

STATE OF FLORIDA

DEPARTMENT OF COMMUNITY AFFAIRS

EMERGENCY MANAGEMENT . HOUSING AND COMMUNITY DEVELOPMENT . RESOURCE PLANNING AND MANAGEMENT

LAWTON CHILES

JAMES F. MURLEY Secretary

Covernor

May 23, 1997

Mr. Jose Fernandez Cellucrete Corp. 11905 NW 99th Avenue Hialeah Gardens, FL 33016

Dear Mr. Fernandez:

This letter is in response to your request for a clarification on how the thermal properties of building properties are determined in Florida's Energy Efficiency Code For Building Construction (the Code).

Commercial applications primarily use U-values, which are determined according to the entena of section 1.1 of Appendix B of the Code. Section 1.1 specifies either use of the ASHRAE Handbook of Fundamentals, data from manufacturer's information or laboratory or field test measurements. Laboratory or field test measurements are obtained by use of specific ASTM standards that utilize a guarded hot plate or hot box, a heat flow meter, or a calibrated hot box.

Residential applications typically consider only the R-value of added insulation products in accordance with the criteria of section 1.2 of Appendix C of the Code. The thermal properties of typical building materials are included in the multipliers provided on Form 600A-93. Any new or emerging technologies for which multipliers are not provided would have to have a methodology established for it by the Department of Community Affairs.

Should you or others have further questions on this issue or others, I can be reached at 904/487-1824.

Sincerely,

Ann L. Stanton

Energy Analyst

1998 REVISIONS

TO THE 1997 Edition of the

FLORIDA ENERGY EFFICIENCY CODE FOR BUILDING CONSTRUCTION

State of Florida
Department of Community Affairs
Building Codes and Standards
2555 Shumard Oak Boulevard
Tallahassee, Florida 32399-2100
(850) 487-1824

James F. Murley, Secretary

124-1991, the EF used shall be the effective water heating efficiency (CA_{ef}) listed for the appliance by the Gas Appliance Manufacturer's Association (GAMA).

From APPENDIX B, Supplemental Information for Chapter 4, the following sections are revised to read:

1.1 General. Information on thermal properties, performance of building envelope sections, and components and heat transfer shall be obtained from the 1997 ASHRAE Handbook of Fundamentals. When the information is not available from this source, the data may be obtained from manufacturer's information based on laboratory or field test measurements.

If laboratory or field test measurements are used for envelope heat transmission, they shall be obtained using one of the following test methods:

1. Guarded Hot Plate:

ASTM C-177-97

2. Heat Flow Meter:

ASTM C-518-91

3. Guarded Hot Box:

ASTM C-236-89

4. Calibrated Hot Box:

ASTM C-976-90

From Appendix C, Supplemental Information for Chapter 6, the following sections are revised to read:

- **2.1 Glass Multipliers.** Three basic underlying assumptions were used in development of the Fla/Res window load correlation coefficients:
 - 1. Frame area equals 25% of the total window area.
 - 2. Frame U-value equals glass U-value equals overall U-value
 - 3. Interior shading factor equals 0.70 in summer and 0.9 in winter.

The general equation for determining the window point multipliers is as follows:

 $PM = A_{1}-SC_{0} + A_{2}-U_{0} + A_{3}-(SC_{0}-U_{0}) + A_{4}-SC_{0}^{2} + A_{5}-U_{0}^{2}$ Equation 6-1a Where:

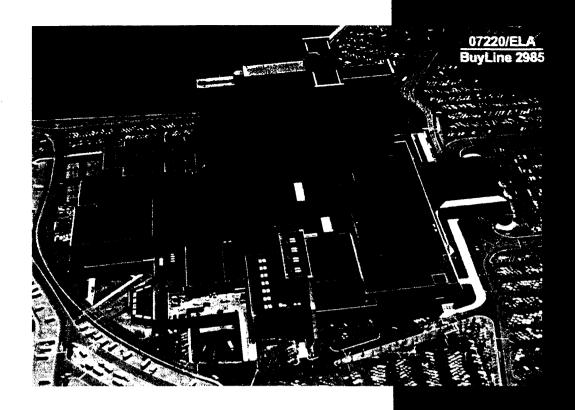
PM= "Point multipliers" (load coefficient in kBtu/ft² of window)

