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**Technical Paper "Microfine Coal Firing Results  
from a Retrofit Gas/Oil-Designed Industrial Boiler"**

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# MICROFINE COAL FIRING RESULTS FROM A RETROFIT

## GAS/OIL-DESIGNED INDUSTRIAL BOILER

Ramesh Patel, Richard W. Borio, Greg Liljedahl  
ABB Power Plant Laboratories  
Combustion Engineering, Inc., Windsor CT 06095

Bruce G. Miller, Alan W. Scaroni  
Energy and Fuels Research Center  
The Pennsylvania State University, University Park PA 16802

Jon G. McGowan  
University of Massachusetts, Amherst MA 01002

### INTRODUCTION/ BACKGROUND

Under U.S. Department of Energy, Pittsburgh Energy Technology Center (PETC) support, the development of a High Efficiency Advanced Coal Combustor (HEACC) has been in progress since 1987 at the ABB Power Plant Laboratories (Rini, et al., 1987, 1988). The initial work on this concept produced an advanced coal firing system that was capable of firing both water-based and dry pulverized coal in an industrial boiler environment (Rini, et al., 1990).

Economics may one day dictate that it makes sense to replace oil or natural gas with coal in boilers that were originally designed to burn these fuels. In recognition of this future possibility, the U.S. Department of Energy, Pittsburgh Energy Technology Center (PETC) has continued to support this program led by ABB Power Plant Laboratories and the Fuels Research Center of Penn State University to develop the HEACC concept. The objective of the current program is to demonstrate the technical and economic feasibility of retrofitting a gas/oil designed boiler to burn micronized coal. In support of this overall objective, the following specific areas were targeted:

- A coal handling/preparation system that can meet the technical requirements for retrofitting microfine coal on a boiler designed for burning oil or natural gas.
- Maintaining boiler thermal performance in accordance with specifications when burning oil or natural gas.
- Maintaining NO<sub>x</sub> emissions at or below 0.6 lb/MBtu (~450 ppm)
- Achieving combustion efficiencies of 98% or higher
- Calculating economic payback periods as a function of key variables

The overall program has consisted of five major tasks:

- 1.0 A review of current state-of-the-art coal firing system components.
- 2.0 Design and experimental testing of a prototype HEACC burner.
- 3.0 Installation and testing of a HEACC system in a commercial retrofit application.
- 4.0 Economic evaluation of the HEACC concept for retrofit applications.
- 5.0 Long term demonstration under commercial user demand conditions

This paper will summarize the latest key experimental results (Task 3) and the economic evaluation (Task 4) of the HEACC concept for retrofit applications.

## BURNER INSTALLATION AND TESTING IN AN INDUSTRIAL BOILER

The overall objective of this program has been to assess the technical and economic viability of displacing premium fuels with micro-fine coal by retrofitting the previously developed High Efficiency Advanced Coal Combustor (HEACC) to a gas/oil designed industrial boiler. This paper summarizes the work involving the retrofit of a complete micro-fine pulverized coal milling and firing system to an existing 15,000 lb/hr package boiler located in the East Steam Plant of Penn State University. Combustion performance-related objectives included steady state operation on 100% coal while achieving a carbon conversion efficiency of 98%, without increasing NO<sub>x</sub> emissions above 0.6 lb/MBtu (~450 ppm). The testing was also designed to show that consistent, reliable operation of entire coal storage/handling and pulverization system could be achieved. Reliable operation of the coal preparation system in concert with satisfactory burner performance would serve as a prerequisite to the demonstration phase of the project.

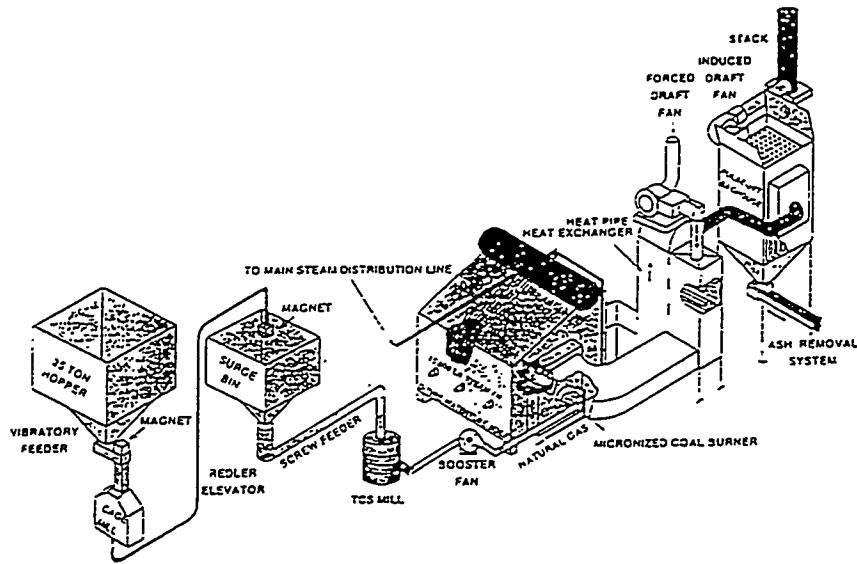
The HEACC burner was previously tested (Task 2) in the Industrial Scale Burner Facility (ISBF) located at Combustion Engineering's ABB Power Plant Laboratories (PPL) in Windsor, Connecticut. A key objective of the 100 hour burner validation tests at PPL was to fine-tune the burner operating characteristics and demonstrate operation over the range of conditions expected for the field boiler tests. All performance goals were successfully achieved during these ISBF tests. The testing at PPL demonstrated the technical validity of the design improvements incorporated into the second generation HEACC. This burner was then installed as part of a complete coal handling and firing system in Penn State's commercial boiler for a 400 hour proof-of-concept test program (Task 3).

A schematic of the micronized coal preparation/firing system at Penn State is shown in Figure 1. As can be seen, the cleaned coal comes on site and is stored in a large hopper. The coal is crushed and sent via a screw feeder to a micronized coal mill (TCS system). The coal is then micronized to ~80% through 325 mesh (~18 microns MMD) in the TCS mill and pneumatically conveyed to the HEACC burner where it is then burned in the boiler. This boiler is an oil/gas designed Tampella Keeler Model DS-15; a package D-type watertube boiler capable of producing 15,000 lb/hr of saturated steam at 300 psig. It represents a typical gas/oil - designed system with a furnace volumetric heat release of 50,000 Btu/hr ft<sup>3</sup>, standard for this class of boiler. Furthermore, its design is similar to that of many other manufacturers' (including Combustion Engineering) models.

## EXPERIMENTAL TESTING RESULTS

### A) OVERVIEW

During the long term test period, the boiler system was operated over a range of operating conditions. Specifically, the boiler was tested over a variety of load ranges, excess air, combustion air damper settings and burner swirl levels. Two coals Brookville Seam and Kentucky were used. Their analyses are summarized in Table 1. During the test period, boiler performance data, emissions data, electric parasitic power and house compressed air consumption data, as well as other data required for the technical and economical analysis of the system were obtained.



**Figure 1** Micronized Coal Combustion System at Penn State

The initial burner tests included a shakedown series of runs using natural gas firing (Jennings, et al., 1994a, 1994b). At the conclusion of baseline natural gas firing, the boiler operation was directed towards hardware optimization (e.g., coal handling/preparation, burner settings) and testing with 100% coal firing. During this phase of the work, a major objective was to obtain consistent, repeatable 100% coal fired runs. This goal, along with minor modifications to the system (discussed in the next section) to increase boiler and carbon conversion efficiency resulted in several short term tests. Subsequently, the chosen hardware configuration was then used during the long term (~400 hr) test program (Task 3).

**Table 1** Selected Analyses of the Brookville and Kentucky Coals

	<u>Brookville Seam</u>	<u>Kentucky</u>
Proximate, wt%		
Moisture	8.2	6.8
Volatile Matter	33.1	33.3
Fixed Carbon	55.8	55.4
Ash	2.9	4.5
HHV, Btu/lb	13,260	13,010
Ash Fusion Temp, °F		
IDT	2,820	2,803
ST	+3,000	+3,000
FT	+3,000	+3,000

#### B) SYSTEM CHARACTERIZATION/MODIFICATIONS

A key objective of the proof of concept testing was to determine the operating characteristics of the complete, integrated system in contrast to the operation of the individual components. Although all of the system components installed at the demonstration boiler host site were proven in either commercial operation or prior testing, the complete system from micro-fine coal production to steam production at this scale had not been previously demonstrated/proven.

The testing at Penn State indicated areas that should be carefully engineered in a commercial design. Furthermore, it was anticipated that if any problems occurred, they would likely be related to the burner (the least developed system component). However, the coal handling/feeding sub-system as it related to boiler system operability proved to be a critical component during initial testing. Some of the key system modifications and operational problems relating to the Penn State boiler are discussed below.

#### TCS Mill

The TCS mill and booster fan operated well without constant supervision. Initial system testing, however, revealed a coal settling problem in the mill outlet duct. This problem was corrected by a specially designed diffuser/transition section fitted to the mill exit. In addition, a detailed experimental study was carried out to characterize the effect of mill air flow rate and mill speed, on coal particle size distribution (PSD) and top size for the two coals tested. This was done as part of an effort to determine the milling conditions necessary to reduce the coal PSD and top size in order to achieve maximum coal combustion efficiency. In addition, the results were used to evaluate the feasibility for external classification to reduce the coal top size. The mill speed was a most important parameter to obtain the desired coal PSD. The results from these tests were used to optimize the mill settings for coal fineness during the experimental test program. Table 2 presents typical optimized mill operating conditions.

**Table 2 Mill Performance Summary**

- Typical mill air flow rate: 370-400 acfm
- Typical coal feed rate: 16.5- 18.5 lb/min

<u>Particle Size (microns)</u>	<u>Brookville Seam Coal</u>	<u>Kentucky Coal</u>
Top Size	190-300	250-275
D <sub>80</sub>	50-70	50-70
D <sub>50</sub>	25-30	25-30

#### Furnace Modifications

The furnace geometry was slightly altered during the test program by installing a ceramic wall at the exit of the radiant section of the boiler. The basic idea was to improve carbon burnout by making better use of the entire boiler volume through changing the gas patterns and temperature profile in the boiler. This was done because analytical (CFD) modeling showed that the flame was skewed from the burner to the furnace outlet and that the entire furnace volume was not being effectively used (Model results were subsequently verified by suction pyrometry).

#### Boiler System Operability

During the initial testing period, a number of operational problems involving the coal handling and boiler system were encountered. They were primarily related to the weather (cold, snow), the coal (particle size, moisture content), the burner/boiler system (unstable/ low u.v. flame scanner signal), or mechanical difficulties (feedwater pump, steam valves). With the exception of the coal handling problems caused by high moisture, these problems were all addressed and solved during the shakedown test series. The coal moisture problems will be fully addressed prior to beginning the 1000 hour demonstration test (Task 5).

### C) SUMMARY OF EXPERIMENTAL RESULTS

Under the 400 hour test program, Brookville Seam and Kentucky coals were evaluated, the furnace geometry was modified by installing a ceramic wall, two coal guns (the RO-II with and without a coal deflector/accelerator and the I-Jet) were tested, and the operating conditions

and without a coal deflector/accelerator and the I-Jet) were tested, and the operating conditions (excess air and firing rate) were varied. During the course of the long term coal only tests, no support fuel was required and the burner operated with excellent ignition stability. A typical summary of the microfine coal firing (both coals) is given in Table 3.

**Table 3 Microfine Coal Firing Results**

Boiler Operation:

Steam Flow Rate (lb/hr)	13,240
Boiler Efficiency (%)	84.1 (3% O <sub>2</sub> )

Combustion Performance

Carbon Conversion Efficiency (%)	95.3
NOx at 3% O <sub>2</sub> (ppm)	413 (0.56 lb/MBtu)
Burner Pressure Drop (in H <sub>2</sub> O)	8

During this test program, key performance variables were monitored in detail: boiler efficiency, combustion efficiency, and NOx emissions. A summary of the results involving these parameters follows.

Boiler Thermal Performance

Boiler thermal performance when firing micro-fine coal was essentially comparable to that achieved when firing natural gas. In fact, because of the greater latent heat loss when burning natural gas (greater formation of water due to higher hydrogen content), firing micro-fine coal actually gave slightly higher boiler efficiencies despite the need to run at higher excess air levels.

During the relatively short operating periods, usually less than 16 hours, ash deposits did not cause significant changes to the boiler thermal performance. It is recognized, however, that longer term operation could result in greater build-up of ash deposits which could impact heat transfer. Because of the relatively short duration of the tests, any build-up of ash deposits would slough off when the boiler was shut down. A better test of the possible impact of ash deposits will occur during the long term demonstration phase of the work (Task 5.0).

NOx Emissions

The NOx emissions target was 0.6 lb NOx per million Btu fired; this translates to about 450 ppm at 3% O<sub>2</sub>. Testing with 100% microfine coal showed that this target was achieved (in general a NOx emissions value of 0.56 lb NOx per million Btu was routinely met) while meeting nearly all other required conditions. It is acknowledged that the optimum conditions for low NOx will generally exacerbate carbon conversion efficiencies. Indeed, this was the case with the HEACC burner and the challenge was to find a reasonable balance between meeting the NOx target while not aggravating the carbon conversion efficiency.

Combustion Efficiency

The target for combustion efficiency was 98%. The highest combustion efficiency obtained during the test program was slightly over 96%. However, this value was not compatible with meeting the NOx target, and was not able to be routinely repeated. A value of 95% combustion efficiency was able to be routinely achieved, and was compatible with meeting the NOx target.

Considerable effort was spent in trying to determine how combustion efficiency might be improved to meet the target. The challenge to meet the combustion efficiency target of 98% is, indeed a very difficult one. The bulk boiler residence time is about 0.7 seconds. Further complicating the task is the aspect ratio of the boiler, i.e. the length of the boiler is not very much greater than its height or width (approximately 8 ft long x 8 ft high x 6 ft wide). It is

aggravates the situation. Burner modifications are being looked at which might increase the particle residence time.

Coal particle size distribution was also evaluated, the premise being that carbon content must be directly proportional to particle size. While the larger particle size fraction of the collected particulate (fly ash) did contain higher carbon contents than the smaller size fractions, the differences were not as great as expected. For example, it would not be possible to dramatically reduce the carbon content of fly ash by eliminating coal particles larger than 150 microns.

## SYSTEM ECONOMICS

This phase of the work involved an economic evaluation of coal firing for existing small industrial boiler installations. In addition to a base case evaluation (the 15,000 lbm/hr natural gas fired Penn State boiler), various economic sensitivity studies which provide insight into the economics for other unit sizes, fuel price scenarios, capacity factors and other variables were carried out. The primary objective of this analysis was to determine how the coal option compares with natural gas firing on an annual basis. With coal firing the capital costs for the retrofit modifications as well as some additional operating and maintenance costs must be justified by the savings in fuel costs. The evaluation summarized here defines the incremental costs and savings on an annual basis as a result of the use of coal as a substitute for natural gas firing. The first year incremental operation and maintenance cost savings and the total retrofit capital requirement were then used to determine a simplified payback period. The details of the data and results have been summarized in a recent publication (Patel, et al., 1995).

### **KEY RESULTS FROM THE ECONOMIC EVALUATION**

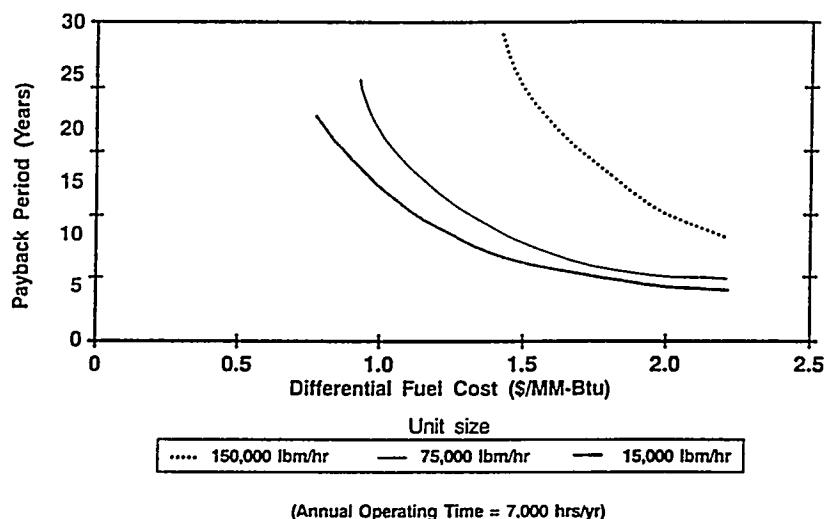
A series of economic comparisons were carried out for the base case and other systems involving different economic input parameters. For these studies a range of differential fuel costs were used, and other sensitivity studies were carried out to determine the effect of unit size, annual operating time, and carbon heat loss on simplified pay back time. Figures 3 to 5 show the results of these sensitivity studies. In addition to differential fuel costs (see Fig. 3), other sensitivity variables studied were shown to have significant effects on payback period. As shown in Fig. 4, increasing unit size is shown to quickly improve the economics. Also, as shown in Fig. 5, changes in the annual operating time from 4000 to 8000 hrs/yr showed significant effects on payback period. Typically industrial boilers have very high capacity factors (the base case for this study used 7000 Hrs/yr (equivalent to an 80 percent capacity factor)). Fig. 8 is of most interest as it shows that variations in carbon heat loss (combustion efficiency) have no significant effect on payback period for the range studied (2 to 6%).

Although this analysis was done relative to natural gas as the base fuel, the results can also be generally applied to oil firing as well. By knowing the differential fuel cost the payback period can be approximated from the attached curves. Although boiler efficiency with oil firing is typically about 5 percent better than with natural gas, the effect on payback period is relatively insignificant as was shown by the results of the carbon heat loss sensitivity study.

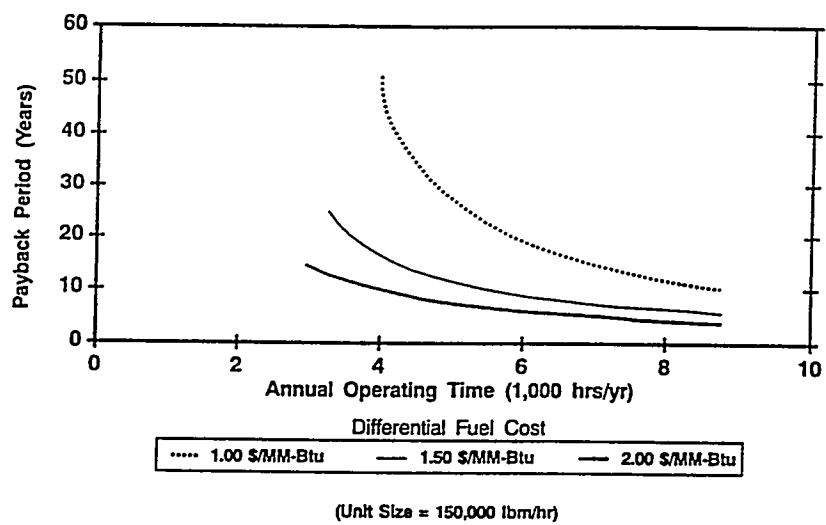
## CONCLUSIONS/ RECOMMENDATIONS

The following specific conclusions are based on the results of the coal fired testing at Penn State and the initial economic evaluation of the HEACC system:

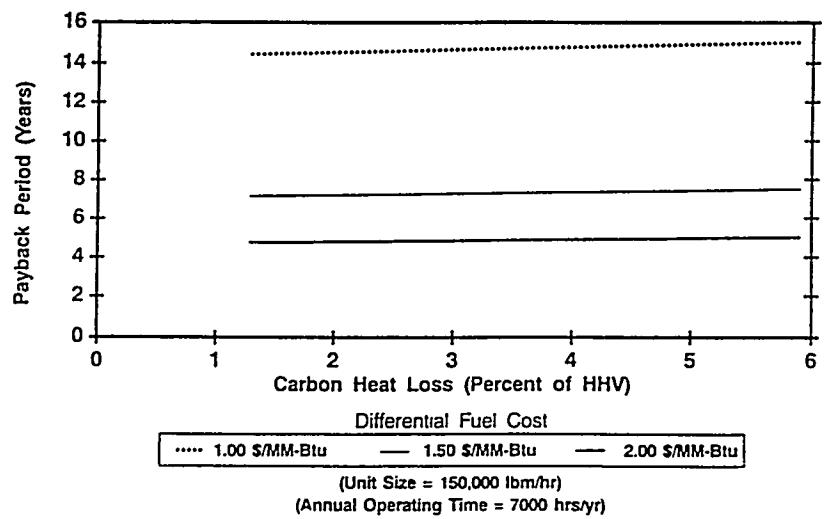
- A coal handling/ preparation system can be designed to meet technical requirements for retrofitting micro-fine pulverized coal.



**Figure 3** Payback Period as a function of Differential Fuel Cost and Unit Size



**Figure 4** Payback Period as a function of Annual Operating Time



**Figure 5** Payback Period as a function of Carbon Heat Loss

- The boiler thermal performance met requirements
- Combustion efficiencies of 95% could be met on a daily average basis, somewhat below the target of 98%
- NOx emissions can meet the target of 0.6 lb/million Btu
- The economic payback was very sensitive to fuel differential cost, unit size, and annual operating hours

As a result of recent long term tests using micronized coal (in another program), Penn State has experienced some convective pass ash deposition problems. To alleviate this problem they are planning to install additional soot blowers. Also, as a result of problems encountered during the 400 hour testing, the following modifications are planned for the Penn State system:

#### Coal feeding improvements

- a) Improved raw coal/ storage and transport
- b) Redesign/installation of a surge bin bottom
- c) Installation of a gravimetric feeder

#### Monitoring of ash deposit effects

- a) Air sparge/soot blower systems
- b) Monitoring effects on heat transfer in the furnace and the convective pass
- c) The use of ash deposition probes

In addition, ABB CE plans to modify the burner for more precise aerodynamic control of the fuel and air streams to improve the combustion efficiency and NOx emissions. Based on the results summarized in this paper the ABB/Penn State team and DOE/PETC have decided to conduct a 1000 hr demonstration (Task 5) of this program; it is currently scheduled to begin in July 1995.

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Table 1. Burner Characterization Summary

Table 1. Burner Characterization Summary

Date	Type	O<sub>2</sub>	CO<sub>2</sub>	CO<sub>3</sub>	CO<sub>4</sub>	CO<sub>5</sub>	CO<sub>6</sub>	CO<sub>7</sub>	CO<sub>8</sub>	CO<sub>9</sub>	CO<sub>10</sub>	CO<sub>11</sub>	CO<sub>12</sub>	CO<sub>13</sub>	CO<sub>14</sub>	CO<sub>15</sub>	CO<sub>16</sub>	CO<sub>17</sub>	CO<sub>18</sub>	CO<sub>19</sub>	CO<sub>20</sub>	CO<sub>21</sub>	CO<sub>22</sub>	CO<sub>23</sub>	CO<sub>24</sub>	CO<sub>25</sub>	CO<sub>26</sub>	CO<sub>27</sub>	CO<sub>28</sub>	CO<sub>29</sub>	CO<sub>30</sub>	CO<sub>31</sub>	CO<sub>32</sub>	CO<sub>33</sub>	CO<sub>34</sub>	CO<sub>35</sub>	CO<sub>36</sub>	CO<sub>37</sub>	CO<sub>38</sub>	CO<sub>39</sub>	CO<sub>40</sub>	CO<sub>41</sub>	CO<sub>42</sub>	CO<sub>43</sub>	CO<sub>44</sub>	CO<sub>45</sub>	CO<sub>46</sub>	CO<sub>47</sub>	CO<sub>48</sub>	CO<sub>49</sub>	CO<sub>50</sub>	CO<sub>51</sub>	CO<sub>52</sub>	CO<sub>53</sub>	CO<sub>54</sub>	CO<sub>55</sub>	CO<sub>56</sub>	CO<sub>57</sub>	CO<sub>58</sub>	CO<sub>59</sub>	CO<sub>60</sub>	CO<sub>61</sub>	CO<sub>62</sub>	CO<sub>63</sub>	CO<sub>64</sub>	CO<sub>65</sub>	CO<sub>66</sub>	CO<sub>67</sub>	CO<sub>68</sub>	CO<sub>69</sub>	CO<sub>70</sub>	CO<sub>71</sub>	CO<sub>72</sub>	CO<sub>73</sub>	CO<sub>74</sub>	CO<sub>75</sub>	CO<sub>76</sub>	CO<sub>77</sub>	CO<sub>78</sub>	CO<sub>79</sub>	CO<sub>80</sub>	CO<sub>81</sub>	CO<sub>82</sub>	CO<sub>83</sub>	CO<sub>84</sub>	CO<sub>85</sub>	CO<sub>86</sub>	CO<sub>87</sub>	CO<sub>88</sub>	CO<sub>89</sub>	CO<sub>90</sub>	CO<sub>91</sub>	CO<sub>92</sub>	CO<sub>93</sub>	CO<sub>94</sub>	CO<sub>95</sub>	CO<sub>96</sub>	CO<sub>97</sub>	CO<sub>98</sub>	CO<sub>99</sub>	CO<sub>100</sub>	CO<sub>101</sub>	CO<sub>102</sub>	CO<sub>103</sub>	CO<sub>104</sub>	CO<sub>105</sub>	CO<sub>106</sub>	CO<sub>107</sub>	CO<sub>108</sub>	CO<sub>109</sub>	CO<sub>110</sub>	CO<sub>111</sub>	CO<sub>112</sub>	CO<sub>113</sub>	CO<sub>114</sub>	CO<sub>115</sub>	CO<sub>116</sub>	CO<sub>117</sub>	CO<sub>118</sub>	CO<sub>119</sub>	CO<sub>120</sub>	CO<sub>121</sub>	CO<sub>122</sub>	CO<sub>123</sub>	CO<sub>124</sub>	CO<sub>125</sub>	CO<sub>126</sub>	CO<sub>127</sub>	CO<sub>128</sub>	CO<sub>129</sub>	CO<sub>130</sub>	CO<sub>131</sub>	CO<sub>132</sub>	CO<sub>133</sub>	CO<sub>134</sub>	CO<sub>135</sub>	CO<sub>136</sub>	CO<sub>137</sub>	CO<sub>138</sub>	CO<sub>139</sub>	CO<sub>140</sub>	CO<sub>141</sub>	CO<sub>142</sub>	CO<sub>143</sub>	CO<sub>144</sub>	CO<sub>145</sub>	CO<sub>146</sub>	CO<sub>147</sub>	CO<sub>148</sub>	CO<sub>149</sub>	CO<sub>150</sub>	CO<sub>151</sub>	CO<sub>152</sub>	CO<sub>153</sub>	CO<sub>154</sub>	CO<sub>155</sub>	CO<sub>156</sub>	CO<sub>157</sub>	CO<sub>158</sub>	CO<sub>159</sub>	CO<sub>160</sub>	CO<sub>161</sub>	CO<sub>162</sub>	CO<sub>163</sub>	CO<sub>164</sub>	CO<sub>165</sub>	CO<sub>166</sub>	CO<sub>167</sub>	CO<sub>168</sub>	CO<sub>169</sub>	CO<sub>170</sub>	CO<sub>171</sub>	CO<sub>172</sub>	CO<sub>173</sub>	CO<sub>174</sub>	CO<sub>175</sub>	CO<sub>176</sub>	CO<sub>177</sub>	CO<sub>178</sub>	CO<sub>179</sub>	CO<sub>180</sub>	CO<sub>181</sub>	CO<sub>182</sub>	CO<sub>183</sub>	CO<sub>184</sub>	CO<sub>185</sub>	CO<sub>186</sub>	CO<sub>187</sub>	CO<sub>188</sub>	CO<sub>189</sub>	CO<sub>190</sub>	CO<sub>191</sub>	CO<sub>192</sub>	CO<sub>193</sub>	CO<sub>194</sub>	CO<sub>195</sub>	CO<sub>196</sub>	CO<sub>197</sub>	CO<sub>198</sub>	CO<sub>199</sub>	CO<sub>200</sub>	CO<sub>201</sub>	CO<sub>202</sub>	CO<sub>203</sub>	CO<sub>204</sub>	CO<sub>205</sub>	CO<sub>206</sub>	CO<sub>207</sub>	CO<sub>208</sub>	CO<sub>209</sub>	CO<sub>210</sub>	CO<sub>211</sub>	CO<sub>212</sub>	CO<sub>213</sub>	CO<sub>214</sub>	CO<sub>215</sub>	CO<sub>216</sub>	CO<sub>217</sub>	CO<sub>218</sub>	CO<sub>219</sub>	CO<sub>220</sub>	CO<sub>221</sub>	CO<sub>222</sub>	CO<sub>223</sub>	CO<sub>224</sub>	CO<sub>225</sub>	CO<sub>226</sub>	CO<sub>227</sub>	CO<sub>228</sub>	CO<sub>229</sub>	CO<sub>230</sub>	CO<sub>231</sub>	CO<sub>232</sub>	CO<sub>233</sub>	CO<sub>234</sub>	CO<sub>235</sub>	CO<sub>236</sub>	CO<sub>237</sub>	CO<sub>238</sub>	CO<sub>239</sub>	CO<sub>240</sub>	CO<sub>241</sub>	CO<sub>242</sub>	CO<sub>243</sub>	CO<sub>244</sub>	CO<sub>245</sub>	CO<sub>246</sub>	CO<sub>247</sub>	CO<sub>248</sub>	CO<sub>249</sub>	CO<sub>250</sub>	CO<sub>251</sub>	CO<sub>252</sub>	CO<sub>253</sub>	CO<sub>254</sub>	CO<sub>255</sub>	CO<sub>256</sub>	CO<sub>257</sub>	CO<sub>258</sub>	CO<sub>259</sub>	CO<sub>260</sub>	CO<sub>261</sub>	CO<sub>262</sub>	CO<sub>263</sub>	CO<sub>264</sub>	CO<sub>265</sub>	CO<sub>266</sub>	CO<sub>267</sub>	CO<sub>268</sub>	CO<sub>269</sub>	CO<sub>270</sub>	CO<sub>271</sub>	CO<sub>272</sub>	CO<sub>273</sub>	CO<sub>274</sub>	CO<sub>275</sub>	CO<sub>276</sub>	CO<sub>277</sub>	CO<sub>278</sub>	CO<sub>279</sub>	CO<sub>280</sub>	CO<sub>281</sub>	CO<sub>282</sub>	CO<sub>283</sub>	CO<sub>284</sub>	CO<sub>285</sub>	CO<sub>286</sub>	CO<sub>287</sub>	CO<sub>288</sub>	CO<sub>289</sub>	CO<sub>290</sub>	CO<sub>291</sub>	CO<sub>292</sub>	CO<sub>293</sub>	CO<sub>294</sub>	CO<sub>295</sub>	CO<sub>296</sub>	CO<sub>297</sub>	CO<sub>298</sub>	CO<sub>299</sub>	CO<sub>300</sub>	CO<sub>301</sub>	CO<sub>302</sub>	CO<sub>303</sub>	CO<sub>304</sub>	CO<sub>305</sub>	CO<sub>306</sub>	CO<sub>307</sub>	CO<sub>308</sub>	CO<sub>309</sub>	CO<sub>310</sub>	CO<sub>311</sub>	CO<sub>312</sub>	CO<sub>313</sub>	CO<sub>314</sub>	CO<sub>315</sub>	CO<sub>316</sub>	CO<sub>317</sub>	CO<sub>318</sub>	CO<sub>319</sub>	CO<sub>320</sub>	CO<sub>321</sub>	CO<sub>322</sub>	CO<sub>323</sub>	CO<sub>324</sub>	CO<sub>325</sub>	CO<sub>326</sub>	CO<sub>327</sub>	CO<sub>328</sub>	CO<sub>329</sub>	CO<sub>330</sub>	CO<sub>331</sub>	CO<sub>332</sub>	CO<sub>333</sub>	CO<sub>334</sub>	CO<sub>335</sub>	CO<sub>336</sub>	CO<sub>337</sub>	CO<sub>338</sub>	CO<sub>339</sub>	CO<sub>340</sub>	CO<sub>341</sub>	CO<sub>342</sub>	CO<sub>343</sub>	CO<sub>344</sub>	CO<sub>345</sub>	CO<sub>346</sub>	CO<sub>347</sub>	CO<sub>348</sub>	CO<sub>349</sub>	CO<sub>350</sub>	CO<sub>351</sub>	CO<sub>352</sub>	CO<sub>353</sub>	CO<sub>354</sub>	CO<sub>355</sub>	CO<sub>356</sub>	CO<sub>357</sub>	CO<sub>358</sub>	CO<sub>359</sub>	CO<sub>360</sub>	CO<sub>361</sub>	CO<sub>362</sub>	CO<sub>363</sub>	CO<sub>364</sub>	CO<sub>365</sub>	CO<sub>366</sub>	CO<sub>367</sub>	CO<sub>368</sub>	CO<sub>369</sub>	CO<sub>370</sub>	CO<sub>371</sub>	CO<sub>372</sub>	CO<sub>373</sub>	CO<sub>374</sub>	CO<sub>375</sub>	CO<sub>376</sub>	CO<sub>377</sub>	CO<sub>378</sub>	CO<sub>379</sub>	CO<sub>380</sub>	CO<sub>381</sub>	CO<sub>382</sub>	CO<sub>383</sub>	CO<sub>384</sub>	CO<sub>385</sub>	CO<sub>386</sub>	CO<sub>387</sub>	CO<sub>388</sub>	CO<sub>389</sub>	CO<sub>390</sub>	CO<sub>391</sub>	CO<sub>392</sub>	CO<sub>393</sub>	CO<sub>394</sub>	CO<sub>395</sub>	CO<sub>396</sub>	CO<sub>397</sub>	CO<sub>398</sub>	CO<sub>399</sub>	CO<sub>400</sub>	CO<sub>401</sub>	CO<sub>402</sub>	CO<sub>403</sub>	CO<sub>404</sub>	CO<sub>405</sub>	CO<sub>406</sub>	CO<sub>407</sub>	CO<sub>408</sub>	CO<sub>409</sub>	CO<sub>410</sub>	CO<sub>411</sub>	CO<sub>412</sub>	CO<sub>413</sub>	CO<sub>414</sub>	CO<sub>415</sub>	CO<sub>416</sub>	CO<sub>417</sub>	CO<sub>418</sub>	CO<sub>419</sub>	CO<sub>420</sub>	CO<sub>421</sub>	CO<sub>422</sub>	CO<sub>423</sub>	CO<sub>424</sub>	CO<sub>425</sub>	CO<sub>426</sub>	CO<sub>427</sub>	CO<sub>428</sub>	CO<sub>429</sub>	CO<sub>430</sub>	CO<sub>431</sub>	CO<sub>432</sub>	CO<sub>433</sub>	CO<sub>434</sub>	CO<sub>435</sub>	CO<sub>436</sub>	CO<sub>437</sub>	CO<sub>438</sub>	CO<sub>439</sub>	CO<sub>440</sub>	CO<sub>441</sub>	CO<sub>442</sub>	CO<sub>443</sub>	CO<sub>444</sub>	CO<sub>445</sub>	CO<sub>446</sub>	CO<sub>447</sub>	CO<sub>448</sub>	CO<sub>449</sub>	CO<sub>450</sub>	CO<sub>451</sub>	CO<sub>452</sub>	CO<sub>453</sub>	CO<sub>454</sub>	CO<sub>455</sub>	CO<sub>456</sub>	CO<sub>457</sub>	CO<sub>458</sub>	CO<sub>459</sub>	CO<sub>460</sub>	CO<sub>461</sub>	CO<sub>462</sub>	CO<sub>463</sub>	CO<sub>464</sub>	CO<sub>465</sub>	CO<sub>466</sub>	CO<sub>467</sub>	CO<sub>468</sub>	CO<sub>469</sub>	CO<sub>470</sub>	CO<sub>471</sub>	CO<sub>472</sub>	CO<sub>473</sub>	CO<sub>474</sub>	CO<sub>475</sub>	CO<sub>476</sub>	CO<sub>477</sub>	CO<sub>478</sub>	CO<sub>479</sub>	CO<sub>480</sub>	CO<sub>481</sub>	CO<sub>482</sub>	CO<sub>483</sub>	CO<sub>484</sub>	CO<sub>485</sub>	CO<sub>486</sub>	CO<sub>487</sub>	CO<sub>488</sub>	CO<sub>489</sub>	CO<sub>490</sub>	CO<sub>491</sub>	CO<sub>492</sub>	CO<sub>493</sub>	CO<sub>494</sub>	CO<sub>495</sub>	CO<sub>496</sub>	CO<sub>497</sub>	CO<sub>498</sub>	CO<sub>499</sub>	CO<sub>500</sub>	CO<sub>501</sub>	CO<sub>502</sub>	CO<sub>503</sub>	CO<sub>504</sub>	CO<sub>505</sub>	CO<sub>506</sub>	CO<sub>507</sub>	CO<sub>508</sub>	CO<sub>509</sub>	CO<sub>510</sub>	CO<sub>511</sub>	CO<sub>512</sub>	CO<sub>513</sub>	CO<sub>514</sub>	CO<sub>515</sub>	CO<sub>516</sub>	CO<sub>517</sub>	CO<sub>518</sub>	CO<sub>519</sub>	CO<sub>520</sub>	CO<sub>521</sub>	CO<sub>522</sub>	CO<sub>523</sub>	CO<sub>524</sub>	CO<sub>525</sub>	CO<sub>526</sub>	CO<sub>527</sub>	CO<sub>528</sub>	CO<sub>529</sub>	CO<sub>530</sub>	CO<sub>531</sub>	CO<sub>532</sub>	CO<sub>533</sub>	CO<sub>534</sub>	CO<sub>535</sub>	CO<sub>536</sub>	CO<sub>537</sub>	CO<sub>538</sub>	CO<sub>539</sub>	CO<sub>540</sub>	CO<sub>541</sub>	CO<sub>542</sub>	CO<sub>543</sub>	CO<sub>544</sub>	CO<sub>545</sub>	CO<sub>546</sub>	CO<sub>547</sub>	CO<sub>548</sub>	CO<sub>549</sub>	CO<sub>550</sub>	CO<sub>551</sub>	CO<sub>552</sub>	CO<sub>553</sub>	CO<sub>554</sub>	CO<sub>555</sub>	CO<sub>556</sub>	CO<sub>557</sub>	CO<sub>558</sub>	CO<sub>559</sub>	CO<sub>560</sub>	CO<sub>561</sub>	CO<sub>562</sub>	CO<sub>563</sub>	CO<sub>564</sub>	CO<sub>565</sub>	CO<sub>566</sub>	CO<sub>567</sub>	CO<sub>568</sub>	CO<sub>569</sub>	CO<sub>570</sub>	CO<sub>571</sub>	CO<sub>572</sub>	CO<sub>573</sub>	CO<sub>574</sub>	CO<sub>575</sub>	CO<sub>576</sub>	CO<sub>577</sub>	CO<sub>578</sub>	CO<sub>579</sub>	CO<sub>580</sub>	CO<sub>581</sub>	CO<sub>582</sub>	CO<sub>583</sub>	CO<sub>584</sub>	CO<sub>585</sub>	CO<sub>586</sub>	CO<sub>587</sub>	CO<sub>588</sub>	CO<sub>589</sub>	CO<sub>590</sub>	CO<sub>591</sub>	CO<sub>592</sub>	CO<sub>593</sub>	CO<sub>594</sub>	CO<sub>595</sub>	CO<sub>596</sub>	CO<sub>597</sub>	CO<sub>598</sub>	CO<sub>599</sub>	CO<sub>600</sub>	CO<sub>601</sub>	CO<sub>602</sub>	CO<sub>603</sub>	CO<sub>604</sub>	CO<sub>605</sub>	CO<sub>606</sub>	CO<sub>607</sub>	CO<sub>608</sub>	CO<sub>609</sub>	CO<sub>610</sub>	CO<sub>611</sub>	CO<sub>612</sub>	CO<sub>613</sub>	CO<sub>614</sub>	CO<sub>615</sub>	CO<sub>616</sub>	CO<sub>617</sub>	CO<sub>618</sub>	CO<sub>619</sub>	CO<sub>620</sub>	CO<sub>621</sub>	CO<sub>622</sub>	CO<sub>623</sub>	CO<sub>624</sub>	CO<sub>625</sub>	CO<sub>626</sub>	CO<sub>627</sub>	CO<sub>628</sub>	CO<sub>629</sub>	CO<sub>630</sub>	CO<sub>631</sub>	CO<sub>632</sub>	CO<sub>633</sub>	CO<sub>634</sub>	CO<sub>635</sub>	CO<sub>636</sub>	CO<sub>637</sub>	CO<sub>638</sub>	CO<sub>639</sub>	CO<sub>640</sub>	CO<sub>641</sub>	CO<sub>642</sub>	CO<sub>643</sub>	CO<sub>644</sub>	CO<sub>645</sub>	CO<sub>646</sub>	CO<sub>647</sub>	CO<sub>648</sub>	CO<sub>649</sub>	CO<sub>650</sub>	CO<sub>651</sub>	CO<sub>652</sub>	CO<sub>653</sub>	CO<sub>654</sub>	CO<sub>655</sub>	CO<sub>656</sub>	CO<sub>657</sub>	CO<sub>658</sub>	CO<sub>659</sub>	CO<sub>660</sub>	CO<sub>661</sub>	CO<sub>662</sub>	CO<sub>663</sub>	CO<sub>664</sub>	CO<sub

