KP 2
 153 PH 10 0 3.2 4.0 4.3 5.1 6.2 7.2
 154 KP 3
 * 1 0 4.5 5.7 6.3 7.7 9.5 11.0
 155 PH 1 0 .87 1.5 4.3 5.7 6.3 7.7 9.5 11.0
 *
 * BEGIN LATERAL "C"
 156 KK SUB_C1
 157 KM SUBAREA C1
 158 KO 21
 159 BA 0.24
 160 LS 0 85
 161 UD 1.59
 * RAINFALL DATA FOR THE 5 YEAR, 10 YEAR , 25 YEAR AND 100 YEAR EVENTS FROM TP40
 * DURATION= 5MIN 15MIN 1HR 2HR 3HR 6HR 12HR 24HR
 162 PH 20 0 2.7 3.4 3.7 4.4 5.1 6.0
 163 KP 2
 164 PH 10 0 3.2 4.0 4.3 5.1 6.2 7.2
 165 KP 3
 * 1 0 4.5 5.7 6.3 7.7 9.5 11.0
 166 PH 1 0 .87 1.5 4.3 5.7 6.3 7.7 9.5 11.0
 *
 * Constricted with ____" pipe
 *
 167 KK C1>C3
 168 KM ROUTE SUB_C1 FROM COMBINING POINT C1 TO C3
 169 KM HEC2 CROSS SECTIONS 17000-22000
 170 KO 21
 171 RS 100 -1
 172 SV 0 1 5 498 1348 1355 1650 1831 1912
 173 SQ 0 5 10 15 20 25 1000 2000 2500
 174 KK SUB_C2
 175 KM SUBAREA C2
 176 KO 21
 177 BA 0.24
 178 LS 0 85
 179 UD 3.17
 * RAINFALL DATA FOR THE 5 YEAR, 10 YEAR , 25 YEAR AND 100 YEAR EVENTS FROM TP40
 * DURATION= 5MIN 15MIN 1HR 2HR 3HR 6HR 12HR 24HR
 180 PH 20 0 2.7 3.4 3.7 4.4 5.1 6.0
 181 KP 2
 182 PH 10 0 3.2 4.0 4.3 5.1 6.2 7.2
 183 KP 3
 * 1 0 4.5 5.7 6.3 7.7 9.5 11.0
 184 PH 1 0 .87 1.5 4.3 5.7 6.3 7.7 9.5 11.0
 *
 * Constricted w/ ____" pipe
 *

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

185 KK C2>C3
 186 KM ROUTE TOTAL FLOW FROM COMBINING POINT C2 TO C3
 187 KM HEC2 CROSS SECTIONS 22000-196700
 188 KO 21
 189 RS 15 -1
 190 SV 0 1 6 1280 3721 3741 4608 5146 5385
 191 SQ 0 10 20 30 40 50 2000 4000 5000

192 KK SUB_C3
 193 KM SUBAREA C3
 194 KO 21
 195 BA 0.87
 196 LS 0 75
 197 UD 8.8
 * RAINFALL DATA FOR THE 5 YEAR, 10 YEAR, 25 YEAR AND 100 YEAR EVENTS FROM TP40
 * DURATION= 5MIN 15MIN 1HR 2HR 3HR 6HR 12HR 24HR
 198 PH 20 0 2.7 3.4 3.7 4.4 5.1 6.0
 199 KP 2
 200 PH 10 0 3.2 4.0 4.3 5.1 6.2 7.2
 201 KP 3
 * 1 0 4.5 5.7 6.3 7.7 9.5 11.0
 202 PH 1 0 .87 1.5 4.3 5.7 6.3 7.7 9.5 11.0

203 KK C3
 204 KM COMBINE SUB_C3 HYDROGRAPH WITH ROUTED HYDROGRAPHS
 205 KO 21
 206 HC 3

207 KK C3>C4
 208 KM ROUTE TOTAL FLOW FROM COMBINING POINT C3 TO C4
 209 KM HEC2 CROSS SECTIONS 10000-17000
 210 KO 21
 211 RS 3 -1
 212 SV 0 4.3 5.1 5.8 6.7 7.25 1144 2709 3396
 213 SQ 0 10 20 30 40 50 2000 4000 5000

214 KK SUB_C4
 215 KM SUBAREA C4
 216 BA 1.60
 217 LS 0 78.3
 218 UD 17.03
 * RAINFALL DATA FOR THE 5 YEAR, 10 YEAR, 25 YEAR AND 100 YEAR EVENTS FROM TP40
 * DURATION= 5MIN 15MIN 1HR 2HR 3HR 6HR 12HR 24HR
 219 PH 20 0 2.7 3.4 3.7 4.4 5.1 6.0
 220 KP 2
 221 PH 10 0 3.2 4.0 4.3 5.1 6.2 7.2
 222 KP 3
 * 1 0 4.5 5.7 6.3 7.7 9.5 11.0
 223 PH 1 0 .87 1.5 4.3 5.7 6.3 7.7 9.5 11.0

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

224 KK C4
 225 KM COMBINE SUB_C4 HYDROGRAPH WITH ROUTED HYDROGRAPH
 226 HC 2

227 KK C4>C5
 228 KM ROUTE TOTAL FLOW FROM COMBINING POINT C4 TO C5
 229 KM HEC2 CROSS SECTIONS 1000-10000
 230 RS 12 -1
 231 SV 0 32 52 76 110 139 4377 6561 7482
 232 SQ 0 20 40 60 80 100 4000 8000 10000

233 KK SUB_C5
 234 KM SUBAREA C5
 235 BA 3.08
 236 LS 0 85.5
 237 UD 18.68

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR, 25 YEAR AND 100 YEAR EVENTS FROM TP40

	* DURATION=		5MIN	15MIN	1HR	2HR	3HR	6HR	12HR	24HR
238 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
239 KP	2									
240 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
241 KP	3									
*	1	0			4.5	5.7	6.3	7.7	9.5	11.0
242 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0

243 KK C5
 244 KM COMBINE SUB_C5 HYDROGRAPH WITH ROUTED HYDROGRAPH FOR THE TOTAL
 245 KM LATERAL "C" HYDROGRAPH
 246 KO 21
 247 HC 2

248 KK B1
 249 KM COMBINE LATERAL "C" WITH B1 HYDROGRAPH
 250 KO 21
 251 HC 2

252 KK B1>B2
 253 KM ROUTE COMBINED FLOW TO COMBINING POINT "B2"
 254 KM HEC2 CROSS SECTIONS 100-12450
 255 RS 12 -1
 256 SV 0 11 13 14 16 18 1507 3395 4234
 257 SQ 0 10 20 30 40 50 2000 4000 5000

258 KK SUB_B2
 259 KM SUBAREA B2
 260 KO 21
 261 BA 1.59
 262 LS 0 84.9
 263 UD 11.77

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR, 25 YEAR AND 100 YEAR EVENTS FROM TP40

* DURATION= 5MIN 15MIN 1HR 2HR 3HR 6HR 12HR 24HR

HEC-1 INPUT

PAGE 8

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
264	PH 20 0 2.7 3.4 3.7 4.4 5.1 6.0
265	KP 2
266	PH 10 0 3.2 4.0 4.3 5.1 6.2 7.2
267	KP 3
*	1 0 4.5 5.7 6.3 7.7 9.5 11.0
268	PH 1 0 .87 1.5 4.3 5.7 6.3 7.7 9.5 11.0
*	
269	KK B2
270	KM COMBINE LATERALS "B" AND "C" FLOWS AT THE MOUTH
271	KO 21
272	HC 2
*	
273	KK MOUTH
274	KM COMBINE LATERAL'S "A", "B", AND "C" FLOWS AT THE MOUTH
275	KO 21
276	HC 2
277	ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

PUT

V

(V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO.

(.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7 Ala

V

V

18 Ala>A1

26 Alb

V

V

37 Alb>A1

45 Alc

V

V

56 Alc>A1

63 A1.....

V

V

67 A1>A2

SUB_A2

83 A2.....

V

V

86 A2>A3

SUB_A3

102 A3.....

V

V

105 A3>A4

SUB_A4

121 A4.....

V

V

124 A4>A5

SUB_A5

140 A5.....

345

SUB_B1

SUB_C1

V

V

167

C1>C3

74

SUB_C2

V

V

.85

C2>C3

.92

SUB_C3

203

C3.....

V

V

207

C3>C4

214

SUB_C4

C4.....

V

V

C4>C5

:33

SUB_C5

C5.....

248

B1.....

V

V

252

B1>B2

?58

SUB_B2

269

B2.....

273

MOUTH.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 08/08/95 TIME 07:55:44 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *

CITY OF DONNA FLOOD STUDY
DESIGN FREQUENCY MODEL 24 -HOUR
FILENAME: DONNA_S.HC1

RUST JOB NO. 67787
AREAS A, B AND C
CSG 07/21/95

5 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 20 MINUTES IN COMPUTATION INTERVAL
IDATE 1JAN95 STARTING DATE
ITIME 0000 STARTING TIME
NQ 500 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 7JAN95 ENDING DATE
NDTIME 2220 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 0.33 HOURS
TOTAL TIME BASE 166.33 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION

NPLAN 3 NUMBER OF PLANS

JR MULTI-RATIO OPTION

RATIOS OF RUNOFF
1.00

* Ala *

8 KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL

IPILOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *
8 KK * A1a>A1 *
* *

.9 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPILOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *
16 KK * A1b *
* *

.27 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPILOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *
37 KK * A1b>A1 *
* *

--39 KO

OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

* * * * *
45 KK * A1c *
* * * * *

--46 KO

OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

* * * * *
56 KK * A1c>A1 *
* * * * *

--57 KO

OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

* * * * *
63 KK * A1 *
* * * * *

4 KO OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

0 KK * A5 *

143 KO OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

* *
* SUB_B1 *
* *

147 KO OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

156 KK * SUB_C1 *

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *
157 KK * C1>C3 *
* *

0 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *
4 KK * SUB_C2 *
* *

6 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *
5 KK * C2>C3 *
* *

168 KO

OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

* *
192 KK * SUB_C3 *
* *

194 KO

OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

* *
203 KK * C3 *
* *

205 KO

OUTPUT CONTROL VARIABLES

IPRNT	5 PRINT CONTROL
IPLOT	0 PLOT CONTROL
QSCAL	0. HYDROGRAPH PLOT SCALE
IPNCH	0 PUNCH COMPUTED HYDROGRAPH
IOUT	21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500 LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333 TIME INTERVAL IN HOURS

* *
* C3>C4 *
* *

10 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *
* C5 *
* *

13 KK OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *
* B1 *
* *

50 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

* *****
* *
* 58 KK * SUB_B2 *
* *

260 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPILOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

269 KK * B2 *

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

3 KK * MOUTH *

5.5 OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPILOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMEINT	0.333	TIME INTERVAL IN HOURS

(

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO FLOWS	
				RATIO 1	
				1.00	
<u>HYDROGRAPH AT</u>	Ala	0.61	1 FLOW	81.	
			TIME	26.67	
			2 FLOW	107.	
			TIME	26.67	
			3 FLOW	181.	
			TIME	26.67	
<u>ROUTED TO</u>	Ala>A1	0.61	1 FLOW	20.	
			TIME	42.33	
			2 FLOW	21.	
			TIME	44.33	
			3 FLOW	23.	
			TIME	48.00	
			** PEAK STAGES IN FEET **		
			1 STAGE	79.45	
			TIME	42.67	
			2 STAGE	79.95	
			TIME	44.67	
			3 STAGE	80.85	
			TIME	48.00	
<u>HYDROGRAPH AT</u>	Alb	0.27	1 FLOW	102.	
			TIME	16.00	
			2 FLOW	131.	
			TIME	16.00	
			3 FLOW	214.	
			TIME	16.00	
<u>ROUTED TO</u>	Alb>A1	0.27	1 FLOW	35.	
			TIME	20.67	
			2 FLOW	37.	
			TIME	22.00	
			3 FLOW	42.	
			TIME	23.33	
			** PEAK STAGES IN FEET **		
			1 STAGE	80.34	
			TIME	21.00	
			2 STAGE	80.70	
			TIME	22.00	
			3 STAGE	81.42	
			TIME	23.33	
<u>HYDROGRAPH AT</u>	A1c	0.13	1 FLOW	36.	
			TIME	16.33	
			2 FLOW	50.	
			TIME	16.00	
			3 FLOW	89.	
			TIME	16.00	
<u>ROUTED TO</u>	A1c>A1	0.13	1 FLOW	26.	
			TIME	18.33	

		2	FLOW	36.	
			TIME	18.33	
		3	FLOW	56.	
			TIME	18.67	
COMBINED AT	A1	1.01	1	FLOW	75.
				TIME	20.00
		2	FLOW	89.	
			TIME	19.00	
		3	FLOW	115.	
			TIME	20.00	
ROUTED TO	A1>A2	1.01	1	FLOW	68.
				TIME	27.33
		2	FLOW	78.	
			TIME	26.67	
		3	FLOW	106.	
			TIME	26.67	
HYDROGRAPH AT	SUB_A2	1.27	1	FLOW	214.
				TIME	20.33
		2	FLOW	294.	
			TIME	20.33	
		3	FLOW	531.	
			TIME	20.00	
COMBINED AT	A2	2.28	1	FLOW	267.
				TIME	20.33
		2	FLOW	351.	
			TIME	20.67	
		3	FLOW	600.	
			TIME	20.33	
ROUTED TO	A2>A3	2.28	1	FLOW	221.
				TIME	33.00
		2	FLOW	290.	
			TIME	33.00	
		3	FLOW	491.	
			TIME	32.67	
HYDROGRAPH AT	SUB_A3	1.06	1	FLOW	157.
				TIME	22.00
		2	FLOW	215.	
			TIME	22.00	
		3	FLOW	386.	
			TIME	22.00	
COMBINED AT	A3	3.34	1	FLOW	279.
				TIME	31.00
		2	FLOW	368.	
			TIME	31.00	
		3	FLOW	630.	
			TIME	30.67	
ROUTED TO	A3>A4	3.34	1	FLOW	237.
				TIME	49.00
		2	FLOW	311.	
			TIME	49.00	
		3	FLOW	529.	
			TIME	48.67	
HYDROGRAPH AT	SUB_A4	2.43	1	FLOW	390.
				TIME	21.33
		2	FLOW	530.	

				TIME	21.33
		3	FLOW		942.
			TIME		21.33
ROUTED AT	A4	5.77	1	FLOW	440.
				TIME	21.33
		2	FLOW		580.
			TIME		21.33
		3	FLOW		992.
			TIME		21.33
ROUTED TO	A4>A5	5.77	1	FLOW	377.
				TIME	29.67
		2	FLOW		498.
			TIME		29.33
		3	FLOW		852.
			TIME		29.33
HYDROGRAPH AT	SUB_A5	2.54	1	FLOW	335.
				TIME	24.67
		2	FLOW		455.
			TIME		24.33
		3	FLOW		803.
			TIME		24.33
2 COMBINED AT	A5	8.31	1	FLOW	662.
				TIME	27.67
		2	FLOW		886.
			TIME		27.67
		3	FLOW		1537.
			TIME		27.33
HYDROGRAPH AT	SUB_B1	2.95	1	FLOW	366.
				TIME	28.33
		2	FLOW		480.
			TIME		28.33
		3	FLOW		807.
			TIME		28.00
HYDROGRAPH AT	SUB_C1	0.24	1	FLOW	163.
				TIME	14.00
		2	FLOW		209.
			TIME		14.00
		3	FLOW		331.
			TIME		13.67
ROUTED TO	C1>C3	0.24	1	FLOW	10.
				TIME	23.00
		2	FLOW		10.
			TIME		21.67
		3	FLOW		10.
			TIME		20.00
HYDROGRAPH AT	SUB_C2	0.24	1	FLOW	101.
				TIME	15.33
		2	FLOW		130.
			TIME		15.33
		3	FLOW		211.
			TIME		15.33
ROUTED TO	C2>C3	0.24	1	FLOW	20.
				TIME	25.67
		2	FLOW		20.
			TIME		25.33

3 FLOW 20.
TIME 23.67

HYDROGRAPH AT SUB_C3 0.87 1 FLOW 122.
TIME 22.00
2 FLOW 170.
TIME 22.00
3 FLOW 310.
TIME 21.67

3 COMBINED AT C3 1.35 1 FLOW 152.
TIME 22.00
2 FLOW 200.
TIME 22.00
3 FLOW 340.
TIME 21.67

ROUTED TO C3>C4 1.35 1 FLOW 126.
TIME 29.33
2 FLOW 164.
TIME 29.00
3 FLOW 276.
TIME 28.67

DROGRAPH AT SUB_C4 1.60 1 FLOW 144.
TIME 31.00
2 FLOW 196.
TIME 30.67
3 FLOW 349.
TIME 30.67

BINDED AT C4 2.95 1 FLOW 268.
TIME 30.00
2 FLOW 357.
TIME 29.67
3 FLOW 621.
TIME 29.33

ROUTED TO C4>C5 2.95 1 FLOW 245.
TIME 43.67
2 FLOW 325.
TIME 43.33
3 FLOW 563.
TIME 43.00

HYDROGRAPH AT SUB_C5 3.08 1 FLOW 309.
TIME 32.33
2 FLOW 406.
TIME 32.33
3 FLOW 686.
TIME 32.00

COMBINED AT C5 6.03 1 FLOW 466.
TIME 39.00
2 FLOW 618.
TIME 38.67
3 FLOW 1057.
TIME 38.67

BINDED AT B1 8.98 1 FLOW 706.
TIME 31.33
2 FLOW 939.
TIME 33.67
3 FLOW 1617.

