

_____ JUDLIN

_____ MARSALONE

_____ CINDY
_____ ✓ DD *LL*

_____ DE

_____ DG

_____ DL

_____ DR

_____ DW

_____ D-1165

*No res
required*
Worm

_____ 29 May SUSPENSE

_____ RELEASE

_____ FILE

_____ DESTROY

DISPOSITION FORM

For use of this form, see AR 340-15; the proponent agency is TAGO.

170006637

REFERENCE OR OFFICE SYMBOL
LMNED-SP

SUBJECT
Lake Pontchartrain, La. & Vic Hurricane Protection Project
17th Street Outfall Canal Butterfly Control Valve Structure
Breakwater Design

TO C/Des Br
C/F&M Br

FROM C/Des Svcs Br

DATE 29 Apr 87
Mr. Stutts/pas/2614

CMT 1

1. Reference is made to my 10 Apr 87 DF, subject as stated above, and to H&H Br CMT 2 dated 21 Apr 87. Copies of the DF's (with enclosures) were hand-carried to your study principals.
2. It is requested that each of your respective offices use the above referenced materials to develop GDM scope designs for the subject breakwater. To minimize delays in furnishing the F&M designs to Des Br, it is requested that F&M Br furnish its input directly to Des with copy furnished to Des Svcs Br.
3. F&M Br should provide its design input to Des Br ASAP but NLT 15 May 87.
4. Since we seek to develop to GDM scope only the most cost-effective plans, it may not be necessary to fully develop all of the alternatives contained in the above referenced DF. Design Branch can, in all probability, make this call once they have received F&M Br's input. We should try to complete the breakwater design and cost estimates NLT 29 May 87.
5. Should you have any questions concerning this request, please contact Mr. Vann Stutts on ext. 2614.

Encls
(hand-carried)


THOMAS E. HARRINGTON, JR.
Chief, Design Services Branch

30 Apr 87

As per telephone conversation with Vann Stutts the suspense date for completing the cost estimate is rescinded. The cost of the breakwater will be provided with the GDM estimates, now scheduled for completion during Aug 87.



D-1165

DISPOSITION FORM

For use of this form, see AR 340-15; the proponent agency is TAGO.

REFERENCE OR OFFICE SYMBOL

SUBJECT

LMNED-SP

Lake Pontchartrain, La. & Vic Hurricane Protection Project -
17th Street Outfall Canal Butterfly Control Value Structure
Breakwater Design

TO C/H&H Br

FROM C/Des Svcs Br

DATE 10 Apr 87
Mr. *[Signature]* /Stutts/pas/2614

CMT 1

1. Reference is made to your 31 Mar 87 DF CMT 4 subject as above, a copy of which is enclosed.
2. The reference DF tabulated several breakwater types along with their associated crown elevations and widths. It is requested that you provide the applicable wave force and pressure diagrams which are required to determine sheet pile penetration and the other structural aspects needed to develop a GDM Scope Design. Also for the double cellular breakwater concept, we will need for you to give us the appropriate spacing between cells so that the greatest attenuation of waves can be achieved. For the rubble structure it will be necessary that you provide a typical design section and the necessary stone gradation and/or armor stone requirements so that we can prepare cost estimates for these plans.
3. The above stated design parameters are needed ASAP but should be provided NLT COB 17 Apr 87.

Encl

[Signature]
THOMAS E. HARRINGTON, JR.
Chief, Design Services Branch

LMNED-HC

TO C/Des Svcs Br

FROM C/H&H Br

DATE 21 Apr 87
Ms. Hote/beb/2489
[Signature]

CMT 2

As requested in CMT 1 enclosed are wave force diagrams for the narrow cellular sheet pile breakwater (encl 2) and for the double cellular breakwater (encl 3). Spacing for the double cellular breakwater is 85 feet between the walls. The cross-section for the rubble breakwater (encl 4) gives the thickness and gradations for either of the rubble alternatives selected. Note that the rubble structure consists of a shell core, geotechnical fabric, 3 feet of graded riprap and a 6-foot layer of uniform stone. Any questions on this information can be directed to Janis Hote at X2489. *[Signature]*

4 Encls
1-3 nc
2-4 added

[Signature]
CECIL W. SOILEAU
Chief, Hydraulics & Hydrologic Branch *[Signature]*

LMNED-HC (LMNED-HC/17 Mar 87)

SUBJECT: Lake Pontchartrain, LA & Vic Hurricane Protection Project - 17th Street
Outfall Canal - Butterfly Control Value Structure Breakwater Design

TO C/Des Svcs Br

FROM C/H&H Br

DATE 31 Mar 87 CMT 4
Ms. Hote/beb/2489
9mH

For the alternative 2 alignment shown on the enclosure the following physical parameters are required to protect the canal from the SPH stage of 11.5 ft NGVD.

