IN-DEPTH SURVEY REPORT:

CONTROL TECHNOLOGY FOR MANUAL TRANSFER OF CHEMICAL POWDERS

AΤ

The B.F. Goodrich Company Marietta, Ohio

REPORT WRITTEN BY: Michael G. Gressel William A. Heitbrink James D. McGlothlin Thomas J. Fischbach

> REPORT DATE: December 1985

REPORT NO.: 149-33

NATIONAL INSTITUTE FOR OCCUPATIONAL SAFETY AND HEALTH Division of Physical Sciences and Engineering Engineering Control Technology Branch 4676 Columbia Parkway Cincinnati, Ohio 45226

PLANT SURVEYED:

B.F. Goodrich

Industrial Plastics Division

Marietta, Ohio

SIC CODE:

3079 Miscellaneous Plastics Products

SURVEY DATE:

December 9-12, 1985

SURVEY CONDUCTED BY:

William A. Heitbrink Michael G. Gressel James D. McGlothlin

EMPLOYER REPRESENTATIVES CONTACTED:

Mr. David W. Smith Safety Manager

Walter A. Wegmiller

Senior Shift Superintendent

Sam Kiggans

Senior Shift Foreman

EMPLOYEE REPRESENTATIVES CONTACTED:

Gary Secoy

Vice-president ICW Local 343

Elmer Gourly

Union Steward ICW Local 343

ANALYTICAL WORK PERFORMED BY:

Utah Biomedical Test Laboratories

Abstract

Fast studies have shown that ventilation provides incomplete dust control during weigh-out and transfer of powders. A field study was conducted in a plastics manufacturing plant to evaluate sources of worker dust exposure at a ventilated booth which was used for the weigh-out and transfer of powdered materials from a large drum to small bags. Real-time air sampling, short-term air sampling, and an ergonomic evaluation was performed to determine activities associated with dust exposure. The sources of dust exposure evaluated were: depth of scooping, clothing, worker anthropometry, work practices, blomechanics, and specific items in the worker's job cycle. An evaluation of air flow patterns at this booth revealed the presence of eddies in front of the worker and in the drum which forced dusty air into the worker's breathing zone. Real-time air sampling and work cycle evaluation showed that dust concentrations were highest when the worker was scooping material out of the drum, and these levels increased dramatically when the worker placed his breathing zone inside the drum to scoop the powder. Short-term dust sampling showed that worker and level of material in the drum significantly affected dust concentrations. Soiled clothing had no affect upon worker dust exposure. Anthropometry and work practices significantly affected the worker's dust exposure. Biomechanical analysis showed that manual lifting and transporting 50 pound bags of powdered material may increase the risk of back injury and should be controlled by administrative and/or engineering measures.

Contents

Introduction	1
Purpose of this study	1
Objectives of this survey	2
Plant and Process Description	3
Work station description	3
Dust exposure limits and possible exposure sources	
Ventilation description	7
Ergonomic Evaluation	11
Worker description	
Job description	
The work cycle	
Job description and work cycle of experienced worker	
Musculoskeletal hazards	
Methodology	21
Experimental Design	
Sampling Procedures	
Results	
Analysis of real time data	
Analysis of filter data	29
Discussion and Conclusions	38
Recommendations	40
	74
References	42
Appendices	
Appendix I - Analysis of Real Time Instrumentation Results	43
appendix 1 Aboryoto of Real lime instrumentation Results ;	73
Appendix II - Anthropometric Questionnaire	63
Appendix III - Biomechanical Strength Analysis	66
Appendix IV - Data Acquisition Program	70
whomen to note mederetern traftem total to the terms of t	, ,
Annendia V - Filter Dota and Real Time Data	94

INTRODUCTION

The National Institute for Occupational Safety and Health (NIOSH) is the primary Federal agency engaged in occupational safety and health research. Located in the Department of Health and Human Services (formerly DHEW), it was established by the Occupational Safety and Health Act of 1970. This legislation mandated NIOSH to conduct a number of research and education programs separate from the standard setting and enforcement functions carried out by the Occupational Safety and Health Administration (OSHA) in the Department of Labor. An important area of NIOSH research deals with methods for controlling occupational exposure to potential chemical and physical hazards. The Engineering Control Technology Branch (ECTB) of the Division of Physical Sciences and Engineering has been given the lead within NIOSH to study the engineering aspects of health hazard prevention and control.

Since 1976, ECTB has conducted a number of assessments of health hazard control technology on the basis of industry, common industrial process, or specific control techniques. Examples of these completed studies include the foundry industry; various chemical manufacturing or processing operations; spray painting; and the recirculation of exhaust air. The objective of each of these studies has been to document and evaluate effective control techniques for potential health hazards in the industry or process of interest, and to create a more general awareness of the need for or availability of an effective system of hazard control measures.

These studies involve a number of steps or phases. Initially, a series of walk-through surveys is conducted to select plants or processes with effective and potentially transferable control concepts or techniques. Next, in-depth surveys are conducted to determine both the control parameters and the effectiveness of these controls. The reports from these in-depth surveys are then used as a basis for preparing technical reports and journal articles on effective hazard control measures. Ultimately, the information from these research activities builds the data base of publicly available information on hazard control techniques for use by health professionals who are responsible for preventing occupational illness and injury.

Purpose of this Study

This study was conducted to evaluate sources of worker dust exposure during the weigh-out and transfer of powdered materials from bags or bins to smaller containers. The ventilation used to control dust generated by this operation appeared to contain dust within the exhaust hood. However, previous studies of these operations always involve some elevation of the worker's dust exposure. The purpose of this study is to determine why ventilation systems for weighing and transfer of powders provide incomplete dust control.

Objectives of this Survey

This survey was undertaken to evaluate dust control at weigh-out and transfer operations. The survey's primary objective was to determine whether the workers' dust exposure was elevated because of dust contaminated clothing and depth at which the worker must scoop from the drum or bin. In order to address this primary objective an ergonomic evaluation was coordinated with air sampling. In addition, real-time air sampling was conducted to identify specific worker activities which generate dust.

PLANT AND PROCESS DESCRIPTION

This plant is part of B.F. Goodrich's Industrial Plastics Division. It was built in 1947, and employs 395 workers. The plant makes a variety of PVC type products such as vinyl backed wall coverings and magnet impregnated plastic stripping. The raw materials for these products are weighed out and then charged into Banbury mixers. After mixing, the plastics are milled, then extruded or calendared into their final form.

This survey was conducted at a ventilated booth which was used to control dust generated by the weigh-out and transfer of powdered raw materials. These powders are assembled into batch lots which are charged into Banbury mixers elsewhere in the plant. During this survey, the powder handled was an acrylic copolymer manufactured by the Rhom and Haas company under the trade name Acryloid K-125 modifier.

At this booth, the worker pre-weighed small batches of the acrylic powder for use elsewhere in the plant. First, the worker emptied fifty-pound bags of powder into a drum until full. He used a scoop to transfer the powder from the drum to a tared bag. Next, he set the bag on a scale and adjusted the weight of powder in the bag. The filled bag was set in a bin behind the scale. The section dealing with ergonomics provides a more detailed description of the worker and his job cycle.

Work Station Description

All work was performed at a ventilation booth shown in Figure 1. In the middle of the "L" shaped work table, there was a hinged platform which was raised to allow a drum of raw material to be placed inside the booth. The scale was set on the work table to the left of the drum. The scale's read-out was on the left wall of the booth at about eye level. The exhaust plenum was the back wall of the booth.

Dust Exposure Limits and Possible Exposure Sources

Bag emptying, manual weigh-out and transfer of powders involves occupational exposure to an airborne dust. For the acrylic material used in this study, there are no specific occupational health standards. Therefore, the nuisance dust exposure limits are assumed to apply. A summary of dust exposure limits for such dusts in Table 1.

The bag emptying and weigh-out and transfer of powders involve a number of potential dust exposure sources which are listed in Table 2. This survey was conducted to evaluate Whether worker clothing and depth of scooping affect worker dust exposure. Because the workers' anthropometry varies, the affect of depth of scooping upon dust exposure may vary with the worker.

Emptying the fifty pound bags of powder into the drum generates a dust exposure for the worker. The dust exposure sources associated with bag

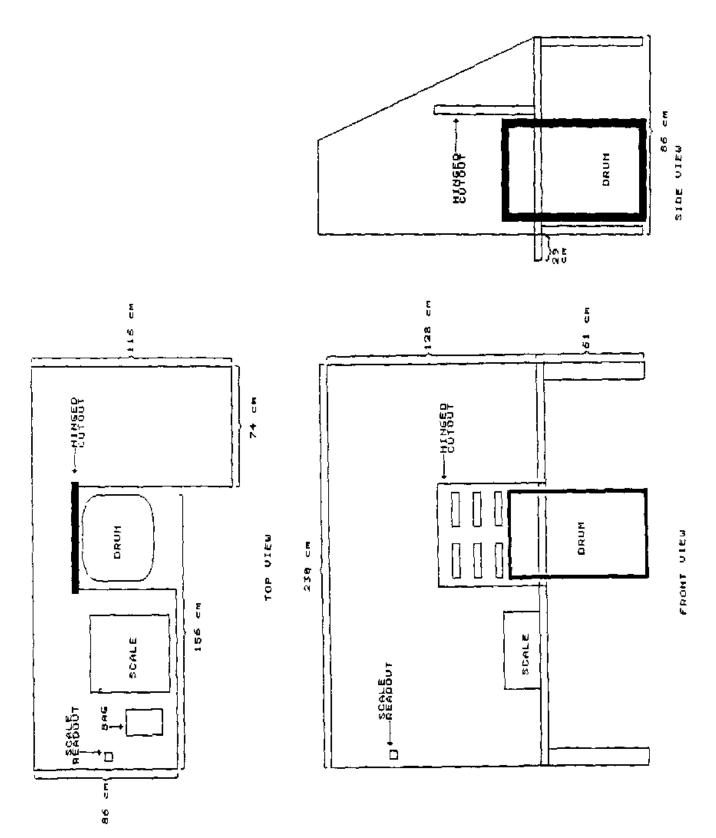


Figure 1 Hood Layout (inside dimensions)

opening include: surface contamination of the bag, opening and emptying the bag, and discarding the empty bag. These exposure sources and methods of controlling these sources of dust exposure have previously been studied and are discussed elsewhere. Table 2 lists the apparent sources of dust exposure.

Table 1. Summary of Exposure Limits

Substance	osha pel ² mg/m ³	ACGIH TLV ³ mg/m ³
Nuisance Dust-Total	15	10
Respirable Dust	5	5

Table 2. Possible Dust Exposure Sources

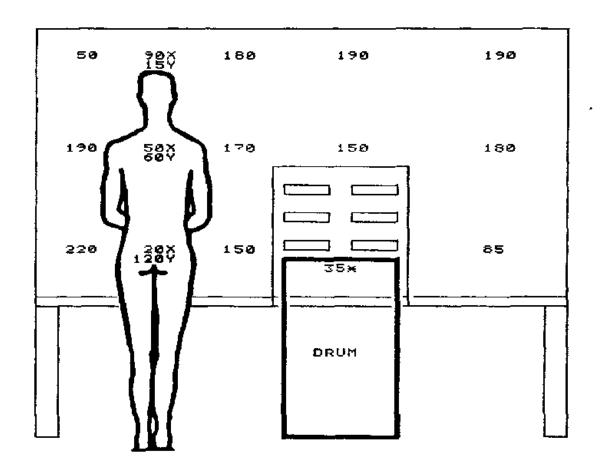
Exposure Source	Comment
Worker clothing	Manual compounding and associated activities generally result in clothing which appear to be dusty and this clothing could become a dust exposure source.
Spillage	Powdered materials are observed to be spilled during manual weigh-out operations. As a result, work surfaces are covered with dust and become sources of dust emissions. This spillage occurs because bags leak dust, scoops are too large in relation to the weigh-out bags, human error, and the handling of emptied powdered material bags.
Dusty bags	Powdered materials are frequently shipped to the plants in bags. Workers transfer materials from these bags to other containers. These bags are frequently dusty and the simple act of lifting them from a pallet to a work surface has been reported to elevate worker dust exposure. 1,4

Table 2. Possible Dust Exposure Sources (continued).

Exposure Source	Comment
Scooping	When the powdered material is stored in drums, the worker must reach into these drums to transfer the powder to a bag which rests on the scale. When the worker is transferring material from a nearly empty drum, his breathing zone is between the local exhaust ventilation and the dust emission sources.
Empty bag disposal	Frequently, workers are scooping solids from paper bags such as three ply kraft bags. When these bags are emptied, they must be discarded. Handling the dust emissions during bag disposal has been treated in a previous study. 1,4
Weigh-out and transfer	Transferring material from one container to another. This operation inevitably creates a dust which is not totally controlled by local exhaust ventilation.
Work practices	During the study of manual weigh-out and transfer operations, differences in work practices between workers may cause large variations in personal dust exposure.

Ventilation Description

The ventilated booth is used in an attempt to capture the airborne dust generated by bag emptying and the weigh-out and transfer of powders. Air flow patterns in this hood were documented by using smoke tubes to determine the direction of the air flow and using a velometer to measure the magnitude of the air flow. All measurements were made with a member of the survey team standing at the hood face, in a manner similar to the worker's normal working position. Figure 2 shows the results of the hood velocity measurements. While air velocities varied from 35 to 220 feet per minute, the direction of flow varied substantially as well. Eddies existed in several places within the hood, the most important being the one found in front of the worker as shown in Figure 3. Air was found to flow straight up the worker's body and into his breathing zone. This air current would force any dust generated close to the worker's waist to flow directly into his breathing zone. Another eddy was discovered inside the drum. The air entered the back area of the drum, moved down to the surface of the powder, and exited from the front of the drum carrying with it some of the powder. As shown in Figure 4, this stream of dusty air flowed over the hinged platform. When the worker was scooping from the bottom of the drum, his breathing zone was in this flow of dusty air.



* Velocity reading taken outside of drum.

All reading are air flow into the hood unless otherwise noted.

"X" direction is into the hood; "Y" direction is vertical.

Figure 2. Air Velocities into Weigh-out Hood

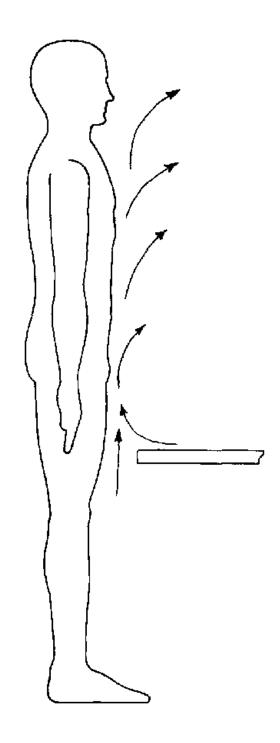


Figure 3. Eddies in Front of Worker.

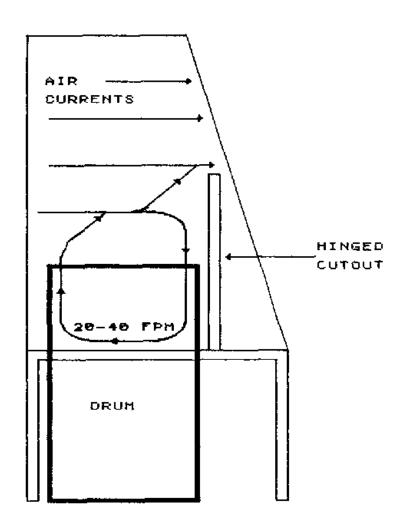


Figure 4. Eddies Due to Hinged Cutout.

Ergonomic Evaluation

Descriptive information and anthropometric measurements were taken on three workers. This data was taken to evaluate the relationship between dust exposure, worker size, and work practices.

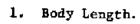
Worker Description

Figure 5 diagrams the anthropometric measurements for these workers. The descriptive and anthropometric results are summarized in Table 3. The descriptive data show that while these workers had some experienced in jobs involving materials weigh-out and transfer, it was not their regular job. The third worker was more than 25 years older than the other two workers, had the highest seniority of the three workers (31 years), and was experienced with a variety of jobs including materials weigh-out and transfer. Anthropometric measurements taken from these 3 workers show the female worker (worker #1) to be in the 30-40th percentile for stature, 5 percentile for height of hips, and 5 percentile for forward reach compared to a standard population. So worker #2 is a tall male who measured in the 90-95 percentile for all anthropometric measurements taken. The third worker was also male and measured in the 40th percentile for most anthropometric categories.

Job Description

Many powdered raw materials are received at the plant in paper bags. The acrylic copolymer powder used during this study, came in plastic lined bags weighing 50 pounds each. The bags of powder were manually lifted from a pallet, carried, and dumped into a fiber drum measuring 33 inches high and 21.5 inches in diameter. The powder was transferred from the drum to 5-pound paper bags via a hand scoop. These small bags containing powder were then weighed on a scale. Usually, two scoops of material were required to achieve the desired weight. Once filled, the bags were manually closed by folding them from the top down. After closing, the bag was placed in a large cardboard bin approximately six feet behind the worker. This fundamental work cycle was repeated until either the drum was empty or the needed number of bags had been weighed out. Occasionally (after approximately 10 bags were weighed out) the worker cleaned the scale of any spilled material by brushing it off with his hand. The worker then retared the scale using a new, clean bag.

The material being weighed in this experiment required 2.64 pounds for each batch. The work standard for this weight was 100 batches in 40 minutes. The workers received incentive pay when they exceeded this standard.



- Shoulder Height.
- 3. Hip Height.
- Shoulder Breadth.
- 5. Foreward Reach.
- 6. Elbow Height.
- 7. Underarm Height.



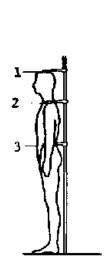


Figure 5. Anthropometric Measurements.

Table 3. Descriptive & Anthropometric Measurements.

	Worker	Worker	Worker		tion Per Male Fer	
Measurement (cm)	1	2	3	5th	50th	95th
Job Title	Utility Worker	Utility Relief	Henshaw Operator			
Gender	Female	Male	Male			
Handedness	Right	Right	Right			
Work Hand	Both	Right	Right			
Age, Years	28	30	55			
Length of Employment	8.5 yr.	9 yr.	3lyr.			
Weight, Pounds	113	161	200 (app	rox.)		
Body Length	164.6	183.7	170.1	154.4	168.0	183.0
Shoulder Height	134.5	153.4	141.1	124.8	137.4	151.7
Hip Height	96.8	111.2	99.4	94.9	103.9	113.5
Shoulder Breadth	40.6	45.9	49.4	36.3	42.3	47.8
Foreword Reach	72.4	86,5	82.9	69.1	77.9	88.8
Elbow Height	100.4	112.2	106.1	96.4	106.7	116.3
Underarm Length	38.3	46.2	43.0	31.9	36.7	41.I

The Work Cycle

A portable video tape ensemble consisting of a recorder, light-sensitive VHS tape, and camera, documented the work cycle. The work cycle was then broken down to fundamental elements as described by Gilbreth⁶ and Armstrong. The video tapes were played back in a laboratory in slow-motion and stop-action to provide detailed information on work practices, posture, and equipment. This procedure helped to determine if certain elements in the cycle could lead to increased dust exposure for the worker.

The work elements during the weigh-out and transfer process were also examined

over time to determine the effect that powder depth in the drum had on cycle times and work practices. This was accomplished by examining the video tape and taking two time measurements for removal of powder from the drum to fill bags in batch weighing process. The first time measurement was for total cycle time of the workers at three drum levels: full, 1/2 full, and near empty. The second time measurement was for time spent scooping powder from the drum. This cycle time began when the worker first grasped the scoop and ended when the worker positioned the scoop over the bag for precise weighing. Table 4 shows the results of the cycle times for different drum powder levels. Table 5 shows the results for scoop cycle times for these same levels. The basic functional elements for the right and left side of the body during the workers' work cycle are shown in Table 6. Table 7 shows the "critical" elements in the fundamental work cycle that may expose the workers to higher levels of dust relative to other elements in the work cycle.

Table 4. Fundamental Cycle Times for Drum Powder Levels (seconds).

Worker	mean	FULL s.d.**	n*	mean s	1/2 FULL	ı	mean s	MPTY .d.	n
1	18.99	1.21	2	_	-	_	22.72	2.26	6
2	-	-	-	29.59	3,29	6	37.88	1.57	5
3	22,55	2.69	6	22.48	1.16	6	26,55	2.37	6

^{*} n - number of samples

Table 5. Scooping Cycle Time for Drum Powder Levels

Worker		FULL		1,	/2 FULL		El	PTY	
	цеац	s.d.	C.V.	mean	s.d.	C.V.	mean	s.d.	C.V.
1	6.43	0.14	2	_	_	-	7.53	0.81	6
2	-	-	-	10,51	2,32	6	10,43	1.28	5
3	6.05	0.50	6	7.17	0.48	6	9.19	0.76	6

^{**} s.d. - standard deviation

Table 6. Fundamental Work Cycle Elements.

Left Side	Side Right Side			
1. Reach for Bag	1. Idle			
2. Grasp Bag	2. Idle			
3. Open Bag	3. Idle			
4. Move Bag over Drum	 Reach for Scoop 			
5. Position Bag over Drum	Load Powder on Scoop			
6. Hold Bag	6. Move Scoop to Bag			
7. Hold Bag	Dump Powder from Scoop to Bag			
8. Move Bag to Scale	8. Hold Scoop			
Position Bag on Scale	9. Move Scoop			
10. Release Bag, Inspect Scale	10. Hold Scoop			
11. Hold Bag	ll. Position Scoop over Bag			
12. Hold Bag	 Add or Remove Powder from Bag with Scoop or Hand 			
13. Release Bag	13. Move Scoop to Drum			
14. Idle, Inspect Scale	14. Release Scoop in Drum or on Table			
15. Grab Bag	15. Grab Bag			
l6. Fold Bag	16. Fold Bag			
17. Release Bag	17. Grab Bag			
18. Idle	18. Move Bag into Shipping Bin			
1 9. Idle	19. Position Bag in Shipping Bin			
20. Move to Booth	20. Move to Booth			

Table 7. Critical Elements in the Work Cycle Which May Increase Dust Exposure.

Side/Element (L=left,R=right)

Comment

- L 3 The worker opens the paper bag by "flicking" his wrist to force air into the bag to open it. This technique is an efficient time saver but may generate residual airborne dust from the surrounding work station.
- R 5,6,7 Scooping powder, moving the powder to the bag, and dumping the powder into the bag may cause significant airborne dust exposure. Dust exposure may be caused by a combination of mechanical transfer of dust from the 55-gallon drum to the bag and the proximity of the worker's breathing zone being near the transfer process. As the drum is emptied the worker has to reach deeper into the drum to get the powder. During this reaching process he partially puts his head into the drum to retrieve the material. Because the drum is an unventilated confined space, it is hypothesized that dust exposure may increase as the drum is emptied by the worker.
- L,R 16 Folding the bag pleats and closing the filled paper bag causes residual air and dust to rapidly escape from the bag. This process forms a small but visible dust "cloud" which migrates toward the worker's breathing zone.