SC_o= Overall shading coefficient of entire installed system including glass, frame and sash and interior treatments

U_o = Overall U-value of entire installed window system, including glass, frame and sash

A_i = Regression coefficients

Coefficients A_1 through A_5 vary by season of the year (2), by climate zone (3), and by glass orientation (8 + horizontal = 9), such that there are 54 sets of A-coefficients needed to fully describe the window "point multipliers" (load correlation coefficients in Florida's Energy Code).



QUALITY ROOF DECKS FOR NEW CONSTRUCTION AND REROOFING APPLICATIONS

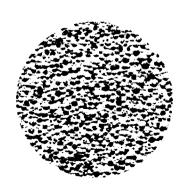
Slope-to-Drain

Lightweight

High R-Value

Superior to Insulation Board

Low Cost



COMPOSITE INSULATING ROOF DECK SYSTEMS

PHYSICAL P	PHYSICAL PROPERTIES												
	Air Dry Density (pcf)	Oven Dry Density (pcf)	Cast Density (pcf)	28-Day Minimum Compressive Strength (psi)	R-value (per inch)								
RANGE IA RANGE IB	21-27	16-20 20-24	26-34	40 80	1.80 1.58								
RANGE IIA RANGE IIB	27-32	24-28 28-32	34-42	160 200	1.34 1.20								
RANGE IIIA RANGE IIIB	32-40	32-38 38-44	42-50	250 300	1.00 0.86								
NOTE: Thermal cond	luctivity is based on the	e minimum dry density	measured at a me	ean temperature of 75 degre	ees F.								

1/2" plywood 3/4" plywood 1/2" gypsum board 5/8" gypsum board 1/2" acoustical tile 3/4" acoustical tile 2" polystyrene board 1-1/2" polystyrene board 1" polystyrene board 1" polystyrene board 1" polystyrene board 1" urethane - sprayed on, 3 pcf 1" fiberboard 3/4" plaster 1" poured perlited gyp 1" poured perlited gyp 1" polyetle board 1.25 air space (heat flow u air space-winter-reflet air space (heat flow d air space-summer-reflet air space (heat flow d air space-summer-reflet air space (heat flow d air space) 1" Foamglass insulati 15/16" Fiberglas® Ro	p-winter) 0.94 ctive surface 1.90 lown-summer) 1.23 lon 2.63 of insulation 2.78

Sources: ASHRAE Handbook of Fundamentals and manufacturer's values.

SEISMIC DATA

Elastizell and steel decking meet Seismic Zone 4 requirements.

These seismic shear values are based on:

- 1. Steel deck need not be web slotted.
- 2. Deck welding pattern of 3-3 in each corrugation.
- 3. When required, Keydeck Mesh Style 2160-2-1619.
- 4. Minimum 2" thick, 200 psi Elastizell.
- 5. EPS with six-3" diameter holes per 2' by 4' board.

Diaphragm Shear Values (lbs./lin. ft.)

For 2" ELASTIZELL Insulating Concrete Over High Tensile Corrugated Steel Deck And From 1" to 4" of EPS Insulation Board

Base Metal Thickness and (Deck Gauge)	Allo Diaphra Mesh	F	
.018" (26 ga)	570	No Mesh	4.5
.020" (26 ga)	630		4.5
.024" (24 ga)	750	460	4.5
.030" (22 ga)	930	640	4.5
.036" (20 ga)	1030	790	4.5

GUIDES and APPROVALS

Underwriters Laboratories:

Wind Uplift Class 90 - Construction Nos. 155 & 480 Fire Ratings - Multiple listings (see previous page)