<u>Breakwater Type</u>	<u>Elevation (ft NGVD)</u>	<u>Crown Width (ft)</u>
Narrow Cellular (sheet pile or timber)	15.5	-
Rubble	12.0	25
(impermeable)	14.0	14
Double Cellular (inner)	11.0	-
(outer)	10.5	-

Rubble mound breakwater can be constructed with the steepest stable side slope and have an outer stone thickness of approximately 9 feet of graded stone over a shell core. These design sections and alinements are preliminary and will have to be model-tested to determine their true wave attenuating characteristics.

Encl


CECIL W. SOILEAU

Chief, Hydraulics & Hydrologic Branch



12

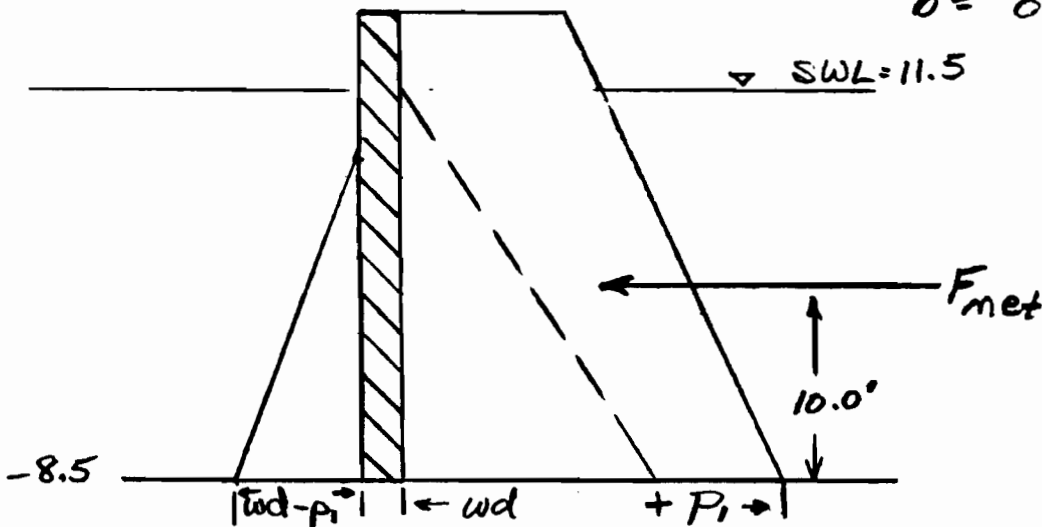
PROJECT	L. PONT + VIC - 1, 7 th ST CANAL	PAGE 1 OF 1	COMPUTED BY	DATE
SUBJECT	SINGLE NARROW CELLULAR BREAKWATER @ 15.5		CHECKED BY	DATE