Table 1. Burner Characterization Summary

**Table 2. Summary of Natural Gas Baseline Testing**

		ABB COMBUSTION ENGINEERING BASELINE GAS SUMMARY				
TEST/DESCRIPTION:		7/25/95	7/25/95	7/25/95	7/26/95	8/1/95
	3% O <sub>2</sub>	2%	O <sub>2</sub>	1%	O <sub>2</sub>	1.5% O <sub>2</sub>
	Prim. Open	Prim. Open	Prim. Open	Prim. Open	Prim. Open	
	Sec. Open	Sec. Open	Sec. Open	Sec. Open	Sec. Open	
	Tert. 25% Op	Tert. 25% Op	Tert. 25% Op	Tert. Open	Tert.75% Op	
	Gas Gun -4"	Gas Gun -4"	Gas Gun -4"	Gas Gun +4"	Gas Gun +4"	
	Coal Gun Out	Coal Gun Out	Coal Gun Out	Coal Gun Out	Coal Gun Out	
<b>WATER/STEAM SIDE</b>						
Steam flow rate; lb/h	12,404	12,387	12,411	15,659	8,609	
Water temperature into boiler; °F	206	207	207	217	217	
Drum pressure; psig	199	200	200	204	194	
Calorimeter temperature; °F	304	304	304	317	313	
Steam temperature; °F	378	379	379	391	387	
Steam quality; %	99.48	99.50	99.50	100.23	99.37	
Blowdown rate; lb/h	3,093	3,099	3,099	3,128	3,054	
<b>AIR,FUEL, FLUE GAS SIDE</b>						
Natural gas flow rate; lb/h, MMBtu/h	567, 13.2	567, 13.2	567, 13.2	732, 17.1	367, 8.6	
Coal flow rate; lb/h, MMBtu/h	Not Applicable (NA)	NA	NA	NA	NA	
Furnace outlet temperature; °F	525	520	517	576	477	
Gas temperature leaving air heater; °F	354	351	349	390	337	
Air temperature entering air heater; °F	175	179	182	173	211	
Air temperature leaving air heater; °F	383	384	384	409	385	
Air temperature into boiler; °F	363	364	365	391	363	
Ash content of particulate; %	NA	NA	NA	NA	NA	
Carbon content of furnace ash; %	NA	NA	NA	NA	NA	
HHV of fly ash; Btu/lb	NA	NA	NA	NA	NA	
HHV of furnace ash; Btu/lb	NA	NA	NA	NA	NA	
Combustion air flow; lb/h	11,112	10,577	10,092	13,279	6,765	
Boiler draft; in H <sub>2</sub> O	-0.07	-0.07	-0.07	-0.08	-0.07	
Boiler efficiency; %	82.84	82.94	83.14	83.03	83.61	
Relative humidity, %	60	60	60	60	60	
Mill air flow rate; lb/h	0	0	0	0	0	
Mill outlet temperature; °F	77	77	72	115	80	
Natural gas temperature; °F	80	80	80	85	98	
<b>EMISSIONS</b>						
O <sub>2</sub> ; %	3.1	2.1	1.1	1.5	1.8	
CO; ppm	45	49	108	37	73	
CO <sub>2</sub> ; %	9.6	10.2	10.6	11.0	11.2	
SO <sub>2</sub> ; ppm	NA	NA	NA	NA	NA	
NO <sub>x</sub> ; ppm	44	44	43	26	48	
Particulates; gr/SCF	NA	NA	NA	NA	NA	
O <sub>2</sub> before and after air heater; %,%	3.1, Not Measured(NM)	2.1, NM	1.1, NM	1.5, NM	1.8,NM	
<b>ECONOMIC ANALYSIS DATA</b>						
ID fan power consumption; w/h	NM	NM	NM	NM	NM	
FD fan power consumption; w/h	NM	NM	NM	NM	NM	
Pulverizer power consumption; w/h	NA	NA	NA	NA	NA	
Booster fan power consumption; w/h	NM	NM	NM	NM	NM	
Ash collection power consumption; w/h	NA	NA	NA	NA	NA	
Crusher power consumption; w/h	NA	NA	NA	NA	NA	
Reclaimer conveyor power consumption; w/h	NA	NA	NA	NA	NA	
Feed screw power consumption; w/h	NA	NA	NA	NA	NA	
Feedwater pump power consumption; w/h	NM	NM	NM	NM	NM	
Total air usage; scfm (Pilot burner)	NM	NM	NM	NM	NM	
Maximum load (based on 14,700 lb steam/h); %	84.38	84.27	84.43	106.52	58.56	
Coal related downtime	NA	NA	NA	NA	NA	

Table 3. Summary of Coal-Fired Testing

TEST/DESCRIPTION:		8/9/95	8/9/95	8/23/95	8/24/95	8/25/95
	Low-NOx	High Comb. Eff.				
	Prim. Closed	Prim. Open	Prim. Open	Prim. Open	Prim. Closed	
	Sec. Closed	Sec. Closed	Sec. 70%	Sec. Open	Sec. Closed	
	Tert. Open	Tert. Closed	Ter. 50%	Tert. 50%	Tert. 50%	
	Gas Gun -8.5° C. Gun 42.25°	Gas Gun -8.5° C. Gun 42.25°	Gas Gun 3° C. Gun 32°	Gas Gun -9° C. Gun -10.5°	Gas Gun -9° C. Gun -11°	
<b>WATER/STEAM SIDE</b>						
Steam flow rate; lb/h		13,466	14,367	13,467	14,417	14,378
Water temperature into boiler; °F		218	219	208	207	207
Drum pressure; psig		191	186	187	183	187
Calorimeter temperature; °F		313	312	302	301	301
Steam temperature; °F		386	384	373	371	372
Steam quality; %		100.0	100.0	99.3	99.3	99.3
Blowdown rate; lb/h		3,027	2,985	2,994	2,967	2,999
<b>AIR,FUEL, FLUE GAS SIDE</b>						
Natural gas flow rate; lb/h, MMBtu/h	Not Applicable (NA)	NA	NA	NA	NA	NA
Coal flow rate; lb/h, MMBtu/h	1,140;16.4	1,140;16.4	1,140;16.4	1,140;16.5	1,140;16.5	
Furnace outlet temperature; °F	588	607	549	539	594	
Gas temperature leaving air heater; °F	403	414	378	378	400	
Air temperature entering air heater; °F	177	183	175	171	166	
Air temperature leaving air heater; °F	427	436	404	395	421	
Air temperature into boiler; °F	404	415	382	377	399	
Ash content of particulate; %	47.55	61.61	30.82	49.94	45.02	
Carbon content of furnace ash; %	NA	NA	NA	NA	NA	
Coal combustion efficiency; %	94.1±1.2	97.2±0.5	89.2±1.3	95.3±0.6	94.5±0.6	
HHV of fly ash; Btu/lb	NA	NA	NA	NA	NA	
HHV of furnace ash; Btu/lb	NA	NA	NA	NA	NA	
Combustion air flow; lb/h	14,615	14,011	14,403	14849	14,442	
Boiler draft; in H2O	0.04	0.03	0.05	-0.04	-0.01	
Boiler efficiency; %	83.44	85.75	80.36	84.7	83.48	
Relative humidity, %	60	60	60	60	60	
Mill air flow rate; acfm,lb/h	341;1,624	326;1,526	356;1,691	360;1,711	359;1,711	
Mill outlet temperature; °F	231	243	211	206	206	
Natural gas temperature; °F	85	93	88	91	79	
<b>EMISSIONS</b>						
O2; %	3.5	2.7	3.4	3.8	3.3	
CO; ppm;lb/MMBtu@3%O2	238;0.20	149;0.12	258;0.22	146;0.13	178;0.15	
CO2; %	15.8	16.5	15.6	15.0	15.3	
SO2; ppm;lb/MMBtu@3%O2	512;1.00	552;0.99	583;1.11	485;0.97	529;1.00	
NOX; ppm;lb/MMBtu@3%O2	371;0.52	684;0.88	281;0.38	443;0.64	439;0.60	
Particulates; gr/SCF	Not Measured (NM)	NM	NM	NM	NM	
<b>ECONOMIC ANALYSIS DATA</b>						
ID fan power consumption; w/h	NM	NM	NM	NM	NM	
FD fan power consumption; w/h	NM	NM	NM	NM	NM	
Pulverizer power consumption; w/h	NM	NM	NM	NM	NM	
Booster fan power consumption; w/h	NM	NM	NM	NM	NM	
Ash collection power consumption; w/h	NA	NA	NA	NA	NA	
Crusher power consumption; w/h	NA	NA	NA	NA	NA	
Reclaimer conveyor power consumption; w/h	NA	NA	NA	NA	NA	
Feed screw power consumption; w/h	NA	NA	NA	NA	NA	
Feedwater pump power consumption; w/h	NM	NM	NM	NM	NM	
Total air usage; scfm (Pilot burner)	NM	NM	NM	NM	NM	
Maximum load (based on 14,700 lb steam/h); %	91.6	97.7	91.6	98.1	97.8	

Table 3. Summary of Coal-Fired Testing

TEST/DESCRIPTION:	8/28/95	8/29/95	8/30/95	8/31/95	9/5/95
	Prim. Open				
	Sec. Open	Sec. Open	Sec. Open	Sec. Open	Sec. 50%
	Tert. 50%				
	Gas Gun -9°				
	C. Gun -10.5°				
<b>WATER/STEAM SIDE</b>					
Steam flow rate; lb/h	14,039	13,938	14,139	13,601	13,122
Water temperature into boiler; °F	206	206	208	207	199
Drum pressure; psig	187	183	186	186	191
Calorimeter temperature; °F	300	301	302	302	301
Steam temperature; °F	372	371	373	372	374
Steam quality; %	99.3	99.3	99.4	99.3	99.3
Blowdown rate; lb/h	2,997	2,966	2,989	2,988	3,030
<b>AIR,FUEL, FLUE GAS SIDE</b>					
Natural gas flow rate; lb/h, MMBtu/h	NA	NA	NA	NA	NA
Coal flow rate; lb/h, MMBtu/h	1,140;16.5	1,140;16.5	1,140;16.5	1,140;16.5	1,098;15.6
Furnace outlet temperature; °F	562	561	566	571	571
Gas temperature leaving air heater; °F	386	389	390	391	389
Air temperature entering air heater; °F	168	177	173	175	171
Air temperature leaving air heater; °F	406	406	406	411	403
Air temperature into boiler; °F	383	387	385	389	377
Ash content of particulate; %	47.90	50.20	53.13	50.95	61.08
Carbon content of furnace ash; %	NA	NA	NA	NA	NA
Coal combustion efficiency; %	94.3±1.1	95.4±0.2	95.9±0.8	95.5±0.4	97.5±0.8
HHV of fly ash; Btu/lb	NA	NA	NA	NA	NA
HHV of furnace ash; Btu/lb	NA	NA	NA	NA	NA
Combustion air flow; lb/h	14,657	14,694	14,935	15,031	14,555
Boiler draft; in H2O	-0.02	-0.03	-0.03	-0.04	-0.02
Boiler efficiency; %	83.88	84.79	85.04	84.32	86.07
Relative humidity, %	60	60	60	60	60
Mill air flow rate; lb/h	388;1,853	356;1,685	390	392;1,871	369;1,775
Mill outlet temperature; °F	197	201	220	188	230
Natural gas temperature; °F	73	91	87	85	79
<b>EMISSIONS</b>					
O2; %	3.5	3.6	3.8	3.5	3.5
CO; ppm;lb/MMBtu@3%O2	129;0.11	166;0.14	114;0.10	118;0.10	119;0.10
CO2; %	15.4	15.4	15.3	15.6	15.9
SO2; ppm;lb/MMBtu@3%O2	474;0.92	511;1.00	538;1.08	478;0.95	540;1.07
NOx; ppm;lb/MMBtu@3%O2	385;0.54	361;0.51	325;0.47	341;0.48	474;0.68
Particulates; gr/SCF	NM	NM	NM	NM	NM
<b>ECONOMIC ANALYSIS DATA</b>					
ID fan power consumption; w/h	NM	NM	NM	NM	NM
FD fan power consumption; w/h	NM	NM	NM	NM	NM
Pulverizer power consumption; w/h	NM	NM	NM	NM	NM
Booster fan power consumption; w/h	NM	NM	NM	NM	NM
Ash collection power consumption; w/h	NA	NA	NA	NA	NA
Crusher power consumption; w/h	NA	NA	NA	NA	NA
Reclaimer conveyor power consumption; w/h	NA	NA	NA	NA	NA
Feed screw power consumption; w/h	NA	NA	NA	NA	NA
Feedwater pump power consumption; w/h	NM	NM	NM	NM	NM
Total air usage; scfm (Pilot burner)	NM	NM	NM	NM	NM
Maximum load (based on 14,700 lb steam/h); %	95.5	94.8	96.2	92.5	89.3

Table 4. Coal Analysis

Date	Weigh Belt Composite	Full Proximate Analysis				Ultimate Analysis				Cal Value (Dry)
		% Moist	% V.M.	% Ash	% F.C.	% C	% H	% N	% S	
24Jul95-		2.38	31.48	6.97	61.55	79.51	5.18	1.55	0.59	6.19
28Jul95		± 0.04	± 0.06	± 0.03	± 0.16	± 0.02	± 0.01	± 0.01	± 0.01	± 10
31Jul95-		2.19	31.54	6.64	61.82	79.75	5.21	1.53	0.60	6.27
04Aug95		± 0.01	± 0.05	± 0.01	± 0.02	± 0.01	± 0.00	± 0.01	± 0.01	± 13
07Aug95-		1.99	31.32	4.57	64.11	82.32	5.29	1.41	0.77	5.64
11Aug95		± 0.04	± 0.05	± 0.03	± 0.21	± 0.01	± 0.00	± 0.01	± 0.01	± 7
21Aug95-		1.87	30.82	4.36	64.82	82.41	5.04	1.40	0.81	5.98
25Aug95		± 0.01	± 0.02	± 0.01	± 0.19	± 0.01	± 0.00	± 0.02	± 0.02	± 2
28Aug95-		1.79	30.94	4.31	64.75	82.78	5.16	1.41	0.85	5.49
01Sep95		± 0.01	± 0.06	± 0.02	± 0.01	± 0.02	± 0.02	± 0.01	± 0.01	± 10
04Sep95-		2.40	30.80	4.34	64.86	82.05	5.21	1.41	0.84	6.15
08Sep95		± 0.03	± 0.17	± 0.03	± 0.74	± 0.07	± 0.00	± 0.01	± 0.01	± 12

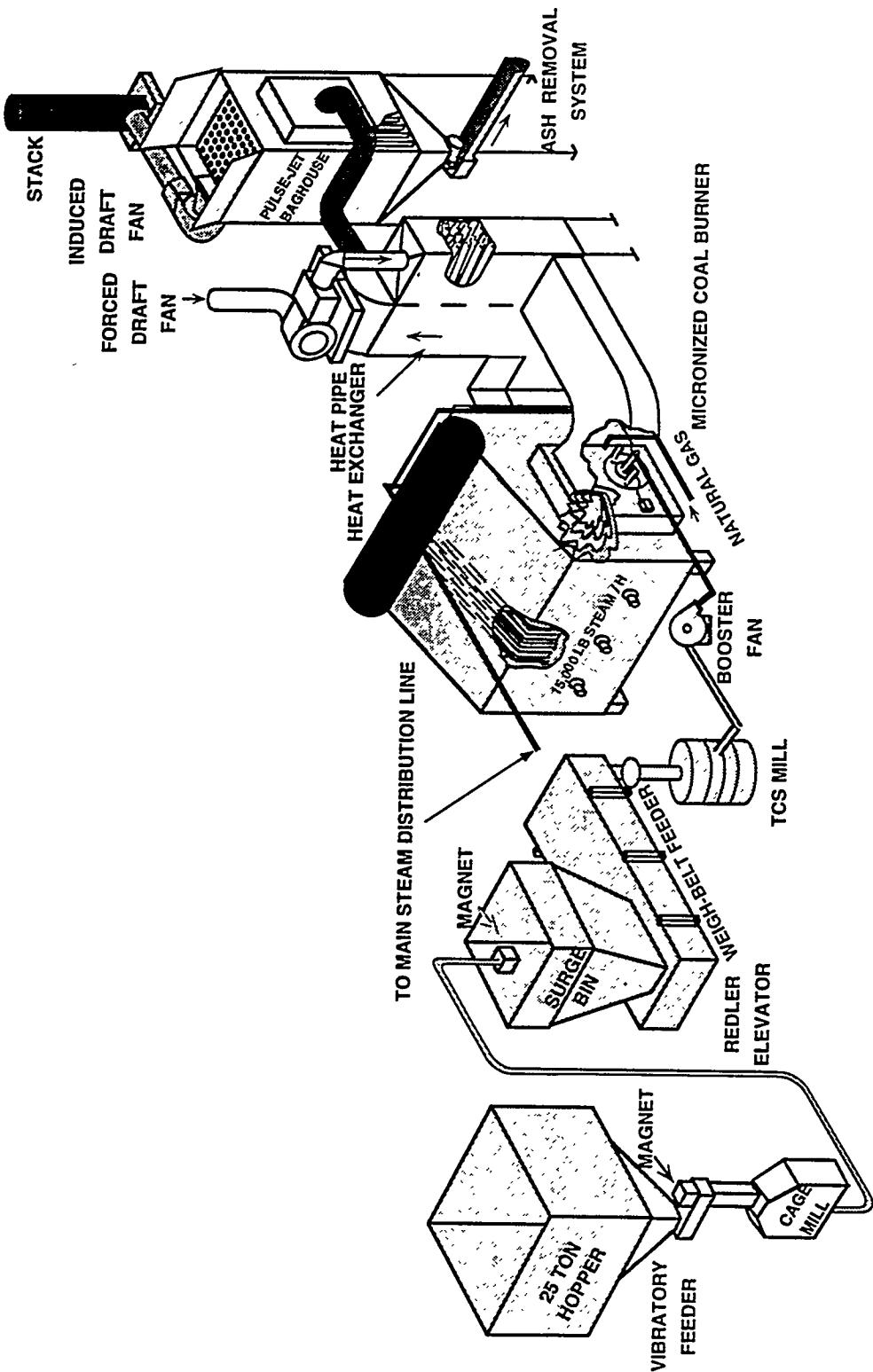
Coal samples are collected on a daily basis from the weigh-belt feeder outlet and weekly composites are made. Upper Freeport seam coal was tested from 07/24/95 through 08/04/95. Middle Kittanning seam coal was tested from 08/07/95 through 09/08/95.

Table 5. Coal Particle Size Distribution for Samples Isokinetically Collected at the Burner Inlet

Test Date	Test Time	Mill Speed (rpm)	Mill Amps	Mill Air Flow (cfm)	Coal Feed Rate (lb/m)	Mill Temp. (F)	Particle Size, in Microns, that is Less Than the Indicated Size				
							Mill Outlet	Top Size	<99	<95	<90
8/9/95	1050	1940	N.M.	352	86.4	226.9	160	80.8	63.3	36.4	21.5
8/9/95	1125	1940	N.M.	351	89.5	226.7	168	129	84.5	65.5	38.0
8/9/95	1445	1940	N.M.	320	97.4	246.3	188	141	73.1	59.3	34.8
8/12/95	1600	1,940	N.M.	341	83.8	214.9	183	133	75.0	60.5	38.7
8/24/95	1130	1940	N.M.	372	19.0	80.4	202.8	188	149	77.7	62.5
8/24/95	1600	1,940	N.M.	361	19.0	84.3	206.3	186	129	83.2	84.0
8/30/95	1220	1940	N.M.	386	19.0	92.0	198.0	188	165	99.0	70.2
8/31/95	1310	1,940	N.M.	390	19.0	85.6	169.7	188	144	75.4	82.3
9/5/95	1315	2080	88	367	18.3	86.0	255.9	188	122	76.2	53.8
9/5/95	1440	2,080	87	386	18.3	80.9	246.8	188	116	73.6	64.8
9/6/95	1345	2080	85	374	18.3	97.3	239.7	163	100	67.2	49.7
9/7/95	1020	2,080	83	393	17.7	80.8	222.0	163	109	74.1	66.5

Table 6. Mill Performance Comparison

Coal Seam:	Brookville	Kentucky	Middle Kittanning	Middle Kittanning
<u>Operating Conditions</u>				
Mill air flow; acfm	370-400	370-400	320-390	365-395
Coal flow; lb/m	16.5-18.5	16.5-18.5	19.0	18.3-19.0
Mill speed; rpm	1,940	1,940	1,940	2,080
<u>Particle Size (<math>\mu\text{m}</math>)</u>				
Top size	190-300	250-275	190	160-190
D <sub>80</sub>	50-70	50-70	45-50	35-40
D <sub>50</sub>	25-30	25-30	20-22	17-19



**Figure 1. MICRONIZED COAL-FIRED BOILER SYSTEM WITH COAL HANDLING MODIFICATIONS**

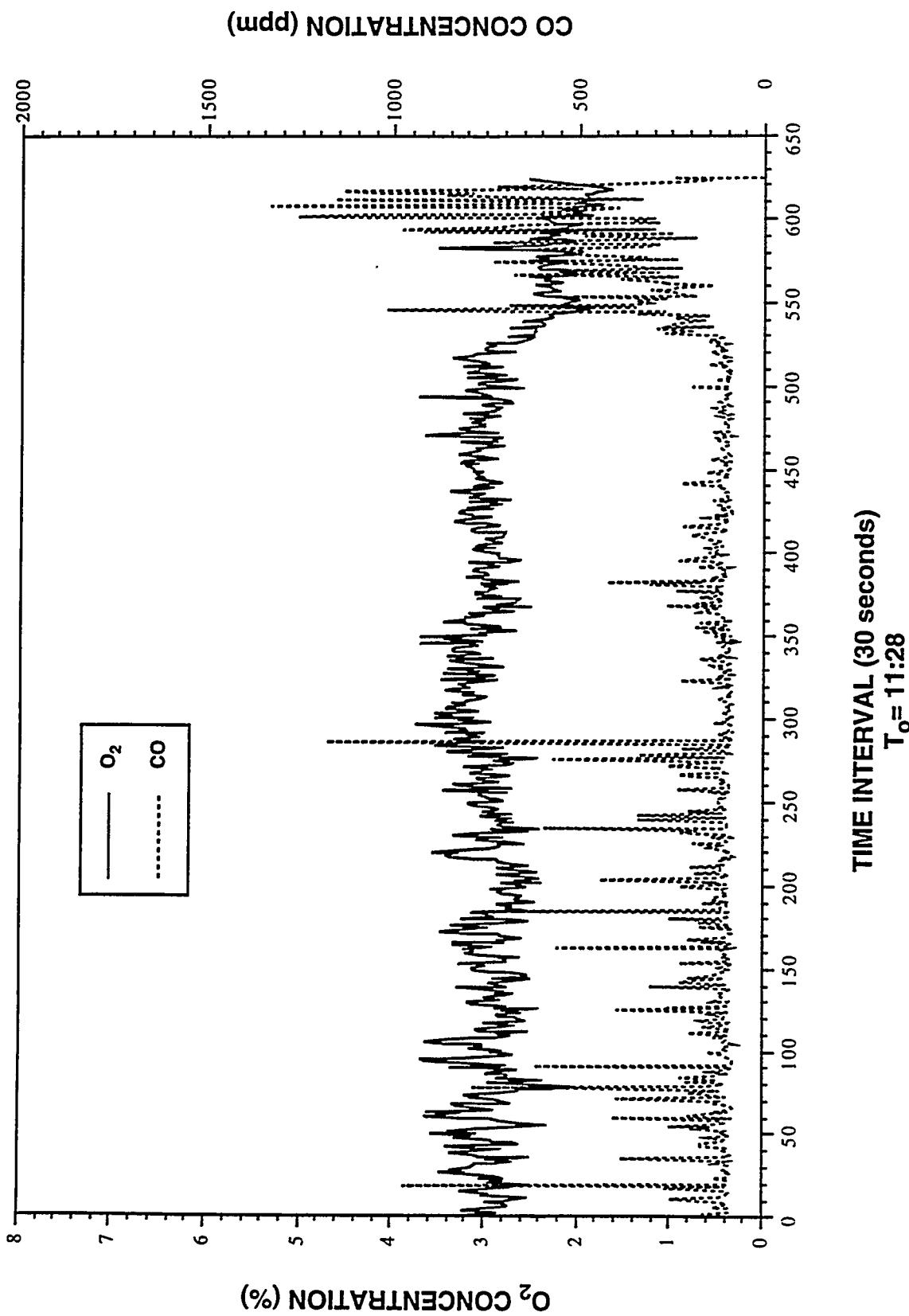


Figure 2.  $O_2$  AND CO CONCENTRATION vs. TIME FOR TESTING CONDUCTED ON 12/07/93

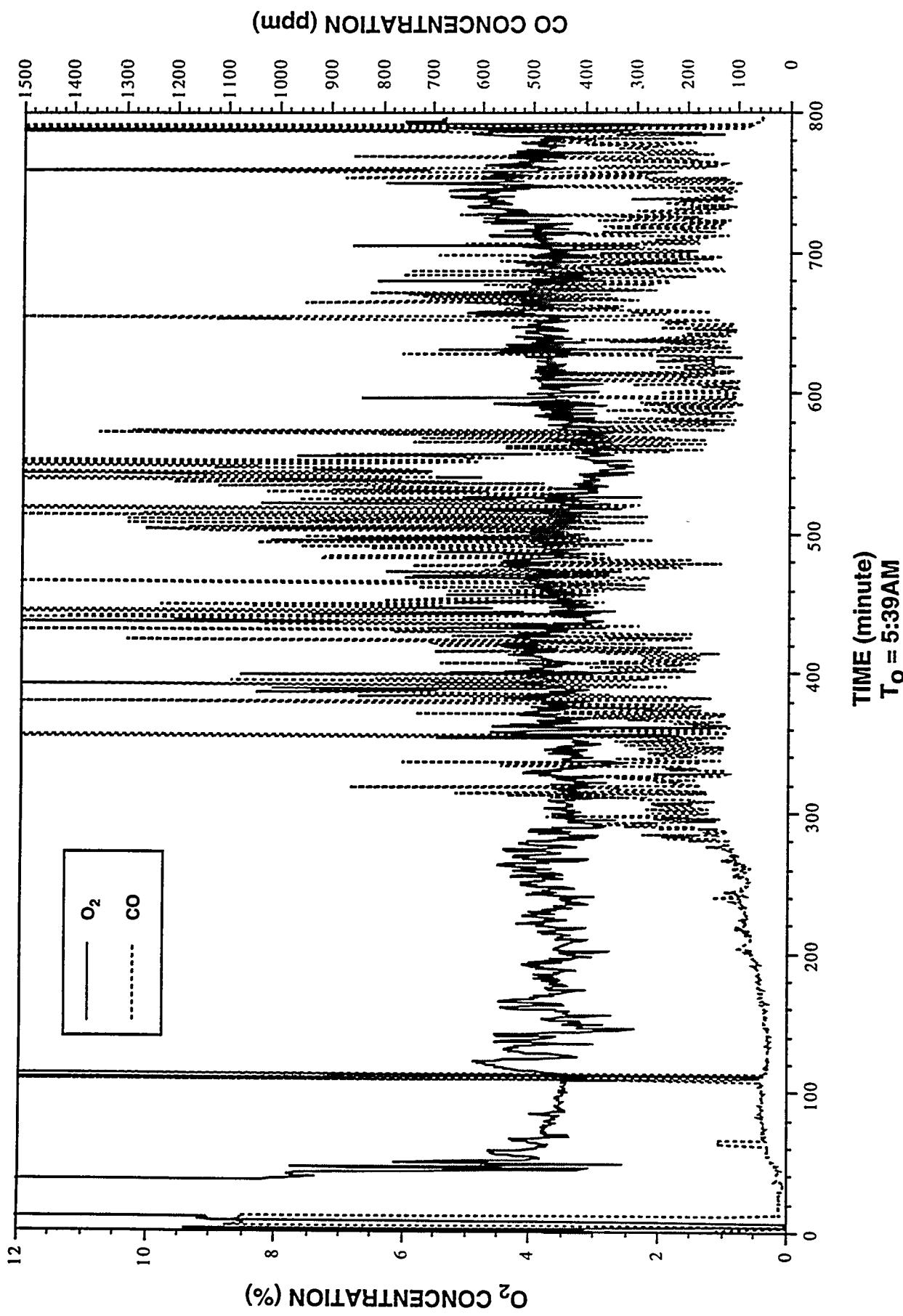


Figure 3.  $O_2$  AND CO CONCENTRATION vs. TIME FOR TESTING CONDUCTED ON 04/28/94

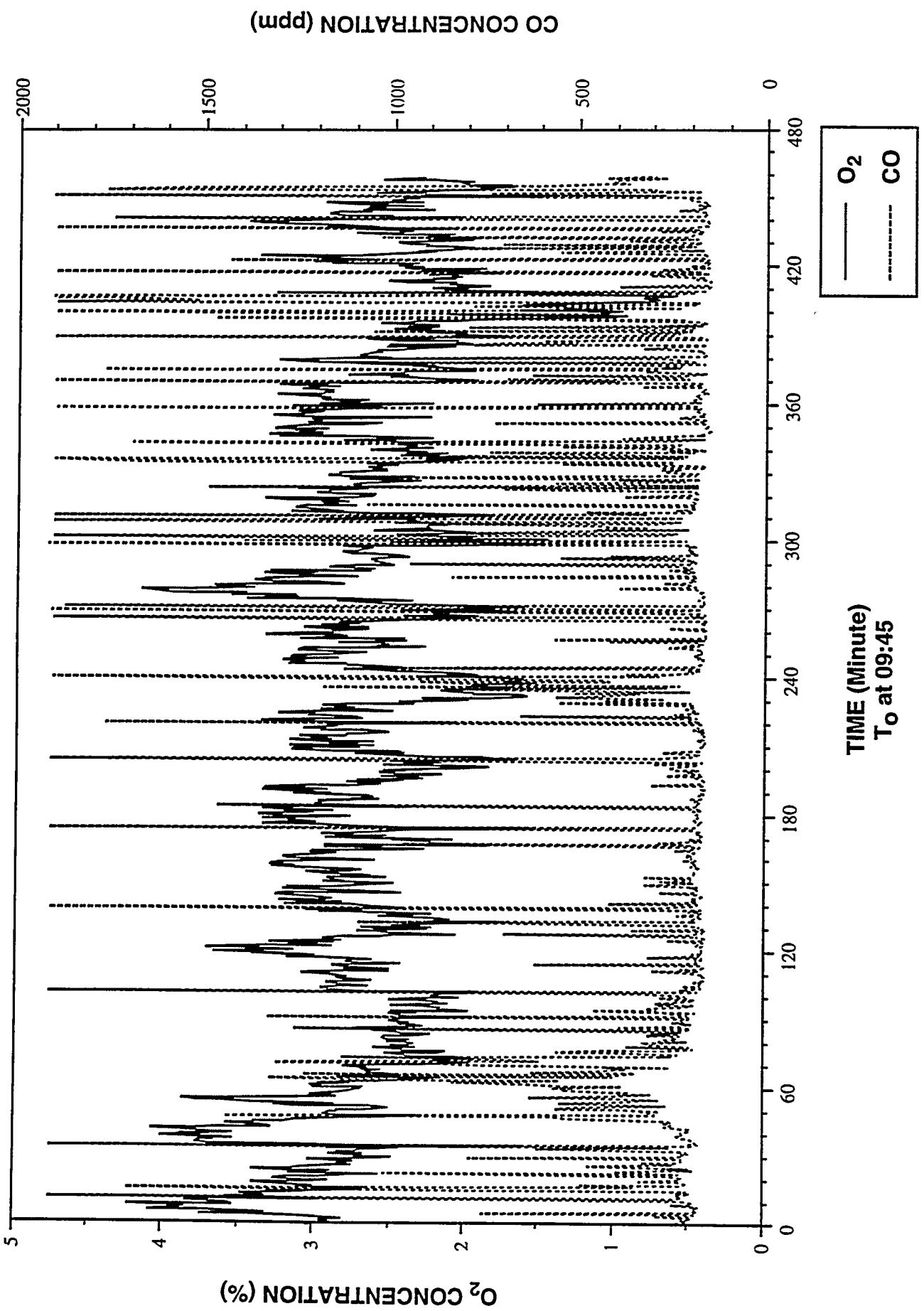


Figure 4. O<sub>2</sub> AND CO CONCENTRATION v. TIME FOR TESTING CONDUCTED ON 08/03/95

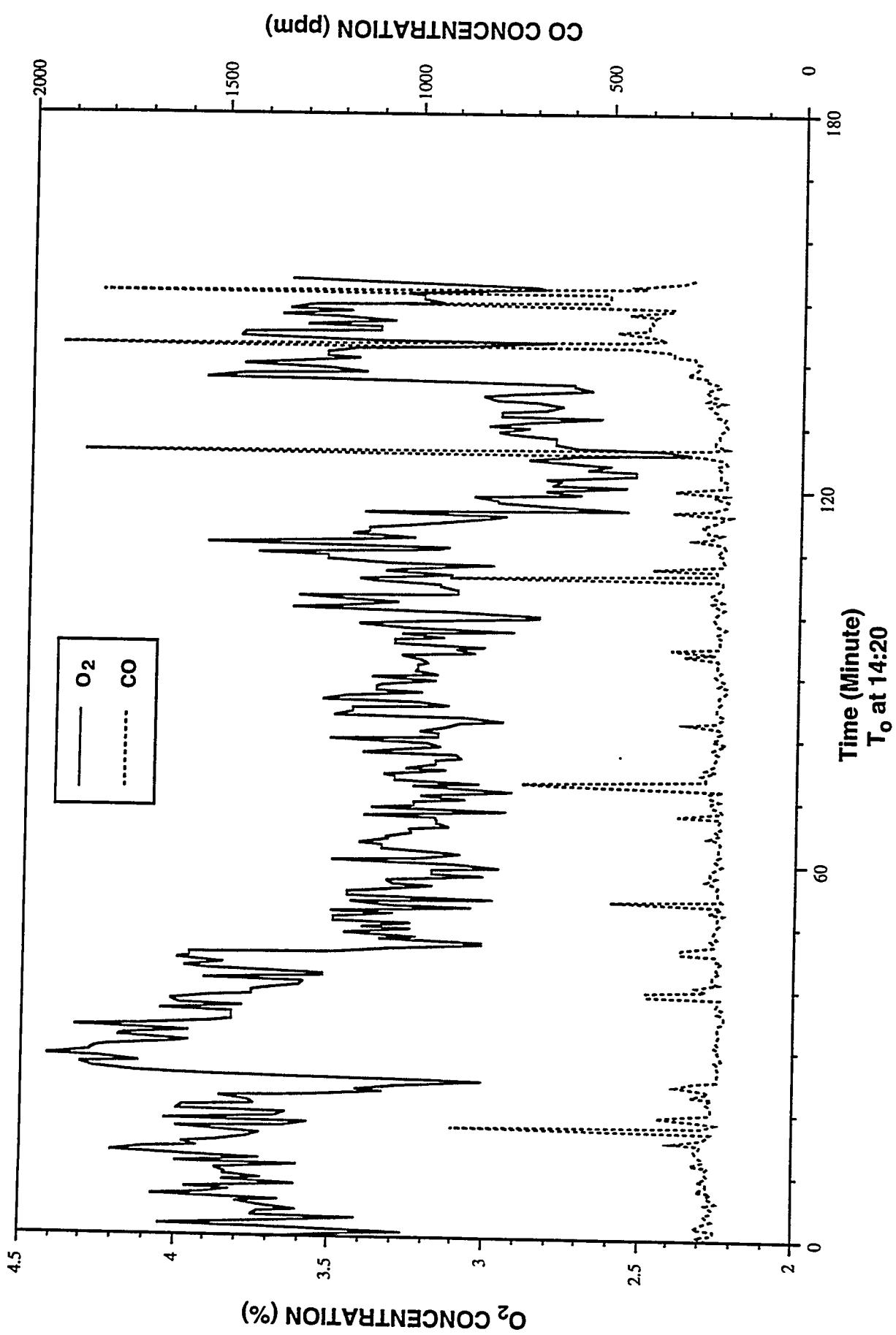


Figure 5. O<sub>2</sub> AND CO CONCENTRATION vs. TIME FOR TESTING CONDUCTED ON 08/23/95

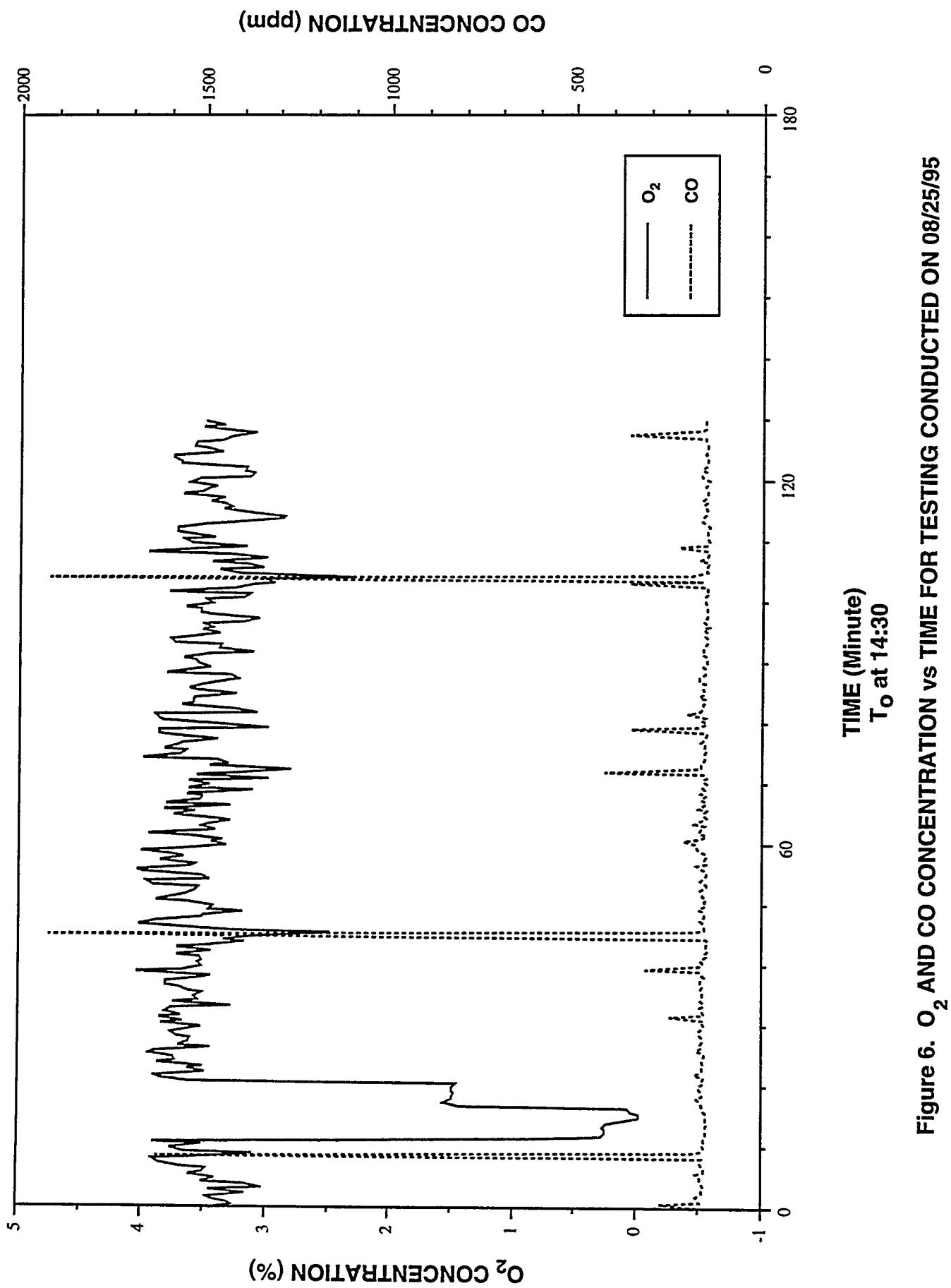


Figure 6. O<sub>2</sub> AND CO CONCENTRATION vs TIME FOR TESTING CONDUCTED ON 08/25/95

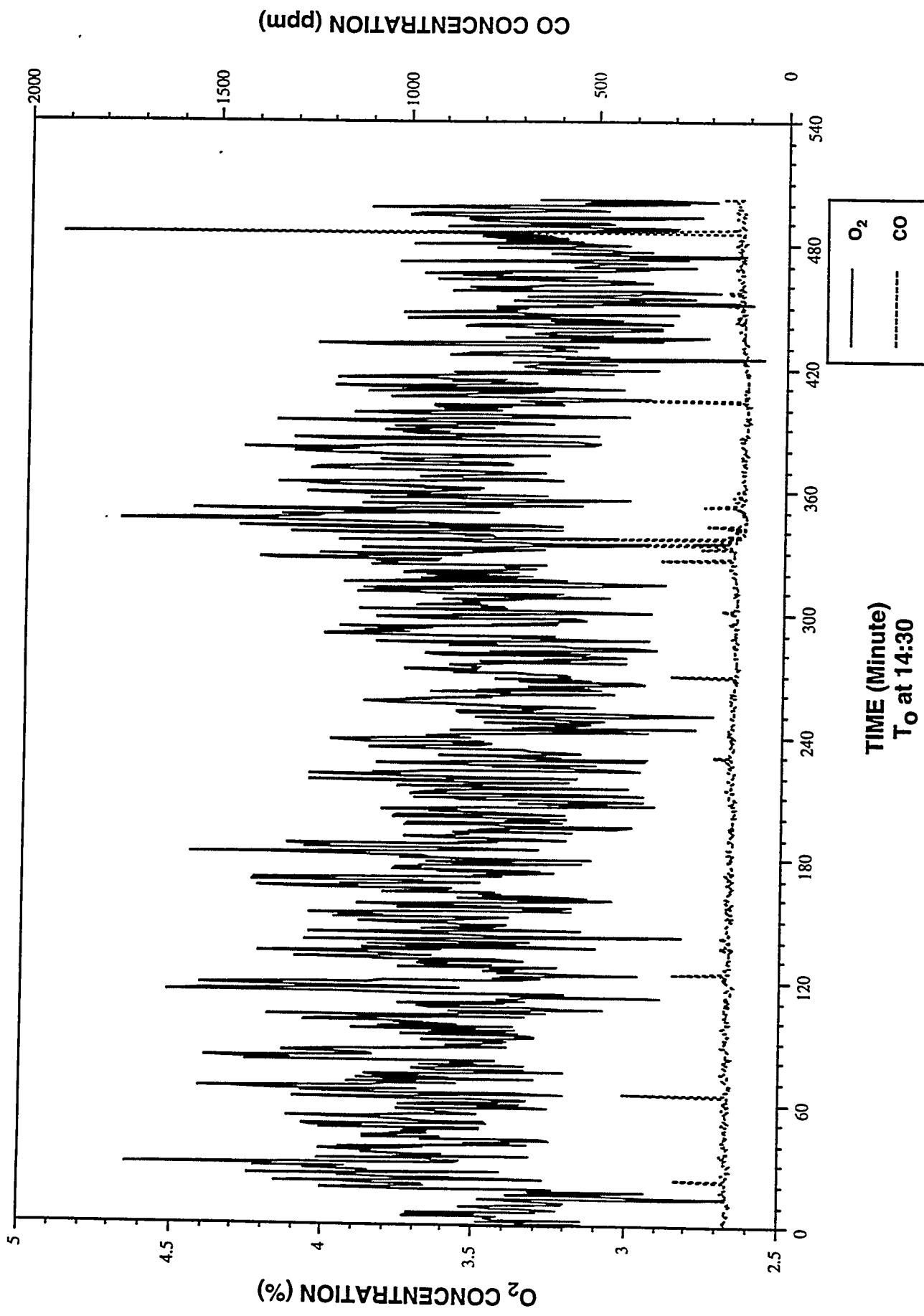


Figure 7. O<sub>2</sub> AND CO CONCENTRATION vs TIME FOR TESTING CONDUCTED ON 08/28/95

