

Environmentally Assisted Cracking in Light Water Reactors

Annual Report January—December 2002

Argonne National Laboratory

U.S. Nuclear Regulatory Commission Office of Nuclear Regulatory Research Washington, DC 20555-0001



Environmentally Assisted Cracking in Light Water Reactors

Annual Report January—December 2002

Manuscript Completed: March 2004 Date Published: June 2005

Prepared by O. K. Chopra, H. M. Chung, R. W. Clark, E. E. Gruber, W. J. Shack, W. K. Soppet, R. V. Strain

Argonne National Laboratory 9700 South Cass Avenue Argonne, IL 60439

W. H. Cullen, Jr., and C. E. Moyer, NRC Project Managers

Prepared for Division of Engineering Technology Office of Nuclear Regulatory Research U.S. Nuclear Regulatory Commission Washington, DC 20555-0001 NRC Job Code Y6388



AVAILABILITY OF REFERENCE MATERIALS IN NRC PUBLICATIONS

NRC Reference Material	Non-NRC Reference Material
As of November 1999, you may electronically access NUREG-series publications and other NRC records at NRC's Public Electronic Reading Room at <u>http://www.nrc.gov/reading-rm.html</u> . Publicly released records include, to name a few, NUREG-series publications; <i>Federal Register</i> notices; applicant, licensee, and vendor documents and correspondence; NRC correspondence and internal memoranda; bulletins and information notices; inspection and investigative reports; licensee event reports; and Commission papers and their attachments. NRC publications in the NUREG series, NRC regulations, and <i>Title 10, Energy</i> , in the Code of <i>Federal Regulations</i> may also be purchased from one of these two sources. 1. The Superintendent of Documents U.S. Government Printing Office Mail Stop SSOP	Documents available from public and special technical libraries include all open literature items, such as books, journal articles, and transactions, <i>Federal</i> <i>Register</i> notices, Federal and State legislation, and congressional reports. Such documents as theses, dissertations, foreign reports and translations, and non-NRC conference proceedings may be purchased from their sponsoring organization. Copies of industry codes and standards used in a substantive manner in the NRC regulatory process are maintained at— The NRC Technical Library Two White Flint North 11545 Rockville Pike Rockville, MD 20852–2738
 Washington, DC 20402–0001 Internet: bookstore.gpo.gov Telephone: 202-512-1800 Fax: 202-512-2250 2. The National Technical Information Service Springfield, VA 22161–0002 www.ntis.gov 1–800–553–6847 or, locally, 703–605–6000 A single copy of each NRC draft report for comment is available free, to the extent of supply, upon written request as follows: 	These standards are available in the library for reference use by the public. Codes and standards are usually copyrighted and may be purchased from the originating organization or, if they are American National Standards, from— American National Standards Institute 11 West 42 nd Street New York, NY 10036–8002 www.ansi.org 212–642–4900
Address: Office of the Chief Information Officer, Reproduction and Distribution Services Section U.S. Nuclear Regulatory Commission Washington, DC 20555-0001 E-mail: DISTRIBUTION@nrc.gov Facsimile: 301–415–2289 Some publications in the NUREG series that are posted at NRC's Web site address http://www.nrc.gov/reading-rm/doc-collections/nuregs are updated periodically and may differ from the last printed version. Although references to material found on a Web site bear the date the material was accessed, the material available on the date cited may subsequently be removed from the site.	Legally binding regulatory requirements are stated only in laws; NRC regulations; licenses, including technical specifications; or orders, not in NUREG-series publications. The views expressed in contractor-prepared publications in this series are not necessarily those of the NRC. The NUREG series comprises (1) technical and administrative reports and books prepared by the staff (NUREG-XXXX) or agency contractors (NUREG/CR-XXX), (2) proceedings of conferences (NUREG/CP-XXXX), (3) reports resulting from international agreements (NUREG/IA-XXXX), (4) brochures (NUREG/BR-XXXX), and (5) compilations of legal decisions and orders of the Commission and Atomic and Safety Licensing Boards and of Directors' decisions under Section 2.206 of NRC's regulations (NUREG-0750).