Factory Mutual Approval Guide

Non-combustible & Class I Roof Deck Construction ICBO

Report Nos. 1381 and 3081

Federal Construction Guide Specification

Section 03501 - May, 1975, Insulating Concrete Roof Decks

Corps of Engineers Guide Specification

CEGS-03501 - June, 1988

Southern Building Code Congress, SBCC Report No. 8254

California State Fire Marshall

Listing 1060-510:2

City and County of San Francisco

General Approval 121 E2.4

City of Los Angeles

Research Report No. 23982

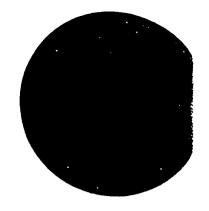
Army Corps of Engineers

September, 1970, CE 204 - Class F

Dade County (Florida)

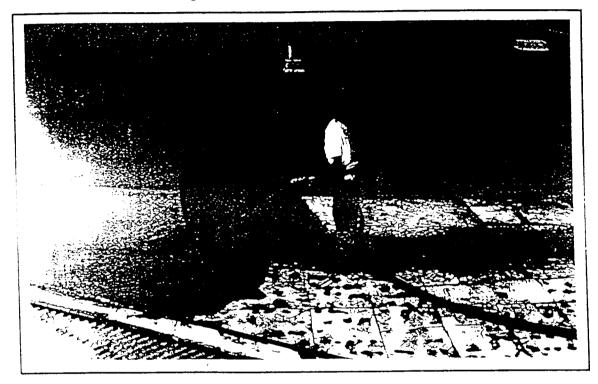
Approval No: 97-0611.03

MEARLCRETE® CELLULAR CONCRETE ROOF DECKS



Lightweight Insulated Cast-In-Place Concrete Roof Deck Systems
On

Galvanized Corrugated Steel Decks Or Concrete Substrates



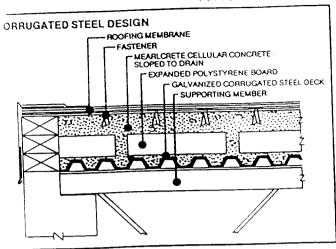


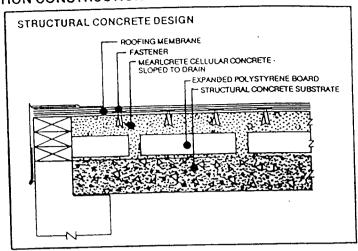
Over 35 Years of Successful Worldwide Roofing Projects Used In Both New Roof Deck Systems Installations & Re-Roofing Projects with BUR & Single Ply Roofing Membranes

TECHNICAL BULLETIN R411F



TYPICAL ROOF INSULATION CONSTRUCTION





MEARLCRETE Roof Deck · Physical Properties Compressive

Wet Density lbs/ft*(1)	Dry Density lbs/ft'	Strength Ibs/in ¹ (2)	*F/(BTU/hr/sq.ft.) per in. Thick
30	25	140	1.49
35	29	210	1.32
33	34	330	1.15
45	38	450	1.02

Rigir/Cement Ratio = 0.50 reinog of ASTM C-495

Actual properties will depend on dement used along conditions and other variables as dictated by job conditions

provals & Guides:

w York City Board of Standard/Appeals (Docket 680-58-SM)

de County, Florida - #96-0919.01

Army Corps of Engineers - CEGS-03510

Roof Decking, Cast-In-Place Low Density Concrete

Technichal Staff Membership Representation:

