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Reprinted 12/10/84

U.S. NATIONAL AVIATION STANDARD FOR THE VOR/DME/TACAN SYSTEMS



September 2, 1982

- DEPAR TMENT OF TRANSPORTATION FEDERAL AVIATION ADMINISTRATION

FOREWORD

Very High Frequency Omnidirectional Radio Range (VOR)/Distance Measuring Equipment (DME)/Tactical Air Navigation (TACAN) is the primary short distance navigational aid used in the National Airspace System (NAS) for air navigation and traffic control. Achievement of navigation system performance requires the definition of system functional and performance characteristics. The purpose of publishing a National Aviation Standard is to describe how the system is operated and how the different elements fit together. It should be noted that although the terms of measurement reference have been changed from Order 1010.55 dated 6/1/70 to allow standardization, the effect on component and system performance is minimal.

It should be recognized that the frequency bands used by the systems described in this standard have been exclusively allocated for aviation navigation. Due to the limited availability of frequencies, these bands will be increasingly utilized by common equipment and other systems. For this reason, designers, manufacturers, and operators of VOR/DME/TACAN equipment should be especially conscious of those paragraphs in the standard which impact on spectrum utilization. This is necessary to avoid present and future electromagnetic interference not only between **common** equipments but also between **o**ther systems as well.

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R**OBERT W. WEDAN** Director, Systems Research and Development Service, ARD-1

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CHAPTER 1. GENERAL

SECTION 1. INTRODUCTION

1. <u>PURPOSE</u>. This order establishes the Very High Frequency Omnidirectional Radio Range (VOR)/Distance Measuring Equipment (DME)/Tactical Air Navigation (TACAN) standard defining the performance required of the system and its components.

2. <u>DISTRIBUTION</u>. This order is distributed to: a) branch level in the organizations of Flight Operations, Airway Facilities, Air Traffic, and Systems Research and Development in Washington headquarters; b) section leve in Airway Facilities Service in regions; and c) sector and sector field offices of the Airway Facilities Service.

3. <u>CANCELLATION</u>. Order 1010.55, "Selection Order: U. **S.** National Aviation Standard for the VORTAC System," dated **6/1/70** is cancelled.

4. <u>IMPLEMENTATION CRITERIA</u>. The National Aviation Standard applies to all VOR, DME, and TACAN round and airborne equipments used in the National Airspace System (NAS₃.

5. <u>DIRECTED ACTION</u>. Subject to applicable rulemaking, programing and budgetary procedures, actions shall be taken by the FAA elements concerned to implement this Standard.

SECTION 2. OVERVIEW

6. <u>GENERAL</u>. Under Public Law 85-726, the Federal Aviation Administration (FAA) is charged with providing for the regulation and promotion of civil aviation in order to best foster its development and safety, and to provide for the safe and efficient use of the airspace by both civil and military aircraft. Explicitly, the Administrator shall develop, modify, test, and evaluate systems, procedures, facilities, and devices, defining their performance characteristics as needed. This effort is directed toward meeting the need for safe and efficient navigation and traffic control of all civil and military aviation operating in a common Civil/Military System.

7. THE VOR/DME/TACAN SYSTEM CHARACTERISTICS.

a. This Standard defines the application and performance characteristics of VOR, DME, and TACAN systems in the United States (U. S.). For ground and airborne components, the material identifies signal, functional, and performance characteristics required to meet operational requirements and to provide compatibility between components of the system.

b. The respective airborne component characteristics for VOR, DME, and TACAN apply In entirety to those components used in aircraft operations performed under Instrument Flight Rules (IFR). However, for other aircraft operations the applicability is limited to requirements identified in chapter 3, section 2 and chapter 4, section 2 as essential to prevent impairment of services to other NAS users. c. In all cases, where a parameter and associated tolerance is identified herein, ground stations shall be maintained within these limits of quality assurance methods including either monitoring, periodic ground or flight inspections, or a combination of these methods.

d. Operators of airborne systems designed, installed, and operated in accordance with the Standard can expect to achieve the system performance which the standard is intended to provide.

e. It is recognized that certain existing components do not comply with all requirements of this Standard. Specific characteristics that are known to deviate from the requirements of this Standard will be corrected or replaced as practical.

8. <u>REVISIONS</u>. This Standard will be revised as the needs of the National Airspace System warrant.

9. <u>RELIABILITY REQUIRED OF THE VOR/DME/TACAN SYSTEM</u>. Due to the critical nature of the radionavigation service, it is essential that the VOR/DME/TACAN system provide high reliability. Both signal strength and frequency protection are provided on a basis of 95 percent time availability at the worst case points of the service volume. At other than worst case points, time availability substantially exceeds 95 percent. (See Appendix 1, paragraph 6.)

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CHAPTER 2. VOR/DME/TACAN SYSTEM

20. VOR/DME/TACAN SYSTEM DESCRIPTION. The VOR/DME/TACAN system is a short distance air navigation system. The ground components provide properly equipped aircraft with bearing, identification, and distance Infotmation referenced to the selected ground component. When the airborne equipment includes a suitable area navigation (RNAV) device operating from data derived from the system, both radial and non-radial routes are afforded. The system provides navigation signals to all civil and military aviation for the safe and efficient conduct of aircraft operations, exercise of air traffic control, and use of airspace.

21. <u>GROUND COMPONENTS</u>. The principal ground components are VOR, DME, and TACAN. VOR and DME are the International Civil Aviation Organization (ICAO) standard navigational aids. VOR provides azimuth information and ground-to-air communications for the **common** NAS. **DME** provides distance Information to all users of the NAS. TACAN provides azimuth information primarily to military users and distance information to all users of the NAS.

22. STATION TYPE DESIGNATIONS. Ground components are Identified by type **desig**nations which **indicate the** service provided. VOR type designations are prefixed by the letter **"B"** when the component provides scheduled voice broadcasts. The letter **"W" is** used when the component does not provide voice transmissions.

Designation	<u>Type of Facility</u>
VOR	VHF navlgation facility, omni-directional azimuth only
DME	UHF navigation facility, distance only
TACAN	UHF navigational facility, omni-directional, azimuth and distance
VOR/DME	Associated VOR and DME navigational facilities
VORTAC	Associated VOR and TACAN navigational facilities

23. <u>SERVICE VOLUMES</u>. Maximum usable range is influenced by a large number of variables. These **include** factors such **as** antenna patterns, propagation variation, ground **terrain**, ground and avionics **equipment** performance, ground and avionics equipment installation and maintenance, traffic loading and traffic distribution. It should be noted that the aviation **community** has many years of operational experience with the **VOR/DME/TACAN** system. Service volumes are predicated on both experience and empirical measurements.

Suff icient safety margin has been incorporated to assure highly reliable system operation. Under worst case conditions, it is recognized that some combinations of avionics and older ground equipments may not provide service with a time availability of 95 percent. Based on operational experience and user feedback, no substantial evidence indicating an adverse operational impact has been shown. In addition, all service volumes are flight inspected prior to **commissioning** for operational use. Nonetheless, ground and airborne equipment should be brought into full compliance with this National Aviation Standard as soon as it is practical.

a. Standard Service Volumes (SSV).

(1) Ground stations are classified according to their intended use. These stations are **available** for use within their service volume. Outside the service volume, reliable service may not be available. For standard use, the airspace boundaries are called standard service volumes. They are defined, in the table below, for the three station classes.

SSV CLASS DESIGNATOR	ALTITUDE AND RANGE BOUNDARIES
T (Terminal)	From 1000 feet (305 m) AGL up to and includin 12,000 feet (3,658 m) AGL at radia3 distances out to 25 nmi (46 km). See Figures 2-3 and 2-4.
L (Low Altitude)	From 1000 feet (305 m) AGL up to and including 18,000 feet (5,486 m) AGL at radial distances out to 40 nmi (74 km). See Figures 2-2 and 2-5.
H (High Altitude)	From 1000 feet (305 m) AGL up to and including 14,500 feet (4,420 m) AGL at radial distances out to 40 nmi (74 km). See Figures 2-1 and 2-5. From 14,500 feet (4,420 m) AGL up to and including 60,000 feet (18,288 m) at radial distances out to 100 nmi (185 km). See Figures 2-1 and 2-5. From 18,000 feet (5,486 m) AGL up to and including 45,000 feet (13,716 m) at radial distances out to 130 nmi (241 km). See Figures 2-1 and 2-5.

(2) These **SSV's** are graphically shown in Figures 2-1 through 2-5. The SSV of a station is indicated by using the class designator as a prefix to the station type designation. (Examples: TVOR, **LDME**, and **HVORTAC**.) (3) Within 25 nmi (46 km), the bottom of the T Service is defined by the curve In Figure 2-4. Within 40 nmi (74 km), the bottoms of the L and H service volumes are defined by the curve in Figure 2-S. In some cases, local conditions (terrain, buildings, trees, etc.) may require that the standard service volume be restricted. The public shall be informed of any such restriction by a Notice to Airman (NOTAM).

NOTE: Metric measurements are given for convenience and are approximations.

b. Expanded Service Volumes. When operational needs require facilities to be used beyond their standard service volumes, the same **signal** standards/tolerances and round/flight check certification procedures will be met. Expanded service vo3**umes (ESVs)** will only be authorized when **conditions** permit (reference Figures 2 through 13 of Appendix 1.).

c. <u>Operational Service Volume</u>. The airspace available for operational use **includes**:

(1) The $\ensuremath{\mathsf{SSV}}$ excluding any portion of the SSV which has been restricted, and

(2) expanded service volumes (ESVs).

d. Vertical Angle Coverage Limitations. Within the operational service volume of each station, azimuth signal information permitting satisfactory performance of airborne components is normally provided from the radio horizon up to an elevation angle of approximately 60 degrees for VOR components and approximately 40 degrees for TACAN components. At higher elevation angles, the azimuth signal information may not be usable. Distance information provided by DME and TACAN will permit satisfactory performance of airborne components from the radio horizon to an elevation angle of not less than 60 degrees.

24. ASSOCIATED COMPONENTS. A VOR and either a DME or TACAN shall be **considered** as associated components only when:

a. operated on a standard frequency pairing as **associated** with paragraph 28;

b. collocated as **defined** in paragraph 25; and

c. complying with the identification provisions of paragraph 32.

25. <u>COLLOCATION LIMITS FOR ASSOCIATED COMPONENTS</u>. DME or TACAN components are **frequency-paired** with VOR. For the **common** system, these components shall be collocated In accordance with one of the following.

a. <u>Coaxial collocation</u>. The VOR and DME or TACAN antenna are located on the same vertical axis. **This** is the usual collocation configuration.









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b. Offset collocation.

(1) For those facilities used in terminal areas for approach purposes or other procedures where the highest position fixing accuracy of system capability is required, the separation of the VOR and DME or TACAN antennas will not exceed 100 feet (30 m). However, at Doppler VOR sites the antennas may be separated by not more than 260 feet (80 m).

(2) For purposes other than those indicated in (1), the separation of the VOR and either the DME or TACAN antennas will not exceed 2000 feet (610 m).

26. <u>RADIO FREQUENCY ALLOCATIONS</u>. Radio frequencies a**llocated** for VOR, DME, and TACAN are those listed in Appendix 3.

27. <u>RADIO FREQUENCY ASSIGNMENTS</u>. Radio frequency assignments for the paired system-components shall be selected from the frequency pairings listed *in* Appendix 3. Channels 1 through 16 and 60 through 69 for both X and Y modes of operation shall not be assigned to components of the common system.

28. RADIO FREQUENCY CHANNEL PAIRING. Appendix 3 shows the pairing of the VHF and UHF components of the VOR/DME/TACAN System. Components associated according to paragraph 24 shallbe assigned on paired frequencies in accordance with this table. Non-associated VOR, DME, and TACAN components shallnot be assigned on paired frequencies unless the separation between the respective corp onents is sufficient to satisfy paragraph 29. This latter separation shdl1 be determined as if each station was in effect an associated frequency pair.

29. <u>FREQUENCY INTERFERENCE PROTECTION</u>. Frequency assignments must not result in interference between stations. Within a station's operational service **volume**, the ratio of the desired signal to any undesired signal must not fall below the selection/rejection capability of the airborne equipment. Paragraphs 29.a through 29.c discuss interference protection needed. The usable **distance** and altitude of aeronautical navigation aids are often limited by the frequency protection provided from other ground stations. The operational service volume shall not extend beyond the frequency protected service volume.

a. Interference Protection of VHF NAVAIDS (ILS and VOR). The following interference signal **protection** ratios shall be provided within the operational service volume of all Instrument Landing System (ILS) and VOR stations with a 95 percent time availability. This is done by controlling the station separation in certain situations.

