

ORDER

8260.52

**UNITED STATES STANDARD
FOR REQUIRED NAVIGATION
PERFORMANCE (RNP) APPROACH
PROCEDURES WITH SPECIAL AIRCRAFT
AND AIRCREW AUTHORIZATION
REQUIRED (SAAAR)**



June 3, 2005

**U. S. DEPARTMENT OF TRANSPORTATION
FEDERAL AVIATION ADMINISTRATION**

FOREWORD

The increased utilization of Area Navigation (RNAV) has improved the flexibility and capability of the National Airspace System (NAS). However, current RNAV applications do not exploit the full spectrum of aircraft/navigation performance capabilities provided by the equipment of some operators. Where the use of these advanced capabilities allow for more efficient routings, a reduction to Decision Altitude (DA) of at least 50 feet, a decrease in visibility by at least $\frac{1}{4}$ mile, or lateral/vertical paths that would otherwise be unavailable, instrument approach procedures (IAP) may be constructed under the Required Navigation Performance (RNP) Special Aircraft and Aircrew Authorization Required (SAAAR) criteria contained in this document. This directive is written for the use of IAP developers. It provides the tools to construct the Obstacle Evaluation Areas (OEA) and evaluate the Obstacle Clearance Surfaces (OCS) associated with an RNP SAAAR approach procedure. This document does not discuss the rationale or philosophical basis of the criteria.

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CHAPTER 1 – GENERAL

1.0 PURPOSE.

This order contains criteria based on the mandatory avionics features for RNP certification (such as track-to-fix capability) under RTCA DO-236 (latest version). It is written for the use of approach procedure designers to develop public RNP SAAAR instrument approach procedures; describing how to construct the Obstacle Evaluation Areas (OEs) and evaluate the Obstacle Clearance Surfaces (OCSs) associated with an RNP SAAAR approach procedure. It does not discuss the rationale or philosophical basis of these criteria.

1.1 DISTRIBUTION.

This order is distributed in Washington headquarters to the branch level in the Offices of Airport Safety and Standards and Communications, Navigation, and Surveillance Systems; to Air Traffic, Airway Facilities, and Flight Standards Services; to the National Flight Procedures Office and the Regulatory Standards Division at the Mike Monroney Aeronautical Center; to branch level in the regional Flight Standards, Airway Facilities, Air Traffic, and Airports Divisions; special mailing list ZVS-827, and to special military and public addressees.

1.2 EFFECTIVE DATE. June 3, 2005.

1.3 BACKGROUND.

The concept of RNP is a significant enhancement to navigable airspace design, use, and management. It was developed by the International Civil Aviation Organization (ICAO) Special Committee on Future Air Navigation Systems (FANS) and is an integral part of the communication, navigation, surveillance, and air traffic management (CNS/ATM) plan envisioned by the Special Committee. For the purposes of this order, RNP levels address obstacle protection associated with RNP accuracy values. The RNP level (RNP x, where x=0.3, 1, 2, etc.) is a variable used to determine the OEA half-width value (in NM) of a segment of an instrument approach procedure.

1.4 DEFINITIONS.

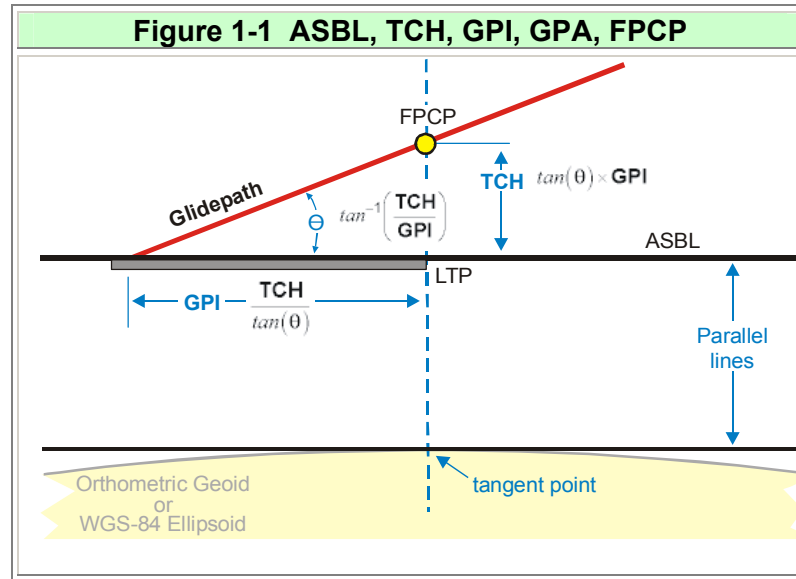
In addition to the definitions common to procedure development contained in various 8260 series orders, the following definitions apply.

1.4.1 3-Dimensional (3-D).

Approach procedures that provide longitudinal, lateral, and vertical path deviation information are 3-D procedures. Instrument landing system (ILS), microwave landing system (MLS), precision approach radar (PAR), lateral navigation/vertical navigation (LNAV/VNAV), LPV, and required navigation performance (RNP) are examples of 3-D procedures.

1.4.2 Approach Surface Baseline (ASBL).

The ASBL is a line aligned to the runway centerline (RCL) that lies in a plane parallel to a tangent to the WGS-Ellipsoid at the landing threshold point. It is used as a baseline reference for vertical measurement of the height of glidepath and OCS (see figure 1-1).



1.4.3 Course Change.

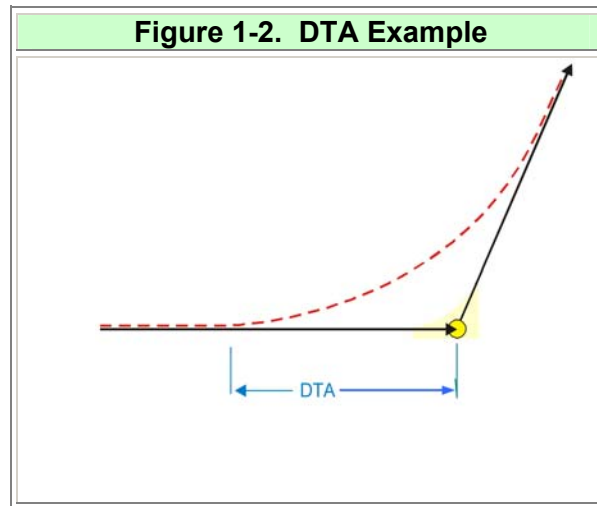
A course change is the mathematical difference between the inbound and outbound tracks at a single fix.

1.4.4 Decision Altitude (DA).

The DA is a barometric altitude (height above mean sea level) at which a missed approach must be initiated if required visual references are not acquired. The DA value is derived from the achieved height above touchdown (HAT) (see paragraph 1.4.13).

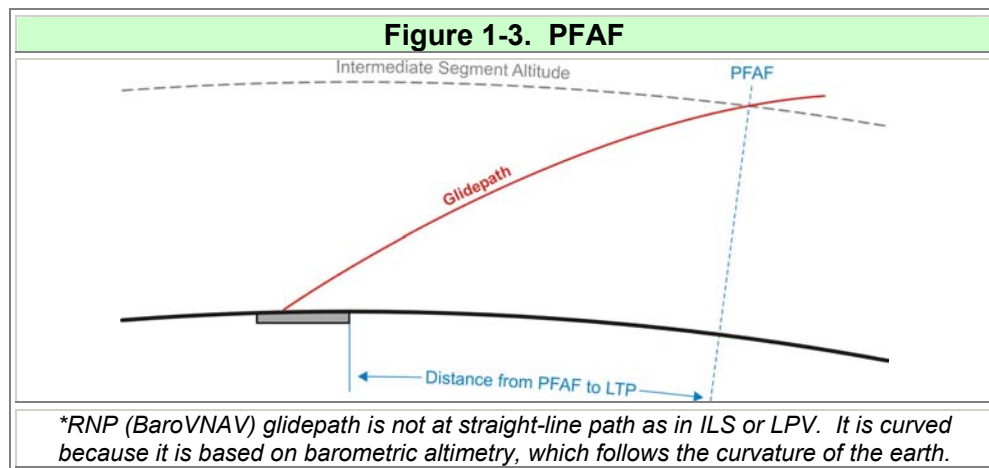
1.4.5 Distance Of Turn Anticipation (DTA).

The distance from (prior to) a fly-by fix that an aircraft is expected to start a turn to intercept the course/track of the next segment (see figure 1-2).



1.4.6 Final Approach Fix (PFAF).

An RNP final approach is 3-D. The final approach fix for all 3-D approach procedures is the point that the glidepath intercepts the intermediate segment minimum altitude (see figure 1-3).



1.4.7 Final Approach Segment (FAS).

The FAS begins at the PFAF and ends at the landing threshold point (LTP). The FAS is typically aligned with the runway centerline extended. The segment OEA is divided into the FAS OCS and the visual segment obstacle identification surface (OIS).

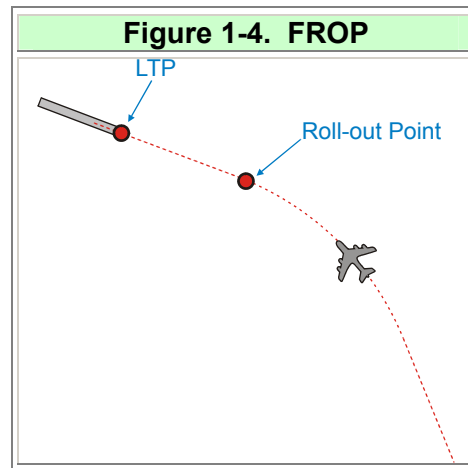
1.4.8 Flight Path Control Point (FPCP).

The FPCP is a 3-D point defined by the LTP geographic position, mean sea level (MSL) elevation, and threshold crossing height (TCH) value. The FPCP is in the vertical plane of the final approach course and is used to relate the glidepath

angle of the final approach track to the landing runway. It is sometimes referred to as the TCH point or reference datum point (RDP). See figure 1-1.

1.4.9 Final Roll-Out Point (FROP).

Where a course change is required within the FAS, the point that the aircraft rolls to a wings-level attitude aligned with the runway centerline extended is considered the FROP (see figure 1-4).



1.4.10 Geographic Positioning Navigation (GPN).

Navigation based on geodetic calculation of geographic position referenced to the WGS-84 ellipsoid. Global positioning system (GPS), wide area augmentation system (WAAS), local area augmentation system (LAAS), flight management system (FMS), RNP, and area navigation (RNAV) are examples of GPN.

1.4.11 Glidepath Angle (GPA).

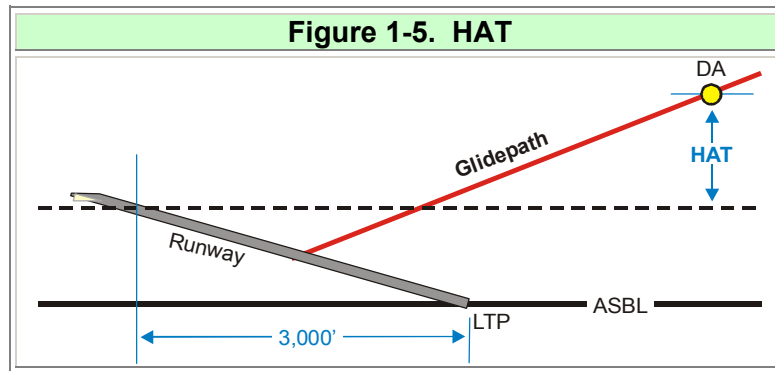
The GPA is the angle of the final approach descent path relative to the ASBL. In this document, GPA is represented in calculations as the Greek symbol theta (θ). See figure 1-1.

1.4.12 Ground Point of Intercept (GPI).

The glidepath intercepts the ASBL at the GPI. The GPI is expressed as a distance in feet from the LTP. The GPI is derived from TCH and glidepath angle values: $GPI = \frac{TCH}{\tan(\theta)}$. See figure 1-1.

1.4.13 Height Above Touchdown (HAT).

The HAT is the height of the DA above the highest point in the first 3,000 ft of the landing runway (touchdown zone elevation). See figure 1-5.



1.4.14 Landing Threshold Point (LTP).

The LTP is the point where the runway centerline (RCL) intersects the runway threshold (RWT). WGS-84/NAD-83 geographic coordinates and height above mean sea level define the LTP (see figures 1-1 and 1-5).

1.4.15 Obstacle Clearance Surface (OCS).

The OCS is an inclined surface conforming to the lateral dimensions of the obstacle evaluation area. An OCS is normally associated with evaluation of 3-D final segments or missed approach/departure climb segments.

1.4.16 Obstacle Evaluation Area (OEA).

The OEA is an area within which obstructions are evaluated by application of the ROC, OCS, or OIS to achieve appropriate vertical clearance. The OEA conforms to the lateral RNP segment width limits.

1.4.17 Obstacle Identification Surface (OIS).

The OIS is an inclined surface conforming to the lateral dimensions of the OEA used for identification of obstacles that may require mitigation to maintain the required level of safety for the applicable segment. An OIS is normally associated with the visual portion of the FAS.

1.4.18 Radius to Fix (RF) Leg.

An RF leg is a constant radius circular path about a defined turn center that terminates at a fix.

1.4.19 Required Navigation Performance (RNP).

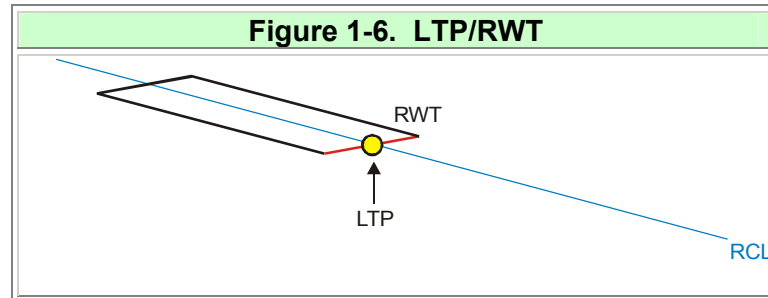
RNP is a statement of the navigational performance required to maintain flight within the OEA associated with instrument procedure segments.

1.4.20 Required Obstruction Clearance (ROC).

Sometimes referred to as required obstacle clearance, ROC is the minimum vertical clearance (in feet) that must exist between aircraft and the highest ground obstruction within the OEA of instrument procedure segments.

1.4.21 Runway Threshold (RWT).

The RWT marks the beginning of the portion of the runway usable for landing. It extends the full width of the runway (see figure 1-6).



1.4.22 Special Aircraft and Aircrew Authorization Required (SAAAR).

Aircraft may be equipped beyond the minimum standard for public RNP criteria and aircrews trained to achieve a higher level of instrument approach performance. SAAAR criteria are based on a higher level of equipment and additional aircrew requirements. Procedures that utilize SAAAR design criteria must be appropriately annotated.

1.4.23 Track to Fix (TF) Leg.

A TF leg is a geodesic path between two fixes.

1.4.24 Visual Glide Slope Indicator (VGSI).

The VGSI is an airport lighting aid that provides the pilot with a visual indication of the aircraft position relative to a specified glidepath to a touchdown point on the runway. Precision approach path indicators (PAPI) and visual approach slope indicators (VASI) are examples of VGSI systems.

1.4.25 Visual Segment.

The visual segment is the portion of the FAS OEA between the DA and the LTP.

1.4.26 Vertical Error Budget (VEB).

The VEB is a set of allowable values that contribute to the total error associated with a VNAV system. Application of equations using the VEB values determines the minimum vertical clearance that must exist between an aircraft on the nominal glidepath and ground obstructions within the OEA of instrument

procedure segments. When the VEB is used in final segment construction, its application determines the OCS origin and slope ratio.

1.5. DATA RESOLUTION.

Perform calculations using at least 0.01 unit of measure. Use calculation accuracy to at least 8 decimal places where calculation is accomplished by automated means. The following list specifies the minimum accuracy standard for documenting data expressed numerically. This standard applies to the documentation of final results only; e.g., a calculated adjusted glidepath angle of 3.04178° is documented as 3.05° . The standard does not apply to the use of variable values during calculation. Do not round intermediate results. Round the final result of calculations for documentation purposes. Use the most accurate data available for variable values.

1.5.1 Documentation Accuracy.

Document values to the following increments:

- WGS-84/NAD-83 latitudes and longitudes to the nearest one hundredth (0.01) arc second.
- LTP MSL elevation to the nearest foot,
- Glidepath angle to the next higher one hundredth (0.01) degree;
- Courses to the nearest one hundredth (0.01) degree;
- Distances to the nearest hundredth (0.01) unit; and
- Temperatures to the nearest hundredth (0.01) degree.

1.6 CALCULATION.

1.6.1 Mathematics Convention.

1.6.1 a. Definition of Mathematical Functions.

$a + b$ indicates addition

$a - b$ indicates subtraction

$a \times b$ or ab indicates multiplication

$\frac{a}{b}$ or a/b or $a \div b$ indicates division

$(a - b)$ indicates the result of the process within the parenthesis

$|a - b|$ indicates absolute value

\approx indicates approximate equality

\sqrt{a} indicates the square root of quantity "a"

a^2 indicates $a \times a$

$\tan(a)$ indicates the tangent of "a" degrees

$\tan^{-1}(a)$ indicates the arc tangent of “a”

$\sin(a)$ indicates the sine of “a” degrees

$\sin^{-1}(a)$ indicates the arc sine of “a”

$\cos(a)$ indicates the cosine of “a” degrees

$\cos^{-1}(a)$ indicates the arc cosine of “a”

1.6.1 b. Operation Precedence (Order of Operations).

