# Arsenic Removal from Drinking Water by Adsorptive Media U.S. EPA Demonstration Project at Rimrock, AZ Final Performance Evaluation Report

by

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Sally Gutierrez, Director National Risk Management Research Laboratory

#### **ABSTRACT**

This report documents the activities performed during and the results obtained from the arsenic removal treatment technology demonstration project at the Arizona Water Company (AWC) facility in Rimrock, AZ. The objectives of the project were to evaluate: (1) the effectiveness of AdEdge's Arsenic Package Unit-100 (APU-100) AD-33<sup>TM</sup> adsorptive media system in removing arsenic to meet the new arsenic maximum contaminant level (MCL) of 10  $\mu$ g/L, (2) the reliability of the treatment system for use at small water facilities, (3) the required system operation and maintenance (O&M) and operator skill levels, and 4) the capital and O&M cost of the technology. The project also characterized water in the distribution system and residuals produced by the treatment process. The types of data collected included system operation, water quality, process residuals, and capital and O&M cost.

The APU-100 treatment system consisted of a 25- $\mu$ m bag filter assembly, two 3-ft  $\times$  6-ft composite fiberglass pressure tanks, a backwash wastewater recycling system, associated piping and Fleck controller valves, and an instrument/control panel. Each tank contained 22 ft<sup>3</sup> of Bayoxide E33 iron-based adsorptive media, which was developed by Bayer AG and branded under the name of AD-33<sup>TM</sup> by AdEdge. Due to the loss of one of AWC's production wells, the system flowrate was reduced from 90 to 30 gal/min (gpm), which prompted a change in system configuration from parallel to series (lead/lag). The reconfigured APU-100 system had a design capacity of 45 gpm and began operation on June 24, 2004. The actual flowrates through the system averaged 30 gpm, corresponding to an empty bed contact time (EBCT) of 5.4 min/tank and a hydraulic loading rate of 4.2 gpm/ft<sup>2</sup>.

Source water contained 43.8 to 81.4 μg/L of total arsenic with As(V) as the predominant species. Prechlorination, although not required for oxidation, was performed to provide disinfection throughout the treatment train and residuals within the distribution system at AWC's discretion. Concentrations of iron, manganese, silica, orthophosphate, and other ions in source water did not appear to impact arsenic removal by the AD-33<sup>™</sup> media. The system operated for 12 or 24 hr/day on a timer with 1 to 2% downtime for repairs and media replacement. After treating 52,150 bed volumes (BV) or 17,164,000 gal of water during Media Run 1A based on 44 ft<sup>3</sup> of media in the lead and lag tanks, the system effluent reached the 10-μg/L arsenic MCL on August 9, 2006. Because the media in the lag tank still had about 50% of adsorptive capacity remaining, only the lead tank was rebedded. After rebedding, the tank positions were switched with Tank B containing partially exhausted media in the lead position and Tank A with virgin media in the lag position. Media Run 1B commenced as such on November 27, 2006. To ensure that normal operations continued following the media changeout, the system was monitored until March 28, 2007.

Backwashing of the media was initially conducted automatically, but due to initiation of several unscheduled backwash events and the need to take operational data and backwash wastewater samples, the programming was changed to manual initiation once every 30 days. The backwash frequency was eventually decreased to quarterly due to minimal differential pressure (Δp) increase across the tanks between backwash events. Backwash was performed using source water for 15 min/tank at approximately 47 gpm, or 6.6 gpm/ft². Backwash wastewater from the lead tank generally contained higher concentrations of all analytes than that from the lag tank, most likely because the lead tank removed the majority of the particulates from source water. A piping loop, a recycle tank, and a metering pump enabled the system to reclaim nearly 100% of the wastewater produced by blending it with intake after prechlorination but prior to the adsorption tanks at a rate of 0.5 gpm.

Comparison of the distribution system sampling results from three residences before and after startup of the APU-100 system showed a decrease in the average arsenic concentration from 48.8 to 19.3  $\mu$ g/L. However, samples of the distribution system water exhibited higher arsenic concentrations than those of

the treatment system effluent due to blending of the treated water with untreated water from other source wells. pH, alkalinity, iron, manganese, lead, and copper concentrations did not appear to be affected by the system operation.

Treatment system residuals included spent media and backwash wastewater. Spent media including 620 lb of AD-33<sup>™</sup> passed the Toxicity Characteristic Leaching Procedure (TCLP) test and could be disposed of as non-hazardous waste at a sanitary landfill. The arsenic loading on the spent media based on inductively coupled plasma-mass spectrometry (ICP-MS) results was 8.3 mg/g, which was about 80% of the arsenic mass loaded on the media based on the arsenic breakthrough curves.

The capital investment cost of the system was \$88,307, consisting of \$63,785 for equipment, \$11,372 for site engineering, and \$13,150 for installation. Using the system's rated capacity of 45 gpm (or 64,800 gal/day [gpd]), the capital cost was \$1,962/gpm (or \$1.36/gpd). The capital cost also was converted to an annualized cost of \$8,335/yr based on a 7% interest rate and a 20-yr return period. During the first year, the system produced approximately 8,505,000 gal of water, so the unit capital cost increased to \$0.98/1,000 gal. These costs do not include the cost of the system enclosure and backwash recycling system, which were funded separately by AWC.

The O&M cost for the treatment system included cost for media replacement and disposal, electricity consumption, and labor. Representing the majority of the O&M cost, the media replacement and disposal cost depended on the media run length, the number of tanks rebedded, and labor and material cost. With the long, 2.1-year duration of the media run and the remaining capacity of the lag tank when the system effluent reached 10  $\mu$ g/L of arsenic, the media of only the lead tank was replaced at a cost of \$10,908, or \$0.64/1,000 gal. The combined electricity and labor cost was an additional \$0.22/1,000 gal for a total O&M cost of \$0.86/1,000 gal.

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#### ABBREVIATIONS AND ACRONYMS

 $\Delta p$  differential pressure

AAL American Analytical Laboratories

ADEQ Arizona Department of Environmental Quality

Al aluminum

AM adsorptive media APU arsenic package unit

As arsenic

AWC Arizona Water Company

Ba barium

BET Brunauer, Emmett, and Teller bgs below ground surface

BL baseline

BV bed volume(s)

Ca calcium

CCR Consumer Confidence Report

Cd cadmium Cl chloride

C/F coagulation/filtration CRF capital recovery factor

DO dissolved oxygen

EBCT empty bed contact time

EPA U.S. Environmental Protection Agency

F fluoride Fe iron

FedEx Federal Express

GFO granular ferric oxide gpd gallons per day gph gallons per hour gpm gallons per minute

HDPE high-density polyethylene

ICP-MS inductively coupled plasma-mass spectrometry

ID identification IX ion exchange

LCR (EPA) Lead and Copper Rule
MCL maximum contaminant level
MDL method detection limit

MDWCA Mutual Domestic Water Consumers Association

Mg magnesium

Mn manganese mV millivolts

Na sodium

NaOCl sodium hypochlorite

ND not detected NS not sampled NSF NSF International

NTU nephlemetric turbidity units

O&M operation and maintenance

ORD Office of Research and Development

ORP oxidation-reduction potential

P&ID piping and instrumentation diagram

Pb lead

PLC programmable logic controller

PO<sub>4</sub> orthophosphate

psi pounds per square inch PVC polyvinyl chloride

QA quality assurance

QA/QC quality assurance/quality control QAPP Quality Assurance Project Plan

RPD relative percent difference

RCRA Resource Conservation and Recovery Act

SDWA Safe Drinking Water Act SM system modification

SiO<sub>2</sub> silica SO<sub>4</sub> sulfate

STMGID South Truckee Meadows General Improvement District

STS Severn Trent Services

TCLP Toxicity Characteristic Leaching Procedure

TDS total dissolved solids

TO Task Order

TOC total organic carbon
TSS total suspended solids

WRWC White Rock Water Company

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#### 1.0 INTRODUCTION

# 1.1 Background

The Safe Drinking Water Act (SDWA) mandates that U.S. Environmental Protection Agency (EPA) identify and regulate drinking water contaminants that may have adverse human health effects and that are known or anticipated to occur in public water supply systems. In 1975 under the SDWA, EPA established a maximum contaminant level (MCL) for arsenic at 0.05 mg/L. Amended in 1996, the SDWA required that EPA develop an arsenic research strategy and publish a proposal to revise the arsenic MCL by January 2000. On January 18, 2001, EPA finalized the arsenic MCL at 0.01 mg/L (EPA, 2001). In order to clarify the implementation of the original rule, EPA revised the rule text on March 25, 2003, to express the MCL as 0.010 mg/L ( $10 \text{ \mug/L}$ ) (EPA, 2003). The final rule required all community and non-transient, non-community water systems to comply with the new standard by January 23, 2006.

In October 2001, EPA announced an initiative for additional research and development of cost-effective technologies to help small community water systems (<10,000 customers) meet the new arsenic standard, and to provide technical assistance to operators of small systems in order to reduce compliance costs. As part of this Arsenic Rule Implementation Research Program, EPA's Office of Research and Development (ORD) proposed a project to conduct a series of full-scale, onsite demonstrations of arsenic removal technologies, process modifications, and engineering approaches applicable to small systems. Shortly thereafter, an announcement was published in the *Federal Register* requesting water utilities interested in participating in Round 1 of this EPA-sponsored demonstration program to provide information on their water systems. In June 2002, EPA selected 17 out of 115 sites to host the demonstration studies. The Arizona Water Company (AWC) water system in Rimrock, AZ, was selected as one of the 17 Round 1 host sites for the demonstration program.

In September 2002, EPA solicited proposals from engineering firms and vendors for cost-effective arsenic removal treatment technologies for the 17 host sites. EPA received 70 technical proposals for the 17 host sites, with each site receiving from one to six proposals. In April 2003, an independent technical panel reviewed the proposals and provided its recommendations to EPA on the technologies that it determined were acceptable for the demonstration at each site. Because of funding limitations and other technical reasons, only 12 of the 17 sites were selected for the demonstration project. Using the information provided by the review panel, EPA, in cooperation with the host sites and the drinking water programs of the respective states, selected one technical proposal for each site. AdEdge's adsorptive media process was selected for the Rimrock facility. Designated as AD-33<sup>™</sup> by AdEdge, the process uses the Bayoxide E33-S media developed by Bayer AG.

## 1.2 Treatment Technologies for Arsenic Removal

The technologies selected for the 12 Round 1 EPA arsenic removal demonstration host sites included nine adsorptive media (AM) systems, one anion exchange system, one coagulation/filtration (C/F) system, and one process modification with iron addition. Table 1-1 summarizes the locations, technologies, vendors, and key source water quality parameters of the 12 demonstration sites. An overview of the technology selection and system design (Wang et al., 2004) and the associated capital costs for each site (Chen et al., 2004) are provided on the EPA website

(http://www.epa.gov/ORD/NRMRL/wswrd/dw/arsenic/index.html). As of January 2008, all of the systems were operational, and 10 performance evaluations were completed.

Table 1-1. Summary of the Round 1 Arsenic Removal Demonstration Sites

			Design	Source	Source Water Qua		
			Flowrate	As	Fe		
Demonstration Site	Technology (Media)	Vendor	(gpm)	(μg/L)	(µg/L)	pН	
WRWC, NH	AM (G2)	ADI	70 <sup>(a)</sup>	39	<25	7.7	
Rollinsford, NH	AM (E33-S)	AdEdge	100	36 <sup>(b)</sup>	46	8.2	
Queen Anne's County, MD	AM (E33-S)	STS	300	19 <sup>(b)</sup>	270 <sup>(c)</sup>	7.3	
Brown City, MI	AM (E33-S)	STS	640	14 <sup>(b)</sup>	127 <sup>(c)</sup>	7.3	
Climax, MN	C/F (Macrolite)	Kinetico	140	39 <sup>(b)</sup>	546 <sup>(c)</sup>	7.4	
Lidgerwood, ND	SM	Kinetico	250	146 <sup>(b)</sup>	1,325 <sup>(c)</sup>	7.2	
Desert Sands MDWCA, NM	AM (E33-S,E33-P)	STS	320	23 <sup>(b)</sup>	39	7.7	
Nambe Pueblo, NM	AM (E33-S)	AdEdge	145	33	<25	8.5	
Rimrock, AZ	AM (E33-S)	AdEdge	90 <sup>(a)</sup>	50	170	7.2	
Valley Vista, AZ	AM (AAFS50/ARM 200)	Kinetico	37	41	<25	7.8	
Fruitland, ID	IX (A300E)	Kinetico	250	44	<25	7.4	
STMGID, NV	AM (GFH/Kemiron)	Siemens	350	39	<25	7.4	

AM = adsorptive media; C/F = coagulation/filtration; E33-P = E33 pelletized; E33-S = E33 granular media; IX = ion exchange; SM = system modification; MDWCA = Mutual Domestic Water Consumer's Association; STMGID = South Truckee Meadows General Improvement District; WRWC = White Rock Water Company STS = Severn Trent Services

- (a) Reduced by 50% due to system reconfiguration from parallel to series operation.
- (b) Arsenic exists mostly as As(III).
- (c) Iron exists mostly as soluble Fe(II).

# 1.3 Project Objectives

The objective of the Round 1 arsenic demonstration program is to conduct 12 full-scale arsenic treatment technology demonstration studies on the removal of arsenic from drinking water supplies. The specific objectives are to:

- Evaluate the performance of the arsenic removal technologies for use on small systems.
- Determine the required system operation and maintenance (O&M) and operator skill levels.
- Characterize process residuals produced by the technologies.
- Determine the capital and O&M cost of the technologies.

This report summarizes the performance of the AdEdge system operated at Rimrock, AZ, from June 24, 2004, through March 28, 2007. The types of data collected included system operation, water quality (both across the treatment train and in the distribution system), residuals, and capital and preliminary O&M cost.

#### 2.0 SUMMARY AND CONCLUSIONS

The performance evaluation study of the AdEdge arsenic package unit (APU)-100 was conducted from June 24, 2004, through March 28, 2007. Based on the information collected during the 33-months of system operation, the following was summarized and concluded relating to the overall project objectives.

Performance of the arsenic removal technology for use on small systems:

- AD-33<sup>TM</sup> media was effective at removing arsenic (existing mostly as As[V]) in source water, reducing its concentrations from 48.3 to 81.4 μg/L to <10 μg/L. Breakthrough at 10 μg/L from the lead tank occurred at 39,180 bed volumes (BV) (1 BV = 22 ft³, the amount in one tank), which represented only 60% of the vendor-projected media run length. Breakthrough at 10 μg/L from the lag tank occurred much later at 52,150 BV (1BV = 44 ft³, the amount in both the lead and lag tanks), twice as long empty bed contact time (EBCT) was believed to have contributed to the longer run length observed.
- Monthly backwash as recommended by the vendor did not appear to benefit the adsorption runs. The frequency was later reduced to quarterly.
- The APU-100 system was capable of reducing arsenic concentrations in the distribution system, although its levels were higher than those in the treated water. This was most likely due to the contribution of untreated water from other wells, which also contained arsenic.

#### Required system *O&M* and operator skill levels:

- The system was easy to operate, requiring minimum operator's attention. Daily demand on the operator was typically 20 min.
- The O&M issues encountered during the performance period were minor, consisting of only a malfunctioning chlorine injector and a few broken pressure gauges and flow meters/totalizers. Unscheduled downtime was <2%.

#### Characteristics of residuals produced by the technology:

- Each backwash event produced 1,460 gal, on average, of wastewater; nearly 100% of the wastewater was reclaimed via a backwash recycle system.
- Backwash wastewater contained less arsenic than raw water, indicating removal of arsenic by the media during backwashing.
- Approximately 10.4 mg of arsenic was loaded on per gram of dry media, equivalent to about 1.04% arsenic loading. The spent media was non-hazardous and could be disposed of at a sanitary landfill.

#### *Capital and O&M cost of the technology:*

- The capital investment for the APU-100 system was \$88,307, including \$63,785 for equipment, \$11,372 for site engineering, and \$13,150 for installation.
- Based on a design capacity of 45 gal/min (gpm), the capital cost was \$1,962/gpm, or \$1.36/gpd.
- Media replacement cost represented the majority of the O&M cost. The media in the lead tank was replaced once at a cost of \$10,908 or \$0.64/1,000 gal, which accounted for 74% of the O&M cost. The rest of the O&M cost was incurred by electricity and labor.

#### 3.0 MATERIALS AND METHODS

# 3.1 General Project Approach

Following the predemonstration activities summarized in Table 3-1, the performance evaluation study of the AdEdge treatment system began on June 24, 2004. Table 3-2 summarizes the types of data collected and/or considered as part of the technology evaluation process. The overall system performance was based on its ability to consistently remove arsenic to below the target MCL of  $10~\mu g/L$  through the collection of water samples across the treatment train. The reliability of the system was evaluated by tracking the unscheduled system downtime and frequency and extent of repair and replacement. The unscheduled downtime and repair information were recorded by the plant operator on a Repair and Maintenance Log Sheet.

The O&M and operator skill requirements were assessed through quantitative data and qualitative considerations, including the need for pre- and/or post-treatment, level of system automation, extent of preventative maintenance activities, frequency of chemical and/or media handling and inventory, and general knowledge needed for relevant chemical processes and related health and safety practices. The staffing requirements for system operation were recorded on an Operator Labor Hour Log Sheet.

The quantity of aqueous and solid residuals generated was estimated by tracking the volume of backwash water produced during each backwash cycle and the need to replace the media upon arsenic breakthrough. Backwash water and spent media were sampled and analyzed for chemical characteristics.

Table 3-1. Predemonstration Study Activities and Completion Dates

Activity	Date
Introductory Meeting Held	July 31, 2003
Request for Quotation Issued to Vendor	August 4, 2003
Draft Letter of Understanding Issued	August 13, 2003
Final Letter of Understanding Issued	September 9, 2003
Vendor Quotation Received	September 9, 2003
Purchase Order Established	October 6, 2003
Letter Report Issued	October 17, 2003
Draft Study Plan Issued	November 26, 2003
Engineering Package Submitted to ADEQ	December 11, 2003
Final Study Plan Issued	December 19, 2003
Approval to Construct Granted by ADEQ	February 18, 2004
Construction Permit Issued by County	March 15, 2004
APU-100 Unit Shipped	March 30, 2004
Initial System Installation and Shakedown Completed	April 22, 2004
Initial Approval of Construction Granted by ADEQ	April 29, 2004
Shed Construction Completed	May 21, 2004
System Re-Configuration Completed	May 27, 2004
Revised Engineering Package Submitted to ADEQ	June 1, 2004
Final Approval of Construction Granted by ADEQ	June 15, 2004
Performance Evaluation Began	June 24, 2004

ADEQ = Arizona Department of Environmental Quality

Table 3-2. Evaluation Objectives and Supporting Data Collection Activities

Evaluation Objective	Data Collection
Performance	-Ability to consistently meet 10 μg/L of arsenic in treated water
Reliability	-Unscheduled system downtime
	-Frequency and extent of repairs including a description of problems,
	materials and supplies needed, and associated labor and cost
System O&M and Operator	-Pre- and post-treatment requirements
Skill Requirements	-Level of system automation for system operation and data collection
	-Staffing requirements including number of operators and laborers
	-Task analysis of preventative maintenance including number, frequency,
	and complexity of tasks
	-Chemical handling and inventory requirements
	-General knowledge needed for relevant chemical processes and health and
	safety practices
Residual Management	-Quantity and characteristics of aqueous and solid residuals generated by
	system operation
System Cost	-Capital cost for equipment, site engineering, and installation
	-O&M cost for media, chemical consumption, electricity usage, and labor

The cost of the system was evaluated based on the capital cost per gpm (or gal/day [gpd]) of design capacity and the O&M cost per 1,000 gal of water treated. This task required tracking the capital cost for equipment, engineering, and installation, as well as the O&M cost for media replacement and disposal, chemical supply, electricity usage, and labor.

## 3.2 System O&M and Cost Data Collection

The plant operator performed daily, weekly, and monthly system O&M and data collection according to instructions provided by AdEdge and Battelle. The plant operator recorded system operational data, such as pressure, flowrate, totalizer, and hour meter readings on a Daily System Operation Log Sheet; checked the sodium hypochlorite (NaOCl) drum level; and conducted visual inspections to ensure normal system operation on a regular basis. If any problems occurred, the plant operator contacted the Battelle Study Lead, who determined if the vendor should be contacted for troubleshooting. The plant operator recorded all relevant information on the Repair and Maintenance Log Sheet. Water quality parameters, including temperature, pH, dissolved oxygen (DO), oxidation-reduction potential (ORP), and residual chlorine were measured and recorded on a Weekly Onsite Water Quality Parameters Log Sheet. Backwash data also were recorded on a Backwash Log Sheet when appropriate.

The capital cost for the arsenic removal system consisted of the cost for equipment, site engineering, and system installation. The O&M cost consisted of the cost for media replacement and spent media disposal, chemical and electricity usage, and labor. Consumption of NaOCl was tracked on the Daily System Operation Log Sheet. Electricity consumption was determined from an electric meter. Labor for various activities, such as the routine system O&M, troubleshooting and repair, and demonstration-related work, was tracked using an Operator Labor Hour Log Sheet. The routine O&M included activities such as completing field logs, replenishing the NaOCl solution, ordering supplies, performing system inspection, and others as recommended by the vendor. The demonstration-related labor, including activities such as performing field measurements, collecting and shipping samples, and communicating with the Battelle Study Lead and the vendor, was recorded, but not used for the cost analysis.

## 3.3 Sample Collection Procedures and Schedules

To evaluate the system performance, samples were collected from the wellhead, treatment plant, and distribution system. The sampling schedules and analytes for each sampling event are listed in Table 3-3. In addition, Figure 3-1 presents a flow diagram of the treatment system along with the analytes and schedules at each sampling location. Specific sampling requirements for analytical methods, sample volumes, containers, preservation, and holding times are presented in Table 4-1 of the EPA-endorsed Quality Assurance Project Plan (QAPP) (Battelle, 2003). The procedure for arsenic speciation is described in Appendix A of the QAPP.

- **3.3.1 Source Water.** During the initial site visit, source water samples were collected and speciated using an arsenic speciation kit described in Section 3.4.1. The sample tap was flushed for several minutes before sampling; special care was taken to avoid agitation, which could cause unwanted oxidation. Analytes for the source water samples are listed in Table 3-3.
- **3.3.2 Treatment Plant Water**. Water samples were collected weekly across the treatment train at the wellhead (IN), after Tank A (TA), and after Tank B (TB) for on- and off-site analyses shown in Figure 3-1 and Table 3-3. Onsite measurements also were made on samples collected from after prechlorination (AC) location. Over the course of the demonstration study, several changes were made to the sampling schedules as listed below and in Table 3-3.
  - Beginning on November 3, 2004, regular weekly sampling was reduced from three times per four week cycle to three times per eight week cycle.
  - Speciation sampling was reduced from monthly to bimonthly beginning on October 20, 2004, and then discontinued after July 12, 2006.
  - Since October 12, 2005, orthophosphate analysis was replaced with total phosphorous analysis due to lack of orthophosphate in raw water and issues related to the short hold time for orthophosphate.
  - Onsite measurements were reduced to monthly beginning April 5, 2006, and to pH, temperature, and chlorine only beginning June 14, 2006.
  - All analyses except for arsenic discontinued on November 28, 2006.
- 3.3.3 Backwash Water. Grab backwash wastewater samples were initially collected directly from the sample tap on the backwash wastewater discharge line during the backwash of each tank and filtered with 0.45-µm disc filters. Grab samples were analyzed for pH and total dissolved solids (TDS), and filtered samples were analyzed for soluble As, Fe, and Mn. Beginning on November 14, 2005, composite samples were collected following a modified procedure to allow for more representative characterization of the wastewater. Connected to the tap on the discharge line, tubing directed a portion of backwash water from the sample tap at approximately 1 gpm into a clean plastic container of adequate volume over the duration of the backwash for each tank. After the content in the container was thoroughly mixed, composite samples were collected and/or filtered onsite with 0.45-µm disc filters. Under this revised procedure, total As, Fe, and Mn and total suspended solids (TSS) also were measured. Backwash water sampling was conducted approximately monthly beginning in October 2004, quarterly beginning in August 2005, and then discontinued after May 2006. Table 3-3 lists the schedule and analytes for the backwash water samples.

Table 3-3. Sample Collection Schedule and Analyses

Sample	Sample	No. of			Collection
Type	Location(s)(a)	Samples	Frequency	Analytes	Date(s)
Source	IN	1	Once	Off-site: As (III), As(V), total	10/22/03
Water				and soluble Al, As, Fe, and	
				Mn, Na, Ca, Mg, Cl, F, SO <sub>4</sub> ,	
				SiO <sub>2</sub> , PO <sub>4</sub> , TOC, turbidity,	
				pH, and alkalinity	
Treatment	IN, TA, and	3	Weekly (b)	Onsite <sup>(c)</sup> : pH, temperature,	See Appendix B
Plant Water	TB			DO, ORP, and $Cl_2$ (free and	
				total)	
				Off-site: total As, Fe, and	
				Mn, SiO <sub>2</sub> , PO <sub>4</sub> <sup>(d)</sup> , turbidity,	
				and alkalinity	
			Monthly <sup>(e)</sup>	Same as above plus the	See Appendix B
				following off-site: As(III),	
				As(V), soluble As, Fe, and	
				$Mn$ , $Ca$ , $Mg$ , $F$ , $NO_3$ , and	
				SO <sub>4</sub>	
Backwash	BW	2	Monthly <sup>(f)</sup>	Off-site: total <sup>(g)</sup> and soluble	See Table 5-5
Water				As, Fe, and Mn, pH, TDS,	
			4.	TSS <sup>(g)</sup> , and turbidity <sup>(g)</sup>	
Distribution	DS (three non-	3	Monthly <sup>(h)</sup>	Off-site: total As, Fe, Mn,	See Table 5-6
Water	LCR homes)			Cu, and Pb, pH, alkalinity	
Residual	Top, middle,	3	Once	Off-site: TCLP metals and	11/08/06
Solids	and bottom of			total Al, As, Ca, Cd, Cu, Fe,	
	Tank A			Mg, Mn, Ni, P, Pb, Si, and	
	1' 1	1 ,		Zn III 1 TA C T	

- (a) Corresponding to sample locations in Figure 3-1, i.e., IN = at wellhead, TA = after Tank A; TB = after Tank B; BW = at backwash water discharge line from Tanks A and B
- (b) Three sets per four-week cycle from 07/07/04 to 10/27/04; three sets per eight-week cycle from 11/03/04 to 09/28/05 and 04/05/06 to 05/17/06; one set per four-week cycle from 11/09/05 to 01/04/06 and 06/14/06 to 08/09/06; and one set per four-week cycle from 11/28/06 to 02/02/07 for total As only.
- (c) Performed for samples taken after prechlorination (AC), TA, and TB. Monthly from 04/05/06 to 08/09/06 and DO and ORP discontinued after 06/14/06.
- (d) PO<sub>4</sub> analysis replaced with total phosphorus analysis since 10/12/05.
- (e) One set per eight-week cycle from 10/20/04 to 02/01/06 and 03/08/06 to 07/12/06, and then discontinued.
- (f) Quarterly from 08/17/05 to 05/17/06 and then discontinued.
- (g) Total As, Fe, and Mn, and TSS analyses performed and turbidity discontinued since 11/14/05.
- (h) Four baseline events before system startup from 12/17/03 through 02/05/04. Discontinued after 10/12/05.

**3.3.4 Distribution System Water**. Samples were collected from the distribution system to determine the impact of the arsenic treatment system on the water chemistry in the distribution system, specifically, the arsenic, lead, and copper levels. From December 2003 to February 2004, four sets of baseline distribution water samples were collected from three locations within the distribution system. Following system startup, distribution system sampling continued on a monthly basis at the same locations. Ideally, the sampling locations selected would have been the historical Lead and Copper Rule (LCR) locations served primarily by the source water well, Well No. 2. However, because the distribution system was supplied by Well No. 2 and five other wells, such LCR locations did not exist (Section 4.1.2). Thus, three non-LCR residences supplied in part by Well No. 2 were monitored by the distribution system sampling.

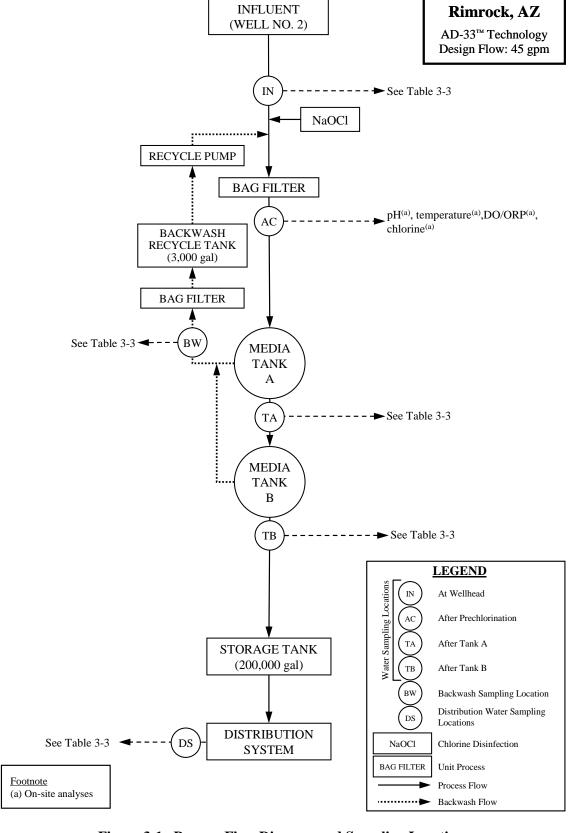


Figure 3-1. Process Flow Diagram and Sampling Locations

The samples were taken following an instruction sheet developed according to the *Lead and Copper Monitoring and Reporting Guidance for Public Water Systems* (EPA, 2002). The homeowners recorded the dates and times of last water usage before sampling and of sample collection for calculation of the stagnation time. All samples were collected from a cold-water faucet that had not been used for at least 6 hr to ensure that stagnant water was sampled.

**3.3.5 Residual Solids.** Because of the very small quantity of solids in backwash wastewater, only spent media was collected for residual solids analyses. A total of three spent media samples were collected from top, middle, and bottom layers of the lead tank (i.e., Tank A) on November 8, 2006. Spent media were sampled using a 5-gal wet/dry shop vacuum that had been thoroughly cleaned and disinfected before sampling. The media collected from each target layer were transferred from the shop vacuum, after mixing with a small garden spade, to a clean 5-gal bucket. A composite sample from each layer was collected into a wide-mouth, 2-gal plastic container for total metal analyses and a Toxicity Characteristic Leaching Procedure (TCLP) test. Metal analyses were conducted on air dried and acid digested samples (see analytes in Table 3-3), and the TCLP test was conducted on an unprocessed sample following the protocol described in the QAPP (Battelle, 2003).