(1) The desired to undesired (D/U) signal ratio between co-channel stations shall not be less than **+20 dB.**

(2) The D/U ratio between VHF NAVAIDS with a nominal 50 kHz frequency separation shall be -34 dB or greater. (-34 dB or -30dB are permissible; -40 dB is not.) Frequency assignments made under this criteria (called the "Final" criteria) insure protection to narrow bandwidth (i.e., 50 kHz) receivers considering both ground and airborne frequency tolerances. A minimum D/U ratio of -7 dB is required to insure protection to wideband (i.e., 100 kHz) receivers using 100 kHz (i.e., even multiples of 50 kHz) ground stations. This value is called the "Interim" criteria. In highly congested parts of the country, the "Interim" criteria may not allow frequency assignments to any new systems. New assignments in these areas would have to be made under the final criteria (-34 dB). As a safeguard when this is done, flight publications will indicate any nearby 100 kHz ground stations which cannot be used without the narrow bandpass characteristics associated with a 50 kHz receiver. This is required due to the insufficient rejection, in the 100 kHz receivers, to signals 50 kHz removed.

(3) The D/U ratio between VHF NAVAIDS with 100 **kHz** frequency separation shall not be less than -46 **dB**. In those parts of the country where 50 **kHz** assignments are made, the D/U ratio between stations with 100 **kHz** frequency separation shall not be less than -50 **dB**.

(4) The D/U ratio between VHF NAVAIDS with more than 100 $\rm kHz$ frequency separation shall not be less than -50 $\rm dB$.

(5) Some peak power deterioration is allowed before the system is shut down. In order to account for this decrease in power, the actual D/U values used for station separation calculations are 3 d8 more protective, e.g. +23 dB vice +20 dB, -31 vice -34 dB, etc.

b. <u>Interference Protection of DME/TACAN</u>. The following interference signal protection ratios shall be provided within the operational service volume of all DME/TACAN stations with a 95 percent time availability. This is done by controlling the station separation in certain cases.

(1) The D/U signal ratio between co-channel DME/TACAN stations shall not be less than **+8 dB.**

(2) The D/U signal ratio between adjacent channel **DME/TACAN** stations shall be as follows. The various D/U ratios have been established recognizing the spectrum control characteristics reflected in paragraph 124 and the spectrum differences between DME and TACAN.

(a) When the undesired station is a TACAN, the D/U ratio shall not be less than -42 ${\bf dB}_{\bullet}$

(b) When the undesired station is an LDME (1000 W transmitter), the D/U ratio shall not be less than -39 ${\bf dB}_{\bullet}$

(c) When the undesired station is a ${\rm TDME}$ (100 W transmitter), the D/U ratio shall not be less than -29 ${\rm dB}_{\rm \bullet}$

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(3) The O/U ratio between DME/TACAN stations with more than 1 MHz frequency separation shall not be less than -50 dB.

(4) Some peak power deterioration is allowed before the system **is** shut down. In order to account for this decrease in power, the actual D/U values used for station separation calculations are 3 **dB** more protective, e.g., +1 **l dB** vice +8 **dB**, -39 **dB** vice -42 **dB**, etc.

c. <u>Protection of Service Volumes Which Extend Beyond National Borders</u>. Stations near the border are normally not frequency-protected for that airspace which lies beyond the national border. Standard service volume and expanded service volume protection may be provided upon proper coordination with Canada or Mexico. This must be done whenever specific airways, routes, or procedures beyond the border are based on ground stations in the U.S.A.

30. <u>COMPONENT IDENTIFICATION SIGNALS</u>. Each ground component shall transmit an identification signal consisting of three letters in International Morse Code. It shall be transmitted at a rate of approximately 7 words per minute. In addition, voice identification in accordance with paragraphs 31 through 33 may be provided by a VOR.

a. <u>Identification Code Characteristics</u>. The identification code characteristics shall conform to the following.

(1) The dots shall be a time duration of \emptyset .1 second to \emptyset .125 second and the dashes three times the dot duration;

(2) The duration between dots and dashes of a code letter shall be equal to that of one dot plus or minus 10 percent;

(3) The time duration between consecutive letters of the identification code group shall not be less than three dots; and

(4) The total period of transmission of an identification code group shall not exceed 5 seconds.

b. <u>Identification Cycle and Synchronization</u>. The repetition and synchronization of component **identification signals** shall conform to paragraphs 31 through 33.

31. INDEPENDENT COMPONENTS. Whenever a facility is operated as a VOR, a DME, or a **TACAN** only, its identification signal shall be transmitted as follows.

a. For VOR providing only code identification signals, each 30 second **interval** is divided into either four or five equal periods. The code identification shall be transmitted during each period.

b. For VOR providing code and voice identification signals, each 30 second interval is divided into four equal periods. The code identification signal shall be transmitted during alternate periods or durin**g** three of four periods. Subject to paragraph 33, voice identification **signals** will occur during the remaining period(s).

c. When voice communication signals are being transmitted by a VOR, the **VOR** code identification signals shall not be suppressed.

d. For DME and TACAN, the International Morse Code identification signal shall be repeated at intervals of 30 seconds.-

32. IDENTIFICATION OF ASSOCIATED COMPONENTS. When a **VOR** and either **a DME** or TACAN are operated as collocated components (see paragraphs 24 and **25)**, the identification signals shall conform to the respective requirements of paragraph 31 except that:

a. The identification code shall be the same for each component;

b. For VOR of paragraphs 31.a and **31.b**, the DME or TACAN identification signal shall be transmitted during one of the periods allocated for **VOR** code identification. The VOR code shall not be transmitted during that period;

c. The International Morse Code identification signals of **VOR**, **DME**, and TACAN shall be synchronized and interlocked such that simultaneous identification transmissions of **VOR/DME** or VOR/TACAN or **ILS/DME** do not occur;

d. When voice **communications** are being transmitted on the **VOR**, the Code identification signals of **DME** and TACAN shall not be suppressed; and

e. Whenever one component is temporarily out of service, the component still operating shall transmit facility identification si nals in accordance with paragraph 32 without regard to the facility type des3**gnation**.

33. PRECEDENCE OF VOR VOICE COMMUNICATIONS. VOR voice identification signals shall not be suppressed for the duration of voice communications or broadcasts.

34. VOR VOICE COMMUNICATIONS SIGNALS. If required, a VOR may provide ground-to-air voice communications.

35. <u>AIRBORNE COMPONENTS</u>. Airborne components of the system consist of VOR components conforming to chapter 3, section 2 and DME and TACAN components conforming to the applicable requirements of chapter 4, section **2** of this Standard.

36. <u>SYSTEM TRAFFIC HANDLING CAPACITY</u>. Each VOR and TACAN ground component of the system provides azimuth and **facility** identification information to an unlimited number of airborne components. DME and TACAN ground components can provide slant range adequate for a peak traffic load of 3375 interrogations per second.

> NOTE: As the traffic density increases beyond full **load**, the system replies at a rate reduced proportionately-to the number of additional interrogators. The ground component could be capable of servicing higher density traffic only if the airborne component could maintain satisfactory operations with reduced reply efficiency (see paragraph 130). The apparent change in numbers from Order 1010.55 dated 6/1/70 does not represent a change in beacon radiated power (for example, see Appendix 1). Therefore, increases in receiver sensitivities of existing airborne equipments are not required to achieve the same ranges that users have experienced in the past. Future designs should not be restricted by this fact.

37. <u>VOR/TACAN/VORTAC SYSTEM AZIMUTH ACCURACY</u>. System azimuth accuracy, expressed in terms of error, is a function of the error factors associated with the ground and airborne components. The total system azimuth accuracy is <u>+</u> 4.5 degrees. (See Appendix 2)

38. SYSTEM DISTANCE ACCURACY. System distance accuracy is a function of the ground and airborne component accuracies. The component values in **this** standard provide a system distance accuracy of \pm Ø.5 nmi (926 m) or 3 percent of the slant range distance, whichever is greater (95 percent probability), when the error values are combined by the root-sum-square method.

39. HIGH ACCURACY CERTIFICATION. Some system accuracy requirements exceed those specified in paragraphs **37** and 38. Some area navigation routes are an example. In order to support prescribed operations, flight inspections will validate the signal and certify its adequacy.

40.-49. <u>RESERVED</u>.

CHAPTER 3. VOR SYSTEMS

SECTION 1. OPERATIONAL CHARACTERISTICS FOR VOR GROUNO COMPONENTS

50. <u>INTRODUCTION</u>. This section identifies standard signal characteristics and tolerances for the VOR portion of the system. These characteristics represent performance which shall be provided throughout the operational service volume as defined in paragraph **23.c.**

51. <u>POLARIZATION</u>. The ground component antenna shall radiate horizontally polarized signals. Any vertically polarized signal components shall be at least 26 **dB** weaker than the horizontally polarized component.

52. RADIO FREQUENCY ACCURACY. The radio frequency **carrier** shall be within **± 0.002** percent of the assigned frequency.

53. <u>SIGNAL STRENGTH IN SPACE</u>. The ground station shall provide a minimum signal power density of -120 dBW/m² (95 percent time availablllty) throughout the operational service volume as defined In paragraph 23.c. At the nearest aircraft position expected during operations, the maximum signal power density expected at an aircraft will be on the order of -34 dBW/m².

NOTE: At 118 MHz, the value -120 dBW/m² corresponds to -123 dBW at the output of a lossless isotropic receiving antenna. The apparent change In numbers from Order 1010.55, dated 6/1/70, does not represent a change in radiated power (for example, see Appendix 1). Therefore, increases in receiver sensitivities of existing airborne equipments are not required to achieve the same service ranges that users have experienced in the past. Future designs should not be restricted by this fact.

54. AZIMUTH SIGNAL CHARACTERISTICS. The VOR shall radiate a radio frequency carrier with two associated 30 Hz modulations. The phase of one of these modulations shall be independent of the **azimuth** of the point of observation (reference phase). The other modulation (variable phase) shall differ from that of the reference phase by an angle equal to the magnetic bearing of the point of observation with respect to the VOR.

a. The radio frequency carrier shall be amplitude modulated by two signals in accordance **with** the following.

(1) Subcarrier Frequency Modulation. One **sig**nal component shall be a subcarrier of 9,960 Hz of constant **amplitude**. It shall be **frequency** modulated at 30 Hz having a deviation **ratio of 16** \pm 1 (i.e., 15 to 17) as follows.

NOTE: The deviation ratio of the signal from a Doppler VOR decreases from the value at the facility by the **cosine** of the vertical angle (i.e., will be as low as 8 at a point 60 degrees above the horizon).

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(a) For the conventional VOR, the **phase** of the 3Ø Hz component of the FM subcarrier Is fixed without respect to azimuth. It**is** termed the **"reference** phase.*

(b) For the Doppler VOR, the phase of the 30 Hz component of the FM subcarrier varies with azimuth. It is **termed** the *variable phase."

(2) <u>Subcarrier Frequency and Accuracy</u>. The subcarrier modulation **mid-frequency** shall be **9,960** Hz **within** + **1.0** percent, and shall carry the 30 Hz frequency modulation.

(3) <u>Subcarrier Modulation Frequency and Accuracy</u>. The modulation frequency shall be 30 Hz within <u>+</u> 1.0 percent.

(4) <u>Subcarrier Amplitude Modulation</u>. Amplitude modulation of the subcarrier shall conform to the following.

(a) For the conventional VOR, the percentage of amplitude modulation of the 9,960 Hz subcarrier shall not exceed **5** percent.

(b) For the Single **Sideband** Doppler VOR, the percentage of amplitude modulation of the 9,960 Hz subcarrier shall not exceed 40 percent when measured at a point at least 1000 feet from the VOR. **When** Double Sideband Doppler VOR **is** installed, this **modulation**, for each sideband, shall not exceed **50** percent.

(5) <u>Sideband Level Subcarrier Harmonics</u>. When **50 kHz** channel assignments are made, the sideband level of the harmonics of the 9,960 Hz component in the radiated signal shall not exceed the following levels referenced to the level of the 9,960 Hz sideband.

Subcarrier	Level
9,960 Hz 2nd harmonic 3rd harmonic 4th harmonic and subsequent harmonics	Ø dB reference - 30 dB - 5Ø dB - 60 dB

55. <u>30 Hz AMPLITUDE MODULATION</u>. The other signal component shall be 30 Hz **ampl**itude modulation as follows.

a. For the conventional VOR, this component results from a rotating field patters, the phase of which varies with azimuth. It is termed the "variable phase" and is of constant amplitude.

b. For the Doppler VOR, this component of constant phase with relation to azimuth, is radiated omnidirectionally. It is termed the "reference phase" and Is of constant amplitude.

56. AMPLITUDE MODULATION FREQUENCY AND ACCURACY. The modulation frequency shall be 30 Hz within + 1.0 percent.

57. <u>DEPTH OF REFERENCE AND VARIABLE PHASE MODULATIONS</u>. The depth of **modulation of** the **radiofrequency carrier due to** the **30** Hz or 9,960 Hz signals shall be within the following limits for **each** signal.

 $28\ {\rm to}\ 32\ {\rm percent}\ {\rm at}\ {\rm all}\ {\rm elevation}\ {\rm angles}\ {\rm from}\ {\rm \emptyset}\ {\rm to}\ 5\ {\rm degrees}\ {\rm above}\ {\rm the}\ {\rm h\&iron;}\ {\rm and}$

b. 25 to 35 percent at all elevation angles between 5 and ${\bf 60}$ degrees above the horizon.