Previous Documents in Series

Environmentally Assisted Cracking in Light Water Reactors Semiannual Report April—September 1985, NUREG/CR-4667 Vol. I, ANL-86-31 (June 1986). October 1985—March 1986, NUREG/CR-4667 Vol. II, ANL-86-37 (September 1987). April—September 1986, NUREG/CR-4667 Vol. III, ANL-87-37 (September 1987). October 1986—March 1987, NUREG/CR-4667 Vol. IV, ANL-87-41 (December 1987). April—September 1987, NUREG/CR-4667 Vol. V, ANL-88-32 (June 1988). October 1987—March 1988, NUREG/CR-4667 Vol. 6, ANL-89/10 (August 1989). April—September 1988, NUREG/CR-4667 Vol. 7, ANL-89/40 (March 1990). October 1988-March 1989, NUREG/CR-4667 Vol. 8, ANL-90/4 (June 1990). April—September 1989, NUREG/CR-4667 Vol. 9, ANL-90/48 (March 1991). October 1989-March 1990, NUREG/CR-4667 Vol. 10, ANL-91/5 (March 1991). April—September 1990, NUREG/CR-4667 Vol. 11, ANL-91/9 (May 1991). October 1990-March 1991, NUREG/CR-4667 Vol. 12, ANL-91/24 (August 1991). April—September 1991, NUREG/CR-4667 Vol. 13, ANL-92/6 (March 1992). October 1991-March 1992, NUREG/CR-4667 Vol. 14, ANL-92/30 (August 1992). April—September 1992, NUREG/CR-4667 Vol. 15, ANL-93/2 (June 1993). October 1992—March 1993, NUREG/CR-4667 Vol. 16, ANL-93/27 (September 1993). April—September 1993, NUREG/CR-4667 Vol. 17, ANL-94/26 (June 1994). October 1993—March 1994, NUREG/CR-4667 Vol. 18, ANL-95/2 (March 1995). April—September 1994, NUREG/CR-4667 Vol. 19, ANL-95/25 (September 1995). October 1994—March 1995, NUREG/CR-4667 Vol. 20, ANL-95/41 (January 1996). April—December 1995, NUREG/CR-4667 Vol. 21, ANL-96/1 (July 1996). January 1996—June 1996, NUREG/CR-4667 Vol. 22, ANL-97/9 (June 1997). July 1996—December 1996, NUREG/CR-4667 Vol. 23, ANL-97/10 (October 1997). January 1997—June 1997, NUREG/CR-4667 Vol. 24, ANL-98/6 (April 1998). July 1997—December 1997, NUREG/CR-4667 Vol. 25, ANL-98/18 (September 1998). January 1998—June 1998, NUREG/CR-4667 Vol. 26, ANL-98/30 (December 1998). July 1998—December 1998, NUREG/CR-4667 Vol. 27, ANL-99/11 (October 1999). January 1999-June 1999, NUREG/CR-4667 Vol. 28, ANL-00/7 (July 2000). July 1999—December 1999, NUREG/CR-4667 Vol. 29, ANL-00/23 (November 2000). January 2000-June 2000, NUREG/CR-4667 Vol. 30, ANL-01/08 (June 2001). July 200—December 2000, NUREG/CR-4667 Vol. 31, ANL-01/09 (April 2002). Environmentally Assisted Cracking in Light Water Reactors Annual Report January-December 2001, NUREG/CR-4667 Vol. 32, ANL-02/33 (June 2003).

Abstract

This report summarizes work performed by Argonne National Laboratory on fatigue and environmentally assisted cracking (EAC) in light water reactors (LWRs) from January to December 2002. Topics that have been investigated include: (a) environmental effects on fatigue crack initiation in carbon and low–alloy steels and austenitic stainless steels (SSs), (b) irradiation–assisted stress corrosion cracking (IASCC) of austenitic SSs in BWRs, (c) evaluation of causes and mechanisms of irradiation-assisted cracking of austenitic SS in PWRs, and (d) cracking in Ni–alloys and welds.

A critical review of the ASME Code fatigue design margins and an assessment of the conservatism in the current choice of design margins are presented. The existing fatigue ε -N data have been evaluated to define the effects of key material, loading, and environmental parameters on the fatigue lives of carbon and low-alloy steels and austenitic SSs. Experimental data are presented on the effects of surface roughness on fatigue crack initiation in these materials in air and LWR environments.