First: Grouping Symbols: *parentheses, brackets, braces, fraction bars, etc.*

Second: Functions: *Tangent, sine, cosine, arcsine and other defined functions*

Third: Exponentiations: *powers and roots*

Fourth: Multiplication and Division: *products and quotients*

Fifth: Addition and Subtraction: *sums and differences*

For example:

$5 - 3 \times 2 = -1$ because multiplication takes precedence over subtraction

$(5 - 3) \times 2 = 4$ because parentheses take precedence over multiplication

$\frac{6^2}{3} = 12$ because exponentiation takes precedence over division

$\sqrt{9 + 16} = 5$ because the square root sign is a grouping symbol

$\sqrt{9} + \sqrt{16} = 7$ because roots take precedence over addition

$\frac{\sin(30^\circ)}{0.5} = 1$ because functions take precedence over division

$\sin(30^\circ / 0.5) = 0.8660254$ because parentheses take precedence over functions

NOTE: Most calculators are programmed with these rules of precedence. When possible, let the calculator maintain all of the available digits of a number in memory rather than re-entering a rounded number. For highest accuracy from a calculator, any rounding that is necessary should be done at the latest opportunity.

1.6.2 Geodetic Calculation.

Geodetic calculations must be based on the WGS-84 ellipsoid model.

1.7 DESIGN CONCEPT.

Use these criteria to develop RNP SAAAR instrument approach procedures. The following basic conditions are considered in the development of obstacle clearance criteria for RNP approach procedures: The aircraft descends and decelerates from the en route environment or a terminal transition route through the initial/intermediate approach segments to the precision final approach fix (PFAF). The aircraft arrives at the DA and continues with visual reference to a landing on the runway or initiates a missed approach. The design of the instrument procedure defines the boundaries of the airspace within which the instrument operation will be conducted. This is the airspace that will “contain”

(account for) all of the major factors influencing GPN: System accuracy, flight technical error, navigation system error, and error values that provide an acceptable level of continuity, availability, and integrity. For obstacle clearance purposes, the boundaries are specified as a nautical mile measurement perpendicular to the designed flight path. This measurement is specified as an RNP value or level. The primary OEA of RNP instrument procedures is defined as $\pm 2 \times \text{RNP}$. Table 1-1 lists RNP values applicable to specific instrument procedure segments.

Table 1-1. RNP Values			
SEGMENT	RNP VALUES		
	MAXIMUM	STANDARD	MINIMUM
Feeder	2	2	1.0
Initial	1	1	0.1
Intermediate	1	1	0.1
Final	0.5	0.3	0.1
Missed Approach	1	1	0.1*

*See paragraph 4.2.1 for limitations of missed approach segment minimum values.

1.8 APPLICABILITY.

Approach procedures developed under these criteria are published under the authority of 14 CFR Part 97.33 and identified as “Special Aircraft and Aircrew Authorization Required.” General criteria contained in the latest editions of Order 8260.3, United States Standard for Terminal Instrument Procedures (TERPS), and RNAV and RNP specific criteria contained in Order 8260.19, Flight Procedures and Airspace, apply unless modified by these criteria.

1.9 PROCEDURE IDENTIFICATION.

Title RNP procedures “**RNAV (RNP) RWY XX.**” Where more than one RNAV approach with different ground-tracks are developed to the same runway, identify each with an alphabetical suffix beginning at the end of the alphabet. Title the procedure with the lowest minimums with the “Z” suffix, etc.

Examples

RNAV (RNP) Z RWY 13L (lowest HAT: example 250 ft)
RNAV (RNP) Y RWY 13L (2nd lowest HAT: example 300 ft)
RNAV (RNP) X RWY 13L (3rd lowest HAT: example 350 ft)

1.10 PUBLISHED MINIMUMS.

RNP approach procedures are 3-dimensional approaches, lateral and vertical path deviation guidance is provided. Circling minimums are not developed.

Evaluate the final segment for an RNP value of 0.3 and a standard RNP 1.0 missed approach, and publish the resulting minimums. If the resulting HAT value is ≥ 300 or no-lights visibility ≥ 1 SM, evaluate using a FAS RNP value <0.3 but ≥ 0.10 and/or a missed approach climb gradient or reduced MAS RNP, as appropriate, to determine lowest possible HAT/no-lights visibility. If at least a 50 ft reduction in HAT or $\frac{1}{4}$ SM reduction in visibility cannot be achieved, publish only the RNP 0.3 minimums, based on RNP 1 missed approach (standard missed approach). If the required reduction in minimums is possible, in addition to the RNP 0.3 minimums based on a standard missed approach, publish the lowest possible minimums. If the difference in minimums allows interim values that differ by at least 50 ft in HAT value or $\frac{1}{4}$ SM visibility, these values may also be published if desired (4 minima lines maximum). Note that RNP values lower than 0.3 may be selected to satisfy operational needs other than reduction of minimums; examples are: to achieve track to airspace separation, track to track separation, or to allow the DA to meet criteria of distance from the FROP.

1.10.1 Minimum Safe Altitudes (MAS).

Apply the MSA criteria contained in Order 8260.3, Volume 1, paragraph 221 for RNAV procedures.

1.11 CALCULATING TRUE AIRSPEED, TURN RADIUS, AND BANK ANGLE.

1.11.1 Calculating True Airspeed.

Determine the true airspeed (K_{TAS}) for the turn using formula 1-1 and the airspeed for the highest category minimums published from table 1-2.

Formula 1-1	
$V_{KTAS} = V_{KIAS} \times [1 + (\text{altitude} \times 0.00002)]$	
Where V_{KIAS} = Indicated Airspeed altitude = Maximum segment altitude in thousands of feet	
Example	
Final Segment, CAT B, 1,500 feet $V_{KTAS} = 120 \times [1 + (1,500 \times 0.00002)] = 123.6$	

Table 1-2. Indicated Airspeed (Knots)						
Segment	Indicated Airspeed by Aircraft Category					
	Cat A	Cat B	Cat C	Cat D	Cat E**	
Initial Intermediate	150	150	240	250	250	
Final	90	120	140	165	As Specified	
Missed Approach (MA)	110	150	240	265	As Specified	
Minimum Airspeed Restriction*	Initial	110	140	210	210	As Specified
	Intermediate	110	140	180	180	As Specified
	Missed	100	130	165	185	As Specified

*Minimum speed restriction value for use to reduce turn radius. Only one speed restriction per approach segment is allowed and the fastest airspeed appropriate for the highest speed category of aircraft serviced by the approach procedure must be used to determine the speed. AFS-400 or appropriate military authority approval is required when more than one speed restriction is desired for a particular approach segment (e.g. initial, intermediate, missed approach). AFS-400 or appropriate military authority approval is also required for missed approach airspeed restrictions when used for other than obstacle/terrain avoidance requirements.

**Publish a chart note indicating the maximum CAT E airspeed.

1.11.2 Calculating Turn Radius For Fly-By Turns.

The turn radius applied at fly-by fixes is based on a standard bank angle of 18° at a true airspeed plus assumed tailwind. Locate the highest speed aircraft category that will be published on the approach procedure and use the appropriate knots indicated airspeed (V_{KIAS}) in table 1-2, using the highest altitude allowed in the turn, calculate the V_{KTAS} using formula 1-1. Obtain the highest expected altitude for feeder routes from the appropriate air traffic control facility. For initial and intermediate segments, use the minimum altitude for the fix prior to the turn fix. Use the tailwind component from table 1-3 for the highest altitude within the turn. (For turns initiated at an altitude located between values in the table, a new tailwind component may be interpolated for that turn. If an interpolated wind value is ever used below 500 ft, then the 0 ft value for wind begins with 15 kts.)

Table 1-3. Tailwind Component (V_{KTW}) For Turn Calculations		
Turn Height Above Airport	Standard Tailwind Component (Knots)*	
500	25	
1,000-2,500	Standard	AFS-400 Approval
1,000	37.5	30
1,500	50	35
2,000	50	40
2,500	50	45
3,000	50	
3,500	55	
4,000	60	
4,500	65	
5,000	70	
5,500	75	
6,000	80	
6,500	85	
7,000	90	
7,500	95	
8,000	100	
8,500	105	
9,000	110	
9,500	115	
10,000	120	
10,500	125	
≥11,000	130	

*Other Tailwind Gradients may be used after a site-specific determination of wind based on that location's meteorological history (using available information from other sources). Document source and value used on procedure form (FAA uses Form 8260-9).

Determine R using formula 1-2. Select the appropriate tailwind component in table 1-3 for the highest altitude within the turn and add the value to true airspeed.

Formula 1-2
$R = (V_{KTAS} + V_{KTW})^2 \times 0.0000449$
where V_{KTAS} = True Airspeed V_{KTW} = Tail wind component
Example
Intermediate Segment, altitude=1,500, Cat A-C Mins Published $R = (247.2 + 50)^2 \times 0.0000449 = 3.966$

1.11.2

a. Turn Radii Based On Nonstandard Bank Angles. The standard design bank angle is 18°. Lower or higher bank angles are allowed for smooth transitions, maintaining stabilized approaches, lower minima, or achieve specific leg lengths (see formula 1-3). Nonstandard bank angles must fall in the window of values listed in table 1-4.

Formula 1-3
$R = \frac{(V_{KTAS} + V_{KTW})^2 \times (1.4589 \times 10^{-5})}{\tan(\phi)}$
Where: ϕ = bank angle V_{KTAS} = See formula 1-1 V_{KTW} = Tailwind Component from table 1-3
Example
RF IF height above airport=5,000, Cat A-D mins Published bank angle = 8°
$R = \frac{(291.5 + 70)^2 \times (1.4589 \times 10^{-5})}{\tan(8)} = 13.566 \text{ NM}$

These criteria apply to construction at or below FL 190. Where turns above FL 190 are required, use a bank angle of 5°. If 5° results in a DTA value greater than 20 NM, then $R = \frac{20}{\tan(0.5 \times \text{track change in degrees})}$

1.11.3

Calculating Bank Angle Associated with a Given RF Leg Flight Track Radius.

Where RF legs are necessary, the required radius must result in a bank angle requirement within the window specified in table 1-4

Table 1-4. Bank Angle Window	
AGL Height*	Bank Angle Window (degrees)
< 500	≤ 3
≥ 500	≤ 25

*Lowest height within the RF segment

NOTE: Missed approach RF turns that are speed limited must limit bank angles to 15° maximum.

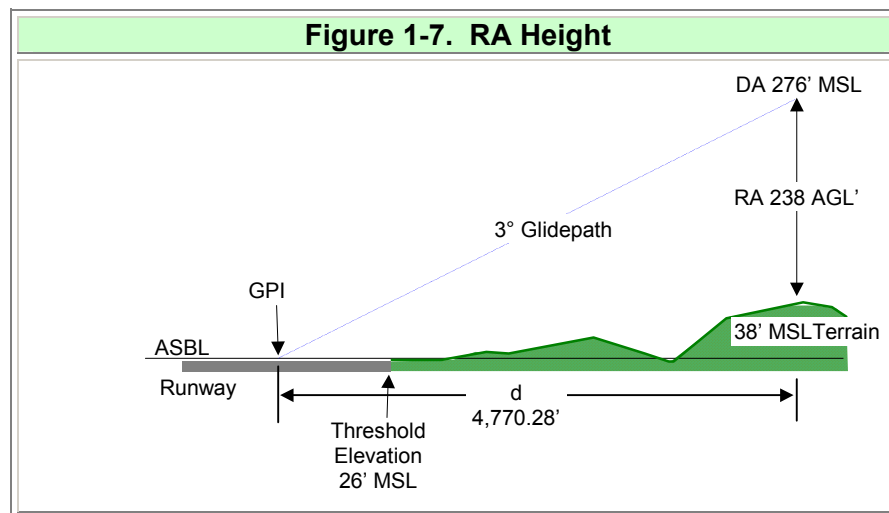
Determine the bank angle requirement associated with a given radius (R) using formula 1-4.

Formula 1-4
Formula 1-4 $\phi = \tan^{-1} \left(\frac{(V_{KTAS} + V_{KTW})^2 \times (1.4589 \times 10^{-5})}{R} \right)$

Example
CAT D aircraft, 4,000 ft, 6.7 NM Radius
$\phi = \tan^{-1} \left(\frac{(270 + 60)^2 \times 1.4589 \times 10^{-5}}{6.7} \right) = 13.34^\circ$

1.12 CALCULATION OF RADIO ALTIMETER (RA) HEIGHT.

Some aircraft bank angles are limited below 400 ft radio altitude (AGL). If any portion of the turn is expected to occur below 400 ft AGL, the Flight Control Computer (FCC – not the FMC) bank angle limitation must be considered for the LNAV mode. In these cases, use the limited bank angle in the turn calculation. Document the limited bank angle on the procedure forms (FAA uses Form 8260-9). AFS-400 (or equivalent DOD agency as appropriate) approval is required for greater bank angles in these cases. To determine RA height at any point on final, determine the distance (d) measured along the final approach course (FAC) from GPI. Obtain the terrain elevation at point (d) feet from GPI on the final course track. Subtract the terrain elevation from the on-glidepath altitude to calculate the RA (see figure 1-7). See formulas 1-5 and 1-6.



Formula 1-5

$$d = \frac{\text{Aircraft Altitude} - \text{Threshold Elev}}{\tan(\theta)}$$

Example

$$d = \frac{276 - 26}{\tan(3)} = 4,770.28'$$

Formula 1-6

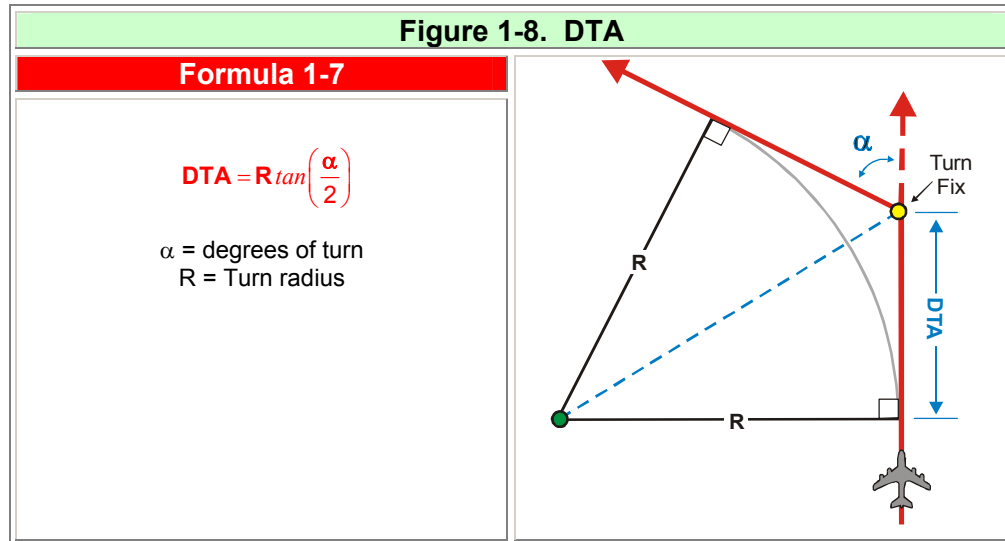
$$\text{RA} = \text{Aircraft Altitude} - \text{Terrain Elev}$$

Example

$$\text{RA} = 276 - 38 = 238$$

1.13 DTA APPLICATION.

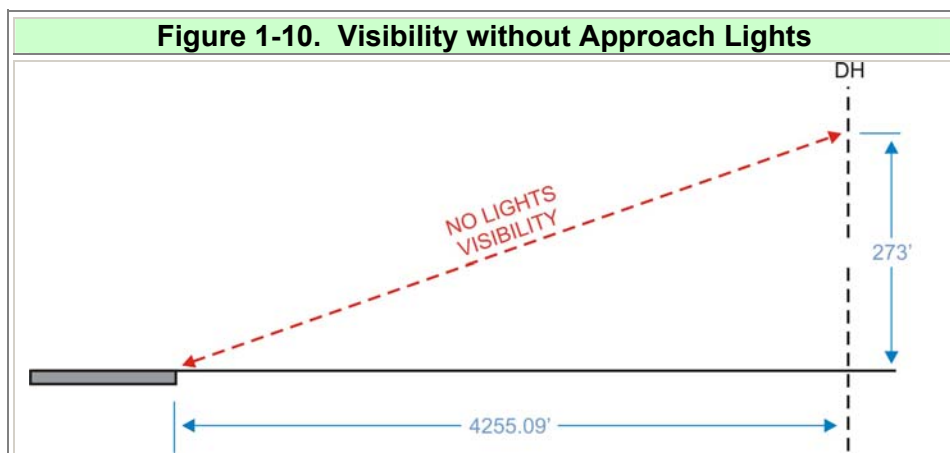
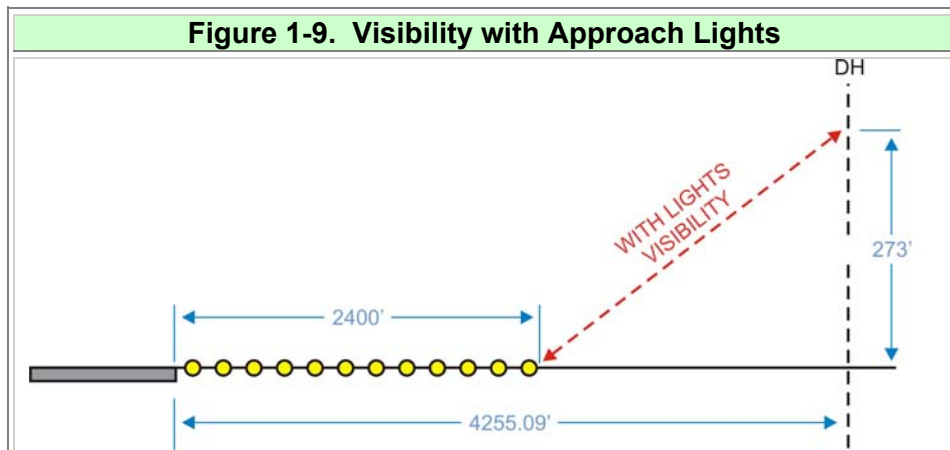
DTA is a calculated value for use in determining minimum straight segment length where a turn is required at the beginning or ending fix (see figure 1-8). See paragraph 2.3 for determination of minimum segment length. Use formula 1-7 to determine DTA for any given turn.



