

# Power Conditioning Systems for High-Megawatt Fuel Cell Plants

Solid State Energy Conversion Alliance (SECA)

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NIST



(NIST/DOE Interagency Agreement)

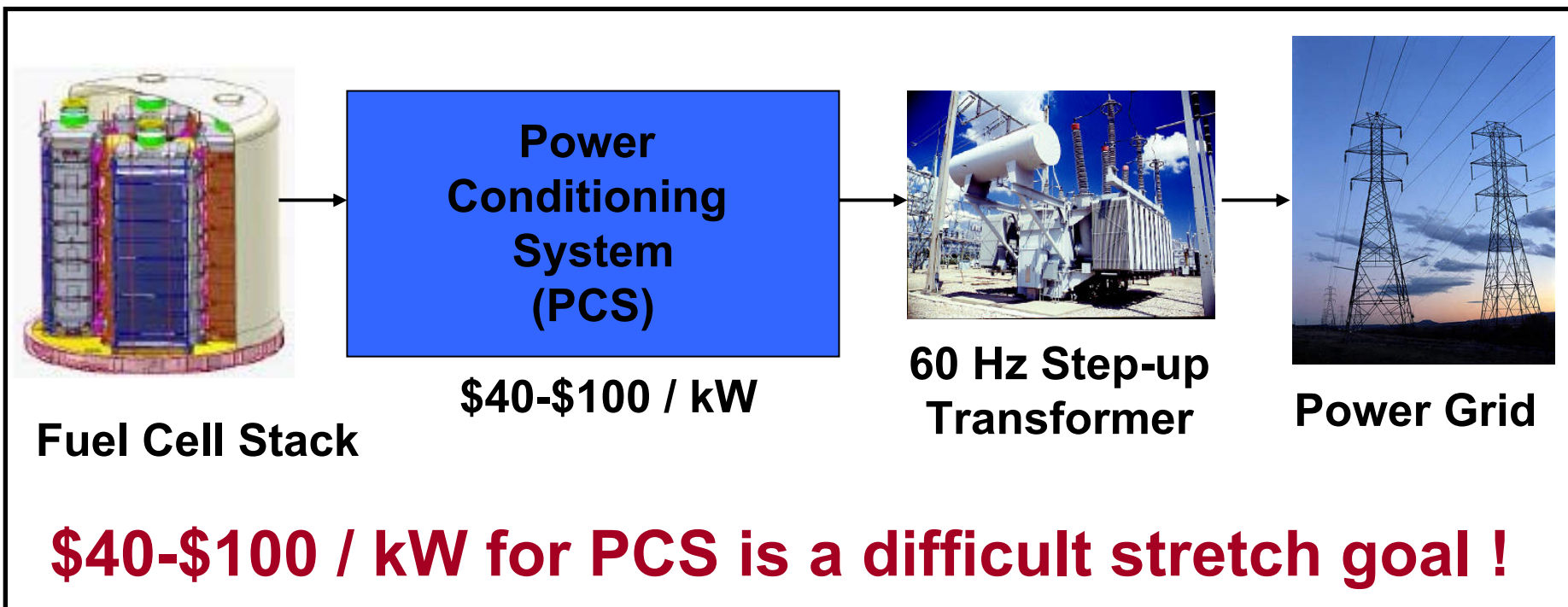


# Outline

- 
- I. **SECA Power Conditioning Systems (PCS)**
  - II. **Technology Impact Analysis**
  - III. **HV-HF SiC Power Devices**
  - IV. **SiC Power Device Cost Reduction**



# SECA Fuel Cell Plant



# Power Conditioning System

## Objective:

- **High-Megawatt Power Conditioning Systems (PCS) are required to convert:**
  - from power produced by Fuel Cells (FC) in power plant
  - to very high voltage and power required for the grid

## Motivation:

- **DoE SECA cost goals:**
  - FC generator plant \$400/kW
  - including \$40-100/kW for PCS
- **Recent Fuel Cell Generator cost (*Fuel Cell Energy Inc.*):**
  - FC generator plant \$3,000/kW
  - including \$260/kW for power converter (to 18 kV AC)
- **Today's SECA cost: \$750/kW + PCS cost**

# High-Megawatt PCS Program Coordination

- **High-Megawatt Converter Workshop: January 24, 2007**
  - Begin to identify technologies requiring development to meet PCS cost and performance goals for the DOE SECA
- **Industry Roadmap Workshop: April 8, 2008**
  - Initiate roadmap process to offer guidance for further development of high-megawatt converters technology
- **Interagency Advanced Power Group (IAPG): April 21-25**
  - Form interagency task group to coordinate Federal programs in high-megawatt converter technologies - under IAPG ESWG
- **National Science Foundation (NSF): May 15-16, 2008**
  - Establish power electronics curriculums and fundamental research programs for alternate energy power converters

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# High Megawatt PCS Technology Impact Analysis

- **Perform Independent Analysis of technologies that may reduce cost of PCS for future FC Power Plants**
- **Methodology for impact study:**
  - Include input from broad power electronics, power component, and power engineering communities
  - Classify power converter architectures, topologies, and component technologies that may reduce cost
  - Calculate cost for each PCS option to estimate advantages of new technologies
  - Use component modeling, and circuit and system simulations to verify and refine calculations



# 300 MW PCS

~700 V  
DC



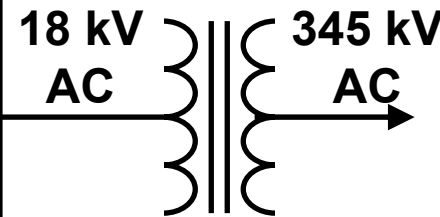
Approx.  
500  
Fuel  
Cells



~700 V  
DC



**Semiconductors**  
**Packaging and Interconnects**  
**HF transformers**  
**Filter Inductors and Capacitors**  
**Cooling System**  
**60 Hz Transformer up to 18 kV**  
**Breakers and Switchgear**



