

TASK 2

MOORING LOAD ESTIMATION UNCERTAINTY

1. SUMMARY

2. MEAN ENVIRONMENT LOADS

- WIND FORCE
- CURRENT FORCE
- WAVE-DRIFT LOAD

3. VESSEL DYNAMIC OFFSETS

- WAVE-FREQUENCY MOTIONS
- LOW-FREQUENCY MOTIONS

4. ESTIMATION OF LF DAMPING FORCES

- VESSEL WAVE-DRIFT DAMPING
- VESSEL VISCOUS DAMPING
- VESSEL AERODYNAMIC DAMPING
- MOORING LINE DAMPING
 - MATERIAL
 - SOIL
 - COUPLED LF-WF MOTIONS

SUMMARY

1. PURPOSE

- TO QUANTIFY LOAD UNCERTAINTIES
- TO PRODUCE INITIAL ENGINEERING ESTIMATES OF LF DAMPING

2. RELATIVE ACCURACY OF MEAN LOADS

	<u>SEMI</u>	<u>SHIP</u>
WIND	GOOD	FAIR
CURRENT	FAIR	FAIR
WAVE	FAIR	FAIR

3. RELATIVE ACCURACY OF MOTIONS

	<u>SEMI</u>	<u>SHIP</u>
WF MOTION	GOOD	GOOD
LF MOTION	POOR	POOR

4. LF DAMPING PER GOMEX 10-YEAR STORM (% OF SYSTEM CRITICAL, WD = 1000')

VESSEL	<u>SEMI (SEDCO 700)</u>		<u>DRILLSHIP (L=380')</u>	
	<u>HEAD</u>	<u>BEAM</u>	<u>HEAD</u>	<u>BEAM</u>
DRIFT DAMPING	.2	.2	1	2.9
VISCOUS	1.7 TO 13	2.5 TO 22	.2 TO 2.3	7 TO 26
AERODYNAMIC	2.7	1.9	2	3.4
<u>MOORING LINES</u>	<u>4.6 TO 9.8</u>	<u>4.6 TO 9.8</u>	<u>4 TO 22</u>	<u>9 TO 24</u>
TOTAL	9 TO 21%	9 TO 34%	7 TO 27%	22 TO 56%

WIND AND CURRENT LOAD

1. VESSEL TYPES

- SEMISUBMERSIBLES
- DRILL SHIPS

2. DATA SOURCE

- MODEL TEST DATA (BASE CASE)
- OPERATIONS MANUALS
- LITERATURE

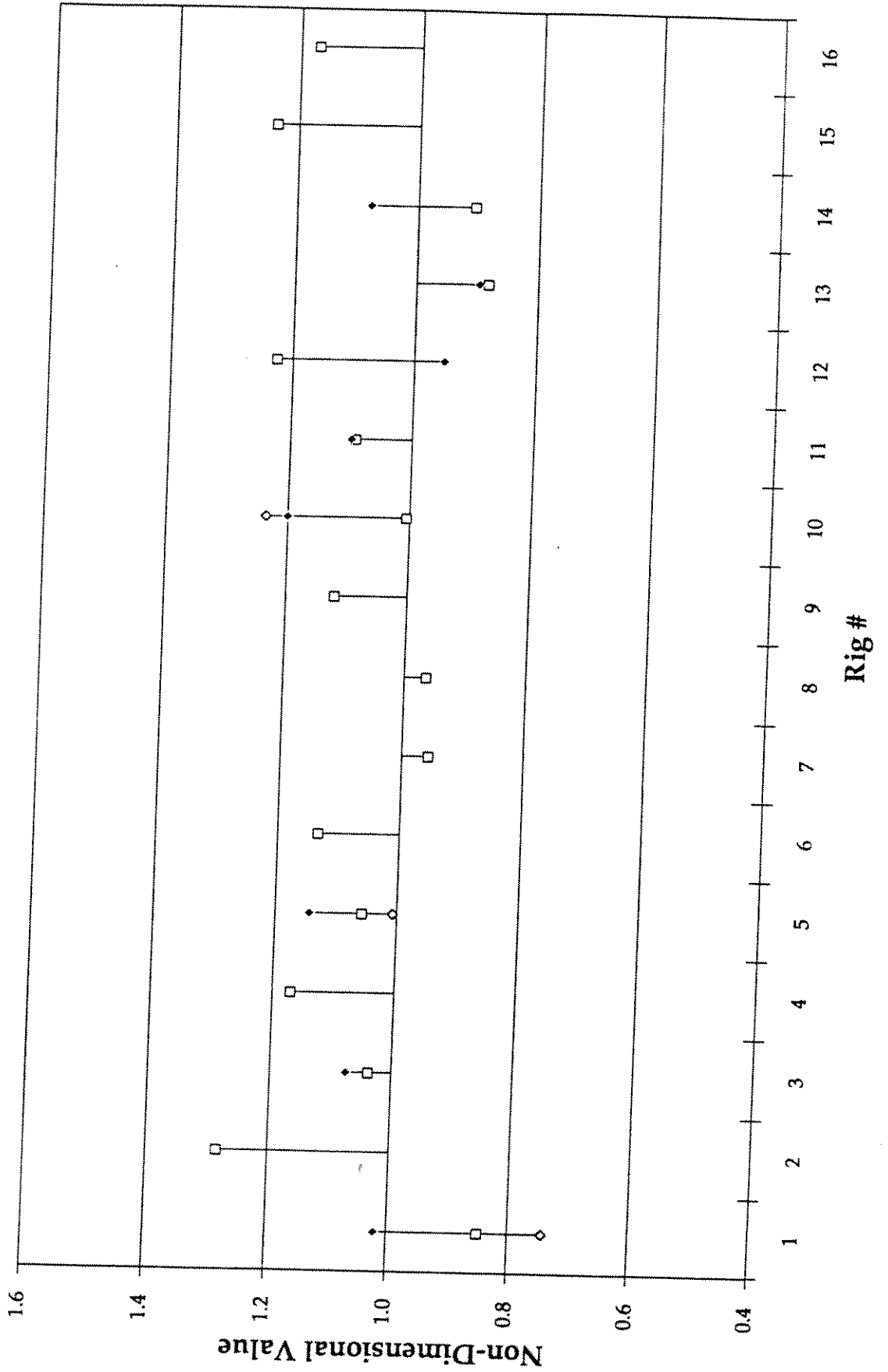
3. MAIN FINDINGS ON SEMISUBMERSIBLES

- REASONABLE AGREEMENT FOR WIND COEFFICIENT
- SUBSTANTIAL BODY OF KNOWLEDGE
(DUE TO STABILITY CONCERNS)
- SIGNIFICANT VARIATION FOR CURRENT COEFFICIENT

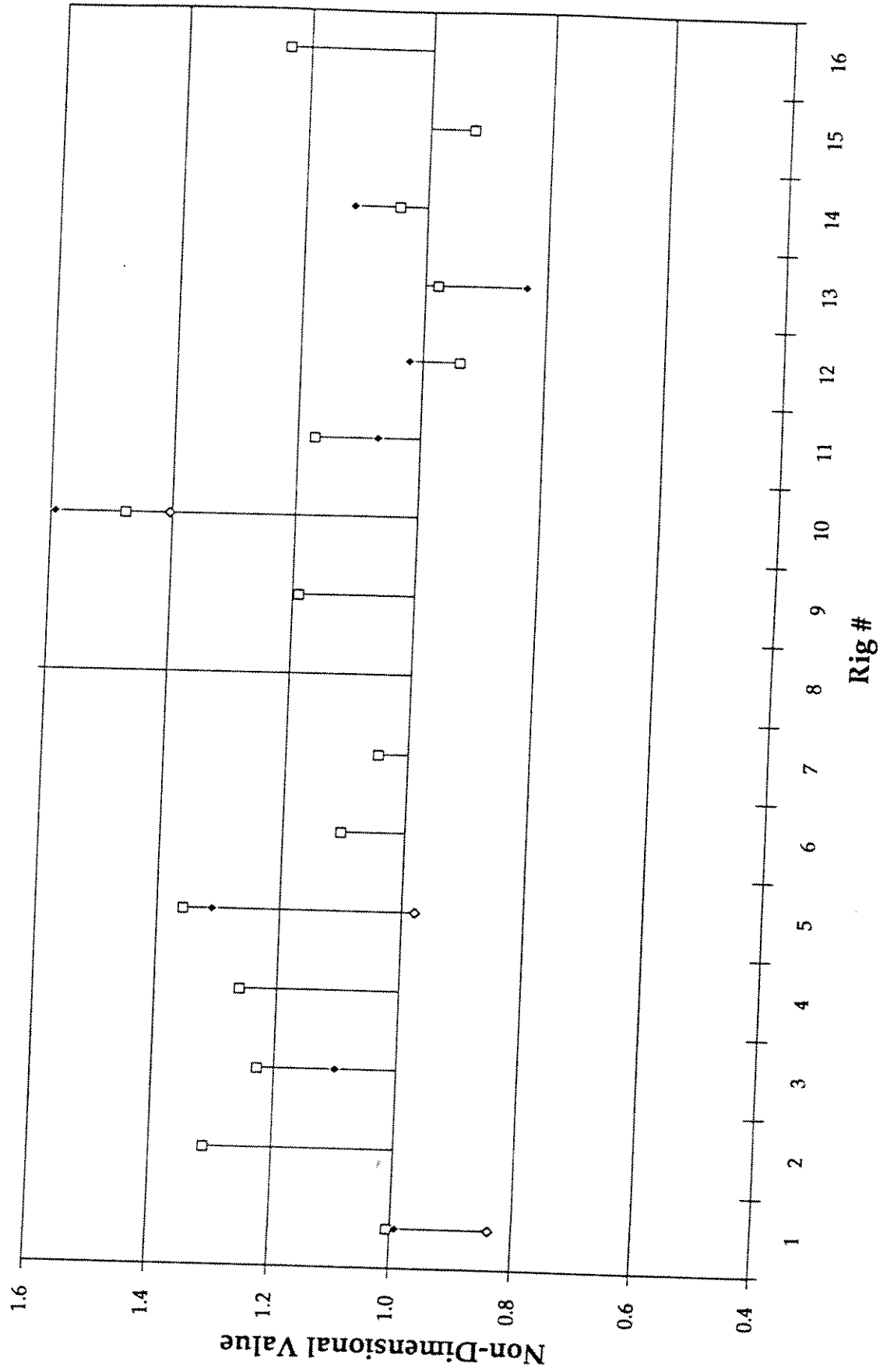
4. MAIN FINDINGS ON DRILL SHIPS

- SCANT INFORMATION
- SIGNIFICANT VARIATION FOR WIND COEFFICIENT
- WIDE SPREAD FOR CURRENT COEFFICIENT

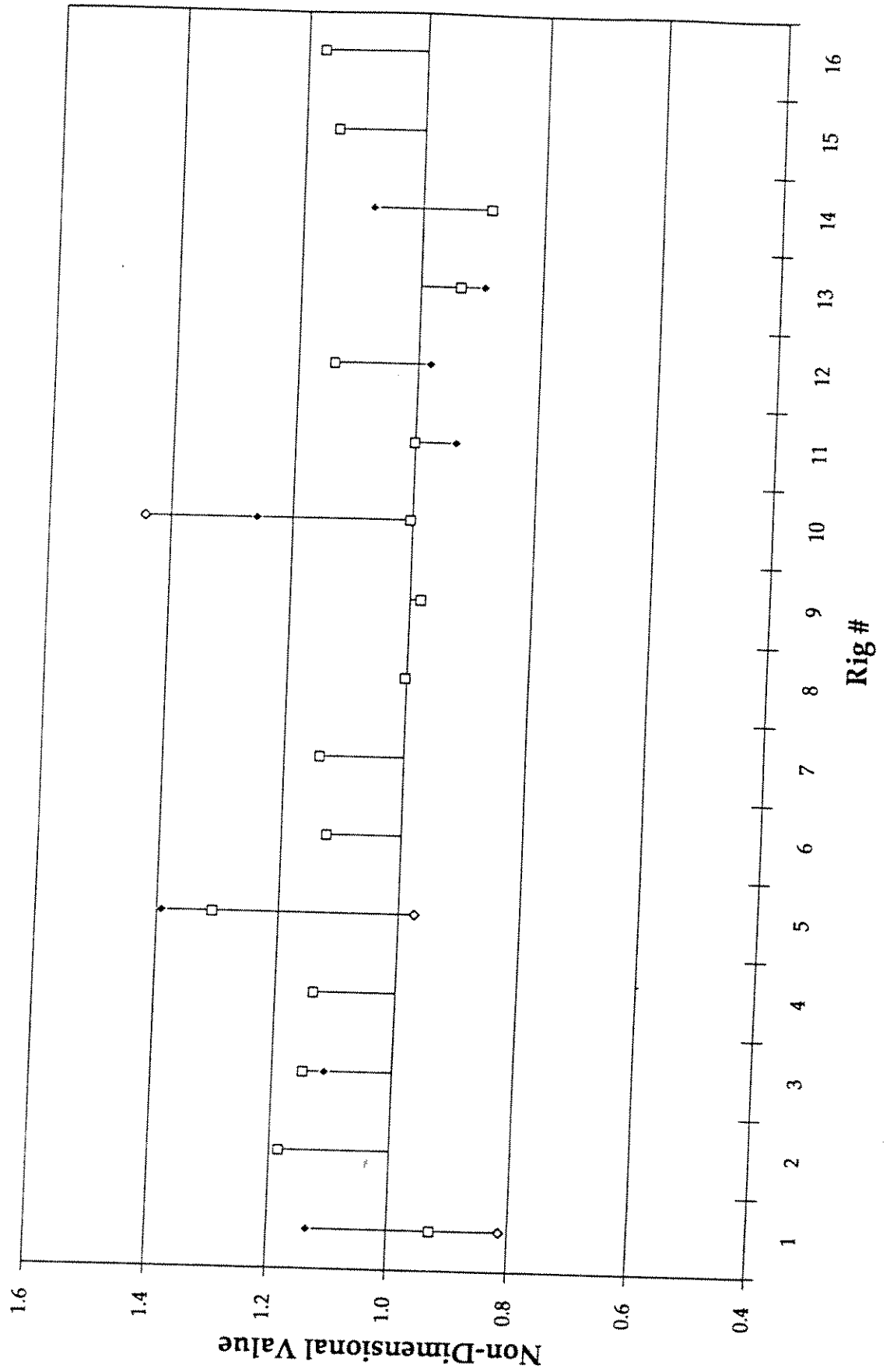
SEMI-SUBMERSIBLE - WIND COEFFICIENT - HEAD SEAS
VALUES NORMALIZED TO MODEL TEST DATA



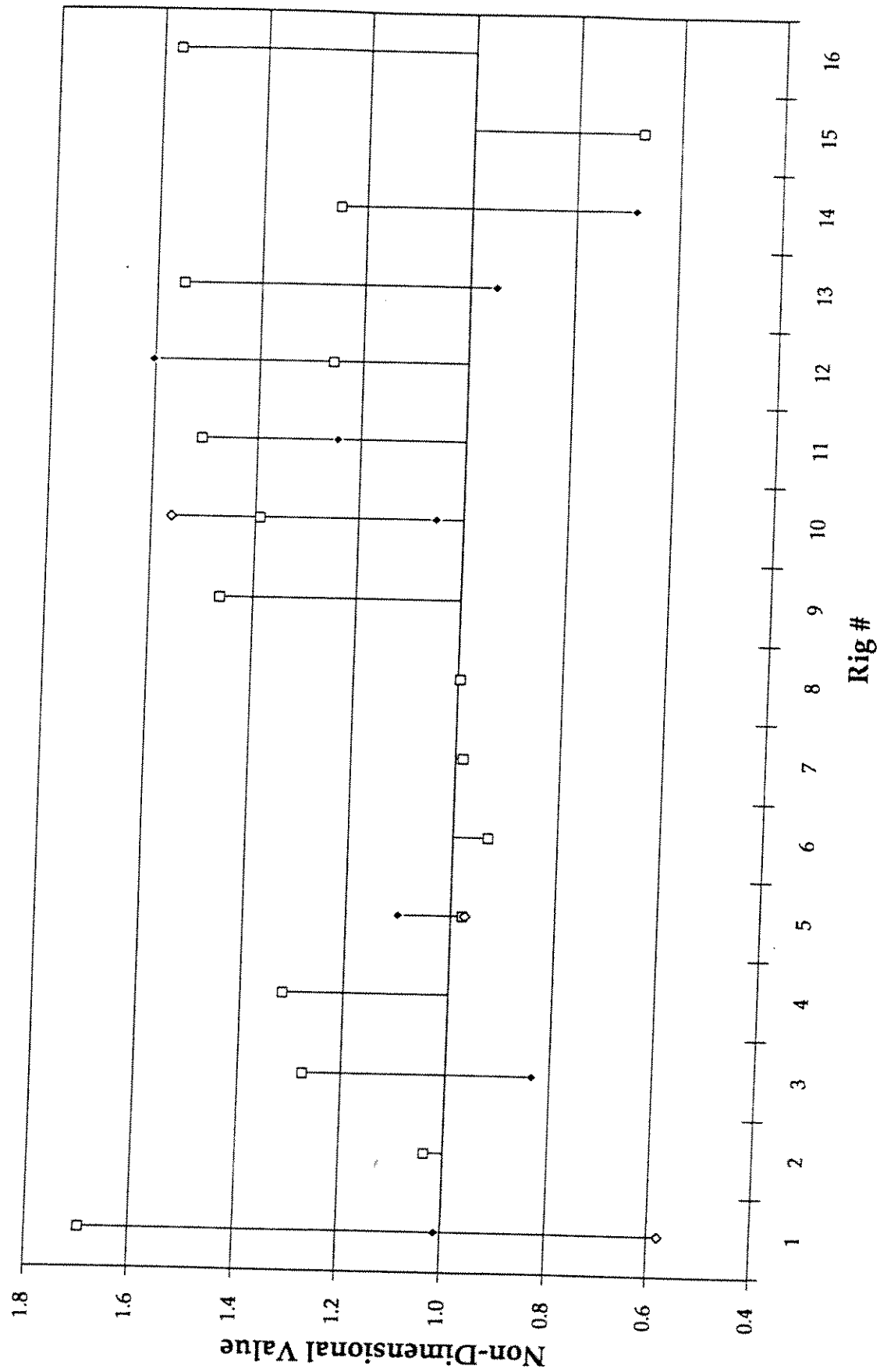
SEMI-SUBMERSIBLE - WIND COEFFICIENT - QUARTERING SEAS
VALUES NORMALIZED TO MODEL TEST DATA



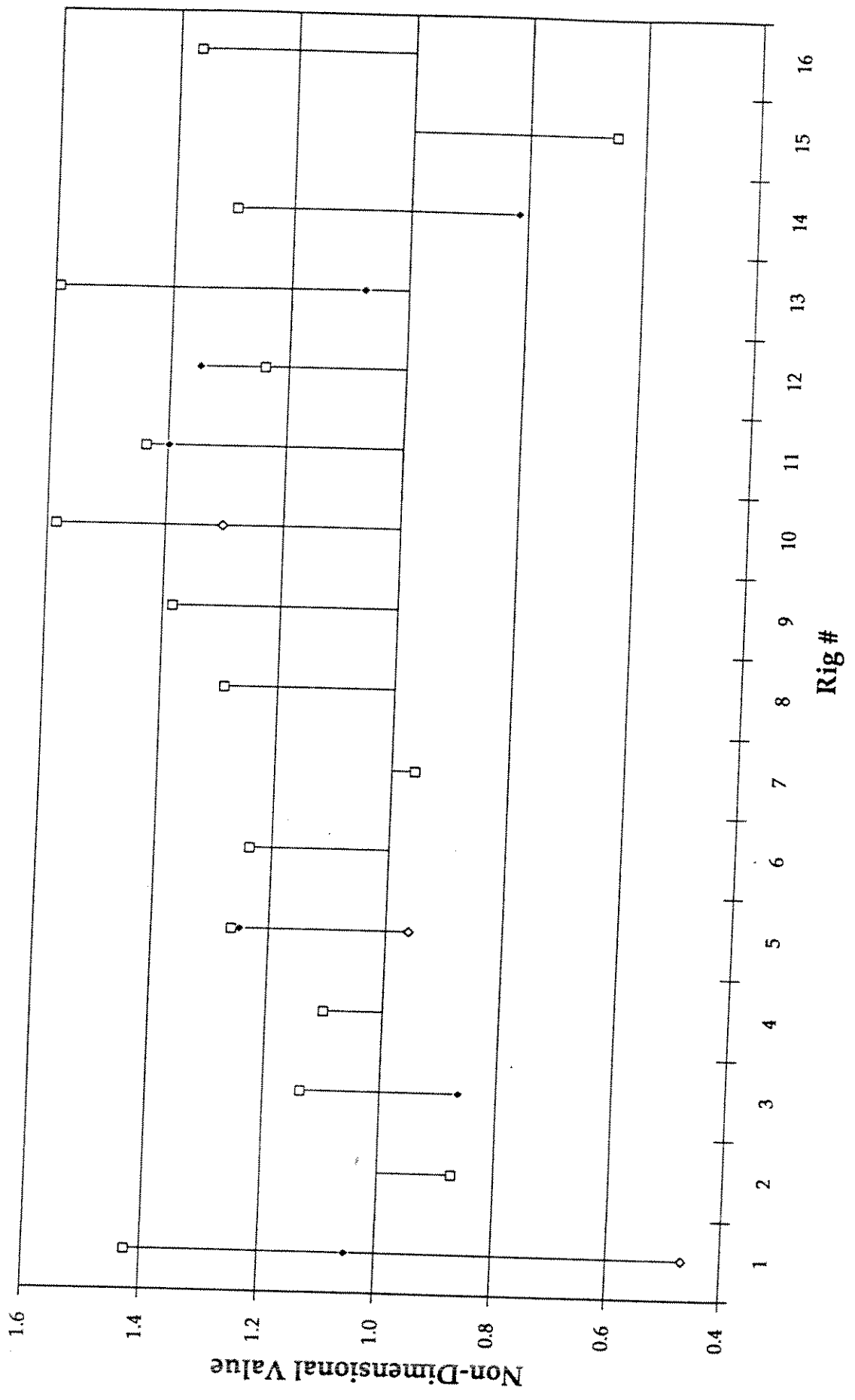
SEMI-SUBMERSIBLE - WIND COEFFICIENT - BEAM SEAS
VALUES NORMALIZED TO MODEL TEST DATA



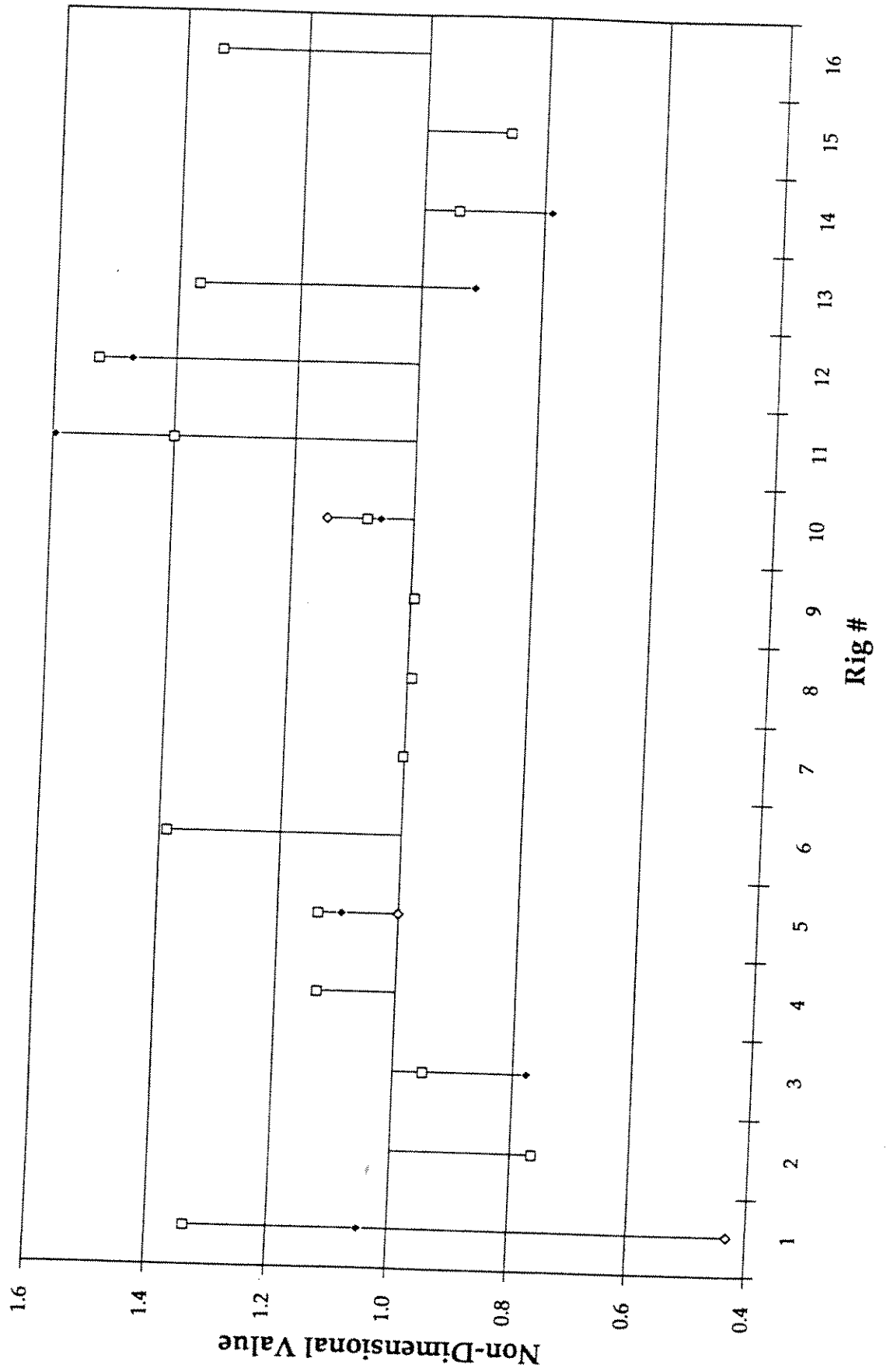
SEMI-SUBMERSIBLE - CURRENT COEFFICIENT - HEAD SEAS VALUES NORMALIZED TO MODEL TEST DATA