Job Description and Work Cycle of Experienced Worker

In the course of performing this survey, a highly experienced worker was observed at another manual weigh-out station. His actions were recorded on video tape to compare his work practices and cycle times to those of the three workers studied. No anthropometric measurements were made on this worker. Table 8 shows the experienced worker's cycle time, and standard deviation, for a similar weigh-out and transfer job. Table 9 shows the elements which comprised this workers basic work cycle. While a smaller weight of material was required, (1.2 pounds versus 2.6 pounds) the batch weighing and material transfer process was similar. The cycle time for this worker was approximately 66 percent less compared to the the average cycle time for the 3 workers above. This difference was primarily the result of efficient work practices and motion economy which eliminated several nonproductive steps. These step saving practices were the result of a worker configured work station where all materials required to perform the weigh-out and transfer process were within

Table 8. Basic Cycle Time for Experienced Worker (seconds).

Work Cycle Time	Standard Deviation	Sample Size
5,35	0.82	5

Table 9. Fundamental Work Cycle Elements
Experienced Worker.

Left Side		R	ight Side
1.	Move hand to bag	1.	Hold scoop
2.	Reach for bag	2.	Hold scoop
3.	Grasp bag	3.	Move scoop to drum
4.	Flick open bag	4.	Position scoop in drum
5.	Idle	5.	Use scoop
6.	Move bag to scale	6.	Move scoop to scale
7.	Position bag on scale	7.	Position scoop over bag
8.	Hold bag	8.	Pour scoop contents into bag
9.	Idle (inspect scale)	9.	Hold scoop
10.	Grasp bag	10.	Hold scoop
11.	Move bag to receiving drum	11.	Hold scoop
12.	Inspect drum (see where to drop bag)	12.	Hold scoop
13.	Position bag	13.	Hold scoop
14.	Release bag	14.	Hold scoop

easy reach. Specific step saving practices included simultaneous use of both hands (the left hand to grab a bag while the right hand reached and scooped powder material), precision weighing of powder into the bag by careful scoop pouring while inspecting the weigh scale, and not folding the bags before putting them into the receiving drum (since the bags were bottom heavy there was no need to fold the bags to secure the powder contents). Because of other job demands, no personal dust measurements could be taken on this worker.

Musculoskeletal Hazards

There appeared to be two types of musculoskeletal hazards involved with this job. The first hazard was the method used by most of the workers to open the small bags for receiving raw material. These workers opened the bags by holding them by a flap and giving them a flick of their wrist. This type of motion may cause wrist and/or elbow tendonitis. The other musculoskeletal hazard was manual lifting and transfer of 50 pound bags of powder from the wooden pallets and carrying them to the fiber drums. Risk factors for manual lifting include weight lifted, size of the load, and frequency of lift. Personal risk factors include gender, age, anthropometry, lift technique, and strength. Because the bulk density of this material was 1.1 g/cc, the bags were large and awkward to handle. Lifting of heavy weights at a distance from the body may cause back injury.

To determine the degree of biomechanical stress during the lift and transfer process, the moment-arms of the body segments were calculated using "frozen" posture angles from the plant videotapes and a software program developed by the University of Michigan, Center for Ergonomics. 8 The anthropometric, posture, and load handling information were coded into a microcomputer Which calculated estimates of the resultant forces and torques created by the load at the hand(s) for the elbows, shoulders, L5/S1 spinal disk, hips, knees, and ankles. In the sample analysis performed here, worker #3 (male) was evaluated for manually lifting a 50 pound bag of powder and transporting it to the drum. Figure 6 shows the worker postured to "pull" the bag closer to his body before lifting. Here, the elbow was the limiting joint for performing this type of movement. This worker appeared very strong and had no difficulty in pulling the load closer to the body before lifting. For the majority of the population, however, there is a significant limitation in the elbow joint for pulling a 50 pound load closer to the body (3% of females capable). This can be a limiting factor when recommending manual material movement techniques. This pull task does not result in any compressive loading of the back. Figure 7 shows the worker postured to lift this load from the pallet. Nearly 90% of average (50 percentile) male and female workers are capable of lifting this 50 pound bag in this posture. 5 Compressive forces for the back, as computed from the posture recorded on video tape, are 4342 Newtons (976 pounds) for average size males and 3613 Newtons (812 pounds) for average size females. The NIOSH Work Practices Guide for Manual Lifting indicates that these back compressive forces may result in an overexertion back injury if not controlled administratively or through engineering controls. [The Work Practices Guide recommends administrative controls when back compressive forces exceed the action limit of 3425 Newtons (770 pounds), and engineering controls when back compressive forces exceed the maximum permissible limit of 6361 Newtons (1430 pounds)]. Work practices and lifting techniques play a large role in limiting the risk for back injuries. To demonstrate this point, calculations were performed for this worker lifting a 50 pound bag at the initial contact point (Figure 6). A high percentage of both male and female employees are capable of lifting such a load, however, the back compressive forces increases to 5456 Newtons (1227 pounds) for the average male and to 4626 Newtons (1040 pounds) for the average female. This is an increase of more than 1000 Newtons for such a subtle difference in lift angle. The workers involved in heavy materials handling should be aware of the subtle but effective techniques for lifting to prevent back injuries.

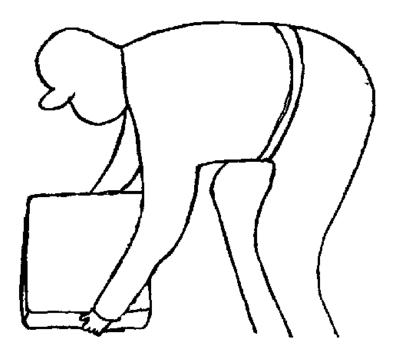


Figure 6. Worker in "Pulling" Position.



Figure 7. Worker in Lifting Position.

METHODOLOGY

Experimental Design

This survey was conducted to evaluate the effects of both dusty clothing and depth of scooping from the drum on the worker's dust exposure. Two hypotheses, therefore, were evaluated and are stated as follows:

- 1. Dusty clothing affects the worker's dust exposure.
- 2. The depth from which the worker scoops powder affects his dust exposure.

A 2x2 factorial experiment with 6 replications was conducted to evaluate the effects of clothing and depth of scooping upon dust concentration. A total of 24 gravimetric runs were conducted over a three day period using a different worker each day. Four runs were conducted in the morning and four in the afternoon. Of these groups of four, one run would look at scooping from the bottom of the drum with clean clothing, one at scooping from the bottom with dirty clothing, one at scooping from the top with dirty clothing, and one at scooping from the top with clean clothing. The dirty clothing used was the worker's own coveralls in which he performed some operations which were considered dusty, such as emptying a bag of powder into the drum. The clean clothing consisted of disposable coveralls which were used once and then discarded. A drum was considered full if it was two thirds or more full and considered empty if one third or less remained in the bottom.

In addition to the gravimetric air sampling, the effect of depth of scooping on dust concentration was further evaluated using real-time instrumentation. A single worker (worker 3) was used to perform this portion of the experiment. It was conducted with dirty clothing and began with a full drum. The worker weighed out material until the drum was nearly empty. During this period, the real-time instruments monitored the respirable dust concentration.

Sampling Procedures

The equipment used in this study is listed in Table 9. For the gravimetric method, air was drawn through a filter and critical flow orifice by a carbon vane pump. The filters were MSA type FWSB 37-millimeter with 5.0 micron pore size which is mounted mounted in a filter cassette. The critical orifices were calibrated at 14-16 liters of air per minute. The filters were connected to the orifices with Tygon tubing and a lure which fastened to the filter cassette. While in the field, flow rates of several of the filters were checked. Because of some variation in the flow rates, all of the filters used were checked in the laboratory for flow rate and pressure drop across the filter. The apparatus used to measure the flow rate and pressure drop is shown in Figure 8. All orifices were calibrated at atmospheric pressure. However, in the field, the pressure at the orifice differed from atmospheric by the pressure drop across the filter. Because the flow rate through a critical orifice is proportional to the upstream absolute pressure 10, the

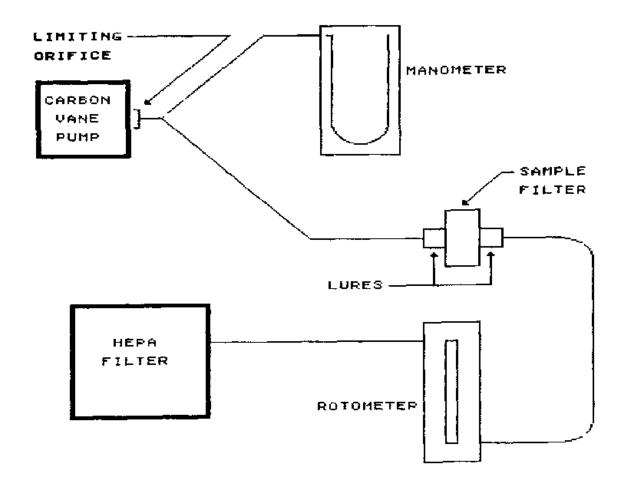


Figure 8. Filter Flow Calibration Assembly.

Table 9. Equipment List

Item	Use
GCA Real-Time Aerosol Monitors-2 (RAM)	Respirable dust monitoring at fixed locations.
PPM Hand-Held Aerosol Monitor (HAM)	Respirable dust monitoring on worker.
Carbon Vane Pumps 15 1pm at 20 inches of Hg vacuum	Sampling of total dust.
MSA Model G Pumps 1.7 1pm	Active sampling for the HAMs.
Video Camera and Recorder with:	Recording of events during real-tim sampling.
Time input including minutes and seconds	
Automatic focus and zoom lense	
TSI Air Velocity Meter	Measuring hood face velocity.
Apple II Plus computer equipped with:	Record analog output of RAMs, HAMs, and event marking switches.
dual disk drives	
AI 13 Card (Interactive Structures)	Analog to digital conversion.
The Clock Card (Mountain Computer)	Internal clock for computer.
Anthropometric Equipment Kit	To take anthropometric measurements of subject workers.

flow rates were corrected for the effect of this pressure loss by using the following equation:

$$Q1 = Q2 (P1 - P2) / P1$$

where, Q1 is actual flow, Q2 is calibrated flow, P1 is atmospheric pressure, and P2 is the filter pressure loss.

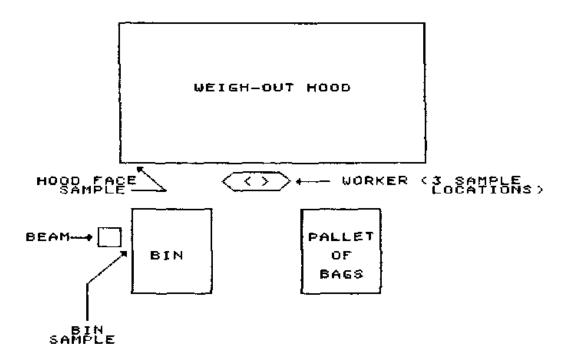
Table 10. Air Sampling Locations
Gravimetric Method

Location Number	Location Description	Comment
1	Stand 28 ft. from hood face	Background sample.
2	I-beam 5 ft, from hood face	Over bin sample.
3	Hood face	1 ft. below worker's head on left wall of hood.
4	Worker's hat	On top of hat.
5	Left worker's lapel	Used on all runs.
6	Right worker's lapel	Not used on first 4 runs.

Just prior to the beginning of a run, all the necessary filters were fastened into place. A run generally last 10 to 20 minutes and usually involved the filling of 24 to 36 bags at 2.64 pounds per bag. The total bags filled along with the total run time, the orifice and calibration flow rate, and the filter number were recorded. Halfway through the run, the drum being used would have to be replaced by another which was full (or one third full). This transfer was never done by the subject worker, but rather by the survey team. At the end of a run the pumps were turned off and the filters recapped. At this point a new set of filter would replace the used ones, and a new run would begin. Gravimetric air sampling locations are given in Table 10 and diagrammed in Figure 9.

For the real-time analysis, two types of instruments were used: HAMs (hand-held aerosol monitor) and RAMs (real-time aerosol monitor). Two RAMs were used, one for background dust and one for dust within the hood, while one HAM was used for monitoring the worker's breathing zone dust concentration. Real-Time sampling locations are given in Table 11.

The RAM's and the HAM's use forward-scattered light to precisely monitor respirable dust concentrations. The instrument's manufacturer claims that the monitors' precision is better than 0.1% full-scale. Calibration curves generally have correlation coefficients better than 99%. However, the instruments calibration does depend upon the aerosol. Rubow and Marplell noted that for two coal dust test aerosols, there was a 20% difference in the slope of the calibration curve. This study bases conclusions upon measuring concentration difference to determine what increases concentration. As long as weighing out the powder does not change its optical properties, the slope of the calibration curve will not change and the study's ability to detect concentration differences will be unaffected.



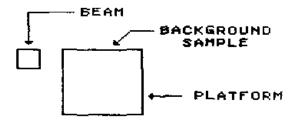


Figure 9. Filter Sample Locations.

The RAMs' and the HAM's analog output were connected to an Apple II Plus computer through an AI 13 analog to digital converter. The computer was programmed to convert these digital signals to voltage values. The computer was further programmed to take readings every two seconds and to store these values in several data files. Each data file contained 100 readings, and it took the computer 30 to 60 seconds to write the readings to the disk. During this time, the computer would not take any readings, so the worker was instructed to stop work until the computer was finished writing the disk. The internal clock of the computer was synchronized with the clock on the video camera. This enabled the video to be viewed along side the computer output and to see what the dust exposure is for any given movement by the worker. This experiment lasted about 22 minutes with 56 bags of powder weighed out. Before the experiment was conducted, the worker emptied three bags of powder into the drum. The experiment was terminated when there was very little powder left in the drum.

Table 11. Sampling Locations Real-Time Sampling

Location Number	Location Description	Comment
1	10 feet from hood face	RAM, background sample.
2	Beside the scale	RAM, interior of hood.
3	Worker's left lapel	HAM, worker breathing zone.

Results

The air sampling data were statistically analyzed to determine which factors affect dust generation. The short term dust samples were analyzed to determine whether worker, clothing, depth of scooping, and sampling location affected dust concentrations. Measurements taken with the HAM and the two Ram's were analyzed to study the association between the analog output of the Ham and the individual components of the job.

Analysis of Real Time Data

The analog output of the real time instrumentation mounted at the locations described in Table 11 were statistically analyzed to resolve two issues:

- 1. How much powder can the worker remove from a full drum before his dust exposure, as measured by the HAM, increases?
- 2. Which components of the worker's job contribute to his dust exposure?

The details of this statistical analysis are summarized in Appendix 1. The analysis involved fitting the analog data to a model which included autoregressive terms and structural terms.

A key assumption in data analysis is the independence of measurements. 12
The autoregressive terms are needed because the successive readings of the instrument response are not independent. This lack of independence is caused by the dynamics of the situation. When a dust generating event occurs, dust concentrations do not increase immediately; transportation time is needed for the air to move the dust cloud from the point of generation to the inlet of the instrument. For example, dust generated by scooping the powder out of the drum will travel 1 to 2 feet in air which is moving at a speed of 0.5 to 1 feet per second. Once, the air arrives at the inlet to the instrument, it is sampled. The instrument was used with a time content of 1 second which implies that the instrument will require 2-3 seconds to complete 90 % of its respond to a step change in concentrations. 13 As a result, instrument response could lag dust generating events by 2-5 seconds. This suggests that autoregressive terms are needed in the analysis.

The model's structural terms included parameters describing the number of bags which have been weighed-out and the specific task that the worker was doing. These tasks were:

- 1. Scooping. During this task, the worker removed material from the drum and poured it into the bag.
- 2. Weighing. Adjusting the final weight of the material in the bag.
- 3. Turning. Placing the bags into the bin.

The data is listed in Appendix V; a plot of the predicted values using the

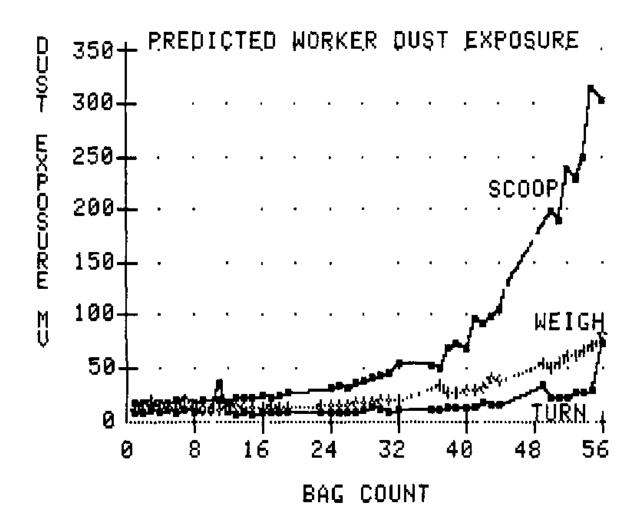


Figure 10. Predicted response of HAM in millivolts plotted as a function of bag count for scooping, weighing and turning. The readings plotted are the last reading taken while scooping, weighing and turning for each bag.

model is shown in Figure 10. This figure shows that the worker's dust exposure (the analog output of the HAM) increased while the worker is scooping. During weighing and turning, the worker's dust exposure either remains constant or fails to increase as fast. Figure 11a, the selected real-time data, and Figure 11b, the selected predicted data, show this through the direction of the slope of the curves during scooping weighing and turning. A positive slope indicates an increase in worker dust exposure, while a negative slope indicates a decrease.

This suggests the most of the workers dust exposure is caused by the scooping of the power from the drum. Dust exposures caused by weighing and turning are either controlled by the ventilation system or are much smaller than the dust exposures caused by scooping. The HAM response during the weighing activity appears to be associated with higher dust exposure than the turning activity. The scooping activity causes an order of magnitude increase in the worker dust exposure and several seconds are required for the instrument's response to reach steady state. Possibly, the difference in exposure between weighing and turning is an artifact caused by the high dust exposures during scooping. However, it is just as possible that weighing contributes to the worker's dust exposure and the difference between the turning and weighing is real.

Analysis of the Filter Data

Statistical analysis of the dust concentration data was conducted to address the study's hypothesis:

Dusty clothing and the level of material in the drum affect the worker's dust exposure.

To address the hypothesis, a factorial experiment was conducted which involved the following variables:

Clothing. The worker wore either dirty work clothing or clean Tyvek clothing.

Drum. The worker scooped material from either the bottom third of a drum or from the top third of the drum.

Location. The sampling locations in Table 10.

Worker. The three workers who worked at the booth.

The concentration data was analyzed as if it were a full factorial experiment involving the four variables listed above. Before analysis, the natural logarithms of the concentrations were taken. The SAS General Linear Models Procedure was used to perform the analysis of variance, while multiple comparison tests were used to examine differences between treatment means. 14

The pressure loss through the filter may have induced some bias in the analysis of the data. As a result, the statistical analysis was done with both censored and uncensored data. Data was censored by deleting data records

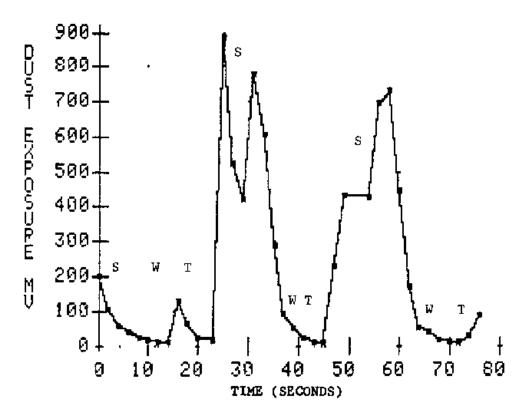


Figure 11a. Actual Real-time Data for Bags 51 Thru 53. S-Scooping, W-Weighing, T-Turning.

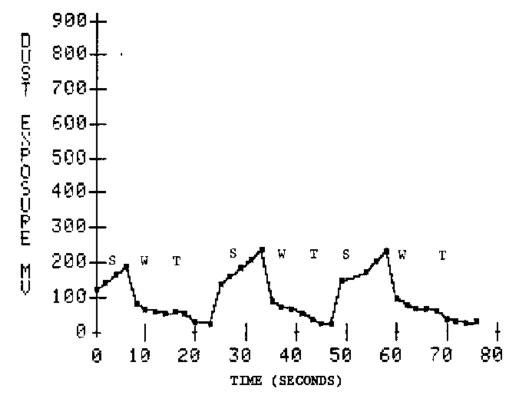


Figure 11b. Predicted Real-time Data for Bags 51 Thru 53. S-Scooping, W-Weighing, T-Turning.

which had pressure losses greater than 48 inches of water and filter weight gains of less than 2 milligrams. Filters with weight gains in excess of 2 milligrams could have increased pressure losses due to loading. For example, three filters had weight gains of over 50 milligrams and pressure losses in excess of 50 inches of water.

Generally, censoring the data did not have a major impact upon the conclusions drawn from the statistical analysis. In some cases, the probabilities associated with interaction terms in the analysis of variance shifted. The data was quite variable. Adjusting the flow rates for the measured pressure loss involved as much as a 20% adjustment in the volume. At worst, the error in the sample volume and computed concentration is 20%. This error is small compared to the errors estimated in the analysis of variance. The geometric standard deviation computed from the mean square error of the analysis of variance was 3. For such data, the two standard deviation limits were one-ninth to nine times the geometric mean.

For both the censored and uncensored data, an analysis of variance showed that location, worker, and depth of scooping from the drum significantly affected concentration. The terms involving the workers' clothing do not appear to affect concentration. As a result, clothing was excluded from subsequent analyses. The results of the analysis conducted for the censored and uncensored data are listed in Table 12.

Table 12. Analysis of Variance Conducted to Evaluate Whether Clothes Affected Concentration

Source of variation	degrees of freedom	Probability of seeing such large differences due to chance	
		Uncensored data	Censored data
location	5	0.0001	0.0001
worker	2	0.0016	0.087
d rum	1	0.0007	0.0026
clothes	10	0, 92	0.54
drum-clothes interaction	1	0.35	0.35
location-clothe	s 5	0.66	0.82
degrees of free for error	dom	123	98

For both the censored and uncensored data, the total dust concentration data was analyzed as if it were a full factorial experiment involving sampling location, worker, and depth of scooping from the drum. The results of the analysis of variance is shown in Table 13. With the exception of the location-worker interaction, separate analysis of the censored and uncensored data leads to the same conclusions. Both analyses show that the height of material in the drum had a very significant affect upon concentrations. In addition, the drum-location interaction and the drum-worker interaction are significant. This implies that the effect of level of material in the drum varies with the sampling location and the worker. As a result, the separate statistical analyses were conducted for the different levels of material in the drum.