### 3.4 Sampling Logistics

- **3.4.1 Preparation of Arsenic Speciation Kits**. The arsenic field speciation method uses an anion exchange resin column to separate the soluble arsenic species, As(V) and As(III) (Edwards et al., 1998). Resin columns were prepared in batches at Battelle laboratories according to the procedures detailed in Appendix A of the QAPP (Battelle, 2003).
- **3.4.2 Preparation of Sampling Coolers.** For each sampling event, a cooler was prepared with the appropriate number and type of sample bottles, disc filters, and/or speciation kits needed. All sample bottles were new and contained appropriate preservatives. Each sample bottle was affixed with a preprinted, colored-coded label consisting of the sample identification (ID), date and time of sample collection, collector's name, site location, sample destination, analysis required, and preservative. The sample ID consisted of a two-letter code for the specific water facility, the sampling date, a two-letter code for a specific sampling location, and a one-letter code designating the arsenic speciation bottle (if necessary). The sampling locations at the treatment plant were color-coded for easy identification (e.g., orange designated TA). The labeled bottles for each sampling location were bagged separately and packed in the cooler.

In addition, all sampling- and shipping-related materials, such as disposable gloves, sampling instructions, chain-of-custody forms, prepaid and addressed FedEx air bills, and bubble wrap, were included. The chain-of-custody forms and FedEx air bills were complete except for the operator's signature and the sample dates and times. After preparation, the sample cooler was sent to the site via FedEx for the following week's sampling event.

**3.4.3 Sample Shipping and Handling.** After sample collection, samples for off-site analyses were packed carefully in the original coolers with wet ice and shipped to Battelle. Upon receipt, the sample custodian checked sample IDs against the chain-of-custody forms and verified that all samples indicated on the forms were included and intact. Discrepancies noted by the sample custodian were addressed with the plant operator by the Battelle Study Lead. The shipment and receipt of all coolers by Battelle were recorded on a cooler tracking log.

Samples for metal analyses were stored at Battelle's Inductively Coupled Plasma-Mass Spectrometry (ICP-MS) Laboratory. Samples for other water quality analyses by Battelle's subcontract laboratories, including American Analytical Laboratories (AAL) in Columbus, OH and TCCI Laboratories in New

Lexington, OH, were packed in coolers at Battelle and picked up by couriers. The chain-of-custody forms remained with the samples from the time of preparation through analysis and final disposition. All samples were archived by the appropriate laboratories for the respective duration of the required hold time and disposed of properly thereafter.

## 3.5 Analytical Procedures

The analytical procedures described in Section 4.0 of the QAPP (Battelle, 2003) were followed by Battelle ICP-MS Laboratory, AAL, and TCCI Laboratories. Laboratory quality assurance/quality control (QA/QC) of all methods followed the prescribed guidelines. Data quality in terms of precision, accuracy, method detection limit (MDL), and completeness met the criteria established in the QAPP (i.e., 20% relative percent difference [RPD], 80 to 120% recovery, and 80% completeness). The quality assurance (QA) data associated with each analyte will be presented and evaluated in a QA/QC Summary Report to be prepared under separate cover upon completion of the Arsenic Demonstration Project.

Field measurements of pH, temperature, DO, and ORP were conducted by the plant operator using a WTW Multi 340i handheld meter, which was calibrated for pH and DO prior to use following the procedures provided in the user's manual. The ORP probe also was checked for accuracy by measuring the ORP of the standard solution and comparing it to the expected value. The plant operator collected a water sample in a clean, plastic beaker and placed the probe in the beaker until a stable value was obtained. The plant operator also performed free and total chlorine measurements using Hach chlorine test kits following the user's manual.

#### 4.0 DEMONSTRATION SITE AND TECHNOLOGY EVALUATED

# 4.1 Site Description

**4.1.1 Existing Facility**. Seven wells owned by AWC supplied water to a population of 2,556 in Rimrock, AZ. Montezuma Haven Wells No. 1 and 2, with a combined capacity of 90 gpm, were selected for the demonstration study. Figure 4-1 shows photographs taken at the site prior to onset of the demonstration study.

Wells No. 1 and 2 were 6-in in diameter and 270- and 165-ft deep, respectively, both with an open borehole extending from 80 ft below ground surface (bgs). The main supply well, Well No. 3, was 1,000-ft deep and capable of producing a sustainable flow at 315 gpm. Before entering the distribution system, a 12% NaOCl solution was used to maintain a free chlorine residual of about 0.3 mg/L (as Cl<sub>2</sub>).

From Summer 2003 to October 2003, Wells No. 1 and 2 were taken off-line for repairs and redevelopment. It was later discovered that Well No. 1 had become dry, and that Well No. 2 produced a sustainable flow of only 31 gpm. This finding prompted a change to the configuration of the two adsorption tanks of the proposed treatment system from parallel to series (Section 4.2). For the purpose of the demonstration study, Well No. 2 was operated for 12 hr/day during most of the 33-month study period.



Figure 4-1. Predemonstration Site Photographs (Clockwise from Top: Condition in July 2003; Well No. 2 Wellhead after Redevelopment; and Chlorine Shed and Emergency Shower Station)

**4.1.2 Distribution System**. The distribution system was supplied by Montezuma Haven Wells No. 2 and 3, and four other production wells not including Well No. 1, which was out of service. The transmission main was constructed of 6-in-diameter asbestos cement piping. Service lines to the

individual homes were mostly black high-density polyethylene (HDPE) or polyvinyl chloride (PVC) piping (including the distribution sampling locations) with some homes having copper or galvanized steel piping. Well No. 2 water entered the distribution system and blended with Well No. 3 water at the fence line of the treatment plant. Additional blending with water from other supply wells occurred further downstream. The blended water was stored in a 200,000-gal tank.

Compliance samples are taken periodically by AWC from the distribution system. Every month, three samples are collected for bacteria analysis. Under the LCR, samples are collected from customer taps at 14 locations every three years. The monitoring results from AWC's Consumer Confidence Reports (CCRs) for 2003 to 2005 (AWC, 2004; 2005; 2006) are summarized in Table 4-1.

**Table 4-1. Distribution System Water Quality Data**Collected by AWC<sup>(a)</sup>

Parameter	Unit	2003	2004	2005
Alpha Emitters	pCi/L	ND-3.5	2.0-7.8	_
Arsenic	μg/L	20-54	ND-51	ND-48
Barium	mg/L	0.3-0.4	_	_
Chlorine	mg/L	_	_	0.3-0.6
Chromium	μg/L	11–15	_	_
Copper	mg/L	$0.4^{(b)}$	_	0.3
Fluoride	mg/L	0.2-0.4	_	_
Lead	μg/L	_	_	13
Nitrate (as N)	mg/L	ND-0.9	ND-1	ND-0.6
Selenium	μg/L	3.2-4.2	_	-
Sodium	mg/L	38–45	_	_
Radium-226	pCi/L	ND-0.2	_	_
Radon <sup>(c)</sup>	pCi/L	60	_	_
Total Trihalomethanes	μg/L	_	ND-2.5	_
Uranium	μg/L	1.3-4.5	_	_

- (a) All other constituents not detected.
- (b) Sampled in 2002.
- (c) Sampled in 1999.

ND = not detected

**4.1.3 Source Water Quality**. Samples of Well No. 2 water were collected on October 22, 2003, for analyses. The results, along with those provided by the facility to EPA for demonstration site selection and those independently collected and analyzed by EPA, are presented in Table 4-2.

Based on the October 22, 2003, sampling results, Well No. 2 contained 63.6  $\mu$ g/L of arsenic existing solely as As(V). Because As(V) adsorbs better with AD-33<sup>TM</sup> media, prechlorination upstream of the treatment process was not required. The source water pH value was 7.1, which was preferred for effective arsenic adsorption by AD-33<sup>TM</sup> media. In general, pH values at the lower end of the 6.5 to 8.5 range are preferred.

The adsorption capacity of  $AD-33^{^{\intercal}}$  media can be impacted by high levels of competing ions such as silica, phosphate, and sulfate. Concentrations of these ions appeared to be low enough not to affect the media's adsorptive capacity for arsenic. The iron and manganese concentrations (36 and 7.5  $\mu$ g/L, respectively) in Well No. 2 water were sufficiently low; therefore, pretreatment for these metals prior to adsorption was not required.

**Table 4-2. Source Water Quality Data** 

Parameter	Unit	Wells No. 1 & 2 AWC Data <sup>(a)</sup>	Well No. 3 AWC Data	Wells No. 1 & 2 EPA Data	Well No. 2 Battelle Data
Sampling Date	-	Not specified	12/30/02	10/03/02	10/22/03
pН	_	7.2	7.6	NS	7.1
Alkalinity (as CaCO <sub>3</sub> )	Mg/L	334	444	374	378
Hardness (as CaCO <sub>3</sub> )	Mg/L	300	NS	330	335
Chloride	Mg/L	25.0	NS	30.8	32.0
Fluoride	Mg/L	NS	0.2	NS	0.5
Nitrate (as N)	Mg/L	NS	0.1	NS	NS
Sulfate	Mg/L	13.0	12.2	11.6	9.5
Silica (as SiO <sub>2</sub> )	Mg/L	27.8	NS	26.3	24.8
Orthophosphate (as P)	Mg/L	< 0.065 <sup>(b)</sup>	NS	< 0.065	< 0.10
TOC	Mg/L	NS	NS	NS	3.4 <sup>(c)</sup>
As (total)	μg/L	50.0	15.0	52.0	63.6
As (soluble)	μg/L	NS	NS	NS	64.8
As (particulate)	μg/L	NS	NS	NS	< 0.10
As(III)	μg/L	NS	NS	NS	< 0.10
As(V)	μg/L	NS	NS	NS	64.8
Fe (total)	μg/L	170 <sup>(b)</sup>	NS	170	36
Fe (soluble)	μg/L	NS	NS	NS	<25
Al (total)	μg/L	NS	NS	<25	13
Al (soluble)	μg/L	NS	NS	NS	<10
Mn (total)	μg/L	NS	NS	< 0.4	7.5
Mn (soluble)	μg/L	NS	NS	NS	8.1
Na (total)	Mg/L	35.0	93	41.6	40.3
Ca (total)	Mg/L	69.0	NS	80.2	82.8
Mg (total)	Mg/L	31.0	NS	31.6	31.0

<sup>(</sup>a) Provided to EPA for site selection.

TOC = total organic carbon; NS = not sampled

## **4.2** Treatment Process Description

AdEdge's APU-100 system is a fixed-bed downflow adsorption system, which uses Bayoxide<sup>®</sup> E33-S granular ferric oxide (GFO) adsorptive media for arsenic removal from drinking water supplies. Developed by Bayer AG, the media is branded and referred to as AD-33<sup>™</sup> by AdEdge. AD-33<sup>™</sup> is delivered in a dry crystalline form and has received NSF International (NSF) approval for use in drinking water under NSF Standard 61. Table 4-3 presents key physical and chemical properties of the media as provided by the vendor.

The original design of the APU-100 system was for the two adsorption tanks to operate in parallel to treat an anticipated flowrate of 90 gpm. However, because Well No. 1 was no longer producing water, the tanks were reconfigured to operate in series for a design capacity of 45 gpm.

For series operation, the media in the lead tank is generally replaced when it completely exhausts its capacity or when the effluent from the lag tank reaches  $10 \mu g/L$  of arsenic. After rebedding, the lead tank with new media, it is switched to the lag position, and the lag tank with the partially exhausted media is

<sup>(</sup>b) Provided by EPA.

<sup>(</sup>c) Datum questionable.

Table 4-3. Physical and Chemical Properties of AD-33<sup>™</sup> Media

Physical Properties					
Parameter	Value				
Matrix	Iron oxide composite				
Physical Form	Dry granular media				
Color	Amber				
Bulk Density (g/cm <sup>3</sup> ) [lb/ft <sup>3</sup> ]	0.45 [28.1]				
BET Surface Area (m <sup>2</sup> /g)	142				
Attrition (%)	0.3				
Moisture Content (%)	<15 (by weight)				
Particle Size Ddistribution	$10 \times 35 \text{ mesh}$				
Crystal Size (Å)	70				
Crystal Phase	α – FeOOH				
Chemical	Analysis				
Constituents	Weight (%)				
FeOOH	90.1				
CaO	0.27				
MgO	1.00				
MnO	0.11				
$SO_3$	0.13				
Na <sub>2</sub> O	0.12				
TiO <sub>2</sub>	0.11				
SiO <sub>2</sub>	0.06				
$Al_2O_3$	0.05				
$P_2O_5$	0.02				
Cl	0.01				

Source: Bayer AG

BET = Brunauer, Emmett, and Teller

switched to the lead position. In theory, the series operation better utilizes the arsenic removal capacity of the media when compared to parallel system design and operation.

The APU-100 system included a bag filter assembly for sediment removal from source water, two pressure tanks arranged in series with hub and lateral underdrains, a backwash recycle system, piping with an automated valve assembly, and an instrument/control panel with flow meters, pressure and differential pressure ( $\Delta p$ ) gauges, and ball valve sample ports. Skid-mounted on a polyurethane coated, welded steel frame, the system was equipped with the necessary valves and schedule 80 PVC piping to allow the adsorption tanks to be switched from lead to lag position and vice versa. Figure 4-2 is a simplified piping and instrumentation diagram (P&ID) of the treatment system. The system's design features are summarized in Table 4-4. Figures 4-3 and 4-4 show integral components of the treatment and backwash recycle processes, respectively. The major process steps included:

- **Intake**. Source water was supplied by Montezuma Haven Well No. 2 at approximately 31 gpm (Item No. 5 in Figure 4-3).
- **Prechlorination**. Although not required for oxidation, a 12% NaOCl solution was injected into raw water prior to the adsorption tanks at AWC's discretion and expense to attain a target free chlorine residual of 0.3 mg/L (as Cl<sub>2</sub>) in the treated water. The feed system consisted of a 1.5-gal/hr (gph) chemical metering pump with adjustable speed and stroke settings and a 30-gal day tank. The metering pump was interlocked with the well pump so

- that both pumps operated at the same time. AWC also provided an emergency eyewash and shower station for safety measures.
- **Bag Filter Filtration.** After prechlorination, a 25-µm bag filter assembly (FSI model BFN12) with replaceable polypropylene filter bags was used to remove any sediment from source water to protect the treatment equipment (Item No. 1 in Figure 4-3).
- Adsorption. The two 3-ft × 6-ft pressure tanks (Structural model 31214) were configured in series, each containing 22 ft³ of AD-33™ media supported by 4.5 ft³ of gravel underbedding. Although 27 ft³ of media was originally proposed per tank, less media was loaded to provide additional freeboard during backwash. The tanks were constructed of composite fiberglass and rated for a 150-pounds per square inch (psi) working pressure (Item No. 3 in Figure 4-3). Influent, effluent, and backwash piping were connected to a Fleck controller valve (Performance Water Products model 3150 Downflow) at the 6-in flanged connection on the top of each tank (Item 2 in Figure 4-3). The influent water entered the tank via the controller valve, flowed downward through the media bed, collected in the underdrain, and traveled upward through riser piping to the outlet of the controller valve. A restrictive orifice located on the effluent piping from each tank provided a safeguard against filter overrun. Based on 22 ft³ of media and 45 gpm of design flowrate, the EBCT through each media bed would be 3.7 min and the hydraulic loading rate would be 6.4 gpm/ft². Based on the actual flowrate of 30 gpm, the EBCT in each tank was 5.4 min and the hydraulic loading rate was 4.2 gpm/ft².

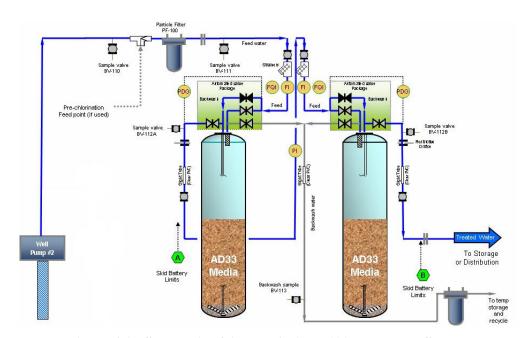


Figure 4-2. Schematic of AdEdge's APU-100 Treatment System

• **Backwash.** Backwash was recommended by the vendor to remove particulates and/or media fines accumulating in the media beds. The process might be initiated either manually or automatically based on a timer (Pentair model 3200NT) or a Δp setting for each tank. After the system was taken offline, upflow backwash using chlorinated water from the well was performed on Tank A followed by Tank B.

• Backwash Wastewater Recycling. Due to lack of sewer or other onsite wastewater discharge options, a backwash recycle loop was included in the system to reclaim the wastewater. The recycling system consisted of a 25-μm bag filter (FSI model BFN12), a 3,000-gal, flat-bottom, HDPE recycle tank with high and low level sensors (Burkert type 8181), and a positive displacement metering pump (ProMinent® Sigma/2 S2BA/S2Ca) (Figure 4-4). A turbine flow meter and a totalizer also were included to monitor flow. Wastewater from the recycle tank was metered into the head of the system between the chlorine injection point and the bag filter assembly at a rate of 0.5 gpm. Relays from the level sensors in the storage tank prevented the tank from overflowing and enabled automatic recycling.

Table 4-4. Design Features for AdEdge's APU-100 Treatment System

Parameter	Value <sup>(a)</sup>	Remarks					
I	Pretreatment						
12% NaOCl (mg/L)	Not required	For providing residuals in					
	_	distribution system					
Bag Filter (μm)	25	For sediment removal					
	Adsorption						
Tank Quantity	2	Series configuration					
Tank Size (ft)	$3 D \times 6 H$	7.1 ft <sup>2</sup> cross-sectional area					
AD-33 <sup>™</sup> Media Volume (ft <sup>3</sup> /tank)	22	27 ft <sup>3</sup> /tank per original design					
Underbedding Volume (ft <sup>3</sup> /tank)	4.5	Gravel					
Maximum Flowrate (gpm)	50						
Design Flowrate (gpm)	45	31 gpm typically expected					
EBCT (min/tank)	3.7	Based on design flowrate					
Water Production (gpd)	32,400	Based on 45 gpm design flowrate					
		and 12 hr/day operation					
Hydraulic Utilization (%)	50	12 hr/day operation					
Water Production (BV/tank/day)	197	Based on 22 ft <sup>3</sup> /tank media					
		volume, 45 gpm design flowrate,					
		and 12 hr/day operation					
Media Capacity to 10-µg/L As Break-	66,000	$1 \text{ BV} = 22 \text{ ft}^3$					
through from Lead Tank (BV)							
Estimated throughput to 10 µg/L	10,860,000	$1 \text{ BV} = 22 \text{ ft}^3 = 165 \text{ gal}$					
As breakthrough from Lead Tank (gal)							
Estimated Media Life (month)	11	Based on media capacity and					
		utilization					
	Backwash						
Frequency (time/month)	1						
Flowrate (gpm)	50						
Hydraulic Loading Rate (gpm/ft <sup>2</sup> )	7						
Duration (min/tank)	15						
Wastewater Production (gal/tank)	750						
Recycle Flowrate (gpm)	0.5						

D = diameter; H = height

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<sup>(</sup>a) AdEdge's original design modified from parallel to series reconfiguration.



**Figure 4-3. Treatment System Components** 

 [1] Inlet Bag Filter, [2] Fleck Controller Valve, [3] Adsorption Tank;
 [4] Instrument/Control Panel; [5] Piping from Wellhead, [6] Piping to Distribution System, and [7] System Enclosure)



Figure 4-4. Backwash Recycling System Components

(From Left: Backwash Bag Filter; 3,000-gal Storage Tank with Level Sensors; and Recycle Pump)

#### **4.3** Treatment System Installation

This section summarizes the system engineering, installation, startup, and shakedown activities, which were carried out by AdEdge and its subcontractor, Fann Environmental, of Prescott, AZ. Installation of the system was completed in mid-April 2004 and reconfiguration of the system from parallel to series was completed in mid-May 2004.

- **4.3.1 System Engineering and Permitting.** Engineering plans for the system permit application were submitted to ADEQ for approval on December 11, 2003. The plans included P&IDs and system specifications, control panel schematics, equipment cut sheets, and drawings of a site plan, treatment plan, and piping plan. After the Approval to Construct was granted on February 18, 2004, a construction permit was applied for and approved by Yavapai County in mid-March 2004. Upon completion of system installation, as-built drawings were submitted to ADEQ and Approval of Construction was granted on April 29, 2004. Following the system reconfiguration, updated information was submitted to ADEQ and a second approval was granted on June 15, 2004.
- **4.3.2 System Installation, Startup, and Shakedown.** Upon arrival of the treatment system on March 30, 2004, the vendor's subcontractor performed off-loading and installation. The installation activities including connections to the existing intake and distribution piping, hydraulic testing (with no media), and media loading were completed on April 20, 2004. Figure 4-5 shows photographs from the media loading. Due to the loss of Well No. 1, piping from Well No. 3 was installed to allow additional flow for media backwash. Because some lubricating oil from the pump shaft was found in Well No. 3 water, a decision was made to forgo this supplementary input for backwash. Battelle provided operator training on data and sample collection from May 6 to 7, 2004.



Figure 4-5. Gravel Underbedding (Left) and AD-33<sup>™</sup> Media (Right) Loading

Because of the reduced flowrate from 90 to 31 gpm, the corresponding EBCT across each tank would have almost tripled from 3.7 to 10.6 min (based on 22 ft<sup>3</sup> of media loaded in each tank) if the system configuration had remained in parallel. To evaluate the system performance near the originally designed EBCT and to fully utilize the media capacity, the tank configuration was changed to series. The required modifications were made in mid-May 2004, and shakedown and startup completed in early June 2004. After the system was sanitized and passed bacteria tests, the performance evaluation began with commencement of Media Run 1A on June 24, 2004.

**4.3.3 System Enclosure.** After the treatment system was installed, a sun shed with a base of  $12 \text{ ft} \times 15 \text{ ft}$  and a height of 9.5 ft was built by AWC over the system in late-May 2004 (Figure 4-6). Constructed of a galvanized steel frame by Versa-Tube, the sun shed was anchored to the concrete pad and sheeted with 29-gauge steel with a specially coated surface. The shed was pre-engineered with loading capacities of 90 mph for wind and  $30 \text{ lb/ft}^2$  for snow. From late-November to mid-December 2004, the sides and ends of the sun shed were enclosed with metal covering; exposed piping was insulated; and heat lamps were installed within the building for added protection from below-freezing temperatures.



Figure 4-6. System Enclosure

(Clockwise from Left: System Installed on Concrete Pad in April 2004; Sun Shed Built in May 2004; and Enclosure Completed in December 2004)

#### 5.0 RESULTS AND DISCUSSION

# 5.1 System Operation

**5.1.1 Service Operation.** The operational data collected during the performance evaluation study are tabulated and attached as Appendix A. Key parameters are summarized in Table 5-1. The system operated with Tank A in the lead position from June 24, 2004, through August 9, 2006 (designated as Run 1A). Starting from August 30, 2006, the system was turned off for well pump maintenance and Tank A rebedding (Section 5.1.3). System operation resumed for Run 1B on November 27, 2006, with Tank B containing partially exhausted media in the lead position and newly-rebedded Tank A in the lag position. Sampling was discontinued and the performance evaluation completed on March 28, 2007 after the results of monitoring confirmed on-spec system operation following the media changeout.

From June 24, 2004 through March 28, 2007, the system operated for a total of 12,024 hr on a 12-hr/day schedule from 8:00 a.m. to 8:00 p.m., except for the winters when the system operated at night from 11:00 p.m. to 11:00 a.m. to prevent system components from being damaged due to freezing ambient conditions, and from December 4, 2006, to March 7, 2007, when the system operated 24 hr/day to compensate for anticipated water shortage due to maintenance on a nearby well. The 12 hr/day run time was preset on a timer. Meanwhile, an hour meter was installed on November 4, 2004 to track total system run time.

Table 5-1. Summary of APU-100 System Operations

Parameter	Unit	Value					
Evaluation Period	Date	06/24/04-03/28/07 <sup>(a)</sup>					
Treatment Operation							
Total Operation Time	hr	12,024					
Daily Operating Time	hr/day	12 or 24					
Average Flowrate [Range]	gpm	30 [16–36]					
Average Hydraulic Loading Rate [Range]	gpm/ft <sup>2</sup>	4.2 [2.3–5.1]					
Average EBCT [Range]	min/tank	5.4 [4.6–10.3]					
Average Δp across Tank [Range]	psi/tank	4.8 [1.5–6.5]					
Media Run Length to 10-μg/L As following Lead Tank	1,000 gal/BV/yr	6,448/39,180 <sup>(b)</sup> /0.8					
Media Run Length to 10-μg/L As following Lag Tank	1,000 gal/BV/yr	17,164/52,150 <sup>(c)</sup> /2.1					
Media Run Length until Tank A Rebedding	1,000 gal/BV/yr	17,426/52,950 <sup>(c)</sup> /2.2					
Media Run Length after Tank A Rebedding	1,000 gal/BV/yr	4,717/14,330 <sup>(c)</sup> /0.3					
Backwash Operation	n						
Backwash Count	No	42 <sup>(d)</sup>					
Time Elapsed between Two Consecutive Backwash Cycles	Month	1–3					
Average Flowrate [Range]	gpm	47 [22–54]					
Average Hydraulic Loading Rate [Range]	gpm/ft <sup>2</sup>	6.6 [3.1–7.6]					
Average Backwash Duration [Range]	min/tank	15 [15–17]					
Wastewater Generated	gal/tank	727 [245–996]					
Total Wastewater Generated	gal	33,100					
Average Recycle Flowrate [Range]	gpm	0.5 [0.5–1.5]					

- (a) System turned off on 08/30/06 and restarted on 11/27/06 after rebedding.
- (b) Based on flow meter of lead tank and volume of media in lead tank.
- (c) Based on flow meter of lag tank and volume of media in both tanks.
- (d) Count for both tanks combined.

During Run 1A, the system produced 6,448,000 gal (or 39,180 BV [1 BV =  $22 \, \mathrm{ft^3}$ ]) and 17,164,000 gal (or 52,150 BV [1 BV =  $44 \, \mathrm{ft^3}$ ]) of water at 10 µg/L of arsenic breakthrough from the lead and lag tanks, respectively. After media changeout, an additional 4,717,000 gal (or 14,330 BV [1 BV =  $44 \, \mathrm{ft^3}$ ]) was produced before sampling was discontinued. System flowrates ranged from 16 to 36 gpm and averaged 30 gpm and the corresponding hydraulic loading rates ranged from 2.3 to 5.1 gpm/ft² and averaged 4.2 gpm/ft². Flowrates as low as 16 gpm were measured when decreasing production by Well No. 2 was observed from June through August 2006 (Figure 5-1). Following the well maintenance, system flowrates returned to the typical values of around 30 gpm. The resulting EBCTs ranged from 4.6 to 10.3 min/tank and averaged 5.4 min/tank, compared to the design value of 3.7 min/tank (note that the design EBCT was calculated based on 22 ft³ of media in each tank and 45 gpm of system flowrate).

 $\Delta p$  readings across each tank ranged from 1.5 to 6.5 psi and averaged 4.8 psi (Figure 5-1). As expected,  $\Delta p$  readings across each tank decreased with decreasing flowrates.  $\Delta p$  readings across Tank A were generally higher (i.e., about 0.5 psi) than those across Tank B, suggesting removal of some sediment by Tank A (the lead tank). During system startup, hydraulic testing performed with no media in the tanks measured a  $\Delta p$  reading of 4.3 psi at 33 gpm. This  $\Delta p$  was thought to have been caused primarily by the Fleck controller valve installed at the top of each tank, as demonstrated by the hydraulic testing performed on another APU-100 system at Rollinsford, NH (Oxenham et al., 2005). The  $\Delta p$  readings across each tank between two consecutive backwash events did not increase significantly, indicating that few particulates or media fines, if any, were accumulating in the media beds.

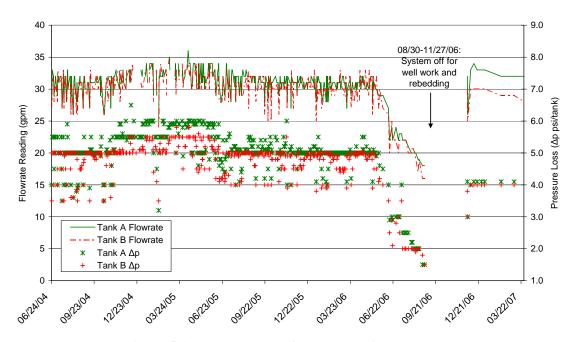


Figure 5-1. Flowrate Readings and Δp Across Tanks

**5.1.2 Backwash Operation**. The system was programmed to backwash automatically at 15 psi of  $\Delta p$  or 27 (for Tank A) or 28 (for Tank B) days of system operation. For the first one and a half months of operation, the system experienced four unscheduled backwash events, possibly caused by >15 psi pressure spikes resulting from the operation of the nearby Well No. 3. Because these backwash events took place unexpectedly, the operator was not onsite to record relevant operational data and take samples. In order to record backwash data and collect backwash wastewater samples, the  $\Delta p$  relays were disengaged on

August 12, 2004, so that backwash would be controlled solely by the 27/28-day timer. Since then, three more unscheduled backwash events occurred before the first set of samples could be taken on October 20, 2004, when the tanks were manually backwashed. After another backwash event was missed on November 15, 2004, the 27/28-day timer setting was changed to 30 days. After November 15, 2004, no other unscheduled backwashes occurred except on December 6, 2005, possibly due to a power outage. The vendor checked the backwash settings, tested the process, and ensured normal operation on December 14, 2005.

Backwash was performed with raw water at 47 gpm or 6.6 gpm/ft<sup>2</sup> (on average). Initially, a monthly backwash was performed as recommended by the vendor. After approximately one year of system operation, the backwash frequency was reduced to quarterly in August 2005. The decrease in backwash frequency was determined mainly by the minimal  $\Delta p$  increase across the tanks between two consecutive backwash events. The backwash duration was generally 15 min/tank, producing approximately 730 gal/tank. However, flows as low as 22 gpm or 3.1 gpm/ft<sup>2</sup> were used for backwash on August 16, 2006, due to decreasing well production. Nonetheless,  $\Delta p$  increase following the backwash was not observed. After media changeout, the system was thoroughly backwashed with anticipated flowrates following the well maintenance.