1.14 CALCULATION OF VISIBILITY MINIMUMS.

Calculate visibility with and without lights. Where approach lights are used to reduce visibility, publish a note containing the no-light visibility. Example note: *"Inoperative table does not apply. Visibility without lights is 1 ½ mile."* Calculate the slant distance from DA to the first light of the approach lighting system of runways served by approach lights or to the landing threshold of runways without approach lights using formula 1-8 rounded to the next higher reportable value (see figures 1-9 and 1-10).

Formula 1-8
<p>Visibility = $\sqrt{(d-l)^2 + H^2}$</p> <p>where d = distance (ft) along ASBL from LTP to DA l = length of lighting system H = DA height above threshold</p>
Example
<p>Example - w lights</p> $\sqrt{(4255.09 - 2400)^2 + 273^2} = 1875.07 \left\{ \frac{3}{8} \text{ SM} \right\}$
<p>Example - w/o lights</p> $\sqrt{4255.09^2 + 273^2} = 4263.84 \left\{ \frac{7}{8} \text{ SM} \right\}$



1.15 EVALUATION OF ACTUAL AND ASSUMED OBSTACLES (AAO).

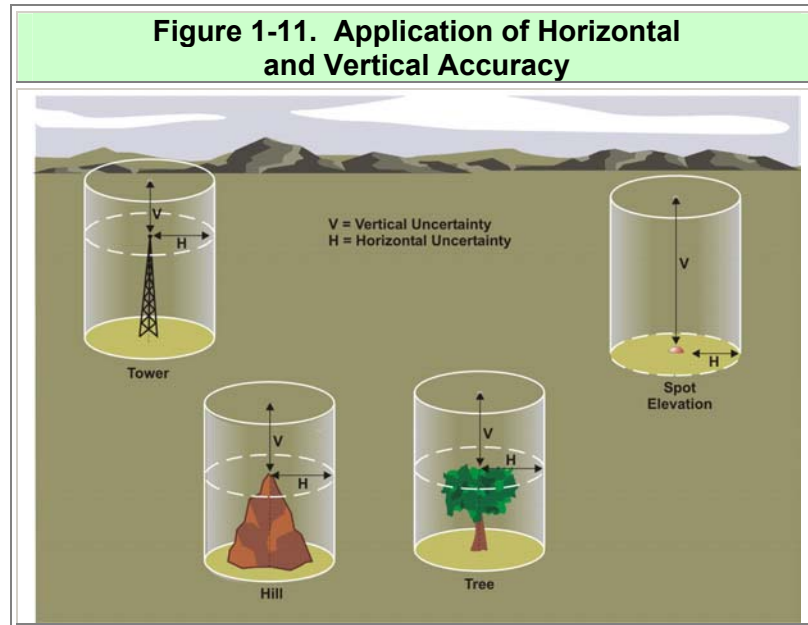
1.15.1 Accuracy Uncertainty Standards.

Apply the vertical and horizontal accuracy standards in Order 8260.19, paragraphs 272, 273, 274, and appendix 2. If specific terrain information (a site inspection, local information, or site survey, etc.) is not available, apply the following:

- The next higher contour line minus one unit of elevation; or if other terrain data formats are used (e.g. DEMs) instead of terrain contour lines, use the DEM data point value, and
- An assumed canopy height consistent with local area vegetation (since canopy height varies throughout the country, verify the height value to use with the FAA regional FPO); or
- An AAO of 199 feet above the next higher gradient line minus one unit of elevation, unless it penetrates the Part 77 surfaces for which a Part 77 survey has been performed.

1.15.2 Application of Vertical and Horizontal Accuracy Uncertainty.

Apply the obstruction vertical and horizontal accuracy code values to all obstructions. From a 3-dimensional perspective, a point described by latitude, longitude, and elevation can be evaluated as a cylinder when applying both vertical and horizontal accuracy (see figure 1-11).



1.16 INFORMATION UPDATE.

For your convenience, FAA Form 1320-19, Directive Feedback Information, is included at the end of this order to note any deficiencies found, clarifications needed, or suggested improvements regarding the contents of this order. When forwarding your comments to the originating office for consideration, please use the "Other Comments" block to provide a complete explanation of why the suggested change is necessary.

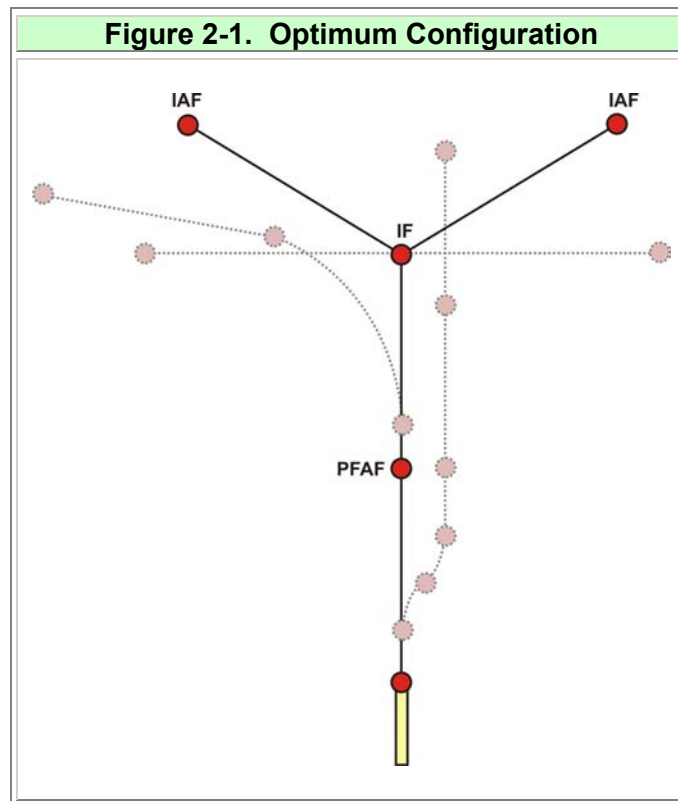
CHAPTER 2. FEEDER, INITIAL, AND INTERMEDIATE SEGMENTS

2.0 GENERAL.

Feeder, initial, and intermediate segments provide a smooth transition from the en route environment to the final approach segment. Descent to glidepath intercept and configuring the aircraft for final approach must be accomplished in these segments. Design RNP segments using the most appropriate leg type (TF or RF) to satisfy obstruction and operational requirements in feeder, initial, intermediate, final, and missed approach segments. Generally, TF legs are considered first but RF legs may be used in lieu of TF-TF turns for turn path control, procedure simplification, or improved flyability.

2.1 CONFIGURATION.

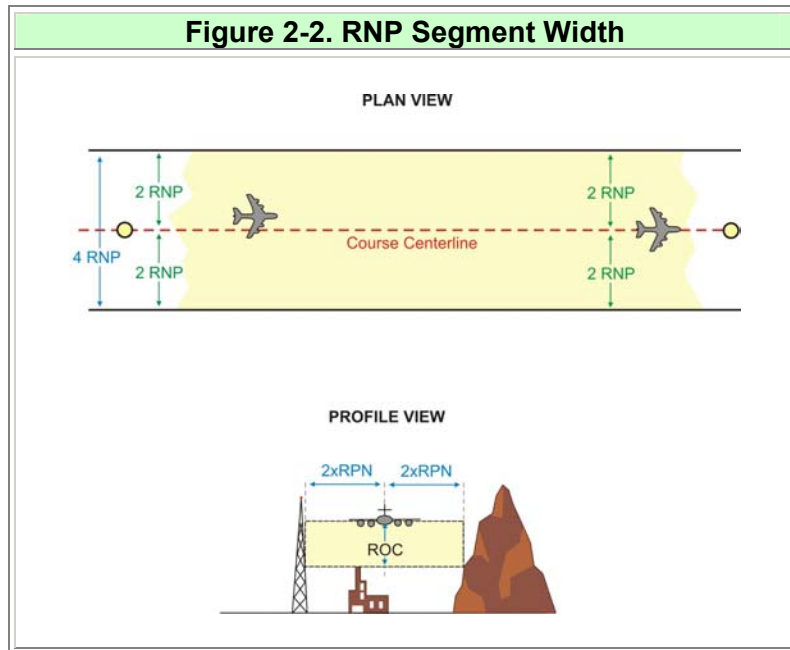
RNP navigation enables the geometry of approach procedure design to be very flexible. The “Y” configuration is preferred where obstructions and air traffic flow allow. The approach design should provide the least complex configuration possible to achieve the desired minimums. See figure 2-1 for examples. Fly-by turns at the PFAF are limited to a maximum of 15°.



2.2 RNP SEGMENT WIDTH.

RNP values are specified in increments of a hundredth (0.01) of a NM. Segment width is defined as $4 \times \text{RNP}$; segment half-width (semi-width) is defined as $2 \times \text{RNP}$

(see figure 2-2). Standard **RNP** values for instrument procedures are listed in table 1-1.



Apply the standard **RNP** values listed in table 2-1 unless a lower value is required to achieve the required ground track or lowest minimums. The lowest RNP values are listed in the “MINIMUM” column of table 2-1.

2.3 RNP SEGMENT LENGTH.

Design segments with sufficient length to accommodate the required descent as close to the OPTIMUM gradient as possible and DTA (see paragraph 1.13) where turns are required. Minimum straight segment (any segment) length is **2xRNP (+DTA as appropriate for fly-by turn constructions)**. Paragraph 2.8 applies where RNP changes occur (RNP value changes 1 RNP prior to fix). The maximum initial segment length (total of all sub segments) is 50 NM.

2.4 RNP SEGMENT DESCENT GRADIENT.

Design instrument approach procedure segments to provide descent at the standard gradient. Where necessary to achieve obstacle clearance, descent gradient may be increased. Table 2-1 lists the standard and maximum allowable descent gradients.

Table 2-1. Descent Gradient Constraints		
SEGMENT	DESCENT GRADIENT (FT/NM)	
	STANDARD	MAXIMUM
Feeder	250	500
Initial	250 **800	500 **1000
Intermediate	≤ 150	Equal to Final Segment Gradient*
Final	318	See Table 3-1

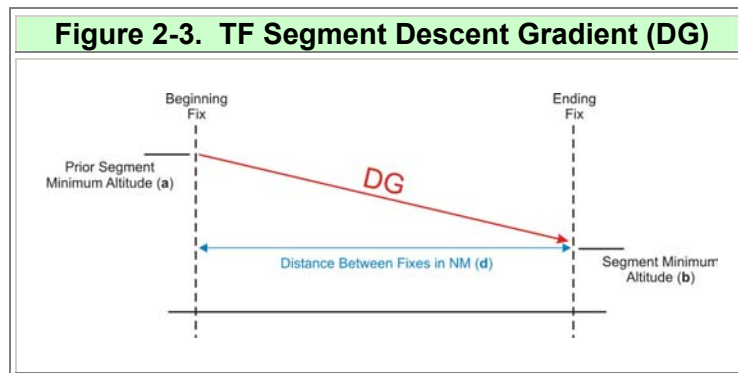
* If a higher than standard gradient is required, a prior segment must provide a gradient to allow the aircraft to configure for final segment descent.

** DoD Only

2.4.1 Descent Gradient Calculation.

2.4.1 a. TF Segments.

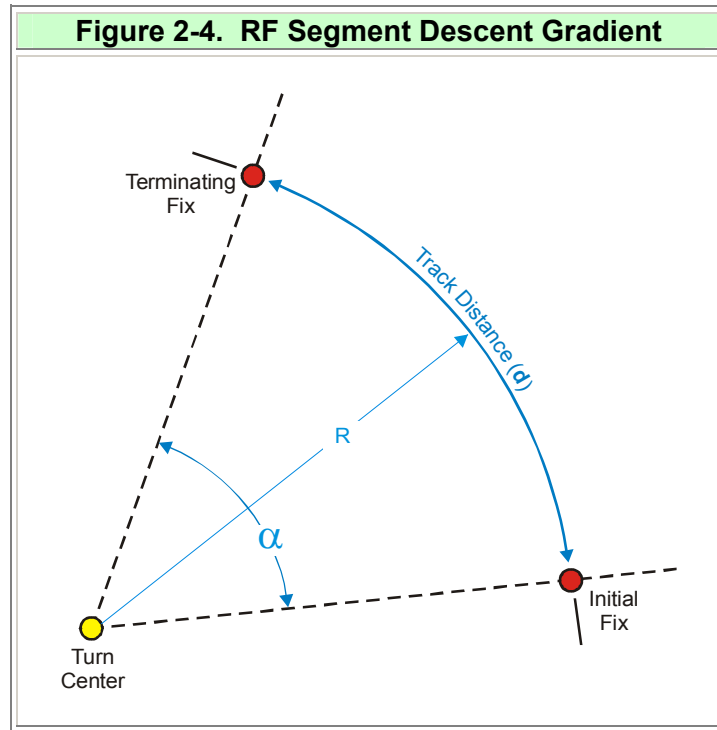
See figure 2-3, and calculate the descent gradient using formula 2-1.



Formula 2-1
$DG = \frac{a - b}{d}$
<p>where a=minimum altitude at beginning fix b=minimum altitude at ending fix d=distance (NM) between fixes</p>
Example
<p>Example: a=4,500 b=3,600 d=5.77</p> $DG = \frac{4,500 - 3,600}{5.77} = 155.98$

2.4.2 RF Segment.

See figure 2-4, and calculate the descent gradient using formula 2-1 where **d** is calculated using formula 2-2.



Formula 2-2

$$d = \frac{\alpha \times R \times \pi}{180}$$

where α = degrees of arc

R = turn radius

Example

$$\alpha = 55^\circ \quad R = 6.0$$

$$d = \frac{55 \times 6.0 \times \pi}{180} = 5.76$$

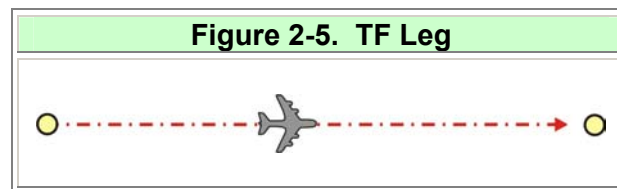
2.5 RNP SEGMENT ROC.

Minimum ROC requirements are listed by segment type in table 2-2.

Table 2-2. Minimum ROC Values	
Segment	ROC Value
Feeder	2000/1000
Initial	1000
Intermediate	500 or VEB Value
Final	VEB

2.6 TF LEG SEGMENT.

A TF leg is a geodesic flight path between two fixes. The first fix is either the previous leg termination fix or the initial (first) fix of a TF leg (see figure 2-5).



2.6.1 OEA Construction of Turns at Fly-By Waypoints that Join Two TF Legs.

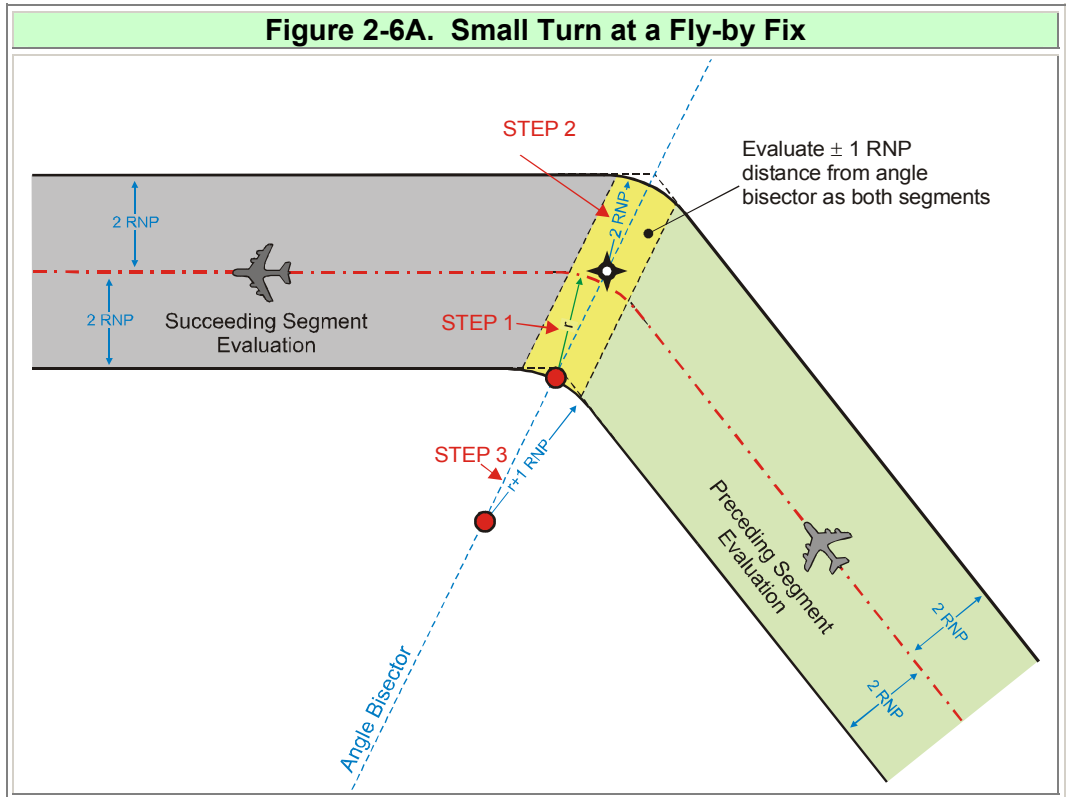
This construction is the standard for fly-by turn construction. Limit turns at a fly-by fix to a maximum of 70° where aircraft are expected to cross (fly-by) the fix at altitudes above FL 190, 120° at and below FL 190. When obstructions prevent use of this construction, consider using an RF leg construction to accomplish the course change (see paragraph 2.7). Construct fly-by turning OEAs using the following steps:

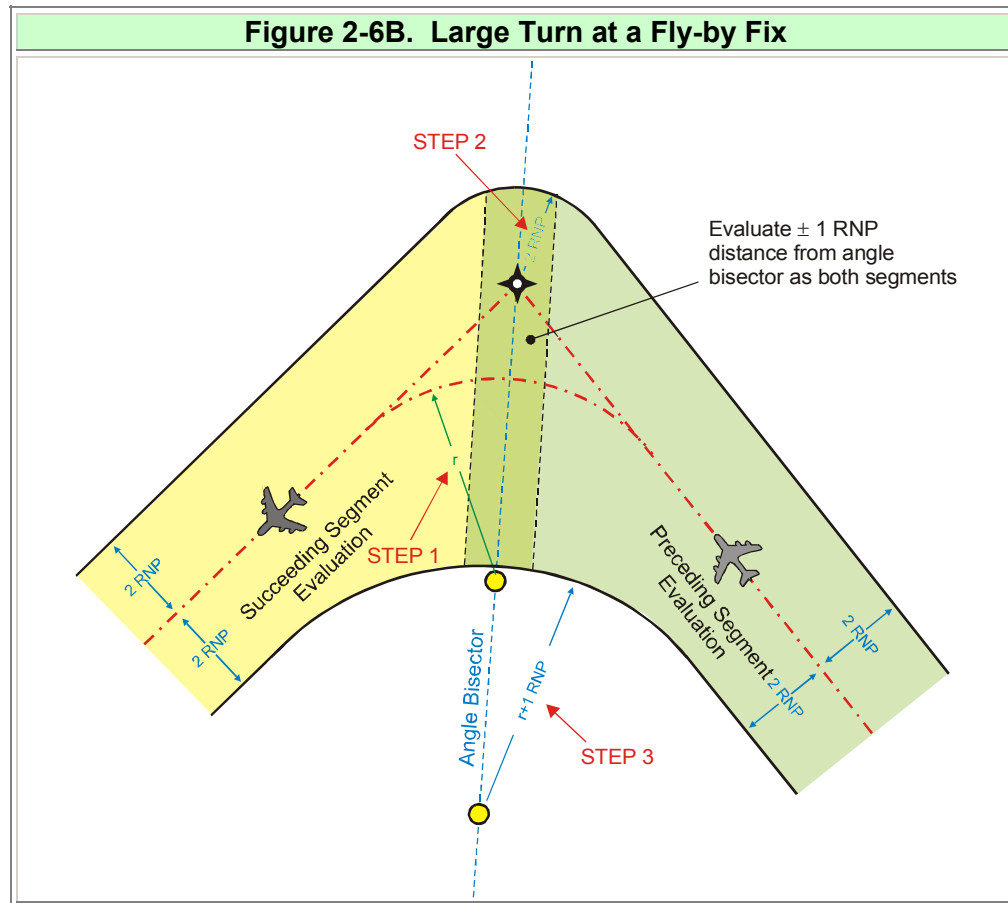
STEP 1: Construct the turning flight path. Determine the turn radius (R) as described in paragraph 1.11.2 (formula 1-2). Placing the origin on the angle bisector line, scribe an arc of radius R tangent to the inbound and outbound legs (see figure 2-4).

STEP 2: Construct the outer OEA boundary line. Using the turn fix as the origin, scribe an arc of radius $2 \cdot \text{RNP}$ tangent to the inbound (or preceding) and outbound (or succeeding) TF legs.

STEP 3: Construct inner turn expansion boundary line. Placing the origin on the angle bisector line, scribe an arc of radius $R + 1 \cdot \text{RNP}$ from the tangent point on the inbound (or preceding) leg inner boundary to the tangent point on the outbound (or succeeding) leg inner boundary.

The evaluation for the succeeding segment begins 1 RNP from the turn fix (example in figure 2-6A) or the angle bisector line (example in figure 2-6B), whichever is encountered first.





2.7

RF LEG SEGMENT.

An RF leg may be designed to accommodate a course change where obstructions prevent the design of a fly-by turn at a fix, or to accommodate other operational requirements. RF legs are used to control the ground track of a turn. The curved leg begins tangent to the previous segment course at its terminating fix and ends tangent to the follow-on course at its beginning fix (see figure 2-7). OEA construction limits turn radius to $\geq 2 \times \text{RNP}$. The obstruction evaluation area boundaries are parallel arcs.

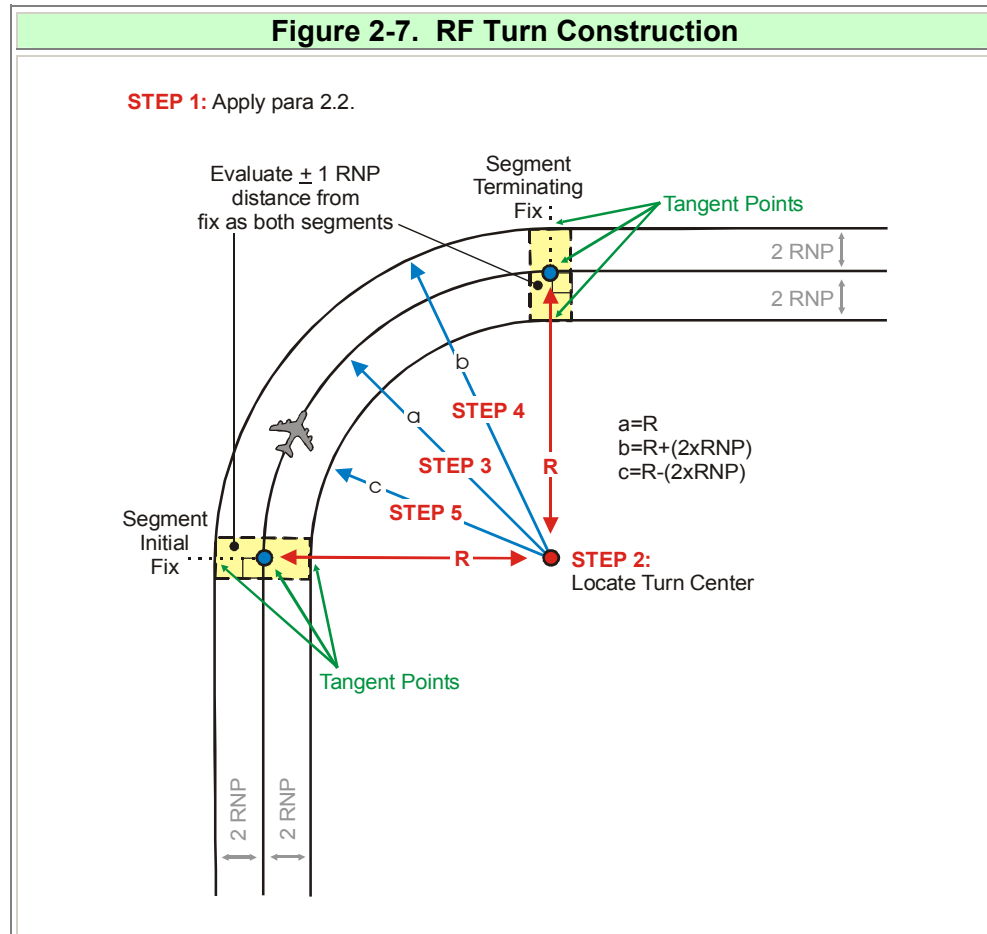
STEP 1. Determine the turn radius (**R**) necessary to avoid obstructions. Apply paragraph 1.11.3 to verify the bank angle associated with **R** is within the table 1-4 specified values.

STEP 2. Locate the turn center at a perpendicular distance “**R**” from the preceding and following segments.

STEP 3. Construct flight path. Scribe an arc of radius “**R**” from the tangent point on the preceding course to the tangent point on the following course.

STEP 4. Construct outer OEA boundary. Scribe an arc of radius $R+2\cdot\text{RNP}$ from the tangent point on the preceding segment outer boundary to the tangent point on the following course outer boundary.

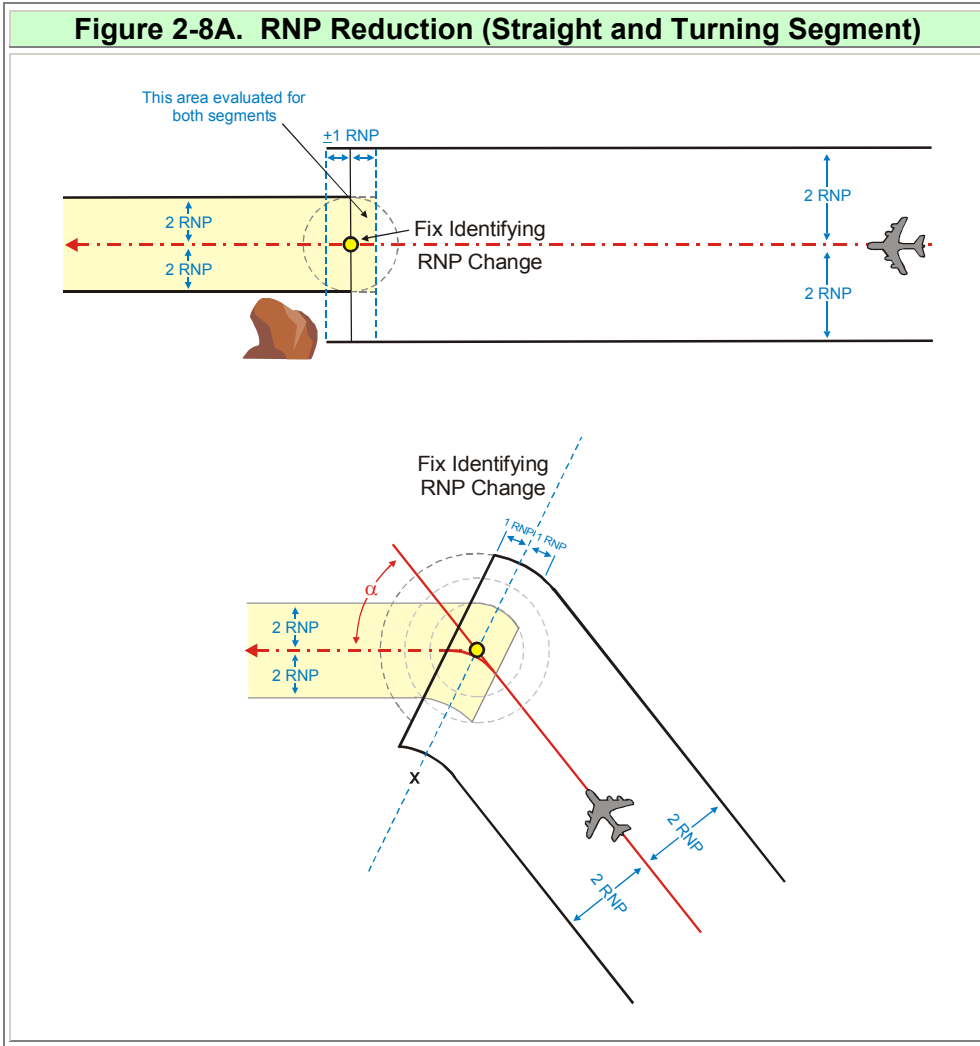
STEP 5. Construct inner OEA boundary. Scribe an arc of radius $R-2\cdot\text{RNP}$ from the tangent point on the preceding segment inner boundary to the tangent point on the following course inner boundary.

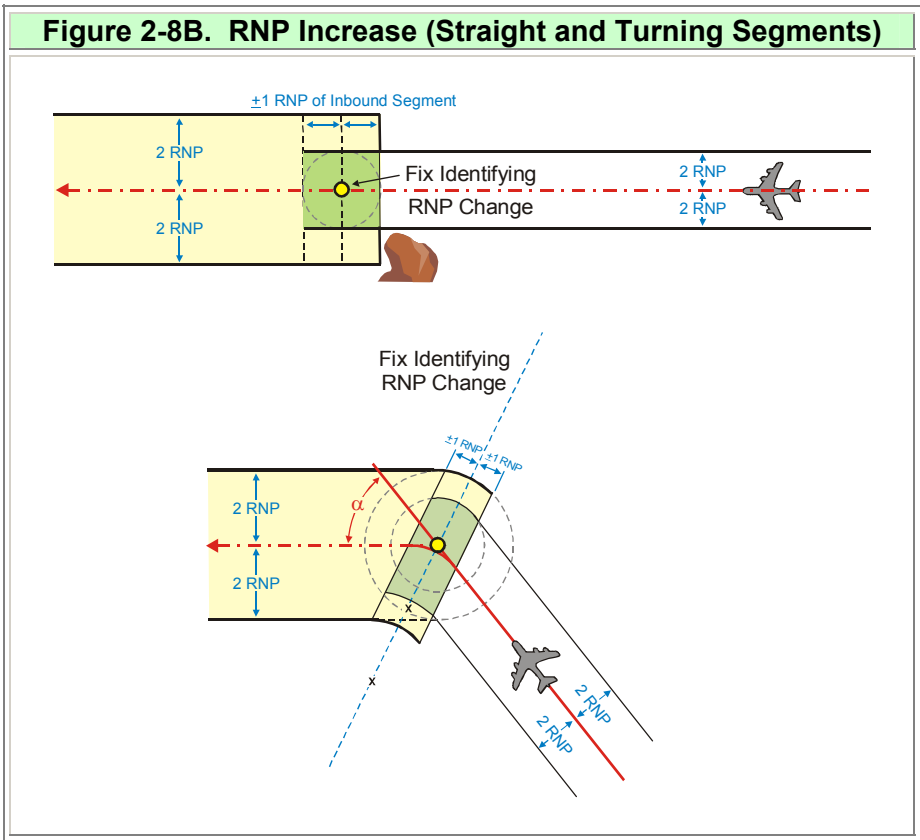


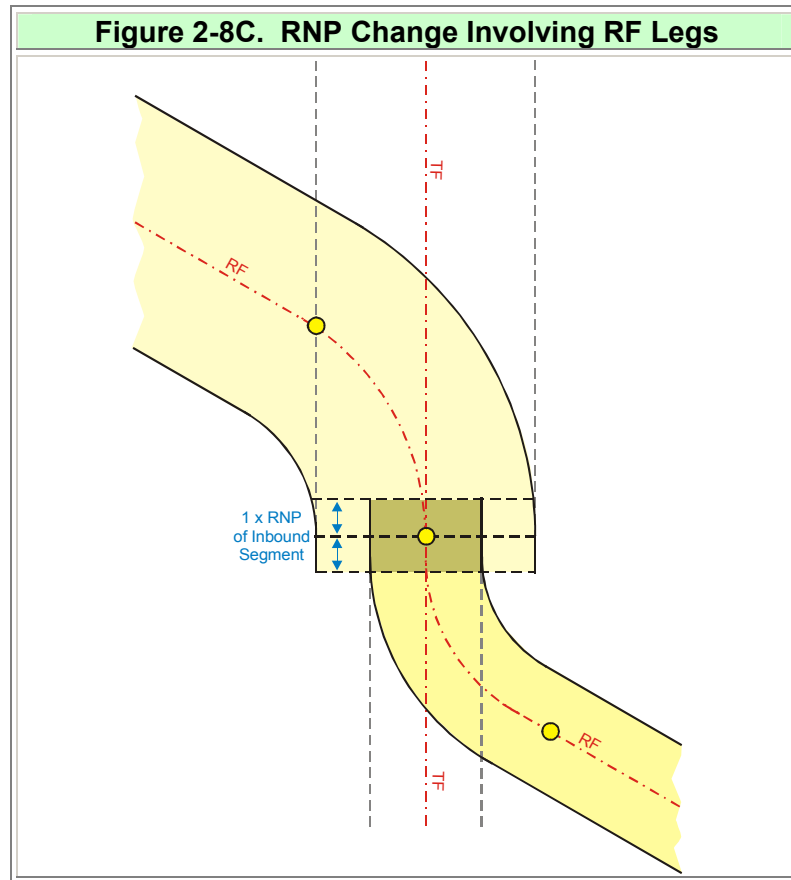
2.8 CHANGING SEGMENT WIDTH (RNP VALUES).

Changes in RNP values must occur at a fix. The aircraft avionics transition to the new RNP value no later than reaching the fix marking the value change. Therefore, the area within ± 1 RNP of the fix must be evaluated for both segments. RNP reduction is illustrated in figure 2-8A, RNP increase is illustrated in figure 2-8B, and RNP changes involving RF legs are illustrated in figure 2-8C.

NOTE: RNP reductions are not allowed on final after passing the PFAF or in segments where the VEB is applied.



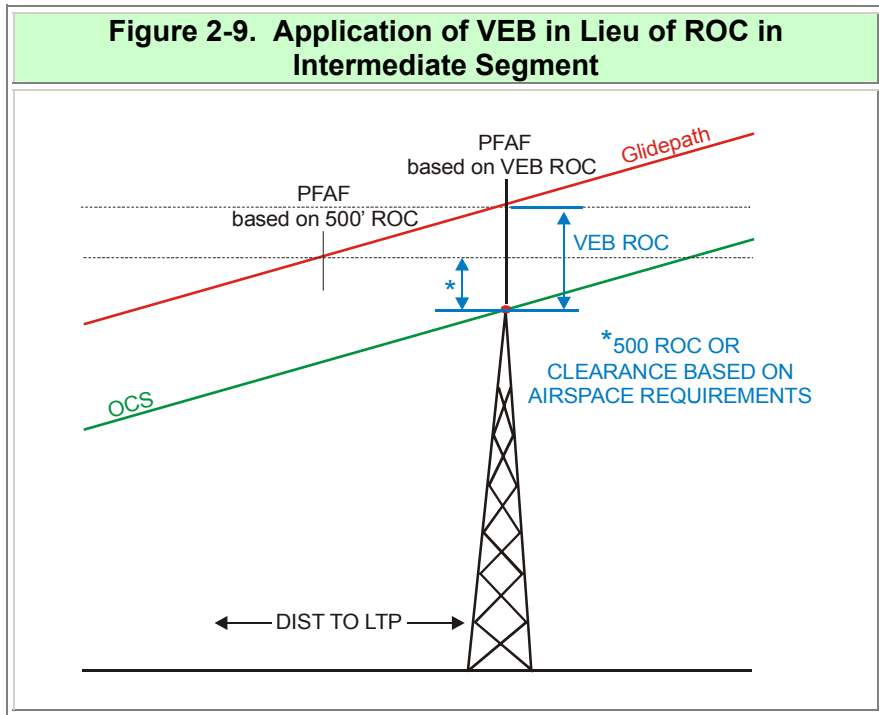




2.9

EFFECTS OF COLD TEMPERATURE IN THE INTERMEDIATE SEGMENT.