Table 13. Analysis of Variance For Complete Data Set.

ource of ariation	Degrees of Freedom	Probability of seeing such large differences due to chance		
		Uncensored data	Censored data	
ocation	5	0.0001	0.0001	
orker	2	0.0001	0.0001	
rum	1	0,0001	0.0001	
ocation-worker nteraction	10	0.0077	0.18	
rum-worker nteraction	2	0.008	0.0017	
ocation-drum nteraction	5	0,0017	0.016	
ocation-drum- orker nteraction	10	0.2	0.5	
egrees of freed or error	om	103	78	

When the drum was full, an analysis of variance summarized in Table 14 showed that both sampling location and worker affected dust concentrations. Multiple range tests were conducted to examine differences in concentration due sampling location and worker. As shown in Table 15, the samples collected on the worker's were significantly higher than the area sampling results. Table 16 summarizes the affect of worker upon the geometric mean dust concentrations based upon all sampling locations. Worker 3, who is more experienced, had lower dust exposures than the other two workers.

Table 14. Summary of Analysis of Variance Concentrations When Drum is Full.

rce of riation	degrees of freedom	Probability of seeing such large differences due to chance			
		Uncensored data	Censored data		
location	5	0.0001	0,0001		
worker	2	0.004	0.018		
location-worker interaction	10	0.07	0.5		
degrees of freedom for the error term		51	41		

Table 15. Comparison of Total Dust Concentrations by Location When Drum is Full.

ocation	Unce	nsore	data .			red Data
	GM (mg/m ³)	N 	Grouping*	GM mg/m ³)	N 	Grouping*
Right lapel of work	er 16	10	A	16	10	A
Left lapel of Worker	r 5	12	В	7.6	10	A,B
Worker's hat	2	12	В	4.6	9	В
Bin	0.47	12	С	0.43	10	C
Background	0.41	12	С	0.43	11	С
Face of hood	0.3	11	С	0.33	9	С

^{*-}The grouping is based upon the Waller-Duncan multiple comparison test. This test is conducted at approximately an overall level of confidence of 95%. Means which have the same letter do not differ significantly.

GM - Geometric Mean

N - Number of samples

Table 16. Comparison of Geometric Mean Dust Concentrations by Worker When Drum is Full.

Worker	Uncensored data Censored Data				ta į	
	GM (mg/m ³)	n	Grouping*	GM (mg/m ³)	N	Grouping*
2	2,3	24	A	2.8	22	A
1	1.9	21	A	2.1	20	A
3	0.73	24	В	0.9	17	В

^{*-}Grouping is Based upon the Waller-Duncan multiple comparison test. Geometric Means with different letters differ significantly.

When the drum was less than one third-full, an analysis of variance summarized in Table 17, showed that sampling location and worker had a significant affect upon dust concentration. As shown in Table 18, samples collected on the worker were much larger than samples collected at fixed locations. Table 19 shows the effect of the worker upon the geometric mean dust concentrations. Worker 2, who had longer body dimensions than the other two workers, had significantly lower dust concentrations than the other two workers.

Table 13 indicates that there is a significant drum-sampling location interaction and worker-sampling location interaction. This indicates that there are significant differences in the geometric mean concentrations between Table 15 and Table 18. Apparently, the workers' dust exposure, as measured by the three personal samples are increased by scooping powder from the bottom third of the drum. The worker-drum interaction in Table 13 indicates the effect of height of material in the drum varied with the worker. Comparing Tables 16 and 19, the dust concentrations measured by worker 2 were apparently unaffected by the level of material in the drum. In contrast, scooping material from the bottom of the drum appears to increase the dust concentrations experienced by workers 1 and 3.

In the preceding analysis, the effect of worker is treated as an experimental block. The workers were tested only one day a piece. As a result, any worker differences may be confounded with conditions in the plant which may have changed from day to day. Because the preceding analysis showed worker to be a significant factor, statistical analysis, presented in Appendix I, was performed on the personal sampling data. An analysis of variance showed that worker, level of material in the drum, and the interaction between these two variables were statistically significant at a level of confidence greater than 95%. Table 20 shows how level of material in the drum affected each worker's dust exposure. The significance of the difference was estimated using linear contrasts.

Table 17. Summary of Analysis of Variance Concentrations When Drum is Empty.

Source of variation	degrees of freedom	Probability of sec differences due to	_
		Uncensored data	Censored data
location	5	0.0001	0.0001
worker	2	0.0018	0.0013
location-worker interaction	10	0.03	0.12
degrees of freedom for the error term		52	37

Table 18. Comparison of Total Dust Concentrations by Location When Drum is Empty.

Uncensored Data			Censored Data		
GM (mg/m ³)	n	Grouping*	GM (mg/m ³)	N	Grouping*
54	10	A	57	10	A
26	12	В	31	11	A
7.9	12	С	12	7	В
0.48	12	D	0.74	7	С
0.42	12	D	0.46	9	С
0.33	12	D	0.43	11	C
	GM (mg/m ³) 54 26 7.9 0.48 0.42	GM (mg/m ³) 54 10 26 12 7.9 12 0.48 12 0.42 12	GM (mg/m ³) 54 10 A 26 12 B 7.9 12 C 0.48 12 D 0.42 12 D	GM (mg/m ³) 54 10 A 57 26 12 B 31 7.9 12 C 12 0.48 12 D 0.74 0.42 12 D 0.46	GM (mg/m ³) 54 10 A 57 10 26 12 B 31 11 7.9 12 C 12 7 0.48 12 D 0.74 7 0.42 12 D 0.46 9

^{*-}The grouping is based upon the Waller-Duncan multiple comparison test. Means which have the same letter do not differ significantly.

Table 19. Comparison of Geometric Mean Dust Concentrations by Worker When Drum is Empty.

Unce	nsored	data	Cens	ored	Data
GM (mg/m ³)	N	Grouping*	GM (mg/m ³)	Ň	Grouping*
3.9	22	A	5.6	17	A
2.7	24	AB	4.9	17	A
2.1	24	В	2.3	21	В
	3.9	3.9 22 2.7 24	3.9 22 A 2.7 24 AB	3.9 22 A 5.6 2.7 24 AB 4.9	2.7 24 AB 4.9 17

^{*-}Grouping is Based upon the Waller-Duncan multiple comparison test. Geometric Means with different letters differ significantly.

Table 20. Effect of Level of Material in Drum upon Geometric Mean of Personal Dust Exposure.

Worker	Drum Con	ndition	Significance of
	Empty	Ful1	Difference
1	49	8.0	0.2
2	14	14	0
3	16	1.4	0.006

Discussion and Conclusions

The two hypotheses, dusty clothing effects worker dust exposure and the depth of scooping from the drum effects worker dust exposure, were evaluated. After analysis of the data collected, the workers' dust exposure when wearing clean clothing was not significantly different from the exposure when wearing dirty clothing. Dusty clothing had no appreciable affect on the worker's dust exposure. The polyethylene-lined plastic bags and limited contact with heavy materials handling during experiment may have limited this type of exposure.

Depth of scooping from the drum, however, significantly affected the workers dust exposure. Depending upon the worker, scooping from the bottom of the drum increased the dust exposure. There appeared to be a possible relationship between the workers size and his dust exposure when scooping from the bottom of the drum. For the tallest worker, there was no significant difference between scooping from the bottom or the top of the drum. The shortest worker, though, had the greatest increase in dust exposure when scooping from the bottom versus the top. Because of the short worker's small arm length, she had to get her face closer to the drum in order to scoop from the bottom.

Work practices may also play a part in worker dust exposure during manual weigh-out of powders. While the tallest worker had no significant difference between the full and empty drums, he had a consistently higher dust exposure than the third worker when scooping from the top of the drum. This would suggest a relationship between work practices and worker dust exposure.

The filter data showed that worker's dust exposure was elevated when scooping from the top of the drum. The worker stands in front of the drum to scoop powder from the drum and to pour powder into the bag. This operation generates dust close to the waist of the worker. The air flow patterns, as shown in Figure 3, suggests that this dusty air is forced into the breathing zone of the worker. The filter data and the real-time data showed, further, that the increase in worker dust exposure was caused by the weigh-out operation, and that it was very close to the worker. The real-time data showed little or no increase in dust levels away from the drum as it was emptied. The filter data showed that there was a concentration gradient across the workers' body, and that it increased as the distance from the sampler to the drum decreased (right lapel to drum, hat to drum). This suggests much of this exposure is caused by scooping material out of drum.

All statistical inferences of the real-time data apply to the specific worker used for the study, as there were no other workers studied. If anything, the fitted model understates the relationship of bag count and scooping the material to an increase in worker dust exposure. Thus, to the extent that bag count is a valid indicator of level of material in the drum, these results show that worker dust exposure increases as the level of material in the drum drops. Furthermore, about half-way into the drum the dust exposure during scooping appears to increase significantly, as measured by the HAM. This increase in worker dust exposure occurs predominantly while the worker is scooping material and it generally decreases (or fails to increase as fast) while the worker weighs the bag or turns to place it in the bin.

While most of the breathing zone samples did exceed the PEL for nuisance dust (15 milligrams per cubic meter), it should be kept in mind that the operation studied may not have represented the day-to-day operations of this job. It should also be noted that the workers evaluated in the study reported limited experience in performing this job. While the results showed abnormally high dust levels, all three workers wore respirable dust respirators during the experiment to protect them from these high levels. Background samples did show that dust concentration levels within the plant to be substantially below the nuisance dust PEL, indicating that the dust was controlled within the vicinity of the weigh-out booth. However, there is definitely potential for dust exposures during this job. The results of this study strongly suggest that the booth ventilation contains the dust emissions generated by this job; but does not adequately control personal dust exposures without the addition of personal protective equipment. The air flow patterns at this booth suggest that the ventilation may even contribute to the worker's dust exposure.

RECOMMENDATIONS

Based upon this study, several recommendation can be made to improve the material weigh-out process, and decrease dust exposure.

- As much as possible, avoid scooping from the bottom of the drum.
 There are several ways of accomplishing this. The use of half-height drums, false bottoms in the drums, or keeping the drum full of the raw material are just three options.
- Remove or reposition the hinged platform from in front of the air intake. This should help to provide more even air flow across the dust source. This should keep the dusty air further from the workers' breathing zone.
- Encourage supplier to use plastic lined bags for raw materials.
 Plastic-lined bags do not sustain as much leakage as other types of bags.
- 4. Consider using methods to reduce stress on the back. A mechanical lift could possibly be used to raise the raw material bags at the booth. This should help reduce the back injury rate related to lifting heavy objects.
- 5. Further research should be performed by NIOSH to find more information about the effects of depth of scooping on worker dust exposure. Furthermore, research on the design of a work station that maintains both acceptable work conditions as well as high efficiency by including both ergonomic and ventilation design principles should be conducted. This research should concentrate on eliminating eddies which force contaminated air into the worker's breathing zone. Furthermore, this research must also consider the lay out of the work station to provide a smooth flowing weigh—out process

In addition, some modifications to the work practices listed in Table 7 can be made. These recommendations are listed in Table 20.

Table 20. Work Practice Recommendations Based upon Elements Shown in Table 7.

	e/Elemen m Table	
L	3	The bag should be opened with two hands one hand to hold the bag and the other to open it. This process takes more time but will reduce potential dust exposure as well as tendinitis problems to the wrist and elbow.
R	5,6,7	Scooping powder, moving the powder to the bag, and dumping the powder into the bag may cause significant airborne dust exposure. Use practices which minimize the height through which powders free-fall through air. Consider the following examples: Before tipping a scoop over to unload it, lay the scoop on top of the powder, raise the handle and gently pull the scoop away from the powder.
L,R	16	Folding the pleates and closing the filled paper bag causes residual air and dust to rapidly escape from the bag. The process small dust "cloud" could be reduced or eliminated by aiming the opening of the bag away from the worker, and closing the bag more carefully.

References

- 1. McKinnery, W. and W. Heitbrink. 1984. Control of Air Contaminants in Tire Manufacturing. NIOSH(DHHS) publication 84-111. Cincinnati, Ohio.
- 2. 29 CFR 1910.1000.
- American Conference of Governmental Industrial Hygienist. 1985.
 Threshold Limit Values for Chemical Substances and Physical Agents in the Work Place with Intended Changes for 1985. Cincinnati, Ohio.
- 4. Heitbrink, W. and W. McKinnery. 1985. <u>Dust Control During Bag Opening</u>, <u>Emptying</u>, and <u>Disposal</u>. NIOSH, DPSE, ECTB Report 144-05b. Cincinnati, Ohio.
- 5. Webb Associates. 1978. Anthropometric Source Book, volume 1. NASA publication 1024. Washington DC.
- 6. Gilbreth, F.B. 1911. Motion Study. Van Nostand. Princeton, NJ.
- Armstrong, T. and J. Foulk, B. Joseph, S. Goldstein. 1982. An
 Investigation of Cumulative Trauma Disorders in a Poultry Processing
 Plant. American Industrial Hygiene Association Journal. 43: 103-116.
- 8. Center for Ergonomics. 1985. University of Michigan. Ann Arbor, MI.
- 9. NIOSH. Work Practices Guide for Manual Lifting. NIOSH. Cincinnati, Ohio.
- 10. Sakiadis B. 1984. Fluid and Particle Mechanics. In: Perry's Chemical Engineer's Handbook. 6 th ed. McGraw-Hill, New York. p5-14
- 11. Rubow, K.L. and V.A. Marple. 1983. <u>Instrument Evaluation Chamber:</u>
 Calibration of Commercial Photometers. In: Aerosols In the Mining and
 Industrial Work Environments. Ann Arbor Science. Ann Arbor, MI.
- 12. SAS. 1982. SAS/ETS User's Guide. SAS Institute. Cary, NC.
- 13. Coughanowr, D. and L. Koppel. 1965. Process Systems Analysis and Control. McGraw Hill. New York.
- SAS. 1982. SAS User's Guide: Statistics. SAS Institute. Cary, NC.

APPENDIX I

Summary of Statistical Analysis

Real-Time Statistical Analysis Results

Objectives of the Analysis

The analysis was directed towards answering the following questions:

- 1. Did the dust exposure of the worker, as measured by the worker ARM readings on the worker's arm, change as the level of material in the barrel decreased, or not, and, if so, was the change an increase or a decrease?
- 2. The work cycle was conceptualized as repeated cycles of scooping material from the barrel and pouring it into a bag, weighing the bag, and finally, turning to place the filled bag into a container. These cycles were conceptualized as having the three phases of scooping, weighing, and turning. A second question was whether the phase of the cycle had any effect on dust exposure of the worker, and , if so, which increased and which decreased dust exposure, and were these effects constant throughout the entire operation or did such effects change as the level of material in the barrel decreased?
- 3. Measures of ambient dust levels were also taken with measurements at the hood and at some distance from the hood in the room where the work occurred. Did these change during the work operation? If so, how did these measures change? And, if so, did such changes account for the changes in worker dust exposure, if any?

Important Modifying Conditions

Readings on each measurement device were recorded every 2 seconds in the internal memory of a computer, except that after each 100 readings the recorder paused to transfer the recorded measurements from internal memory to external storage on a diskette. The computer also recorded the time of each measurement. Thus, there are gaps in the data after each 100 measurements. During data collection the worker was asked to wait when the observers became aware that the transfer was occurring. However, there was usually some delay before the onset of the transfer was detected by the observers and the worker usually continued working for short times while there was no dust measurement.

It is believed that there is a lag of at least 2 seconds between a change in the level of dust reaching any of the three dust measuring devices until that change is registered on the reading of that device. Preparation of the Data for Analysis

Three indicator variables were defined as followed:

SCOOF: = 1 if the worker was involved with scooping material from the barrel to put into the bag , and

= 0 otherwise;

WEIGH: = 1 if the worker was weighing the bag, and

= 0 otherwise;

TURN: = 1 if the worker was turning to place the filled bag in the

container, and

= 0 otherwise.

These indicator variables were scored by viewing a videotape of the work operation which included time recordings at intervals of two seconds. Thus, there was a coincident score for each of these variables for each of the three simultaneous recordings of dust measurements. This videotape was reviewed a second time to score the three indicator variables during the times that the worker continued his work while the computer was transferring data to the diskette. There were no associated dust measurements with these additional scores.

The scores on the three indicator variables were used to create four additional variables used in the analysis:

BAGCNT: Each time the worker initiated the scooping phase of a new cycle, this variable was incremented by 1. This is equivalent to incrementing this variable by 1 each time SCOOP changed from 0 to 1. However, this incrementation was lagged by 2 seconds to accommodate the lag in the dust measures described above. Thus, BAGCNT was incremented by 1 two seconds after SCOOP changed from 0 to 1. The initial value of BAGCNT was 0. This variable is an approximate surrogate measure of the level of material in the barrel as the latter should decrease approximately as a function of the number of bags of material removed from the barrel.

SCP: This was 0 except that after the SCOOP variable changed from 0 to 1, with a lag of two seconds, SCP was incremented by 1 every two seconds until two

seconds after the SCOOP variable changed from 1 to 0. SCP is an approximate measure of the time spent scooping material from the barrel in a particular cycle, with a lag of two seconds.

WGH :

This variable is an approximate measure of the time spent weighing the bag in a particular cycle. WGH was 0 except that after the WEIGH variable changed from 0 to 1, with a lag of two seconds, WGH was incremented by 1 every two seconds until two seconds after the WEIGH variable changed from 1 to 0.

TRN:

This variable is an approximate measure of the time spent turning and placing the bag in the container in a particular cycle. TRN was 0 except that after the TURN variable changed from 0 to 1, with a lag of two seconds, TRN was incremented by 1 every two seconds until two seconds after the TURN variable changed from 1 to 0.

The three dependent or response variables for the analysis are WORKER, the dust measurements recorded on the arm of the worker; HOOD, the dust measurements recorded in the hood multiplied by 5 to achieve a scale comparable to that for the worker dust exposure measurements; and AMBNT the dust measurements recorded away from the hood multiplied by 5 to achieve a scale comparable to that for the worker dust exposure measurements. The analysis used the natural logarithms of these measures as a preliminary analysis indicated that the variances of these measurements increased with their overall level.

Analysis to Fulfill Objectives

The objectives of the analysis may be restated in terms of the variables introduced above as follows:

Objective 1:

BAGCNT is a surrogate measure of the level of the barrel. If the level of dust as recorded on the arm of the worker, is not related to the level of the barrel then WORKER (after transforming to the logarithm of the original measures) should not change as the level of the material in the barrel decreases. If WORKER is positively related to BAGCNT, then it may be concluded that worker exposure increases as the level of the barrel decreases. Thus, the first objective was to determine if WORKER is positively related to BAGCNT or not.

Objective 2:

If worker dust exposure is not related to what the worker is doing during each cycle of filling a bag, then WORKER should not be related to SCP, WGH, or TRN. On the other hand, if scooping material increases dust exposure then the longer the worker spends scooping material, the higher the dust levels should increase, and, consequently, WORKER should be positively related to SCP independently of BAGCNT. Corresponding statements can be made relating the effects of weighing and turning to WGH and TRN, respectively. Thus, the second objective had three sub-objectives:

- a) to determine if SCP is positively related to BAGCNT or not;
- b) to determine if WCH is related to BAGCNT or not, and, if it is, to determine the direction of the relationship; and
- c) to determine if TRN is related to BAGCNT or not, and, if it is, to determine the direction of the relationship.

Objective 3:

If the ambient dust levels are not affected by the worker's work, then neither HOOD nor AMBNT should be related to the analytical variables. If such is not the case, then the difference between WORKER and some function of the ambient dust measures would be analyzed for a relationship to the analytical variables. If the relationship vanishes, then it could be concluded that any relationship of worker dust exposures to the work is a function of changes in ambient dust levels rather than to the work. If there is a relationship, then it reflects an effect of the work on the worker's dust exposure level.

Because changes in dust measures are not immediately registered on the measurement devices but are delayed and because there a tendency for dust levels to subside somewhat slowly once dust levels have been increased, a positive autocorrelation between successive measures of dust was anticipated and substantiated by a preliminary analysis. This violates a key assumption of the statistical models for most statistical analyses: that errors are independently distributed. The presence of these autocorrelations was accommodated by use of an autoregressive time series analysis, which includes parameters to account for the autocorrelations, so that inferences about the parameters of interest can be made. The statistical model includes two major components: the autoregressive effects to account for the unwanted statistical dependency, and the "structural" part which includes the effects of the variables of interest for fulfilling the objectives of the study. The first component was there to facilitate the analysis involving the second

component. Thus, most of the remaining discussion concentrates on the second or structural component and ignore the first or time series component.

The strategy for the analysis was to fit a parsimonious regression model involving the relation of WORKER (the logarithm of the variable is understood) to the variables BAGCNT, SCP, TRN, and WGH. Preliminary results for Objectives 1 and 2 were obtained by tests of hypotheses concerning the coefficients of the variables BAGCNT, SCP, TRN, and WGH after fitting models linear in those variables. But then more complex models, if needed, were to be fit to determine if the preliminary results accurately indicate the direction and form of the relationship and to provide a good practical description of how dust levels were related to the variables in the study. The objective was not necessarily to closely model the response but to model the response sufficiently to provide a fair representation of the manner in which the response was related to the variables used so that the objectives of the analysis could be fulfilled.

Terms were added in the following order only if the two sided t-test that the coefficient of a variable is 0 was rejected at the .05 level. In the case in which three variables were added, the criterion was that the two sided t-test of the hypothesis that the coefficient of a variable is 0 is rejected at the (.05/3) level for at least one of the three variables.

BAGCNT SCP, WGH, TRN BAGCNT² BAGCNT×SCP, BAGCNT×WGH, BAGCNT×TRN SCP², WGH², TRN²

The SAS procedure AUTOREG was used for the analysis. Up to 25 autoregressive terms could have been included and backward elimination was used to fit an autoregression model.

Results

The criterion for adding sets of terms was fulfilled in each case. The preliminary results for Objectives 1 and 2 are as follows:

Objective 1

The hypothesis that the coefficient of BAGCNT is 0 in a linear model including only a constant and BAGCNT must be rejected as the t-test is significant at the .0001 level. The point estimate of the coefficient is positive which indicates that dust exposure increases as the number of bags filled increases, or as the level of material remaining in the barrel decreases.

Objective 2

The hypothesis that WORKER is not affected by any one or more of the three variables, SCP, WGH, or TRN must be rejected because of the additions to the regression sum of squares associated with adding these variables to the model with BAGCNT alone. t-test of the hypothesis that the coefficient of SCP is zero is significant at the .0001 level (which exceeds the criterion). The point estimate of the coefficient of SCP is positive which indicates that dust exposure increases the longer the worker is scooping material from the barrel. The t-test of the hypothesis that the coefficient of WGH is zero is not significant at the .05 level (at the .40 level). The point estimate of the coefficient of WGH is positive. These results do not support a relationship of time the worker is weighing material to the dust level. Finally, the t-test of the hypothesis that the coefficient of TRN is zero is significant at the .0001 level (which exceeds the criterion). The point estimate of the coefficient of TRN is negative which indicates that dust exposure decreases the longer the worker is turning to place the filled bag in the container.