**\$40-\$100 / kW**

**Ripple < 2%**  
**Stack Voltage Range**  
**~700 to 1000 V**

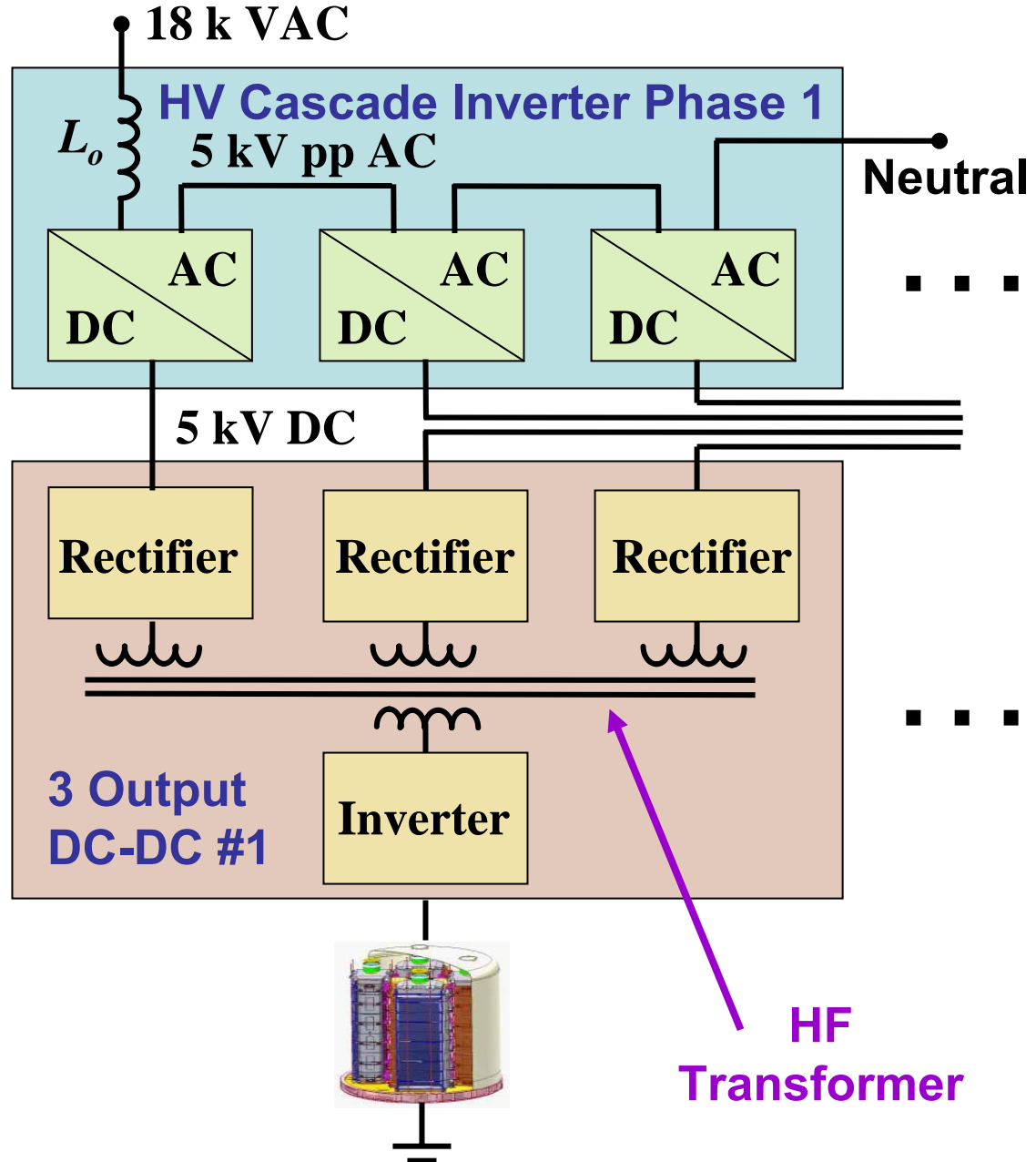
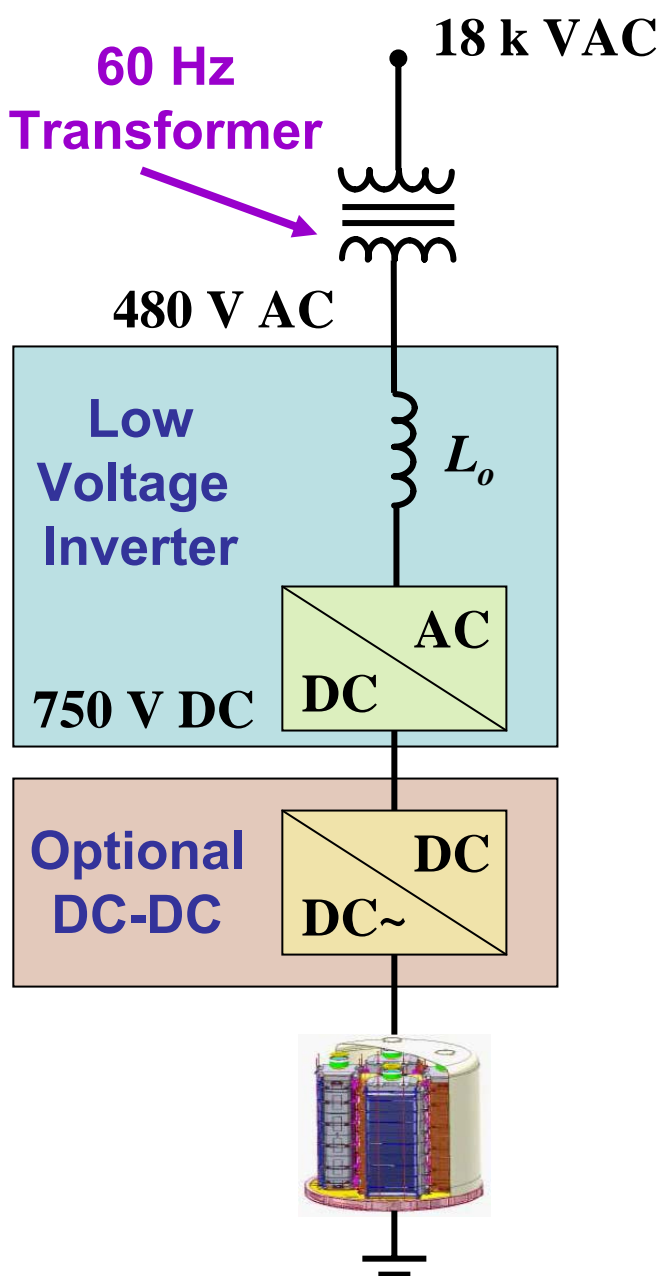
**IEEE – 519**  
**IEEE – 1547**  
**Harmonic Distortion**  
*Future: HVDC transmission ?*



# Power Converter Architectures

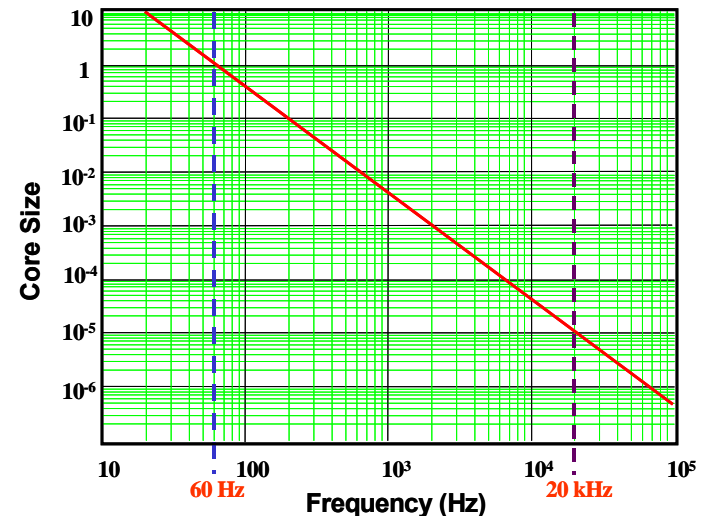
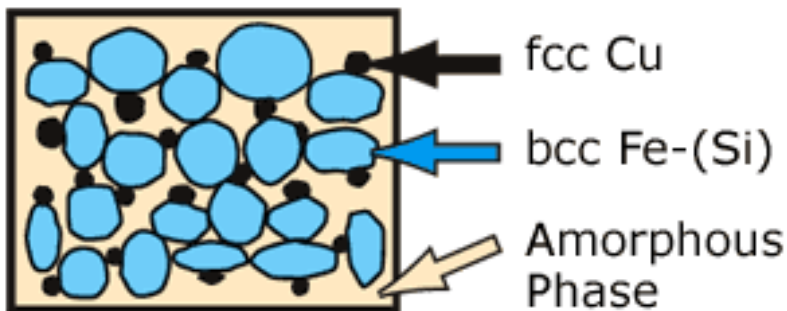
- **Low-Voltage Inverters (460 V AC):**
  - Require high inverter current for each FC module
  - and large number of Inverters for 300 MW Plant
- **Medium-Voltage Inverters (4160 V AC):**
  - Lower inverter current for each FC module
  - Combine multiple FCs with single high power inverter
- **High-Voltage Inverters (18 kV AC):**
  - Replaces 60 Hz transformer with isolation from HF transformer
  - Cascade enables: 18 kV AC inverter by series connection, and interleaved switching decreases losses and filter requirement

