

APPENDIX IV

Sediment Trend Statistics for All Selected Sample Lines (see Fig. 4)

Definitions:

- (i) R^2 = multiple correlation coefficient derived from the mean, sorting and skewness of each sample pair making up a significant trend. This is a relative indication of how well the samples are related by transport.
- (ii) Case B: Sediments becoming finer, better sorted and more negatively skewed in the direction of transport.
- (iii) Case C: Sediments becoming coarser, better sorted and more positively skewed in the direction of transport.
- (iv) N = number of possible pairs in the line of samples.
- (v) X = number of pairs making a particular trend in a specific direction.
- (vi) X = Z-score statistic: ** are those trends significant at the 99% level. * are those trends significant at the 95% level. (Only trends at the 99% level are accepted.)
- (vii) Down = transport in the “down-line” direction.
Up = transport in the “up-line” direction.
- (viii) Status defines the dynamic behaviour of the sediments making up the line of samples (i.e., Net Erosion, Net Accretion, Dynamic Equilibrium etc.) See Appendix I for a complete explanation.

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|----|--------|---------------------|
| 1 | B Down: | 0.78 | 10 | 4 | 2.63** | Net Accretion |
| | Up: | | 10 | 1 | -0.24 | |
| | C Down: | | 10 | 0 | -1.20 | |
| | Up: | | 10 | 1 | -0.24 | |
| 2 | B Down: | 0.92 | 6 | 4 | 4.01** | Net Accretion |
| | Up: | | 6 | 2 | 1.54 | |
| | C Down: | | 6 | 0 | -0.93 | |
| | Up: | | 6 | 0 | -0.93 | |
| 3 | B Down: | 0.97 | 21 | 7 | 2.89** | Net Accretion |
| | Up: | | 21 | 1 | -1.07 | |
| | C Down: | | 21 | 0 | -1.73 | |
| | Up: | | 21 | 1 | -1.07 | |
| 4 | B Down: | 0.94 | 45 | 18 | 5.58** | Net Accretion |
| | Up: | | 45 | 3 | -1.18 | |
| | C Down: | | 45 | 0 | -2.54 | |
| | Up: | | 45 | 2 | -1.63 | |
| 5 | B Down: | 0.95 | 66 | 30 | 8.10** | Net Accretion |
| | Up: | | 66 | 4 | -1.58 | |
| | C Down: | | 66 | 2 | -2.33 | |
| | Up: | | 66 | 3 | -1.95 | |
| 6 | B Down: | 0.94 | 55 | 22 | 6.17** | Net Accretion |
| | Up: | | 55 | 4 | -1.17 | |
| | C Down: | | 55 | 0 | -2.80 | |
| | Up: | | 55 | 6 | -0.36 | |
| 7 | B Down: | 0.45 | 91 | 31 | 6.22** | Net Accretion |
| | Up: | | 91 | 3 | -2.65 | |
| | C Down: | | 91 | 3 | -2.65 | |
| | Up: | | 91 | 17 | 1.78* | |
| 8 | B Down: | 0.84 | 136 | 44 | 7.00** | Net Accretion |
| | Up: | | 136 | 7 | -2.59 | |
| | C Down: | | 136 | 1 | -4.15 | |
| | Up: | | 136 | 19 | 0.52 | |
| 9 | B Down: | 0.82 | 105 | 33 | 5.86** | Dynamic Equilibrium |
| | Up: | | 105 | 18 | 1.44 | |
| | C Down: | | 105 | 0 | -3.87 | |
| | Up: | | 105 | 5 | -2.40 | |
| 10 | B Down: | 0.91 | 28 | 14 | 6.00** | Net Accretion |
| | Up: | | 28 | 2 | -0.86 | |
| | C Down: | | 28 | 0 | -2.00 | |
| | Up: | | 28 | 4 | 0.29 | |
| 11 | B Down: | 0.94 | 55 | 13 | 2.50** | Dynamic Equilibrium |
| | Up: | | 55 | 8 | 0.46 | |
| | C Down: | | 55 | 1 | -2.40 | |
| | Up: | | 55 | 0 | -2.80 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|----|--------|----------------|
| 12 | B Down: | | 10 | 0 | -1.20 | Net Erosion |
| | Up: | | 10 | 2 | 0.72 | |
| | C Down: | 0.93 | 10 | 4 | 2.63** | |
| | Up: | | 10 | 1 | -0.24 | |
| 13 | B Down: | | 15 | 4 | 1.66* | Net Erosion |
| | Up: | | 15 | 2 | 0.10 | |
| | C Down: | 0.85 | 15 | 5 | 2.44** | |
| | Up: | | 15 | 3 | 0.88 | |
| 14 | B Down: | 0.85 | 6 | 5 | 5.25** | Net Accretion |
| | Up: | | 6 | 0 | -0.93 | |
| | C Down: | | 6 | 0 | -0.93 | |
| | Up: | | 6 | 0 | -0.93 | |
| 15 | B Down: | | 36 | 2 | -1.26 | Net Erosion |
| | Up: | | 36 | 2 | -1.26 | |
| | C Down: | 0.70 | 36 | 15 | 5.29** | |
| | Up: | | 36 | 4 | -0.25 | |
| 16 | B Down: | | 66 | 4 | -1.58 | Net Erosion |
| | Up: | | 66 | 2 | -2.33 | |
| | C Down: | 0.56 | 66 | 21 | 4.75** | |
| | Up: | | 66 | 9 | 0.28 | |
| 17 | B Down: | | 91 | 7 | -1.39 | Net Erosion |
| | Up: | | 91 | 7 | -1.39 | |
| | C Down: | 0.82 | 91 | 33 | 6.85** | |
| | Up: | | 91 | 9 | -0.75 | |
| 18 | B Down: | | 91 | 4 | -2.34 | Net Erosion |
| | Up: | | 91 | 13 | 0.52 | |