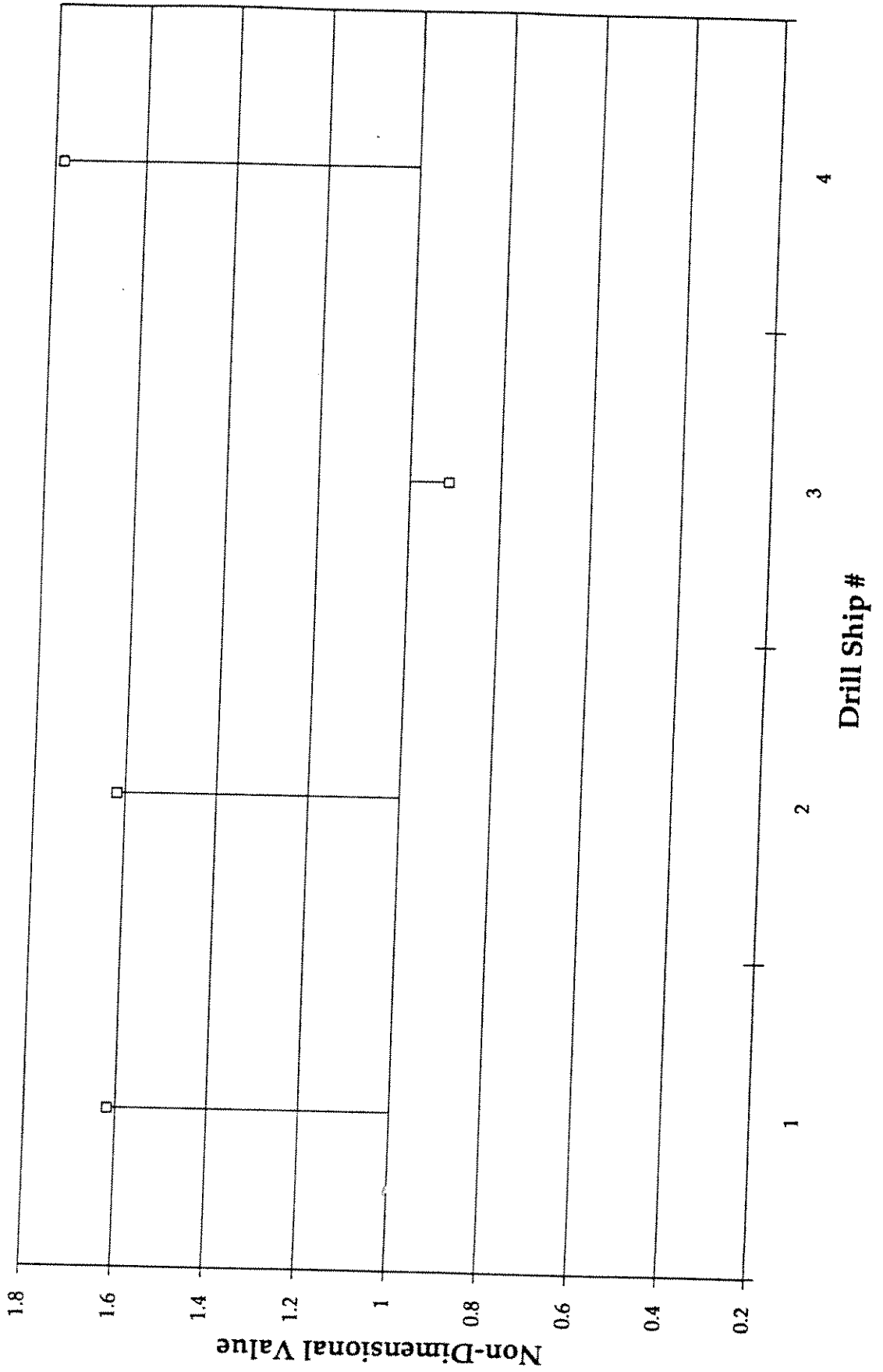
SEMI-SUBMERSIBLE - CURRENT COEFFICIENT - QUARTERING SEAS
VALUES NORMALIZED TO MODEL TEST DATA



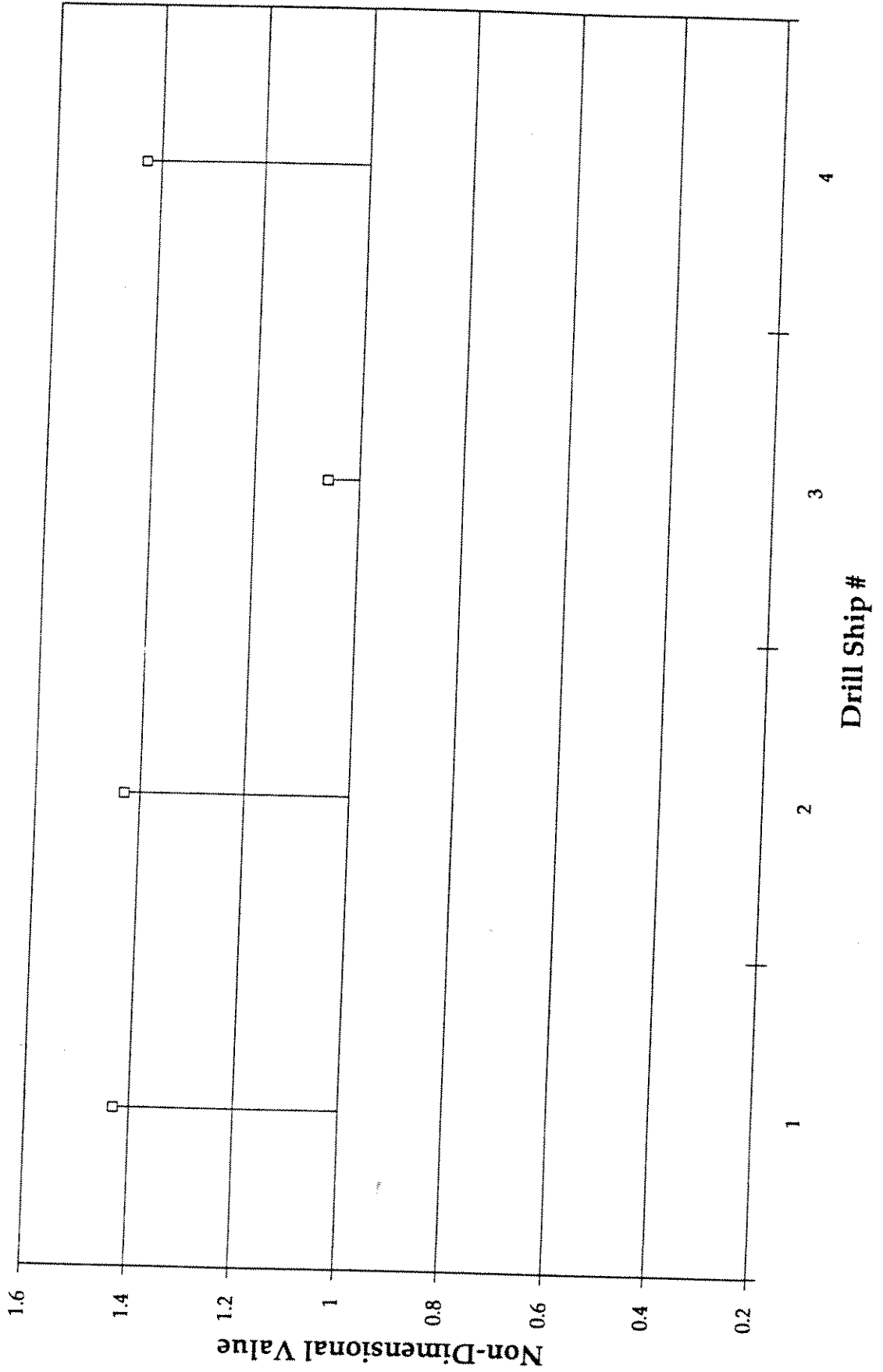
SEMI-SUBMERSIBLE - CURRENT COEFFICIENT - BEAM SEAS VALUES NORMALIZED TO MODEL TEST DATA



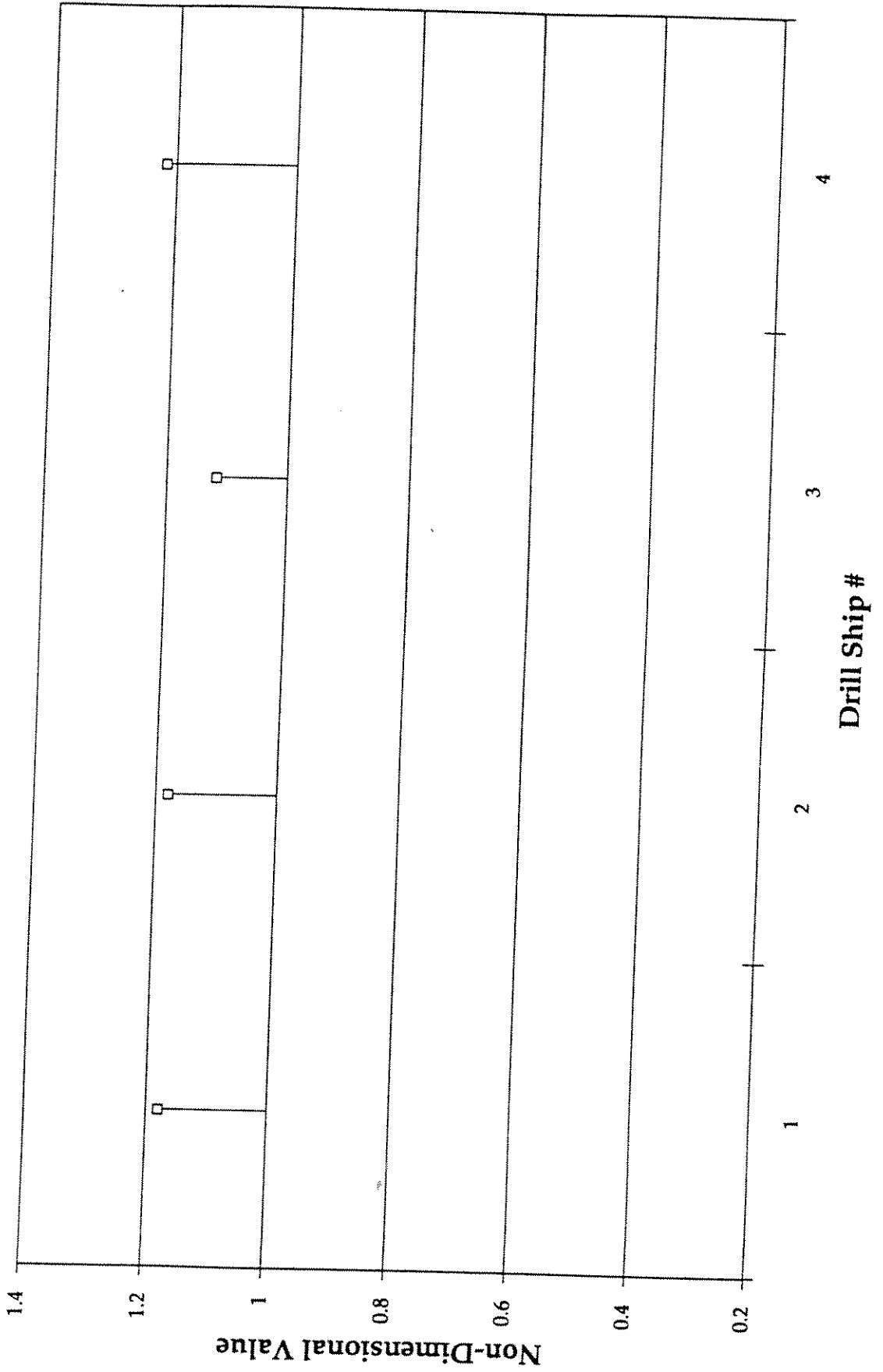
DRILL SHIP - WIND COEFFICIENT - HEAD SEAS
VALUES NORMALIZED TO MODEL TEST DATA



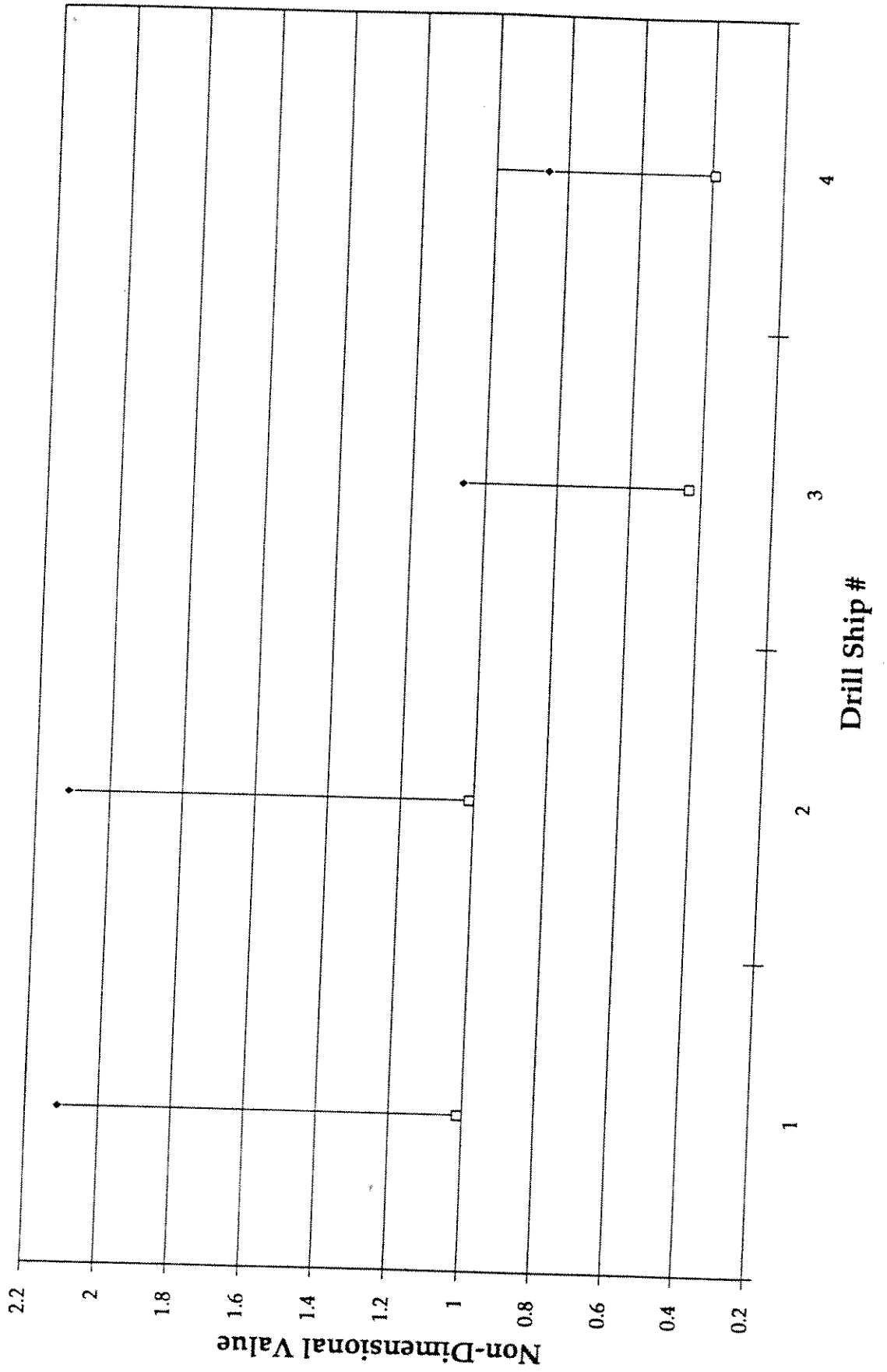
**DRILL SHIP - WIND COEFFICIENT - QUARTERING SEAS
VALUES NORMALIZED TO MODEL TEST DATA**



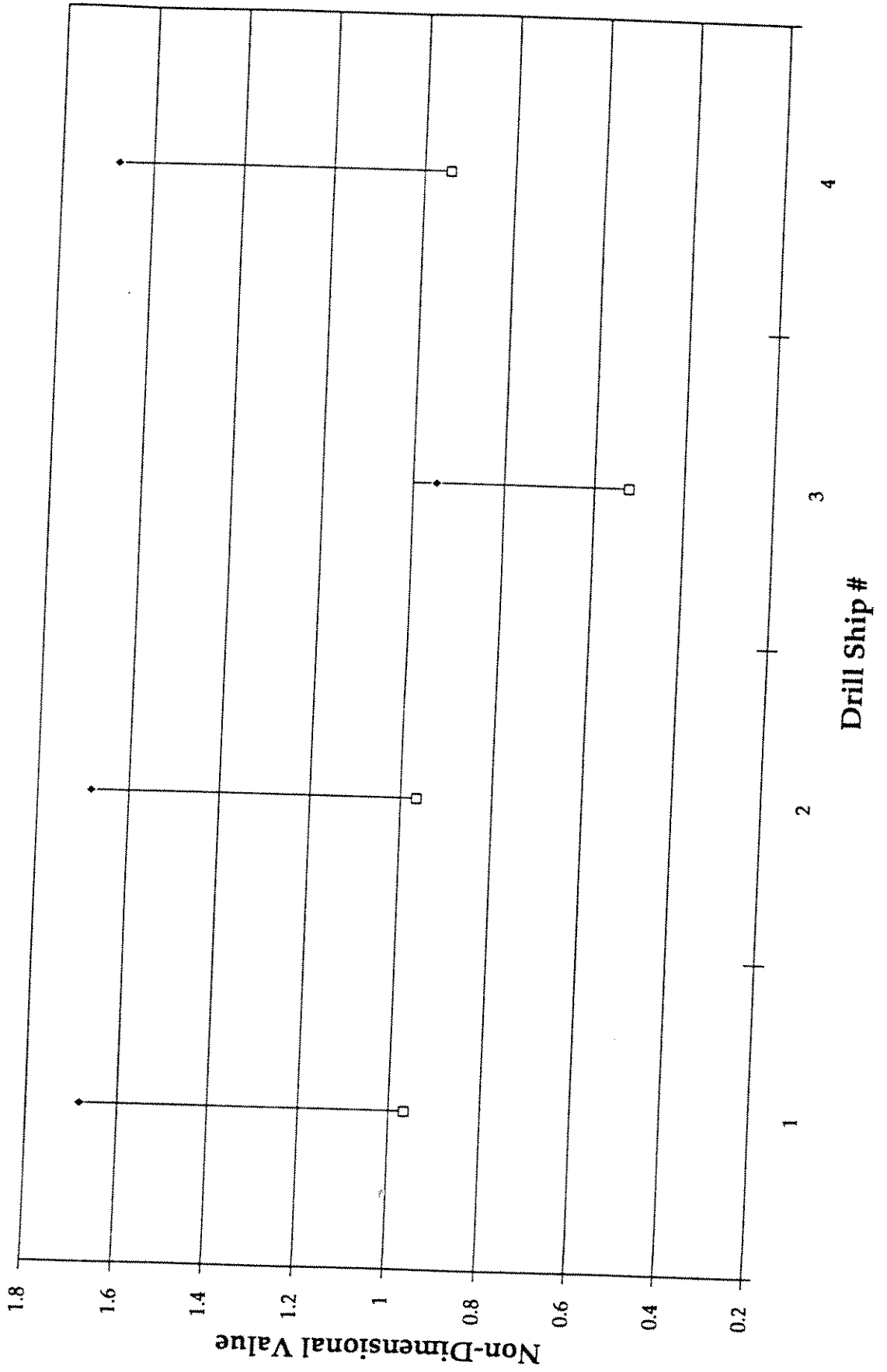
**DRILL SHIP - WIND COEFFICIENT - BEAM SEAS
VALUES NORMALIZED TO MODEL TEST DATA**



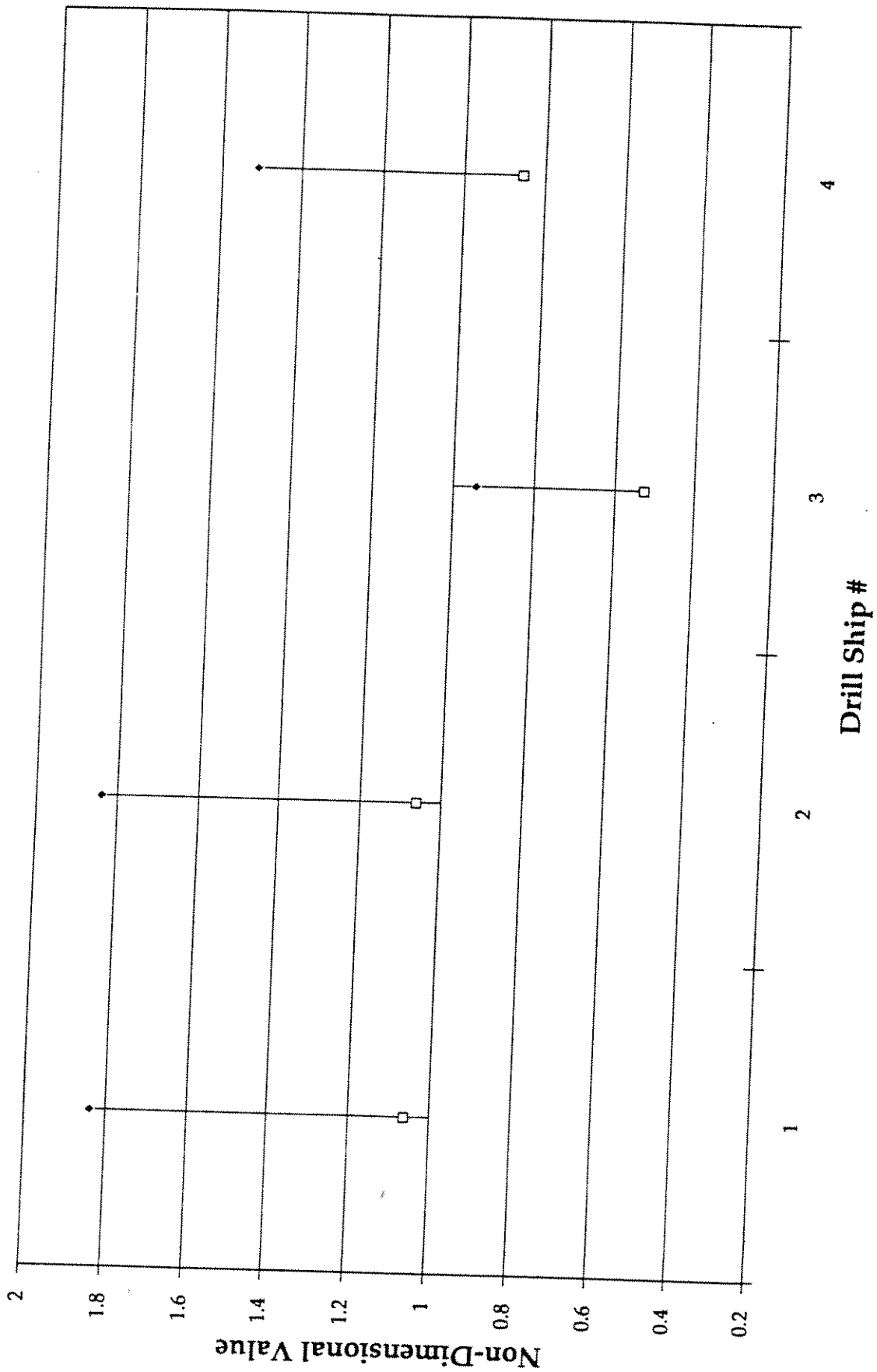
DRILL SHIP - CURRENT COEFFICIENT - HEAD SEAS
VALUES NORMALIZED TO MODEL TEST DATA



DRILL SHIP - CURRENT COEFFICIENT - QUARTERING SEAS
VALUES NORMALIZED TO MODEL TEST DATA



DRILL SHIP - CURRENT COEFFICIENT - BEAM SEAS
VALUES NORMALIZED TO MODEL TEST DATA



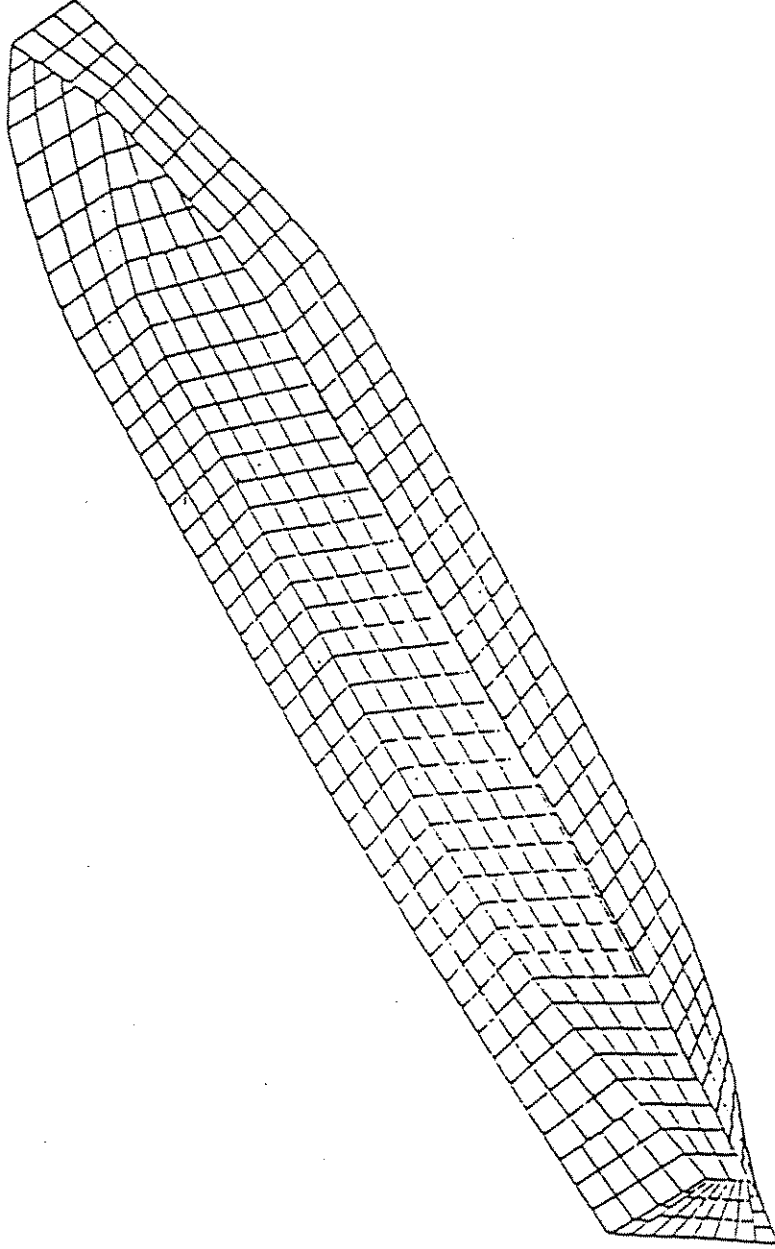
WAVE-DRIFT FORCE AND WF/LF MOTIONS

1. DATA SOURCE : FPS 2000 PROJECT

- A TURRET-MOORED TANKER
- RESULTS FROM SEVEN ORGANIZATIONS

2. SCOPE OF COMPARISON

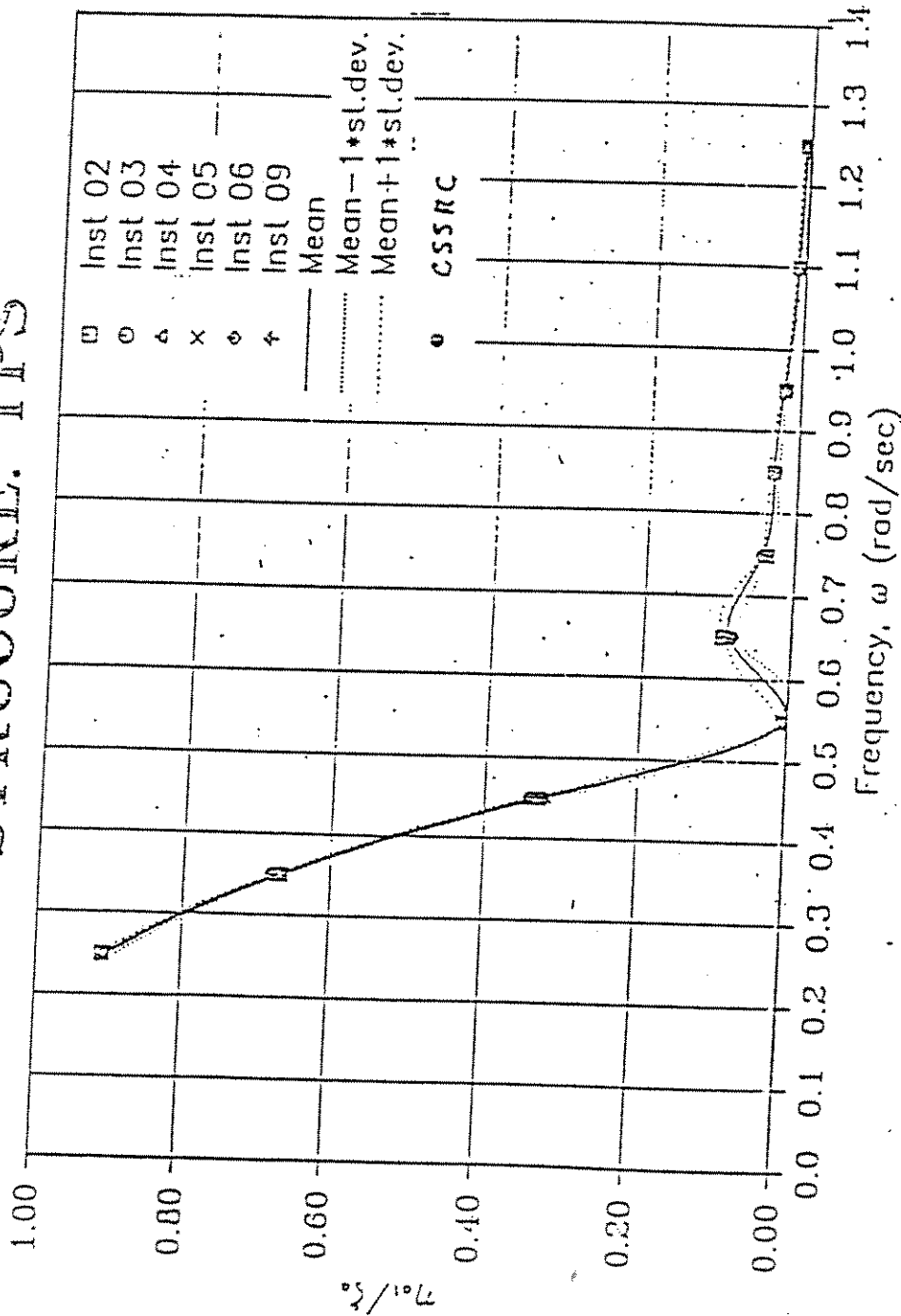
<u>WAVE-FREQUENCY</u>	<u>RELATIVE CONSISTENCY</u>
<ul style="list-style-type: none">• SURGE FORCE	GOOD
<ul style="list-style-type: none">• SURGE MOTION	EXCELLENT
<u>LOW-FREQUENCY</u>	
<ul style="list-style-type: none">• DRIFT-FORCE COEFF.	SIGNIFICANT VARIATION
<ul style="list-style-type: none">• LF MOTION	WIDE SPREAD