TIME 33.00

JTED TO B1>B2 8.98 1 FLOW 693.
TIME 42.00
2 FLOW 920.
TIME 42.33
3 FLOW 1576.
TIME 42.33

PROGRAPH AT SUB_B2 1.59 1 FLOW 234.
TIME 25.00
2 FLOW 309.
TIME 25.00
3 FLOW 522.
TIME 24.67

COMBINED AT B2 10.57 1 FLOW 741.
TIME 40.00
2 FLOW 978.
TIME 40.33
3 FLOW 1672.
TIME 40.67

COMBINED AT MOUTH 18.88 1 FLOW 1142.
TIME 30.67
2 FLOW 1515.
TIME 30.33
3 FLOW 2599.
TIME 30.00

*** NORMAL END OF HEC-1 ***

FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 08/08/95 TIME 07:55:24 *

* * U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
* *

X	X	XXXXXX	XXXXX	X
X	X	X	X	XX
X	X	X	X	X
XXXXXX	XXXX	X	XXXXX	X
X	X	X	X	X
X	X	X	X	X
X	X	XXXXXX	XXXXX	XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*DIAGRAM

1 ID CITY OF DONNA FLOOD STUDY RUST JOB NO. 67787
 2 ID DESIGN FREQUENCY MODEL 24 -HOUR AREA I
 3 ID FILENAME: DONNA_I.HC1 CWW 07/26/95
 4 IT 20 01JAN95 0000 500
 5 IO 5 0 0
 6 JP 3

7 KK SUB_I1
 8 KM SUBAREA I1
 9 BA 0.46
 10 LS 0 76.1
 11 UD 8.44

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR AND 100 YEAR EVENTS FROM TP40

	* DURATION=		SMIN	15MIN	1HR	2HR	3HR	6HR	12HR	24HR
12 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
13 KP	2									
14 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
15 KP	3									
16 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0

*

17 KK RT I1
 18 KM ROUTE FLOWS THROUGH 18" RESTRICTOR PIPE
 19 KM HEC2 CROSS SECTIONS
 20 RS 1 -1
 21 SV 0 3 8 300
 22 SE 80.5 83.5 86.5 87.0
 23 SQ 0 18 24 25
 *

24 KK SUB_I2
 25 KM SUBAREA I2
 26 BA 0.67
 27 LS 0 76.1
 28 UD 6.25

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR AND 100 YEAR EVENTS FROM TP40

	* DURATION=		SMIN	15MIN	1HR	2HR	3HR	6HR	12HR	24HR
29 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
30 KP	2									
31 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
32 KP	3									
33 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0

*

34 KK RT I2
 35 KM ROUTE FLOWS THROUGH 24" RESTRICTOR PIPE UNDER EXPRESSWAY
 36 RS 1 -1
 37 SV 0 1 3 300
 38 SE 81 83.5 86 86.5
 39 SQ 0 20 29 30
 *

*

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

40 KK SUB_I3
41 KM SUBAREA I3
42 KO 21
43 BA 2.18
44 LS 0 76.1
45 UD 16.5

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR AND 100 YEAR EVENTS FROM TP40

*	DURATION=	5MIN	15MIN	1HR	2HR	3HR	6HR	12HR	24HR		
46	PH	20	0		2.7	3.4	3.7	4.4	5.1	6.0	
47	KP	2									
48	PH	10	0		3.2	4.0	4.3	5.1	6.2	7.2	
49	KP	3									
50	PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0

51 KK COMB1
52 KM COMBINE I1 AND I2 ROUTED FLOWS AND I3 HYDROGRAPH
53 KO 21
54 HC 3
*

55 KK I1>I2
56 KM ROUTE FLOWS THROUGH CHANNEL I (FROM EXPRESSWAY TO MOUTH)
57 RS 11 -1
58 SV 0 5 15 34 65 1071 3263
59 SQ 0 10 50 100 200 500 2000
*

60 ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT

(V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7 SUB_I1

V

V

17 RT_I1

24 SUB_I2

V

V

34 RT_I2

40 SUB_I3

V

V

51 COMBI.....

V

V

55 I1>I2

**) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 08/08/95 TIME 07:55:24 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *

CITY OF DONNA FLOOD STUDY
DESIGN FREQUENCY MODEL 24 -HOUR
FILENAME: DONNA_I.HC1

RUST JOB NO. 67787

AREA I

CWW 07/26/95

5 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 20 MINUTES IN COMPUTATION INTERVAL
IDATE 1JAN95 STARTING DATE
ITIME 0000 STARTING TIME
NQ 500 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 7JAN95 ENDING DATE
NDTIME 2220 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 0.33 HOURS
TOTAL TIME BASE 166.33 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION

NPLAN 3 NUMBER OF PLANS

JR MULTI-RATIO OPTION

RATIOS OF RUNOFF

1.00

* *
* SUB_I3 *
* *

KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL

I PLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
I PNCH	0	PUNCH COMPUTED HYDROGRAPH
I OUT	21	SAVE HYDROGRAPH ON THIS UNIT
I SAV1	1	FIRST ORDINATE PUNCHED OR SAVED
I SAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

*

>1 KK * COMB1 *

*

3 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
I PLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
I PNCH	0	PUNCH COMPUTED HYDROGRAPH
I OUT	21	SAVE HYDROGRAPH ON THIS UNIT
I SAV1	1	FIRST ORDINATE PUNCHED OR SAVED
I SAV2	500	LAST ORDINATE PUNCHED OR SAVED
TIMINT	0.333	TIME INTERVAL IN HOURS

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

ERATION	STATION	AREA	PLAN	RATIOS APPLIED TO FLOWS	
				RATIO 1	
				1.00	
HYDROGRAPH AT	SUB_I1	0.46	1	FLOW	69.
				TIME	21.67
			2	FLOW	96.
				TIME	21.67
			3	FLOW	173.
				TIME	21.33
ROUTED TO	RT_I1	0.46	1	FLOW	24.
				TIME	30.33
			2	FLOW	24.
				TIME	32.33
			3	FLOW	24.
				TIME	35.33
			** PEAK STAGES IN FEET **		
			1	STAGE	86.55
				TIME	31.33
			2	STAGE	86.59
				TIME	33.00
			3	STAGE	86.73
				TIME	36.00
HYDROGRAPH AT	SUB_I2	0.67	1	FLOW	129.
				TIME	19.00
			2	FLOW	176.
				TIME	19.00
			3	FLOW	317.
				TIME	19.00
ROUTED TO	RT_I2	0.67	1	FLOW	29.
				TIME	28.67
			2	FLOW	29.
				TIME	30.00
			3	FLOW	30.
				TIME	32.33
			** PEAK STAGES IN FEET **		
			1	STAGE	86.11
				TIME	29.67
			2	STAGE	86.17
				TIME	30.67
			3	STAGE	86.37
				TIME	33.00
HYDROGRAPH AT	SUB_I3	2.18	1	FLOW	188.
				TIME	30.33
			2	FLOW	260.
				TIME	30.33
			3	FLOW	471.
				TIME	30.00
COMBINED AT	COMB1	3.31	1	FLOW	242.
				TIME	30.33

2	FLOW	313.
	TIME	30.33
3	FLOW	525.
	TIME	30.00

RC	ED TO	I1>I2	3.31	1	FLOW	201.
					TIME	47.67
				2	FLOW	227.
					TIME	58.00
				3	FLOW	353.
					TIME	67.00

*** NORMAL END OF HEC-1 ***

*
FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 08/08/95 TIME 07:56:09 *

*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*

X	X	XXXXXX	XXXX	X
X	X	X	X	XX
X	X	X	X	X
XXXXXX	XXXX	X	XXXX	X
X	X	X	X	X
X	X	X	X	X
X	X	XXXXXX	XXXX	XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*DIAGRAM

1 ID CITY OF DONNA FLOOD STUDY RUST JOB NO. 67787
 2 ID DESIGN FREQUENCY MODEL 24 -HOUR AREA UEMD
 3 ID FILENAME: DONNA_UM.HC1
 4 IT 20 01JAN95 0000 500 CWW 07/26/95
 5 IO 5 0 0
 6 JP 3

7 KK SUB_U1
 8 KM SUBAREA U1
 9 BA 1.25
 10 LS 0 85.2
 11 UD 5.67

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR AND 100 YEAR EVENTS FROM TP 40

	* DURATION:		5MIN	15MIN	1HR	2HR	3HR	6HR	12HR	24HR
12 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
13 KP	2									
14 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
15 KP	3									
16 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0
*										

17 KK SUB_U2
 18 KM SUBAREA U2
 19 KO 21
 20 BA 3.91
 21 LS 0 76.7
 22 UD 14.43

* RAINFALL DATA FOR THE 5 YEAR, 10 YEAR AND 100 YEAR EVENTS FROM TP 40

	* DURATION:		5MIN	15MIN	1HR	2HR	3HR	6HR	12HR	24HR
23 PH	20	0			2.7	3.4	3.7	4.4	5.1	6.0
24 KP	2									
25 PH	10	0			3.2	4.0	4.3	5.1	6.2	7.2
26 KP	3									
27 PH	1	0	.87	1.5	4.3	5.7	6.3	7.7	9.5	11.0
*										

28 KK U1
 29 KO 21
 30 HC 2
 *

31 KK U1>U2
 32 KM ROUTE SUB_U1 AND SUB_U2 FROM U1 TO U2
 33 RS 7 -1
 34 SV 0 3 4 6 7 9 1626
 35 SQ 0 10 20 30 40 50 2000
 *
 *
 36 ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

PUT

(V) ROUTING (- - ->) DIVERSION OR PUMP FLOW

NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7 SUB_U1

17 . SUB_U2

28 U1

V

V

31 U1>U2

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 08/08/95 TIME 07:56:09 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *

CITY OF DONNA FLOOD STUDY
DESIGN FREQUENCY MODEL 24 -HOUR
FILENAME: DONNA_UM.HC1

RUST JOB NO. 67787

AREA UEMD

CWW 07/26/95

5 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 20 MINUTES IN COMPUTATION INTERVAL
IDATE 1JAN95 STARTING DATE
ITIME 0000 STARTING TIME
NQ 500 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 7JAN95 ENDING DATE
NDTIME 2220 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 0.33 HOURS
TOTAL TIME BASE 166.33 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION

NPLAN 3 NUMBER OF PLANS

JR MULTI-RATIO OPTION

RATIOS OF RUNOFF

1.00

K *
* SUB_U2 *
*

KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL

I PLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 500 LAST ORDINATE PUNCHED OR SAVED
TIMINT 0.333 TIME INTERVAL IN HOURS

* *
8 KK * U1 *
* *

3 KO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL
I PLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 500 LAST ORDINATE PUNCHED OR SAVED
TIMINT 0.333 TIME INTERVAL IN HOURS

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OF RATION	STATION	AREA	PLAN	RATIOS APPLIED TO FLOWS	
				RATIO 1	
				1.00	
HYDROGRAPH AT	SUB_U1	1.25	1	FLOW	336.
				TIME	18.33
			2	FLOW	435.
				TIME	18.33
			3	FLOW	724.
				TIME	18.00
HYDROGRAPH AT	SUB_U2	3.91	1	FLOW	384.
				TIME	28.00
			2	FLOW	529.
				TIME	28.00
			3	FLOW	955.
				TIME	28.00
2 COMBINED AT	U1	5.16	1	FLOW	484.
				TIME	20.33
			2	FLOW	654.
				TIME	24.67
			3	FLOW	1165.
				TIME	24.67
ROL TO	U1>U2	5.16	1	FLOW	456.
				TIME	34.33
			2	FLOW	619.
				TIME	34.33
			3	FLOW	1100.
				TIME	34.33

** NORMAL END OF HEC-1 ***

APPENDIX B

Existing Conditions HEC-2 Model

HEC-2 WATER SURFACE PROFILES *
*
Y sion 4.6.2; May 1991 *
*
RUN DATE 08AUG95 TIME 08:08:43 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

x x XXXXXXXX XXXXX XXXXX
x x x x x x x x
x x x x x x x x
XXXXXXX XXXX X XXXXX XXXXX
x x x x x x x x
x x x x x x x x
x x XXXXXXXX XXXXX XXXXX

08AUG95 08:08:43

PAGE 1

THIS RUN EXECUTED 08AUG95 08:08:43

3C-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

CITY OF DONNA *
CHANNEL "A" *
EXISTING CONDITIONS *
FILENAME: CHA_100.IH2 *
MODEL STARTS UPSTREAM OF THE LEVEE PUMP STRUCTURE AND PROCEEDS UPSTREAM TO *
VICTORIA RD. NORTH OF STILES ROAD. PLAN & PROFILE DRAWINGS FOR DRAINAGE *
IMPROVEMENTS BY MELDEN & HUNT, INC. AND SIGLER, WINSTON, GREENWOOD & *
ASSOCIATES, INC. DATED 1990 WERE USED TO CREATE CROSS SECTIONS FOR THIS *
MODEL. SOME MODIFICATIONS WERE MADE AFTER FIELD VERIFICATION OF THESE *
PLANS. THE TOPOGRAPHIC MAP PROVIDED BY THE CITY WAS USED TO CREATE SOME *
OF THE CROSS SECTIONS IN THIS MODEL.

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
T2 5-YEAR 24 HOUR FLOWS EXISTING MODEL
T3 FILENAME: CHA_100.IH2 CSG 07/31/95

I CHECK	INQ	N INV	ID IR	STR T	METRIC	H VINS	Q	W SEL	F Q
	2			.0008				68.59	
N PROF	I PLOT	PR PV S	X SEC V	X SEC H	FN	ALL DC	IB W	CH NIM	I TRACE
1		-1							

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38 1 43 55 26 56 60 4 66 63

LPRINT NUMSEC ***** REQUESTED SECTION NUMBERS *****

-10 -10

IHL EQ ICOPY SUBDIV STRT DS RMILE

1

FL OWS FROM DONNA_S1.OH1

5-YR 10-YR 100-YR

QT	3	662	886	1537						
NC	0.9	0.9	0.04	.1	.3					
	100	8	9915	10085						
GR	75.0	8415	64.8	9915	64.8	9965	55.87	9995	55.87	10005
	64.8	10035	64.8	10085	75.0	11585				

	350	8	9910	10090	150	375	250			
GR	75.0	8410	68.5	9910	68.5	9960	56.07	9995	56.07	10005
	68.5	10040	68.5	10090	75.0	11590				

X1	680	8	9910	10090	360	300	330			
GR	75.0	8410	74.3	9910	74.3	9960	56.43	9995	56.43	10005
	74.3	10040	74.3	10090	75.0	11590				

	1180	8	9915	10085	560	430	500			
GR	75.0	8415	70.6	9915	70.6	9965	56.97	9995	56.97	10005
	70.6	10035	70.6	10085	75.0	11585				

X1	1490	10	9915	10085	220	470	310			
GR	75.0	8415	75.0	9600	70.7	9915	70.7	9965	57.24	9995
	57.24	10005	70.7	10035	70.7	10085	75.0	10700	75.0	11585

SPECIAL CULVERT BRIDGE NUM 1

CULVERT SIZE: 7' X 10'

NC			0.3	0.5			*			
	1540	10	9915	10085	50	50	50			
X3	10			9995	67	10005	67			
GR	75.0	8415	75.0	9715	71.2	9915	71.2	9965	57.29	9995
	57.29	10005	71.2	10035	71.2	10085	75.0	10800	75.0	11585

	1.013	0.5	3.0	170	10	7	60	8.2	57.35	57.29
X1	1600	10	9915	10085	60	60	60			
X2		2	0	71.7						
	10		9995	71.7	10005	71.7				
GR	75	8415	75	9715	71.7	9915	71.7	9965	57.35	9995
	57.35	10005	71.7	10035	71.7	10085	75	10800	75	11585

GR	1650	10	9915	10085	50	50	50			
GR	75	8415	75	9715	72.3	9915	72.3	9965	57.40	9995
GR	57.4	10005	72.3	10035	72.3	10085	75	10800	75	11585
NC	0.9	0.9	0.04	.1	.3					
GR	1850	10	9910	10090	250	150	200			
GR	75	8410	75	9710	73.2	9910	73.2	9960	57.57	9995
GR	57.57	10005	73.2	10040	73.2	10090	75	10800	75	11590
X1	2400	10	9910	10090	570	520	550			
GR	76	8410	75	9810	74.5	9910	74.5	9960	58.10	9995
C	58.10	10005	74.5	10040	74.5	10090	75	10800	76	11590
X1	2900	10	9910	10090	530	460	500			
C	76	8410	75	9500	73.2	9910	73.2	9960	58.57	9995
C	58.57	10005	73.2	10040	73.2	10090	75	10700	75.5	11590
GR	3600	9	9915	10085	700	700	700			
GR	75	8415	75	9000	70.0	9915	70.0	9965	59.27	9995
GR	59.27	10005	70.0	10035	70.0	10085	75	11585		
X1	4720	10	9922	10078	1120	1120	1120			
GR	75	8422	75	8700	71.2	9922	71.2	9972	60.39	9995
C	60.39	10005	71.2	10028	71.2	10078	75	10400	75	11578
SPECIAL BRIDGE BRIDGE NUM 2										
ULVERT SIZE: 10' X 7'										
NC	0.3	0.5								
X1	4770	10	9922	10078	20	110	50			
X3	10		9995		69	10005	69			
C	75	8422	75	8600	71.2	9922	71.2	9972	60.32	9995
C	60.32	10005	71.2	10028	71.2	10078	75	10500	75	11578
S	1.013	0.5	3.0	156	7	10	45	8.2	60.33	60.32
X1	4810	10	9922	10078	45	45	45			
X2		2	0	71.2						
X	10		9995	71.2	10005	71.2				
GR	75	8422	75	8700	71.2	9922	71.2	9972	60.33	9995
GR	60.33	10005	71.2	10028	71.2	10078	75	10500	77	11578