| | C Down: | 0.88 | 91 | 21 | 3.05** | |
| | Up: | | 91 | 15 | 1.15 | |
| 19 | B Down: | | 91 | 5 | -2.02 | Net Erosion |
| | Up: | | 91 | 11 | -0.12 | |
| | C Down: | 0.85 | 91 | 25 | 4.32** | |
| | Up: | | 91 | 15 | 1.15 | |
| 20 | B Down: | | 105 | 13 | -0.04 | Net Erosion |
| | Up: | | 105 | 7 | -1.81 | |
| | C Down: | 0.78 | 105 | 29 | 4.68** | |
| | Up: | | 105 | 14 | 0.26 | |
| 21 | B Down: | | 66 | 3 | -1.95 | Net Erosion |
| | Up: | | 66 | 6 | -0.84 | |
| | C Down: | 0.92 | 66 | 15 | 2.51** | |
| | Up: | | 66 | 7 | -0.47 | |
| 22 | B Down: | | 45 | 5 | -0.28 | Net Erosion |
| | Up: | | 45 | 2 | -1.63 | |
| | C Down: | 0.88 | 45 | 16 | 4.68** | |
| | Up: | | 45 | 7 | 0.62 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|--------|--------|---------------------|
| 23 | B Down: | 0.75 | 105 | 24 | 3.21** | Net Accretion |
| | Up: | | 105 | 7 | -1.81 | |
| | C Down: | 105 | 11 | -0.63 | | |
| | Up: | 105 | 11 | -0.63 | | |
| 24 | B Down: | 0.92 | 105 | 31 | 5.27** | Net Accretion |
| | Up: | | 105 | 10 | -0.92 | |
| | C Down: | 105 | 8 | -1.51 | | |
| | Up: | 105 | 5 | -2.40 | | |
| 25 | B Down: | 0.92 | 66 | 15 | 2.51** | Mixed Case |
| | Up: | | 66 | 2 | -2.33 | |
| | C Down: | 0.65 | 66 | 19 | 4.00** | |
| | Up: | 66 | 13 | 1.77* | | |
| 26 | B Down: | 0.76 | 28 | 11 | 4.29** | Net Accretion |
| | Up: | | 28 | 0 | -2.00 | |
| | C Down: | 28 | 1 | -1.43 | | |
| | Up: | 28 | 3 | -0.29 | | |
| 27 | B Down: | 0.94 | 66 | 18 | 3.63** | Net Accretion |
| | Up: | | 66 | 2 | -2.33 | |
| | C Down: | 66 | 8 | -0.09 | | |
| | Up: | 66 | 4 | -1.58 | | |
| 28 | B Down: | 0.97 | 15 | 6 | 3.22** | Dynamic Equilibrium |
| | Up: | | 15 | 0 | -1.46 | |
| | C Down: | 15 | 0 | -1.46 | | |
| | Up: | 15 | 1 | -0.68 | | |
| 29 | B Down: | 0.98 | 21 | 8 | 3.55** | Net Accretion |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 21 | 0 | -1.73 | | |
| | Up: | 21 | 2 | -0.41 | | |
| 30 | B Down: | 0.98 | 15 | 6 | 3.22** | Dynamic Equilibrium |
| | Up: | | 15 | 0 | -1.46 | |
| | C Down: | 15 | 1 | -0.68 | | |
| | Up: | 15 | 0 | -1.46 | | |
| 31 | B Down: | 0.96 | 21 | 9 | 4.21** | Net Accretion |
| | Up: | | 21 | 3 | 0.25 | |
| | C Down: | 21 | 4 | 0.91 | | |
| | Up: | 21 | 3 | 0.25 | | |
| 32 | B Down: | 0.93 | 28 | 7 | 2.00* | Net Erosion |
| | Up: | | 28 | 1 | -1.43 | |
| | C Down: | 28 | 9 | 3.14** | | |
| | Up: | 28 | 4 | 0.29 | | |
| 33 | B Down: | 0.98 | 21 | 5 | 1.57 | Net Erosion |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 21 | 8 | 3.55** | | |
| | Up: | 21 | 5 | 1.57 | | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|-------|---------|---------------------|
| 34 | B Down: | 0.85 | 21 | 8 | 3.55** | Net Accretion |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 21 | 0 | -1.73 | | |
| | Up: | 21 | 4 | 0.91 | | |
| 35 | B Down: | 1.00 | 6 | 3 | 2.78** | Dynamic Equilibrium |
| | Up: | | 6 | 0 | -0.93 | |
| | C Down: | 6 | 0 | -0.93 | | |
| | Up: | 6 | 2 | 1.54 | | |
| 36 | B Down: | 0.96 | 10 | 5 | 3.59** | Dynamic Equilibrium |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | 10 | 0 | -1.20 | | |
| | Up: | 10 | 3 | 1.67* | | |
| 37 | B Down: | | 91 | 8 | -1.07 | Dynamic Equilibrium |
| | Up: | | 91 | 4 | -2.34 | |
| | C Down: | 0.72 | 91 | 41 | 9.39** | |
| | Up: | | 91 | 14 | 0.83 | |
| 38 | B Down: | | 136 | 11 | -1.56 | Net Erosion |
| | Up: | | 136 | 11 | -1.56 | |
| | C Down: | 0.87 | 136 | 74 | 14.78** | |
| | Up: | | 136 | 14 | -0.78 | |
| 39 | B Down: | | 210 | 25 | -0.26 | Net Erosion |
| | Up: | | 210 | 30 | 0.78 | |
| | C Down: | 0.80 | 210 | 99 | 15.18** | |
| | Up: | | 210 | 11 | -3.18 | |
| 40 | B Down: | | 210 | 24 | -0.47 | Net Erosion |
| | Up: | | 210 | 35 | 1.83* | |
| | C Down: | 0.84 | 210 | 108 | 17.06** | |
| | Up: | | 210 | 11 | -3.18 | |
| 41 | B Down: | | 190 | 25 | 0.27 | Net Erosion |
| | Up: | | 190 | 29 | 1.15 | |
| | C Down: | 0.85 | 190 | 92 | 14.97** | |
| | Up: | | 190 | 12 | -2.58 | |
| 42 | B Down: | | 253 | 29 | -0.50 | Net Erosion |
| | Up: | | 253 | 23 | -1.64 | |
| | C Down: | 0.85 | 253 | 138 | 20.22** | |
| | Up: | | 253 | 18 | -2.59 | |