3-D HYDRODYNAMIC MODEL

Source: FPS 2000 Project
Turret Moored Production System (TPS)

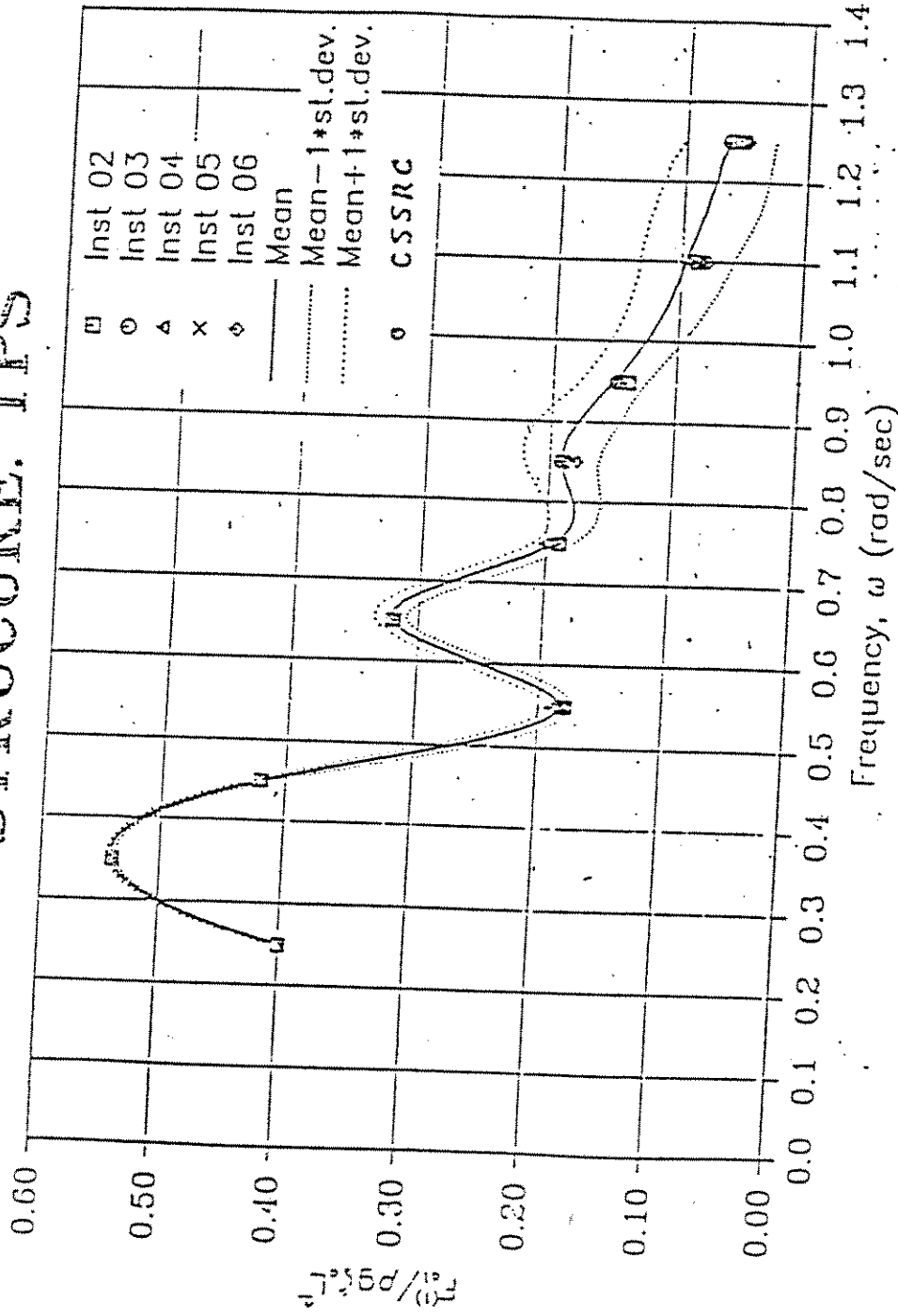
STRUCTURE: TPS



COMPARISON OF WAVE FREQUENCY SURGE RAO

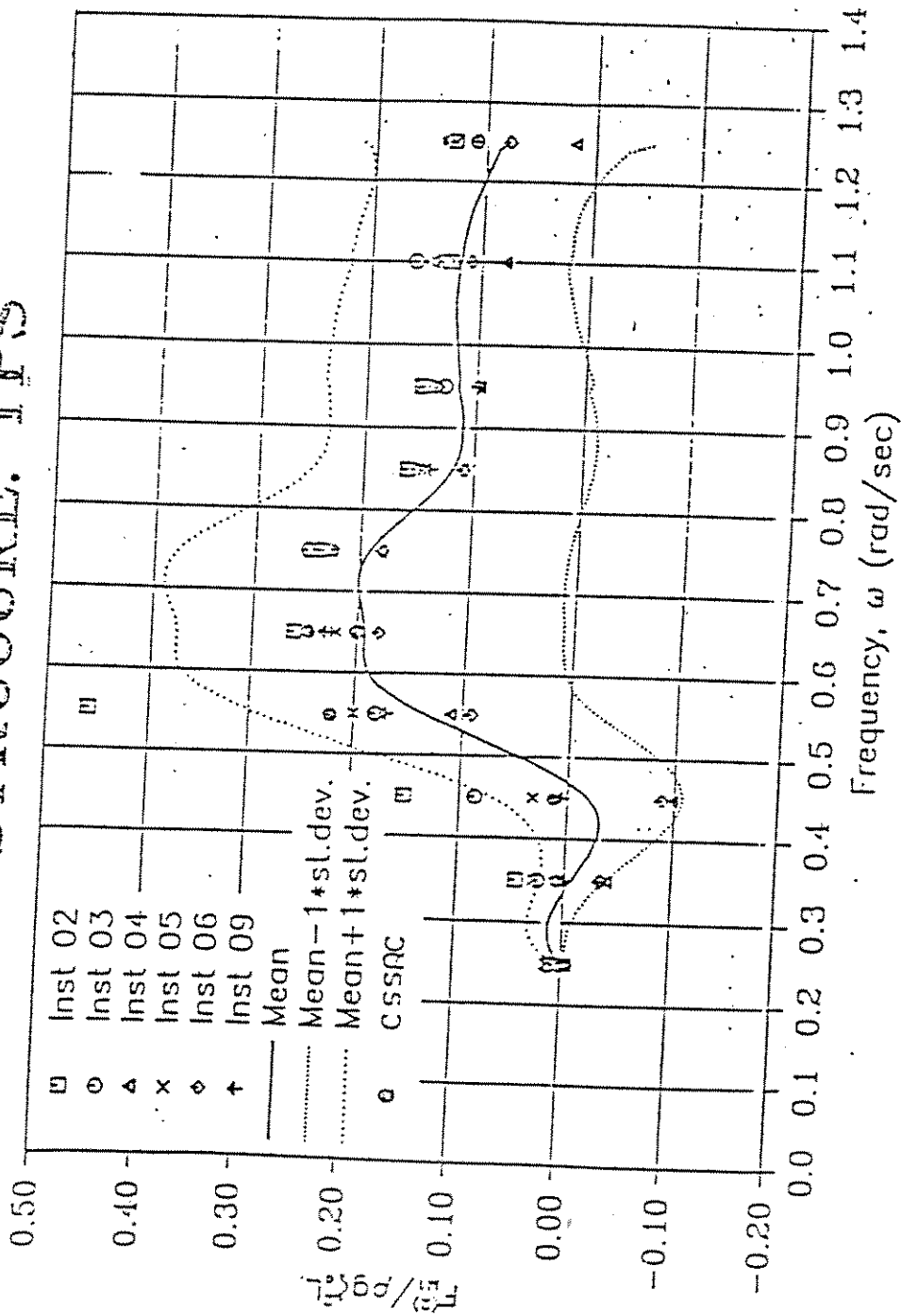
Source: FPS 2000 Project
Turret Moored Production System (TPS)

STRUCTURE: TPS

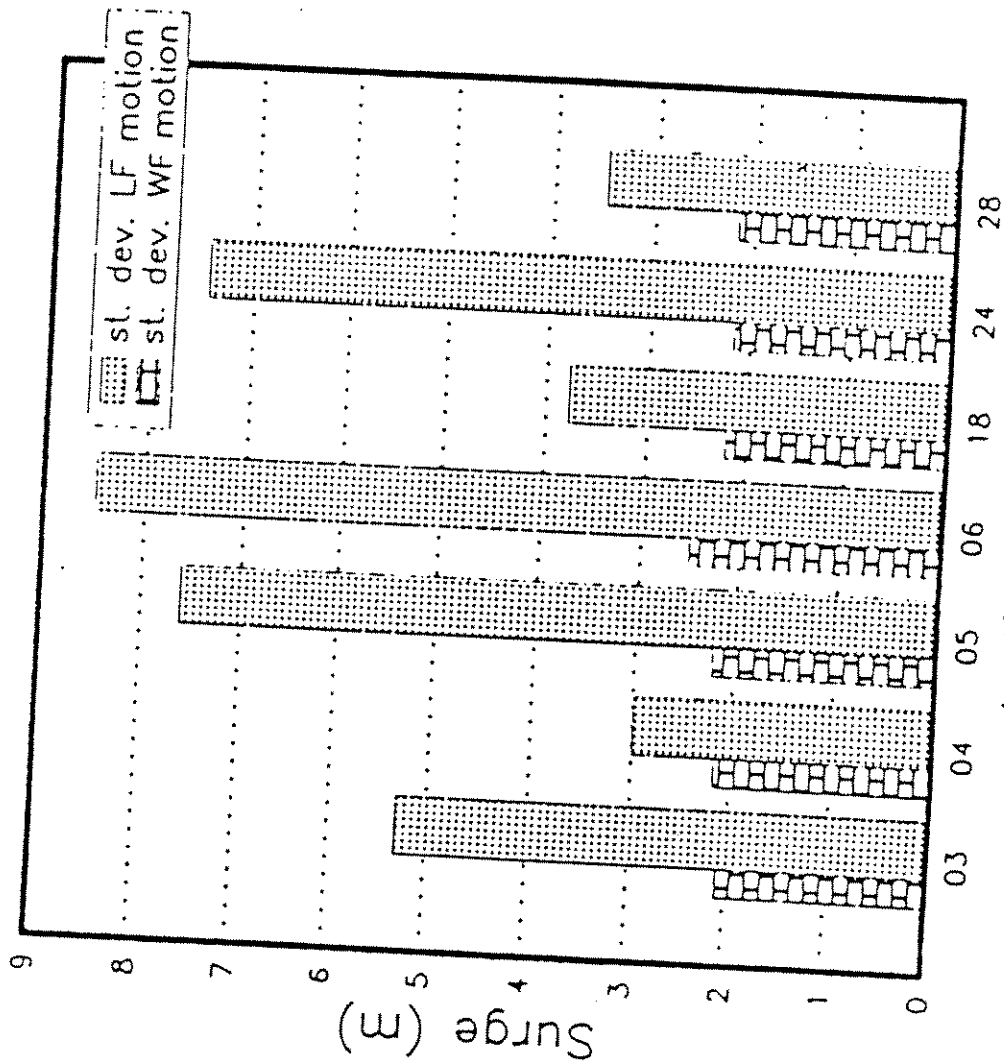


COMPARISON OF WAVE FREQUENCY SURGE FORCE

STRUCTURE: TPS



COMPARISON OF WAVE DRIFT FORCE COEFFICIENTS



Institution No:

TPS. Motion response in design condition ($H_s = 15.5$ m). Standard deviations of first order (WF) and low frequency (LF) motion response in surge. 10 degrees heading to the waves

VESSEL LF DAMPING
GVA 5000 4-COLUMN SEMISUBMERSIBLE

1. COMPUTATIONAL METHOD

- MIT/DnV JIS FOR TLP
- LIMITATIONS
 - 4-COLUMNS
 - PONTOONS IGNORED
- PRINCIPAL INVESTIGATOR: PAUL SCLAVONOUS

2. STUDY MATRIX

- SIGNIFICANT WAVE HEIGHTS (P-M): 30', 40', AND 50'
- WAVE HEADINGS: 0°, 22.5°, AND 45°
- SYSTEM STIFFNESS (KIPS/FT): 5, 10, AND 20
- WAVE-DAMPING AND VISCOUS-DAMPING

3. A DESIGN CASE : GOMEX 10-YEAR STORM
(ASSUMING K = 10 KIPS/FT)

	<u>DAMPING (% OF SYSTEM CRITICAL)</u>	
	<u>HEAD SEA</u>	<u>BEAM SEA</u>
WAVE DAMPING	2.8%	2.8%
<u>VISCOUS DAMPING</u>	<u>1.7%</u>	<u>4.5%</u>
TOTAL	4.5%	7.3%

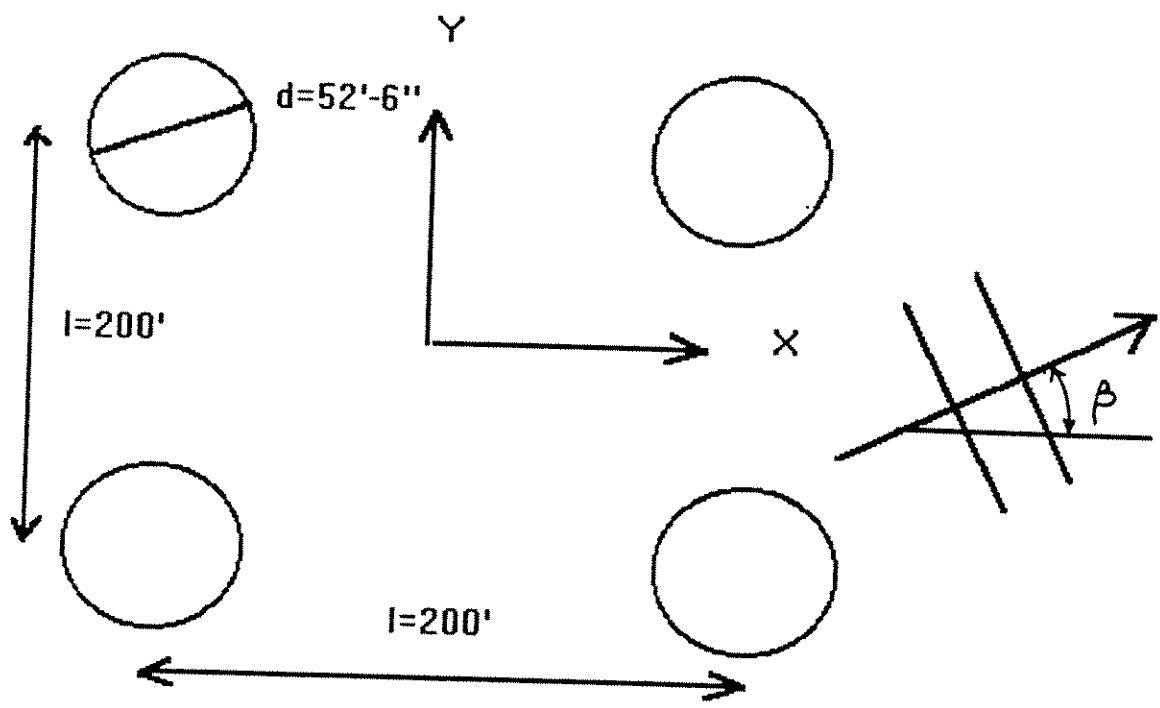
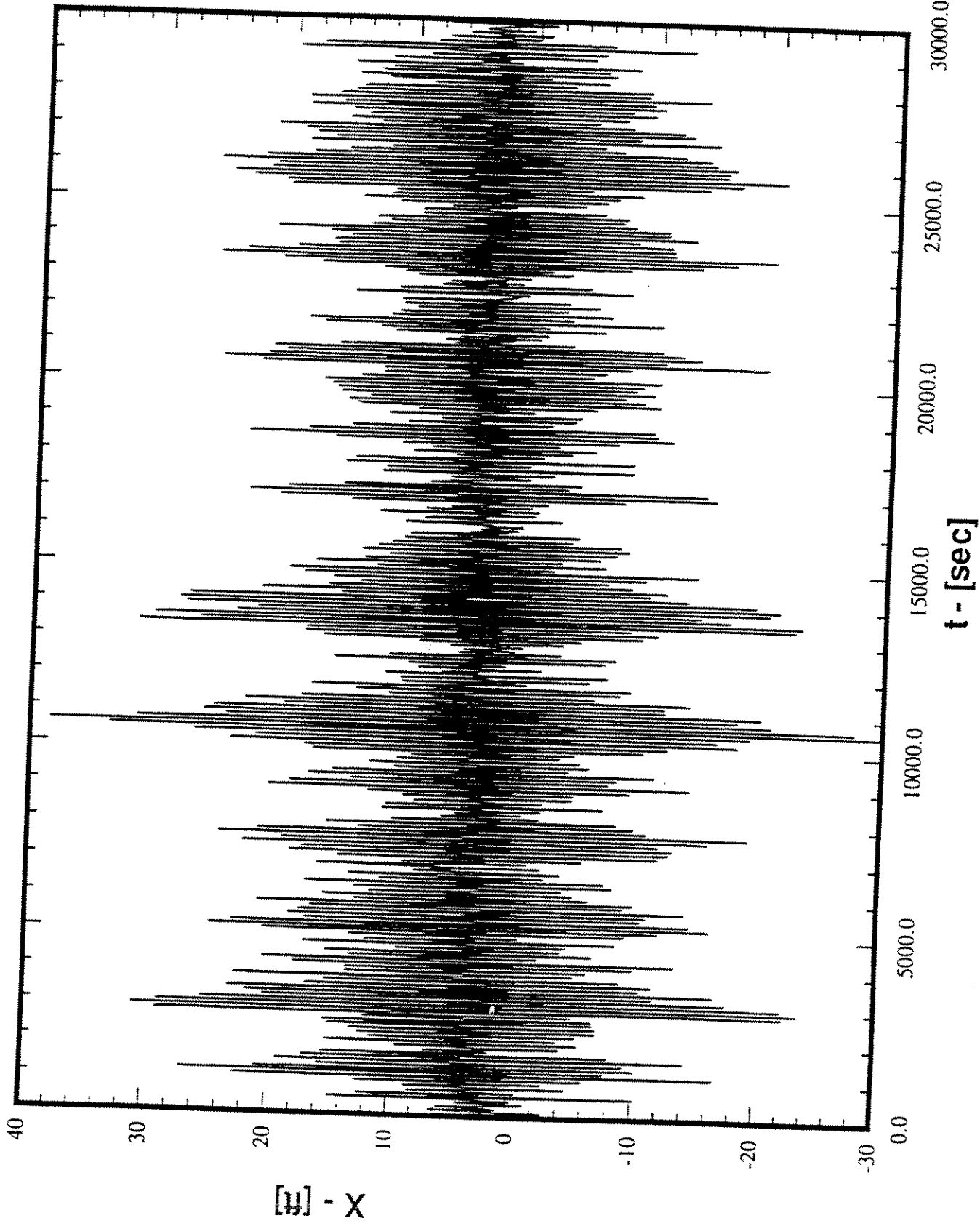


FIG. 1

Slow Drift Motion - Surge



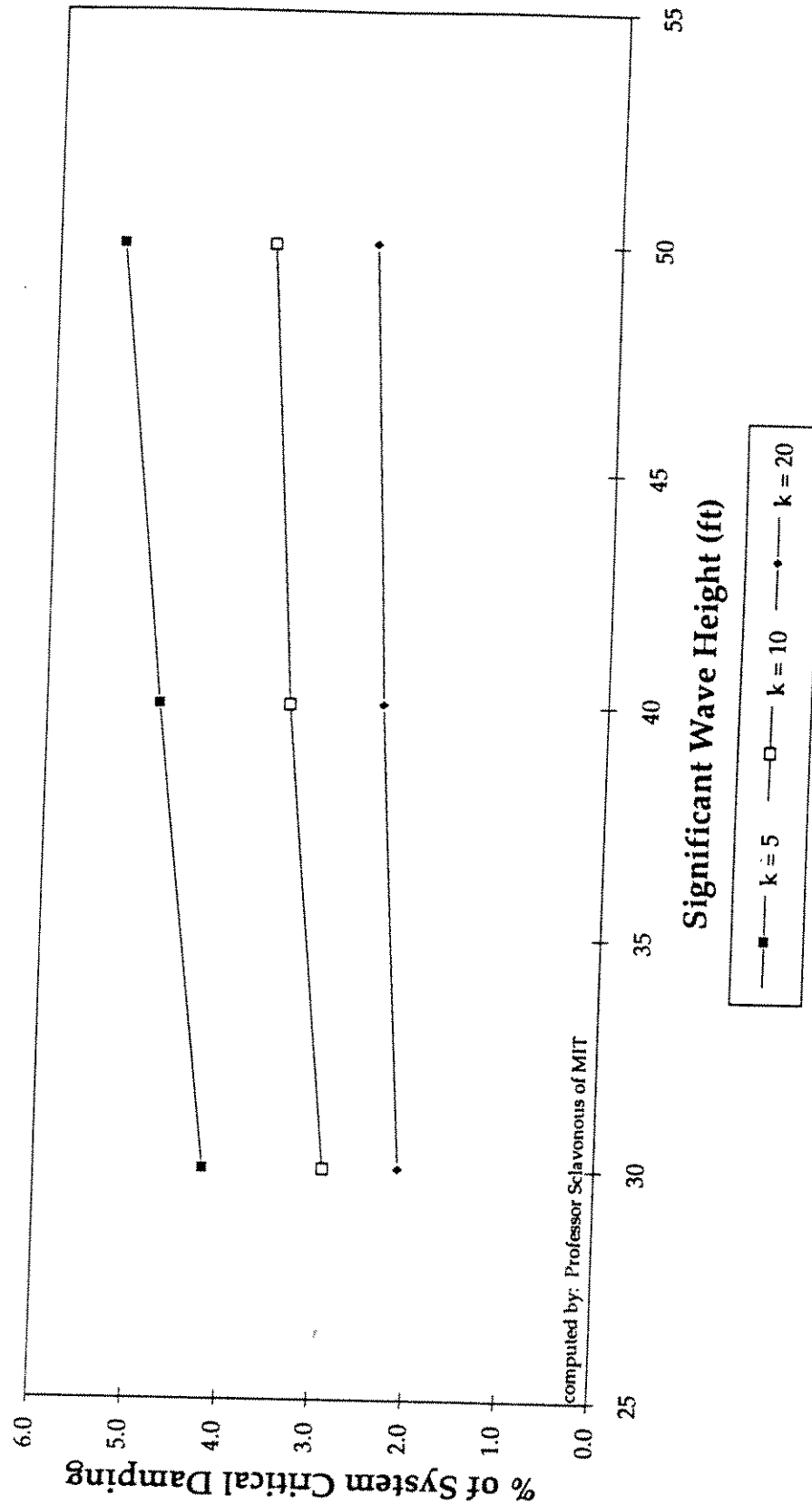
$H_s = 40$ [ft]