$$H_i = 1.67 H_s = 13.0$$

$$h_o = 9.6$$

$$d = -8.5 + 11.5 = 20$$

$$b = -8.5 + 15.5 = 24$$



$$y_c = d + h_o + H_i = 20 + 9.6 + 13 = 42.6$$

$$y_t = d + h_o - H_i = 20 + 9.6 - 13 = 16.6$$

$$p_1 = w H_i / \cosh(2\pi d/L) = 650 \text{ \#/ft}$$

$$w d = (64)(20) = 1280 \text{ \#/ft}^2$$

$$P_c = w d + p_1 = 1280 + 650 = 1930 \text{ \#/ft}^2$$

$$P_t = w d - p_1 = 1280 - 650 = 630 \text{ \#/ft}^2$$

$$F_c = F_{wd} + F_{wave} = (0.85 + 0.5) w d^2 = 34600$$

$$F_t = F_{wd} - F_{wave} = (0.5 - 0.34) w d^2 = 4100$$

$$\text{For } 15.5 \text{ ft wall } b/y_c^3 = 24/42.6^3 = 0.56$$

$$r_s = .81 \quad r_m = 0.60$$

$$F_c' = r_s F_c = .81(34560) = 28000$$

$$F_{net} = F_c' - F_t = 28000 - 4100 = \underline{23900 \text{ \#/ft}}$$

$$M_c = M_{wd} + M_{wave} = (.167 + .67) w d^3 = 428400$$

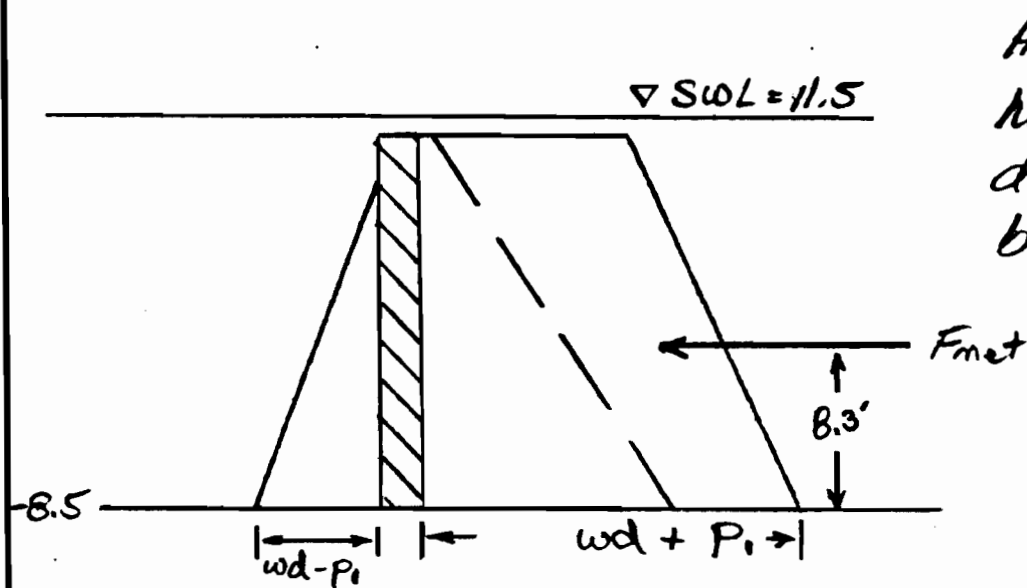
$$M_t = M_{wd} - M_{wave} = (.167 - .132) w d^3 = 17700$$

$$M_c' = r_m M_c = 0.6(428373) = 257000$$

$$M_{net} = M_c' - M_t = 257000 - 17700 = \underline{239,300 \text{ ft}\#\text{/ft}}$$

$$X_{net} = \frac{M_{net}}{F_{net}} = \frac{239300}{23900} = 10.0 - 8.5 = \underline{+1.5 \text{ ft mgvd}}$$

PROJECT <i>L. Port + Vc - 1/1 St Canal</i>	PAGE <i>1</i> OF <i>2</i>	COMPUTED BY	DATE
SUBJECT <i>DOUBLE CELLULAR BREAKWATER (OUTSIDE @ D.S.)</i>		CHECKED BY	DATE