# HF Transformer versus 60 Hz Transformer



# High-Frequency Transformer

- **Baseline: Traditional Ferrite Material**
  - Expensive processing for high-power, high frequency (HF)
  - Mature technology; cost may NOT decrease
- **HF magnetic materials: Nano-crystalline or Metglas<sup>®</sup>**
  - Size and cost decrease inversely proportional to frequency
  - Emerging commercial technology; cost continues to decrease
  - *What is cost break-point for HF magnetic material?*



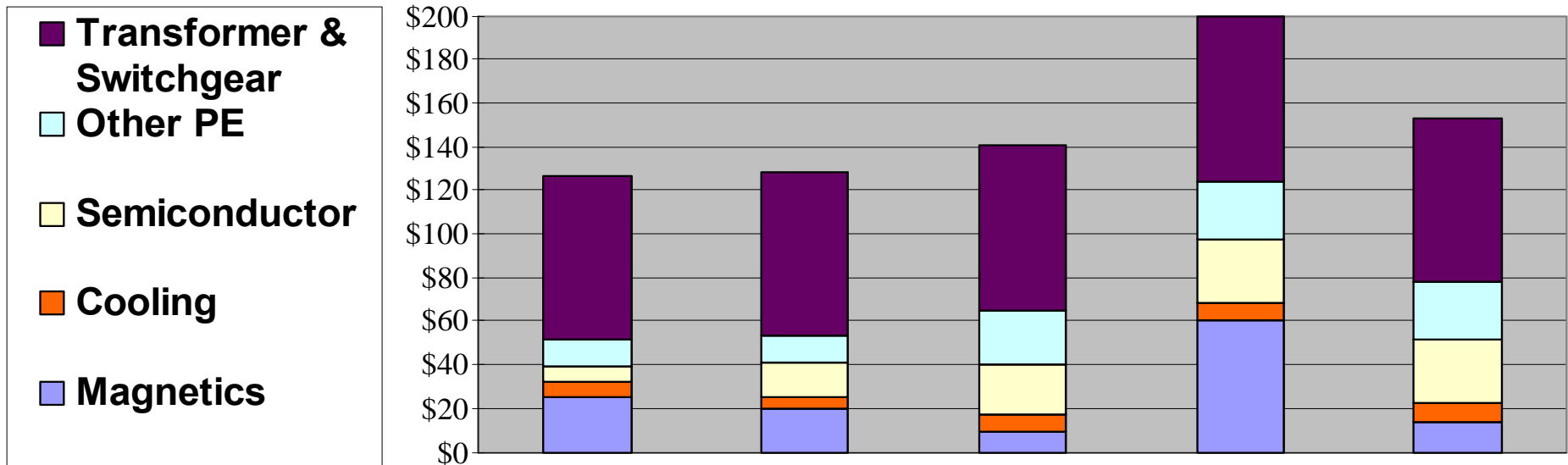
# High-Voltage Semiconductors

- **Baseline: High-Voltage (HV) Silicon devices (IGBT, IGCT)**
  - Typically ~6.5 kV blocking voltage maximum
  - Requires multi-level inverter for 4160 V AC
  - Low switching frequency (< 500 Hz) requires larger filter
- **High-Voltage, High-Frequency SiC Switch and Diodes**
  - **12 kV, 20 kHz SiC MOSFET switch and SiC Schottky diode:**
    - Less inverter levels due to higher voltage
    - Less loss, lower heat removal cost
    - Less filter inductance required due to higher frequency
  - **15 kV, 5 kHz SiC IGBT switch and SiC PiN diode:**
    - Higher current per die than SiC MOSFET, therefore lower cost
  - *What is cost break point for HV-HF SiC power semiconductors?*

# Advanced Technology Cost

- Future, high-volume costs: 5 to 10 years, 1 GW/yr
- **Advanced Technology Goals and Cost Break Points**
  - 1.2 kV Schottky diodes: **\$0.2/A**
  - 12 kV Schottky diodes: **\$1/A**
  - 12 kV Half-bridge SiC-MOSFET/SiC-Schottky: **\$10/A**
  - 15 kV SiC-PiN: **\$0.4/A**
  - 15 kV SiC-IGBT/SiC-PiN Module: **\$3.3/A**
  - High-Frequency transformer: **\$2/kW**
  - Power Electronics DC-DC, DC-AC: **150 % overhead**
  - 60Hz Transformer and Switchgear: **50 % overhead**

# Estimated \$/kW: LV Inverter



<b>Inverter Voltage</b>	<b>Low</b>	<b>Low</b>	<b>Low</b>	<b>Low</b>	<b>Low</b>
<b>Converter Stages</b>	<b>One</b>	<b>One</b>	<b>Two</b>	<b>Two</b>	<b>Two</b>
<b>LV-SiC Schottky</b>		<b>yes</b>	<b>yes</b>	<b>yes</b>	<b>yes</b>
<b>HF Transformer</b>				<b>Ferrite</b>	<b>Nano</b>
<b>60 Hz Transformer</b>	<b>yes</b>	<b>yes</b>	<b>yes</b>	<b>yes</b>	<b>yes</b>