$\beta = 0$

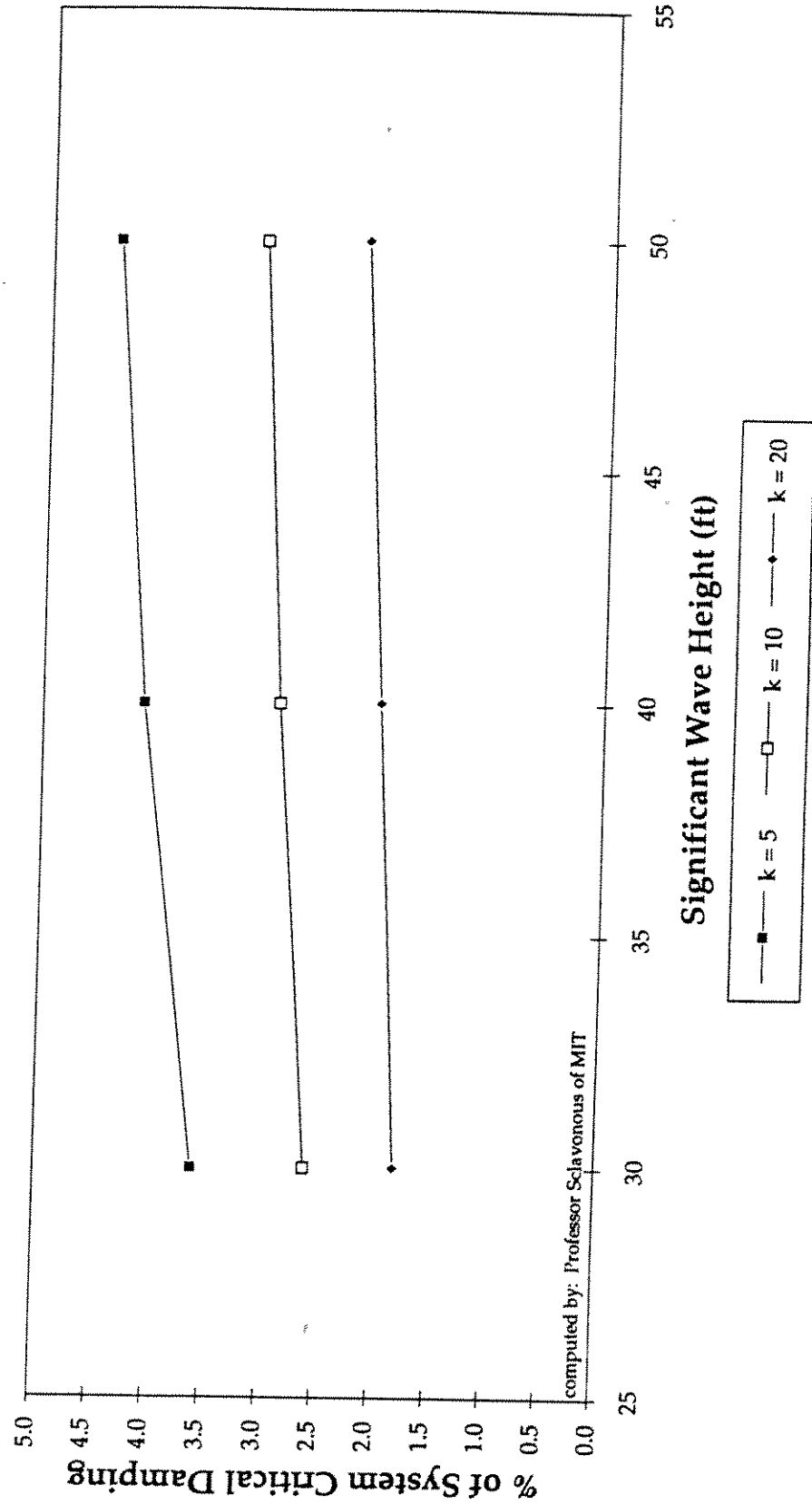
$C_D = 0$

$k_y = 10$ [kips/ft]

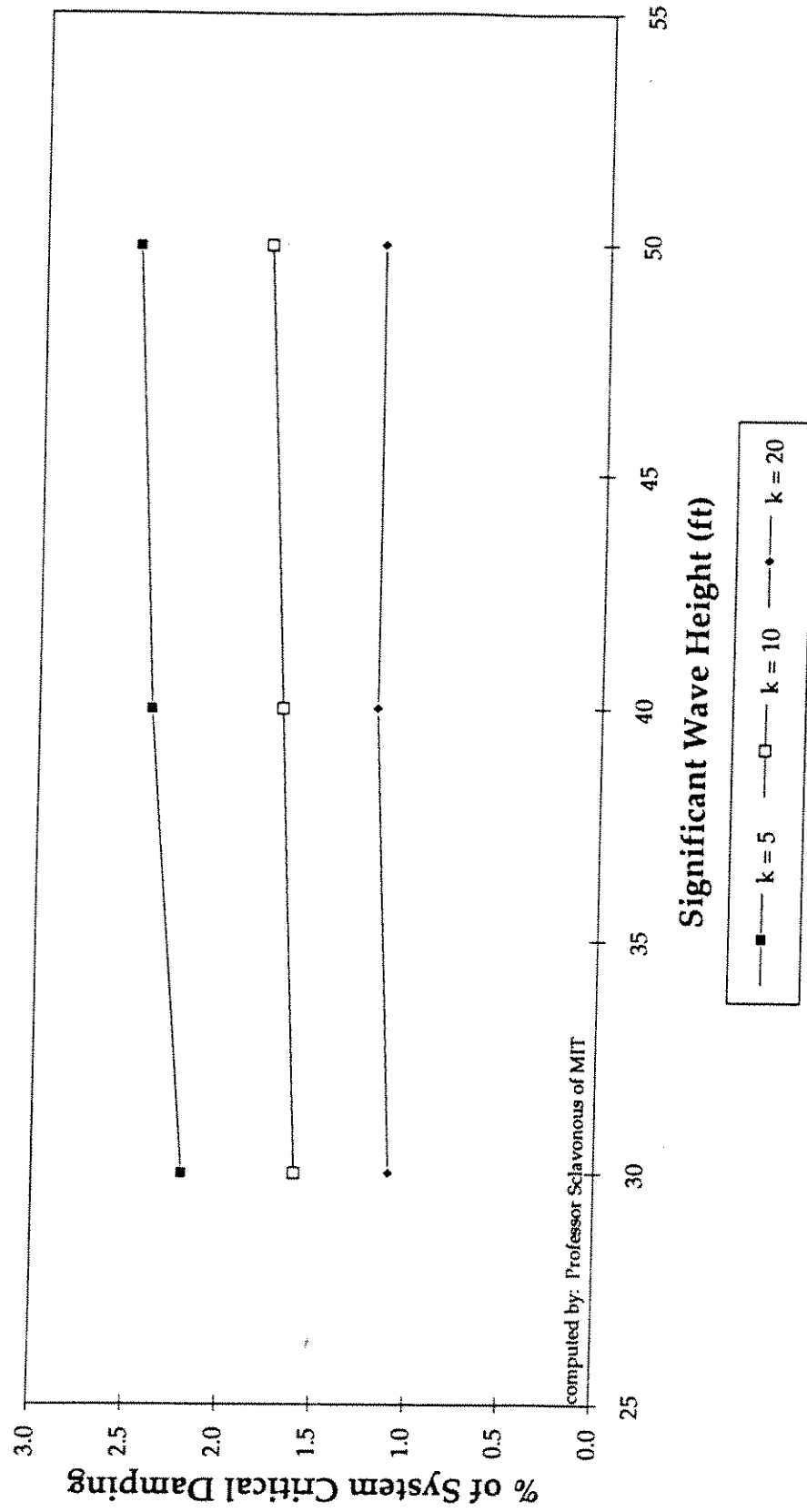
**SEMI-SUBMERSIBLE/FPS (GVA 5000 CLASS)
LF SURGE WAVE DRIFT DAMPING
HEADING ANGLE = 0.0 DEGREES**



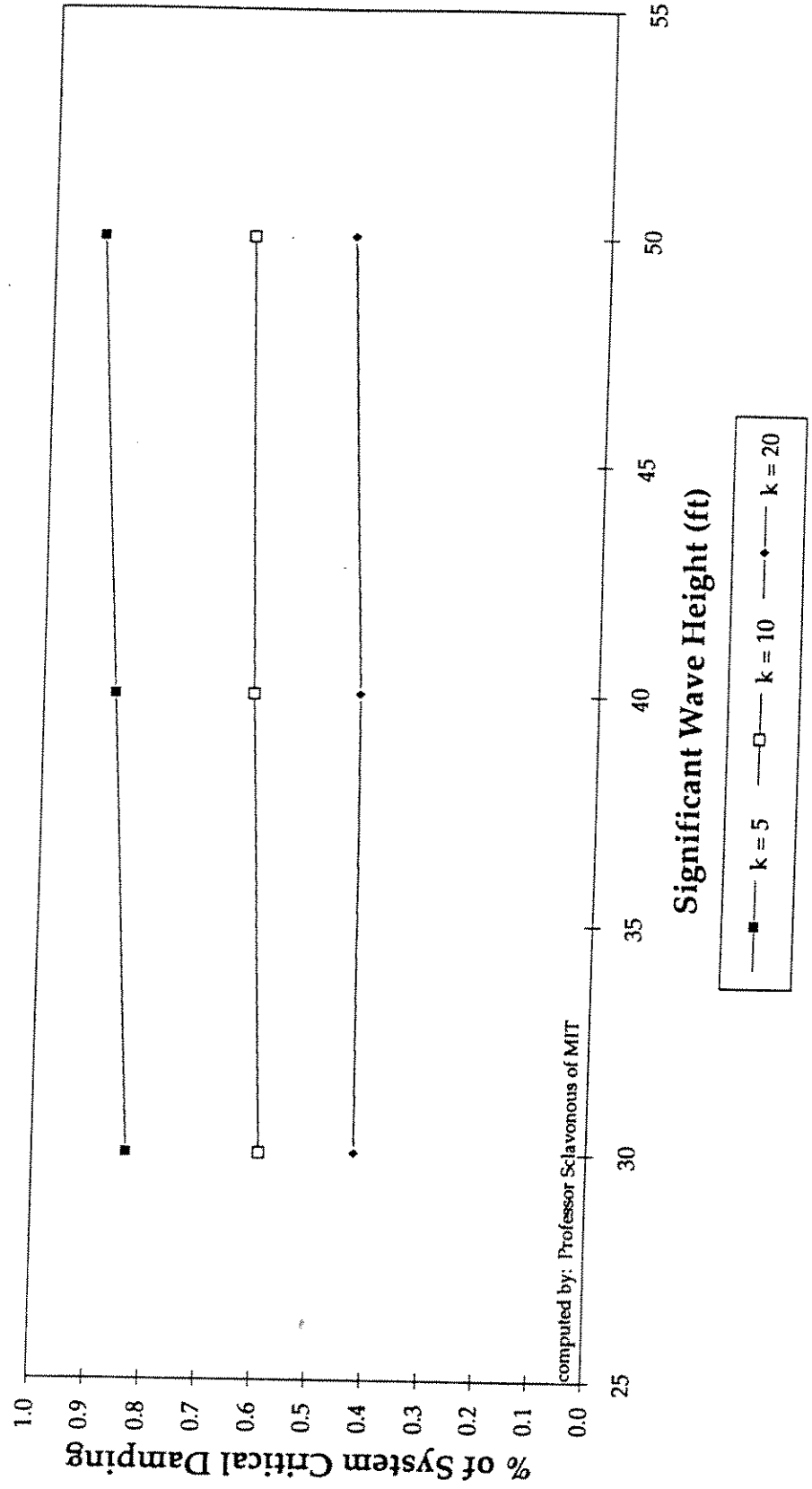
**SEMI-SUBMERSIBLE/FPS (GVA 5000 CLASS)
LF SURGE WAVE DRIFT DAMPING
HEADING ANGLE = 22.5 DEGREES**



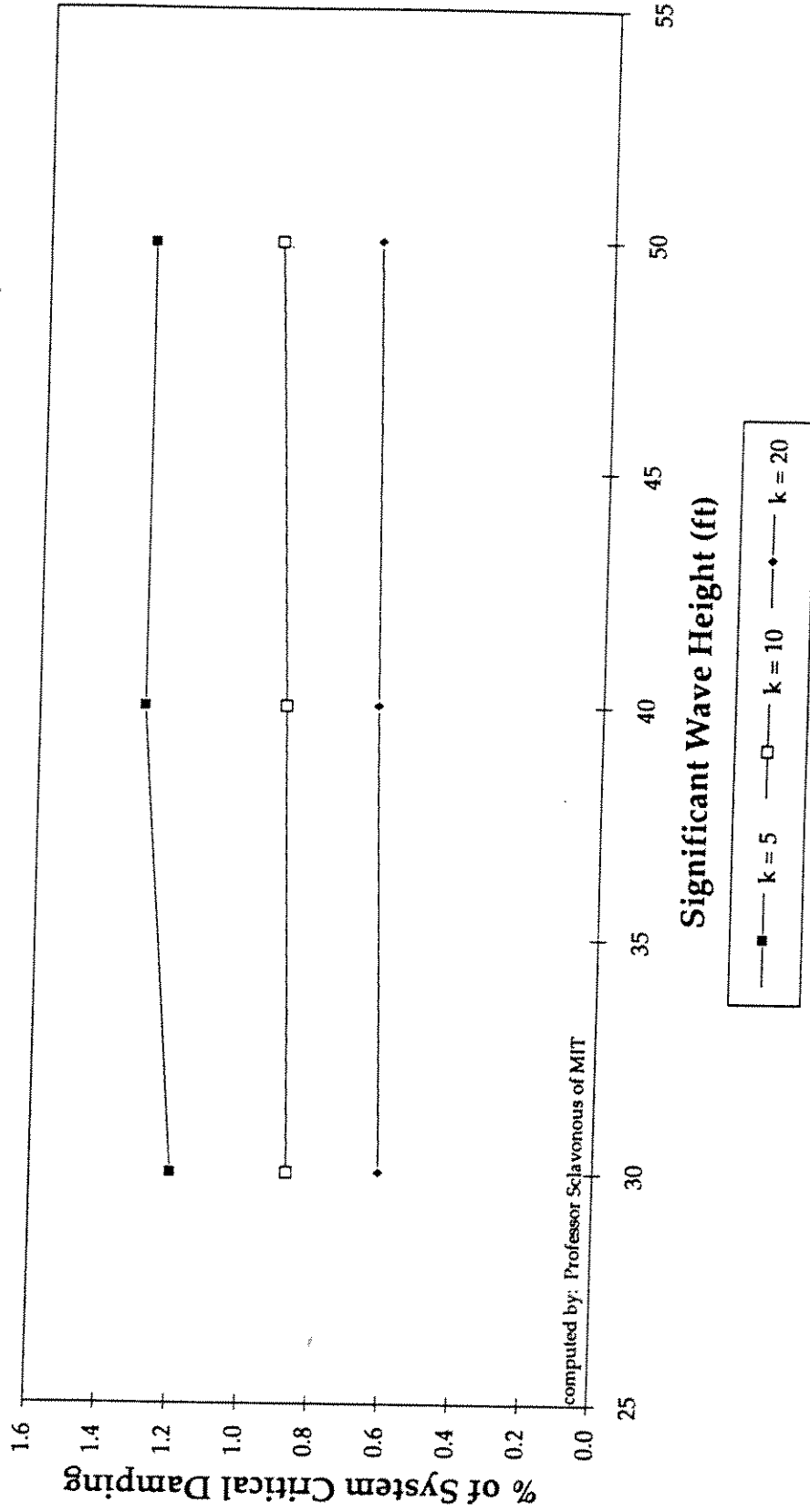
**SEMI-SUBMERSIBLE/FPS (GVA 5000 CLASS)
LF SURGE WAVE DRIFT DAMPING
HEADING ANGLE = 45.0 DEGREES**



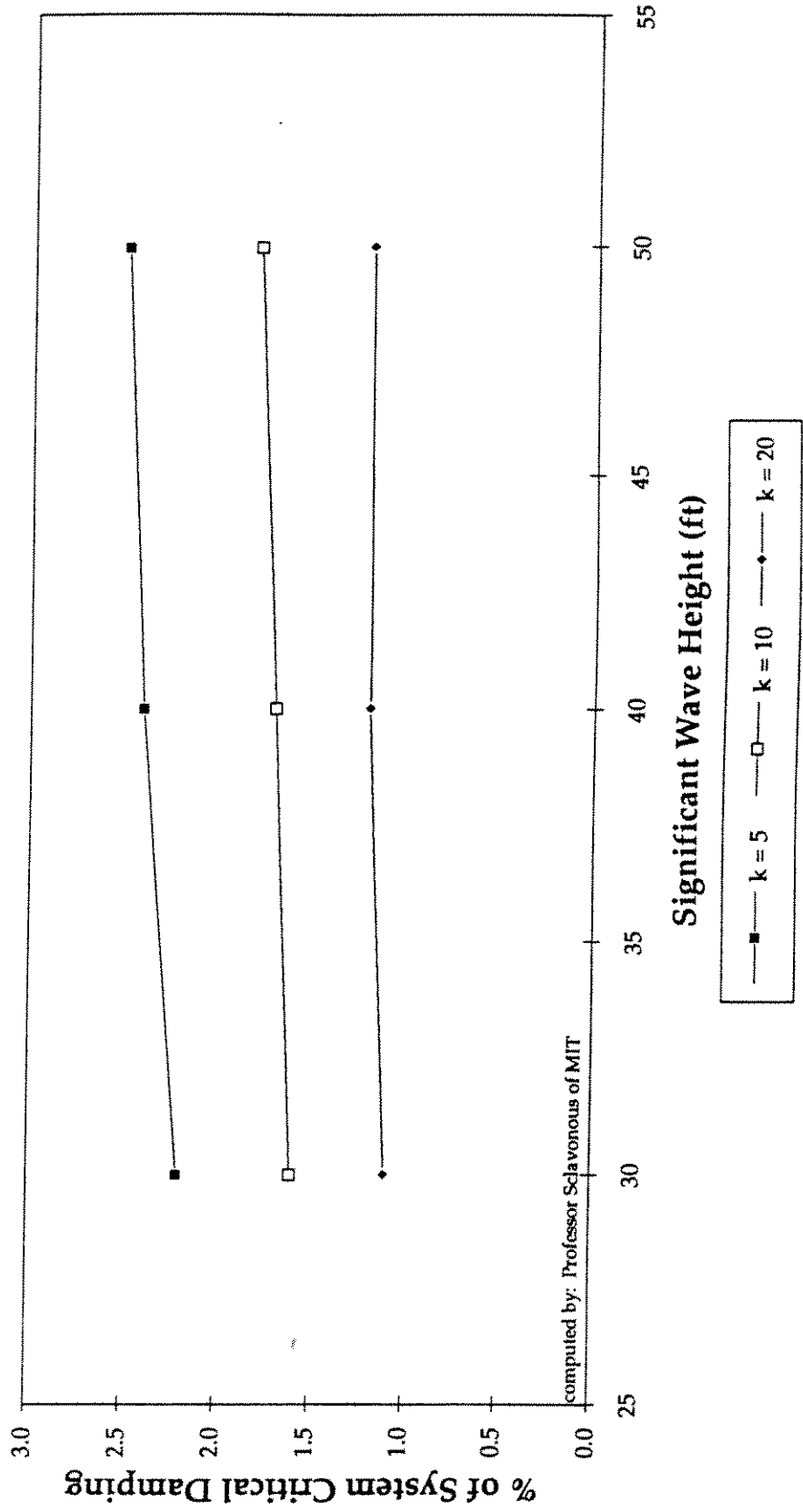
**SEMI-SUBMERSIBLE/FPS (GVA 5000 CLASS)
LF SWAY WAVE DRIFT DAMPING
HEADING ANGLE = 0.0 DEGREES**



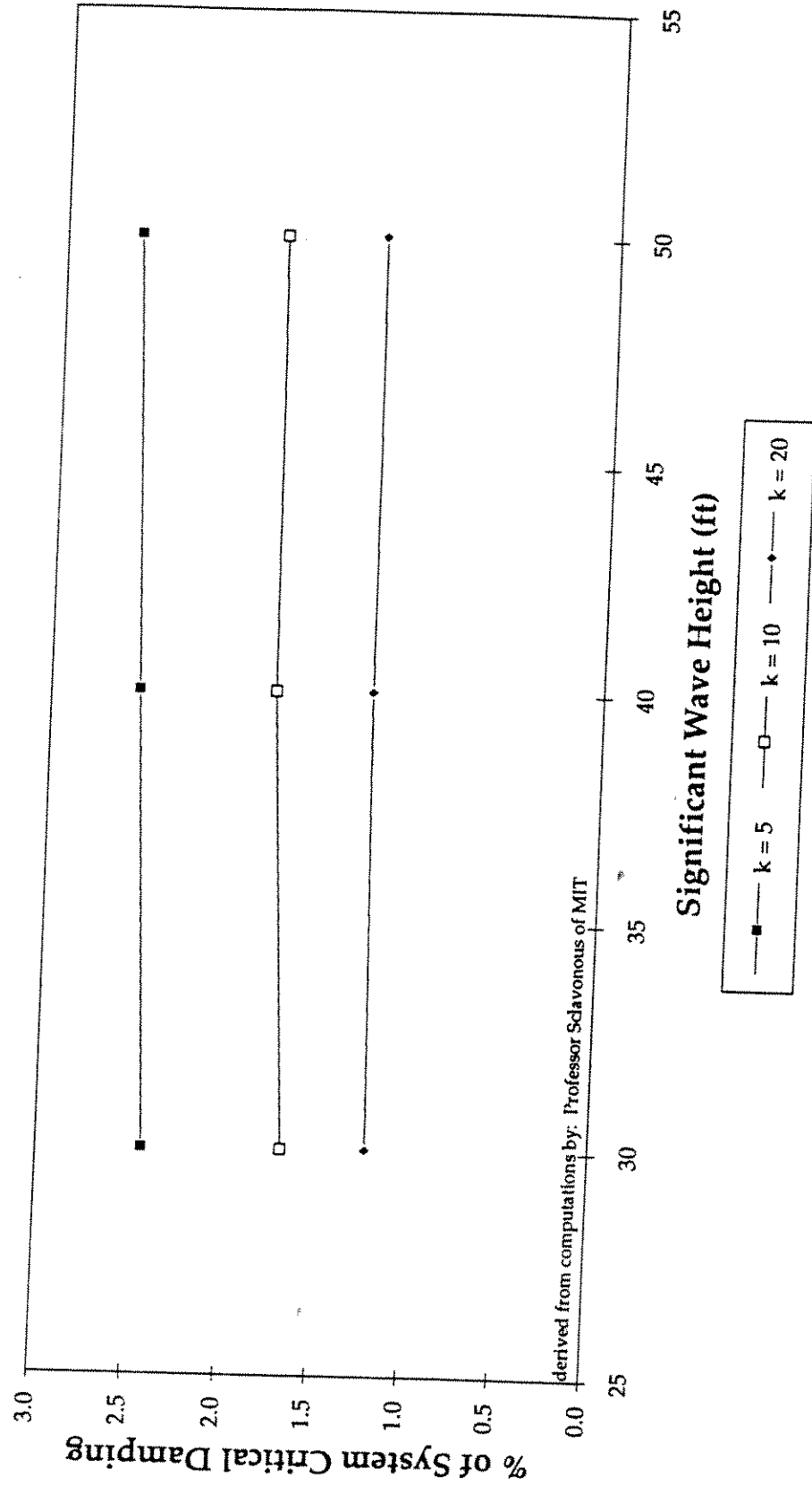
**SEMI-SUBMERSIBLE/FPS (GVA 5000 CLASS)
LF SWAY WAVE DRIFT DAMPING
HEADING ANGLE = 22.5 DEGREES**



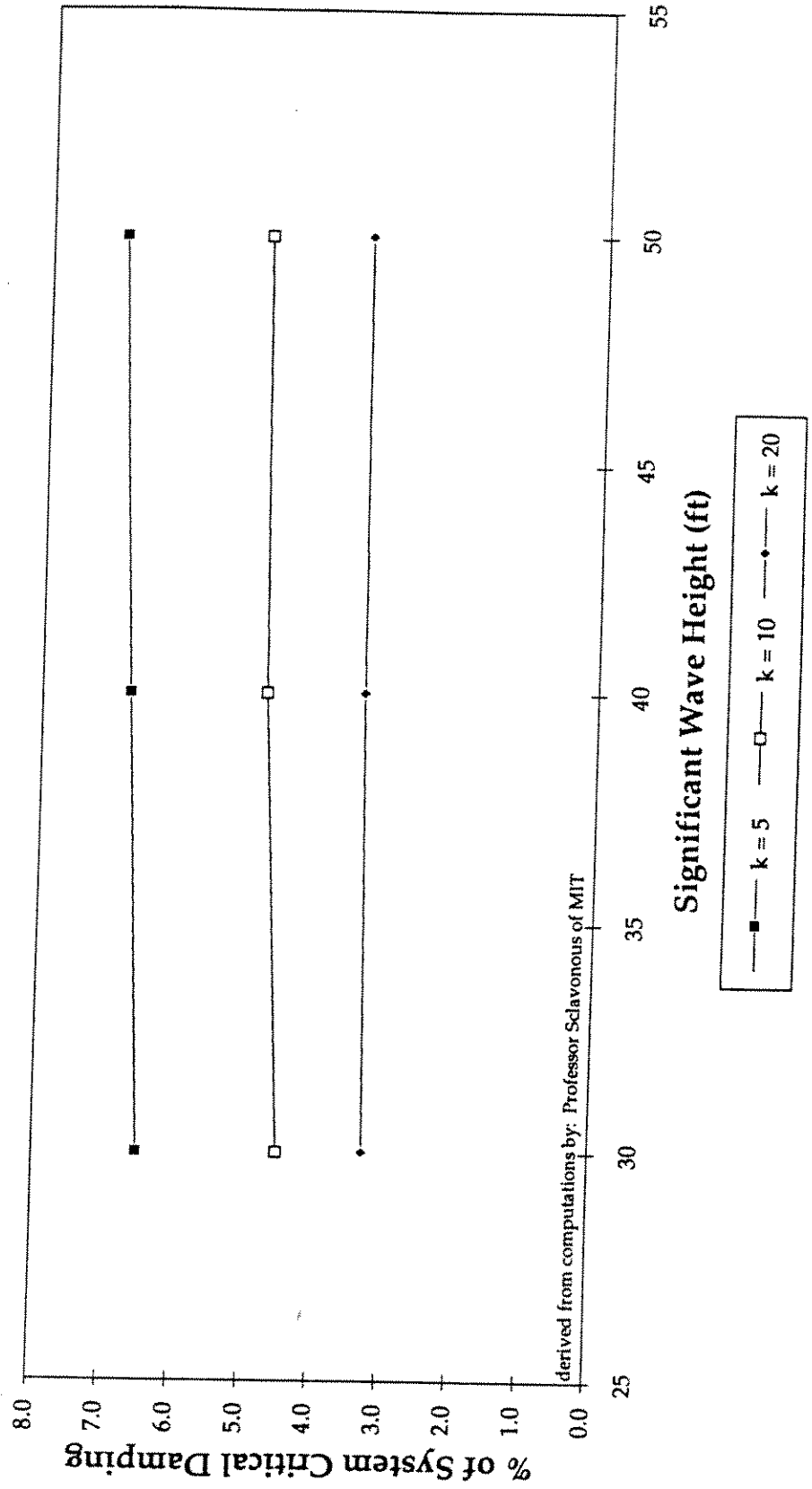
**SEMI-SUBMERSIBLE/FPS (GVA 5000 CLASS)
LF SWAY WAVE DRIFT DAMPING
HEADING ANGLE = 45.0 DEGREES**



**SEMI-SUBMERSIBLE/FPS (GVA 5000 CLASS)
LF SURGE VISCOUS DAMPING
HEADING ANGLE = 0.0 DEGREES**



SEMI-SUBMERSIBLE/FPS (GVA 5000 CLASS)
LF SWAY VISCOUS DAMPING
HEADING ANGLE = 90.0 DEGREES



VESSEL LF DAMPING
SEDCO 700 SEMISUBMERSIBLE

1. COMPUTATIONAL METHODS

- MORA 3-D PROGRAM: WAVE DAMPING
- LINEARIZATION: VISCOUS DAMPING
- RATIONALIZED PROCEDURE: CURRENT AND WIND
- COLINEAR CORRELATED WIND-WAVE-CURRENT

2. STUDY MATRIX: COMPARABLE TO GVA 5000

3. A DESIGN CASE: GOMEX 10-YEAR STORM
(ASSUMING K = 10 KIPS/FT)

	<u>DAMPING (% OF SYSTEM CRITICAL)</u>	
	<u>HEAD SEA</u>	<u>BEAM SEA</u>
WAVE DRIFT DAMPING	0.2%	0.2%
VISCOUS DAMPING		
• NO CURRENT	1.7%	2.5%
• 1.8-KNOT CURRENT	13%	22%
AERODYNAMIC DAMPING (72-KNOT WIND)	2.7%	1.9%
TOTAL	5-16%	5-24%

- LF MAX. MOTION: 13 FT.
- LF PERIOD: 90 SEC.
- LF MAX. VELOCITY: 0.9 FT/SEC (0.5 KTS)
- MOORING SYSTEM STIFFNESS: 12 KIPS/FT
(1000' WD)

CHAPTER 4 - MORFRED

oncoming waves and decreases during the half-cycle where the structure tends to move with the waves thus giving rise to a damping force. Based on the work done in a full cycle, the wave damping coefficient may be related to the gradient of the mean drift force as

$$\bar{b}_1(f) = \frac{2\pi f^2}{g} \cos\beta \frac{dF_1^{(2)}}{df_e}$$

$$\bar{b}_3(f) = \frac{2\pi f^2}{g} \sin\beta \frac{dF_3^{(2)}}{df_e}$$

where

$F_i^{(2)}$ = the mean drift force in the i-direction.

f = wave frequency.

f_e = wave encounter frequency.

g = acceleration of gravity.