Several problems occurred with the backwash recycle pump and a control valve. In mid-August 2004, after a leak on the backwash recycle line was repaired, the shut-off valve from the backwash recycle pump was inadvertently left unopened. Consequently, when the recycle pump came on during a backwash on August 23, 2004, it was dead-headed, causing damages to the diaphragm. The recycle pump was fixed on September 1, 2004, and a pressure relief valve was installed on the pump discharge to prevent future problems. A control valve for Tank A began sticking after backwash on June 8, 2005, causing the tank not to return to service mode after backwash. The valve was repaired by the vendor on July 26, 2005. Additional problems were experienced with the backwash recycle pump after the media changeout on November 27, 2006. The system stopped recognizing the programmable logic controller (PLC) input signal from the level sensor in the recycle tank used to operate the recycle pump. Due to scheduling conflicts and troubleshooting difficulties, this issue was not resolved by the vendor until March 28, 2007.

- **5.1.3 Media Changeout.** A media changeout request was made to the vendor and its subcontractor on August 16, 2006. Due to scheduling conflicts and media disposal and other issues, the changeout did not take place until almost three months later on November 8, 2006. After the tanks were drained and the pumps and isolation valves were turned off, the freeboards of Tanks A and B were measured at 17.3 and 19.0 in, respectively, from the flange at the top of each tank to the top of each media bed. The spent media and underbedding in Tank A were sampled and/or removed as described in Section 3.3.5. The tank was then half-filled with water before loading of 4.5 ft<sup>3</sup> of underbedding gravel and 22 ft<sup>3</sup> of virgin media through a large funnel. The tank was then completely filled with water and the media soaked to eliminate entrapped air. After the media was thoroughly backwashed, the freeboard of the tank was measured at 16.5 in, which was comparable to the 17.3-in measurement before rebedding. It appeared that minimum media loss was experienced over the 2.1 yr of system operation.
- **5.1.4 Residual Management.** The backwash wastewater recycling system (Section 4.2) reclaimed nearly 100% of the backwash wastewater produced. Recycling was accomplished by blending the supernatant in the recycle tank with the influent water between the chlorine injection point and bag filter at a rate of 0.5 gpm (see Figure 3.1). Solids and media fines produced during backwash were removed by a 25 µm bag filter, which required replacement after each backwash. Any remaining solids not removed by the bag filter were allowed to settle in the recycle tank; accumulation was so negligible that removal and disposal of these solid were not needed during the course of the 33-month study period. If required, solid removal from the recycle tank would be a considerable undertaking because the flat-bottom is not

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conducive to solid collection, and because the only access point to solid is at the top of the approximately 8-ft tall tank. The associated O&M requirements for sites with higher solid loading could easily be accommodated by using a conical-bottom recycle tank.

Spent media was the only quantifiable residual produced by operation of the treatment system. After treating 17,500,000 gal of water in 2.2 yr, approximately 620 lb of spent media and 450 lb of gravel underbedding were removed from the lead tank. After they were subjected to and passed the TCLP test (Section 5.2.4), the media were disposed of by Waste Management, Inc.

**5.1.5 System/Operation Reliability and Simplicity.** Unscheduled backwashes, problems with the recycling pump and one control valve (Section 5.1.2), and delays on media changeout (Section 5.1.3) were the primary source of concerns during this performance evaluation study. Other O&M issues encountered were problems with the chlorine injector, inlet and outlet pressure gauges, recycle flow meter, and backwash totalizer. The pressure gauges, flow meter, and totalizer were damaged as a result of unusually cold weather in late November 2004. The inlet and outlet pressure gauges broke a second time on December 19, 2005. The unscheduled downtime for system component repairs amounted to about 1 to 2% of the total system run time.

The simplicity of system operation and operator skill requirements are discussed according to pre- and post-treatment requirements, levels of system automation, operator skill requirements, preventative maintenance activities, and frequency of chemical/media handling and inventory requirements.

- 5.1.5.1 Pre- and Post-Treatment Requirements. Although not required for treatment, chlorine was injected upstream of the adsorption tanks to provide disinfection throughout the treatment train and a chlorine residual within the distribution system. A 25-µm bag filter following the chlorine injection point was used to remove sediment from the inlet water. No post-treatments were required.
- 5.1.5.2 System Automation. The system was equipped with a backwash control to initiate backwash automatically by a timer and/or a  $\Delta p$  setpoint. Because the system experienced a number of unscheduled backwashes at the beginning of system operation (Section 5.1.2), the automatic backwash control was disabled so that the operator could take backwash data and samples during each manual backwash. Backwash wastewater recycling also was accomplished automatically as operation of the recycle pump was controlled by the level sensors in the reclaim tank.
- 5.1.5.3 Operator Skill Requirements. Under normal operating conditions, the daily demand on the operator was typically 20 min for visual inspection of the system and recording of operational parameters on the log sheets. During backwash, the operator spent approximately 2 hr onsite to collect operational data and perform backwash wastewater sampling. Under normal system operation, backwash can be initiated automatically, as such, the operator's presence would not be necessary.

In Arizona, operator certifications are classified by grade on a scale of 1 (least complex) to 4 (most complex) according to facility type, size, complexity, and population served (ADEQ, 2005). One AWC operator had a Level 4 Distribution Grade and a Level 4 Treatment Grade, and the other had a Level 4 Distribution Grade and a Level 3 Treatment Grade. After receiving proper training by the vendor during the system startup, the operator understood the system and was able to work with the vendor to troubleshoot and perform minor onsite repairs.

**5.1.5.4 Preventative Maintenance Activities.** Preventative maintenance tasks recommended by the vendor are summarized in Table 5-2. The system had few moving parts that required regular maintenance per the O&M manual. Replacement bag filters were installed without the use of special equipment. With vendor's concurrence, the frequency for backwash and bag filter replacement was reduced from monthly

to quarterly or upon 6 to 7 psi  $\Delta p$  rise (Section 5.1.2). Many of the tasks such as sampling and analysis and operational data recording including pressure checks were conducted more frequently due to the nature of the demonstration project.

Because the backwash bag filter assembly was located before the recycle tank, bag filters had to be replaced after each backwash event. If the backwash bag filter had been located after the recycle tank, its replacement frequency could be reduced by allowing solids to settle in the recycle tank. To have the bag filter after the recycle tank, however, could increase the need for solids removal from the recycle tank.

**Table 5-2. Recommended Routine Maintenance Activities** 

	Frequency				
Task	Daily	Weekly	Monthly	Quarterly	
Ensure Normal System Operation	V				
Check Site Security	V				
Check for Leaks and Integrity					
Read Inlet/Outlet Pressure and Δp Gauges					
Check Backwash Recycle Tank Level					
Record Totalizer Throughput					
Record System Flowrate					
Check Effluent Water Clarity					
Backwash and Replace Backwash Bag Filter			$\sqrt{(a)}$	$\sqrt{(b)}$	
Check Inlet Bag Filter for Debris/Sediment					
Conduct Sampling and Analysis <sup>(c)</sup>			V	√	
Perform Equipment Maintenance <sup>(d)</sup>					

Source: AdEdge, 2004

- (a) At beginning of system operation.
- (b) or 6 to 7 psi  $\Delta p$ .
- (c) Frequency depending on anticipated proximity to arsenic breakthrough.
- (d) Per O&M manual.

5.1.5.5 Chemical/Media Handling and Inventory Requirements. Chemical usage was not required except for disinfection. AWC coordinated the supply of 12% NaOCl supply with Hill Brothers Chemical Co., refilled the day tank when required, and provided an emergency eyewash and shower station for safety measures. Rebedding of the lead tank was required when the lag tank effluent reached 10-μg/L of arsenic after 2.1 yr of system operation or 17,146,000 gal of water treated. Media sampling and removal were labor-intensive, taking 45 labor hr (i.e., 15 hr each for three people). In contrast, media loading took only 9 labor hr (3 hr each for three people).

# **5.2** System Performance

**5.2.1 Treatment Plant Sampling**. The treatment plant water was sampled on 64 occasions (including five duplicate samples), with field speciation performed on 16 occations. Table 5-3 summarizes the analytical results of arsenic, iron, and manganese at the IN, TA, and TB sampling locations. Table 5-4 summarizes the results of the other water quality parameters including those measured onsite at the IN, AC, TA, and TB sampling locations. Appendix B contains a complete set of analytical results.

Table 5-3. Summary of Arsenic, Iron, and Manganese Results

Parameter	Sampling	Sample	Concentration (µg/L)			Standard
(Figure, if any)	Location	Count	Minimum	Maximum	Average	Deviation
As (total) (Figure 5-3)	IN	64	43.8	81.4	59.7	9.5
	TA	64	0.7	56.1	-	-
	TB	64	0.2	31.7	-	-
As (soluble)	IN	16	50.2	66.7	57.3	5.1
	TA	16	0.9	41.9	ı	-
	TB	16	0.3	7.3	ı	-
As (particulate) (Figure 5-2)	IN	16	< 0.1	21.7	3.8	6.4
	TA	16	< 0.1	15.2	3.0	4.7
	TB	16	< 0.1	1.1	0.3	0.3
As(III) (Figure 5-2)	IN	16	0.3	2.2	1.1	0.5
	TA	16	0.3	2.7	1.0	0.6
	TB	16	0.2	1.9	0.8	0.5
As(V) (Figure 5-2)	IN	16	48.1	65.5	56.2	5.1
	TA	16	< 0.1	41.7	-	-
	TB	16	< 0.1	7.0	-	-
Fe (total)	IN	59 <sup>(a)</sup>	<25	27.2	<25	1.9
	TA	60	<25	31.1	<25	3.5
	TB	60	<25	55.7	<25	7.7
Fe (soluble)	IN	16	<25	<25	<25	-
	TA	16	<25	<25	<25	-
	TB	16	<25	<25	<25	-
Mn (total)	IN	60	< 0.1	1.6	0.3	0.3
	TA	60	< 0.1	1.2	0.1	0.2
	TB	59 <sup>(b)</sup>	< 0.1	0.9	0.1	0.2
Mn (soluble)	IN	16	< 0.1	1.1	0.3	0.3
	TA	16	< 0.1	0.7	0.1	0.2
	TB	16	< 0.1	0.6	0.1	0.1

<sup>(</sup>a) One outlier (i.e.,  $127 \mu g/L$  on 09/22/04) omitted.

One-half of the detection limit used for nondetect results and duplicates included for calculations.

5.2.1.1 Arsenic. Total arsenic concentrations in source water ranged from 43.8 to 81.4 µg/L and averaged 59.7 µg/L, with As(V) as the predominant soluble species at 56.2 µg/L (Table 5-3). Figure 5-2 contains bar charts showing the concentrations of particulate arsenic, As(III), and As(V) for each speciation sampling event. (Note that results for TA and TB in Figure 5-2 were plotted on reduced scales compared to IN to better show the effluent species.) The arsenic concentrations measured during this period were consistent with that of source water collected on October 22, 2003 (Table 4-2). Generally, low levels of particulate arsenic and As(III) existed in raw water at average concentrations of 3.8 and 1.1 ug/L, respectively. However, highly elevated particulate arsenic concentrations (e.g., up to 21.7 ug/L on March 8, 2006) were observed beginning in February 2006, possibly due to overextraction from the source well. Most of particulate arsenic was trapped in the media beds (and later removed during backwash) as evident by the decrease in concentrations from 3.8 to 3.0 and then to 0.3 µg/L at IN, TA, and TB, respectively. As much as 2.2 µg/L As(III) was measured in source water and not completely oxidized with chlorine addition. Because the AD-33<sup>TM</sup> media had little capacity for As(III), up to 2.7 and 1.9 µg/L of As(III) were measured in the tank effluent even in the presence of 0.3 mg/L (as Cl<sub>2</sub>) of free chlorine (Table 5-3).

<sup>(</sup>b) One outlier (i.e.,  $12.4 \mu g/L$  on 02/02/05) omitted.

**Table 5-4. Summary of Other Water Quality Parameter Results** 

Parameter	Sampling		Sample	(	Concentration	1	Standard
(Figure, if any)	Location	Unit	Count	Minimum	Maximum	Average	Deviation
4.11 11 11	IN	mg/L	60	330	414	379	14
Alkalinity	TA	mg/L	60	345	424	380	12
(as CaCO <sub>3</sub> )	TB	mg/L	60	351	410	381	13
	IN	mg/L	16	0.2	0.4	0.3	0.1
Fluoride	TA	mg/L	16	0.2	0.5	0.3	0.1
	TB	mg/L	16	0.2	0.4	0.3	0.1
	IN	mg/L	16	8.1	11	9.7	0.6
Sulfate	TA	mg/L	16	7.8	10	9.6	0.6
	TB	mg/L	16	8.1	11	9.7	0.7
0.1.1.1.	IN	mg/L	11 <sup>(a)</sup>	< 0.06	< 0.10	< 0.06	0.0
Orthophosphate	TA	mg/L	11 <sup>(a)</sup>	< 0.06	< 0.10	< 0.06	0.0
(as P)	TB	mg/L	11 <sup>(a)</sup>	< 0.06	< 0.10	< 0.06	0.0
	IN	μg/L	14	<10	20.4	10.2	5.8
Phosphorus	TA	μg/L	14	<10	21.4	11.7	5.9
(as P)	TB	μg/L	14	<10	10.9	<10	2.1
	IN	mg/L	60	23.6	27.6	25.6	0.8
Silica	TA	mg/L	60	23.9	27.5	25.5	0.9
(as SiO <sub>2</sub> )	TB	mg/L	60	23.7	27.4	25.4	0.9
	IN	mg/L	16	0.2	0.6	0.2	0.1
Nitrate	TA	mg/L	16	0.2	0.3	0.2	0.0
(as N)	TB	mg/L	16	0.2	0.3	0.2	0.0
	IN	NTU	60	0.1	0.7	0.2	0.2
Turbidity	TA	NTU	60	0.1	1.6	0.3	0.3
1 dicitally	TB	NTU	60	0.1	3.4	0.3	0.5
	IN	S.U.	50	6.8	7.1	6.9	0.1
	AC	S.U.	50	6.8	7.6	7.0	0.2
pH	TA	S.U.	50	6.7	7.1	7.0	0.1
	TB	S.U.	50	6.8	7.1	6.9	0.1
	IN	°C	51	18.6	26.1	21.0	1.3
	AC	°C	51	19.2	24.5	20.8	1.0
Temperature	TA	°C	51	19.4	26.7	20.9	1.2
	TB	°C	51	19.6	24.0	21.0	1.1
	IN	mg/L	48	3.2	6.0	3.9	0.5
T-0	AC	mg/L	48	3.0	6.8	4.2	0.9
DO	TA	mg/L	48	3.0	6.6	3.9	0.6
	TB	mg/L	48	3.0	6.9	3.9	0.6
	IN	mV	48	148	510	305	125
0.00	AC	mV	48	365	646	597	46
ORP	TA	mV	48	565	688	630	29
	ТВ	mV	48	470	710	639	39
E CII :	AC	mg/L	51	0.2	0.5	0.4	0.1
Free Chlorine	TA	mg/L	51	0.2	0.5	0.3	0.1
(as Cl <sub>2</sub> )	TB	mg/L	51	0.2	0.5	0.3	0.1
T. 1 Cl. 1	AC	mg/L	50	0.2	0.7	0.4	0.1
Total Chlorine	TA	mg/L	50	0.2	0.6	0.4	0.1
(as Cl <sub>2</sub> )	TB	mg/L	50	0.2	0.6	0.4	0.1
m . 1.77 . 1	IN	mg/L	16	287	384	327	26
Total Hardness	TA	mg/L	16	298	397	334	27
(as CaCO <sub>3</sub> )	TB	mg/L	16	298	377	331	22

**Table 5-4. Summary of Other Water Quality Parameter Results (Continued)** 

Parameter	Sampling		Sample	(	Concentration	1	Standard
(Figure, if any)	Location	Unit	Count	Minimum	Maximum	Average	Deviation
Ca Hardness	IN	mg/L	16	171	241	198	16
(as CaCO <sub>3</sub> )	TA	mg/L	16	161	236	199	19
(us cuco <sub>3</sub> )	TB	mg/L	16	174	235	199	14
M II 1	IN	mg/L	16	110	151	129	11
Mg Hardness (as CaCO <sub>3</sub> )	TA	mg/L	16	112	161	135	12
(as CaCO <sub>3</sub> )	TB	mg/L	16	115	149	132	11

<sup>(</sup>a) Data invalid from 01/01/05 to 10/03/05 due to laboratory issue.

One-half of the detection limit used for nondetect results and duplicates included for calculations.

The key parameter for evaluating the effectiveness of the APU-100 system was the arsenic concentration in the treated water. Shown in Figure 5-3, the arsenic breakthrough curves are presented as gallons of water treated with the number of bed volumes to arsenic breakthrough at  $10 \,\mu\text{g/L}$  from the lead and lag tanks specified. Bed volumes of the lead tank were calculated based on the amount of media in the lead tank only; however, bed volumes of the lag tank were calculated based on the combined media volume in both lead and lag tanks since water exiting the lag tank had been treated by this entire media volume. Initially, the lead tank (TA) removed the majority of arsenic from source water until its capacity gradually decreased. Afterwards, the lag tank (TB) served as an effective polishing unit, removing arsenic to <10  $\,\mu\text{g/L}$  throughout most of Run 1A. Both breakthrough curves in Figure 5-3a gradually increased over time, but effluent concentrations of the lead tank were largely influenced by the fluctuating source water arsenic concentrations (including elevated levels of particulate arsenic) near the end of Run 1A. The lag tank, however, was able to dampen the fluctuations observed and produce rather steady arsenic concentrations in the tank effluent.

Breakthrough of arsenic at  $10 \mu g/L$  from Tank A occurred at 39,180 BV, which was 60% of the vendor-estimated working capacity, i.e., 66,000 BV, based on  $22 \text{ ft}^3$  of media in the lead tank as shown in Table 4-4. In theory, the media should have outperformed the projection, because the system was operating with a longer EBCT than was originally designed (i.e.,  $5.4 \text{ vs. } 3.7 \text{ min/tank [based on } 22 \text{ ft}^3 \text{ of media and } 45 \text{ gpm of design flowrate]}$ ), which potentially could help increase the media run length.

Breakthrough of arsenic at  $10 \,\mu\text{g/L}$  from Tank B, or the entire system, occurred at 52,150 BV (1 BV = 44 ft<sup>3</sup>), which was 33% higher than the 39,180 BV observed following the lead tank. The average EBCT of the system was 10.8 min, which was twice as long as that of the lead tank only. The longer EBCT apparently benefited arsenic adsorption, extending the media run length for 33%.

Starting with a partially exhausted Tank B in the lead position and newly rebedded Tank A in the lag position on November 27, 2006, Media Run 1B was carried out to ensure that normal system operations continued following the media changeout. Results of the initial sampling indicated that the arsenic concentration in Tank B had dropped from 9.8 (as lag tank on August 9, 2006) to 6.2 µg/L (as lead tank on November 28, 2006). Because intraparticle mass transport is believed to be a rate-limiting step (Badruzzaman et al., 2004; Lin and Wu, 2001), the system downtime from August 30 to November 27, 2006, might have temporarily facilitated and improved pore diffusion by allowing additional time for arsenic on the media surface to move into the pores and provide more easily accessible sites for adsorption. Total arsenic concentrations continued to be monitored through March 7, 2007, when the sampling was discontinued and the performance evaluation was completed (Figure 5-3b).

**5.2.1.2 Iron and Manganese.** Low concentrations of total and soluble iron and manganese existed in source water and throughout the treatment system. Total iron concentrations were near or below the

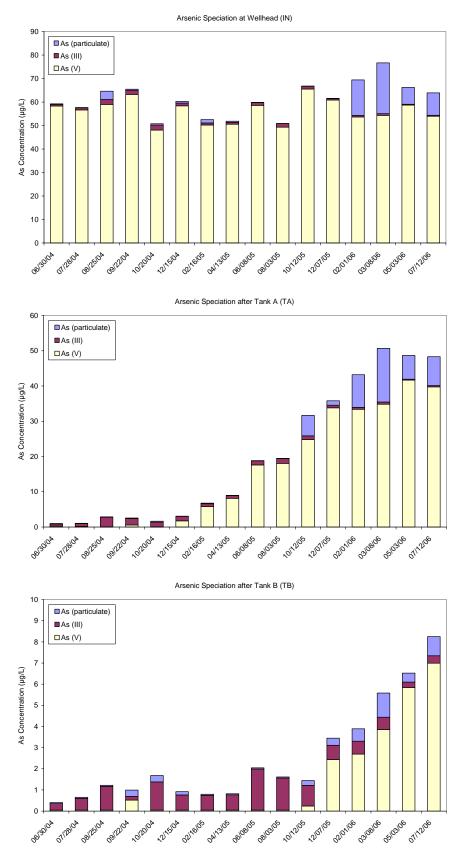


Figure 5-2. Arsenic Species During Media Run 1A at Wellhead, After Tank A, and After Tank B

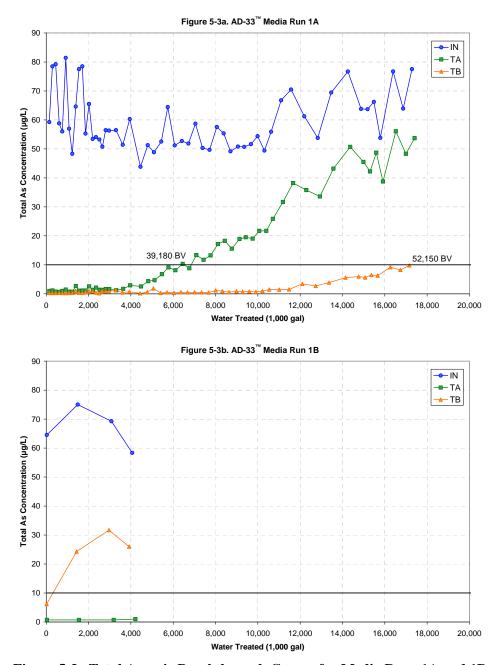


Figure 5-3. Total Arsenic Breakthrough Curves for Media Runs 1A and 1B

25- $\mu$ g/L method reporting limit for all samples with one exception (i.e., 127  $\mu$ g/L at IN on September 22, 2004). Soluble iron concentrations were <25  $\mu$ g/L for all samples. Total manganese levels ranged from <0.1 to 1.6  $\mu$ g/L except for one outlier (i.e., 12.4  $\mu$ g/L at TB on February 2, 2005), with the majority existing as soluble manganese. Average total and soluble manganese levels in raw water were reduced from 0.3  $\mu$ g/L to 0.1  $\mu$ g/L after the adsorption tanks, indicating some removal by the media.

**5.2.1.3 Onsite Measurements.** Average pH values across the treatment train were 6.9 to 7.0, which were the lowest among the 12 Round 1 demonstration sites (Table 1-1). Near neutral pH is desirable for

adsorptive media, which, in general, have greater arsenic removal capacities when treating lower-pH water. Source water was oxidizing as indicated by the relatively high DO and ORP levels, which averaged 3.9 mg/L and 305 millivolts (mV), respectively. These measurements might explain the absence of As(III) in source water. As a result of prechlorination, ORP readings at the AC, TA, and TB locations increased to the range of 365 to 710 mV. Free and total chlorine residuals measured at the TA and TB locations were comparable to those measured at the AC location, indicating little or no chlorine consumption by the AD-33<sup>TM</sup> media.

- **5.2.1.4 Other Water Quality Parameters.** Alkalinity, fluoride, sulfate, orthophosphate, phosphorus, silica, nitrate, and turbidity concentrations were relatively low and remained fairly constant throughout the treatment train. Total hardness ranged from 287 to 397 mg/L (as CaCO<sub>3</sub>), consisting of approximately 60% of calcium hardness and 40% of magnesium hardness. Hardness was not significantly affected by the treatment process.
- **5.2.2 Backwash Water Sampling**. Backwash wastewater was sampled in 13 sampling events. The analytical results are presented in Table 5-5. (Note that Sampling Events 11, 12, and 13 followed a modified sampling procedure as described in Section 3.3.3.) pH values of the backwash wastewater, ranging from 7.0 to 7.9, were somewhat higher than those of raw water (Table 5-4). Arsenic concentrations in the backwash wastewater from Tank A and, especially, Tank B, were lower than those in raw water used for backwash (except for Event 13), indicating removal of arsenic by the media during backwash. During Event 13, overextraction of the source well most likely contributed to the elevated particulate arsenic concentration as discussed in Section 5.2.1.1. The backwash wastewater from Tank A contained higher amounts of turbidity and particulate iron and manganese than from Tank B, suggesting filtering of most of particulates by Tank A. Nonetheless, the amounts removed by Tank A were minute, as reflected by the low levels of TSS, i.e., <1 to 16 mg/L, in the backwash wastewater. The sampling events did not show significant differences for pH or TDS between the two tanks.
- **5.2.3 Distribution System Water Sampling**. The results of the 20 distribution system water sampling events (including four baseline [BL] events) are summarized in Table 5-6. Water from the source well, Well No. 2, blended with water from up to five other wells within the distribution system would impact the water quality at the three sampling locations as discussed in Section 3.3.4. The most noticeable change since system startup was the decrease in arsenic concentrations. After system startup, arsenic concentrations, which ranged from 20.8 to 80.1 μg/L and averaged 48.8 μg/L during baseline sampling, were reduced to the range of 2.2 to 45.6 μg/L and average of 19.3 μg/L. Water samples from the distribution system exhibited significantly higher arsenic concentrations than those following the treatment system due to the contribution of untreated water from other wells which also contained arsenic (Tables 4-1 and 4-2).

pH, alkalinity, manganese, lead, and copper concentrations after system startup were comparable to baseline levels except for the pH results for Event BL2 at all locations and the manganese result for Event BL1 at DS2. Furthermore, lead and copper concentrations were well below the action levels of 15 and  $1,300 \, \mu g/L$ , respectively. Although iron levels appeared to decrease somewhat compared to the baseline levels, the system operation probably did not influence this reduction since Well No. 2 source water contained little or no iron.

Table 5-5. Backwash Water Sampling Results

																ล
	(əlqnlos) uJV	µg/L	0.1	<0.1	0.5	0.1	<0.1	0.3	<0.1	0.5	0.1	0.1	<0.1	0.1	<0.1	
	(Istot) nIM	ηg/L	SN	SN	SN	SN	SN	SN	SN	SN	SN	SN	<0.1	0.3	1.0	
	Fe (soluble)	ηg/L	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	
	Fe (total)	µg/L	SN	SN	SN	SN	SN	SN	NS	SN	SN	NS	58.2	<25	123	
	As (particulate)	µg/L	SN	SN	SN	SN	SN	SN	SN	SN	SN	NS	<0.1	<0.1	4.2	
Tank B	(sldulos) sA	ηg/L	2.7	1.6	4.5	13.2	7.5	13.2	10.2	20.0	16.6	18.7	23.9	36.1	37.0	
L	(Istot) sA	µg/L	SN	SN	SN	SN	NS	SN	SN	SN	SN	NS	23.3	33.7	41.2	
	SST	mg/L	SN	SN	SN	SN	SN	SN	NS	SN	SN	SN	$NA^{(a)}$	5	7	
	SQT	mg/L	442	306	464	444	$NA^{(a)}$	512	470	$NA^{(a)}$	486	434	$NA^{(a)}$	422	428	
	Turbidity	NTU	6.5	25	4.3	7.6	$NA^{(a)}$	3.4	$6.6^{(b)}$	$NA^{(a)}$	7.1	8.9	$NA^{(a)}$	SN	SN	1.1
	Hq	S.U.	7.3	7.1	7.1	7.2	$NA^{(a)}$	7.4	7.2	$NA^{(a)}$	7.0	7.3	$NA^{(a)}$	7.2	7.2	
	Mn (soluble)	ηg/L	0.1	0.4	<0.1	<0.1	<0.1	9.0	<0.1	0.3	0.1	0.3	$NA^{(c)}$	0.5	<0.1	1.1
	(Istot) nIM	µg/L	SN	SN	SN	SN	SN	SN	SN	SN	SN	SN	12.8	1.8	9.1	
	Fe (soluble)	µg/L	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	$NA^{(c)}$	<25	<25	C C L
	Fe (total)	ηg/L	SN	SN	SN	SN	SN	SN	SN	SN	SN	SN	423	273	1,456	1.1
1	sA (particulate)	µg/L	SN	SN	SN	SN	SN	SN	SN	SN	SN	SN	$NA^{(c)}$	9.4	44.5	1
[ank A	(sldulos) sA	μg/L	48.2	48.0	50.7	51.7	52.2	55.4	47.6	49.6	48.2	55.5	$NA^{(c)}$	59.3	52.8	1 1.
L	(Istot) sA	µg/L	SN	SN	SN	SN	SN	SN	SN	SN	SN	SN	55.6	9.89	97.3	
	SST	mg/L	SN	SN	SN	SN	SN	SN	SN	SN	SN	NS	7	5	16	
	SQT	NTU mg/L mg/L	486	358	462	446	414	564	486	466	440	438	430	420	420	
	<b>Viibidiu</b> T	NTU	22	45	19	16	37	19	44 <sub>(b)</sub>	32	52	28	SN	SN	SN	
	Hq	S.U.	7.3	7.1	7.1	7.3	7.2	7.4	7.2	2.7	0.7	7.9	7.3	7.2	7.2	1 1
	Sampling Event	Date	10/20/04	12/15/04	01/19/05	02/16/05	03/16/05	04/13/05	05/11/05	20/80/90	20/90/20	08/17/05	11/14/05	02/12/06	05/11/06	1.1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	Sa J	No.	1	2	3	4	5	9	7	8	6	10	11	12	13	A T A

NA = not available; NS = not sampled; TDS = total dissolved solids; TSS = total suspended solids

(a) Insufficient sample for analysis due to loss during transit.

(b) Analyzed outside of hold time.

(c) Laboratory error.