When establishing the intermediate segment minimum altitude (glidepath intercept altitude), compare the difference between the 500-ft intermediate ROC value and the ROC value provided by the VEB OCS if extended to the controlling obstacle along track distance from LTP. If the VEB ROC value exceeds 500, apply this ROC value in lieu of 500 ft in the intermediate segment (see figure 2-9). Applying VEB ROC will raise the intermediate segment altitude. Where this application yields PFAF to LTP distances greater than 7.5 NM, Flight Technologies and Procedures Division, AFS-400, approval is required.



CHAPTER 3. FINAL APPROACH SEGMENT (FAS)

3.0 GENERAL.

RNP approaches are 3-D procedures; the final segment provides the pilot with final segment vertical and lateral path deviation information based on Baro VNAV systems. Therefore, RNP procedures may not be developed for locations with full time remote altimeter or where the final segment overlies precipitous terrain. The glidepath qualification surface (GQS) described in Order 8260.3, Volume 3, paragraph 2.12 must be clear in order to publish a 3-D procedure to the runway (for procedures with an RF turn in the final segment, the GQS terminates at the DA or FROP, whichever is closer to LTP). The final approach segment OCS is based on limiting the vertical error performance of Baro VNAV avionics systems to stated limits. Minimum and maximum temperature limitations are specified on the approach chart for aircraft that do not have temperature-compensating systems. The minimum height above touchdown (HAT) value is 250 ft.

3.1 FINAL SEGMENT RNP VALUES.

Evaluate the final segment for an RNP value of 0.3. If the resulting HAT value is ≥ 300 or no-lights visibility ≥ 1 SM, evaluate using an RNP value <0.3 but ≥ 0.10 to determine the largest RNP value that will yield the lowest possible HAT/no-lights visibility. If at least a 50 ft reduction in HAT or $\frac{1}{4}$ SM reduction in visibility cannot be achieved, publish only the RNP 0.3 minimums. See related paragraph 1.10.

3.2 GLIDEPATH ANGLE AND TCH REQUIREMENTS.

The OPTIMUM (design standard) glidepath angle is 3° . Lower angles require Flight Standards approval. Glidepath angles higher than 3° are authorized only where obstacles prevent use of 3° or minimum temperature limitations restrict approach availability when the approach is operationally needed. Table 3-1 lists the highest allowable glidepath angle by aircraft category. If the required glidepath angle is greater than the maximum for an aircraft category, do not publish minimums for the category. Table 3-2 lists standard threshold crossing height (TCH) values and recommended ranges of values appropriate for cockpit-to-wheel height groups 1 through 4. Three-dimensional (3-D) procedures serving the same runway should share common TCH and glidepath angle values. If an instrument landing system (ILS) serves the runway, use the ILS TCH and glidepath angle values. If there is no ILS but a visual glide slope indicator (VGSi) system with a suitable TCH and glidepath angle serves the runway, use the VGSi TCH and glidepath angle. Otherwise, select an appropriate TCH value from table 3-2, and **3° glidepath angle**.

Table 3-1. Maximum Glidepath Angle (θ)			
Category	θ	Gradient	
		FT/NM	%
A (80 knots or less)	6.4	682	11.22
A (81-90 knots)	5.7	606	9.98
B	4.2	446	7.34
C	3.6	382	6.29
D&E	3.1	329	5.42

Table 3-2. TCH Requirements			
Representative Aircraft Type	Approximate Glidepath-to-Wheel Height	Recommended TCH \pm 5 Feet	Remarks
<u>HEIGHT GROUP 1</u> General aviation, Small commuters, Corporate turbojets, T-37, T-38, C-12, C-20, C-21, T-1, Fighter Jets	10 Feet or less	40 Feet	Many runways less than 6,000 ft long with reduced widths and/or restricted weight bearing which would normally prohibit landings by larger aircraft.
<u>HEIGHT GROUP 2</u> F-28, CV-340/440/580, B-737, C-9, DC-9, C-130, T-43, B-2, S-3	15 Feet	45 Feet	Regional airport with limited air carrier service.
<u>HEIGHT GROUP 3</u> B-727/707/720/757, B-52, C-135, C-141, C-17, E-3, P-3, E-8	20 Feet	50 Feet	Primary runways not normally used by aircraft with ILS glidepath-to-wheel heights exceeding 20 ft.
<u>HEIGHT GROUP 4</u> B-747/767/777, L-1011, DC-10, A-300, B-1, KC-10, E-4, C-5, VC-25	25 Feet	55 Feet	Most primary runways at major airports.

- NOTE 1: To determine the minimum allowable TCH, add 20 ft to the glidepath-to-wheel height.
 NOTE 2: To determine the maximum allowable TCH, add 50 ft to the glidepath-to-wheel height.
 NOTE 3: Publish a note indicating the VGSI not coincident with the procedure GPA when the VGSI angle is more than 0.2° from the GPA, or when the VGSI TCH is more than 3 ft from the procedure TCH.

The glidepath angle should not result in a descent rate (**DR**) greater than 1,000 ft-per-minute for aircraft served by the procedure. Use formula 3-1 to calculate the **DR** for any given 3-D procedure.

Formula 3-1
$DR = V_{KIAS} \times (1 + 0.00002p) \times \sin(\theta) \times 101.26859$ <p>Where: V_{KIAS} = Indicated Airspeed p = PFAF Altitude θ = Glidepath Angle</p>
Example
$V_{KIAS} = 165 \quad p = 2,100 \quad \theta = 3^\circ$ $DR = 165 \times (1 + 0.00002 \times 2,100) \times \sin(3) \times 101.26859 = 911.227 \text{ ft}/_{\text{min}}$

3.2.1 Controlling the Effects of Temperature on the Glidepath Angle.

RNP final segment vertical guidance is provided by barometric VNAV. The effective glidepath angle (actual angle flown) depends on the temperature deviation from standard (**ISA**) associated with airport elevation. ISA for the airport may be calculated using formula 3-2.

NOTES:

1. The formula for conversion from Celsius to Fahrenheit is also given; however, the use of ISA values in calculation of minimum and maximum angles below will always use Celsius values.
2. Examples 3-2 through 3-8 in this section use PFAF altitude 2000, Airport and LTP elevation 400, Glidepath angle (θ) 3°.

Formula 3-2
$ISA^\circ C = 15^\circ - \frac{\text{airport elevation}}{500}$ $ISA^\circ F = (1.8 \times ISA^\circ C) + 32$
Example
$ISA^\circ C = 15^\circ - \frac{400}{500} = 14.2^\circ C$ $ISA^\circ F = (1.8 \times 10.40) + 32 = 57.56^\circ F$

The approach procedure should offer obstacle protection within a temperature range that can reasonably be expected to exist at the airport. Establish the lower temperature limit from the 5-year average lowest temperature for the coldest month of the year (**ACT**). Determine the difference (ΔISA_{Low}) between this temperature and ISA temperature for the airport using formula 3-3.

Formula 3-3
$\Delta ISA_{Low} = -(ISA - ACT)$ <p>where ACT = Average Cold Temperature</p>
Example
$\Delta ISA_{Low} = -(14.2 - [-15.0]) = -29.2^\circ C$ <p>where ISA = 14.2°C ACT = -15.0°C</p>

The effective glidepath angle at ΔISA_{LOW} ($\theta_{\Delta ISA_{LOW}}$) must not be less than 0.917θ (0.917 times the published glidepath angle). For example, $0.917 \times 3.0^\circ = 2.75^\circ$. Calculate the $\theta_{\Delta ISA_{LOW}}$ using formula 3-4.

Formula 3-4
$\theta_{\Delta ISA_{LOW}} = \tan^{-1} \left(\frac{a + e}{r} \right)$
<p>where a = PFAF altitude - LTP Elevation</p> $e = \Delta ISA_{LOW} \times (0.19 + [0.0038 \times a]) + 0.032 \times a + 4.9$ $r = \frac{a}{\tan(\theta)}$ <p>θ = Published Glidepath Angle</p>
Example
$\theta_{\Delta ISA_{LOW}} = \tan^{-1} \left(\frac{1600 + [-126.98]}{30529.82} \right) = 2.76$ <p>where $a = 2,000 - 400$</p> $e = -29.2 \times (0.19 + [0.0038 \times 1,600]) + 0.032 \times 1,600 + 4.9$ $r = \frac{1,600}{\tan(3)}$

If the effective glidepath angle is less than 0.917θ , calculate the ΔISA_{LOW} to achieve an angle of 0.917θ using formula 3-5.

Formula 3-5
$\Delta ISA_{LOW} = \frac{-el - (0.032 \times a) - 4.9}{0.19 + (0.0038 \times a)}$
<p>where el = PFAF altitude - b</p> $b = r \times \tan(0.917\theta) + \text{LTP elevation}$ $r = \frac{a}{\tan(\theta)}$ <p>a = PFAF altitude - LTP elevation</p>
Example
$\Delta ISA_{LOW} = \frac{-133.56 - (0.032 \times 1,600) - 4.9}{0.19 + (0.0038 \times 1,600)} = -30.25$ <p>where $el = 2000 - b$</p> $b = 30,529.82 \times \tan(2.75) + 400$ $r = \frac{1,600}{\tan(3)}$ <p>$a = 2,000 - 400$</p>

Determine the **published** low temperature limitation for the procedure derived from formula 3-6, using the ΔISA_{LOW} derived from formula 3-3 or 3-5 as appropriate. If the temperature history for the location indicates the low temperature limitation is frequently encountered during established busy

recovery times, consider raising the glidepath angle to the lowest angle (within table 3-1 limits) that will make the approach usable more often.

Formula 3-6
$NA_{\text{below}} = ISA + \Delta ISA_{\text{LOW}}$
Example
$NA_{\text{below}} = 10.4 + [-25.4] = -15^{\circ}\text{C}$ or $1.8 \times [-15] + 32 = 5^{\circ}\text{F}$

Higher than ISA temperatures produce higher effective angles than the designed glidepath angle. Determine the maximum ΔISA_{HIGH} (above ISA) that will produce the maximum allowed glidepath angle (α) using formula 3-7 where the maximum glidepath angle is 1.13 times the table 3-1 maximum value for the fastest published approach category.

Formula 3-7
$\Delta ISA_{\text{HIGH}} = \frac{eh - (0.032 \times a) - 4.9}{0.19 + (0.0038 \times a)}$
<p>where $eh = c - \text{PFAF altitude}$</p> <p>$c = r \times \tan(\alpha) + \text{LTP elevation}$</p> <p>$r = \frac{a}{\tan(\theta)}$</p> <p>$a = \text{PFAF altitude} - \text{LTP elevation}$</p> <p>$\alpha = \text{Maximum Allowed Glidepath Angle}$</p> <p>$\theta = \text{Published Glidepath Angle}$</p>
Example
$\Delta ISA_{\text{HIGH}} = \frac{208.46 - (0.032 \times 1600) - 4.9}{0.19 + (0.0038 \times 1600)} = 24.3^{\circ}\text{C}$
<p>where $eh = 2208.46 - 2000$</p> <p>$c = 30529.82 \times \tan(3.39) + 400$</p> <p>$r = \frac{1600}{\tan(3)}$</p> <p>$a = 2000 - 400$</p>

Determine the **published** high temperature limitation for the procedure derived from formula 3-8.

Formula 3-8
$NA_{\text{above}} = ISA + \Delta ISA_{\text{HIGH}}$
Example
$NA_{\text{above}} = 10.4 + 33.68 = 44.08^{\circ}\text{C}$ or $1.8 \times 44.08 + 32 = 111.34^{\circ}\text{F}$

3.3 TURNS IN THE FAS.

Fly-by turns are not allowed in the FAS. Where turns are necessary, use an RF leg. Design procedures that incorporate an RF turn in the final segment to establish the aircraft on a straight segment aligned with the runway centerline prior to reaching DA. The Final Rollout Point (FROP) is the initial fix of the straight segment (see figure 3-1). Locate the FROP at the greatest distance resulting from application of formulas 3-9 and 3-10A/B as appropriate.

Apply formula 3-9 to assure rollout occurs at least 500 ft above LTP elevation.

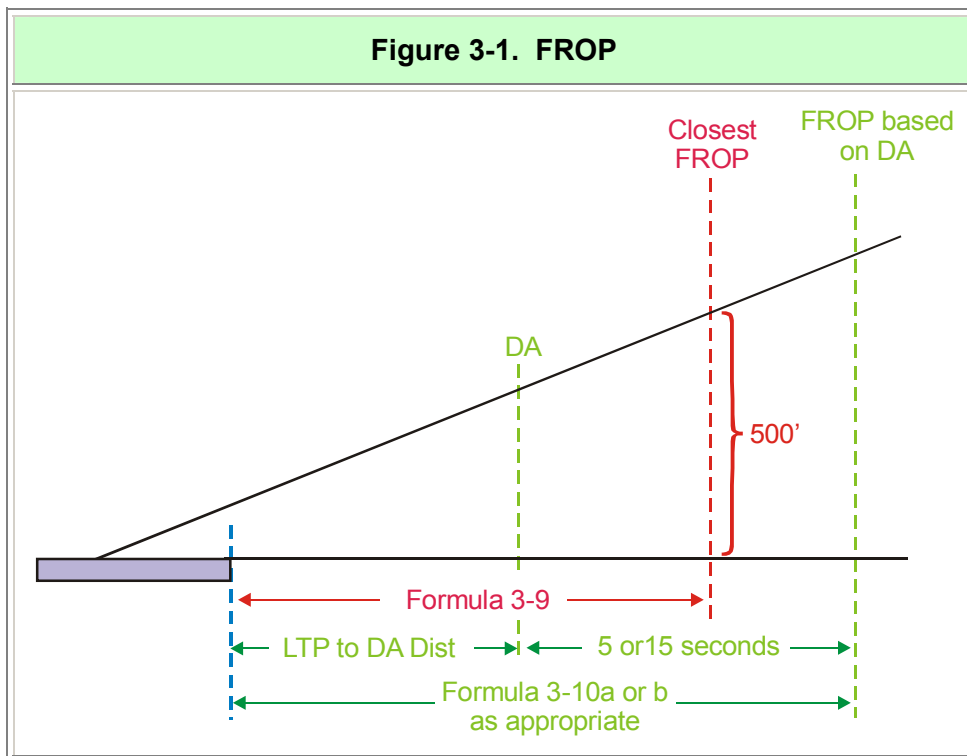
Formula 3-9 (500' above LTP)
$D_{500} = \frac{500 - TCH}{\tan(\theta)}$
where θ = glidepath angle
Example
$D_{500} = \frac{500 - 52}{\tan(3)} = 8548.35'$
where $\theta = 3^\circ$ TCH = 52 feet

Apply formula 3-10A where the initial MAS RNP value is standard (RNP 1.0) or the MAS is based on conventional NAVAIDs.

Formula 3-10A (5 sec stabilization)
$D_{5sec} = \frac{HAT - TCH}{\tan(\theta)} + (V_{TAS} + 15) \times 8.44$
where θ = glidepath angle V_{TAS} = final segment true airspeed
Example
Cat D 165 Kts, Altitude 2000, $\theta=3^\circ$, TCH=52, HAT=300 $V_{TAS} = 165 \times [1 + (2000 \times 0.00002)] = 171.60$ $D_{5sec} = \frac{300 - 52}{\tan(3)} + (171.60 + 15) \times 8.44 = 6307.03$

Apply formula 3-10B where the initial MAS RNP value is restricted to less than 1.0.