American Concrete Institute

American Society for Testing and Materials

National Roof Deck Contractors Association

South Florida Roof Deck Association

Roof Consultants Institute

TYPICAL CORRUGATED STEEL DECK LOADS/SPAN TABLE

THREE SPAN CONDITION - ALLOWABLE UNIFORM ROOF LOADS IN POUNDS PER SQUARE FOOT

THREE	SPAN	COND	11011-7	CCO										1	1	1
Depth of Corrugation	ibs. per	Mament of Inertia In ⁴ /ft	Section Modulus In ³ /ft	3′ -0″	3' -6"	4′ -0~	4′ -6″	5′ -0″	5′ -6″	6′ -0″	6′ -6″	7' -0~	7′ -6‴	8′ -0″	8′ -6″	9' -0"
9/16" to	0.76 to 0.95	0.010 to 0.013	0.032 to 0.039	99- 131	75- 96	58- 73	47- 58	38- 47-		_	-	_	-	-	-	
9/16" to	1.0 to 1.18	0.013 to 0.084	0.046 to 0.118	140- 279	100- 209	80- 221	175	50- 142	41- 117	34- 98	84	72	63	55	44	36-
15/16" to	1.37 to 1,50	0.083 to 0.136	0.105 to 0.146	-	-	204- 273	161 216	131- 175	108- 144	91- 121	101	89	78	68	59	53
1-5/16" to	1.68 to	0.100 to 0.183	0.143 to 0.209	_	-	226- 343	206- 271	167- 220	138- 181	116- 153	101-	85- 112	98	86	67	66
1-5/16" to	2.0 to	0.122 to 0.164	0.170 to	-	_	300- 422					121- 160	98- 138	86- 120	75- 105	90	60- 77
	Depth of Corrugation 9/16" to 19/32" 9/16" to 1-5/16" to 1-3/8" 1-5/16" to 1-3/8" 1-5/16" to 1-3/8" 1-5/16" to 1-3/8"	Depth of Corrugation Sq. Ft. 9/16" 0.76 to 19/32" 0.95 9/16" 1.0 to 1-5/16" 1.18 15/16" 1.37 to 1-3/8" 1.50 1-5/16" 1.68 to 1-3/8" 1.90 1-5/16" 2.0 to 10	Depth of corrugation Sq. Ft. Ibs. per corrugation Sq. Ft. In-1/ft Sq. Ft. In-1/ft 10 0.010 to 19/32" 0.95 0.013 to 1-5/16" 1.18 0.084 1.5/16" 1.37 to 1-3/8" 1.50 0.136 1.3/8" 1.50 0.183 1.5/16" 2.0 0.183 1.5/16" 2.0 0.183 1.5/16" 2.0 0.183	Depth of Corrugation Section of Inertial Ine	Depth of Corrugation Sq. Ft. Section inertia in form to	Depth of Corrugation ibs. per sq. Ft. Moment of inertia in /ft Section Modulus in /ft 3'-0" 3'-6" 9/16" to to to 19/32" 0.95 0.010 to to 131 96 131 96 19/32" 0.95 0.013 0.039 131 96 100 to to 279 209 9/16" 1.0 to to to 1.18 0.084 0.118 1.5/16" 1.37 to to to 1.38 0.084 0.118 15/16" to to to 1.36 0.146 1-5/16" 1.37 to 1.38" 1.50 0.136 0.146 0.146 1.3/8" 1.90 0.183 0.209	Depth of Corrugation Section inertia Section Section	Depth of Corrugation lbs. per Sq. Ft. int/ft Moment of Inertia Int/ft Section Modulus Int/ft 3'-0" 3'-6" 4'-0" 4'-6" 9/16" to 19/32" 0.76 to 10 to 10 to 13 to 19/32" 0.010 to 13 to 13 to 10	Depth of Corrugation lbs. per sq. Ft. Moment of inertial nertial inertial inertia	Depth of Corrugation lbs. per Sq. Ft. int/ft Moment of Inertia Sq. Ft. int/ft Section Modulus Int/ft 3'-6" 4'-0" 4'-6" 5'-0" 5'-6" 9/16" to 19/32" 0.76 to 10 to 10 to 19/32" 0.010 to 10 to 13 to 10	Depth of Carrugation Section Modulus Section Modulus Section Modulus Section Modulus Section Modulus Section Modulus Section Section Modulus Section Section Section Modulus Section Section Section Modulus Section Section Section Section Section Section Section Modulus Section S	Depth of Corrugation lbs. per linertia of inertia of to to 19/32" Section depth of inertia of inertia of inertia of inertia in first in	Depth of corrugation Section inertia for to to to to to to 1-5/16" 1.68 to 1-3/8" 1.90 0.183 0.209 1.5/16" 1.90 0.183 0.209 1.5/16" 1.90 0.183 0.209 1.5/16" 1.90 0.183 0.209 1.5/16" 1.5/16" 2.0	Depth of Corrugation Ibs. per inertia of inertia of inertia of inertia of inertia of inertia in first in fi	Depth of Corrugation Sq. Ft. Inf/ft Section to finertia Section to finertia Sq. Ft. Inf/ft Section to finertia Section Section to finertia Section Section for finertia Sectio	Depth of Sq. Ft. Ibs. of