The fitted model for the worker dust exposure measurements was a second order model in the explanatory or analytical variables, e.g. it included all terms in

(1+BAGCNT+SCP+WGH+TRN)²

(since all the crossproduct terms among SCP, WGH, and TRN are zero).

While there was evidence of lack of fit, examination of the residuals indicated that the fitted model conservatively represented the trends to be described. Inspection of residuals plotted by time did not indicated marked time relationship to lack of fit.

The fitted model for the worker dust exposure measurements is the sum of the following four components:

- $-4.56 + .00256 \times BAGCNT + .00083 \times BAGCNT^{2}$
 - .146xSCP +.0003xBAGCNTxSCP -.0032xSCP2
- -.044xWGH -.0054xRAGCNTxWGH +.038xWGH²
- -.434xTRN -.0089xBAGCNTxTRN +.119xTRN2

BAGCNT ranged from 0 to 56 while SCP ranged from 0 to 5, WGH from 0 to 6, and TRN from 0 to 6.

Examination of the coefficients of the fitted model and the plots of the values predicted by this model support the preliminary results and indicate:

- i. Worker dust exposure level increases dramatically as a function of BAGCNT.
- 2. For SCP, for any constant value of BAGCNT, the linear slope which is positive predominates and the slope increases as BAGCNT increases.
- 3. For WGH, at any given level of BAGCNT, worker exposure decreases but the slope increases with WGH, but the slope decreases as BAGCNT increases.
- 4. For TRN, at any given level of BAGCNT, worker exposure decreases as TRN increases but this is moderated by an increase of the slope as TRN increases, but the slope decreases as BAGCNT increases.

These relationships are illustrated in Figure 11b. In Figure 11b, the predicted value of worker exposure while SCP is positive is indicated by the points plotted with "S", while WGH is positive predicted values are indicated by the points plotted with "W", and while TRN is positive predicted values are indicated by the points plotted with "T".

Confidence Intervals for Parameter Estimates

The estimates of the coefficients of the terms in the model are restated below with estimates of their standard errors and 95% confidence intervals. The intervals should be interpreted cautiously because they are not simultaneously valid at the 95% confidence level, these are averages from a model with statistically significant (but not practically significant) lack of fit, and the estimators of the coefficients are correlated. These statistics are based on the full fitted model, which accounts for the fact that in some cases, e.g., for the coefficient of BAGCNT, the addition of the term in the order described above resulted in an estimate of the coefficient that was statistically significant, i.e., different from 0, but the estimate of the same coefficient in the full fitted model is not statistically significantly different from 0.

Table I: Estimates of Coefficients, Standard Error Estimates, and 95% Non-simultaneous Confidence Intervals

TERM	ESTIMATE OF	STANDARD ERROR	95 % CONFIDEN	CE INTERVAL
	COEFFICIENT	ESTIMATE	LOWER LIMIT	UPPER LIMIT
BAGCNT	.0026	.0112	019	.025
SCP	.1455	.1253	10 0	.391
WGH	0444	.1092	258	.170
TRN	4335	.1144	658	209 ***
BAGCNT ²	.000838	.000185	,00048	.0012 ***
SCPxBAGCNT	.000295	.00168	003	.0036
WGHxBAGCNT	00543	.001787	009	002 *
TRNxBAGCNT	00889	.001723	012	0055 ***
SCPxSCP	0032	.0277	057	.052
WGHxWGH	.038	.02237	006	.082
TRNxTRN	.1186	.02337	.075	.162 ***

Meaning of Symbols

- * Significance at the .05 (two tail) level;
- ** Significance at the .01 (two tail) level;
- *** Significance at the .001 (two tail) level;

If the terms with non-significant estimates of coefficients are deleted and the resulting model is fitted to the data, the resulting fitted model becomes (all estimates of coefficients of terms would be nominally significant):

- $-4.377 + .00095 BAGCNT^2$
- -.0084 BAGCNT x WGH + .036 WGH²
- -.586 TRN -.010 BAGCNT x TRN + .153 TRN²

This model implies that:

Worker dust level increases quadratically with BAGCNT;

The increase with BAGCNT is not increased nor decreased during the "scooping" phase of the cycle;

At any level of BAGCNT, worker dust levels decrease during the "weighing" phase of the cycle with the magnitude of the decrease increasing with BAGCNT, but this decrease becomes progressively smaller the longer the worker spends weighing; and at any level of BAGCNT, worker dust levels decrease more (relative to the decrease during weighing) during the "turning" phase of the work cycle, with this decrease becoming greater as BAGCNT increases but it is moderated the longer the worker spends in the "turning" cycle.

A hidden implication is that the increase in worker dust exposure levels occurs during the "scooping" phase of the work cycle, as the dust level tends to decrease in both of the other phases of the cycle.

The practical conclusions, i.e., the implications for the correlates of dust generation during the entire task and for each work cycle, are the same for either the "full" fitted model or the "reduced" model. The additional "sum of squares" accounted for by regression in the "full" model relative to the "reduced" model is statistically significant. This implies that one or more or some function of the coefficients deleted from the "full" model would be significant if added to the "reduced" model. Since it is doubtful that finding the term or terms that would account for this would alter the basic practical implications of the results concerning dust generation, no further investigations were undertaken. All plots used the predicted values from the "full" fitted model.

Results of the Analyses of Ambient Dust Measures

Both measures of ambient dust levels were also related to the worker variables. The fitted model for HOOD was as complex as that for WORKER while only a linear term in BAGCNT was needed for AMBNT. The difference of WORKER - HOOD was then analyzed and the relationships found for WORKER alone were approximated.

When residuals were examined, the predicted values tended to be too small when SCP was positive and were too large when SCP was negative.

Conclusions

All statistical inferences apply to the specific worker used for the study as there are no degrees of freedom for between worker differences. If anything, the fitted model understates the relation of BAGCNT, and scooping the material, on increases in the level of worker dust exposure. Thus, to the extent that BAGCNT is a valid indicator of level of material in the barrel, these results support the proposition that worker dust exposure increases as the level of material drops in the barrel, and that the increases in worker dust exposure occur predominantly while the worker is scooping material while worker dust exposure decreases (or fails to increase as fast) while the worker weighs the bag or turns and places the bag in the container.

If anything, ambient dust levels are increased by the work and the changes related to the work can not be explained by independent coincidental changes in ambient levels, although with non-experimental data there must be some doubt about this as well as any other conclusions from these results.

The conclusions of the analysis would not be materially different if the results of the analysis of the dust level measurements had been used rather than the results from the analysis of the logarithms of those measurements.

Figure 10 plots worker dust exposure against the count of bags either filled or being filled and it may be observed that much of the increase occurs after the about half of the 56 bags have been filled.

Filter Data Statistical Analysis Results

Design

This was a planned study to determine the adequacy of dust control technology.

Three workers were studied on three separate days, once in the morning and again in the afternoon. For each study period the worker was observed with two sets of clothing and scooping material from a drum filled to two levels, one-half full or completely full. Six different dust measurements were recorded simultaneously for each combination of clothing and drum level: three personal measures of dust exposure which were at the right shoulder, the left shoulder, and on the hat; and two background locations. The background locations were at the face of the bin, at the bin, and in the room.

Right shoulder readings were added after the first day and are not present for one worker.

The objectives are to determine if drum level affects dust exposure of the worker as measured by the measurements on or at his body and if type of clothing worn increases, decreases, or has no effect on the dust exposure of the worker. The two background measurements provide information about non-experimental sources of contamination which might affect the results of the study.

Analysis Strategy

The background measurements and the body measurements were studied separately. If the background measurements are related to the factors of interest in the study, these measures would be used to adjust the body measurements for the effects of background contamination.

Different measures for the same worker may be related to characteristics of the worker which cannot be randomized or controlled. If the basic experimental unit is the time segment in which the worker does a particular task, it is clear that these are unique to each worker-morning-or-afternoon session (hereafter, worker session). Different units in the same session may be related or subject to common sources of distortion. Within each session the order in which the worker performed the activities of the experiment was randomized so that the units were randomized within sessions.

The three body measurements and the three background measurements were taken simultaneously. Since each measurement instrument operates independently there is no reason to expect that their respective measurement errors would be correlated. Thus, it seems reasonable to assume that any differences reflect measurement differences.

If each worker session is considered as a block, then the study may be viewed as a randomized block design at each type of measurement, i.e. the randomized units are the four time segments in which a worker performed the scooping of material. The statistical inferences pertain to the three specific workers on the two respective occasions that each were studied. Generalizations beyond this must be based on non-statistical considerations, e.g., expert knowledge, etc.

There are two major sources of variance: between units and within units. The between units variance may be analyzed into between workers, between treatments, between sessions within workers and the interactions of these. Within unit variance may be analyzed into between measurement location, and (between) interactions between measurement location and the identifiable between unit factors, such as workers, sessions, treatments, and the interactions among these.

Regarding the between unit portion, it has been often argued (e.g. Scheffe, Davis) that, since units were not randomly assigned across blocks, that the treatment effects are confounded with treatment x unit interactions and that treatment x block interactions are also confounded with treatment x unit interactions. Since there is no true replicate, there is no source which is attributable solely to error and treatment x unit interactions which might be a comparison Thus, to obtain a comparison factor it is necessary to factor. assume that either some or all of the treatment x block interactions are zero, so that the corresponding nominal treatment x block interactions term may be used as the comparison, or that the treatment by unit interaction is zero. Unlike most "textbook" randomized block designs, there are three independent (by assumption) measures on each unit so that the unit by location of measure interaction should be free of treatment by unit interaction.

In this case the total treatment by block interaction sum of squares may be partitioned into two major sources: (1) Clothing type and drum level by worker; and (2) Clothing type and drum level by session within worker. (Each of these may be further partitioned into three sources as well.) The sum of the variance attributable to interactions of sessions within worker and the treatments seems a logical candidate for the comparison term for testing hypotheses concerning between unit factors of interest, i.e., clothes, drum levels, workers, etc. The interaction term involving location of measure, sessions within worker, and the treatments appears to be a logical candidate for the comparison term for the "within" units portion of the analysis. However, it is possible that the unit differences, especially those common to the same worker, are so small that there is little difference between the comparison term for the between units and the comparison term for the within units portions of the analysis. In that case, these could be combined to increase the power of the analysis.

Preliminary analysis suggested that the analysis use the logarithms of the measurements.

Background Readings Results

The analysis departed from the above in that it proceeded immediately as though the design were a factorial in worker, drum level, clothing, and location of measurement with session as a replicate, save for the "main" effect of session within worker. This seems reasonable in that background sources of dust should not be caused by the worker and the entire notion of the "units" as associated with the workers does not seem applicable.

The F-ratio for total regression, i.e., all sources put together, was 1.80 with 47 and 23 degrees of freedom, which achieves the 0.065 significance level, which is consistent with the null hypothesis, but barely so, that background sources of dust were not related to the factors of interest. None of the main effects would be significant if analyzed separately but the variation among workers is nearly so (p less than .056), while the session within worker (P less than .02) effects would be significant. These results might reflect differences in background levels on different occasions which are confounded with worker and worker session effects, the blocks for the study. The clothes by drum (P less than 0.005), and the drum by location of measurement (P less than .001), interactions would be significant if analyzed separately. The results of the analysis of variance are shown in Table I.

Body Measurement Results

The SAS procedure PROC GLM was used for the analysis. All sums of squares reported are "Type III" sums of squares, in the terminology of SAS PROC GLM. Thus, these cannot be meaningfully added, nor are they statistically independent. The main advantage is that each reflects an adjustment for the effects of all other factors in the model and closely approximate the "extra sum of squares" for the factor as if it were the last one added to the model. In this case, the actual design is only slightly unbalanced so that the differences between the "Type I" sum of squares and the ones shown were never enough to substantially change the conclusions. The results are shown in Table II.

The mean square for the treatments by session within worker is 3.53 with 12 degrees of freedom(df), while the location by treatments by session within worker mean square is 1.424 with 20 df. The ratio of 2.48 is statistically significant at the 0.05 level. Thus, it appears not wise to combine these for a single comparison term.

Among the various component sources for the treatments by session within worker interaction, the mean squares range from 2.07 for the sessions within worker to 4.88 for the sessions within worker by drum level; each has 3 df. These do not appear enough noteworthy to

attempt to narrow the choice of comparison further.

Two factors or sources seem clearly large regardless of how they might be analyzed: between workers and between measurement locations. Neither of these is of particular interest.

On the other hand, the results seem equally clear that there is little difference between the levels of dust for the two types of clothing no matter how analyzed. The same is true, i.e., the effects appear small at most, for the clothes by drum level interaction and every other interaction term involving clothes.

As shown in Table II, the mean square for drum level is more than ten times the size of the session within worker by treatments interaction. The ratio is statistically significant at the 0.066 level using a F-test with 1 and 12 degrees of freedom. The F-test for drum level by worker interaction barely misses significance at the 0.05 level although the mean square appears elevated and the actual probability level is .052.

No other source was statistically significant.

Contrasts

Analyses of contrasts between drum levels and between drum levels by worker are shown in Table III on the transformed logarithm scale.

For drum level, the estimated difference is 1.49, which is 4.44 on the original scale. The 95% confidence intervals shown apply for the transformed scale, only. However, the end points have been transformed back to the original scale, but these do not yield a 95% confidence interval on the original scale.

Two sets of estimates are provided for the drum and worker contrasts: drum level within worker, or the differences between full and empty for each individual worker; and drum by worker, which refers to the interaction contrasts of drum by worker, i.e., the contrasts among the first set, e.g., the first contrast of the first set to the average of the other two (multiplied by 2), etc.

For the drum within worker contrasts, a set of three intervals is given in Table III. This set of intervals is a 95% confidence interval set. For worker I the estimated drum effect is slightly greater than the average while the amount of fill of the drum almost has no effect for worker 2, and the estimated effect is much higher than the average for worker 3. Nevertheless, the drum by worker interaction was not statistically significant as indicated by the fact that none of the F-ratios for the three drum by worker contrasts is significant at the .05 level.

Reanalysis

As noted above the available evidence provides no support for any effect of the clothing changes for these workers. What if the analysis had excluded clothing as a factor? Any answer from these data is somewhat speculative since an analysis is after the fact. However, the data was analyzed by adding the sums of squares involving clothing to the error sums of squares, in an appropriate manner for both the between units and the within units analysis. The results, of course, are "after the fact" and are intended to generate suggestions for future work. This is not equivalent to ignoring clothing in the analysis but these results approximate those that would have occurred had clothing been ignored because of the design is nearly balanced. The results are shown in Tables IV and V.

The main difference is that the worker by drum interaction achieves statistical significance.

Table I. Analysis of Background Dust Concentration.

166.20108003 \$4.41701399
160_69870202
TYPE 1 53
0,61386716
7,61839241
1,73092007
4,41809233
12,86519223
1.18542772
7.55429375
0.48775556
39,60622045
1,64800698
1,33626354
4,50057580
2,64543390
6,01584029
16,20118609
5,22330902
4,92010107
4,56329322

Loc refers to the location of the dust concentration measurement.

Notes
1. These dust concentrations were measured at the face of the hood, at the bin, and in the room.

Table II. Analysis of Variance of Logarithms of Dust Exposure Measurements on Workers.

Ditueen 'Units'	t		Xanara		(B) 18/4 \ J)	
Billiagen 'Units' Verkers						
Herkors						
	N	38.28	19.13	5.42	0.02	
Dam tavel	-	8.3	96.36	10.76	0.01	
Herker by Orun Level	N	26.73	13.36	ድ.	0.052	
Cbthing	1	1.09	1.09	0.31	0.59	
Worker by Clothing	CI.	6.94	3,47	96. 0	0.60	
Drum by Clathes	-	90.0	0.06	0.02	0.89	
Merker by Srum by Clothes	N	0.01	0.01	0.02	0.99	
•						
Error	٨	5	,	¥	è	
KADIACATATHOFKAPI	7 K	2.7	÷ 8	f :	9.0	Lomparad
To Cother) P	5	8	2.63	6.0	3
5.074	•		:		; ;	Hithin
by Clothas	**	9.53	3,18	2.23	0.12	4 4 4 4 4 4
Sectoral for						מעד ניפ
Error	2	42.36	3.53	2.48	0.03	Error
Teal Between 'Units 23	2					
Hithin "Units"						
Leetion of						
Messurenent	N	53.13	26.57	18.66	1000.0	
Lestion × Horker	▼ -	6.54	1.64	1.15	0.36	
Lication × Drum	N	0.64	O. 32	0.22	8.0	
CENTENT X MONTRE	•	5	65	*	9	
Lecetion × Cithes	- N	1.68		66.0	95.0	
Leation # Morker	ı		•		}	
* Clothes	•	8,40	2.10	<u>.</u> .	0.25	
Lication × Drus						
x Clothes	~	0-22	0.11	90.0	0.93	
Letton × Worker	•	7	9	•	ço c	
AUTOLIA × CLOUNES	r	0.0	67.0	21.0	× .	
Error						
Legation × Repl C Hor	ю.					
x Drug x						
" * Orun × Clothe	n (
Idal Error Guthin)	N	28.48	1.4			
Idel Hithin Units	*					
Canad Total	٧					

Table III. Analysis of Contrasts Between Drum Levels and Drum Level by Worker.

	(5) rul > (5) rul > (5) rul >	Garand) Garand) Garand)		arage difference arage difference arage difference	
Description	Morkerls empty-full (so Horkerls empty-full (so Morkerls empty-full (so	Marker 1 septy-ful) (sometime of the septy-ful)		Morker 1 difference va everage difference Morker 2 difference vs everage difference Morker 1 difference vs everage difference	Empty va full full vs ampty
enc. Upper	\$ 1 2 \$ 2 7	• Interval) 27 57 8 24 145 17			1 383 (terval) 3 985
95 % Confidence Lower Upp	-0 609 -2,329 0 683	95 2 Confadenc 0.544 0.092 1.979			0 562 r Confidence In 1.75
T · ratio	2 11 -0 13 3 69	Original Scale (not a 95 2 Confidence Interval) 77 57 0.092 6 24 1.979 145 17		0 450 -2 546 2 018	4 0.454 3.29 0.562 1.383 Original Scale (not 4.752 Confidence Interval) 1.75 3.965
td Err	0 886 0 7926 0 767	Origina		0 595 0 634 635 635	1 4904 (0,454 Original S
Estimata Std	1,871 -0 11 2 8302	ა ე მ გამ		0 292 -1 614 1.323	- F
	Cereul tangous) 1,871 (Simul tangous) -0 11 (Simul tangous) 2,8302			(Simultaneous) 0 292 (simultaneous) -1 614 (simultaneous) 1.323	
P level (P < value)	18 1S			, 6 , 5 , 8 8	10
F-retto	767 101			378	£ 2
. 1	5 25 0 0227 16 02			617 618	37- 992
Squares	25 0 25 0 35 0 36 0 36 0 36 0 36 0 36 0 36 0 36 0 36			0 86 22 89 14 38	% &
\	សសស ភូស្ស			~ ~ N	Ħ
Contrast Orus eithen Korker	Drum as than Horker I Orum as than Horker 2 Orum as than Horker 3		Drum by Norker Interaction	Drug by Horker I Drug by Horker 2 Orus by Horker 3	Drum Lovel

BETHEEN NEWN SQUARE FOR ERROR 3,6300

Table IV. Analysis After Adding All Sum of Squares Involving Clothing to the Error Sum of Squares.

Source	ŧ	Solution		F-Ratso	F-Ratio P Level (P < value)
Between 'Units'	1 1 7	 			
Horkers	ę,	38.26	19.13	6.8 2	0.0064
Drum Level Morker by Orien Level	 ⟨V	8,8	85.55 18.58	13.55	0.002
Error	9	\$.08	2.80	2.27	0.0209#
Total Between "Units	ĸ		¥	*Comparad to	s wa thin
Hithin 'Units'					
Location of					
Messurement	N	53.13	26.575	21.49	0.0001
Location × Morker	T	Ţ,	1.64	1.32	87.0
Location × Orum	N	0.64	0.32	X	0.72
R Drum	۳	10.01	25.50	2.03	
Total Error Gathin	N	39.55	1.2	<u>}</u>	• • •
Fotal Aithin Units	8				
Grand Fatal	8				

Table V. Analysis of Contrasts Involving Drum Level and Drum Level and Worker After Clothing Sum of Squares is Added to the Error Sum of Squares.

Contrast	¥	1	1	1			1						
Drum within Horker	i	Squeros				Î	Estrato	Estimate Std Err T-ratio95 % Confidence Louer Louer Upp	T-T-8110	No. Conf	Aderica Upper	Description	
Drum within worker! Drum within worker? Drum within worker?	имк	55 75 0 064 0 054	6 25 0 02 16 02	1.87 6 01 7 71	0 999 0 999 0 0065	(Similtangous) (Similtangous) (Similtangous)	- 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6	9 6 6 6 8 8 7 8 8 7 8 8	4 16	0 0 0 4 0 0 4 0 0 5 0 0	*-+ 86:1	Norker I expty-full Norker 21 expty-full Norker 5, expty-full	Caseultangou Caseultangou (Sieultangous
Prue by Marker Intersection							04.10 6.49 0.50 0.90 8.93) Scale ()	ot • 95.	Confude 0 71 0 12 2.50	Original Scalm (not a 95 / Confidence Interval) 6 49 0 71 59.25 4, 0 90 0 12 46.47 4, 6 95 2.60 114.95 4,	Horkert: ampty-full Horkert: ampty-full Horkert: ampty-full Horkert: ampty-full	(simultenseus (simultenseus (simultenseus
Drue by Norker I Drue by Norker 2 Prue by Norker 3	NNN	52 5 88 8	0 11 14 19 19	0 + 4 21 8 86 85	0.08 0.03 0.103	(Simultersous) (Simultersous) (Simultersous)	0 291 ~1.614 1 323	000 8 % 8	888 888			Mortearl difference vs average difference Mortearl difference vs average difference Mortearl difference vs average difference	Age difference age difference
Orus Literal	-	%	27.99	13,55	0 002		1 4904	0 40 Original	3 68 304	0 66 (mat • 9	1,23 5 7 Confuda	0 66 1.23 Eapty vs. full (mit e 25 2 Confidence Interval	
Error Meen Squere		2 B 0 4 0					‡			<u>;</u>	₹. ₹	Empty va. full	

APPENDIX II

Anthropometric Questionnaire

NATIONAL INSTITUTE FOR OCCUPATIONAL SAFETY AND HEALTH DIVISION OF PHYSICAL SCIENCES AND ENGINEERING ENGINEERING CONTROL TECHNOLOGY BRANCH

ACTIVE SURVEILLANCE QUESTIONNAIRE DEVELOPED FOR B.F.GOODRICH

Date: No Day Year
Worker ID: Job Title
Worker Name: First Last
Gender: 1 Male 2 Female
Handedness: Right Left Both Work Hand: Rt Lt Bo _
Date of Birth: Mo Day Year Age
Length of Employment with B.F.Goodrich: Mo Years
Length of Employment at this Plant: Mo Years
When did you start this job? Ho Day Year
Is this the only job you do? Yes No
If No, what other jobs do you perform:
Approximately what percentage of time is spent during an 8-hour work shift performing this job? Percentage How much material do you "Bag" during an 8-hour work shift? Pounds No. of Bags (Company Production data: Pounds Bags).
Do you have any suggestions about improving your job?