| 43 | B Down: | | 210 | 25 | -0.26 | Net Erosion |
| | Up: | | 210 | 31 | 0.99 | |
| | C Down: | 0.69 | 210 | 91 | 13.51** | |
| | Up: | | 210 | 7 | -4.02 | |
| 44 | B Down: | | 276 | 31 | -0.64 | Net Erosion |
| | Up: | | 276 | 39 | 0.82 | |
| | C Down: | 0.64 | 276 | 127 | 16.84** | |
| | Up: | | 276 | 10 | -4.46 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|-----|---------|----------------|
| 45 | B Down: | | 325 | 37 | -0.61 | Net Erosion |
| | Up: | | 325 | 51 | 1.74* | |
| | C Down: | 0.60 | 325 | 145 | 17.51** | |
| | Up: | | 325 | 10 | -5.14 | |
| 46 | B Down: | | 325 | 36 | -0.78 | Net Erosion |
| | Up: | | 325 | 38 | -0.44 | |
| | C Down: | 0.81 | 325 | 156 | 19.35** | |
| | Up: | | 325 | 7 | -5.64 | |
| 47 | B Down: | | 666 | 73 | -1.20 | Net Erosion |
| | Up: | | 666 | 97 | 1.61 | |
| | C Down: | 0.43 | 666 | 335 | 29.50** | |
| | Up: | | 666 | 26 | -6.71 | |
| 48 | B Down: | | 528 | 61 | -0.66 | Net Erosion |
| | Up: | | 528 | 61 | -0.66 | |
| | C Down: | 0.72 | 528 | 257 | 25.13** | |
| | Up: | | 528 | 56 | -1.32 | |
| 49 | B Down: | | 741 | 76 | -1.85 | Net Erosion |
| | Up: | | 741 | 99 | 0.71 | |
| | C Down: | 0.46 | 741 | 359 | 29.59** | |
| | Up: | | 741 | 48 | -4.96 | |
| 50 | B Down: | | 595 | 54 | -2.53 | Net Erosion |
| | Up: | | 595 | 88 | 1.69* | |
| | C Down: | 0.52 | 595 | 293 | 27.10** | |
| | Up: | | 595 | 42 | -4.01 | |
| 51 | B Down: | | 28 | 3 | -0.29 | Net Erosion |
| | Up: | | 28 | 6 | 1.43 | |
| | C Down: | 0.98 | 28 | 12 | 4.86** | |
| | Up: | | 28 | 5 | 0.86 | |
| 52 | B Down: | | 36 | 4 | -0.25 | Net Erosion |
| | Up: | | 36 | 4 | -0.25 | |
| | C Down: | 1.00 | 36 | 22 | 8.82** | |
| | Up: | | 36 | 4 | -0.25 | |
| 53 | B Down: | | 36 | 4 | -0.25 | Net Erosion |
| | Up: | | 36 | 4 | -0.25 | |
| | C Down: | 0.97 | 36 | 25 | 10.33** | |
| | Up: | | 36 | 1 | -1.76 | |
| 54 | B Down: | | 21 | 0 | -1.73 | Net Erosion |
| | Up: | | 21 | 5 | 1.57 | |
| | C Down: | 0.93 | 21 | 9 | 4.21** | |
| | Up: | | 21 | 1 | -1.07 | |
| 55 | B Down: | | 946 | 69 | -4.84 | Net Erosion |
| | Up: | | 946 | 86 | -3.17 | |
| | C Down: | 0.39 | 946 | 287 | 16.59** | |
| | Up: | | 946 | 123 | 0.47 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|-----|---------|----------------|
| 56 | B Down: | | 820 | 66 | -3.85 | Net Erosion |
| | Up: | | 820 | 72 | -3.22 | |
| | C Down: | 0.42 | 820 | 247 | 15.26** | |
| | Up: | | 820 | 122 | 2.06* | |
| 57 | B Down: | | 903 | 87 | -2.60 | Net Erosion |
| | Up: | | 903 | 69 | -4.41 | |
| | C Down: | 0.30 | 903 | 248 | 13.60** | |
| | Up: | | 903 | 135 | 2.23* | |
| 58 | B Down: | | 861 | 72 | -3.67 | Net Erosion |
| | Up: | | 861 | 67 | -4.19 | |
| | C Down: | 0.37 | 861 | 256 | 15.29** | |
| | Up: | | 861 | 119 | 1.17 | |
| 59 | B Down: | | 780 | 82 | -1.68 | Net Erosion |
| | Up: | | 780 | 53 | -4.82 | |
| | C Down: | 0.25 | 780 | 193 | 10.34** | |
| | Up: | | 780 | 118 | 2.22* | |
| 60 | B Down: | | 741 | 80 | -1.40 | Net Erosion |
| | Up: | | 741 | 56 | -4.07 | |
| | C Down: | 0.29 | 741 | 182 | 9.93** | |
| | Up: | | 741 | 109 | 1.82* | |
| 61 | B Down: | 0.68 | 210 | 41 | 3.08** | Mixed Case |
| | Up: | | 210 | 12 | -2.97 | |
| | C Down: | 0.54 | 210 | 89 | 13.09** | |
| | Up: | | 210 | 4 | -4.64 | |
| 62 | B Down: | 0.74 | 136 | 28 | 2.85** | Mixed Case |
| | Up: | | 136 | 12 | -1.30 | |
| | C Down: | 0.72 | 136 | 58 | 10.63** | |
| | Up: | | 136 | 2 | -3.89 | |
| 63 | B Down: | | 120 | 16 | 0.28 | Net Erosion |
| | Up: | | 120 | 12 | -0.83 | |
| | C Down: | 0.72 | 120 | 57 | 11.59** | |
| | Up: | | 120 | 1 | -3.86 | |
| 64 | B Down: | | 105 | 12 | -0.33 | Net Erosion |
| | Up: | | 105 | 19 | 1.73* | |
| | C Down: | 0.53 | 105 | 54 | 12.06** | |
| | Up: | | 105 | 1 | -3.58 | |
| 65 | B Down: | | 91 | 12 | 0.20 | Net Erosion |
| | Up: | | 91 | 12 | 0.20 | |
| | C Down: | 0.82 | 91 | 49 | 11.93** | |
| | Up: | | 91 | 1 | -3.29 | |
| 66 | B Down: | 0.83 | 10 | 5 | 3.59** | Net Accretion |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | | 10 | 2 | 0.72 | |