**Risk Level:**

**Low**

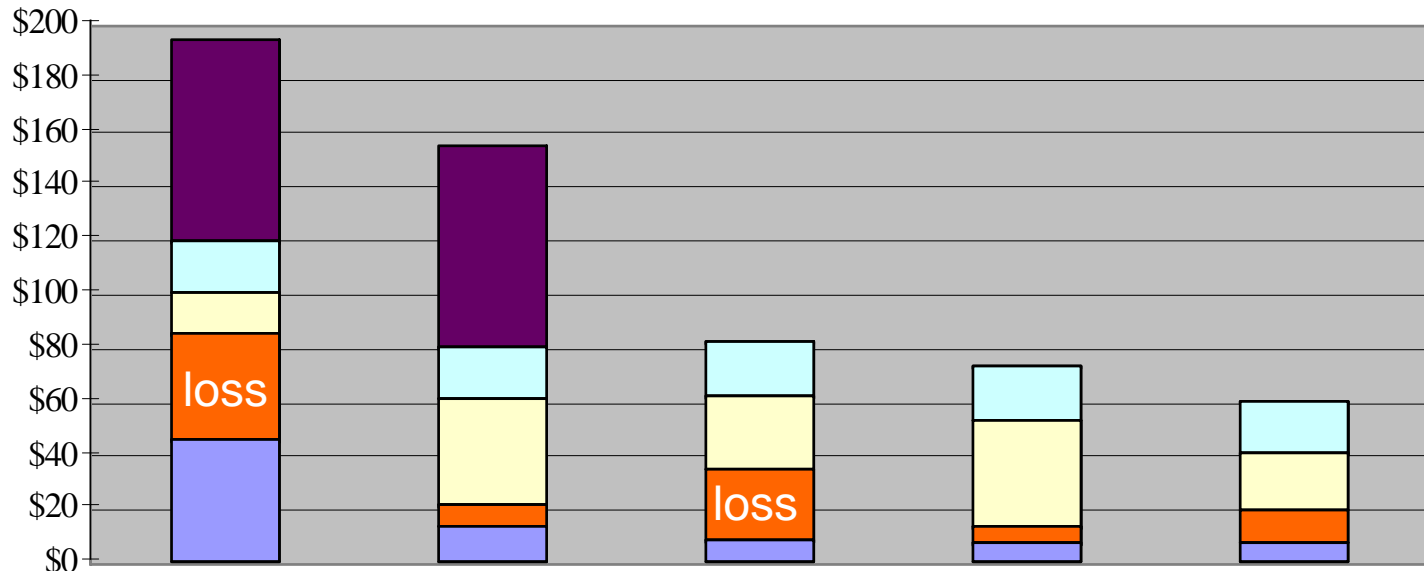
**Moderate**

**Considerable**

**High**

# Estimated \$/kW: MV & HV Inverter

- Transformer & Switchgear
- Other PE
- Semiconductor
- Cooling
- Magnetics



<b>Inverter Voltage</b>	<b>Medium</b>	<b>Medium</b>	<b>High</b>	<b>High</b>	<b>High</b>
<b>HV-SiC Diode</b>		<b>Schottky</b>	<b>Schottky</b>	<b>Schottky</b>	<b>PiN</b>
<b>HV-SiC Switch</b>		<b>MOSFET</b>		<b>MOSFET</b>	<b>IGBT</b>
<b>HF Transformer</b>	<b>Nano</b>	<b>Nano</b>	<b>Nano</b>	<b>Nano</b>	<b>Nano</b>
<b>60 Hz Transformer</b>	<b>yes</b>	<b>yes</b>			

**Risk Level:**

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**Considerable**

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# SiC Power Devices

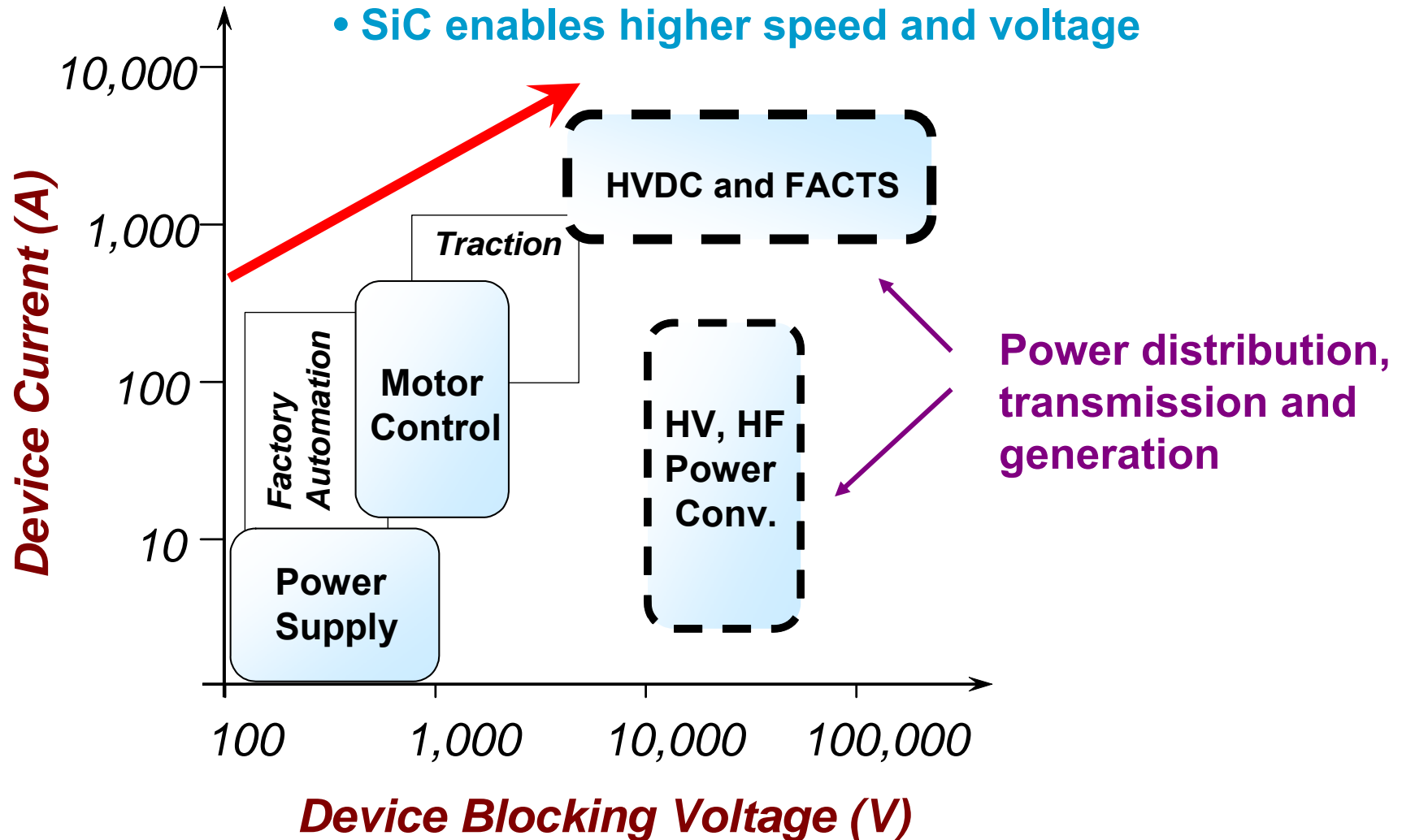
SiC wide bandgap material enables better electrical and thermal performance than Si power devices

Semi-Conductor Material	Energy Bandgap (eV)	Breakdown Electric Field (V/cm)	Thermal Conductivity (W/m·K)	Saturated Electron Drift Velocity (cm/sec)
4H-SiC	3.26	$2.2 \cdot 10^6$	380	$2.0 \cdot 10^7$
Si	1.12	$2.5 \cdot 10^5$	150	$1.0 \cdot 10^7$

- Handles higher temperature: larger bandgap
- Higher voltage, current and speed: larger breakdown field
- Fault tolerance, Pulsed: intrinsic-temperature, saturation-velocity and thermal-conductivity

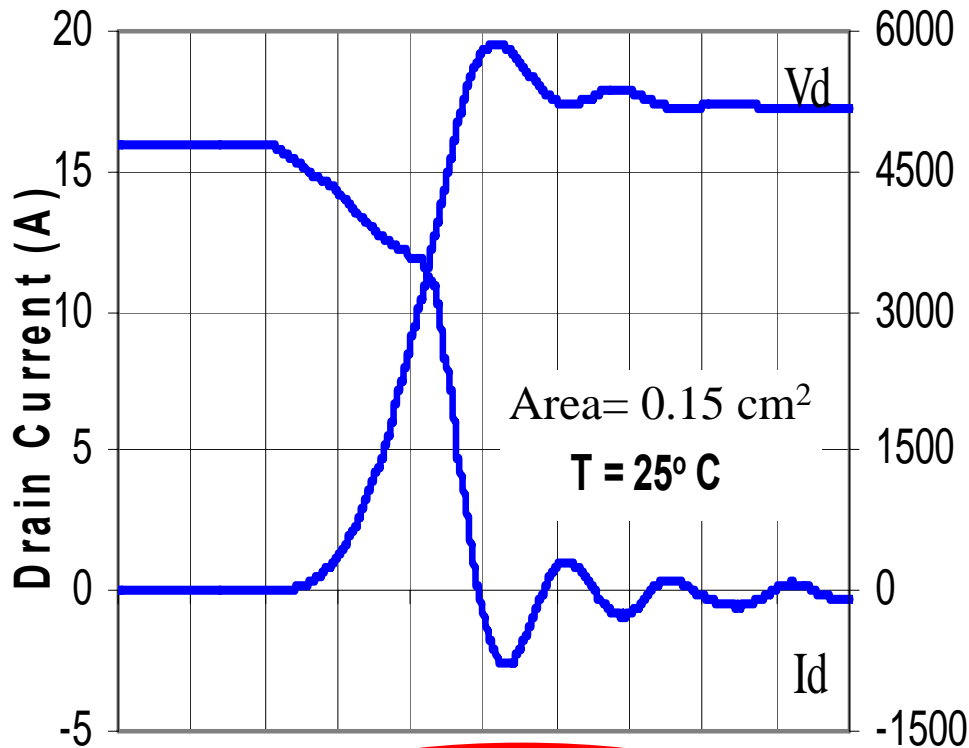
# Switch-Mode Power Applications

- **Switching speed decreases with voltage**
- **SiC enables higher speed and voltage**