Formula 3-10B (15 sec stabilization)
$D_{15sec} = \frac{HAT - TCH}{\tan(\theta)} + (V_{TAS} + 15) \times 25.32$ <p>where θ = glidepath angle V_{TAS} = final segment true airspeed</p>
Example
<p>Cat D 165 Kts, Altitude 2000, $\theta=3^\circ$, TCH=52, HAT=300</p> $V_{TAS} = 165 \times [1 + (2000 \times 0.00002)] = 171.60$ $D_{15sec} = \frac{300 - 52}{\tan(3)} + (171.60 + 15) \times 25.32 = 9456.83$



3.4 DETERMINING PFAF LOCATION. (In all cases, the PFAF will be identified as a named fix.)

The OPTIMUM alignment is a TF segment straight in from PFAF to LTP on runway centerline extended. If necessary, the TF course may be offset by up to 3°. Where the course is offset, it must cross runway centerline extended at least 1500 out from LTP. A final segment may be designed using an RF leg segment

when obstacles or operational requirements prevent a straight-in approach from PFAF to LTP. Determine the along-track distance from the LTP (FTP if offset) to the point the glidepath intercepts the intermediate segment minimum altitude (D_{PFAF}). Calculate D_{PFAF} using formula 3-11. Determine which leg (TF or RF) the PFAF is located on by comparing D_{PFAF} to the leg lengths

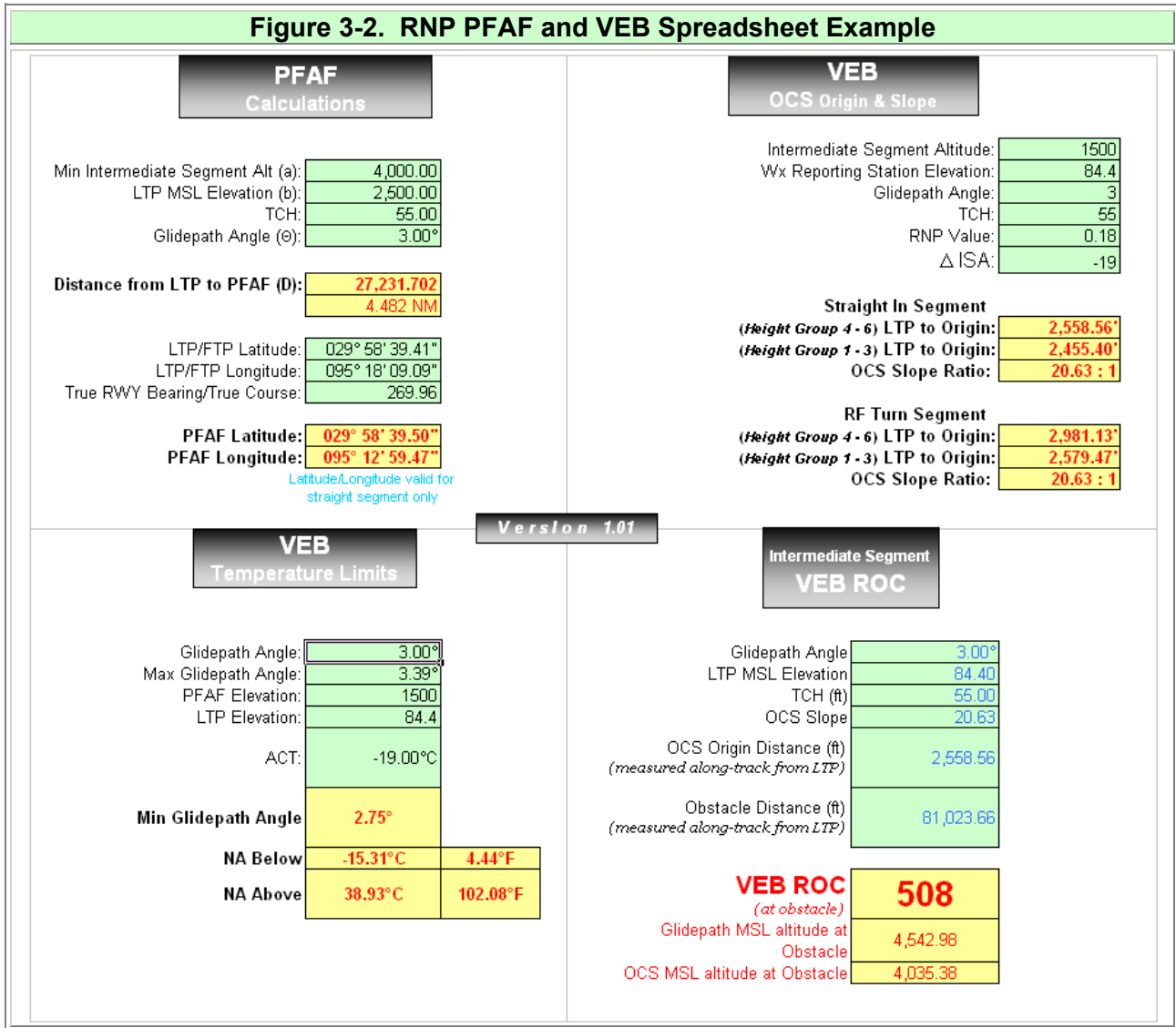
Formula 3-11	
$D_{PFAF} = 364,609 \left[90 - \theta - \sin^{-1} \left(\frac{\sin(90 + \theta) 20,890,537}{(a - b - tch) + 20,890,537} \right) \right]$	
Where: a = minimum intermediate altitude b = LTP elevation in feet θ = glidepath angle tch = threshold crossing height	
Example	
a = 2000 b = 400 tch = 52 $\theta = 3^\circ$	
$D_{PFAF} = 364,609 \left[90 - 3 - \sin^{-1} \left(\frac{\sin(90 + 3) 20,890,537}{(2000 - 400 - 52) + 20,890,537} \right) \right] = 29147.454$	

3.4.1

PFAF LOCATED ON TF LEG.

Geodetically calculate the latitude and longitude of the PFAF using the reverse true course of the TF leg (true course – 180°) and D_{PFAF} measured along-track from the LTP (FTP if offset). Where the FAS consists of a single TF leg, a Microsoft Excel spreadsheet (see figure 3-2) is provided on the AFS-420 website to calculate D_{PFAF} and the WGS-84 latitude and longitude of the PFAF. Go to the following Internet link:

<http://av-info.faa.gov/terps/> - Then select link: RNP SAAAR VEB.



3.4.2 PFAF Located on RF Leg.

The PFAF must be located at the initial fix of a TF or RF segment. Where the PFAF must be located within an RF segment, the segment must be broken into two segments, each having the same radius and turn center, with the PFAF coincident with the initial fix of the second segment. The length in feet of the RF leg from the FROP to PFAF can be calculated by formula 3-12.

Formula 3-12
Length_{RF} = D_{PFAF} - D_{FROP}
Example
Length _{RF} = 29147.45 - 8548.35 = 20599.10 where D _{PFAF} = 29147.45 (from formula 3-9) D _{FROP} = 8548.35 (from formula 3-10)

The number of degrees of arc given a specific arc length may be calculated using formula 3-13.

Formula 3-13
Degrees of Arc [ϕ]: $\phi = \frac{180 \cdot L}{\pi \cdot R}$

Conversely, the length of an arc given a specific number of degrees of arc may be calculated using formula 3-14.

Formula 3-14
Length of Arc [L]: $L = \frac{\phi \cdot \pi \cdot R}{180}$

3.4.2

a. Determining RF PFAF Location Relative to LTP. This method may be used for calculating WGS-84 latitude and longitude (see figure 3-3). Several software packages will calculate a geographical coordinate derived from Cartesian measurements from the LTP. Use formulas 3-15 and 3-16 to obtain the Cartesian values.

STEP 1: Determine the flight track distance (D_{PFAF}) from LTP to PFAF under formula 3-9.

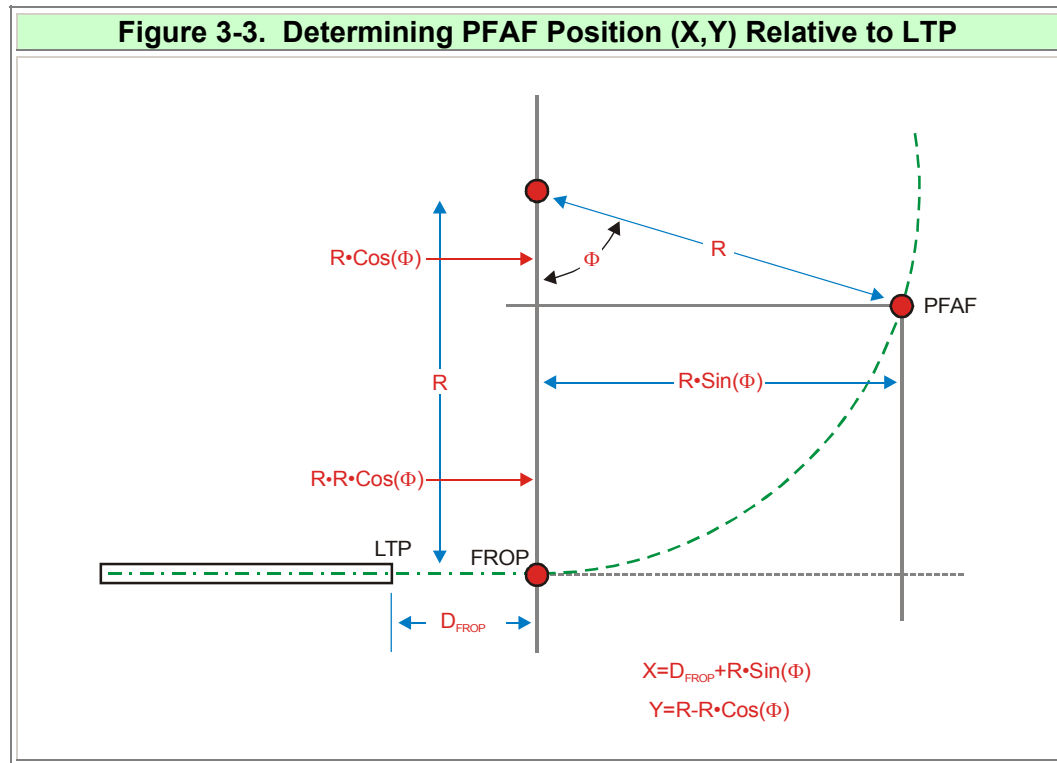
STEP 2: Determine the distance (D_{FROP}) from LTP to the FROP (see paragraph 3.3).

STEP 3: Subtract D_{FROP} from D_{PFAF} to calculate the distance around the arc to the PFAF from the FROP. Use formula 3-13 to determine number of degrees of arc; conversely, use formula 3-14 to convert degrees of arc to length.

If the PFAF is in the RF segment, determine its X,Y coordinates using formulas 3-15 and 3-16:

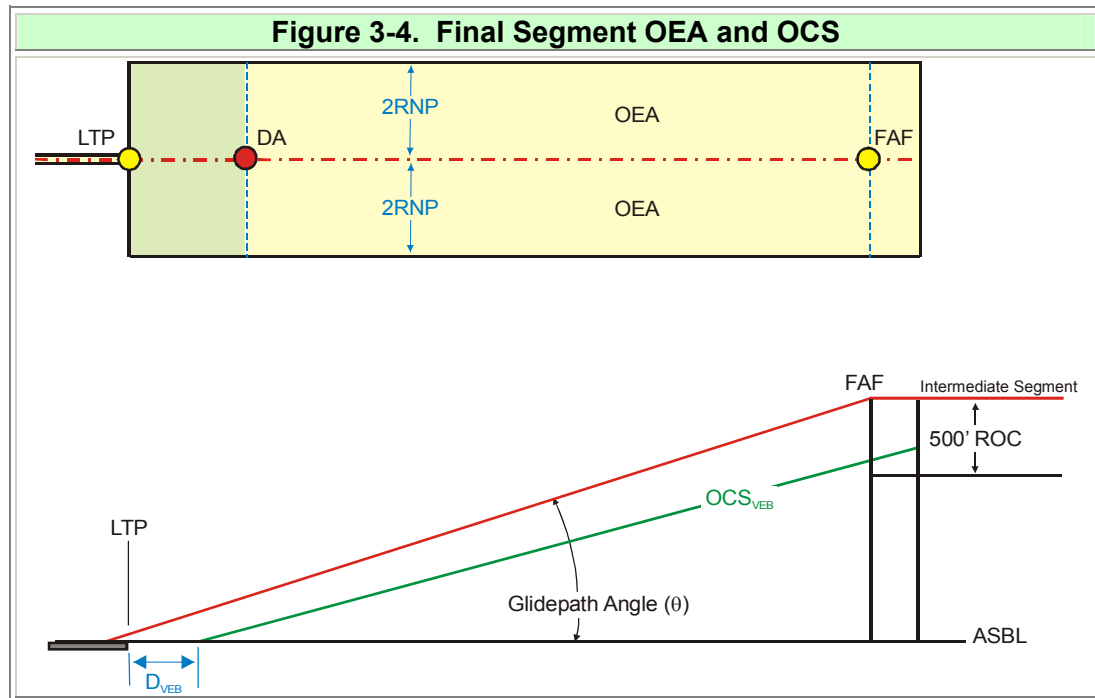
Formula 3-15
$X = D_{FROP} + R \cdot \sin(\phi)$

Formula 3-16
$Y = R - [R \cdot \cos(\phi)]$



3.5 FINAL SEGMENT OEA.

The final segment OEA begins $1 \times RNP$ prior to the PFAF and extends to the LTP/FTP. The OEA contains a sloping OCS to evaluate obstructions prior to DA, and a visual segment surface from DA to LTP (see figure 3-4).



The OCS origin distance from LTP (D_{VEB}) and its slope are determined through application of the Vertical Error Budget (**VEB**). The VEB calculations require input of values for two variables: final segment RNP value and temperature ($^{\circ}\text{C}$) deviation ($\Delta\text{ISA}_{\text{Low}}$) below the airport ISA temperature. A link to a Microsoft Excel spreadsheet that performs the VEB calculations is available on the internet at the following address: <http://av-info.faa.gov/terps/> under the label "RNP SAAAR VEB". See figure 3-2.

Calculate the MSL elevation of the OCS at any distance 'd' from RWT using formula 3-17.

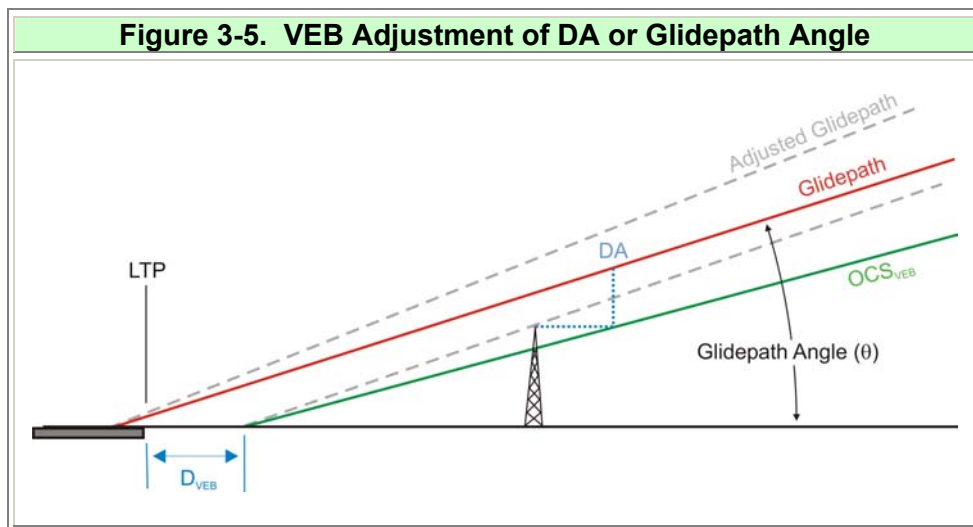
Formula 3-17
$\text{VEB}_{\text{MSL}} = \text{LTP}_{\text{elev}} + \frac{d - D_{\text{VEB}}}{\text{OCS}_{\text{slope}}}$
<p>where d = distance along course centerline from RWT D_{VEB} = distance of OCS origin from LTP $\text{OCS}_{\text{slope}}$ = OCS slope from VEB calculations</p>
Example
$\text{VEB}_{\text{MSL}} = 400 + \frac{4107.23 - 3559.42}{20.71} = 426.45$
<p>where $d = 4107.23$ $D_{\text{VEB}} = 3559.42$ $\text{OCS}_{\text{slope}} = 20.71$ $\text{LTP}_{\text{elev}} = 400$</p>

3.5.1 Obstacle Evaluation.

If the FAS OCS is not penetrated, the MINIMUM HAT value of 250 ft applies. **Limitation: The distance from LTP to DA must not be less than the distance from LTP to OCS origin (D_{VEB}).** Determine the DA using formula 3-18.

Formula 3-18
$DA = HAT + TDZE$

Obstacles that penetrate an OCS may be mitigated by one of the following actions: remove or lower obstacle, lower the RNP value for the segment (if appropriate), adjust the lateral path, raise glidepath angle, raise TCH (within table 3-2 limits), or adjust HAT (see figure 3-5 and formula 3-19).

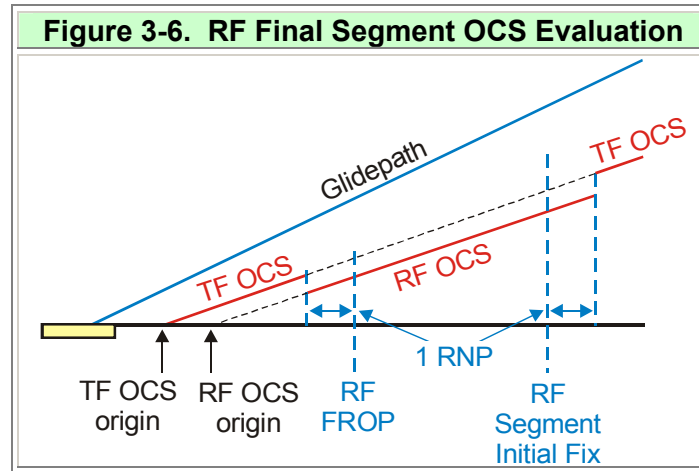


NOTE: D_{VEB} decreases slightly when glidepath angle is increased. Therefore if the angle is increased to accommodate a penetration, the VEB must be recalculated and the OCS re-evaluated.

Formula 3-19
$HAT_{adjusted} = \tan(\theta) \cdot (d + p \cdot OCS_{VEB}) + TCH + (LTP_{elev} - TDZE)$ <p>where θ = glidepath angle d = distance (ft) LTP to obstacle p = amount of penetration (ft) OCS_{VEB} = Slope of VEB OCS</p>
Example
$HAT_{adjusted} = \tan(3) \cdot (4315 + 8 \cdot 20.71) + 52 + (400 - 405) = 281.82$ <p>where $\theta = 3^\circ$ $d = 4315$ $p = 8'$ $OCS_{VEB} = 20.71$ $LTP_{elev} = 400$ $TDZE = 405$</p>

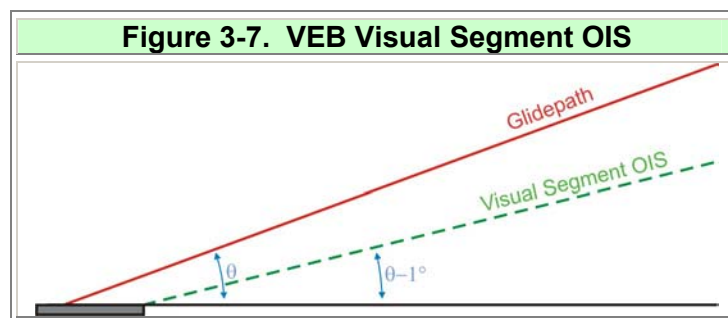
3.5.2 Applying VEB OCS to RF Final Segments.

Where RF legs are incorporated in the final segment, the OCS slope ratio will be consistent for the straight and curved path portions; however, the OCS origin will be different because the variables for aircraft body geometry is different for straight and curved path legs. The OCS elevation at any point is equal to the surface elevation of the course centerline abeam it (see figure 3-6).