	4860	10	9922	10078	40	60	50			
GR	75	8422	75	8600	71.0	9922	71.0	9972	60.56	9995
GR	60.56	10005	71.0	10028	71.0	10078	75	10500	75	11578
NC	0.9	0.9	0.04	0.1	0.3					
	5360	10	9922	10078	500	500	500			
	75	8422	75	8700	72.2	9922	72.2	9972	61.07	9995
GR	61.07	10005	72.2	10028	72.2	10078	75	10500	75	11578
X1	5960	10	9917	10083	600	600	600			
GR	80	8200	75	8900	74.0	9917	74	9967	61.67	9995
	61.67	10005	74.0	10033	74.0	10083	75	10300	75	11583
X1	6220	10	9917	10083	220	300	260			
	77	8417	75	8900	74.0	9917	74	9967	61.95	9995
GR	61.95	10005	74.0	10033	74.0	10083	75	10400	75	11583
	6900	10	9915	10085	1000	300	680			
GR	80	9200	75	9800	71.7	9915	71.7	9965	62.47	9995
GR	62.47	10005	71.7	10035	71.7	10085	75	10300	75	11585
X1	7020	10	9915	10085	110	120	120			
	80	9600	75	9900	72.5	9915	72.5	9965	62.59	9995
	62.59	10005	72.5	10035	72.5	10085	75	10400	75	11585
 SPECIAL CULVERT BRIDGE NUM 3 CULVERT SIZE: 10' X 6'										
NC			0.3	0.5			*			
							*			
	7070	10	9915	10085	50	50	50			
X3	10		9995		67	10005	67			
	80	9600	75	9900	73.7	9915	73.7	9965	64.05	9995
	64.05	10005	73.7	10035	73.7	10085	75	10300	75	11585
	1.013	0.5	3.0	170	6	10	50	8.2	64	64
X1	7120	8	9915	10085	50	50	50			
		2	0	73.7						
	10		9995		76.5	10005	76.5			
GR	80	9500	76.5	9915	76.5	9965	63.92	9995	63.92	10005
GR	76.5	10035	76.5	10085	76.5	11585				

	7170	9	9915	10085	120	5	50			
GR	80	8415	80	9600	77.5	9915	77.5	9965	62.66	9995
GR	62.66	10005	77.5	10035	77.5	10085	77.5	11585		

NC	.9	.9	.04	.1	.3					
	7320	9	9915	10085	155	145	150			
	80	8415	80	9700	77.5	9915	77.5	9965	62.76	9995
GR	62.76	10005	77.5	10035	77.5	10085	77.5	11585		

X1	8000	9	9917	10083	660	700	680			
GR	80	8417	80	9600	76.1	9917	76.1	9967	63.31	9995
C	63.31	10005	76.1	10033	76.1	10083	76.1	11585		

X3	8330	9	9917	10083	450	240	330			
C	80	8417	80	9600	75.2	9917	75.2	9967	63.46	9995
G	63.46	10005	75.2	10033	75.2	10083	75.2	11585		

X	8680	9	9917	10083	100	510	350			
GR	80	8417	80	9700	75.5	9917	75.5	9967	63.74	9995
GR	63.74	10005	75.5	10033	75.5	10083	75.5	11585		

X1	9280	10	9917	10083	600	600	600			
G	80	8417	80	9700	74.5	9917	74.5	9967	64.16	9995
C	64.16	10005	74.5	10033	74.5	10083	75	10200	75	11587

X	9780	10	9922	10078	500	500	500			
C	80	8417	80	9700	74.6	9922	74.6	9972	64.51	9995
GR	64.51	10005	74.6	10028	74.6	10078	75	10300	75	11578

5-YR 10-YR 100-YR

QT	3	440	580	992						
X	9930	10	9922	10078	150	150	150			
G	80	8422	80	9500	74.8	9922	74.8	9972	64.61	9995
GR	64.61	10005	74.8	10028	74.8	10078	75	10200	75	11578

P E C I A L C U L V E R T B R I D G E N U M 4
C U L V E R T S I Z E : 10' X 6'

*

*

N .9 .9 .04 0.3 0.5

	9980	10	9922	10078	50	50	50			
	10			9995	72	10005	72			
GR	80	8422	80	9500	74.5	9922	74.5	9972	65.57	9995
GR	65.57	10005	74.5	10028	74.5	10078	75	10400	75	11578
SC	1.013	0.5	3.0	156	6	10	60	8.2	65.94	65.57
	10040	10	9922	10078	60	60	60			
			2	0	74.5					
X3	10			9995	74.5	10005	74.5			
GR	80	8422	80	9500	74.5	9922	74.5	9972	65.94	9995
GR	65.94	10005	74.5	10028	74.5	10078	75	10400	75	11578
	10120	10	9922	10078	5	240	80			
	80	8422	80	9500	75.9	9922	75.9	9972	64.83	9995
GR	64.83	10005	75.9	10028	75.9	10078	80	10500	80	11578
	.9	.9	.04	.1	.3					
	10270	10	9920	10080	150	150	150			
	80	8420	80	9500	76.2	9920	76.2	9970	64.93	9995
GR	64.93	10005	76.2	10030	76.2	10080	80	10500	80	11580
	10410	10	9910	10090	350	50	140			
GR	80	8410	80	9500	76.1	9910	76.1	9960	64.99	9995
GR	64.9	10005	76.1	10040	76.1	10090	80	10500	80	11590
X1	10510	10	9917	10083	250	50	100			
	80	8417	80	9700	76.3	9917	76.3	9967	65.04	9995
	65.04	10005	76.3	10033	76.3	10083	80	10300	80	11583
	10570	10	9915	10085	10	170	60			
	80	8415	80	9700	76.5	9915	76.5	9965	65.11	9995
GR	65.11	10005	76.5	10035	76.5	10085	80	10300	80	11585
X1	10680	10	9917	10083	50	220	110			
GR	80	8417	80	9700	76.8	9917	76.8	9967	65.21	9995
GR	65.21	10005	76.8	10033	76.8	10083	80	10300	80	11583
X1	11060	10	9920	10080	340	440	380			
	80	8420	80	9800	76.2	9920	76.2	9970	65.49	9995
GR	65.49	10005	76.2	10030	76.2	10080	80	10200	80	11580

11940	10	9920	10080	880	880	880				
GR 83		9200	80	9500	76.3	9920	76.3	9970	66.11	9995
GR 66.11		10005	76.3	10030	76.3	10080	80	11400	80	11580

SPECIAL CULVERT BRIDGE NUM 5
CULVERT SIZE: 7' X 8'

			0.3	0.5						
11990	10	9922	10078	50	50	50				
GR 83	9100	80	9200	76.2	9922	76.2	9972	66.12	9995	
GR 66.12	10005	76.2	10028	76.2	10078	80	11500	85	12100	

SC 1.013	0.5	3.0	156	7	8	60	8.2	66.13	66.12	
12050	9	9922	10078	60	60	60				
X3 10		2	0	76.2						
80 8422		80	9200	76.2	9922	76.2	9972	66.13	9995	
66.13	10005	76.2	10028	76.2	10078	80	11600			

12100	10	9925	10075	50	50	50				
GR 66.14	8425	80	9200	74.8	9925	74.8	9975	66.14	9992	
	10008	74.8	10025	74.8	10075	80	11600	85	11800	

NC .9	.9	.04	.1	.3						
12660	10	9925	10075	560	560	560				
GR 66.2	8100	75	9200	74.1	9925	74.1	9975	66.20	9992	
	10008	74.1	10025	74.1	10075	75	10600	80	12200	

12860	10	9925	10075	600	600	600				
GR 66.26	8100	80	9100	73.6	9925	73.6	9975	66.26	9992	
	10008	73.6	10025	73.6	10075	75	10900	80	11575	

X1 13280	10	9925	10075	500	380	420				
85 8425	80	9200	75	9600	72.5	9925	72.5	9975		
66.3 9992	66.3	10008	72.5	10025	72.5	10075	80	11575		

— 30 IN. IRRIGATION PIPE CROSSING W/ TOP ELEV. OF 72.51 AT 14000

NOT MODELED

*

14280	10	9925	10075	1000	1000	1000					
GR 85	8500	80	9100	72.5	9925	72.5	9975	66.40	9992		
GR 66.4	10008	72.5	.. 10025	72.5	10075	80	10900	85	11500		

X1 14530	10	9925	10075	230	290	250					
GR 85	8500	80	9100	73.2	9925	73.2	9975	66.43	9992		
GR 66.43	10008	73.2	10025	73.2	10075	80	10900	85	11500		

SPECIAL BRIDGE

BRIDGE NUM 6

***CULVERT SIZE: 9' X 6'

NC		0.3	0.5			*					
----	--	-----	-----	--	--	---	--	--	--	--	--

	5-YR	10-YR	100-YR								
QT 3	353	465	796								
XL 14580	10	9925	10075	70	40	50					
	10		9995	73	10005	73					
.. 85	8500	80	9100	74.5	9925	74.5	9975	65.97	9992		
GR 65.97	10008	74.5	10025	74.5	10075	80	10900	85	11500		

SC 1.013	0.5	3.0	156	6	9	70	8.2	65.97	65.97		
	14650	10	9922	10078	70	70	70				
		2	0	74.5							
X3 10			9995	74.5	10005	74.5					
GR 85	8500	80	9100	74.5	9922	74.5	9972	65.97	9992		
GR 65.97	10008	74.5	10028	74.5	10078	80	10900	85	11500		
CROSS SECTIONS		14580 & 14650			*						

14710	8	9925	10075	230	10	60					
GR 73.8	8425	73.8	9925	73.8	9975	66.44	9992	66.44	10008		
GR 73.8	10025	73.8	10075	73.8	11575						

NC		.1	.3								
	14960	8	9925	10075	270	270	270				
GR 73.8	8425	73.8	9925	73.8	9975	66.47	9992	66.47	10008		
GR 73.8	10025	73.8	10075	73.8	11575						

X1 15080	8	9925	10075	5	400	120					
GR 75.1	8425	75.1	9925	75.1	9975	66.49	9992	66.49	10008		
GR 75.1	10025	75.1	10075	75.1	11575						

	16210	8	9925	10075	1130	1130	1130			
GR	73.6	8425	73.6	9925	73.6	9975	66.58	9992	66.58	10008
GR	73.6	10025	73.6	10075	73.6	11575				
X1	16410	8	9917	10083	60	450	200			
GR	77.6	8417	77.6	9917	77.6	9967	66.61	9992	66.61	10008
	77.6	10033	77.6	10083	77.6	11583				
	16710	8	9917	10083	300	300	300			
	77.5	8417	77.5	9917	77.5	9967	66.64	9992	66.64	10008
GR	77.5	10033	77.5	10083	77.5	11583				
	17370	8	9917	10083	660	660	660			
GR	77.6	8417	77.6	9917	77.6	9967	66.71	9992	66.71	10008
	77.6	10033	77.6	10083	77.6	11583				
X1	17530	8	9915	10085	10	170	60			
	77.4	8415	77.4	9915	77.4	9965	66.72	9992	66.72	10008
	77.4	10035	77.4	10085	77.4	11585				
	17660	9	9917	10083	220	50	130			
	80	8417	80	9500	78.0	9917	78.0	9967	66.73	9992
GR	66.73	10008	78.0	10033	78.0	10083	78	11583		
X1	17860	9	9917	10083	200	200	200			
GR	80	8417	80	9500	77.8	9917	77.8	9967	66.75	9992
	66.75	10008	77.8	10033	77.8	10083	77.8	11583		
	18060	8	9915	10085	200	200	200			
	80.2	8415	80.2	9915	80.2	9965	66.77	9992	66.77	10008
GR	80.2	10035	80.2	10085	80.2	11585				
	18220	8	9905	10095	10	400	160			
GR	82.5	8405	82.5	9905	82.5	9955	66.8	9992	66.8	10008
	82.5	10045	82.5	10095	85	11595				
X1	18720	10	9905	10095	500	500	500			
	85	8405	85	9000	82.2	9905	82.2	9955	66.85	9992
	66.85	10008	82.2	10045	82.2	10095	85	11000	85	11595

GR	19220	10	9917	10083	500	500	500			
GR	85	8417	85	9000	78.8	9917	78.8	9967	66.90	9992
GR	66.90	10008	78.8	10033	78.8	10083	80	10500	84	11583

5-YR 10-YR 100-YR

DT	3	279	368	630						
GR	19370	8	9917	10083	300	50	150			
GR	82	8417	79.5	9917	79.5	9967	66.91	9992	66.91	10008
GR	79.5	10033	79.5	10083	85	11583				

X1	19570	8	9917	10083	350	120	200			
GR	78.5	8417	78.5	9917	78.5	9967	66.93	9992	66.93	10008
GR	78.5	10033	78.5	10083	80	11583				

GR	19720	8	9917	10083	350	350	350			
GR	79.2	8417	79.2	9917	79.2	9967	66.97	9992	66.97	10008
GR	79.2	10033	79.2	10083	80	11583				

SPECIAL BRIDGE BRIDGE NUM 7

CULVERT SIZE: 8' X 5' (BUT FILLED WITH 2' OF MUD)
SEDIMENT MODELED ON X3 CARDS THROUGH CULVERT

*

*

			0.3	0.5						
GR	19780	10	9925	10075	10	170	50			
GR	10	68.98		9995	73	10005	73			
GR	85	8425	80	9000	77.3	9925	77.3	9975	66.98	9995
GR	66.98	10005	77.3	10025	77.3	10075	80	10300	82	11575

SC	1.013	0.5	3.0	156	5	8	60	8.2	66.99	66.98
----	-------	-----	-----	-----	---	---	----	-----	-------	-------

I	19840	10	9922	10078	60	60	60			
X3	10	68.99		9995	77.3	10005	77.3			
C	85	8422	80	9000	77.3	9922	77.3	9972	66.99	9995
C	66.99	10005	77.3	10028	77.3	10078	80	10300	82	11578

I	19890	10	9920	10080	50	50	50			
GR	85	8420	80	9000	76.8	9920	76.8	9970	66.99	9992
GR	66.99	10008	76.8	10030	76.8	10080	80	10500	82	11580

.1 .3

X1	20210	10	9920	10080	320	320	320			
	85	8420	80	9000	77.5	9920	77.5	9970	67.02	9992
	67.02	10008	77.5	10030	77.5	10080	80	10900	81	11580

	21060	8	9915	10085	850	850	850			
	85	8000	80.2	9915	80.2	9965	67.11	9992	67.11	10008
GR	80.2	10035	80.2	10085	80.2	11585				

SPECIAL BRIDGE BRIDGE NUM 8
CULVERT SIZE: 6' x 6'

0.3 0.5

X1	21180	8	9925	10075	280	50	100			
	10			9995	73	10005	73			
	79.0	8425	79.0	9925	79.0	9975	67.11	9995	67.11	10005
GR	79.0	10025	79.0	10075	79.0	11575				

SC	1.013	0.5	3.0	156	6	6	80	8.2	67.12	67.11
----	-------	-----	-----	-----	---	---	----	-----	-------	-------

	21260	8	9922	10078	80	80	80			
			2	0	79.0					
X3	10			9995	79.0	10005	79.0			
	79.0	8422	79.0	9922	79.0	9972	67.12	9995	67.12	10005
	79.0	10028	79.0	10078	79.0	11578				

CROSS SECTIONS 21180 & 21260 *

	21300	8	9927	10073	90	10	40			
GR	77.4	8427	77.4	9927	77.4	9977	67.12	9992	67.12	10008
GR	77.4	10023	77.4	10073	77.4	11573				

NC				.1 .3						
----	--	--	--	-------	--	--	--	--	--	--

	21450	8	9920	10080	150	150	150			
GR	77.4	8420	77.4	9920	77.4	9950	67.13	9992	67.13	10008
GR	77.4	10030	77.4	10080	80	11580				

X1	22810	9	9917	10083	1360	1360	1360			
	80	8417	77.1	9917	77.1	9967	67.27	9992	67.27	10008
	77.1	10033	77.1	10083	80	10600	83	11583		

	22960	9	9917	10083	50	250	150			
GR	77.2	8417	77.2	9917	77.2	9967	67.29	9992	67.29	10008
GR	77.2	10033	77.2	10083	80	10500	82	11583		
X1	23320	10	9925	10075	230	450	360			
GR	78	8425	75	9800	74.6	9925	74.6	9975	67.33	9992
	67.33	10008	74.6	10025	74.6	10075	75	10200	79	11575
	23520	9	9922	10078	300	110	200			
	80	8422	75.0	9922	75.0	9972	67.35	9992	67.35	10008
GR	75.0	10028	75.0	10078	80	10900	81	11578		
	23680	9	9925	10075	300	60	160			
GR	78	8425	74.2	9925	74.2	9975	67.36	9992	67.36	10008
	74.2	10025	74.2	10075	80	10700	82	11575		
X1	24080	9	9925	10075	400	400	400			
	76.5	8425	76.5	9925	76.5	9975	67.40	9992	67.40	10008
	76.5	10025	76.5	10075	80	10700	82	11575		
	24380	8	9925	10075	20	400	300			
	75.8	8425	75.8	9925	75.8	9975	67.43	9992	67.43	10008
GR	75.8	10025	75.8	10075	80	11575				
X1	24680	8	9927	10073	300	300	300			
GR	76.0	8427	76.0	9927	76.0	9977	67.46	9992	67.46	10008
	76.0	10023	76.0	10073	80	11573				
X1	24830	8	9927	10073	280	50	150			
	80	8427	76.0	9927	76.0	9977	67.48	9992	67.48	10008
GR	76.0	10023	76.0	10073	80	11573				
	24960	8	9927	10073	300	30	130			
GR	75.6	8427	75.6	9927	75.6	9977	67.49	9992	67.49	10008
GR	75.6	10023	75.6	10073	80	11573				

SPECIAL BRIDGE BRIDGE NUM 9

CULVERT SIZE: 8' X 4.5'

(BUT FILLED WITH 1.5' OF MUD)

*

*

0.3 0.5

	5-YR	10-YR	100-YR							
	3	267	351	600						
X3	25060	8	9925	10075	100	100	100			
	10			9995	74.5	10005	74.5			
GR	75.0	8425	75.0	9925	75.0	9975	67.65	9995	67.65	10005
	75.0	10025	75.0	10075	80	11575				

	1.013	0.5	3.0	156	4.5	8	60	8.2	68.00	67.65
X1	25120	8	9922	10078	60	60	60			
X2			2	0	75.0					
	10			9995	75.0	10005	75.0			
GR	75.0	8422	75.0	9922	75.0	9972	68.00	9995	68.00	10005
	75.0	10028	75.0	10078	80	11578				