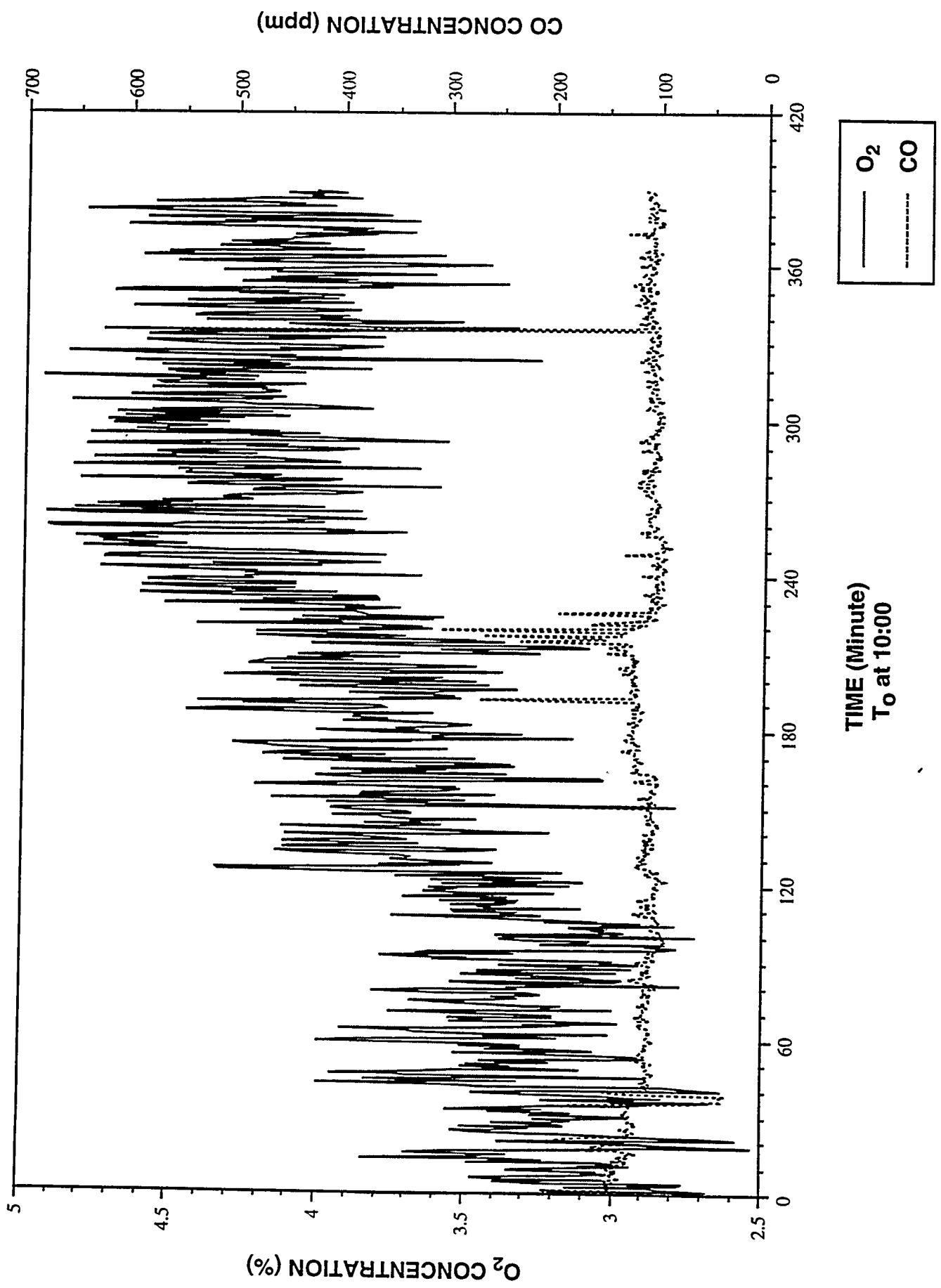


Figure 8. O<sub>2</sub> and CO CONCENTRATION vs TIME FOR TESTING CONDUCTED ON 08/30/95

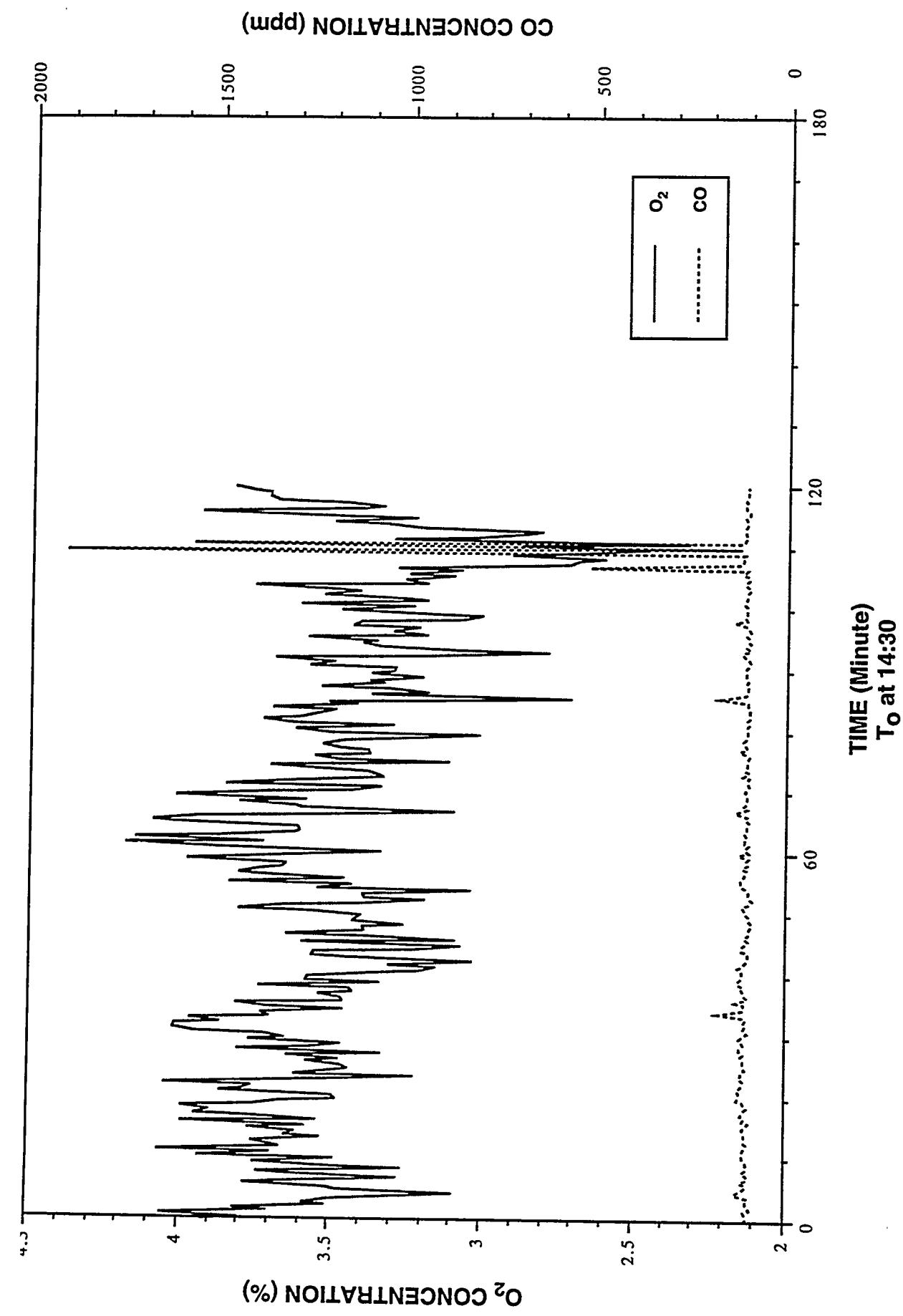


Figure 9. O<sub>2</sub> AND CO CONCENTRATION vs TIME FOR TESTING CONDUCTED ON 09/05/95

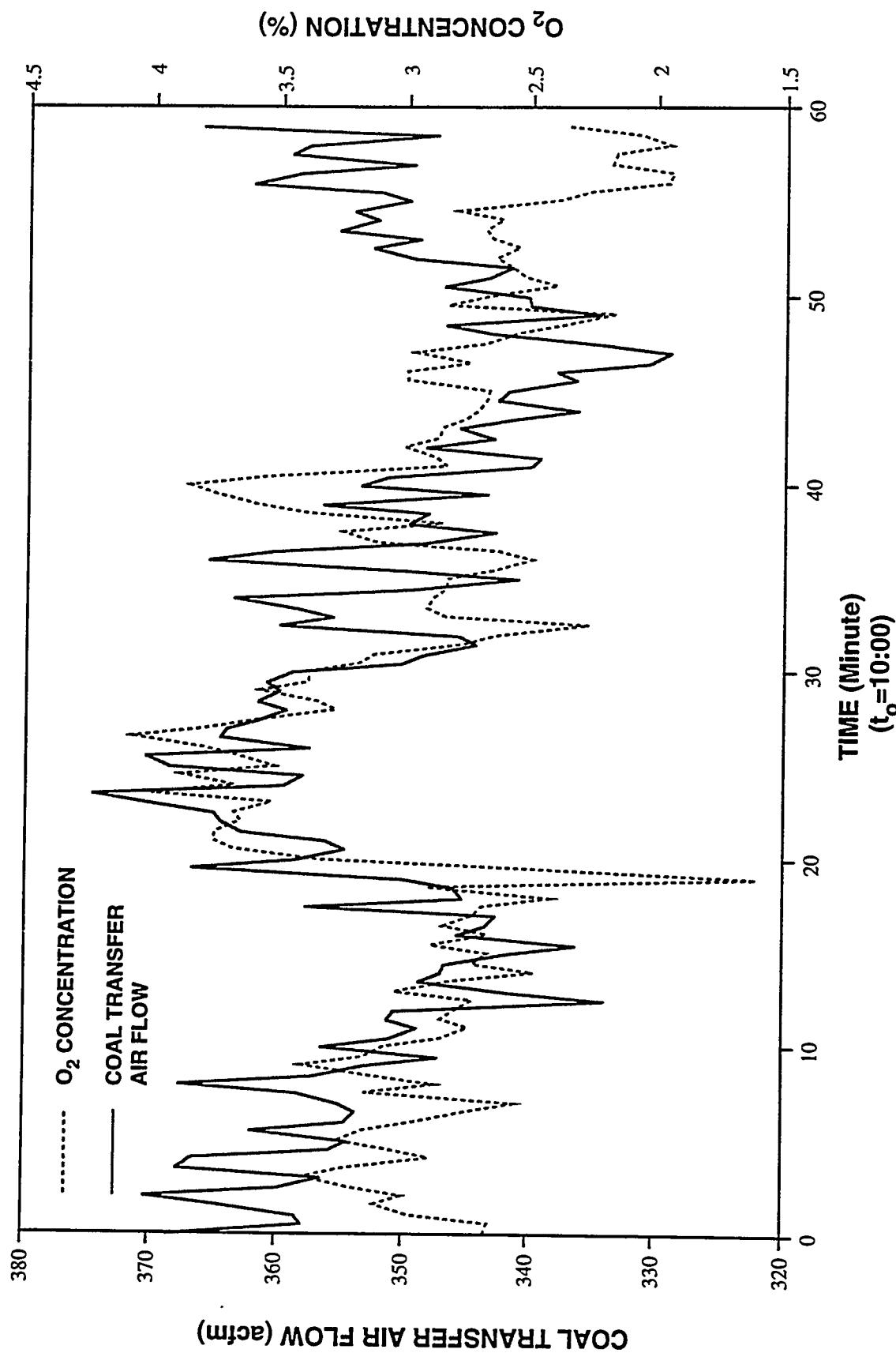


Figure 10. COAL TRANSFER AIR FLOW AND OXYGEN CONCENTRATION vs TIME FOR TESTING CONDUCTED ON 08/03/95

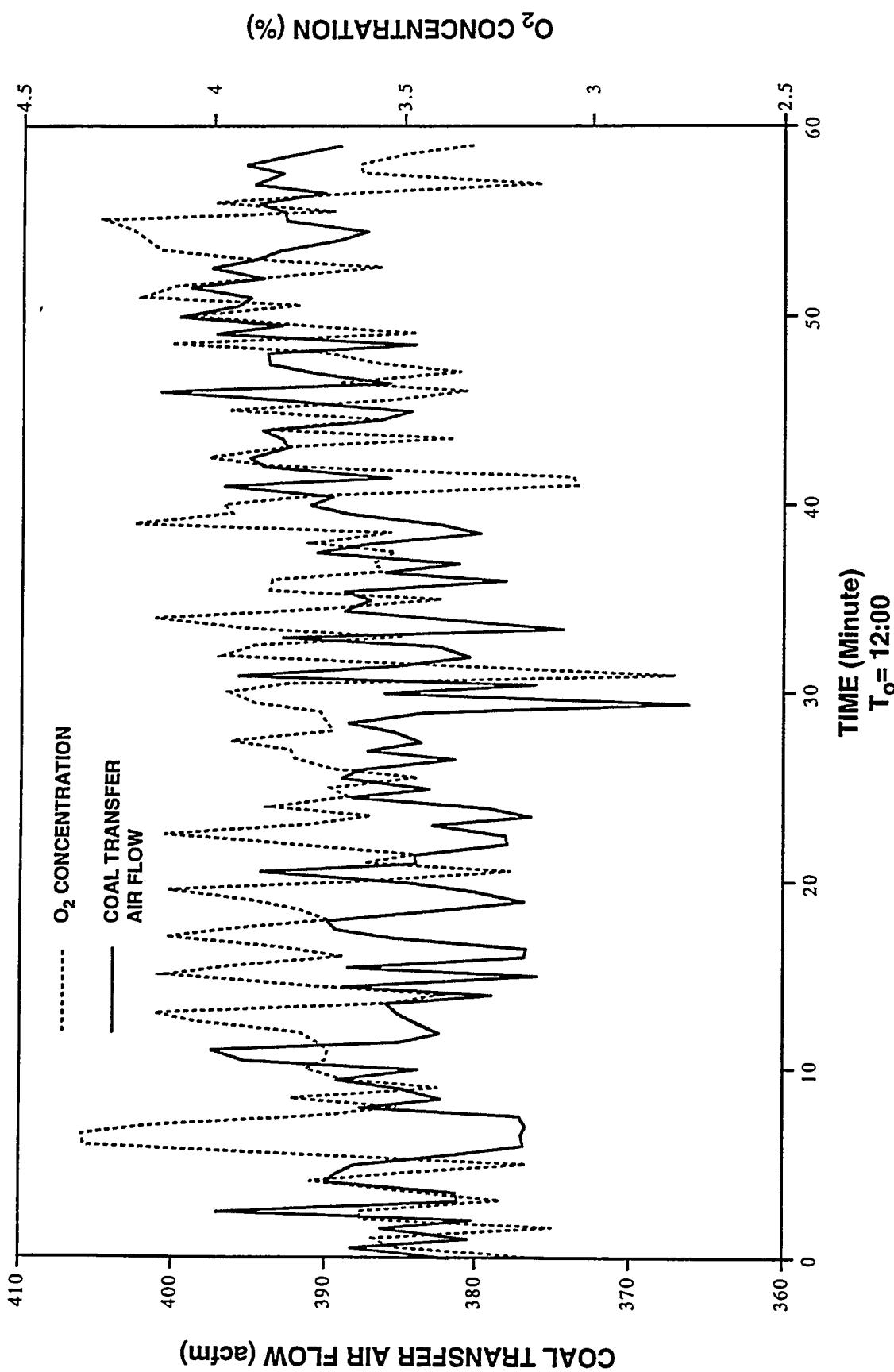


Figure 11. COAL TRANSFER AIR FLOW AND OXYGEN CONCENTRATION vs TIME FOR TESTING  
CONDUCTED ON 08/30/95

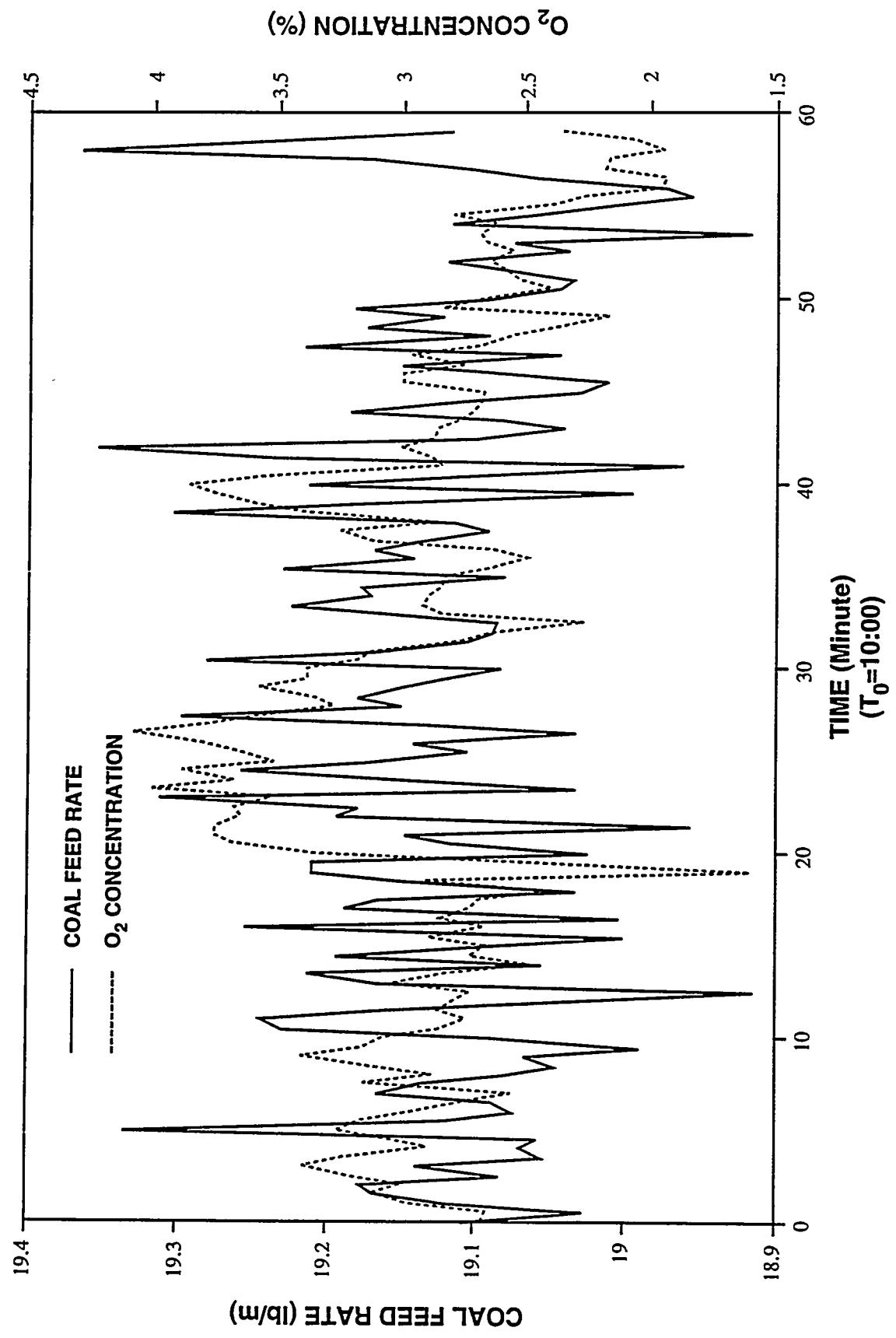


Figure 12. COAL FEED RATE AND OXYGEN CONCENTRATION vs TIME FOR THE TESTING CONDUCTED ON 08/03/95  
 $(T_0=10:00)$

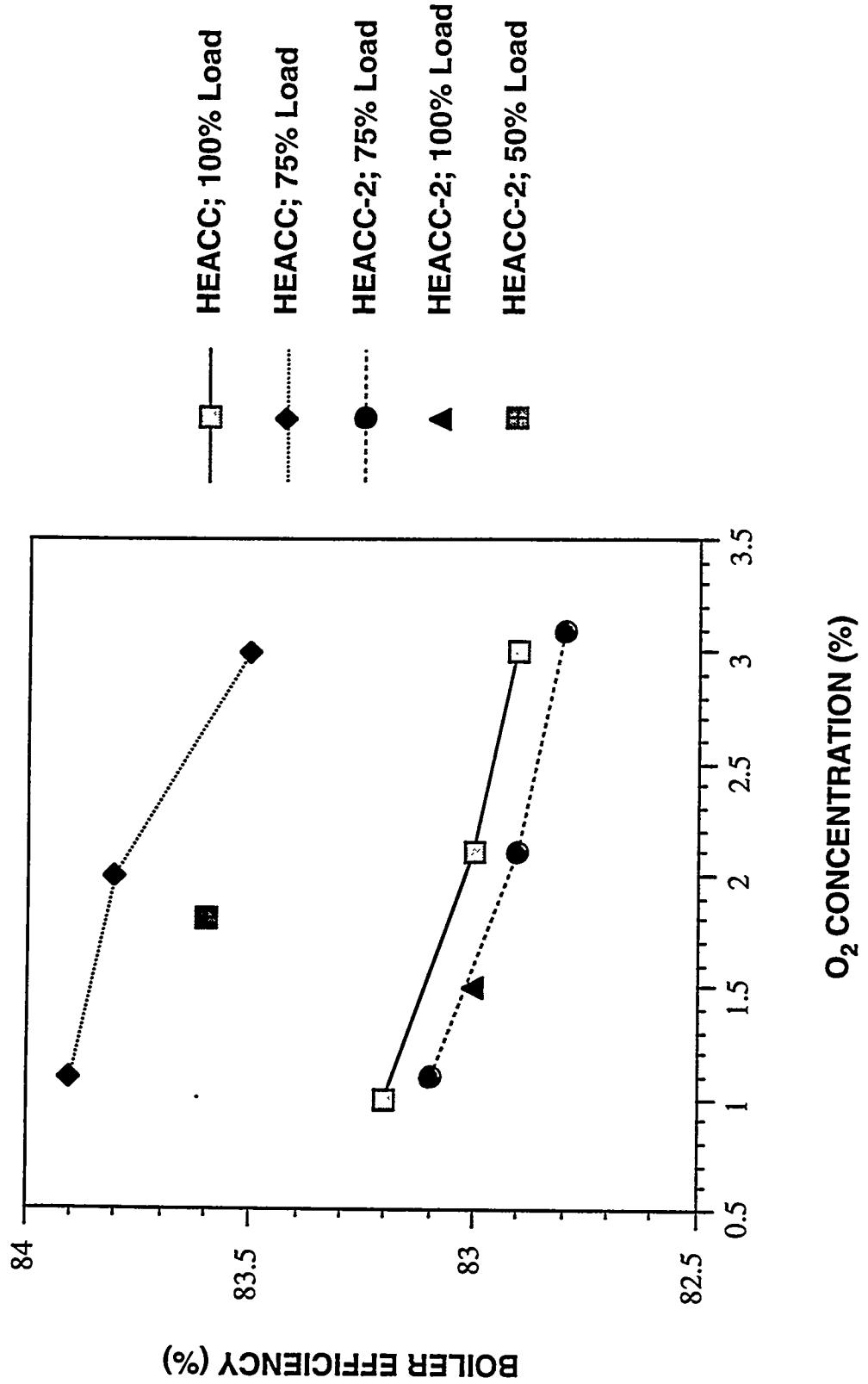
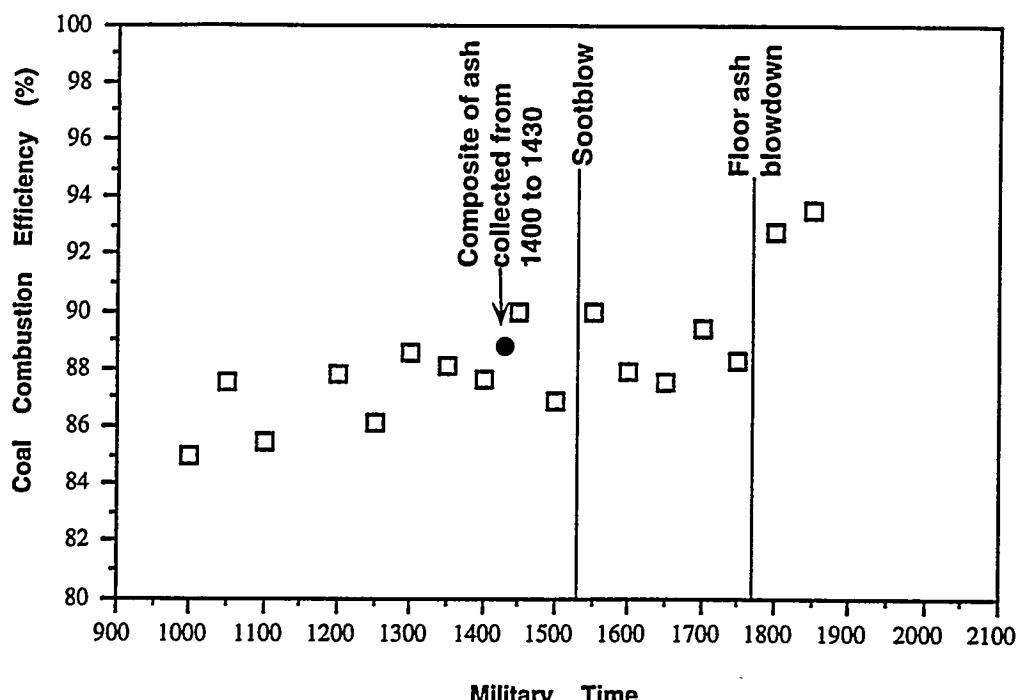
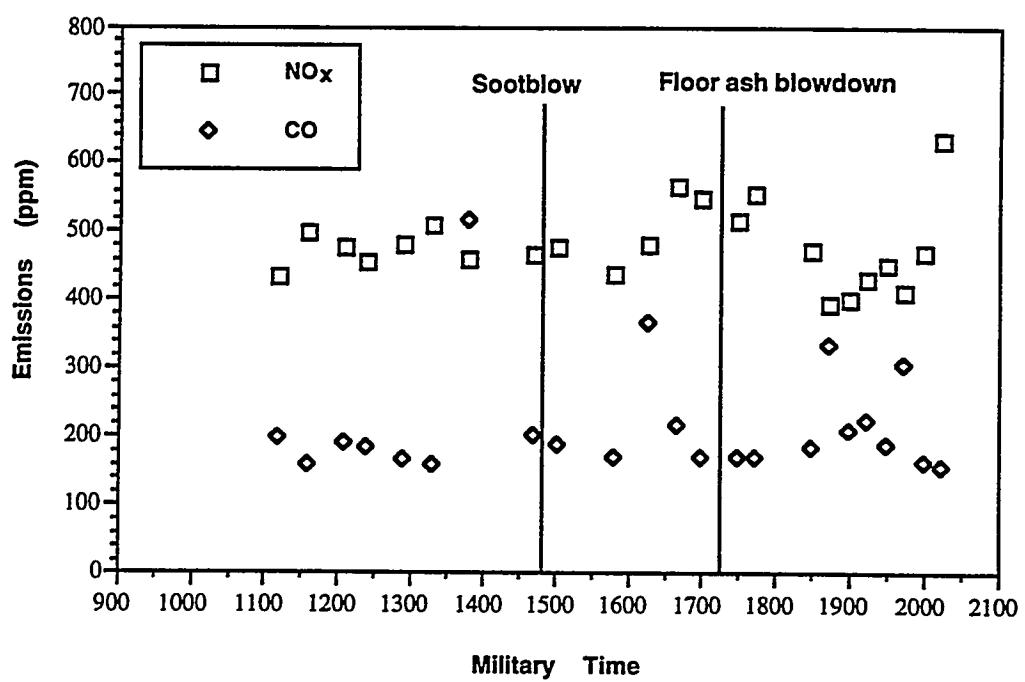


Figure 13. BOILER EFFICIENCY AS A FUNCTION OF O<sub>2</sub> CONCENTRATION FOR THE HEACC AND HEACC-2

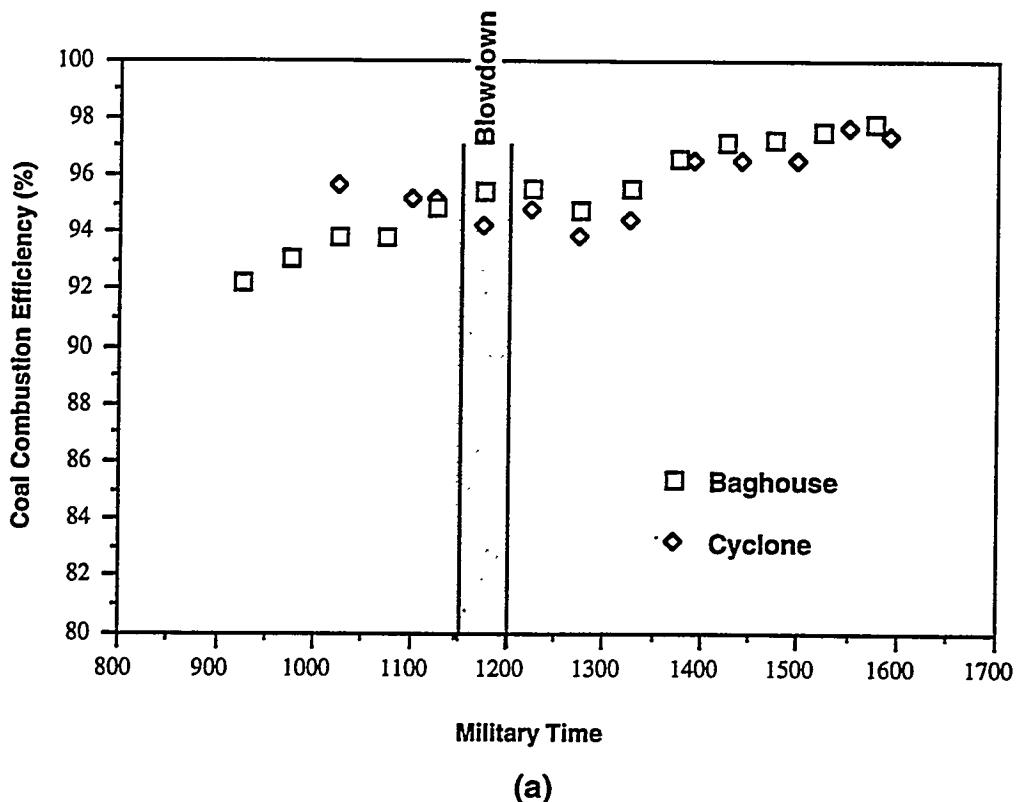


(a)

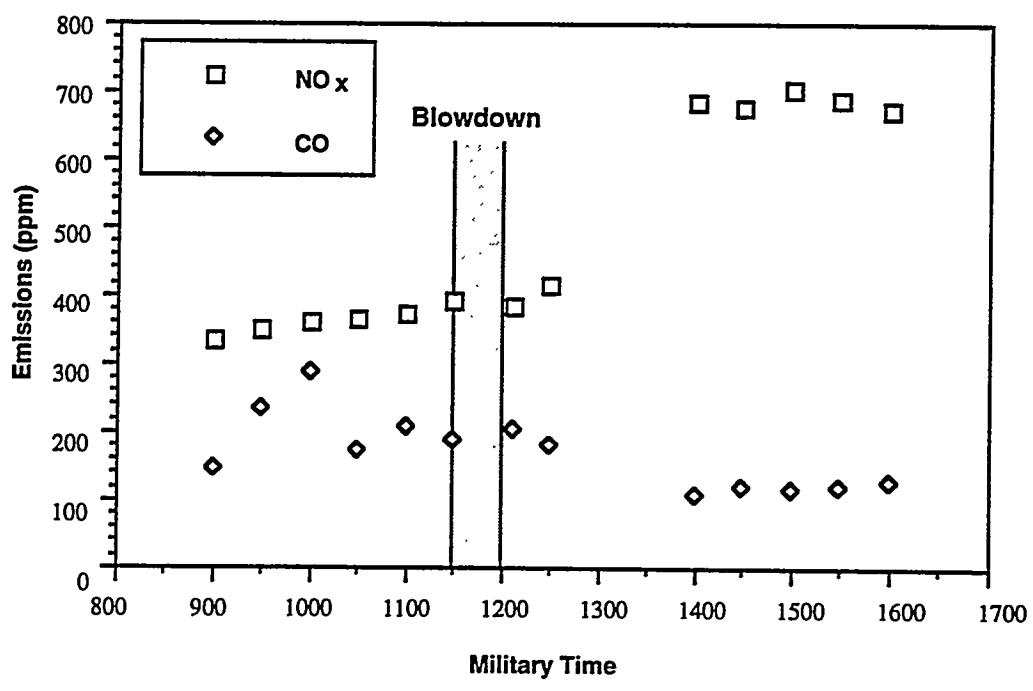


(b)

**Figure 14. COAL COMBUSTION EFFICIENCY BASED ON THE BAGHOUSE ASH SAMPLES (a) AND EMISSIONS (b) AS A FUNCTION OF TIME FOR THE TESTING CONDUCTED ON 08/03/95**

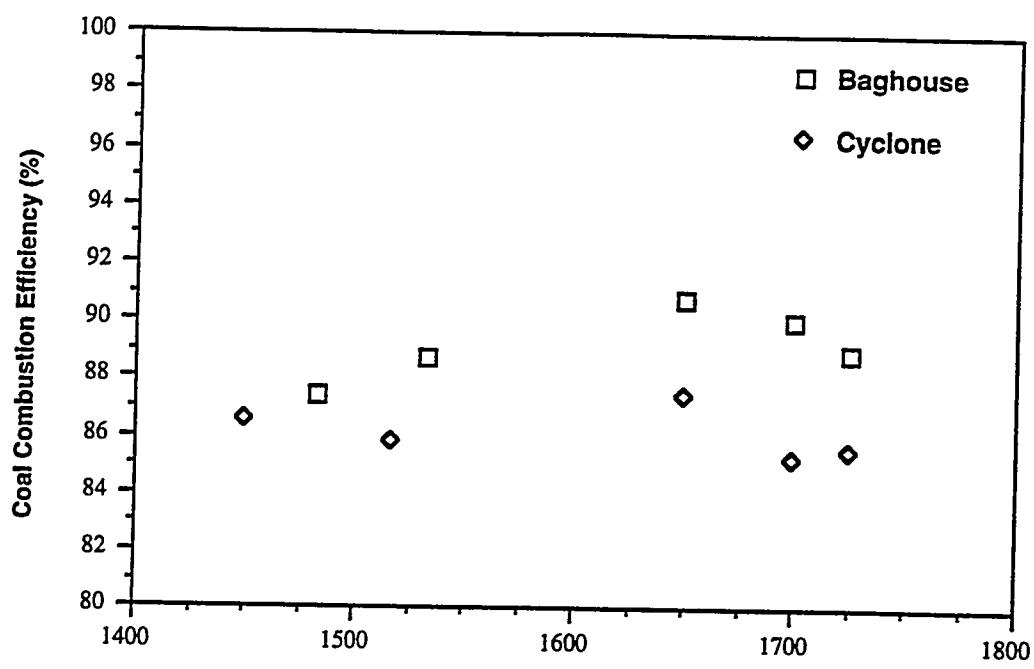


(a)



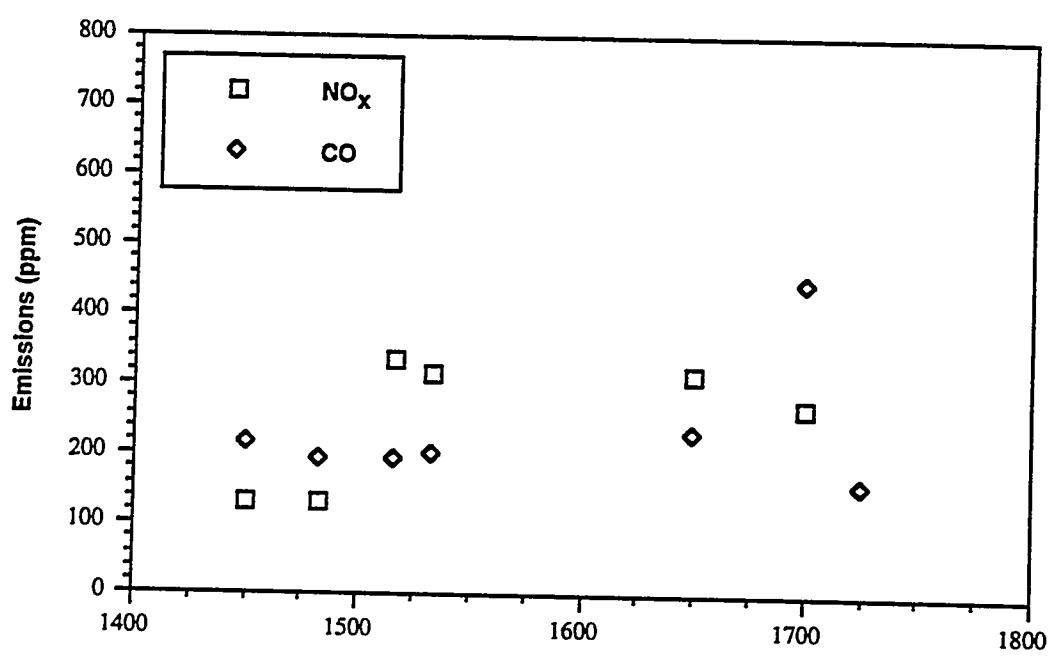
(b)

**Figure 15. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 08/09/95**



Military Time

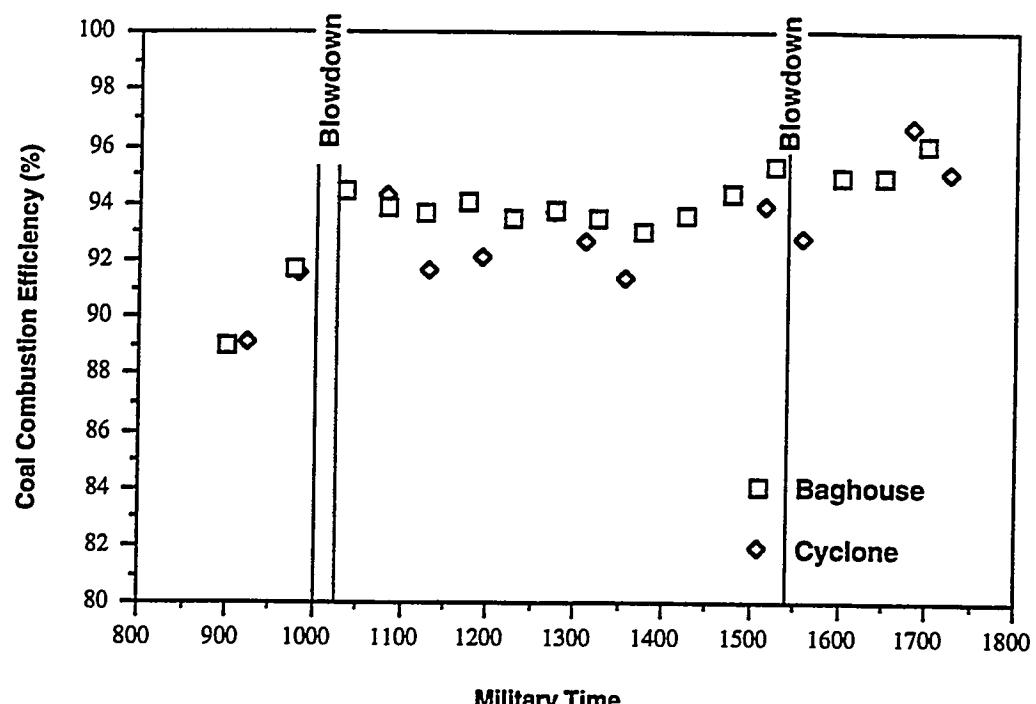
(a)