Crack growth tests were performed in BWR environments on SSs irradiated to 0.9 and $2.0 \times 10^{21} \text{ n} \cdot \text{cm}^{-2}$. The crack growth rates (CGRs) of the irradiated steels are a factor of \approx 5 higher than the disposition curve proposed in NUREG–0313 for thermally sensitized materials. The CGRs decreased by an order of magnitude in low–dissolved oxygen (DO) environments.

Slow-strain-rate tensile (SSRT) tests were conducted in high-purity 289°C water on steels irradiated to \approx 3 dpa. The bulk S content correlated well with the susceptibility to intergranular SCC in 289°C water. The IASCC susceptibility of SSs that contain >0.003 wt.% S increased drastically. Bend tests in inert environments at 23°C were conducted on broken pieces of SSRT specimens and on unirradiated specimens of the same materials after hydrogen charging. The results of the tests and a review of other data in the literature indicate that IASCC in 289°C water is dominated by a crack-tip grain-boundary process that involves S. An initial IASCC model has been proposed.

A crack growth test was completed on mill annealed Alloy 600 in high–purity water at 289°C and 320°C under various environmental and loading conditions. The results from this test are compared with data obtained earlier on several other heats of Alloy 600.

Foreword

For over 34 years Argonne National Laboratory has been a prime contractor to the Office of Nuclear Regulatory Research (RES) for studies of the environmental degradation of structural materials in light water reactor environments. This document is the 2002 annual report of the program studies. The program has evolved to keep pace with the most critical of the contemporary issues facing the industry and the NRC. Task 1 focused on the environmental degradation of fatigue life of pressure boundary materials. Task 2 addresses irradiation-assisted stress corrosion cracking (IASCC) of stainless steels in BWR environments, and a parallel program (Task 3) is addressing IASCC of stainless steels in pressurized water reactor (PWR) environments. Task 4, the study of crack growth rates in nickel-base alloys typically used in vessel penetrations, is currently focused on testing alloy 600 and its associated weld metal, alloys 182 and 82. Task 4 will test alloy 690 and its associated weld metal, alloys 152 and 52, which are the materials of choice for most replacement vessel head penetrations.

In earlier years, ANL research produced the finding that the fatigue life of stainless steels is degraded to a greater degree in de-oxygenated, PWR-like environments than it is in boiling water reactor (BWR) environments. Research completed in 2002 provided added confirmation of that result, further characterized the microstructural aspects of fatigue crack initiation, and evaluated the effects of surface roughness on fatigue life degradation of low-carbon steels, low-alloy steels, and stainless steels. The database for the environmental degradation of fatigue lives in stainless steels buttresses the NRC position *vis a vis* the ASME code - that the underlying computational logic and application of the design curves for the fatigue life of pressure boundary and internal components fabricated from stainless steel is non-conservative, and needs revision.

Cracking of nickel-base alloys commonly used in vessel penetrations was initially manifested in pressurizer nozzles and heater sleeves, which normally operate in a temperature range somewhat higher than other reactor components. When cracking was observed in vessel head penetrations, RES incorporated crack growth rate studies in the ANL test program. Although most plant observations of cracking have occurred in PWRs, the ANL test program is testing these materials under both BWR and PWR conditions. These results will be used to support flaw evaluations and the associated requests for continued operations that are proposed to the NRC.

In the future, the IASCC work will test materials that have received higher radiation doses, and will involve more microstructural characterization of such materials. Studies of void swelling and stress corrosion cracking studies of cast or welded stainless steels will also enter the test program. The SCC studies of nickel-base alloys will begin to refocus on alloys 690 and its associated weld metal, alloy 152, including cold-worked and heat-affected zone forms of the wrought material.