58. PHASE RELATIONSHIPS OF REFERENCE AND VARIABLE PHASE SIGNALS. The fundamental of the reference and variable **phase** modulations **shall** be in phase along the radial corresponding to magnetic north.

NOTE: The reference and variable phase modulations are in phase when the maximum value of the sum of the radio frequency carrier and the sideband energy due to the amplitude modulation signal occurs at the same time as the highest frequency of the frequency modulation signal.

59. C<u>ODE IDENTIFICATION SIGNAL CHARACTERISTICS</u>. The characteristics of the code identification signal shall conform to the following.

a. Tone Modulation Frequency and Accuracy. The modulation frequency shall be $1,020 \pm 50$ Hz.

b. <u>Depth of Modulation</u>. The depth to which the radio frequency carrier **is** modulated by the code identification signal shall be:

(1) 5.0 \pm 1 percent where voice services are provided.

(2) 4 to 10 percent at components where voice services are not provided.

60. <u>VOICE IDENTIFICATION AND COMMUNICATIONS SIGNAL CHARACTERISTICS</u>. The characteristics of voice identification and voice communications **signals**, when provided, shall conform to the following.

a. Voice Channel Frequency Response. Throughout the frequency range from 300 to 2 200 Hz, the frequency response characteristics for the voice channel shall'be within 3 dB of the response at 1,000 Hz.

b. Depth of Modulation. The depth to which the radio frequency carrier is modulated by voice **signals** shall not be greater than 30 ± 2 percent.

61. <u>MONITORING</u>. The radiated signal shall be monitored and removed from **service** upon **recognition** of unsafe operation.

62.-79. R<u>ESERVED</u>.

SECTION 2. OPERATIONAL CHARACTERISTICS FOR VOR AIRBORNE COMPONENTS

80. INTRODUCTION. This section specifies functional capability and performance characteristics required of VOR airborne components. The term "component" describes the complete aircraft installation. This includes the antenna and its transmission line, the receiver, electrical power source(s), identification and voice **communications** signal reproduction devices, and selector and display instrumentation devices for bearing and course indication. Airborne components used in the performance of aircraft operations under IFR must meet all requirements. For other aircraft operations the requirements are limited to those of paragraphs 80 and 90. Components should be capable of performing as specified throughout the operational service volume of ground stations. The applicable performance requirements should be met when the ground stations are operating in accordance with this standard.

81. <u>RECEIVER STABILITY</u>. For each channel in use, the receiver's center frequency shall be in accordance with Appendix 3. The receiver stability shall be \pm 0.005 percent or better.

82. <u>RECEIVER SENSITIVITY</u>. Based on the signal power density of paragraph 53, the airborne component shall provide the sensitivity necessary to display navigation information to the accuracy specified. Clear and distinct reproduction of communications and identification signals shall be provided. (See also Appendix 1.)

83. <u>REJECTION OF UNDESIRED SIGNALS</u>. The airborne component shall provide undesired signal rejection characteristics adequate to assure the specified performance. For co-channel and adjacent-channel ILS and VOR signals, the D/U ratios of paragraph 29.a shall apply.

84. MISTUNING PROTECTION. Mistuning by 50 **kHz** may result in erroneous information not readily apparent to the user if no VOR carrier is present on the tuned channel. Provision shall be made to protect against mistuning an airborne receiver by operational, mechanical, or electronic means.

85. FACILITY IDENTIFICATION AND VOICE SIGNALS. The airborne component shall provide the pilot with positive **identification** of the ground component.

86. BEARING AND COURSE DEVIATION INFORMATION. The airborne component shall provide devices for unambiguous determination of the aircraft magnetic bearing with respect to the selected ground component. This display shall show the aircraft deviation from the selected course.

87. <u>COURSE DEVIATION DISPLAYS</u>. The response, readability, and resolution of course deviation displays shall enable the pilot to determine the direction and extent of the aircraft deviation from the selected course.

88. <u>WARNING FUNCTION</u>. The airborne component shall provide a warning indication whenever the azimuth signals necessary for the prescribed performance are not present. This warning shall be clearly evident to the pilot.

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89. ACCURACY OF BEARING ANØ COURSE DEVIATION INFORMATION. The total airborne component error, in Dearing and Clurse deviation information as displayed to the pilot, shall not exceed \pm 3.0 degrees (95 percent probability) at any bearing.

90. <u>RADIATION</u>. Radiation from airborne components shall not result in derogation of operational use to other system users or in the derogation of other aeronautical services.

91.-109. <u>RESERVED.</u>

CHAPTER 4. DME AND TACAN SYSTEMS

SECTION 1. OPERATIONAL CHARACTERISTICS FOR DME AND TACAN GROUND COMPONENTS

110. <u>INTRODUCTION</u>. This section identifies standard signal and performance characteristics for DME and TACAN ground components. These characteristics represent the performance which shall be provided throughout the operational service volumes defined in paragraph **23.c.** Requirements apply to both DME and TACAN components, unless noted otherwise.

111. <u>POLARIZATION</u>. The ground component antenna shall radiate and receive a vertically polarized signal. Any horizontally polarized signal components shall be at least 26 **dB** weaker than the vertically polarized component.

112. TRANSPONDER RESPONSE TO INTERROGATION SIGNALS. The response of the **transponder** to interrogation signals shall conform to paragraphs 113 through **120.**

NOTE: At the ground component antenna, the presence of CW signals within <u>*</u> 3.0 MHz of the nominal value of the interrogation frequency at a signal power density of -113 **dBW/m²** or more, will normally derogate the performance of the system. Steps should be taken to avoid this situation.

113. <u>INTERROGATION RADIO FREQUENCY</u>. For each channel in use, the center frequency of the transponder's interrogation and reply frequencies shall be in accordance with Appendix 3.

- 114. SENSITIVITY TO INTERROGATION SIGNALS. Transponder sensitivity is specified as that minimum value of peak pulse power **density** (prior to intercept by the ground component antenna) which will result in a transponder reply efficiency of 70 percent. (See Appendix 1)
 - NOTE: Ground components may not respond to interrogations as specified if the difference in level of the constituent pulses of interrogation pulse pairs is greater than 1 dB.

115. <u>ON-CHANNEL SENSITIVITY</u>. For interrogation signals within \pm 100 kHz of the assigned frequency, having a repetition rate no greater than 200 pulse pairs per second and pulse pair spacing of exactly 12.0 microseconds (36.0 micro econds for Y channel), DME sensitivity shall be not less than -101.5 dBW/3 . Under thq same conditions, the TACAN sensitivity shall be not less than -104.5 dBW/m .

NOTE: At 1150 MHz, the value -101.5 **dBW/m²** corresponds to -124.0 **dBW** at the output of a **lossless** isotropic receiving antenna. Similarly, the value -104.5 **dBW/m²** corresponds to -127.0 **dBW.** (See Appendix 1) 116. SENSITIVITY AT OTHER PULSE SPACINGS. When the spacing of the constituent pulses of interrogation pulse pairs differs from the design center value (12.0 microseconds for X channel; 36.0 microseconds for Y channel) by \pm 0.5 microseconds or less, the sensitivity of paragraph 115 shall not be reduced by more than 1 dB. When the spacing differs by \pm 3 microseconds and more from nominal, the reduction in sensitivity shall be at least 70 dB with respect to the level of paragraph 115.

117. VARIATION OF SENSITIVITY WITH INTERROGATION LOADING. When the beacon is loaded with 3175 additional pulse pairs per second at a level of -65 **dBm** (referenced at the input to the transponder receiver with the transponder's echo suppression circuits disabled), the sensitivity of the receiver shall not be reduced by more than 1 **dB** from the value measured in paragraph 115.

118. <u>SENSITIVITY TO ADJACENT CHANNEL INTERROGATIONS</u>. Interrogation signals removed 900 kHz or more from the assigned channel interrogation frequency and having an amplitude up to 80 **dB** above the on-channel sensitivity of the component shall not elicit a reply from that component.

119. <u>TRANSPONDER DEAD TIME</u>. Dead time is the time **immediately** following an accepted interrogation decode for reply processing, during which succeeding interrogations receive no reply. The transponder dead time shall normally be 60 microseconds for X channels (72 microseconds for Y channels).

120. <u>ECHO SUPPRESSION DEAD TIME</u>. The retriggerable blanking gate (RTBG) (see paragraph 145.b) is typically set such that the effective dead time is a nominal 150 microseconds. When required for a particular site, the effective dead time may be increased up to a nominal 250 microseconds.

121. <u>TRANSPONDER OUTPUT SIGNAL CHARACTERISTICS</u>. The transponder shall conform to paragraphs 122 through 150.

122. <u>FREQUENCY STABILITY</u>. For each channel in use, the center frequencies of the ground station's transmitter and receiver shall be in accordance with Appendix 3. Frequency stability shall be ± 0.001 percent or better for equipments purchased after July 1980. The stability of older ground stations shall be ± 0.002 percent or better.

NOTE: Stabilities of older equipment need not be increased to ± 0.001 percent.

123. <u>SIGNAL STRENGTH IN SPACE</u>. Within that part of the operational service volume that is above 18,000 feet (5,486 m) AGL, a minimum signal power density of -91.5 **dBW/m²** (95 percent time availability) shall be provided. Within that part of the operational service volume that is below 18,000 feet (5,486 m) AGL, a minimum signal power density of -86.0 **dBW/m²** shall be provided. Signal power shall be determined by the average over one second of the equivalent peak pulse voltage waveform. At the nearest aircraft position expected **during** operations, the maximum signal power density expected during flight will be on the order of -17.0 **dBW/m²**.

NOTE: At 1213 MHz, the value -91.5 dBW/m² corresponds to -114.5 dBW at the output of a logsless isotropic receiving antenna. Similarly, -86.0 dBW/m² corresponds to -109.0 dBW. The apparent change in numbers from the old standard does not represent a change in beacon radiated power (for example, see Appendix 1). Therefore, increases in receiver sensitivities of existing airborne equipments are not required to achieve the same service ranges that users have experienced in the past. Future designs should not be restricted by this fact.

124. RADIO SPECTRUM. The spectrum of the pulse modulated signal shall be as follows.

a. The equivalent isotropic radiated power (EIRP) contained in a Ø.5 MHz band **centered** on a frequency either Ø.8 MHz above or Ø.8 MHz below the nominal channel frequency shall (in both instances) not exceed 200 milliwatts (except that the power relative to center frequency shall not exceed -50 dB).

b. The EIRP contained in a $\emptyset.5$ **MHz** band centered on a frequency either 2. \emptyset MHz above or 2. \emptyset MHz below the nominal channel frequency shall (in both instances) not exceed 2 milliwatts (except that the power relative to center frequency shall not exceed -7 \emptyset **dB**).

c. Each lobe of the spectrum will be generally of lesser amplitude than the adjacent lobe nearer the nominal channel frequency.

125. <u>SPURIOUS RADIATION</u>. The RF output level, during the interval between occurrence of the desired pulse pairs, shall not exceed a level which is 80 **dB** below the maximum power level during a pulse. In addition, between the pulses of each pair there shall be an interval for 1.0 microsecond or greater in length during which the RF output level does not exceed a level which is 50 **dB** below the maximum power level of the weaker pulse of the pair.

126. PULSE SHAPE. The following, as limited by the requirements of paragraphs 124 and 125, shall apply to all radiated pulses.

a. <u>Pulse Rise Time</u>. The time required for the pulse to rise from 10 to 90 percent of its maximum voltage amplitude shall not be less than 0.1 microsecond nor more than 3.0 microseconds.

b. <u>Pulse Top</u>. Between the points on the **leading** and trailing edges which are 95 percent of the maximum voltage amplitude, the instantaneous amplitude of the pulse shall not fall below a value which is 95 percent of the maximum voltage amplitude of the pulse.

c. <u>Pulse Duration</u>. The pulse duration, as measured at the 5Ø percent maximum voltage amplitude points, shall be 3.5 ± Ø.5 microseconds.

d. <u>Pulse Decay Time</u>. The pulse decay time, from the 90 percent point to the 10 percent point of the maximum voltage amplitude, shall be such that the remaining requirements of this standard shall be satisfied.

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127. <u>PULSE COOING</u>. Transponder output signals shall consist of paired pulses. Ine spacing of the pulses is measured between the 50 percent maximum voltage amplitude points on the leading edge of each RF **pulse**. The pulse spacing shall be:

a. $12.0 \stackrel{\bullet}{=} 0.25$ microseconds for X channels; or

b. 30.0 ± 3.25 microseconds for Y channels.

128. <u>PULSE POWER VARIATION</u>. The peak power of the constituent pulses of any pair shall not differ by more than 1 **dB**.

129. <u>DISTANCE REPLY SIGNALS</u>. Distance reply signals, consisting of pulse pairs, are transmitted in response to interrogations.

130. <u>REPLY EFFICIENCY</u>. Reply efficiency is defined as the percentage of interrogations from a specific interrogator to which the transponder replies within a given time interval when the transponder is under specified load conditions. The reply efficiency for interrogation signals at and above the minimum sensitivity levels of paragraph 114 shall be at least 70 percent for all interrogation loadings up to the maximum for which the transponder is designed (3375 interrogations per second).