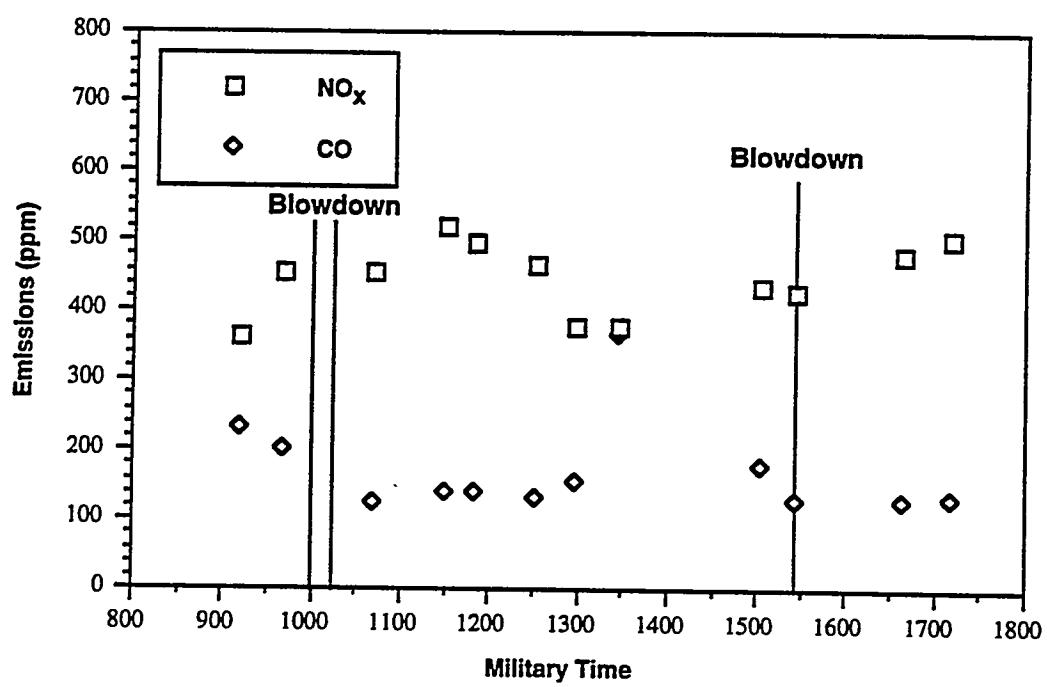
Military Time

(b)

**Figure 16. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 08/23/95**

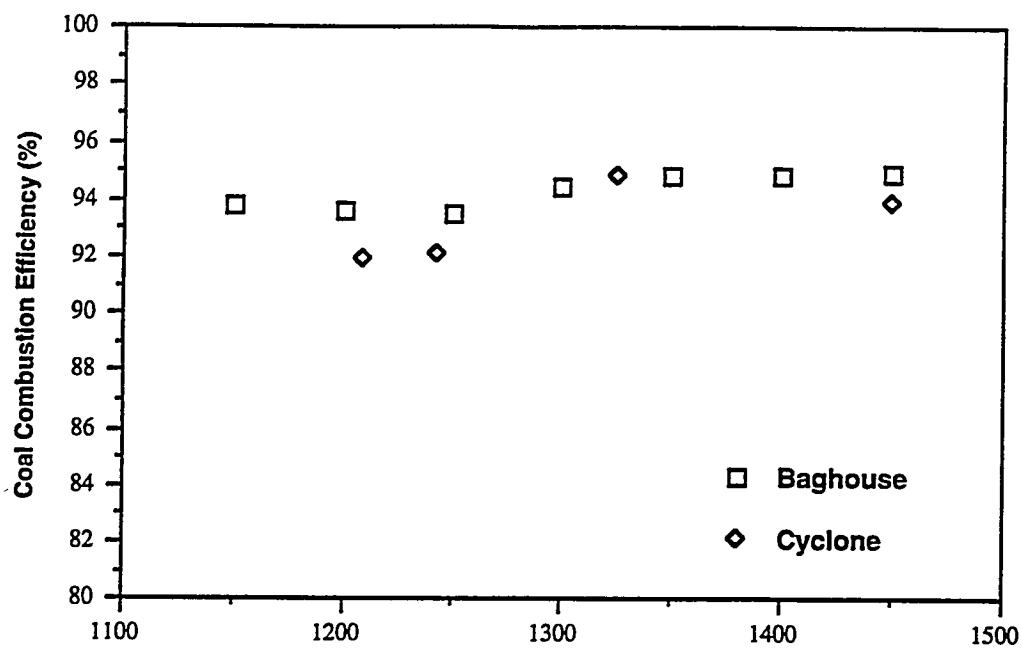


(a)

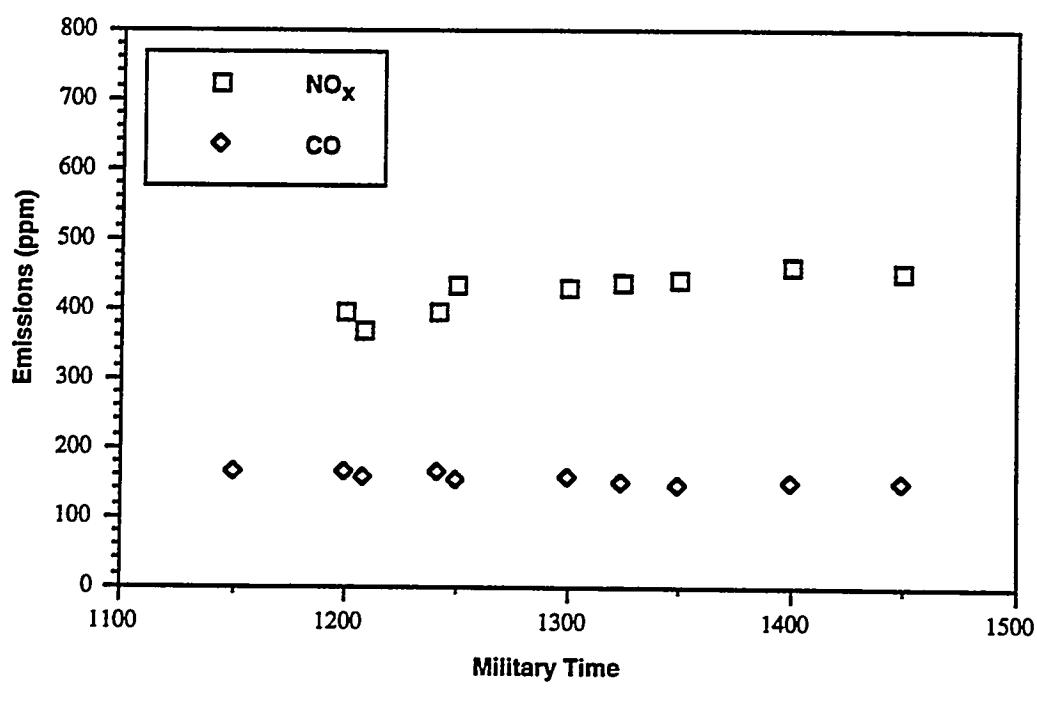


(b)

**Figure 17. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 08/24/95**

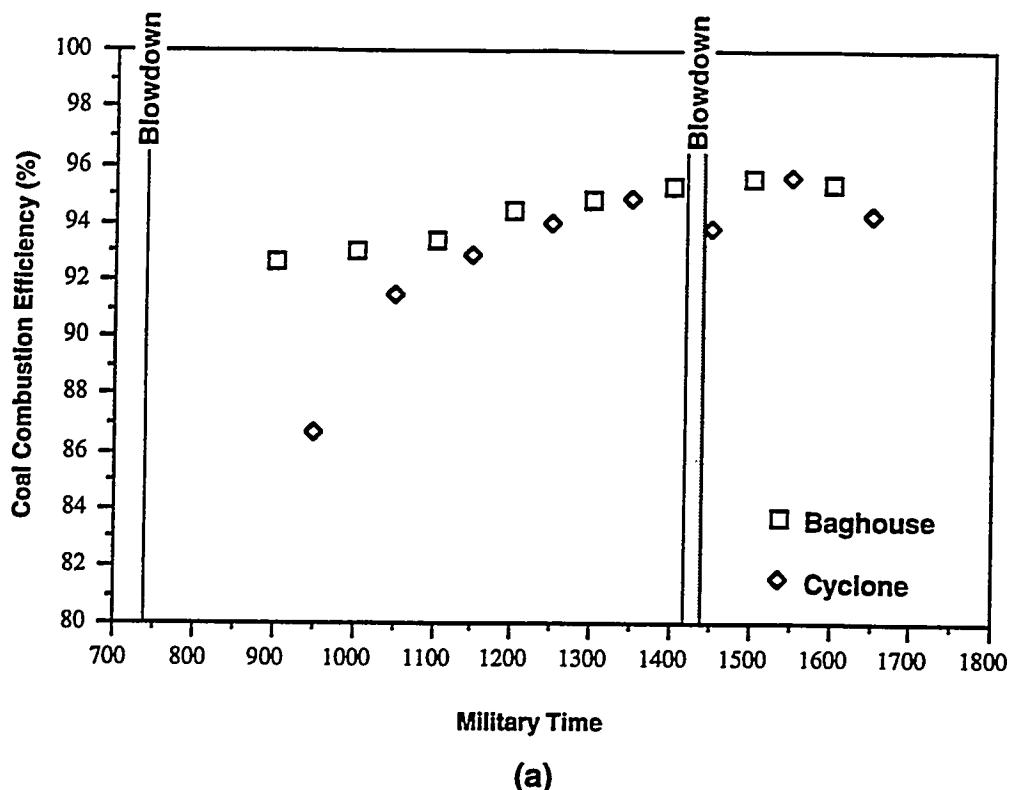


(a)

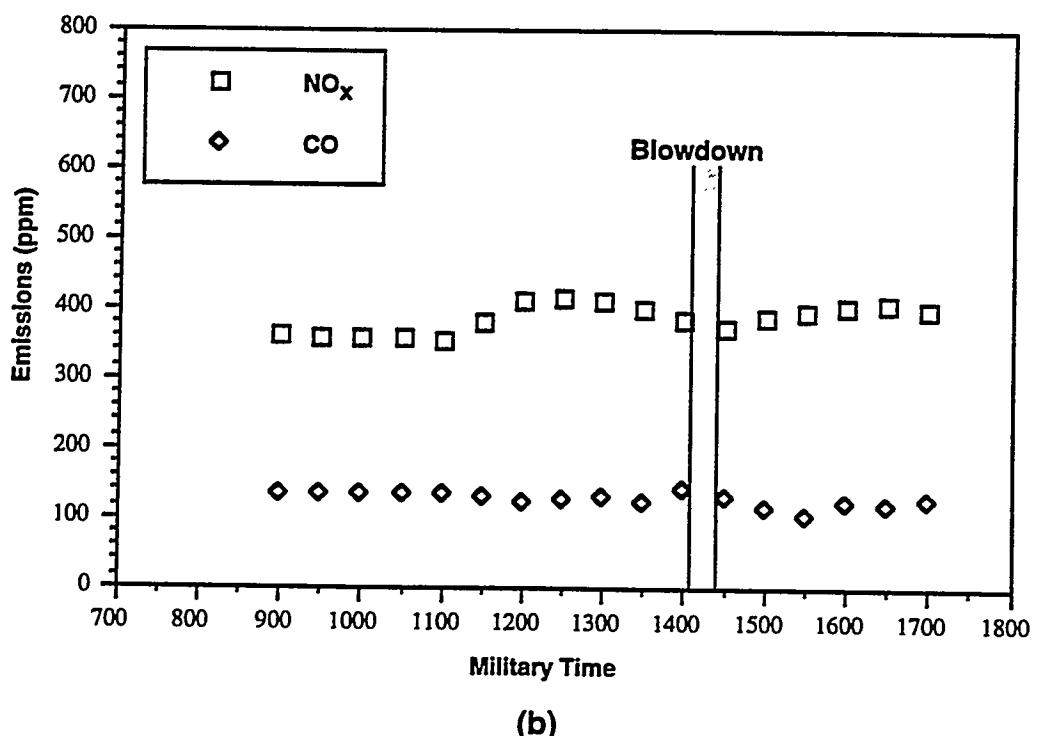


(b)

**Figure 18. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 08/25/95**

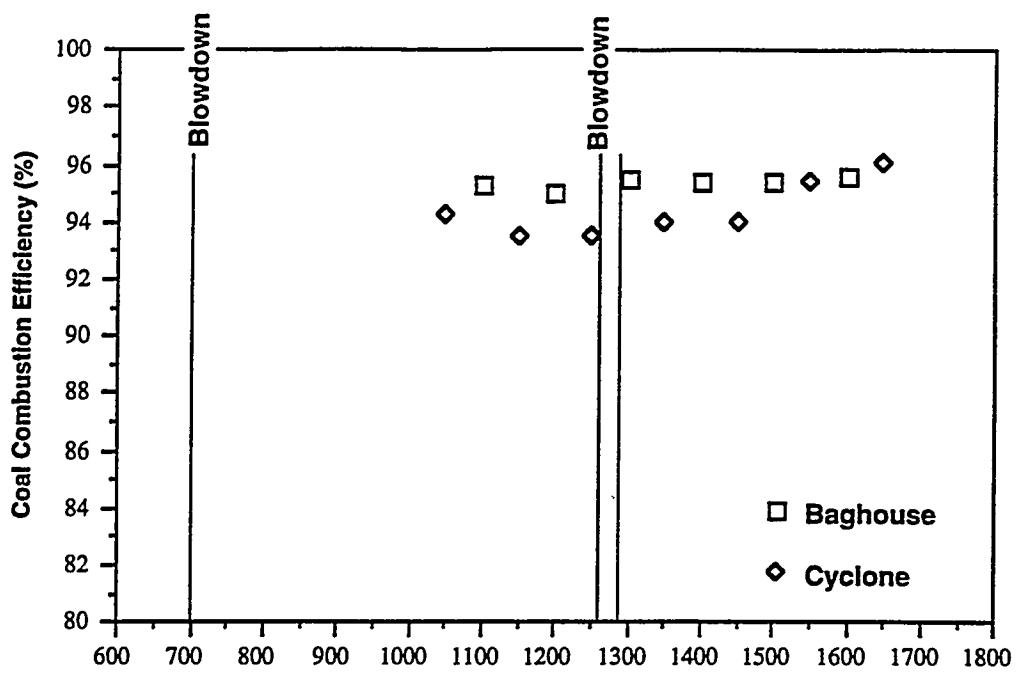


(a)

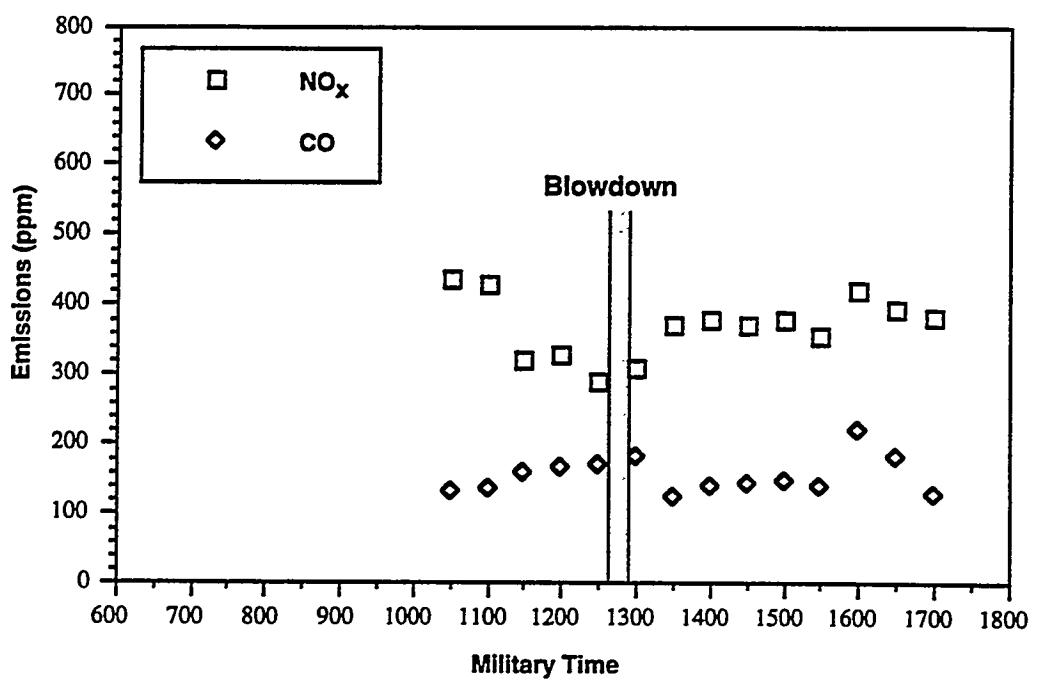


(b)

**Figure 19. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 08/28/95**

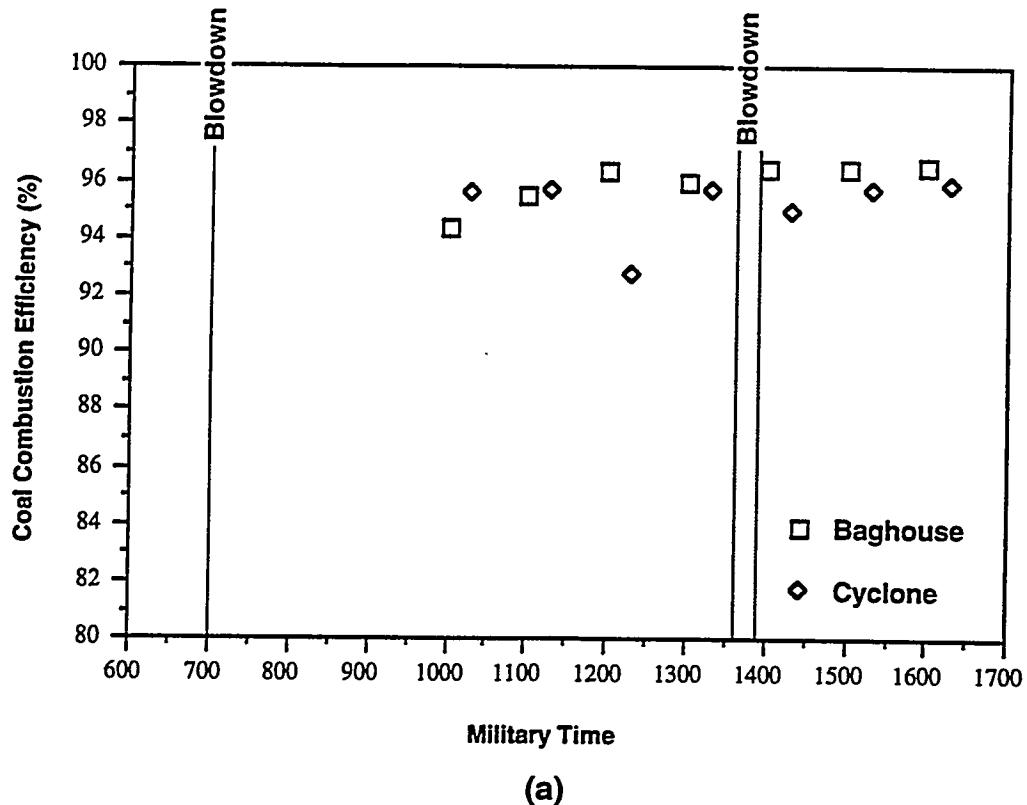


(a)

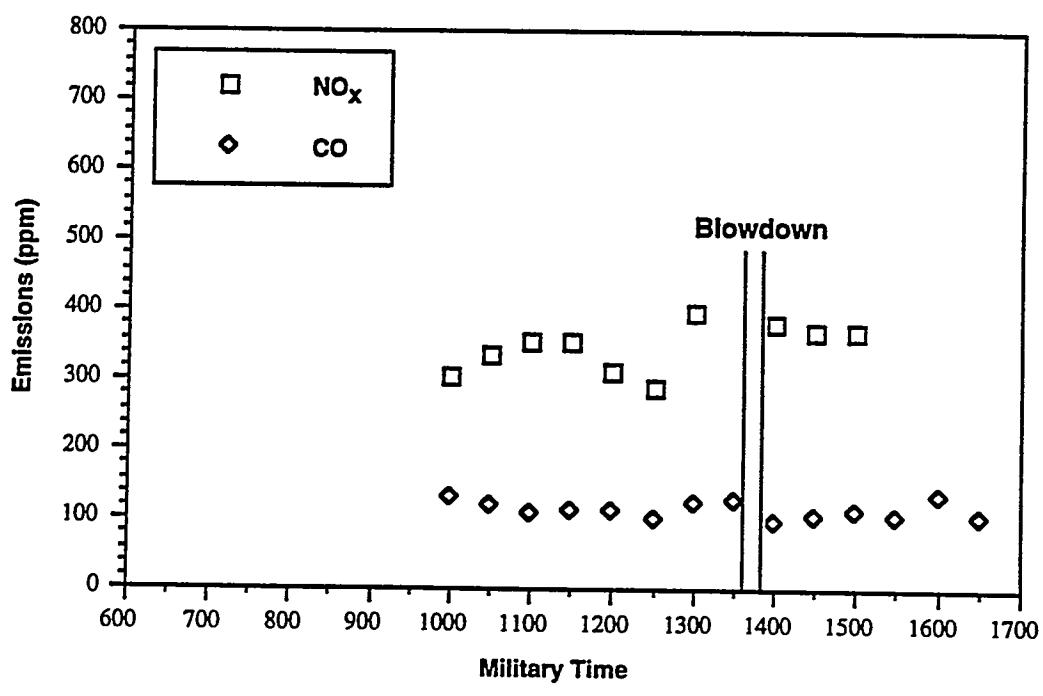


(b)

**Figure 20. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 08/29/95**

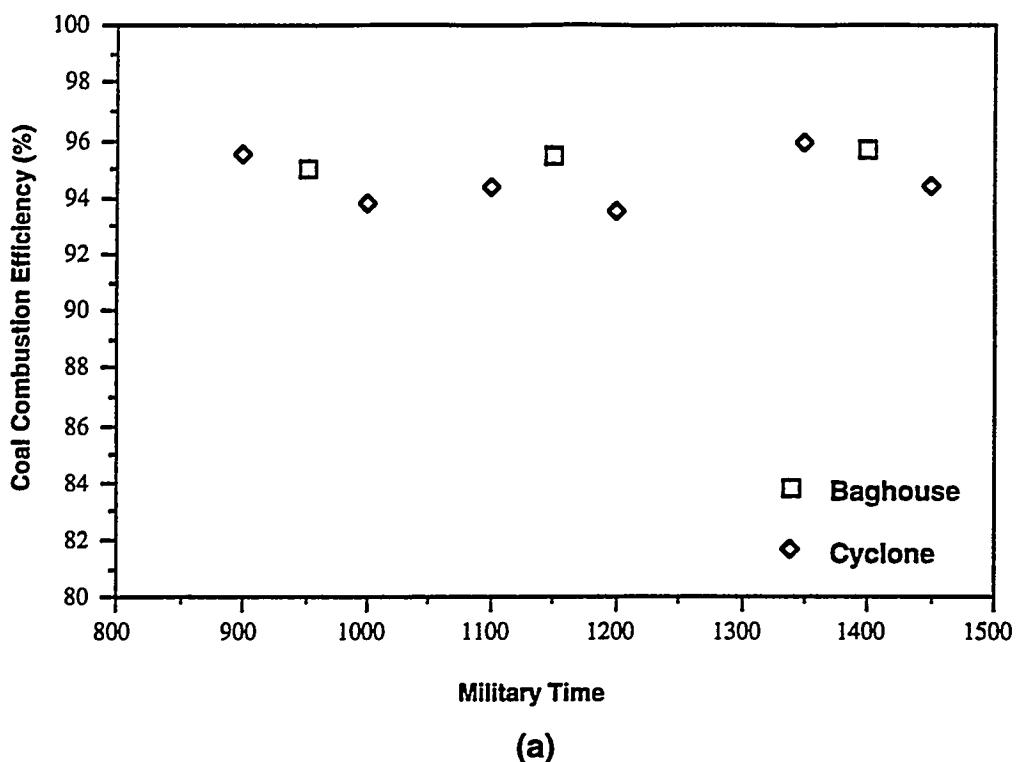


(a)

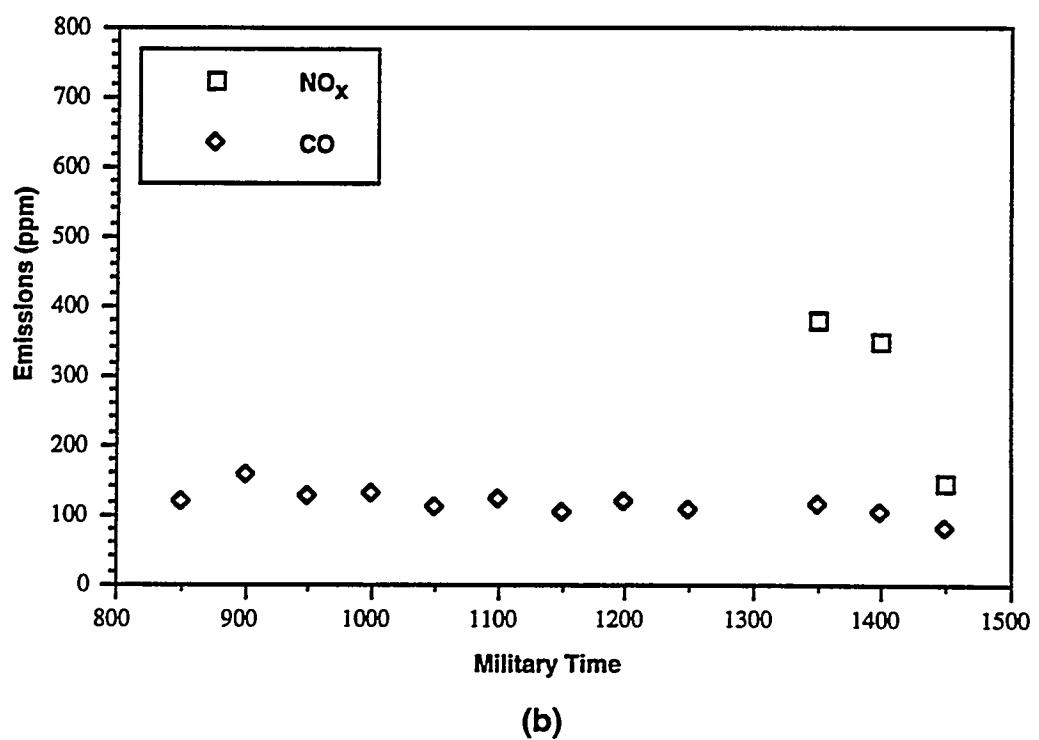


(b)

**Figure 21. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 08/30/95**

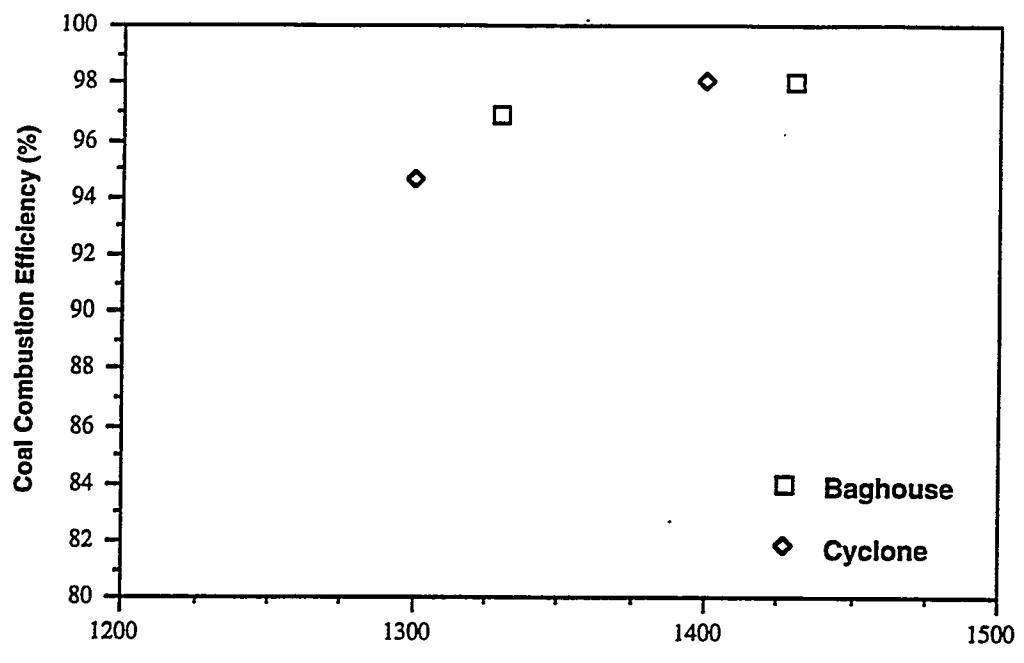


(a)

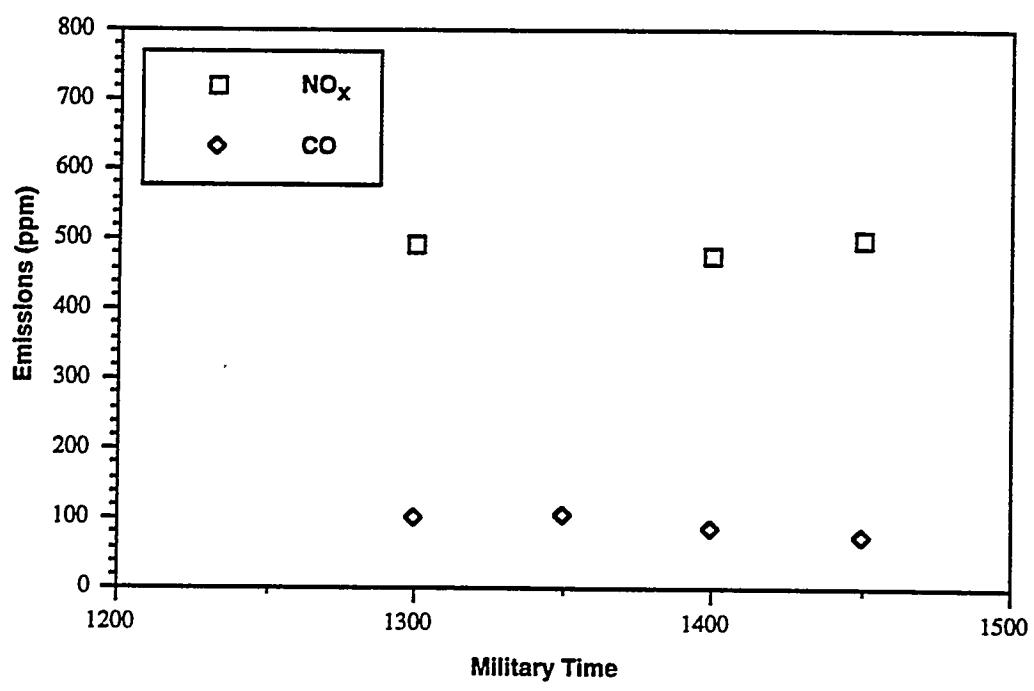


(b)

**Figure 22. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 08/31/95**

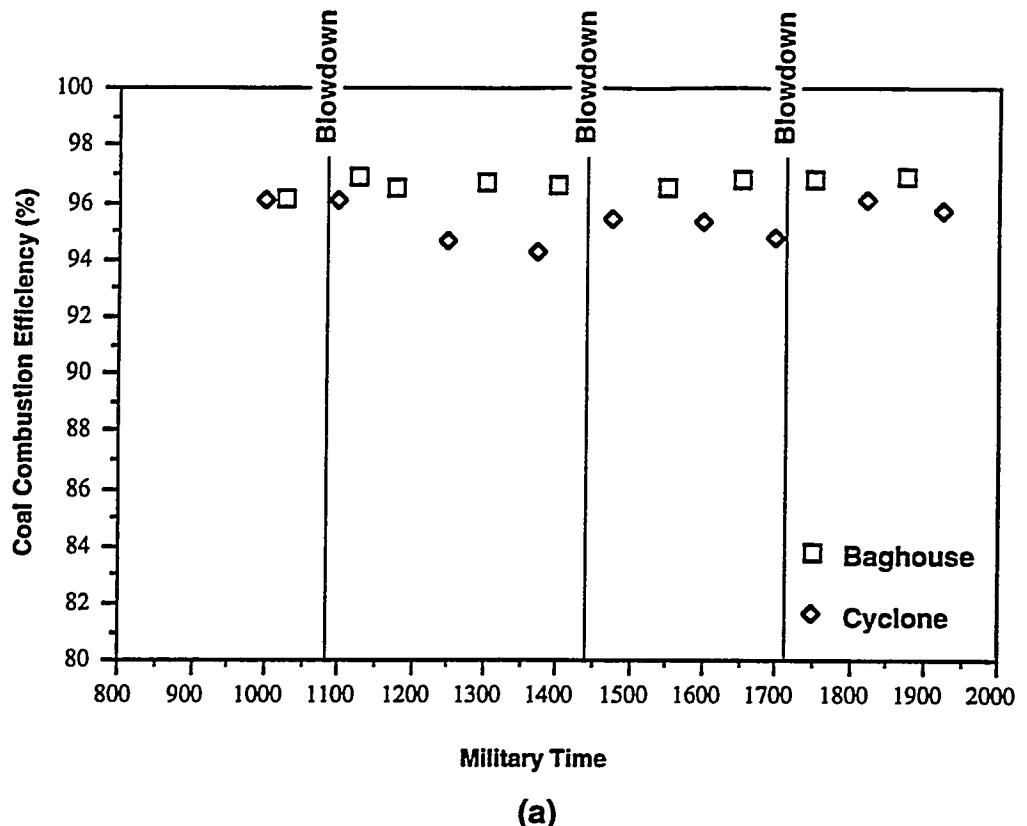


(a)

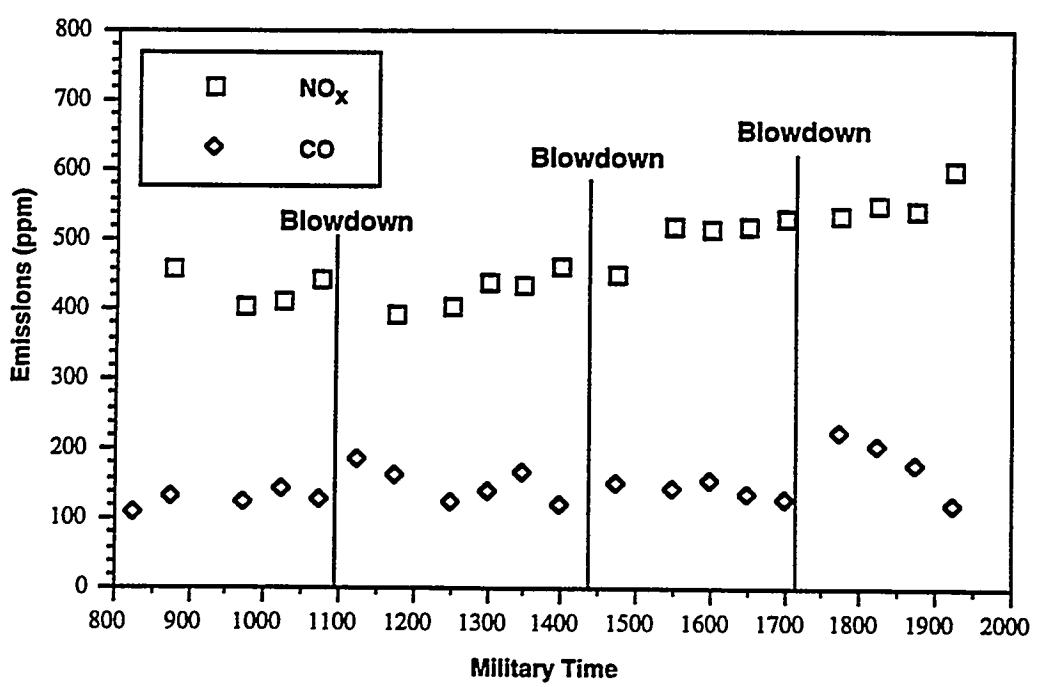


(b)

**Figure 23. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 09/05/95**

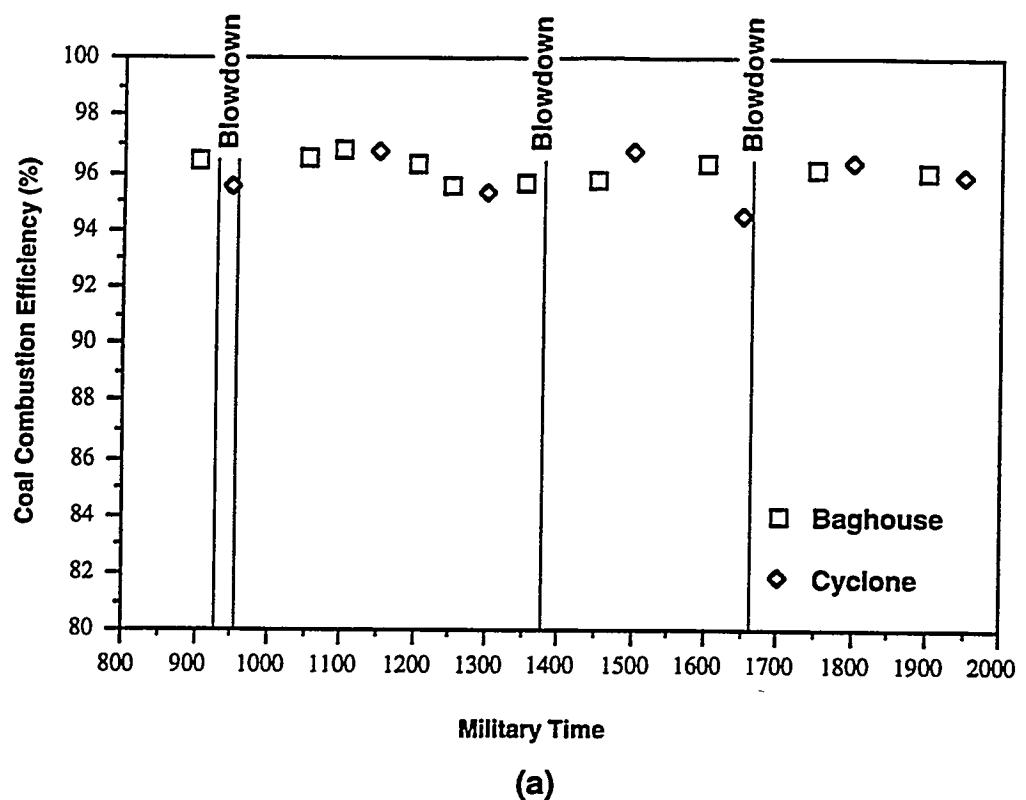


(a)

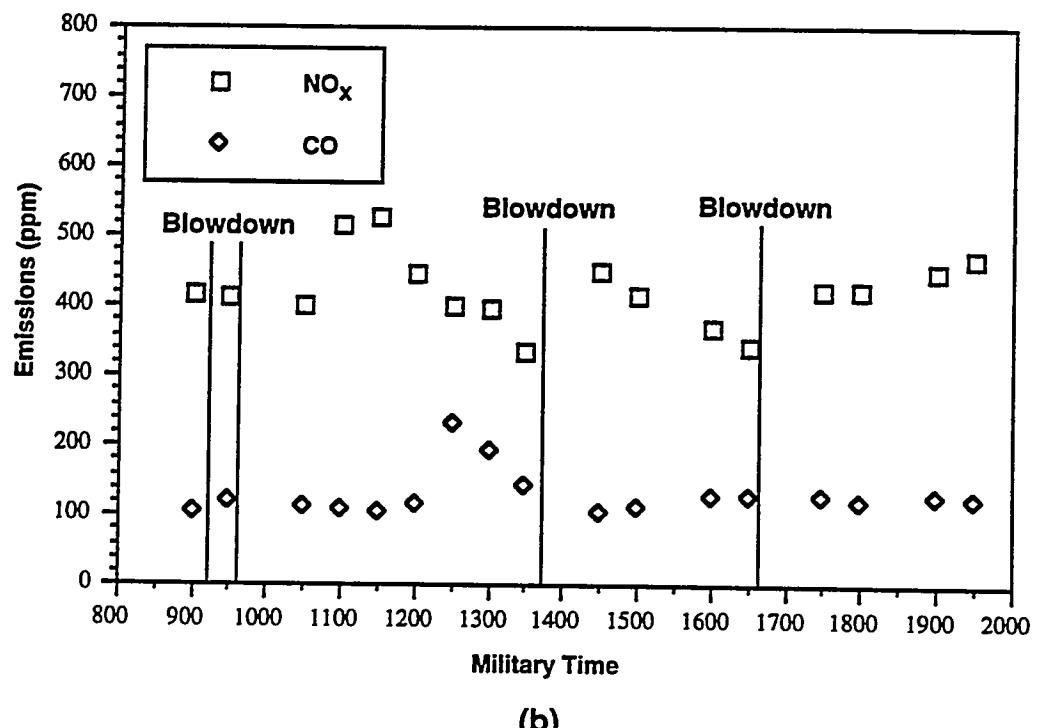


(b)

Figure 24. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 09/06/95

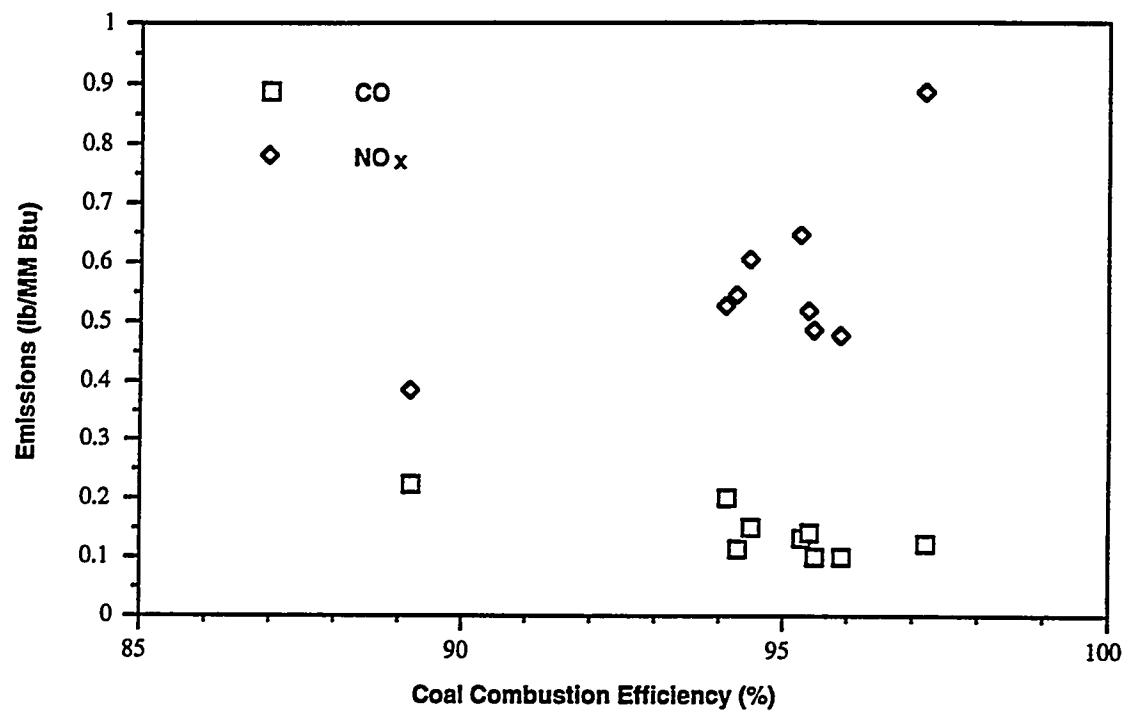


(a)

