## The hybrid-isentropic grid generator in FIM

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## FIM

## short for FFFVIM

#### Flow-following / Finite-volume Icosahedral

#### Vertical grid considerations

- Geophysical fluids are "shallow" ... but still rich in vertical structure. Inadvertent vertical mixing must be avoided.
- Strong flows often occur near boundaries (top, bottom, side). Grid should provide good resolution there and make it easy to apply boundary conditions. ( $\sigma$  coordinate
- Grid points that follow vertical motion ("Lagrangian" grid) can prevent numerical dispersion during wave-induced vertical transport. (θ coordinate )
- Sloping coordinate surfaces can make it difficult to compute the horizontal pressure gradient. (*z*, *p*, or  $\eta$  coordinate )
- Fluids tend to form discontinuities (fronts). High resolution near fronts would be desirable. ( $\theta$  coordinate )

#### Lagrangian vertical coordinate: <u>Pros</u> and <u>Cons</u>

("Lagrangian" = isentropic in atmospheric applications)

Major Pros:

- Subgridscale horizontal eddy **mixing** has no false diabatic component
- Numerical dispersion errors associated with vertical transport are minimized
- Optimal finite-difference representation of frontal zones & frontogenesis

Major Cons:

- Coordinate-ground intersections are inevitable (atmosphere doesn't fit snugly into x,y,θ grid box)
- Poor vertical resolution in weakly stratified regions
- Elaborate transport operators needed to achieve conservation

#### The $x, y, \theta$ grid box



Major Cons:

- Coordinate-ground intersections are inevitable (atmosphere doesn't fit snugly into x,y,θ grid box)
- Poor vertical resolution in weakly stratified regions

Fixes:

- Reassign grid points from underground portion of *x*,*y*,*θ* grid box to above-ground "s" surfaces
- Low stratification => large portion of x,y,θ grid box is underground => no shortage of grid points available for re-deployment as "s" points

=> A "hybrid" grid appears to have distinct advantages – both from a grid-economy and a vertical resolution perspective

#### The $x, y, \theta$ grid box



Grid degeneracy is main reason for introducing hybrid vertical coordinate

"Hybrid" means different things to different people:

 linear combination of 2 or more conventional coordinates (examples: p+sigma, p+theta, p+theta+sigma)
 ALE (Arbitrary Lagrangian-Eulerian) coordinate

ALE maximizes size of isentropic subdomain

### ALE: "Arbitrary Lagrangian-Eulerian" coordinate

- Original concept (Hirt et al., 1974): maintain Lagrangian character of coordinate but "re-grid" intermittently to keep grid points from fusing.
- In FIM, we apply ALE in the vertical only and regrid for 2 reasons:
  - (1) to maintain minimum layer thickness;

(2) to nudge an entropy-related thermodynamic variable toward a prescribed layer-specific "target" value by importing fluid from above or below.

Process (2) renders the grid <u>quasi-isentropic</u>

## The FIM grid generator

#### **Design Principles:**

- Choice of  $\theta$  or pot. energy conservation
- Monotonicity-preserving (no new  $\theta$  extrema during re-gridding)
- Layer too cold<sup>1</sup> => entrain warmer<sup>1</sup> air from above
- Layer too warm<sup>1</sup> => entrain colder<sup>1</sup> air from below
- Maintain finite layer thickness near surface but allow massless layers aloft
- Minimize diurnal vertical migration of coordinate layers by keeping non-isentropic layers near bottom of air column.

<sup>1</sup>in terms of potential temperature

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• Process (2) renders the grid **<u>quasi-isentropic</u>** 











### The FIM grid generator (cont'd - 1)

- Determine how much air from the neighboring layer ("source layer") would be needed to restore target pot. temperature.
- The amount needed,  $\Delta p_{need}$ , may exceed the amount available,  $\Delta p_{avail}$ , in source layer.
- The amount ultimately transferred is  $min(\Delta p_{need}, \Delta p_{avail} \Delta p_{min})$ .
- The minimum thickness  $\Delta p_{min}$  is prescribed.