| | Up: | | 10 | 0 | -1.20 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|----|-------|--------|----------------|
| 67 | B Down: | 0.92 | 6 | 3 | 2.78** | Net Accretion |
| | Up: | | 6 | 0 | -0.93 | |
| | C Down: | 6 | 0 | -0.93 | | |
| | Up: | 6 | 2 | 1.54 | | |
| 68 | B Down: | 0.96 | 10 | 4 | 2.63** | Mixed Case |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | 0.81 | 10 | 6 | 4.54** | |
| | Up: | 10 | 0 | -1.20 | | |
| 69 | B Down: | | 28 | 1 | -1.43 | Net Erosion |
| | Up: | | 28 | 3 | -0.29 | |
| | C Down: | 0.77 | 28 | 16 | 7.14** | |
| | Up: | 28 | 3 | -0.29 | | |
| 70 | B Down: | | 36 | 5 | 0.25 | Net Erosion |
| | Up: | | 36 | 3 | -0.76 | |
| | C Down: | 0.64 | 36 | 11 | 3.28** | |
| | Up: | 36 | 9 | 2.27* | | |
| 71 | B Down: | 0.50 | 21 | 7 | 2.89** | Net Accretion |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 21 | 2 | -0.41 | | |
| | Up: | 21 | 1 | -1.07 | | |
| 72 | B Down: | 0.71 | 45 | 12 | 2.87** | Net Accretion |
| | Up: | | 45 | 1 | -2.08 | |
| | C Down: | 45 | 3 | -1.18 | | |
| | Up: | 45 | 5 | -0.28 | | |
| 73 | B Down: | 0.92 | 55 | 25 | 7.39** | Net Accretion |
| | Up: | | 55 | 3 | -1.58 | |
| | C Down: | 55 | 9 | 0.87 | | |
| | Up: | 55 | 1 | -2.40 | | |
| 74 | B Down: | 0.92 | 66 | 32 | 8.84** | Net Accretion |
| | Up: | | 66 | 3 | -1.95 | |
| | C Down: | 66 | 9 | 0.28 | | |
| | Up: | 66 | 1 | -2.70 | | |
| 75 | B Down: | 0.91 | 55 | 23 | 6.57** | Net Accretion |
| | Up: | | 55 | 0 | -2.80 | |
| | C Down: | 55 | 10 | 1.27 | | |
| | Up: | 55 | 5 | -0.76 | | |
| 76 | B Down: | 0.97 | 66 | 32 | 8.84** | Net Accretion |
| | Up: | | 66 | 0 | -3.07 | |
| | C Down: | 66 | 12 | 1.40 | | |
| | Up: | 66 | 7 | -0.47 | | |
| 77 | B Down: | 0.96 | 66 | 31 | 8.47** | Net Accretion |
| | Up: | | 66 | 1 | -2.70 | |
| | C Down: | 66 | 10 | 0.65 | | |
| | Up: | 66 | 6 | -0.84 | | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|----|--------|----------------|
| 78 | B Down: | 0.96 | 66 | 32 | 8.84** | Net Accretion |
| | Up: | | 66 | 0 | -3.07 | |
| | C Down: | | 66 | 11 | 1.02 | |
| | Up: | | 66 | 6 | -0.84 | |
| 79 | B Down: | 0.96 | 91 | 37 | 8.12** | Net Accretion |
| | Up: | | 91 | 3 | -2.65 | |
| | C Down: | | 91 | 16 | 1.47 | |
| | Up: | | 91 | 9 | -0.75 | |
| 80 | B Down: | 0.94 | 120 | 45 | 8.28** | Net Accretion |
| | Up: | | 120 | 3 | -3.31 | |
| | C Down: | | 120 | 17 | 0.55 | |
| | Up: | | 120 | 14 | -0.28 | |
| 81 | B Down: | 0.95 | 91 | 38 | 8.44** | Net Accretion |
| | Up: | | 91 | 2 | -2.97 | |
| | C Down: | | 91 | 14 | 0.83 | |
| | Up: | | 91 | 11 | -0.12 | |
| 82 | B Down: | 0.95 | 91 | 37 | 8.12** | Net Accretion |
| | Up: | | 91 | 2 | -2.97 | |
| | C Down: | | 91 | 13 | 0.52 | |
| | Up: | | 91 | 12 | 0.20 | |
| 83 | B Down: | 0.97 | 45 | 21 | 6.93** | Net Accretion |
| | Up: | | 45 | 1 | -2.08 | |
| | C Down: | | 45 | 7 | 0.62 | |
| | Up: | | 45 | 1 | -2.08 | |
| 84 | B Down: | 0.97 | 78 | 33 | 7.96** | Net Accretion |
| | Up: | | 78 | 8 | -0.60 | |
| | C Down: | | 78 | 13 | 1.11 | |
| | Up: | | 78 | 3 | -2.31 | |
| 85 | B Down: | 0.97 | 45 | 21 | 6.93** | Net Accretion |
| | Up: | | 45 | 2 | -1.63 | |
| | C Down: | | 45 | 10 | 1.97* | |
| | Up: | | 45 | 2 | -1.63 | |
| 86 | B Down: | 0.94 | 66 | 24 | 5.86** | Net Accretion |
| | Up: | | 66 | 0 | -3.07 | |
| | C Down: | | 66 | 12 | 1.40 | |
| | Up: | | 66 | 10 | 0.65 | |
| 87 | B Down: | 0.92 | 66 | 25 | 6.23** | Net Accretion |
| | Up: | | 66 | 0 | -3.07 | |
| | C Down: | | 66 | 11 | 1.02 | |
| | Up: | | 66 | 10 | 0.65 | |
| 88 | B Down: | 0.93 | 78 | 28 | 6.25** | Net Accretion |
| | Up: | | 78 | 0 | -3.34 | |
| | C Down: | | 78 | 10 | 0.09 | |
| | Up: | | 78 | 11 | 0.43 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|----|--------|----------------|
| 89 | B Down: | 0.91 | 55 | 20 | 5.35** | Net Accretion |
| | Up: | | 55 | 1 | -2.40 | |
| | C Down: | | 55 | 12 | 2.09* | |
| | Up: | | 55 | 1 | -2.40 | |
| 90 | B Down: | 0.83 | 45 | 13 | 3.32** | Net Accretion |
| | Up: | | 45 | 1 | -2.08 | |
| | C Down: | | 45 | 6 | 0.17 | |
| | Up: | | 45 | 5 | -0.28 | |
| 91 | B Down: | 0.80 | 78 | 23 | 4.54** | Net Accretion |