β = wave incidence angle.

$b_i(f)$ = the i-the component damping coefficient.

The mean value of the wave damping for a wave spectrum is given by

$$b_{1mw} = 2 \int_0^{\infty} S(f) \frac{b_1(f)}{(H/2)^2} df$$

The wave damping coefficient $b_1(f)$ is proportional to the wave amplitude squared, i.e., $(H/2)^2$, since $b_1(f)$ is proportional to the mean drift force.

The viscous damping is computed by the same linearized method as used in the response to wave frequency. The total mean damping is given by the sum of the wave damping and viscous damping, $b_{im} = b_{imw} + b_{imv}$.

The drift response analysis disregards the yawing motion and deals only with motion in the

ASSUMPTIONS/APPROXIMATIONS

1. COLINEAR/CORRELATED WIND-WAVE-CURRENT

<u>H_s</u>	<u>WIND SPEED</u>	<u>CURRENT VELOCITY</u>
20'	36 KTS	0.6 KTS
30'	72 KTS	1.8 KTS
40'	108 KTS	3.0 KTS
50'	132 KTS	4.4 KTS

2. API RP-2P LF MOTIONS

$$\text{LF RMS} = (\text{REF. RMS}) \sqrt{18/K}$$

$$\text{LF SIG.} = 2 * (\text{LF RMS})$$

$$\text{LF MAX} = 3 * (\text{LF RMS})$$

3. API RP-2P WF MOTION RAOS

WF RMS BY SPECTRAL ANALYSIS

$$\text{WF SIG} = 2 * (\text{WF RMS})$$

$$\text{WF MAX} = 1.86 * (\text{WF SIG})$$

COMPUTATIONAL METHOD

1. LINEARIZED LF VISCOUS DAMPING (C_{LC})

$$C_{LC} = \frac{8}{3\pi} C_{DC} * V_{LF}$$

C_{DC} = CURRENT FORCE COEFFICIENT

V_{LF} = LF VELOCITY AMPLITUDE

2. EFFECTS OF A STRONG COLINEAR CURRENT

$$F_{DRAG} = C_{DC} [V_{CURR} + V_{LF}(t)]^2$$

$$F_{DAMPING} = (2 * C_{DC} * V_{CURR}) V_{LF}(t)$$

$$C_{DAMPING} = 2 * C_{DC} * V_{CURR}$$

$$C_{CRITICAL} = 2 * \sqrt{(M + A) K}$$

$$DAMPING RATIO = C_{DAMPING} / C_{CRITICAL}$$

3. EFFECTS OF A STRONG COLINEAR WIND (SOURCE: PROFESSOR VICKERY OF U. OF WESTERN ONTARIO)

$$C_{DAMPING} = 2 * C_{DW} * V_{WIND}$$

C_{DW} = WIND FORCE COEFFICIENT

VESSEL/MOORING PARTICULARS
SEDCO 700 SEMISUBMERSIBLE IN OBLIQUE SEA

MOORING

<u>PARTICULARS</u>	<u>3000' WD</u>	<u>1000' WD</u>	<u>300' WD</u>
NO. OF LINES	8	8	8
MOORING PATTERN	45° SYM.	45° SYM.	45° SYM.
LINE SEGMENT 1 (FROM ANCHOR)	3" ORQ CHAIN 2000'	3" ORQ CHAIN 2000'	3" ORQ CHAIN 4000'
LINE SEGMENT 2	3 3/8" WIRE 7000'	3 3/8" WIRE 5000'	---

VESSEL PARTICULARS
(SLUGS)

MASS	1.51E+06	1.51E+06	1.51E+06
SURGE ADDED MASS	5.15E+05	5.15E+05	5.15E+05
SWAY ADDED MASS	1.28E+06	1.28E+06	1.28E+06

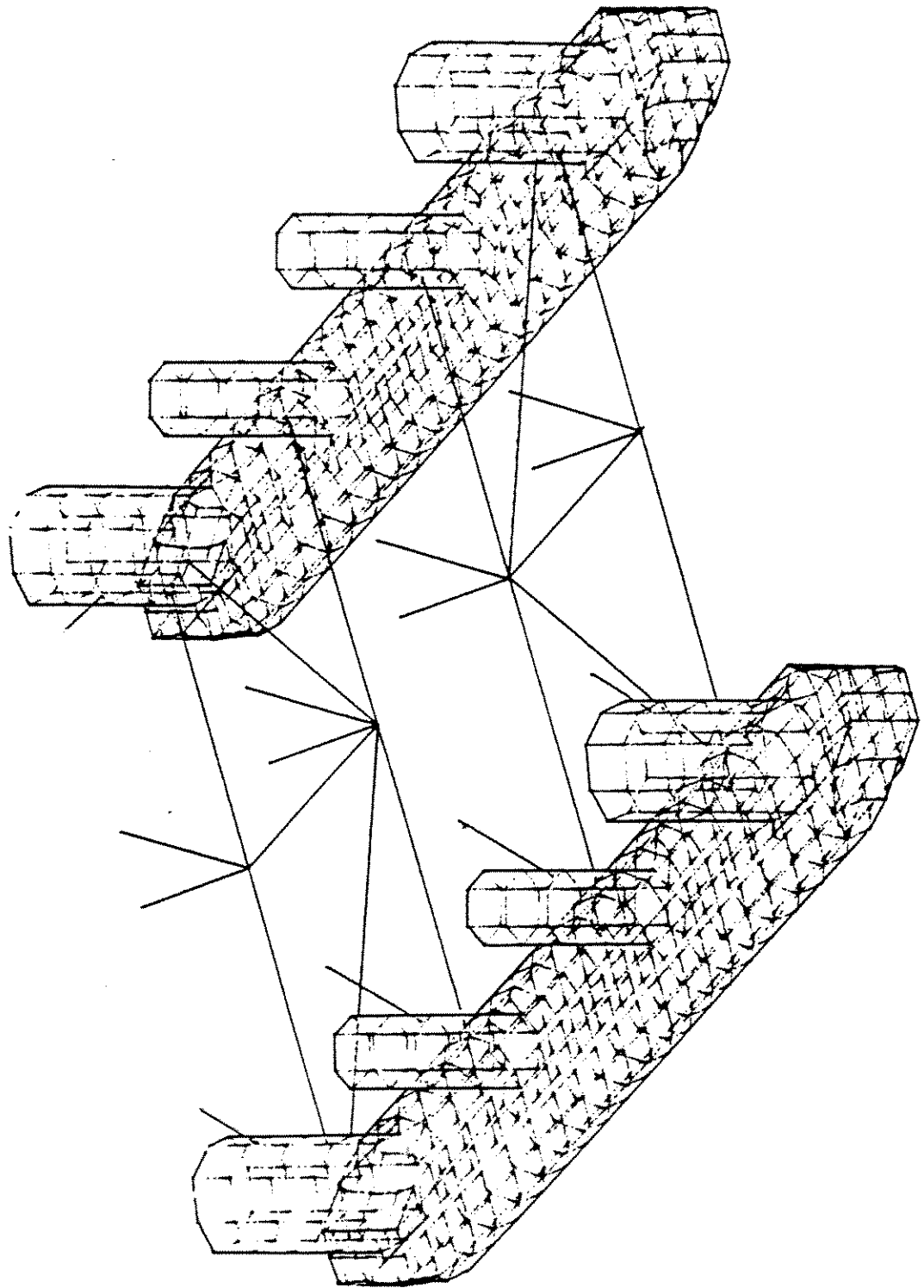
<u>MEAN ENV. LOAD</u>	668 KIPS	668 KIPS	668 KIPS
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<u>MOORING SYSTEM STIFFNESS (LBS/FT)</u>	3700	12200	28800
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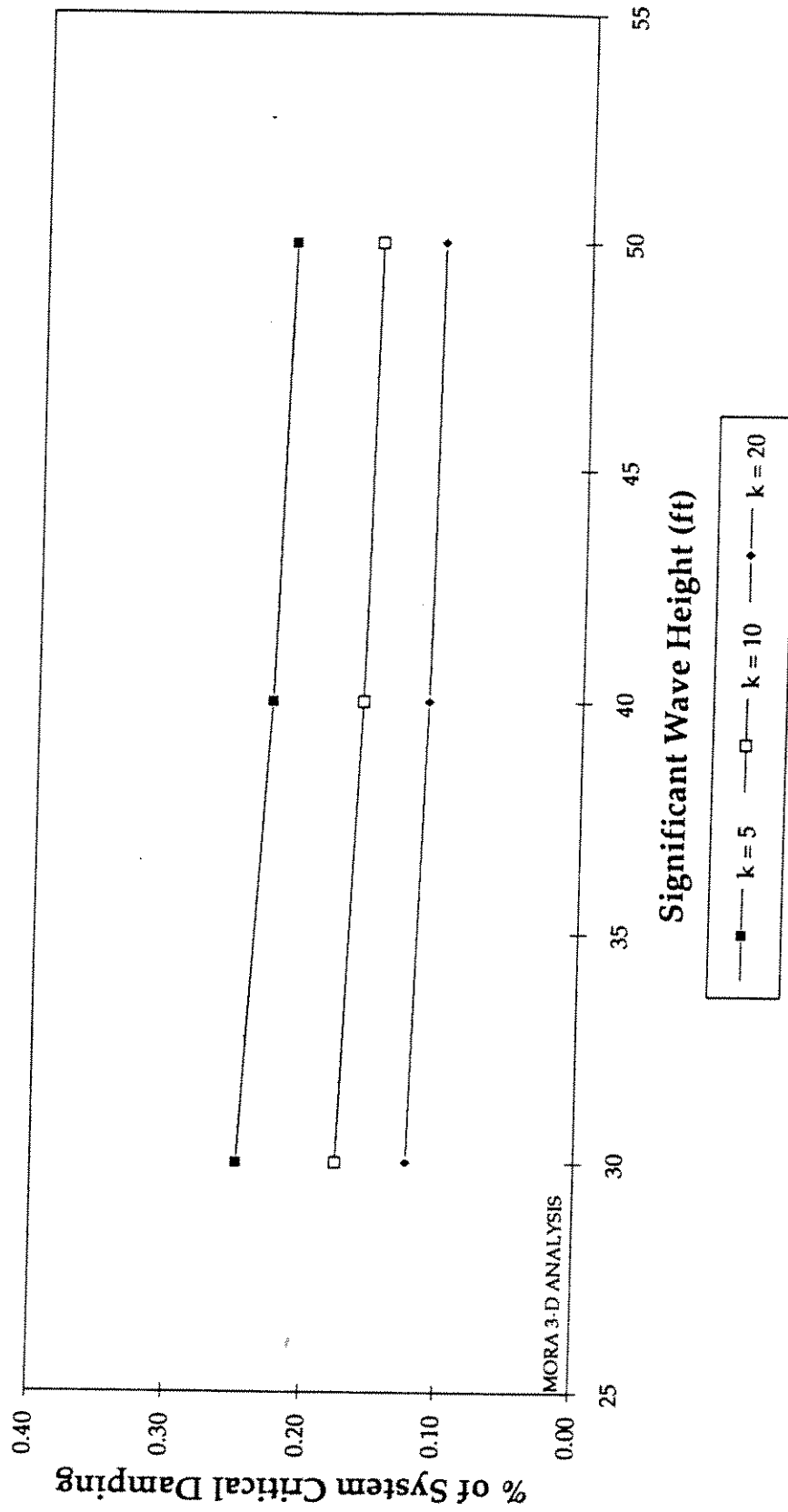
VESSEL MOTIONS

LF MAX. MOTION*	22 FT.	13 FT.	9 FT.
LF PERIOD	160 SEC.	90 SEC.	60 SEC.
WF MEAN MOTION (RMS)	3.3 FT.	3.3 FT.	3.3 FT.

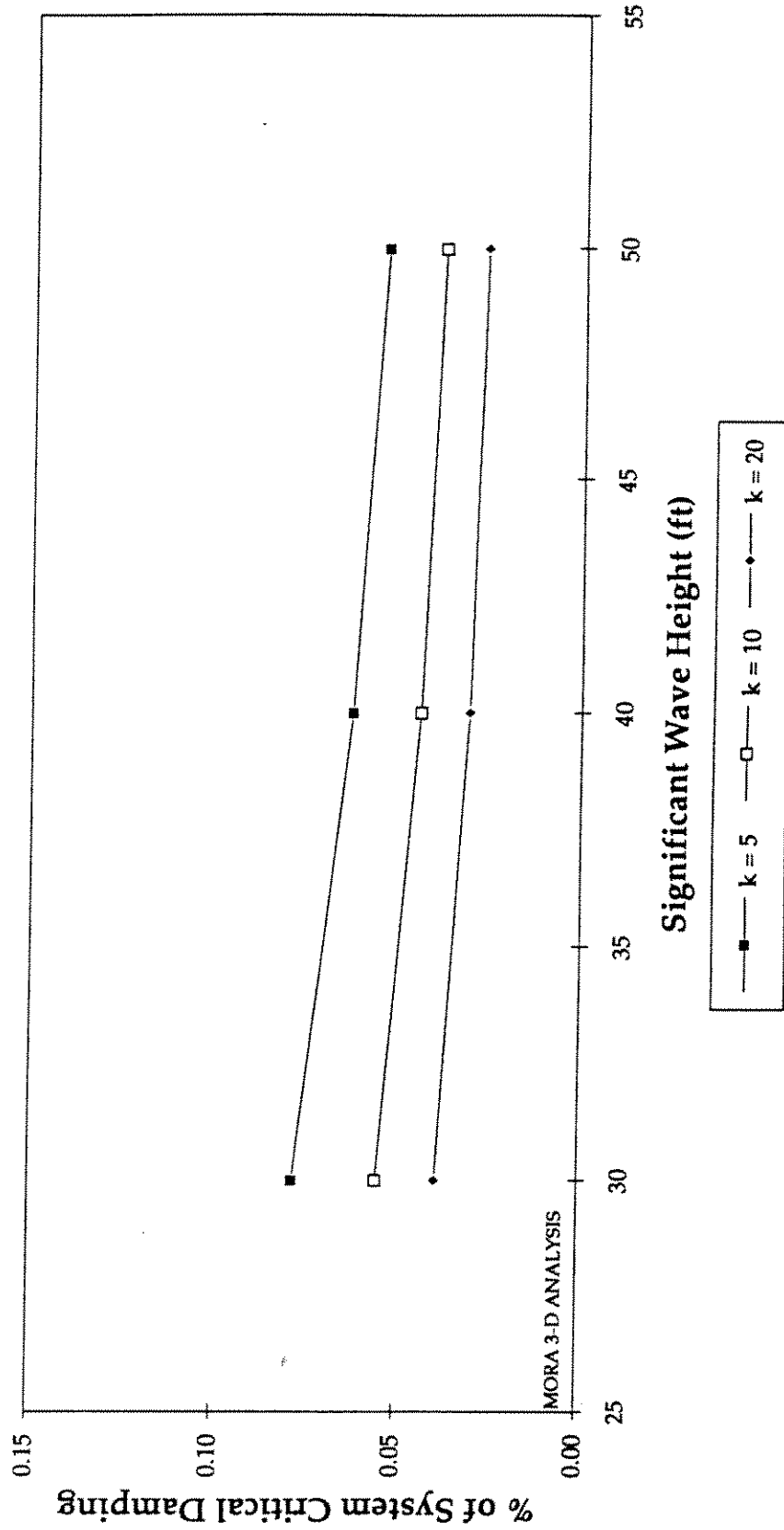
* API RP-2P BEAM SEA LF VALUES.



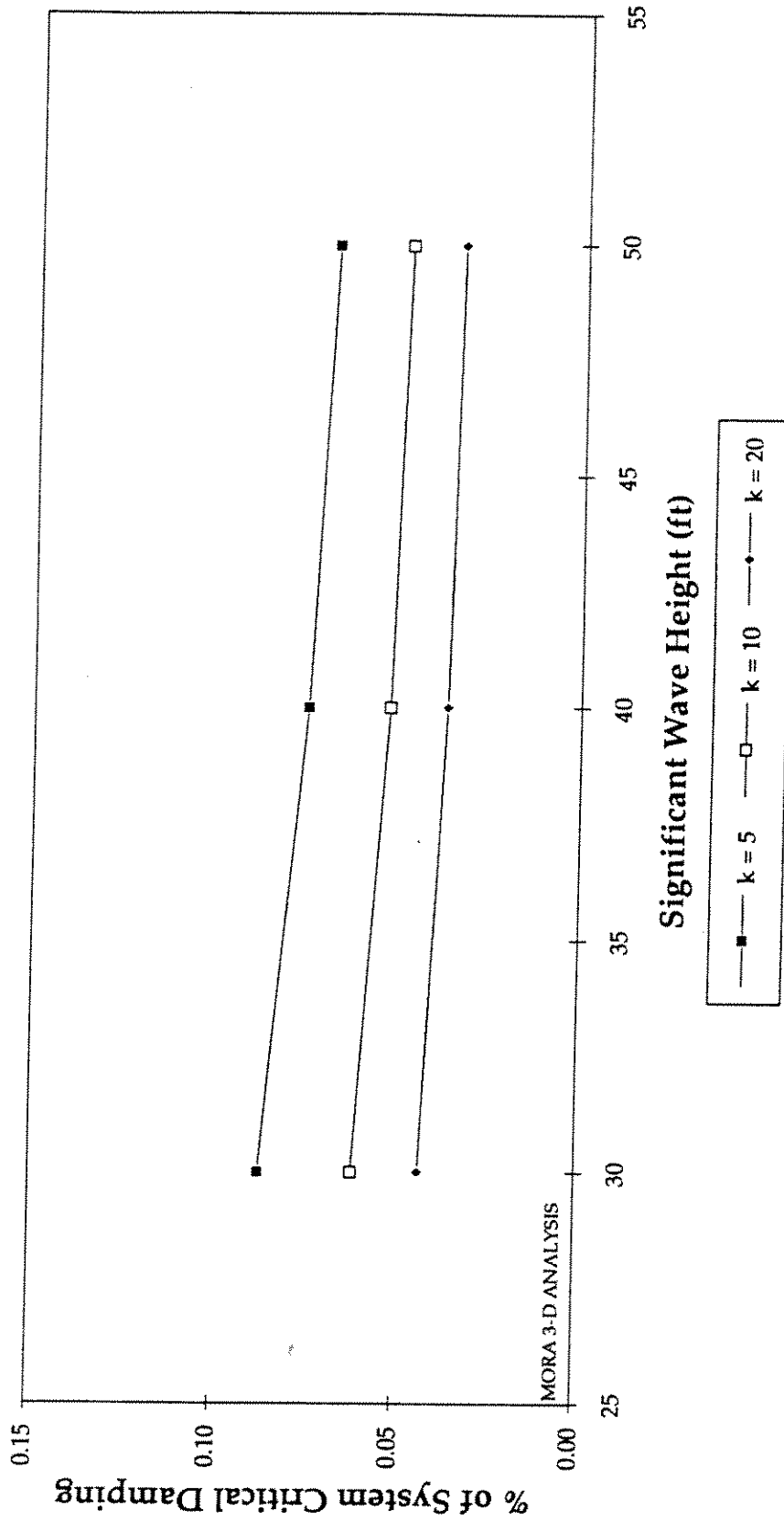
SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
LF SURGE WAVE DRIFT DAMPING
HEADING ANGLE = 0.0 DEGREES



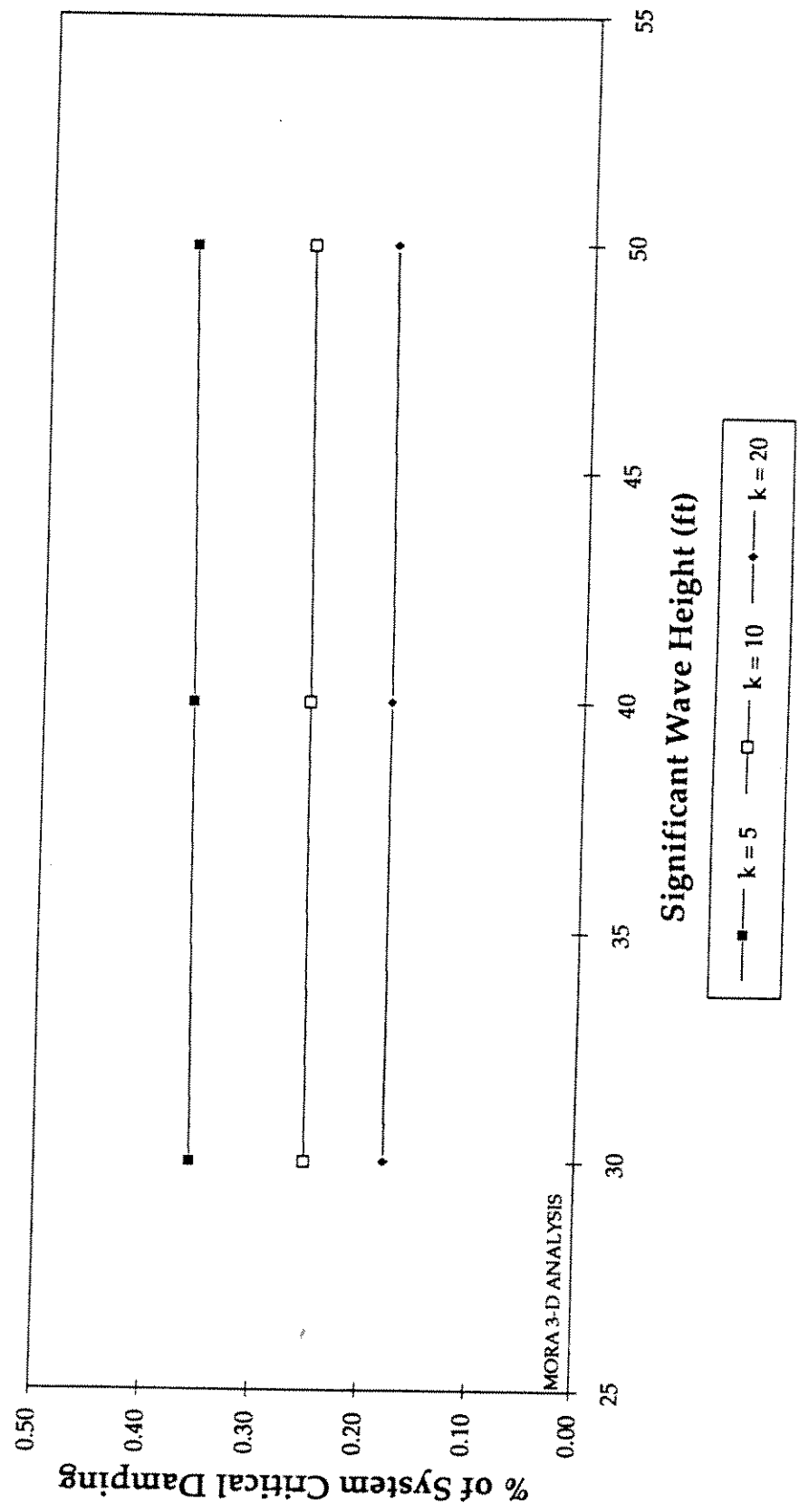
**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
LF SURGE WAVE DRIFT DAMPING
HEADING ANGLE = 45.0 DEGREES**



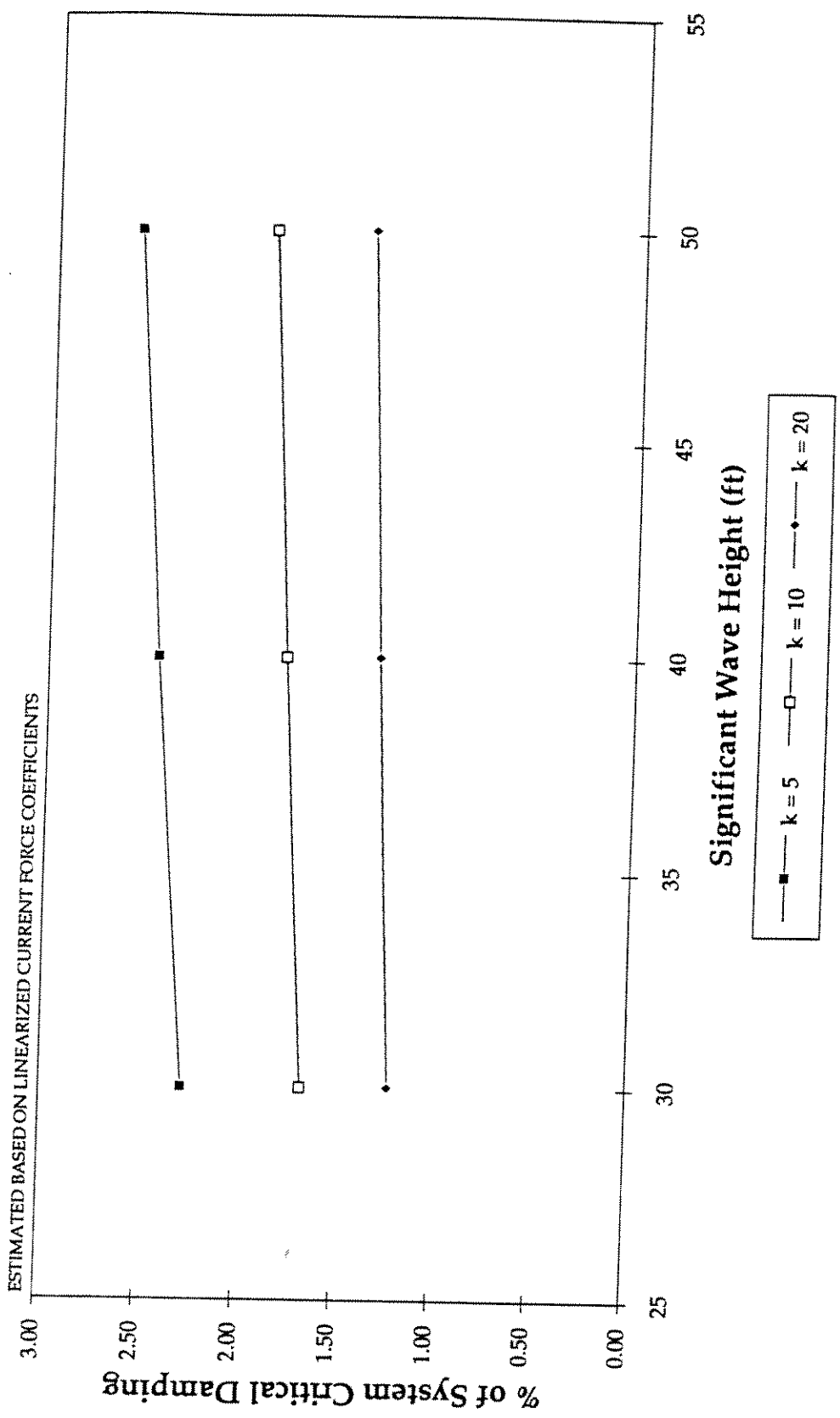
**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
LF SWAY WAVE DRIFT DAMPING
HEADING ANGLE = 45.0 DEGREES**