Note: Loads Shown Are For Steel Decks Only

Siplast Roof Insulation THERMAL VALUES

\$ siplast

Roof insulations must perform the basic function of helping to control fluctuations in building interior temperature relative to changing exterior temperatures. By reducing interior temperature fluctuations, the comfort of building habitants is improved and the air conditioning or heating costs can be controlled. Several factors affect the selection of design thermal values for insulation materials. The performance of roof insulation is also affected by additional factors relative to application of the system.

Roof Insulation Thermal Values

The thermal values of insulation materials are determined by ASTM standard test methods. ASTM standards C 518 and/or C 177 define specific conditions known as steady-state for determination of a material's thermal properties. In summary, these steady-state conditions for determination of K-factors are:

- 1. The material must be homogeneous through its thickness.
- The insulation mean temperature must remain constant during the thermal property measuring process (steady-state condition).
- 3. The insulation must maintain constant mass during the measuring process.

The result of these measurements is the thermal conductivity or K-factor for the material at the specific mean temperature during measurement. The typical mean temperature used by insulation manufacturers is either 40°F or 75°F. Other mean temperatures may be used but may not be representative of roof temperature conditions in the U.S. The R-value or thermal resistance value is determined from the above test measurements using the formula:

$$R = \frac{1}{K \text{ factor}}$$

The R-value is expressed as R per inch for design purposes. Table 1 shows R-values for Siplast Roof Insulation materials and other insulation materials.

Roof Insulation Design

Generally when a designer specifies an insulation, he or she may request that the roof insulation provide a minimum R-value or, when a sloped system is installed that the insulation meet an average R-value. To assist the designer, manufacturers publish tables of insulation values for various thicknesses or combination of materials used in roof insulation.

Table 1

R-Values of Roof Deck Components	R/Inch	Definitions
Zonolite Insulating Concrete 1:6 Mix, 1"	1.49	Thermal Conductivity (k) - the thermal transmission, by conductance only,
NVS Concrete, 1"	0.90	through a one-inch thickness of homogeneous material. Express as BTU-
Insulcel Concrete, 1"	1.30	in./hr. sq. ft. °F.
Zonocel Concrete, 1"	1.10	Thermal Conductance (C) - similar to thermal conductivity but broader. It
Insulperm Insulating Board, 1"	4.00	applies to any thickness of homogeneous and heterogeneous material. Expressed
Steel Decking	0.00	as BTU/hr. sq. ft. °F.
Structural Concrete (140 pcf), 1"	0.08	Thermal Resistance (R) - the reciprocal of thermal conductance (C). Expressed as
Medium Weight Concrete (100 pcf), 1"	0.28	°F hr. sq. ft./BTU.
Glass Fiber Board, 1*	3.70	Thermal Transmittance (U) - also known as overall heat transfer coefficient. The
Expanded Perlite Board, Organic Bonded, 1"	2.78	transmission of heat through a construction air to air. Expressed as
Gypsum Formboard, ½"	0 45	BTU/hr sq ft. °F
Outside Air Film (heat flow up - winter)	0.17	
Outside Air Film (heat flow down - summer) 7 ½ " mph	0.25	
Inside Air Film (heat flow up - winter)	0.61	
Inside Air Film (heat flow down - summer)	0.92	
Built-Up Roofing	0.33	
Polyisocyanurate: Fiberglass Faced, 1"	5.60	
Poured Gypsum (12.5% wood chips), 1"	0.60	•
Extruded Polystyrene (1.8 - 3.5 pcf), 1"	5.00	