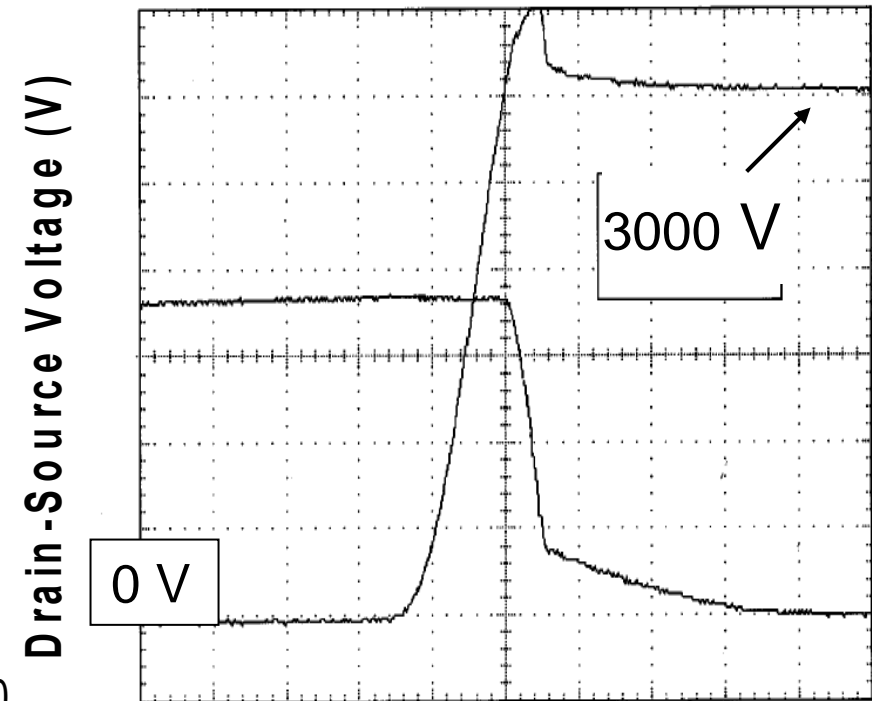
# SiC Power MOSFET: High Speed at High Voltage

SiC MOSFET: 10 kV, 30 ns



15 ns /div

Silicon IGBT: 4.5 kV, 2us



1us /div

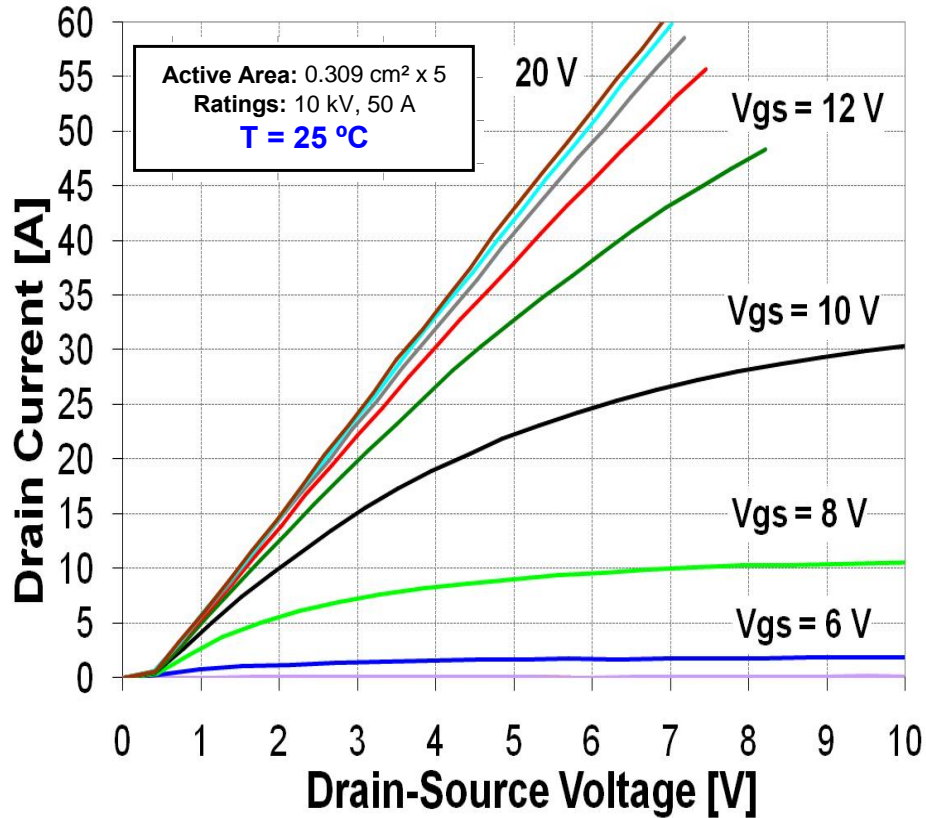
# DARPA High Power Electronics Program

- Phase 2 developed HV-HF SiC power devices:
- Phase 3 goal to develop 13.8 kV, 2.7 MVA Solid State Power Substation (SSPS)

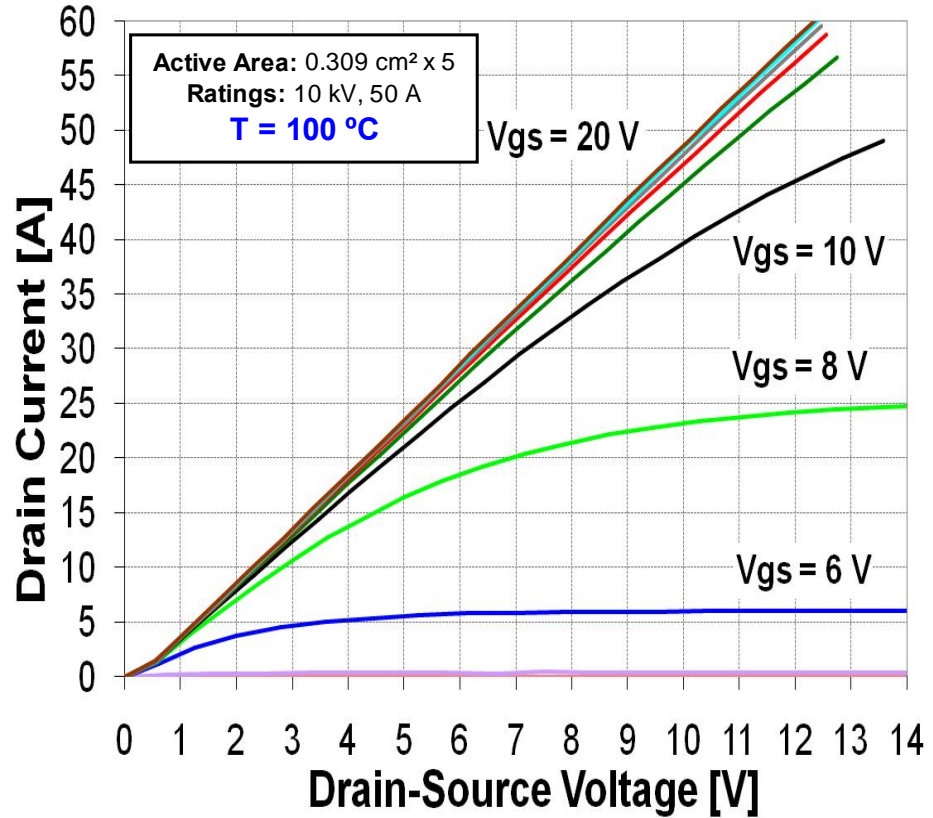
DARPA High Power Electronics Phase 2 Device Development				
	Pin, (JBS) (single die)	MOSFET (single die)	IGBT* (single die)	Half Bridge Module
BV (V)	10 kV	10 kV	15 kV*	10 – 15 kV
Ion (A)	45 A (18 A)	18 A	25 A	110 A
Tj (°C)	200 C	200 C	200 C	200 C
Fsw (Hz)	20 kHz	20 kHz	20 kHz	20 kHz