ANTHROPOMETRIC DATA STANDING POSITION

Date: Mo _	Day	Year	
Worker ID:		1 . Gody length	
1 Body Len	gth	2. Shoulder heig 3. Height of hips	
2 Shoulder	Height	· <u> </u>	
3 Height o	f Hips	•	cm cm
4 Shoulder	breadth	·· <u> </u>	(,3
	Reach in grasping) \ \ _		5
6 Elbow He:	ight · _		2
7 Underarm (elbow to	length ofingertip)	•	
Work Area:	Container Height _	_ 	
	Container Diameter	·-	
•	Distance between co	ontainer and measuring	g area
	Measuring area tabl	le height	•
	Bag height		
	Material transfer t	cool: Weight	_ Size: Height
	length	Handle diame	eter
	Handle length		

APPENDIX III

Biomechanical Strength Analysis

STATIC STRENGTH PROGRAM (<2.0) ANALYSIS SUMMAPY FOP: MARIETTA OHIO B.F.GOODRICH

INDEPENDENT VAPIABLES	MALE	FEMALE
HEIGHT (M)	1.77 75.20	1.62 62.10
FORCE EXERTED/HAND (N) DIRECTION OF FORCE X XX NUMBER OF HANDS USED IN TASY	111.20 0.00 2	111.20 0.00 2

POSTURE ANALYZED:

THIOL	ANGLE **
ELBOM	-50
SHOULDER	-80
HIP	5
KNEE	130
W MKLE	75

* - ANGLE OF FORCE ACTING UPON THE HAND

ANALYST: JAMES D. MCGLOTHLIN

** - ANGLES ARE ABOUTER+) / BELOWIF-) PIGHTWARD HOPIZONTAL AYIS

PROPORTION OF POPULATION WITH SUFFICIENT STRENGTH CAPABILITY

DATE:02-09-1984 TIME:20:44:15

J01NT	% MALES CAPABLE	% FEMALES CAPABLE
ELBOM	61	3
SHOULDER	2 7	21
LON BACK (L5/51)	99	13
HIP	9 9	9 8
KNEE	97	무 승
ANYLE .	& \$	99
COMPRESSIVE FORCE (N)	MALE	FEMALE
AT L5/S1 DISK	-304	-734

STATIC STRENGTH PROGRAM (02.0) ANALYSIS SUMMARY FOR: MARIETTA OHIO B.F.GOODRICH

INDEPENDENT VARIABLES	MALE	FEMALE
HEIGHT (M) WEIGHT (KG)	1.77 75.20	1.62 62.10
FORCE EYERTED/HAND (M) DIRECTION OF FORCE * ** NUMBER OF HANDS USED IN TASK	111.20 -90.00 2	111.20 -90.00 2

POSTURE ANALYZED:

TidIOL	ANGLE *
ELBON	-80
SHOULDER	-95
HIP	5
KNEE	130
ANKLE	78

* - AMGLE OF FORCE ACTING UPON THE HAND

** - ANGLES ARE ABOVE(+) /BELOW(-) RIGHTWARD HORIZONTAL AYIS

PPOPORTION OF POPULATION WITH SUFFICIENT STRENGTH CAPABILITY

JOINT	% MALES CAPABLE	% FEMALES CAPABLE
ELBOV	90	6 0
SHOULDER	0 0	99
LOM BACK (L5/91)	9 9	9∉
HIP	94	2 7
KNEE	99	99
ANKLE ,	98	98
ADVENIENCE PORCE (NO	MALE	FEMALE
COMPRESSIVE FORCE (N)	4242	2/12
AT L5/S1 DISK	4342	3613

ANALYST: JAMES D. MCGLOTHLIN

DATE:02-09-1986 TIME:20:39:32

STATIC STRENGTH PROGRAM (+2.0) ANALYSIS SUMMARY FOR: MARIETTA OHIO B.F.GOODRICH

INDEPENDENT VARIABLES	MALE	FEMALE	
MEIGHT (M)	1.77 75.20	1.62 62.10	
NUMBER OF HANDS USED IN TASK	111.20 -90.00 2	111.20 -90.00 2	

POSTUPE AMALYZED:

JOINT	ANGLE
ELBOM	-50
SHOULDER	-89
HIP	5
KMEE	130
ANKLE	75

* - ANGLE OF FORCE ACTING UPON THE HAND

** - ANGLES ARE ABOVE(+) /BELOW(-) RIGHTWARD HORIZONTAL AMIS

------MODEL PREDICTIONS----------

PROPORTION OF POPULATION WITH SUFFICIENT STRENGTH CAPABILITY

JOINT	MALES CAPABLE	% FEMALES CAPABLE
ELBON	99	86
FOM BUCK (F2/81)	9 <u>9</u>	6 3 83
KMEE HIb	60 õe	72 e e
ANKLE .	• €	φž
COMPRESSIVE FORCE (N)	MALE	FEMALE
AT L5/S1 DISK	5 456	4626

ANALYST: JAMES D. MCGLOTHLIM

DATE:02-09-1986 TIME:20:30:58

APPENDIX IV

Data Acquisition Program

560 590	LØAD REM 9	IS144 GOSUB RETURN & REM COLOR= GOSUB ON PRINT STOF PRINT WAIT GOSUB RE RETURN LOAD DEF
		01/26 04:23:50.168"
		60TO 5490
	D\$ = CH	1 R\$ (41
	ZP = 0	
600	HEX\$ ≠ '	'0123456789ABCDEF"
65 0		\$(16),DBC\$(13),FARM\$(1 (13),TM\$(100)
440		_(15),CH(16),GAIN(15),
000		
		RT(16),V(16),VOLTS(16
),RDG(1	
6 70)\$:"BLOAD READ CLOCK.O
	BJ.A#TO	
690		1 TO 10: READ BYTE: FOLE
		BYTE: NEXT
700		24,168,104,166,227
710		54,72,152,72,96
700		= 1 TO 13: READ DSC\$(I
): NEXT	
740		'EQUIFMENT
	• • 11	
750		RUN NUMBER
	* * ^H	
7 <i>5</i> 0		ACTIVE CHANNELS
	"	
770		CHANNEL CODES
7 000	7. " 04.T4 U	ETCENAME
780	DATA "	FILENAME,,
790		OUTFUT FORMAT
1 1 10		DO TO TOMBLE SERVICE
800		GAIN CONTROL
For the tar	******	OMIN CONTROLLITIES
810		CALIBRATION CONSTANTS
		Cherent Fair Condition
820		READING INTERVAL
OT 1.	DO 10	VEHNTIAG TAG FILAUFFERN
870	*	# OF READINGS
650	- " "	# Or ICHCINGO. FILLE.
840		FRINTER OPTION
CHO	DMIM	LECTION DE L'EDING.
850		FRINTER SLOT
650	"	LICTIALITY COUNTY APPEA
860		EXECUTE / OUIT
200	DH!A	EXEMPLE 7 DULLINGS
910		. 1 TO T. CEAR OF#/!*
710		: 1 TO I: READ OF\$(I):
000	NEXT	PACH HIELEGONALISH NGACZ
920		GAS","TELEGRAFH","SAS/
	TELEGRA	irn

```
940
     FOR I = 1 TO I: READ PO$(I):
      NEXT
950
     DATA
            "READINGS", "OFF"
970
     FOR I = 0 TO 7: READ GC$(I):
      NEXT
780
     DATA
          " (0) +0.0 TO +5.0 V".
     " (1) +0.0 TD +1.0 V"
990
     DATA
           " (2) +0.0 TD +0.5 V".
     " (T) +0.0 TO +0.1 V"
1000
     DATA " (4) -5.0 TO +5.0 V"
     , " (5) -1.0 TB +1.0V"
     DATA " (6) -0.5 TO +0.5 V"
1010
     , " (7) -0.1 TO +0.1 V"
1030
     FOR I = 1 TO 17: READ PD$(I
     :FARM*(I) = PD*(I): NEXT
     DATA "RAMS","1"," "." ","T
1040
     EMF", "SAS", " "
     DATA "1-- 1", "00 MIN 10 SE
1050
     C","100","OFF","O","E/D/ CR
1060 \text{ RM} = 1:\text{NC} = 0:\text{RC} = "":\text{FL} = 1:\text{RC}
     "TEMF"
1070 DLY = 10:NR = 100:FD = 2:FS =
1080
    FOR I = 0 TO 15:CAL(I) = 0:
      NEXT
1090 LFF = 50:0F = 1:RC = 0:REWR =
     100:VM = 2
1110 \text{ SLOT} = 5
1100 PRINT : FRINT Ds: "NOMON CIO
1140 TEXT : HOME : FRINT CHR# (
     140): HOME : SFEED= 255
1150 FORE 04,16
1160 GOSUB 5170
1170 FOR I = 1 TO T9: PRINT "-":
     : NEXT : FFINT
1180
     INVERSE : FRINT "
     RETURN FOR NO CHANGE
      ": NORMAL
1190 HOME : FRINT "CLEARING MEMO
     RY...FLEASE WAIT":X = FRE (
    .9)
1200 \text{ LINE} = 1
1205 IF ZF
                O THEN GOTO 140
     0
1206 \text{ ZP} = \text{ZP} + 1
1210 FG = 0:FI = 1
```

1270

1570

HOME

NEXT

PD\$(I): NEXT

1300 FOR I = 1 TO 11:PARM\$(I) =

1360 FOR I = 0 TO 15:GC(I) = 0: NEXT

FOR I = 0 TO 15: CAL(I) = 0:

```
1190 \text{ PARM$(8)} = "1-- 1"
```

- 1400 PDFE J4.0: VTAB 1: HTAB 1: GOSUB 5280: PDFE J4.16: HOME
- 1420 HOME : GOSUB 5000: LINE = 2: GOSUB 5010
- 1430 PRINT "ENTER THE RUN NUMBER
- 1440 INPUT "(2 DISITS MAXIMUM 01 -99) -- "#R\$
- 1450 IF R\$ = "" THEN GOTD 1500
- 1470 RN = 8
- 1480 PARM\$(LINE) = R\$: GOSUB 5010
- 1500 HBME : 60588 5700:LINE = 3: 60588 5710
- 1510 PRINT "CHANNELS TO READ"
- 1520 INPUT "(0123456789ABCDEF)--
- 1570 IF R# = "" THEN GOTO 1870
- 1540 R = LEN (R\$)
- 1550 IF R 16 THEN GOTO 1500
- 1560 FOR I = 1 TO R: FOR J = 1 TO 16
- 1570 IF MID\$ (HEX\$,J,1) = MID\$ (R\$,I,1) THEN J = 16: GOTO 1
- 1580 NEXT J
- 1590 PRINT: FOR F = 1 TO 5: CALL 198: NEXT: FRINT ""; MID\$ (R\$,I,1);" NOT VALID": FOR PSE = 1 TO 2000: NEXT: I = R: J = 16: GOTO 1500
- 1600 NEXT I
- 1610 FOR I = 1 TO R 1: FOR J = I + 1 TO R
- 1620 IF I = J THEN GOTO 1650
- 1670 IF MID\$ (R\$,I,1) MID\$ (R\$,J,1) THEN GOTO 1650
- 1640 FOR F = 1 TO 5: CALL 198 : NEXT : PRINT : PRINT : FRINT ."'"; MID\$ (R\$,I,1);" DUFLIC ATED":I = R:J = R: FOR FSE = 1 TO 2000: NEXT : GOTO 1500
- 1650 NEXT J
- 1660 NEXT I
- 1670 NC = R:AC\$ = R\$:RC\$ = R\$
- 1680 FC\$ = "": FOR I = 1 TO NC:FC \$ = FC\$ + " " + MID\$ (RC\$,I ,1): NEXT
- 1690 FOR I = 1 TO R
- 1700 CH\$ = MID\$ (AC\$, I.1)
- 1710 CH = VAL (CH\$)

- 1720 IF ASC (CH\$), 64 AND ASC (CH\$) 71 THEN CH = ASC (CH\$) SS
- 1730 CH(I) = CH
- 1740 CAL(CH) = 1
- 1750 NEXT
- 1740 IF NO 8 THEN GOTO 1830
- 1770 HOME
- 1780 PRINT "WARNING: THERE MAY B E SOME SAS PROBLEMS"
- 1790 PRINT " WHEN USING THIS MANY CHANNELS."
- 1800 PRINT " IF SO, USE 'NONUM' TO FARELAWN."
- 1810 FRINT
- 1820 PRINT "FRESS A FEY ":: GET FB\$: PRINT
- 1BIO PARM\$(LINE) = R\$:FARM\$(LINE + 1) = R\$: BOSUE 5I10
- 1840 FARM\$(7) = "": FOR I = 1 TO LEN (AC\$):FARM\$(7) = PARM\$(7) + STR\$ (GC(CH(I))): NEXT
- 1850 GOSUB 5280
- 1870 HOME : GOSUB 5000:LINE = 4: GOSUB 5010
- 1880 IF NC = 0 THEN 60TO 2110
- 1890 FRINT "ENTER THE CHANNEL CD
- 1900 PRINT "(1 CHARACTER FER CHA NNEL)"
- 1910 PRINT " (DO NOT USE ANY BLA NES)"
- 1920 PRINT "(YOU SHOULD ENTER "; NC;" CODES)"
- 19I0 INFUT " --- ":R\$
- 1946 IF R\$ = "" THEN GOTO 2110
- 1950 IF LEN (R#) NO THEN CALL 198: FAINT : FAINT "TOO F EW CODES": GOTO 2040
- 1960 IF LEN (R\$) NO THEN CALL
 198: FRINT : FRINT "TOO M
 'ANY CODES": GOTO 2040
- 1970 FOR I = 1 TO NC: FOR J = I + 1 TO NC
- 1980 IF I = J THEN GOTO IO10
- 1990 IF MID\$ (R\$.I.1) MID\$ (R\$.J.1) THEN GOTO 2010
- 2000 I = NC:J = NC: CALL 198: PRINT : FRINT "DUFLICATE CODE FOUN D": GOTO 2040
- 2010 NEXT J
- 2020 NEXT I
- 2000 6070 2060

- 2040 FOR I = 1 TO 2000: NEXT
- 2050 GDTD 1870
- 2060 RC\$ = R\$
- 2070 FOR I = 1 TO NC:CO\$(I) = MID\$ (RC\$,I,1): NEXT
- 2080 FC\$ = "": FOR I = 1 TD NC:FC \$ = FC\$ + " " + MID\$ (RC\$,I ,1): NEXT
- 2090 PARM\$(LINE) = R\$: GOSUB 5010
- 2110 HOME : GOSUB 5000 LINE = 5: GOSUB 5010
- 2:20 PRINT "ENTER THE FILENAME"
- 21TO INPUT "(16 CHARS MAXIMUM) -- ":R\$
- 2140 IF R\$ = "" THEN GOTO 2200
- 2150 R\$ = LEFT\$ (R\$,16)
- 2160 IF LEFT\$ (R\$,1) "A" OR LEFT\$ (R\$,1) "Z" THEN GOTO 2110
- 2170 FL\$ ≈ R\$
- 2180 PARM#(LINE) = R#: GOSUB 5710
- 2200 HOME : GOSUB 5700:LINE = 6: GOSUB 5710
- 2210 FRINT "SELECT THE OUTFUT FO RMAT: ": FRINT
- 2230 INFUT "WHICH (1-T) --- "4R\$
- 2240 IF R\$ = "" THEN GOTO 2290
- 2250 R = VAL (R\$): IF R = 1 OF R I THEN GOTO 2200
- 2260 OF = F
- 2270 FARM\$(LINE) = DF\$(QF): GQSUB 5710
- 2290 HOME : BOSUB 5300:LINE = 7: GOSUE 5310
- 2100 PRINT "GAIN CONTROL: (FEY CR) ":
- 2010, SET R#: PRINT
- 2020 IF 6\$ = CHR\$ (10) THEN GOTO 2560
- 2420 PRINT : FOR I = 0 TO T: PRINT GC\$(I):GC\$(I + 4): NEXT : PRINT
- 2430 INPUT "CHANNEL ID , GAIN CO NTROL (0-7) -- ":CH\$,6C\$
- 2440 CS\$ = CH\$: GOSUB 6050
- 2450 IF CS = 0 THEN FRINT "CHAN NEL NOT ACTIVE": GDTO 2490

- 2460 GC = VAL (GC\$): IF GC = 0 AND GC = 7 THEN GDTD 2
- 2470 FRINT "INVALID GAIN CONTROL
- 2480 FOR FSE = 1 TO 2000: NEXT: 60TO 2290
- 2490 GC(CH) = GC
- 2500 PARM\$(7) = "": FOR I = 1 TD LEN (AC\$):FARM\$(7) = PARM\$(7) + STR\$ (GC(CH(I))): NEXT
- 2510 IF SC = 0 THEN GAIN(CH) = 4 .99878
- 2520 IF GC = 1 THEN GAIN(CH) = 0 .99976
- 25TO IF 6C = 2 THEN GAIN(CH) = 0 .49988
- 2540 IF GC = T THEN GAIN(CH) \pm 0.09598
- 2541 IF GC = 4 THEN GAIN(CH) = 4 .99878
- 2542 IF GC = 5 THEN GAIN(CH) = 0 .99976
- 2543 IF GC = 6 THEN GAIN(CH) = 0 .49988
- 2544 IF GC = 7 THEN GAIN(CH) = 0
- 2550 GOSUB 5710: GOTO 2290
- 2560 AG = 8: FOA I ≈ 0 TO 15
- 2570 IF GC(I) AO THEN AG = GC(I)
- 2580 NEYT
- 2400 HOME : GOSUB 5TOO:LINE = 8: GOSUB 5T10
- 2610 PRINT "0/8 1/9 2/A 3/B 4/C 5/D 6/E 7/F"
- 2620 FDR I = 0 TO 15
- 2630 IF I / $\Omega = INT (I / 2)$ THEN INVERSE
- 2640 FRINT LEFT\$: STR\$ (CAL(I)) + " ".4);
- 2650, NORMAL
- 2660 PRINT " ";
- 2670 NEXT : FRINT
- 2680 PRINT "CALIBRATION CONSTANT S: (FEY CR) ";
- 2690 GET R#: PRINT
- 2700 IF R# = EHR\$ (17) THEN GOTO T220
- 2720 INFUT "CHANNEL ID , CAL. VALUE -- / ":CH\$,CC\$
- 2710 AC = LEN (AC\$)
- 2740 FOR I = 1 TO AC

- 2750 IF MID\$ (AC\$,I,1) = CH\$ THEN I = AC: GDTO 2780
- 2760 NEXT
- 2770 PRINT : PRINT : PRINT : PRINT "NDT AN ACTIVE CHANNEL": CALL 198: GDTD 2800
- 2780 CC = VAL (CC*): IF CC =
 1000 OR CC = 1000 THEN
 PRINT: FRINT: PRINT: PRINT
 "CONSTANT OUT OF RANGE": CALL
 198: GOTO 2800
- 2790 GDTD 2810
- T800 FOR FSE = 1 TO 2000: NEXT: 80TO 2400
- 2810 FOR I = 1 TO 16
- 2820 IF MID\$ (HEX\$,I,1) = CH\$ THEN CAL(I 1) = VAL (CC\$::I = 16: 6070 2840
- 2810 NEXT
- 2840 MN = CAL(0):MX = CAL(0)
- 2850 FOR I = 1 TO 15
- 2860 IF CAL(1) MN THEN MN = CA L(I)
- 28-0 IF CAL(I) MY THEN MX = CA L(I)
- 2880 NEXT
- 289(FARM\$(LINE) = LEFT\$ (STR\$ (MN',6) + "-- " + LEFT\$ (STR\$ (MY).6): GOSUB 5010
- 3200 GDTD 2600
- ZD20 HOME : GOSUB 5J00:LINE = 9:
 GDSUB 5J10
- 1220 FRINT "ENTER THE INTERVAL B
 ETWEEN"
- 1240 INFUT "READINGS (SECONDS) -- ":54: PRINT
- 1250 IF R\$ = "" THEN GOTD 1350
- D270 IF R INT (R) THEN GOTO
- 3280 DLY = R
- 1290.MIN = INT (DLY / 60):SEC = DLY MIN * 60
- 3000 DLY# = ""
- 3310 DLY\$ = DLY\$ + RIGHT\$ ("0" + STR\$ (MIN),2) + " MIN "
- DITO PARM#(LINE) = DLY#: GOSUB 5T
- 3360 PRINT "# OF READINGS FER IN STRUMENT"