$$H_i = 1.67 H_s = 13.0$$

$$h_o = 9.6$$

$$d = -8.5 + 11.5 = 20$$

$$b = -8.5 + 10.5 = 19$$

$$y_c = d + h_o + H_i = 20 + 9.6 + 13 = 42.6$$

$$y_t = d + h_o - H_i = 20 + 9.6 - 13 = 16.6$$

$$w_d = (64)(20) = 1280 \text{ \# / ft}^2$$

$$p_i = w_d H_i / \cosh(2\pi d/L) = 650 \text{ \# / ft}^2$$

$$p_c = w_d + p_i = 1930 \text{ \# / ft}^2$$

$$p_t = w_d - p_i = 630 \text{ \# / ft}^2$$

$$F_c = F_{wd} + F_{wse} = (0.85 + 0.5) w_d^2 = 34600$$

$$F_t = F_{wd} + F_{wle} = (0.5 - 0.34) w_d^2 = 4100$$

$$\text{For } 10.5 \text{ ft wall } b/y_c = 19/42.6 = 0.45$$

$$r_s = 0.70 \quad r_m = 0.43$$

$$F_c' = r_s F_c = 0.7(34600) = 24200$$

$$F_{net} = F_c' - F_t = 24200 - 4100 = \underline{20100 \text{ \# / ft}}$$

$$M_c = M_{wd} + M_{wse} = (.167 + .67) w_d^3 = 428400$$

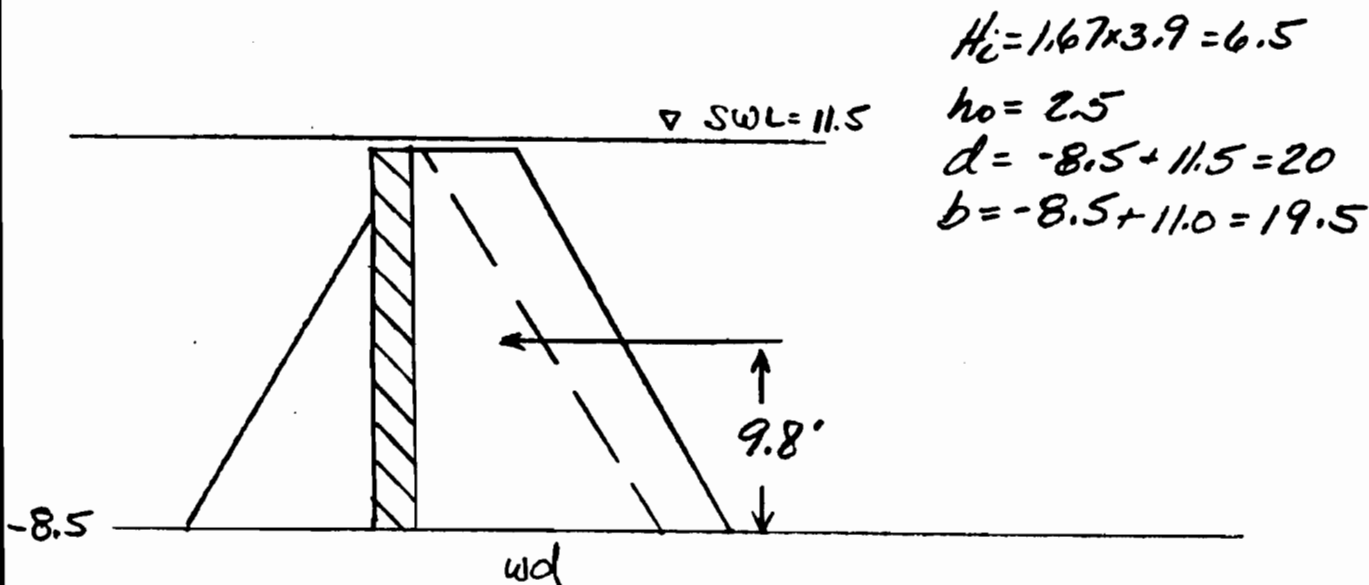
$$M_t = M_{wd} + M_{wle} = (.167 - .132) w_d^3 = 17700$$

$$M_c' = r_m M_c = 0.43(428400) = 184200$$

$$M_{net} = M_c' - M_t = 184200 - 17700 = \underline{166500 \text{ ft \# / ft}}$$

$$X_{net} = \frac{M_{net}}{F_{net}} = \frac{166500}{20100} = 8.3 - 8.5 = -0.2 \text{ ft neg'd}$$