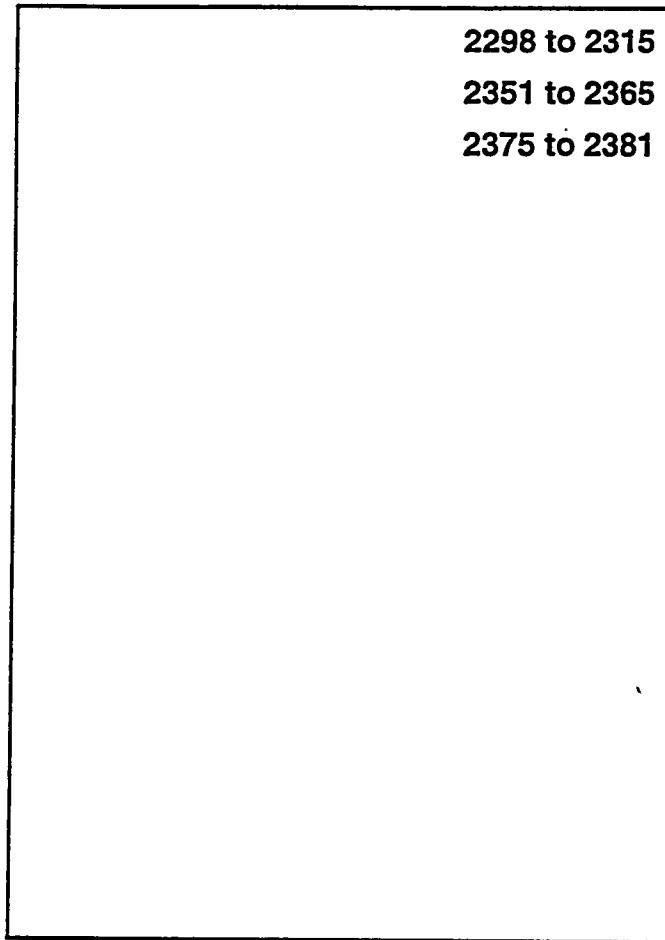


(b)

**Figure 25. COAL COMBUSTION EFFICIENCY (a) AND EMISSIONS (b)  
AS A FUNCTION OF TIME FOR THE TESTING ON 09/07/95**



**Figure 26. RELATIONSHIP BETWEEN COAL COMBUSTION EFFICIENCY AND CO AND NO<sub>x</sub> EMISSIONS FOR THE STEADY-STATE TESTING LISTED IN TABLE 3**



**CONVECTIVE  
PASS  
ENTRANCE**

**BURNER**

**Figure 27. GAS TEMPERATURES (°F) IN THE DEMONSTRATION BOILER  
WHEN FIRING MICRONIZED COAL ON 08/30/95**

	1845	2229	2316	
2071	2053	2229		CONVECTIVE PASS ENTRANCE
2177		2143	2247	
	2195	2229	2316	
1961	2229	2264		
1905	2036	2281		
				BURNER

**Figure 28. GAS TEMPERATURES (°F) IN THE DEMONSTRATION BOILER  
WHEN FIRING MICRONIZED COAL ON 08/31/95**

## **Appendix A. Boiler Efficiency Spreadsheets**

### **Natural Gas Baseline Tests**

#### Test Dates

07/25/95 -- 75% load, 1% O<sub>2</sub>

07/25/95 -- 75% load, 2% O<sub>2</sub>

07/25/95 -- 75% load, 3% O<sub>2</sub>

07/26/95 -- 100% load

08/01/95 -- 50% load

### **Micronized Coal Tests**

#### Test Dates

08/09/95 -- Low-NO<sub>x</sub>

08/09/95 -- High Combustion Efficiency

08/23/95

08/24/95

08/25/95

08/28/95

08/30/95

08/31/95

09/05/95

A	B	C	D	E	F
1 Demonstration	Boiler Data				
2 Date of Operation	7/25/95 Natural Gas Baseline Testing - MEACC II				
3	100% Gas; Prim. Open, Sec. Open, Tent. 25% Open, Gas Gun -4", Coal Gun Out, 1% O2				
4 Pressures and Temperatures	Steam Data				
5					
6 Drum Steam Pressure (psig)	200 Enthalpy of Sat. Liq. (Btu/lb)	356			
7 Feed Water Temperature (°F)	207 Enthalpy of Feed Water (Btu/lb)	175 (Sat. liquid @ Feed water temp.)			
8 Steam Quality ( % )	99.5 Steam Production Rate (PPH)	12,411			
9 Gas Temp leaving Boiler (°F)	517 Blow down Rate (PPH)				
10 Gas Temp. Leaving Air Heater (°F)	349 Enthalpy of water vapor at Givg Temp (Btu/lb)	3,099			
11 Air Temp Entering Air Heater (°F)	182 Enthalpy of water at fuel inlet temp. (Btu/lb)	1174 (Sup. steam @ 1psi&gas lvg temp)			
12 Air Temp leaving Air Pre Heater (°F)	384 Enthalpy of vapor at fuel inlet temp. (Btu/lb)	42 (Sat. liq. @ mill inlet temp.)			
13 Air Temp Entering Boiler (°F)	365	1060 (Sat. vapor @ mill inlet temp.)			
14 Mill Inlet Temperature (°F)	74				
15 Mill air flow rate (lb/h)	0 Coal Firing Rate (lb/min)	567			
16 Burner Inlet temperature (°F)	79 Coal H.H. Value (Btu/lb)	0 Gas Firing Rate (Btu/h)			
17 FUEL DATA	Coal Moisture Content (%)	0 Gas Cal. Value (Btu/lb)			
18 Proximate Analysis		23,346			
19 Moisture (Wt%)	Ultimate Analysis (Wt%: d.b)				
20 Volatile Matter (Wt%)					
21 Fixed Carbon (Wt%)					
22 Ash (Wt%)					
23	Carbon	0 Methane	95.54		
24 HHV (Btu/lb: d.b)	Hydrogen	0 Ethane	2.48		
25	Nitrogen	0 Propane	0		
26	Sulfur	0 Butane	0.43		
27	Oxygen	0 Hydrogen Sulfide	0		
28	Ash	0 Carbon Dioxide	1.55		
29	Total	0 Nitrogen			
30 Flue Gas Analysis		Others			
31		Total	100		
32 Oxygen (%)		Moisture (wt%)	0.05		
33 Carbon Dioxide (%)	1.1				
34 Carbon Monoxide (PPM)	10.6 Ash in Dry Char/Refuse				
35 Sulfur Dioxide (PPM)	108 TOTAL CARBON CONVERSION				
36 Oxides of Nitrogen (PPM)	NA COAL CARBON CONVERSION				
37	43				
38					
39					
40					
41					
42					

A	B	C Summary of Boiler Performance	D	E	F
43					
44					
45	Date of Operation	7/25/95			
46	Total Firing Rate				
47	Gas Support (%)				
48	Excess air used (%)				
49					
50					
51	Boiler Operating Conditions				
52					
53					
54	Theoretical flue gas composition				
55	Carbon Dioxide	9.16			
56	Water vapor	18.18			
57	Oxygen	0.89			
58	Nitrogen	71.77			
59	Sulfur Dioxide (ppm)	0			
60	Total	100.00			
61	Boiler Efficiency Details				
62	Heat loss due to Dry gas (%)				
63	Heat loss due to unburned carbon				
64	Heat loss due to unburned carbon in dust				
65	Heat loss due to moisture in "as Fired Fuel"				
66	Heat loss due to moisture produced from burning hydrogen in fuel				
67	Heat loss due to moisture in combustion air				
68	Heat loss due to formation of carbon monoxide				
69	Heat loss due to radiation				
70	Heat loss due to steam drum blowdown				
71	Total Losses				
72	Heat Credits				
73	1. Heat supplied by duct burner to entering air				
74	2. Heat supplied by primary (transport) air				
75	BOILER EFFICIENCY (%)				
76					
77					
78					
79					
80					
81					
82					
83					

1	G	H	I	J	K	L	M	N	O	P	Q
2											
3											
4											
5	Fuel Gas Composition (Dry. Vol%)										
6	Methane	95.54	Density at 60°F (lb/cu ft)	0.04246	0.04056628						
7	Ethane	2.48		0.08029	0.00199119						
8	Propane	0		0.1196	0						
9	Butane	0.43		0.1582	0.00068026						
10	Hydrogen Sulfide	0		0.09109	0						
11	Carbon Dioxide	0		0.117	0						
12	Nitrogen	1.55		0.07439	0.00115305						
13	Total	100									
14			Density of N. gas (lb/cu ft) =	0.04439078							
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	0	As Fired Coal Composition (wt)								
23	Coal Heat Input(Btu/h)	0	Carbon	0.00							
24	Gas Heat Input (Btu/h)		Hydrogen	0.00							
25	Total Firing Rate	13237182	Nitrogen	0.00							
26	Gas Calorific Value (Btu/lb)	23346	Sulfur	0.00							
27	Gas Firing Rate (lb/h)	567	Oxygen	0.00							
28	Gas Support (% of Heat)	100.00	Ash	0.00							
29	Fraction of coal	0	Moisture	0							
30	Fraction of GAS	1	Total	0							
31			HHV								
32			Dry ash%	0							
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

G	H	I	J	K	L	M	N	O	P	Q
<b>43 Calculation of Air Requirement and Theoretical Products of Composition</b>										
44										
45										
46 Carbon= %C/(100-12) : 1 mole =				Theoretical Oxygen Requirement						
47 Hydrogen= %H/(100-2) : 0.5 mole =			0.06113197 moles							
48 Sulfur= %S/(100-32) : 1 mole =			0.05998862 moles							
49			0 moles							
50 Oxygen required= Sum of the 3			0.12112059 moles							
51 Oxygen available in the Fuel= %O/(100-32)			0							
52 Net Oxygen required =			0.12112059 moles							
53 Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =			0.57676472 moles/lb of as fired fuel							
54										
55										
<b>56 Calculation of Products of combustion</b>										
57										
58 Excess air used (%)			= 100(0.21*0.57676472/0.21)=							
59			4.93							
60 Actual Dry air Required (moles) = (1+E,A%) * total air required =										
61 dry air in lbs/lb of "as fired" fuel			0.60518525							
62			= moles of air*29.97 =							
63 Actual wet air used/lb of "as fired" fuel (assuming 60% RH and 80°F) =			18.137402							
64										
65			lbs of dry air * 1.0013							
66 Weight of products of combustion = Actual wet air used + weight of fuel			18.1609806							
67										
68 Actual weight of products =			lbs of fuel burned * Wt of Products/lb of fuel							
69										
70			19.1609806 lb/lb of fuel							
71										
72			10.864 lb of flue gas							
73										
74										
75										
76										
77										
78										
79										
80										
81										
82										
83										

R	S	T	U	V	W	X	Y	Z
<b>1 Calculation of Theoretical Composition of Products</b>								
2								
3								
4								
5 Carbon Dioxide	(= moles of carbon /lb of fuel)		0.06113197	Wet Flue Gas Composition (%)	9.16		Dry Flue Gas Comp. (%)	11.19
6 Water	(moles of water in fuel + moles of water in combustion air)		0.12131494		18.18			0.00
7 Oxygen			0.00596831		0.89			1.09
8 Nitrogen			0.47902356		71.77			87.71
9 Sulfur Dioxide			0		0			0.00
10 Total			0.66743879		100.00			100.00
11 Carbon Conversion	100 Carbon Conversion of Coal NA							
12	100.00							
13								
14 Boiler Efficiency	Calculations							
15								
16 These calculations are based on ASME PTC 4.1 using heat loss method								
17								
18 1. Pounds of dry gas per pound of "as fired" composite fuel								
19								
20 $W_g = (\% \text{ d.b.}) \cdot C_{\text{Efficiency}} \cdot (44.01 \text{ (CO}_2) + 32.00 \text{ (O}_2) + 28.01 \text{ (N}_2) + 28.01 \text{ (CO)} / 12.01 \text{ (CO}_2 + \text{CO}) + 12.01 \text{ (S)} / 32.07$								
21								
22	17.13060591 lb/lb of as fired fuel							
23								
24 1. Heat loss due to dry gas (%)	$L_{wg} = W_g \cdot 0.24 \cdot (\text{Gas lvg temp from air heater} - \text{mill inlet temp}) / \text{HHV} \cdot 100$							
25								
26	2. Heat loss due to unburned carbon							
27								
28	$L_{uc} = \% \text{ Carbon in the "as Fired Fuel"} \cdot (1 - \text{Comb. Efficiency}) \cdot 14,500$							
29								
30								
31	3. Heat loss due to moisture in dust							
32								
33	$L_{moisture} = \text{Moisture in Fuel} \cdot \text{Enthalpy of vapor at gas leaving temp} - \text{Enthalpy of water at mill inlet} / \text{HHV} \cdot 100$							
34								
35 4. Heat loss due to moisture in "as Fired Fuel"								
36								
37 $L_{ml} =$								
38								
39								
40								
41 5. Heat loss due to moisture produced from burning hydrogen in fuel								
42								

R	S	T	U	V	W	X	Y	Z
43 Lmh=	8.936 % hydrogen in "as fired" fuel	(Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV						
44								
45								
46 6. Heat loss due to moisture in combustion air	Theoretical lb of air required for complete combustion/lb of "as fired" fuel	$(11.52\% \text{ carbon}) + 34.57\% \text{ hydrogen} - \% \text{ oxygen}(8) + 4.32\% \text{ sulfur})/HHV =$						
47								
48								
49								
50								
51								
52 Actual dry air =	$(1 + \% \text{ Excess air}/100) \text{ lb/lb of "as fired" fuel}$	16.75 lb/lb of "as fired" fuel						
53								
54 Moisture in air =	$0.013 \text{ lb/lb of dry air}$ moisture in air • (enthalpy of water vapor leaving air heater enthalpy of vapor at mill inlet temp.)	$0.22842674 \text{ lbs/lb of "as fired" fuel}$						
55 Lma =								
56								
57								
58								
59 7. Heat loss due to formation of carbon monoxide	$\text{CO}/(\text{CO}_2 + \text{CO}) \cdot 10160 \cdot \text{Combustion Efficiency} \cdot \% \text{ carbon in "as fired fuel}$	0.03						
60 Lco =								
61								
62								
63 8. Heat loss due to radiation	$10 \exp(0.62 \cdot 0.42 \log Q)$	1.41						
64								
65								
66								
67								
68 Total Losses (%)							16.80 %	
69 HEAT CREDITS								
70								
71 1. Heat supplied by duct burner to entering air								
72 2. Heat supplied by primary (transport) air								
73								
74 Boiler Efficiency (%) =							83.14 %	
75								
76 Combustion Air Flow (%) =							10,092 lb/h	
77								
78								
79								
80								
81								
82								
83								

A	B	C	D	E	F
1 Demonstration	7/25/95 Natural Gas Baseline Testing - HFA:CC II				
2 Date of Operation	100% Gas/Plm. Open, Sec. Open, Tert. 25% Open, Gas Gun -4", Coal Gun Out, 2% O2				
3 Pressures and Temperatures					
4 Steam Data					
5					
6 Drum Steam Pressure (Psi)	200 Enthalpy of Sat. Lq. (Btu/lb)	356			
7 Feed Water Temperature (°F)	207 Enthalpy of Feed Water (Btu/lb)	175 (Sat. liquid @ Feed water temp.)			
8 Steam Quality (%)	99.5 Steam Production Rate (PPH)	12,387			
9 Gas Temp.Leaving Boiler (°F)	520 Blow down Rate (PPH)	3,099			
10 Gas Temp.Leaving Air Heater (°F)	351 Enthalpy of water vapor at Givg Temp (Btu/lb)	1175 (Sup. steam @ 1psia&gas lvg temp)			
11 Air Temp Entering Air Heater (°F)	179 Enthalpy of water at fuel inlet temp. (Btu/lb)	43 (Sat. lq. @ mill inlet temp.)			
12 Air Temp leaving Air Pre Heater (°F)	384 Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1060 (Sat. vapor @ mill inlet temp.)			
13 Air Temp Entering Boiler (°F)	364				
14 Mill Inlet Temperature (°F)	75				
15 Mill air flow rate (lb/h)	0 Coal Firing Rate (lb/min)	0 Gas Firing Rate (Btu/h)	567		
16 Burner Inlet temperature (°F)	79 Coal H.H. Value (Btu/lb)	0 Gas Cal. Value (Btu/lb)	23,346		
17 FUEL DATA	Coal Moisture Content (%)	0			
18 Proximate Analysis					
19 Moisture (Wt%)					
20 Volatile Matter (Wt%)					
21 Fixed Carbon (Wt%)					
22 Ash (Wt%)	Carbon	0 Methane	95.54		
23	Hydrogen	0 Ethane	2.48		
24 HHV (Btu/lb, d.b)	Nitrogen	0 Propane	0		
25	Sulfur	0 Butane	0.43		
26	Oxygen	0 Hydrogen Sulfide	0		
27	Ash	0 Carbon Dioxide	1.55		
28	Total	0 Nitrogen	0		
29		Others			
30 Flue Gas Analysis		Total	100		
31	Oxygen (%)	Moisture (wt%)	0.05		
32	Carbon Dioxide (%)				
33	Carbon Monoxide (PPM)				
34	Sulfur Dioxide (PPM)	10.2 Ash in Dry Char/Refuse	0		
35	Oxides of Nitrogen (PPM)	4.9 TOTAL CARBON CONVERSION	100.00		
36		NA CARBON CONVERSION	0.00		
37		4.4			
38					
39					
40					
41					
42					

A	B	C	D	E	F
43		Summary of Boiler Performance			
44					
45					
46	Date of Operation	7/25/95			
47					
48					
49					
50	Boiler Operating Conditions				
51					
52					
53					
54	Total Firing Rate	13.237182 MMBtu/h			
55	Gas Support (%)	100.00 %			
56	Excess air used (%)	9.96 %			
57					
58	Actual mass of products of combustion	11358.41111 lb/lb of "as fired" fuel			
59					
60	Theoretical flue gas composition	%			
61	Carbon Dioxide	8.78			
62	Water vapor	17.43			
63	Oxygen	1.73			
64	Nitrogen	72.07			
65	Sulfur Dioxide (ppm)	0			
66	Total	100.00			
67	Boiler Efficiency Details				
68					
69	1. Heat loss due to Dry gas (%)	5.05			
70	2. Heat loss due to unburned carbon	0.00			
71	3. Heat loss due to unburned carbon in dust	Negligible			
72	4. Heat loss due to moisture in "as Fired Fuel"	0.00			
73	5. Heat loss due to moisture produced from burning hydrogen in fuel	10.40			
74	6. Heat loss due to moisture in combustion air	0.12			
75	7. Heat loss due to formation of carbon monoxide	0.92			
76	8. Heat loss due to radiation	1.41			
77	9. Heat loss due to steam drum blowdown				
78	Total Losses	16.99			
79	Heat Credits				
80	1. Heat supplied by duct burner to entering air	-91.59 Btu/lb of "as fired fuel"			
81	2. Heat supplied by primary (transport) air	0.00 Btu/lb of "as fired fuel"			
82		16.99			
83	BOILER EFFICIENCY (%)	82.94			

1	G	H	I	J	K	L	M	N	O	P	Q
2											
3											
4	Fuel Gas Composition (Dry. Vol%)										
5											
6	Methane	95.54		0.04246	0.040566281						
7	Ethane	2.48		0.08029	0.00199119						
8	Propane	0		0.1196	0						
9	Butane	0.43		0.1502	0.00068026						
10	Hydrogen Sulfide	0		0.09109	0						
11	Carbon Dioxide	0		0.1117	0						
12	Nitrogen	1.55		0.07439	0.00115305						
13	Total	100									
14	Density of N <sub>2</sub> gas (lb/cu ft) =			0.04439078							
15											
16											
17											
18	Determination of Percent Gas Support										
19											
20											
21											
22	Coal Firing Rate (lb/h)	0									
23	Coal Heat Input(lb/h)	0									
24	Gas Heat Input (lb/h)										
25	Total Firing Rate	13237182									
26	Gas Calorific Value (Btu/lb)	23346									
27	Gas Firing Rate (lb/h)	567									
28	Gas Support (% of heat)	100.00									
29	Fraction of coal	0									
30	Fraction of GAS	1									
31											
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

G	H	I	J	K	L	M	N	O	P	Q
<b>4.3 Calculation of Air Requirement and Theoretical Products of Combustion</b>										
4.4										
4.5										
4.6	Carbon = %C/(100-12) * 1 mole =									
4.7	Hydrogen = %H/(100-2)*0.5 mole =									
4.8	Sulfur = %S/(100-32) * 1 mole =									
4.9										
5.0	Oxygen required = Sum of the 3 Oxygen available in the Fuel = %O/(100-32)									
5.1										
5.2	Net Oxygen required =									
5.3	Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =									
5.4										
5.5	0.57676472 moles/lb of as fired fuel									
5.6	Calculation of Products of combustion									
5.7										
5.8	Excess air used (%)									
5.9										
6.0	Actual Dry air Required (moles) = [(1+E,A%)*									
6.1	total air required =									
6.2	= moles of air*29.97 =									
6.3	Actual wet air used/lb of "as fired" fuel (assuming 60% RH and 80°F) =									
6.4										
6.5	=									
6.6	Actual wet air used = Actual wet air used + weight of fuel =									
6.7										
6.8	Actual weight of Products =									
6.9										
7.0										
7.1										
7.2										
7.3										
7.4										
7.5										
7.6										
7.7										
7.8										
7.9										
8.0										
8.1										
8.2										
8.3										

R	S	T	U	V	W	X	Y	Z
<b>1 Calculation of Theoretical Composition of Products</b>								
2								
3								
4								
5 Carbon Dioxide	(=moles of carbon /lb of fuel)		0.06113197	Wet Flue Gas Composition (%)		Dry Flue Gas Comp. (%)		
6 Water	(moles of water in fuel + moles of water in combustion air)		0.1213778	8.78	10.63			
7			0.01206692	17.43	0.00			
8 Oxygen			0.50196596	1.73	2.10			
9 Nitrogen			0.69654265	72.07	87.27			
10 Sulfur Dioxide			0	0	0.00			
11 Total			100	100.00	100.00			
12 Carbon Conversion	Carbon Conversion of Coal NA							
13	100.00							
14 Boiler Efficiency	Efficiency Calculations							
15								
16 These calculations are based on ASME PTC 4.1 using heat loss method								
17								
18 1. Pounds of dry gas per pound of "as fired" composite fuel								
19								
20 $Wg = ((C\% \text{ db}) + C \text{ Efficiency}) / (44.01 \text{ (CO}_2) + 32.00 \text{ (O}_2) + 28.02 \text{ (N}_2) + (28.01 \text{ (CO)} / 12.01 \text{ (CO}_2 + \text{CO})) + 12.01 \text{ (S)} / 32.07$								
21								
22	17.7975154 lb/lb of as fired fuel							
23								
24 1. Heat loss due to dry gas (%)	$Lwg = Wg * 0.24 * (\text{Gas Ig temp from air heater} - \text{mill inlet temp}) / \text{HHV} * 100$							
25								
26								
27 2. Heat loss due to unburned carbon	% Carbon in the "as fired Fuel" * (1-Comb. Efficiency) * 14.500							
28								
29 $Luc = % \text{ Carbon in the "as fired Fuel"} * (1-\text{Comb. Efficiency}) * 14.500$								
30								
31								
32 3. Heat loss due to unburned carbon in dust	Negligible							
33								
34 4. Heat loss due to moisture in "as Fired Fuel"								
35								
36	Moisture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet) / HHV * 100							
37 $Lmf =$								
38								
39								
40								
41 5. Heat loss due to moisture produced from burning hydrogen in fuel	$0.00 =$							
42								

R	S	T	U	V	W	X	Y	Z
43 Lmh=	8.936 *% hydrogen in "as fired" fuel* (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV					10.40		
44	-							
45	-							
46 6. Heat loss due to moisture in combustion air	Theoretical lb of air required for complete combustion/lb of "as fired" fuel							
47	$(11.52\% \text{ carbon} + 34.57\% \text{ hydrogen} - \% \text{ oxygen})/8 + 4.32 (\% \text{ sulfur})/\text{HHV} =$							
48	$(11.52\% \text{ carbon} + 34.57\% \text{ hydrogen} - \% \text{ oxygen})/8 + 4.32 (\% \text{ sulfur})/\text{HHV} =$							
49								
50								
51								
52 Actual dry air =	$(1+\%) \text{ Excess air}/100 \text{ lb/lb of "as fired" fuel}$							
53	18.41 lb							
54 Moisture in air =	$0.013 \text{ lb/lb of dry air} \cdot (\text{enthalpy of water vapor leaving air heater} - \text{enthalpy of vapor at mill inlet temp.})$							
55 Lma =								
56								
57								
58								
59 7. Heat loss due to formation of carbon monoxide	$\text{CO}/(\text{CO}_2 + \text{CO}) \cdot 10160 \cdot \text{Combustion Efficiency}^* \% \text{ carbon in "as fired fuel"}$							
60 Lco =								
61								
62								
63 8. Heat loss due to radiation	$10 \exp(0.62 - 0.42 \log Q)$							
64								
65								
66								
67								
68 Total Losses (%)								
69 HEAT CREDITS								
70								
71 1. Heat supplied by duct burner to entering air								
72 2. Heat supplied by primary (transport) air								
73								
74 Boiler Efficiency (%) =								
75								
76 Combustion Air Flow (%) =								
77								
78								
79								
80								
81								
82								
83								

$0.23938825 \text{ lbs/lb of "as fired" fuel}$   
 $-91.59 \text{ Btu/lb of "as Fired" Fuel}$   
 $0.00 \text{ Btu/lb of "as Fired" Fuel}$

0.12

0.02

1.41

16.99 %

82.94 %

10,577 lb/h

A	B	C	D	E	F
1 Demonstration	7/25/95 Natural Gas Baseline Testing - IMACC II				
2 Date of Operation	100% Gas; Prim. Open, Sec. Open, Tent. 25% Open, Gas Gun -4", Coal Gun Out, 3% O2				
3 Pressures and Temperatures	Steam Data				
4					
5					
6 Drum Steam Pressure (Psig)	199 Enthalpy of Sat. Liq. (Btu/lb)	355			
7 Feed Water Temperature (°F)	206 Enthalpy of Feed Water (Btu/lb)	175 (Sat. liquid @ Feed water temp.)			
8 Steam Quality ( % )	99.5 Steam Production Rate (PPH)	12,404			
9 Gas Temp.Leaving Boiler (°F)	525 Blow down Rate (PPH)	3,093			
10 Gas Temp. Leaving Air Heater (°F)	354 Enthalpy of water vapor at Gvg Temp (Btu/lb)	1176 (Sup. steam @ 1psia&gas lvg temp)			
11 Air Temp Entering Air Heater (°F)	175 Enthalpy of water at fuel inlet temp. (Btu/lb)	53 (Sat. liq. @ mill inlet temp.)			
12 Air temp leaving Air Pre Heater (°F)	383 Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1060 (Sat. vapor @ mill inlet temp.)			
13 Air Temp Entering Boiler (°F)	363				
14 Mill Inlet Temperature (°F)	85				
15 Mill air flow rate (lb/h)	0 Coal Firing Rate (lb/min)	567			
16 Burner inlet temperature (°F)	79 Coal H.H. Value (Btu/lb)	23,346			
17 FUEL DATA	Coal Moisture Content (%)				
18 Proximate Analysis	Ultimate Analysis (Wt%, d.b)				
19 Moisture (Wt%)	Carbon	0 Methane	95.54		
20 Volatile Matter (Wt%)	Hydrogen	0 Ethane	2.48		
21 Fixed Carbon (Wt%)	Nitrogen	0 Propane	0		
22 Ash (Wt%)	Sulfur	0 Butane	0.43		
23	Oxygen	0 Hydrogen Sulfide	0		
24 HHV (Btu/lb, d.b)	Ash	0 Carbon Dioxide	1.55		
25	Total	0 Nitrogen			
26		Others			
27		Total	100		
28		Moisture (wt%)	0.05		
29					
30 Flue Gas Analysis					
31					
32 Oxygen (%)	3.1				
33 Carbon Dioxide (%)	9.6 Ash in Dry Char/Refuse				
34 Carbon Monoxide (PPM)	45 TOTAL CARBON CONVERSION	0			
35 Sulfur Dioxide (PPM)	NA CARBON CONVERSION	100.00			
36 Oxides of Nitrogen (PPM)	44	0.00			
37					
38					
39					
40					
41					
42					

A	B	C	D	E	F
43		Summary of Boiler Performance			
44					
45					
46 Date of Operation	7/25/95				
47					
48					
49					
50					
51 Boiler Operating Conditions					
52					
53					
54 Total Firing Rate			13.237182 MMBtu/h		
55 Gas Support (%)			100.00 %		
56 Excess air used (%)			15.53 %		
57					
58 Actual mass of products of combustion			11904.65983 lb/lb of "as fired" fuel		
59					
60 Theoretical flue gas composition					
61 Carbon Dioxide	%	9.39			
62 Water vapor		16.67			
63 Oxygen		2.58			
64 Nitrogen		72.36			
65 Sulfur Dioxide (ppm)		0			
66 Total		100.00			
67 Boiler Efficiency Details					
68					
69 1. Heat loss due to Dry gas (%)			5.22		
70 2. Heat loss due to unburned carbon			0.00		
71 3. Heat loss due to unburned carbon in dust			Negligible		
72 4. Heat loss due to moisture in "as Fired Fuel"			0.00		
73 5. Heat loss due to moisture produced from burning hydrogen in fuel			10.31		
74 6. Heat loss due to moisture in combustion air			0.12		
75 7. Heat loss due to formation of carbon monoxide			0.01		
76 8. Heat loss due to radiation			1.41		
77 9. Heat loss due to steam drum blowdown			0.00		
78 Total Losses			17.08		
79 Heat Credits					
80 1. Heat supplied by duct burner to entering air					
81 2. Heat supplied by primary (transport) air					
82					
83 BOILER EFFICIENCY (%)					
			82.84		

1	G	H	I	J	K	L	M	N	O	P	Q
2											
3											
4											
5	Fuel Gas Composition (Dy. Vol%)	95.54	Density at 60°F (lb/cu.ft)	0.04246	Gas Composition from Volume % to Wt%	lbs in each Cu.ft of gas					
6	Methane	2.48		0.04056628							
7	Ethane	0		0.08029	0.00199119						
8	Propane	0.43		0.1196	0						
9	Butane	0.43		0.1582	0.00068026						
10	Hydrogen Sulfide	0		0.09109	0						
11	Carbon Dioxide	0		0.117	0						
12	Nitrogen	1.55		0.07439	0.00115305						
13	Total	100									
14					Density of N. gas (lb/cu.ft) =	0.04439078					
15											
16											
17											
18					Determination of Percent Gas Support						
19											
20											
21	Coal Firing Rate (lb/h)	0			As Fired Coal Composition (Wt)						
22	Coal Heat Input(Btu/h)	0			Carbon	73.36					
23	Coal Heat Input(Btu/h)	0			Hydrogen	24.00					
24	Gas Heat Input (Btu/h)	13237182			Nitrogen	2.60					
25	Gas Heat Input (Btu/h)	13237182			Sulfur	0.00					
26	Total Firing Rate	23346			Oxygen	0.00					
27	Gas Calorific Value (Btu/lb)	567			Ash	0.00					
28	Gas Firing Rate (lb/h)	100.00			Moisture	0.05					
29	Gas Support (% of Heat)	0			Total	100.00					
30	Fraction of coal	1			HHV						
31	Fraction of GAS	0			Dry Ash	0					
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

	G	H	I	J	K	L	M	N	O	P	Q
4.3	Calculation of Air Requirement and Theoretical Products of Combustion										
4.4											
4.5											
4.6	Carbon = %C/(100*12) * 1 mole =				Theoretical Oxygen Requirement						
4.7	Hydrogen = %H/(100*2) * 0.5 mole =				0.06113197 moles						
4.8	Sulfur = %S/(100*32) * 1 mole =				0.05998862 moles						
4.9					0 moles						
5.0	Oxygen required = Sum of the 3 Oxygen available in the Fuel = %O/(100*32)				0.12112059 moles						
5.1					0						
5.2	Net Oxygen required =				0.12112059 moles						
5.3	Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =				0.57676472 moles/lb of as fired fuel						
5.4											
5.5											
5.6	Calculation of Products of combustion										
5.7											
5.8	Excess air used (%)				= 100(0.21/0.21*0.57676472)=						
5.9					15.53						
6.0	Actual Dry air Required (moles) = (1+E,A%) * total air required =										
6.1	Dry air in lbs/lb of "as fired" fuel										
6.2											
6.3	Actual wet air used/lb of "as fired" fuel (assuming 60% R.H and 80°F) =										
6.4											
6.5											
6.6	Weight of products of combustion = Actual wet air used + weight of fuel										
6.7											
6.8	Actual weight of products =										
6.9											
70					lbs of fuel burned * Wt of Products/lb of fuel						
71											
72											
73											
74											
75											
76											
77											
78											
79											
80											
81											
82											
83											

R	S	T	U	V	W	X	Y	Z
<b>1 Calculation of Theoretical Composition of Products</b>								
2	-	-	-	-	-	-	-	-
3	-	-	-	-	-	-	-	-
4	-	-	-	-	-	-	-	-
5 Carbon Dioxide 6 Water 7 Oxygen 8 Nitrogen 9 Sulfur Dioxide 10 Total 11 Total 12 Carbon Conversion 13 - 14 Boiler 15 -	(=moles of carbon /lb of fuel) ( moles of water in fuel +moles of water in combustion air)	-	0.06113197 0.12144729 0.01880872 0.52732796 0 0.72871594	8.39 16.67 2.58 72.36 0 100.00	Dry Flue Gas Comp. (%) 10.07 0.00 3.10 86.84 0.00 100.00	-	-	-
16 These calculations are based on ASME PTC 4, using heat loss method	-	-	-	-	-	-	-	-
17	1. Pounds of dry gas per pound of "as fired" composite fuel	-	-	-	-	-	-	-
18	Wg = ((c% d.b) * C.Efficiency *(44.01 *(CO2) + 32.00 *(O2) + 28.02 *(N2) + (28.01 *(CO)/12.01 *(CO2+CO)) + 12.01 *(S)/32.07	-	-	-	-	-	-	-
19	21 18.87437722 lb/lb of as fired fuel	-	-	-	-	-	-	-
20	22 1. Heat loss due to dry gas (%)	Lwg = Wg * 0.24 * (Gas lg temp from air heater - mill inlet temp)/HHV *100	-	-	-	-	-	-
21	23 2. Heat loss due to unburned carbon	-	-	-	-	-	-	-
22	24 3. Heat loss due to moisture in "as Fired Fuel"	-	-	-	-	-	-	-
23	25 4. Heat loss due to moisture in water at mill inlet/HHV*100	Moisture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet)/HHV*100	-	-	-	-	-	-
24	26 5. Heat loss due to moisture produced from burning hydrogen in fuel	= 0.00	-	-	-	-	-	-
25	27	-	-	-	-	-	-	-
26	28	-	-	-	-	-	-	-
27	29	-	-	-	-	-	-	-
28	30	-	-	-	-	-	-	-
29	31	-	-	-	-	-	-	-
30	32	-	-	-	-	-	-	-
31	33	-	-	-	-	-	-	-
32	34	-	-	-	-	-	-	-
33	35	-	-	-	-	-	-	-
34	36	-	-	-	-	-	-	-
35	37	-	-	-	-	-	-	-
36	38	-	-	-	-	-	-	-
37	39	-	-	-	-	-	-	-
38	40	-	-	-	-	-	-	-
39	41	-	-	-	-	-	-	-
40	42	-	-	-	-	-	-	-

R	S	T	U	V	W	X	Y	Z
43 Lmfh=	8.936 % hydrogen in "as fired" fuel" [Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp]/HHV							10.31
44								
45								
46 6. Heat loss due to moisture in combustion air	Theoretical lb of air required for complete combustion/lb of "as fired" fuel = $(11.52\% \text{ carbon}) + 34.57\% \text{ hydrogen} - \% \text{ oxygen}/81 + 4.32\% \text{ sulfur}/1111V =$							
47								
48								
49								
50								
51								
52 Actual dry air =	(1+ % Excess air/100) lb/lb of "as fired" fuel							
53								
54 Moisture in air =	0.013 lb/lb of dry air							
55								
56								
57								
58								
59 7. Heat loss due to formation of carbon monoxide	CO/(CO <sub>2</sub> +CO)*10 <sup>60</sup> * Combustion Efficiency * % carbon in "as fired fuel" =							
60								
61								
62								
63 8. Heat loss due to radiation	10 exp (0.62-0.42 log Q)							
64								
65								
66								
67								
68 Total Losses (%)								
69 HEAT CREDITS								
70								
71 1. Heat supplied by duct burner to entering air								
72 2. Heat supplied by primary (transport) air								
73								
74 Boiler Efficiency (%) =								
75								
76 Combustion Air Flow (%) =								
77								
78								
79								
80								
81								
82								
83								

$$\begin{aligned} & \cdot 96.23 \text{ Btu/lb of "as Fired" Fuel} \\ & 0.00 \text{ Btu/lb of "as Fired" Fuel} \\ & 82.84 \% \end{aligned}$$

11,112 lb/h

A	B	C	D	E	F
<b>1 Demonstration</b>		<b>Boiler Data</b>			
2 Date of Operation	7/26/95	Natural Gas Baseline Testing - HEACC II			
3 Pressures and Temperatures	100% Gas; Prim. Open, Sec. Open, Tert. Open, Gas Gun +4", Coal Gun Out, 1.5% O2				
4		Steam Data			
5					
6 Drum Steam Pressure (Psig)	20.4	Enthalpy of Sat. Liq. (Btu/lb)	357		
7 Feed Water Temperature (°F)	21.7	Enthalpy of Feed Water (Btu/lb)	1.85	(Sat. liquid @ Feed water temp.)	
8 Steam Quality (%)	100.23	Steam Production Rate (PPH)	15,659		
9 Gas Temp. Leaving Boiler (°F)	57.6	Blow down Rate (PPH)	3,128		
10 Gas Temp. Leaving Air Heater (°F)	39.0	Enthalpy of water vapor at Givg Temp (Btu/lb)	1192	(Sup. steam @ 1psi&gas lvg temp)	
11 Air Temp Entering Air Heater (°F)	17.3	Enthalpy of water at fuel inlet temp. (Btu/lb)	59	(Sat. liq. @ mill inlet temp)	
12 Air temp leaving Air Pre Heater (°F)	40.9	Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1060	(Sat. vapor @ mill inlet temp)	
13 Air Temp Entering Boiler (°F)	39.1				
14 Mill Inlet Temperature (°F)	9.1				
15 Mill air flow rate (lb/min)	0	Coal Firing Rate (lb/min)	0	Gas Firing Rate (Btu/h)	732
16 Burner inlet temperature (°F)	89	Coal H.H. Value (Btu/lb)	0	Gas Cal. Value (Btu/lb)	23,346
17 FUEL DATA		Coal Moisture Content (%)	0		
18 Proximate Analysis					
19 Moisture (Wt%)		Ultimate Analysis (Wt%, d.b)		Gas Analysis (Dry Vol%)	
20 Volatile Matter (Wt%)				Methane	95.54
21 Fixed Carbon (Wt%)				Ethane	2.48
22 Ash (Wt%)				Propane	0
23		Carbon	0	Bulane	0.43
24 HHV (Btu/lb, d.b)		Hydrogen	0	Hydrogen Sulfide	0
25		Nitrogen	0	Carbon Dioxide	1.55
26		Sulfur	0	Nitrogen	
27		Oxygen	0	Others	
28		Ash	0	Total	100
29		Total	0	Moisture (wt%)	0.05
30 Flue Gas Analysis					
31 Oxygen (%)	1.5				
32 Carbon Dioxide (%)		Ash in Dry Char/Refuse	0		
33 Carbon Monoxide (PPM)		TOTAL CARBON CONVERSION	100.00		
34 Sulfur Dioxide (PPM)		NA CARBON CONVERSION	0.00		
35 Oxides of Nitrogen (PPM)		26			
36					
37					
38					
39					
40					
41					
42					

A	B	C	D	E	F
43	44	Summary of Boiler Performance			
45	46 Date of Operation	7/26/95			
47	48				
49	50				
51	Boiler Operating Conditions				
52	53				
54	Total Firing Rate	17.089272 MMBtu/h			
55	Gas Support (%)	100.00 %			
56	Excess air used (%)	6.94 %			
57	Actual mass of products of combustion =	14280.2447 lb/lb of "as fired" fuel			
58	Actual mass of products of combustion =				
59	60 Theoretical flue gas composition %				
61	Carbon Dioxide	9.00			
62	Water vapor	17.87			
63	Oxygen	1.24			
64	Nitrogen	71.89			
65	Sulfur Dioxide (ppm)	0			
66	Total	100.00			
67	Boiler Efficiency Details				
68	69 1. Heat loss due to Dry gas (%)	5.09			
70	2. Heat loss due to unburned carbon	0.00			
71	3. Heat loss due to unburned carbon in dust	Negligible			
72	4. Heat loss due to moisture in "as Fired Fuel"	0.00			
73	5. Heat loss due to moisture produced from burning hydrogen in fuel	10.41			
74	6. Heat loss due to moisture in combustion air	0.13			
75	7. Heat loss due to formation of carbon monoxide	0.01			
76	8. Heat loss due to radiation	1.27			
77	9. Heat loss due to steam drum blowdown	0.00			
78	Total Losses	16.91			
79	Heat Credits				
80	1. Heat supplied by duct burner to entering air	-80.16 Btu/lb of "as fired fuel"			
81	2. Heat supplied by primary (transport) air	0.00 Btu/lb of "as fired fuel"			
82					
83	BOILER EFFICIENCY (%)	83.03			