Table 5-6. Distribution System Sampling Results

			na	T	7.	2.	-2	.1	7	7.	116	£.	.2	4	.3	5.	.5	.5	.3	9:	6.	7	.2	1:
			пЭ	T/gn T	2.68	64.2	142	121	107	. 46.7		43.3	68.2	124	72.3	999	49.5	35.5	123	32.6	42.9	107	82.2	1 <0.1
	4)		9d	hg/L	1.3	1.0	2.1	1.1	2.1	1.4	2.4	1.3	1.8	2.7	1.3	1.3	0.7	0.8	2.1	1.0	1.2	2.0	1.9	<0.1
	dence		пМ	µg/L	0.3	9.0	0.3	0.3	0.1	0.3	1.8	0.7	0.5	0.8	4.8	0.5	0.5	0.3	1.4	0.2	0.2	<0.1	0.4	<0.1
DS3	Resi	1st Draw	9 <del>Т</del>	µg/L	<25	<25	<25	47.9	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25
Q	Non-LCR Residence	1st ]	s <b>A</b>	hg/L	37.1	49.5	47.0	52.7	22.7	45.6	23.3	21.3	15.6	14.4	6.6	15.7	15.6	6.6	20.6	19.8	39.1	19.6	23.4	27.3
	Non		Alkalinity (as CaCO <sub>3</sub> )	mg/L	407	419	336	406	413	395	381	394	418	394	360	401	410	410	431	392	418	414	418	383
			Hd	S.U.	7.2	8.2	7.1	7.1	7.2	6.9	7.0	7.0	7.1	7.2	7.0	7.3	7.2	7.5	7.4	7.1	6.9	6.9	7.0	7.2
			Stagnation Time	hr	8.5	0.9	7.8	7.0	5.3	7.5	7.3	6.5	6.3	9.0	8.3	7.5	8.5	8.0	8.3	8.0	0.6	8.8	7.9	8.8
			Сu	ηg/L	106	64.0	128	34.4		2.99	33.8	129		139	142	32.4	147	47.2	49.0		131	113	107	10.0
			9d	ηg/L	1.6	2.4	3.8	8.0		4.3	2.9	7.0		9.9	3.9	1.6	3.9	2.3	7.3		5.0	5.2	4.3	0.7
	nce		пМ	hg/L	68.4	9.0	0.3	0.2	lable	0.3	0.3	3.0	lable	1.1	0.7	0.1	3.4	0.5	8.0	lable	0.3	0.2	0.2	0.1
7	Reside	raw	<del>9</del> Т	µg/L	182	<25	<25	40.2	unavai	<25	<25	<25	unavai	<25	<25	<25	<25	<25	<25	unavai	<25	<25	<25	<25 0.1
DS2	Non-LCR Residence	1st Draw	s <b>A</b>	η J/gη	20.8	48.4	57.0	52.2	Homeowner unavailable	28.5	9.3	. 8.61	Homeowner unavailable	21.8	21.2	21.2	20.0	20.3	33.9	Homeowner unavailable	23.6		13.6	17.6
	Non-		Alkalinity (as CaCO <sub>3</sub> )	mg/L µ	405   2	407 2	371	406	Home	395 2	373	410	Home	403 2	396	437   2	442 2	437 2	413	Home	427 2	378	405	392
			Hq	S.U. n	7.2	8.5	7.2	7.1		6.9	6.9	6.9		7.2	7.1	7.3	7.3	7.5	7.3		6.9	7.0		7.3
			Stagnation Time	hr	7.0	11.3	0.11	8.6		10.0	10.5	0.6		0.6	7.0	6.5	9.5	10.0	17.0		17.5	7.0	9.5	10.0
			Cu	hg/L	119	24.2	24.0	31.3	147	112	194	9.66	79.5	52.5	38.3	89.4	51.8	0.79	58.0	108	118	25.9	24.7	36.1
			9d	ηg/L	2.3	0.5	1.2	0.5	4.4	8.8	4.4	2.9	1.4	4.1	1.1	1.1	1.3	3.4	1.7	1.5	2.4	1.5	6.0	0.4
	nce		иМ	η J/gμ	1.2	8.0	0.2	0.5	<0.1	0.3	1.3	9.4	0.4	0.7	0.5	<0.1	0.4	0.3	6.0	0.3	0.2	<0.1	0.2	
1	Non-LCR Residen	.aw	Fe	µg/L µ		<25	<25	46.1	<25   <	<25	<25	<25	<25	<25	<25	<25 <	<25	<25	<25	<25	<25	<25 <	<25	<25 <0.
DS1	CR	1st Draw	sA.	µg/L µ	38.5	49.3	80.1	52.8 4	1.7	5.4	- 0.81	22.9	21.2	. 15.0		6.0 <sup>(e)</sup> <	26.1	20.2	6.5	18.0	22.3	2.2	24.8	5.9
	Non-I		Alkalinity (as CaCO <sub>3</sub> )	mg/L µ	387   3	411 4	367 8	394 5	373 1	379 1	402 1	406 2	418 2	370 1	408 2	392 6	433 2	418 2	404	405	409 2	NA <sup>(f)</sup>		383 ;
			Hd	S.U. m	7.1   3	8.9	7.2 3	7.1   3	7.2   3	6.9	7.2 4	6.7 4	7.0 4	7.1 3	7.1 4	7.5   3	7.3   4	7.6 4	7.6	7.2 4	7.0 4	7.3 N		7.2 3
			Stagnation Time	hr S	12.0	14.0	34.0	23.0	11.0	20.5	12.0	19.0	7.5	0.6	9.5	0.6	11.0	10.0	6.0	10.01	9.5	7.0	0.9	11.0
	I	1	Sampling Event	Date	12/17/03 <sup>(a)</sup>	01/06/04	01/21/04	02/05/04	07/28/04 <sup>(b)</sup>	08/26/04 <sup>(b)</sup>	09/22/04 <sup>(c)</sup>	10/20/04	11/17/04	$12/15/04^{(b)}$	01/12/05 <sup>(b,d)</sup>	$02/09/05^{(b)}$	03/09/02 <sub>(p)</sub>	04/06/05 <sup>(b)</sup>	05/04/05 <sup>(b)</sup>	(q)\$0/80/90	07/07/05 <sup>(b)</sup>	08/09/02 <sub>(p)</sub>	09/14/05	$10/12/05^{(g)}$
			<b>9</b> 1	No.	BL1	BL2	BL3	BL4	1	2	3	4	5	9	7	8	6	10	111	12	13	14	15	16

(a) Sample DS2 collected from nearby residence. (b) Sample DS1 collected on previous day. (c) Sample DS1 taken on 09/30/04; pH analyzed outside of hold time. (d) Samples DS1 and DS2 switched for this event; correct results shown. (e) Rerun result similar to original result. (f) Insufficient sample for analysis. (g) Samples DS1, DS2, and DS3 collected on 10/11/05, 10/13/05, and 10/12/05, respectively.

Lead action level = 15 µg/L; copper action level = 1.3 mg/L; BL = baseline sampling; NA = data not available

**5.2.4 Spent Media Sampling.** The treatment system was shut down on August 30, 2006, and spent media samples were collected from Tank A on November 8, 2006, and analyzed as discussed in Section 3.3.5. TCLP and total metals results are presented in Tables 5-7 and 5-8, respectively. The TCLP results indicated that only barium was detected at 1.5 mg/L and that the media was non-hazardous and could be disposed of in a sanitary landfill.

The ICP-MS results of the spent media indicated that the media, as expected, contained mostly iron at 569 mg/g (as Fe), or 904 mg/g (as FeOOH), which matches closely with the 90.1% (by weight) specified by Bayer AG (Table 4-3). The spent media also contained trace levels of Ca, Mg, Mn, Si, Al, and P at 3.8, 1.4, 2.0, 0.23, 0.33, and 1.5 mg/g, respectively, which, except for Mn and P, also match closely with Bayer AG's analyses. Trace amounts of Mn and P, both detected in source water, apparently were removed by the AD-33<sup>TM</sup> media, increasing the respective loadings from the baseline levels of 0.11 and 0.02% to 0.52 and 0.34%. The spent media also appeared to have removed some amounts of Cu and Pb from source water, as evidenced by the decreasing loadings from the top to the bottom of Tank A.

The arsenic loading on the spent media based on the ICP-MS results was 8.3 mg/g (average across bed from Table 5-8). For comparison to the spent media results, the adsorptive capacity was calculated by dividing the arsenic mass represented by the area between the influent and lead tank breakthrough curves, as shown in Figure 5-3a, by the amount of dry media in each tank. The dry weight of the media, i.e., 527 lb, was calculated based on a wet weight of 620 lb (i.e.,  $22 \text{ ft}^3$  of media at  $28.1 \text{ lb/ft}^3$ ) and a maximum moisture content of 15% (Table 4-3). Using this approach, the arsenic loading for the spent media was 10.4 mg/g, of which 80% was recovered via ICP-MS analysis. The arsenic loading on the media in Tank B was calculated to be 4.9 mg/g, which further supported the decision to rebed only Tank A due to the remaining capacity of the media in Tank B. This value (4.9 mg/g) was close to that of 5.2 mg/g calculated for the media in Tank A at the  $10-\mu\text{g/L}$  arsenic breakthrough point (as of March 30, 2005).

Table 5-7. TCLP Results of a Composite Spent Media Sample

	Concentration
RCRA Metal	mg/L
Arsenic	< 0.10
Barium	1.5
Cadmium	< 0.010
Chromium	< 0.010
Lead	< 0.050
Mercury	< 0.0020
Selenium	< 0.10
Silver	< 0.010

RCRA = Resource Conservation and Recovery Act

Table 5-8. Metals' Analysis of Spent Media

Tank A	Mg	Al	Si	P	Ca	Fe	Mn	Ni	Cu	Zn	As	Cd	Pb	As/Fe
Location	mg/g	mg/g	μg/mg											
Top	1.4	0.39	0.25	1.4	4.0	579	2.1	0.13	0.57	1.2	8.7	< 0.0005	0.03	15.0
Middle	1.3	0.29	0.19	1.4	3.8	557	2.0	0.13	0.36	1.2	8.6	< 0.0005	0.01	15.4
Bottom	1.4	0.30	0.26	1.6	3.7	570	1.9	0.13	0.11	1.3	7.8	0.00	0.00	13.7

### 5.3 Cost Information

- **5.3.1 Facility Cost.** As part of the facility requirements, AWC provided an enclosure, an eye wash station, and a backwash wastewater recycling system. The total cost for the sun shed structure was \$13,677, which included \$3,500 for materials and \$10,177 for labor to assemble the structure. The backwash recycling system cost \$11,546 for material, engineering, and installation. These costs were not included in the cost analysis because they were funded separately by AWC and not included under the demonstration project.
- **5.3.2 System Cost.** The system cost was evaluated based on the capital cost per gpm (or gpd) of design capacity and the O&M cost per 1,000 gal of water treated. The capital investment for the equipment, site engineering, and installation was \$88,307 (Table 5-9). The equipment cost was \$63,785 (or 72.2% of the total capital investment), which included the cost for two pressure tanks,  $44 \text{ ft}^3$  of AD- $33^{\text{TM}}$  media, piping and valves, instrumentation and controls, field services (for operator training, technical support, and system shakedown), miscellaneous materials and supplies, and a change order for system reconfiguration from parallel to series operation.

Table 5-9. Capital Investment for AdEdge's APU-100 System

			% of Capital
Description	Quantity	Cost	Investment Cost
Equipmer	ıt		
Adsorption Tanks	2	\$21,800	_
AD-33 <sup>™</sup> Media	44 ft <sup>3</sup>	\$10,690	_
Piping and Valves	1	\$7,520	_
Instrumentation and Controls	1	\$4,575	_
O&M Manual, Operator Training, Technical Support	1	\$3,800	_
Procurement, Assembly, Labor, Shakedown	1	\$12,575	_
Freight	1	\$1,855	_
Change Order for System Reconfiguration	1	\$880	_
Equipment Total	ı	\$63,785	72.2%
Engineerii	ng		
Materials, Submittals, FedEx, Postage, Supplies	1	\$75	_
Oversight, Specification Preparation	1	\$3,420	_
Design, Drawings, Coordination	1	\$4,970	_
Review Meeting, Airfare, Lodging, and Meals	1	\$1,017	_
Change Order for System Reconfiguration	ı	\$1,890	_
Engineering Total	ı	\$11,372	12.9%
Installatio	n		
Subcontractor	1	\$6,750	_
Vendor Labor	4 days	\$3,040	_
Vendor Travel	4 days	\$1,290	_
Change Order for System Reconfiguration	_	\$2,070	_
Installation Total	Ī	\$13,150	14.9%
Total Capital Investment <sup>(a)</sup>	_	\$88,307	100%

\$11,546 for backwash recycling system not included.

The engineering cost included preparation of the engineering plans, system layout and footprint, drawings of site and piping plans, and equipment cut sheets for the permit application submittal (Section 4.3.1). The cost also included resubmission of the redesigned system layout and piping plans following reconfiguration to ADEQ for approval. The engineering cost of \$11,372 was 12.9% of the total capital investment.

The installation cost included equipment and labor to unload and install the APU-100 system, perform the piping tie-ins and electrical work, load and backwash the media, and reconfigure the system (Section 4.3.2). The installation cost of \$13,150 was 14.9% of the total capital investment.

The capital cost of \$88,307 was normalized to \$1,962/gpm (\$1.36/gpd) of design capacity using the system's design capacity of 45 gpm (or 64,800 gpd). The capital cost also was converted to an annualized cost of \$8,335/yr by multiplying a capital recovery factor (CRF) of 0.09439 based on a 7% interest rate and a 20-yr return period. If the system had operated for 24 hr/day, 7 day/week at the 45-gpm design flowrate to produce 23,652,000 gal/yr, the unit capital cost would have been \$0.35/\$1,000 gal. During the first year, the system produced approximately 8,505,000 gal of water (based on flow meter after the lead tank), so the unit capital cost increased to \$0.98/1,000 gal.

**5.3.3 O&M Cost.** The O&M cost included media replacement and disposal, incremental chemical supply, electricity, and labor as summarized in Table 5-10. Because the system was under warranty, no additional cost was incurred for repairs. Due to the long duration of Media Run 1A, it was most cost-effective to replace the media of the lead tank only when the lag tank effluent reached 10  $\mu$ g/L of arsenic. The media replacement cost of one tank was \$10,908, including \$5,830 for 22 ft<sup>3</sup> of AD-33 media (or \$265/ft<sup>3</sup>), \$4,240 for labor, and \$375 for spent media analysis, and \$463 for freight.

By averaging the media replacement cost over the life of the media, the cost per 1,000 gal of water treated was calculated as shown in Figure 5-4. Note that after the partially exhausted lag tank is switched to the lead position with the newly rebedded tank in the lag position, the run length for the subsequent run will be shorter than the initial run, thus resulting in an increased replacement frequency and cost than presented in Table 5-10.

Chemical usage consisted of NaOCl, which was added to provide disinfection and residual in the distribution system. Since NaOCl was not required for the treatment process, its usage was not included in the O&M cost. Electricity consumption was approximately 2.07 kWh/day based on electric meter readings for one day (or 12 hr) of system operation (including usage from the recycle pump). Therefore, the electricity cost was \$0.008/1,000 gal of water treated. The routine, non-demonstration related labor activities (Section 5.1.5.4), including preventative maintenance activities and repairs, consumed 15 to 20 min/day. Based on this time commitment and a labor rate of \$21/hr, the labor cost was \$0.22/1,000 gal of water treated.

By averaging the total O&M cost over the life of the media, the cost per 1,000 gal of water treated was plotted as a function of the media run length as shown in Figure 5-4. Note that the bed volumes were calculated based on the quantity of media in both tanks (i.e., 44 ft<sup>3</sup> or 330 gal).

Table 5-10. O&M Cost for AdEdge's APU-100 System (Run 1A)<sup>(a)</sup>

Cost Category	Value	Remarks
Medi	ia Replacement and	Disposal
Media Cost (\$)	\$5,830	\$265/ft <sup>3</sup> ; 22 ft <sup>3</sup> for one tank
Labor Cost (\$)	\$4,240	
Spent Media Analysis (\$)	\$375	Including TCLP test
Travel (\$)	\$0	None
Freight (\$)	\$463	
Subtotal (\$)	\$10,908	
Media Replacement and Disposal Cost		Based on 17,164,000 gal until 10-μg/L
(\$/1,000 gal)	\$0.64	arsenic breakthrough from lag tank
	Chemical Usage	?
Chemical Cost (\$)	\$0.000	No additional chemicals required
	Electricity	
Electricity Cost (\$/kWh)	\$0.089	Rate provided by AWC
Electricity Usage (kWh/day)	2.07	Based on 12 hr/day operation
Electricity Cost (\$/1,000 gal)	\$0.008	
	Labor	
Labor (hr/week)	1.6	15 to 20 min/day, 5 day/week
Labor Cost (\$/1,000 gal)	\$0.22	Labor rate = \$21/hr
		Based upon media run length at 10-µg/L
Total O&M cost (\$/1,000 gal)	\$0.86	arsenic breakthrough

<sup>(</sup>a) O&M cost based upon replacement of lead tank media only.

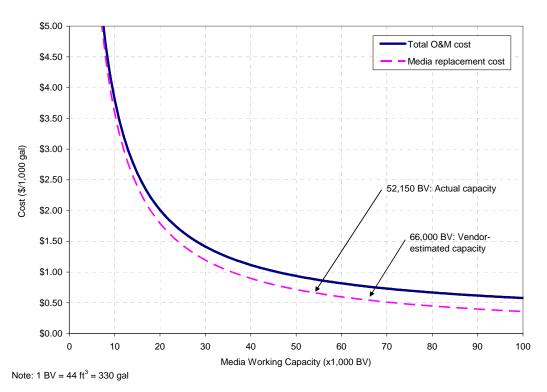


Figure 5-4. Media Replacement (Lead Tank) and Total O&M Cost (Run 1A)

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## APPENDIX A OPERATIONAL DATA

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

					Tank A F	A Flow Meter			Tank B F	Tank B Flow Meter		Р	Н		Pressure		Re	Recycling
Date and Time	Hour	Lead/L	Well #3	Flowr	Totalizer	Elow	Nolime	Flowr	Totalizer	Elow	Nolime	٨	<u> </u>	Į d	Between	Outlet	Flow	Totalizer
1	hr	ag A/B	On/Off	gpm	5	gal		gbm		gal		-	+	psig	psig	psig	gpm	gal
06/24/04 12:32	NA	A/B	ΝA	28	23971	ΨN	NA	27	23294	AN	NA	4.0	3.5	105	104	100+	0	0
06/25/04 11:30	NA	A/B	NA	33	44991	21020	128	31	44375	21081	64	5.5	2.0	98	96	92	0	0
06/28/04 09:17	NA	A/B	NA	32	108441		513	32	108075	84781	258	5.5	2.0	100	96	93	0	0
06/29/04 09:19	¥.	A/B	Ψ.	29	131386		653	28	130974	107680	327	4.5	4.0	105	103	100+	1.5	287
06/30/04 16:01	¥ S	A/B	¥ ∑	3	166117	142146	864	90	165692	142398	433	5.0	2.0	19	100	06	0	511
07/02/04 14:56	ξŽ	A/B	Z Z	32	209871		1130	33	209636	186342	566	5.5	5.0	9 2	96	98	0	511
07/06/04 13:30		A/B	NO	29	297899		1665	28	297866	274572	834	4.0	4.0	105	109	100+	0	511
07/07/04 09:00	NA	A/B	OFF	32	312011		1750	33	311809	288515	877	5.5	4.5	100	95	94	0	511
07/08/04 16:32		A/B	ΝΑ	32	348968		1975	32	349009	325715		5.0	2.0	100	26	93	0	511
07/09/04 13:35		A/B	NA	31	365938	341967	2078	31	366086	342792	1042	2.0	2.0	100	26	94	0	511
07/12/04 13:30		A/B	Ν	32	433271		2487	31	433584	410290	1247	5.0	2.0	100	96	92	0	511
07/13/04 10:00		A/B	ΝA	32	449425		2585	32	449865	426571	1296	5.0	5.0	100	92	93	0	511
07/14/04 09:30	ΑN	A/B	ΑN	32	470700		2715	32	471247	447953	1361	5.5	2.0	100	93	92	0	511
07/15/04 13:30	NA	A/B	NO	30	500630		2897	31	500527	477233	1450	4.5	4.5	101	100	87	0.5	851
07/16/04 14:25	NA	A/B	NO	27	525019		3045	27	524715	501421	1524	3.5	3.5	110	110	100+	0.5	1220
07/19/04 09:30	NA	A/B	ΝΑ	32	584077		3404	33	583614	560320	1702	5.5	2.0	66	36	92	0	1290
07/20/04 08:57	ΝΑ	A/B	NO	28	605379		3533	27	604867	581573	1767	4.0	3.5	102	104	104	0	1290
07/21/04 14:02	A	A/B	ΑN	31	637557		3729	30	637111	613817	1865	2.0	4.9	100	97	94	0	1290
07/22/04 16:12	NA	A/B	ΑN	32	664233		3891	32	663800	640506	1946	2.0	2.0	66	92	93	0	1290
07/23/04 14:48	NA	A/B	ΑN	32	683833	659862	4010	31	683350	660056	2006	2.0	4.5	100	96	94	0	1290
07/26/04 09:16	NA	A/B	NA	28	740859		4356	28	740026	716732	2178	4.0	4.0	102	102	101	1	1420
07/27/04 14:12	NA	A/B	ΝΑ	32	772923		4551	32	772091	748797	2275	5.9	2.0	100	92	93	1	1910
07/28/04 09:46	A A	A/B	AN	33	787316		4639	32	786508	763214	2319	5.5	2.0	100	92	92	0	2060
07/29/04 09:01	¥:	A/B	ΨZ:	30	808295		4766	30	807403	784109	2382	5.0	5.0	9	96	94	0	2060
07/30/04 16:18	ΑA	A/B	ΑN	31	844137		4984	31	843320	820026	2492	2.0	2.0	100	96	94	0	2060
08/02/04 10:29	NA	A/B	NA	32	890668		5318	31	898410		2659	2.0	2.0	100	96	06	0	2060
08/03/04 09:27	NA	A/B	NA	32	919909		5444	31	919248		2722	5.0	4.5	100	96	06	0	2060
08/04/04 09:47	AA	A/B	ΝΑ	27	943057		5585	26	942185	918891	2792	4.0	3.6	105	103	96	0	2060
08/05/04 08:58	AA	A/B	ΝA	32	963804		5711	30	962970	939676	2855	2.0	5.0	100	96	90	0	2060
08/06/04 14:25	NA	A/B	NA	30	996229		2908	30	995478	972184	2954	2.0	2.0	100	86	90	0	2060
08/09/04 09:45	NA	A/B	N O	26	1055151	1031180	6266	26	1054232	1030938	3132	3.6	3.6	103	104	66	0	2060
08/10/04 16:09	NA	A/B	OFF	31	1089574		6475	30	1087899	1064605	3235	2.0	2.0	100	86	06	0.5	2130
08/11/04 11:09	Α V	A/B	OFF	32	1102913		6557	31	1100798	1077504	3274	2.0	2.0	100	97	06	0.5	2330
08/12/04 09:19	¥ :	A/B	OFF F	32	1122569		9299	31	1120172	1096878	3333	5.0	5.0	9 5	97	8	0.5	2630
08/13/04 17:18	¥.	A/B	7.	30	1.160528	_	/069	30	115/685	1134391	3447	2.0	2.0	200	16	90	0	2840
08/16/04 09:00	Ϋ́	A/B	NO.	28	1214460		7234	26	1210860	1187566	3608	3.8	3.8	105	103	86	0	2840
08/17/04 12:00	ΑĀ	A/B	OFF	31	1240824		7395	30	1236957	1213663	3688	2.0	4.8	100	86	06	0	2840
08/18/04 09:00	¥	A/B	NO :	28	1259075		7505	56	1255175	1231881	3743	3.9	3.5	105	103	97	0	2840
08/19/04 11:30	Y E	A/B	NO.	29	1284888		7662	29	1280719	1257425	3821	4.0	3.9	101	101	96	0	2840
08/20/04 15:34	Ϋ́	A/B	OFF	30	1315490		7848	31	1310625	1287331	3911	2.0	2.0	100	86	06	0	2840
08/23/04 10:18	AA	A/B	OFF	32	1375391		8212	31	1369612	1346318	4091	2.0	4.5	100	96	06	AA	NA
08/24/04 12:31	A	A/B	OFF	31	1401393	`	8370	30	1395087	1371793	4168	2.0	4.5	100	96	06	0	2840
08/25/04 09:12	¥	A/B	OFF	31	1418118		8472	30	1411570	1388276	4218	2.0	4.5	100	97	06	0	2840
08/26/04 13:54	Α	A/B	OFF	31	1449870	1425899	8665	30	1442950	1419656	4313	2.0	4.5	100	97	68	0	2840
08/27/04 15:31	Ϋ́	A/B	OFF	31	1475337	1451366	8820	31	1468239	1444945	4390	2.0	4.6	100	26	06	0	2840

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

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1690905 5138 1702278 5172 1736433 5276
1725572 1702278 1759727 1736433 1780911 1757617 1835049 1811755
11065     27       11200     31       11337     33       11470     31
1820898 11065 1843150 11200 1865616 11337 1887475 11470 1920125
121 587 446
32 1867 32 1867 31 18896 31 19114
90 OFF
ABB
<b>XXXXXXX</b>
09/02/04 13:54 09/03/04 12:42 09/08/04 10:57 09/09/04 17:29 09/10/04 16:45 09/14/04 09:43 09/14/04 09:30 09/16/04 08:22

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

			_	ומוויע	TATION MELE							;		LICOSTIC		6	
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	eter ag	Well #3	ate	Totalizer	Cum. Flow	Volume	ate	Totalizer	Cum. Flow	Volume	TA	HB is	Inlet	Tanks	Outlet	Rate	Totalizer
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11:17	+	-	31	1557388		9318		1549642	1526348	4638	5.0		100	97	06	0	2840
11:00	H	H	32	1578093	ľ	9444		1570127	1546833	4700	5.5		100	26		0.5	3100
	NA A/B	3 OFF	32	1605790		9612		1597517	1574223	4783	5.0		100	96		0	3370
21	+	4	30	1625872		9734		1617330	1594036	4843	5.0		100	97		0	3370
~!	-	_	30	1723558		10328		1714199	1690905	5138	5.0	5.0	100	97	90	0	3370
			31	1734996	1711025	10398	31	1725572	1702278	5172	5.0	5.0	100	97		0	3370
		3 OFF	31	1769316		10606		1759727	1736433	5276	5.0		100	26		0	3370
			31	1790558	1766587	10735	31	1780911	1157617	5340	5.0		100	96	06	0	3370
	_	_	27	1844869	1820898	11065	27	1835049	1811755	2029	3.9	3.5	102	103	66	0	3370
		3 OFF	32	1867121	1843150	11200	31	1857243	1833949	5572	5.1	5.0	100	95		0	3370
			31	1889587	1865616	11337	33	1879663	1856369	5640	5.1	2.0	100	95		0	3370
08:22			31	1911446		11470	31	1901462	1878168	5707	5.5		100	96		0	3370
	NA A/B		31	1944096	1920125	11668	31	1933954	1910660	5805	5.1	2.0	100	36	06	0	3370
	_	_	31	2011723	1987752	12079	30	2001410	1978116	6010	5.0	4.9	100	96	91	0	3370
	H		31	2029216	2005245	12185	30	2018904	1995610	6063	5.0	4.9	100	96	91	0	3370
	NA A/E		31	2050996		12318		2040690	2017396	6130	5.0	4.9	100	96	91	0	3370
			31	2074455	2050484	12460	30	2064162	2040868	6201	5.0	4.9	100	96	91	0	3370
			31	2101154	2077183	12623	30	2090817	2067523	6282	4.9	4.8	100	26	91	0	3370
			32	2167484		13026	32	2156478	2133184	6481	5.0	4.8	100	96		0.5	3630
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09/30/04 11:16 N		_	31	2236812		13447		2225389	2202095	6691	5.0		100	97		0.5	4690
	4	_	31	2264087		13613		2252590	2229296	6774	5.0		100	97		0	4849
10/05/04 10:42 N	1	3 OFF	32	2348918		14128	31	2337120	2313826	7030	5.0		100	96		0	4849
		_	29	2383918		14341		2372015	2348721	7136	4.9		102	100		0	4849
		_	32	2394302		14404		2382373	2359079	7168	5.2		100	96		0	4849
	-	_	31	2417168	•	14543	29	2405125	2381831	7237	5.5		100	96		0	4849
10/12/04 17:29 N	NA A/B	NO S	27	2515357		15140		2502458	2479164	7533	4.0		102	104		0	4849
	+	_	26	2538203		15279	26	2525203	2501909	7602	3.5		104	107		0	4849
	+	4	26	2561400		15419		2548271	2524977	7672	4.0		103	105		0	4849
	A/B	4	31	2644969		15927	31	2631513	2608219	7925	5.0		100	98		0	4849
	+	4	31	2667528		16064	32	2654020	2630726	7993	5.1	5.0	100	97	91	0 0	4849
10/20/04 10:35 N	NA A/B	75	31	2682128	2658157	16153	31	266/888	2644594	8035	5.1	9.4 0.4	100	76	9	0.5	4870
┸	+	+	27	2706630		16840		7784677	6200002	0100	0.0		5 5	90	•	3 0	5323
┸	+	+	2 5	2827402		17036		2811839	2788545	8473	5.4	5.0	100	76		0 0	6323
	<u> </u>	_	31	2840201	2816230	17114		2824366	2801072	8511	5.0	5.0	100	96		0	6323
			27	2864858		17264	29	2848575	2825281	8584	4.0	3.6	109	105	1	0	6323
10/29/04 14:18 N	NA A/B	3 OFF	32	2895024	2871053	17447	31	2878185	2854891	8674	4.6	4.6	100	86	66	0	6323
		Ц	31	2966104	2942133	17879	32	2948057	2924763	8887	5.5	5.1	100	96		0	6327
		NO 8	29	2982700		17980		2964350	2941056	8936	4.0	4.0	105	101	96	0	6327
			31	3002182		18098		2983630	2960336	8995	5.1	5.0	100	86		0	6327
	3.2 A/B	3 OFF	32			18289		3014434	2991140	9088	5.0	5.0	100	86		0	6327
11/05/04 12:36 13	_		32	3052755		18405	30	3033038	3009744	9145	5.1	2.0	100	97	86	0	6327
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EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