X1	25220	8	9930	10070	200	20	100			
GR	75.0	8430	75.0	9930	75.0	9980	68.38	9995	68.38	10005
	75.0	10020	75.0	10070	75.0	11570				

NC				.1	.3					
----	--	--	--	----	----	--	--	--	--	--

	15550	9	9930	10070	30	350	230			
GR	75.0	8430	75.0	9930	75.0	9980	68.75	9995	68.75	10005
	75.0	10020	75.0	10070	80	10900	81	11570		

X1	26560	8	9920	10080	1010	1010	1010			
	79.2	8420	79.2	9920	79.2	9950	69.78	9995	69.78	10005
	79.2	10030	79.2	10080	79.2	11580				

--SPECIAL BRIDGE BRIDGE NUM 10

CULVERT SIZE: 8' X 4'

			0.3	0.5				*		
X1	26670	8	9925	10075	110	110	110			
X2	10			9995	74.5	10005	74.5			
	82.0	8425	82.0	9925	82.0	9975	68.6	9995	68.6	10005
	82.0	10025	82.0	10075	82.0	11575				

1.013	0.5	3.0	156	4	8	55	8.2	68.6	68.6
-------	-----	-----	-----	---	---	----	-----	------	------

08AUG95 08:08:43

PAGE 14

26725	8	9922	10078	55	55	55				
			2	0	82.0					
X3	10			9995	82.0	10005	82.0			
GR	82.0	8422	82.0	9922	82.0	9972	68.6	9995	68.6	10005
	82.0	10028	82.0	10078	82.0	11578				
CROSS SECTIONS		26670 & 26725			*					

26780	8	9920	10080	55	55	55				
GR	82.0	8420	82.0	9920	82.0	9950	70.12	9995	70.12	10005
GR	82.0	10030	82.0	10080	82.0	11580				

NC			.1	.3						
X1	27180	8	9920	10080	400	400	400			
GR	83.0	8420	83.0	9920	83.0	9950	70.52	9995	70.52	10005
GR	83.0	10030	83.0	10080	83.0	11580				

X1	27310	8	9922	10078	270	30	130			
GR	83.2	8422	83.2	9922	83.2	9972	70.62	9995	70.62	10005
	83.2	10028	83.2	10078	83.2	11578				

X1	27520	8	9920	10080	320	80	210			
GR	83.2	8420	83.2	9920	83.2	9950	70.77	9995	70.77	10005
GR	83.2	10030	83.2	10080	83.2	11580				

X1	27720	8	9920	10080	300	50	200			
GR	83.4	8420	83.4	9920	83.4	9950	70.92	9995	70.92	10005
GR	83.4	10030	83.4	10080	83.4	11580				

5-YR 10-YR 100-YR

GR	3	127	157	228						
GR	28140	8	9922	10078	395	465	420			
GR	83.5	8422	83.5	9922	83.5	9972	71.37	9995	71.37	10005
GR	83.5	10028	83.5	10078	83.5	11578				

X1	28460	8	9920	10080	220	420	320			
GR	83.4	8420	83.4	9920	83.4	9950	71.72	9995	71.72	10005
GR	83.4	10030	83.4	10080	83.4	11580				

X1	28960	8	9922	10078	500	500	500			
GR	83.5	8422	83.5	9922	83.5	9972	72.22	9995	72.22	10005
GR	83.5	10028	83.5	10078	83.5	11578				

08AUG95 08:08:43

PAGE 15

29500	8	9925	10075	460	680	540			
GR	84.0	8425	84.0	9925	84.0	9975	72.77	9995	72.77
GR	84.0	10025	84.0	10075	84.0	11575			10005

5-YR 10-YR 100-YR

DT	3	75	89	115					
	30250	8	9925	10075	700	800	750		
---	83.6	8425	83.6	9925	83.6	9975	73.52	9995	73.52
GR	83.6	10025	83.6	10075	83.6	11575			10005

ILEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF PROFILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR DETAILS.

08AUG95 08:08:43

PAGE 17

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
10-YEAR 24 HOUR FLOWS EXISTING MODEL
T3 FILENAME: CHA_100.IH2

CSG 07/31/95

J	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	-10	3			.0008				69.24	
J	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	2		-1							

IHLEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
P FILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
D AILS.

08AUG95 08:08:43

PAGE 18

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
100-YEAR 24 HOUR FLOWS EXISTING MODEL

T3 FILENAME: CHA_100.IH2 CSG 07/31/95

ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
-10	4			.0008				70.87	
NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
15		-1							

JBLEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
OPFILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
DETAILS.

THIS RUN EXECUTED 08AUG95 08:08:49

EC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE--ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

FILENAME: CHA 100.IH2

MARY PRINTOUT

SECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
100.000	64.91	662.00	.01	1.76	.01	100.00	203.57	.00	75.00
100.000	65.34	886.00	.02	1.98	.02	99.91	327.37	.00	75.00
100.000	66.35	1537.00	.04	2.45	.04	99.10	625.54	.00	75.00
*	350.000	65.03	662.00	.00	2.10	.00	100.00	60.44	250.00
*	350.000	65.47	886.00	.00	2.59	.00	100.00	62.91	250.00
*	350.000	66.48	1537.00	.00	3.75	.00	100.00	68.65	250.00
	680.000	65.16	662.00	.00	2.80	.00	100.00	44.22	580.00
	680.000	65.66	886.00	.00	3.42	.00	100.00	46.15	580.00
	680.000	66.81	1537.00	.00	4.88	.00	100.00	50.67	580.00
	1180.000	65.51	662.00	.00	2.69	.00	100.00	47.58	1080.00
	1180.000	66.13	886.00	.00	3.20	.00	100.00	50.34	1080.00
	1180.000	67.64	1537.00	.00	4.30	.00	100.00	56.96	1080.00
	1490.000	65.71	662.00	.00	2.70	.00	100.00	47.80	1390.00
	1490.000	66.40	886.00	.00	3.18	.00	100.00	50.82	1390.00
	1490.000	68.04	1537.00	.00	4.18	.00	100.00	58.14	1390.00
	1540.000	65.38	662.00	.00	8.18	.00	100.00	10.00	1440.00
	1540.000	65.83	886.00	.00	10.37	.00	100.00	10.00	1440.00
*	1540.000	68.77	1537.00	.00	11.20	.00	100.00	35.33	1440.00
	1600.000	68.10	662.00	.00	6.16	.00	100.00	10.00	1500.00
	1600.000	71.10	886.00	.00	6.45	.00	100.00	10.00	1500.00
	1600.000	70.74	1537.00	.00	11.48	.00	100.00	10.00	1500.00
	1650.000	68.82	662.00	.00	1.76	.00	100.00	55.98	1550.00
*	1650.000	71.90	886.00	.00	1.56	.00	100.00	68.38	1550.00
*	1650.000	73.36	1537.00	.02	1.97	.02	99.73	529.54	1550.00

ECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
1850.000	68.86	662.00	.00	1.66	.00	100.00	60.57	1750.00	75.00
1850.000	71.92	886.00	.00	1.46	.00	100.00	74.29	1750.00	75.00
1850.000	73.44	1537.00	.01	2.06	.01	99.99	303.68	1750.00	75.00
2400.000	68.97	662.00	.00	1.84	.00	100.00	56.38	2300.00	76.00
2400.000	71.99	886.00	.00	1.61	.00	100.00	69.27	2300.00	76.00
* 2400.000	73.61	1537.00	.00	2.30	.00	100.00	76.19	2300.00	76.00
2900.000	69.08	662.00	.00	1.79	.00	100.00	60.27	2800.00	75.50
* 2900.000	72.05	886.00	.00	1.56	.00	100.00	74.47	2800.00	75.50
2900.000	73.80	1537.00	.02	2.01	.02	99.90	516.31	2800.00	75.50
3600.000	69.25	662.00	.00	1.75	.00	100.00	65.77	3500.00	75.00
3600.000	72.16	886.00	.02	1.09	.02	97.67	1209.42	3500.00	75.00
* 3600.000	73.96	1537.00	.03	1.30	.03	93.44	2082.60	3500.00	75.00
* 4720.000	69.62	662.00	.00	2.42	.00	100.00	49.26	4620.00	75.00
* 4720.000	72.41	886.00	.02	1.61	.02	99.23	648.70	4620.00	75.00
* 4720.000	74.15	1537.00	.04	1.80	.04	95.95	1355.73	4620.00	75.00
* 4770.000	69.37	662.00	.00	7.20	.00	100.00	17.76	4670.00	75.00
* 4770.000	72.43	886.00	.05	2.48	.05	98.06	719.47	4670.00	75.00
* 4770.000	74.16	1537.00	.06	2.29	.06	92.59	1516.39	4670.00	75.00
* 4810.000	70.74	662.00	.00	6.36	.00	100.00	10.00	4715.00	77.00
0.000	72.46	886.00	.06	2.83	.06	97.51	699.76	4715.00	77.00
* 4810.000	74.15	1537.00	.07	2.49	.07	91.94	1431.46	4715.00	77.00
* 4860.000	71.55	662.00	.01	1.54	.01	99.85	393.86	4765.00	75.00
* 4860.000	72.60	886.00	.02	1.47	.02	98.53	851.94	4765.00	75.00
* 4860.000	74.22	1537.00	.03	1.72	.03	94.89	1561.90	4765.00	75.00
5360.000	71.70	662.00	.00	1.95	.00	100.00	53.93	5265.00	75.00
* 5360.000	72.81	886.00	.02	1.91	.02	99.76	514.54	5265.00	75.00
5360.000	74.38	1537.00	.04	2.10	.04	96.66	1434.81	5265.00	75.00
5960.000	71.86	662.00	.00	1.96	.00	100.00	56.30	5865.00	75.00
* 5960.000	73.05	886.00	.00	2.17	.00	100.00	61.67	5865.00	75.00
* 5960.000	74.76	1537.00	.03	2.57	.03	99.40	1101.57	5865.00	75.00
6220.000	71.94	662.00	.00	2.00	.00	100.00	56.40	6125.00	75.00
* 6220.000	73.13	886.00	.00	2.20	.00	100.00	61.94	6125.00	75.00
6220.000	74.99	1537.00	.03	2.44	.03	98.78	1484.79	6125.00	75.00
6900.000	72.21	662.00	.01	1.45	.01	99.97	221.28	6805.00	75.00
* 6900.000	73.36	886.00	.02	1.36	.02	99.66	335.92	6805.00	75.00
* 6900.000	75.24	1537.00	.03	1.56	.02	98.47	1814.06	6805.00	75.00
7020.000	72.24	662.00	.00	1.75	.00	100.00	68.47	6925.00	75.00
* 7020.000	73.39	886.00	.02	1.62	.02	99.89	287.63	6925.00	75.00
7020.000	75.26	1537.00	.03	1.75	.03	98.64	1700.74	6925.00	75.00

	SECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
*	7070.000	72.23	662.00	.00	3.24	.00	100.00	56.82	6975.00	75.00
*	7070.000	73.37	886.00	.00	3.22	.00	100.00	67.06	6975.00	75.00
**	7070.000	75.26	1537.00	.05	2.69	.03	98.75	1701.39	6975.00	75.00
*	7120.000	73.36	662.00	.00	7.00	.00	100.00	10.00	7025.00	76.50
**	7120.000	73.23	886.00	.00	9.51	.00	100.00	10.00	7025.00	76.50
**	7120.000	72.91	1537.00	.00	17.10	.00	100.00	10.00	7025.00	76.50
*	7170.000	74.31	662.00	.00	1.69	.00	100.00	57.12	7075.00	77.50
**	7170.000	75.00	886.00	.00	2.05	.00	100.00	59.90	7075.00	77.50
**	7170.000	78.78	1537.00	.02	1.81	.03	95.56	1831.29	7075.00	77.50
**	7320.000	74.34	662.00	.00	1.70	.00	100.00	57.14	7225.00	77.50
**	7320.000	75.04	886.00	.00	2.06	.00	100.00	59.98	7225.00	77.50
**	7320.000	78.83	1537.00	.02	1.80	.03	95.36	1784.50	7225.00	77.50
**	8000.000	74.47	662.00	.00	1.72	.00	100.00	58.84	7905.00	76.10
**	8000.000	75.21	886.00	.00	2.07	.00	100.00	62.09	7905.00	76.10
**	8000.000	78.98	1537.00	.03	1.41	.04	88.19	1902.22	7905.00	76.10
**	8330.000	74.54	662.00	.00	1.64	.00	100.00	62.82	8235.00	75.20
**	8330.000	75.36	886.00	.01	1.87	.01	99.66	1678.62	8235.00	75.20
**	8330.000	79.03	1537.00	.02	1.21	.04	84.93	1920.64	8235.00	75.20
**	8680.000	74.60	662.00	.00	1.70	.00	100.00	61.70	8585.00	75.50
**	8680.000	75.60	886.00	.01	1.91	.01	99.85	1672.59	8585.00	75.50
**	8680.000	79.06	1537.00	.02	1.27	.04	85.77	1839.81	8585.00	75.50
**	9280.000	74.80	662.00	.01	1.49	.01	99.98	249.25	9185.00	75.00
**	9280.000	75.85	886.00	.02	1.39	.02	96.43	1723.12	9185.00	75.00
**	9280.000	79.12	1537.00	.02	1.12	.04	84.87	1852.23	9185.00	75.00
**	9780.000	75.05	662.00	.01	1.64	.01	99.80	1674.64	9685.00	75.00
**	9780.000	75.99	886.00	.02	1.53	.03	94.69	1713.02	9685.00	75.00
**	9780.000	79.15	1537.00	.03	1.22	.04	82.79	1843.47	9685.00	75.00
**	9930.000	75.13	440.00	.01	1.13	.01	99.63	1682.76	9835.00	75.00
**	9930.000	76.04	580.00	.02	1.03	.02	94.13	1755.84	9835.00	75.00
**	9930.000	79.17	992.00	.02	.80	.03	81.76	2010.33	9835.00	75.00
*	9980.000	75.16	440.00	.03	1.73	.02	98.21	1706.32	9885.00	75.00
*	9980.000	76.05	580.00	.03	1.33	.04	89.13	1775.06	9885.00	75.00
*	9980.000	79.18	992.00	.02	.87	.03	76.58	2014.91	9885.00	75.00
*	10040.000	75.20	440.00	.04	2.17	.04	96.37	1710.08	9945.00	75.00
**	10040.000	76.05	580.00	.04	1.52	.05	85.89	1774.77	9945.00	75.00
**	10040.000	79.18	992.00	.03	.90	.04	74.03	2015.89	9945.00	75.00
*	10120.000	75.28	440.00	.00	1.33	.00	100.00	53.42	10025.00	80.00
**	10120.000	76.10	580.00	.01	1.46	.01	99.99	197.96	10025.00	80.00
**	10120.000	79.18	992.00	.02	1.10	.02	97.53	832.96	10025.00	80.00

	SECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
*	10270.000	75.30	440.00	.00	1.29	.00	100.00	56.01	10175.00	80.00
*	10270.000	76.13	580.00	.00	1.49	.00	100.00	59.69	10175.00	80.00
*	10270.000	79.20	992.00	.02	1.11	.02	97.87	822.55	10175.00	80.00
	10410.000	75.32	440.00	.00	1.00	.00	100.00	75.12	10315.00	80.00
*	10410.000	76.17	580.00	.00	1.12	.00	100.00	196.53	10315.00	80.00
*	10410.000	79.22	992.00	.02	.92	.02	98.25	835.09	10315.00	80.00
	10510.000	75.33	440.00	.00	1.20	.00	100.00	61.21	10415.00	80.00
*	10510.000	76.18	580.00	.00	1.38	.00	100.00	65.45	10415.00	80.00
*	10510.000	79.22	992.00	.02	1.07	.02	98.98	509.20	10415.00	80.00
	10570.000	75.34	440.00	.00	1.17	.00	100.00	63.86	10475.00	80.00
*	10570.000	76.19	580.00	.00	1.33	.00	100.00	68.40	10475.00	80.00
*	10570.000	79.23	992.00	.02	1.07	.02	99.11	504.84	10475.00	80.00
	10680.000	75.34	440.00	.00	1.26	.00	100.00	58.99	10585.00	80.00
*	10680.000	76.20	580.00	.00	1.44	.00	100.00	63.13	10585.00	80.00
*	10680.000	79.23	992.00	.02	1.16	.02	99.18	496.44	10585.00	80.00
	11060.000	75.39	440.00	.00	1.34	.00	100.00	56.20	10965.00	80.00
*	11060.000	76.32	580.00	.01	1.47	.01	100.00	167.58	10965.00	80.00
*	11060.000	79.28	992.00	.02	1.14	.02	99.33	354.16	10965.00	80.00
	11940.000	75.52	440.00	.00	1.42	.00	100.00	56.13	11845.00	80.00
*	11940.000	76.71	580.00	.01	1.37	.01	99.92	350.95	11845.00	80.00
*	11940.000	79.37	992.00	.02	1.11	.02	95.08	1604.98	11845.00	80.00
	11990.000	75.46	440.00	.00	3.80	.00	100.00	40.60	11895.00	85.00
*	11990.000	76.73	580.00	.04	2.47	.04	99.50	454.03	11895.00	85.00
*	11990.000	79.37	992.00	.03	1.38	.03	90.10	1945.90	11895.00	85.00
	12050.000	76.03	440.00	.00	5.56	.00	100.00	8.00	11955.00	80.00
*	12050.000	76.93	580.00	.06	2.92	.06	98.29	590.19	11955.00	80.00
*	12050.000	79.37	992.00	.04	1.51	.04	87.61	2026.30	11955.00	80.00
	12100.000	76.65	440.00	.01	.76	.01	97.72	950.31	12005.00	80.00
*	12100.000	77.10	580.00	.02	.89	.02	96.67	1143.22	12005.00	80.00
*	12100.000	79.40	992.00	.02	.92	.02	90.43	2135.70	12005.00	80.00
*	12660.000	76.68	440.00	.02	.60	.01	88.21	2306.83	12565.00	80.00
*	12660.000	77.13	580.00	.02	.70	.02	85.93	2551.28	12565.00	80.00
*	12660.000	79.42	992.00	.02	.72	.02	76.54	3788.80	12565.00	80.00
	12860.000	76.70	440.00	.01	.56	.02	90.62	1606.65	13165.00	80.00
*	12860.000	77.16	580.00	.01	.66	.02	89.11	1727.36	13165.00	80.00
*	12860.000	79.44	992.00	.02	.74	.02	83.00	2329.32	13165.00	80.00
	13280.000	76.71	440.00	.01	.48	.01	92.12	1455.94	13585.00	80.00
*	13280.000	77.17	580.00	.02	.58	.01	91.05	1584.61	13585.00	80.00
*	13280.000	79.45	992.00	.02	.69	.02	86.14	2221.56	13585.00	80.00

ECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMDX
14280.000	76.73	440.00	.01	.50	.01	94.74	1082.14	14585.00	85.00
14280.000	77.20	580.00	.01	.60	.01	93.97	1184.54	14585.00	85.00
14280.000	79.47	992.00	.02	.72	.02	90.27	1684.42	14585.00	85.00
14530.000	76.74	440.00	.01	.56	.01	95.69	1007.95	14835.00	85.00
14530.000	77.20	580.00	.02	.67	.02	94.87	1121.06	14835.00	85.00
14530.000	79.48	992.00	.02	.77	.02	90.84	1673.09	14835.00	85.00
* 14580.000	76.74	353.00	.02	.75	.02	96.15	821.22	14885.00	85.00
* 14580.000	77.20	465.00	.02	.84	.02	95.04	961.15	14885.00	85.00
* 14580.000	79.48	796.00	.02	.82	.02	89.64	1643.53	14885.00	85.00
14650.000	76.74	353.00	.02	.78	.02	95.70	827.14	14955.00	85.00
14650.000	77.20	465.00	.02	.87	.02	94.58	965.56	14955.00	85.00
14650.000	79.48	796.00	.02	.82	.02	89.24	1647.41	14955.00	85.00
* 14710.000	76.75	353.00	.01	.36	.01	69.75	3150.00	15015.00	73.80
* 14710.000	77.22	465.00	.01	.42	.01	67.98	3150.00	15015.00	73.80
* 14710.000	79.49	796.00	.02	.46	.02	62.82	3150.00	15015.00	73.80
14960.000	76.75	353.00	.01	.36	.01	69.65	3150.00	15285.00	73.80
14960.000	77.22	465.00	.01	.42	.01	67.89	3150.00	15285.00	73.80
14960.000	79.49	796.00	.02	.46	.02	62.77	3150.00	15285.00	73.80
* 15080.000	76.75	353.00	.01	.53	.01	79.78	3150.00	15405.00	75.10
* 0.000	77.22	465.00	.02	.59	.02	76.20	3150.00	15405.00	75.10
15080.000	79.50	796.00	.02	.56	.02	66.79	3150.00	15405.00	75.10
* 16210.000	76.77	353.00	.01	.34	.01	68.27	3150.00	16535.00	73.60
* 16210.000	77.25	465.00	.01	.40	.01	66.70	3150.00	16535.00	73.60
* 16210.000	79.51	796.00	.02	.44	.02	62.13	3150.00	16535.00	73.60
* 16410.000	76.77	353.00	.00	.89	.00	100.00	62.27	16735.00	77.60
* 16410.000	77.25	465.00	.00	1.09	.00	100.00	64.43	16735.00	77.60
* 16410.000	79.52	796.00	.02	.87	.02	84.19	3166.00	16735.00	77.60
16710.000	76.79	353.00	.00	.88	.00	100.00	62.70	17035.00	77.50
16710.000	77.27	465.00	.00	1.08	.00	100.00	64.89	17035.00	77.50
16710.000	79.54	796.00	.02	.85	.02	83.29	3166.00	17035.00	77.50
17370.000	76.82	353.00	.00	.89	.00	100.00	62.44	17695.00	77.60
17370.000	77.32	465.00	.00	1.09	.00	100.00	64.70	17695.00	77.60
17370.000	79.58	796.00	.02	.86	.02	83.61	3166.00	17695.00	77.60
17530.000	76.83	353.00	.00	.84	.00	100.00	67.11	17755.00	77.40
17530.000	77.32	465.00	.00	1.02	.00	100.00	69.61	17755.00	77.40
17530.000	79.59	796.00	.02	.79	.02	82.75	3170.00	17755.00	77.40
17660.000	76.83	353.00	.00	.91	.00	100.00	60.83	17885.00	78.00
17660.000	77.33	465.00	.00	1.11	.00	100.00	63.04	17885.00	78.00
17660.000	79.59	796.00	.01	1.01	.02	92.47	1999.08	17885.00	78.00

JECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
17860.000	76.85	353.00	.00	.90	.00	100.00	61.68	18085.00	77.80
17860.000	77.35	465.00	.00	1.10	.00	100.00	63.95	18085.00	77.80
17860.000	79.62	796.00	.01	.96	.02	91.35	2009.22	18085.00	77.80
18060.000	76.86	353.00	.00	.96	.00	100.00	56.56	18285.00	80.20
18060.000	77.36	465.00	.00	1.18	.00	100.00	58.59	18285.00	80.20
18060.000	79.62	796.00	.00	1.48	.00	100.00	67.70	18285.00	80.20
18220.000	76.87	353.00	.00	.88	.00	100.00	63.45	18445.00	82.50
18220.000	77.38	465.00	.00	1.07	.00	100.00	65.86	18445.00	82.50
18220.000	79.64	796.00	.00	1.34	.00	100.00	76.53	18445.00	82.50
18720.000	76.89	353.00	.00	.87	.00	100.00	64.43	18945.00	85.00
18720.000	77.42	465.00	.00	1.06	.00	100.00	66.95	18945.00	85.00
18720.000	79.69	796.00	.00	1.32	.00	100.00	77.93	18945.00	85.00
19220.000	76.92	353.00	.00	.95	.00	100.00	58.10	19445.00	84.00
19220.000	77.45	465.00	.00	1.15	.00	100.00	60.34	19445.00	84.00
* 19220.000	79.76	796.00	.01	1.23	.01	99.61	641.47	19445.00	84.00
19370.000	76.93	279.00	.00	.78	.00	100.00	55.79	19595.00	82.00
19370.000	77.47	368.00	.00	.94	.00	100.00	57.92	19595.00	82.00
19370.000	79.79	630.00	.01	1.12	.01	99.97	412.66	19595.00	82.00
19570.000	76.94	279.00	.00	.74	.00	100.00	59.28	19795.00	78.50
0.000	77.48	368.00	.00	.90	.00	100.00	61.62	19795.00	78.50
* 19570.000	79.82	630.00	.02	.84	.01	92.79	2999.21	19795.00	78.50
19720.000	76.95	279.00	.00	.77	.00	100.00	56.82	20145.00	79.20
19720.000	77.50	368.00	.00	.93	.00	100.00	59.06	20145.00	79.20
19720.000	79.86	630.00	.01	1.00	.01	97.11	2911.88	20145.00	79.20
* 19780.000	76.95	279.00	.00	1.65	.00	100.00	47.43	20195.00	82.00
* 19780.000	77.52	368.00	.01	1.69	.01	99.96	240.77	20195.00	82.00
- 19780.000	79.86	630.00	.02	1.05	.02	94.78	1243.04	20195.00	82.00
* 19840.000	77.51	279.00	.03	2.39	.03	99.89	247.16	20255.00	82.00
* 19840.000	77.82	368.00	.04	2.22	.04	99.35	377.27	20255.00	82.00
- 19840.000	79.86	630.00	.03	1.21	.03	92.94	1240.41	20255.00	82.00
* 19890.000	77.63	279.00	.01	.55	.01	99.67	506.43	20305.00	82.00
* 19890.000	77.92	368.00	.01	.66	.01	99.37	628.17	20305.00	82.00
* 19890.000	79.88	630.00	.01	.70	.01	95.71	1447.81	20305.00	82.00
20210.000	77.65	279.00	.00	.66	.00	99.99	261.34	20625.00	81.00
- 20210.000	77.94	368.00	.01	.78	.01	99.88	467.94	20625.00	81.00
20210.000	79.89	630.00	.01	.77	.01	95.66	1826.67	20625.00	81.00
* 21060.000	77.69	279.00	.00	.70	.00	100.00	59.63	21475.00	80.20
* 21060.000	78.00	368.00	.00	.88	.00	100.00	60.96	21475.00	80.20
21060.000	79.94	630.00	.00	1.16	.00	100.00	68.90	21475.00	80.20

RECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
21180.000	77.68	279.00	.00	1.56	.00	100.00	41.26	21575.00	79.00
* 21180.000	77.99	368.00	.00	1.91	.00	100.00	43.34	21575.00	79.00
- 21180.000	79.95	630.00	.03	1.40	.03	84.61	3150.00	21575.00	79.00
* 21260.000	79.03	279.00	.01	2.23	.01	99.47	3156.00	21655.00	79.00
* 21260.000	79.33	368.00	.04	1.91	.04	88.51	3156.00	21655.00	79.00
21260.000	80.09	630.00	.05	1.57	.05	72.04	3156.00	21655.00	79.00
* 21300.000	79.13	279.00	.01	.39	.01	80.55	3146.00	21695.00	77.40
- 21300.000	79.40	368.00	.01	.47	.01	78.43	3146.00	21695.00	77.40
21300.000	80.12	630.00	.02	.65	.02	73.98	3146.00	21695.00	77.40
21450.000	79.14	279.00	.01	.33	.00	91.46	2661.67	21845.00	77.40
- 21450.000	79.40	368.00	.01	.41	.01	90.01	2814.07	21845.00	77.40
21450.000	80.13	630.00	.02	.58	.01	86.17	3160.00	21845.00	77.40
-- 22810.000	79.15	279.00	.01	.36	.01	96.77	1596.05	23205.00	80.00
22810.000	79.42	368.00	.01	.45	.01	95.96	1784.64	23205.00	80.00
22810.000	80.16	630.00	.01	.64	.01	93.33	2238.69	23205.00	80.00
-- 22960.000	79.15	279.00	.01	.34	.01	89.96	1956.94	23355.00	77.20
22960.000	79.43	368.00	.01	.42	.01	88.77	1997.32	23355.00	77.20
22960.000	80.17	630.00	.02	.60	.01	85.92	2174.18	23355.00	77.20
* 23320.000	79.16	279.00	.01	.25	.01	82.25	3150.00	23715.00	78.00
* 0.000	79.43	368.00	.01	.31	.01	80.88	3150.00	23715.00	78.00
* 23320.000	80.18	630.00	.01	.45	.01	77.64	3150.00	23715.00	78.00
23520.000	79.16	279.00	.01	.28	.01	91.14	2087.32	23915.00	80.00
23520.000	79.43	368.00	.01	.34	.01	90.34	2214.30	23915.00	80.00
23520.000	80.18	630.00	.01	.51	.01	87.95	2601.34	23915.00	80.00
23680.000	79.16	279.00	.01	.25	.01	86.09	2184.34	24075.00	78.00
23680.000	79.43	368.00	.01	.31	.01	85.18	2213.80	24075.00	78.00
23680.000	80.18	630.00	.01	.47	.01	82.91	2354.62	24075.00	78.00
* 24080.000	79.16	279.00	.01	.33	.01	83.64	2125.11	24475.00	76.50
* 24080.000	79.44	368.00	.01	.41	.01	82.56	2174.13	24475.00	76.50
* 24080.000	80.19	630.00	.02	.59	.01	79.93	2357.20	24475.00	76.50
24380.000	79.16	279.00	.01	.28	.01	78.55	2851.09	24775.00	75.80
24380.000	79.44	368.00	.01	.35	.01	77.49	2949.45	24775.00	75.80
24380.000	80.20	630.00	.02	.50	.01	74.79	3150.00	24775.00	75.80
24680.000	79.17	279.00	.01	.30	.01	78.53	2833.46	25075.00	76.00
24680.000	79.44	368.00	.01	.37	.01	77.38	2937.26	25075.00	76.00
24680.000	80.20	630.00	.02	.53	.01	74.46	3146.00	25075.00	76.00
24830.000	79.17	279.00	.01	.35	.01	90.13	2521.40	25225.00	80.00
24830.000	79.44	368.00	.01	.43	.01	88.88	2729.24	25225.00	80.00
24830.000	80.20	630.00	.01	.61	.01	85.11	3146.00	25225.00	80.00

JECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
24960.000	79.17	279.00	.01	.28	.01	76.77	2862.56	25355.00	75.60
24960.000	79.45	368.00	.01	.34	.01	75.77	2957.20	25355.00	75.60
24960.000	80.21	630.00	.02	.50	.01	73.19	3146.00	25355.00	75.60
25060.000	79.17	267.00	.01	.25	.01	67.47	2900.99	25455.00	80.00
25060.000	79.45	351.00	.01	.31	.01	66.90	2984.47	25455.00	80.00
25060.000	80.21	600.00	.02	.45	.01	65.33	3150.00	25455.00	80.00
25120.000	79.17	267.00	.01	.25	.01	67.50	2908.22	25515.00	80.00
25120.000	79.45	351.00	.01	.31	.01	66.98	2992.06	25515.00	80.00
25120.000	80.22	600.00	.02	.44	.01	65.51	3156.00	25515.00	80.00
25220.000	79.17	267.00	.01	.22	.01	61.14	3140.00	25615.00	75.00
25220.000	79.45	351.00	.01	.27	.01	60.59	3140.00	25615.00	75.00
25220.000	80.22	600.00	.02	.40	.02	59.34	3140.00	25615.00	75.00
25550.000	79.17	267.00	.01	.26	.01	72.92	2333.09	25845.00	75.00
25550.000	79.45	351.00	.01	.33	.01	72.31	2379.56	25845.00	75.00
25550.000	80.22	600.00	.02	.48	.01	70.76	2618.68	25845.00	75.00
26560.000	79.19	267.00	.00	.63	.00	100.00	79.89	26855.00	79.20
26560.000	79.50	351.00	.01	.73	.01	98.16	3160.00	26855.00	79.20
* 26560.000	80.28	600.00	.02	.91	.02	90.40	3160.00	26855.00	79.20
26670.000	79.19	267.00	.00	1.62	.00	100.00	35.03	26965.00	82.00
26670.000	79.50	351.00	.00	2.00	.00	100.00	36.70	26965.00	82.00
* 26670.000	80.25	600.00	.00	2.93	.00	100.00	40.68	26965.00	82.00
26725.000	80.93	267.00	.00	2.16	.00	100.00	10.00	27020.00	82.00
* 26725.000	82.06	351.00	.02	2.42	.02	98.96	3156.00	27020.00	82.00
26725.000	82.68	600.00	.06	2.01	.06	80.39	3156.00	27020.00	82.00
26780.000	81.02	267.00	.00	.58	.00	100.00	74.25	27075.00	82.00
* 26780.000	82.18	351.00	.00	.62	.00	99.43	3160.00	27075.00	82.00
26780.000	82.74	600.00	.01	.88	.01	95.30	3160.00	27075.00	82.00
27180.000	81.03	267.00	.00	.64	.00	100.00	68.97	27475.00	83.00
27180.000	82.19	351.00	.00	.70	.00	100.00	75.41	27475.00	83.00
27180.000	82.77	600.00	.00	1.10	.00	100.00	78.70	27475.00	83.00
27310.000	81.04	267.00	.00	.88	.00	100.00	48.09	27605.00	83.20
27310.000	82.19	351.00	.00	.97	.00	100.00	52.33	27605.00	83.20
27310.000	82.77	600.00	.00	1.53	.00	100.00	54.46	27605.00	83.20
27520.000	81.05	267.00	.00	.67	.00	100.00	67.86	27815.00	83.20
27520.000	82.21	351.00	.00	.73	.00	100.00	74.37	27815.00	83.20
27520.000	82.81	600.00	.00	1.14	.00	100.00	77.75	27815.00	83.20
27720.000	81.06	267.00	.00	.69	.00	100.00	66.86	28015.00	83.40
27720.000	82.21	351.00	.00	.75	.00	100.00	73.36	28015.00	83.40
27720.000	82.82	600.00	.00	1.16	.00	100.00	76.79	28015.00	83.40

	CNNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
*	28140.000	81.07	127.00	.00	.46	.00	100.00	46.79	28435.00	83.50
*	28140.000	82.23	157.00	.00	.47	.00	100.00	51.18	28435.00	83.50
*	28140.000	82.86	228.00	.00	.62	.00	100.00	53.57	28435.00	83.50
	28460.000	81.08	127.00	.00	.36	.00	100.00	66.08	28755.00	83.40
	28460.000	82.23	157.00	.00	.36	.00	100.00	73.03	28755.00	83.40
	28460.000	82.87	228.00	.00	.47	.00	100.00	76.85	28755.00	83.40
*	28960.000	81.08	127.00	.00	.51	.00	100.00	46.14	29255.00	83.50
*	28960.000	82.24	157.00	.00	.51	.00	100.00	50.86	29255.00	83.50
*	28960.000	82.87	228.00	.00	.67	.00	100.00	53.45	29255.00	83.50
	29500.000	81.10	127.00	.00	.61	.00	100.00	39.64	29795.00	84.00
	29500.000	82.25	157.00	.00	.62	.00	100.00	43.76	29795.00	84.00
	29500.000	82.89	228.00	.00	.80	.00	100.00	46.04	29795.00	84.00
	30250.000	81.12	75.00	.00	.39	.00	100.00	40.15	30545.00	83.60
	30250.000	82.27	89.00	.00	.37	.00	100.00	44.72	30545.00	83.60
	30250.000	82.92	115.00	.00	.43	.00	100.00	47.32	30545.00	83.60

* HEC-2 WATER SURFACE PROFILES *
* *
* Version 4.6.2; May 1991 *
* *
* RUN DATE 08AUG95 TIME 08:09:18 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

X X XXXXXXXX XXXXX XXXXX
X X X X X X X
X X X X X X X
XXXXXXX XXXXX X XXXXX XXXXX
X X X X X X X
X X X X X X X
X X XXXXXXXX XXXXX XXXXX

08AUG95 08:09:18

PAGE 1

***** THIS RUN EXECUTED 08AUG95 08:09:18

** EC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

--CITY OF DONNA
CHANNEL "B"
EXISTING CONDITIONS
FILENAME: CHB_100.IH2
MODEL STARTS UPSTREAM OF THE LEVEE PUMP STRUCTURE AND PROCEEDS UPSTREAM TO
TO THE CONFLUENCE OF CHANNEL "B" AND CHANNEL "C". THE MODEL THEN PROCEEDS
UP CHANNEL "B".