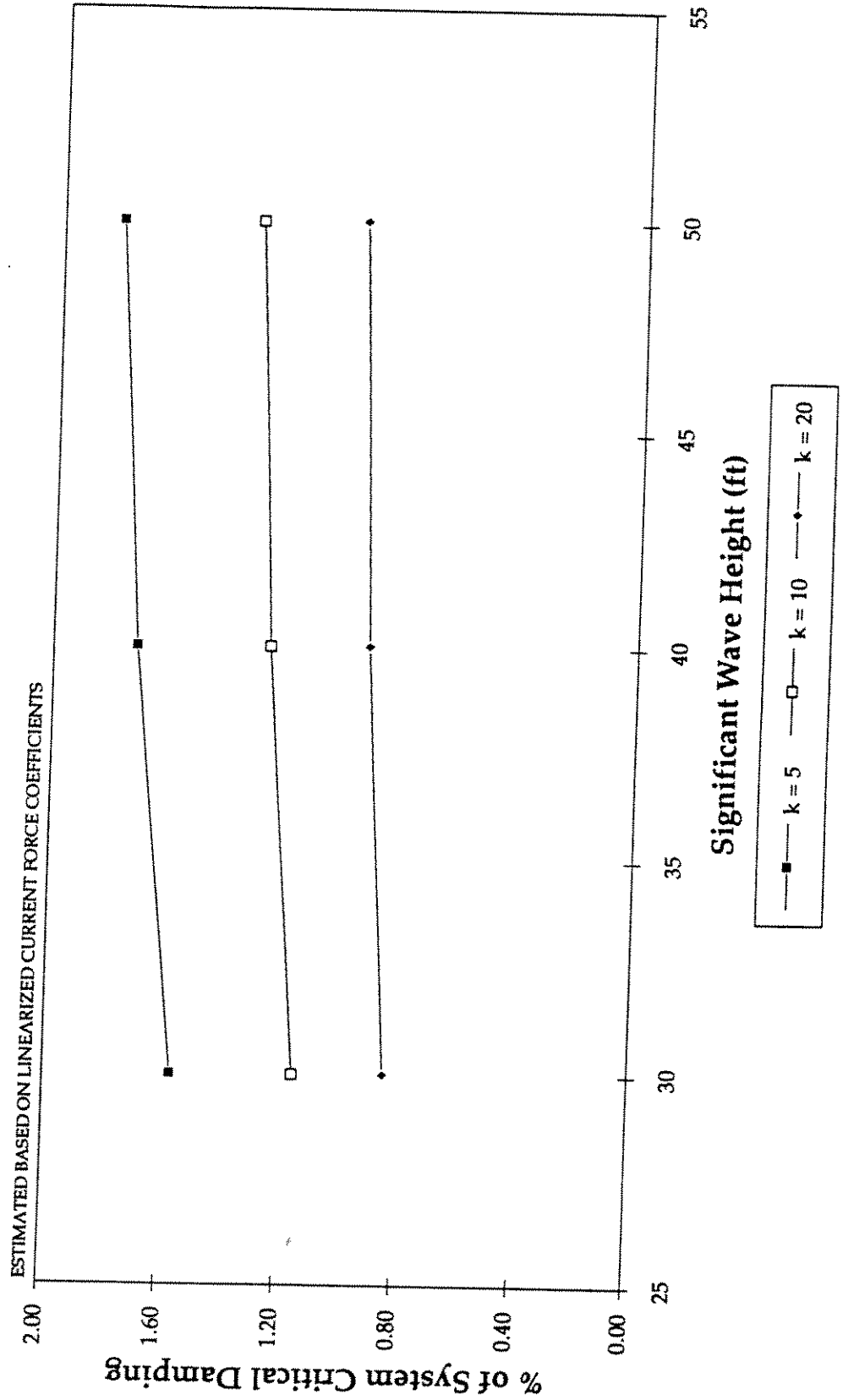
**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
 LE SWAY WAVE DRIFT DAMPING
 HEADING ANGLE = 90.0 DEGREES**



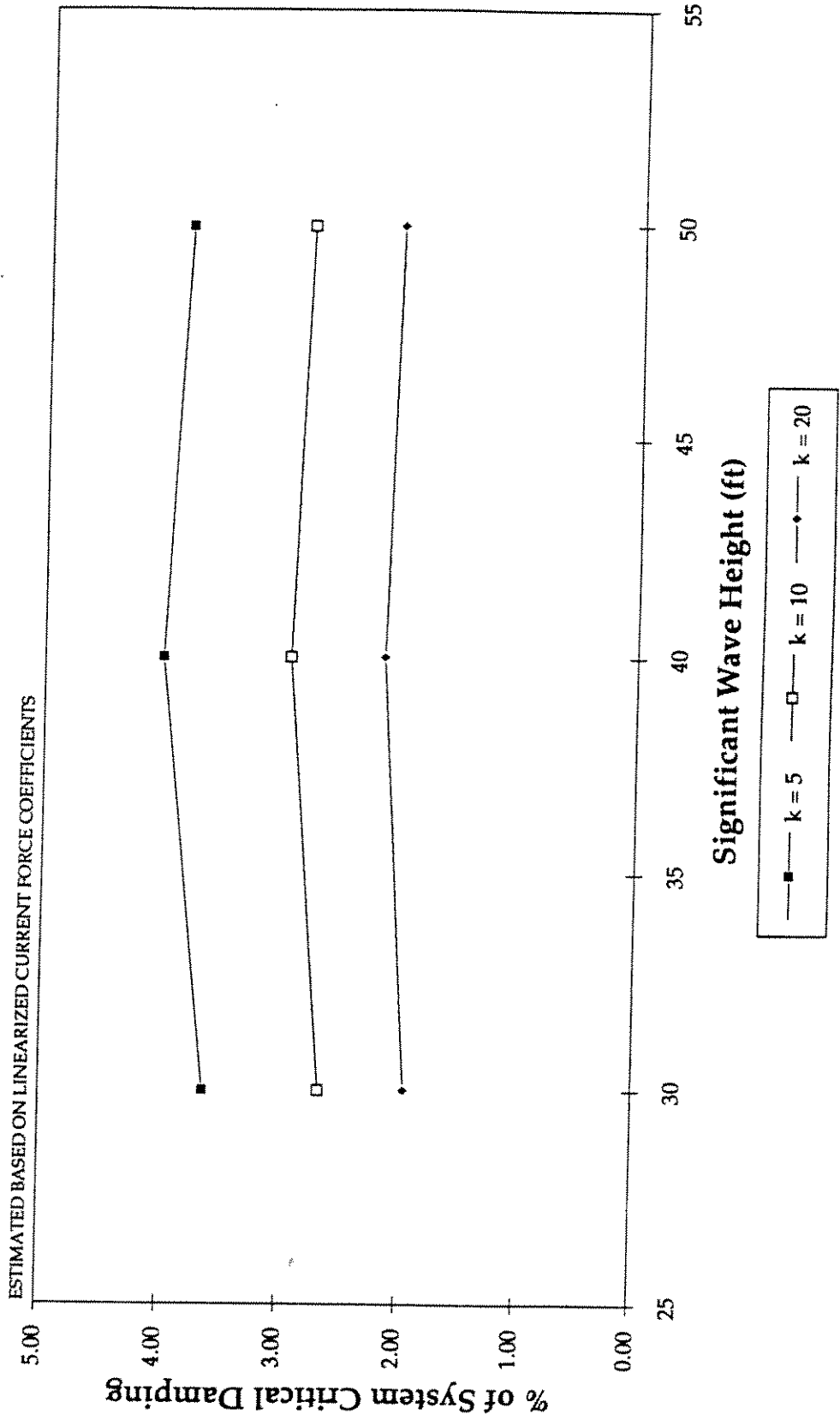
**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
 LF SURGE VISCOUS DAMPING
 (NO CURRENT, LF MOTION ONLY)
 HEADING ANGLE = 0.0 DEGREES**



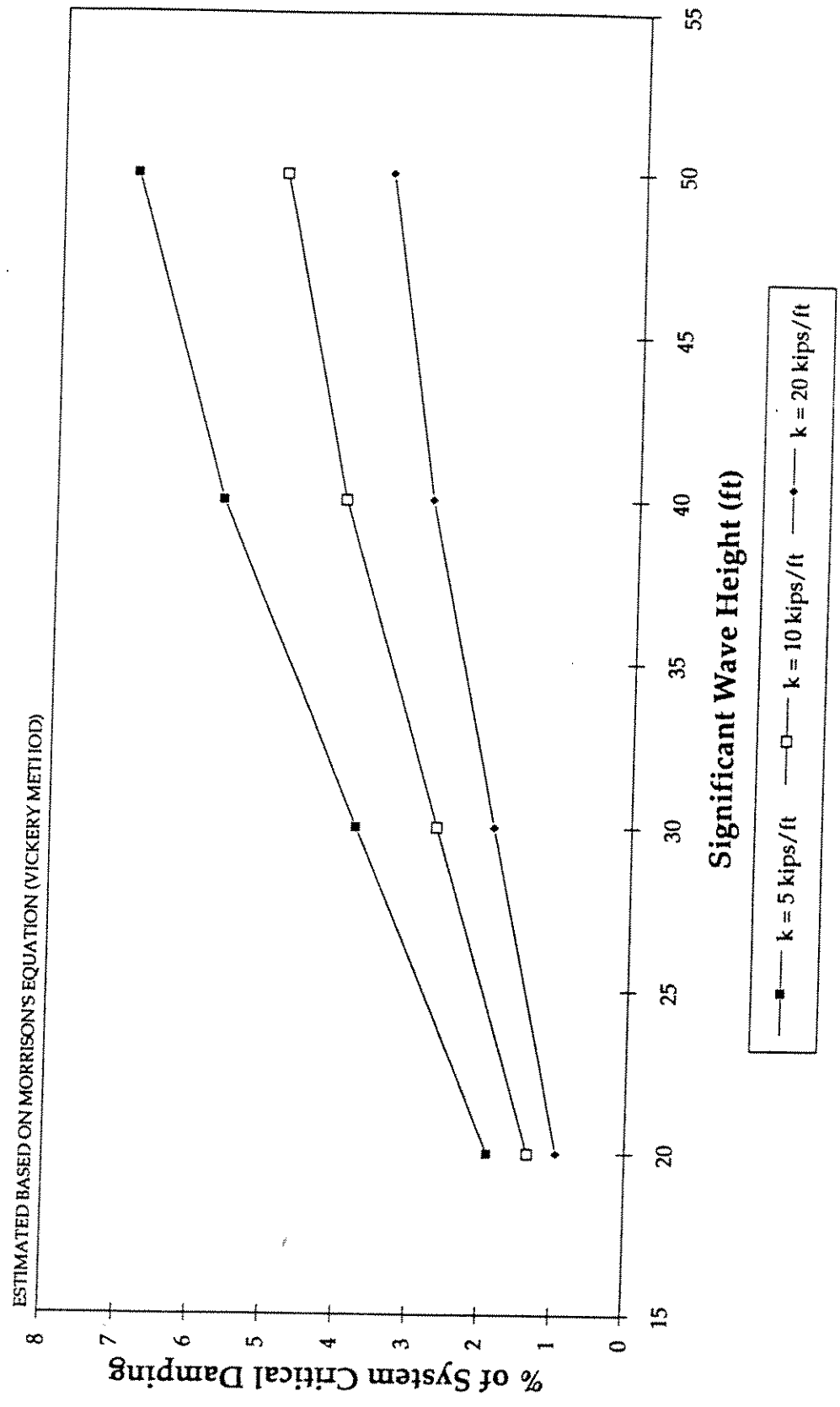
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LF VISCOUS DAMPING
(NO CURRENT, LF MOTION ONLY)
HEADING ANGLE = 45.0 DEGREES**



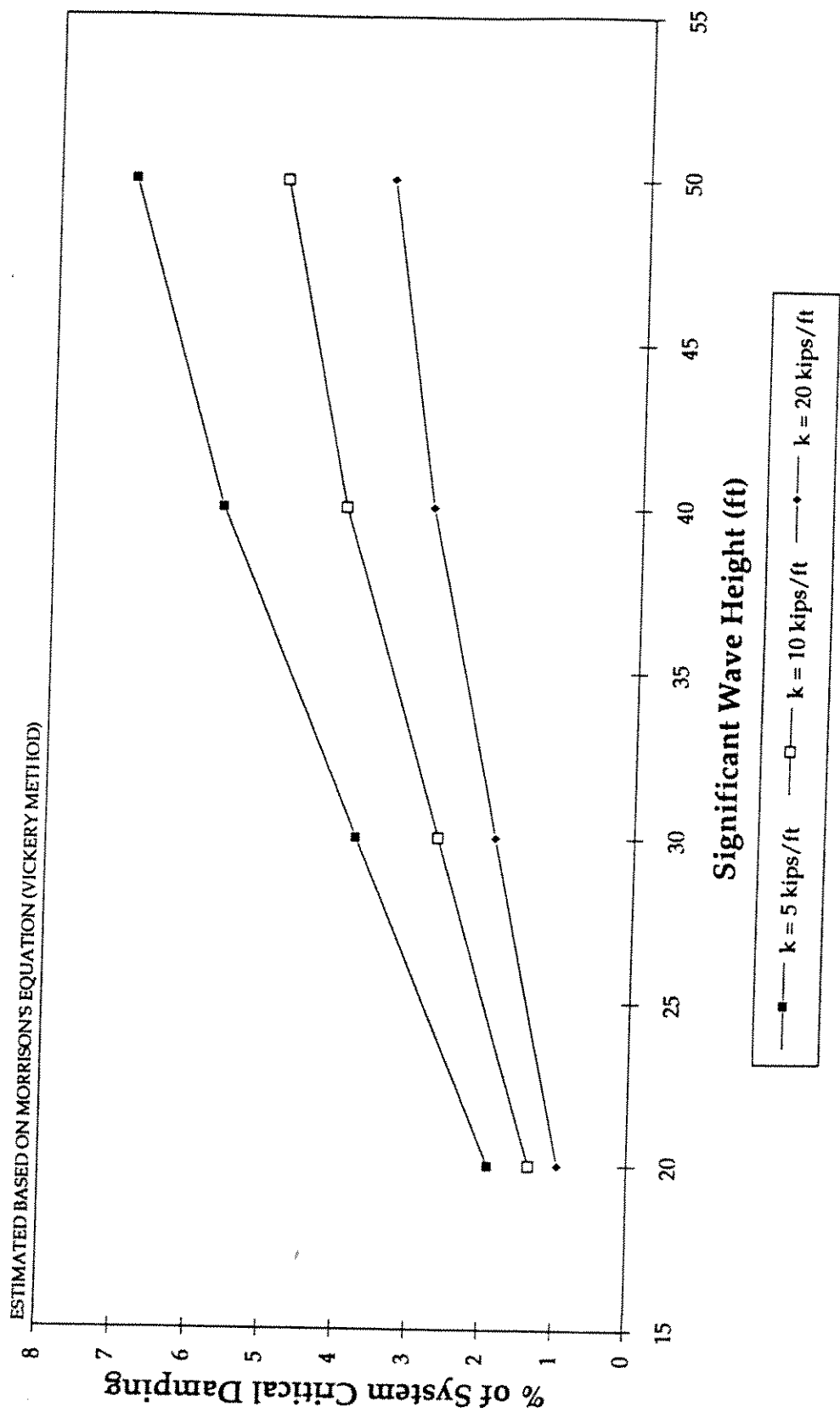
**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
LF SWAY VISCOUS DAMPING
(NO CURRENT, LF MOTION ONLY)
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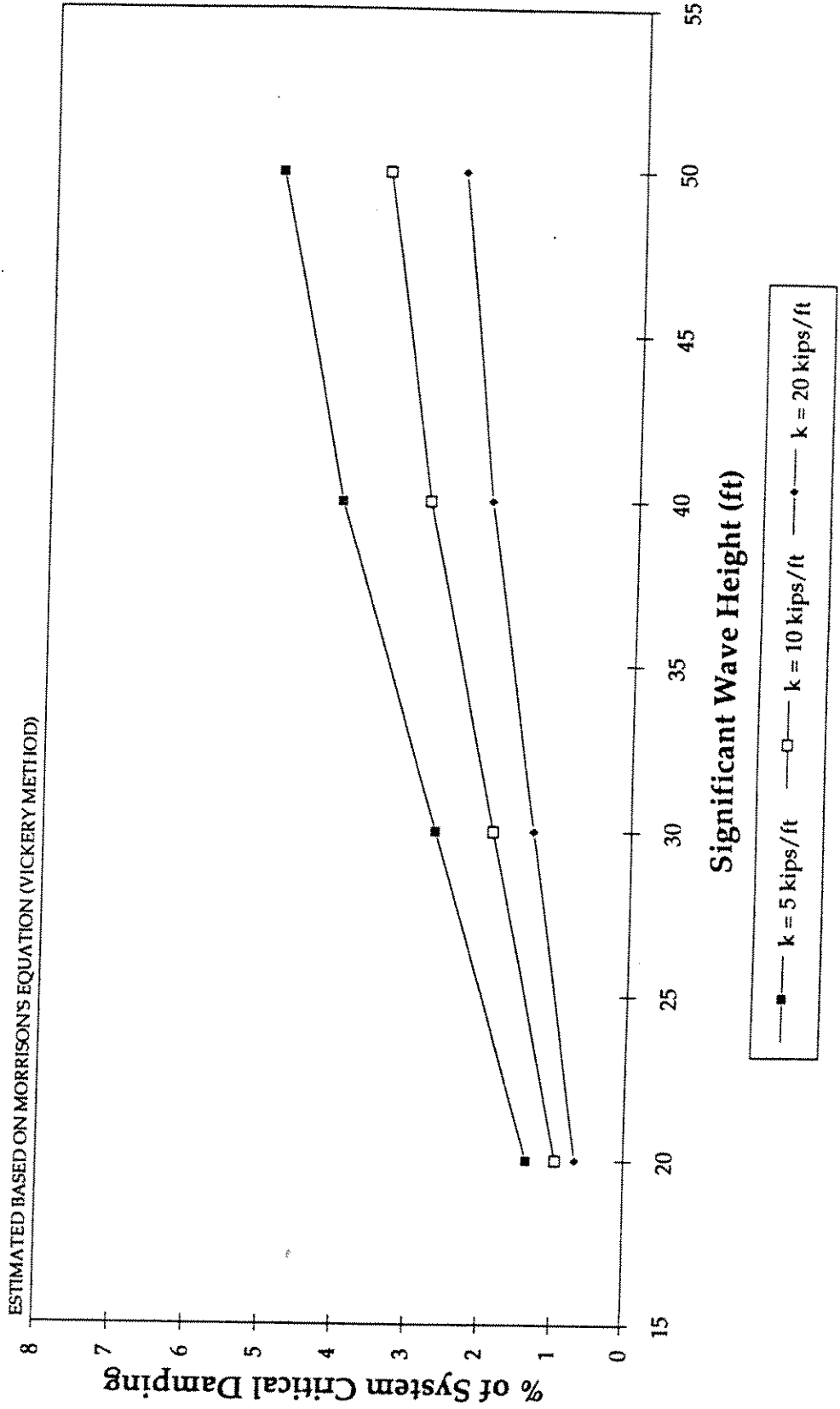
**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
 LF WIND INDUCED DAMPING
 (LF MOTION PLUS WIND)
 HEADING ANGLE = 0.0 DEGREES**



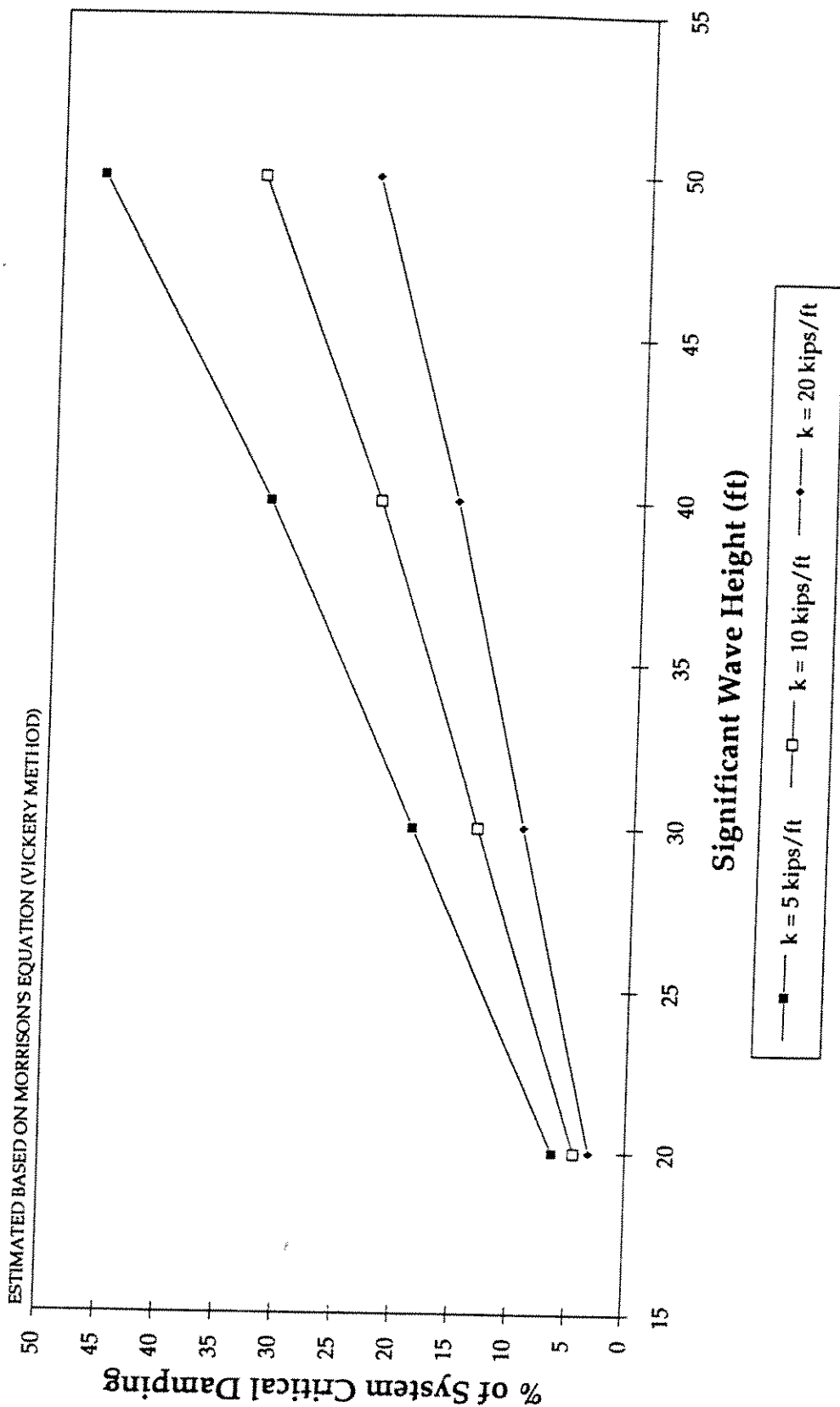
SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
LF WIND INDUCED DAMPING
(LF MOTION PLUS WIND)
HEADING ANGLE = 45.0 DEGREES



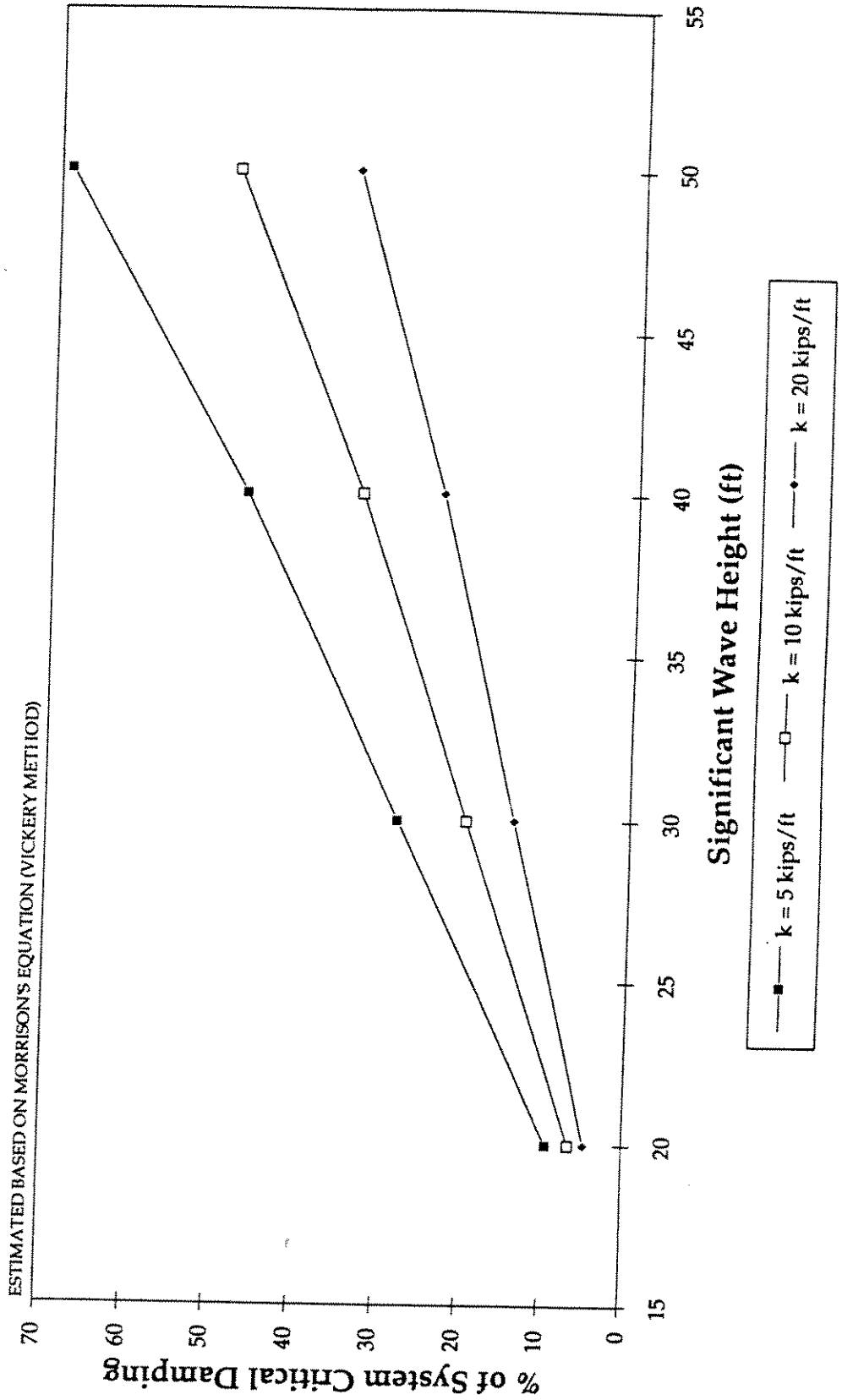
**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
 LF WIND INDUCED DAMPING
 (LF MOTION PLUS WIND)
 HEADING ANGLE = 90.0 DEGREES**