Carl J. Paperiello, Director Office of Nuclear Regulatory Research

Contents

Ab	stract			iii
Fo	reword .			v
Ex	ecutive	Summary.		xiii
Ac	knowled	dgments		XV
1	Introdu	uction		1
2	Enviro Auster	nmental E nitic Stainle	Effects on Fatigue Crack Initiation in Carbon and Low–Alloy Steels and ess Steels	3
	2.1	2.1 Introduction		
	2.2	Experimental		4
	2.3	Fatigue e	-N Data in LWR Environments	5
		2.3.1	Carbon and Low-Alloy Steels	5
		2.3.2	Austenitic Stainless Steels	6
		2.3.3	Effects of Surface Finish	8
	2.4	Statistica	I Model	8
	2.5	Incorpora	ating Environmental Effects	10
		2.5.1	Fatigue Design Curves	10
		2.5.2	Fatigue Life Correction Factor	12
	2.6 Margins in ASME Code Fatigue Design Curves			12
		2.6.1	Material Variability and Data Scatter	14
		2.6.2	Size and Geometry	16
		2.6.3	Surface Finish	17
		2.6.4	Loading Sequence	17
		2.6.5	Fatigue Design Curve Margins Summarized	19
3	Irradiation–Assisted Stress Corrosion Cracking of Austenitic Stainless Steel in BWRS		21	
	3.1 Slow-Strain-Rate-Tensile Test of Model Austenitic Stainless Steels Irradiated in the Halden Reactor		21	
		3.1.1	Introduction	21
		3.1.2	Experimental Procedure	22

		3.1.3	Results of SSRT Testing	23
		3.1.4	S Effect in High-Carbon and Low-Carbon Steels	29
		3.1.5	Results of Fractography	30
		3.1.6	Grain-Boundary Segregation of S and C	32
	3.2	Crack Gi Reactor	rowth Rate Test of Austenitic Stainless Steels Irradiated in the Halden	33
		3.2.1	Introduction	33
		3.2.2	Experimental	34
		3.2.3	Crack Growth Rates of Irradiated Stainless Steels in BWR Environments	37
4	Evaluation of Causes and Mechanisms of Irradiation-Assisted Cracking of Austenitic Stainless Steel in PWRs			43
	4.1	Introduction		43
	4.2	2 Irradiation of Austenitic Stainless Steels in the BOR-60 Reactor		43
	4.3	Studies of	on Intergranular-Fracture Characteristics	45
		4.3.1	Intergranular Fracture in Inert Environment	45
		4.3.2	Initial Model of IASCC	48
5	Cracki	ng of Nick	cel Alloys and Welds	51
	5.1	Introduct	tion	51
	5.2	2 Experimental		52
	5.3	Results		53
		5.3.1	Fatigue Crack Growth Rates	56
		5.3.2	SCC Crack Growth Rates	60
6	Summ	ary		63
	6.1	Environr	nental Effects on Fatigue ε–N Behavior	63
	6.2	2 Irradiation–Assisted Stress Corrosion Cracking of Austenitic Stainless Steel in BWRs		64
	6.3	Irradiatio	on-Assisted Cracking of Austenitic Stainless Steel in PWRs	65
	6.4	Environr	nentally Assisted Cracking of Alloys 600 and 690 in LWR Water	65
Re	ferences	5		67

Figures

1.	Effect of surface roughness on the fatigue life of A106–Gr B carbon steel and A533–Gr B low–alloy steel in air and high–purity water at 289°C
2.	Effect of surface roughness on the fatigue life of Type 316NG and Type 304 SSs in air and high–purity water at 289°C
3.	Fatigue design curves developed from the statistical model for carbon steels, low-alloy steels, and austenitic stainless steels in LWR environments under service conditions where one or more critical threshold values are not satisfied, and all threshold values are satisfied 11
4.	Fatigue data for carbon and low–alloy steel and Type 304 stainless steel components
5.	Estimated cumulative distribution of the parameter A in the statistical models for fatigue life for heats of carbon and low–alloy steels and austenitic SSs in air and water environments
6.	Schematic illustration of growth of short cracks in smooth specimens as a function of fatiguelife fraction and crack velocity as a function of crack length18
7.	Schematic illustration of bending fracture in air and in vacuum
8.	Percent IGSCC correlated with bulk content of: Cr, Ni, Si, P, C, N, and O
9.	Percent IGSCC correlated with bulk S content, fluence 2.0×10^{21} n cm ⁻²
10.	Percent IGSCC of Type 304 and 316 steels that contain low, medium, and high concentrations of S for three fluence levels
11.	Percent IGSCC vs. bulk S content for high-C, low-C, and low-C high-purity grades of Types 304 and 316 SS
12.	IASCC susceptibility of low- and high-sulfur heats of comparable chemical composition:304 SS, SSRT test, this study; HP 304L, SSRT test, Tsukada and Miwa 1995; 316L,expanding-tube test, Kasahara et al. 1993; 316L, expanding tube test, Jacobs et al. 1993; and348, expanding tube test, Garzarolli et al. 1988
13.	Percent IGSCC from SSRT test of low-S heats of high- and low-C steels: Type 304 and 304L SSs; 316 and 316L SSs; and 348 and 348L SSs
14.	Fracture surface morphology produced during SSRT test in 289°C water and during bending in 23°C air after SSRT test in 289°C water
15.	Auger electron peak heights of S and C on or near grain boundaries in Type 304 SS BWR tubes irradiated to 2 x 10^{21} n cm ⁻² : S and C peak heights from ductile and IG fracture surfaces, from Heat A-1 tube; depth-profiles of S and C, from Heats A-1 and B tubes
16.	Configuration of compact–tension specimen for this study
17.	Schematic diagram of recirculating water system
18.	Change in crack length and ECP of Pt and SS electrodes for specimen C3–B after DO level in feedwater was decreased from \approx 400 to <30 ppb