***** ASSUMED BW=15 & SS=2:1 D/S OF BRIDGE # 2, ASSUMED BW=10 & SS=2:1 U/S OF #2 *****

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
5-YEAR 24 HOUR FLOWS EXISTING MODEL CHANNEL "B"
T3 FILENAME: CHB_100.IH2 CSG 04/17/95

FLOWS FROM DONNA_S1.HC1

ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
-10	2			.0004				60	
NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
1			-1						

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	1	43	55	26	56	60	4	66	63
J5 LPRNT	NUMSEC	***** REQUESTED SECTION NUMBERS *****							
-10	-10								

J6 IHLEQ ICOPY SUBDIV STRTDS RMILE

1

5-YR 10-YR 100-YR

08AUG95 08:09:18

PAGE 2

CONFLUENCE W/CHANNEL "A"

5-YR 10-YR 100-YR

SPECIAL CULVERT BRIDGE NUM 1

CULVERT SIZE: 1-60" & 1-48" MODELED AS 2-54" CMP

SPECIAL CULVERT BRIDGE NUM 2

CULVERT SIZE: 1-60" CMP

5-YR 10-YR 100-YR

EM 493

SPECIAL CULVERT BRIDGE NUM 3

CULVERT SIZE: 1-60" CMP

CONFLUENCE OF CHANNEL "B" AND "C"

5-YR 10-YR 100-YR

SPECIAL CULVERT BRIDGE NUM 4

CULVERT SIZE: 1-48" CMP

SPECIAL CULVERT BRIDGE NUM 5

CULVERT SIZE: 1-2'x3' RCB

08AUG95 08:09:18

PAGE 3

LAST CROSS SECTION OF CHANNEL "B"

LEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
OFILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
DETAILS.

08AUG95 08:09:18

PAGE 5

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
10-YEAR 24 HOUR FLOWS EXISTING MODEL CHANNEL "B"
FILENAME: CHB_100.IH2

CSG 04/03/95

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	-10	3			.0004				62	
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	2				-1					

IHL_EQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF PROFILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR DETAILS.

08AUG95 08:09:18

PAGE 6

T RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
T 100-YEAR 24 HOUR FLOWS EXISTING MODEL CHANNEL "B"
T FILENAME: CHB_100.IH2 CSG 04/03/95

J	I	CHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	-10		4			.0004				66	
J	I	NPROM	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	15				-1						

IHLEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
FILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
DE ILS.

THIS RUN EXECUTED 08AUG95 08:09:21

C-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE-- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

FILENAME: CHB_100.IH2

MARY PRINTOUT

SECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
100.000	68.53	1142.00	.03	1.80	.03	96.32	1781.88	.00	70.00
100.000	69.16	1515.00	.04	2.00	.04	93.66	2366.14	.00	70.00
100.000	70.57	2599.00	.06	2.41	.06	86.09	3156.00	.00	70.00
1000.000	68.89	1142.00	.03	1.80	.03	96.09	1965.06	900.00	75.00
1000.000	69.52	1515.00	.04	1.99	.04	93.12	2639.39	900.00	75.00
1000.000	70.93	2599.00	.06	2.36	.05	84.44	3677.95	900.00	75.00
1500.000	69.03	741.00	.02	1.12	.02	95.46	2113.89	1400.00	75.00
1500.000	69.66	978.00	.02	1.24	.02	92.36	2794.23	1400.00	75.00
1500.000	71.08	1672.00	.04	1.47	.03	83.49	3763.33	1400.00	75.00
2000.000	69.12	741.00	.02	1.30	.02	97.84	1830.85	1900.00	75.00
2000.000	69.75	978.00	.02	1.41	.02	94.74	2779.43	1900.00	75.00
2000.000	71.16	1672.00	.04	1.60	.04	84.64	3810.11	1900.00	75.00
3000.000	69.39	741.00	.01	1.45	.01	99.81	852.03	2900.00	75.00
3000.000	70.01	978.00	.02	1.58	.02	98.29	1917.12	2900.00	75.00
3000.000	71.39	1672.00	.03	1.82	.04	90.98	2787.95	2900.00	75.00
4000.000	69.52	741.00	.02	.86	.02	93.56	1755.63	3900.00	75.00
* 4000.000	70.15	978.00	.02	.99	.02	91.68	2058.77	3900.00	75.00
* 4000.000	71.55	1672.00	.03	1.31	.03	87.05	2695.83	3900.00	75.00
5000.000	69.59	741.00	.02	.95	.02	96.99	1126.82	4900.00	75.00
5000.000	70.23	978.00	.02	1.09	.02	95.65	1365.57	4900.00	75.00
5000.000	71.65	1672.00	.03	1.43	.03	92.41	1900.13	4900.00	75.00
5650.000	69.64	741.00	.02	.94	.02	97.48	954.11	5550.00	75.00
5650.000	70.28	978.00	.02	1.09	.02	96.36	1148.86	5550.00	75.00
5650.000	71.73	1672.00	.03	1.44	.03	93.65	1585.03	5550.00	75.00

	SECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
*	5700.000	69.64	741.00	.03	1.52	.03	97.24	831.47	5600.00	74.00
*	5700.000	70.28	978.00	.04	1.63	.04	95.64	1066.39	5600.00	74.00
*	5700.000	71.73	1672.00	.05	1.91	.05	91.88	1592.78	5600.00	74.00
	5780.000	69.63	741.00	.03	1.83	.03	97.81	810.06	5680.00	74.00
	5780.000	70.27	978.00	.03	1.90	.03	96.72	1035.93	5680.00	74.00
	5780.000	71.71	1672.00	.04	2.17	.04	94.20	1547.67	5680.00	74.00
*	5830.000	69.69	741.00	.02	1.08	.02	98.51	942.54	5730.00	74.00
*	5830.000	70.32	978.00	.02	1.23	.02	97.27	1236.70	5730.00	74.00
*	5830.000	71.76	1672.00	.03	1.56	.03	93.80	1906.09	5730.00	74.00
	6000.000	69.71	741.00	.02	1.07	.02	98.34	1017.45	5900.00	75.00
	6000.000	70.34	978.00	.02	1.21	.02	96.99	1335.69	5900.00	75.00
	6000.000	71.79	1672.00	.03	1.54	.03	93.27	2055.24	5900.00	75.00
	7000.000	69.82	741.00	.02	.97	.02	95.11	1463.78	6900.00	75.00
	7000.000	70.46	978.00	.02	1.11	.02	93.28	1762.80	6900.00	75.00
	7000.000	71.93	1672.00	.03	1.42	.03	89.00	2443.50	6900.00	75.00
	8000.000	69.94	741.00	.00	1.85	.00	100.00	59.72	7900.00	75.00
*	8000.000	70.75	978.00	.02	1.85	.02	99.36	1001.44	7900.00	75.00
*	8000.000	72.17	1672.00	.04	2.09	.04	94.17	2536.05	7900.00	75.00
	8950.000	70.25	741.00	.02	1.54	.02	97.38	1460.95	8850.00	75.00
	0.000	71.12	978.00	.03	1.52	.03	93.04	2340.79	8850.00	75.00
	8950.000	72.49	1672.00	.04	1.75	.04	84.58	3410.38	8850.00	75.00
*	9000.000	70.28	741.00	.05	2.36	.05	94.10	1480.80	8900.00	75.00
*	9000.000	71.13	978.00	.05	2.04	.05	87.52	2350.53	8900.00	75.00
*	9000.000	72.51	1672.00	.06	2.09	.05	77.29	3418.42	8900.00	75.00
	9080.000	70.26	741.00	.04	2.61	.04	94.09	2039.29	8980.00	74.00
*	9080.000	71.12	978.00	.04	2.20	.04	87.90	3289.26	8980.00	74.00
*	9080.000	72.50	1672.00	.04	2.21	.04	77.86	4911.21	8980.00	74.00
	9130.000	70.37	741.00	.03	1.66	.03	95.52	1857.93	9030.00	74.00
	9130.000	71.18	978.00	.03	1.62	.03	89.99	2859.38	9030.00	74.00
	9130.000	72.54	1672.00	.04	1.80	.05	79.30	4551.14	9030.00	74.00
*	10000.000	70.64	741.00	.03	1.26	.03	90.93	2206.38	9900.00	75.00
	10000.000	71.39	978.00	.03	1.32	.03	86.36	2725.92	9900.00	75.00
	10000.000	72.74	1672.00	.04	1.59	.05	78.91	3453.50	9900.00	75.00
	11000.000	70.89	741.00	.03	1.46	.03	94.16	2077.54	10900.00	75.00
	11000.000	71.60	978.00	.03	1.50	.03	89.08	2499.32	10900.00	75.00
	11000.000	72.94	1672.00	.04	1.75	.05	81.13	3152.12	10900.00	75.00
*	12000.000	71.08	741.00	.02	1.07	.02	88.85	2308.85	11900.00	75.00
*	12000.000	71.78	978.00	.03	1.17	.03	84.92	2536.78	11900.00	75.00
*	12000.000	73.13	1672.00	.04	1.47	.04	78.95	2978.01	11900.00	75.00

SECNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
12250.000	71.11	741.00	.02	1.06	.02	88.67	2318.66	12150.00	75.00
12250.000	71.81	978.00	.03	1.16	.03	84.73	2549.33	12150.00	75.00
12250.000	73.16	1672.00	.04	1.45	.04	78.79	2991.30	12150.00	75.00
12300.000	71.12	706.00	.03	1.04	.03	84.46	2363.62	12200.00	75.00
12300.000	71.81	939.00	.03	1.13	.03	80.61	2583.33	12200.00	75.00
12300.000	73.17	1617.00	.04	1.41	.05	74.96	3010.97	12200.00	75.00
12400.000	71.11	706.00	.02	1.27	.02	89.81	2316.59	12300.00	75.00
12400.000	71.81	939.00	.02	1.37	.03	86.82	2544.13	12300.00	75.00
12400.000	73.16	1617.00	.03	1.70	.04	82.42	2986.37	12300.00	75.00
12450.000	71.14	366.00	.01	.39	.01	63.49	3317.30	12350.00	68.00
12450.000	71.84	480.00	.02	.42	.02	61.33	3357.25	12350.00	68.00
12450.000	73.20	807.00	.02	.53	.02	58.50	3435.35	12350.00	68.00
13000.000	71.17	366.00	.02	.77	.02	79.50	3818.10	12900.00	75.00
13000.000	71.86	480.00	.02	.72	.02	71.55	4222.42	12900.00	75.00
13000.000	73.22	807.00	.02	.75	.03	62.29	5013.37	12900.00	75.00
14000.000	71.49	366.00	.02	1.28	.02	90.15	3505.20	13900.00	75.00
14000.000	72.04	480.00	.03	1.14	.03	79.34	3919.53	13900.00	75.00
* 14000.000	73.31	807.00	.03	1.03	.03	65.33	4875.19	13900.00	75.00
14150.000	71.57	366.00	.02	1.20	.02	88.32	3560.64	14050.00	75.00
14150.000	72.09	480.00	.03	1.11	.03	78.74	3938.31	14050.00	75.00
14150.000	73.33	807.00	.03	1.02	.03	65.27	4864.12	14050.00	75.00
14200.000	71.53	366.00	.00	3.81	.00	100.00	30.76	14100.00	75.00
14200.000	72.01	480.00	.00	4.27	.00	100.00	37.26	14100.00	75.00
* 14200.000	73.32	807.00	.07	3.10	.07	85.44	3743.21	14100.00	75.00
14270.000	73.57	366.00	.03	1.73	.03	84.65	3846.99	14170.00	75.00
* 14270.000	73.77	480.00	.03	1.86	.03	80.84	4091.89	14170.00	75.00
* 14270.000	74.24	807.00	.04	2.16	.04	74.56	4664.12	14170.00	75.00
14320.000	73.62	366.00	.01	1.15	.01	99.20	3333.66	14220.00	75.00
14320.000	73.82	480.00	.02	1.34	.02	96.53	3633.73	14220.00	75.00
14320.000	74.29	807.00	.03	1.72	.03	88.80	4336.35	14220.00	75.00
15000.000	73.83	366.00	.02	1.00	.02	89.37	3645.20	14900.00	78.00
15000.000	74.07	480.00	.02	1.14	.02	85.18	3831.48	14900.00	78.00
15000.000	74.60	807.00	.04	1.43	.04	77.42	4254.14	14900.00	78.00
* 15150.000	73.86	366.00	.02	.69	.02	75.93	4105.87	15050.00	78.00
* 15150.000	74.10	480.00	.02	.81	.02	73.20	4268.81	15050.00	78.00
* 15150.000	74.65	807.00	.03	1.08	.03	68.05	4652.14	15050.00	78.00
15200.000	73.87	366.00	.02	.61	.02	60.10	4356.83	15100.00	80.00
15200.000	74.11	480.00	.03	.72	.03	58.44	4514.45	15100.00	80.00
15200.000	74.66	807.00	.03	.96	.04	55.44	4871.59	15100.00	80.00

	CNO	CWSEL	Q	VLOB	VCH	VROB	QCHP	TOPWID	CUMDS	TELMX
*	15270.000	73.87	366.00	.01	.88	.01	79.83	4360.91	15170.00	80.00
*	15270.000	74.11	480.00	.01	1.04	.01	78.93	4516.06	15170.00	80.00
*	15270.000	74.66	807.00	.02	1.42	.02	77.23	4866.54	15170.00	80.00
*	15320.000	73.88	366.00	.02	.58	.02	67.75	4356.31	15220.00	78.00
*	15320.000	74.12	480.00	.02	.68	.02	65.66	4517.06	15220.00	78.00
*	15320.000	74.68	807.00	.03	.93	.03	61.87	4875.83	15220.00	78.00
*	16000.000	73.96	366.00	.02	.91	.02	81.00	3613.07	15900.00	78.00
*	16000.000	74.22	480.00	.03	1.03	.03	77.18	3738.98	15900.00	78.00
*	16000.000	74.80	807.00	.04	1.29	.04	70.67	4025.15	15900.00	78.00
*	17000.000	74.31	366.00	.02	1.26	.02	89.91	3222.17	16900.00	80.00
*	17000.000	74.58	480.00	.03	1.36	.03	84.69	3264.39	16900.00	80.00
	7000.000	75.18	807.00	.05	1.60	.05	76.01	3361.72	16900.00	80.00
*	18000.000	74.62	366.00	.03	.91	.03	75.95	3291.59	17900.00	80.00
*	18000.000	74.90	480.00	.03	1.01	.03	72.56	3329.80	17900.00	80.00
*	18000.000	75.53	807.00	.04	1.26	.04	67.12	3417.42	17900.00	80.00

HEC-2 WATER SURFACE PROFILES *

* sion 4.6.2; May 1991 *

RUN DATE 08AUG95 TIME 08:09:37 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

X X XXXXXXXX XXXXX XXXXX
X X X X X X X X
X X X X X X X X
XXXXXXX XXXX X XXXXX XXXXX
X X X X X X X X
X X X X X X X X
X X XXXXXXXX XXXXX XXXXXXX

THIS RUN EXECUTED 08AUG95 08:09:37

BC-2 WATER SURFACE PROFILESVersion 4.6.2; May 1991

--CITY OF DONNA *
CHANNEL "C" *
EXISTING CONDITIONS *
FILENAME: CHC_100.IH2 *
THE MODEL STARTS AT THE CONFLUENCE OF CHANNEL "B" AND CHANNEL "C" AND *
PROCEEDS UP CHANNEL "C". *

***** ASSUMED BW=10 AND S:S=2:1

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
5 -YEAR 24 HOUR FLOWS EXISTING MODEL CHANNEL "C"
T3 FILENAME: CHC_100.IH2 CSG 04/17/95

T	CHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	-10	2			0				71.16	
N	NPREF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	1				-1					

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	1	43	23	24	56	60	4	66	63
----	---	----	----	----	----	----	---	----	----

J5 LPRNT NUMSEC ***** REQUESTED SECTION NUMBERS *****

-10	-10
-----	-----

J6 IHLEQ ICOPY SUBDIV STRTDS RMILE

1

CONFLUENCE OF CHANNEL "B" AND "C"
5-YR 10-YR 100-YR

5-YR 10-YR 100-YR

5-YR 10-YR 100-YR

11TH STREET

CULVERT SIZE: MULTIPLE BOXES WITH A 36" UNDERNEATH
MODEL WITH NORMAL BRIDGE ROUTINE

DOWNSTREAM NORMAL BRIDGE SECTION (2)

UPSTREAM NORMAL BRIDGE SECTION (3)

LAST CROSS SECTION OF CHANNEL "C"

CHANNEL C-2: NO PROFILES EXIST FOR THIS CHANNEL THEREFORE MODELED
WITH PICTURES AND FIELD NOTES.