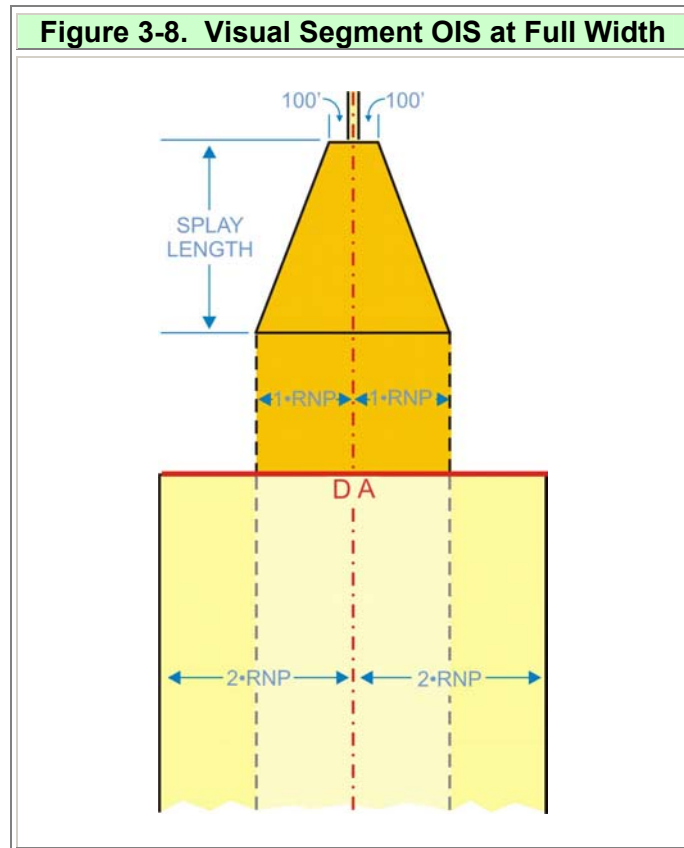
3.6 VISUAL SEGMENT EVALUATION.

Apply Order 8260.3, United States Standard for Terminal Instrument Procedures (TERPS), Volume 1, paragraph 251. In addition, apply an obstacle identification surface (OIS) that originates at the LTP and extends to the DA point at an angle of one degree less than the glidepath angle (see figure 3-7).



The OIS half-width at the LTP is 100 ft outside the runway edge. It splays at an angle of 10° relative to course until reaching a width of $\pm 1 \cdot \text{RNP}$, which it maintains until contacting the final segment OEA at DA (see figure 3-8).

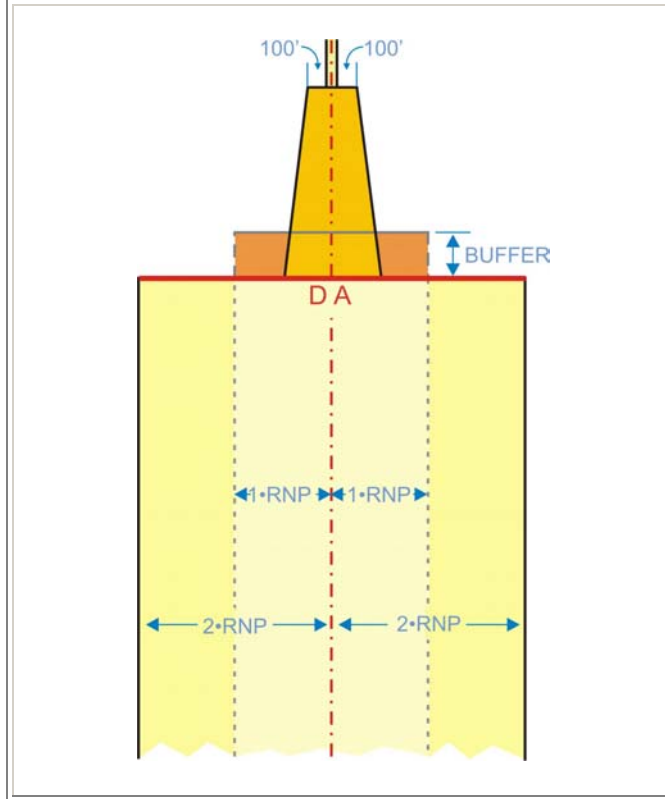
Formula 3-20	
\mathbf{Splay}_{length}	$= \frac{(1 \cdot \mathbf{RNP} \cdot 6076.11548) - \left(100 + \frac{\mathbf{Rwy Width}}{2}\right)}{\tan(10)}$
Example	
\mathbf{Splay}_{length}	$= \frac{(1 \times 0.15 \cdot 6076.11548) - \left(100 + \frac{150}{2}\right)}{\tan(10)} = 4176.43$
	where RNP = 0.15 Rwy Width = 150



Calculate the segment length (\mathbf{Splay}_{length}) required to reach $\pm 1 \cdot \mathbf{RNP}$ using formula 3-20. If \mathbf{Splay}_{length} is greater than the distance from LTP to DA, construct a $\pm 1 \cdot \mathbf{RNP}$ buffer area aligned with the runway centerline extended from the DA point toward the LTP for a distance of " \mathbf{D}_{buffer} " as shown in formula 3-21 and figure 3-9 based on largest category minima published and the PFAF altitude. The buffer OIS is a continuation of the VEB OCS from DA to the OCS origin, or \mathbf{D}_{buffer} , whichever is less. An obstacle may penetrate the visual/buffer OIS (figures 3-8 and 3-9) provided it is charted and appropriate mitigations are identified and approved by AFS-400.

Formula 3-21
$D_{\text{buffer}} = (V_{\text{KTAS}} + 10) \cdot 8.44$
Example
$D_{\text{buffer}} = (171.93 + 10) \times 8.44 = 1535.49$

Figure 3-9. Visual Segment Not at Full Width



CHAPTER 4. MISSED APPROACH SEGMENT (MAS)

4.0 GENERAL.

These criteria are based on the following assumptions:

- Aircraft climb at a rate of at least 200 ft/NM (3.29%) in the missed approach segment.
- A non-guided missed approach is not RNP and is treated as dead-reckoning navigation (subject to 15° OEA splay).
- The OEA expansion where FAS RNP levels less than RNP-1 are continued into the MAS is based on IRU drift rates of 8 NM per hour.
- For RNP levels less than 1, turns are not allowed below 500 ft measured AGL
- A 50-ft height loss is inherent in MA initiation.

The standard MA construction is a continuation of the final approach course. The OEA expands at a 15° splay from the FAS RNP value to a value of 1.0, using a 40:1 OCS slope ratio. Missed approach RF turns that are speed limited must limit bank angles to 15° maximum. If necessary, RNP may be discontinued at the MAP or any subsequent fix and a conventional MAS constructed under Order 8260.3, Volume 1, chapter 2.

4.1 MAS SEGMENT LEG TYPES.

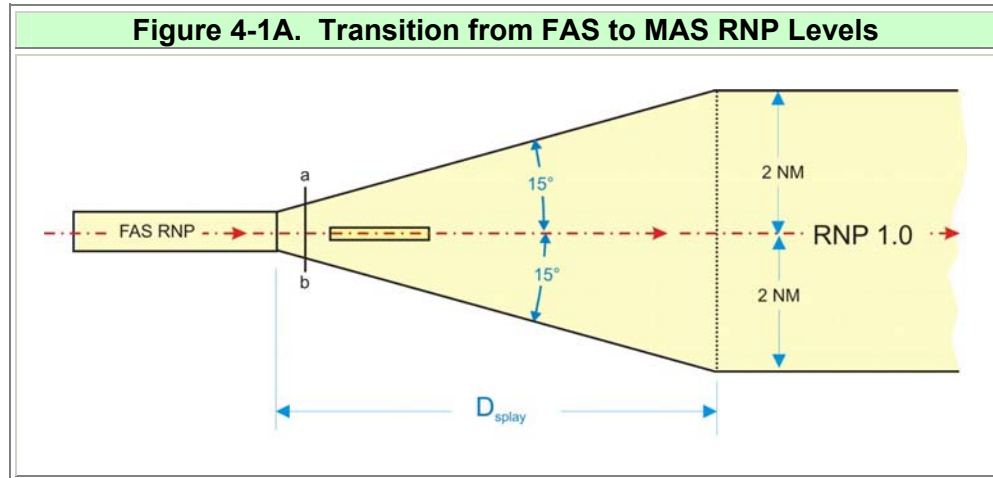
The missed approach route is a series of segments. The following leg types are authorized for missed approach procedure design:

- **Track-to-Fix TF**
- **Radius-to-Fix RF**

Additionally, if the RF leg RNP value is <1.0, the RF leg length must comply with paragraph 4.2.1.

4.2 MA SEGMENT RNP LEVEL.

The standard MA segment splays from the FAS width at DA, 15° relative to course centerline, to a width of ± 2 NM (RNP 1.0). See figure 4-1A.



The along-track distance (NM) required to complete the splay may be calculated using formula 4-1.

Formula 4-1
$D_{\text{splay}} = 7.464(1 - \text{RNP}_{\text{FAS}})$
Example
$D_{\text{splay}} = 7.464(1.0 - 0.3) = 5.23$ where $\text{RNP}_{\text{MAS}} = 1.0$ $\text{RNP}_{\text{FAS}} = 0.3$

Turns are not allowed until the splay is complete. If turns are required before D_{splay} , consider another construction technique; e.g., applying paragraph 4.2.1 or a conventional TERPS MAS.

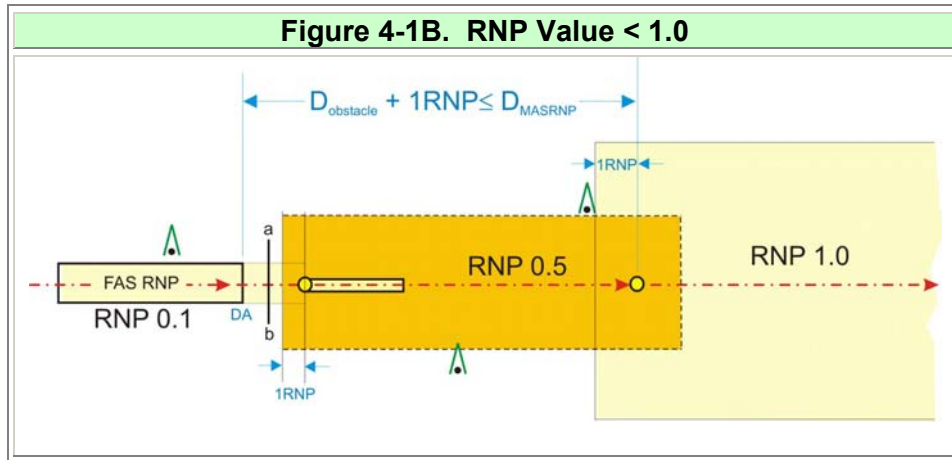
4.2.1 RNP Values < 1.

Where turns are necessary, the turn initiation must occur after passing 500 ft AGL and at least D_{MASturn} feet from DA. When possible, the turn should not occur until after DER. Calculate D_{MASturn} using formula 4-2.

Formula 4-2
$D_{\text{MASturn}} = 16.88 \times (V_{\text{KIAS}} \times [1 + (0.00002a)] + 10)$ where V_{KIAS} = Indicated airspeed from table 1-2 a = Decision Altitude
Example
$D_{\text{MASturn}} = 16.88 \times (165 \times [1 + (0.00002 \times 650)] + 10) = 2990.21$ where V_{KIAS} = 165 Cat D indicated airspeed from table 1-2 $a = 650$

Where the 40:1 OCS is penetrated and the resulting HAT or visibility can be reduced by at least 50 ft or ¼ SM respectively, consider limiting the MAS RNP value until clearing the obstruction. Use the largest RNP value (FAS RNP ≤ MAS RNP ≤ 1.0) that clears the obstruction. The maximum distance (NM) (D_{MASRNP}) that the < 1.0 RNP value may be extended into the MAS is calculated using formula 4-3 (see figure 4-1B).

NOTE: Use of MAS RNP values < 1.0 requires track guidance (TF or RF leg segments). Paragraph 2.8 applies to RNP increases.



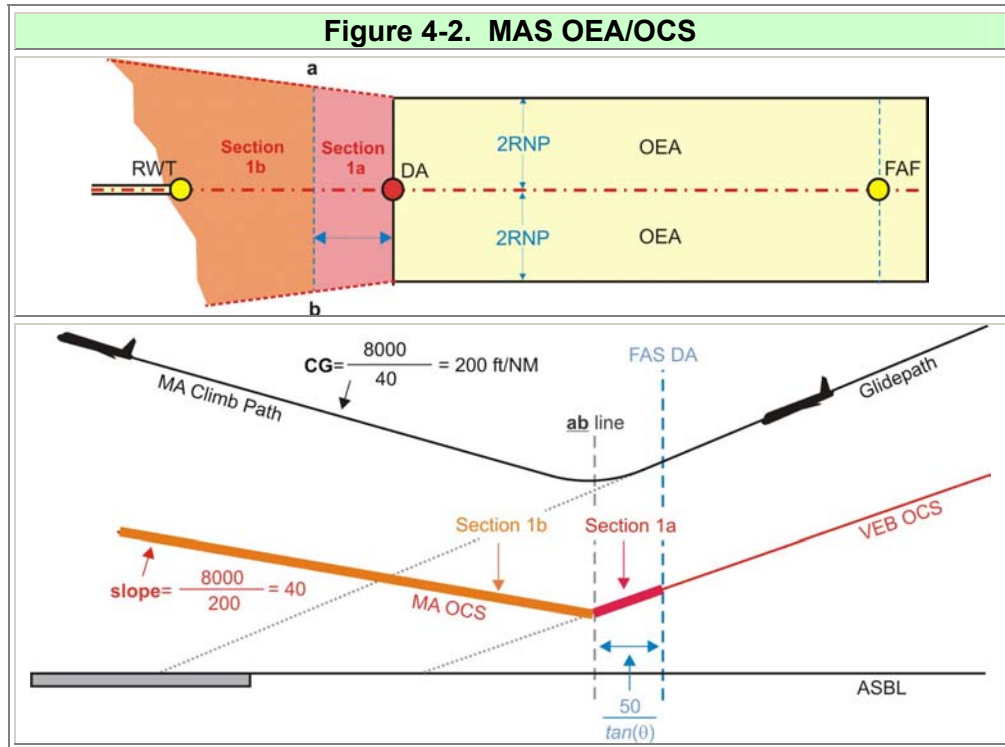
Formula 4-3
$D_{MASRNP} = 20.625 \times RNP_{MAS} - 1.031$
Example
$D_{MASRNP} = 20.625(0.3) - 1.031 = 5.16$ where $RNP_{MAS} = 0.3$

4.3 MA SEGMENT OCS EVALUATION.

The MAS is composed of OCS sections 1a and 1b (see figure 4-2). Sections 1a and 1b are separated by the ab line. Section 1a OCS extends from the DA point downward at the VEB OCS slope ratio for a distance of $D_{heightloss}$ (calculated using formula 4-4) measured along the final course track to the ab line. From the ab line, section 1b OCS rises at a 40:1 slope. Obstacles must not penetrate the OCS.

Formula 4-4
$D_{heightloss} = \frac{HL}{\tan(\theta)}$
where HL = Assumed Height Loss

Example
$D_{\text{heightloss}} = \frac{50}{\tan(3)} = 954.06$ <p>where HL = 50</p>



Calculate the MSL height of the missed approach surface (HMAS) at the **ab** line (**HMAS_{ab}**) using formula 4-5.

Formula 4-5
$HMAS_{ab} = LTP_{\text{elev}} + \frac{D_{DA} - D_{OCS\text{origin}} - \frac{HL}{\tan(\theta)}}{VEB_{OCS\text{slope}}}$ <p>where D_{DA} = Distance from LTP to DA $D_{OCS\text{origin}}$ = Distance from LTP to OCS origin $VEB_{OCS\text{slope}}$ = Final segment OCS slope HL = Height loss</p>
Example
$HMAS_{ab} = 400 + \frac{4732.12 - 2585.64 - \frac{50}{\tan(3)}}{20.72} = 457.55$ <p>where $D_{DA} = 4770.28$ $D_{OCS\text{origin}} = 2585.64$ $VEB_{OCS\text{slope}} = 20.72$ HL = 50</p>

The MSL height of the section 1b surface ($H_{\text{section1b}}$) at any obstruction can be calculated using formula 4-6 after determining distance ($D_{\text{section1b}}$) by measuring the along-track centerline distance from the ab line to a point abeam the obstruction.

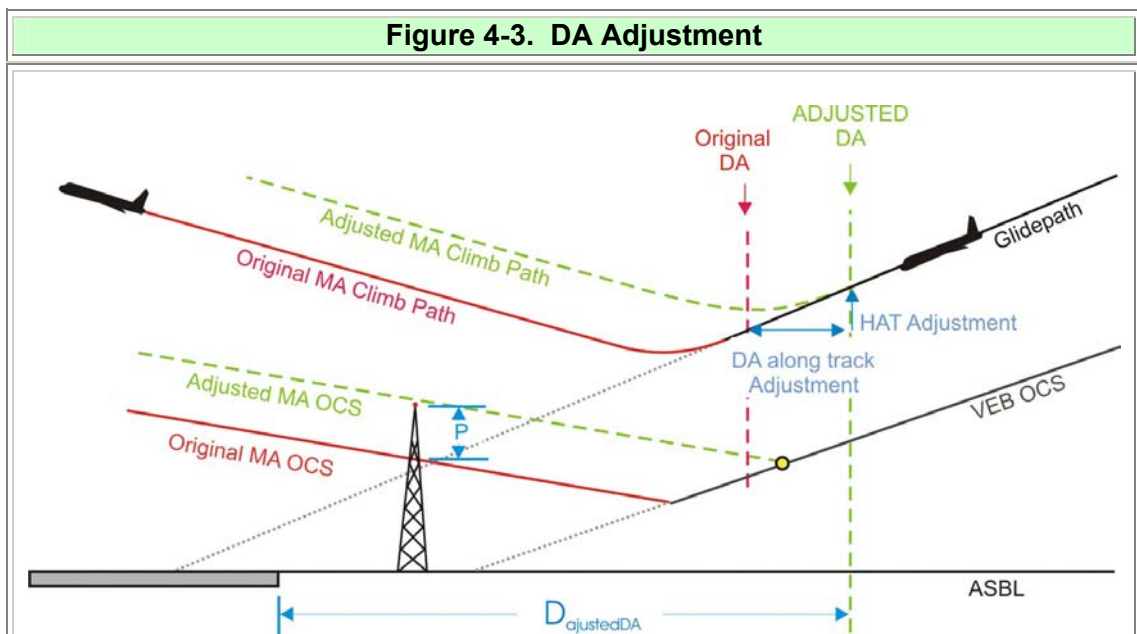
Formula 4-6	
$H_{\text{section1b}} = \text{HMAS}_{\text{ab}} + \frac{D_{\text{section1b}}}{\text{MA OCS}_{\text{slope}}}$	
Example	
$H_{\text{section1b}} = 457.55 + \frac{13548}{40} = 796.25$	
where $\text{HMAS}_{\text{ab}} = 457.55$	
$D_{\text{section1b}} = 13548$	

4.3.1 OCS Penetrations.

Where obstructions penetrate the OCS, take one or more of the following actions to achieve the lowest possible DA:

- Remove or lower the obstruction.
- Use RNP level < 1.0 to place obstacle outside the OEA.
- Alter MA track.
- Adjust DA.
- Require MA climb gradient.