PROJECT <u>L.P.R.T. + VIC - 17th St. Canal</u>	PAGE <u>2</u> OF <u>2</u>	COMPUTED BY	DATE
SUBJECT <u>DOUBLE CELLULAR BREAKWATER (INSIDE @ 11.0)</u>		CHECKED BY	DATE



$$y_c = d + h_o + H_i = 20 + 2.5 + 6.5 = 29.0$$

$$y_t = d + h_o - H_i = 20 + 2.5 - 6.5 = 16.0$$

$$wd = 64(20) = 1280$$

$$P_i = wH_i / \cosh(2\pi d/L) = 44(6.5) / 1.28 = 325$$

$$P_c = wd + P_i = 1280 + 325 = 1605 \text{ \#/ft}^2$$

$$P_t = wd - P_i = 1280 - 325 = 955 \text{ \#/ft}^2$$

$$F_c = F_{wd} + F_{wave} = (0.5 + .34)wd^2 = 21500$$

$$F_t = F_{wd} + F_{wave} = (0.5 - .22)wd^2 = 7100$$

$$\text{For } 11.0 \text{ ft wall } b/y_c = 19.5/29 = 0.67$$

$$r_s = 0.89 \quad r_m = 0.75$$

$$F_c' = r_s F_c = 0.89(21500) = 19100$$

$$F_{net} = F_c' - F_t = 19100 - 7100 = 12000 \text{ \#/ft}$$

$$M_c = M_{wd} + M_{wave} = (.167 + .22)wd^3 = 198000$$

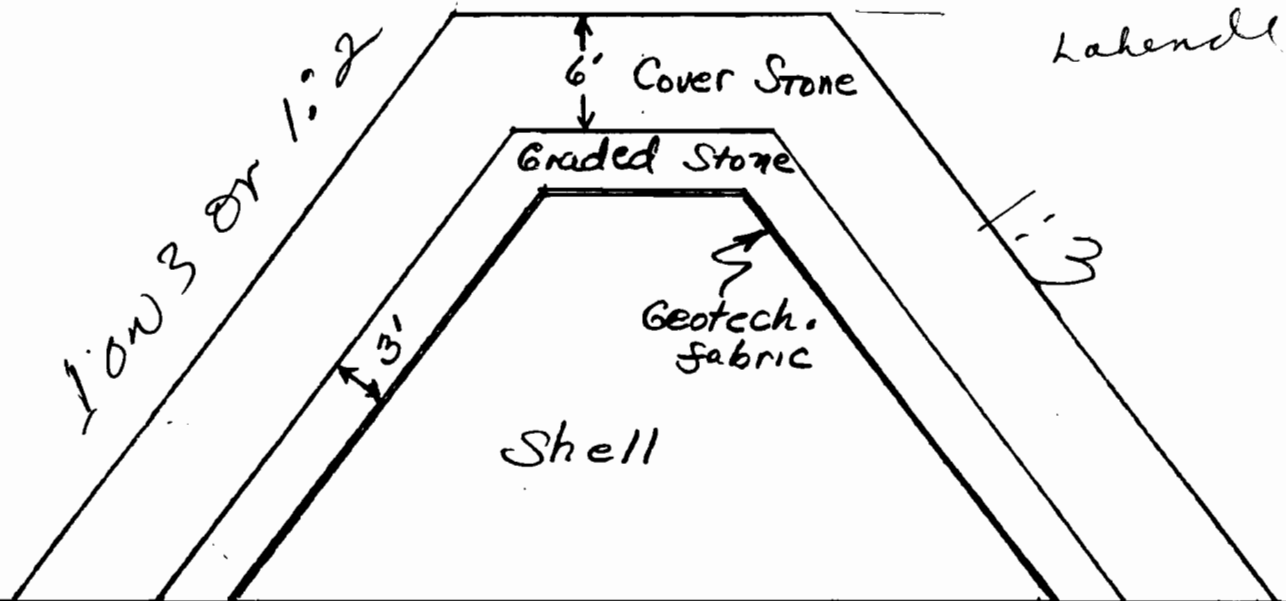
$$M_t = M_{wd} + M_{wave} = (.167 - .106)wd^3 = 31100$$

$$M_c' = r_m M_c = 0.75(198000) = 148500$$

$$M_{net} = M_c' - M_t = 148500 - 31100 = 117400 \text{ ft}\#\text{/ft}$$

$$X_{net} = \frac{M_{net}}{F_{net}} = \frac{117400}{12000} = 9.8 - 8.5 = +1.3 \text{ ft mgvd}$$