#### The FIM grid generator (cont'd - 2)

- The condition  $\Delta p_{need} > \Delta p_{avail}$  typically occurs under the following conditions:
  - receiving layer is much warmer that target
  - restoration to target pot. temperature requires more mass from source layer than is available.
- The likelihood for this to happen is greatest at low latitudes immediately above the surface
   => low-latitude near-surface layers are more likely to end up with constant thickness than layers elsewhere.

### The FIM grid generator (cont'd - 3)

- Major challenge: achieve smooth lateral transition between prescribed-thickness and isentropic segments of a coordinate layer.
- Goal: avoid sideways-looking algorithms, i.e., accomplish transition through clever vertical re-gridding alone.
- Solution (at least a step in the right direction): employ a "cushion" function. Details of the algorithm are as follows ....

#### The FIM grid generator (cont'd - 4)

- The cushion function, which sets the final thickness of the source layer,
  - leaves large positive  $\Delta p$  values unchanged:  $cush(\Delta p) = \Delta p \quad (\Delta p_{need} << \Delta p_{avail})$
  - returns a (small) constant value if  $\Delta p$  is large negative:  $cush(\Delta p)=const.$  ( $\Delta p_{need} >> \Delta p_{avail}$ )
  - links the two cases above by a smoothly varying function for intermediate values of  $\Delta p$ .





source: /tg2/projects/fim/bleck/trunk/FIMrun/fim5 50 4 1779881/

# Continuity equation in generalized ("s") coordinates



prognostic eqns.)

$$\begin{cases} u_{t} - \eta v + \left(\dot{s}\frac{\partial p}{\partial s}\right)\frac{\partial u}{\partial p} = -\frac{\partial\left(M + V^{2}/2\right)}{\partial x} + \Pi\frac{\partial \theta}{\partial x} \\ v_{t} + \eta u + \left(\dot{s}\frac{\partial p}{\partial s}\right)\frac{\partial v}{\partial p} = -\frac{\partial\left(M + V^{2}/2\right)}{\partial y} + \Pi\frac{\partial \theta}{\partial y} \end{cases}$$
Note: no explicit mixing terms 
$$\begin{cases} \left(\frac{\partial p}{\partial s}\right)_{t} + \nabla_{s} \cdot \left(\vec{V}_{h}\frac{\partial p}{\partial s}\right) + \frac{\partial}{\partial s}\left(\dot{s}\frac{\partial p}{\partial s}\right) = 0 \\ \left(\theta\frac{\partial p}{\partial s}\right)_{t} + \nabla_{s} \cdot \left[\left(\vec{V}_{h}\frac{\partial p}{\partial s}\right)\theta\right] + \frac{\partial}{\partial s}\left[\left(\dot{s}\frac{\partial p}{\partial s}\right)\theta\right] = \frac{\partial p}{\partial s}\frac{\dot{H}}{C_{p}T} \\ \frac{\partial M}{\partial \theta} = \Pi \qquad where \quad \Pi = c_{p}(p/p_{0})^{R/c_{p}}, \quad M = gz + \Pi\theta \\ \left(q\frac{\partial p}{\partial s}\right)_{t} + \nabla_{s} \cdot \left[\left(\vec{V}_{h}\frac{\partial p}{\partial s}\right)q\right] + \frac{\partial}{\partial s}\left[\left(\dot{s}\frac{\partial p}{\partial s}\right)q\right] = Source \end{cases}$$

## **Closing remarks**

- After some startup problems, the ALEbased grid generator meets design criteria and is working well.
- Vertical advection terms in FIM can be evaluated in several ways. We presently use the conservative, monotonicitypreserving, unconditionally stable piecewise linear method (PLM).
- In light of FIM's future use as an AGCM, all transport & mixing algorithms are conservative (a step up from RUC).