1	G	H	I	J	K	L	M	N	O	P	Q
2											
3											
4											
5	Fuel Gas Composition (Dry Vol%)										
6	Methane	95.54									
7	Ethane	2.48									
8	Propane	0									
9	Butane	0.43									
10	Hydrogen Sulfide	0									
11	Carbon Dioxide	0									
12	Nitrogen	1.55									
13	Total	100									
14	Density of N <sub>2</sub> gas (lb/cu.ft) =	0.04439078									
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	0									
23	Coal Heat Input (Btu/h)	0									
24											
25	Gas Heat Input (Btu/h)	17089272									
26	Total Firing Rate	17089272									
27	Gas Calorific Value (Btu/lb)	23346									
28	Gas Firing Rate (lb/h)	732									
29	Gas Support (% of Heat)	100.00									
30	Fraction of coal	0									
31	Fraction of GAS	1									
32											
33											
34	HHV	0									
35	Dry ash%	0									
36											
37											
38											
39											
40											
41											
42											

G	H	I	J	K	L	M	N	O	P	Q
43 Calculation of Air Requirement and Theoretical Products of Combustion										
44										
45										
46 Carbon= $\frac{\%C}{(100 \cdot 12)} \cdot 1 \text{ mole}$										
47 Hydrogen= $\frac{\%H}{(100 \cdot 2)} \cdot 0.5 \text{ mole}$										
48 Sulfur= $\frac{\%S}{(100 \cdot 32)} \cdot 1 \text{ mole}$										
49										
50 Oxygen required= Sum of the 3										
51 Oxygen available in the Fuel= %O/(100·32)										
52 Net Oxygen required =										
53 Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =										
54										
55										
56 Calculation of Products of combustion										
57										
58 Excess air used (%)										
59										
60 Actual Dry air Required (moles) = $(1+E\%) \cdot$ total air required =										
61 Dry air In lbs/lb of "as fired" fuel										
62										
63 Actual wet air used/lb of "as fired" fuel (assuming 60% RH and 80°F) =										
64										
65										
66 Weight of products of combustion = Actual wet air used + weight of fuel =										
67										
68 Actual weight of products =										
69										
70										
71										
72										
73										
74										
75										
76										
77										
78										
79										
80										
81										
82										
83										

R	S	T	U	V	W	X	Y	Z
1 Calculation of Theoretical Composition of Products								
2								
3								
4								
5 Carbon Dioxide	(=moles of carbon /lb of fuel)		0.06113197	Wet Flue Gas Composition (%)		Dry Flue Gas Comp. (%)		
6 Water	( moles of water in fuel + moles of water in combustion air)		0.12134001	9.00		10.96		
7 Oxygen			0.00840044	17.87		0.00		
8 Nitrogen			0.48817299	1.24		1.51		
9 Sulfur Dioxide			0	71.89		87.59		
10 Total			0.67904541	0		0.00		
11 Carbon Conversion				100.00		100.00		
12 Carbon Conversion	Carbon Conversion of Coal NA							
13 Boiler Efficiency	Efficiency Calculations							
14 Boiler								
15								
16 These calculations are based on ASME PTC 4.1 using heat loss method								
17								
18 1. Pounds of dry gas per pound of "as fired" composite fuel								
19								
20 $W_g = \frac{((\% \text{ d.b.}) \cdot \text{C.Efficiency} \cdot 144.01 \cdot (\text{CO}_2) + 32.00 \cdot (\text{O}_2) + 28.01 \cdot (\text{N}_2) + (28.01 \cdot (\text{CO}_2 + \text{CO}))}{16.56327899 \text{ lb/lb of as fired fuel}}$								
21								
22								
23								
24 1. Heat loss due to dry gas (%)	$L_{wg} = W_g \cdot 0.24 \cdot (\text{Gas Avg temp from air heater} - \text{mill inlet temp})/\text{HHV} \cdot 100$							
25								
26								
27 2. Heat loss due to unburned carbon								
28								
29 $L_{uc} = \text{% Carbon in the "as fired Fuel"} \cdot (1 \cdot \text{Comb. Efficiency}) \cdot 14,500$								
30								
31								
32 3. Heat loss due to unburned carbon in dust								
33								
34								
35 4. Heat loss due to moisture in "as Fired Fuel"								
36								
37 $L_{m} = \text{Moisture in Fuel} \cdot (\text{Enthalpy of vapor at gas leaving temp} - \text{Enthalpy of water at mill inlet})/\text{HHV} \cdot 100$								
38								
39								
40								
41 5. Heat loss due to moisture produced from burning hydrogen in fuel								
42								

R	S	T	U	V	W	X	Y	Z
43 Lmh=	0.936 % hydrogen in "as fired" fuel* (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV							
44								
45								
46 6. Heat loss due to moisture in combustion air								
47 Theoretical lb of air required for complete combustion/lb of "as fired" fuel ((11.52% carbon) + 34.57(% hydrogen) + 4.32 (% sulfur))/HHV =								
48								
49								
50								
51								
52 Actual dry air = (1+ % Excess air/100) lb/lb of "as fired" fuel								
53	17.91lb							
54 Moisture in air = 0.013 lb/lb of dry air	0.23279819 lbs/lb of "as fired" fuel							
55 Lma =	moisture in air * (enthalpy of water vapor leaving air heater - enthalpy of vapor at mill inlet temp.)							
56								
57								
58								
59 7. Heat loss due to formation of carbon monoxide CO/(CO <sub>2</sub> +CO) * 10160 * Combustion Efficiency* % carbon in "as fired fuel"								
60 Lco =								
61								
62								
63 8. Heat loss due to radiation	10 exp (0.62-0.42 log Q)							
64								
65								
66								
67								
68 Total Losses (%)								
69 HEAT CREDITS								
70								
71 1. Heat supplied by duct burner to entering air								
72 2. Heat supplied by primary (transport) air								
73								
74 Boiler Efficiency (%) =								
75								
76 Combustion Air Flow (%) =								
77								
78								
79								
80								
81								
82								
83								

Demonstration		Boiler Data	
Date of Operation	1-Aug	Test Matrix # burner characterization	
<b>FUEL DATA</b>			
Dust Steam Pressure (Psi)	191.35	Enthalpy of Sat. Lg. (Btu/lb)	353.52
Feed Water Temperature (°F)	217.26	Enthalpy of Feed Water (Btu/lb)	185.47
Steam Quality (% moisture)	99.97	Steam Production Rate (pph)	8600.15
Gas Temp leaving Boiler (°F)	477	Flow down Rate (pph)	105.25
Gas Temp leaving Air Heater (°F)	64	Enthalpy of water vapor at flue Temp (Btu/lb)	1168.01
Air Temp entering Air Heater (°F)	0	Enthalpy of water at flue end temp. (Btu/lb)	51.71
Air Temp leaving Air Pre Heater (°F)	97	Enthalpy of vapor at flue end temp. (Btu/lb)	1000.36
Air Temp entering Boiler (°F)	361	Sat. steam (lb/gas at flue temp.)	1333.01
Mill Inlet Temperature (°F)		Gas Flow Rate (lb/h)	367.62
Mill air flow rate (lb/h)		Gas Cal. Value (Btu/lb)	2334.6
Burner inlet temperature (°F)		Gas Analysis (Dry Vol%)	
<b>Proximate Analysis</b>		Gas Analysis (Dry Vol%)	
Moisture (Wt%)	3.42	Ultimate Analysis (Wt%: d.b)	
Volatile Matter (Wt%)	30.82		
Fixed Carbon (Wt%)	59.07		
Ash (Wt%)	6.01		
<b>HHV (Btu/lb, d.b)</b>		HHV (Btu/lb, d.b)	
Carbon	79.11	Carbon	1.80
Hydrogen	5.09	Hydrogen	1.21
Nitrogen	1.52	Nitrogen	0.05
Sulfur	0.52	Sulfur	0.05
Oxygen	0.01	Oxygen	0.05
Ash	0.01	Ash	0.05
Total	100.00	Total	100.00
<b>Flue Gas Analysis</b>		Flue Gas Analysis	
Oxygen (%)	1.80	Ash in dry Char/Fuse	1.21
Carbon Dioxide (%)	1.21	Total CARBON CONVERSION	73.37
Carbon Monoxide (ppm)	0.01	CO <sub>2</sub> CARBON CONVERSION	3.77
Sulfur Dioxide (ppm)	0.01	CO <sub>2</sub> CARBON CONVERSION	47.76
Oxides of Nitrogen (ppm)	0.01		

Summary of Boiler Performance		
Date of Operation	1-Aug	
Boiler Operating Conditions		
Total Flue Gas	8,582,556.52	MMBtu/h
Gas Supply (%)	100.00	%
Excess air used (%)	8.49	%
Actual mass of products of combustion =	7,720,402.74	lb/lb of "as fired" fuel
Theoretical flue gas composition %		
Carbon Dioxide	8.89	%
Water vapor	17.64	%
Oxygen	1.49	%
Nitrogen	71.96	%
Sulfur Dioxide (ppm)	0	
Total	100.0	%
Boiler Efficiency Details		
1. Heat loss due to Dry gases (%)	4.24	
2. Heat loss due to unburned carbon	0.00	
3. Heat loss due to unburned carbon in dust	Negligible	
4. Heat loss due to moisture in "as Fired Fuel"	0.00	
5. Heat loss due to moisture produced from burning hydrogen in fuel	10.25	
6. Heat loss due to moisture in combustion air	0.11	
7. Heat loss due to formation of carbon monoxide	0.02	
8. Heat loss due to radiation	1.69	
9. Heat loss due to steam drum blowdown	0.00	
<b>Total Losses</b>	<b>16.31</b>	
Heat Credits		
1. Heat supplied by duct burner to curing & kiln	-103.06	lb/lb of "as fired fuel"
2. Heat supplied by mill to primary (transport) air	0.00	lb/lb of "as fired fuel"
BOILER EFFICIENCY (%)		<b>83.61</b>

Boiler Performance Calculations		N. Gas Composition (Wt%)		As Fired (Wt%)	
Fuel Gas Composition (Dry Vol%)	Conversion of Gas Composition from Volume % to Wt%	Density at 60°F (lb/cu. ft)	lbs in each cu. ft. of gas	Carbon	73.40
Methane	95.51	0.01246	0.0403663	Hydrogen	24.01
Ethane	2.48	0.08029	0.0019912	Nitrogen	2.60
Propane	0	0.1106	0	Sulfur	0.00
Butane	0.41	0.1512	0.0004803	Oxygen	0.00
Hydrogen Sulfide	0	0.09109	0	Moisture	0.00
Carbon Dioxide	0	0.117	0	Total	100.00
Nitrogen	1.55	0.07439	0.001153		0
<b>Total</b>	<b>100</b>				<b>100.00</b>
Density of N. gas (lb/cu.ft) =		<b>0.0444</b>			
Determination of Percent Gas Support					
Coal Firing Rate (lb/h)	0	As Fired Coal Composition (Wt)	76.42	"As Fired" Fuel (coal + nat. gas) Composition (Wt%)	73.46
Coal Heat Input (Btu/h)	0	Carbon	4.92	Carbon	24.00
(Gas Heat Input / Btu/h)	8582456.5	Hydrogen	1.45	Hydrogen	2.60
Total Firing Rate	8582456.5	Nitrogen	0.50	Nitrogen	0.00
(Gas Calorific Value (Btu/lb)	23146	Sulfur	6.60	Sulfur	0.00
(Gas Firing Rate (lb/h))	167.62	Oxygen	5.82	Oxygen	0.00
<b>Gas Support (% of Heat)</b>	<b>100.00</b>	Ash	3.42	Ash	0.00
Fraction of coal	0	Moisture	99.13	Moisture	0.05
Fraction of GAS	1	Total		Total	100.00
Wt% of Dry Ash		133.097		111V	
Wt% of Dry Ash		6.03		Dry Ash	

Calculation of Air Requirement and Theoretical Products of Combustion	
Carbon = $\frac{4}{12}C/(100 \cdot 12) \cdot 1 \text{ mole} =$	Theoretical Oxygen Requirement 0.06113197 moles
Hydrogen = $\frac{1}{2}H/(100 \cdot 2) \cdot 0.5 \text{ mole} =$	0.050998862 moles
Sulfur = $\frac{3}{32}S/(100 \cdot 32) \cdot 1 \text{ mole} =$	0 moles
Oxygen required = Sum of the 3 Oxygen available in the Fuel = $\% O/(100 \cdot 32) =$	0.12112059 moles
Net Oxygen required =	0
Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =	0.57676472 moles/lb of as fired fuel
<b>Calculation of Products of combustion</b>	
Excess air used (%)	= 100(0.21/0.21) = 200% N <sub>2</sub> + CO <sub>2</sub> = 8.49
Actual Dry air Required (moles) = (100%) total air required =	0.6257118
Dry air in lbs/lb of "as fired" fuel	18.752573
Actual wet air used/lb of "as fired" fuel (assuming 60% R.H. and 80°F) =	18.776954
Weight of products of combustion = Actual wet air used + weight of fuel =	19.776951 lb/m of fuel
Actual weight of products =	7270.4 lb/hr of flue gas

## Calculation of Theoretical Composition of Products

Calculation of Theoretical Composition of Products		Wet Flue Gas Composition (%)	Dry Flue Gas Comp. (%)
Carbon Dioxide (=moles of carbon/lb of fuel)	0.06111197	8.89	10.79
Water (moles of water in fuel + moles of water in combustion air)	0.12135917 0.01027682 0.49522928 0 0.68880044	17.64 1.49 7.98 0 100.00	0.00 1.81 87.40 0.00 100.00
Oxygen			
Nitrogen			
Sulfur Dioxide			
Total			
Boiler Efficiency	Calculations		
These calculations are based on ASME IFC 4.1 using heat loss method			
1. Pounds of dry gas per pound of "as fired" composite fuel			
WE =	$((\text{Efficiency} * 144.01 (\text{CO}_2) + 32.00 (\text{O}_2) + 28.02 (\text{N}_2) + 28.0) (\text{CO}) / 12.01 (\text{CO}_2)) + 12.01 (\text{S}) / 32.07$		
1. Heat loss due to dry gas (%)	$1.00 - WE * 0.24 * (359.75 / \text{MIV} * 100)$		
2. Heat loss due to unburned carbon			
LUC =	% Carbon in the "as fired Fuel" * (1-Comb. Efficiency) * 14,500		
3. Heat loss due to unburned carbon in dust			
4. Heat loss due to moisture in "as Fired Fuel"			
LHF =	Moisture in fuel (enthalpy of vapor at gas leaving furnace) Enthalpy of water at initial inlet / MIV * 100		
5. Heat loss due to moisture produced from burning hydrogen in fuel			
			10.25

5

L.mfb =	$8.936 \cdot \% \text{ hydrogen in 'as fired' fuel} \cdot (\text{enthalpy of vapor leaving air heater} - \text{enthalpy of water at null inlet temp}) / \text{HV}$			
<b>6. Heat loss due to moisture in combustion air</b>	$\text{Theoretical lb of air required for complete combustion/lb of 'as fired' fuel} = (11.52\% \text{ carbon}) + 34.51(\% \text{ hydrogen} + \% \text{ oxygen}) + 4.32(\% \text{ sulfur}) / \text{HV} =$	$16.73 \text{ lb/lb of 'as fired' fuel}$	$0.11$	
Actual dry air =	$(1 + \% \text{ excess air}) / \text{lb/lb of 'as fired' fuel}$			
Moisture in air =	$0.013 \text{ lb/lb of dry air}$	$0.2361743 \text{ lb/lb of 'as fired' fuel}$		
L.mfa =	moisture in air • (enthalpy of water vapor leaving air heater - enthalpy of vapor at null inlet temp)			
<b>7. Heat loss due to formation of carbon monoxide</b>	$Lco = CO/(CO_2+CO) \cdot 0.0160 \cdot \text{Combustion Efficiency} \cdot \% \text{ carbon in 'as fired fuel}}$		$0.02$	
<b>8. Heat loss due to radiation</b>	$10 \text{ cfp} (0.62 \cdot 0.42 \text{ log Q})$		$1.69$	
<b>Total Losses (%) HEAT CREDITS</b>			$16.31$	%
1. Heat supplied by duct burner to entering air			$-103.06$	Blus/lb of 'as fired' fuel
2. Heat supplied by null to primary (transport) air			$0.00$	Blus/lb of 'as fired' fuel
<b>Boiler Efficiency (%) =</b>			$83.61$	%
<b>Combustion Air Flow (lb/hr) =</b>			$6765$	lb/h

A	B	C	D	E	F
1 Demonstration		Boiler Data			
2 Date of Operation	8/9/95 am				
3 Pressures and Temperatures					
4					
5					
6 Drum Steam Pressure (psig)	19.0lb/min coal; Plm. 0%, Sec. 0%, Tert. 100%;Coal gun 42.25";Gas Gun -8.5; Xfer 340 acfm; O2 3.5%				
7 Feed Water Temperature (°F)					
8 Steam Quality (% moisture)					
9 Gas Temp.Leaving Boiler (°F)					
10 Gas Temp. Leaving Air Heater (°F)	190.9 Enthalpy of Sat. Lq. (Btu/lb)	346.4			
11 Air Temp Entering Air Heater (°F)	217.9 Enthalpy of Feed Water (Btu/lb)	186.2 (Sat. liquid @ Feed water temp.)			
12 Air temp leaving Air Pre Heater (°F)	100.0 Steam Production Rate (PPH)	13.466.4			
13 Air Temp Entering Boiler (°F)	587.9 Blow down Rate (PPH)	3.026.9			
14 Mill Inlet Temperature (°F)	403.1 Enthalpy of water vapor at Gvg Temp (Btu/lb)	1.243.1 (Sup. steam @ 1psia&gas lvg temp)			
15 Mill air flow rate (lb/h)	177.2 Enthalpy of water at fuel inlet temp. (Btu/lb)	57.6 (Sat. liq. @ mill inlet temp.)			
16 Burner Inlet temperature (°F)	427.2 Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1.100.7 (Sat. vapor @ mill inlet temp.)			
17 FUEL DATA	404.2 Calorimeter Temperature (°F)	312.5			
18 Proximate Analysis	89.6				
19 Moisture (Wt%)	1.623.5 Coal Firing Rate (lb/h)	114.0 Gas Firing Rate (lb/h)			
20 Volatile Matter (Wt%)	187.9 Coal H.M. Value (Btu/lb)	144.1 Gas Cal. Value (Btu/lb)			
21 Fixed Carbon (Wt%)	Coal Moisture Content (%)	4.45			
22 Ash (Wt%)					
23					
24 HHV (Btu/lb, d.b)	1.99 Ultimate Analysis (Wt%, d.b)		Gas Analysis (Dry Vol%)		
25	31.32				
26	64.11				
27	4.92	82.32 Methane			
28	Hydrogen	5.29 Ethane			
29	144.14 Nitrogen	2.41 Propane			
30	Sulfur	0.77 Butane			
31	Oxygen	5.64 Hydrogen Sulfide			
32	Ash	4.57 Carbon Dioxide			
33	Total	100 Nitrogen			
34		Others			
35		Total	100		
36		Moisture (wt%)	0.05		
37					
38					
39					
40					
41					
42					

A	B	C	D	E	F
43		Summary of Boiler Performance			
44					
45 Date of Operation	8/9/95am				
46					
47					
48					
49					
50					
51 Boiler Operating Conditions					
52					
53					
54 Total Flue Gas Rate	16.43200755 MMBtu/h				
55 Gas Support (%)	0.00 %				
56 Excess air used (%)	19.31 %				
57					
58 Actual mass of products of combustion	16053.15136 lb/lb of "as fired" fuel				
59					
60 Theoretical flue gas composition	%				
61 Carbon Dioxide	14.42				
62 Water Vapor	6.31				
63 Oxygen	3.26				
64 Nitrogen	75.96				
65 Sulfur Dioxide (ppm)	506				
66 Total	100.00				
67 Boiler Efficiency Details					
68					
69 1. Heat loss due to Dry gas (%)					
70 2. Heat loss due to unburned carbon					
71 3. Heat loss due to unburned carbon in dust					
72 4. Heat loss due to moisture in "as Fired Fuel"					
73 5. Heat loss due to moisture produced from burning hydrogen in fuel					
74 6. Heat loss due to moisture in combustion air					
75 7. Heat loss due to formation of carbon monoxide					
76 8. Heat loss due to radiation					
77 9. Heat loss due to steam drum blowdown					
78 Total Losses					
79 Heat Credits					
80 1. Heat supplied by duct burner to entering air					
81 2. Heat supplied by mill to primary (transport) air					
82					
83 BOILER EFFICIENCY (%)					
84					
85					

1	G	H	I	J	K	L	M	N	O	P	Q
2											
3											
4											
5	Fuel Gas Composition (Dry. Vol%)	95.54									
6	Methane	2.48	0.04246	0.04056628	73.40	73.3583626					
7	Ethane	0	0.08029	0.00199119	24.01	23.9954486					
8	Propane	0	0.1196	0	2.60	2.59618878					
9	Butane	0.43	0.1582	0.00068026	0.00	0					
10	Hydrogen Sulfide	0	0.09109	0	0.00	0					
11	Carbon Dioxide	0	0.1117	0	0.00	0.05					
12	Nitrogen	1.55	0.07439	0.00115305	100.00	100.00					
13	Total	1.00									
14											
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	1140	16431960	As Fired Coal Composition (Wt)	78.66	"As Fired" Fuel (coal+nat. gas) Composition (Wt%)					
23	Coal Heat Input(Btu/h)	0	16431960	Carbon	5.05	78.66					
24	Gas Heat Input (Btu/h)	0	23346	Hydrogen	1.35	5.05					
25	Total Firing Rate	16431960	0	Nitrogen	0.74	1.35					
26	Gas Calorific Value (Btu/lb)	23346	0	Sulfur	5.39	0.74					
27	Gas Firing Rate (lb/h)	0	0.00	Oxygen	4.37	5.39					
28	Gas Support (% of heat)	0.00	1	Ash	4.37	4.37					
29	Fraction of coal	1	0	Moisture	4.45	4.45					
30	Fraction of GAS	0	100.00	Total	100.00	100.00					
31	HHV	14414	4.57	Dry Ash	4.57	14414					
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

G	H	I	J	K	L	M	N	O	P	Q
<b>4.3 Calculation of Air Requirement and Theoretical Products of Combustion</b>										
4.4										
4.5 Carbon= %C/(100*12) *1 mole =			Theoretical Oxygen Requirement							
4.6 Hydrogen= %H/(100*2)*0.5 mole =			0.0655473 moles							
4.7 Sulfur= %S/(100*32) *1 mole =			0.01263649 moles							
4.8			0.00022992 moles							
4.9										
5.0 Oxygen required= Sum of the 3			0.0784137 moles							
5.1 Oxygen available in the Fuel= %O/(100*32)			0.00168407							
5.2 Net Oxygen required =			0.07672964 moles							
5.3 Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =			0.36537922 moles/lb of as fired fuel							
5.4										
5.5										
<b>5.6 Calculation of Products of combustion</b>										
5.6										
5.7 Excess air used (%)			= $100(CO_2/CO_2)(0.214 \cdot N_2 \cdot (O_2/CO_2))$ =							
5.8			19.31							
5.9										
6.0 Actual Dry air Required (moles) = $(1+E_A\%)$ total air required =										
6.1 Dry air in lbs/lb of "as fired" fuel			= moles of air*29.77 =							
6.2			0.43592685							
6.3 Actual wet air used/lb of "as fired" fuel (assuming 60% RH and 80°F) =			13.0647276							
6.4										
6.5			13.0817117							
6.6 Weight of products of combustion = Actual wet air used + weight of fuel										
6.7										
6.8 Actual weight of products =			lbs of fuel burned * Wt of products/lb of fuel							
6.9			14.0817117 lb/lb of fuel							
7.0			16053.1514 lb of flue gas							
7.1										
7.2										
7.3										
7.4										
7.5										
7.6										
7.7										
7.8										
7.9										
8.0										
8.1										
8.2										
8.3										
8.4										
8.5										

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4									
5 Carbon Dioxide	(moles of carbon /lb of fuel)		0.0655473	Wet Flue Gas Composition (%)		Dry Flue Gas Comp. (%)			
6 Water	( moles of water in fuel +moles of water in combustion air)		0.02868876	14.42		15.39			
7			0.014815			0.00			
8 Oxygen			0.34530942			3.48			
9 Nitrogen			0.00022992	75.96		81.08			
10 Sulfur Dioxide			0.05057678			0.05			
11 Total			0.4545904	100.00		100.00			
12									
13									
14 Boiler	Efficiency								
15	Calculations								
16	These calculations are based on ASME PTC 4.1 using heat loss method								
17									
18	1. Pounds of dry gas per pound of "as fired" composite fuel								
19									
20	Wg = ((C% db) * C.Efficiency *(44.01 (CO2) + 32.00 (O2) + 28.02 (N2) + (28.01 (CO)/(CO2+CO)) + 12.01 (S)/(CO2+CO)) * 32.07								
21									
22	11.94631506 lb/lb of as fired fuel								
23									
24	1. Heat loss due to dry gas (%) Lwg = Wg * 0.24 * (359.75)/HHV * 100								
25									
26									
27	2. Heat loss due to unburned carbon								
28	% Carbon in the "as fired fuel" : (1-Comb.Efficiency) * 14.500								
29	Lug =								
30									
31									
32	3. Heat loss due to unburned carbon in dust								
33									
34									
35	4. Heat loss due to moisture in "as Fired Fuel"								
36									
37	Moliture in Fuel (Enthalpy of vapor at gas leaving temp.)								
38									
39	Enthalpy of water at mill inlet)/HHV * 100								
40									
41	5. Heat loss due to moisture produced from burning hydrogen in fuel								
42									

	R	S	T	U	V	W	X	Y	Z	AA
4.3	$L_{mH} =$	0.936 % hydrogen in "as fired" fuel	(Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/ $\eta_{HV}$							
4.4										
4.5										
4.6	6. Heat loss due to moisture in combustion air									
4.7	Theoretical lb of air required for complete combustion/lb of "as fired" fuel									
4.8	$= \frac{(11.52\% \text{ carbon}) + 34.57\% \text{ hydrogen}}{10.61 \text{ lb/lb of "as fired" fuel}}$									
4.9										
5.0										
5.1										
5.2	Actual dry air =	(1+%) Excess air/lb of "as fired" fuel								
5.3		12.66 lb								
5.4	Moisture in air =	0.013 lb /lb of dry air	0.16452349 lbs/lb of "as fired" fuel							
5.5	$L_{ma} =$	moisture in air * (enthalpy of water vapor leaving air heater - enthalpy of vapor at mill inlet temp.)								
5.6										
5.7										
5.8										
5.9	7. Heat loss due to formation of carbon monoxide									
6.0	$L_{CO} =$	$CO/(CO_2+CO) \cdot 10160 \cdot \text{Combustion Efficiency} \cdot \% \text{ carbon in "as fired fuel}}$								
6.1										
6.2										
6.3	8. Heat loss due to radiation	$10 \cdot \exp(0.62 \cdot 0.42 \log Q)$								
6.4										
6.5										
6.6										
6.7										
6.8	Total Losses (%)									
6.9	HEAT CREDITS									
7.0										
7.1	1. Heat supplied by duct burner to entering air									
7.2	2. Heat supplied by mill to primary (transport) air									
7.3										
7.4	Boiler Efficiency (%) =									
7.5										
7.6	7.7 Combustion Air Flow (lb/hr) =									
7.7										
7.8										
7.9										
8.0										
8.1										
8.2										
8.3										
8.4										
8.5										

A	B	C	D	E	F
1 Demonstration		Boiler Data			
2 Date of Operation	8/9/95 pm				
3					
4 Pressures and Temperatures					
5					
6 Drum Steam Pressure (psig)					
7 Feed Water Temperature (°F)					
8 Steam Quality ( % moisture)					
9 Gas Temp.Leaving Boiler (°F)					
10 Gas Temp.Leaving Air Heater (°F)					
11 Air Temp Entering Air Heater (°F)					
12 Air Temp leaving Air Pre Heater (°F)					
13 Air Temp Entering Boiler (°F)					
14 Mill Inlet Temperature (°F)					
15 Mill air flow rate (lb/h)					
16 Burner Inlet temperature (°F)					
17 FUEL DATA					
18 Proximate Analysis					
19 Moisture (Wt%)					
20 Volatile Matter (Wt%)					
21 Fixed Carbon (Wt%)					
22 Ash (Wt%)					
23					
24 HHV (Btu/lb, d.b)					
25					
26					
27					
28					
29					
30 Flue Gas Analysis					
31					
32 Oxygen (%)					
33 Carbon Dioxide (%)					
34 Carbon Monoxide (PPM)					
35 Sulfur Dioxide (PPM)					
36 Oxides of Nitrogen (PPM)					
37					
38					
39					
40					
41					
42					

A	B	C Summary of Boiler Performance	D	E	F
43					
44					
45					
46	Date of Operation	8/9/95pm			
47					
48					
49					
50					
51	Boiler Operating Conditions				
52					
53					
54	Total Firing Rate				
55	Gas Support (%)				
56	Excess air used (%)				
57					
58	Actual mass of products of combustion =				
59					
60	Theoretical flue gas composition %				
61	Carbon Dioxide	15.02			
62	Water vapor	6.56			
63	Oxygen	2.53			
64	Nitrogen	75.84			
65	Sulfur Dioxide (ppm)	5.27			
66	Total	100.00			
67	Boiler Efficiency Details				
68					
69	1. Heat loss due to Dry gas (%)				
70	2. Heat loss due to unburned carbon				
71	3. Heat loss due to unburned carbon In dust				
72	4. Heat loss due to moisture In "as Fired Fuel"				
73	5. Heat loss due to moisture produced from burning hydrogen In fuel				
74	6. Heat loss due to moisture In combustion air				
75	7. Heat loss due to formation of carbon monoxide				
76	8. Heat loss due to radiation				
77	9. Heat loss due to steam drum blowdown				
78	Total Losses				
79	Heat Credits				
80	1. Heat supplied by dual burner to entering air				-62.61 Bl/lb of "as fired fuel"
81	2. Heat supplied by mill to primary (transport) air				33.24 Bl/lb of "as fired fuel"
82					
83	BOILER EFFICIENCY (%)				85.75
84					
85					

	G	H	I	J	K	L	M	N	O	P	Q
1											
2											
3											
4											
5	Fuel Gas Composition (Dry. Vol%)	95.54	Density at 60°F (lb/cu.ft)	0.04246	0.040566620	lbs in each Cu.ft of gas					
6	Methane	2.48		0.08029	0.00199119						
7	Ethane	0		0.1196	0						
8	Propane	0		0.1582	0.00068026						
9	Bulane	0.43		0.09109	0						
10	Hydrogen Sulfide	0		0.1117	0						
11	Carbon Dioxide	0		0.07439	0.00115305						
12	Nitrogen	1.55									
13	Total	100									
14											
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	1140									
23	Coal Heat Input(Btu/h)	16431960									
24											
25	Gas Heat Input (Btu/h)	0									
26	Total Firing Rate	16431960									
27	Gas Calorific Value (Btu/lb)	23346									
28	Gas Firing Rate (lb/h)	0									
29	Gas Support (% of Heat)	0.00									
30	Fraction of coal	1									
31	Fraction of GAS	0									
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

## Conversion of Gas Composition from Volume % to Wt%

	N. Gas Composition (Wt%, d.b.)	As Fired (wt%)
Carbon	73.40	73.3583626
Hydrogen	24.01	23.9954486
Nitrogen	2.60	2.59618878
Sulfur	0.00	0
Oxygen	0.00	0
Moisture	0.00	0.05
Total	100.00	100.00

## Boiler Performance Calculations

	"As Fired" Fuel (coal+nat. gas) Composition (Wt%)
Carbon	78.66
Hydrogen	5.05
Nitrogen	1.35
Sulfur	0.74
Oxygen	5.39
Ash	4.37
Moisture	4.45
Total	100.00

	G	H	I	J	K	L	M	N	O	P	Q
43	Calculation of Air Requirement and Theoretical Products of Combustion										
44											
45					Theoretical Oxygen Requirement						
46	Carbon= %C/(100*12) *1 mole =				0.0655473 moles						
47	Hydrogen= %H/(100*2)*0.5 mole =				0.01263649 moles						
48	Sulfur= %S/(100*32) *1 mole =				0.00022992 moles						
49											
50	Oxygen required= Sum of the 3 Oxygen available In the Fuel= %O/(100*32)				0.0784137 moles						
51	Net Oxygen required =				0.00168407						
52	Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =				0.07672964 moles						
53											
54											
55											
56	Calculation of Products of combustion										
57											
58	Excess air used (%)				- 100(O2.C/(O2)/(0.264*N2/(0.2*(CO2))=						
59											
60	Actual Dry air Required (moles) = (1+E,A%)* total air required =				0.41791173						
61	Dry air In lbs/lb of "as fired" fuel				12.5248146						
62											
63	Actual wet air used/lb of "as fired" fuel (assuming 60% R.H and 80°F)=				= moles of air*29.97 =						
64											
65											
66	Weight of products of combustion = Actual wet air used + weight of fuel				12.5410969						
67											
68	Actual weight of products =										
69											
70											
71											
72											
73											
74											
75											
76											
77											
78											
79											
80											
81											
82											
83											
84											
85											

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4									
5 Carbon Dioxide	(=moles of carbon /lb of fuel)								
6 Water	(moles of water in fuel + moles of water in combustion air)								
7 Oxygen									
8 Nitrogen									
9 Sulfur Dioxide									
10 Total									
11									
12									
13									
14 Boiler Efficiency	Calculations								
15									
16 These calculations are based on ASME PTC 4.1 using heat loss method									
17									
18 1. Pounds of dry gas per pound of "as fired" composite fuel									
19 Wg =									
20									
21									
22									
23									
24 1. Heat loss due to dry gas (%)	Lwg = Wg * 0.24 * (359.75)/HHV * 100								
25									
26									
27 2. Heat loss due to unburned carbon									
28									
29 Luc =	% Carbon in the "as fired Fuel" * (1-Comb. Efficiency) * 14,500								
30									
31									
32 3. Heat loss due to unburned carbon in dust	Negligible								
33									
34									
35 4. Heat loss due to moisture in "as Fired Fuel"									
36									
37 Lmi =	Moisture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet)/HHV*100								
38									
39									
40									
41 5. Heat loss due to moisture produced from burning hydrogen in fuel	= 3.70								
42									

R	S	T	U	V	W	X	Y	Z	AA
4.3 $L_{mih} =$	8.936 % hydrogen in "as fired" fuel" (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV								
4.4									
4.5									
4.6 6. Heat loss due to moisture in combustion air	Theoretical lb of air required for complete combustion/lb of "as fired" fuel								
4.7	=								
4.8	=								
4.9									
5.0									
5.1									
5.2 Actual dry air =	$(1 + \% \text{ Excess air}/100) \text{ lb/lb of "as fired" fuel}$								
5.3									
5.4 Moisture in air =	$0.013 \text{ lb/lb of dry air}$	$0.1577244 \text{ lbs/lb of "as fired" fuel}$							
5.5 $L_{ma} =$	moisture in air * (enthalpy of water vapor leaving air heater - enthalpy of vapor at mill inlet temp.)								
5.6									
5.7									
5.8									
5.9 7. Heat loss due to formation of carbon monoxide	$\text{CO}/(\text{CO}_2 + \text{CO}) \cdot 10^{16} \cdot \text{Combustion Efficiency} \cdot \% \text{ carbon in "as fired fuel}}$								
6.0 $L_{co} =$									
6.1									
6.2									
6.3 Heat loss due to radiation	$10 \exp(0.62 \cdot 0.42 \log Q)$								
6.4									
6.5									
6.6									
6.7									
6.8 Total Losses (%)									
6.9 HEAT CREDITS									
7.0									
7.1 1. Heat supplied by duct burner to entering air									
7.2 2. Heat supplied by mill to primary (transport) air									
7.3									
7.4 Boiler Efficiency (%) =									
7.5									
7.6									
7.7 Combustion Air Flow (lb/hr) =									
7.8									
7.9									
8.0									
8.1									
8.2									
8.3									
8.4									
8.5									

$$(11.52\% \text{ carbon}) + 34.57\% \text{ hydrogen} - \% \text{ oxygen}/8) + 4.32\% \text{ sulfur})/\text{HHV} =$$

$$0.16$$

$$0.05$$

$$1.29$$

$$14.22\%$$

$$14011 \text{ lb/h}$$

$$85.75\%$$

$$62.61 \text{ lb/lb of "as Fired" Fuel}$$

$$33.24 \text{ lb/lb of "as Fired" Fuel}$$

A <b>Demonstration</b>	B	C <b>Boiler Data</b>	D	E	F
1 Date of Operation	8/23/95				
2					
3					
4					
5					
6 Drum Steam Pressure (Psig)					
7 Feed Water Temperature (°F)					
8 Steam Quality ( % moisture)					
9 Gas Temp.Leaving Boiler (°F)					
10 Gas Temp. Leaving Air Heater (°F)					
11 Air Temp Entering Air Heater (°F)					
12 Air Temp leaving Air Pre Heater (°F)					
13 Air Temp Entering Boiler (°F)					
14 Mill Inlet Temperature (°F)					
15 Mill air flow rate (lb/h)					
16 Burner inlet temperature (°F)					
17 FUEL DATA					
18 Proximate Analysis					
19 Moisture (Wt%)					
20 Volatile Matter (Wt%)					
21 Fixed Carbon (Wt%)					
22 Ash (Wt%)					
23					
24 HHV (Btu/lb, d.b)					
25					
26					
27					
28					
29					
30 Flue Gas Analysis					
31					
32 Oxygen (%)					
33 Carbon Dioxide (%)					
34 Carbon Monoxide (PPM)					
35 Sulfur Dioxide (PPM)					
36 Oxides of Nitrogen (PPM)					
37					
38					
39					
40					
41					
42					

A	B	C	D	E	F	
4.3		Summary of Boiler Performance				
4.4						
4.5						
4.6 Date of Operation	23-Aug					
4.7						
4.8						
4.9						
5.0						
5.1 Boiler Operating Conditions						
5.2						
5.3						
5.4 Total Firing Rate		16.46619081 MMBtu/h				
5.5 Gas Support (%)		0.00 %				
5.6 Excess air used (%)		18.75 %				
5.7						
5.8 Actual mass of products of combustion =		15836.41255 lb/lb of "as fired" fuel				
5.9						
6.0 Theoretical flue gas composition	%					
6.1 Carbon Dioxide	14.63					
6.2 Water vapor	6.15					
6.3 Oxygen	3.18					
6.4 Nitrogen	75.99					
6.5 Sulfur Dioxide (ppm)	539					
6.6 Total	100.00					
6.7 Boiler Efficiency Details			%			
6.8						
6.9 1. Heat loss due to Dry gas (%)						
7.0 2. Heat loss due to unburned carbon						
7.1 3. Heat loss due to unburned carbon in dust						
7.2 4. Heat loss due to moisture in "as Fired Fuel"						
7.3 5. Heat loss due to moisture produced from burning hydrogen in fuel						
7.4 6. Heat loss due to moisture in combustion air						
7.5 7. Heat loss due to formation of carbon monoxide						
7.6 8. Heat loss due to radiation						
7.7 9. Heat loss due to steam drum blowdown						
7.8 Total Losses			0.00			
7.9 Heat Credits			19.59			
8.0 1. Heat supplied by duct burner to entering air				-68.60	Blu/b of "as fired fuel"	
8.1 2. Heat supplied by mill to primary (transport) air					-37.70	Blu/b of "as fired fuel"
8.2						
8.3 BOILER EFFICIENCY (%)				80.36		
8.4						
8.5						

1	G	H	I	J	K	L	M	N	O	P	Q
2											
3											
4											
5	Fuel Gas Composition (Dry, Vol%)										
6	Methane	95.54									
7	Ethane	2.48									
8	Propane	0									
9	Butane	0.43									
10	Hydrogen Sulfide	0									
11	Carbon Dioxide	0									
12	Nitrogen	0									
13	Total	1.55									
14		100									
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	1140									
23	Coal Heat Input(Btu/lb)	16466160									
24											
25	Gas Heat Input (Btu/lb)	0									
26	Total Firing Rate	16466160									
27	Gas Calorific Value (Btu/lb)	23346									
28	Gas Firing Rate (lb/h)	0									
29	Gas Support % of Heat	0.00									
30	Fraction of coal	1									
31	Fraction of GAS	0									
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

5	Conversion of Gas Composition from Volume % to Wt%			Boiler Performance Calculations			N. Gas Composition (Wt%, d.b)			As Fired (w%)		
6	Fuel Gas Composition (Dry, Vol%)			Density at 60°F (lb/cu.ft)	0.04246	0.04056628	Carbon	73.40		73.3583626		
7	Ethane	2.48		0.08029	0.00199119	Hydrogen	24.01		23.9954486			
8	Propane	0		0.1196	0	Nitrogen	2.60		2.59618878			
9	Butane	0.43		0.1582	0.00068026	Sulfur	0.00		0			
10	Hydrogen Sulfide	0		0.09109	0	Oxygen	0.00		0			
11	Carbon Dioxide	0		0.117	0	Ash	0.00		0.05			
12	Nitrogen	0		0.07439	0.00115305	Moisture	100.00		100.00			
13	Total	1.55				Total=						
14		100										
15												
16												
17												
18												
19												
20												
21												
22												
23												
24												
25												
26												
27												
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30												
31												
32												
33												
34												
35												
36												
37												
38												
39												
40												
41												
42												

25	Gas Heat Input (Btu/lb)	0										
26	Total Firing Rate	16466160										
27	Gas Calorific Value (Btu/lb)	23346										
28	Gas Firing Rate (lb/h)	0										
29	Gas Support % of Heat	0.00										
30	Fraction of coal	1										
31	Fraction of GAS	0										
32												
33												
34												
35												
36												
37												
38												
39												
40												
41												
42												