Authority for Values: ASHRAE <u>Handbook of</u>
<u>Fundamentals</u>, 1981, Independent Laboratories,
Manufacturer's Literature.
NRCA Roofing and Waterproofing Manual, Third Edition







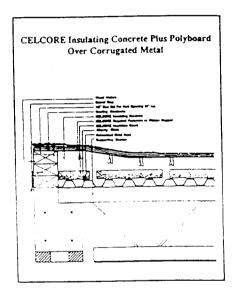


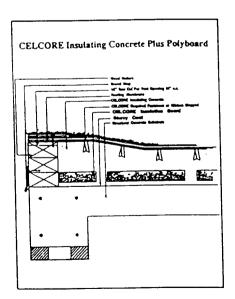
Celcore Roof Insulation

CELCORE INCORPORATED

775 US Hwy 70 West Black Mountain, N.C. 28711 (704) 669-4875 (704) 669-4874 Fax

Web Site: www.celcoreinc.com Fax on Demand: (704) 669-4874





THE PRODUCT

Basic Use: Celcore Foam Concentrate is mixed with water and generated into a preformed foam for addition to a cement/water slurry mixture to create a <u>closed cell</u> cellular concrete of a specific density. Typical air dry densities are in the range of 28 - 39 pcf. Oven dry densities are in the range of 24 - 36 pcf. Typical usages for Celcore Cellular Concrete are poured-in-place insulating applications and geotechnical fills.

Celcore Cellular Insulating Concrete is a key component of a Celcore Cellular Insulating Roof Deck System. Celcore Cellular Insulating Concrete may be used in conjunction with expanded polystyrene board to produce a thermally efficient, fire rated, Underwriter's Laboratories Approved, Factory Mutual Approved, South Florida Approved insulation assembly.

Celcore Cellular Concrete can be poured over some existing roof membranes in reroofing applications, galvanized steel deck form, precast concrete, or poured-in-place structural concrete. Celcore monolithic insulating concrete roof deck fills placed over metal deck form can be designed into structures as shear diaphragms. These composite systems provide good resistance to shear forces which may result from wind or seismic activity. Shear diaphragms provide bracing to the structures they cover acting to transfer and distribute an acting load force through-out the structure.

Composition and Materials. Celeore Foam Concentrate contains no synthetic surfactants. It is comprised of natural saponified rosins and is protein stabilized. Celeore Foam Concentrate is non-corrosive, non-hazardous and readily biodegradable. It is packaged in (5) gallon pails and displays the UL and FMRC mark on the product label.

CELCORE'S TECHNICAL INFORMATION is available through print and electronic media. You have two options for obtaining the following information electronically. Celcore's Web Site - www.celcoreinc.com or via Celcore's Fax on Demand System by calling (704) 669-4874 and following the menu instructions. The information that is available is as follows:

- (1) CSI formatted specification for Celcore's Roof Insulation -
- (2) Roof over existing roof specifications
- (3) Celcore PVA curing compound specifications
- (4) Thin Patch patching material specifications
- (5) Diaphragm design information and tables
- (6) Product Data Sheets
- (7) Celcore Quality Control Guidelines
- (8) Factory Mutual Product Approval Listings
- (9) South Florida Product Approval Listings
- (10) Material Safety Data Sheets
- (11) Geo Technical specifications
- (12) Polystyrene board configuration & installation

THE ENVIRONMENT

Celcore Roof Insulation is a superb product to use in meeting the World's environmental concerns. The foundation for Celcore's Foam Concentrate does not contain man made chemicals. Celcore Foam Concentrate is non-corrosive, non-hazardous, and biodegradable.