NOTE: To provide service under adverse echo conditions or to handle increased traffic, it may be necessary to reduce the reply efficiency. To be able to receive the same service during traffic overload conditions, airborne receivers should be capable of operating properly with reply efficiencies at least as low as 50 percent.

131. <u>REPLY DELAY TIME</u>. Reply delay time is defined as the time of all delay introduced by the ground component in replying to **interrogations**. When airborne components are to indicate distance with respect to the transponder site, the zero-distance reply delay time shall be 50.0 microseconds ± 0.25 microseconds for X channels (56.0 microseconds ± 0.25 microseconds for Y channels). This represents the time between the 50 percent voltage point on the leading edge of the first pulse of the interrogation pulse pair and the corresponding point on the first pulse of the reply pulse pair.

> NOTE: In older facilities, the reply delay time is referenced to the second pulse of interrogation and reply pulse pairs. The nominal value of reply delay time in these instances is 50 microseconds for both X and Y channels.

132. <u>RANDOM PULSE PAIR SIGNALS</u>. In addition to distance reply pairs, the ground component shall radiate random pulse pairs, defined as squitter, in **order to** maintain a total pulse pair rate in accordance with paragraphs 133 and 134.

133. <u>DME COMPONENTS</u>. For DME ground components, the total pulse rate, **exclusive** of identification pulses, shall be within the range of 700 up to 2850 pulse pairs per second, in the absence of high traffic density. 134. TACAN COMPONENTS. For TACAN ground components, the total pulse pair rate, exclusive of code identification signal and reference burst pulses, shall be 2700 ± 90 pulse pairs per second, in the absence of high traffic **density**. For a transponder dead time of 60 microseconds (for X channels), the distribution of random pulse pairs shall conform to Figure 4-1.

135. <u>PULSE PAIR RATE</u>. To provide greater traffic handling capacity (than the total output pulse pair rates of paragraph 133 and 134), the equipment shall have the capability to increase to as high as 5000 ± 150 pulse pairs per second as a function of actual traffic loading. Under this condition it will be impossible to maintain the output pulse pair spacing distribution of Figure 4-1. Accordingly, new TACAN airborne equipment design should avoid the use of circuits in which azimuth **indication** is sensitive to transponder output pulse count and spacing distribution. (See paragraph 130.)

136. <u>GROUND COMPONENT RANGE ACCURACY</u>. The ground component shall not contribute more than Ø.1 nmi (185 m) to overall system error.

137. <u>CODE IDENTIFICATION SIGNAL CHARACTERISTICS</u>. Subject to the provisions of paragraph 137.a, code identification signals shall consist of groups of two pulse pairs transmitted for the duration of dots and dashes in accordance with paragraph 30.a. The spacing between the first and second pulse pairs constituting each pulse **group**, as measured between the 50 percent voltage amplitude points on the leading edge of the first pulse of each pair, shall be 100 ± 10 microseconds. The repetition rate shall conform to the following.

a. <u>DME Components</u>. For ground components providing DME service only, the identification signamay consist of either one or two pulse pairs In a group. The group repetition rate shall be 1350 - 10 groups per second.

b. TACAN Components. For TACAN ground components, the repetition rate shall be 1350 groups per second (\pm 0.23 percent) which is phase-locked within ± 50.0 microseconds of the tenth harmonic of the 135 Hz bearing reference signal. The first pulse of each **identification** signal pulse group shall occur 740 \pm 50 microseconds after the first pulse of any 40 degree sector reference signals.

138. TACAN AZIMUTH SIGNAL CHARACTERISTICS. TACAN azimuth signals consist of North (main or coarse) and 40 degree sector (auxlliary or fine) bearing reference signals and 15 Hz (coarse) and 135 Hz (fine) amplitude modulation variable bearing signals. The azimuth signals radiated by the antenna shall conform to the following.

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139. <u>BEARING REFERENCE SIGNALS</u>. Transmission of the North and 40 degree sector **bearing** reference **signal**s shall occur synchronously with antenna pattern **rotation**. For each rotation of the antenna pattern, one North reference signal shall be transmitted. Following the North reference signal at each of eight consecutive angular increments of 40 degrees, the 40 degree sector reference signal shall be transmitted. A ninth 40 degree sector reference signal, which otherwise would coincide in time with the North reference signal, shall not be transmitted. The characteristics of reference signals shall be as follows.

a. North Reference Signal.

(1) For X channels, the North reference signal shall consist of a group of 12 pulse pairs. Spacing between the two pulses of a pair shall be 12 ± 0.25 microseconds. Spacing between the first pulse of each pulse pair shall be 30.0 ± 0.3 microseconds. Spacings are measured at the 50 percent voltage amplitude points on the leading edges of the pulses.

(2) For Y channels, the North reference signal shall consist of a group of 13 single pulses. Spacing between the pulses shall be $3\emptyset.\emptyset \stackrel{+}{=} \emptyset.3$ microseconds. Spacings are measured at the **50** percent voltage amplitude points on the leading edges of the pulses.

b. 40 Degree Sector Reference Signals.

(1) For X channels, the 40 degree sector reference signal shall consist of a group of 6 pulse pairs. Spacing between the two pulses of a pair shall be 12 \pm 0.25 microseconds. Spacing between the first pulse of each pulse pair shall be 24.0 \pm 0.25 microseconds. Spacings are measured at the 50 percent voltage amplitude points on the leading edges of the pulses.

(2) For Y channels, the 4Ø degree sector reference **signal** shall consist of a group of 13 single pulses having a spacing of 15.℃ - Ø.25 microseconds. Spacings are measured at the 5Ø percent voltage amplitude points on the leading edges of the pulses.

140. VARIABLE BEARING SIGNALS. The variable bearing signals shall be produced by a rotating directional antenna pattern which results in a composite amplitude modulation of the transponder radio frequency **pulse** signals at 15 and 135 Hz. The characteristics of the variable bearing signals shall be as follows.

a. <u>Amplitude Modulation Frequencies and Accuracy</u>. The amplitude modulation frequencies shall nominally be 15.0 and 135.0 Hr. Each frequency shall vary from the nominal values in exact **synchronism** with an antenna pattern rotation rate of 900 (± 0.23 percent) rotations per minute.

b. Depth of Modulation. At all elevation angles from -2 to +40 degrees relative to the horizon, the individual modulation components shall be 21 \pm 9 percent. At all elevation angles from -2 to 50 degrees, the sum of the 15 and 135 Hz modulation components including the harmonics shall not exceed 55 percent. Further, within the angles from -2 to +2 degrees relative to the horizon, the maximum variation in depth of modulation for the 15 and 135 Hz components shall not, for each frequency, vary more than \pm 4 percent from the respective median values within the angles specified.

141. <u>RELATIONSHIPS OF REFERENCE AND VARIABLE BEARING SIGNALS</u>. On the magnetic North radial from the antenna, the relationships **of** the **reference** and variable signals shall conform to the following.

a. <u>Coarse Bearing Signal</u>. The inflection point on the negative slope of the 15 Hz amplitude modulation component shall coincide within $_$ 2.Ø azimuth degrees of the 5Ø percent amplitude points on the leading edge of:

(1) the tenth pulse of the North reference signals for X channels; or

(2) the sixth pulse of the North reference signal for Y channels.

b. Fine Bearing Signals. The inflection point on the negative slope of the 135 Hz amplitude modulation component shall coincide within ± 0.33 degrees azimuth of the average position of the 50 percent amplitude **point** on the leading edge of:

(1) the twelfth pulse of the 40 degree sector reference signal for X channels; or

(2) the eleventh pulse of the 4Ø degree sector reference signal for Y channels.

142. <u>PRECEDENCE OF PULSE TRANSMISSIONS</u>. The order of precedence for transmission of transponder pulse signals shall be in accordance with the following.

a. <u>DME Components</u>. For ground components **providing** DME service only, the **precedence sha**ll be:

(1) International Morse Code Identification Signals

- (2) Distance Reply Signals
- (3) Random Pulse **Pair** Signals

Neither distance reply nor random pulse pair signals shall be transmitted during the "key-down" Interval of International Morse Code identification signal transmission.

- b. TACAN Components. For TACAN components, the precedence shall be:
 - (1) Bearing Reference Signals
 - (2) International Morse Code Identification Signals
 - (3) Distance Reply Signals
 - (4) Random Pulse Signals

Neither code identification, distance reply, nor random pulse pair signals shall be transmitted during the interval required for transmission of all pulses in each bearing reference signal. Distance reply and random pulse pair signals shall not be transmitted during the **"key-down"** interval of code identification signal transmissions.

143. <u>REJECTION OF UNDESIRED SIGNALS</u>. The ground component shall provide **undesired signal rejection** characteristics adequate to assure the specified perfonance. This includes co-channel and adjacent-channel DME/TACAN signals.

144. <u>RECEIVER DECODER</u>. The decoder shall decode and produce an output pulse from interrogation signal pulse pairs occurring at spacings **within** the range **of**:

a. 12 \pm Ø.5 microseconds for X channels, or

b. 36 \pm Ø.5 microseconds for Y channels.

145. <u>ECHO SUPPRESSION</u>. Echo suppressions shall be provided in accordance with the following subparagraphs.

a. <u>Short Distance Echoes</u>. Synchronous pulse signals occurring between the **constituent** pulses of a **direct** path interrogation pulse pair and which are also superimposed on the leading or **trailing** edge of the second pulse of the **direct** path pulse pair, shall not affect the time of decoding of the direct pulse pair by an amount in excess of Ø.15 microseconds. Neither shall the reply efficiency be reduced by more than 10 percentage points from that measured in the absence of the echo pulse. These requirements shall be met when the RF Input signal level of the direct path pulse pair has any level from 10 **dB** above threshold triggering level to an absolute level of **-10 dBm** and the echo pulse has any level up to the level of the **direct** pulse pair and for all direct pulse pair spacings of paragraph 175. b. Long Distance Echoes. A separate echo suppression (Retriggerable Blanking Gate (RTBG)) circuit shall be provided in order to prevent the generation of multiple replies to aircraft interrogations having echoes which are delayed with respect to the direct path signal in excess of receiver dead time setting. The echo suppression circuit shall be triggered by the decoding of the direct signal pulse pair only when the level of the pulses exceeds a pre-established level. Such triggering shall result in the generation of a receiver desensitizing pulse starting at the time of pulse decoding nominally adjusted to 150 ± 10.0 microseconds with an upper limit of 300 microseconds. The degree of receiver desensitization shall be to a level 3.0 dB above the level of the direct path signal and shall hold over the entire duration of the echo suppression pulse, unless retriggered by a signal stronger by \emptyset to 6 dB than the direct path signal, and over a range of input signals from 10 dB above threshold triggering level to -15 dBm. The echo suppression circuit pre-established level will nominally be -70 dBm.

146. <u>DECODER DISCRIMINATION</u>. The decoder shall provide a minimum of 7Ø dB rejection to:

a. paired pulses whose spacing differs by 3.0 microseconds or more from the **nominal** value given in paragraph 144,

b. paired pulses with spacings within the range of paragraph 144 where either pulse has a width of Ø.8 microsecond or less, and

c. single pulses of any width including widths within the range of pulse spacings of paragraph 144.

147. <u>RECEIVER RECOVERY TIME</u>. The recovery time of the receiver and its associated video circuitry shall be such that the sensitivity to desired interrogations is not reduced by more than 1 **dB** when desired interrogations occur 8.0 microseconds and more after the reception of undesired pulses of any width having levels up to 60 **dB** above the sensitivity of the receiver in the absence of such undesired pulses. The desired interrogations shall be RF pulse pairs conforming to the characteristics specified in paragraphs 173 through 179. Undesired pulses shall conform to the same requirements except that the pulse spacing shall be outside the limits of paragraph 175.

148. DESENSITIZATION BY CW. The presence of CW interference signals on the assigned channel frequency or elsewhere within the receiver pass-band shall not reduce the on-channel sensitivity by more than 2 **dB** from the value measured in the absence of CW interference provided that the level of the interference is no higher than 10 **dB** below the level of the desired on-channel signal. Additionally, the reply efficiency to a single aircraft interrogation shall not be reduced by more than 10 percent when the level of the interfering CW signal. The CW sensing circuit shall not reduce the receiver gain by more than 1 **dB** when pulses 8.0 microseconds wide or wider are received at a rate of 37,000 per second at a level 10 **dB** below receiver sensitivity. (This is to preclude premature receiver desensitization, if the receiver is exposed to a high Pulse Repetition Frequency (PRF) pulse multiplexed signal.)

149. <u>MONITORING</u>. The radiated signals shall be monitored and removed from service upon recognition of unsafe operations.

150.-169. R<u>ESERVED</u>.