4.3.1 a. DA Adjustment. See figure 4-3. To determine the DA required to mitigate a MA OCS penetration, determine the amount of increase required in the HAT value using formula 4-7.



Formula 4-7
$HAT_{\text{adjustment}} = \frac{p \tan(\theta) MA_{\text{OCS Slope}} VEB_{\text{OCS Slope}}}{MA_{\text{OCS Slope}} + VEB_{\text{OCS Slope}}}$ <p>where p = amount of penetration (ft) θ = glidepath angle</p>
Example
$HAT_{\text{adjustment}} = \frac{18 \tan(3) 40 \times 20.72}{40 + 20.27} = 12.88$ <p>where p = 18 $\theta = 3$ $VEB_{\text{OCSslope}} = 20.72$ $MA_{\text{OCSslope}} = 40$</p>

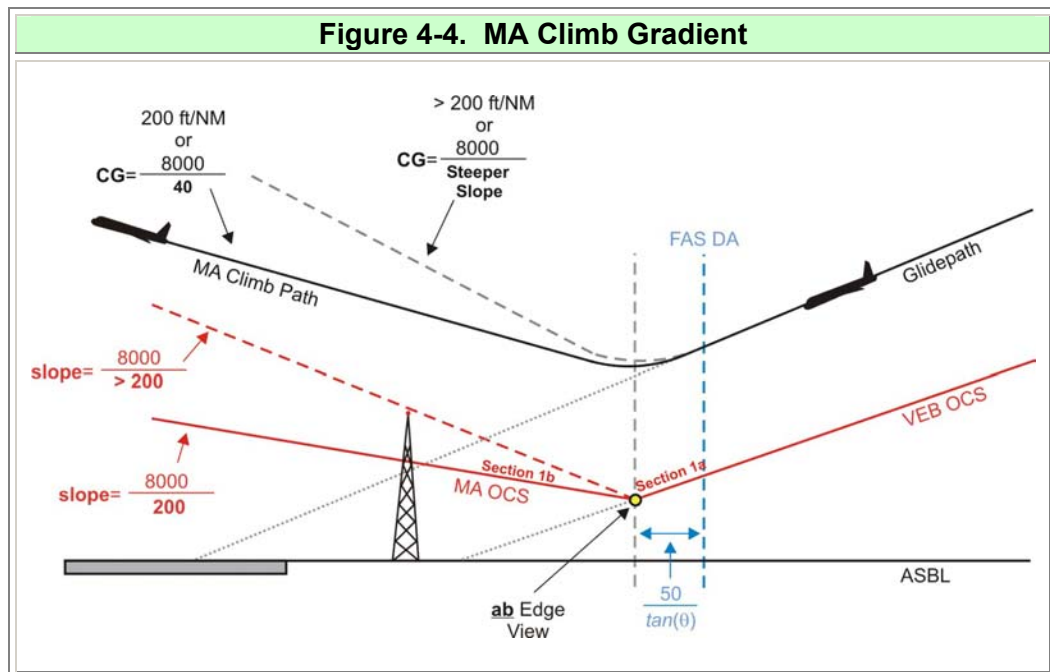
Calculate the distance from LTP to DA using formula 4-8.

Formula 4-8
$D_{\text{adjustedDA}} = \frac{HAT_{\text{FAS}} + HAT_{\text{adjustment}} - TCH + (TDZE - LTP_{\text{elev}})}{\tan(\theta)}$ <p>where θ = Glidepath angle TDZE = Touchdown Zone elevation LTP_{elev} = LTP elevation</p>
Example
$D_{\text{adjustedDA}} = \frac{300 + 12.88 - 52 + (403 - 400)}{\tan(3)} = 5034.98$ <p>where θ = Glidepath angle TCH = 52 TDZE = 403 $LTP_{\text{elev}} = 400$ $HAT_{\text{FAS}} = 300$ $HAT_{\text{adjustment}} = \text{result from formula 4-x}$</p>

Finally, calculate the adjusted DA value using formula 4-9.

Formula 4-9
$DA_{adjusted} = \tan(\theta)D_{adjustedDA} + (LTPe_{lev} + TCH)$
Example
$DA_{adjusted} = \tan(3)4977.81 + (400 + 52) = 712.88$ where $\theta = 3$ degrees $D_{adjustedDA} = 4977.81$ $LTPe_{lev} = 400$ $TCH = 52$

- 4.3.1 b. **Calculating MA climb gradient.** See figure 4-4. Where the section 1b OCS is penetrated and resulting HAT or visibility can be reduced by at least 50 ft or ¼ SM respectively, consider avoiding the obstruction by requiring an MA climb gradient.



To determine the climb gradient required to clear a section 1b obstacle, apply formula 4-10.

Formula 4-10	
$MA_{CG} = \frac{8000(OBS_{elev} - HMAS_{ab})}{D_{abobs}}$	
where OBS_{elev} = Obstruction MSL elevation $HMAS_{ab}$ = MSL height of HMAS at ab line D_{abobs} = distance (ft) from ab line to obstacle measured along MA course	
Example	
$MA_{CG} = \frac{8000(649 - 457.55)}{5409} = 283.16$	
where OBS_{elev} = 649 $HMAS_{ab}$ = 457.55 D_{abobs} = 5409	

If the climb gradient exceeds 425 ft/NM, evaluate the MAS using the OCS slope appropriate for 425 ft/NM (18.82:1) and adjust DA for the remaining penetration per paragraph 4.3.1a.

4.3.1

b. (1) Calculating CG termination altitude. Calculate the altitude above which the climb gradient is no longer required using formula 4-11. Round the result to the next higher 100 ft increment.

Formula 4-11	
$TA_{CG} = (DA - 50) + CG \times D_{abobs}$	
CG = climb gradient D_{abobs} = distance (ft) from ab line to obstacle	
Example	
$TA_{CG} = (713 - 50) + 284 \times \frac{5409}{6076} = 915.82 \text{ round up to } 1000$	
$CG = 284$ $D_{abobs} = 5409'$ $DA = 713$	

APPENDIX 1. VERTICAL ERROR BUDGET (VEB) REQUIRED OBSTACLE CLEARANCE (ROC) EQUATION EXPLANATION

The required obstacle clearance (ROC) for the VEB is derived by combining known three standard deviation variations by the root-sum of squares method (RSS) and multiplying by four thirds to determine a combined four standard deviation (4σ) value. Bias errors are then added to determine the total ROC.

The sources of variation included in the ROC for the VEB are:

Actual navigation performance error (**anpe**)
 Waypoint precision error (**wpr**)
 Flight technical error (**fte**) **fixed at 75 ft**
 Altimetry system error (**ase**)
 Vertical angle error (**vae**)
 Automatic terminal information system (**atis**) **fixed at 20 ft**

The bias errors for the ROC are:

Body geometry error (**bg**)
 International standard atmosphere temperature deviation (**isad**)
 Semi-span for narrow body **fixed at 68**
 Semi-span for wide body **fixed at 131**

The ROC equation which combines these is:

$$\text{roc} = \text{bg} - \text{isad} + \frac{4}{3} \sqrt{\text{anpe}^2 + \text{wpr}^2 + \text{fte}^2 + \text{ase}^2 + \text{vae}^2 + \text{atis}^2}$$

Three Standard Deviation Formulas for Root-Sum of Squares Computations:

The anpe: $\text{anpe} = 1.225 \cdot \text{rnp} \cdot \frac{1852}{0.3048} \cdot \tan \theta$

The wpr: $\text{wpr} = 60 \cdot \tan \theta$

The fte: $\text{fte} = 75$

The ase: $\text{ase} = -8.8 \cdot 10^{-8} \cdot (\text{elev})^2 + 6.5 \cdot 10^{-3} \cdot (\text{elev}) + 50$

The vae: $\text{vae} = \left(\frac{\text{elev} - \text{ltpelev}}{\tan \theta} \right) (\tan \theta - \tan(\theta - 0.01^\circ))$

The atis: $\text{atis} = 20$

Bias Error Computations:

The isad: $\text{isad} = \frac{(\text{elev} - \text{ltpelev}) \cdot \Delta \text{ISA}}{288 + \Delta \text{ISA} - 0.5 \cdot 0.00198 \cdot \text{elev}}$

The bg bias: Straight segments fixed values: narrow body **bg = 15**
wide body 25

RF segments: narrow body **bg = semispan · sin φ**
wide body **bg = semispan · sin φ**

Sample Calculations:

Design Variables

Applicable facility temperature minimum is 20° C below standard: (**ΔISA = -20**)

Required navigational performance (RNP) is .14 NM: (**rnp = 0.14**)

Wing semispan of 68 ft: (**semispan = 68**)

Special Aircraft and Aircrew Authorization Required (SAAAR) Fixed Values

Vertical flight technical error (FTE) of two standard deviations is assumed to be **75 ft**: (**fte = 75**)

Automatic terminal information service (ATIS) two standard deviation altimeter setting vertical error is assumed to be **20 ft**: (**atis = 20**)

The maximum assumed bank angle is **18°**: (**φ = 18°**)

Glidepath Variables

Precision Final Approach Fix Altitude (PFAF) is 4,500 ft: (**4,500ft**)

Landing Threshold Point Elevation (ltpelev): (**ltpelev = 1200**)

Threshold Crossing Height (tch): (**tch = 55**)

Glide Path Angle (θ): **θ = 3**

Calculations:

$$\text{roc} = \text{bg} - \text{isad} + \frac{4}{3} \sqrt{\text{anpe}^2 + \text{wpr}^2 + \text{fte}^2 + \text{ase}^2 + \text{vae}^2 + \text{atis}^2}$$

$$\text{anpe} = 1.225 \cdot \text{rnp} \cdot \frac{1852}{0.3048} \cdot \tan \theta$$

The anpe: $= 1.225 \cdot 0.14 \cdot \frac{1852}{0.3048} \cdot \tan 3^\circ$

$$\text{wpr} = 60 \cdot \tan \theta$$

The wpr: $= 60 \cdot \tan 3^\circ$
 $= 3.1445$

The fte: $\mathbf{fte} = 75$

The ase: $\mathbf{ase} = -8.8 \cdot 10^{-8} \cdot (\mathbf{elev})^2 + 6.5 \cdot 10^{-3} \cdot (\mathbf{elev}) + 50$

$$\begin{aligned}\mathbf{ASE}_{250} &= -8.8 \cdot 10^{-8} \cdot (\mathbf{ltpelev} + 250)^2 + 6.5 \cdot 10^{-3} \cdot (\mathbf{ltpelev} + 250) + 50 \\ &= -8.8 \cdot 10^{-8} \cdot (1200 + 250)^2 + 6.5 \cdot 10^{-3} \cdot (1200 + 250) + 50 \\ &= 59.2400\end{aligned}$$

$$\begin{aligned}\mathbf{ASE}_{\text{pfaf}} &= -8.8 \cdot 10^{-8} \cdot (\mathbf{PFAF})^2 + 6.5 \cdot 10^{-3} \cdot (\mathbf{PFAF}) + 50 \\ &= -8.8 \cdot 10^{-8} \cdot (4500)^2 + 6.5 \cdot 10^{-3} \cdot (4500) + 50 \\ &= 77.4680\end{aligned}$$

The vae: $\mathbf{vae} = \left(\frac{\mathbf{elev} - \mathbf{ltpelev}}{\tan \theta} \right) (\tan \theta - \tan(\theta - 0.01^\circ))$

$$\begin{aligned}\mathbf{VAE}_{\text{pfaf}} &= \left(\frac{\mathbf{PFAF} - \mathbf{ltpelev}}{\tan \theta} \right) (\tan \theta - \tan(\theta - 0.01^\circ)) \\ &= \left(\frac{4500 - 1200}{\tan 3^\circ} \right) (\tan 3^\circ - \tan(3^\circ - 0.01^\circ)) \\ &= 11.0200\end{aligned}$$

$$\begin{aligned}\mathbf{VAE}_{250} &= \left(\frac{250}{\tan \theta} \right) (\tan \theta - \tan(\theta - 0.01^\circ)) \\ &= \left(\frac{250}{\tan 3^\circ} \right) (\tan 3^\circ - \tan(3^\circ - 0.01^\circ)) \\ &= .8349\end{aligned}$$

The isad: $\mathbf{isad} = \frac{(\mathbf{elev} - \mathbf{ltpelev}) \cdot \Delta \mathbf{ISA}}{288 + \Delta \mathbf{ISA} - 0.5 \cdot 0.00198 \cdot \mathbf{elev}}$

$$\begin{aligned}\mathbf{ISAD}_{\text{pfaf}} &= \frac{(\mathbf{PFAF} - \mathbf{ltpelev}) \cdot \Delta \mathbf{ISA}}{288 + \Delta \mathbf{ISA} - 0.5 \cdot 0.00198 \cdot (\mathbf{PFAF})} \\ &= \frac{(4500 - 1200) \cdot (-20)}{288 - 20 - 0.5 \cdot 0.00198 \cdot (4500)} \\ &= -174.5432\end{aligned}$$

$$\begin{aligned}\mathbf{ISAD}_{250} &= \frac{250 \cdot \Delta \mathbf{ISA}}{288 + \Delta \mathbf{ISA} - 0.5 \cdot 0.00198 \cdot (\mathbf{ltpelev} + 250)} \\ &= \frac{250 \cdot (-20)}{288 - 20 - 0.5 \cdot 0.00198 \cdot (1200 + 250)} \\ &= -18.7572\end{aligned}$$

The bg: $\mathbf{bg} = \mathbf{semispan} \cdot \sin \phi$
 $= 68 \cdot \sin 18^\circ$
 $= 21.0132$

$$\begin{aligned} \text{ROC}_{250} &= \text{bg} - \text{ISAD}_{250} + \frac{4}{3} \sqrt{\text{anpe}^2 + \text{wpr}^2 + \text{fte}^2 + \text{ASE}_{250}^2 + \text{VAE}_{250}^2 + \text{atis}^2} \\ &= 21.0132 + 18.7572 + \frac{4}{3} \sqrt{54.6117^2 + 3.1445^2 + 75^2 + 59.2400^2 + 0.8349^2 + 20^2} \\ &= 189.0049 \end{aligned}$$

$$\begin{aligned} \text{ROC}_{\text{pfaf}} &= \text{bg} - \text{ISAD}_{\text{pfaf}} + \frac{4}{3} \sqrt{\text{anpe}^2 + \text{wpr}^2 + \text{fte}^2 + \text{ASE}_{\text{pfaf}}^2 + \text{VAE}_{\text{pfaf}}^2 + \text{atis}^2} \\ &= 21.0132 + 174.5432 + \frac{4}{3} \sqrt{54.6117^2 + 3.1445^2 + 75^2 + 77.4680^2 + 11.020^2 + 20^2} \\ &= 359.6163 \end{aligned}$$

Calculating the Obstacle Clearance Surface (OCS) Slope Ratio

The OCS slope is calculated by taking the difference in heights of the OCS surface at ROC_{pfaf} and ROC₂₅₀:

$$\text{OCS}_{\text{slope}} = \frac{\left(\frac{\text{pfaf} - \text{ltpelev} - 250}{\tan \theta} \right)}{(\text{pfaf} - \text{ROC}_{\text{pfaf}}) - (250 - \text{ROC}_{250})}$$

Calculating the OCS LTP to Origin Distance

The OCS origin is calculated by taking the distance from threshold of the 250 ft point of the designed glidepath and subtracting the distance along the OCS slope from zero to the ROC₂₅₀ point.

$$\text{OCS}_{\text{origin}} = \left(\frac{250 - \text{tch}}{\tan \theta} \right) - (250 - \text{ROC}_{250}) \cdot \text{OCS}_{\text{slope}}$$



U.S. Department
of Transportation

**Federal Aviation
Administration**

Directive Feedback Information

Please submit any written comments or recommendations for improving this directive, or suggest new items or subjects to be added to it. Also, if you find an error, please tell us about it.

Subject: Order 8260.RNP SAAAR, United States Standard for Required Navigation Performance (RNP) Approach Procedures with Special Aircraft and Aircrew Authorization Required (SAAAR)

To: DOT/FAA
Flight Procedure Standards Branch, AFS-420
P.O. Box 25082
Oklahoma City, OK 73125

(Please check all appropriate line items)

An error (procedural or typographical) has been noted in paragraph _____ on page _____.

Recommend paragraph _____ on page _____ be changed as follows:
(attach separate sheet if necessary)

In a future change to this directive, please include coverage on the following subject:
(briefly describe what you want added):

Other comments:

I would like to discuss the above. Please contact me.

Submitted by: _____ Date: _____

FTS Telephone Number: _____ Routing Symbol: _____