G	H	I	J	K	L	M	N	O	P	Q
43 Calculation of Air Requirement and Theoretical Products of Composition										
44										
45 Carbon= %C/(100-12) *1 mole =										
46 Hydrogen= %H/(100-2)*0.5 mole =										
47 Sulfur= %S/(100-32)*1 mole =										
48										
49 Oxygen required= Sum of the 3										
50 Oxygen available In the Fuel= %O/(100-32)	0.07775337 moles									
51 Net Oxygen required =	0.00178223									
52 Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =	0.07597115 moles									
53										
54										
55										
56 Calculation of Products of combustion										
57 Excess air used (%)										
58										
59 Actual Dry air Required (moles) = (1+E,A%) * total air required =	100XO2-CO2/10(0.264*12-O2-CO2)=	18.75								
60										
61 Dry air In lbs/lb of "as fired" fuel										
62										
63 Actual wet air used/lb of "as fired" fuel (assuming 60% R.I. and 80°F)=										
64										
65										
66 Weight of products of combustion = Actual wet air used + weight of fuel=										
67										
68 Actual weight of products =										
69										
70										
71										
72										
73										
74										
75										
76										
77										
78										
79										
80										
81										
82										
83										
84										
85										

	R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>										
2										
3										
4										
5 Carbon Dioxide	(moles of carbon /lb of fuel)									
Water	(moles of water in fuel + moles of water in combustion air)									
6 Oxygen										
7 Nitrogen										
8 Sulfur Dioxide										
9 Total										
10										
11										
12										
13										
14 Boiler	Efficiency	Calculations								
15										
16	These calculations are based on ASME PTC 4.1 using heat loss method									
17										
18	1. Pounds of dry gas per pound of "as fired" composite fuel									
19										
20	$Wg = \frac{((\% d.b) \cdot C. Efficiency)}{(44.01 (CO_2) + 32.00 (O_2) + 28.02 (N_2) + (28.01 (CO_2+CO)) + 12.01 (S_2O_3))} \cdot 100$									
21										
22	11.44711808 lb/lb of as fired fuel									
23										
24	1. Heat loss due to dry gas (%)	$L_{vg} = Wg \cdot 0.24 \cdot (359.75)/HHV \cdot 100$								
25										
26	2. Heat loss due to unburned carbon									
27										
28										
29	$L_{uc} = \% \text{ Carbon in the "as fired Fuel"} \cdot (1-\text{Comb. Efficiency}) \cdot 14,500$									
30										
31	3. Heat loss due to unburned carbon in dust									
32										
33										
34	4. Heat loss due to moisture in "as Fired Fuel"									
35										
36										
37 Lmf:	Molality in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet)/HHV*100									
38										
39										
40										
41	5. Heat loss due to moisture produced from burning hydrogen in fuel									
42										

	R	S	T	U	V	W	X	Y	Z	AA
43	$L_{mfb} =$	$8.936 * \% \text{ hydrogen in "as fired" fuel}$ (Enthalpy of vapor leaving air heater)								
44			Enthalpy of water at mill inlet temp)/HIV							
45										
46	<b>6. Heat loss due to moisture in combustion air</b>									
47	Theoretical lb of air required for complete combustion/lb of "as fired" fuel									
48	$= \frac{(1.52\% \text{ carbon}) + 34.57\% \text{ hydrogen}}{(\% \text{ oxygen}) + 4.32 (\% \text{ sulfur})}/\text{HIV} =$									
49										
50										
51	<b>Actual dry air =</b>	$(1 + \% \text{ Excess air}/100) \text{ lb/lb of "as fired" fuel}$								
52		$12.47/\text{lb}$								
53	<b>Moisture in air =</b>	$0.013 \text{ lb/lb of dry air}$								
54		$0.16213203 \text{ lbs/lb of "as fired" fuel}$								
55	<b>Moisture in air =</b>	$\text{enthalpy of water vapor leaving air heater}$								
56		$-\text{enthalpy of vapor at mill inlet temp.}$								
57										
58										
59	<b>7. Heat loss due to formation of carbon monoxide</b>									
60	$L_{co} =$	$CO/(CO_2+CO) \cdot 10160 \cdot \text{Combustion Efficiency} \cdot \% \text{ carbon in "as fired" fuel}$								
61										
62										
63	<b>8. Heat loss due to radiation</b>	$10 \exp(0.62 \cdot 0.42 \log Q)$								
64										
65										
66										
67										
68	<b>Total Losses (%)</b>									
69	<b>HEAT CREDITS</b>									
70										
71	1. Heat supplied by duct burner to entering air									
72	2. Heat supplied by mill to primary (transport) air									
73										
74	<b>Boiler Efficiency (%) =</b>									
75										
76										
77	<b>Combustion Air Flow (lb/hr) =</b>									
78										
79										
80										
81										
82										
83										
84										
85										

A	B	C	D	E	F
1 Demonstration		Boiler Data			
2 Date of Operation	8/24/95	Steam Data			
3	19.0lb/min coal; Prlm. 100%, Sec. 100%, Tert. 50%;Coal gun -10.5";Gas Gun -9";Xter 380 acfm; O2 3.75%				
4 Pressures and Temperatures					
5					
6 Drum Steam Pressure (Psi)		183.44 Enthalpy of Sat. Liq. (Btu/lb)	343.3		
7 Feed Water Temperature (°F)		206.55 Enthalpy of Feed Water (Btu/lb)	174.7	(Sat. liquid @ Feed water temp.)	
8 Steam Quality (% moisture)		99.3 Steam Production Rate (PPH)	14416.55		
9 Gas Temp Leaving Boiler (°F)		539.36 Blow down Rate (PPH)	2967.46		
10 Gas Temp Leaving Air Heater (°F)		377.94 Enthalpy of water vapor at Gvg Temp (Btu/lb)	1,231.6	(Sup. steam @ 1psi&gas lvg temp)	
11 Air Temp Entering Air Heater (°F)		171.10 Enthalpy of water at fuel inlet temp. (Btu/lb)	54.3	(Sat. liq. @ mill inlet temp.)	
12 Air Temp Leaving Air Pre Heater (°F)		394.80 Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1,099.2	(Sat. vapor @ mill inlet temp.)	
13 Air Temp Entering Boiler (°F)		376.58 Calorimeter Temperature (°F)	300.9		
14 Mill Inlet Temperature (°F)		86.25			
15 Mill air flow rate (lb/h)		1,711 Coal Firing Rate (lb/h)	1140	Gas Firing Rate (lb/h)	
16 Burner Inlet temperature (°F)		183.20 Coal H.H. Value (Btu/lb)	1444	Gas Cal. Value (Btu/lb)	
17 FUEL DATA		Coal Moisture Content (%)	3.67		
18 Proximate Analysis					
19 Moisture (Wt%)		1.87 Ultimate Analysis (Wt%, d.b)		Gas Analysis (Dry Vol%)	
20 Volatile Matter (Wt%)		30.82			
21 Fixed Carbon (Wt%)		64.82			
22 Ash (Wt%)		4.43 Carbon	82.41	Methane	
23		Hydrogen	5.04	Ethane	
24 HHV (Btu/lb, d.b)		14444 Nitrogen	1.4	Propane	
25		Sulfur	0.81	Butane	
26		Oxygen	5.98	Hydrogen Sulfide	
27		Ash	4.36	Carbon Dioxide	
28		Total	100	Nitrogen	
29				Others	
30 Flue Gas Analysis				Total	100
31				Moisture (wt%)	0.06
32 Oxygen (%)		3.76			
33 Carbon Dioxide (%)		15.03			
34 Carbon Monoxide (PPM)		146.15			
35 Sulfur Dioxide (PPM)		484.88			
36 Oxides of Nitrogen (PPM)		442.91			
37					
38					
39					
40					
41					
42					

A	B	C	D	E	F
4.3					
4.4					
4.5	Date of Operation	24-Aug			
4.6					
4.7					
4.8					
4.9					
5.0					
5.1	Boiler Operating Conditions				
5.2					
5.3					
5.4	Total Firing Rate		16.46620994 MMBtu/h		
5.5	Gas Support (%)		0.00 %		
5.6	Excess air used (%)		21.21 %		
5.7					
5.8	Actual mass of products of combustion		16291.52447 lb/lb of "as fired" fuel		
5.9					
6.0	Theoretical flue gas composition	%			
6.1	Carbon Dioxide		14.36		
6.2	Water vapor		5.92		
6.3	Oxygen		3.53		
6.4	Nitrogen		76.14		
6.5	Sulfur Dioxide (ppm)		5.29		
6.6	Total		100.00		
6.7	Boiler Efficiency Details			%	
6.8					
6.9	1. Heat loss due to Dry gas (%)			6.21	
7.0	2. Heat loss due to unburned carbon			3.75	
7.1	3. Heat loss due to unburned carbon in dust			Negligible	
7.2	4. Heat loss due to moisture in "as Fired Fuel"			0.30	
7.3	5. Heat loss due to moisture produced from burning hydrogen in fuel			3.54	
7.4	6. Heat loss due to moisture in combustion air			0.15	
7.5	7. Heat loss due to formation of carbon monoxide			0.05	
7.6	8. Heat loss due to radiation			1.29	
7.7	9. Heat loss due to steam drum blowdown			0.00	
7.8	Total Losses			15.28	
7.9	Heat Credits				
8.0	1. Heat supplied by duct burner to entering air			-58.27	Blu/b of "as fired fuel"
8.1	2. Heat supplied by mill to primary (transport) air			35.72	Blu/b of "as fired fuel"
8.2	BOILER EFFICIENCY (%)			84.70	
8.3					
8.4					
8.5					

1	G	H	I	J	K	L	M	N	O	P	Q
2											
3											
4											
5	Fuel Gas Composition (Dry, Vol%)										
6	Methane	95.54	Density at 60°F (lb/cu.ft)	0.04246	Conversion of Gas Composition from Volume % to Wt%	0.04056628	lbs in each cu.ft of gas				
7	Ethane	2.48		0.08029		0.00199119					
8	Propane	0		0.1196		0					
9	Bulane	0.43		0.1582		0.00068026					
10	Hydrogen Sulfide	0		0.09109		0					
11	Carbon Dioxide	0		0.117		0					
12	Nitrogen	1.55		0.07439		0.00115305					
13	Total	100									
14					Density of N. gas (lb/cu.ft) =	0.04439078					
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	1140									
23	Coal Heat Input(Btu/h)	16466160									
24											
25	Gas Heat Input (Btu/h)	0									
26	Total Firing Rate	16466160									
27	Gas Calorific Value (Btu/lb)	23346									
28	Gas Firing Rate (lb/h)	0									
29	Gas Support (% of Heat)	0.00									
30	Fraction of Coal	1									
31	Fraction of GAS	0									
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

Boiler Performance Calculations		N. Gas Composition (Wt%, d.b)		As Fired (w%)	
Carbon	73.40	73.3583626			
Hydrogen	24.01	23.9954486			
Nitrogen	2.60	2.59618870			
Sulfur	0.00	0			
Oxygen	0.00	0			
Moisture	0.00	0.05			
Total=	100.00	100.00			

"As Fired" Fuel (coal+nat. gas) Composition (Wt%)		"As Fired" Fuel (coal+nat. gas) Composition (Wt%)	
Carbon	79.39	79.39	
Hydrogen	4.86		
Nitrogen	1.35		
Sulfur	0.78		
Oxygen	5.76		
Ash	4.20		
Moisture	3.67		
Total	100.00	100.00	

	G	H	I	J	K	L	M	N	O	P	Q
43	<u>Calculation of Air Requirement and Theoretical Products of Combustion</u>										
44											
45											
46	Carbon = $\frac{\%C}{12} \cdot 1 \text{ mole}$ =				Theoretical Oxygen Requirement						
47	Hydrogen = $\frac{\%H}{2} \cdot 0.5 \text{ mole}$ =				0.06615463 moles						
48	Sulfur = $\frac{\%S}{32} \cdot 1 \text{ mole}$ =				0.01213758 moles						
49					0.00024384 moles						
50	Oxygen required = Sum of the 3				0.07853604 moles						
51	Oxygen available in the Fuel = $\frac{\%O}{(100 \cdot 32)}$				0.00180017						
52	Net Oxygen required =				0.07673588 moles						
53	Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =										
54											
55											
56	<u>Calculation of Products of combustion</u>										
57											
58	Excess air used (%)				= $100(O_2 \cdot CO_2)/(0.264 \cdot N_2 \cdot O_2 \cdot CO_2) =$						
59					21.21						
60	Actual Dry air Required (moles) = $(1 + E, A\%) \cdot$ total air required =										
61	Dry air in lbs/lb of "as fired" fuel										
62	Actual wet air used/lb of "as fired" fuel (assuming 60% R.H. and 80°F) =										
63	= $\frac{\text{moles of air} \cdot 29.97}{\text{lbs of dry air} \cdot 1.0013}$										
64											
65											
66	Weight of products of combustion = Actual wet air used + weight of fuel										
67											
68	Actual weight of products =										
69											
70											
71											
72											
73											
74											
75											
76											
77											
78											
79											
80											
81											
82											
83											
84											
85											

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4									
5 Carbon Dioxide	(moles of carbon /lb of fuel)								
6 Water	( moles of water in fuel + moles of water in combustion air)								
7 Oxygen									
8 Nitrogen									
9 Sulfur Dioxide									
10 Total									
11									
12									
13									
14 Boiler Efficiency	Calculations								
15									
16 These calculations are based on ASME PTG 4.1 using heat loss method									
17									
18 1. Pounds of dry gas per pound of "as fired" composite fuel									
19									
20 Wg = ((c% db) * C. Efficiency * (44.01 (CO2) + 32.00 (O2) + 28.02 (N2) + (28.01 (CO2+CO)) + 12.01 (S)/32.07									
21									
22									
23									
24 1. Heat loss due to dry gas (%) Lwg = Wg * 0.24 : (359.75)/11HV * 100									
25									
26									
27 2. Heat loss due to unburned carbon	% Carbon in the "as fired Fuel" : (1-Comb. Efficiency) * 14,500								
28									
29 Luc =									
30									
31									
32 3. Heat loss due to unburned carbon in dust	Negligible								
33									
34									
35 4. Heat loss due to moisture in "as Fired Fuel"									
36									
37 Umf = Moisture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet)/HTIV*100									
38									
39									
40									
41 5. Heat loss due to moisture produced from burning hydrogen in fuel	3.54								
42									

R	S	T	U	V	W	X	Y	Z	AA
43 Lmh=	8.936 % hydrogen in "as fired" fuel (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV								
44									
45									
46 6. Heat loss due to moisture in combustion air									
47 Theoretical lb of air required for complete combustion/lb of "as fired" fuel									
48 = $(11.52\% \text{ carbon}) + 34.57(\% \text{ hydrogen} + \% \text{ oxygen}/8) + 4.32 (\% \text{ sulfur})/11\text{HV} =$									
49									
50									
51 Actual dry air = $(1 + \% \text{ Excess air}/100) \text{ lb/lb of "as fired" fuel}$									
52									
53 Moisture in air = $12.86 \text{ lb}$									
54									
55 Lma = $0.013 \text{ lb/lb of dry air}$ moisture in air • (enthalpy of water vapor leaving air heater - enthalpy of vapor at mill inlet temp.)									
56									
57									
58 59.7. Heat loss due to formation of carbon monoxide									
60 Lco = $\text{CO}/(\text{CO}_2 + \text{CO}) \cdot 10.60 \cdot \text{Combustion Efficiency} \cdot \% \text{ carbon in "as fired" fuel}$									
61									
62									
63 6. Heat loss due to radiation									
64									
65									
66									
67 Total Losses (%)									
68 HEAT CREDITS									
69									
70									
71 1. Heat supplied by duct burner to entering air									
72 2. Heat supplied by mill to primary (transport) air									
73									
74 Boiler Efficiency (%) =									
75									
76									
77 Combustion Air Flow (lb/hr) =									
78									
79									
80									
81									
82									
83									
84									
85									

A	B	C	D	E	F
1 Demonstration		Boiler Data			
2 Date of Operation	8/25/95				
3					
4 Pressures and Temperatures					
5					
6 Drum Steam Pressure (Psig)		187.4 Enthalpy of Sat. Lq. (Btu/lb)	344.9		
7 Feed Water Temperature (°F)		207.2 Enthalpy of Feed Water (Btu/lb)	175.3	(Sat. liquid @ Feed water temp.)	
8 Steam Quality (% moisture)		99.3 Steam Production Rate (PPH)	14,378.5		
9 Gas Temp.Leaving Boiler (°F)		594.2 Blow down Rate (PPH)	2,999.0		
10 Gas Temp. Leaving Air Heater (°F)		399.7 Enthalpy of water vapor at Gvg Temp (Btu/lb)	1,241.6	(Sup. steam @ 1psia&gas lvg temp)	
11 Air Temp Entering Air Heater (°F)		165.9 Enthalpy of water at fuel inlet temp. (Btu/lb)	52.0	(Sat. liq. @ mill inlet temp.)	
12 Air temp leaving Air Pre Heater (°F)		421.1 Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1,096.3	(Sat. vapor @ mill inlet temp.)	
13 Air Temp Entering Boiler (°F)		398.8 Calorimeter Temperature (°F)	301.0		
14 Mill Inlet Temperature (°F)	83.9				
15 Mill air flow rate (lb/h)		1,710.5 Coal Firing Rate (lb/h)	1140	Gas Firing Rate (lb/h)	0
16 Burner Inlet Temperature (°F)		184.1 Coal H.H. Value (Btu/lb)	1444	Gas Cal. Value (Btu/lb)	23346
17 FUEL DATA		Coal Moisture Content (%)	3.89		
18 Proximate Analysis					
19 Moisture (Wt%)		1.87 Ultimate Analysis (Wt%, d.b)			
20 Volatile Matter (Wt%)		30.82			
21 Fixed Carbon (Wt%)	64.82				
22 Ash (Wt%)		4.36 Carbon	82.41	Methane	95.54
23		Hydrogen	5.04	Ethane	2.48
24 HHV (Btu/lb, d.b)		14444 Nitrogen	1.4	Propane	0
25		Sulfur	0.81	Butane	0.43
26		Oxygen	5.98	Hydrogen Sulfide	0
27		Ash	4.36	Carbon Dioxide	1.55
28		Total	100	Nitrogen	
29				Others	
30 Flue Gas Analysis				Total	100
31				Moisture (wt%)	0.05
32 Oxygen (%)		3.31			
33 Carbon Dioxide (%)		15.30			
34 Carbon Monoxide (PPM)		178.04	43.89		
35 Sulfur Dioxide (PPM)		528.92	94.25		
36 Oxides of Nitrogen (PPM)		439.46	94.25		
37					
38					
39					
40					
41					
42					

A	B	C	D	E	F
43		Summary of Boiler Performance			
44					
45	Date of Operation	25-Aug			
46					
47					
48					
49					
50					
51	Boiler Operating Conditions				
52					
53					
54	Total Firing Rate		16.4662089 MMBtu/h		
55	Gas Support (%)		0.00 %		
56	Excess air used (%)		16.16 %		
57					
58	Actual mass of products of combustion =		15876.54885 lb/lb of "as fired" fuel		
59	Theoretical flue gas composition %				
60	Carbon Dioxide	14.71			
61	Water vapor	6.09			
62	Oxygen	3.10			
63	Nitrogen	76.05			
64	Sulfur Dioxide (ppm)	542			
65	Total	100.00			
66	Boiler Efficiency Details				
67					
68					
69	1. Heat loss due to Dry gas (%)				
70	2. Heat loss due to unburned carbon				
71	3. Heat loss due to unburned carbon in dust				
72	4. Heat loss due to moisture in "as Fired Fuel"				
73	5. Heat loss due to moisture produced from burning hydrogen in fuel				
74	6. Heat loss due to moisture in combustion air				
75	7. Heat loss due to formation of carbon monoxide				
76	8. Heat loss due to radiation				
77	9. Heat loss due to steam drum blowdown				
78	Total Losses				
79	Heat Credits				
80	1. Heat supplied by duct burner to entraining air				
81	2. Heat supplied by mill to primary (transport) air				
82					
83	BOILER EFFICIENCY (%)				
84					
85					

1	G	H	I	J	K	L	M	N	O	P	Q
2	—	—	—	—	—	—	—	—	—	—	—
3	—	—	—	—	—	—	—	—	—	—	—
4	—	—	—	—	—	—	—	—	—	—	—
5	Fuel Gas Composition (Dy. Vol%)	Conversion of Gas Composition from Volume % to Wt%	Density at 60°F (lb/cuft)	lbs in each Cu.ft of gas	Boiler Performance Calculations	—	—	—	—	—	—
6	Methane	95.54	0.04246	0.040566628	—	—	—	—	—	—	—
7	Ethane	2.48	0.08029	0.00199119	—	—	—	—	—	—	—
8	Propane	0	0.1196	0	—	—	—	—	—	—	—
9	Bulane	0.43	0.1582	0.00068026	—	—	—	—	—	—	—
10	Hydrogen Sulfide	0	0.09109	0	—	—	—	—	—	—	—
11	Carbon Dioxide	0	0.117	0	—	—	—	—	—	—	—
12	Nitrogen	1.55	0.07439	0.00115305	—	—	—	—	—	—	—
13	Total	100	—	—	—	—	—	—	—	—	—
14	—	—	—	—	—	—	—	—	—	—	—
15	—	—	—	—	Intensity of N. gas (lb/cu.ft) =	0.04439078	—	—	—	—	—
16	—	—	—	—	—	—	—	—	—	—	—
17	—	—	—	—	—	—	—	—	—	—	—
18	—	—	—	—	—	—	—	—	—	—	—
19	—	—	—	—	Determination of Percent Gas Support	—	—	—	—	—	—
20	—	—	—	—	—	—	—	—	—	—	—
21	—	—	—	—	—	—	—	—	—	—	—
22	Coal Firing Rate (lb/h)	1140	—	—	As Fired Coal Composition (wt%)	—	—	—	—	—	—
23	Coal Heat Input(Btu/h)	16466160	—	—	Carbon	79.20	—	—	—	—	—
24	Gas Heat Input (Btu/h)	0	—	—	Hydrogen	4.84	—	—	—	—	—
25	Gas Total Firing Rate	16466160	—	—	Nitrogen	1.35	—	—	—	—	—
26	Gas Calorific Value (Btu/lb)	23346	—	—	Sulfur	0.78	—	—	—	—	—
27	Gas Firing Rate (lb/h)	0	—	—	Oxygen	5.75	—	—	—	—	—
28	Gas Support (% of Heat)	0.00	—	—	Ash	4.19	—	—	—	—	—
29	Fraction of coal	1	—	—	Moisture	3.89	—	—	—	—	—
30	Fraction of GAS	0	—	—	Total	100.00	—	—	—	—	—
31	—	—	—	—	HHV	14444	—	—	—	—	—
32	—	—	—	—	Dry ash%	4.36	—	—	—	—	—
33	—	—	—	—	—	—	—	—	—	—	—
34	—	—	—	—	—	—	—	—	—	—	—
35	—	—	—	—	—	—	—	—	—	—	—
36	—	—	—	—	—	—	—	—	—	—	—
37	—	—	—	—	—	—	—	—	—	—	—
38	—	—	—	—	—	—	—	—	—	—	—
39	—	—	—	—	—	—	—	—	—	—	—
40	—	—	—	—	—	—	—	—	—	—	—
41	—	—	—	—	—	—	—	—	—	—	—
42	—	—	—	—	—	—	—	—	—	—	—

	G	H	I	J	K	L	M	N	O	P	Q
4.3	Calculation of Air Requirement and Theoretical Products of Combustion										
4.4											
4.5											
4.6	Carbon= %C/(100-12) * 1 mole =				Theoretical Oxygen Requirement						
4.7	Hydrogen= %H/(100-12)*0.5 mole =				0.06600354 moles						
4.8	Sulfur= %S/(100-32) * 1 mole =				0.01210986 moles						
4.9					0.00024328 moles						
5.0	Oxygen required= Sum of the 3 Oxygen available In the Fuel= %O/(100-32)				0.07835668 moles						
5.1					0.00179606						
5.2	Net Oxygen required =				0.07656063 moles						
5.3	Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =										
5.4											
5.5											
5.6	Calculation of Products of combustion										
5.7											
5.8	Excess air used (%)				= 100(XO2-CO2)/10.264*1N2*(CO2-CO2)=						
5.9											
6.0	Actual Dry air Required (moles) = (1+E,A%)* total air required =					18.16					
6.1	Dry air In lbs/lb of "as fired" fuel										
6.2											
6.3	Actual wet air used/lb of "as fired" fuel (assuming 60% RH and 80°F) =										
6.4											
6.5											
6.6	Weight of products of combustion = Actual wet air used + weight of fuel=										
6.7											
6.8	Actual weight of products =										
6.9											
7.0											
7.1											
7.2											
7.3											
7.4											
7.5											
7.6											
7.7											
7.8											
7.9											
8.0											
8.1											
8.2											
8.3											
8.4											
8.5											

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4									
5 Carbon Dioxide (=moles of carbon /lb of fuel) (=moles of water in fuel +moles of water in combustion air)									
6 Water			0.06600354	14.71					
7 Oxygen			0.02731322	6.09					
8 Nitrogen			0.01389993	3.10					
9 Sulfur Dioxide			0.34123122	7.65					
10 Total			0.00024328	0.05421957					
11			0.4486912	100.00					
12									
13									
14 Boiler	Efficiency	Calculations							
15									
16	These calculations are based on ASME PTC 4, using heat loss method								
17	1. Pounds of dry gas per pound of "as fired" composite fuel								
18	Wg = ((C% d.b.) + C Efficiency) * (44.01 (CO <sub>2</sub> ) + 32.00 (O <sub>2</sub> ) + 28.02 (N <sub>2</sub> ) + (28.01 (CO)/12.01 (CO <sub>2</sub> +CO)) + 12.01 (S)/32.07								
19	21								
20	Wg = 12.42096983 lb/lb of as fired fuel								
21	22								
22	23								
23	24 1. Heat loss due to dry gas (%)								
24	Lwg = Wg * 0.24 * (359.75)/HHV * 100								
25	25								
26	26 2. Heat loss due to unburned carbon								
27	27								
28	28								
29	29 LUC = % Carbon in the "as Fired Fuel" : (1-Comb. Efficiency) * 14,500								
30	30								
31	31								
32	32 3. Heat loss due to unburned carbon in dust								
33	33								
34	34 4. Heat loss due to moisture in "as Fired Fuel"								
35	35 Moisture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet)/HHV*100								
36	36								
37	37 Lml=								
38	38								
39	39								
40	40								
41	41 5. Heat loss due to moisture produced from burning hydrogen in fuel								
42	42								

R	S	T	U	V	W	X	Y	Z	AA
43 Lmfh=	8.936 "% hydrogen in "as fired" fuel" (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV								
44									
45									
46 Heat loss due to moisture in combustion air									
47 Theoretical lb of air required for complete combustion/lb of "as fired" fuel									
48	$= \frac{(11.52\% \text{ carbon}) + 34.57\% \text{ hydrogen} \% \text{ oxygen}(8)}{0.16}$								
49									
50									
51 Actual dry air =	$(1 + \% \text{ Excess air}/100) \text{ lb/lb of "as fired" fuel}$								
52									
53 Moisture in air =	0.013 lb/lb of dry air								
54									
55 Lma =	0.16257482 lbs/lb of "as fired" fuel								
56									
57									
58 Heat loss due to formation of carbon monoxide									
59	$\text{CO}/(\text{CO}_2 + \text{CO}) \cdot 10^{16} : \text{Combustion Efficiency} \% \text{ carbon in "as fired fuel"}$								
60 Lco =									
61									
62 Heat loss due to radiation									
63	$10 \exp(0.62 - 0.42 \log Q)$								
64									
65									
66									
67									
68 Total Losses (%)									
69 HEAT CREDITS									
70									
71 1. Heat supplied by duct burner to entering air									
72 2. Heat supplied by mill to primary (transport) air									
73									
74 Boiler Efficiency (%) =									
75									
76									
77 Combustion Air Flow (lb/hr) =									
78									
79									
80									
81									
82									
83									
84									
85									

A	B	C	D	E	F
1 Demonstration	8/28/95	Boiler Data			
2 Date of Operation					
3					
4 Pressures and Temperatures					
5					
6 Drum Steam Pressure (PSIG)					
7 Feed Water Temperature (°F)					
8 Steam Quality ( % moisture)					
9 Gas Temp Leaving Boiler (°F)					
10 Gas Temp Leaving Air Heater (°F)					
11 Air Temp Entering Air Heater (°F)					
12 Air Temp leaving Air Pre Heater (°F)					
13 Air Temp Entering Boiler (°F)					
14 Mill Inlet Temperature (°F)					
15 Mill air flow rate (lb/h)					
16 Burner Inlet temperature (°F)					
17 FUEL DATA					
18 Proximate Analysis					
19 Moisture (Wt%)		1.87 Ultimate Analysis (Wt%, d.b)			
20 Volatile Matter (Wt%)		30.82			
21 Fixed Carbon (Wt%)		64.82			
22 Ash (Wt%)		4.37			
23		Carbon			
24 HHV (Btu/lb., d.b)		14490			
25		Hydrogen			
26		Nitrogen			
27		Sulfur			
28		Oxygen			
29		Ash			
30 Flue Gas Analysis		Total			
31					
32 Oxygen (%)				Total	100
33 Carbon Dioxide (%)		3.51		Mixture (wt%)	0.05
34 Carbon Monoxide (PPM)		15.35			
35 Sulfur Dioxide (PPM)		129.16		Ash in Dry Char/Refuse	
36 Oxides of Nitrogen (PPM)		474.10		TOTAL CARBON CONVERSION	47.9
37		384.70		COAL CARBON CONVERSION	94.40
38					94.40
39					
40					
41					
42					

A	B	C	D	E	F
43		Summary of Boiler Performance			
44					
45					
46 Date of Operation	28-Aug				
47					
48					
49					
50					
51 Boiler Operating Conditions					
52					
53					
54 Total Fliring Rate		16.5186479 MMBtu/h			
55 Gas Support (%)		0.00 %			
56 Excess air used (%)		19.52 %			
57					
58 Actual mass of products of combustion =		16096.49797 lb/lb of "as fired" fuel			
59 Theoretical flue gas composition	%				
60 Carbon Dioxide	14.46				
61 Water vapor	6.17				
62 Oxygen	3.29				
63 Nitrogen	76.02				
64 Sulfur Dioxide (ppm)	557				
65 Total	100.00				
66 Boiler Efficiency Details		%			
67					
68					
69 1. Heat loss due to Dry gas (%)		6.20			
70 2. Heat loss due to unburned carbon		4.43			
71 3. Heat loss due to unburned carbon in dust		Negligible			
72 4. Heat loss due to moisture in "as Fired Fuel"		0.37			
73 5. Heat loss due to moisture produced from burning hydrogen in fuel		3.60			
74 6. Heat loss due to moisture in combustion air		0.16			
75 7. Heat loss due to formation of carbon monoxide		0.04			
76 8. Heat loss due to radiation		1.28			
77 9. Heat loss due to steam drum blowdown		0.00			
78 Total Losses		16.08			
79 Heat Credits					
80 1. Heat supplied by duct burner to entering air		72.09	Blu/lb of "as fired fuel"		
81 2. Heat supplied by mill to primary (transport) air		36.56	Blu/lb of "as fired fuel"		
82					
83 BOILER EFFICIENCY (%)		83.88			
84					
85					

1	G	H	I	J	K	L	M	N	O	P	Q
2											
3											
4											
5	Fuel Gas Composition (Dry Vol%)	95.54	Density at 60°F (lb/cu.ft)	0.04246	Gas Composition from Volume % to Wt%	lbs in each cu.ft of gas					
6	Methane	2.48		0.040566628							
7	Ethane	0		0.08029	0.00199119						
8	Propane	0.43		0.1196	0						
9	Butane	0		0.1582	0.00068026						
10	Hydrogen Sulfide	0		0.09109	0						
11	Carbon Dioxide	0		0.117	0						
12	Nitrogen	1.55		0.07439	0.00115305						
13	Total	100									
14											
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	1140									
23	Coal Heat Input(Btu/h)	16518600									
24											
25	Gas Heat Input (Btu/h)	0									
26	Total Firing Rate	16518600									
27	Gas Calorific Value (Btu/lb)	23346									
28	Gas Firing Rate (lb/h)	0									
29	Gas Support % of Heat	0.00									
30	Fraction of coal	1									
31	Fraction of GAS	0									
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

## Conversion of Gas Composition from Volume % to Wt%

6	Methane	95.54	Density at 60°F (lb/cu.ft)	0.04246	Gas Composition from Volume % to Wt%	lbs in each cu.ft of gas					
7	Ethane	2.48		0.08029	0.00199119						
8	Propane	0		0.1196	0						
9	Butane	0.43		0.1582	0.00068026						
10	Hydrogen Sulfide	0		0.09109	0						
11	Carbon Dioxide	0		0.117	0						
12	Nitrogen	1.55		0.07439	0.00115305						
13	Total	100									

Density of N. gas (lb/cu.ft) =

$$0.04439078$$

## Determination of Percent Gas Support

14											
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	1140									
23	Coal Heat Input(Btu/h)	16518600									
24											

25	Gas Heat Input (Btu/h)	0	Density at 60°F (lb/cu.ft)	0.04246	Gas Composition from Volume % to Wt%	lbs in each cu.ft of gas					
26	Total Firing Rate	16518600		0.08029	0.00199119						
27	Gas Calorific Value (Btu/lb)	23346		0.1196	0						
28	Gas Firing Rate (lb/h)	0		0.1582	0.00068026						
29	Gas Support % of Heat	0.00		0.09109	0						
30	Fraction of coal	1		0.117	0						
31	Fraction of GAS	0		0.07439	0.00115305						
32											

33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

## N. Gas Composition (Wt%, d.b)

As Fired

Gas Composition (wt%)

73.40

73.3583626

23.9954486

2.59618878

0

0

0

0

0

0

100.00

100.00

0

0

0

0

0

0

0

0

0

0

0

0

0

HfV

Dry Ash

4.31

4.31

0

0

0

HfV

Dry Ash

0

0

0

0

0

G	H	I	J	K	L	M	N	O	P	Q
<b>4.3 Calculation of Air Requirement and Theoretical Products of Combustion</b>										
4.4										
4.5 Carbon= %C/(100-12) *1 mole =				Theoretical Oxygen Requirement						
4.6 Hydrogen= %H/(100-12) *0.5 mole =				0.06587908 moles						
4.7 Sulfur= %S/(100-32) *1 mole =				0.012395 moles						
4.8				0.00025367 moles						
4.9 Oxygen required= Sum of the 3										
50 Oxygen available In the Fuel= %O/(100-32)				0.07845226 moles						
51 Net Oxygen required =				0.00163842 moles						
52 Net Oxygen required =				0.07681383 moles						
53 Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =										
54				0.36578016 moles/lb of as fired fuel						
55										
<b>56 Calculation of Products of combustion</b>										
57										
58 Excess air used (%)										
59										
60 Actual Dry air Required (moles) = (1+E,A%) * total air required =										
61 Dry air In lbs/lb of "as fired" fuel				= moles of air*29.97 =						
62										
63 Actual wet air used/lb of "as fired" fuel (assuming 60% R.H and 80°F)=										
64										
65				lbs of dry air : 1.0013						
66 Weight of products of combustion = Actual wet air used + weight of fuel=										
67										
68 Actual weight of products =										
69										
70										
71										
72										
73										
74										
75										
76										
77										
78										
79										
80										
81										
82										
83										
84										
85										

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4									
5 Carbon Dioxide	(=moles of carbon /lb of fuel)	0.06587908	Wet Flue Gas Composition (%)	14.46	Dry Flue Gas Comp. (%)	15.41			
6 Water	(moles of water in fuel + moles of water in combustion air)	0.02808531		6.17		0.00			
7 Oxygen		0.01499689		3.29		3.51			
8 Nitrogen		0.3463104		76.02		81.02			
9 Sulfur Dioxide		0.00025367		0.05568776		0.06			
10 Total		0.45552535		100.00		100.00			
11									
12									
13									
14 Boiler Efficiency	Efficiency	Calculations							
15									
16	These calculations are based on ASME PTG 4, using heat loss method								
17									
18	1. Pounds of dry gas per pound of "as fired" composite fuel								
19	Wg =								
20	(fc% d.b) * C.Efficiency *(44.01 *(CO2) + 32.00 *(O2) + 28.02 *(N2) + (28.01 *(CO)/12.01 *(CO2+CO)) + 12.01 *(S)/32.07								
21									
22	12.383991157 lb/lb of as fired fuel								
23	2. Heat loss due to dry gas (%)	Lwg = Wg * 0.24 * (359.75)/HHV * 100							
24									
25									
26	2. Heat loss due to unburned carbon								
27									
28	3. Heat loss due to moisture in the "as fired Fuel"	% Carbon in the "as fired Fuel" * (1-Comb.Efficiency) * 14,500							
29	Luc =								
30									
31									
32	3. Heat loss due to unburned carbon in dust								
33									
34	4. Heat loss due to moisture in "as Fired Fuel"								
35									
36	Molsture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet)/HHV*100								
37									
38									
39									
40	5. Heat loss due to moisture produced from burning hydrogen in fuel								
41									
42									

	R	S	T	U	V	W	X	Y	Z	AA
43	Lmfh=	B.936 % hydrogen in "as fired" fuel" (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV								
44										
45										
46	6. Heat loss due to moisture in combustion air									
47	Theoretical lb of air required for complete combustion/lb of "as fired" fuel									
48	=	(11.52(% carbon) + 34.57(% hydrogen-% oxygen)/8) + 4.32 (% sulfur))/HHV=								
49										
50										
51	Actual dry air =	(14% Excess air/100) lb/lb of "as fired" fuel								
52		12.69 lb								
53	Moisture in air =	0.013 lb /lb of dry air								
54	Lma =	moisture in air * (enthalpy of water vapor leaving air heater - enthalpy of vapor at mill inlet temp.)								
55										
56										
57										
58										
59	7. Heat loss due to formation of carbon monoxide									
60	Lco =	CO/(CO <sub>2</sub> +CO)·10160 : Combustion Efficiency								
61		% carbon in "as fired" fuel								
62										
63	8. Heat loss due to radiation	10 exp (0.62-0.42log O)								
64										
65										
66										
67										
68	Total Losses (%)									
69	HEAT CREDITS									
70										
71	1. Heat supplied by duct burner to entering air									
72	2. Heat supplied by mill to primary (transport) air									
73										
74	Boiler Efficiency (%)=									
75										
76										
77	Combustion Air Flow (lb/hr)=									
78										
79										
80										
81										
82										
83										
84										
85										

A	B	Boiler Data	C	D	E	F
1 Demonstration						
2 Date of Operation	8/29/95					
3	19.0lb/min coal; Prim. 0%, Sec. 0%, Tert. 100%;Coal gun -9";Xter 400 acfm; O2 3.75%					
4 Pressures and Temperatures						
5						
6 Drum Steam Pressure (Psi)		183.3 Enthalpy of Sat. Ltg. (Btu/lb)		343.2		
7 Food Water Temperature (°F)		206.3 Enthalpy of Feed Water (Btu/lb)		174.5 (Sat. liquid @ Feed water temp.)		
8 Steam Quality (% moisture)		99.3 Steam Production Rate (PPH)		13,938.2		
9 Gas Temp.Leaving Boiler (°F)		560.8 Blow down Rate (PPH)		2,966.2		
10 Gas Temp. Leaving Air Heater (°F)		388.9 Enthalpy of water vapor at Givg Temp (Btu/lb)		1,236.6 (Sup. steam @ 1psia&gas lvg temp)		
11 Air Temp Entering Air Heater (°F)		177.2 Enthalpy of water at fuel inlet temp. (Btu/lb)		55.6 (Sat. liq. @ mill inlet temp.)		
12 Air temp leaving Air Pre Heater (°F)		406.3 Enthalpy of vapor at fuel inlet temp. (Btu/lb)		1,096.3 (Sat. vapor @ mill inlet temp.)		
13 Air Temp Entering Boiler (°F)		387.1 Calorimeter Temperature (°F)		301.4		
14 Mill Inlet Temperature (°F)		87.6				
15 Mill air flow rate (lb/h)		1,685.2 Coal Flying Rate (lb/h)		1140 Gas Flying Rate (lb/h)		
16 Burner Inlet Temperature (°F)		180.3 Coal H.H. Value (Btu/lb)		14,490 Gas Cal. Value (Btu/lb)		0
17 FUEL DATA		Coal Moisture Content (%)		4.51		233.46
18 Proximate Analysis						
19 Moisture (Wt%)		1.79 Ultimate Analysis (Wt% d.b)				
20 Volatile Matter (Wt%)		30.94				
21 Fixed Carbon (Wt%)		64.75				
22 Ash (Wt%)		4.26 Carbon		82.78 Methane		95.54
23		Hydrogen		5.16 Ethane		2.48
24 HHV (Btu/lb, d.b)		14490 Nitrogen		1.41 Propane		0
25		Sulfur		0.85 Butane		0.43
26		Oxygen		5.49 Hydrogen Sulfide		0
27		Ash		4.31 Carbon Dioxide		1.55
28		Total		100 Nitrogen		
29				Others		
30 Flue Gas Analysis				Total		100
31				Moisture (wt%)		0.05
32 Oxygen (%)		3.55				
33 Carbon Dioxide (%)		15.40	Ash In Dry Char/Refuse			
34 Carbon Monoxide (PPM)		165.58	TOTAL CARBON CONVERSION			
35 Sulfur Dioxide (PPM)		511.21	COAL CARBON CONVERSION			
36 Oxides of Nitrogen (PPM)		361.43				
37						
38						
39						
40						
41						
42						