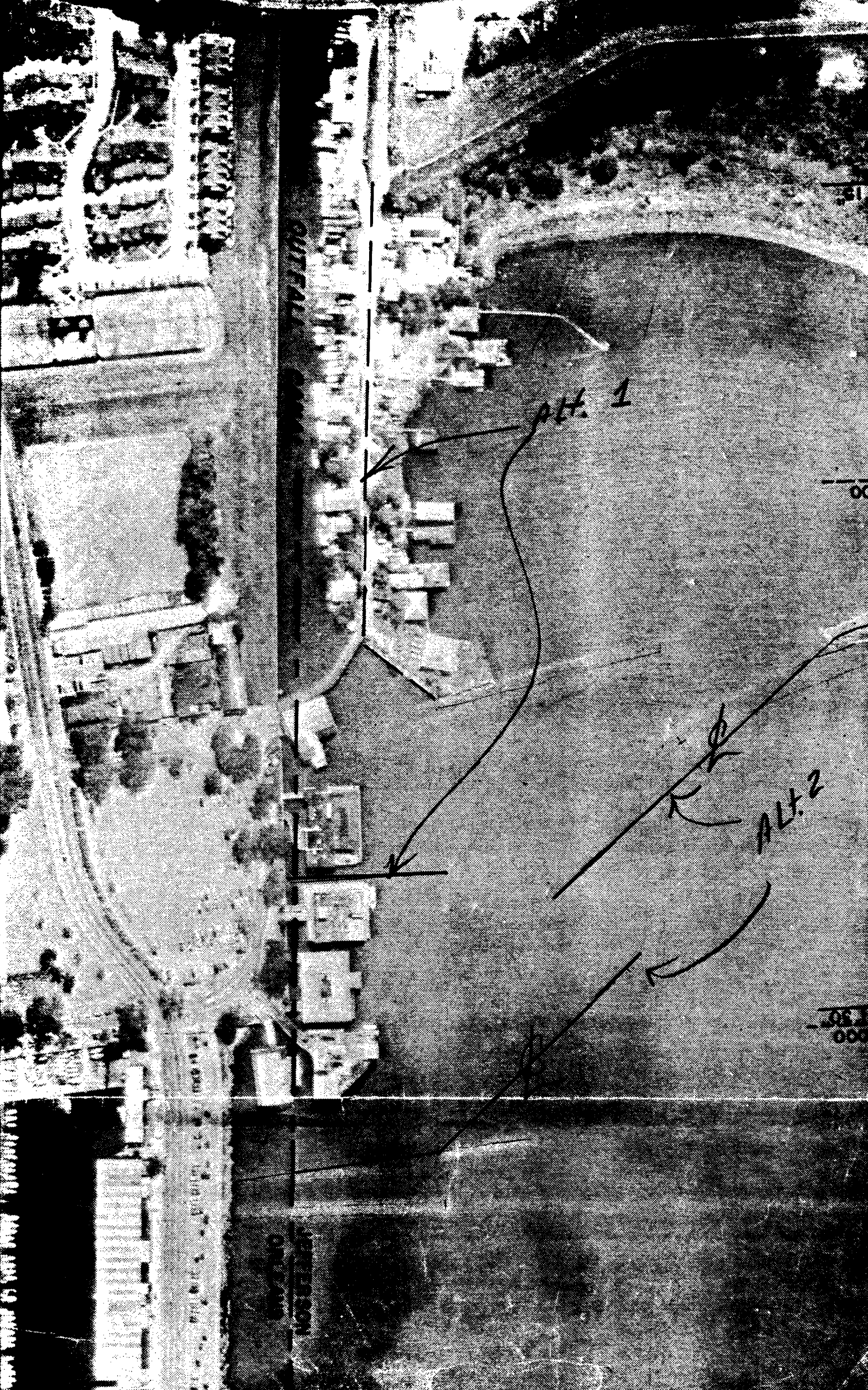
PROJECT <i>L. Pont - 17th St Canal</i>	PAGE 1 OF 1	COMPUTED BY	DATE
SUBJECT <i>TYPICAL RUBBLE BREAKWATER</i>		CHECKED BY	DATE



Cover Stone $W = 3900\#$ $W_{upper} = 4900\#$
 $W_{lower} = 2900\#$

Graded Stone

Percent Lighter by Weight	Weight lbs.
100	2200 - 900
50	930 - 440
15	460 - 130



CUTFALL

ALT. 1

ALT. 2

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