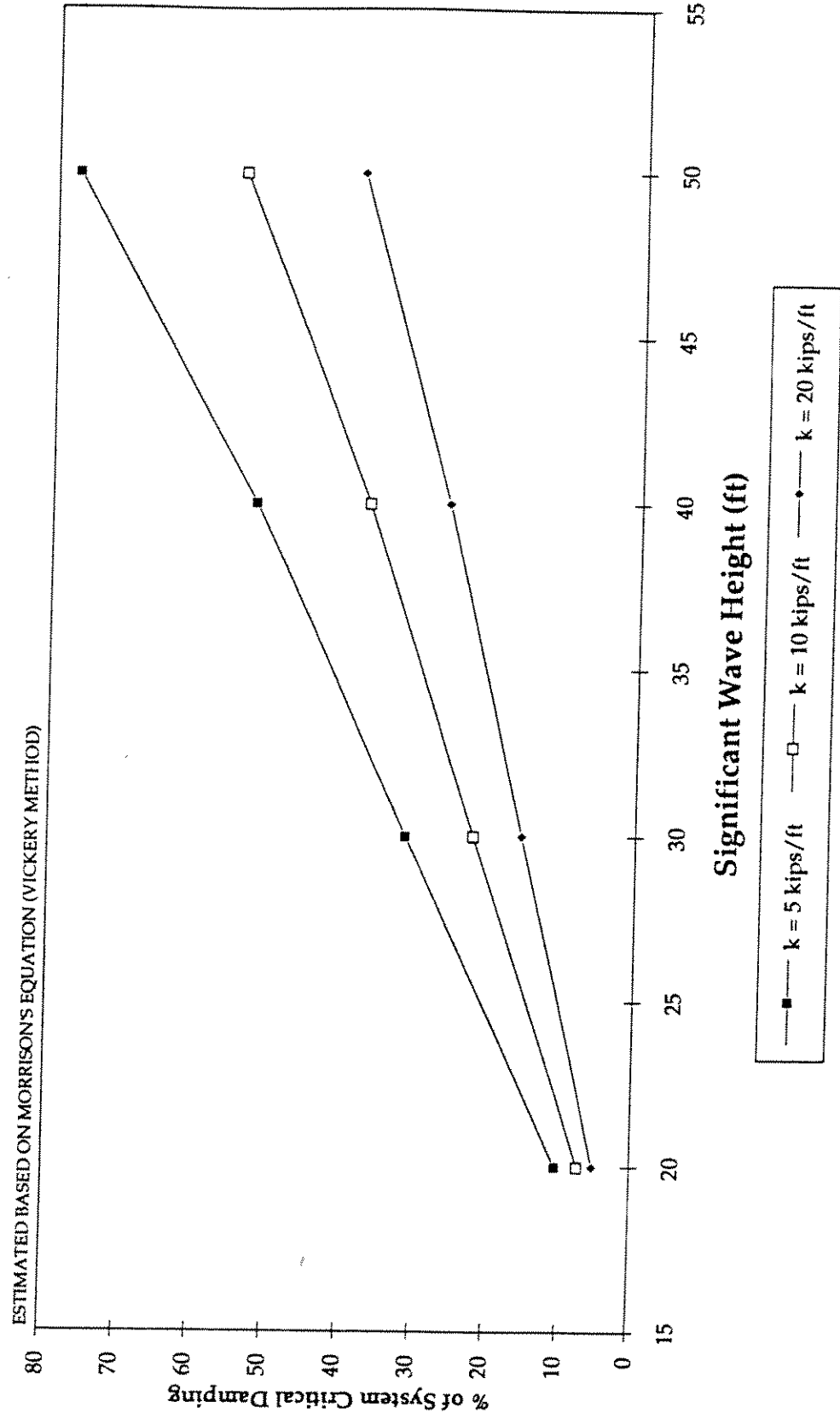
**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
LF CURRENT INDUCED DAMPING
(LF MOTION PLUS CURRENT)
HEADING ANGLE = 0.0 DEGREES**



SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
LF CURRENT INDUCED DAMPING
(LF MOTION PLUS CURRENT)
HEADING ANGLE = 45.0 DEGREES



**SEMI-SUBMERSIBLE (SEDCO 700 CLASS)
 LF CURRENT INDUCED DAMPING
 (LF MOTION PLUS CURRENT)
 HEADING ANGLE = 90.0 DEGREES**



VESSEL LF DAMPING
DRILLSHIP (380' X 70' X 26')

1. COMPUTATIONAL METHODS: REF. SEDCO 700

2. STUDY MATRIX: REF. SEDCO 700

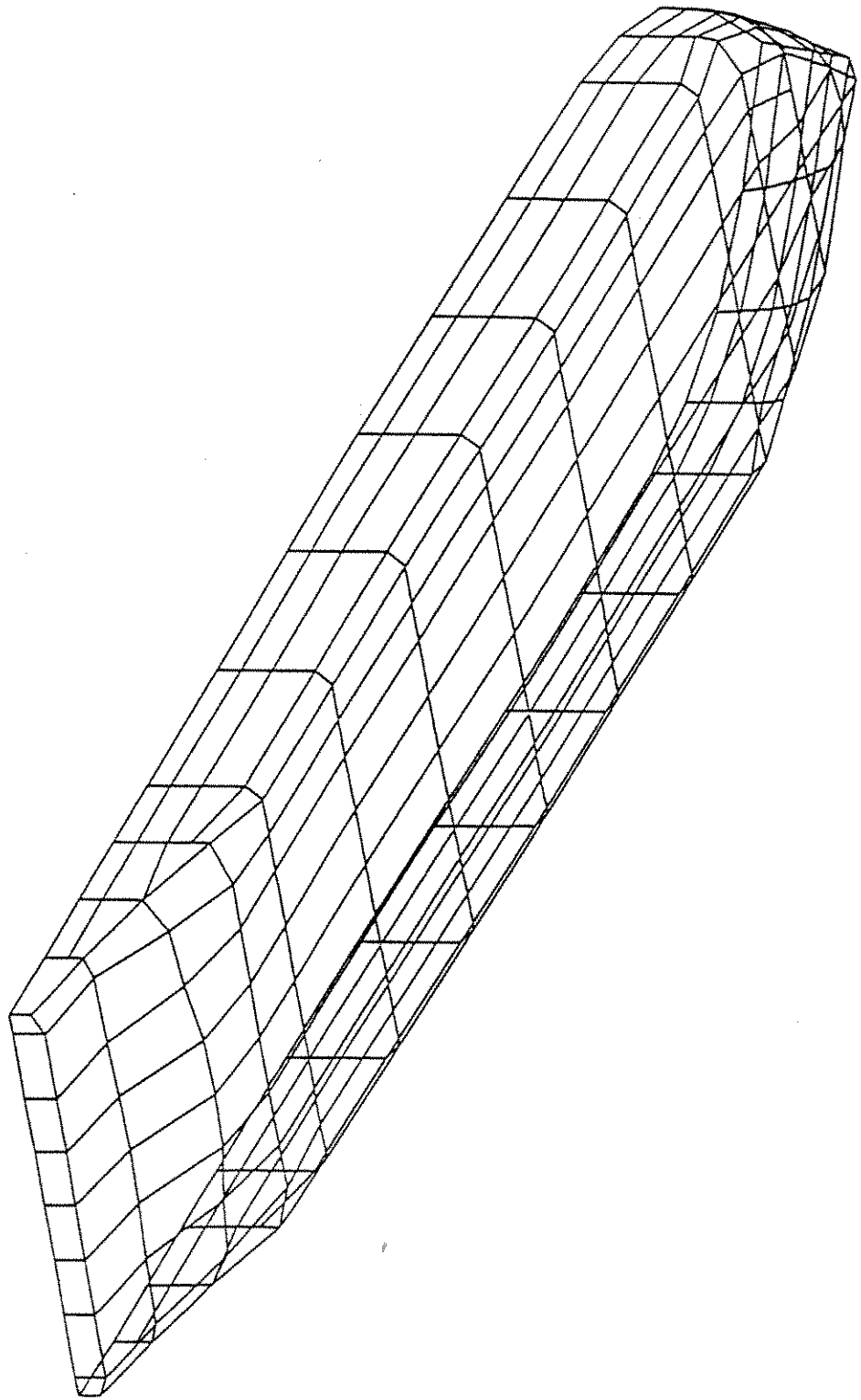
3. A DESIGN CASE: GOMEX 10-YEAR STORM

	<u>DAMPING (% OF SYSTEM CRITICAL)</u>	
	<u>HEAD SEA</u>	<u>BEAM SEA</u>
WAVE DRIFT DAMPING	1%	2.9%
VISCOUS DAMPING		
• NO CURRENT	0.2%	6.7%
• 1.8-KNOT CURRENT	2.3%	26%
AERODYNAMIC DAMPING (<u>72-KNOT WIND</u>)	1.9%	3.4%
TOTAL	1.6-5.3%	13-32%

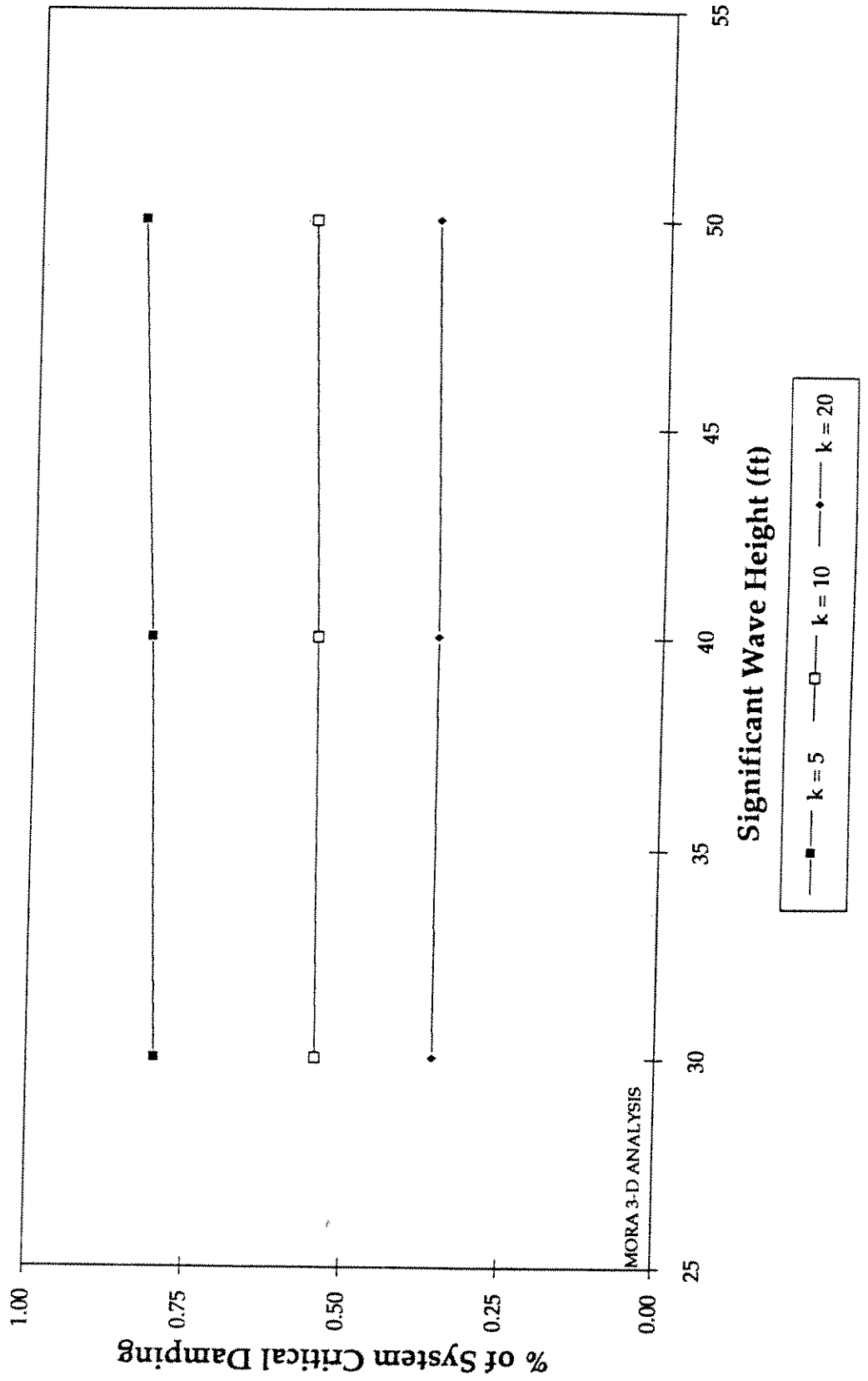
- LF MAX. MOTION: 12 FT. 22 FT.
- LF PERIOD: 120 SEC. 80 SEC.
- LF MAX. VELOCITY: 0.7 FT/SEC 1.9 FT./SEC
(0.4 KTS) (1.1 KTS)
- MOORING SYSTEM STIFFNESS 2.7 KIPS/FT 6.8 KIPS/FT
(1000' WD)

VESSEL/MOORING PARTICULARS
DRILLSHIP (L X B X D = 380' X 70' X 26')

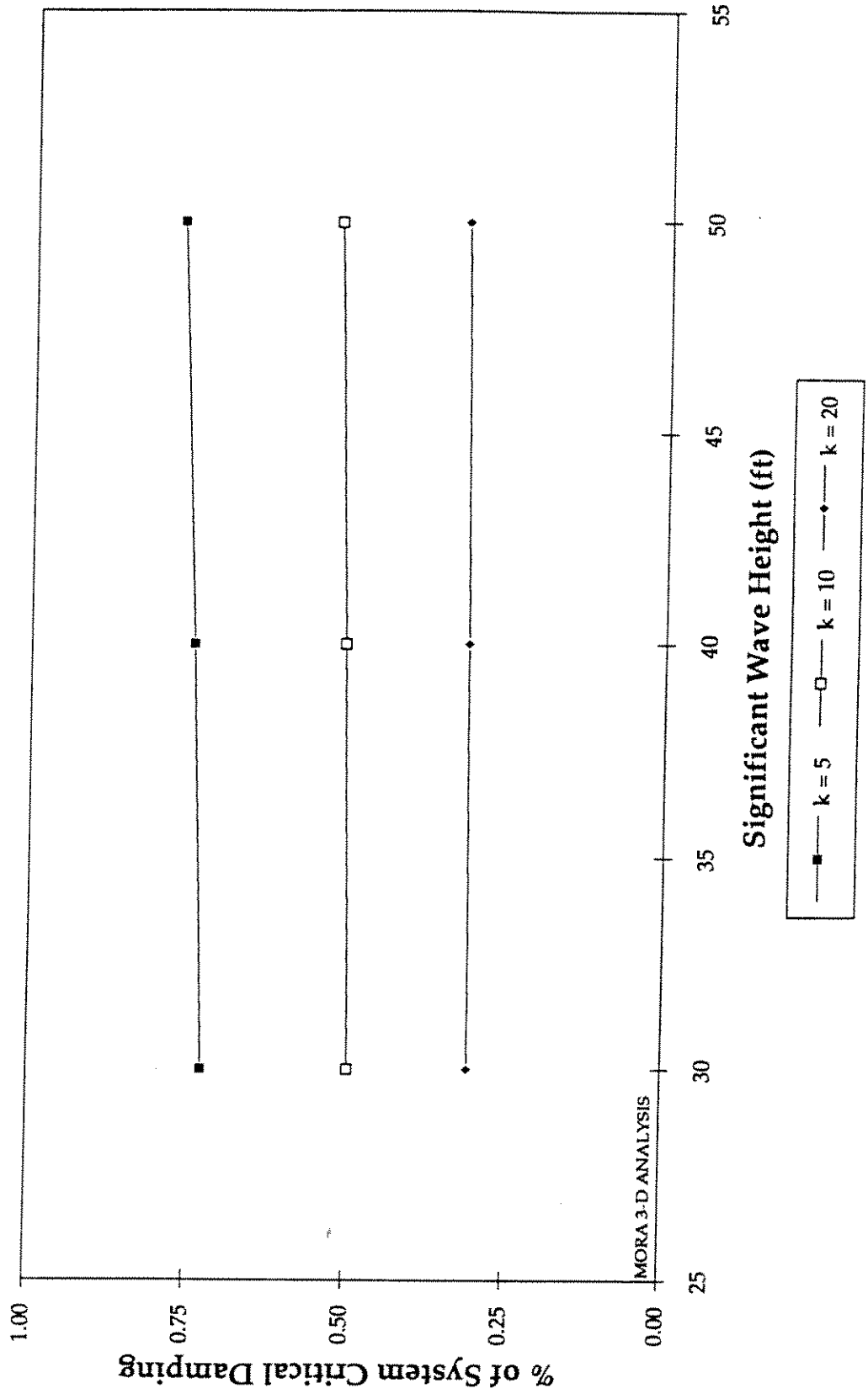
<u>MOORING PARTICULARS</u>	<u>3000' WD</u>		<u>1000' WD</u>		<u>300' WD</u>	
	<u>HEAD SEA</u>	<u>BEAM SEA</u>	<u>HEAD SEA</u>	<u>BEAM SEA</u>	<u>HEAD SEA</u>	<u>BEAM SEA</u>
NO. OF LINES	8	8	8	8	8	8
MOORING PATTERN	45°	60°	45°	60°	45°	60°
LINE SEGMENT 1 GRADE 3 2.5" CHAIN	2000'	2000'	2000'	2000'	4000'	4000'
LINE SEGMENT 2 2.5" WIRE	3500'	3500'	1500'	1500'	---	---
<u>VESSEL PARTICULARS</u>						
MASS (SLUGS)	8.39E+05	8.39E+05	8.39E+05	8.39E+05	8.39E+05	8.39E+05
ADDED MASS (SLUGS)	5.88E+04	5.89E+05	5.88E+04	5.89E+05	5.88E+04	5.89E+05
<u>MEAN ENV. LOAD (KIPS)</u>	195	590	195	590	195	590
<u>MOORING SYSTEM STIFFNESS (LBS/FT)</u>	600	2900	2700	6800	7900	21350
<u>VESSEL MOTIONS</u>						
LF MAX. MOTIONS	20'	31.8'	12.5'	21.8'	8.1'	13.3'
LF PERIODS (SEC.)	210	120	120	80	70	50
WF MOTION (RMS)	4.9'	6.7'	4.9'	6.7'	4.9'	6.7'



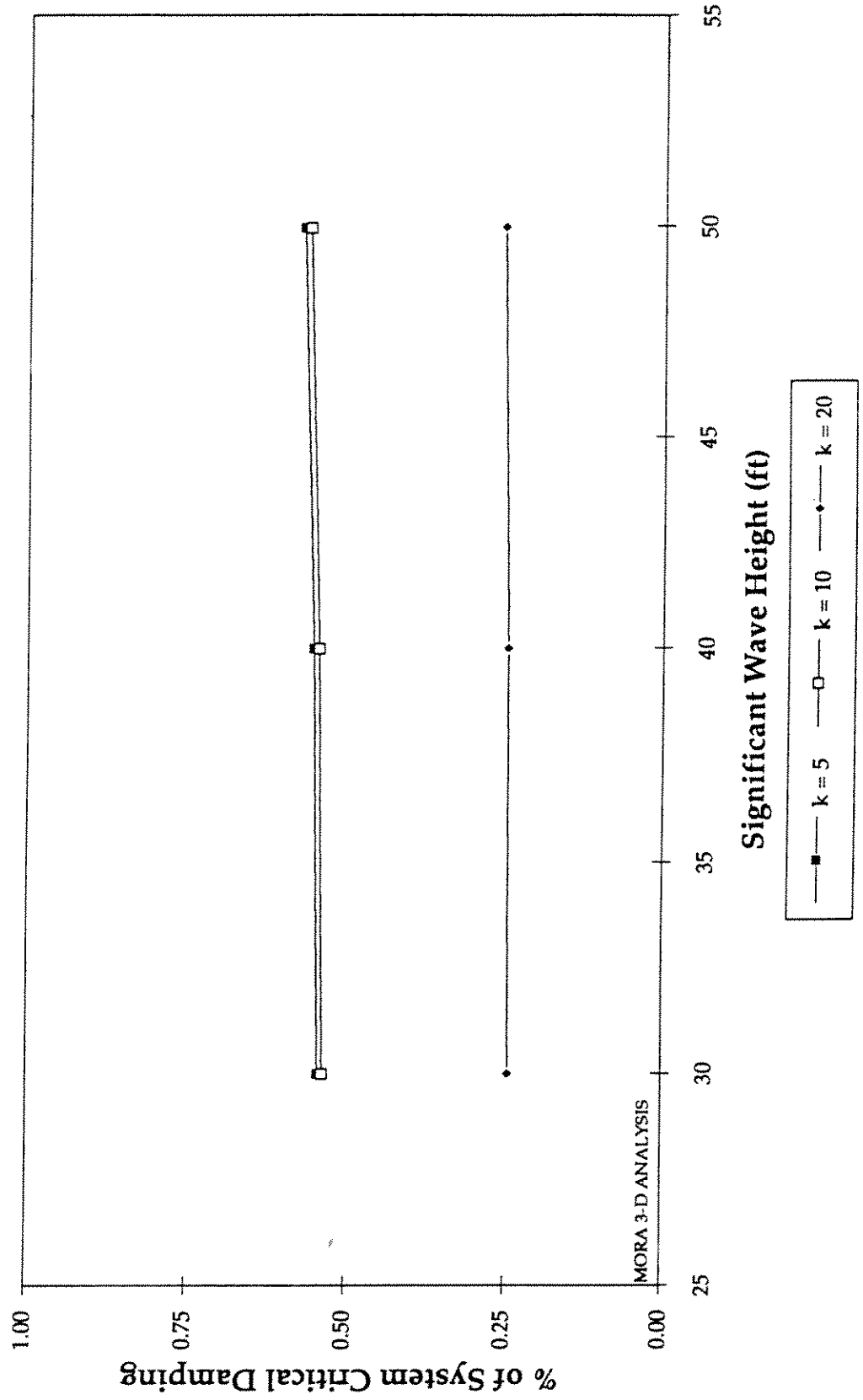
**DRILL SHIP (L x B x D = 380' x 70' x 26')
LF SURGE WAVE DRIFT DAMPING
HEADING ANGLE = 0.0 DEGREES**



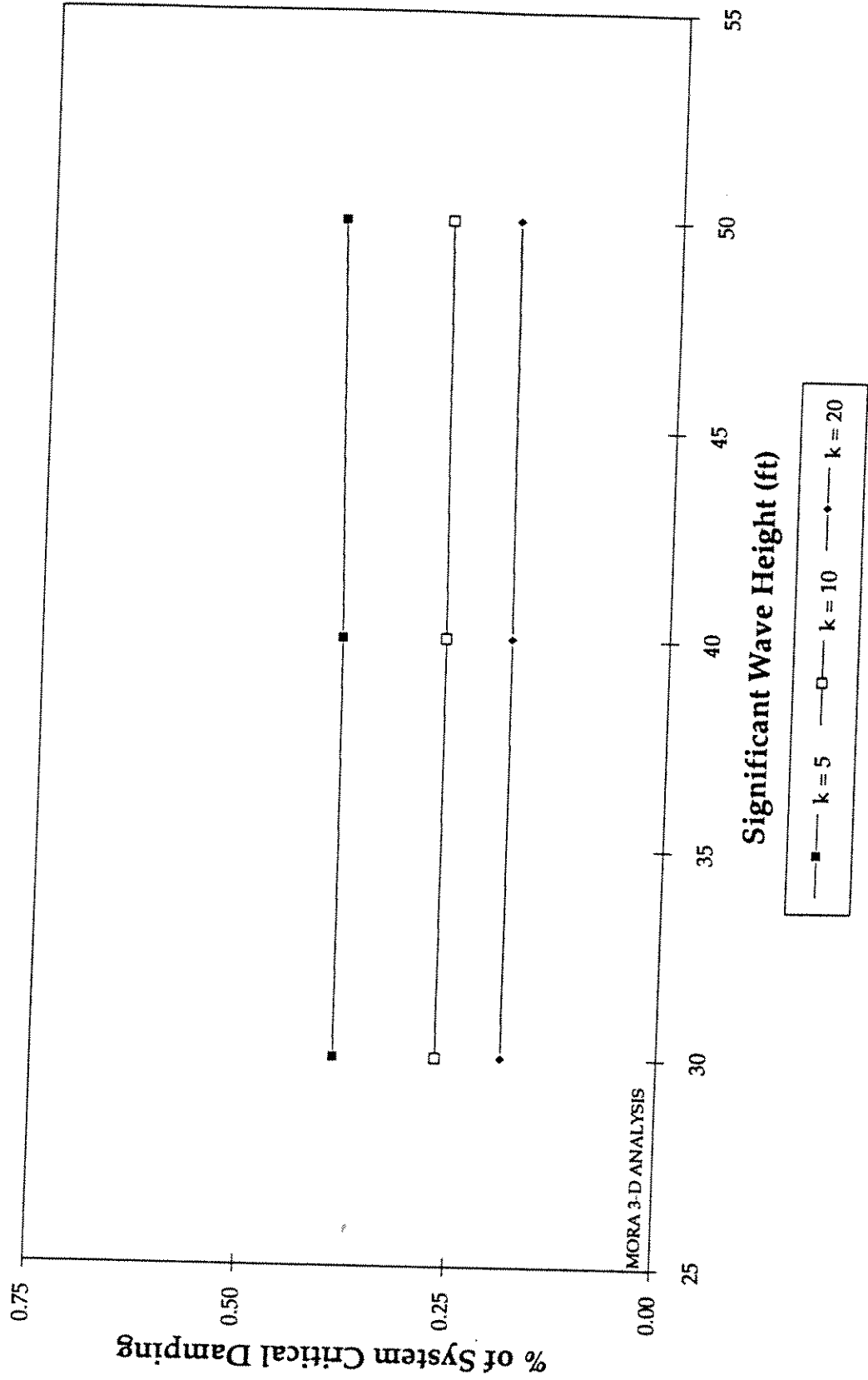
DRILL SHIP (L x B x D = 380' x 70' x 26')
LF SURGE WAVE DRIFT DAMPING
HEADING ANGLE = 30.0 DEGREES