# 50 A, 10 kV SiC Half-Bridge Module MOSFET Output Characteristics

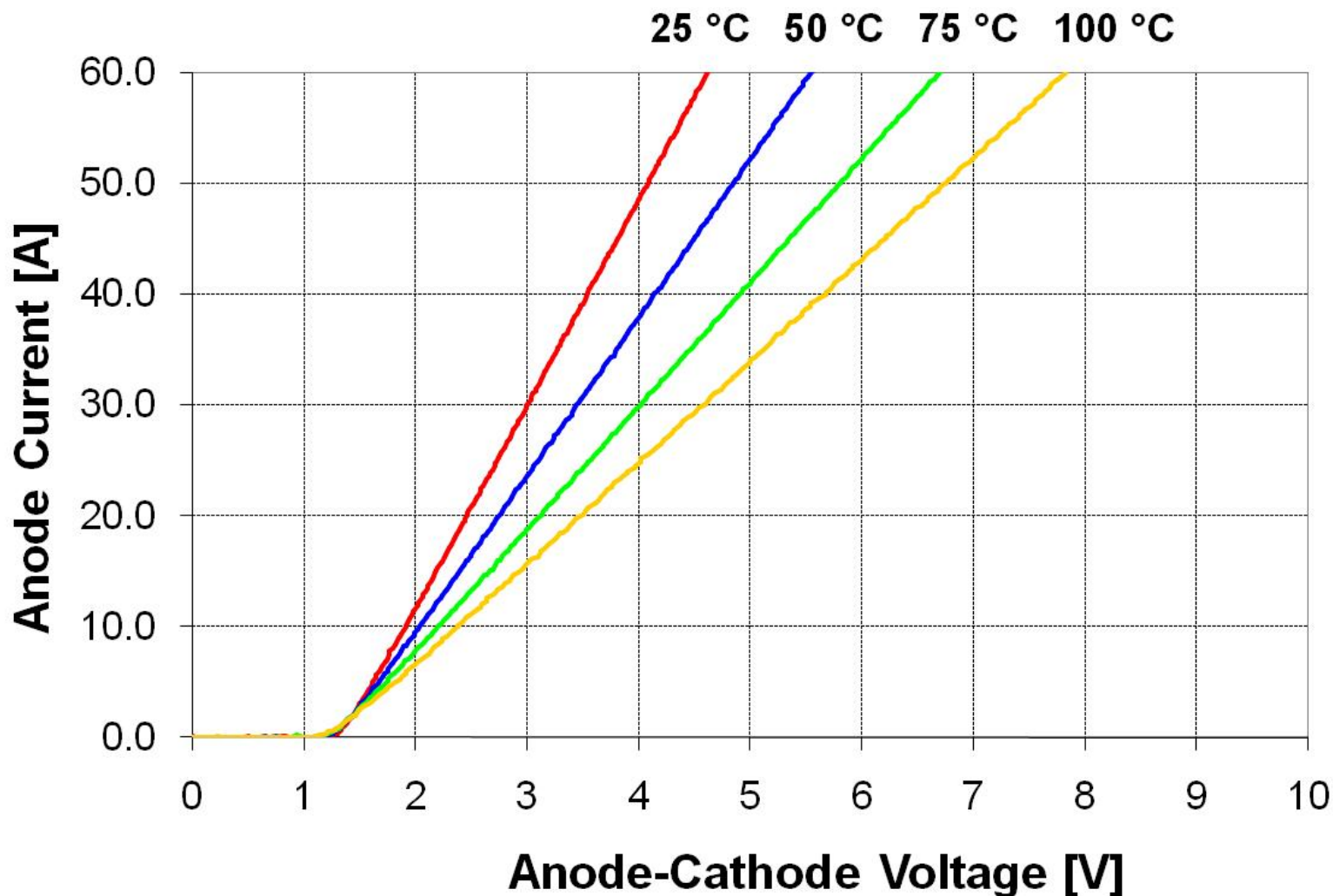
25 °C



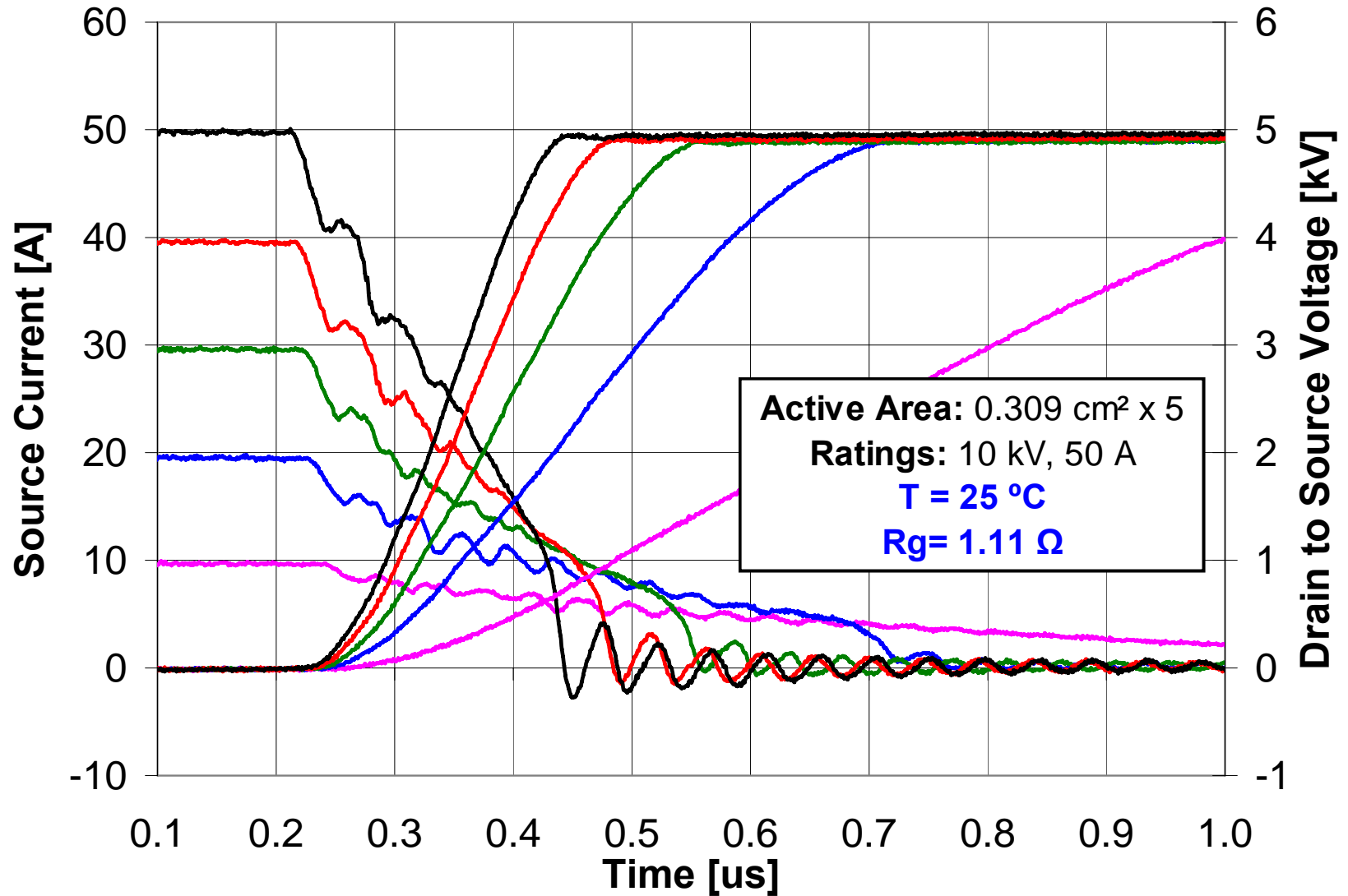
100 °C



# 50 A, 10 kV SiC Half-Bridge Module JBS Diode Output Characteristics



# 50 A, 10 kV SiC Half-Bridge Module Inductive Load Switching



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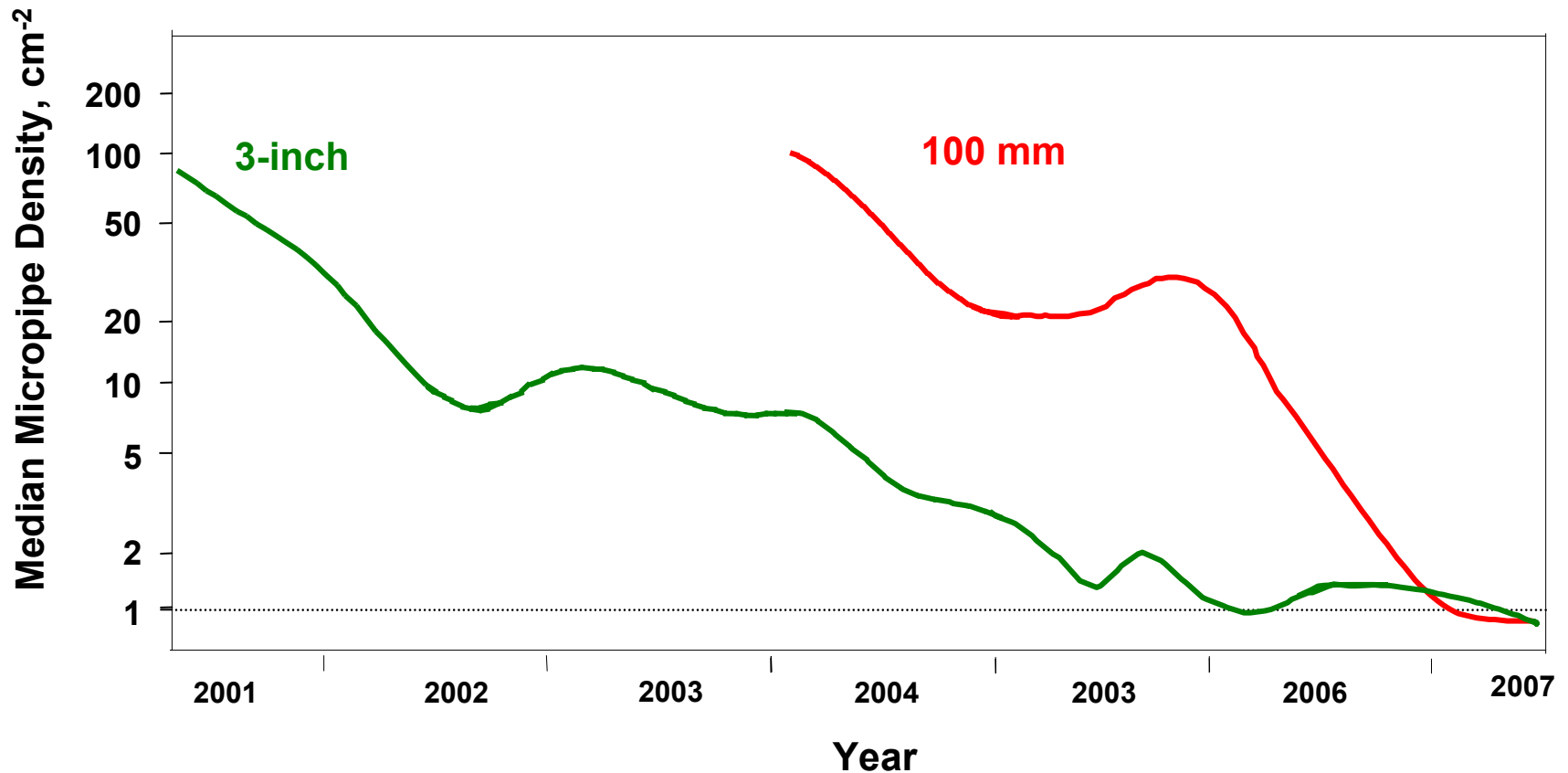


# SiC Power Device Cost Reduction

- **Improved Crystal Quality required for power devices**
  - High conductivity, high field strength type wafers (4HN)