19.	Plots of crack length and K _{max} vs. time for specimen C3–B in high–purity water at 289°C
20.	Plots of crack length and K _{max} vs. time for specimen C16–B in high–purity water at 289°C
21.	Plots of crack length and K _{max} vs. time for specimen C3–C in high–purity water at 289°C
22.	Photomicrograph of fracture surface of specimen C3–B
23.	CGR data for irradiated austenitic SSs under cyclic loading at 289°C in high–purity water with \approx 300 ppb and <30 ppb dissolved oxygen.
24.	Crack growth rate under constant load for irradiated austenitic SSs in high-purity water
25.	Tensile specimens irradiated in the BOR-60 reactor
26.	Disk-specimen capsules irradiated in the BOR-60 reactor
27.	Susceptibility to IG fracture in 289°C water and in inert environment at 23°C
28.	Schematic illustration of various threshold boundaries applicable to disorder-induced melting or amorphization of Ni–S–H grain-boundary thin film
29.	Schematic illustration of a proposed IASCC model
30.	Crack–length–vs.–time plot for mill–annealed Alloy 600 specimen in high–purity water at 289 and 320°C: 100–1200 h, 1100–2500 h, and 2400–3600 h
31.	Change in crack length and ECP of Pt and stainless steel electrodes when the dissolved oxygen was decreased from \approx 300 to 5 ppb
32.	Photograph of the fracture surface of Alloy 600 specimen CT31-04
33.	SEM photomicrograph of the fracture surface of Alloy 600 specimen CT31–04 after the surface oxide film was chemically removed
34.	Photomicrograph of a region in the middle of the specimen showing the entire crack extension, typical fracture surface in region IG-1, transition from IG to TG, and typical fracture surface in region IG-2.
35.	Low- and high-magnification photomicrographs comparing the fracture surface in region IG-1 and IG-2.
36.	Fatigue CGR data for mill–annealed and 30% cold worked Alloy 600 in high–purity water with \approx 300 ppb DO at 289°C and \approx 5 ppb DO at 320°C
37.	Fatigue CGR data for several heats of Alloy 600 in high–purity water with ≈300 ppb DO at 289°C and <10 ppb DO at 320°C
38.	SCC CGR data for mill–annealed Heat NX131031 of Alloy 600 in high–purity water with \approx 300 ppb DO at 289°C and \approx 5 ppb DO at 320°C
39.	Estimated cumulative distribution of the parameter A in the Scott model for CGR for heats of Alloy 600