				L	Tank A F	k A Flow Meter			Tank B F	Tank B Flow Meter		dР			Pressure		Re	Recycling
Date and Time	Hour	Lead/L		Flowr				Flowr			Bed				Between		Flow	
	Meter	ag	Well #3	ate	Totalizer	Cum. Flow	Volume	ate	zer	Cum. Flow	Volume	۲.	$^+$	lnlet	Tanks	Outlet	Rate	Totalizer
	ηľ	A/B	On/Off	gpm	gal			gpm	gal	gal		psi		psig	psig	psig	gpm	gal
11/09/04 11:19	59.9	A/B	OFF	32	3143725		18958	31	3122431	3099137	9416	5.5	2.0	100	97		0	6330
11/10/04 16:57	77.7	A/B	OFF	32	3177995	3154024	19166	32	3156140	3132846	9519	5.5	2.0	101	96		0	6330
11/12/04 17:15	102.0	A/B	OFF	31	3225113	3201142	19453	33	3202655	3179361	0996	5.5	2.0	100	96		0	6330
11/15/04 18:03	139.1	A/B	OFF	30	3296170		19885	33	3272583	3249289	9873	2.0	2.0	101	66	1	0.5	6451
11/16/04 10:12	143.6	A/B	OFF	32	3304356		19934	31	3280723	3257429	2686	5.9	5.1	100	97		0.5	6565
11/17/04 09:46		A/B	OFF	32	3326877		20071	28	3303126	3279832	9962	5.5	5.0	101	98		0.5	6913
11/18/04 14:49		A/B	구 다	32	3359732		20271	33	3335681	3312387	10064	5.9	5.0	101	97		0.5	7406
11/19/04 15:40	184.7	A/B	OFF	31	3384711		20423	32	3360410	3337116	10140	5.5	2.0	101	66		0.5	7784
11/22/04 09:38		A/B	OFF	32	3443037		20777	30	3418182	3394888	10315	5.6	5.1	100	97		0	7905
11/23/04 10:00		A/B	OFF	33	3466574		20920	33	3441496	3418202	10386	5.5	2.0	101	98		0	7905
11/24/04 14:11	240.7	A/B	OFF	31	3492632		21078	31	3467298	3444004	10464	5.5	2.0	101	97	98	0	7905
11/29/04 10:14	299.1	A/B	OFF	30	3605433		21764	30	3579122	3555828	10804	0.9	2.0	122*	97	,	0	7908
11/30/04 10:47	310.1	A/B	OFF	31	3629181		21908	32	3602681	3579387	10876	5.5	2.0	NA	86		0	7908
12/01/04 10:58	NA	A/B	OFF	32	3652572	3628601	22050	33	3625889	3602595	10946	5.4	2.0	NA	26	NA	0	7908
12/06/04 09:35	382.5	A/B	OFF	33	3766441		22742	33	3738862	3715568	11289	5.5	5.5	NA	96		0	7908
12/07/04 09:15	394.4	A/B	OFF	33	3788938	3764967	22879	31	3761091	3737797	11357	5.5	2.0	NA	97	NA	0	7908
12/08/04 10:04	406.7	A/B	OFF	31	3813731	3789760	23030	32	3785617	3762323	11431	5.5	2.0	NA	26	NA	0	7908
12/09/04 09:32	418.3	A/B	OFF	33	3835866		23164	33	3807480	3784186	11498	5.5	5.3	NA	26	NA	0	2062
12/10/04 14:00	432.1	A/B	OFF	33	3863117	3839146	23330	31	3834341	3811047	11580	6.5	5.5	NA	46	NA	0	7908
12/13/04 08:15	A	A/B	OFF	33	3927415	3903444	23720	34	3897613	3874319	11772	5.5	5.0	NA	86	NA	0	7908
12/14/04 14:00	Α̈́	A/B	OFF	33	3957724		23905	33	3927319	3904025	11862	5.5	5.1	Ν	98	NA	0	7908
12/15/04 17:00		A/B	OFF	AN	3982673	3958702	24056	AN	3950999	3927705	11934	ΑN	A	AN	85		0	23
12/16/04 15:13	505.2	A/B	OFF	33	4008571	3984600	24214	31	3976384	3953090	12011	0.9	5.5	NA	97	NA	0.5	403
12/17/04 16:39		A/B	OFF	AN	4032260		24358	ΝΑ	3999641	3976347	12082	ΝΑ	NA	NA	NA		NA	751
12/20/04 17:14		A/B	OFF	NA	4103115		24788	NA	4068989	4045695	12292	NA	NA	NA	NA		0	1610
12/21/04 09:24		A/B	OFF	32	4122253		24904	33	4087888	4064594	12350	5.5	2.0	NA	97		0	1610
12/22/04 15:02		A/B	OFF	AN	4149825	•	25072	ΝΑ	4114985	4091691	12432	ΝA	NA	NA	NA		0	1610
12/27/04 15:15	636.0	A/B	OFF	NA	4266102		25779	NA	4229848	4206554	12781	NA	NA	NA	NA		0	1610
12/28/04 10:05	A	A/B	OFF	32	4286326		25902	31	4249930	4226636	12842	5.5	5.1	NA	97		0	1610
12/29/04 14:33	659.8	A/B	NO	A		4288052	26058	ΑN	4275421	4252127	12920	ΑN	NA	NA	NA		0	1610
12/31/04 11:01	683.1	A/B	OFF	33	4357919	4333948	26337	31	4321069	4297775	13058	5.5	5.1	NA	97		0	1610
01/03/05 11:07	718.8	A/B	OFF	32	4427087	Ì	26757	30	4389855	4366561	13267	5.5	5.1	A	98		0	1612
01/04/05 09:34	729.4	A/B	OFF	33		Ì	26879	30	4409801	4386507	13328	5.9	5.2	NA	97	AA	0	1615
01/06/05 11:26	755.4	A/B	OFF		4497385	4473414	27184	31	4459637	4436343	13479	5.9	5.1	NA	97	NA	0	1615
01/10/05 10:27	¥	A/B	OFF	32	4588277	4564306	27736	33	4549897	4526603	13754	5.5	2.0	N A	97	NA.	0	1615
01/11/05 10:08	813.2	A/B	OFF	33	4590667	4566696	27751	33	4552270	4528976	13761	0.9	5.5	Y :	97	¥ :	0	1615
01/12/05 08:59	823.8	A/B	占	34	4612117		27881	33	4573178	4549884	13824	5.9	5.4	NA.	97	YA S	0	1615
01/14/05 16:49	879.6	A/B	OFF	31	4723345	4699374	28557	33	4681745	4658451	14154	6.0	2.5	104	97		0	1615
01/17/05 11:56	915.7	A/B	OFF	ΑΝ		4771307	28994	ΑN	4751893	4728599	14367	ΑN	ΝΑ	A	NA		0	1615
01/18/05 09:19	925.5	A/B	OFF	33	4814502	4790531	29111	31	4770599	4747305	14424	5.9	5.4	103	88		0	1615
01/19/05 12:45	939.7	A/B	OFF	34	4842508	4818537	29281	33	4797759	4774465	14507	0.9	5.5	103	94		0.5	1668
01/24/05 09:53	975.2	A/B	OFF	34	4914174		29717	34	4868118	4844824	14721	0.9	5.4	104	98		0.5	2704
01/25/05 08:58	986.1	A/B	OFF	33	4935926	Ì	29849	33	4889629	4866335	14786	0.9	5.5	104	86		0.5	3036
01/26/05 11:05		A/B	OFF	34	4964184		30021	32	4917217	4893923	14870	0.9	5.1	104	96		0.5	3440
01/27/05 10:14		A/B	NO	29	4986039	Ì	30154	28	4938853	4915559	14935	5.0	4.4	107	100	93	0.5	3764
01/28/05 15:08	1028.1	A/B	OFF	AN	5019189	4995218	30355	AN	4971767	4948473	15035	Ν Α	NA	ΝΑ	NA		0	4055

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

					Tank A F	k A Flow Meter			Tank B F	Tank B Flow Meter		дÞ			Pressure		Re	Recycling
Date and Time	Hour	Lead/L	:	Flowr		i	Bed	Flowr		i					Between -	•	Flow	:
	Meter	ag AB	Well #3 On/Off	ate	Totalizer	Cum. Flow	Volume	ate	Totalizer	Cum. Flow	Volume	TA	TB	Inlet	Tanks	Outlet	Rate	Totalizer
01/31/05 09:55	1062.3	A/B	OFF	32	5086168	27	30762	32	5038276	5014982	15238	ıc	_	104	26	88	0	4055
02/01/05 16:00	1075.6	A/B	OFF	Ν V	5112646		30923	NA	5064534	5041240	15317	NA	Ϋ́	Z A V	NA N	NA A	0	4055
02/02/05 11:20		A/B	OFF	33	5135971		31065	33	5087715	5064421	15388	5.5	5.1	103	97	88	0	4055
02/03/05 08:45		A/B	NO	29	5153884		31174	29	5105543	5082249	15442	4.5	4.1	107	102	94	0	4055
02/04/05 16:16		A/B	7.5	NA P	5182326		31346	AN S	5133796	5110502	15528	NA C	NA	A S	NA		0	4055
02/08/05 10:47	1170.2	A/B	750	32	5297104	5273133	32044	31	5248015	5224721	15875	5.0	5.0	100	S 66	89	0	4055
02/09/05 10:05		A/B	OFF	32	5318931		32176	32	5269749	5246455	15941	5.5	5.1	104	98		0	4055
02/10/05 09:00	1192.6	A/B	OFF	33	5340324		32306	32	5291091	5267797	16006	5.5	5.3	104	86		0	4055
02/11/05 11:08	1206.2	A/B	OFF	32	5367723	5343752	32473	34	5318390	5295096	16089	5.5	2.0	104	98	88	0	4055
02/15/05 10:35	1254.2	A/B	OFF	32	5462717	5438746	33050	32	5412813	5389519	16376	2.5	2.0	104	86		0	4060
02/16/05 11:05	1265.8	A/B	OFF	33	5486396		33194	32	5435484	5412190	16444	0.9	5.1	104	96		0.5	4117
02/17/05 10:33	1277.8	A/B	OFF	33	5510522		33341	31	5459325	5436031	16517	0.9	5.5	104	96	88	0.5	4468
02/18/05 11:54	1290.7	A/B	OFF	32	5513120		33357	32	5461900	5438606	16525	5.9	5.1	104	66	`	0.5	4839
02/22/05 10:17	1337.2	A/B	OFF	33	2606998		33927	32	5553239	5529945	16802	5.5	2.0	104	98		0	5694
02/23/05 10:09	1349.1	A/B	OFF	33	5630977		34073	33	5576539	5553245	16873	5.5	5.1	104	96	88	0	5694
02/24/05 09:06	1359.9	A/B	OFF	33	5652469		34203	29	5597591	5574297	16937	5.5	2.0	104	98		0	5694
02/25/05 16:46	1374.0	A/B	NO	NA	5681376	5657405	34379	NA	5625653	5602359	17022	NA	NA	NA	NA		0	5694
02/28/05 08:58	1407.3	A/B	OFF	34	5748368	5724397	34786	34	5690798	5667504	17220	5.8	5.3	104	98		0	5694
03/02/05 09:24		A/B	OFF	35	5797131		35082	34	5738226	5714932	17364	2.8	5.4	104	99	88	0	5694
03/03/05 11:05		A/B	OFF	33	5825380		35254	35	5765640	5742346	17448	5.9	5.5	104	97		0	5694
03/04/05 15:05		A/B	NO	ΝΑ	5850439		35406	Ν Α	5789651	5766357	17521	Ν Α	ΑN	Z A	AN		0	5694
03/07/05 09:31	1491.4	A/B	OFF	34	5919211		35824	32	5855916	5832622	17722	5.9	5.5	104	97	88	0	5894
03/08/05 15:26	1505.2	A/B	OFF	NA	5947481		35996	NA	5883084	5859790	17804	N S	Y S	Y Y	NA:		0	5894
03/09/05 15:59	1517.1	A/B	OFF	NA	5971533		36142	NA NA	5906386	5883092	17875	AN I	Υ V	Y S	NA S		0	5894
03/10/05 08:39	1526.3	A/B	OFF	32	5989742		36253	32	5924129	5900835	17929	5.9	5.5	105	88		0	5894
03/11/05 14:26	1540.9	A/B	ON	NA	6020129		36438	NA	5953383	5930089	18018	NA	NA	ΝΑ	NA		0	5894
03/14/05 09:30	1574.9	A/B	OFF	32	6088744		36854	33	6019922	5996628	18220	5.9	5.5	105	98		0	5894
03/15/05 10:50	1588.0	A/B	OFF	34	6115750		37019	33	6045938	6022644	18299	5.9	2.5	104	97		0	5894
03/16/05 08:00	1597.0	A/B	NO	31	6133650		37127	29	6063495	6040201	18353	2.0	2.0	106	98		0	5894
03/17/05 08:46	1609.4	A/B	OFF	33	6159461		37284	32	6087891	6064597	18427	0.9	2.8	104	97	68	0.5	6021
03/18/05 17:02	1623.9	A/B	다	NA	6189230		3/465	NA	6116938	6093644	18515	NA	NA	ΝA	NA		0	6447
03/21/05 10:12	1658.4	A/B	OFF	34	6259086		37890	33	6185027	6161733	18722	9.9	5.2	104	88	88	0	7328
03/22/05 09:40	1669.7	A/B	OFF	32	6281871		38028	32	6207279	6183985	18789	5.9	5.5	104	89	68	0	7328
03/23/05 11:21	1683.3	A/B	남	33	6309100		38194	31	6233889	6210595	18870	5.9	5.5	104	88		0	7328
03/24/05 16:40		A/B	7.5	Y Z	6333095		38339	A Z	6257541	6234247	18942	AN S	A Z	Z Z	NA NA	NA Z	0	7328
03/28/05 14:06	17/0/1	Q Q	ב ב	¥ < Z	64072997	6403416	200404	<u> </u>	6250634	2667629	19013	ζ < 2	ζ < 2 Z	ζ < 2	Y V		0	7328
03/20/05 00:35	17526	2 0	ב ב	YY CC	6421361		30912	Y C	6360769	1261250	19223	2 0	Z 4	100	N 00		0	7220
03/30/05 09:26	1765 5	Δ <u>Δ</u>	ב ב	33	6446729		39184	4 %	7077059	6371503	19263	0.0 8	5.0 7.7	101	90	00 00	0 0	7328
03/31/05 09:16	1776.3	A/B	7	3, 6	6493593		39315	30	6415987	6397659	19424	0.0	2.5	108	102		0 0	7328
04/04/05 44:40	1000	ם פ		0 0	0493393		30013	00	0413307 651390F	6400644	13424	t n	t 1	200	102		0	7220
04/04/05 11.19	1020.0	מַ כַּ		25	0392327		39910	ဂ္ဂ	0001000	0490311	19720		2.5	10 5	30			7000
04/05/05 10:48	1837.2	A A	7 5	33	6615187		40054	33	6536228	6512934	19789	5.6	2.5	104	97	88	0	7328
04/06/05 15:36	1849.8	A'B	OFF.	Y :	6640145		40205	N :	/880969	6537593	19864	Z :	Z :	¥ :	Z :		0	7328
04/07/05 16:29	1861.7	A/B	OFF	NA	0/ /6999		40349	NA S	6584247	6560953	19935	NA I	Α V	Vγ.	NA I		0	7328
04/08/05 14:17	1868.7	A/B	OFF	33	8677708	6653737	40434	33	6298005	6574711	19977	2.8	2.5	105	1/6	88	0	7328

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

					Tank A F	κ A Flow Meter			Tank B F	Tank B Flow Meter		р	dP		Pressure		R	Recycling
Date and Time	Hour	Lead/L	Woll #2	Flowr	Totalizar		Bed	Flowr	Totolitor	, moles	Bed	ŕ	P	2	Between	10	Flow	Totaliza
	hr	A/B	On/Off	gpm	gal	gal		gbm		gal		psi	psi	psig	psig	psig	gpm	gal
04/11/05 11:14	1902.2	A/B	OFF	36	6744490	6720519	40839	34	0663930	6640636	20177	5.9	5.5	104	26	68	0	7328
04/12/05 11:45	1915.1	A/B	OFF	35	6769857	6745886	40993	34	6688978	6665684	20253	0.9	5.8	105	97	06	0	7328
04/13/05 07:30		A/B	OFF	34	6785197		41087	33	6704130	980899	20299	0.9	5.8	105	26	06	0	7328
04/14/05 11:00	1938.5	A/B	OFF	34 34	6817030 6838395	6793059 6814424	41280	33	6734745	6711451	20392	6.0	5.5	105	97	06	0.5	8022
04/18/05 14:30		A/B	NO	30	6921707		41916	30	6837851	6814557	20705	5.0	5.0	107	101	93	0	8931
04/20/05 11:31	2012.3	A/B	NO	31	6963999	6940028	42173	30	6879575	6856281	20832	5.0	4.9	107	101	93	0	8931
04/21/05 12:09	2020.1	A/B	OFF	33	6979520		42268	33	6894870	6871576	20879	0.9	5.5	104	26	68	0	8931
04/22/05 14:36		A/B	OFF	34	7008297	6984326	42442	33	6923246	6899952	20965	5.9	5.5	104	97	88	0	8931
04/25/05 13:45	2070.3	A/B	OFF	34	7079621	7055650	42876	33	6993594	0000269	21179	5.9	5.5	105	26	68	0	8931
04/26/05 16:45	2085.7	A/B	OFF	33		7	43061	32	7023634	7000340	21270	6.0	5.5	105	97	88	0	8931
04/27/05 10:32	2091.2	A/B	OFF	33	7121605	' '	43131	33	7035028	7011734	21304	5.9	5.4	105	86	88	0	8931
_	2102.9	A/B	45	33		`	43266	34	7056963	7033669	21371	5.9	5.2	105	86	68	0	8931
04/29/05 16:32	2122.1	A/B	NO	30	7182069	7158098	43498	30	7094744	7071450	21486	5.0	4.5	108	101	95	0	8931
05/02/05 13:48		A/B	NO	30	7249253		43907	31	7160993	7137699	21687	4.6	4.4	108	103	92	0	8931
05/03/05 13:17	2167.7	A/B	OFF	34	7271983		44045	34	7183391	7160097	21755	6.0	5.6	104	98	88	0	8931
		A/B	N O	30	7288280	7264309	44144	30	7199462	7176168	21804	5.0	5.0	108	102	93	0	8931
05/05/05 13:31		A/B	NO	31	7319966		44336	30	7230715	7207421	21899	5.0	4.5	108	101	93	0	8931
05/06/05 14:43		A/B	OFF	34	7346749	7322778	44499	31	7257140	7233846	21979	6.0	5.5	104	98	89	0	8931
05/09/05 09:29		A/B	NO	31	7408975		44877	30	7318530	7295236	22166	5.0	4.6	108	102	98	0	8931
05/10/05 10:28		A/B	OFF	34	7434485		45032	31	7343756	7320462	22243	5.9	5.4	105	97		0	8931
05/11/05 08:30	2260.4	A/B	NO	31	7454512		45154	31	7363585	7340291	22303	5.0	4.8	108	102		0	8931
05/12/05 08:00	2272.2	A/B	NO	31	7478212		45298	31	7386221	7362927	22372	5.0	4.8	108	102	95	0.5	9248
05/13/05 13:00		A/B	OFF	34	7512395		45506	32	7419923	7396629	22474	6.0	5.5	106	98		0.5	9734
05/16/05 09:42	2322.5	A/B	NO	30	7577780		45903	32	7484426	7461132	22670	5.0	4.5	109	104	96	0	10538
05/17/05 09:47	2334.8	A/B	OFF	32	7601788		46049	32	7508093	7484799	22742	5.9	5.2	105	66	90	0	10538
05/18/05 15:07		A/B	NO	31	7636716		46261	30	7542552	7519258	22847	5.1	5.0	106	100	92	0	10538
05/23/05 09:27	2407.7	A/B	OFF	32	7747128	7	46932	32	7649935	7626641	23173	5.8	5.5	105	66	06	0	10538
05/24/05 09:07	2419.6	A/B	OFF	34	7771155	_	47078	33	7673116	7649822	23243	5.9	5.5	105	66	88	0	10538
		A/B	OFF	34	7798620	_	47245	33	7699640	7676346	23324	5.9	5.5	105	66	06	0	10538
05/26/05 08:40		A/B	NO L	32	7819144	<u> </u>	47370	30	7719595	7696301	23384	8.4 8.0	4.5	108	102	95	0	10538
05/27/05 16:45		A/B	7 1	34	7860113	`	47619	34	181.6677	1,135893	23505	5.5 1	5.4	co.	97	06	0	88COL
05/31/05 09:57	2505.8	A/B	7 5	34	7002640	`	48132	32	767677	781/832	23/54	5.5	5.2	105	97	98	0	10538
06/01/05 16:43	2524.0	2 A	בין	95 22	7008110	7929046	46309	32	7801057	7868663	23000	5.5 0.5	5.7	105	66 66	06	0	10538
_	2546.6	A/B	OFF	32	8028056	Τ~	48639	33	7920685	7897391	23995	5.8	. 2	105	86		0	10538
06/06/05 15:23	2584.4	A/B	OFF	33	8103916		49100	33	7993978	7970684	24218	5.9	5.4	105	86		c	10538
06/07/05 13:13		A/B	OFF	33	8123811		49221	31	8013258	7989964	24277	5.5	5.1	105	97	90	0	10538
06/08/05 10:00	2603.7	A/B	NO	31	8141844			30	8030813		24330	5.0	4.8	105	102		0	10538
06/09/05 10:00	2615.7	A/B	NO	29	8166136	8142165		29	8053634	8030340	24399	4.8	4.2	109	102		9.0	10858
06/13/05 14:30	2664.1	A/B	OFF	33	8262128			32	8147515	8124221	24685	5.5		104	86		0.5	12088
	2675.9	A/B	OFF	33	8285731	8261760	50205	32	8170129	8146835	24753	5.5	5.0	106	86		0	12088
	2683.5	A/B	OFF	34	8301036		50298	30	8184680	8161386	24798	5.9	5.2	106	98		0	12088
06/16/05 11:25	2697.7	A/B	NO	30	8329836		50473	28	8212046	8188752	24881	4.6	1.4	110	103	96	0	12088
06/17/05 15:56	2714.3	A/B	NO	30			50675	28	8244031	8220737	24978	4.8	4.2	109	102	96	0	12088
06/20/05 09:24	2744.3	A/B	NO	28	8422922	8398951	51039	28	8301802	8278508	25153	4.8	4.2	109	103	97	0	12088

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

					Tank A F	k A Flow Meter			Tank B F	Tank B Flow Meter		ВP	L		Pressure		Re	Recycling
Date and Time	Hour	Lead/L		Flowr			Bed	Flowr			Bed				Between		Flow	
	Meter	ag A/B	Well #3	ate	Totalizer	Cum. Flow	Volume	ate	Totalizer	Cum. Flow	Volume	T A	TB	Inlet	Tanks	Outlet	Rate	Totalizer
00.001	0.000	ָ ֪֞֝֞֝֞֝֞֝֝֞֝֞֝֞֝֓֞֝֞֝֓֓֞֝		- C	94770750		74.000	100	gar	gai	00030	- N	-	919	Palg	Paig 004	90	981
06/22/05 10:30	2704.7	A A	200	67	8472259	8448288	51339	28	8320099	8326805	25300	7.4	7.4	- 0	103	001.	0	12088
06/24/05 15:02	02000	ב ב		67	0494030		51470	67	03/2303	090000	23300	, n	1.4	100	00	Se		12000
06/27/05 13:55	2.98.2 NA	A/B	- N	30	8596930	8572959	52096	20	8472476	8449182	25672	4.4	0.0	109	103	96	0 0	12088
06/28/05 15:24	2847.9	A/B	NO	29	8623299		52256	28	8498135	8474841	25750	4.4	4.1	110	103	26	0	12088
06/29/05 09:46	2854.5	A/B	NO	30	8636181		52335	30	8510646	8487352	25788	4.8	4.2	109	102	96	0	12088
06/30/05 09:55	2866.8	A/B	NO	30	8660434		52482	30	8534051	8510757	25859	4.9	4.4	109	101	96	0	12088
07/01/05 15:48	2884.9	A/B	OFF	34	8695429	8671458	52695	33	8567897	8544603	25962	5.4	2.0	105	98	06	0	12088
07/05/05 14:11	2932.1	A/B	OFF	30	8786414	8762443	53248	30	8656450		26231	2.0	2.0	105	26	06	0	12088
07/06/05 08:00	2938.3	A/B	NO	30	8798083	8774112	53319	28	8667915	8644621	26266	4.9	4.3	105	100	06	0	12088
07/07/05 08:58	2951.1	A/B	OFF	33	8822760		53469	32	8691560	8668266	26338	5.5	2.0	105	26	06	0.5	12418
_	2970.5	A/B	OFF	31	8829990		53695	30	8727748	8704454	26448	5.6	2.0	105	97	06	0.5	12942
-	3006.1	A/B	NO	28	8927782		54107	28	8793516	8770222	26647	4.5	4.0	110	102	96	0	13452
	3017.8	A/B	OFF	32	8949528		54239	32	8814692	8791398	26712	5.1	4.9	105	87	06	0	13452
	3026.1	A/B	OFF	33	8965572		54336	32	8830271	2269088	26759	5.1	2.0	106	98	06	0	13452
	3036.9	A/B	OFF	33	8988425	8964454	54475	32	8849575	8826281	26818	5.1	2.0	106	86	06	0	13452
$\vdash$	3085.8	A/B	OFF	31	9077394	9053423	55016	32	8939776	8916482	27092	5.2	4.9	105	26	6	0	13452
-	3098.4	A/B	OFF	32	9100845		55158	30	8962875	8939581	27162	5.2	2.0	105	26	06	0	13452
07/20/05 17:07	3117.8	A/B	OFF	32	9137432	9113461	55381	30	8998883	6855768	27271	5.2	2.0	105	26	06	0	13452
	3126.3	A/B	NO	28	9153108		55476	28	9014321	8991027	27318	4.0	4.0	110	103	96	0	13452
	3139.9	A/B	OFF	32	9179099	9155128	55634	30	9039784	9016490	27396	5.1	2.0	105	97	06	0	13452
_	3170.2	A/B	OFF	32	9236804		52985	31	9096171	9072877	27567	5.1	2.0	104	26	06	0	13452
07/26/05 08:30	3181.3	A/B	OFF	32	9257866		56113	31	9116834	9093540	27630	5.1	5.0	105	98	06	0	13452
07/27/05 13:30	3196.5	A/B	OFF	32	9286958		56289	31	9145039	9121745	27716	2.0	4.9	104	97	90	0	13747
07/28/05 10:00	3205.3	A/B	OFF	31	9303471		56390	30	9161253	9137959	27765	5.1	4.9	105	97	06	0	13747
07/29/05 11:00	3218.9	A/B	NO	29	9329436	9305465	56548	29	9186908	9163614	27843	4.1	4.0	109	102	98	0	13747
-	3256.2	A/B	OFF	32	9400245		56978	31	9256407	9233113	28054	5.1	2.0	106	26	36	0	13747
_	3270.2	A/B	NO	29	9427211	9403240	57142	30	9282369	9259075	28133	4.4	4.1	109	101	96	0	13747
	3283.4	A/B	NO	30	9452963	9428992	57298	29	9307022	9283728	28208	4.5	4.2	109	101	93	0	13747
_	3289.1	A/B	OFF	32	9464168		57366	29	9317756	9294462	28240	2.0	2.0	108	97	92	0	13747
_	3308.2	A/B	OFF	33	9500919	9476948	57590	29	9353436	9330142	28349	2.0	2.0	107	97	91	0	13747
08/08/05 10:45	3339.5	A/B	OFF	32	9561750	9537779	57959	30	9411832	9388538	28526	5.0	2.0	106	97	88	0	13747
08/09/05 09:30	3350.7	A/B	OFF	32	9583390	9559419	58091	31	9432561	9409267	28589	2.0	2.0	107	97	92	0	13747
08/10/05 12:30		A/B	OFF	32	9612512		58268	31	9460748	9437454	28675	5.1	2.0	107	97	90	0	13747
08/11/05 11:30	3376.9	A/B	OFF	32	9634529		58402	31	9481779	9458485	28739	5.1	5.0	107	97	06	0	13747
08/12/05 16:44	3394.0	A/B	OFF	33	9667841		58604	32	9513861	9490567	28836	5.1	2.0	107	97	92	0	13747
08/15/05 09:33	3423.4	A/B	OFF	32	9724754		58950	30	9568794	9545500	29003	2.0	2.0	106	97	88	0	13747
08/17/05 13:15	3449.3	A/B	OFF	32	9774656		59253	33	9617017	9593723	29150	5.1	2.0	107	97	06	0.5	13890
08/18/05 09:49	3457.7	A/B	OFF	32	9790540		59350	27	9632641	9609347	29197	5.2	2.0	107	97	90	0.5	14127
08/19/05 14:59	3475.0	A/B	OFF	32	9823674		59551	31	9665271	9641977	29296	5.4	2.0	105	97	90	0.5	14618
08/22/05 10:24	3507.0	A/B	OFF	32	9884693		59922	32	9725167	9701873	29478	5.5	4.8	108	97	92	0	15115
08/23/05 10:28		A/B	OFF	32	9908120		60064	32	9747914	9724620	29547	2.0	2.0	107	97	92	0	15115
	3538.1	A/B	OFF	31	9944394		60285	31	9783282	9759988	29655	5.2	2.0	107	97	90	0	15115
	3542.8	A/B	OFF	31	9953242		60338	31	9791942	9768648	29681	5.4	4.9	108	97	92	0	15115
	3561.7	A/B	OFF	32	9989501		60228	32	9827501	9804207	29789	5.2	2.0	107	97	90	0	15115
08/29/05 10:18	3592.1	A/B	OFF	32	10047028	10023057	80609	32	9883968	9860674	29961	5.4	4.9	107	87	06	0	15115