  - Zero Micropipe (ZMP™)
  - Dislocation density reduction
- **Wafer diameter expansion required**
  - 100 mm is now cost-effective, production platform
  - 150 mm expected in 2009/2010 depending on market needs
- **Improved device processing yield for large die area**
- **Specific needs for different power application type**
  - high temperature
  - very high frequency
  - high voltage

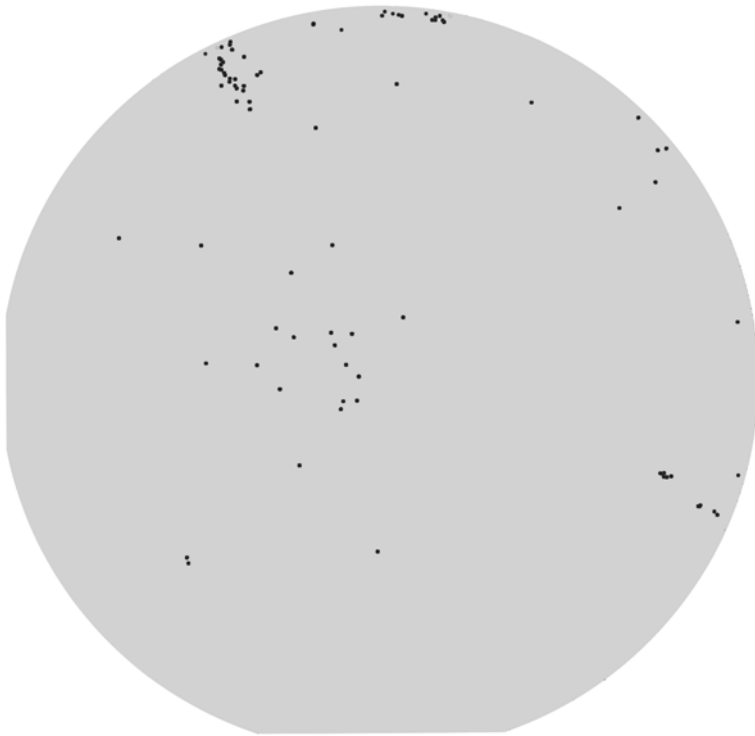
# Reduction of Micropipe Density

Monthly median micropipe density in 2007  
on 100 mm, 4HN wafers was 0.8 cm<sup>-2</sup>