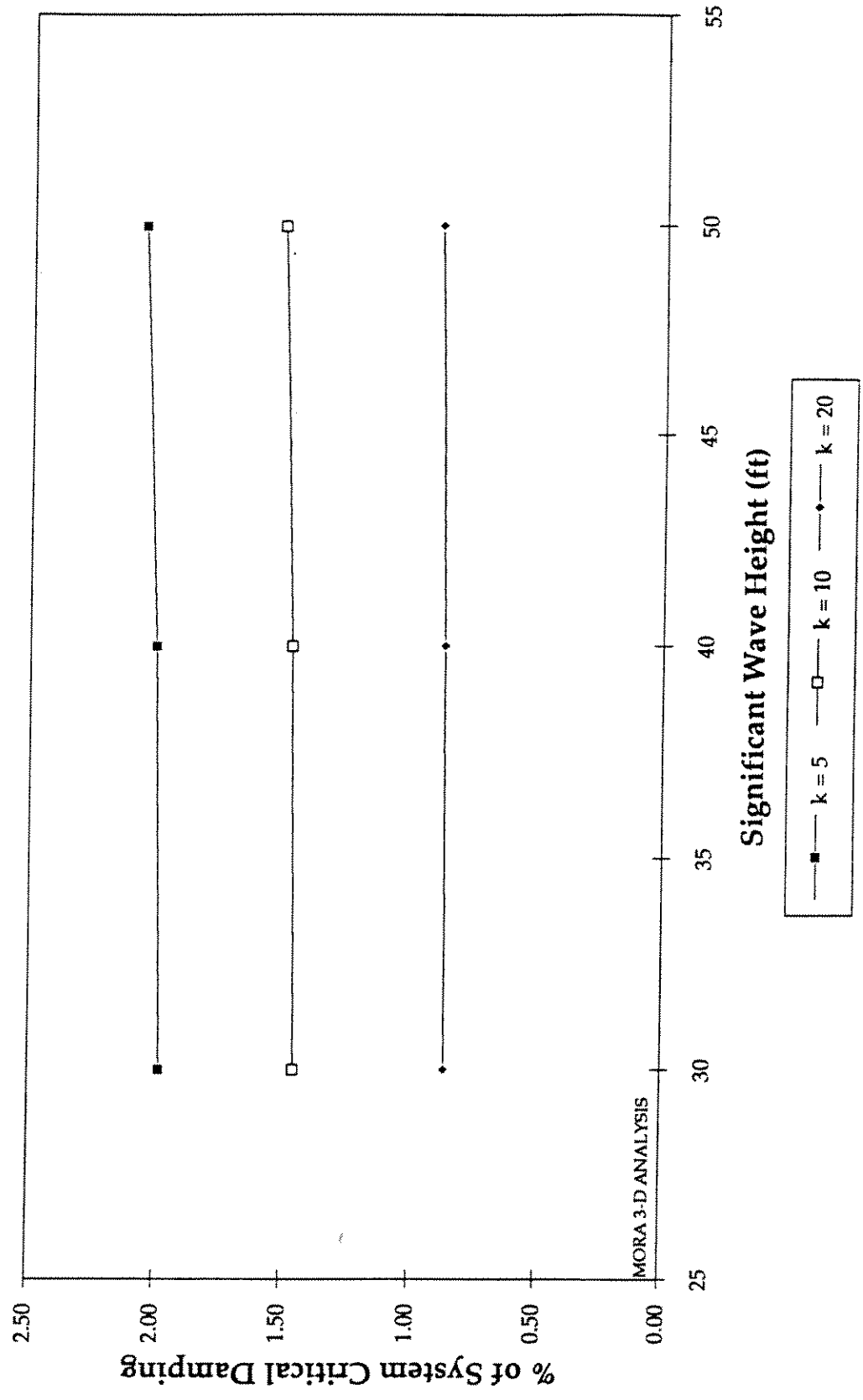
DRILL SHIP (L x B x D = 380' x 70' x 26')
LF SURGE WAVE DRIFT DAMPING
HEADING ANGLE = 60.0 DEGREES



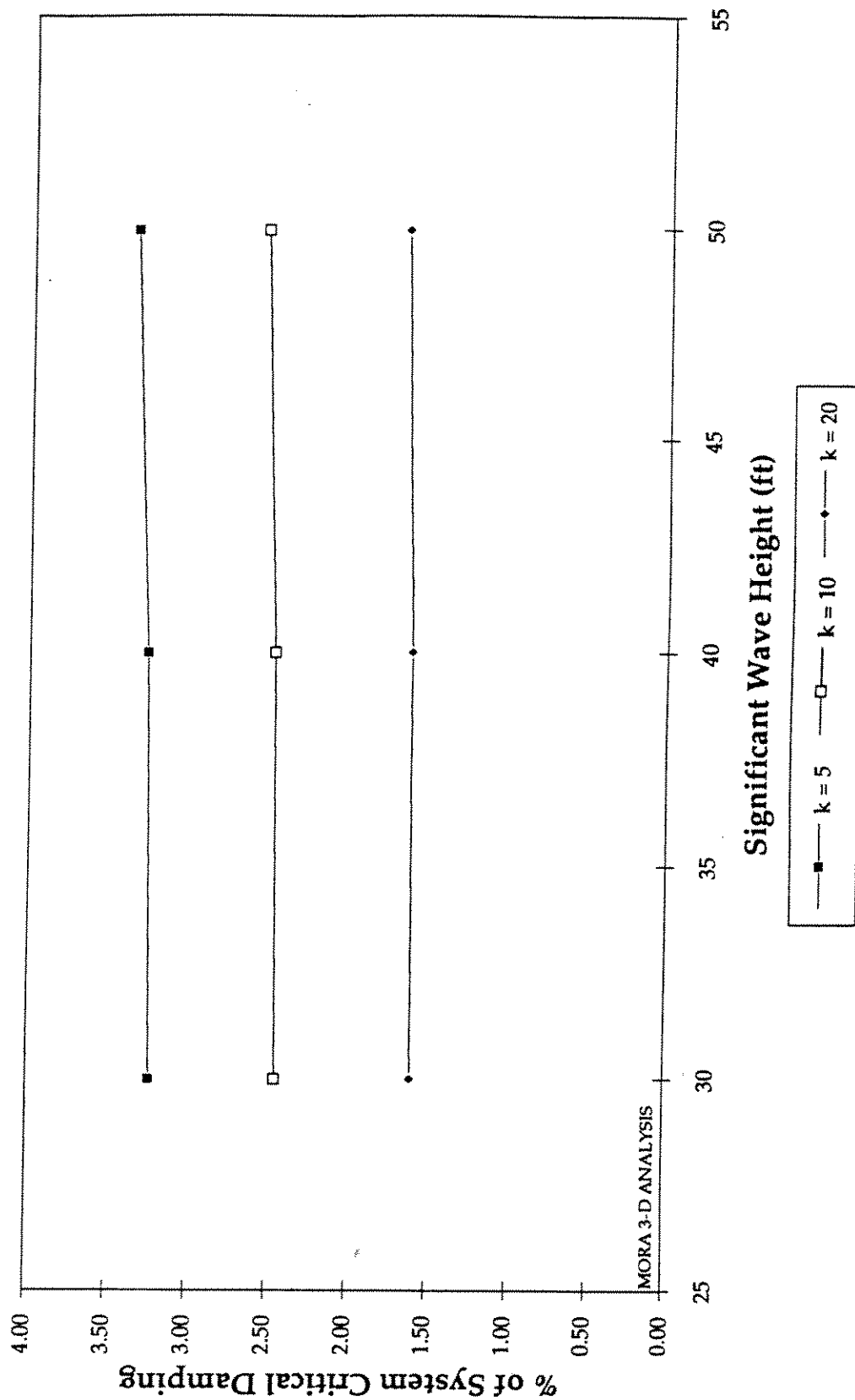
DRILL SHIP (L x B x D = 380' x 70' x 26')
LF SWAY WAVE DRIFT DAMPING
HEADING ANGLE = 30.0 DEGREES



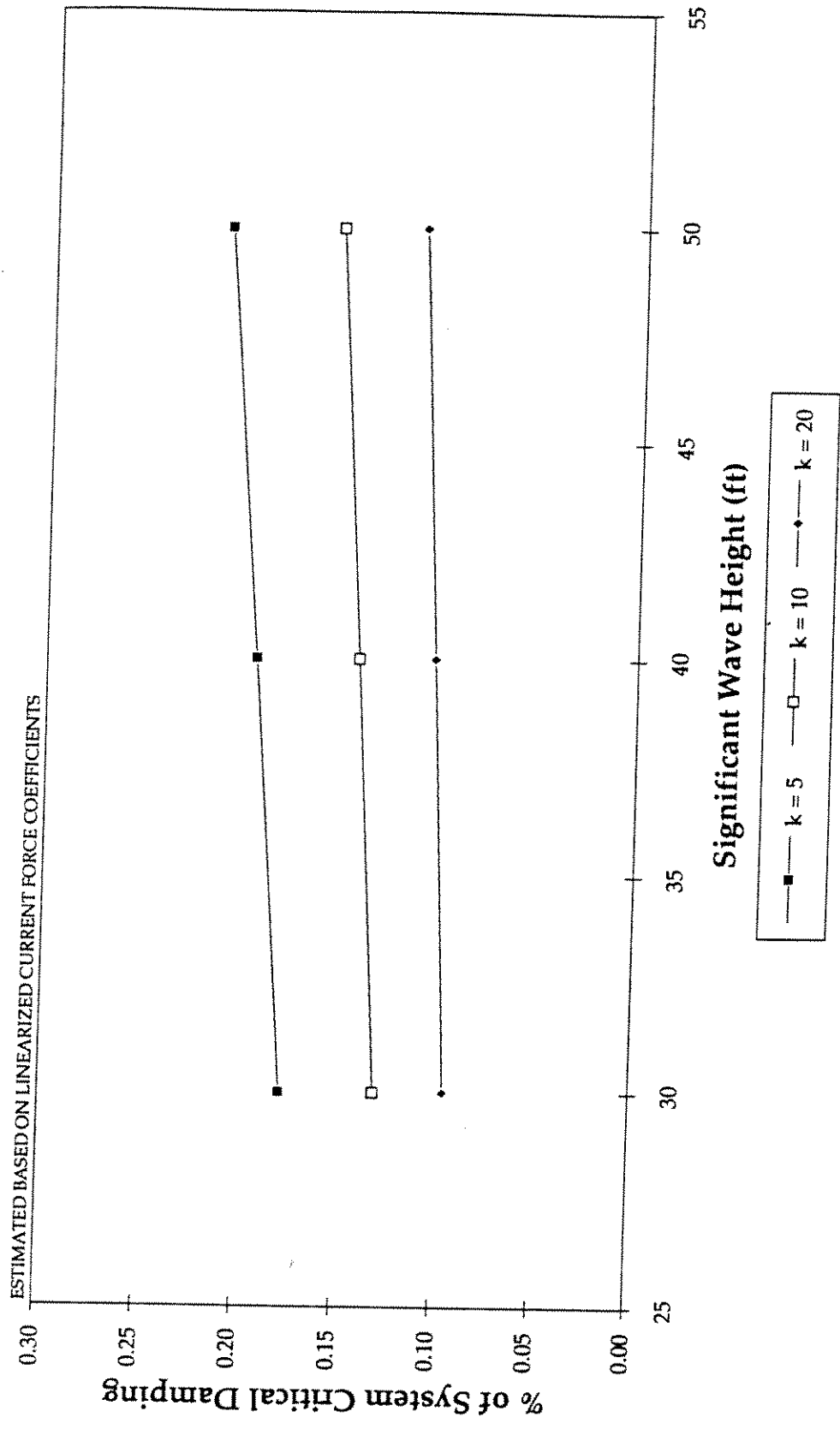
DRILL SHIP (L x B x D = 380' x 70' x 26')
LF SWAY WAVE DRIFT DAMPING
HEADING ANGLE = 60.0 DEGREES



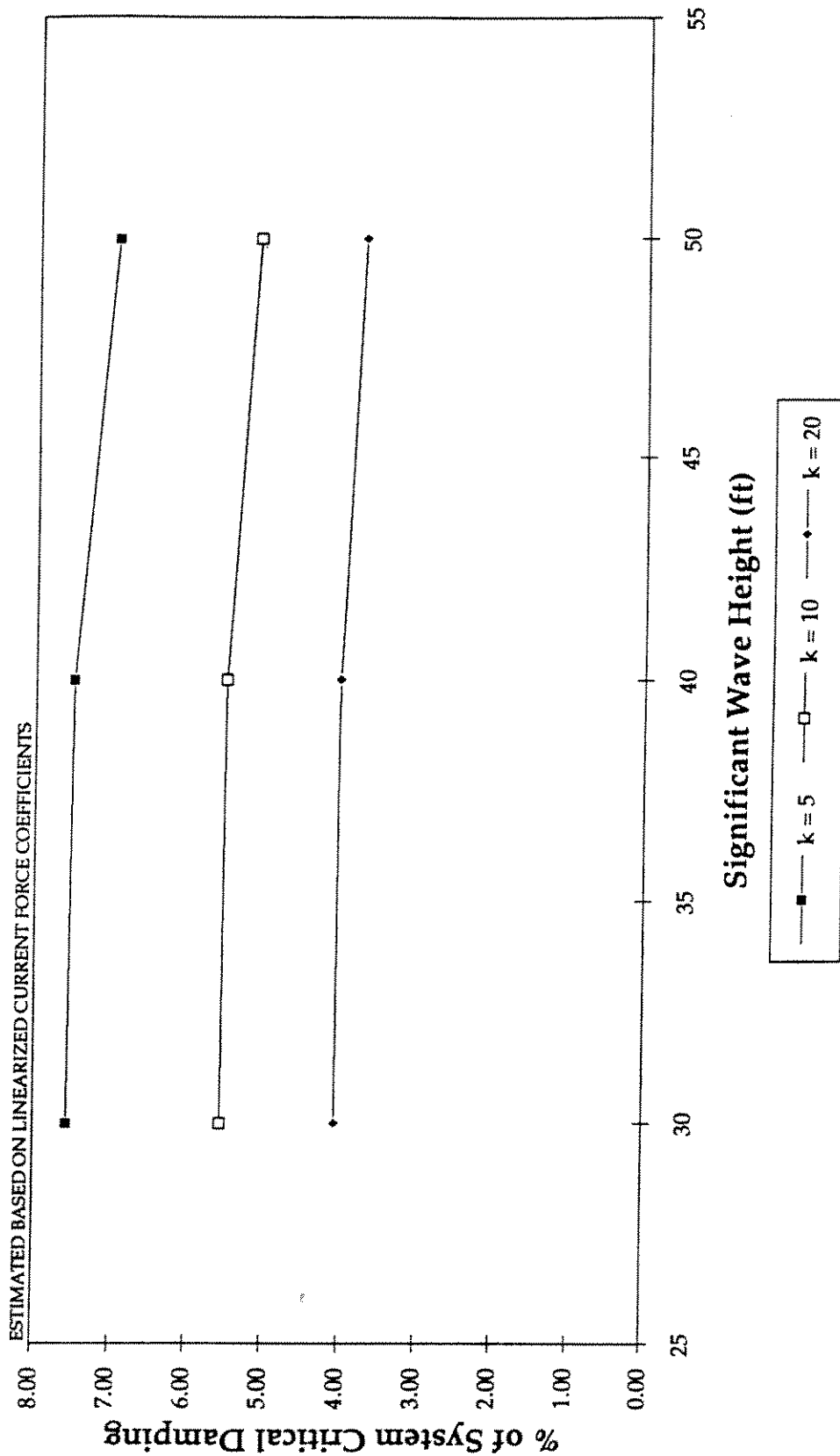
DRILL SHIP (L x B x D = 380' x 70' x 26')
LF SWAY WAVE DRIFT DAMPING
HEADING ANGLE = 90.0 DEGREES



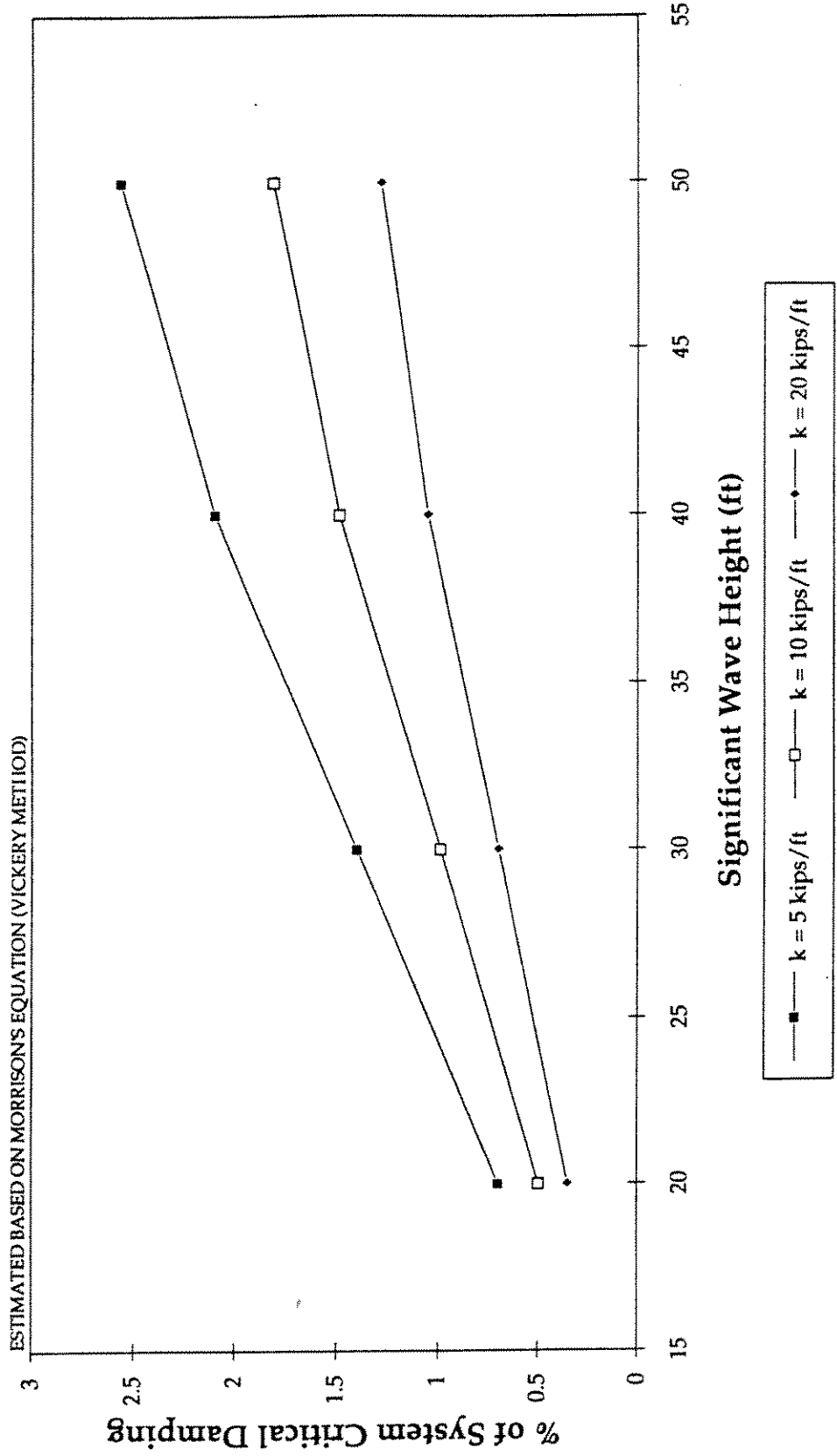
DRILL SHIP (L x B x D = 380' x 70' x 26')
LF SURGE VISCOUS DAMPING
(NO CURRENT, LF MOTION ONLY)
HEADING ANGLE = 0.0 DEGREES



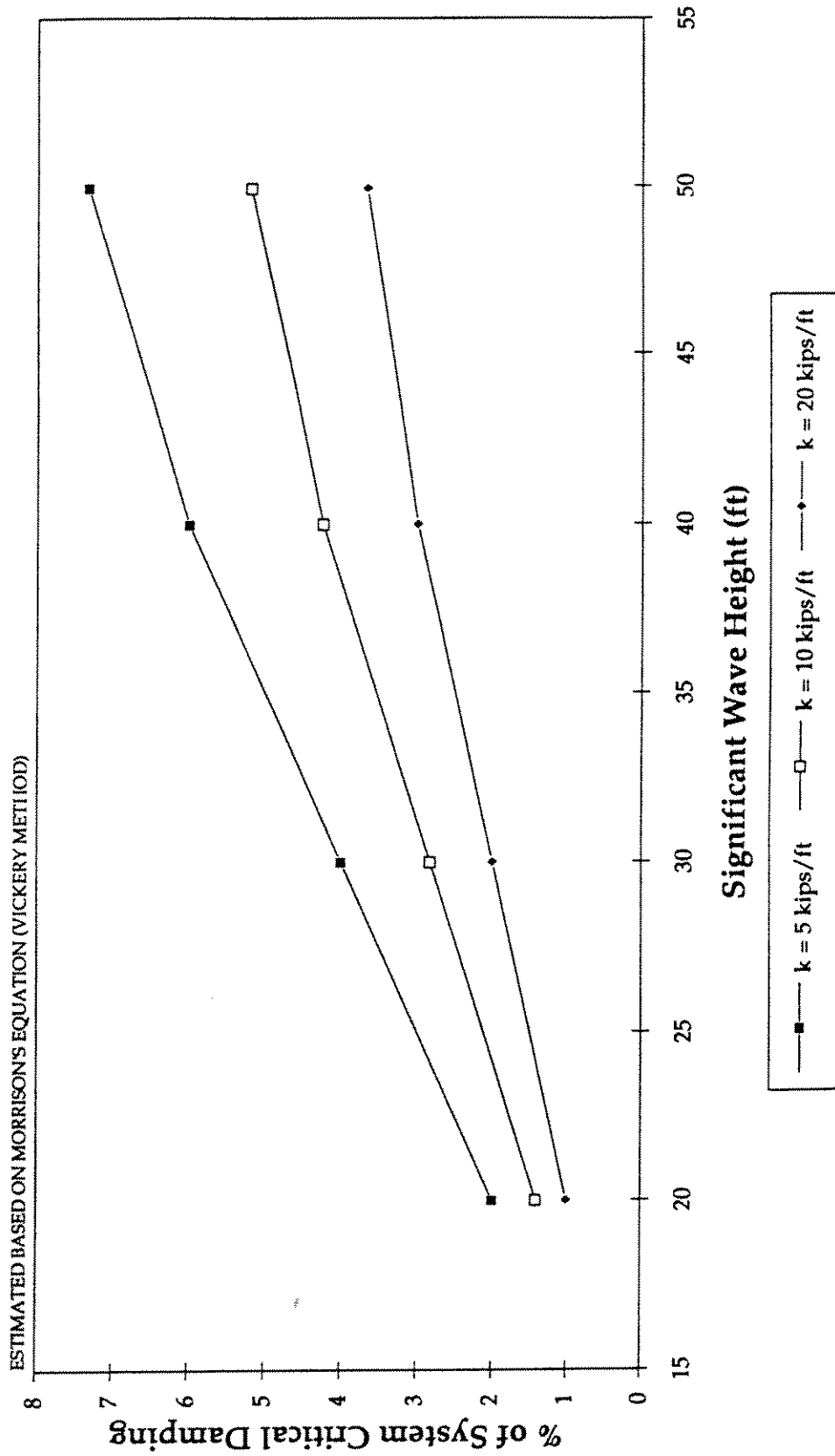
DRILL SHIP (L x B x D = 380' x 70' x 26')
LF SWAY VISCOUS DAMPING
(NO CURRENT, LF MOTION ONLY)
HEADING ANGLE = 90.0 DEGREES



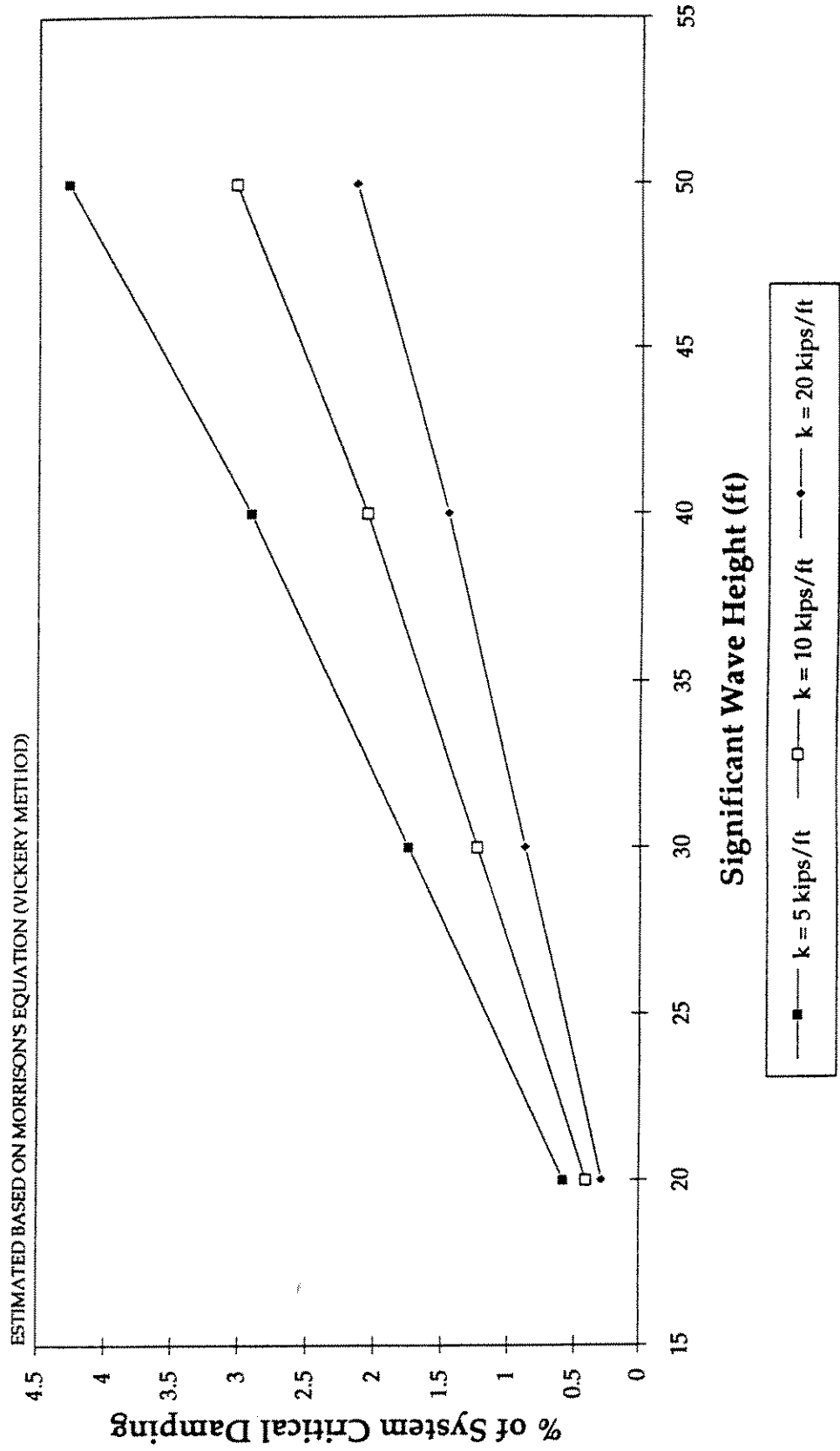
DRILL SHIP (L x B x D = 380' x 70' x 26')
LF WIND INDUCED DAMPING
(LF MOTION PLUS WIND)
HEADING ANGLE = 0.0 DEGREES



DRILL SHIP (L x B x D = 380' x 70' x 26')
LF WIND INDUCED DAMPING
(LF MOTION PLUS WIND)
HEADING ANGLE = 90.0 DEGREES



DRILL SHIP (L x B x D = 380' x 70' x 26')
LF CURRENT INDUCED DAMPING
(LF MOTION PLUS CURRENT)
HEADING ANGLE = 0.0 DEGREES



DRILL SHIP (L x B x D = 380' x 70' x 26')
LF CURRENT INDUCED DAMPING
(LF MOTION PLUS CURRENT)
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