Tables

1.	Chemical composition of austenitic and ferritic steels for fatigue tests	4
2.	Values of parameter A in the statistical model for carbon steels as a function of the percentage of the population bounded and the confidence level	6
3.	Values of parameter A in the statistical model for low–alloy steels as a function of the percentage of the population bounded and the confidence level	6
4.	Values of parameter A in the statistical model for austenitic stainless steels as a function of the percentage of the population bounded and the confidence level	6
5.	Factors to be applied to mean ϵ -N curve	9
6.	Elemental composition of 27 commercial and laboratory-fabricated austenitic SSs irradiated in the Halden Reactor	23
7.	Results of slow-strain-rate tensile test and fractographic analysis on austenitic stainlesssteels irradiated to ≈ 3 dpa in Halden Reactor at 289°C in helium	24
8.	Composition of austenitic stainless steels irradiated at 289°C in helium to 3 dpa in the Halden Reactor, correlated with results of SEM fractography after SSRT test in 289°C water and bend test in 23°C air	24
9.	Composition of model austenitic stainless steels irradiated in the Halden reactor	35
10.	Tensile properties of irradiated austenitic stainless steels at 288°C	35
11.	Crack growth results for Specimen C3–B of Type 304 stainless steel in high–purity water at 289°C	37
12.	Crack growth results for Specimen C3–C of Type 304 SS in high–purity water at 289°C	38
13.	Crack growth results for Specimen C16–B of Type 316 SS in high–purity water at 289°C	38
14.	Accumulated dose of 12 bundles containing tensile specimens and 4 capsules containing disk specimens discharged from BOR-60 reactor after irradiation at 322°C	14
15.	Summary of number, steel type, and material state of tensile specimens irradiated to ≈ 5 or ≈ 10 dpa in BOR-60 reactor.	45
16.	Tests on BWR components; SSRT test in 289°C water and bend fracture in 23°C vacuum after H-charging. 4	16
16. 17.	Tests on BWR components; SSRT test in 289°C water and bend fracture in 23°C vacuum after H-charging.4Composition of Alloy 600 Heat NX131031 base metal.5	46 52

Executive Summary

The existing fatigue ϵ -N data for carbon and low-alloy steels and wrought and cast austenitic SSs have been evaluated to define the effects of key material, loading, and environmental parameters on the fatigue lives of these steels. The fatigue lives of carbon and low-alloy steels and austenitic SSs are decreased in LWR environments. The magnitude of the reduction depends on temperature, strain rate, DO level in water, and, for carbon and low-alloy steels, S content in steel. The threshold values of the critical parameters and the effects of other parameters (such as water conductivity, water flow rate, and material heat treatment) on the fatigue life of the steels are summarized.

Experimental data are presented on the effects of surface roughness on the fatigue life of carbon and low-alloy steels and austenitic stainless steels in air and LWR environments. For austenitic SSs, the fatigue life of roughened specimens is a factor of ≈ 3 lower than that of the smooth specimens in both air and low-DO water. For carbon and low-alloy steels, the fatigue life of roughened specimens is lower than that of smooth specimens in air but is the same in high-DO water.

Statistical models are presented for estimating the fatigue life of carbon and low-alloy steels and wrought and cast austenitic SSs as a function of material, loading, and environmental parameters. Two approaches are presented for incorporating the effects of LWR environments into ASME Section III fatigue evaluations.

Because of material variability, data scatter, and component size and surface, the fatigue life of actual components is different from that of laboratory test specimens under a similar loading history, the mean ε -N curves for laboratory test specimens are adjusted by factors of 2 on stress and 20 on cycles to obtain design curves for components. These factors should not be considered safety margins, but they were intended to cover the effects of variables that can influence fatigue life but were not investigated in the tests that provided the data for the curves. Data available in the literature have been reviewed to evaluate the margins on cycles and stress. The results indicate that the current ASME Code requirements of a factor of 2 on stress and 20 on cycle are reasonable, and do not contain excess conservatism that can be assumed to account for the effects of LWR environments.

Crack growth tests have been performed in simulated BWR environments at $\approx 289^{\circ}$ C on Type 304 SS (Heat C3) irradiated to 0.9 and 2.0 x 10²¹ n·cm⁻² and Type 316 SS (Heat C16) irradiated to 2.0 x 10²¹ n·cm⁻² at $\approx 288^{\circ}$ C in a helium environment. The results indicate significant enhancement of CGRs of irradiated steel in the normal water chemistry BWR environment. The CGRs of irradiated steels are a factor of ≈ 5 higher than the disposition curve proposed in NUREG–0313 for sensitized austenitic SSs in water with 8 ppm DO. Actual enhancement in the same purity water is greater than 5. The CGRs of Type 304 SS irradiated to 0.9 and 2.0 x 10²¹ n·cm⁻² and of Types 304 and 316 SS irradiated to 2.0 x 10²¹ n·cm⁻², are comparable.