A	B	C	D	E	F
43					
44					
45					
46 Date of Operation	29-Aug				
47					
48					
49					
50					
51 Boiler Operating Conditions					
52					
53					
54 Total Firing Rate		16.51865049 MMBtu/h			
55 Gas Support (%)		0.00 %			
56 Excess air used (%)		19.83 %			
57					
58 Actual mass of products of combustion =		16133.72495 lb/lb of "as fired" fuel			
59					
60 Theoretical flue gas composition %					
61 Carbon Dioxide	14.43				
62 Water vapor	6.15				
63 Oxygen	3.34				
64 Nitrogen	76.03				
65 Sulfur Dioxide (ppm)	555				
66 Total	100.00				
67 Boiler Efficiency Details		%			
68					
69 1. Heat loss due to Dry gas (%)		6.24			
70 2. Heat loss due to unburned carbon		3.40			
71 3. Heat loss due to unburned carbon in dust		Negligible			
72 4. Heat loss due to moisture in "as Fired Fuel"		0.37			
73 5. Heat loss due to moisture produced from burning hydrogen in fuel		3.59			
74 6. Heat loss due to moisture in combustion air		0.16			
75 7. Heat loss due to formation of carbon monoxide		0.06			
76 8. Heat loss due to radiation		1.20			
77 9. Heat loss due to steam drum blowdown		0.00			
78 Total Losses		15.18			
79 Heat Credits					
80 1. Heat supplied by duct burner to entering air					-60.56 Btu/lb of "as fired fuel"
81 2. Heat supplied by mill to primary (transport) air					33.65 Btu/lb of "as fired fuel"
82					
83 BOILER EFFICIENCY (%)					84.79
84					
85					

G	H	I	J	K	L	M	N	O	P	Q
1										
2										
3										
4										
5	Fuel Gas Composition (Dy. Vol%)									
6	Methane	95.54								
7	Ethane	2.48	0.04246	0.04056628						
8	Propane	0	0.08029	0.00199119						
9	Bulane	0.43	0.1196	0						
10	Hydrogen Sulfide	0	0.1582	0.00068026						
11	Carbon Dioxide	0	0.09109	0						
12	Nitrogen	1.55	0.117	0						
13	Total	100	0.07439	0.00115305						
14	Density of N. gas (lb/cu.ft) =	0.04439078								
15										
16										
17										
18	Determination of Percent Gas Support									
19										
20										
21										
22	Coal Firing Rate (lb/h)	1140								
23	Coal Heat Input (Btu/h)	16518600								
24										
25	Gas Heat Input (Btu/h)	0								
26	Total Firing Rate	16518600								
27	Gas Calorific Value (Btu/b)	23346								
28	Gas Firing Rate (lb/h)	0								
29	Gas Support (% of Heat)	0.00								
30	Fraction of coal	1								
31	Fraction of GAS	0								
32										
33										
34										
35										
36										
37										
38										
39										
40										
41										
42										

G	H	I	J	K	L	M	N	O	P	Q
<b>43 Calculation of Air Requirement and Theoretical Products of Combustion</b>										
44										
45										
46 Carbon= %C/(100*12) *1 mole =				Theoretical Oxygen Requirement						
47 Hydrogen= %H/(100*2)*0.5 mole =				0.06587219 moles						
48 Sulfur= %S/(100*32) *1 mole =				0.01231821 moles						
49				0.00025365 moles						
50 Oxygen required= Sum of the 3										
51 Oxygen available in the Fuel= %O/(100*32)				0.07844404 moles						
52 Net Oxygen required =				0.00163825						
53 Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =				0.07680579 moles						
54										
55				0.36574186 moles/lb of as fired fuel						
<b>56 Calculation of Products of combustion</b>										
57										
58 Excess air used (%)				= 10XO2(CO2)/(0.261*N2*(CO2))=						
59										
60 Actual Dry air Required (moles) = (1+E.A%)* total air required =				19.83						
61 Dry air in lbs/lb of "as fired" fuel										
62				= moles of air*29.97 =						
63 Actual wet air used/lb of "as fired" fuel (assuming 60% R.H and 80°F)=				0.4382821						
64				13.1553144						
65				13.1523903						
66 Weight of products of combustion = Actual wet air used + weight of fuel=										
67										
68 Actual weight of Products =				14.1523903 lb/lb of fuel						
69				16133.7249 lb of flue gas						
70										
71										
72										
73										
74										
75										
76										
77										
78										
79										
80										
81										
82										
83										
84										
85										

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4									
5 Carbon Dioxide	(moles of carbon /lb of fuel)		0.065872.9	14.43			Dry Flue Gas Comp. (%)	15.37	
6 Water	( moles of water in fuel + moles of water in combustion air)		0.02809064	6.15				0.00	
7			0.01523345	3.34				3.55	
8 Oxygen			0.34717007	76.03				81.01	
9 Nitrogen			0.00025365	0.05554845				0.06	
10 Sulfur Dioxide			0.45661998	100.00				100.00	
11 Total									
12									
13 Boiler	Efficiency	Calculations							
14									
15									
16	These calculations are based on ASME PTG-4, using heat loss method								
17									
18	1. Pounds of dry gas per pound of "as fired" composite fuel								
19									
20	Wg' =	C.Efficiency * (44.01 * (CO2) + 32.00 * (O2) + 28.02 * (N2) + (28.01 * (CO)) + 12.01 * (S)/32.07)							
21									
22	12.50466265 lb/lb of as fired fuel								
23									
24	1. Heat loss due to dry gas (%)	Lwg' = Wg' * 0.24 * (359.75)/HHV * 100							
25									
26	2. Heat loss due to unburned carbon								
27									
28	Luc = % Carbon in the "as fired Fuel" * (1-Comb.Efficiency) * 14,500								
29									
30									
31	3. Heat loss due to unburned carbon in dust								
32									
33	4. Heat loss due to moisture in "as Fired Fuel"								
34									
35	Moisture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet)/HHV*100								
36									
37	Lmi=								
38									
39									
40	5. Heat loss due to moisture produced from burning hydrogen in fuel								
41									
42									

R	S	T	U	V	W	X	Y	Z	AA
43 $L_m(h) =$	8.936 *% hydrogen in "as fired" fuel* (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV								
44									
45									
46 <b>6. Heat loss due to moisture in combustion air</b>	<b>Theoretical lb of air required for complete combustion/lb of "as fired" fuel</b>								
47	$= \frac{(11.52(\% \text{ carbon}) + 34.57(\% \text{ hydrogen}-\% \text{ oxygen}8) + 4.32 (\% \text{ sulfur})}/\text{HHV}}{0.16541221 \text{ lbs/lb of "as fired" fuel}}$								
48									
49									
50									
51									
52 <b>Actual dry air =</b>	<b>(1+%) Excess air/100) lb/lb of "as fired" fuel</b>								
53	$= 12.72/\text{lb}$								
54 <b>Moisture in air =</b>	<b>0.013 lb /lb of dry air</b>								
55	<b>moisture in air : (enthalpy of water vapor leaving air heater - enthalpy of vapor at mill inlet temp.)</b>								
56									
57									
58									
59 <b>7. Heat loss due to formation of carbon monoxide</b>	<b><math>\text{CO}/(\text{CO}_2+\text{CO})10^{16}0 : \text{Combustion Efficiency} * \% \text{ carbon in "as fired fuel}}</math></b>								
60	$\text{LCO} =$								
61									
62									
63 <b>8. Heat loss due to radiation</b>	<b><math>10 \exp(0.62-0.42 \log Q)</math></b>								
64									
65									
66									
67									
68 <b>Total Losses (%)</b>	<b>15.18 %</b>								
69 <b>HEAT CREDITS</b>									
70									
71	1. Heat supplied by duct burner to entering air								
72	2. Heat supplied by mill to primary (transport) air								
73									
74 <b>Boiler Efficiency (%) =</b>	<b>84.79 %</b>								
75									
76									
77 <b>Combustion Air Flow (lb/hr) =</b>	<b>14694 lb/h</b>								
78									
79									
80									
81									
82									
83									
84									
85									

A	B	C	D	E	F
1 Demonstration					
2 Date of Operation	8/30/95				
3	19.0lb/min coal; Prim. 100%, Sec. 100%, Tert. 50%;Coal gun -9";Xfer 390 acfm; O2 3.75%				
4 Pressures and Temperatures					
5					
6 Drum Steam Pressure (Psi)					
7 Feed Water Temperature (°F)	186.1 Enthalpy of Sat. Liq. (Btu/lb)	344.4			
8 Steam Quality (% moisture)	207.6 Enthalpy of Feed Water (Btu/lb)	175.7 (Sat. liquid @ Feed water temp.)			
9 Gas Temp Leaving Boiler (°F)	99.4 Steam Production Rate (PPH)	14,138.7			
10 Gas Temp Leaving Air Heater (°F)	565.5 Blow down Rate (PPH)	2,988.5			
11 Air Temp Entering Air Heater (°F)	389.8 Enthalpy of water vapor at Givg Temp (Btu/lb)	1,237.0 (Sup. steam @ 1psi&gas lvg temp)			
12 Air Temp Leaving Air Pre Heater (°F)	173.0 Enthalpy of water at fuel inlet temp. (Btu/lb)	59.1 (Sat. liq. @ mill inlet temp.)			
13 Air Temp Entering Boiler (°F)	405.6 Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1,096.3 (Sat. vapor @ mill inlet temp.)			
14 Mill Inlet Temperature (°F)	385.1 Calorimeter Temperature (°F)	301.8			
15 Mill air flow rate (lb/h)	91.1				
16 Burner Inlet temperature (°F)	1,838.0 Coal Firing Rate (lb/h)	1140	Gas Firing Rate (lb/h)		
17 FUEL DATA	179.9 Coal H.H. Value (Btu/lb)	14490	Gas Cal. Value (Btu/lb)	0	23346
18 Proximate Analysis	Coal Moisture Content (%)	4.35			
19 Moisture (Wt%)	1.87 Ultimate Analysis (Wt% d.b)		Gas Analysis (Dry Vol%)		
20 Volatile Matter (Wt%)	30.82				
21 Fixed Carbon (Wt%)	64.82				
22 Ash (Wt%)	4.37 Carbon	82.78 Methane	95.54		
23	Hydrogen	5.16 Ethane	2.48		
24 HHV (Btu/lb, d.b)	14490 Nitrogen	1.41 Propane	0		
25	Sulfur	0.85 Butane	0.43		
26	Oxygen	5.49 Hydrogen Sulfide	0		
27	Ash	4.31 Carbon Dioxide	1.55		
28	Total	100 Nitrogen			
29		Others			
30 Flue Gas Analysis		Total	100		
31		Moisture (wt%)	0.05		
32 Oxygen (%)	3.80				
33 Carbon Dioxide (%)	15.30	53.13			
34 Carbon Monoxide (PPM)	113.54	95.90			
35 Sulfur Dioxide (PPM)	537.82	95.90			
36 Oxides of Nitrogen (PPM)	324.73				
37					
38					
39					
40					
41					
42					

A	B	C	D	E	F
43		Summary of Boiler Performance			
44					
45					
46 Date of Operation	30-Aug				
47					
48					
49					
50					
51 Boiler Operating Conditions					
52					
53					
54 Total Firing Rate		16.51065313 MMBtu/h			
55 Gas Support (%)		0.00 %			
56 Excess air used (%)		21.60 %			
57					
58 Actual mass of products of combustion =		16380.19131 lb/lb of "as fired" fuel			
59					
60 Theoretical flue gas composition	%				
61 Carbon Dioxide		14.23			
62 Water vapor		6.05			
63 Oxygen		3.58			
64 Nitrogen		76.08			
65 Sulfur Dioxide (ppm)		548			
66 Total		100.00			
67 Boiler Efficiency Details					
68					
69 1. Heat loss due to Dry gas (%)			6.26		
70 2. Heat loss due to unburned carbon			3.25		
71 3. Heat loss due to unburned carbon in dust			Negligible		
72 4. Heat loss due to moisture in "as Fired Fuel"			0.35		
73 5. Heat loss due to moisture produced from burning hydrogen in fuel			3.59		
74 6. Heat loss due to moisture in combustion air			0.16		
75 7. Heat loss due to formation of carbon monoxide			0.04		
76 8. Heat loss due to radiation			1.28		
77 9. Heat loss due to steam drum blowdown			0.00		
78 Total Losses			14.93		
79 Heat Credits					
80 1. Heat supplied by duct burner to entering air			66.12	Blw/b of "as fired fuel"	
81 2. Heat supplied by mill to primary (transport) air			35.14	Blw/b of "as fired fuel"	
82					
83 BOILER EFFICIENCY (%)			85.04		
84					
85					

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	8010	8011	8012	8013	8014	8015	8016	8017	8018	8019	8020	8021	8022	8023	8024	8025	8026	8027	8028	8029	8030	8031	8032	8033	8034	8035	8036	8037	8038	8039	8040	8041	8042	8043	8044	8045	8046	8047	8048	8049	8050	8051	8052	8053	8054	8055	8056	8057	8058	8059	8060	8061	8062	8063	8064	8065	8066	8067	8068	8069	8070	8071	8072	8073	8074	8075	8076	8077	8078	8079	8080	8081	8082	8083	8084	8085	8086	8087	8088	8089	8090	8091	8092	8093	8094	8095	8096	8097	8098	8099	80100	80101	80102	80103	80104	80105	80106	80107	80108	80109	80110	80111	80112	80113	80114	80115	80116	80117	80118	80119	80120	80121	80122	80123	80124	80125	80126	80127	80128	80129	80130	80131	80132	80133	80134	80135	80136	80137	80138	80139	80140	80141	80142	80143	80144	80145	80146	80147	80148	80149	80150	80151	80152	80153	80154	80155	80156	80157	80158	80159	80160	80161	80162	80163	80164	80165	80166	80167	80168	80169	80170	80171	80172	80173	80174	80175	80176	80177	80178	80179	80180	80181	80182	80183	80184	80185	80186	80187	80188	80189	80190	80191	80192	80193	80194	80195	80196	80197	80198	80199	80200	80201	80202	80203	80204	80205	80206	80207	80208	80209	80210	80211	80212	80213	80214	80215	80216	80217	80218	80219	80220	80221	80222	80223	80224	80225	80226	80227	80228	80229	80230	80231	80232	80233	80234	80235	80236	80237	80238	80239	80240	80241	80242	80243	80244	80245	80246	80247	80248	80249	80250	80251	80252	80253	80254	80255	80256	80257	80258	80259	80260	80261	80262	80263	80264	80265	80266	80267	80268	80269	80270	80271	80272	80273	80274	80275	80276	80277	80278	80279	80280	80281	80282	80283	80284	80285	80286	80287	80288	80289	80290	80291	80292	80293	80294	80295	80296	80297	80298	80299	80300	80301	80302	80303	80304	80305	80306	80307	80308	80309	80310	80311	80312	80313	80314	80315	80316	80317	80318	80319	80320	80321	80322	80323	80324	80325	80326	80327	80328	80329	80330	80331	80332	80333	80334	80335	80336	80337	80338	80339	80340	80341	80342	80343	80344	80345	80346	80347	80348	80349	80350	80351	80352	80353	80354	80355	80356	80357	80358	80359	80360	80361	80362	80363	80364	80365	80366	80367	80368	80369	80370	80371	80372	80373	80374	80375	80376	80377	80378	80379	80380	80381	80382	80383	80384	80385	80386	80387	80388	80389	80390	80391	80392	80393	80394	80395	80396	80397	80398	80399	80400	80401	80402	80403	80404	80405	80406	80407	80408	80409	80410	80411	80412	80413	80414	80415	80416	80417	80418	80419	80420	80421	80422	80423	80424	80425	80426	80427	80428	80429	80430	80431	80432	80433	80434	80435	80436	80437	80438	80439	80440	80441	80442	80443	80444	80445	80446	80447	80448	80449	80450	80451	80452	80453	80454	80455	80456	80457	80458	80459	80460	80461	80462	80463	80464	80465	80466	80467	80468	80469	80470	80471	80472	80473	80474	80475	80476	80477	80478	80479	80480	80481	80482	80483	80484	80485	80486	80487	80488	80489	80490	80491	80492	80493	80494	80495	80496	80497	80498	80499	80500	80501	80502</th

G	H	I	J	K	L	M	N	O	P	Q
<b>4.3 Calculation of Air Requirement and Theoretical Products of Combustion</b>										
4.4										
4.5										
4.6	Carbon = %C/(100-12) * 1 mole =			Theoretical Oxygen Requirement						
4.7	Hydrogen = %H/(100-2) * 0.5 mole =			0.06598256 moles						
4.8	Sulfur = %S/(100-32) * 1 mole =			0.01233885 moles						
4.9				0.00025407 moles						
5.0	Oxygen required = Sum of the 3									
5.1	Oxygen available In the Fuel = %O/(100-32)			0.07857548 moles						
5.2	Net Oxygen required =			0.001641 moles						
5.3	Theoretical Dry Air for Combustion = Net Oxygen required / 0.21 =			0.07693448 moles						
5.4										
5.5										
5.6	<b>Calculation of Products of combustion</b>									
5.7										
5.8	Excess air used (%)			= 100(O2-CO2)/(102-102-CO2)=						
5.9					21.60					
6.0	Actual Dry air Required (moles)	= (1+E,A%) * total air required =								
6.1	Dry air in lbs/lb of "as fired" fuel									
6.2										
6.3	Actual wet air used/lb of "as fired" fuel (assuming 60% R.H and 80°F) =									
6.4										
6.5										
6.6	Weight of products of combustion = Actual wet air used + weight of fuel =									
6.7										
6.8	Actual weight of products =									
6.9										
7.0										
7.1										
7.2										
7.3										
7.4										
7.5										
7.6										
7.7										
7.8										
7.9										
8.0										
8.1										
8.2										
8.3										
8.4										
8.5										

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4	Carbon Dioxide	=moles of carbon /lb of fuel)	0.06598256	Wet Flue Gas Composition (%)		Dry Flue Gas Comp. (%)			
5	Water	(moles of water in fuel + moles of water in combustion air)	0.02805862	14.23	15.14				
6	Oxygen		0.01661769	6.05	0.00				
7	Nitrogen		0.35286159	3.58	3.81				
8	Sulfur Dioxide		0.00025407	76.08	80.98				
9	Total		0.46377454	0.05478315	0.06				
10				100.00	100.00				
11									
12									
13	Boiler	Efficiency							
14		Calculations							
15									
16	These calculations are based on ASME PTC 4, using heat loss method								
17	1. Pounds of dry gas per pound of "as fired" composite fuel								
18	Wg = ((C% db) * C.Efficiency *(44.01 (CO2) + 32.00 (O2) + 28.02 (N2) + (20.01 (CO)/12.01 (CO2+CO)) + 12.01 (S)/32.07								
19									
20	Wg = 12.64431686 lb/lb of as fired fuel								
21									
22	1. Heat loss due to dry gas (%)	Lwg = Wg * 0.24 * (359.75)/HHV * 100							
23									
24	2. Heat loss due to unburned carbon								
25									
26	3. Heat loss due to moisture in "as Fired Fuel"								
27									
28	4. Heat loss due to moisture in "as Fired Fuel"								
29									
30	Moisture In Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at milli liter)/HHV * 100								
31									
32	5. Heat loss due to moisture produced from burning hydrogen in fuel								
33									
34									
35									
36									
37									
38									
39									
40									
41									
42									

R	S	T	U	V	W	X	Y	Z	AA
43 Lmlh=	8.936 % hydrogen in "as fired" fuel (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV								
44									
45									
46 6. Heat loss due to moisture in combustion air	Theoretical lb of air required for complete combustion/lb of "as fired" fuel								
47	(11.52% carbon) + 34.57(% hydrogen-% oxygen/8) + 4.32 (% sulfur))/HHV=								
48									
49									
50									
51									
52 Actual dry air =	10.64 lb/lb of "as fired" fuel								
53									
54 Moisture in air =	(1+% Excess air/100) lb/lb of "as fired" fuel								
55	12.93lb								
56									
57									
58									
59 7. Heat loss due to formation of carbon monoxide	0.013 lb /lb of dry air moisture in air (enthalpy of water vapor leaving air heater - enthalpy of vapor at mill inlet temp.)								
60 LCO =	CO/(CO <sub>2</sub> +CO):10160 * Combustion Efficiency * % carbon in "as fired" fuel								
61									
62									
63 8. Heat loss due to radiation	10 exp (0.62-0.42log Q)								
64									
65									
66									
67									
68 Total Losses (%)									
69 HEAT CREDITS									
70									
71 1. Heat supplied by duct burner to entering air									
72 2. Heat supplied by mill to primary (transport) air									
73									
74 Boiler Efficiency (%)=									
75									
76									
77 Combustion Air Flow (lb/hr)=	14935 lb/h								
78									
79									
80									
81									
82									
83									
84									
85									

A	B	C	D	E	F
1 Demonstration		Boiler Data			
2 Date of Operation	8/31/95				
3					
4 Pressures and Temperatures					
5					
6 Drum Steam Pressure (PSig)					
7 Feed Water Temperature (°F)					
8 Steam Quality (% moisture)					
9 Gas Temp.Leaving Boiler (°F)					
10 Gas Temp. Leaving Air Heater (°F)					
11 Air Temp Entering Air Heater (°F)					
12 Air temp leaving Air Pre Heater (°F)					
13 Air Temp Entering Boiler (°F)					
14 Mill Inlet Temperature (°F)					
15 Mill air flow rate (lb/h)					
16 Burner Inlet temperature (°F)					
17 FUEL DATA					
18 Proximate Analysis					
19 Moisture (Wt%)					
20 Volatile Matter (Wt%)					
21 Fixed Carbon (Wt%)					
22 Ash (Wt%)					
23					
24 HHV (Btu/lb., d.b.)					
25					
26					
27					
28					
29					
30 Flue Gas Analysis					
31					
32 Oxygen (%)					
33 Carbon Dioxide (%)					
34 Carbon Monoxide (PPM)					
35 Sulfur Dioxide (PPM)					
36 Oxides of Nitrogen (PPM)					
37					
38					
39					
40					
41					
42					

19.0lb/min coal; Prim. 100%, Sec. 100%, Tert. 50%;Coal gun -10.5";Gas Gun -9";Xfer 300 actin; O2 3.5%					
<b>Steam Data</b>					
186.0 Enthalpy of Sat. Liq. (Btu/lb)	344.4				
207.4 Enthalpy of Feed Water (Btu/lb)	175.5	(Sat. liquid @ Feed water temp.)			
99.3 Steam Production Rate (PPH)	13,601.1				
570.9 Blow down flate (PPH)	2,908.3				
390.8 Enthalpy of water vapor at Givg Temp (Btu/lb)	1,237.5	(Sup. steam @ 1psia&gas lvg temp)			
175.2 Enthalpy of water at fuel inlet temp. (Btu/lb)	51.1	(Sat. liq. @ mill inlet temp.)			
411.4 Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1,096.3	(Sat. vapor @ mill inlet temp.)			
388.6 Calorimeter Temperature (°F)	301.6				
83.1					
1,870.8 Coal Firing Rate (lb/h)	1140	Gas Firing Rate (lb/h)			
172.6 Coal I.H. Value (Btu/lb)	14490	Gas Cal. Value (Btu/lb)	0		
Coal Moisture Content (%)	1.79				23346
<b>Gas Analysis (Dry Vol%)</b>					
82.78 Methane	95.54				
5.16 Ethane	2.48				
1.41 Propane	0				
0.85 Butane	0.43				
Oxygen	5.49	Hydrogen Sulfide	0		
Ash	4.31	Carbon Dioxide	1.55		
Total	100	Nitrogen			
		Others			
		Total	100		
		Moisture (wt%)	0.05		

TOTAL CARBON CONVERSION

COAL CARBON CONVERSION

50.37

95.29

95.29

A	B	C	D	E	F
43					
44					
45					
46 Date of Operation	31-Aug				
47					
48					
49					
50					
51 Boiler Operating Conditions					
52					
53					
54 Total Firing Rate		16.51865037 MMBtu/h			
55 Gas Support (%)		0.00 %			
56 Excess air used (%)		19.19 %			
57					
58 Actual mass of products of combustion =		16477.64683 lb/lb of "as fired" fuel			
59					
60 Theoretical flue gas composition %					
61 Carbon Dioxide		14.55			
62 Water vapor		5.86			
63 Oxygen		3.26			
64 Nitrogen		76.27			
65 Sulfur Dioxide (ppm)		560			
66 Total	100.00				
67 Boiler Efficiency Details					
68					
69 1. Heat loss due to D/F gas (%)					
70 2. Heat loss due to unburned carbon					
71 3. Heat loss due to unburned carbon in dust					
72 4. Heat loss due to moisture in "as Fired Fuel"					
73 5. Heat loss due to moisture produced from burning hydrogen in fuel					
74 6. Heat loss due to moisture in combustion air					
75 7. Heat loss due to formation of carbon monoxide					
76 8. Heat loss due to radiation					
77 9. Heat loss due to steam drum blowdown					
78 Total Losses				0.00	
79 Heat Credits				15.64	
80 1. Heat supplied by duct burner to entering air					
81 2. Heat supplied by mill to primary (transport) air					
82					
83 BOILER EFFICIENCY (%)					
84					
85					

	G	H	I	J	K	L	M	N	O	P	Q
1											
2											
3											
4											
5	Fuel Gas Composition (Dry Vol%)	Conversion of Gas Composition from Volume % to Wt%									
6	Methane	95.54	Density at 60°F (lb/cu.ft)	0.04246	lbs in each cu.ft of gas						
7	Ethane	2.46		0.04056628							
8	Propane	0		0.00199119							
9	Butane	0.43		0.1196							
10	Hydrogen Sulfide	0		0.1582							
11	Carbon Dioxide	0		0.00068026							
12	Nitrogen	1.55		0.09109							
13	Total	100		0.117							
14				0.07439	0.00115305						
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	1140	As Fired Coal Composition (wt)	81.30	"As Fired" Fuel (coal+nat. gas) Composition (wt%)						
23	Coal Heat Input(Btu/h)	16518600	Carbon	5.07	Carbon	81.30					
24	Gas Heat Input (Btu/h)	0	Hydrogen	1.38	Hydrogen	5.07					
25	Total Firing Rate	16518600	Nitrogen	0.83	Nitrogen	1.38					
26	Gas Calorific Value (Btu/lb)	23346	Sulfur	5.39	Sulfur	0.83					
27	Gas Firing Rate (lb/h)	0	Oxygen	4.23	Oxygen	5.39					
28	Gas Support (% of Heat)	0.00	Ash	1.79	Ash	4.23					
29	Fraction of coal	1	Moisture	100.00	Moisture	1.79					
30	Fraction of GAS	0	Total		Total	100.00					
31											
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

	G	H	I	J	K	L	M	N	O	P	Q
43	Calculation of Air Requirement and Theoretical Products of Combustion										
44											
45											
46	Carbon = %C/(100·12) mole =				Theoretical Oxygen Requirement						
47	Hydrogen = %H/(100·2) 0.5 mole =				0.06774853 moles						
48	Sulfur = %S/(100·32) 1 mole =				0.01266909 moles						
49					0.00026087 moles						
50	Oxygen required = Sum of the 3 Oxygen available in the Fuel = %O/(100·32)				0.08067849 moles						
51					0.00168492 moles						
52	Net Oxygen required =				0.07899358 moles						
53	Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =										
54					0.37615989 moles/lb of as fired fuel						
55											
56	Calculation of Products of combustion										
57											
58	Excess air used (%)				= 100(2·CO2)/(0.264·N2·(O2·CO2)) =						
59					19.19						
60	Actual Dry air Required (moles) = (1+E.A%) · total air required =				0.44833529						
61	Dry air in lbs/lb of "as fired" fuel				13.4366086						
62											
63	Actual wet air used/lb of "as fired" fuel (assuming 60% R.H and 80°F) =				13.4540762						
64											
65	lbs of dry air · 1.0013										
66	Weight of products of combustion = Actual wet air used + weight of fuel										
67											
68	Actual weight of products =				14.4540762 lb/lb of fuel						
69					16477.6448 lb of flue gas						
70											
71											
72											
73											
74											
75											
76											
77											
78											
79											
80											
81											
82											
83											
84											
85											

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4									
5 Carbon Dioxide	(=moles of carbon /lb of fuel)	0.06774853	Wet Flue Gas Composition (%)			Dry Flue Gas Comp. (%)			
6 Water	(moles of water in fuel + moles of water in combustion air)	0.02730305	14.55	15.46					
7		0.01515683	5.86	0.00					
8 Oxygen		0.01515683	3.26	3.46					
9 Nitrogen		0.35511209	76.27	81.02					
10 Sulfur Dioxide		0.00026087	0.05603109	0.06					
11 Total		0.46558137	100.00	100.00					
12									
13									
14 Boiler	Efficiency	Calculations							
15									
16	These calculations are based on ASME PTC 4.1 using heat loss method								
17	1. Pounds of dry gas per pound of "fired" composite fuel								
18	Wg = ((C% db) + C Efficiency) * (44.01 (CO <sub>2</sub> ) + 32.00 (O <sub>2</sub> ) + 28.02 (N <sub>2</sub> ) + (28.01 (CO)/12.01 (CO <sub>2</sub> +CO)) + 12.01 (S)/32.07								
19									
20									
21	12.68718171	lb/lb of "as fired" fuel							
22									
23									
24	1. Heat loss due to dry gas (%)	Lwg' = Wg' * 0.24 * (359.75)/HHV * 100		6.47					
25									
26									
27	2. Heat loss due to unburned carbon								
28									
29	WUC = % Carbon in "as fired Fuel" * (1 - Comb. Efficiency) * 14.500			3.83					
30									
31									
32	3. Heat loss due to unburned carbon in dust	Negligible							
33									
34									
35	4. Heat loss due to moisture in "as Fired Fuel"								
36									
37	Wml = Moisture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill inlet)/HHV * 100			0.15					
38									
39									
40	5. Heat loss due to moisture produced from burning hydrogen in fuel			3.71					
41									
42									

	R	S	T	U	V	W	X	Y	Z	AA
43	Lmfh=	0.936 % hydrogen in "as fired" fuel" (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV								
44										
45										
46	6. Heat loss due to moisture in combustion air									
47	Theoretical lb of air required for complete combustion/lb of "as fired" fuel									
48	= $(11.52\% \text{ carbon}) + 34.57(\% \text{ hydrogen} \% \text{ oxygen}/8) + 4.32 (\% \text{ sulfur})/\text{HHV}$									
49										
50										
51	Actual dry air =	(1 + % Excess air/100) lb/lb of "as fired" fuel								
52		= $13.02/1b$								
53	Moisture in air =	0.013 lb /lb of dry air								
54	Lma =	moisture in air * (enthalpy of water vapor leaving air heater - enthalpy of vapor at mill inlet temp.)								
55										
56										
57										
58										
59	7. Heat loss due to formation of carbon monoxide									
60	Lco =	$\text{CO}/(\text{CO}_2 + \text{CO}) \cdot 10160 \cdot \text{Combustion Efficiency} \cdot \% \text{ carbon in 'as fired' fuel}$								
61										
62										
63	8. Heat loss due to radiation	$10 \cdot \exp(0.62 \cdot 0.42 \log Q)$								
64										
65										
66										
67										
68	Total Losses (%)									
69	HEAT CREDITS									
70										
71	1. Heat supplied by duct burner to entering air									
72	2. Heat supplied by mill to pitman (transport) air									
73										
74	Boiler Efficiency (%) =									
75										
76										
77	Combustion Air Flow (lb/hr) =									
78										
79										
80										
81										
82										
83										
84										
85										

A	B	C	D	E	F
1 Demonstration		Boiler Data			
2 Date of Operation	9/5/95	18.3lb/min coal; Pilin. 100%, Sec. 50%, Tert. 50%;Coal gun -10.5".Gas Gun -9"; Xter 375 actm; O2 3.5%			
3	9/5/95	PC 78% FINE TEST			
4 Pressures and Temperatures					
5		Steam Data			
6 Drum Steam Pressure (Psig)	191.3	Enthalpy of Sat. Liq. (Btu/lb)	346.6		
7 Feed Water Temperature (°F)	198.7	Enthalpy of Feed Water (Btu/lb)	166.8	(Sat. liquid @ Feed water temp.)	
8 Steam Quality (% moisture)	99.3	Steam Production Rate (PPH)	13,121.7		
9 Gas Temp Leaving Boiler (°F)	571.3	Blow down Rate (PPH)	3,030.2		
10 Gas Temp. Leaving Air Heater (°F)	388.6	Enthalpy of water vapor at Gvg Temp (Btu/lb)	1,236.5	(Sup. steam @ 1psia&gas lvg temp)	
11 Air Temp Entering Air Heater (°F)	170.5	Enthalpy of water at fuel inlet temp. (Btu/lb)	47.8	(Sat. liq. @ mill inlet temp.)	
12 Air Temp leaving Air Pre Heater (°F)	402.8	Enthalpy of vapor at fuel inlet temp. (Btu/lb)	1,096.3	(Sat. vapor @ mill inlet temp.)	
13 Air Temp Entering Boiler (°F)	376.9	Calorimeter Temperature (°F)	301.0		
14 Mill Inlet Temperature (°F)	79.7				
15 Mill air flow rate (lb/h)	1,775.1	Coal Firing Rate (lb/h)	1098	Gas Firing Rate (lb/h)	
16 Burner inlet temperature (°F)	195.3	Coal H.H. Value (Btu/lb)	14,533	Gas Cal. Value (Btu/lb)	233,460
17 FUEL DATA		Coal Moisture Content (%)	0.75		
18 Proximate Analysis					
19 Moisture (Wt%)	1.87	Ultimate Analysis (Wt%, d.b)			
20 Volatile Matter (Wt%)	30.82				
21 Fixed Carbon (Wt%)	64.82				
22 Ash (Wt%)	3.78	Carbon	82.05	Methane	95.54
23		Hydrogen	5.21	Ethane	2.48
24 HHV (Btu/lb, d.b)	14,533	Nitrogen	1.41	Propane	0
25		Sulfur	0.84	Butane	0.43
26		Oxygen	6.15	Hydrogen Sulfide	0
27		Ash	4.34	Carbon Dioxide	1.55
28		Total	100	Nitrogen	
29				Others	
30 Flue Gas Analysis				Total	100
31				Moliture (wt%)	0.05
32 Oxygen (%)	3.49				
33 Carbon Dioxide (%)	15.89	Ash In Dry Char/Refuse			
34 Carbon Monoxide (PPM)	118.94	TOTAL CARBON CONVERSION	61.18		
35 Sulfur Dioxide (PPM)	540.05	COAL CARBON CONVERSION	97.50		
36 Oxides of Nitrogen (PPM)	474.31		97.50		
37					
38					
39					
40					
41					
42					

A	B	C	D	E	F
43		Summary of Boiler Performance			
44					
45					
46 Date of Operation	5-Sep				
47					
48					
49					
50					
51 Boiler Operating Conditions					
52					
53					
54 Total Firing Rate	15.95729518	MMBtu/h			
55 Gas Support (%)	0.00	%			
56 Excess air used (%)	19.60	%			
57					
58 Actual mass of products of combustion =	15949.55197	lb/lb of "as fired" fuel			
59 Theoretical flue gas composition	%				
60 Carbon Dioxide	14.50				
61 Water vapor	5.82				
62 Oxygen	3.32				
63 Nitrogen	76.30				
64 Sulfur Dioxide (ppm)	557				
65 Total	100.00				
66					
67 Boiler Efficiency Details					
68					
69 1. Heat loss due to Dry gas (%)					
70 2. Heat loss due to unburned carbon					
71 3. Heat loss due to unburned carbon in dust					
72 4. Heat loss due to moisture in "as Fired Fuel"					
73 5. Heat loss due to moisture produced from burning hydrogen in fuel					
74 6. Heat loss due to moisture in combustion air					
75 7. Heat loss due to formation of carbon monoxide					
76 8. Heat loss due to radiation					
77 9. Heat loss due to steam drum blowdown					
78 Total Losses	13.89				
79 Heat Credits					
80 1. Heat supplied by duct burner to entering air					
81 2. Heat supplied by mill to primary (transport) air					
82					
83 BOILER EFFICIENCY (%)	86.07				
84					
85					

	G	H	I	J	K	L	M	N	O	P	Q
1											
2											
3											
4											
5	Fuel Gas Composition (Dry. Vol%)										
6	Methane	95.54	Density at 60°F (lb/cu.ft)	0.04246	0.04056628	lbs in each cu.ft of gas					
7	Ethane	2.48		0.08029	0.00199119						
8	Propane	0		0.1196	0						
9	Butane	0.43		0.1502	0.0006026						
10	Hydrogen Sulfide	0		0.09109	0						
11	Carbon Dioxide	0		0.117	0						
12	Nitrogen	1.55		0.07439	0.00115305						
13	Total	100									
14											
15											
16											
17											
18											
19											
20											
21											
22	Coal Firing Rate (lb/h)	1098									
23	Coal Heat Input (Btu/h)	15957234									
24											
25	Gas Heat Input (Btu/h)	0									
26	Total Firing Rate	15957234									
27	Gas Calorific Value (Btu/lb)	23346									
28	Gas Firing Rate (lb/h)	0									
29	Gas Support (% of Heat)	0.00									
30	Fraction of coal	1									
31	Fraction of GAS	0									
32											
33											
34											
35											
36											
37											
38											
39											
40											
41											
42											

	G	H	I	J	K	L	M	N	O	P	Q
<b>4.3 Calculation of Air Requirement and Theoretical Products of Combustion</b>											
4.4											
4.5											
4.6 Carbon= %C/(100-12) * 1 mole =					Theoretical Oxygen Requirement						
4.7 Hydrogen= %H/(100-2) * 0.5 mole =					0.06786219 moles						
4.8 Sulfur= %S/(100-32) * 1 mole =					0.01292731 moles						
4.9					0.00026053 moles						
5.0 Oxygen required= Sum of the 3					0.08105003 moles						
5.1 Oxygen available in the Fuel= %O/(100-32)					0.00190746						
5.2 Net Oxygen required =					0.07914257 moles						
5.3 Theoretical Dry Air for Combustion = Net Oxygen required/0.21 =											
5.4											
5.5											
5.6 Calculation of Products of combustion											
5.7											
5.8 Excess air used (%)					= 100(CO2/(CO2)/(0.264*(O2-CO2)) =						
5.9											
6.0 Actual Dry air Required (moles) = (1+E,A%) * total air required =											
6.1 Dry air in lbs/lb of "as fired" fuel					= moles of air*20.97 =						
6.2											
6.3 Actual wet air used/lb of "as fired" fuel (assuming 60% N2 and 80°F) =											
6.4											
6.5											
6.6 Weight of products of combustion = Actual wet air used + weight of fuel =											
6.7											
6.8 Actual weight of products =											
6.9											
7.0											
7.1											
7.2											
7.3											
7.4											
7.5											
7.6											
7.7											
7.8											
7.9											
8.0											
8.1											
8.2											
8.3											
8.4											
8.5											

R	S	T	U	V	W	X	Y	Z	AA
<b>1 Calculation of Theoretical Composition of Products</b>									
2									
3									
4									
5	Carbon Dioxide	(moles of carbon /lb of fuel)		0.06786219	Wet Flue Gas Compositon (%)		Dry Flue Gas Comp. (%)		
6	Water	(moles of water in fuel + moles of water in combustion air)		0.0272469	14.50	15.40			
7				0.01551118	5.82	0.00			
8	Oxygen			0.35700561	3.32	3.52			
9	Nitrogen			0.00026053	76.30	81.02			
10	Sulfur Dioxide			0.46788641	0.05568259	0.06			
11	Total			100.00		100.00			
12									
13									
14	Boiler Efficiency	Calculations							
15									
16	These calculations are based on ASME PTG 4.1 using heat loss method								
17									
18	1. Pounds of dry gas per pound of "as fired" composite fuel								
19									
20	Wg' =	((E% db) : C Efficiency : (4.01 (CO <sub>2</sub> ) + 32.00 (O <sub>2</sub> ) + 28.02 (N <sub>2</sub> ) + (28.01 (CO)/12.01 (CO <sub>2</sub> +CO)) + 12.01 (S)/32.07)							
21									
22	12.76327165 lb/lb of as fired fuel								
23									
24	1. Heat loss due to dry gas (%)	Lwg' = Wg' : 0.24 : (359.75)/HHV * 100							
25									
26	2. Heat loss due to unburned carbon								
27									
28									
29	Luc =	% Carbon in the "as fired Fuel" : (1. Comb. Efficiency) : 14.500							
30									
31									
32	3. Heat loss due to unburned carbon in dust						Negligible		
33									
34									
35	4. Heat loss due to moisture in "as Fired Fuel"						0.06		
36									
37	Lm' =	Moisture in Fuel (Enthalpy of vapor at gas leaving temp - Enthalpy of water at mill Intlet)/HHV * 100							
38									
39									
40									
41	5. Heat loss due to moisture produced from burning hydrogen in fuel						3.78		
42									

R	S	T	U	V	W	X	Y	Z	AA
43 Lmh=	8.936 % hydrogen in "as fired" fuel* (Enthalpy of vapor leaving air heater- Enthalpy of water at mill inlet temp)/HHV								
44									
45									
46. Heat loss due to moisture in combustion air	Theoretical lb of air required for complete combustion/lb of "as fired" fuel = $(11.52\% \text{ carbon}) + 34.57\% \text{ hydrogen} - \% \text{ oxygen}(\%) + 4.32 (\% \text{ sulfur})/\text{HHV}$					0.16			
47									
48									
49									
50									
51 Actual dry air = $(1+\% \text{ Excess air}/100) \text{ lb/lb of "as fired" fuel}$		10.94 lb/lb of "as fired" fuel							
52 Moisture in air = $0.013 \text{ lb/lb of dry air}$									
53									
54 Moisture in air = $0.013 \text{ lb/lb of dry air}$									
55									
56									
57									
58									
59. Heat loss due to formation of carbon monoxide	$\text{CO}/(\text{CO}_2 + \text{CO}) \cdot 10^{16} \text{ : Combustion Efficiency}^* \% \text{ carbon in "as fired fuel}}$								
60 Lco =									
61									
62									
63. B. Heat loss due to radiation	$10 \exp(0.62 \cdot 0.42 \log Q)$								
64									
65									
66									
67									
68 Total Losses (%)									
69 HEAT CREDITS									
70									
71 1. Heat supplied by duct burner to entering air									
72 2. Heat supplied by mill to primary (transport) air									
73									
74 Boiler Efficiency (%)=							86.07 %		
75									
76									
77 Combustion Air Flow (lb/hr)=								14555 lb/h	
78									
79									
80									
81									
82									
83									
84									
85									