SECTION 2. OPERATIONAL CHARACTERISTICS FOR DME AND TACAN AIRBORNE COMPONENTS

170. <u>INTRODUCTION</u>. This section specifies functional capability and performance characteristics required of DME and TACAN airborne components. The term "component" as used In this order, includes the complete aircraft installation. This includes such items as the antenna and its transmission line, the interrogator, the electrical power source(s), identification signal reproduction or display devices, and the distance indicator; when applicable, it also includes select and display instrumentation devices for bearing and course indication. Airborne components used in the performance of aircraft operations under IFR must meet all requirements. For other **aircraft** operations the requirements are limited to paragraphs 170, 175, 176, 179 and 180. Requirements apply to both DME and TACAN components unless otherwise noted. Components should be capable of performing as specified throughout the operational service volume of ground stations. The applicable performance requirements should be met when the ground stations are operating in accordance with this standard.

171. INTERROGATOR SIGNAL CHARACTERISTICS. Paragraphs 172 through 180 identify interrogation signal characteristics and tolerances applicable to the radiated signal.

172. INTERROGATION RADIO FREQUENCIES AND ACCURACY. The Interrogator shall transmit on the appropriate frequency in accordance with Appendix 3. The center frequency of the interrogation shall be within \pm 100 kHz of the channel frequency.

173. PULSE CHARACTERISTICS. The radio frequency pulse envelope shall have characteristics as **follows**.

a. <u>Pulse Rise Time</u>. The time required for the pulse to rise from 10 to 90 percent of its maximum voltage amplitude shall nominally be 2.5 microseconds. It shall not exceed 3.0 microseconds. The minimum rise time is governed by the spectrum requirements of paragraph 179.

b. <u>Pulse Top</u>. Between the points on the leading and trailing edges which are 95 percent of the maximum voltage amplitude, the instantaneous amplitude of the pulse shall not fall below a value which is 95 percent of the maximum voltage amplitude of the pulse.

c. <u>Pulse Duration</u>. The pulse duration, as measured at the 50 percent maximum voltage **amplitude** points, shall be 3.5 ± 0.5 microseconds.

Chap 4 Par 149 d. <u>Pulse Decay Time</u>. The time required for the pulse to fall from 90 to 10 percent of the maximum voltage amplitude shall nominally be 2.5 microseconds. It shall not exceed 3.5 microseconds. The minimum decay time is governed by the spectrum requirements of paragraph 179.

174. PULSE POWER VARIATION. The peak power of the constituent pulses of any pair shall not differ by more than 1 dB.

Note: If the difference in level of the constituent pulses of interrogation pulse pairs is greater than 1.0 **dB**, ground components may not respond to interrogations.

175. <u>PULSE CODING</u>. Interrogation signals shall consist of **paired** pulses. Spacings are measured at the 50 percent voltage amplitude points on the pulse rise **time** of each pulse. The pulse spacing shall be:

- a. 12.0 ± 0.5 microseconds for X channels; or
- b. 36.0 ± 0.5 microseconds for Y channels.

176. <u>INTERROGATION SIGNAL REPETITION RATE</u>. The average interrogator pulse pair repetition rate shall not exceed 30 pairs of pulses per second. This assumes that interrogators are tracking at least 95 percent of the time. The repetition rate may be increased during search, but it shall not exceed 150 pulse pairs per second.

177. <u>VARIATION OF REPETITION RATE</u>. The variation in time between successive interrogations shall be sufficient to preclude mistaking distance reply pulses . intended for another airborne component tuned to the same ground facility. It shall also preclude capture of the interrogations of one interrogator within the ground component dead time caused by the Interrogations of other avionics.

178. SIGNAL STRENGTH IN SPACE.

a. When referenced to a point in space prior to the ground station antenna intercept, the airborne component of aircraft operating above 18,000 feet (,486 m) AGL shall provide a minimum signal power density of -102.5 dBW/m² (95 percent time availability). For aircraft operating below 18,000 (5,486 m) AGL, the minimum signal power density shall be -99.0 dBW/m².

b. These specified power densities will assure a minimum reply efficiency of 70 percent when:

(1) the pulse frequency is within \pm 100 kHz of the assigned center frequency;

(2) the pulse spacing is within \pm Ø.5 microseconds of nominal design center; and

(3) the beacon loading is 3375 pulse pairs per second with the echo suppression circuits disabled.

c. For the various operational service volumes currently employed in the ATC environment, the interrogator's EIRP shall be a minimum of +29.0 dBW for those aircraft operating above 18,000 feet (5,486 m) AGL and +19.0 dBW for those operating below 18,000 feet (5,486 m) AGL. These EIRP's will provide to the ground beacon the power densities necessary for satisfactory performance. Since EIRP levels greater than +33.0 dBW may impair system performance, the interrogator's EIRP shall not exceed this value. (See Appendix 1)

179. RADIO SPECTRUM. The spectrum of the RF interrogation signal shall be such that at least 90 percent of the energy, including FM components, in each pulse shall be within **a** 0.5 MHz band centered on the nominal channel frequency.

180. <u>RADIATION</u>. Radiation from airborne components shall not result in derogation of the operational use of this system by other users or in the derogation of other aeronautical services. Neither shall other users derogate the operational use of this system by valid **DME** or TACAN users. At all frequencies between 960 and 1215 **MHz**, the level of radiated CW signals, as referenced to an isotropic radiator, shall not exceed -60 **dBW**.

181. <u>COMPONENT FUNCTIONAL CAPABILITIES AND PERFORMANCE</u>. These subparagraphs identify functional and operational performance requirements applicable to the airborne component.

182. <u>RECEIVER RADIO FREQUENCIES</u>. For each channel in use, the receiver's center frequency shall be in accordance with Appendix 3.

183. <u>RECEIVER SENSITIVITY</u>. Based on the signal power density of paragraph 123, the airborne components shall provide the sensitivity necessary to acquire and display navigation information to the accuracy specified. Clear and distinct reproduction of identification signals shall be provided. (See Appendix 1)

184. <u>REJECTION OF UNDESIRED SIGNALS</u>. The airborne component shall provide undesired signal rejection characteristics adequate to assure the specified performance. For co-channel and adjacent channel DME and TACAN signals, this requirement shall be met when the respective signals provide desired to undesired (D/U) signal ratios up to the maximum values stated in paragraph 29.b. At these D/U ratios, a positive identification signal shall be provided to identify the ground component.

185. DISTANCE INFORMATION. The airborne component shall measure and display the slant range distance (in nautical miles) between the aircraft and the selected ground component.

Note: The airborne component should not be capable of displaying excessive distances. Distances should be considered excessive for a given receiver if that receiver cannot reasonably be expected to operate at that distance.

186. WARNING FUNCTION, DISTANCE. The airborne component shall provide a warning indication whenever the airborne component is neither tracking a distance reply signal nor operating from memory (see paragraph 188). This warning shall be clearly evident to the pilot.

187. <u>ACCURACY OF DISTANCE INFORMATION</u>. When the airborne component error is combined by root-sum-square with a ground component error of Ø.1 nmi (185 m), the total error in slant range distance information, as displayed to the pilot, shall not (except during memory per paragraph 188) exceed Ø.5 nmi (926 m) or 3 percent of the actual distance, whichever is greater (95 percent probability).

188. MEMORY FUNCTIONS. The airborne component shall provide a memory function which, upon loss of a suitable reply signal while tracking, will cause the **display of** distance information to continue for a period not to exceed 15 seconds. The minimum distance memory shall be sufficient to cover the loss of distance reply signals during transmission of the ground component identification signal. The distance displayed during memory shall be within

1.0 nmi (1852 m) of the indication upon resumption of the tracking function.

189. TACAN BEARING AND COURSE DEVIATION INFORMATION. The airborne component shall provide devices for unambiguous determination of the aircraft magnetic bearing with respect to each selected ground component and for display of the aircraft deviation from the selected course.

190. <u>COURSE DEVIATION DISPLAYS</u>. The response, readability, and resolution of course deviation displays **shall** permit the pilot to determine the direction and extent of the aircraft deviation from the selected course.

191. WARNING FUNCTION, BEARING. The airborne component shall provide a warning **indication** whenever the azimuth signals are not present and when the component is not operating in memory. This warning shall be clearly evident to the pilot.

192. <u>ACCURACY OF BEARING AND COURSE DEVIATION INFORMATION</u>. At any bearing, the total airborne component error in bearing and course deviation information shall not exceed [▲] 3.Ø degrees (95 percent probability) as displayed to the pilot.

193.-209. R<u>ESERVED</u>.

9840**.1** Appendix 1

APPENDIX 1. COVERAGE.

RADIO PROPAGATION. Propagation losses vary as a function of time. For 1. a given EIRP, the correct density at a point in space will fluctuate. In addition, propagation loss will vary from site to site. This variation is a function of several factors including atmospheric refractivity, surface reflectivity, wave polarization, etc. Since the **VOR/DME/TACAN** system is a safety service, signals must be highly reliable. With this in mind, conservative assumptions have been made for the inputs to the propagation model. Figures 2 through 13 show standard VOR, DME, and TACAN signal strengths (95 percent time availability) at various points in space. A time availability of 95 percent means that, at a given point in space, the instantaneous signal strength will be greater than or equal to the value shown 95 percent of the time. Although propagation losses will differ from site to site, the signal strength curves of this appendix are recommended for purposes of standardization. It is important to remember that for the distance function of DME and TACAN both the ground-to-air and air-to-ground transmissions must be considered.

2. <u>GROUND STATION</u>. The **EIRP's** and resultant signal strength in space curves **g**iven in Figures 2 through 13 are nominal. Allowances should be made for different **EIRP's** and for other variations in station characteristics. Some ground stations may have higher cable losses (e.g., mountain top installations sometimes require longer cable runs). In addition, intervening terrain may increase the transmission path loss. Should this occur, it may be necessary to reduce the service volume accordingly.

3. <u>VOR COVERAGE</u>.

a. The power density specified in paragraph 53 (-120 **dBW/m²**) is equivalent to -123 **dBW** power available at the output of a **lossless** isotropic antenna (at 118 MHz). Allowance must be made for the airborne antenna and for cable and insertion losses. Users will balance their airborne power budgets in different ways. Two examples are shown below.

	Example 1	Example 2
Power Available Airborne Antenna Gain* Airborne Losses Receiver Sensitivity	-123 dBW +2.2 dBi -2.2 dB -123 dBW	-123 dBW -1 dBi -4 dB

b. Many other examples could be given. It is the user's responsibility to insure that the airborne installation will allow proper operation at the minimum signal strength of paragraph 53. (In considerin airborne antenna gain, antenna pattern variation should not be neglected.3

*NOTE: Does not consider variations due to antenna locations or other factors which influence antenna gain due to shielding.

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4. DME/TACAN (UPLINK) COVERAGE

a. The power densities specified in paragraph 123 are referenced to the powers available at a point in space. Allowance must be made for the airborne antenna and for cable and insertion losses, Users will balance their airborne power budgets in different ways. Two examples of how users might balance their airborne power budgets for the DME and TACAN are shown as follows:

	Example 1		Example 2	
	DME (100W)	TACAN	DME (100W)	TACAN
Power Available Airborne Antenna Airborne Losses Rx Sensitivity	-109.0 Gain* +2.0 -3.0 -110.0	-114.5 dBW +2.0 dBi -3.0 dB -115.5 dBW	-109.0 + 0.5 -1.5 -110.0	-114.5 dBW +0.5 dBi -1.5 dB -115.5 dBW

b. Many other examples could be given. It is the user's responsibility to insure that the airborne installation will allow proper operation at the minimum signal strengths of paragraph 123. An airborne DME installation with 1 dB of loss (antenna pattern, cable and insertion losses, signal splitters, etc.) would require a sensitivity of -110.0 dBW. An airborne TACAN installation with 1 dB of loss would require a sensitivity of -115.5 dBW. When the total loss is different than 1 dB, a corresponding adjustment must be made to determine the required sensitivity. In considering airborne antenna gain, antenna pattern variation should not be neglected.

5. DME/TACAN (DOWNLINK) COVERAGE.

a. The minimum power density specified in paragraph 178 for the input to the ground station antenna is -99.0 dBW/m^2 for DME and -102.5 dBW/m^2 for TACAN. These power density values are necessary to generate a reply efficiency of 70 percent from the transponder during periods when the transponder is under heavy load and when the interrogation signal is within + 100 kHz of the nominal channel frequency and its pulse pair spacing is within +0.5 microseconds of the nominal system value. The association of interrogator signal strength and transponder sensitivity is as follows.

*Note: Does not consider variations due to antenna locations or other factors which influence antenna gain due to shielding.