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

								T	$\top$		1																											T						_
Recyclina	6	Totalizer	gal	15115	15115	15115	15115	10110	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15113	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	15115	10110	15115	2
Rec	Flow	Rate	gpm	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0 0	0 0	0	0	0	0	0	0	> 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	>
r		Outlet	psig	06	06	92	96	38	06	06	06	06	06	06	06	96	06	92	38	36	92	92	06	92	98	85	35	92	92	92	92	96	92	96	92	06	06	92	06	06	06	35	88	
Pressure	Between		psig	87	87	87	101	97	97	97	97	26	97	26	26	103	97	96	97	187	97	96	96	26	104	97	97	96	26	26	6	102	96	97	26	96	96	97	6	87	97	30,	07	
Pre	Betv			106	107	107	109	100	107	107	106	106	107	107	108	112	108	108	108	111	108	107	107	107	112	108	100	108	90	108	108	110	108	108	108	108	108	108	107	108	106	2 5	710	
_		Inlet	psig																																									
무	_	TB	psi	4.6	0.4.6			0.0						Ц				5.0		0.0		1.9	5 5.0			4.8							5.0			4.6					3 4.9			
		T	2	0.5				5.0	┸				5.2	Ц				5.1		1.C	L		5.5	Ш		_		5.4	L				5.1			5.0		_			5.3		0.4	
	Bed	Volume		30050	30113	30164	30275	30231	30741	30968	30985	31061	31237	31442	31467	31539	31646	31712	31916	32021	32099	32190	32368	32461	32509	32567	32012	33366	33396	33514	33537	33646	33818	33949	34013	34067	34257	34356	34387	34461	34558	34729	34603	
w Meter		Cum. Flow	gal	9889957	9910837	9927459	9964216	1000001	10117358	10192161	10197749	10222771	10280569	10348193	10356553	10380198	10415411	10437057	10504305	10515591	10564484	10594280	10652914	10683405	10699211	10718461	1072230	10981260	10991275	11030120	11037737	11073542	11130226	11173451	11194480	11212106	11274622	11308203	11317374	11341898	11373585	11429901	1424199	27/2
Tank B Flow Meter							9987510	- 0		_			10303863 1							10538885	Ļ	1 0617574	0676208 1		10722505 1	10741755 1	4		L	-		_	11153520 1		Ĺ	11235400 1	1297916 1				11396879 1	_	116/1493	
Ľ		Totalizer					•													-		106	,	,										Ĺ		112	l			Ц	1	1	1 1 1	
	Flowr	ate	gpm	31		31	28	30	32	30	3	30	32	32	30	26	3	31	30	30	32	31	32	29	25	31	30	31	30	29	30	26	31	308	30	31	31	30	31	30	31	2 5	77	
	Bed	Volume		61090	61226	61323	61551	62114	62501	62964	62999	63153	63510	63928	63979	64125	64343	64476	04890	65102	65261	65444	62805	65993	06099	66208	67240	67826	67888	68126	68173	68394	68742	80069	69138	69246	69631	69838	69895	70045	70253	20207	70005	
A Flow Meter		Cum. Flow	gal	10053005	10075325	10091349	10128890	4000000	10285139	10361397	10367084	10392467	10451163	10519946	10528401	10552403	10588227	10610204	106/831/	0713246	10739300	10769497	0828870	10859730	0875736	10895207	110930139	11161452	11171593	11210883	1218577	1254844	11312242	1355974	11377296	11395139	11458471	11492531	11501847	11526622	11560836	11010040	1040300	
A Flo		er		926	596		861		Ţ,	368	ľ	1438	134	917 1	372 1		198	175	7,7	714	271 1	468	341 1	. 101	707		0 00	423			248	315	213			110 1	442 1			293	307	8 0	`	
Tank		Totalize	gal	10076	100993	10115	10152	10243	10309	10385	10391	10416	10475	10543	10552	10576	10612	10634	10702	10713	10763	10793	10852	10883	108997	10919	111060	11185	11195	11234	11242	11278	11336	11379	11401	11419	11482	11516	11525	11550	115848	1040	116004	
	Flowr	ate	gpm	31	32	32	30	ى د	32	32	31	31	31	31	31	28	31	32		3. S	32	30	32	31	29	31	- 00	31	31	31	31	29	32	31	30	31	31	30	32	31	31	32	07	
	•	Well #3	On/Off	OFF	OFF	OFF	NO C	ב ב	OFF	NO	OFF	OFF	7 5	7 5	OFF	OFF	OFF	OFF	NO	OFF	ב ב	OFF	OFF	OFF	OFF	NO :	7 1	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ב ב	110							
ľ	Lead/L			A/B	A/B	A/B	A/B	2 0	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	0 Q	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	A/B	ַבְּלָ	2 4								
	Hour	Meter		3608.2			3648.1			3770.4	3773.6	3787.1	3818.1	3854.6	3859.2	3871.9	3890.9	3902.5	3938.8	3944.8	3971.2	3987.1	4018.7	4035.3		4054.3	4012.3	4195.5			4226.0		4275.9	4299.3	4310.5	4320.0	4353.6	4371.7			4406.8		4449.9	1
	Ford	Date and IIme		08/30/05 14:03	/31/05 14:00	09/01/05 09:56	09/02/05 17:31	09/06/05 17:34	09/09/05 14:24	09/12/05 18:04	09/13/05 08:57	09/14/05 10:15	09/16/05 16:57	09/19/05 16:50	09/20/05 09:12	09/21/05 09:47	/22/05 16:29	09/23/05 16:00	72/05 15:36	09/27/05 09:23	09/29/05 11:23	09/30/05 15:09	10/03/05 10:08	10/04/05 14:35	10/05/05 11:00	10/06/05 09:12	10/01/05 13:33	10/17/05 16:18	/18/05 09:30	10/19/05 18:17	10/20/05 10:12	10/21/05 17:26	10/24/05 11:00	10/26/05 10:19	10/27/05 09:24	10/28/05 14:04	10/31/05 11:06	11/01/05 17:01	11/02/05 09:43	/03/05 11:47	11/04/05 16:39	/01/05 10.24	11/08/05 10:57	

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

			-		IANKAF	A Flow Meter			I ank b	I ANK B FIOW METER		<u> </u>	_		Pressure		ž	Recycling
Date and Time		Lead/L		Flowr			Bed	Flowr			Bed				Between	,	Flow	
	Meter	ag	Well #3	ate	Totalizer	Cum. Flow	Volume	ate	zer	Cum. Flow	Volume	$\dashv$	+	Inlet	Tanks	Outlet	Rate	Totalizer
	JII	A G	10/10	mdg	gai	gal		gbm	gai	gal				bisd	bsig	bsıg	gpm	gal
11/15/05 17:00	4536.0	A/B	7.0	31	11826912	11802941	71724	30	1163/458	11614164	35289	5.1	6.4	30,	96	90	0.5	15522
11/16/05 16:27	4552.7	A/B	S 13	27	11858080	11834109	71914	29	11668285	11644991	35382	0.4	0.4	112	104	96	0.5	16010
11/71/05 10:19	_	מ מ	ב ב	24	- 10	11035557	72520	50	11768503	11745209	35687	2. A	0.0 R	00.0	97	35	5.5	16334
11/22/05 13:20		A/B	OFF.	31	11989320	11965349	72711	31	11797907	11774613	35776	5.0	4.6	108	97	06	0	16334
11/28/05 10:37	4693.1	A/B	OFF	31	12121394	12097423	73514	31	11928098	11904804	36172	5.0	4.9	107	26	06	0	16334
11/29/05 09:41	4704.4	A/B	NO	29	12142811	12118840	73644	29	11949244	11925950	36236	4.5	4.0	110	102	96	0	16334
11/30/05 10:12	4717.1	A/B	OFF	32	12166165	12142194	73786	30	11972288	11948994	36306	2.0	4.5	108	26	92	0	16334
12/01/05 14:12	4733.3	A/B	OFF	31	12196751	12172780	73972	30	12002502	11979208	36398	5.1	2.0	105	96	06	0	16334
12/02/05 14:22	4745.7	A/B	OFF	31	12219644	12195673	74111	30	12025126	12001832	36466	2.0	2.0	108	26	06	0	16334
12/05/05 17:26	4785.3	A/B	OFF	32	12293908	12269937	74562	31	12098345	12075051	36689	2.0	4.6	108	96	92	0	16334
12/06/05 11:35	4791.7	A/B	OFF	31	12305709	12281738	74634	31	12109942	12086648	36724	2.0	4.6	108	26	06	0	16334
12/07/05 09:30	4801.3	A/B	NO	32	12323575	12299604	74742	31	12127187		36777	5.1	4.8	108	26	06	0.5	16445
12/08/05 11:26	4815.4	A/B	OFF	31	12350329	12326358	74905	32	12153894	12130600	36858	2.0	4.5	108	96	85	0.5	16859
12/09/05 12:47	4828.9	A/B	OFF	31	12375855	12351884	75060	32	12178641		36933	2.0	4.5	108	26	92	0	16970
12/12/05 13:41	4865.3	A/B	OFF	30	12444309	12420338	75476	31	12246261	12222967	37138	2.0	4.6	108	86	95	0	16969
12/13/05 15:30		A/B	OFF	31	12470869	12446898	75637	30	12272512	12249218	37218	2.0	4.8	108	26	92	0	16969
12/14/05 10:00	4886.1	A/B	OFF	31	12483160	12459189	75712	30	12284644	12261350	37255	2.0	4.8	108	26	92	0	16969
12/15/05 10:24	4898.6	A/B	OFF	30	12506930	12482959	75857	30	12307967	12284673	37326	2.0	4.8	108	26	90	0	17046
12/19/05 09:00	4945.6	A/B	OFF	31	12594669	12570698	76390	31	12394830	12371536	37590	2.0	4.9	NA	26	NA	0	17046
12/20/05 10:30	4959.0	A/B	OFF	31		12595751	76542	31	12419638	12396344	37665	2.0	4.9	A A	97	Υ Y	0	17046
12/21/05 10:00	4970.7	A/B	OFF	30	12642262	12618291	76679	30	12441925	12418631	37733	2.0	4.9	NA	97	Α	0	17046
12/22/05 16:46	4989.9	A/B	OFF	31	12677448	12653477	76893	32	12475779	12452485	37836	2.0	2.0	NA	97	NA	0	17046
12/27/05 11:57		A/B	OFF	31	12782236	12758265	77530	30	12580323	12557029	38153	5.1	4.8	NA	26	NA	0	17046
12/28/05 10:00		A/B	OFF	31		12777503	77646	30	12599304	12576010	38211	5.1	4.9	NA	26	A	0	17046
12/29/05 09:09	5067.6	A/B	OFF	32	12822799	12798828	77776	31	12620385	12597091	38275	5.0	2.0	NA	97	NA	0	17046
01/03/06 17:11	5136.6	A/B	OFF	31	12951474	12927503	78558	30	12747775	12724481	38662	5.2	4.9	NA	26	NA	0	17046
01/04/06 10:52	5142.4	A/B	OFF	32	12962384	12938413	78624	30	12758551	12735257	38695	2.0	4.9	NA	96	NA	0	17046
01/05/06 08:30	5152.2	A/B	OFF	30		12956749	78736	33	12776667	12753373	38750	2.0	4.9	NA	26	A	0	17046
01/06/06 15:10	5171.1	A/B	OFF	31	13016134	12992163	78951	32	12811702		38856	5.2	2.0	NA	97	NA	0	17046
01/09/06 08:32		A/B	NO	28	13072457	13048486	79293	25	12867467	12844173	39026	4.1	3.8	NA	103	NA	0	17046
01/10/06 16:42		A/B	OFF	32	13110211	13086240	79523	31	12904801		39139	5.1	4.9	NA	97	NA	0	17046
01/11/06 09:25		A/B	OFF	31	13119286	13095315	79578	28	12913760	12890466	39166	5.1	2.0	NA	26	Ä	0	17046
01/12/06 09:58	5239.1	A/B	PFF FF	31	13143237	13119266	79723	30	12937427	12914133	39238	5.1	6.4	NA V	97	AN S	0	17046
01/13/06 13:20	5555.5	ָבְ בַּ	ב ב	32	13173033	13131662	19921	87	12909399	12940303	39330		0.0	000	97	8	0	17046
01/16/06 09.39	53023	0 Q		٠ د	13254001	13237522	80472	200	13021239	13031303	39507	0.0	0. T	103	97	06 0	0	17046
01/18/06 17:05	5319.1	A/B	. HO	300	13292885		80633	300	13085544	13062250	39688	5.0	4.9	102	97	8 8	0	17046
01/19/06 10:00	5324.3	A/B	OFF	31		_	80692	30	13095162	13071868	39718	5.1	2.0	102	26	06	0	17046
01/20/06 16:14	5342.6	A/B	NO	29	13336767	13312796	80899	27	13129051	13105757	39821	4.5	3.9	105	100	95	0	17046
01/23/06 09:28	5372.4	A/B	OFF	28	13392515	13368544	81238	28	13184043	13160749	39988	4.2	4.0	105	102	96	0	17046
01/24/06 16:39	5391.8	A/B	OFF	30	13428623		81458	30	13219770	13196476	40096	2.0	4.8	102	86	06	0	17046
01/25/06 16:18	5403.6	A/B	OFF	31			81592	29	13241694	13218400	40163	2.0	2.0	102	26	06	0	17046
01/26/06 13:24		A/B	OFF	31	13468232	13444261	81698	30	13259030	13235736	40216	2.0	2.0	102	97	06	0	17046
01/30/06 09:40		A/B	NO	28	13552347	13528376	82209	30	13342307	13319013	40469	4.1	3.9	107	102	35	0	17046
01/31/06 10:12	5470.0	A/B	OFF	32	13574880	13550909	82346	29	13364371	13341077	40536	2.0	2.0	102	97	90	0	17046

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

					Tank A F	k A Flow Meter			Tank B F	Tank B Flow Meter		Р			Pressure		Re	Recycling
Date and Time	Hour	Lead/L		Flowr	:	i	Bed	Flowr	:	i	Bed	i	1		Between		Flow	
	Meter	ag A/R	Well #3	ate	Totalizer	Cum. Flow	Volume	ate	Totalizer	Cum. Flow	Volume	<u>ا</u>	+	Inlet	Tanks	Outlet	Kate	Totalizer
70.04	= 7	ָ ק		uldb	gai	gai	00,400	gbin	gal	gal	10004	lsd V		psig	psig	)isd	gpın	gai
02/01/06 10:21	5462.4	0 X	S G	32	13622566	13573626	82636	30	1336/0/6	13388283	40005	0. C	ы Э	100	104	000	0 0	17046
02/03/06 16:43	5513.1	A/B	NO S	28	13655366	13631395	82835	300	13444092	13420798	40778	4.5	4.0	105	101	95	0	17046
02/06/06 09:36	5542.6	A/B	OFF	31	13710347	13686376	83170	32	13498557	13475263	40943	5.0	2.0	103	46	06	0	17046
02/07/06 10:39	62223	A/B	OFF	31	13735360	13711389	83322	31	13523375	13500081	41019	5.0	4.9	103	46	06	0	17046
02/08/06 09:31	6.9955	A/B	OFF	32	13756133	13732162	83448	30	13543974	13520680	41081	2.0	4.9	103	26	06	0	17046
02/09/06 09:03	5578.7	A/B	OFF	31	13777697	13753726	83579	31	13565327	13542033	41146	5.0	4.7	104	26	06	0	17046
02/10/06 14:24	5296.2	A/B	OFF	30	13810507	13786536	83778	29	13597829	13574535	41245	2.0	2.0	101	96	06	0	17046
02/13/06 09:57	5628.4	A/B	OFF	31	13870469	13846498	84143	30	13657256	13633962	41426	2.0	4.9	103	26	06	0	17046
02/14/06 13:00	5644.1	A/B	OFF	31	13899550	13875579	84319	30	13686045	13662751	41513	2.0	4.8	102	46	68	0	17046
02/15/06 09:00	5651.9	A/B	OFF	31	13914029	13890058	84407	30	13700395	13677101	41557	2.0	4.8	102	46	. 89	0	17046
02/17/06 13:25	5680.3	A/B	OFF	31	13967257	13943286	84731	59	13752459	13729165	41715	2.0	4.9	103	26	06	0.5	17871
02/21/06 10:24	5726.2	A/B	OFF	30	14052141	14028170	85247	30	13836534	13813240	41970	2.0	4.5	103	46		0	18147
02/22/06 09:39	9'2829	A/B	OFF	31	14073075	14049104	85374	30	13857251	13833957	42033	2.0	4.8	102	96		0	18147
02/23/06 09:08	5749.2	A/B	OFF	30	14094513	14070542	85504	31	13878460	13855166	42098	2.0	4.9	103	96		0	18147
02/24/06 13:00	5765.7	A/B	OFF	31	14124826	14100855	82688	31	13908472	13885178	42189	2.0	4.9	105	96		0	18147
02/27/06 10:12	5799.1	A/B	OFF	31	14186417	14162446	86063	31	13969479	13946185	42374	2.0	4.5	102	26		0	18147
02/28/06 10:03	5811.1	A/B	OFF	32	14208458	14184487	86196	32	13991295	13968001	42440	5.0	4.5	102	26	06	0	18147
03/01/06 09:46	5823.1	A/B	OFF	31	14230332	14206361	86329	33	14012925	13989631	42506	5.0	4.4	103	26	. 06	0	18147
03/02/06 09:25	5834.9	A/B	OFF	30	14251995	14228024	86461	31	14034347	14011053	42571	2.0	4.5	103	97	91	0	18147
03/06/06 08:56	5883.2	A/B	OFF	32		14317540	87005	30	14122679	14099385	42840	5.0	4.5	103	97	91	0	18147
03/07/06 08:36	5895.1	A/B	OFF	32	14363575	14339604	87139	30	14144475	14121181	42906	5.0	4.5	103	97		0	18147
03/08/06 10:30	5909.3	A/B	OFF	32	14389539	14365568	87297	30	14170139	14146845	42984	5.0	4.4	105	26	06	0	18147
03/09/06 14:52	5925.7	A/B	OFF	31	14419956	14395985	87482	29	14200242	14176948	43075	2.0	4.5	103	26	06	0	18147
03/10/06 14:38	5937.7	A/B	OFF	31	14442175	14418204	87617	29	14222212	14198918	43142	5.0	4.5	103	97	. 30	0	18147
03/13/06 09:24	5969.1	A/B	OFF	30	14499221	14475250	87963	32	14279124	14255830	43315	2.0	4.5	103	96	06	0	18147
03/14/06 09:07	5981.0	A/B	OFF	31	14521661	14497690	88100	28	14300850	14277556	43381	5.0	4.9	103	96	90	0	18147
03/15/06 09:09	5993.2	A/B	NO	27	14544115	14520144	88236	29	14323065	14299771	43449	4.1	3.9	106	103		0	18147
03/16/06 10:30	6006.7	A/B	OFF	30	14568595	14544624	88385	29	14347291	14323997	43522	5.0	4.9	103	96	90	0	18147
03/20/06 10:00	6054.4	A/B	OFF	31	14657330	14633359	88924	30	14435059	14411765	43789	2.0	4.8	104	96		0	18147
03/21/06 16:26	6073.7	A/B	OFF	31	14693234	14669263	89142	32	14470576	14447282	43897	2.0	2.0	104	96		0	18147
03/22/06 14:58	6084.4	A/B	OFF	32		14689174	89263	32	14490217	14466923	43956	5.1	4.9	103	96		0	18147
03/24/06 16:50	6110.7	A/B	OFF	29	14761852	14737881	89559	27	14538348	14515054	44103	4.2	4.0	105	101		0	18147
03/27/06 09:02	6139.5	A/B	OFF	31	יואי	14791323	89884	30	14591157	14567863	44263	5.0	4.5	103	97		0	18147
03/29/06 09:48	0.4010	A/B	<u> </u>	30	14861749	1483///8	90.166	87	14637115	14613821	44403	0.c	0.0	104	90		0	18147
03/31/06 16:24	7.28.19	A/B	7 5	30	14919782	14895811	90519	78	14694554	146/1260	445//	0.0	2.0	103	97		0	18147
04/03/06 09:04		0 X	1 11	ر د د	149/4160	14920209	90850	30	14/46252	14727858	44/40	0.0	ь. Б. С	102	97	- G	0 0	18147
04/05/06 09:14	_	7 A	- L	3 8	15019762	14995791	91032	30	14793291	14769997	44877	7 0	0.0	104	70	9	0	18147
04/06/06 10:20	62627	A/B	OFF	30	15044705	15020734	91278	30	14817909	14794615	44952	2.0	2.6	103	76	91	0	18147
04/07/06 16:25	6281.0	A/B	OFF	31	15078882	15054911	91486	28	14851638	14828344	45055	5.0	5.0	102	97	06	0	18147
04/10/06 10:02	6311.2	A/B	OFF	31	15134563	15110592	91824	28	14906823	14883529	45222	5.0	5.0	103	26	06	0	18147
04/11/06 09:57	6323.3	A/B	OFF	31	15157471	15133500	91963	28	14929104	14905810	45290	5.0	5.0	103	97	06	0	18147
04/12/06 10:18		A/B	OFF	32	15180919	15156948	92106	33	14952248	14928954	45360	5.0	5.0	102	97		0	18147
04/13/06 09:35	6347.3	A/B	OFF	31	15202283	15178312	92236	30	14973340	14950046	45424	2.0	2.0	102	46		0	18147
04/14/06 14:21	6364.3	A/B	OFF	30	15234224	15210253	92430	32	15004900	14981606	45520	2.0	2.0	103	86	06	0	18147
			1		-								1					

EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

				Iank A F							;			Lessale		-	
Date and Time		# II W	Flowr	Totalizar	mole and	Bed	Flowr	Totalizar	mole and	Bed	ŕ	2	4014	Between	*O #10	Flow	Totalizar
hr	AVB	JJO/uO	gbm	gal	gal		gpm	gal	gal	a non	psi -	psi is	psig	psig	psig	gpm	gal
04/17/06 09:55 6396.	2	OFF	32	÷	15270143	92794	31	15064081	15040787	45700	5.5	5.0	102		)6		18147
04/18/06 10:30 6409.:	7	OFF	31	15317499	15293528	92936	31	15087194	15063900	45770	5.1	2.0	102	97	06	0 (	18147
	.0 A/B	OFF	32	15335733		93047	31	15105208	15081914		5.1	5.0	102	97	)6	0 (	18147
_	_	OFF	31	15360560		93198		15129713	15106419		5.1	5.0	102	97	)6	0	18147
	_	OFF	31	15393895		93400		15162566	15139272		5.5	5.0	102	98	)6	0	18147
04/24/06 08:57 6480.8	8 A/B	OFF	30	15450227	15426256	93742	33	15218285	15194991	46169	2.0	4.9	103	86	.6	0	18147
6 10:17 6491.5	L	OFF	30		15446236	93864	30	15238095	15214801	46229	5.2	4.8	102	26	06	0	18147
04/28/06 15:44 6521.3		OFF	31	15526235	15502264	94204	30	15293195	15269901	46396	5.0	4.8	103	98	91	0	18147
05/01/06 09:24 6551.6	L	OFF	30	15582515	15558544	94546	29	15348554	15325260	46564	2.0	4.9	102	86	06	0	18147
05/02/06 10:54 6565.3	L	OFF	30	15608029		94701	33	15373668	15350374	46641	5.0	4.9	101	97	06	0	18147
-	_	OFF	31	15626650	15602679	94815	30	1539	AN	ΑN	5.1	4.9	102	97	06	0	18147
_	_	OFF	32	15683501	15659530	95160	32	15447916	15424622	46866	5.0	5.0	103	97	91	0	18147
05/08/06 09:02 6636.6	┡	OFF	32	15738939	15714968	95497	31	15502595	15479301	47032	5.0	4.8	102	97	16	0	18147
		NO	28	15761981	15738010	95637	26	15525303	15502009	47101	4.1	3.9	105	102	)6	0	18147
	.4 A/B	OFF	31	15786431		95785	30	15549413	15526119	47175	5.0	2.0	102	97	06	0	18147
05/11/06 10:42 6674.9		OFF	30	15809513		95926	32	15572156	15548862	47244	5.1	2.0	101	98		0	18147
05/12/06 15:01 6691.4	<u> </u>	OFF	31	15839966	15815995	96111		15602128	15578834	47335	2.0	4.5	102	97		0	18147
05/15/06 10:11 6723.2		OFF	30	15898105	15874134	96464	30	15659420	15636126	47509	5.0	4.9	101	26	91	0	18147
05/17/06 08:50 6746.:	2	OFF	30	15940100	15916129	96719	32	15700792	15677498	47635	4.9	4.5	103	97	76	0 7	18147
05/22/06 09:50 6808.0	_	OFF	29	16052050	16028079	97400	27	15811485	15788191	47971	2.0	4.1	102	96	91	0	18147
05/24/06 10:00 6832.6	.6 A/B	OFF	29	16096980	16073009	97673	30	15854988	15831694	48103	4.6	4.2	101	97	91	0	18147
05/31/06 10:35 6918.5	.5 A/B	OFF	29	16249404	16225433	98599	27	16005244	15981950	48560	4.5	4.0	100	46	91	0	19153
06/12/06 09:06 7063.5	.5 A/B	NO	27	16493174	16469203	100080		16245932	16222638	49291	4.0	3.5	104	101	96	0	19153
06/14/06 14:26 7093.1		NO	22	16538489	16514518	100356	20	16290798	16267504	49427	2.9	2.5	101	96		0 (	19153
06/19/06 09:41 7149.3	L	OFF	24	16619819	16595848	100850	25	16371519	16348225	49673	3.0	2.9	96	84		0 (	19153
06/21/06 09:16 7173.3	.3 A/B	NO	22	16654163	16630192	101059	22	16405587	16382293	49776	2.9	2.1	101	100	66	0 8	19153
06/28/06 10:06 7259.5	.5 A/B	OFF	24	16776981	16753010	101805	22	16527171	16503877	50145	3.0	2.8	96	94	06	0 (	19153
07/03/06 10:10 7320.6		OFF	22	16862233	16838262	102323	20	16611740	16588446	50402	3.0	3.0	96	94	06	0	19153
_	.5 A/B	OFF	23	16894723	16870752	102520	22	16644007	16620713	20200	3.0	2.5	86	94	85	0	19153
07/10/06 09:53 7405.4	4	OFF	23	16979702	16955731	103037	22	16728392	16705098	50757	4.0	3.5	92	96	06	0 (	19153
07/12/06 12:15 7432.2		OFF	22	17016599	16992628	103261	22	16764976	16741682	50868	2.5	2.0	94	92		0 6	19153
07/17/06 08:30 7489.6	.6 A/B	OFF	22	17089490	17065519	103704	22	16837581	16814287	51089	2.5	2.0	92	93	06	0	19153
06 10:30 7516.	_	OFF	22	17123085	17099114	103908	22	16871032	16847738	51190	2.5	2.0	95	93		0	19153
07/24/06 10:18 7576.5	_	OFF	21	17199655	17175684	104373	20	16947251	16923957	51422	2.5	2.0	92	92	06	0 (	19153
		OFF	20	17306311	17282340	105022	20	17053404	17030110	51744	2.2	2.0	92	94	6	0	19153
08/02/06 09:51 7685.9	.9 A/B	OFF	20	17336224	17312253	105203	21	17083209	17059915	51835	2.2	2.0	92	93	)6	0 (	19153
06 09:55 7746.9	Ш	OFF	20	17412012	17388041	105664	20	17158558	17135264	52064	2.0	2.0	94	93	)6	0 (	19153
08/09/06 09:46 7771.2		OFF	20	17441042	17417071	105840	19	17187481	17164187	52152	2.0	1.9	94	93	06	0 (	19153
	9	OFF	19	17513794	17489823	106282	17	17260085	17236791	52372	2.0	2.0	93	66	)6	0 (	19153
-		OFF	19	17545866	17521895	106477	19	17291792	17268498	52469	2.0	2.0	63	92	)6	0.5	19182
08/23/06 17:20 7949.3		OFF	18	17647726	17623755	107096	16	17393291	17369997	52777	1.5	1.8	94	06	16	0	19857
08/28/06 08:31 8001.5		OFF	18	17703458	17679487	107435	16	17448958	17425664	52946	1.5	1.5	63	66	.6	0	19857
11/07/06 00:00 NA	NA	NA	NA	NA	AN	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	۱ NA	NA
		OFF	32	17733317	0	NA	30	17479226	0	0	4.1	3.8	103	100	66		19857
11/28/06 08:40 8062.8	.8 B/A	NO	26	17752542	19225	58	25	17496940	17714	108	3.0	3.0	109	106	102	0	19857
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EPA Arsenic Demonstration Project at Rimrock, AZ - Daily System Operation Log Sheet

					Tank A F	A Flow Meter			Tank B	Tank B Flow Meter		dР			Pressure		Re	Recycling
Time of the	Hour	Lead/L		Flowr			Bed	Flowr			Bed				Between		Flow	
Date and IIIIe	Meter	ag	Well #3	ate	Totalizer	Cum. Flow	Volume	ate	Totalizer	Cum. Flow	Volume	Δ	ТВ	Inlet	Tanks	Outlet	Rate	Totalizer
	hr	Α⁄Β	On/Off	mdb	gal	gal		mdb	gal	gal		psi	psi	psig	psig	psig	dbm	gal
12/11/06 10:30	8294.1	B/A	OFF	34	18202419	469102	1425	30	17912510	433284	2633	4.1	4.0	102	101	66	0	19857
12/18/06 09:00	8460.6	B/A	OFF	33	18530106	682962	2421	30	18216417	737191	4480	4.1	4.0	102	101	66	0	19857
12/27/06 10:13 8677.6	9.7798	B/A	OFF	33	18956487	1223170	3716	30	18612813	1133587	6889	4.1	4.0	104	100	66	0	19857
01/03/07 00:00	8844.2	B/A	OFF	33	19281942	1548625	4705	30	18915750	1436524	8729	4.1	4.0	104	101	66	0	19857
02/07/07 09:30	9684.4	B/A	OFF	32	20921512	3188195	2896	58	20435149	2955923	17963	4.1	4.0	103	100	66	0	19857
03/07/07 07:15	10223	B/A	OFF	32	21958312	4224995	12837	58	21395094	3915868	23796	4.1	4.0	103	101	94	0	19857
03/28/07 11:30	10482	B/A	OFF	32	22449876	4716559	14331	28	21849540	4370314	26558	3.9	3.9	103	101	94	0.5	19871

Note: Bed volume calculation based on 22  $\mathrm{tt}^3$  of media per vessel. Highlighted rows indicate backwash; highlighted columns indicated calculated values; NA = data not available.