| | Up: | | 78 | 4 | -1.97 | |
| | C Down: | | 78 | 13 | 1.11 | |
| | Up: | | 78 | 10 | 0.09 | |
| 92 | B Down: | 0.79 | 66 | 15 | 2.51** | Net Accretion |
| | Up: | | 66 | 1 | -2.70 | |
| | C Down: | | 66 | 9 | 0.28 | |
| | Up: | | 66 | 1 | -2.70 | |
| 93 | B Down: | 0.88 | 36 | 13 | 4.28** | Net Accretion |
| | Up: | | 36 | 0 | -2.27 | |
| | C Down: | | 36 | 7 | 1.26 | |
| | Up: | | 36 | 1 | -1.76 | |
| 94 | B Down: | 0.80 | 66 | 17 | 3.26** | Net Accretion |
| | Up: | | 66 | 1 | -2.70 | |
| | C Down: | | 66 | 9 | 0.28 | |
| | Up: | | 66 | 3 | -1.95 | |
| 95 | B Down: | 0.77 | 66 | 16 | 2.88** | Net Accretion |
| | Up: | | 66 | 1 | -2.70 | |
| | C Down: | | 66 | 8 | -0.09 | |
| | Up: | | 66 | 5 | -1.21 | |
| 96 | B Down: | 0.88 | 45 | 16 | 4.68** | Net Accretion |
| | Up: | | 45 | 0 | -2.54 | |
| | C Down: | | 45 | 9 | 1.52 | |
| | Up: | | 45 | 5 | -0.28 | |
| 97 | B Down: | 0.93 | 36 | 13 | 4.28** | Net Accretion |
| | Up: | | 36 | 2 | -1.26 | |
| | C Down: | | 36 | 7 | 1.26 | |
| | Up: | | 36 | 2 | -1.26 | |
| 98 | B Down: | 0.71 | 231 | 45 | 3.21** | Net Accretion |
| | Up: | | 231 | 18 | -2.16 | |
| | C Down: | | 231 | 33 | 0.82 | |
| | Up: | | 231 | 7 | -4.35 | |
| 99 | B Down: | 0.71 | 253 | 55 | 4.44** | Net Accretion |
| | Up: | | 253 | 22 | -1.83 | |
| | C Down: | | 253 | 31 | -0.12 | |
| | Up: | | 253 | 14 | -3.35 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|-----|---------|----------------|
| 100 | B Down: | 0.80 | 325 | 78 | 6.27** | Net Accretion |
| | Up: | | 325 | 38 | -0.44 | |
| | C Down: | 0.80 | 325 | 41 | 0.06 | |
| | Up: | | 325 | 27 | -2.29 | |
| 101 | B Down: | 0.87 | 351 | 83 | 6.31** | Mixed Case |
| | Up: | | 351 | 17 | -4.34 | |
| | C Down: | 0.72 | 351 | 115 | 11.48** | |
| | Up: | | 351 | 49 | 0.83 | |
| 102 | B Down: | 0.85 | 435 | 102 | 6.90** | Mixed Case |
| | Up: | | 435 | 42 | -1.79 | |
| | C Down: | 0.64 | 435 | 123 | 9.95** | |
| | Up: | | 435 | 63 | 1.25 | |
| 103 | B Down: | 0.82 | 630 | 154 | 9.07** | Mixed Case |
| | Up: | | 630 | 63 | -1.90 | |
| | C Down: | 0.65 | 630 | 152 | 8.82** | |
| | Up: | | 630 | 67 | -1.42 | |
| 104 | B Down: | 0.75 | 630 | 200 | 14.61** | Mixed Case |
| | Up: | | 630 | 51 | -3.34 | |
| | C Down: | 0.70 | 630 | 136 | 6.90** | |
| | Up: | | 630 | 69 | -1.17 | |
| 105 | B Down: | 0.77 | 378 | 117 | 10.85** | Mixed Case |
| | Up: | | 378 | 17 | -4.70 | |
| | C Down: | 0.67 | 378 | 86 | 6.03** | |
| | Up: | | 378 | 47 | -0.04 | |
| 106 | B Down: | 0.80 | 351 | 86 | 6.80** | Mixed Case |
| | Up: | | 351 | 12 | -5.14 | |
| | C Down: | 0.61 | 351 | 84 | 6.48** | |
| | Up: | | 351 | 44 | 0.02 | |
| 107 | B Down: | 0.82 | 496 | 82 | 2.72** | Mixed Case |
| | Up: | | 496 | 36 | -3.53 | |
| | C Down: | 0.74 | 496 | 210 | 20.09** | |
| | Up: | | 496 | 75 | 1.76* | |
| 108 | B Down: | 0.85 | 210 | 38 | 2.45** | Mixed Case |
| | Up: | | 210 | 24 | -0.47 | |
| | C Down: | 0.78 | 210 | 112 | 17.89** | |
| | Up: | | 210 | 16 | -2.14 | |
| 109 | B Down: | 0.91 | 66 | 19 | 4.00** | Mixed Case |
| | Up: | | 66 | 4 | -1.58 | |
| | C Down: | 0.77 | 66 | 26 | 6.61** | |
| | Up: | | 66 | 3 | -1.95 | |
| 110 | B Down: | 0.89 | 105 | 22 | 2.62** | Mixed Case |
| | Up: | | 105 | 5 | -2.40 | |
| | C Down: | 0.66 | 105 | 59 | 13.54** | |
| | Up: | | 105 | 4 | -2.69 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|-----|---------|----------------|
| 111 | B Down: | 0.86 | 253 | 44 | 2.35** | Mixed Case |
| | Up: | | 253 | 15 | -3.16 | |
| | C Down: | 0.81 | 253 | 100 | 13.00** | |
| | Up: | | 253 | 28 | -0.69 | |
| 112 | B Down: | 0.99 | 15 | 5 | 2.44** | Mixed Case |
| | Up: | | 15 | 1 | -0.68 | |
| | C Down: | 0.99 | 15 | 7 | 4.00** | |
| | Up: | | 15 | 2 | 0.10 | |
| 113 | B Down: | | 55 | 2 | -1.99 | Net Erosion |
| | Up: | | 55 | 4 | -1.17 | |
| | C Down: | 0.82 | 55 | 39 | 13.10** | |
| | Up: | | 55 | 2 | -1.99 | |
| 114 | B Down: | | 28 | 0 | -2.00 | Net Erosion |
| | Up: | | 28 | 1 | -1.43 | |
| | C Down: | 0.98 | 28 | 25 | 12.29** | |
| | Up: | | 28 | 0 | -2.00 | |
| 115 | B Down: | | 28 | 0 | -2.00 | Net Erosion |