OME

TACAN

1112	1746.740	
-94.Ø + 6.7	-97.0 dBm + 3.0 dB	 Transponder Sensitivity per paragraph 115 Net coupling to receiver per (1) +8.2 dBi DME Antenna Gain on horizon -1.5 dB Net Losses (cable and insertion) (2) t4.5 dBi TACAN Antenna Gain on horiron -1.5 dB Net Losses (cable and insertion)
-87.3	-94.Ø dBm	: Receiver input for 70 percent Efficiency per paragraph 115
+ 2.0	+ 2.Ø dB	: Sensitivity Reduction per paragraphs 116 and 117
-85.3	-92.Ø dBm	: Receiver Input for 70 percent efficiency

b. It is the user's responsibility to provide that signal strength to insure proper operation for those conditions stated in paragraph 178. For the requirement of 70 percent reply efficiency:

DME	TACAN	
-85.0	-92.Ø dBm	: Receiver Input per conditions of paragraph 178
- 6.7	- 3.Ø dB	: Net coupling per Antenna
-91.7	-95.Ø dBm	: Signal Strength at the antenna input
-99.2	-102.5 dBW/m ²	: Power Density at the antenna input
-99.Ø	-102.5 dBW/m ²	: Value used in paragraph 178

TIME AVAILABILITY. At a point in space, signal strength will vary with 6. time even when the ground transmitter's EIRP remains constant. A similar statement could be made for D/U signal ratios. This variation is largely due to propagation effects under different environmental conditions. Examples include atmospheric refractivity, seasonal changes in ground cover, and surface reflectivity. Numerous other factors are also involved. Although it is difficult to describe accurately all the variables involved, the situation can be adequately covered by statistical treatment. A helpful concept, in a statistical discussion of reliability, is **time** availability. It is that percentage of **time** that a given signal strength or D/U ratio is met or exceeded. Figure 1 shows an example of signal strength as a function of time availability. For a time **availab**ility of 95 percent, the sig**n**al strength is -120 **dBW/m²**. This means that a signal strength of -120 **dBW/m²** or greater is present 95 percent of the **time.** For a time availability of 50 percent, the signal strength is -117 dBW/m² at the same point in space assuming the same constant ground station characteristics. In a similar manner, the signal strength present for any given percentage of the time can be read from the graph. This graph does not, however, take transmitter downtime into account.



FIGURE 1. SIGNAL TIME AVAILABILITY

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FIGURE 3. TACAN (RTB-2) SIGNAL STRENGTH IN SPACE - LONG RANGE









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FIGURE 13. MONTEK DME SIGNAL STRENGTH IN SPACE - SHORT RANGE

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APPENDIX 2. SYSTEM ACCURACY.

1. <u>SYSTEM 4CCURACY</u>. The accuracies described and quantified below represent the normal error budget for a VOR/DME/TACAN system that includes basic avionics with analog indicators, a typical ground station, and an environment that does not include errors caused by excessive multipath. Margin for pilot induced flight technical error is also included. The error terms* are defined as follows.

2. BEARING ERROR COMPONENT DEFINITION.

a. <u>Radial Signal Error (Eg)</u>. Radial signal error is the difference between the nominal magnetic **bearing** to a point of measurement from the ground component and the bearing indicated by the ground component signal at the same point. The radial signal error **is** associated with the ground component and nominalsignal path errors but excludes other error factors. It is made up of the following.

(1) certain constant elements such as course displacement errors and most site and terrain effect errors which may be considered as fixed for long $\boldsymbol{\cdot}$. periods of time.

(2) certain' random variable errors which can be expected to vary about the essentially constant value.

b. <u>Airborne Component Error (Ea)</u>. Airborne component error is that error attributable to the inability of the airborne equipment to translate correctly the bearing information contained in the radial signal. This element embraces all factors in the airborne component which introduce errors in the information presented to the pilot. (Errors resulting from the use of compass information in some VOR and TACAN displays are not included.)

c. Instrumentation Error (Ei). This component consists of the limitation of the omni-bearing selector (OBS) units due to the resolution of the device and the inherent error of translating the pilot input to the avionic comparator. This comparator derives the difference between the actual radial computed and the selected radial which the pilot requires. This difference is normally displayed on a course deviation indicator (CDI) whose errors are considered a part of (Ea).

d. Flight Technical Error (Ef). Flight technical error refers to the accuracy with which the pilot controls the aircraft as measured by his success in causing the indicated aircraft position to match the indicated **command** for desired position. It does not include procedural blunders.

*Note: Quantitative values assume 95 percentile distribution.

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e. <u>Aggregate Error (Es)</u>. Aggregate error is the difference between the magnetic bearing to a point of measurement from the ground component and the bearing indicated by airborne components. This is the error in the information presented to the pilot (exclusive of any errors resulting from use of compass information). It takes into account not only the ground component and propagation path errors but also the error contributed by the airborne component and its instrumentation. The entire radial signal error, both fixed and variable, is used.

3. <u>ERROR COMBINATION</u>. Since the errors above, when considered on a total system basis (not any individual radials or components) are independent variables, they may be combined by the root-sum-square (RSS) method to calculate aggregate system error (Es) when the same probability is given to each element. For purposes of this standard, each element is considered to have 95 percent probability.

a. <u>Radial Signal Error (Eg)</u>. In practice, based on a significant number of accumulated data points, the radial signal error value (Eg) has been found to be +1.4 degrees (95 percent probability).

b. <u>Airborne Component Error (Ea)</u>. This component is strictly limited to those errors attributable to the avionics. In other words, this value excludes that which is due to the auto-couple of navigation deviation signals to aircraft controls and other output devices such as the omni-bearing selector (OBS), either in the manual or auto-couple mode. This value (Ea) has been estimated to be approximately **+3.0** degrees and may vary as to the quality of the avionics. This distribution-is considered normal both from a capability standpoint between manufacturers and a quality standpoint by any one manufacturer. Recent avionics have shown the capability to reduce this error.

C. Instrumentation Error (Ei). This represents the remainder of the avionics error that is excluded from **paragraph** 3.b of this Appendix. This error is approximately **+2.0** degrees when a manual analog **OBS is** utilized. Digital **OBS** devices and auto-couple would decrease this error significantly. This latter configuration is not addressed in this analysis, but could represent a considerable improvement to the total error budget, if implemented.

d. Flight Technical Error (Ef). As defined in paragraph 2.d of this Appendix, the value which is attributable to this error component is +2.3 degrees. Although this error may not be completely independent of **other** errors, independence is assumed in this analysis. Empirical data indicates that this value may be pessimistic.

e. <u>System Use Error (Es)</u>. Airways, routes, and terminal area procedures in the United States are designed on the basis of a system use accuracy of **+4.5** degress (95 percent probability). The system use error value is derived **as** follows:

Radial Signal Error (Eg): Airborne Component Error (Ea): Instrumentation Setting	<pre>+1.4 degrees (95% probability) +3.0 degrees (95% probability)</pre>
Error (Ei): Flight Technical Error (Ef):	+ 2.0 degrees (95% probability) -2.3 degrees (95% probability)
System Use Error 🖛	$(Eg^2 + Ea^2 + Ei^2 + Ef^2)^{1/2}$
=	$(1.4^2 + 3.0^2 + 2.0^2 + 2.3^2)^{1/2}$
Ŧ	$(1.96 + 9.00 + 4.00 + 5.29)^{1/2}$
*	$(20.25)^{1/2}$
-	<u>+</u> 4.5 degree (95% probability)
4. <u>DISTANCE ERROR</u> . Refer to p	paragraph 187 of this standard.

	Chan. Freq.	Thterr. Freq.	Reply Freq.		
Ch an. No.	MHz	MHz	MHz		
1X		1025	962		
14		1025	1088		
2X		1026	963		
2 Y		1026	1089		
3x		1027	964		
3Y		1027	1090		
4x		1028	965		
4Y		1028	1Ø91		
5X		1029	966		
5Y		1029	1092		
6X		1030	967		
<u>6</u> Y		1030	1093		
/X		1031	968		
/ Y		1031	1094		
8X		1Ø32	969		
89		1032	1095		
98		1033	97Ø		
9 Y		1033	1096		
		1034	971		
		1034	1097		
117		1035	9/2		
		1035	1098		
12X 12V		1036	9/3		
121		1036	1099		
		103/	9/4		
		103/	1100		
14X 1/V		1030	9/5 1101		
141 15v		1030	1101		
157		1039	9/0 1100		
168		10/0 10/0			
167		1040 1040	9// 1100		
101		1040	1103		

APPENDIX 3 VOR-DME-TACAN CHANNEL FREQUENCIES AND PAIRING

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	VHF	DME-TACA	AN	
Chan. No.	Chan. Freq. MHz	Interr. Freq. <i>MHz</i>	Reply Freq. MHz	
17X"	108.00 VOR	1041	978	
177*	108.05 VOR	1041	1104	
18X*	108.10 ILS	1042	979	
18Y	108.15 ILS	1042	1105	
19x	108.20 VOR	1043	98Ø	
19Y	1Ø8.25 VOR	1Ø43	11Ø6	
20X	108.30 ILS	1Ø44	981	
20 Y	108.35 ILS	1044	1107	
21x	108.40 VOR	1045	982	
21Y	108.45 VOR	1Ø45	1108	
22x	108.50 ILS	1Ø46	983	
22Y	108.55 ILS	1Ø46	11Ø9	
23X	1Ø8.6Ø VOR	1047	984	
23Y	1Ø8.65 VOR	1047	1110	
24X	108.70 ILS	1Ø48	985	
24Y	1Ø8.75 ILS	1048	1111	
25X	108.80 VOR	1Ø49	986	
25Y	1Ø8.85 VOR	1049	1112	
26X	108.90 ILS	1050	987	
26Y	108.95 ILS	1050	1113	
27X	109.00 VOR	1051	988	
27Y	109.05 VOR	1051	1114	
28X	109.10 ILS	1052	989	
28Y	109.15 ILS	1052	1115	
29x	109.20 VOR	1053	990	
29Y	109.25 VOR	1053	1116	
30X	109.30 ILS	1054	991	
30 Y	109.35 ILS	1054	111/	
31x	109.40 VOR	1055	992	
31Y	109.45 VOR	1055	1118	
32X	109.50 ILS	1050	993	
32Y	109.55 ILS	1050	1119	
33X 22V	109.00 VUK	1057	994 1100	

VOR-DME-TACAN	CHANNEL	FREQUENCIES	AND	PAIRING-Continued
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* The frequencies associated with Channels 17X, **17Y** and 18X are test frequencies. Assignments may be made to VOR test signals (**VOTs**), ramp testers, radiating test generators, and other test facilities. ILS, VOR, and DME-TACAN assignments should not be made on these channels. This has been coordinated with the FCC. See 47 CFR Section **87.521(d);** FCC Rules and Regulations, Part 87, paragraph **87.521(d)**.

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Appendix 3

	VHF	<u>DME - TACAN</u>	
Chan.No.	Chan. Freq. MHz	Interr.Freq. MHZ	Reply Freq. MHz
34x	109.70 ILS		
34Y	109.75 ILS	1058	1121
35X	109.80 VOH	1059	996
35 Y	1Ø9.85 VOR	1059	1122
36X	109.90 ILS	1060	997
36Y	109.95 ILS	1060	1123
37x	110.00 VOR	1061	998
37Y	110.05 VOR	1061	1124
38X	110.10 ILS	1062	999
38Y	110.15 JLS	1Ø62	1125
39x	110.20 VOR	1Ø63	1000
39Y	110.25 VOR	1Ø63	1126
40X	110.30 ILS	1Ø64	1001
40 Y	110.35 ILS	1Ø64	1127
41x	110.40 VOR	1Ø65	1002
41Y	110.45 VOR	1Ø65	1128
42x	110.50 ILS	1Ø66	1003
42Y	110.55 ILS	1Ø66	1129
43x	110.60 VOR	1Ø67	1004
43Y	11Ø.65 VOR	1Ø67	1130
44x	110.70 ILS	1Ø68	1005
44Y	110.75 ILS	1Ø68	1131
45x	110.80 VOR	1Ø69	1006
45Y	110.85 VOR	1Ø69	1132
46X	110.90 ILS	1070	1007
46Y	110.95 ILS	1070	1133
47x	111.00 VOR	1071	1008
4 / Y	111.05 VOR	1071	1134
48X	111.10 165	10/2	1009
48Y	111.15 ILS	10/2	1135
49x	111.20 VUR	10/3	1010
49Y	111.25 VUK	10/3	1130
5UX 50V	111.30 ILS 111 25 VIC	10/4 107/	1011 1127
5U T	111 /0 VOD	10/4 1075	1012
	111 / VOR	C / UL 1 م ד ד	1120
511 52V	111.43 VUK 111 50 TI C	C/UL 1076	1012
52A 52V	111 55 TH S	1076	1120