In low–DO environment with low electrochemical potentials (ECPs), the CGRs of the irradiated steels decreased by an order of magnitude in tests in which the K validity criterion was satisfied, e.g., Heat C3 of Type 304 SS irradiated to $0.9 \times 10^{21} \text{ n} \cdot \text{cm}^{-2}$ and Heat C16 of Type 316 SS irradiated to $2 \times 10^{21} \text{ n} \cdot \text{cm}^{-2}$. No beneficial effect of decreased DO was observed for Heat C3 of Type 304 SS irradiated to $2 \times 10^{21} \text{ n} \cdot \text{cm}^{-2}$, but in this case the applied K values during the low ECP portion of the test exceeded those required to meet the K validity criterion.

Slow-strain-rate tensile (SSRT) tests were conducted in high-purity 289°C water on steels irradiated to \approx 3 dpa in helium in the Halden Reactor. At \approx 3 dpa, the bulk S content provided the best and the only

good correlation with the susceptibility to intergranular (IG) SCC in 289°C water. Good resistance to IASCC was observed in Type 304 and 316 stainless steels that contain very low concentrations of S of ≈ 0.002 wt.% or less. The IASCC susceptibility of Type 304, 304L, 316, and 316L steels that contain >0.003 wt.% S increased drastically. Steels containing ≥ 0.008 wt.% were very susceptible at high fluence. These observations indicate that the deleterious effect of S plays a dominant role in the failure of core internal components at high fluence.

In contrast to Type 304 and 316 stainless steels, a low concentration of S of $\approx 0.001-0.002$ wt.% does not necessarily render low-carbon Types 304L and 316L, or high-purity-grade steel resistant to IASCC. This suggests that high concentration of C is beneficial in reducing the deleterious effect of S and that threshold S concentration to ensure good IASCC resistance is lower in a low-carbon steel than in a high-carbon steel.

A comprehensive irradiation experiment in the BOR-60 Reactor is under progress to obtain a large number of tensile and disk specimens irradiated under PWR-like conditions at \approx 325°C to 5, 10, and 40 dpa. Irradiation to \approx 5 and \approx 10 dpa has been completed.

Tests performed on the materials irradiated in the Halden BWR reactor may also give some insight into potential mechanisms for IASCC that are also relevant to PWRs. After exposure to the conditions of the SSRT test in BWR water, susceptibility to intergranular cracking in an inert environment was determined by rapid bending in air at 23°C. Similar tests were also performed on hydrogen-charged specimens in vacuum. Both types of bend fracture exhibited similar characteristics suggesting that in both cases the failures occurred due to hydrogen-induced intergranular failure. However, steels that showed high susceptibility to IGSCC in 289°C water exhibited low susceptibility to intergranular cracking in the tests at 23°C air or vacuum, and vice versa. This indicates that although intergranular cracking in 23°C is dominated by H-induced embrittlement of ordinary grain boundaries, other processes control IASCC in 289°C water. On the basis of this investigation, and studies on binary Ni–S and cracktip microstructural characteristics of LWR core internal components reported in literature, an initial IASCC model has been proposed.

The resistance of Ni alloys to environmentally assisted cracking in simulated LWR environments is being evaluated. A crack growth test was completed on mill annealed (MA) Alloy 600 (Heat NX131031) specimen in high–purity water at 289 and 320°C under various environmental and loading conditions. The results from this test are compared with data obtained earlier on several other heats of Alloy 600.

In a high–DO environment at 289°C, nearly all of the heats and heat treatment conditions that have been investigated show enhanced growth rates. The growth rates for MA (Heat NX131031) are slightly higher than for the other heats of Alloy 600. In contrast to the behavior in high–DO water, environmental enhancement of fatigue CGRs of Alloy 600 in low–DO water seems to depend on material condition, e.g., materials with high yield strength and/or low grain boundary coverage of carbides.

The SCC crack growth rates of Heat NX131031 in high–DO water at 289°C are comparable to those in low–DO water at 320°C. The results from the present study are compared with data obtained on several other heats of Alloy 600. In a PWR environment, the CGR of Heat NX131031 corresponds to the 53rd percentile of the distribution for the sample of heats of Alloy 600. For example, Heat NX131031 represents an average heat.

Acknowledgments

The authors thank T. M. Galvin, R. W. Clark, and J. Tezak for their contributions to the experimental effort. This work is sponsored by the Office of Nuclear Regulatory Research, U.S. Nuclear Regulatory Commission, under Job Code Y6388; Program Manager: William H. Cullen, Jr.; Tasks 2 and 3 Manager: Carol E. Moyer.