## APPENDIX B ANALYTICAL DATA TABLES

Analytical Results from Long-Term Sampling, Rimrock, AZ

Sampling Date			:/90	06/30/04			0//0	07/07/04			07/1	07/14/04			07/2	07/21/04	
Sampling Location Parameter U	on Unit	NI	AC	TA	TB	N	AC	TA	TB	NI	AC	TA	TB	N	AC	TA	TB
Bed Volume	$10^{3}$	I	ı	6.0	0.4	ı	1	1.8	6.0	ı	ı	2.7	1.4	Ι	1	3.7	1.9
Alkalinity	$mg/L^{\rm (a)}$	355	-	367	351	330	-	382	365	383	1	371	367	379	Ι	375	383
Fluoride	mg/L	0.3	_	0.3	0.3	ı	_	-	Ι	ı	I	ı	1	1	-	1	ı
Sulfate	mg/L	9.4	_	9.4	9.4	-	_	_	-	-	-	-	_	_	_	-	1
Nitrate (as N)	mg/L	0.3	ı	0.3	0.3	ı	-	-	ı	ı	I	ı	- 1	1	ı	ı	ı
Orthophosphate (as P)	mg/L	<0.1	ı	<0.1	<0.1												
Silica (as SiO <sub>2</sub> )	mg/L	26.0	1	25.4	23.9	25.7	1	24.4	24.1	24.0	ı	24.3	23.9	26.1	ı	25.9	25.1
Turbidity	UTU	0.5	ı	0.3	0.4	0.3	ı	0.2	9.0	<0.1	ı	0.2	6.0	0.3	ı	0.3	0.4
Hd	ı	7.0	7.4	7.0	7.0	7.0	7.2	7.0	7.0	7.0	7.2	7.1	7.1	6.9	7.2	7.0	7.0
Temperature	သ	21.5	21.2	22.9	23.7	24.1	22.3	21.9	22.1	22.4	22.4	22.7	23.1	24.1	23.5	23.1	23.2
DO	mg/L	3.8	4.9	3.6	3.8	4.1	5.0	4.1	3.7	3.5	4.7	3.7	3.6	4.7	8.9	9.9	6.9
ORP	mV	475	259	637	649	476	969	969	611	488	209	619	628	510	809	621	624
Free Chlorine (as Cl <sub>2</sub> )	mg/L	1	0.4	0.4	0.4	ı	0.4	0.4	0.4	ı	0.4	0.4	0.4	-	0.5	0.5	0.4
Total Chlorine (as Cl <sub>2</sub> )	mg/L	_	9.0	9.0	0.6	-	0.7	9.0	0.5	-	9.0	9.0	9.0	_	0.5	0.5	0.5
Total Hardness	$mg/L^{\rm (a)}$	287	_	298	299	1	_	-	1	_	_	_	I	1	_	-	I
Ca Hardness	$mg/L^{\rm (a)}$	171	_	175	174	ı	_	-	ı	_	_	_	I	1	-	ı	I
Mg Hardness	$mg/L^{\rm (a)}$	116	-	123	124	-	-	-	1	1	1	1	ı	1	1	-	1
As (total)	ng/L	59.2	_	1.0	0.3	78.5	_	1.2	0.3	79.2	-	0.8	0.3	58.8	_	0.7	0.4
As (soluble)	ng/L	59.1	_	6.0	0.3	ı	_	1	ı	ı	_	-	ı	ı	_	ı	ı
As (particulate)	ng/L	0.1	_	0.1	<0.1	ı	_	-	ı	-	_	-	ı	ı	-	ı	ı
As (III)	ng/L	0.8	_	9.0	0.3	ı	-	1	I	ı	-	_	I	1	-	ı	ı
As (V)	ηg/L	58.3	-	0.3	<0.1	-	-	_	_	-	-	-	ı	-	_	-	1
Fe (total)	ng/L	<25	_	<25	<25	<25	_	<25	<25	<25	_	<25	<25	<25	_	<25	47.3
Fe (soluble)	ng/L	<25	_	<25	<25	1	_	-	_	-	_	_	_	1	_	-	1
Mn (total)	µg/L	1.0	Ţ	0.4	0.4	0.7	Ţ	<0.1	<0.1	0.4	1	<0.1	<0.1	1.6	1	0.4	0.4
Mn (soluble)	µg/L	1.1	ı	0.7	0.6	I	ı	ı	ı	ı	ı	I	I	I	ı	ı	I
OJeJ sy (e)				1													1

(a) As CaCO<sub>3</sub>. IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B.

# Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			.//0	07/28/04			08/04/04	4/04			08/11/04	1/04			08/18/04	8/04	
Sampling Location Parameter U	on Unit	NI	AC	TA	TB	N	AC	TA	TB	ZI	AC	TA	TB	N	AC	TA	TB
Bed Volume	$10^{3}$	_	-	4.6	2.3	-	ı	5.6	2.8	_	ı	9.9	3.3	_	ı	7.5	3.7
Alkalinity	$mg/L^{\rm (a)}$	369	_	381	377	379	1	367	395	376	ı	376	381	363	ı	375	367
Fluoride	mg/L	0.3	-	0.3	0.3	-	Ι	-	-	-	Ι	_	Ι	_	_	_	-
Sulfate	T/gm	10.0	_	10.0	10.0	Ι	-	-	-	_	_	_	_	_	_	_	-
Nitrate (as N)	T/gm	0.2	ı	0.2	0.2	I	ı	ı	ı	I	I	ı	ı	ı	I	ı	ı
Orthophosphate (as P)	mg/L	<0.1	-	<0.1	<0.1	<0.1	1	<0.1	<0.1	<0.1	-	<0.1	<0.1	<0.1	_	<0.1	<0.1
Silica (as $SiO_2$ )	T/gm	24.6	ı	24.5	24.3	25.3	ı	25.6	25.0	25.3	I	25.2	25.0	25.6	I	25.6	25.3
Turbidity	UTN	0.2	ı	0.3	0.2	0.3	1	0.3	0.5	0.1	1	0.2	0.1	0.3	I	0.4	0.7
Hd	1	7.0	7.2	7.1	7.1	7.0	7.0	7.0	7.0	7.0	7.2	7.1	7.0	7.0	7.4	7.1	7.0
Temperature	J <sub>o</sub>	26.1	24.5	26.7	24.0	22.0	21.7	21.0	21.1	21.9	21.0	21.2	21.1	22.0	21.7	21.3	22.2
DO	mg/L	4.4	5.5	4.2	4.1	4.2	4.1	4.0	3.8	4.2	5.8	4.1	4.1	4.1	4.5	3.9	5.1
ORP	MV	484	590	669	613	203	609	634	647	247	287	627	641	239	552	614	622
Free Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.5	0.5	0.4	-	0.5	0.4	0.4	_	0.4	0.4	0.4	_	0.4	0.4	0.4
Total Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.0	9.0	0.5	-	0.5	0.5	0.5	_	0.4	0.4	0.4	_	0.4	0.4	0.4
Total Hardness	$mg/L^{\rm (a)}$	351	_	397	352	_	1	1	-	_	-	_	-	_	_	_	_
Ca Hardness	$mg/L^{\rm (a)}$	208	_	236	207	ı	ı	1	I	ı	ı	_	Ι	-	ı	-	-
Mg Hardness	$mg/L^{\rm (a)}$	143	_	161	145	-	1	_	-	_	1	_	-	_	_	_	_
As (total)	$\mu g/L$	56.0	-	1.0	0.3	81.4	1	1.4	0.3	57.0	ı	0.7	0.3	48.3	ı	0.7	0.3
As (soluble)	$\mu g/L$	57.6	ı	1.0	0.3	ı	ı	ı	ı	ı	ı	ı	ı	ı	I	ı	ı
As (particulate)	$\mu g/L$	<0.1	ı	<0.1	<0.1	ı	ı	ı	ı	ı	ı	ı	ı	ı	I	ı	ı
As (III)	µg/L	1.0	ı	0.8	9.0	ı	ı	ı	I	ı	I	I	ı	I	I	ı	ı
As (V)	T/Bn	56.6	_	0.2	<0.1	I	Ι	-	-	-	-	_	_	_	_	_	-
Fe (total)	η/gπ	<25	_	<25	<25	<25	_	<25	<25	<25	_	<25	<25	<25	_	<25	<25
Fe (soluble)	$\mu g/L$	<25	Ι	<25	<25	ı	ı	ı	ı	ı	ı	1	ı	1	ı	1	-
Mn (total)	µg/L	0.3	ı	<0.1	<0.1	0.5	ı	<0.1	<0.1	0.8	ı	0.2	<0.1	0.4	I	<0.1	0.1
Mn (soluble)	$\mu g/L$	0.4	ı	<0.1	<0.1	ı	1	ı	ı	1	ı	ı	1	ı	1	ı	ı

(a) As  $CaCO_3$ . IN = at inlet; AC = after prechlorination (field parameters only); <math>TA = after tank A; TB = after tank B.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			08/2	08/25/04			09/01/04	1/04			09/08/04	3/04			09/15/04	5/04	
Sampling Location Parameter	on Unit	Z	AC	TA	TB	Z	AC	TA	TB	Z	AC	TA	TB	Z	AC	TA	TB
Bed Volume	$10^{3}$	_	ı	8.5	4.2	-	-	9.4	4.7	-	_	10.4	5.2	_	-	11.3	5.6
Alkalinity	$mg/L^{(a)}$	329	-	363	367	371	I	375	371	383	I	375	375	372 376	-	376 372	372 384
Fluoride	mg/L	0.3	-	0.3	0.3	_	_	_	-	_	_	_	_	_	-	_	1
Sulfate	mg/L	10.0	-	8.6	10.0	1	-	-	ı	ı	-	ı	-	-	-	I	ı
Nitrate (as N)	mg/L	0.2	ı	0.2	0.2	_	_	-	ı	ı	_	-	-	_	ı	I	ı
Orthophosphate (as P)	mg/L	<0.1	ı	<0.1	<0.1	<0.1	ı	<0.1	<0.1	<0.1	I	<0.1	<0.1	<0.06	-	<0.06	<0.06
Silica (as SiO <sub>2</sub> )	mg/L	26.7	-	27.2	26.9	25.3	ı	25.2	25.1	25.6	I	25.2	25.6	25.9 25.6	-	25.6 25.0	25.9 25.5
Turbidity	NTU	0.1	-	0.1	<0.1	0.1	1	0.3	0.2	0.1	-	0.1	0.2	0.6	-	0.5	0.6
Hd	_	7.0	7.0	7.0	6.9	7.1	7.6	7.1	7.1	6.9	7.1	6.9	6.9	7.1	7.4	7.1	7.1
Temperature	°C	21.9	21.2	21.2	21.4	21.2	21.6	21.2	21.2	22.6	22.3	21.5	22.0	21.5	21.9	21.2	21.3
DO	mg/L	3.3	4.7	3.6	3.4	4.6	4.5	4.4	4.6	3.5	3.4	3.6	3.5	3.8	6.1	4.9	4.7
ORP	mV	210	610	649	658	213	809	637	637	431	642	899	685	226	578	619	633
Free Chlorine (as Cl <sub>2</sub> )	mg/L	ı	0.5	0.3	0.3	ı	0.4	0.3	0.3	ı	0.4	0.4	0.4	ı	0.4	0.4	0.4
Total Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.5	0.4	0.4	1	0.4	0.4	0.4	ı	0.5	0.5	0.5	-	0.4	0.4	0.4
Total Hardness	$mg/L^{(a)}$	305	1	319	328	1	-	-	ı	ı	-	ı	-	-	-	I	ı
Ca Hardness	$mg/L^{\rm (a)}$	183	I	182	182	ı	ı	ı	ı	ı	ı	ı	ı	ı	ı	ı	ı
Mg Hardness	$mg/L^{\rm (a)}$	122	ı	137	145	ı	ı	ı	ı	ı	ı	ı	ı	ı	ı	ı	ı
As (total)	µg/L	64.6	I	2.7	1.0	77.5	ı	1.1	0.4	78.5	I	1.1	0.4	55.3 60.2	ı	11 11	0.5
As (soluble)	µg/L	61.1	-	2.8	1.2	-	-	-	1	-	-	-	-	_	_	-	-
As (particulate)	µg/L	3.5	_	<0.1	<0.1	ı	1	ı	ı	ı	ı	ı	ı	ı	_	ı	I
As (III)	µg/L	2.1	_	2.7	1.1	I	ı	ı	ı	ı	ı	I	-	ı	_	ı	ı
As (V)	µg/L	59.0	_	0.1	0.1	_	_	-	-	-	_	_	-	_	-	_	_
Fe (total)	µg/L	<25	ı	<25	<25	<25	ı	<25	<25	<25	ı	<25	<25	\$\$\$	ı	\$25	\$25
Fe (soluble)	µg/L	<25	-	<25	<25	-	-	-	-	-	-	-	_	_	-	-	-
Mn (total)	µg/L	1.4	_	1.2	0.9	0.4	1	<0.1	<0.1	0.3	I	<0.1	0.1	0.4	-	0.2	0.1
Mn (soluble)	µg/L	0.5	ı	0.3	0.1	ı	ı	1	1	-	ı	1	ı	1	ı	ı	ı

(a) As  $CaCO_3$ . IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			/60	09/22/04			09/29/04	9/04			10/06/04	5/04			10/1	10/13/04	
Sampling Location Parameter U	on Unit	NI	AC	TA	TB	N	AC	TA	TB	ZI	AC	TA	TB	NI	AC	TA	TB
Bed Volume	$10^{3}$	_	-	12.3	6.1	-	_	13.4	9.9	_	-	14.3	7.1	_	_	15.3	7.6
Alkalinity	${\rm mg/L}^{\rm (a)}$	369	-	373	373	369	-	369	369	370	-	370	370	353	-	345	353
Fluoride	mg/L	0.4	_	0.5	0.3	Ι	-	_	-	-	-	-	I	-	_	-	_
Sulfate	mg/L	8.9	-	8.8	8.7	_	_	_	_	_	_	_	_	_	-	_	_
Nitrate (as N)	mg/L	0.2	ı	0.2	0.2	I	ı	-	ı	ı	ı	ı	I	ı	ı	ı	ı
Orthophosphate (as P)	mg/L	<0.06	ı	<0.06	<0.06	<0.06	ı	<0.06	>0.06	<0.06	ı	>0.06	<0.06	<0.06	I	<0.06	<0.06
Silica (as SiO <sub>2</sub> )	mg/L	25.9	ı	25.7	25.6	25.6	ı	25.8	25.8	25.7	ı	25.6	25.0	24.9	ı	25.2	24.9
Turbidity	UTN	0.1	ı	<0.1	0.1	<0.1	ı	<0.1	0.1	0.3	ı	0.5	0.2	0.2	ı	0.2	0.2
Hd	ı	7.0	7.4	7.0	7.0	7.0	7.0	7.0	7.1	7.0	7.0	7.0	7.0	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	NA <sup>(b)</sup>
Temperature	သ	20.1	20.0	20.2	20.3	20.9	21.0	21.0	21.0	20.8	20.6	20.7	20.6	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	NA <sup>(b)</sup>
DO	mg/L	4.1	6.4	5.7	4.2	4.1	5.2	4.4	4.2	3.9	6.3	3.5	4.0	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	NA <sup>(b)</sup>
ORP	Λm	214	584	909	622	224	268	909	617	148	552	290	593	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>
Free Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.4	0.4	0.4	-	0.3	0.3	0.3	-	0.2	0.2	0.2	-	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>
Total Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.5	0.4	0.4	Ι	0.4	0.4	0.4	-	0.2	0.2	0.2	-	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$
Total Hardness	$mg/L^{\rm (a)}$	332	_	340	332	_	_	_	-	_	_	-	_	_	_	_	_
Ca Hardness	$mg/L^{\rm (a)}$	191	Ι	196	201	ı	-	-	ı	ı	ı	ı	-	Ι	-	1	-
Mg Hardness	$mg/L^{\rm (a)}$	141	-	143	131	1	_	_	-	-	_	1	-	-	-	-	_
As (total)	μg/L	65.5	I	2.6	1.0	53.5	ı	1.4	6.0	54.1	ı	2.1	0.4	53.2	ı	1.4	0.2
As (soluble)	μg/L	65.0	Ι	2.4	0.7	ı	I	Ι	I	ı	ı	ı	I	I	ı	ı	ı
As (particulate)	ng/L	0.5	_	0.2	0.3	-	-	_	1	-	-	-	-	-	_	_	1
As (III)	ηg/L	1.8	-	1.8	0.2	Ι	-	-	ı	-	-	ı	-	1	-	-	1
As (V)	µg/L	63.2	_	0.6	0.5	1	-	_	-	-	_	-	-	-	_	-	-
Fe (total)	ηg/L	127	_	27	99	<25	_	<25	<25	<25	_	<25	<25	<25	_	<25	<25
Fe (soluble)	µg/L	<25	-	<25	<25	ı	-	-	ı	-	-	1	Ι	ı	-	-	-
Mn (total)	µg/L	0.8	I	0.3	0.5	0.3	ı	0.4	0.2	0.1	ı	0.2	<0.1	0.4	ı	<0.1	<0.1
Mn (soluble)	µg/L	0.4	ı	0.1	0.1	ı	ı	ı	ı	I	I	ı	I	ı	ı	ı	ı
(a) As CaCO. (b) Onsite water quality parameter not measured	site water c	mality para	meter not	measured													

<sup>(</sup>a) As CaCO<sub>3</sub>. (b) Onsite water quality parameter not measured. IN = at inlet; AC = after tank B; NA = data not available.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			10/2	10/20/04			10/27/04	7/04			11/03/04	3/04			11/17/04	,/04	
Sampling Location Parameter U	on Unit	NI	AC	TA	TB	NI	AC	TA	TB	ZI	AC	TA	TB	N	AC	TA	TB
Bed Volume	$10^{3}$	_	_	16.2	8.0	_	_	17.1	8.5	_	_	18.1	0.6	_	_	20.1	10.0
Alkalinity	$mg/L^{\rm (a)}$	277	_	377	373	98£	_	382	390	369	-	377	369	390	_	386	390
Fluoride	mg/L	0.4	ı	0.3	0.4	_	ı	ı	-	-	-	ı	I	-	-	1	ı
Sulfate	mg/L	8.6	-	9.4	9.6	_	-	-	I	_	-	1	I	_	_	1	ı
Nitrate (as N)	mg/L	0.2	-	0.2	0.2	I	ı	ı	I	ı	ı	I	I	I	ı	ı	ı
Orthophosphate (as P)	mg/L	<0.06	ı	<0.06	<0.06	<0.06	ı	<0.06	<0.06	<0.06	ı	>0.06	<0.06	<0.06	1	>0.06	<0.06
Silica (as SiO <sub>2</sub> )	mg/L	24.9	ı	25.0	24.6	25.2	ı	25.5	25.3	24.7	ı	25.0	25.0	25.6	ı	25.1	25.1
Turbidity	NTU	0.1	-	0.1	0.2	0.1	ı	0.1	0.3	0.2	ı	0.2	0.2	0.3	1	0.3	0.3
Hd	ı	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	6.9	6.9	6.9	6.9	6.9 <sup>(b)</sup>	6.9	6.9	8.9
Temperature	သ	20.1	20.1	20.3	20.3	19.5	19.8	19.7	19.7	20.4	20.6	20.6	20.6	20.7 <sup>(b)</sup>	20.7	21.2	20.8
DO	mg/L	4.0	4.5	4.1	4.1	4.2	3.6	3.7	3.6	4.0	3.8	4.1	3.9	3.8(b)	4.0	3.5	4.1
ORP	mV	190	637	681	710	216	552	577	290	180	491	265	591	504 <sup>(b)</sup>	619	640	651
Free Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.2	0.2	0.2	_	0.3	0.3	0.3	_	0.3	0.3	0.3	_	0.3	0.3	0.3
Total Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.2	0.2	0.2	_	0.4	0.4	0.4	-	0.4	0.4	0.4	-	0.3	0.3	0.3
Total Hardness	$mg/L^{\rm (a)}$	366	_	365	361	_	_	_	-	_	_	_	-	_	_	-	_
Ca Hardness	$mg/L^{\rm (a)}$	214	_	214	212	_	-	-	-	_	-	-	-	_	_	-	_
Mg Hardness	$mg/L^{\rm (a)}$	152	_	150	149	-	_	-	ı	-	-	Ι	_	_	-	1	_
As (total)	µg/L	50.8	1	1.3	1.0	56.5	ı	1.6	0.8	56.3	ı	1.6	0.8	56.5	ı	1.3	1.3
As (soluble)	µg/L	50.2	_	1.1	0.7	ı	ı	ı	ı	ı	-	ı	I	ı	ı	ı	ı
As (particulate)	µg/L	9.0	_	0.3	0.3	_	-	-	-	_	-	-	-	_	_	-	_
As (III)	µg/L	2.2	_	1.3	1.3	-	-	-	ı	-	-	Ι	Ι	-	-	ı	_
As (V)	µg/L	48.0	_	<0.1	<0.1	_	_	-	-	_	-	1	-	_	_	1	-
Fe (total)	µg/L	<25	_	<25	<25	<25	_	27.0	<25	<25	_	31.1	<25	<25	_	<25	<25
Fe (soluble)	µg/L	<25	_	<25	<25	-	-	-	ı	-	-	-	Ι	-	ı	1	_
Mn (total)	µg/L	0.6	ı	<0.1	0.3	0.2	ı	0.2	<0.1	0.3	ı	0.4	0.2	<0.1	ı	<0.1	0.9
Mn (soluble)	ng/L	1.0	ı	<0.1	<0.1	_	-	ı	ı	-	-	ı	1	1	1	1	ı
(a) As CaCO. (b) Measurement mossibly taken from incorrect location	urement	possibly tak	en from in	ncorrect loc	ation												

(a) As CaCO<sub>3</sub>. (b) Measurement possibly taken from incorrect location. IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B.

# Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			12/(	12/01/04			12/15/04 <sup>(b)</sup>	(04 <sup>(b)</sup>			01/02	01/05/05 <sup>(c)</sup>			01/19/05	50/6	
Sampling Location Parameter	on Unit	ZI	AC	TA	TB	N	AC	TA	TB	ZI	AC	TA	TB	ZI	AC	TA	TB
Bed Volume	$10^{3}$	_	_	22.1	10.9	-	-	24.1	11.9	_	_	27.2	13.5	-	_	29.3	14.5
Alkalinity	${\rm mg/L}^{\rm (a)}$	365 365	ı	365 365	365 370	383	ı	370	366	380	-	372	389	378	1	387	374
Fluoride	mg/L	-	_	-	-	0.4	1	0.4	0.3	_	-	-	-	1	1	-	1
Sulfate	mg/L	ı	_	-	1	6.7	ı	9.1	8.8	_	-	-	-	1	ı	-	ı
Nitrate (as N)	mg/L	_	_	-	-	0.2	_	0.2	0.2	_	_	_	ı	_	_	-	-
Orthophosphate (as P)	mg/L	<0.06	-	<0.06	<0.06	<0.06	ı	<0.06	<0.06	ı	ı	I	ı	ı	I	ı	ı
Silica (as SiO <sub>2</sub> )	mg/L	25.5 25.3	_	25.2 25.4	25.3 25.3	25.9	1	26.4	26.3	26.1	_	26.3	26.9	23.9	Ι	24.8	24.9
Turbidity	NTU	0.1	-	0.1	0.1	0.2	ı	0.2	0.1	0.3	I	<0.1	0.2	<0.1	I	<0.1	<0.1
Hd	ı	7.0	6.9	6.9	6.9	6.9	6.9	6.9	6.9	$NA^{(d)}$	$NA^{(d)}$	$NA^{(d)}$	$NA^{(d)}$	7.1	7.0	7.0	7.0
Temperature	J <sub>o</sub>	20.1	21.2	20.6	21.1	20.6	20.1	20.4	20.0	20.5	20.7	20.7	20.3	21.1	20.9	20.9	20.3
DO	mg/L	4.3	3.4	3.9	3.5	4.0	3.2	3.5	3.4	3.5	4.1	3.4	4.1	4.3	4.0	4.1	4.1
ORP	mV	267	626	646	673	230	618	099	672	223	571	605	470	214	620	645	829
Free Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.4	0.4	0.4	_	0.3	0.3	0.3	_	0.2	0.2	0.2	_	0.4	0.4	0.4
Total Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.5	0.5	0.5	_	0.4	0.3	0.3	_	$NA^{(e)}$	$NA^{(e)}$	$NA^{(e)}$	_	0.5	0.5	0.5
Total Hardness	$mg/L^{\rm (a)}$	_	_	-	1	384	-	374	377	_	_	_	-	-	_	-	_
Ca Hardness	$mg/L^{\rm (a)}$	_	_	_	_	241	_	234	235	_	_	_	_	_	_	_	_
Mg Hardness	$mg/L^{\rm (a)}$	_	_	_	_	143	-	140	142	_	_	_	_	_	1	_	1
As (total)	µg/L	51.4 52.3	ı	1.7	0.4 0.4	60.3	ı	3.0	8.0	43.8	ı	2.5	0.2	51.3	I	4.4	9.0
As (soluble)	µg/L	_	_	_	_	59.6	_	3.0	9.0	_	_	_	_	_	_	_	_
As (particulate)	µg/L	_	_	_	_	0.7	_	<0.1	0.2	_	_	_	_	_	_	_	_
As (III)	µg/L	_	_	_	-	1.2	-	1.3	0.7	_	_	_	_	_	_	_	_
As (V)	$\mu g/L$	_	_	-	1	58.4	-	1.7	<0.1	_	_	_	-	-	_	-	_
Fe (total)	hg/L	<25 <25	-	<25 <25	<25 <25	<25	-	<25	<25	<25	_	<25	<25	<25	-	<25	<25
Fe (soluble)	µg/L	_	_	1	1	<25	ı	<25	<25	_	-	-	-	1	1	-	-
Mn (total)	µg/L	0.1	_	<0.1	<0.1 <0.1	0.3	-	<0.1	0.2	<0.1	_	<0.1	<0.1	0.2	1	<0.1	0.3
Mn (soluble)	µg/L	_	_	_	-	0.1	_	<0.1	<0.1	_	_	_	_	_	_	_	_
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<sup>(</sup>a) As CaCO<sub>3</sub>. (b) Water quality measurements taken on 12/16/04. (c) Water quality measurements taken on 01/06/05. (d) pH probe not working properly. (e) Onsite water quality parameter not measured. IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B; NA = data not available.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			02/0	02/02/05			02/16/05	20/9			03/02/05	2/05			03/16/05	5/05	
Sampling Location Parameter	on Unit	N	AC	TA	TB	N	AC	TA	TB	NI	AC	TA	TB	N	AC	TA	TB
Bed Volume	$10^{3}$	_	-	31.1	15.4	-	-	33.2	16.4	1	-	35.1	17.4	-	-	37.1	18.4
Alkalinity	$mg/L^{\rm (a)}$	414	1	387	405	392	I	374	405	378 378	ı	369 373	391 386	388	1	392	401
Fluoride	T/gm	_	_	_	-	0.3	-	0.3	0.3	-	-	-	-	_	_	-	_
Sulfate	mg/L	_	_	_	-	10.0	-	10.0	10.0	-	1	-	-	_	_	-	_
Nitrate (as N)	T/gm	-	-	_	-	0.3	_	0.3	0.3	-	-	1	1	-	_	1	_
Silica (as $SiO_2$ )	T/gm	24.9	ı	24.5	24.8	27.6	-	27.5	27.4	26.2 26.2	ı	26.4 26.3	26.5 26.1	26.4	1	26.4	25.8
Turbidity	UTN	0.1	-	<0.1	<0.1	0.1	1	<0.1	0.2	<0.1	1	0.1	0.1	<0.1	1	0.1	<0.1
Hd	_	8.9	8.9	8.9	8.9	6.9	6.9	6.9	6.9	6.9	6.9	6.9	8.9	8.9	8.9	8.9	6.8
Temperature	J <sub>o</sub>	18.6	19.2	19.7	20.1	20.4	20.0	20.2	20.1	20.5	20.2	20.2	20.3	18.8	19.5	19.4	19.6
DO	mg/L	4.2	3.9	3.6	4.2	3.6	3.6	3.6	3.7	3.4	3.3	4.1	4.1	4.8	4.4	4.5	3.6
ORP	mV	258	643	664	670	448	643	671	693	490	625	654	673	209	616	645	656
Free Chlorine (as Cl <sub>2</sub> )	mg/L	1	0.5	0.4	0.4	1	0.4	0.3	0.3	1	0.3	0.3	0.3	-	0.3	0.3	0.3
Total Chlorine (as Cl <sub>2</sub> )	mg/L	Ι	0.5	0.5	0.5	1	0.5	0.4	0.4	ı	0.4	0.4	0.4	-	0.3	0.4	0.4
Total Hardness	${\rm mg/L}^{\rm (a)}$	-	_	_	-	302	-	311	305	-	1	_	_	_	-	_	_
Ca Hardness	$mg\!/\!L^{\rm (a)}$	ı	ı	_	ı	183	ı	161	188	ı	ı	1	1	ı	ı	-	_
Mg Hardness	${\rm mg/L}^{\rm (a)}$	Ι	1	_	-	119	I	150	117	ı	I	ı	ı	-	-	ı	_
As (total)	µg/L	48.8	ı	4.7	1.9	52.5	ı	8.9	0.3	64.4 67.4	I	9.1	0.5	51.2	I	8.2	0.4
As (soluble)	μg/L	ı	1	_	ı	51.1	ı	9.9	0.3	1	ı	ı	ı	ı	I	ı	_
As (particulate)	μg/L	ı	ı	_	ı	1.4	ı	0.2	<0.1	ı	ı	ı	ı	ı	ı	ı	_
As (III)	µg/L	ı	ı	-	ı	6.0	ı	8.0	0.7	ı	ı	ı	ı	ı	ı	ı	1
As (V)	μg/L	ı	1	_	ı	50.2	ı	5.8	<0.1	1	ı	ı	ı	ı	I	ı	_
Fe (total)	T/Brl	<25	1	<25	32.7	<25	1	<25	<25	<25 <25	1	<25 <25	<25 <25	<25	-	<25	<25
Fe (soluble)	μg/L	ı	ı	ı	ı	<25	ı	<25	<25	ı	ı	ı	ı	ı	ı	ı	1
Mn (total)	µg/L	1.2	ı	0.2	12.4	0.3	ı	<0.1	<0.1	<0.1	ı	<0.1	0.1	<0.1	ı	<0.1	<0.1
Mn (soluble)	µg/L	_	_	_	-	<0.1	-	<0.1	<0.1	1	ı	1	1	1	ı	1	1
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<sup>(</sup>a) As  $CaCO_3$ . IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			03/3	03/30/02			04/13/05	3/05			04/27/05	20/2			05/11/05	20/1	
Sampling Location Parameter	on Unit	Z	AC	TA	TB	Z	AC	TA	TB	ZI	AC	TA	TB	Z	AC	TA	TB
Bed Volume	$10^{3}$	-	-	39.2	19.4	1	ı	41.1	20.3	I	ı	43.1	21.3	-	1	45.2	22.3
Alkalinity	$mg/L^{\rm (a)}$	383	_	378	383	401	1	424	410	405	-	396	396	400	1	396	400
Fluoride	mg/L	_	I	_	_	0.3	1	0.3	0.3	I	I	_	_	I	I	1	l
Sulfate	mg/L	ı	I	ſ	I	8.1	ı	7.8	8.1	I	I	ı	ı	ı	I	1	ı
Nitrate (as N)	mg/L	_	-	_	-	0.2	1	0.2	0.2	_	-	_	_	-	ı	-	_
Silica (as $SiO_2$ )	mg/L	26.1	_	26.1	26.0	27.0	1	27.3	27.0	26.1	-	26.3	26.1	26.0	1	26.2	26.2
Turbidity	NTU	<0.1	_	<0.1	<0.1	0.2	1	0.4	<0.1	0.1	_	0.1	<0.1	<0.1	1	<0.1	<0.1
Hq	1	6.9	6.9	6.9	8.9	6.9	6.9	6.9	6.9	6.8	6.9	6.9	6.9	6.9	6.9	6.9	6.9
Temperature	J <sub>o</sub>	20.6	20.1	20.2	20.2	20.0	20.0	20.2	20.3	20.9	20.3	20.5	20.5	19.8	20.0	20.0	20.0
DO	mg/L	0.9	3.4	3.6	3.5	3.8	3.9	4.1	3.9	4.7	3.3	5.4	4.3	3.5	3.6	3.7	3.7
ORP	mV	308	365	899	989	201	909	631	648	467	646	089	694	217	580	909	613
Free Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.4	0.4	0.4	-	0.4	0.4	0.4	-	0.5	0.5	0.5	_	0.5	0.5	0.5
Total Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.5	5.0	0.5	Ι	0.4	0.4	0.4	-	9.0	9.0	9.0	-	9.0	9.0	0.6
Total Hardness	${\rm mg/L}^{\rm (a)}$	-	_	_	-	325	-	322	326	I	I	_	_	-	_	-	_
Ca Hardness	$mg/L^{(a)}$	_	_	_	_	199	1	190	197	-	_	_	_	_	1	_	_
Mg Hardness	$mg/L^{\rm (a)}$	-	_	_	_	126	_	131	129	ı	_	_	_	_	_	-	_
As (total)	µg/L	52.7	-	10.3	0.5	51.9	1	8.8	0.5	58.7	1	13.3	0.5	50.3	1	11.7	0.5
As (soluble)	µg/L	ı	Ι	ı	ı	51.4	ı	8.9	0.4	ı	ı	-	-	ı	ı	ı	_
As (particulate)	$\mu g/L$	ı	Ι	ı	ı	0.5	ı	<0.1	<0.1	ı	ı	-	-	ı	ı	ı	_
As (III)	µg/L	ı	I	-	-	0.8	_	0.7	0.7	ı	ı	-	-	-	_	ı	_
As (V)	µg/L	-	_	-	-	50.6	Ι	8.2	<0.1	I	ı	_	-	-	1	1	_
Fe (total)	µg/L	<25	_	<25	<25	27.2	_	<25	<25	<25	_	<25	<25	<25	_	<25	25.8
Fe (soluble)	µg/L	ı	Ι	-	-	<25	1	<25	<25	ı	-	_	-	-	1	ı	_
Mn (total)	µg/L	0.5	I	0.4	0.4	0.2	ı	<0.1	<0.1	0.4	ı	0.2	0.2	<0.1	ı	<0.1	<0.1
Mn (soluble)	µg/L	-	_	_	-	0.2	1	<0.1	<0.1	ı	1	-	ı	ı	1	ı	ı
														•		•	

(a) As CaCO<sub>3</sub>.

IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			05/2	05/25/05			90/80/90	8/05			06/22/05	2/05			01/06/05	2/05	
Sampling Location Parameter	n Unit	N	AC	TA	TB	N	AC	TA	TB	IN	AC	TA	TB	N	AC	TA	TB
Bed Volume	$10^{3}$	_	_	47.2	46.6	-	1	49.3	24.3	-	-	51.3	25.3	ı	-	53.3	26.3
Alkalinity	${\rm mg/L}^{\rm (a)}$	392 401	ı	401 401	401 397	400	I	387	387	374	I	374	383	374	ı	374	374
Fluoride	mg/L	_	_	-	-	0.3	1	0.2	0.2	-	-	_	_	-	_	_	_
Sulfate	mg/L	1	_	_	_	11.0	1	10.0	11.0	-	ı	I	I	ı	-	1	_
Nitrate (as N)	mg/L	Ι	_	_	-	9.0	1	0.3	0.3	I	1	I	1	ı	ı	1	_
Silica (as SiO <sub>2</sub> )	mg/L	25.6 25.3	1	25.9 25.0	25.3 25.9	26.8	I	26.6	26.5	25.3	I	25.3	25.3	26.2	ı	26.1	25.9
Turbidity	NTU	0.2	_	1.3	0.2	<0.1	1	<0.1	<0.1	0.7	1	6.0	0.2	0.2	-	<0.1	0.1
Hd	_	7.0	7.0	7.0	7.0	8.9	8.9	8.9	8.9	7.0	7.0	7.1	7.0	7.1	7.0	7.0	7.0
Temperature	°C	20.9	20.6	20.6	20.7	21.4	20.8	21.1	21.1	21.0	21.1	21.0	21.0	21.1	20.7	20.6	20.9
DO	mg/L	4.1	3.0	3.3	3.5	3.3	3.3	3.5	3.5	3.2	3.3	3.1	3.0	3.5	3.3	3.4	3.8
ORP	mV	194	571	809	611	447	594	620	627	182	009	628	637	182	580	618	624
Free Chlorine (as Cl <sub>2</sub> )	mg/L	1	0.5	0.5	0.5	-	0.3	0.3	0.3	-	0.3	0.3	0.3	ı	0.3	0.3	0.3
Total Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.5	0.5	0.5	-	0.3	0.3	0.3	_	0.3	0.3	0.3	_	0.3	0.3	0.3
Total Hardness	$mg/L^{\rm (a)}$	ı	_	-	Ι	323	I	323	329	1	ı	I	I	ı	-	1	_
Ca Hardness	$mg/L^{\rm (a)}$	I	_	ı	ı	197	ı	196	204	-	1	ı	ı	I	ı	-	_
Mg Hardness	$mg/L^{\rm (a)}$	Ι	_	Ι	Ι	127	I	126	125	1	I	I	I	I	ı	ı	_
As (total)	µg/L	49.7 50.3	ı	13.3 13.3	0.4	57.6	I	17.2	1.2	55.4	1	18.3	0.9	49.2	ı	15.6	0.5
As (soluble)	µg/L	ı	I	ı	ı	59.8	ı	18.8	1.1	ı	_	ı	ı	ı	ı	1	1
As (particulate)	µg/L	I	ı	ı	ı	<0.1	ı	<0.1	<0.1	ı	ı	ı	ı	I	ı	ı	ı
As (III)	µg/L	I	1	ı	ı	1.2	ı	1.2	1.9	-	_	ı	ı	ı	ı	1	1
As (V)	$\mu g/L$	ı	I	ı	ı	58.6	ı	17.6	<0.1	ı	ı	ı	ı	ı	ı	ı	1
Fe (total)	µg/L	<25 <25	-	<25 <25	<25 25</td <td>&lt;25</td> <td>ı</td> <td>&lt;25</td> <td>&lt;25</td> <td>&lt;25</td> <td>I</td> <td>&lt;25</td> <td>&lt;25</td> <td>&lt;25</td> <td>ı</td> <td>&lt;25</td> <td>&lt;25</td>	<25	ı	<25	<25	<25	I	<25	<25	<25	ı	<25	<25
Fe (soluble)	$\mu g/L$	1	_	-	-	<25	1	<25	<25	-	1	1	-	ı	-	-	1
Mn (total)	µg/L	0.1	1	<0.1	<0.1	0.2	ı	<0.1	0.1	0.3	1	0.2	0.2	0.2	ı	<0.1	<0.1
Mn (soluble)	µg/L	ı	-	1	ı	0.2	ı	0.1	<0.1	ı	ı	1	ı	ı	1	ı	ı
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(a) As CaCO<sub>3</sub>.

IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			07/2	07/21/05			08/03/02	3/05			08/17/05	20/2			08/31/05	50/1	
Sampling Location Parameter U	on Unit	NI	AC	TA	TB	N	AC	TA	TB	N	AC	TA	TB	N	AC	TA	TB
Bed Volume	$10^{3}$	-	I	55.5	27.3	-	-	57.3	28.2	-	-	59.3	29.2	-	1	61.2	30.1
Alkalinity	$mg/L^{\rm (a)}$	374	_	374	378	383	ı	378	378	374	1	383	387	365	1	378	374
Fluoride	mg/L	_	_	_	_	0.3	1	0.3	0.3	_	_	_	_	_	1	_	_
Sulfate	mg/L	I	I	1	I	10.0	1	10.0	10.0	ı	I	ı	ı	ı	I	ı	ı
Nitrate (as N)	mg/L	-	_	_	-	0.3	1	0.2	0.2	-	1	_	_	_	-	_	-
Silica (as SiO <sub>2</sub> )	mg/L	24.8	_	25.0	24.8	24.4	1	24.8	25.0	25.4	1	25.2	25.3	26.6	1	27.3	27.1
Turbidity	UTU	0.3	1	1.6	3.4	0.1	ı	0.1	0.1	<0.1	ı	<0.1	0.1	0.3	I	0.2	0.1
Hd	1	6.9	0.7	7.0	6.9	7.0	6.9	6.9	6.9	6.9	7.0	6.9	6.9	6.9	7.0	6.9	6.9
Temperature	J <sub>o</sub>	22.1	21.4	22.5	22.8	21.7	21.2	21.5	22.0	21.3	21.0	21.0	21.5	22.5	21.4	21.8	22.7
DO	mg/L	3.3	3.1	3.4	3.6	3.5	3.4	3.3	3.7	3.6	4.3	3.9	3.6	3.3	4.0	3.5	3.7
ORP	mV	439	809	628	989	434	611	630	642	399	593	593	633	470	612	610	809
Free Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.2	0.2	0.2	-	0.4	0.3	0.3	1	0.3	0.2	0.2	_	0.3	0.3	0.3
Total Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.3	0.3	0.3	-	0.5	0.4	0.4	_	0.3	0.3	0.3	-	0.4	0.4	0.4
Total Hardness	${\rm mg/L}^{\rm (a)}$	1	_	_	-	296	-	301	306	-	ı	_	-	-	_	-	_
Ca Hardness	$mg/L^{(a)}$	_	-	-	_	186	1	188	191	ı	ı	_	-	_	1	_	-
Mg Hardness	$mg/L^{\scriptscriptstyle (a)}$	-	-	_	_	110	-	112	115	_	-	_	-	_	_	_	_
As (total)	µg/L	50.8	ı	18.9	0.9	50.7	ı	19.5	0.7	51.6	-	19.1	0.8	54.4	ı	21.7	0.7
As (soluble)	µg/L	ı	ı	-	ı	50.8	ı	19.5	0.7	_	_	-	-	-	ı	ı	_
As (particulate)	µg/L	ı	1	ı	ı	<0.1	ı	<0.1	<0.1	_	_	_	_	1	ı	ı	_
As (III)	µg/L	ı	1	ı	ı	1.5	_	1.4	1.5	_	_	_	_	-	_	ı	_
As (V)	µg/L	I	ı	ı	ı	49.3	ı	18.1	<0.1	_	_	_	_	-	ı	ı	_
Fe (total)	µg/L	<25	1	<25	<25	<25	ı	<25	<25	<25	_	<25	<25	<25	ı	<25	<25
Fe (soluble)	µg/L	ı	1	-	ı	<25	_	<25	<25	_	_	_	_	-	_	ı	_
Mn (total)	µg/L	0.2	ı	<0.1	0.1	<0.1	ı	<0.1	<0.1	0.2	ı	0.1	<0.1	0.3	ı	<0.1	<0.1
Mn (soluble)	µg/L	ı	ı	1	ı	<0.1	1	<0.1	<0.1	ı	I	ı	ı	ı	ı	ı	-

(a) As  $CaCO_3$ . IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			09/1	09/14/05			09/28/05	8/05			10/1	10/12/05			11/09/05	/05	
Sampling Location Parameter U	on Unit	N	AC	TA	TB	Z	AC	TA	TB	N.	AC	TA	TB	Z	AC	TA	TB
Bed Volume	$10^{3}$	-	_	63.2	31.1	-	ı	65.1	32.0	-	-	$NA^{(b)}$	$NA^{(b)}$	1	1	70.9	34.9
Alkalinity	$mg/L^{\rm (a)}$	374	-	378	374	383	-	387	396	378	_	383	387	378	1	378	396
Fluoride	mg/L	1	_	_	-	1	I	1	1	0.2	-	0.2	0.2	1	1	-	I
Sulfate	mg/L	_	_	_	_	-	-	-	-	10	_	6.6	6.6	_	_	_	1
Nitrate (as N)	mg/L	ı	I	_	ı	Ι	I	ı	ı	0.2	I	0.2	0.2	ı	I	-	1
Phosphorus (as P)	µg/L	-	-	_	-	-	-	-	-	16.8	-	14.8	<10	11.5	-	12.1	<10
Silica (as SiO <sub>2</sub> )	mg/L	23.6	-	23.9	23.7	26.7	I	26.7	26.4	24.9	ı	24.2	23.9	25	ı	24.7	25.3
Turbidity	NTU	0.1	ı	0.3	0.4	0.1	ı	<0.1	0.1	<0.1	ı	<0.1	<0.1	0.1	ı	<0.1	<0.1
Hd	ı	7.0	7.0	0.7	7.0	7.0	7.0	6.7	7.0	$NA^{(c)}$	$NA^{(c)}$	(c)	$NA^{(c)}$	7.0	7.0	7.0	7.0
Temperature	J <sub>o</sub>	20.7	20.5	20.5	20.4	21.0	20.6	20.9	21.4	NA <sup>(c)</sup>	NA <sup>(c)</sup>	NA <sup>(c)</sup>	NA <sup>(c)</sup>	20.2	20.2	20.3	20.3
DO	mg/L	3.9	3.8	4.0	4.0	3.7	3.7	4.1	3.9	$NA^{(c)}$	$NA^{(c)}$	ω <b>(</b> Θ)	$NA^{(c)}$	3.7	3.7	4.0	4.0
ORP	mV	199	295	565	603	469	009	618	631	$NA^{(c)}$	$NA^{(c)}$	$NA^{(c)}$	$NA^{(c)}$	181	559	594	603
Free Chlorine (as Cl <sub>2</sub> )	mg/L	ı	0.3	0.3	0.3	ı	0.3	0.2	0.2	ı	$NA^{(c)}$	NA <sup>(c)</sup>	$NA^{(c)}$	1	0.3	0.2	0.2
Total Chlorine (as Cl <sub>2</sub> )	mg/L	1	0.4	0.4	0.4	-	0.3	0.3	0.3	-	$NA^{(c)}$	$NA^{(c)}$	$NA^{(c)}$	1	0.3	0.3	0.3
Total Hardness	$mg/L^{\rm (a)}$	_	_	_	-	-	-	-	-	322	_	325	328	1	_	_	_
Ca Hardness	$mg/L^{\rm (a)}$	-	_	_	-	_	-	-	-	196	_	861	199	-	_	_	1
Mg Hardness	$mg/L^{\rm (a)}$	-	-	_	-	Ι	Ι	Ι	1	125	-	127	129	ı	1	-	1
As (total)	µg/L	49.4	-	21.7	1.0	55.9	Ι	25.9	1.5	8.99	-	$31.7^{(d)}$	1.4	70.5	1	38.2	1.5
As (soluble)	µg/L	-	-	_	-	1	1	_	_	66.7	_	$25.9^{(d)}$	1.2	-	_	_	1
As (particulate)	$\mu g/L$	ı	ı	-	ı	I	ı	ı	ı	11.5	-	5.8	0.2	ı	ı	ı	1
As (III)	$\mu g/L$	ı	I	-	I	I	ı	ı	ı	1.2	ı	1.0	1.0	ı	ı	ı	1
As (V)	µg/L	_	_	_	-	-	-	-	-	57.0	_	24.8	0.2	1	_	_	_
Fe (total)	µg/L	<25	_	<25	<25	<25	_	<25	<25	<25	_	<25	<25	<25	_	<25	<25
Fe (soluble)	µg/L	-	_	_	-	-	-	-	_	<25	_	<25	<25	-	_	_	1
Mn (total)	µg/L	<0.1	I	<0.1	<0.1	<0.1	ı	<0.1	<0.1	<0.1	ı	<0.1	<0.1	<0.1	ı	<0.1	<0.1
Mn (soluble)	µg/L	ı	ı	1	ı	I	ı	ı	I	<0.1	ı	<0.1	<0.1	ı	ı	ı	1
(a) As CaCO <sub>3</sub> . (b) Daily readings not recorded this week. (c) Onsite water quality parameter not measured. (d) Reanalysis indicated similar result.	ly readings	s not record	ed this we	ek. (c) Ons	ite water qu	ality param	eter not me	asured. (d)	Reanalysis	indicated s	similar resu	ılt.					

(a) As CaCO<sub>3</sub>. (b) Daily readings not recorded this week. (c) Onsite water quality parameter not measured. (d) Reanalysis indicated similar result. IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B; NA = data not available.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			12/(	12/07/05			01/04/06	4/06			02/01/06	1/06			90/80/20	90/	
Sampling Location Parameter	on Unit	N	AC	TA	TB	N	AC	TA	TB	IN	AC	TA	TB	N	AC	TA	TB
Bed Volume	$10^{3}$	_	_	74.7	36.8	_	-	78.6	38.7	-	-	82.5	40.6	-	-	87.3	43.0
Alkalinity	${\rm mg/L}^{\rm (a)}$	383	_	383	378	968	1	396	396	390	I	382	386	277	ı	381	381
Fluoride	mg/L	0.2	-	0.2	0.2	ı	ı	ı	ı	0.2	ı	0.2	0.2	0.2	1	0.2	0.2
Sulfate	mg/L	10	_	10	10	-	-	-	-	10	Ι	10	10	10	-	10	10
Nitrate (as N)	mg/L	0.2	_	0.2	0.2	_	ı	ı	ı	0.2	ı	0.2	0.2	0.2	1	0.2	0.2
Phosphorus (as P)	mg/L	<10	_	<10	<10	12.7	1	15.1	<10	<10	I	<10	<10	15.4	ı	17.0	<10
Silica (as SiO <sub>2</sub> )	mg/L	25.2	-	25.5	25.7	25.4	ı	25.2	25.2	26.3	1	26.4	26.2	24.7	1	23.9	24.3
Turbidity	NTU	0.1	_	<0.1	<0.1	0.2	ı	0.4	0.1	0.1	ı	<0.1	<0.1	6.3	ı	9.0	0.3
Hd	1	6.9	7.0	6.9	6.9	6.9	8.9	8.9	8.9	8.9	8.9	8.9	8.9	6.9	6.9	6.9	6.9
Temperature	သ	19.9	5.61	19.9	19.9	7.61	19.8	19.9	20.0	20.0	19.9	20.0	20.1	19.7	19.4	19.6	19.6
DO	mg/L	3.6	3.9	3.8	3.9	4.0	4.0	4.3	4.2	4.1	3.8	3.8	3.8	3.7	3.5	3.0	3.6
ORP	mV	205	265	611	633	232	630	649	663	475	634	663	683	481	644	671	684
Free Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.3	0.2	0.2	_	0.3	0.3	0.3	_	0.3	0.3	0.3	_	0.4	0.4	0.4
Total Chlorine (as Cl <sub>2</sub> )	mg/L	-	0.3	0.3	0.3	-	0.4	0.4	0.4	1	0.3	0.3	0.3	-	0.4	0.4	0.4
Total Hardness	$mg/L^{\rm (a)}$	325	_	337	341	-	Ι	1	Ι	330	1	339	353	341	-	342	346
Ca Hardness	$mg/L^{\rm (a)}$	199	_	207	205	-	-	-	Ι	202	-	206	208	206	-	207	208
Mg Hardness	$mg/L^{\scriptscriptstyle (a)}$	125	_	130	136	-	1	1	-	128	ı	134	144	135	-	135	138
As (total)	µg/L	61.2	-	35.8	3.4	53.8	ı	33.6	2.7	$69.4^{(b)}$	ı	$43.2^{(b)}$	3.9	76.7	ı	50.7	5.6
As (soluble)	µg/L	61.6	-	34.6	3.1	ı	ı	ı	ı	54.3 <sup>(b)</sup>	ı	$33.9^{(b)}$	3.3	55.0	ı	35.5	4.4
As (particulate)	µg/L	<0.1	_	1.3	0.3	ı	1	ı	ı	15.1	1	9.3	9.0	21.7	-	15.2	1.1
As (III)	µg/L	0.7	_	0.7	0.7	-	Ι	ı	ı	0.7	1	0.5	0.6	0.7	-	0.6	0.6
As (V)	µg/L	6.09	-	33.8	2.4	ı	1	ı	ı	53.7	1	33.4	2.7	54.3	-	34.8	3.9
Fe (total)	µg/L	<25	_	<25	<25	<25	1	<25	<25	<25	1	<25	<25	<25	ı	<25	<25
Fe (soluble)	µg/L	<25	_	<25	<25	ı	1	ı	ı	<25	1	<25	<25	<25	-	<25	<25
Mn (total)	µg/L	0.2	ı	0.2	0.2	<0.1	ı	<0.1	<0.1	<0.1	1	<0.1	<0.1	0.1	ı	0.1	<0.1
Mn (soluble)	µg/L	0.2	I	0.1	0.1	ı	ı	I	ı	<0.1	ı	<0.1	<0.1	<0.1	ı	<0.1	<0.1
Page (4) CoCO: (b) Begin	nolveic inc	(h) Deservice indicated (h)	lar recult								1						

(a) As  $CaCO_3$ . (b) Reanalysis indicated similar result. IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			04/(	04/05/06			04/19/06	90/6			02/03/06	3/06			05/17/06	90/2	
Sampling Location Parameter U	on Unit	ZI	AC	TA	TB	Z	AC	TA	TB	Z	AC	TA	TB	Z	AC	TA	TB
Bed Volume	$10^{3}$	_	_	91.1	44.9	-	-	93.0	45.8	-	-	94.8	NA	-	-	2.96	47.6
Alkalinity	${ m mg/L}^{(a)}$	372	_	376	376	406	_	401	388	374	-	386	382	380 384	_	388 380	384 355
Fluoride	mg/L	ı	ı		ı	ı	ı	1	ı	0.3	ı	0.2	0.3	I	ı	I	ı
Sulfate	mg/L	ı	ı	-	ı	I	1	-	ı	6	-	6	6	I	-	I	ı
Nitrate (as N)	mg/L	ı	ı	1	ı	I	ı	1	ı	0.2	ı	0.2	0.2	I	-	I	ı
Phosphorus (as P)	ng/L	<10	_	10.7	<10	20.4	_	21.4	10.4	<10	_	13.4	<10	<10 <10	_	<10 <10	<10 <10
Silica (as SiO <sub>2</sub> )	mg/L	25.3	I	24.4	25.0	24.7	_	24.3	24.4	26.0	_	25.6	25.9	26.8 26.3	_	26.7 26.2	25.7 26.4
Turbidity	UTU	0.3	ı	0.5	9.0	0.3	ı	0.4	0.2	0.3	ı	0.2	0.2	0.3	ı	0.2	0.4
Hd	ı	6.9	6.9	6.9	6.9	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	$NA^{(b)}$	7.0	7.0	6.9	6.9	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	$NA^{(b)}$
Temperature	J <sub>o</sub>	19.3	19.5	19.6	19.6	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	$NA^{(b)}$	20.5	20.4	20.9	20.7	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	NA <sup>(b)</sup>
DO	mg/L	3.7	3.7	3.8	3.5	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	3.7	3.9	3.8	3.8	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	NA <sup>(b)</sup>
ORP	MV	211	616	649	659	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	217	646	999	685	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	NA <sup>(b)</sup>
Free Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.4	0.4	0.4	_	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	_	0.4	0.4	0.4	_	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$
Total Chlorine (as Cl <sub>2</sub> )	mg/L	_	0.4	0.4	0.4	Ι	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	-	0.4	0.4	0.4	_	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$
Total Hardness	${\sf mg/L}^{\rm (a)}$	_	-	1	I	I	-	ı	ı	342	_	332	341	_	_	1	ı
Ca Hardness	$mg/L^{\rm (a)}$	_	_	_	-	_	_	_	_	204	_	198	202	_	_	_	-
Mg Hardness	${\rm mg/L}^{\rm (a)}$	_	-	1	-	Ι	-	ı	ı	138	-	135	138	_	_	Ι	ı
As (total)	hg/L	63.8	_	45.5	6.0	63.7	_	42.2	5.6	66.2	-	48.7	6.5	53.8 54.3	_	38.8 39.2	6.3
As (soluble)	η/gπ	_	_	_	-	-	_	-	-	59.1	_	41.9	6.1	_	_	_	_
As (particulate)	µg/L	1	-	_	ı	ı	-	ı	I	7.1	-	6.7	0.4	ı	_	1	_
As (III)	µg/L	ı	ı	_	ı	ı	-	ı	I	0.3	_	0.3	0.3	I	_	ı	_
As (V)	η/gπ	_	-	1	I	I	-	ı	ı	28.7	_	41.7	5.8	_	_	1	ı
Fe (total)	hg/L	<25	_	<25	<25	<25	_	<25	<25	<25	_	<25	<25	<25 <25	_	<25 <25	<25 <25
Fe (soluble)	µg/L	-	-	_	-	ı	-	ı	I	<25	-	<25	<25	ı	_	1	_
Mn (total)	µg/L	<0.1	I	<0.1	<0.1	0.2	ı	0.1	0.1	<0.1	1	<0.1	<0.1	0.1	1	<0.1	<0.1
Mn (soluble)	hg/L	-	-		ı	_	-	-	1	<0.1	_	<0.1	<0.1	-	_	-	-
(a) As CaCO <sub>3</sub> . (b) Onsite water quality parameter not measured.	site water q	uality para	meter not 1	neasured.													

(a) As CaCO<sub>3</sub>. (b) Onsite water quanty parameter not measured. IN = at inlet; AC = after tank B; NA = ata not available. IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B; NA = ata not available.

## Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date			06/1	06/14/06			07/12	07/12/06 <sup>(c)</sup>			60/80	(p)90/60/80	
Sampling Location Parameter U	on Unit	NI	AC	TA	TB	IN	AC	TA	TB	NI	AC	TA	TB
Bed Volume	$10^{3}$	_	-	100.4	49.4	_	_	103.3	50.9	_	-	105.8	52.2
Alkalinity	${ m mg/L}^{(a)}$	378	ı	386	386	377	ı	390	373	378	ı	386	382
Fluoride	mg/L	-	-	_	-	0.2	-	0.2	0.2	_	-	_	-
Sulfate	mg/L	1	ı	_	1	10	1	10	10	_	ı	_	ı
Nitrate (as N)	mg/L	ı	I	I	I	0.2	ı	0.2	0.2	-	ı	I	ı
Phosphorus (as P)	µg/L	18.0	ı	20.0	10.9	13.4	I	14.3	<10	<10	ı	<10	<10
Silica (as SiO <sub>2</sub> )	mg/L	27.0	I	26.8	26.5	25.4	I	24.8	25.5	25.0	ı	24.0	24.2
Turbidity	NTU	0.5	ı	0.5	0.2	0.3	ı	0.4	0.1	0.2	ı	0.4	0.4
Hď	ı	6.9	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
Temperature	သ	21.2	20.6	21.7	22.4	21.5	20.7	21.1	21.1	21.2	20.8	21.2	21.7
DO	mg/L	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	NA <sup>(b)</sup>	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	$NA^{(b)}$	NA <sup>(b)</sup>
ORP	mV	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	$NA^{(b)}$	NA <sup>(b)</sup>	$NA^{(b)}$	$NA^{(b)}$
Free Chlorine (as Cl <sub>2</sub> )	mg/L	ı	0.5	0.5	0.5	1	0.3	0.3	0.3	I	0.4	0.4	0.4
Total Chlorine (as Cl <sub>2</sub> )	mg/L	1	0.5	0.5	0.5	ı	0.3	0.3	0.3	-	0.4	0.4	0.4
Total Hardness	$mg/L^{(a)}$	ı	_	_	1	304	ı	314	303	-	ı	_	ı
Ca Hardness	${\rm mg/L}^{\rm (a)}$	ı	-	-	1	185	ı	192	185	-	ı	1	ı
Mg Hardness	${ m mg/L}^{(a)}$	-	-	-	1	119	Ι	122	118	-	1	1	ı
As (total)	µg/L	76.7	1	56.1	9.2	63.9	ı	48.3	8.2	77.5	-	53.7	8.6
As (soluble)	µg/L	ı	-	ı	ı	54.4	ı	40.1	7.3	ı	ı	ı	I
As (particulate)	µg/L	ı	-	1	I	9.5	ı	8.2	6.0	ı	1	1	ı
As (III)	µg/L	ı	_	-	Ι	0.4	-	0.4	0.4	-	_	-	ı
As (V)	µg/L	ı	-	-	Ι	54.0	ı	39.8	7.0	-	1	1	ı
Fe (total)	µg/L	<25	ı	<25	<25	<25	ı	<25	<25	<25	ı	<25	<25
Fe (soluble)	µg/L	ı	ı	I	I	<25	ı	<25	<25	ı	ı	ı	ı
Mn (total)	µg/L	0.1	ı	<0.1	<0.1	0.7	ı	0.6	9.0	<0.1	ı	<0.1	0.1
Mn (soluble)	µg/L	ı	ı	ı	I	0.2	ı	0.1	0.2	ı	ı	I	ı
(a) As CaCO. (b) Oneite water quality parameter not measured (c) Due to low	e water ana	lity naramet	er not me	senred (c)	Die to low	Wafer level	arra ll ava	s well name throttled from 31	from 31 to	275 gnm since 06/16/06	100 OF/16/	,UK	F

<sup>(</sup>a) As CaCO<sub>3</sub>. (b) Onsite water quality parameter not measured. (c) Due to low water levels, well pump throttled from 31 to <25 gpm since 06/16/06. (d) TA and TB sample bottles likely switched and corrected for this event. IN = at inlet; AC = after prechlorination (field parameters only); TA = after tank A; TB = after tank B; NA = data not available.

Analytical Results from Long-Term Sampling, Rimrock, AZ (Continued)

Sampling Date	d)		11/28/06 <sup>(a)</sup>			01/03/07			02/01/07			03/01/07	
Sampling Location Parameter U	ion Unit	NI	TA	TB	IN	TA	TB	N	TA	TB	NI	TA	TB
Bed Volume	$10^{3}$	-	0.1	0.1	_	4.7	8.7	_	7.6	18.0	_	12.8	23.8
As (total)	µg/L	64.5	0.7	6.2	75.0	0.7	24.3	69.3	0.7	31.7	58.4	1.0	26.0

(a) System offline and well pump pulled for cleaning on 08/30/06. System operation resumed on 11/27/06 after Tank A media replaced and tank positions switched. Partially exhausted Tank B continues operation in lead position.

IN = at inlet; TA = after tank A; TB = after tank B.