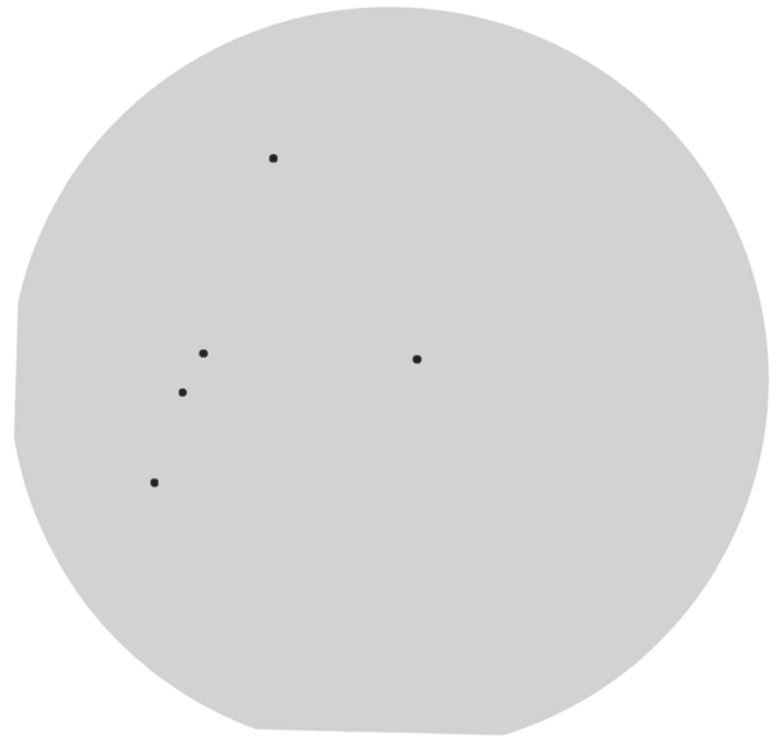
# Micropipe Density in 2007 (100 mm 4HN)

**Typical**



**1 cm<sup>-2</sup>**

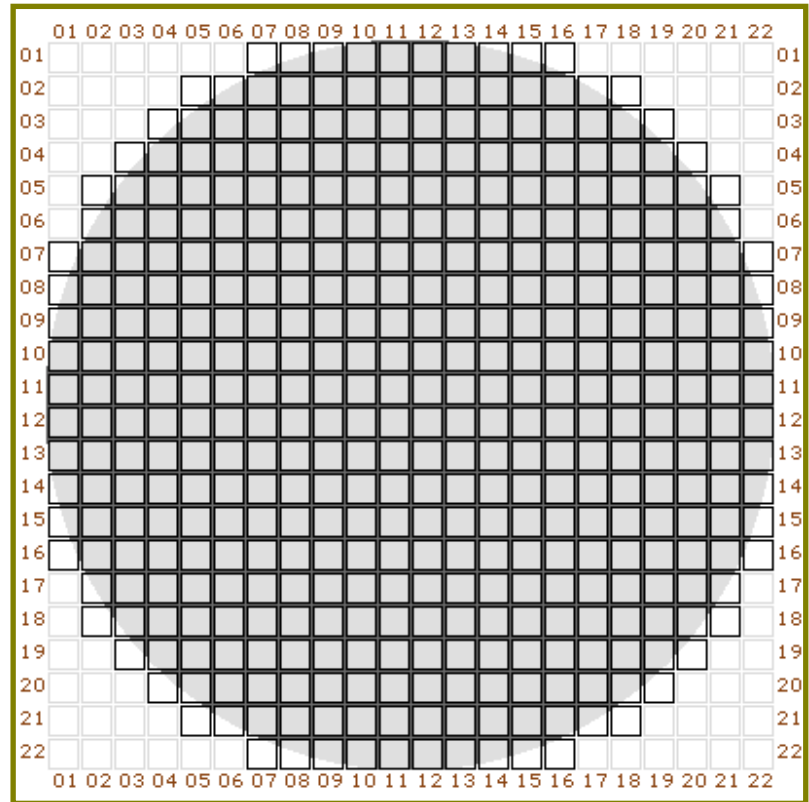
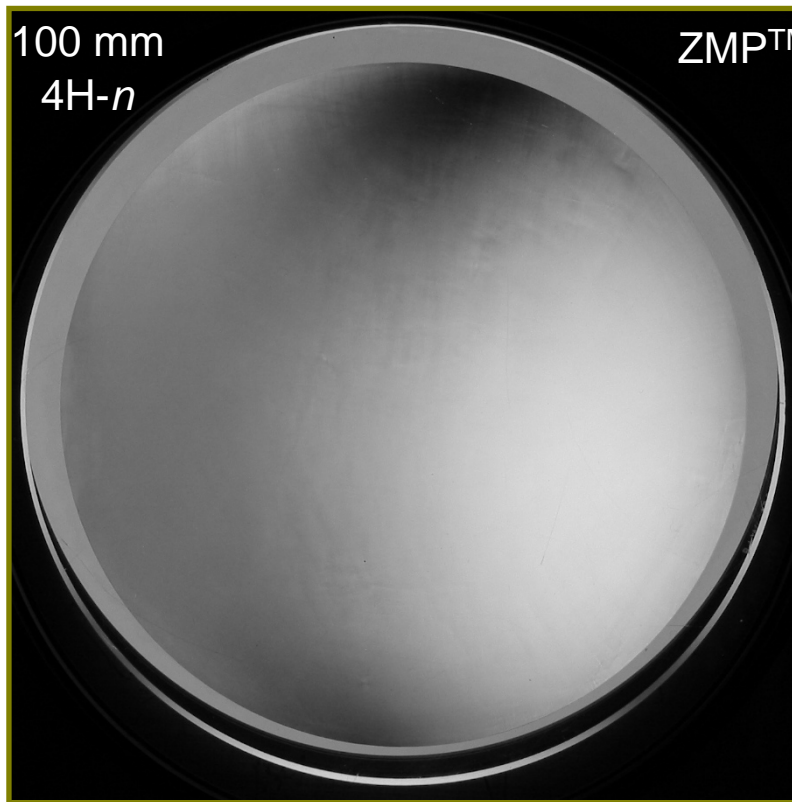
**Low**



**0.06 cm<sup>-2</sup>**

# 100 mm 4HN Zero Micropipe (ZMP™)

Zero Micropipes with no edge exclusion



# Focus on Advancements for High Voltage Devices

- **Wafers with reduced 1c screw dislocation density**
- **Epitaxial structures for >10kV devices**
  - reduce 'killer' epitaxy defect density to  $<1 \text{ cm}^{-2}$
  - Improve uniformity of thickness and doping
  - Increase production volumes
- **Junction termination, surface passivation and packaging are specific to high voltage devices**
- **Minority carrier type devices (e.g. IGBTs, PiN diodes)**
  - Higher current densities for high blocking voltage devices
  - Requires low basal plane dislocation material

# Conclusion

- **SECA goal of \$40-\$100 / kW for Fuel Cell Plant PCS is difficult**
- **Federal, Industry, and NSF coordination initiated to address High-Megawatt PCS requirements**
- **Analysis of technologies to reduce cost of PCS**
  - high-frequency magnetic materials
  - HV-HF SiC semiconductors
- **High voltage inverter enables**
  - using low-cost HF transformer
  - instead of costly 60 Hz transformer
- **Cost reduction program required for HV-HF devices**