- TITO INPUT "(2000 MAXIMUM) -- "
- 3380 IF R\$ = "" THEN GOT9 3430
- 3390 R = VAL (R\$): IF R 1 OR R > 2000 THEN GOTO 3350
- 3400 NR = R
- 3410 PARM\$(LINE) = R\$: GOSUB 5310
- 3430 HDME : GOSUB 5300:LINE = 11 : GOSUB 5310
- 3440 PRINT "FRINTER OPTION": PRINT
- T460 PRINT
- 3470 INFUT "SELECT (1-2) -- "4R
- 3480 IF R\$ = "" THEN GOTO 3540
- 1490 R = VAL (R\$): IF R 1 DF R
 2 THEN GOTO 3430
- 3500 P0 = R
- 3505 IF PO = 1 THEN PARM\$(LINE +
 1) = "1":F5 = 1
- 1520 PARM#/LINE) = PO#(R): GDSUB 5110
- 3540 HOME : SOSUB 5300:LINE = 12 : GDSUB 5310
- 3560 IF R\$ = "" THEN GOTO 3610
- 1570 R = VAL (R\$): IF R 0 OR R 7 THEN GOTO 3540
- 3580 PS = K
- 3590 FARM\$(LINE) = R\$: GOSUB 5710
- 3610 HOME : GOSU9 5300:LINE ≈ 13 : GOSUB 5310
- D620 INFUT "E(XECUTE) / D(UIT) -- ":R\$
- 1630 IF R\$ = "" THEN GOTO 1420
- 3640. IF R\$ "E" AND R\$ "D" THEN GOTO 3610
- 3650 IF R\$ = "0" THEN POLE 34.0
 : PRINT : PRINT "---FROGRAM
 TERMINATED---": END
- 3660 IF NC = 0 THEN 60TO 1500
- 3670 IF (F0 = 2 AND PS = 0) OR (PD = 1 AND PS = 0) THEN GOTO 3540
- 3690 OP\$ = D\$ + "OPEN "
- 3700 CL\$ = D\$ + "CLOSE "
- 7710 UF\$ = D\$ + "UNLOCH "

```
0720 RD$ = D$ + "READ "
0710 WR$ = D$ + "WRITE "
3740 DE# = D# + "DELETE "
3750 HOME
3760 \text{ RDG} = 0
     INVERSE: VTAB 15: HTAB 1: FRINT
3770
     " FRESS CONTROL-D TO TERMINA
     TE THIS RUN ": NORMAL : HOME
3780 PDFE - 16068,0
     IF PO = 2 THEN GOTO 3830
3790
      PRINT : FRINT Ds: "PR#":PS
3800 ·
T810
     GOSUB 5690
JBJO FOR M = 1 TO NA
B40 RD6 = RD6 + 1
3B50
      GOSUP 4760
7860 GOSUB 4610
0870 PRINT M:") ": MID$ (CT$.7.8
     );" ";: FOR + = 1 TO NC: FRINT
      INT (RDG(RDG,CH(F)) * 1000 +
     .5) / 1000;" ":: NEXT : FRINT
     : GQTQ 4380
4580
    IF M = NR THEN GOTO 45TO
4T90 IF (M / LPF) = INT (M / LP
     F) THEN FRINT CHR$ (12): IF
    FO = 1 THEN GOSUB 5690
4400 Pt = FEEt ( - 16384)
4410 IF F
               160 THEN GDTO 4
    450
4420
    HOME : FLASH : VTAB 20: HTAB
     17: PRINT " FAUSE ": NORMAL
    :Y = FRE (9): VTAB 22: HTAB
    8: PRINT "PRESS ANY FEY TO C
    ONTINUE": FORE -16768.0
    IF FEE! ( - 16084) 127 THEN
      G010 4410
4440
     HOME
4450 POFE - 16068.0
4460 IF FF = 145 THEN M = NR: BOTO
    4550
4470
    IF ADG
              = REWE AND FO = 1
     THEN FRINT : PFINT D#: "FR#
    ٠o٣
4480 IF RDG
              = REWR AND DF
    2 THEN 60SUB 4800
4490 IF RDG
               = REWE AND OF
    1 THEN GOSUB 4900
4500 IF RDG
               = REWR AND FO = 1
     THEN PRINT : FAINT D#: "FR#
    ":FS
4510 IF RDG

⇒ REWR THEN RDG ==

    0:FI = FI + 1
4520 GDSUB 5340
45TO NEXT M
```

```
4540
     POFE - 16068,0
     PRINT : PRINT CHR# (12): PRINT
4550
     : PRINT Ds:"PR#0"
4560
                - 2 THEN GOSUB 48
      IF OF
     00
     IF OF
4570
                  1 THEN GOSUB 49
     30
45B0
      GOSUB 5100
4590
     GOTO 1140
4610 \quad FOR \quad I = 0 \quad TO \quad 15
4620 AIIT = - 16256 + SLOT * 16
4600 PORE AIID.16 * GC(I) + I
4640 VOLTS(I) = FEEF (AIIC + 1) *
     256 + FEE! (AIII)
4650 NEXT I
4670 \text{ FOR I} = 0 \text{ TO } 15
     IF GC(I) 4 THEN VOLTS(I) =
4680
     VOLTS(I) * GAIN(I) / 4095 *
     CAL(I): GOTO 4700
4490 \text{ VOLTS}(1) = -(2048 - \text{VOLTS})
     IVY * GAIN(I) / 2048 * CAL(I
     ١.
4700 NEXT I
4710 FOF I = 1 TO NO
4720 \text{ RDG}(\text{RDG},\text{CH}(\text{I})) = \text{VOLTS}(\text{CH}(\text{I}))
     >
4770
     MEXI 1
4740 RETURN
4760
     CALL 768
4770 \text{ TM$(RDG)} = \text{MID$(CT$,7,8)}
4780 PETURN
4800 RC = 1: FKINT
4810 \text{ FD$} = "SAS." + FL$ + "." +
                                     STR#
     (FI)
     FRINT OF$;FO$; PRINT CL$;FO
4820
     $: PRINT DESERGE
4821
     FRINT OP$:FO$
4830 FRINT WESTEDS
4840 FOR I = 1 TO FDG
4850
     FOR J = 1 TO NO
4860 FRINT INT (RDS(I,CH(J)) *
     1000 + .5) / 1000%" ";
4870. NEXT
4880 FRINT TM$(I):" ";RN;FC$
4B90
      NEXT
4900 FRINT CL#;FO#
4910
      RETURN
4930 RC = 2: FRINT
4940 FO$ = "TGPH." + FL$ + "." +
      STR$ (FI)
4950
      FRINT OF $: FO$: PRINT CL$: FO
     $: FRINT DE$:FO$
     PRINT DP$:FD$
4951
4960 FRINT WR#: F8#
```

```
4970 FOR I = 1 TO NO
4980 L = 3
4990 FOR J = 1 TO RDG
5000 L = L + LEN (STR$ (INT (R
     DG(J,CH(I)) * 1000 + .5) / 1
     000)) + 10
     IF L 70 THEN FRINT "--":
5010
     L = 0: GOTO 5000
5020 PRINT TM$(J);","; STR$ ( INT
     (RDG(J_*CH(I)) * 1000 + .5) /
     1000);" ";
50to
     NEXT
5040 FRINT "--"
5050 FRINT "END OF CHANNEL ":CH(
     I)
SOAD NEXT
5070 FRINT CL#:FO#
50B0 RETURN
5100 HOME : PRINT "READ DATA FIL
    E " (Y/N) -- ":
5110 GET YNS: IF YNS
                          "Y" AND
             "N" THEN GDTO 5110
     YN#
5120 IF YN$ = "N" THEN GOTO 525
    Ü.
5130 TEXT : HOME : PRINT : PRINT
    D$:"CATALOG": PRINT : PRINT
5140 PRINT : INPUT "DATA FILE TO
      READ -- "; DF$
5150 IF DF$ = "" THEN GOTO 5250
5155 PRINT ' PRINT D$, "VERIFY ";
    DF$
5160 INFUT "FRINTER SLOT 1 ( CR
    =SCREEN) --- ":OS$
5170 \text{ OS} = \text{VAL (OS$): IF OS}
                              0 OR
        7 THEN GOTO 5160
    05
5180 IF OS
               O THEN PRINT D$
     :"PR#":0S
5190 PRINT D$: "MON I"
5200 FRINT D$:"OPEN ":DF$
5210' PRINT D#: "READ ":DF#
5220 GET +4' PRINT +4:: GOTD 521
    0
5230 PRINT : IF OS
                        O THEN FRINT
    D$; "PR#0"
5240 FRINT : PRINT D#; "CLOSE "; D
    F≇
5245 FRINT : PRINT D#: "NOMDN I"
5247 GOTD 5100
5250 RETURN
```

(I): NEXT

```
5280 FOR I = 1 TO 1T: VTAB I: HTAB
     24: CALL - 868: PRINT PARM#
     (I): NEXT
5290 RETURN
5300 VTAB LINE: HTAB 24: CALL -
    868: FRINT FARM# (LINE): HOME
     : RETURN
5310 VTAB LINE: HTAB 24: CALL -
     868: INVERSE : PRINT FARM#(L
     INE): NORMAL : HOME : RETURN
5540 T(1) ≈ VAL ( MID$ (FT$,7,2)
5050 T(2) = VAL \in MID = (FT = 10, I)
    ))
5060 T(3) = VAL ( MID# (FT#,10,2)
    ) )
5370 \text{ T}(4) = VAL ( MID$ (FT$,16,3)
     \rightarrow
5080 T(C) = T(C) → DUY
5090 FOR I = 0 TO 1 STEP - 1
5400 \text{ TTL} = \text{T}/\text{I}^{\circ}
5410 T(I) = TTL - INT (TTL / 60)
      * 60
5420 IF I
            1 THEN T(1 - 1) =
    T(I - 1) + INT (TTL / 60)
54TO NEXT
5440 ET$ = MID$ (FT$,1,6) + RIGHT$
     ("O" + STA$ (T(1)),1) + ":"
     + FIGHT$ ("0" + STE$ (T(2
    )),2) + "," + RIGHT$ ("O" +
     STR# (T(T)),2) + "." + RIGHT#
     ("0000" + STR$ (T(4)).5)
5450 CALL 768
5460 IF FT# ET$ THEN GOTO 545
    O
5470 RETURN
5490 ER = FEEF (222)
5500 CALL 805
5510 IF FD = 1 OR FO = 2 THEN PRINT
     · PRINT D&: "PR#O"
             5 AND ER 6 THEN
5520 IF ER
     HOME : FOR BELL = 1 TO 5: CALL
      - 198: NEYT : PRINT
      IF ER = 4 THEN GOTO 5590
5530
     IF ER = 5 THEN GOTO 5600
5540
     IF ER = 6 THEN GOTO 5610
5550
     IF ER = 8 THEN GOTO 5620
5560
     JF ER = 9 THEN 60TO 5600
5570
5575 IF EF = 5T OF ER = 49 OF ER
     = 191 DR ER = 254 THEN GOTO
     1140: REM BAD INPUT
```

```
5590 FRINT "WRITE PROTECT ERROR"
     : PRINT : PRINT "REMOVE THE
     WRITE PROTECT TAB": PRINT "E
     XISTING ON THIS DISLETTE.": GOTO
     5640
5600 RC = 0: GOTO 5230
5610 RC = 0: GOTO 5100
5620 PRINT "I/O ERROR": PRINT : FRINT
     "MAKE SURE DISHETTE WAS INIT
     IALIZED": FRINT "MAKE SURE D
     DOR ON DRIVE IS CLOSED.": GOTO
     5640
5610 PRINT DE$:FO$: PRINT "DISE
     FULL ERROR": FRINT : PRINT "
     INSERT ANOTHER INITIALIZED D
     ISLETTE": PRINT "TO SAVE THE
      CURRENT READINGS."
5640 FRINT : FRINT "FRESS ANY FE
     Y TO RETRY ":: GET | B#
5450 PRINT : HOME
5660 IF RC 2 THEN RC \approx 0:I \approx
    RDG:J = NC: GDTO 4800
5670 IF RC = 2 THEN RC = 0:I = N
    C:J = RDG: BOTO 4900
5690 PRINT : PRINT
5700 PG = FG ≁ 1
5710 PRINT "DATA ACQUISITION....
     . " =
5710 CALL 768
5730 PRINT CT#:
5740 PRINT SPC( 9): "FAGE ":PG
5750 FRINT "RUN NUMBER.... ....
     .":EN: SFC( 5):
5760 FRINT "ACTIVE CHANNELS....
     .":AC$; SPC( 5);
5770 FRINT "FILENAME........
     . " : FL =
57BO FRINT
57°0 RETURN
6050 CS = 0:CH = - 1
6060 AC = LEN (AC$)
6070 FOR I = 1 TD AC
6080 \cdot IF \quad MID$ (AC$,I,1) = CS$ THEN
    I = AC:CS = 1: GOTD 6110
6090 NEXT
6100 GBTD 6130
6110 CH = VAL (CS$)
6120 IF ASC (CS$)
                    64 AND ASC
     (CS\$) 71 THEN CH = ASC (C
    5$) - 55
6150 RETURN
```

APPENDIX V

Real-time and Filter Data

Filter Data

A complete listing of the filter data is listed. There were tWo types of clothing worn for the experiment, clean, which was the disposable clothing, and dirty, which was the workers' own coveralls. The two drum levels (signified as DRUM) were full, being two-thirds or more full, and empty, being one-third full or less. There were six sampling locations and are shown in Figure 9. Flow is given in standard cubic feet per hour, pressure drop across the filter (F DROF) in inches of water, weight on the filter (WEIGHT) in milligrams, and concentration in milligrams per cubic meter.

Real-time Data

The real-time data is given as strings. The members of the string are as follows:

1	RAM, inside the hood, volts.
2	RAM, background, volts.
3	HAM, worker lapel, volts.
4,5,6	Event markings.
7	Time, hours:minutes:seconds.
8	Run number.
9,10,11,	
12,13,14	Active channel numbers.

FILTER DATA

CLOTHING	DRUM	LOCATION	WORKER	FLOW	P DROP	WEIGHT	CONCENTRATION
Dirty	Full	Back Ground	1	29	32	0.04	0.142
Dirty	Full	Bin	1	30	33	0.04	0.136
Dirty	Ful1	Face	1	29	35	0.05	0.180
Dirty	Full	Hat	1	29	37	0.15	0.546
Dirty	Full	Left Lapel	1	29	37	0.25	0.903
Dirty	Empty	Back Ground	1	17	50	0.05	0.154
Dirty	Empty	Bın	1	25	50	0.10	0.294
Dirty	Empty	Face	1	29	34.5	0,11	0.325
Dirty	Empty	Hat	1	29	44	15.52	47,069
Dirty	Empty	Left Lapel	1	28	50	105.58	325,592
Clean	Full	Back Ground	1	29	30	0.01	0.049
Clean	Full	Bin	1	27	50	0.04	0.197
Clean	Fu11	Face	1	29	34	0.04	0.197
Clean	Full	Hat	1	29	37	5,13	25,700
Clean	Full	Left La pel	1	29	36	0.26	1,290
Clean	Empty	Back Ground	1	29	31.5	0.05	0.244
Clean	Empty	Bin	1	30	35	0.03	0.141
Clean	Empty	Face	1	10	50	0.07	0.359
Clean	Empty	Hat.	1	17	50	1,90	9.814
Clean	Empty	Left Lapel	1	28	40	18.47	92.160
Clean	Full	Back Ground	1.	29	31.5	0.05	0,258
Clean	Full	Bin	1	30	33	0.04	0.198
Clean	Ful1	Face	1	29	34	0.04	0.208
Clean	Full	Hat	1	29	36	0.18	0.946
Clean	Fu11	Left Lapel	1	28	38	3,11	16.317
Clean	Ful1	Right Lapel	1	28	38	4.36	22.719
Dirty	Empty	Back Ground	1	29	33	0.07	0.339
Dirty	Empty	Bin	1	30	32.5	0.07	0.323
Dirty	Empty	Pace	1	30	35.5	0.10	0.488
Dirty	Empty	Hat	1	17	50	0,55	2.810
D1rty	Empty	Left Lapel	1	28	45	35.73	178.766
Dirty	Empty	Right Lapel	1	28	50	75.66	381.226
Dirty	Full	Back Ground	1	29	32	0.23	1.350
Dirty	Ful1	Bin	1	30	35	1.49	8.413
Dirty	Ful1	Face	1.	29	38	7.71	46.004
Dirty	Ful1	Hat	1	29	33	5.58	33.077
Dirty	Ful1	Left Lapel	ı	28	40	15.17	91.011
Dirty	Ful1	Right Lapel	1	29	39.5	15.36	91.395
Clean	Empty	Back Ground	1	29	33	0.10	0.500
Clean	Empty	Bin	1	30	3 5	0.11	0.528
Clean	Empty	Face	1	29	37	0.08	0.405
Clean	Empty	Hat	1	29	37	1.43	7.283
Clean	Empty	Left Lapel	1	28	42	2.21	11.332
Clean	Empty	Right Lapel	1	28	50	90.11	469.169
Clean	Empty	Back Ground	2	29	31.5	0.01	0.035
Clean	Empty	Bin	2	14	50	0.06	0.211
Clean	Empty	Face	2	29	36	0.08	0.284
Çlean	Empty	Hat	2	28	50	1.52	5.643
							· -

FILTER DATA

CLOTHING	DRUM	LOCATION	WORKER	FLOW	P DROP	WEIGHT	CONCENTRATION
Clean	Empty	Left Lapel	2	28	49	4,34	15,956
Clean	Empty	Right Lapel	2	29	39.5	14.41	51.252
Dirty	Full	Back Ground	2	12	50	0.03	0.112
Dirty	Full	Bin	2	22	50	0.05	0.179
Dirty	Ful1	Pace	2	29	38	0.06	0.217
Dirty	Full	Haţ	2	29	37	0.65	2.365
Dirty	Full	Left Lapel	2	28	38	2.66	9.636
Dirty	Full	Right Lapel	2	28	40	4.27	15.447
Dirty	Empty	Back Ground	2	29	29.5	0.00	0.000
Dirty	Empty	Bin	2	30	33.5	0.02	0.069
Dirty	Empty	Face	2 2 2 2 2	14	50	0.11	0,413
Dirty	Empty	Hat	2	29	33	0.99	3.577
Dirty	Empty	Left Lapel	2	28	39	3,10	11,304
Dirty	Empty	Right Lapel	2	28	34	2.54	9.075
Clean	Full	Back Ground	2	29	32.5	0.02	0.069
Clean	Full	Bin	2	30	34	0.08	0.263
Clean	Ful1	Face	2	29	37	0.12	0.417
Clean	Ful1	Hat	2	29	38	0.75	2,632
Clean	Full	Left Lapel	2	28	37.5	1.65	5,742
Clean	Full	Right Lapel		28	45	3,99	14.077
Dirty	Empty	Back Ground	2 2 2	29	33	0.04	0.194
Dirty	Empty	Bin	2	30	33	0.07	0.323
Dirty	Empty	Face	2	29	34	0.10	0.486
Dirty	Empty	Hat	2	29	37	2,69	13.259
Dirty	Empty	Left Lapel	2	29	37	1.63	7.979
Dirty	Empty	Right Lapel	2	28	36.5	7.67	37,237
Clean	Empty	Back Ground	2	29	31	0.02	0.095
Clean	Empty	Bin	2	30	32.5	0.03	0.136
Clean	Empty	Face	2	29	33	0.27	1.287
Clean	Empty	Hat	2	29	37.5	1.09	5,294
Clean	Empty	Left Lapel	2	28	40	9.20	44.681
Clean	Empty	Right Lapel	2	29	31	3.38	15,912
Clean	Full	Back Ground	2	29	28	0.00	0.000
Clean	Fu11	Bin	2	30	32.5	0.03	0.165
Clean	Fu11	Face	2	29	34	0.12	0.695
Clean	Ful1	Hat	2	29	38	5.75	33.883
Clean	Full	Left Lapel	2	28	40	16.18	95.204
Clean	Fu11	Right Lapel	2	28	41	14.74	86.372
Dirty	Full	Back Ground	2	29	28.5	0.25	1.324
Dirty	Fu11	Bin	2	30	33	0.04	0.205
Dirty	Full	Face	2	30	31	0.05	0,267
Dirty	Full	Hat	2	29	37	1.85	10.095
Dirty	Full	Left Lapel	2	29	37	4.26	23.087
Dirty	Full	Right Lapel	2	29	32	3,50	18.586
Clean	Empty	Back Ground	3	29	34	0.10	0.412
Clean	Empty	Bin	3	24	50	0.21	0.863
Clean	Empty	Face	3	23	50	-0.01	-0.043
Clean	Empty	Hat	3	28	50	1.45	6.291
ATEUM	ոտելեն	Hat	•	-0	20	4.70	0,271

FILTER DATA

CLOTHING	DRUM	LOCATION	WORKER	FLOW	P DROP	WEIGHT	CONCENTRATION
Clean	Empty	Left Lapel	3	27	50	0.97	4,180
Clean	Empty	Right Lapel	3	28	38	18,54	76.757
Dirty	Empty	Back Ground	3	29	31	0.01	0.047
Dirty	Empty	Bin	3	30	32	0.14	0.625
Dirty	Empty	Face	3 3 3	21	50	-0.01	-0.049
Dirty	Empty	Hat	3	29	40	1,52	7,317
Dirty	Empty	Left Lapel	3	26	50	2.67	13.123
D1rty	Empty	Right Lapel	3	28	38	19.71	93.076
Clean	Full	Back Ground	3 3 3 3 3 3	29	31	0.00	0.000
Clean	Fu11	Bin	3	30	32	0.04	0.195
Clean	Full	Face	3	25	50	0.00	0.000
Clean	Full	Hat	3	26	50	0.11	0.594
Clean	Fu11	Left Lapel	3	26	50	0.29	1.555
Clean	Full	Right Lapel	3	29	31	0.54	2.729
Dirty	Ful1	Back Ground	3	29	31.5	0.34	1.753
Dirty	Full	${\tt Bin}$	3	30	32	0.08	0.394
Dirty	Fu11	Face	3 3 3	24	50	0.01	0.054
Dirty	Full	Hat	3	23	50	0.07	0.382
Dirty	Full	Left Lapel	3	27	50	0.10	0.542
Dirty	Full	Right Lapel	3	28	34	1.45	7.474
Dirty	Fu11	Back Ground	3 3	29	30	0.04	0.243
Dirty	Full	Bin	3	30	32.5	0.09	0.525
Dirty	Fu11	Face	3 3	29	32	0.03	0.183
Dirty	Full	Hat	3	25	50	-0.01	-0.065
Dirty	Full	Left Lapel	3	29	35	0.17	1.047
Dirty	Ful1	Right Lapel	3	29	34	1.33	8.115
Clean	Fu11	Back Ground	3	29	31	0.08	0.519
Clean	Full	Bin	3	30	32	0.02	0.124
Clean	Full	Face	3	29	39	-0.01	-0.066
Clean	Fu11	Hat	3	29	36	0.09	0.596
Clean	Full	Left Lapel	3	29	34.5	0.28	1.835
Clean	Ful1	Right Lapel	3	29	35.5	1.43	9,332
Dirty	Empty	Back Ground	3	29	30.5	0.06	0.416
Dirty	Empty	\mathtt{Bin}	3	30	34.5	0.21	1.404
Dirty	Empty	Face	3	26	50	0.01	0.073
Dirty	Empty	Hat	3	25	50	0.14	1.031
Dirty	Empty	Left Lapel	3	28	38	0.56	3.963
Dirty	Empty	Right Lapel	3	29	35	8.56	59,678
Clean	Empty	Back Ground	3	29	30	0.07	0.453
Clean	Empty	Bin	3	30	33	0.04	0.249
Clean	Empty	Face	3 3 3	29	33.5	0.16	1.046
Clean	Empty	Hat	3	29	43	10.61	71.649
Clean	Empty	Left Lapel	3	28	44	21.80	146.603
Clean	Empty	Right Lapel	3	28	37	3.14	20.574