Celcore Roof Insulation

CELCORE CELLULAR CONCRETE TECHNICAL DATA

Cast (wet) Density

36 to 49 pounds per cubic foot (Pcf)

Air Dry Density

27 to 39 Pcf

Compressive Strength

175 pounds per square inch (Pst),

Drying Shrinkage Thermal Expansion

0.20 to 0.40

Thérmal Resistance

 $5.0 \text{ to } 7.0 \times 10$

R" = 2.22 per inch thick (average for temp. range 18° - 190°F)

TYPICAL CELCORE MIX DESIGNS

Cast Density 36 pcf Type I Cement 663 lbs. Mix Water 29 gals.		38 pcf	40 pcf	42 pcf	45 pcf		
		703 lbs. 742 lbs.		782 lbs.	850 lbs.		
		31 gals. 32 gals.		34 gals.	37 gals.		
Celcore Foam	19.80 cu. ft.	19.32 cu. ft.	18.94 cu. ft.	18.51 cu. ft.	17.75 cu. ft.		
Concrete Yield	I cu. yard	l cu. yard	1 cu. yard	l cu. yd.	1 cu. yard		
Theroretical Psi	175 psi	225 psi	250 psi	300 psi	350 (+) psi		

"U" FACTOR TABLES FOR CELCORE INSULATING FILL OVER CORRUGATED METAL DECKS & STRUCTURAL CONCRETE SUBSTRATES

Thickness of . CELCORE	Thickness of EPS in	PS in 15/16" Corrugation depth			24 Gauge metal deck 1 1/2" Corrugation depth				auge metal Corrugation		Structural Concrete Substrate Thickness 5 1/2" Density 142 pcf			
concrete over top of deck corregations,	Inches R/In.=3.85	Weight of the Deck	ck HEAT FLOW		Weight of No ceiling the Deck HEAT FLOW		ding	Weight of the Deck	"U" FACTOR No colling REAT FLOW		Wedght of CELCORE	"U" FACTOR No celling HEAT FLOW		
structural concrete or EPS Insulation	Neminal density @ 1 pcf	Composite in the/sq. ft.	UP	DOWN	Composited in lbs:/sq. ft.	U₽	DOWN	Composite in lbs./sq. ft.	UP	DOWN	Deck in bs./sq. ft.	UP	DOWN	
	0	6.08	.139	.132	6.91	.128	.123	7.20	.128	.123	4.00	.140	.113	
2''	1	6.68	.090	.087	7.49	.086	.083	7.78	.086	.083	5.08	.091	.088	
	1 1/2	6.73	.077	.075	7.54	.074	.072	7.83	.074	.072	5.13	.078	.075	
	2	6.77	.067	.065	7.58	.065	.063	7.87	.065	.063	5.17	.067	.066	
	2 1/2	6.81	.059	.058	7.62	.057	.056	7.91	.057	.056	5.21	.060	.058	
	3	6.85	.053	.052	7.66	.052	.051	7.95	.052	.051	5.25	.054	.051	
	3 1/2	6.89	.048	.047	7.70	.047	.046	- 7.99	.047	.046	5.29	.049	.048	
	4	6.93	.044	.043	7.74	.043	.042	8.03	.043	.042	5.33	.044	.044	
	0	7.08	.123	.117	7.91	· kıı.	.110	8_20	.114	.100	5.00	.124	.118	
	1	7.68	.083	.080	8.49	.079	.077	8.78	.079	.077	6.08	.084	.081	
	11/2	7.73	.072	.070	8.54	.069	.067	8.83	.069	.067	6.13	.072	.069	
2 1/2"	2	7.77	.060	.061	8.58	.061	.059	8.87	.061	.059	6.17	.063	.062	
2 112	2 1/2	7.81	.056	.055	8.62	.054	.053	8.91	.054	.053	6.21	.057	.055	
	1 3	7.85	.051	.050	8.66	.049	.049	8.95	.049	.049	6.25	.051	.049	
i	3 1/2	7.89	.046	.045	8.70	.045	.044	8.99	.045	.044	6.29	.047	.046	
	4	7.93	.042	.042	8.74	.041	.041	9.03	.041	.041	6.33	.042	.042	
	0	8.08	.106	.102	8.91	.100	.096	9.20	.100	.096	6.00	.107	.103	
	1	8.68	.075	.073	9.49	.072	.070	9.78	.072	.070	7.08	.076	.074	
	1 1/2	8.73	.066	.064	9.54	.063	.062	9.83	.063	.062	7.13	.066	.063	
3"	2	8.77	.058	.057	9.58	.057	.055	9.87	.057	.055	7.17	.059	.057	
1	2 1/2	8.81	.052	.051	9.62	.051	.050	9.91	.051	.050	7.21	.053	.052	
i	3	8.85	.048	.047	9.66	.046	.046	9.95	.046	.046	7.25	.048	.047	
	3 1/2	8.89	.044	.043	9.70	.043	.042	9.99	.043	.042	7.29	.044	.043	
İ	4	8.93	.040	.040	9.74	.039	.039	10.03	.039	.039	7.33	.040	.040	