| | Up: | | 28 | 0 | -2.00 | |
| | C Down: | 0.98 | 28 | 25 | 12.29** | |
| | Up: | | 28 | 0 | -2.00 | |
| 116 | B Down: | | 10 | 0 | -1.20 | Net Erosion |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | 0.98 | 10 | 9 | 7.41** | |
| | Up: | | 10 | 0 | -1.20 | |
| 117 | B Down: | | 15 | 2 | 0.10 | Net Erosion |
| | Up: | | 15 | 1 | -0.68 | |
| | C Down: | 0.99 | 15 | 11 | 7.12** | |
| | Up: | | 15 | 0 | -1.46 | |
| 118 | B Down: | 0.92 | 15 | 5 | 2.44** | Mixed Case |
| | Up: | | 15 | 1 | -0.68 | |
| | C Down: | 0.97 | 15 | 8 | 4.78** | |
| | Up: | | 15 | 0 | -1.46 | |
| 119 | B Down: | | 21 | 0 | -1.73 | Net Erosion |
| | Up: | | 21 | 3 | 0.25 | |
| | C Down: | 0.97 | 21 | 13 | 6.85** | |
| | Up: | | 21 | 0 | -1.73 | |
| 120 | B Down: | | 21 | 6 | 2.23* | Net Erosion |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 1.00 | 21 | 9 | 4.21** | |
| | Up: | | 21 | 0 | -1.73 | |
| 121 | B Down: | | 28 | 2 | -0.86 | Net Erosion |
| | Up: | | 28 | 4 | 0.29 | |
| | C Down: | 0.69 | 28 | 12 | 4.86** | |
| | Up: | | 28 | 1 | -1.43 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|----|---------|---------------------|
| 122 | B Down: | | 28 | 5 | 0.86 | Net Erosion |
| | Up: | | 28 | 1 | -1.43 | |
| | C Down: | 0.68 | 28 | 10 | 3.71** | |
| | Up: | | 28 | 3 | -0.29 | |
| 123 | B Down: | | 28 | 1 | -1.43 | Net Erosion |
| | Up: | | 28 | 1 | -1.43 | |
| | C Down: | 0.99 | 28 | 9 | 3.14** | |
| | Up: | | 28 | 6 | 1.43 | |
| 124 | B Down: | 0.84 | 171 | 74 | 12.17** | Net Accretion |
| | Up: | | 171 | 1 | -4.71 | |
| | C Down: | | 171 | 31 | 2.23* | |
| | Up: | | 171 | 26 | 1.07 | |
| 125 | B Down: | 0.88 | 136 | 47 | 7.78** | Net Accretion |
| | Up: | | 136 | 3 | -3.63 | |
| | C Down: | | 136 | 10 | -1.81 | |
| | Up: | | 136 | 7 | -2.59 | |
| 126 | B Down: | | 136 | 15 | -0.52 | Net Erosion |
| | Up: | | 136 | 4 | -3.37 | |
| | C Down: | 0.78 | 136 | 43 | 6.74** | |
| | Up: | | 136 | 20 | 0.78 | |
| 127 | B Down: | 0.82 | 153 | 43 | 5.84** | Net Accretion |
| | Up: | | 153 | 1 | -4.43 | |
| | C Down: | | 153 | 20 | 0.21 | |
| | Up: | | 153 | 12 | -1.74 | |
| 128 | B Down: | | 153 | 26 | 1.68* | Dynamic Equilibrium |
| | Up: | | 153 | 6 | -3.21 | |
| | C Down: | 0.22 | 153 | 36 | 4.13** | |
| | Up: | | 153 | 14 | -1.25 | |
| 129 | B Down: | 0.87 | 120 | 38 | 6.35** | Mixed Case |
| | Up: | | 120 | 2 | -3.59 | |
| | C Down: | 0.82 | 120 | 31 | 4.42** | |
| | Up: | | 120 | 19 | 1.10 | |
| 130 | B Down: | 0.68 | 91 | 28 | 5.27** | Mixed Case |
| | Up: | | 91 | 3 | -2.65 | |
| | C Down: | 0.43 | 91 | 24 | 4.00** | |
| | Up: | | 91 | 4 | -2.34 | |
| 131 | B Down: | 0.79 | 78 | 23 | 4.54** | Mixed Case |
| | Up: | | 78 | 2 | -2.65 | |
| | C Down: | 0.57 | 78 | 34 | 8.30** | |
| | Up: | | 78 | 6 | -1.28 | |
| 132 | B Down: | 0.75 | 91 | 25 | 4.32** | Mixed Case |
| | Up: | | 91 | 1 | -3.29 | |
| | C Down: | 0.52 | 91 | 45 | 10.66** | |
| | Up: | | 91 | 5 | -2.02 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|----|----|--------|---------------------|
| 133 | B Down: | 0.73 | 91 | 23 | 3.68** | Mixed Case |
| | Up: | | 91 | 1 | -3.29 | |
| | C Down: | 0.14 | 91 | 27 | 4.95** | |
| | Up: | | 91 | 5 | -2.02 | |
| 134 | B Down: | 0.58 | 91 | 26 | 4.64** | Mixed Case |
| | Up: | | 91 | 0 | -3.61 | |
| | C Down: | 0.37 | 91 | 19 | 2.42** | |
| | Up: | | 91 | 4 | -2.34 | |
| 135 | B Down: | 0.99 | 78 | 22 | 4.19** | Mixed Case |
| | Up: | | 78 | 4 | -1.97 | |
| | C Down: | 0.40 | 78 | 17 | 2.48** | |
| | Up: | | 78 | 8 | -0.60 | |
| 136 | B Down: | 1.00 | 78 | 18 | 2.82** | Mixed Case |
| | Up: | | 78 | 3 | -2.31 | |
| | C Down: | 0.59 | 78 | 23 | 4.54** | |
| | Up: | | 78 | 10 | 0.09 | |
| 137 | B Down: | 1.00 | 66 | 16 | 2.88** | Mixed Case |
| | Up: | | 66 | 2 | -2.33 | |
| | C Down: | 0.70 | 66 | 18 | 3.63** | |
| | Up: | | 66 | 8 | -0.09 | |
| 138 | B Down: | | 78 | 13 | 1.11 | Dynamic Equilibrium |
| | Up: | | 78 | 1 | -3.00 | |
| | C Down: | 0.96 | 78 | 24 | 4.88** | |
| | Up: | | 78 | 10 | 0.09 | |
| 139 | B Down: | | 66 | 13 | 1.77* | Dynamic Equilibrium |
| | Up: | | 66 | 0 | -3.07 | |