Real-time Data

```
.029 .049 JE-07 2E-03 ZE-03 ZE-03 13:34:16 2 0 1 2 3 4 5
.007 .049 4E-00 DE-00 DE-00 4E-00 10:04:18 D 0 1 D 0 4 5
.014 .048 .012 1.289 2E-00 2E-00 13:04:20 2 0 1 2 0 4 5
.056 .049 .015 1.288 2E-00 2E-00 10:34:22 2 0 1 2 3 4 5
.052 .05 .015 1.288 1E-03 2E-03 13:34:24 2 0 1 2 3 4 5
.044 .051 .015 1.287 2E-03 4E-03 17:74:27 2 0 1 2 7 4 5
.039 .049 .01 1.287 2E-03 2E-03 13:74:29 2 0 1 2 3 4 5
.007 .052 5E-00 4E-00 1.287 1E-00 1T:04:01 2 0 1 2 T 4 5
.004 .051 .01 DE-00 4E-00 1.288 10:04:00 D 0 1 D 0 4 5
.001 .052 .01 2E-07 2E-07 1.2BP 17:04:05 2 0 1 2 3 4 S
.034 .054 .014 ZE-03 4E-03 4E-03 13:34:37 2 0 1 2 3 4 5
.041 .051 .013 1.287 2E-07 2E-03 13:34:79 2 0 1 2 3 4 5
.078 .05 PE-OI 1.187 RE-OI RE-OI 1I:I4:41 R 0 1 R 5 4 5
.080 .056 .009 2E-00 1.287 2E-00 10:04:40 2 0 1 2 0 4 5
.078 .054 .029 DE-01 1.287 DE-01 11; D4:45 D 0 1 D
.059 .054 .017 2E-00 1.287 2E-00 10:04:47 2 0 1 2 T 4 5
.054 .054 01 DE-00 1.287 DE-00 10:34:49 D 0 1 D 3 4 5
.044 OS 5E-07 RE-03 1.287 RE-03 13:74:51 R 0 1 R 7 4 5
1008 1052 AE-00 2E-00 4E-00 1.287 10:04:50 2 0 1 2
.007 .056 8E-00 2E-00 4E-00 1.287 10:04:55 2 0 1 2 0 4 5
.004 .06 .015 DE-00 4E-00 1.287 10:04:57 D 0 1 D 0 4 5
.014 .059 .011 2E-03 4E-03 4E-03 17:14:59 2 0 1 2 7 4 5
.000 .059 .01 1.287 2E-00 4E-00 10:05:01 2 0 1 2 7 4 5
.049 .057 .01 1.287 ZEHOD ZEHOD 17:05:00 Z 0 1 Z 0 4 5
.054 .059 .015 1.285 1E-03 RE-03 13:35:06 2 0 1 2 7 4 5
.049 .056 .019 .059 2E-01 2E-01 11:15:08 2 0 1 2 I
.046 .054 .017 2E-03 1.287 DE-03 13 D5:10 2 0 1 2 3 4 5
.049 .052 .016 2E-03 1.287 2E-03 13:75:12 2 0 1 2 7 4 5
.04% .05 BE-07 4E-03 1.2B5 1E-07 17:75:14 2 0 1 2 0 4 5
.049 .050 6E-01 0E-01 1.085 1E-01 10:05:16 D 0 1 D 0 4 5
.049 .051 66-00 DE-07 1.285 DE-07 17:75:18 D 0 1 D 7 4 5
.040 .05 .070 PE-01 .040 PE-01 10:05:20 2 0 1 2 0 4 5
.039 .051 .031 2E-07 2E-07 1.287 13:35:22 2 0 1 2 7
.034 .051 .014 25-01 4E-03 1.287 13:35:24 2 0 1 2 3 4 5
.004 .054 .012 28-07 28-07 1.287 10:05:26 2 0 1 2 7 4 5
.037 .054 .011 1.284 2E-03 4E-03 17:35:2B 2 0 1 2 7 4 5
.040 .052 .01 1.284 1E-07 DE-07 13:75:70 2 0 1 2 7 4 5
.048 .056 .015 5E-01 1.284 DE-07 13:35:32 2 0 1 2 7 4 5
.044 .054 9E-01 2E-03 1.284 2E-03 1T:35:74 2 0 1 2 3 4 5
.04 .051 .016 .016 1.284 DE-OI II:35:76 2 0 1 2 T 4 5
009 .051 .016 DE-00 1.284 DE-00 10:05:08 D 0 1 D 7 4 5
.014..054 .014 2E-03 1.284 2E-03 13:75:40 2 0 1 2 3 4 5
.000 .052 .002 2E-00 .154 2E-00 13:05:42 2 0 1 2 0 4 5
.029 .051 .054 DE-07 4E-07 1.287 17:75:45 D 0 1 D 7 4 5
.032 .051 .021 2E-03 2E-03 1.287 13:35:47 2 0 1 2 7 4 5
.031 .05 9E-01 2E-03 4E-03 1.287 13:35:49 2 0 1 2 3 4 5
.029 .05 .015 1.284 2E-00 4E-00 10:05:51 2 0 1 2 0 4 5
.04 .051 8E-01 1.284 2E-03 2E-07 13:35:57 2 0 1 2 3 4 5
.051 .05 .014 1.284 2E-07 2E-07 17:75:55 1 0 1 7 7 4 5
.044 .051 .011 1.284 1E-03 4E-03 13:35:57 2 0 1 2 3 4 5
```

```
.043 .05 .013 .011 1.207 2E-03 13:35:59 2 0 1 2 3 4 5
.046 .049 .012 2E-03 1,284 2E-03 13:36:01 2 0 1 2 3 4 5
.046 .05 8E-05 2E-05 1.284 2E-05 15:56:05 2 0 1 2 5 4 5
.042 .05 8E-03 2E-03 4E-03 1.285 13:34:05 2 0 1 2 3 4 5
.008 .05 4E-00 2E-00 4E-00 1.287 10:36:07 2 0 1 0 5 4 5
.034 .048 7E-03 2E-03 4E-03 1.285 13:36:09 2 0 1 2 7 4 5
.034 .046 4E-03 2E-07 2E-07 1.285 13:74:11 2 0 1 2 5 4 5
.043 .049 DE-01 1.283 2E-03 4E-03 13:36:13 2 0 1 2 3 4 5
.048 .049 5E-03 1.284 1E-03 4E-03 13:36:15 2 0 1 2 3 4 5
.046 .049 .01 1.280 DE-03 DE-03 13:36:17 D 0 1 2 5 4 5
.044 .05 7E-03 4E-03 1.284 2E-03 13:36:19 2 0 1 2 7 4 5
.039 .049 8E-03 2E-03 1,284 2E-03 13:36:21 2 0 1 2 3 4 5
.035 .05 66-03 2E-03 1.284 2E-03 13:76:23 2 0 1 2 3 4 5
.037 .049 AE-01 2E-03 1.284 2E-03 13:36:26 2 0 1 2 3 4 5
.007 .049 8E-03 2E-03 2E-03 1.284 13:36:28 2 0 1 2 3 4 5
.034 .049 6E-03 2E-03 2E-03 1.285 13:36:30 2 0 1 2 3 4 5
.004 .049 8E-03 2E-03 2E-03 4E-03 13:36:32 2 0 1 2 3 4 5
.014 .048 5E-01 1.283 2E-03 2E-01 13:36:34 2 0 1 2 3 4 5
.039 .048 9E-00 1.280 2E-00 4E-00 10:06:06 2 0 1 2 0 4 5
.037 .048 .016 1.283 2E-03 2E-03 17:36:38 2 0 1 2 3 4 5
.034 .049 .01 4E-03 1.2B3 2E-03 13:36:40 2 0 1 2 3 4 5
.005 .049 .01 PE-00 1.280 RE-00 10:06:42 2 0 1 2 0 4 5
.004 .049 5E-00 2E-00 1.2B0 2E-00 10:06:44 0 0 1 0
.031 .048 .135 QE-03 1.283 QE-03 17:76:46 2 0 1 2 7 4 5
.029 .046 .09 2E-07 1.284 1E-07 17:36:48 2 0 1 2 7
.027 .048 .031 2E-03 1.283 2E-03 13:36:50 2 0 1 2 3 4 5
.027 .046 .02 2E-03 9E-03 4E-03 10:06:52 2 0 1 2 3 4 5
.027 .048 7E-01 2E-01 4E-01 1.284 13:36:54 2 0 1 2 1 4 5
.028 .048 5E+03 2E-03 2E-03 4E-03 13:34:56 2 0 1 2 3 4 5
.029 .048 8E-00 1.280 2E-00 2E-00 10:06:58 2 0 1 2
.032 .048 9E-01 1.282 2E-03 2E-03 13:37:00 2 0 1 2
.040 .046 .02 1/282 2E-03 2E-03 13:37:02 2 0 1 2 3 4 5
.046 .051 .026 1.282 DE-00 DE-00 10:07:05 D 0 1 D 0 4 5
.044 .049 .029 2E-03 4E-03 4E-03 13:37:07 2 0 1 2 3 4 5
.040 .045 .06 2E-07 1.284 2E-03 13:07:09 2 0 1 2 3
.040 .046 .007 2E-00 1.280 2E-00 13:07:11 2 0 1 2 0 4 5
.044 .044 .019 2E-07 1.2B2 1E-07 13:37:13 2 0 1 2 7 4 5
.008 .046 .017 2E-03 4E-03 1.284 13:07:15 2 0 1 2 3 4 5
.007 .046 .015 2E-00 2E-00 1.284 10:07:17 2 0 1 2 D 4 5
.048 .046 7E-01 1.282 2E-01 4E-03 13:17:19 2 0 1 2 1 4 5
.051 .048 SE-01 1.282 RE-03 2E-03 13:37:21 2 0 1 2 7 4 5
.054..051 .081 1.282 2E-00 2E-00 10:07:20 2 0 1 2 0 4 5
.051 .051 .052 1.282 DE-03 DE-03 13:37:25 D 0 1 D 3 4 S
.046 .052 .000 1.282 2E-00 2E-00 10:07:27 2 0 1 2 0 4 5
.046 .054 .019 1.281 RE-01 RE-01 11:37:29 2 0 1 2 7 4 5
.045 .054 .011 2E-03 1.282 2E-03 13:37:31 2 0 1 2 3 4 5
.046 .054 7E-07 2E-03 2E-03 1.284 13:37:33 2 0 1 2 3 4 5
.044 .054 5E-00 2E-00 2E-00 1.284 10:07:05 2 0 1 2
.042 .054 5E-03 1.282 2E-03 4E-03 13:37:37 2 0 1
.04 .05 5E-03 1.281 2E-03 2E-03 13:37:39 2 0 1 2 3 4 5
```

```
.04 .049 DE-03 4E-03 DE-03 4E-03 13:38:48 2 0 1 2 3 4 5
.042 .048 1E-03 4E-03 2E-03 2E-03 13:38:50 2 0 1 2 7 4 5
.04 .049 1E-03 ZE-03 ZE-03 ZE-03 17:38:52 2 0 1 2 3 4 5
.007 .048 £E-00 1.287 £E-00 2E-00 10:08:54 £ 0 1 2 0 4 5
.046 .049 TE-00 1.284 1E-00 2E-00 iT:T8:56 2 0 1 2 0 4 5
.073 .049 5E-01 1.284 2E-03 2E-03 13:38:59 2 0 1 2 3 4 5
.062 .048 .028 1.284 1E-01 4E-03 13:39:01 2 0 1 2 3 4 5
.054 .046 .054 2E-00 1.284 1E-00 10:09:00 2 0 1 2 0 4 5
.045 .046 .025 2E-03 1.284 2E-03 13:39:05 2 0 1 2 3 4 5
.042 .046 .014 2E-03 1.284 2E-03 13:39:07 2 0 1 2 3 4 5
.009 .049 9E-03 DE-07 1.284 DE-07 13:39:09 D 0 1 D 7 4 5
.042 .05 .01 2E-07 2E-07 1.284 17:39:11 2 0 1 2 7 4 5 .04 .05 8E-07 2E-07 2E-07 1.284 17:39:17 2 0 1 2 7 4 5
.007 .05 6E-00 2E-00 4E-00 1.284 10:09:15 2 0 1 2 0 4 5
.007 .05 4E-07 1.284 1E-05 4E-05 10:39:17 2 0 1 2 5 4 5
.074 .05 JE-07 1.285 1E-05 2E-05 17:59:19 2 0 1 2 7 4 5
.04 .049 7E-00 1.282 2E-00 2E-00 10:07:20 2 0 1 2 3 4 5
.044 .048 .017 1.282 2E-07 2E-07 17:79:26 2 0 1 2 7 4 5
.048 | 049 .012 1.282 1E-07 4E-07 17;79:28 2 0 1 2 7 4 5
.046 .048 .015 2E-01 1.282 2E-03 17:T9:30 2 0 1 2 3 4 5
.042 .048 .012 PE-01 1.282 PE-01 15:75:72 P 0 1 P 5 4 5
.039 .05 8E-03 2E-03 1.282 2E-03 13:39:34 2 0 1 2 3 4 5
.037 .051 .017 2E-01 1.282 2E-03 13:39:36 2 0 1 2 3 4 5
.032 .052 .01 2E-01 4E-03 1.284 17:39:78 2 0 1 2 T 4 5
.014 .050 5E-01 2E-01 2E-03 1.284 13:39:40 2 0 1 2 3 4 5
.007 .054 86-00 1.282 26-00 46-00 10:09:42 2 0 1 2 0 4 5
.049 .054 .014 1.282 2E-07 2E-07 17:79:44 2 0 1 2 3
.056 .056 .015 1.282 2E-01 4E-01 10:19:46 D 0 1 D 1 4 5
.051 .056 .016 1.282 2E-03 2E-03 13:79*48 2 0 1 2 3 4 5
.046 .056 .007 DE-00 1.282 DE-00 10:09:50 2 0 1 2 0 4 5
.042 .059 .022 2E-03 1.282 2E-03 17 39;52 2 0 1 2
.078 .059 .012 2E-03 1.282 2E-07 13:T9:54 2 0 1 2 T 4 5
.007 .056 6E-00 2E-00 1.282 2E-00 10:09:56 2 0 1 2 0 4 5
.037 .056 .011 25-03 46-01 1,284 17:79:58 2 0 1 2 T 4 5
.014 .056 .015 DE-01 DE-01 1.281 10:40:00 2 0 1 2 0 4 5
.004 .054 8E-03 1.207 2E-07 .017 10:40:02 2 0 1 2 T 4 5
.007 .054 6E-03 1.281 DE-03 DE-01 13:40:05 1 0 1 1 3 4 5
.046 .054 4E-00 1.281 2E-00 2E-00 1T:40:07 2 0 1 2 T 4 5
.049 .056 .01T 1.281 2E-07 2E-07 10:40:09 2 0 1 2 5 4 5
.046 .056 .012 1.281 28-07 28-07 17:40:11 2 0 1 2 3 4 5
.019 .059 .01 2E-01 1.281 2E-01 11:40:13 2 0 1 2 3 4 5
.037·.059 5E-07 2E-07 1.282 2E-07 17:40:15 2 0 1 2 7 4 5
.018 .059 4E-01 CE-01 1.081 CE-01 11:40:17 0 0 1 0 0 4 5
.039 .059 .024 2E-03 4E-03 1.283 13:40:19 2 0 1 2 3 4 5
.017 .059 .012 2E-03 4E-01 1.2B0 10:40:21 2 0 1 2 0 4 5
.017 .059 BE-03 2E-03 2E-03 1.283 13:40:23 2 0 1 2 3 4 5
.037 .059 6E-03 1.281 2E-03 4E-03 13:40:25 2 0 1 2 3 4 5
.062 .057 7E-03 1.281 1E-03 2E-03 13:40:27 2 0 1 2 3 4 5
.07 .057 .012 1.281 2E-03 DE-03 13:40:29 2 0 1 2 3 4 5
.06 .056 .016 1.281 2E-03 2E-03 13:40:31 2 0 1 2 3 4 5
```