(CRI L/17)



April 7, 1997

Mr. Jose E. Fernandez Cellucrete Corp. 11905 N.W. 99th Ave. Hialeah Gardens, FL 33018

Dear Mr. Fernandez:

I have perused the Westinghouse report titled "Lightweight Concrete Materials and Structural Systems for Water Tanks for Thermal Storage" (C00-4703-26) and dated December 1980. The test method used in this report does not conform to any ASTM consensus industry accepted thermal test method. The four (4) methods generally accepted are ASTM C177 (guarded hot plate), C518 (heat flow meter), C236 (guarded hot box) and C976 (calibrated hot box).

If you have any questions, please contact me at (813) 578-4351.

Sincerely,

R. G. Miller, PhD, P.E.

Manager

Materials Testing Services

RGM:dds

CELCORE "R" VALUE TESTING PROCEDURE

COO-4703-26

Advanced Energy Systems Division



LIGHTWEIGHT CONCRETE MATERIALS AND STRUCTURAL SYSTEMS FOR WATER TANKS FOR THERMAL STORAGE

A TAN REPORT

Prepared by R.W. Buckman, Jr. G.G. Elia Y. Ichikawa

DECEMBER 1980

Prepared for The United States Department of Energy Under Contract EM78 C 02 4703 Amaged Amaged Prepared for the United States Department of Energy Under Contract EM78 C 02 4703 Amaged Prepared for the United States Department of Energy Under Contract EM78 C 02 4703 Amaged Prepared for the United States Department of Energy Under Contract EM78 C 02 4703 Amaged Prepared for United States Department of Energy Under Contract EM78 C 02 4703 Amaged Prepared for United States Department of Energy Under Contract EM78 C 02 4703 Amaged Prepared for United States Department of Energy Under Contract EM78 C 02 4703 Amaged Prepared For United States Department of Energy Under Contract EM78 C 02 4703 Amaged Prepared For United States Department Of Energy Under Contract EM78 C 02 4703 Amaged Prepared For United States Department On Under Contract EM78 C 02 4703 Amaged Prepared For United States Department On Under Contract EM78 C 02 4703 Amaged Prepared For United States Department On Under Contract EM78 C 02 4703 Amaged Prepared For United States Department On Under Contract EM78 C 02 4703 Amaged Prepared For United States Department On Under Contract EM78 C 02 4703 Amaged Prepared For United States Department On United States D

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