| | C Down: | 0.92 | 66 | 22 | 5.12** | |
| | Up: | | 66 | 9 | 0.28 | |
| 140 | B Down: | | 78 | 12 | 0.77 | Dynamic Equilibrium |
| | Up: | | 78 | 2 | -2.65 | |
| | C Down: | 0.93 | 78 | 29 | 6.59** | |
| | Up: | | 78 | 11 | 0.43 | |
| 141 | B Down: | | 66 | 9 | 0.28 | Dynamic Equilibrium |
| | Up: | | 66 | 1 | -2.70 | |
| | C Down: | 0.96 | 66 | 21 | 4.75** | |
| | Up: | | 66 | 13 | 1.77* | |
| 142 | B Down: | | 66 | 4 | -1.58 | Dynamic Equilibrium |
| | Up: | | 66 | 1 | -2.70 | |
| | C Down: | 0.91 | 66 | 16 | 2.88** | |
| | Up: | | 66 | 11 | 1.02 | |
| 143 | B Down: | | 78 | 14 | 1.46 | Dynamic Equilibrium |
| | Up: | | 78 | 1 | -3.00 | |
| | C Down: | 0.95 | 78 | 18 | 2.82** | |
| | Up: | | 78 | 12 | 0.77 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|----|----|---------|---------------------|
| 144 | B Down: | | 45 | 7 | 0.62 | Dynamic Equilibrium |
| | Up: | | 45 | 2 | -1.63 | |
| | C Down: | 0.94 | 45 | 15 | 4.23** | |
| | Up: | | 45 | 7 | 0.62 | |
| 145 | B Down: | | 3 | 0 | -0.65 | Dynamic Equilibrium |
| | Up: | | 3 | 0 | -0.65 | |
| | C Down: | 1.00 | 3 | 3 | 4.58** | |
| | Up: | | 3 | 0 | -0.65 | |
| 146 | B Down: | | 15 | 0 | -1.46 | Dynamic Equilibrium |
| | Up: | | 15 | 1 | -0.68 | |
| | C Down: | 0.99 | 15 | 10 | 6.34** | |
| | Up: | | 15 | 4 | 1.66* | |
| 147 | B Down: | | 10 | 0 | -1.20 | Dynamic Equilibrium |
| | Up: | | 10 | 1 | -0.24 | |
| | C Down: | 0.99 | 10 | 6 | 4.54** | |
| | Up: | | 10 | 3 | 1.67* | |
| 148 | B Down: | | 10 | 0 | -1.20 | Dynamic Equilibrium |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | 1.00 | 10 | 7 | 5.50** | |
| | Up: | | 10 | 2 | 0.72 | |
| 149 | B Down: | | 6 | 0 | -0.93 | Net Erosion |
| | Up: | | 6 | 2 | 1.54 | |
| | C Down: | 0.94 | 6 | 3 | 2.78** | |
| | Up: | | 6 | 0 | -0.93 | |
| 150 | B Down: | | 28 | 0 | -2.00 | Dynamic Equilibrium |
| | Up: | | 28 | 0 | -2.00 | |
| | C Down: | 0.99 | 28 | 24 | 11.71** | |
| | Up: | | 28 | 2 | -0.86 | |
| 151 | B Down: | | 21 | 0 | -1.73 | Dynamic Equilibrium |
| | Up: | | 21 | 1 | -1.07 | |
| | C Down: | 0.98 | 21 | 14 | 7.51** | |
| | Up: | | 21 | 6 | 2.23* | |
| 152 | B Down: | | 21 | 0 | -1.73 | Dynamic Equilibrium |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 0.97 | 21 | 13 | 6.85** | |
| | Up: | | 21 | 6 | 2.23* | |
| 153 | B Down: | | 15 | 1 | -0.68 | Dynamic Equilibrium |
| | Up: | | 15 | 0 | -1.46 | |
| | C Down: | 0.90 | 15 | 9 | 5.56** | |
| | Up: | | 15 | 4 | 1.66* | |
| 154 | B Down: | | 45 | 2 | -1.63 | Dynamic Equilibrium |
| | Up: | | 45 | 3 | -1.18 | |
| | C Down: | 0.90 | 45 | 21 | 6.93** | |
| | Up: | | 45 | 10 | 1.97* | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|----|----|--------|---------------------|
| 155 | B Down: | | 55 | 6 | -0.36 | Dynamic Equilibrium |
| | Up: | | 55 | 3 | -1.58 | |
| | C Down: | 0.97 | 55 | 28 | 8.61** | |
| | Up: | | 55 | 9 | 0.87 | |
| 156 | B Down: | | 55 | 9 | 0.87 | Dynamic Equilibrium |
| | Up: | | 55 | 4 | -1.17 | |
| | C Down: | 0.93 | 55 | 20 | 5.35** | |
| | Up: | | 55 | 4 | -1.17 | |
| 157 | B Down: | | 55 | 9 | 0.87 | Dynamic Equilibrium |
| | Up: | | 55 | 2 | -1.99 | |
| | C Down: | 0.93 | 55 | 15 | 3.31** | |
| | Up: | | 55 | 5 | -0.76 | |
| 158 | B Down: | | 45 | 2 | -1.63 | Dynamic Equilibrium |
| | Up: | | 45 | 2 | -1.63 | |
| | C Down: | 0.66 | 45 | 21 | 6.93** | |
| | Up: | | 45 | 7 | 0.62 | |
| 159 | B Down: | | 45 | 2 | -1.63 | Dynamic Equilibrium |
| | Up: | | 45 | 3 | -1.18 | |
| | C Down: | 0.82 | 45 | 18 | 5.58** | |
| | Up: | | 45 | 10 | 1.97* | |
| 160 | B Down: | | 91 | 4 | -2.34 | Dynamic Equilibrium |
| | Up: | | 91 | 11 | -0.12 | |
| | C Down: | 0.77 | 91 | 32 | 6.54** | |
| | Up: | | 91 | 15 | 1.15 | |
| 161 | B Down: | | 36 | 5 | 0.25 | Dynamic Equilibrium |
| | Up: | | 36 | 3 | -0.76 | |
| | C Down: | 0.97 | 36 | 14 | 4.79** | |
| | Up: | | 36 | 9 | 2.27* | |
| 162 | B Down: | 0.88 | 66 | 18 | 3.63** | Net Accretion |
| | Up: | | 66 | 2 | -2.33 | |
| | C Down: | | 66 | 9 | 0.28 | |
| | Up: | | 66 | 14 | 2.14* | |
| 163 | B Down: | 0.77 | 66 | 15 | 2.51** | Net Accretion |