5-YR 10-YR 100-YR

5-YR 10-YR 100-YR

SPECIAL CULVERT CHANNEL C-2

CULVERT SIZE: 1-24" RCP

ROSSING UNDER ELEVATED IRRIGATION DITCH

CONFLUENCE OF THE CHANNEL "C2a" AND "C-2b"

PROCEED UP CHANNEL "C2a" WHICH IS ON THE EAST CHANNEL IN THE "U".
ELEVATED IRRIGATION DITCH TO THE SOUTH

ROUTED FLOWS FROM SUB_C1

ELEVATED IRRIGATION DITCH TO THE SOUTH

LEVATED IRRIGATION DITCH TO THE SOUTH

--
SPECIAL CULVERT CHANNEL C-2a
CULVERT SIZE: 1-48" RCP CULVERT FLOWLINE 1' HIGHER THAN CHANNEL FLOWLINE

BOTTOM WIDTH = 6 FEET

--
SPECIAL CULVERT CHANNEL C-2a
BOTTOM WIDTH = 6 FEET
CULVERT SIZE: 1-48" RCP

BOTTOM WIDTH = 6 FEET

--
BOTTON WIDTH = 6 FEET

BOTTOM WIDTH = 6 FEET

--
DTTOM WIDITH = 4 FEET

CONFLUENCE OF THE CHANNEL "C2a" AND "C-2b"
PROCEED UP CHANNEL "C2b" WHICH IS ON THE WEST CHANNEL IN THE "U".

ELEVATED IRRIGATION DITCH TO THE SOUTH

--
LEVATED IRRIGATION DITCH TO THE WEST
M WIDTH = 6 FEET

--
LEVATED IRRIGATION DITCH TO THE WEST
OTTON WIDTH = 6 FEET

--
ELEVATED IRRIGATION DITCH TO THE WEST
OTTON WIDTH = 6 FEET

BOTTOM WIDTH = 6 FEET

--
SPECIAL CULVERT CHANNEL C-2b
LOTTON WIDTH = 6 FEET
CULVERT SIZE: 1-36" RCP

OTTON WIDTH = 6 FEET

BOTTOM WIDTH = 6 FEET

I EQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF PROFILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR DETAILS.

08AUG95 08:09:37

PAGE 5

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
10 -YEAR24 HOUR FLOWS EXISTING MODEL CHANNEL "C"
FILENAME: CHC_100.IH2 CSG 04/03/95

ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
-10	3			0				71.86	
NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
2		-1							

IHLREQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
P FILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
D VILS.

08AUG95 08:09:37

PAGE 6

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
100-YEAR 24 HOUR FLOWS EXISTING MODEL CHANNEL "C"
FILENAME: CHC_100.IH2

CSG 04/03/95

ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
-10	4			0				73.24	
NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
15			-1						

IHLEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
FILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
AILS.

THIS RUN EXECUTED 08AUG95 08:09:40

EC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE-. ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

FILENAME: CHC_100.IH2

MARY PRINTOUT

SECNO	CWSEL	Q	XLBEL	RBEL	VROB	QCHP	TOPWID	CUMDS	TELMX
1000.000	71.16	466.00	71.20	71.20	.00	100.00	63.84	.00	75.00
1000.000	71.86	618.00	71.20	71.20	.01	94.80	3683.32	.00	75.00
1000.000	73.24	1057.00	71.20	71.20	.02	81.40	4769.16	.00	75.00
2000.000	71.24	466.00	70.50	70.50	.01	94.22	3469.98	1000.00	75.00
* 2000.000	71.96	618.00	70.50	70.50	.02	87.17	3776.57	1000.00	75.00
2000.000	73.32	1057.00	70.50	70.50	.02	77.26	4349.13	1000.00	75.00
3000.000	71.30	411.00	70.50	70.50	.01	93.91	3540.73	2000.00	75.00
3000.000	72.01	546.00	70.50	70.50	.01	87.45	3868.18	2000.00	75.00
3000.000	73.37	938.00	70.50	70.50	.02	77.77	4500.09	2000.00	75.00
4000.000	71.34	411.00	70.20	70.20	.01	91.52	3521.62	3000.00	75.00
4000.000	72.05	546.00	70.20	70.20	.01	85.84	3744.06	3000.00	75.00
4000.000	73.41	938.00	70.20	70.20	.02	77.66	4166.00	3000.00	75.00
4250.000	71.35	411.00	70.70	70.70	.01	96.22	3243.95	3250.00	75.00
4250.000	72.05	546.00	70.70	70.70	.01	90.66	3324.45	3250.00	75.00
4250.000	73.42	938.00	70.70	70.70	.02	82.09	3479.61	3250.00	75.00
4300.000	71.35	411.00	70.80	70.80	.01	96.00	3230.81	3300.00	75.00
4300.000	72.05	546.00	70.80	70.80	.02	89.18	3314.26	3300.00	75.00
4300.000	73.42	938.00	70.80	70.80	.02	79.42	3475.09	3300.00	75.00
4370.000	71.35	411.00	70.80	70.80	.01	96.05	3227.76	3370.00	75.00
4370.000	72.06	546.00	70.80	70.80	.02	89.33	3311.81	3370.00	75.00
4370.000	73.42	938.00	70.80	70.80	.02	79.63	3473.92	3370.00	75.00
4420.000	71.36	411.00	70.80	70.80	.01	95.77	3226.40	3420.00	75.00
4420.000	72.06	546.00	70.80	70.80	.02	88.81	3310.31	3420.00	75.00
4420.000	73.42	938.00	70.80	70.80	.02	78.96	3472.34	3420.00	75.00

ECNO	CWSEL	Q	XLBEL	RBEL	VROB	QCHP	TOPWID	CUMDS	TELMX
5000.000	71.40	411.00	70.60	70.60	.01	93.69	3344.98	4000.00	75.00
5000.000	72.10	546.00	70.60	70.60	.01	87.35	3501.53	4000.00	75.00
5000.000	73.46	938.00	70.60	70.60	.02	78.22	3806.86	4000.00	75.00
* 6000.000	71.43	411.00	68.80	68.80	.01	70.31	3526.13	5000.00	75.00
* 6000.000	72.13	546.00	68.80	68.80	.02	67.08	3626.01	5000.00	75.00
6000.000	73.49	938.00	68.80	68.80	.02	62.79	3822.58	5000.00	75.00
6250.000	71.44	411.00	68.80	68.80	.02	66.36	3527.51	5250.00	75.00
6250.000	72.14	546.00	68.80	68.80	.02	62.18	3627.25	5250.00	75.00
6250.000	73.50	938.00	68.80	68.80	.03	56.59	3822.67	5250.00	75.00
* 6260.000	71.43	337.00	68.80	68.13	.04	63.46	1383.22	5260.00	75.00
* 6260.000	72.13	449.00	68.80	68.13	.05	56.23	1484.21	5260.00	75.00
* 6260.000	73.49	775.00	68.80	68.13	.07	45.88	1681.10	5260.00	75.00
6300.000	71.45	337.00	68.80	68.80	.05	53.05	1398.37	5300.00	75.00
6300.000	72.14	449.00	68.80	68.80	.06	45.94	1499.52	5300.00	75.00
6300.000	73.51	775.00	68.80	68.80	.08	36.46	1699.07	5300.00	75.00
6370.000	71.44	337.00	68.80	68.80	.06	40.08	1400.25	5370.00	75.00
6370.000	72.14	449.00	68.80	68.80	.06	39.42	1499.51	5370.00	75.00
6370.000	73.49	775.00	68.80	68.80	.07	38.18	1696.22	5370.00	75.00
* 6380.000	71.49	337.00	68.80	68.80	.02	78.80	1389.81	5380.00	75.00
* 0.000	72.17	449.00	68.80	68.80	.03	73.50	1489.38	5380.00	75.00
* 6380.000	73.52	775.00	68.80	68.80	.04	64.79	1685.67	5380.00	75.00
* 6420.000	71.54	337.00	68.80	68.80	.01	67.34	3408.96	5420.00	75.00
* 6420.000	72.24	449.00	68.80	68.80	.01	64.52	3476.63	5420.00	75.00
* 6420.000	73.63	775.00	68.80	68.80	.02	60.81	3611.28	5420.00	75.00
7000.000	71.55	337.00	68.90	68.90	.01	68.48	3402.63	6000.00	75.00
7000.000	72.25	449.00	68.90	68.90	.01	65.51	3470.42	6000.00	75.00
7000.000	73.64	775.00	68.90	68.90	.02	61.64	3604.37	6000.00	75.00
8000.000	71.57	337.00	69.50	69.50	.01	72.19	3329.89	7000.00	75.00
8000.000	72.27	449.00	69.50	69.50	.02	68.18	3392.10	7000.00	75.00
8000.000	73.66	775.00	69.50	69.50	.02	63.25	3516.37	7000.00	75.00
9000.000	71.60	337.00	69.20	69.20	.01	67.75	3193.19	8000.00	75.00
9000.000	72.29	449.00	69.20	69.20	.02	64.73	3208.04	8000.00	75.00
9000.000	73.69	775.00	69.20	69.20	.02	61.02	3237.85	8000.00	75.00
* 10000.000	71.63	268.00	70.00	70.00	.02	69.68	3453.39	9000.00	75.00
* 10000.000	72.32	357.00	70.00	70.00	.02	64.69	3587.97	9000.00	75.00
10000.000	73.71	621.00	70.00	70.00	.02	59.00	3859.88	9000.00	75.00
* 11000.000	71.84	268.00	73.00	73.00	.00	100.00	35.36	10000.00	80.00
* 11000.000	72.54	357.00	73.00	73.00	.00	100.00	38.15	10000.00	80.00
* 11000.000	74.00	621.00	73.00	73.00	.04	80.50	3549.44	10000.00	80.00

SECNO	CWSEL	Q	XLBEL	RBEL	VROB	QCHP	TOPWID	CUMDS	TELMX
12000.000	72.44	268.00	77.00	77.00	.00	100.00	31.75	11000.00	80.00
12000.000	73.19	357.00	77.00	77.00	.00	100.00	34.72	11000.00	80.00
12000.000	74.70	621.00	77.00	77.00	.00	100.00	40.78	11000.00	80.00
* 13000.000	73.44	212.00	80.00	80.00	.00	100.00	27.71	12000.00	80.00
* 13000.000	74.17	281.00	80.00	80.00	.00	100.00	30.64	12000.00	80.00
13000.000	75.76	484.00	80.00	80.00	.00	100.00	37.03	12000.00	80.00
* 14000.000	75.19	212.00	82.00	82.00	.00	100.00	24.78	13000.00	82.00
* 14000.000	75.82	281.00	82.00	82.00	.00	100.00	27.28	13000.00	82.00
14000.000	77.28	484.00	82.00	82.00	.00	100.00	33.09	13000.00	82.00
15000.000	77.39	212.00	83.50	83.50	.00	100.00	25.58	14000.00	83.50
15000.000	77.97	281.00	83.50	83.50	.00	100.00	27.91	14000.00	83.50
15000.000	79.33	484.00	83.50	83.50	.00	100.00	33.30	14000.00	83.50
16000.000	79.15	212.00	85.00	85.00	.00	100.00	26.58	15000.00	85.00
16000.000	79.75	281.00	85.00	85.00	.00	100.00	29.00	15000.00	85.00
16000.000	81.15	484.00	85.00	85.00	.00	100.00	34.61	15000.00	85.00
16500.000	79.86	212.00	85.50	85.50	.00	100.00	27.43	15500.00	85.50
16500.000	80.48	281.00	85.50	85.50	.00	100.00	29.92	15500.00	85.50
16500.000	81.91	484.00	85.50	85.50	.00	100.00	35.64	15500.00	85.50
* 16950.000	80.66	212.00	86.00	86.00	.00	100.00	24.63	15950.00	86.00
16950.000	81.26	281.00	86.00	86.00	.00	100.00	27.05	15950.00	86.00
* 16950.000	82.66	484.00	86.00	86.00	.00	100.00	32.65	15950.00	86.00
* 17000.000	80.63	212.00	86.20	86.20	.00	100.00	10.00	16000.00	86.20
* 17000.000	81.13	281.00	86.20	86.20	.00	100.00	10.00	16000.00	86.20
* 17000.000	82.14	484.00	86.20	86.20	.00	100.00	10.00	16000.00	86.20
* 17200.000	100.54	212.00	100.00	100.00	.01	93.37	3146.00	16200.00	86.70
* 17200.000	100.67	281.00	100.00	100.00	.01	91.55	3146.00	16200.00	86.70
* 17200.000	101.00	484.00	100.00	100.00	.02	87.64	3146.00	16200.00	86.70
* 17250.000	100.55	152.00	100.00	86.90	.00	71.48	1673.00	16250.00	86.90
* 17250.000	100.68	200.00	100.00	86.90	.00	71.44	1673.00	16250.00	86.90
* 17250.000	101.02	340.00	100.00	86.90	.00	71.35	1673.00	16250.00	86.90
18000.000	100.55	152.00	100.00	87.00	.00	70.35	1671.00	17000.00	87.00
18000.000	100.68	200.00	100.00	87.00	.00	70.32	1671.00	17000.00	87.00
18000.000	101.02	340.00	100.00	87.00	.00	70.24	1671.00	17000.00	87.00
18450.000	100.55	152.00	100.00	87.50	.00	69.92	1670.00	17450.00	87.50
18450.000	100.68	200.00	100.00	87.50	.00	69.89	1670.00	17450.00	87.50
18450.000	101.02	340.00	100.00	87.50	.01	69.81	1670.00	17450.00	87.50
18500.000	100.55	75.00	87.50	87.50	.00	52.14	3140.00	17500.00	87.50
18500.000	100.68	90.00	87.50	87.50	.00	52.12	3140.00	17500.00	87.50
18500.000	101.02	126.00	87.50	87.50	.00	52.08	3140.00	17500.00	87.50

ECNO	CWSEL	Q	XLBEL	RBEL	VROB	QCHP	TOPWID	CUMDS	TELMX
* 18550.000	100.55	75.00	87.50	87.50	.00	76.45	3140.00	17550.00	87.50
* 18550.000	100.69	90.00	87.50	87.50	.00	76.44	3140.00	17550.00	87.50
* 18550.000	101.02	126.00	87.50	87.50	.00	76.42	3140.00	17550.00	87.50
* 18650.000	100.55	75.00	87.50	87.50	.00	50.41	3134.00	17650.00	87.50
* 18650.000	100.69	90.00	87.50	87.50	.00	50.40	3134.00	17650.00	87.50
* 18650.000	101.02	126.00	87.50	87.50	.00	50.37	3134.00	17650.00	87.50
* 18700.000	100.55	75.00	87.50	87.50	.00	75.18	3134.00	17700.00	87.50
* 18700.000	100.69	90.00	87.50	87.50	.00	75.18	3134.00	17700.00	87.50
* 18700.000	101.03	126.00	87.50	87.50	.00	75.16	3134.00	17700.00	87.50
* 18750.000	100.55	75.00	87.50	87.50	.00	53.03	3134.00	17950.00	87.50
* 18750.000	100.69	90.00	87.50	87.50	.00	53.00	3134.00	17950.00	87.50
* 18750.000	101.03	126.00	87.50	87.50	.00	52.93	3134.00	17950.00	87.50
- 19000.000	100.55	29.00	88.00	88.00	.00	51.82	3130.00	18200.00	88.00
- 19000.000	100.69	32.00	88.00	88.00	.00	51.79	3130.00	18200.00	88.00
- 19000.000	101.03	38.00	88.00	88.00	.00	51.73	3130.00	18200.00	88.00
- 20000.000	100.55	29.00	88.00	88.00	.00	50.47	3126.00	19200.00	88.00
- 20000.000	100.69	32.00	88.00	88.00	.00	50.45	3126.00	19200.00	88.00
- 20000.000	101.03	38.00	88.00	88.00	.00	50.40	3126.00	19200.00	88.00
- 21000.000	100.55	29.00	90.00	90.00	.00	47.44	3116.00	21200.00	90.00
0.000	100.69	32.00	90.00	90.00	.00	47.43	3116.00	21200.00	90.00
0.000	101.03	38.00	90.00	90.00	.00	47.41	3116.00	21200.00	90.00
- 17250.000	100.55	152.00	86.90	86.90	.00	56.86	3146.00	21250.00	86.90
- 17250.000	100.68	200.00	86.90	86.90	.00	56.82	3146.00	21250.00	86.90
- 17250.000	101.02	340.00	86.90	86.90	.00	56.71	3146.00	21250.00	86.90
- 173000.000	100.55	152.00	100.00	87.00	.00	71.51	1673.00	21300.00	87.00
- 173000.000	100.68	200.00	100.00	87.00	.00	71.47	1673.00	21300.00	87.00
- 173000.000	101.02	340.00	100.00	87.00	.00	71.39	1673.00	21300.00	87.00
- 180000.000	100.55	152.00	100.00	87.00	.00	69.26	1669.00	22000.00	87.00
- 180000.000	100.68	200.00	100.00	87.00	.00	69.24	1669.00	22000.00	87.00
- 180000.000	101.02	340.00	100.00	87.00	.00	69.17	1669.00	22000.00	87.00
- 190000.000	100.55	31.00	100.00	88.50	.00	68.52	1667.00	23000.00	88.50
- 190000.000	100.68	33.00	100.00	88.50	.00	68.49	1667.00	23000.00	88.50
- 190000.000	101.02	37.00	100.00	88.50	.00	68.42	1667.00	23000.00	88.50
- 195000.000	100.55	31.00	100.00	88.50	.00	67.27	1665.00	23500.00	88.50
- 195000.000	100.68	33.00	100.00	88.50	.00	67.25	1665.00	23500.00	88.50
- 195000.000	101.02	37.00	100.00	88.50	.00	67.19	1665.00	23500.00	88.50
- 195050.000	100.55	31.00	88.50	88.50	.00	49.25	3130.00	23550.00	88.50
- 195050.000	100.68	33.00	88.50	88.50	.00	49.24	3130.00	23550.00	88.50
- 195050.000	101.02	37.00	88.50	88.50	.00	49.21	3130.00	23550.00	88.50

	ICNO	CWSEL	Q	XLBEL	RBEL	VROB	QCHP	TOPWID	CUMDS	TELMX
* 195150.000	100.55	31.00	88.50	88.50	.00	74.71	3130.00	23650.00	88.50	
* 195150.000	100.69	33.00	88.50	88.50	.00	74.70	3130.00	23650.00	88.50	
* 95150.000	101.02	37.00	88.50	88.50	.00	74.69	3130.00	23650.00	88.50	
* 195200.000	100.55	31.00	88.50	88.50	.00	51.92	3130.00	23700.00	88.50	
* 195200.000	100.69	33.00	88.50	88.50	.00	51.89	3130.00	23700.00	88.50	
* 95200.000	101.02	37.00	88.50	88.50	.00	51.82	3130.00	23700.00	88.50	
196700.000	100.55	31.00	90.00	90.00	.00	52.28	3130.00	23750.00	90.00	
* 96700.000	100.69	33.00	90.00	90.00	.00	52.24	3130.00	23750.00	90.00	
96700.000	101.02	37.00	90.00	90.00	.00	52.16	3130.00	23750.00	90.00	

HEC-2 WATER SURFACE PROFILES

* SION 4.6.2; May 1991

RUN DATE 08AUG95 TIME 08:09:52 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

X X XXXXXXXX XXXXX
X X X X X X XXXXX
X X X X X X
XXXXXXX XXXX X XXXXX XXXXX
X X X X X X
X X X X X X X
X X XXXXXXXX XXXXX XXXXXXXX

08AUG95 08:09:52

PAGE 1

THIS RUN EXECUTED 08AUG95 08:09:52

EC-2 WATER SURFACE PROFILES

Version 4.6.2, May 1991

CITY OF DONNA *
CHANNEL I *
EXISTING CONDITIONS *
FILENAME: CHI_100.IH2 *
MODEL STARTS APPROXIMATELY 15000 FEET DOWNSTREAM OF HIGHWAY 83 AND PROCEEDING*
JPSTREAM TO JUST DOWNSTREAM OF EXPRESSWAY (HWY 83) *

T1 RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
T2 5-YEAR FREQUENCY
FILENAME: CHI_100.IH2 CWW 07/26/95

J1 ICHECK INQ NINV IDIR STRT METRIC HVINS Q WSEL FQ
-10 2 0.0005 60
J2 NPROF IPLOT PRFVS XSECV XSECH FN ALLDC IBW CHNIM ITRACE
1 -1

VARIABLE CODES FOR SUMMARY PRINTOUT

38 1 43 23 24 26 42 14 60 63

LPRNT NUMSEC *****REQUESTED SECTION NUMBERS*****

-10 -10

IHLREQ ICOPY SUBDIV STRTDS RMILE

1

SPECIAL CULVERT
CULVERT SIZE: 48" Culvert (ASSUMED)

08AUG95 08:09:52

PAGE 2

SPECIAL CULVERT

CULVERT SIZE: 48" Culvert (ASSUMED)

--SPECIAL CULVERT

CULVERT SIZE: 48" Culvert (ASSUMED)

08AUG95 08:09:52

PAGE 3

SEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
DFILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
DETAILS.