VOR-DME-TACAN CHANNEL FREQUENCIES AND PAIRING-Continued

984Ø. 1 Appendix 3

	VHF	DME - TACAN		
Chan. No.	Chan. Freq. MHz	Interr. Freq. MHz	Reply Freq. MHz	
53x	111.6Ø VOR	1077	1014	
53Y	111.65 VOR	1077	114Ø	
54x	111.7Ø ILS	1078	1Ø15	
54Y	111.75 ILS	1078	1141	
55x	111.8Ø VOR	1079	1Ø16	
55Y	111.85 VOR	1079	1142	
56X	111.90 ILS	1080	1017	
56Y	111.95 ILS	1080	1143	
57x	112.00 VOR	1081	1018	
5/Y	112.05 VOR	1081	1144	
588	112.10 VUR	1082	1019	
58Y	112.15 VOR	1082	1145	
59X	112.20 VUR	1083	1020	
591 607	112.25 VUR	1083	1140	
DUX		1084	1021	
001 61 V		1084	1147	
01X 61V		1005	1022	
628		1000	1140	
627		1080	1023	
638		1087	1024	
63Y		1087	1150	
64X		1088	1151	
64Y		1088	1025	
65X		1089	1152	
65Y		1089	1026	
66X		1090	1153	
66H		1090	1027	
67X		1 Ø91	1154	
67Y		1091	1028	
68X		1092	1155	
68Y		1092	1029	
69X		1093	1156	
69Y	112.3Ø VOR	1094 1093	1030	
70X		1004	1157	
/UY	110 210 VOD	1094	1031	
/ 1 X 7 1 V	112.5-30 VUK	1095	1130 1022	
/ 1 T 7 2 V	112.45 VUK	1005	1150 1150	
72Y	112.55 VOR	1090	1033	

VOR-DME-TACAN CHANNEL FREQUENCIES AND PAIRING-Continued

9840,1 Appendix 3

Chan. No. Chan. Freq. Interr Freq. Reply Freq. 73x 112.60 VOR 1097 1160 73y 112.65 VOR 1097 1034 74x 112.70 VOR 1098 1161 74x 112.70 VOR 1098 1035 75x 112.80 VOR 1099 1036 75y 112.80 VOR 1099 1036 76X 112.90 VOR 1100 1163 76Y 112.95 VOR 1101 1038 77x 113.00 VOR 1102 1165 78x 113.15 VOR 1102 1039 79x 113.25 VOR 1103 1040 80x 113.30 VOR 1103 1040 80x 113.30 VOR 1105 1168 81Y 113.45 VOR 1106 1043 81Y 113.60 VOR		VHF	DMF-TACA	N	
73x 112.60 VOR 1097 1160 73Y 112.65 VOR 1097 1034 74x 112.70 VOR 1098 1035 75x 112.80 VOR 1099 1162 75x 112.80 VOR 1099 1162 75x 112.80 VOR 1099 1036 76x 112.90 VOR 1100 1163 76Y 112.90 VOR 1100 1037 77x 113.00 VOR 1101 1038 78X 113.10 VOR 1102 1165 78Y 113.20 VOR 1103 1066 79Y 113.25 VOR 1103 1040 80x 113.30 VOR 1105 1168 81Y 113.45 VOR 1105 1164 81Y 113.45 VOR 1106 1043 81Y 113.56 VOR 1106	Chan. No.	Chan. Freq. MHz	Interr . Freq. MHZ	Reply Freq . MHz	
73Y 112.65 VOR 1097 1034 74x 112.70 VOR 1098 1161 74Y 112.75 VOR 1099 1035 75x 112.86 VOR 1099 1036 76X 112.90 VOR 1100 1163 76Y 112.95 VOR 1100 1163 76Y 112.95 VOR 1101 1164 77x 113.06 VOR 1101 1164 77Y 113.15 VOR 1102 1039 78X 113.16 VOR 1102 1039 79x 113.20 VOR 1103 1166 79Y 113.20 VOR 1103 1040 80X 113.30 VOR 1104 1041 81X 113.40 VOR 1105 1442 80Y 113.35 VOR 1106 1169 81X 113.45 VOR 1106 1169 82Y 113.55 VOR 1106 1444	73x	112.60 VOR	1097	1160	
74x 112.70 VOR 1098 1161 74y 112.75 VOR 1099 1162 75x 112.86 VOR 1099 1036 76x 112.90 VOR 100 1163 76x 112.90 VOR 1100 1037 77x 113.00 VOR 1101 1068 77x 113.00 VOR 1101 1038 78x 113.10 VOR 1102 1035 79x 113.25 VOR 1103 1040 80x 113.30 VOR 1103 1040 80x 113.30 VOR 1104 1167 80y 113.30 VOR 1104 1167 80y 113.35 VOR 1106 1169 81x 113.40 VOR 1106 1169 81y 113.45 VOR 1106 1042 82x 113.55 VOR 1106 1043 83x 113.66 VOR 1107 1170	73Y	112.65 VOR	1097	1034	
747 112.5 VOR 1099 1162 75x 112.88 VOR 1099 1036 76X 112.95 VOR 1000 1163 76Y 112.95 VOR 1100 1163 76Y 112.95 VOR 1100 1063 77x 113.00 VOR 1101 1164 77Y 113.00 VOR 1101 1038 78X 113.19 VOR 1102 1039 79x 113.20 VOR 1103 1166 79Y 113.25 VOR 1103 1066 79Y 113.25 VOR 1103 1066 80X 113.30 VOR 1104 1067 80X 113.35 VOR 1105 1040 81X 113.40 VOR 1105 1042 82Y 113.55 VOR 11066 1043 81Y 113.56 VOR 1106 1069 82Y 113.65 VOR 1106 1044 83X 113.66 VOR 1107 1044 84X 113.70 VOR 1106 1045 85X 113.86 VOR	/4x	112.70 VOR	1098	1161	
/5x 112.80 VOR 1099 1162 75y 112.85 VOR 1099 1036 76X 112.99 VOR 1100 1163 76Y 112.99 VOR 1100 1037 77x 113.00 VOR 1101 1038 78X 113.10 VOR 1101 1038 78X 113.10 VOR 1102 1039 79x 113.20 VOR 1103 1166 79Y 113.25 VOR 1103 1040 80X 113.30 VOR 1103 1046 80X 113.30 VOR 1104 1041 81X 113.45 VOR 1105 1168 81Y 113.45 VOR 1105 1042 82X 113.50 VOR 1106 1043 83Y 113.66 VOR 1107 1044 84X 113.75 VOR 1108	/4Y	112./5 VOR	1098	1035	
75Y 112.85 VUR 1099 1036 76X 112.96 VOR 1100 1163 76Y 112.95 VOR 1100 1037 77x 113.06 VOR 1101 1164 77Y 113.05 VOR 1101 1038 78X 113.16 VOR 1102 1039 79x 113.25 VOR 1103 1166 79Y 113.25 VOR 1103 1066 79Y 113.35 VOR 1104 1067 80X 113.36 VOR 1105 1168 81Y 113.45 VOR 1105 1042 82X 113.56 VOR 1106 1043 81Y 113.45 VOR 1106 1043 82Y 113.56 VOR 1107 1170 83Y 113.66 VOR 1107 1170 83Y 113.56 VOR 1108	/5X	112.80 VUR	1099	1162	
76% 112.95 VOR 1100 163 76Y 112.95 VOR 1101 1037 77x 113.00 VOR 1101 1038 78X 113.10 VOR 1102 105 78X 113.15 VOR 1102 1039 79x 113.25 VOR 1103 1066 79Y 113.25 VOR 1103 1066 79Y 113.25 VOR 1104 1067 80X 113.35 VOR 1105 1168 81X 113.46 VOR 1105 1042 82X 113.55 VOR 1106 1043 81Y 113.66 VOR 1107 1044 82X 113.66 VOR 1107 1044 83X 113.66 VOR 1107 1044 844 113.75 VOR 1108 1045 85X 113.80 VOR 1109 10	/5Y	112.85 VUR	1099	1036	
701 112.95 VOR 1100 1007 77x 113.06 VOR 1101 1164 77Y 113.05 VOR 1102 1038 78x 113.16 VOR 1102 1039 79x 113.25 VOR 1103 1166 79Y 113.25 VOR 1103 1040 80X 113.30 VOR 1104 1067 80Y 113.35 VOR 1104 1067 80Y 113.35 VOR 1105 1168 81X 113.46 VOR 1106 1042 82X 113.56 VOR 1106 1043 83X 113.66 VOR 1107 1044 84X 113.75 VOR 1108 1045 85X 113.86 VOR 1109 1172 86Y 113.85 VOR 1100 1446 86X 113.90 VOR 1111	/0X 76V	112.90 VUR 112 OF VOD	1100	103	
7/X 113.05 VOR 1101 1038 78X 113.10 VOR 1102 1039 78X 113.12 VOR 1102 1039 78Y 113.20 VOR 1103 1066 79Y 113.25 VOR 1103 1040 80X 113.30 VOR 1104 1167 80Y 113.35 VOR 1105 1044 81X 113.46 VOR 1105 1042 82X 113.55 VOR 1106 168 81Y 113.45 VOR 1106 1042 82X 113.55 VOR 1106 1043 83X 113.66 VOR 1107 1044 84Y 113.75 VOR 1108 1042 85X 113.86 VOR 1107 1044 84Y 113.77 VOR 1108 1045 85X 113.86 VOR 1107 1044 84Y 113.85 VOR 1109 1046	/01	112.95 VUR	1100	1037	
78X 113.10 1101 103 78X 113.15 VOR 1102 1039 79Y 113.20 VOR 1103 1166 79Y 113.20 VOR 1103 1066 79Y 113.25 VOR 1104 1067 80X 113.30 VOR 1104 1067 80Y 113.35 VOR 1105 1168 81X 113.45 VOR 1105 1042 82X 113.50 VOR 1106 1043 83X 113.60 VOR 1106 1043 83X 113.60 VOR 1107 1170 83Y 113.55 VOR 1106 1044 84X 113.70 VOR 1107 1044 84X 113.70 VOR 1108 1045 85Y 113.80 VOR 1109 1044 84X 113.90 VOR 1109 1046 86X 113.90 VOR 1110 1172 86Y	//X 77V	113.00 VUK 112 05 VOD	11Ø1 11Ø1	1104	
76X 113.15 VOR 1102 103 78Y 113.20 VOR 1103 1166 79Y 113.25 VOR 1104 167 80X 113.30 VOR 1104 1067 80Y 113.35 VOR 1104 1041 81X 113.46 VOR 1105 1168 81Y 113.45 VOR 1106 1169 82X 113.56 VOR 1106 169 82Y 113.55 VOR 1106 1041 83X 113.66 VOR 1107 1044 84X 113.70 VOR 1107 1044 84X 113.70 VOR 1107 1044 84X 113.70 VOR 1108 1171 84Y 113.70 VOR 1109 1045 85X 113.80 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1111 1048	771 70V	112 10 VOR	1101	1030	
781 113.13 VOR 1102 1033 79Y 113.25 VOR 1103 1040 80X 113.30 VOR 1104 167 80Y 113.35 VOR 1104 1041 81X 113.46 VOR 1105 1168 81Y 113.45 VOR 1106 1169 82X 113.50 VOR 1106 1042 82X 113.55 VOR 1106 1043 83X 113.60 VOR 1107 1044 84Y 113.75 VOR 1108 1171 84Y 113.75 VOR 1108 1045 85X 113.80 VOR 1109 1172 86Y 113.90 VOR 1100 1047 85X 113.90 VOR 1110 1048 86X 113.90 VOR 1110 1047 87X 114.00 VOR 1111 1173 86Y 114.10 VOR 1111 1048	/0A 70V	113.10 VOR 112 15 VOD	1102	1100	
79Y 113.25 VOR 1103 1040 80X 113.35 VOR 1104 1167 80Y 113.35 VOR 1104 1041 81X 113.40 VOR 1105 1168 81Y 113.45 VOR 1105 1042 82X 113.50 VOR 1106 1042 82Y 113.55 VOR 1106 1042 82Y 113.55 VOR 1106 1042 83X 113.60 VOR 1107 1170 83Y 113.65 VOR 1108 1171 84Y 113.75 VOR 1108 1044 84X 113.75 VOR 1108 1044 84Y 113.75 VOR 1108 1045 85X 113.80 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1111 1048 88X 114.00 VOR 1111 1048	701 70v	113.15 VUR 113.20 VOD	1102	1035	
80x 113.23 V0R 1104 1167 80y 113.35 V0R 1104 1041 81x 113.40 V0R 1105 1168 81y 113.40 V0R 1105 1168 81y 113.40 V0R 1105 1168 81x 113.40 V0R 1106 1169 82x 113.50 V0R 1106 1043 82x 113.55 V0R 1107 1170 83x 113.65 V0R 1107 1044 84y 113.70 VOR 1107 1044 84x 113.75 V0R 1108 1071 85x 113.80 V0R 1109 1045 85x 113.80 V0R 1109 1046 86x 113.90 V0R 1110 1173 86y 113.95 V0R 1110 1047 87x 114.00 V0R 1111 1048 88x 114.16 V0R 1112 1175	79X 70V	113.20 VOR 113.25 VOD	1103	10/0	
807 113.35 V0R 1107 1007 807 113.35 V0R 1105 1168 811 113.40 V0R 1105 1168 811 113.45 V0R 1106 1169 821 113.55 V0R 1106 1042 822 113.55 V0R 1106 1043 83X 113.66 V0R 1107 1170 83Y 113.65 V0R 1108 1044 84Y 113.75 V0R 1108 1045 85X 113.80 V0R 1109 1172 84Y 113.75 V0R 1109 1046 86X 113.90 V0R 1100 1047 85Y 113.80 V0R 1111 1174 86Y 114.05 V0R 1111 1174 87Y 114.00 V0R 1111 1174 87Y 114.00 V0R 1112 1049 88X 114.10 V0R 1112 1050	808	113.25 VOR	1103	1167	
81X 113.40 VOR 1105 1168 81Y 113.45 VOR 1105 1042 82X 113.50 VOR 1106 1169 82Y 113.55 VOR 1106 1043 83X 113.60 VOR 1107 1170 83Y 113.65 VOR 1107 1044 84X 113.70 VOR 1108 1171 84Y 113.75 VOR 1108 1045 85X 113.80 VOR 1109 1172 85Y 113.85 VOR 1109 1046 86X 113.90 VOR 1110 1047 86Y 113.90 VOR 1110 1047 86Y 113.90 VOR 1111 1048 86Y 114.00 VOR 1111 1047 87Y 114.00 VOR 1111 1048 88X 114.10 VOR 1112 1049 89Y 114.20 VOR 1113 1050	807	113.36 VOR	1104	1041	
81Y 113.15 VOR 1105 1042 82X 113.50 VOR 1106 1169 82Y 113.55 VOR 1106 1043 83X 113.60 VOR 1107 1044 84X 113.70 VOR 1107 1044 84X 113.70 VOR 1108 1045 85X 113.80 VOR 1109 1172 85Y 113.80 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.90 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.00 VOR 1111 1048 88X 114.10 VOR 1111 1048 88X 114.10 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90Y 114.30 VOR 1113 1052	81 X	113 40 VOR	1105	1168	
82X 113.50 VOR 1106 1169 82Y 113.55 VOR 1106 1043 83X 113.60 VOR 1107 1170 83Y 113.65 VOR 1107 1044 84X 113.70 VOR 1108 1045 84Y 113.75 VOR 1108 1045 85X 113.80 VOR 1109 1172 85Y 113.80 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.400 VOR 1111 1048 88X 114.10 VOR 1112 1075 88Y 114.20 VOR 1113 1176 89Y 114.20 VOR 1113 1050 90x 114.30 VOR 1113 1050 90x 114.30 VOR 1115 1178	81 Y	113.45 VOR	1105	1042	
82Y 113.55 VOR 1106 1043 83X 113.60 VOR 1107 1170 83Y 113.65 VOR 1107 1044 84X 113.70 VOR 1108 1171 84Y 113.75 VOR 1108 1045 85X 113.80 VOR 1109 1172 85Y 113.85 VOR 1109 1046 86X 113.90 VOR 1110 1047 86Y 113.95 VOR 1110 1047 86Y 113.95 VOR 1111 1173 86Y 114.05 VOR 1111 1047 87X 114.05 VOR 1111 1047 88X 114.10 VOR 1112 1175 88Y 114.20 VOR 1113 1176 89Y 114.20 VOR 1113 1050 90X 114.30 VOR 1114 1177 90Y 114.450 VOR 1115 1178	82X	113.50 VOR	1106	1169	
83X 113.60 VOR 1107 1170 83Y 113.65 VOR 1107 1044 84X 113.70 VOR 1108 1171 84Y 113.75 VOR 1109 1172 85X 113.80 VOR 1109 1045 85X 113.80 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.90 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.00 VOR 1111 1048 88X 114.10 VOR 1111 1048 88X 114.10 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90X 114.30 VOR 1114 1177 90Y 114.45 VOR 1115 1178	82Y	113.55 VOR	1106	1043	
83Y 113.65 VOR 1107 1044 84X 113.70 VOR 1108 1171 84Y 113.75 VOR 1108 1045 85X 113.80 VOR 1109 1172 85Y 113.85 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.05 VOR 1111 1048 88X 114.10 VOR 1111 1048 88X 114.10 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.20 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.450 VOR 1115 1052	83X	113.6Ø VOR	1107	1170	
84X 113.70 VOR 1108 1171 84Y 113.75 VOR 1108 1045 85X 113.80 VOR 1109 1172 85Y 113.85 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.00 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91Y 114.40 VOR 1115 1178 91Y 114.50 VOR 1115 1052 92x 114.50 VOR 1116 1053 93x 114.60 VOR 1117 1180	83Y	113.65 VOR	1107	1044	
84Y 113.75 VOR 1108 1045 85X 113.80 VOR 1109 1172 85Y 113.85 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.05 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.15 VOR 1113 1176 89X 114.20 VOR 1113 1050 90x 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1053 93x 114.60 VOR 1117 1180 93x 114.65 VOR 1117 1180	84X	113.7Ø VOR	11Ø8	1171	
85X 113.80 VOR 1109 1172 85Y 113.85 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.05 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.15 VOR 1112 1049 89X 114.20 VOR 1113 1050 90x 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1178 91Y 114.55 VOR 1116 1179 92x 114.50 VOR 1116 1053 93x 114.60 VOR 1117 1180	84Y	113.75 VOR	11Ø8	1045	
85Y 113.85 VOR 1109 1046 86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.00 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.15 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.30 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.40 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1809	85X	113.8Ø VOR	1109	1172	
86X 113.90 VOR 1110 1173 86Y 113.95 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.05 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.15 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180	85Y	113.85 VOR	11Ø9	1Ø46	
86Y 113.95 VOR 1110 1047 87X 114.00 VOR 1111 1174 87Y 114.05 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.15 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90X 114.30 VOR 1114 1177 90Y 114.35 VOR 1115 1178 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.50 VOR 1116 1053 93x 114.60 VOR 1117 1180 93X 114.65 VOR 1117 1654	86X	113.9Ø VOR	1110	1173	
87X 114.00 VOR 1111 1174 87Y 114.05 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.15 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.20 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180	86Y	113.95 VOR	1110	1047	
87Y 114.05 VOR 1111 1048 88X 114.10 VOR 1112 1175 88Y 114.15 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180	87X	114.ØØ VOR	1111	1174	
88X 114.10 VOR 1112 175 88Y 114.15 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180	87Y	114.05 VOR	1111	1048	
88Y 114.15 VOR 1112 1049 89X 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180	888	114.10 VOR	1112	11/5	
89x 114.20 VOR 1113 1176 89Y 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180 93y 114.65 VOR 1117 1180	881	114.15 VUR	1112	1049	
897 114.25 VOR 1113 1050 90x 114.30 VOR 1114 1177 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180 93Y 114.65 VOR 1117 1054	891	114.20 VUR	1113		
90x 114.30 VOR 1114 1077 90Y 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180 93y 114.65 VOR 1117 1054	891 00v	114.25 VUK	1113	1050	
907 114.35 VOR 1114 1051 91X 114.40 VOR 1115 1178 91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180 93Y 114.65 VOR 1117 1054	90X	114.30 VUK			
91Y 114.45 VOR 1115 1052 92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180 93Y 114 65 VOR 1117 1054	30 T 01 Y	114.33 VUK	1114 1115	1001 1170	
92x 114.50 VOR 1116 1179 92Y 114.55 VOR 1116 1053 93x 114.60 VOR 1117 1180 93y 114.65 VOR 1117 1054	01V	11/ /5 VOR	1115	1052	
92Y 114.55 VOR 1116 1053 93X 114.60 VOR 1117 1180 93Y 114.65 VOR 1117 1654	911 92v	114.45 VOR 114 50 VOD	1115	1170	
93x 114.60 VOR 1110 1055 93y 114.65 VOR 1117 1180	928	114 55 VOR	1110	1052	
93V 114.65 VOR 1117 100	93x	114 6Ø VOR	1110	1180	
	93Y	114.65 VOR	1117	1054	