| | Up: | | 66 | 3 | -1.95 | |
| | C Down: | | 66 | 3 | -1.95 | |
| | Up: | | 66 | 7 | -0.47 | |
| 164 | B Down: | | 21 | 0 | -1.73 | Net Erosion |
| | Up: | | 21 | 1 | -1.07 | |
| | C Down: | 0.90 | 21 | 16 | 8.83** | |
| | Up: | | 21 | 2 | -0.41 | |
| 165 | B Down: | | 10 | 0 | -1.20 | Dynamic Equilibrium |
| | Up: | | 10 | 1 | -0.24 | |
| | C Down: | 0.99 | 10 | 6 | 4.54** | |
| | Up: | | 10 | 2 | 0.72 | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|-----|----|---------|---------------------|
| 166 | B Down: | | 10 | 0 | -1.20 | Net Erosion |
| | Up: | | 10 | 2 | 0.72 | |
| | C Down: | 1.00 | 10 | 4 | 2.63** | |
| | Up: | | 10 | 3 | 1.67* | |
| 167 | B Down: | | 10 | 0 | -1.20 | Dynamic Equilibrium |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | 1.00 | 10 | 6 | 4.54** | |
| | Up: | | 10 | 3 | 1.67* | |
| 168 | B Down: | | 10 | 0 | -1.20 | Dynamic Equilibrium |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | 0.99 | 10 | 8 | 6.45** | |
| | Up: | | 10 | 2 | 0.72 | |
| 169 | B Down: | | 120 | 1 | -3.86 | Dynamic Equilibrium |
| | Up: | | 120 | 6 | -2.48 | |
| | C Down: | 0.43 | 120 | 30 | 4.14** | |
| | Up: | | 120 | 20 | 1.38 | |
| 170 | B Down: | | 120 | 13 | -0.55 | Dynamic Equilibrium |
| | Up: | | 120 | 5 | -2.76 | |
| | C Down: | 0.84 | 120 | 62 | 12.97** | |
| | Up: | | 120 | 23 | 2.21* | |
| 171 | B Down: | | 105 | 1 | -3.58 | Dynamic Equilibrium |
| | Up: | | 105 | 6 | -2.10 | |
| | C Down: | 0.78 | 105 | 58 | 13.24** | |
| | Up: | | 105 | 21 | 2.32* | |
| 172 | B Down: | | 45 | 0 | -2.54 | Dynamic Equilibrium |
| | Up: | | 45 | 0 | -2.54 | |
| | C Down: | 0.98 | 45 | 35 | 13.24** | |
| | Up: | | 45 | 9 | 1.52 | |
| 173 | B Down: | | 45 | 1 | -2.08 | Dynamic Equilibrium |
| | Up: | | 45 | 1 | -2.08 | |
| | C Down: | 0.84 | 45 | 28 | 10.09** | |
| | Up: | | 45 | 7 | 0.62 | |
| 174 | B Down: | | 36 | 0 | -2.27 | Dynamic Equilibrium |
| | Up: | | 36 | 0 | -2.27 | |
| | C Down: | 0.99 | 36 | 31 | 13.35** | |
| | Up: | | 36 | 3 | -0.76 | |
| 175 | B Down: | | 36 | 0 | -2.27 | Dynamic Equilibrium |
| | Up: | | 36 | 0 | -2.27 | |
| | C Down: | 0.99 | 36 | 23 | 9.32** | |
| | Up: | | 36 | 2 | -1.26 | |
| 176 | B Down: | 0.84 | 36 | 11 | 3.28** | Net Accretion |
| | Up: | | 36 | 0 | -2.27 | |
| | C Down: | | 36 | 4 | -0.25 | |
| | Up: | | 36 | 8 | 1.76* | |

| Line | | R2 | N | X | Z | Interpretation |
|------|---------|------|----|-------|--------|---------------------|
| 177 | B Down: | 0.91 | 55 | 29 | 9.02** | Net Accretion |
| | Up: | | 55 | 0 | -2.80 | |
| | C Down: | 55 | 3 | -1.58 | | |
| | Up: | 55 | 11 | 1.68* | | |
| 178 | B Down: | 0.80 | 55 | 22 | 6.17** | Net Accretion |
| | Up: | | 55 | 1 | -2.40 | |
| | C Down: | 55 | 11 | 1.68* | | |
| | Up: | 55 | 12 | 2.09* | | |
| 179 | B Down: | | 21 | 3 | 0.25 | Net Accretion |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 0.99 | 21 | 13 | 6.85** | |
| | Up: | | 21 | 3 | 0.25 | |
| 180 | B Down: | | 21 | 1 | -1.07 | Net Accretion |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 0.99 | 21 | 16 | 8.83** | |
| | Up: | | 21 | 3 | 0.25 | |
| 181 | B Down: | | 21 | 2 | -0.41 | Net Accretion |
| | Up: | | 21 | 0 | -1.73 | |
| | C Down: | 0.99 | 21 | 15 | 8.17** | |
| | Up: | | 21 | 3 | 0.25 | |
| 182 | B Down: | | 28 | 6 | 1.43 | Dynamic Equilibrium |
| | Up: | | 28 | 0 | -2.00 | |
| | C Down: | 0.96 | 28 | 14 | 6.00** | |
| | Up: | | 28 | 7 | 2.00* | |
| 183 | B Down: | | 10 | 0 | -1.20 | Dynamic Equilibrium |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | 0.97 | 10 | 5 | 3.59** | |
| | Up: | | 10 | 3 | 1.67* | |
| 184 | B Down: | | 10 | 1 | -0.24 | Dynamic Equilibrium |
| | Up: | | 10 | 0 | -1.20 | |
| | C Down: | 0.96 | 10 | 6 | 4.54** | |
| | Up: | | 10 | 3 | 1.67* | |
| 185 | B Down: | | 3 | 0 | -0.65 | Dynamic Equilibrium |
| | Up: | | 3 | 0 | -0.65 | |
| | C Down: | 1.00 | 3 | 3 | 4.58** | |
| | Up: | | 3 | 0 | -0.65 | |
| 186 | B Down: | | 3 | 0 | -0.65 | Dynamic Equilibrium |
| | Up: | | 3 | 0 | -0.65 | |
| | C Down: | 1.00 | 3 | 3 | 4.58** | |
| | Up: | | 3 | 0 | -0.65 | |