08AUG95 08:09:52

PAGE 4

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
10-YEAR FREQUENCY

FILENAME: CHI_100.IH2 CWW 07/26/95

ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
-10	3			.0005				60	
NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
.2				-1					

IHLEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
>FILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
TAILS.

08AUG95 08:09:52

PAGE 5

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
100-YEAR FREQUENCY

FILENAME: CHI_100.IH2

CWW 07/26/95

ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
-10	4			.0005				60	
NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
15				-1					

LEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF PROFILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR DETAILS.

THIS RUN EXECUTED 08AUG95 08:09:54

MC-2 WATER SURFACE PROFILESVersion 4.6.2; May 1991

NOTE - ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

FILENAME: CHI_100.IH2

MARY PRINTOUT

SECNO	CWSEL	Q	XLBEL	RBEL	VCH	ELMIN	QCH	QCHP	TELMX
1000.000	79.50	240.00	80.00	80.00	1.90	74.00	240.00	100.00	80.00
1000.000	80.61	310.00	80.00	80.00	1.15	74.00	261.59	84.38	80.00
1000.000	81.08	520.00	80.00	80.00	1.36	74.00	394.81	75.92	80.00
2000.000	80.00	240.00	80.50	80.50	1.90	74.50	240.00	100.00	80.50
2000.000	81.11	310.00	80.50	80.50	1.15	74.50	261.47	84.35	80.50
2000.000	81.58	520.00	80.50	80.50	1.36	74.50	394.73	75.91	80.50
3000.000	80.50	240.00	81.00	81.00	1.90	75.00	240.00	100.00	81.00
3000.000	81.61	310.00	81.00	81.00	1.15	75.00	261.49	84.35	81.00
3000.000	82.08	520.00	81.00	81.00	1.36	75.00	394.72	75.91	81.00
4000.000	81.00	240.00	81.50	81.50	1.90	75.50	240.00	100.00	81.50
4000.000	82.11	310.00	81.50	81.50	1.15	75.50	261.57	84.38	81.50
4000.000	82.58	520.00	81.50	81.50	1.36	75.50	394.76	75.92	81.50
5000.000	81.50	240.00	82.00	82.00	1.90	76.00	240.00	100.00	82.00
5000.000	82.61	310.00	82.00	82.00	1.15	76.00	261.46	84.34	82.00
5000.000	83.08	520.00	82.00	82.00	1.36	76.00	394.73	75.91	82.00
6000.000	81.97	220.00	82.50	82.50	1.75	76.50	220.00	100.00	82.50
6000.000	83.08	280.00	82.50	82.50	1.06	76.50	237.71	84.90	82.50
6000.000	83.53	450.00	82.50	82.50	1.21	76.50	344.51	76.56	82.50
* 6500.000	82.01	220.00	82.50	82.50	1.73	76.50	220.00	100.00	82.50
* 6500.000	83.12	280.00	82.50	82.50	1.16	76.50	263.81	94.22	82.50
* 6500.000	83.58	450.00	82.50	82.50	1.41	76.50	407.97	90.66	82.50
6530.000	82.87	220.00	82.50	82.50	1.09	76.50	212.65	96.66	82.50
6530.000	83.13	280.00	82.50	82.50	1.14	76.50	263.33	94.05	82.50
6530.000	83.58	450.00	82.50	82.50	1.40	76.50	407.70	90.60	82.50

SCNO	CWSEL	Q	XLBEL	RBEL	VCH	ELMIN	QCH	QCHP	TELMX
* 7000.000	82.94	220.00	83.00	83.00	1.55	77.00	220.00	100.00	83.00
* 7000.000	83.34	280.00	83.00	83.00	1.35	77.00	256.10	91.46	83.00
* 7000.000	83.77	450.00	83.00	83.00	1.47	77.00	364.89	81.09	83.00
8000.000	83.27	220.00	83.50	83.50	1.62	77.50	220.00	100.00	83.50
8000.000	84.01	280.00	83.50	83.50	1.14	77.50	242.89	86.75	83.50
8000.000	84.40	450.00	83.50	83.50	1.33	77.50	354.32	78.74	83.50
* 9000.000	83.33	220.00	83.50	83.50	1.59	77.50	220.00	100.00	83.50
* 9000.000	84.10	280.00	83.50	83.50	1.17	77.50	264.17	94.35	83.50
* 9000.000	84.51	450.00	83.50	83.50	1.46	77.50	410.06	91.12	83.50
9030.000	83.86	220.00	83.50	83.50	1.09	77.50	212.75	96.70	83.50
9030.000	84.11	280.00	83.50	83.50	1.15	77.50	263.71	94.18	83.50
9030.000	84.52	450.00	83.50	83.50	1.45	77.50	409.65	91.03	83.50
* 10000.000	84.11	220.00	84.00	84.00	1.36	78.00	216.01	98.19	84.00
* .0000.000	84.44	280.00	84.00	84.00	1.21	78.00	247.36	88.34	84.00
* .0000.000	84.85	450.00	84.00	84.00	1.38	78.00	357.79	79.51	84.00
* 11000.000	84.84	220.00	84.50	84.50	1.05	78.50	200.85	91.30	84.50
.1000.000	85.02	280.00	84.50	84.50	1.14	78.50	242.85	86.73	84.50
11000.000	85.41	450.00	84.50	84.50	1.32	78.50	353.27	78.50	84.50
12000.000	85.36	220.00	85.00	85.00	1.05	79.00	200.38	91.08	85.00
1.000	85.53	280.00	85.00	85.00	1.11	79.00	241.31	86.18	85.00
12000.000	85.93	450.00	85.00	85.00	1.30	79.00	351.73	78.16	85.00
13000.000	85.86	220.00	85.50	85.50	1.03	79.50	199.48	90.67	85.50
13000.000	86.03	280.00	85.50	85.50	1.11	79.50	241.19	86.14	85.50
13000.000	86.43	450.00	85.50	85.50	1.30	79.50	351.24	78.05	85.50
* 13400.000	85.90	220.00	85.50	85.50	1.07	79.50	212.13	96.42	85.50
* 13400.000	86.07	280.00	85.50	85.50	1.20	79.50	265.15	94.70	85.50
* 13400.000	86.47	450.00	85.50	85.50	1.49	79.50	411.14	91.36	85.50
13440.000	86.08	220.00	85.50	85.50	.93	79.50	207.90	94.50	85.50
13440.000	86.08	280.00	85.50	85.50	1.19	79.50	264.77	94.56	85.50
13440.000	86.49	450.00	85.50	85.50	1.47	79.50	410.57	91.24	85.50
* 14000.000	86.25	200.00	86.00	86.00	1.06	80.00	188.18	94.09	86.00
* 14000.000	86.29	230.00	86.00	86.00	1.17	80.00	213.79	92.95	86.00
* 14000.000	86.67	350.00	86.00	86.00	1.24	80.00	290.54	83.01	86.00
15000.000	86.79	200.00	86.50	86.50	1.01	80.50	185.40	92.70	86.50
15000.000	86.88	230.00	86.50	86.50	1.06	80.50	207.40	90.17	86.50
.5000.000	87.20	350.00	86.50	86.50	1.21	80.50	288.34	82.38	86.50

HEC-2 WATER SURFACE PROFILES *

*
sion 4.6.2; May 1991 *

*
RUN DATE 08AUG95 TIME 08:10:08 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

X	X	XXXXXX	XXXX	XXXX
X	X	X	X X	X X
X	X	X	X	X
XXXXXX	XXXX	X	XXXX	XXXX
X	X	X	X	X
X	X	X	X X	X
X	X	XXXXXX	XXXX	XXXXXX

08AUG95 08:10:08

PAGE 1

***** THIS RUN EXECUTED 08AUG95 08:10:08

***IEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

***CITY OF DONNA

UPPER EAST MAIN DRAIN CHANNEL

EXISTING CONDITIONS

FILENAME: UEMD_100.IH2

MODEL STARTS APPROXIMATELY 9300 FEET DOWNSTREAM OF HIGHWAY 83 AND PROCEEDING UPSTREAM TO JUST DOWN STREAM OF EXPRESSWAY (HWY 83)

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY

T2 5-YEAR 24 HOUR FLOWS EXISTING MODEL
FILENAME: UEMD_100.IH2 CWW 07/28/95

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	-10	2			0.0005				60	
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	1		-1							

*** VARIABLE CODES FOR SUMMARY PRINTOUT

38	1	43	23	24	26	42	14	60	63
----	---	----	----	----	----	----	----	----	----

LPRNT NUMSEC ***** REQUESTED SECTION NUMBERS *****

-10 -10

IHLREQ ICOPY SUBDIV STRTDS RMILE

1

*** SPECIAL CULVERT

CULVERT SIZE: 48"RCP

*

*

08AUG95

08:10:08

PAGE 2

SPECIAL CULVERT

CULVERT SIZE: 1-48" RCP

08AUG95 08:10:08

PAGE 3

: EQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
1 >FILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
DETAILS.

08AUG95 08:10:08

PAGE 4

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
10-YEAR 24 HOUR FLOWS EXISTING MODEL
FILENAME: UEMD_100.IH2

CWW 07/28/95

J	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	-10	3			0.0005				60	
J	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	.2				-1					

IHLEQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF
FILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR
.ILS.

08AUG95 08:10:08

PAGE 5

RUST JOB NO: 67787 CITY OF DONNA DRAINAGE STUDY
100-YEAR24 HOUR FLOWS EXISTING MODEL
FILENAME: UEMD_100.IH2 CWW 07/28/95

ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
-10	4			0.0005				60	
NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
15				-1					

EQ = 1. THEREFORE FRICTION LOSS (HL) IS CALCULATED AS A FUNCTION OF PROFILE TYPE, WHICH CAN VARY FROM REACH TO REACH. SEE DOCUMENTATION FOR DETAILS.

THIS RUN EXECUTED 08AUG95 08:10:09

EC-2 WATER SURFACE PROFILESVersion 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

FILENAME: UEMD_100.IH2

MARY PRINTOUT

SECNO	CWSEL	Q	XLBEL	RBEL	VCH	ELMIN	QCH	QCHP	TELMX	
1000.000	81.95	460.00	81.30	81.30	1.35	72.84	406.78	88.43	81.30	
1000.000	82.27	620.00	81.30	81.30	1.48	72.84	515.55	83.15	81.30	
1000.000	83.04	1100.00	81.30	81.30	1.79	72.84	819.27	74.48	81.30	
*	1050.000	81.95	460.00	81.35	81.35	1.49	72.85	442.98	96.30	81.35
*	1050.000	82.26	620.00	81.35	81.35	1.71	72.85	583.94	94.18	81.35
*	1050.000	83.04	1100.00	81.35	81.35	2.20	72.85	993.04	90.28	81.35
	1100.000	82.16	460.00	81.40	81.40	1.36	72.86	438.15	95.25	81.40
	1100.000	82.41	620.00	81.40	81.40	1.62	72.86	580.75	93.67	81.40
	1100.000	83.13	1100.00	81.40	81.40	2.15	72.86	991.77	90.16	81.40
*	1150.000	82.17	460.00	81.45	81.45	1.27	72.89	402.03	87.40	81.45
*	1150.000	82.44	620.00	81.45	81.45	1.45	72.89	515.42	83.13	81.45
*	1150.000	83.18	1100.00	81.45	81.45	1.79	72.89	823.79	74.89	81.45
	2000.000	82.57	460.00	82.00	82.00	1.38	73.31	415.87	90.41	82.00
	2000.000	82.86	620.00	82.00	82.00	1.54	73.31	529.16	85.35	82.00
	2000.000	83.63	1100.00	82.00	82.00	1.85	73.31	838.51	76.23	82.00
	3000.000	83.09	460.00	82.50	82.50	1.36	73.81	413.94	89.99	82.50
	3000.000	83.40	620.00	82.50	82.50	1.50	73.81	525.50	84.76	82.50
	3000.000	84.17	1100.00	82.50	82.50	1.82	73.81	834.71	75.88	82.50
	4000.000	83.54	460.00	82.80	82.80	1.26	74.31	399.18	86.78	82.80
	4000.000	83.87	620.00	82.80	82.80	1.39	74.31	507.29	81.82	82.80
	4000.000	84.65	1100.00	82.80	82.80	1.71	74.31	810.86	73.71	82.80
	5000.000	83.92	400.00	83.20	83.20	1.13	74.81	348.10	87.02	83.20
	5000.000	84.24	520.00	83.20	83.20	1.20	74.81	426.25	81.97	83.20
	5000.000	85.02	890.00	83.20	83.20	1.41	74.81	655.52	73.65	83.20

	SCNO	CWSEL	Q	XLBEL	RBEL	VCH	EIMIN	QCH	QCHP	TELMX
	5200.000	83.99	400.00	83.40	83.40	1.21	74.91	358.06	89.52	83.40
	5200.000	84.30	520.00	83.40	83.40	1.28	74.91	436.97	84.03	83.40
	5200.000	85.09	890.00	83.40	83.40	1.48	74.91	667.29	74.98	83.40
*	5250.000	83.99	400.00	83.50	83.50	1.36	74.94	388.20	97.05	83.50
*	5250.000	84.30	520.00	83.50	83.50	1.49	74.94	493.41	94.89	83.50
*	5250.000	85.08	890.00	83.50	83.50	1.84	74.94	808.05	90.79	83.50
	5300.000	84.37	400.00	83.60	83.60	1.15	74.96	380.72	95.18	83.60
	5300.000	84.58	520.00	83.60	83.60	1.36	74.96	488.59	93.96	83.60
	5300.000	85.08	890.00	83.60	83.60	1.89	74.96	813.16	91.37	83.60
*	5350.000	84.38	400.00	83.70	83.70	1.12	74.99	353.99	88.50	83.70
*	5350.000	84.60	520.00	83.70	83.70	1.27	74.99	441.88	84.98	83.70
*	5350.000	85.11	890.00	83.70	83.70	1.65	74.99	696.86	78.30	83.70
	6000.000	84.62	400.00	84.10	84.10	1.22	75.31	365.88	91.47	84.10
	6000.000	84.86	520.00	84.10	84.10	1.36	75.31	453.73	87.26	84.10
	6000.000	85.44	890.00	84.10	84.10	1.70	75.31	706.55	79.39	84.10
	7000.000	84.92	400.00	85.50	85.50	1.67	75.81	400.00	100.00	85.50
	7000.000	85.23	520.00	85.50	85.50	2.06	75.81	520.00	100.00	85.50
*	7000.000	86.17	890.00	85.50	85.50	2.21	75.81	805.65	90.52	85.50
	8000.000	85.17	400.00	86.40	86.40	1.75	76.31	400.00	100.00	86.40
	8000.000	85.59	520.00	86.40	86.40	2.11	76.31	520.00	100.00	86.40
	8000.000	87.14	890.00	86.40	86.40	2.03	76.31	802.21	90.14	86.40
	9000.000	85.43	340.00	87.00	87.00	1.56	76.81	340.00	100.00	87.00
	9000.000	85.94	440.00	87.00	87.00	1.83	76.81	440.00	100.00	87.00
	9000.000	87.80	720.00	87.00	87.00	1.59	76.81	645.52	89.66	87.00
	9300.000	85.50	340.00	88.00	88.00	1.58	76.96	340.00	100.00	88.00
	9300.000	86.03	440.00	88.00	88.00	1.85	76.96	440.00	100.00	88.00
	9300.000	87.89	720.00	88.00	88.00	2.21	76.96	720.00	100.00	88.00