VOR-DME-TACAN CHANNEL FREQUENCIES AND PAIRING-Continued

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984Ø.1 Appendix 3

	VHF	DME-TACAN		
Chan. No.	Chan. Freq. MHZ	Interr. Freq. MHZ	Reply Freq. MHz	
94x	114.7Ø VOR	1118	1181	
94Y	114.75 VOR	1118	1055	
95x	114.80 VDR	1119	1182	
95Y	114.85 VOR	1119	1056	
96X	114.90 VOR	1120	1183	
96Y	114.95 VOR	1120	1057	
97x	115.00 VOR	1121	1184	
97Y	115.05 VOR	1121	1058	
98X	115.10 VOR	1122	1185	
98Y	115.15 VUK	1122	1059	
99X	115.20 VUR	1123	1186	
99 Y	115.25 VUK	1123	1060	
	115.30 VUK	1124	1061	
	115.35 VUK	1124	1100	
	115.40 VOR 115.45 VOD	1120	100	
1011	115.45 VUR 115 50 VOD	1125	1100	
1020	115.50 VOR	1120	103	
1021 103x	115.55 VOR	1120	1190	
1037	115.65 VOR	1127	1064	
104x	115 70 VOR	1128	1191	
104Y	115.75 VOR	1128	1065	
105X	115.80 VOR	1129	1192	
105Y	115.85 VOR	1129	1066	
106X	115.9Ø VOR	1130	1193	
106Y	115.95 VOR	1130	1067	
1Ø7x	116.ØØ VOR	1131	1194	
107Y	116.Ø5 VOR	1131	1Ø68	
1Ø8X	116.1Ø VOR	1132	1195	
108Y	116.15 VOR	1132	1069	
109X	116.20 VOR	1133	1196	
1094	116.25 VOR	1133	1070	
11Øx	116.30 VOR	1134	1197	
	116.35 VUK	1134	1100	
	116.40 VUK	1135	1198	
	116.45 VUK	1135	10/2	
112X 112V	116 FE VOD	1130	1072	
112Y	116.55 VUK	1130 7611	1200	
113X 113V	110.00 VUK	113/	1074	
114x	116 70 VOR	1137 1138	1201	
11/IV	116 75 VOR	1120	1075	

	VHF	DME-TACAN		
Chan.No.	Chan. Freq. MHz	Interr. Freq. MHz	ReplyFreq . MHZ	
315X	116.80 VOR	1139	1202	
115Y	116.85 VOR	1139	1076	
116X	116.90 VOR	1140	1203	
116Y	116.95 VOR	1140	1077	
117x	117.ØØ VOR	1141	1204	
117Y	117.Ø5 VOR	1141	1078	
118X	117.1Ø VOR	1142	1205	
118Y	117.15 VOR	1142	1079	
119x	117.20 VOR	1143	1206	
119Y	117.25 VOR	1143	1080	
120X	117.3Ø VOR	1144	1207	
120Y	117.35 VOR	1144	1081	
121X	117.4Ø VOR	1145	12Ø8	
121Y	117.45 VOR	1145	1Ø82	
122x	117.5Ø VOR	1146	1209	
122Y	117.55 VOR	1146	1083	
123X	117.6Ø VOR	1147	1210	
123Y	117.65 VOR	1147	1084	
124X	117.7Ø VOR	1148	1211	
124Y	117.75 VOR	1148	1Ø85	
125X	117.8Ø VOR	1149	1212	
125Y	117.85 VOR	1149	1Ø86	
126X	117.9Ø VOR	115Ø	1213	
1264	117.95 VOR	1150	1Ø87	

VOR-DME-TACAN CHANNEL FREQUENCIES AND PAIRING-Continued

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APPENDIX 4. DEFINITIONS.

AGL	Above Ground Level
AIM	Airman's Information Manual
ATC	Air Traffic Control
CDI	Course Deviation Indicator
CW	Continuous Wave
dB	Decibels
dBi	Gain in decibels relative to an isotropic antenna
dBm	Decibels of power with respect to a milliwatt
dBW	Decibels of power with respect to a watt
dBW/m ²	Power density per square meter
DME	Distance Measuring Equipment
DSBDVOR	Double Sideband Ooppler Very High Frequency Omnidirectional Radio Range
D/U Ratio	Desired to Undesired Ratio
EIRP	Equivalent Isotropic Radiated Power
ESV	Expanded Service Volume
FAA	Federal Aviation Administration
FTE	Flight Technical Error
H	High Altitude Service Volume
HVORTAC	High Altitude Very High Frequency Omnidirectional
	Radio Range and Tactical Air Navigation
HZ	Hertz
ICAO	International Civil Aviation Organization
IFR	Instrument Flight Rules
ILS	Instrument Landing System
kHz	Kilohertz
L	Low Altitude Service Volume
LDME	Low Altitude Distance Measuring Equipment
m	meter
MHZ	Megahertz
NAS	National Airspace System
NAVAIDS	Navigational Aids
nmi	Nautical Mile
NOTAM	Notice to Airman
OBS	Omni Bearing Selector
RF	Radio Frequency
RNAV	Area Navigation
RSS	Root-Sum-Square
SSV	Standard Service Volume

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<u>APPENDIX 4. DEFINITIONS</u> (continued)

Т	Terminal Service Volume
TACAN	Tactical Air Navigation
TVOR	Terminal Very High Frequency Omnidirectional Radio Range
UHF	Ultra High Frequency
VHF	Very High Frequency
VOR	Very High Frequency Omnidirectional Radio Range
VOR/DME	Very High Frequency Omnidirectional Radio Range/
	Distance Measuring Equipment
VORTAC	Very High Frequency Omnidirectional Radio Range
	and Tactical Air Navigation
X Channel and	Frequency pairing for Distance Measuring
Y Channel	Equipment and Tactical Air Navigation