.054 .056 .045 4E-03 1.281 1E-03 13:40:33 2 0 1 2 3 4 5 .046 .056 .055 2E-03 1.281 2E-03 13:40:35 2 0 1 2 3 4 5 .04 .056 .025 2E-03 1.281 2E-03 13:40:37 2 0 1 2 3 4 5 .038 .057 9E-03 2E-03 1.2B1 2E-03 13:40:39 2 0 1 2 3 4 5 .014 .059 .01 DE-03 DE-03 1.282 13:40:41 2 0 1 2 J 4 5 .034 .057 9E-03 2E-03 2E-03 1.282 13:40:43 2 0 1 2 3 4 5 .074 .06 4E-03 2E-03 2E-03 1.282 13:40:46 2 0 1 2 3 4 5 .034 .059 4E-07 1.281 2E-03 4E-03 13:40:48 2 0 1 2 3 4 5 .042 .056 &E-QT 1.281 2E-QT 2E-QT 13:40:50 2 0 1 2 3 4 5 .056 .059 .067 1.279 2E-01 4E-03 13:40:52 2 0 1 2 3 4 5 .051 .06 .055 4E-01 1.281 2E-01 11:40:54 2 0 1 2 3 4 5 .046 .056 .14 RE-00 1.281 RE-00 17:40:56 R 0 1 R 0 4 5 .04 .059 .051 DE-03 1.281 DE-03 10:40:58 D 0 1 D 3 4 5 .008 .059 .018 2E-03 7E-03 1.265 13:41:00 2 0 1 2 3 4 5 .019 .056 .01 DE-01 4E-01 1.2B2 15:41:02 D 0 1 2 3 4 5 .038 .054 7E-03 GE-03 GE-03 1.282 13:41:04 2 0 1 2 3 4 5 .008 .056 6E-00 1.281 DE-00 4E-00 10:41:06 D 0 1 D 0 4 5 .078 .056 4E-07 1.281 1E-07 4E-07 17:41:08 2 0 1 2 3 4 5 .040 .056 BE-00 1.279 2E-00 2E-00 10:41:10 2 0 1 0 .046 .056 .017 1.279 2E-07 2E-07 17:41:12 2 0 1 2 7 4 5 .046 .056 .016 .466 1.278 ZE-OI 13:41:14 Z O 1 Z 3 4 5 .046 .056 .021 2E-07 1.281 2E-07 17:41:16 2 0 1 2 7 4 5 .044 .056 .015 QE-07 1.281 QE-07 17:41:18 C 0 1 C T 4 5 .04% .056 BE-0% 2E-0% 1.28% 2E-0% i%:41:20 2 0 % 2 % 4 5 .04 .054 5E-07 2E-07 .015 2E-07 17:41 2D 0 0 1 0 3 4 5 .079 .054 .017 2E-07 4E-07 1.282 17:41:25 2 0 1 2 7 4 5 .007 .054 9E-00 DE-00 DE-00 1.D8D 10:41:27 D 0 1 D 0 4 5 .04 .054 .014 2E-07 2E-07 1.282 13:41:29 2 0 1 2 7 4 5 .044 .054 6E-03 1.279 2E-03 2E-03 13:41:31 2 0 1 2 3 4 5 .041 .054 .011 1.279 2E-01 4E-01 15:41:33 2 0 1 2 3 4 5 .044 .054 9E-0T 1.279 2E-0T 4E-0T 1T:41:T5 2 0 1 2 T 4 5 .046 .052 .024 1.279 2E+03 2E+03 13:41:37 2 0 1 2 3 4 5 .044 .051 .017 .066 1.279 DE-00 10:41:09 D 0 1 D 0 4 5 .046 .054 .014 DE-07 1.281 DE-07 17:41:41 2 0 1 2 3 4 5 .046 .054 7E-03 2E-07 1.281 2E-07 17:41:43 2 0 1 2 3 4 5 .044 .059 .02 2E-03 .227 1.234 13:41:45 2 0 1 2 7 4 5 .040 .06 .012 2E-00 4E-00 1.281 10:41:47 2 0 1 2 0 4 5 .044 .06 .011 2E-07 2E-07 1.281 17:41:49 2 0 1 2 .049 .059 .012 2E-03 2E-03 1.281 13:41:51 2 0 1 2 3 4 5 .048 .056 .014 DE-00 DE-00 1.281 iT:41:50 D 0 1 D 0 4 5 .051 .054 .015 1.279 1E-03 4E-03 17:41:55 2 0 1 .054.,054 .017 1.279 2E-01 2E-01 10:41:57 2 0 1 2 .059 .054 .031 1.279 REHOW 4EHOW 17:41:59 R 0 1 R 7 4 5 .061 .056 .051 QE-05 1.279 QE-05 15:42:01 2 0 1 2 T 4 5 .06 .054 .015 2E-0T 1.279 2E-0T 1T:42:0T 2 0 1 T T 4 5 .060 .051 .01 QE-00 1.279 QE-00 10:40*06 2 0 1 2 3 4 5 .061 .051 .219 2E-00 1.279 2E-00 10:42:08 2 0 1 2 0 4 5 .056 .052 .104 2E+00 4E-00 1.281 17:42:10 2 0 1 2 3 4 5 .061 .052 .017 RE-01 RE-03 1.282 11:41:12 1 0 1 2 1 4 5 .061 .056 .014 2E-03 2E-03 .068 13:42:14 2 0 1 2 3 4 5

```
.03B .051 5E-00 2E-00 4E-00 4E-00 10:40:20 2 0 1 2 0 4 5
.018 .054 SE-03 2E-03 4E-03 4E-03 17:47:25 2 0 1 2 3 4 5
-018 -054 4E-01 1.281 2E-01 2E-01 15:43:27 2 0 1 2 3 4 5
.OTB .054 4E-00 1.082 2E-00 4E-00 10:40:29 2 0 1 2 0 4 5
.043 .057 .011 1.282 2E+03 2E+03 13:43:31 2 0 1 2 3 4 5
-068 .06 .011 1.281 ZE-07 ZE-03 13:40:74 Z O 1 Z 3 4 5
.060 .060 .00 1.281 26-00 26-00 10:40:06 0 0 1 0 0 4 5
.051 .06 .025 4E-03 1.281 2E-03 13:43:38 2 0 1 2 3 4 5
.048 .060 .040 2E-00 1.281 2E-00 10:40:40 2 0 1 2 0 4 5
.044 .060 .015 QE-00 1.281 QE-00 10:40:40 0 0 1 0 0 4 5
.039 .066 .015 2E-03 1.281 2E-03 13:43:44 2 0 1 2 3 4 5
.04 .060 .016 2E-03 4E-03 1.282 13:43:46 2 0 1 2 3
-04 -062 BE-00 2E-00 4E-00 1.282 10:40:48 2 0 1 2 0 4 5
.039 .041 5E-03 1.281 2E-03 4E-03 17:43:50 2 0 1 2 3 4 5
.009 .061 5E-01 1.279 2E-03 2E-01 13:43:52 2 0 1 2 3
.04 .061 5E-0J 1.281 2E-0J 2E-0J 1J:4J:54 2 0 1 2 J 4 5
.062 .062 .018 1.279 2E-03 4E-03 13:47:58 2 0 1 2 3 4 5
.059 .06 .021 1.279 1E-01 2E-03 13:44:00 2 0 1 2 3 4 5
.054 .06 .047 RE-00 1.281 RE-00 10:44:02 2 0 1 2 5 4 5
.049 .06 .035 PE-03 1.281 PE-03 13:44:04 P 0 1 P J 4 5
.046 .061 .017 2E-03 1.281 2E-03 13:44:06 2 0 1 2 3 4 5
.045 .06 .012 2E-05 5E-07 1.281 15:44:08 2 0 1 2 7 4 5
.042 .062 6E-03 CE-03 CE-03 1.281 17:44:11 2 0 1 2 3 4 5
.04 .061 4E-05 DE-05 DE-05 1.DB2 15:44:17 2 0 1 2 5 4 5
.046 .041 5E-03 2E-03 4E-03 1.282 13:44:15 2 0 1 2 3 4 5
.068 .062 .016 1.279 2E-03 4E-03 13:44:17 2 0 1 2 3 4 5
.088 .062 .071 1.279 2E-07 4E-07 13:44:19 2 0 1 2 5 4 5
.060 .065 .104 1.279 1E-00 4E-00 15:44:20 0 0 1 0 7 4 5
.054 .060 .070 1.279 2E-00 2E-00 10:44:25 2 0 1 2 0 4 5
.049 .061 .021 4E-03 1.279 2E-03 13:44:27 2 0 1 2 3 4 5
.044 .041 7E-05 2E-05 1.279 2E-05 15:44:19 2 0 1 2 5 4 5
.046 .061 .071 PE-03 4E-07 1.281 13:44:71 P 0 1 P 3 4 5 .046 .059 .019 PE-03 PE-07 1.281 17:44:77 P 0 1 P 7 4 5
.044 .06 8E-01 2E-01 2E-02 4E-01 13:44:35 2 0 1 2 3 4 5
.045 .06 6E-05 1.279 2E-05 4E-05 10:44:58 2 0 1 2 3 4 5
.044 .061 5E-03 1.279 2E-03 2E-03 13:44:40 2 0 1 2 3 4 5
.07 .06 .014 1.279 1E-03 4E-03 13:44:42 2 0 1 2 7 4 5
.061 .06 .071 1.279 DE-07 DE-07 17:44:44 2 0 1 D 7 4 5
.056 .066 .045 1.277 2E-03 2E-03 13'44:46 2 0 1 2 3 4 5
.049..062 .024 4E-03 1.279 2E-03 13:44:50 2 0 1 2 3 4 5
.048 .059 .019 DE-01 1.279 1E-01 11:44:51 2 0 1 2 1 4 5
.046 .057 .011 2E-03 1.279 2E-03 13:44:54 2 0 1 2 3 4 5
.042 .059 .017 1.252 6E-03 4E-03 13:44:56 2 0 1 2 3 4 5
.049 .059 9E-03 1.279 2E-03 2E-03 13:44:58 2 0 1 2 3 4 5
.051 .059 .01 1.279 1E-03 2E-03 13:45:00 2 0 1 2 3 4 5
.05 .056 .117 1.278 1E-03 2E-03 13.45:02 2 0 1 2 3 4 5
.049 .054 .035 1.279 1E-03 2E-03 13:45:04 2 0 1 2 3 4 5
.05 .052 .071 26-03 1.279 16-07 13:45:06 2 0 1 2 3 4 5
```

```
.051 .054 .025 2E-03 1.278 2E-03 13:45:08 2 0 1 2 3 4 5
.05 .054 .015 DE-00 1.279 DE-07 17:45:10 D 0 1 D 0 4 5
.048 .054 .011 2E-07 1.279 1E-07 17:45:12 2 0 1 2 7 4 5
.046 ,054 .01 2E-03 1.279 2E-03 13:45:14 2 0 1 2 3 4 5
.044 .056 .01 DE-07 4E-03 1.281 13:45:16 2 0 1 2 3 4 5
.044 .054 8E-03 2E-03 2E-03 5E-03 13:45:19 2 0 1 2 3 4 5
.044 .054 7E-03 1.278 DE-03 DE-03 13:45:21 2 0 1 2 3 4 5
.044 .054 8E-03 1.278 2E-03 4E-03 13:45:23 2 0 1 2 3 4 5
.048 .055 .017 1.278 DE-07 DE-07 13:45:25 D 0 1 2 T 4 5
.061 .059 .044 2E-03 1.279 2E-03 13:45:27 2 0 1 2 3 4 5
.054 .06 .054 2E-00 1.279 1E-00 13:45:29 2 0 1 2 0 4 5
.048 .06 .158 2E-03 1.279 2E-03 13:45:31 2 0 1 2 3 4 5
1049 .06 .072 CE-01 1.279 CE-03 13:45:13 2 0 1 2 3 4 5
.046 .062 .027 2E-03 1.279 2E-03 13:45:35 2 0 1 2 3 4 5
.042 .061 .03 DE-03 1.279 DE-03 13:45:37 D 0 1 D 3 4 5
.042 .061 .026 2E-00 4E-00 4E-00 10:45:09 2 0 1 2 0 4 5
.039 .06 .02 CE-03 4E+03 1.281 13:45:41 2 0 1 2 3 4 5
.038 .059 .011 2E-03 2E-03 1.279 13:45:43 2 0 1 2 3 4 5
.04 .059 6E-01 DE-03 DE-01 1.279 13:45:45 1 0 1 1 T
.054 .059 .024 2E-03 2E-03 1.279 13:45:47 2 0 1 2 3 4 5
.061 .059 .00 1.277 DE-03 4E-01 11:45:49 D 0 1 D T 4 5
.059 .056 .016 1.278 2E-07 2E-07 17:45:51 2 0 1 2 7 4 5
.056 .054 .060 1.277 2E-00 2E-00 10:45:50 2 0 1 2 0 4 5
.05 .051 .07 1.277 2E-03 2E-03 13:45:55 2 0 1 2 3 4 5
.05 .049 .042 1 277 PE-OT 2E-OT 17:45:57 2 0 1 2 7 4 5
.056 .048 .018 2E-01 1.279 2E-01 13:45:59 2 0 1 2 3 4 5
.05 .049 .01 2E-03 1.278 2E-03 13:46:02 2 0 1 2 3 4 5
.049 .048 .021 2E-03 1.279 2E-03 13:46:04 2 0 1 2 3 4 5
.046 .05 .021 2E+03 4E-03 1.279 13:46:06 2 0 1 2 7 4 5
.046 .048 .017 1.277 2E-07 4E-07 13:46:08 2 0 1 2 7 4 5
.059 .049 .019 1.277 1E-05 4E-05 15:46:10 C 0 1
.063 .05 .018 .065 1.262 2E-03 1T:46:12 2 0 1 2 3 4 5
.(71 05 .027 CE-03 1.278 CE-03 13:46:14 C 0 1 C T 4 5
.048 .049 .025 DE-05 1.278 DE-05 10:46:16 D 0 1 D 5 4 5
.059 .049 .015 DE-01 1.278 DE-03 13:46:18 2 0 1 2 3 4 5
.05 .049 .011 ZE-03 1.278 ZE-03 13:46:20 2 0 1 2 3 4 5
.046 .049 9E-00 2E-00 1.278 2E-00 10:46:22 2 0 1 2 0 4 5
.046 .049 .014 DE-OT DE-OT 1.279 10:46:04 D O 1 D 3 4 5
.05 .049 BE-01 2E-03 2E-03 1.279 13:46:26 2 0 1 2 3 4 5
.048 .049 4E-01 DE-01 DE-01 .034 10:46:DB D 0 1 D 3 4 5
.046 .051 6E-01 1.277 2E-03 4E-01 11:46:30 2 0 1 2 3 4 5
.0591.054 .027 1.277 DE-03 DE-03 17:46:32 2 0 1 2 3 4 5
.059 .056 .014 1.277 2E-01 2E-01 11:46:14 2 0 1 2 3 4 5
.054 .059 .025 1.277 2E+00 2E-00 10:46:06 0 0 1 2 0 4 5
.049 .056 .079 1.277 1E-01 4E-03 13:46:38 2 0 1 2 3 4 5
.049 .054 .011 2E-01 1.278 2E-01 10:46:40 2 0 1 2 3 4 5
.048 .056 .017 2E-03 1.277 1E-03 13:46:43 2 0 1 2 3 4 5
.042 .052 .098 2E-0T .482 2E-0T 1T:46:45 2 0 1 2 T 4 5
.049 .056 .055 2E-03 2E-03 1.279 13:46:47 2 0 1 2 3 4 5
.044 .06 .026 2E-03 2E-03 1.279 13:46:49 2 0 1 2 3 4 5
```

```
.045 .062 7E-03 4E-03 4E-03 4E-03 13:47:58 2 0 1 2 3 4 5
.044 .062 3E-03 2E+03 2E-03 2E-03 10:48:00 2 0 1 2 3 4 5
.044 .062 TE-0T 1.281 DE-0T DE-0T 15:48:02 D 0 1 D 7 4 5
.044 .065 7E+05 1.279 1E+05 2E+05 15:48:04 2 0 1 2 3 4 5
.044 .062 .015 1.279 DE-01 DE-01 13:48:06 D 0 1 D T 4 5
.040 .060 .040 1.268 1.268 1E-05 15:48:08 0 0 1 0 7 4 5
.042 .062 .029 1.26B 1.267 2E-03 13:4B:10 2 0 1 2 3 4 5
.040 .060 .025 5E-00 1.278 2E-00 10:48:12 2 0 1 2 7 4 5
-044 -066 -067 2E-03 1.279 2E-03 17:48:14 1 0 1 2 3 4 5
-044 .06 .027 2E-00 1.279 2E-00 10:48:16 2 0 1 2 0 4 5
.040 .061 .02 DE-00 4E-00 1.281 17:48:19 0 0 1 0 0 4 5
.042 .065 .027 2E-03 4E-03 1.279 13:48:21 2 0 1 2 7 4 5
.008 .048 .01 DE-00 2E-00 1.279 10:48:20 2 0 1 2 0 4 5
.078 .066 6E-03 2E-07 4E-07 .145 13:48:25 2 0 1 2 7 4 5
.043 .066 6E-03 1.278 2E-03 2E-03 10:48:27 2 0 1 2 3 4 5
-082 -065 -18 1.277 2E-03 4E-03 13:48:29 2 0 1 2 3 4 5
.073 .062 .118 1.277 2E-03 2E-03 13:48:31 2 0 1 2 3 4 5
.066 .060 .046 1.277 2E-00 2E-00 10:48:00 2 0 1 2 0 4 5
.059 .061 .041 2E-03 1.278 2E-03 13:48:35 2 0 1 2
.05 .063 .028 2E-03 1.278 2E-03 13:48:37 2 0 1 2 3 4 5
.046 .063 .016 DE-07 1.278 DE-03 13:48:39 2 0 1 2 3 4 5
.040 .065 .010 2E-00 4E-00 1.279 10:48:41 2 0 1
.04 .07 .005 QE-00 4E-00 1.279 10:48:40 2 0 1 2 0 4 5
.04 .068 .015 ZE-OT DE-OT 1.279 15:48:45 2 0 1 2 T 4 5
.039 .068 .01 2E-03 4E-03 1.279 13:48:47 2 0 1 2 3 4 5
.04 .066 8E-01 1.277 2E-01 4E-01 13:48:49 2 0 1 2 3 4 5
.056 .07 .142 1.277 2E-03 4E-03 13:48:51 2 0 1 2 3
.076 .071 .072 1.277 1E-63 2E-03 13:48:53 2 0 1 2 3 4 5
.081 .068 .062 1.277 2E-03 2E-03 13:48:55 2 0 1 2 7 4 5
.070 .071 .090 4E-00 1.070 DE-00 10:48:57 2 0 1 2 0
.047 .07 .328 1E-03 1.278 1E-03 13:49:00 2 0 1 2 3 4 5
.059 .071 .109 2E-03 1.278 2E-03 13:49:02 2 0 1 2 3 4 5
.054 .075 .064 2E-01 1.277 1E-01 15:49:04 2 0 1
.054 .073 .028 2E-03 4E-03 1.279 13:49:06 2 0 1 2
.054 .071 .011 2E-01 4E-01 1.279 15:49:08 2 0 1 2 5
.054 .076 6E-07 2E-03 2E-01 1.279 13:49:10 2 0 1 2 3 4 5
.056 .070 7E-03 2E-03 2E-03 1.279 13:49:12 2 0 1 2 3
.051 .070 6E-03 RE-03 RE-03 1.279 13:49:14 2 0 1 2 7 4 5
.059 .073 .016 2E-01 2E-01 .228 13:49:16 2 0 1 2
.059 .070 .00 1.277 2E-03 4E-05 15:49:18 2 0 1 2 7 4 5
.059 .071 .082 1.277 DE-00 2E-00 10:49:22 2 0 1 2
.057..070 .048 1.277 2E-00 0E-00 10:49:04 0 0 1 0 0 4 5
.056 .073 .017 1.277 2E-03 2E-03 13:49:27 2 0 1 2 3 4 5
.052 .077 .011 1.277 REHOT REHOT 10:49:29 2 0 1 2 0 4 5
.05 .070 .014 DE-00 4E-00 1.279 10:49:01 2 0 1 2 T 4 5
.049 .071 .011 2E-03 2E-03 4E-03 13:49:33 2 0 1 2 3 4 5
.045 .071 7E-00 2E-00 2E-00 2E-00 10:49:05 2 0 1 2 0 4 5
.048 .071 8E-03 2E-03 2E-03 13:49:37 2 0 1 2 3 4 5
.062 .073 .021 1.278 2E-03 2E-03 13:49:39 2 0 1 2 7 4 5
.073 .073 .059 1.277 2E+03 2E-03 13:49:41 2 0 1 2 3 4 5
```

```
.046 .071 .029 2E-03 4E-03 4E-03 13:52:33 2 0 1 2 3 4 5
.046 .071 .14 REHOT REHOT 4EHOT 13:52:35 2 0 1 2 3
.046 .073 .068 1.279 REHOT REHOT 10:52:37 R 0 1 R 3 4 5
.046 .07T .147 4E-03 1.279 2E-07 13:52:39 2 0 1 2 3 4 5
.046 .071 .06 IE-03 1.279 IE-03 13:52:41 I 0 1 I T 4 5
.045 .070 .018 2E-00 1.279 2E+00 10:52:40 2 0 1 2 T
.046 .070 .02 2E-03 1.279 2E-03 10:52:45 2 0 1 2 T 4 5
.044 .071 .018 2E-01 2E-05 1.279 11:52:47 2 0 1 2 1 4 5
.048 .077 .019 DE-03 DE-07 1.279 13:52:49 D 0 1 D 7 4 5
.045 .076 .017 2E-03 2E-03 1.279 13:52:51 2 0 1 2 3 4 5
.045 .077 .015 1.078 2E-07 DE-03 17:50:57 2 0 1 2 3 4 5
.046 .076 .01 1.277 2E-03 4E-03 13:52:55 2 0 1 2 T 4 5
.048 .078 .071 1.277 2E-01 2E-03 13:52:57 2 0 1 2 3 4 5
.080 .076 .160 1.077 DEHOT DEHOT 10.50:59 0 0 1 0 7 4 5
.070 .070 .107 DE-00 1.077 DE-00 10:50:01 D 0 1 D 0 4 5
.06T .071 .042 1.277 2E-03 4E-03 13:50:00 2 0 1 2 7 4 5
.06 .071 .120 7E-00 1.277 2E-00 17:50:05 2 0 1 2 T 4 5
.056 .074 .145 2E-00 1.277 2E-00 10:50:07 2 0 1 2 0 4 5
.054 .073 .49B 1E-03 1.277 2E-03 13:53:10 2 0 1 2 3 4 5
.051 .071 .011 2E-00 1.277 2E-00 10:50:12 2 0 1 2 0 4 5
.05 .071 .068 ZE-03 1.277 1E-03 13:53:14 2 0 1 2 3 4 5
.048 .074 .025 2E-03 1.277 2E-03 17:50:16 2 0 1 2 3 4 5
.048 .076 .016 DE-03 4E-01 1.179 11:50:18 D 0 1 D T 4 5
.046 .070 .015 2E-07 2E-07 1.279 13:53:20 2 0 1 2 3 4 5
.044 .076 .014 DE-03 DE-03 1.079 13:53:22 2 0 1 2 3 4 5
.048 .077 .011 DE-00 4E-00 1.279 10:50:24 D 0 1 D 0 4 5
.049 .077 .04 1.277 2E-03 4E-03 13:53:26 2 0 1 2 7 4 5
.05 .070 .201 1.276 2E+00 2E+07 17:50:28 2 0 1 2 7 4 5
.054 .068 .106 1.277 2E-01 2E-01 17:50:T0 2 0 1 2 T 4 5
.054 .071 .054 1.276 DE-05 DE-05 15:55:52 2 0 1 2 5 4 5
.050 .07 .009 4E-00 1.277 DE-00 10:50:74 2 0 1 2 0 4 5
.049 .07 .019 DE-03 1.277 DE-03 17:53:36 D 0 1 D 3 4 5
,045 .071 .012 2E-03 1.277 2E-03 13:53:38 2 0 1 2 3 4 5
.044 .068 6E-00 2E-00 1.277 2E-00 1T:50:40 2 0 1 2 0 4 5
.040 .07 8E-03 2E-03 1.277 2E-03 13:53:42 2 0 1 2 3 4 5
.040 .07 .127 DE-01 4E-00 1.279 10:50:44 D 0 1 D 0 4 5
.040 .048 .048 0E-03 0E-07 1.077 13:53:44 0 0 1 2 3 4 5
.041 .068 .02 2E-01 2E-01 1.278 11:51:48 2 0 1 2 1 4 5
.049 .068 .014 1.277 DEHOT DEHOT 10:50:51 D 0 1 D 0
.051 .07 .884 1.271 2E-01 2E-03 13:53:51 2 0 1 2 3 4 5
.084 .07 .500 1.074 DE-OD DE-OD 10:50:55 D O 1 D 3 4 5
.054,.071 .421 1.271 2E-01 2E-03 13:51:57 2 0 1 2 3 4 5
.054 .070 .777 1E-03 1.277 2E-03 13:57:59 2 0 1 2 3 4 5
.05 .076 .600 1E-00 1.277 2E-00 10:54:01 2 0 1 2 0 4 5
.049 .073 .29 1E-03 1.277 1E-03 13*54:03 2 0 1 2 3 4 5
.049 .070 .091 2E-03 1.277 2E-03 10:54:05 2 0 1 2 3 4 5
.049 .068 .042 PE-03 .717 1.273 13:54:07 2 0 1 2 3 4 5
.048 .068 .022 2E-03 4E-03 1.277 13:54:09 2 0 1 2 3 4 5
.049 .071 .011 2E-03 4E-03 1.278 13:54:11 2 0 1 2 3 4 5
.05 .068 .011 1.193 2E-03 5E-03 13:54:13 2 0 1 2 3 4 5
```

```
.052 .066 .231 1.274 2E-03 4E-03 13:54:15 2 0 1 2 3 4 5
.052 .066 .43 1.273 2E-03 2E-03 13:54:17 2 0 1 2 3 4 5
.057 .066 .428 1.273 26-03 26-03 13:54:22 2 0 1 2 3 4 5
.054 .068 .695 1.277 2E-03 2E-03 13:54:24 2 0 1 2
.049 .06B .732 1.273 2E-07 4E-07 13:54:26 2 0 1 2 3 4 5
.046 .060 .446 1E~00 1,276 2E-00 10:54:28 2 0 1 2 0 4 5
.044 .062 .167 CE-03 1.276 CE-03 13:54:30 2 0 1 2 3 4 5
.044 .062 .053 2E-03 1.276 2E-03 13:54:32
                                          2012345
.048 .062 .076 DE-01 4E-01 1.277 13:54:34 2 0 1 2 3 4 5
.049 .063 .017 2E-03 4E-03 4E-03 13:54:16 2 0 1 2 3 4 5
.045 .060 .011 1.276 2E-00 2E-00 10:54:08 2 0 1 2 7 4 5
.046 .066 9E-03 1.276 DE-03 DE-03 13:54:40 D 0 1 D 3 4 5
.046 .066 .027 1.274 1E-03 2E-03 13:54:42 2 0 1 2 3 4 5
.049 .068 .086 .27 1.259 2E-03 13:54:44 2 0 1 2 T 4 5
.056 .066 .070 1.270 REHOT REHOT 10:54:46 R 0 1 R 3 4 S
.060 .065 .24 1.274 1E-00 2E-00 10:54:48 2 0 1 2 T 4 5
.061 .060 .426 1.270 REHOU REHOU 10:54:50 R 0 1 R 0 4 5
.054 .062 .289 1.273 2E-03 2E-03 13:54:52 2 0 1 2 7 4 5 .046 .063 .125 1.274 2E-03 4E-03 13:54:54 2 0 1 2 7 4 5
.040 .07 .046 DE-UT 1.277 DE-UT 10:54:56 D O 1 D T 4 5
.042 .066 .021 2E-03 1.276 2E-03 13:54:58 2 0 1 2 3 4 5
.046 .060 .016 DE-01 1.076 DE-01 11:55:01 D 0 1 D I 4 5
1049 .066 .094 2E+01 4E+03 1.277 13:55:01 2 0 1 2 3 4 5
.049 .060 .049 2E-01 2E-01 1.277 13:55:05 D 0 1 D 3 4 5
.06 .061 .024 2E-03 4E-03 4E-03 13:55:07 2 0 1 2 3 4 5
.072 .066 .02 1.277 2E-03 4E-07 10:55:09 2 0 1 2 3 4 5
.111 .066 .142 1.274 2E-03 4E-03 13:55:11 D 0 1 D 7 4 5
.117 .066 .080 1.070 2E-00 2E-00 10:55:17 2 0 1 2 0 4 5
.112 .060 .102 1.274 2E-07 2E-07 10:55:15 2 0 1 2 0 4 5
.090 .060 1 1.070 DE-00 DE-00 10:55:17 D 0 1 D T 4 5
.077 .060 .856 1.270 CE-00 CE-00 10:55:19 C 0 1 C C 4 5
.068 .062 .492 1.272 2E-0J 2E-0J 13:55:21 2 0 1 2 J 4 5
.059 .066 .150 2E-03 1.276 2E-03 13:55 23 2 0 1 2 3 4 5
.051 .065 .044 2E-01 1.274 1E-01 11:55:25 2 0 1
.049 .062 .065 2E-03 1.276 2E-03 13:55:27 2 0 1 2 3 4 5
.046 .062 .041 QE-07 4E-07 1.277 17:55:29 2 0 1 2 T 4 5
.046 .062 .019 2E-07 2E-07 1.277 13:55:31 2 0 1 2 3
1046 .065 .009 2E-00 4E-00 1.277 10:55:00 2 0 1 2
.05 .065 .022 1.274 2E-03 2E-03 13:55°35 2 0 1 2 3 4 5
.056 .060 .010 1.274 DE-00 4E-00 10:55:07 2 0 1 2 0 4 5
.061 .066 .011 1.274 2E-03 1E-03 13:55:39 2 0 1 2 3 4 5
.245..065 .371 1.273 2E-05 2E-07 13:55:42 2 0 1 2 7 4 5
.206 .068 .025 2E-03 1.276 2E-03 17:55:44 1 0 1 2 3 4 5
.151 .071 .47% 1.070 DE-07 DE-07 10:55:46 2 0 1 2 3 4 5
.115 .071 .545 2E-03 1.274 2E-03 13:55:48 2 0 1 2 3
.098 .07 .231 1E-03 1.274 2E-03 13:56:50 2 0 1 2 3 4 5
.077 .068 .074 2E-03 5E-03 4E-03 13:55:52 2 0 1 2 3 4 5
.076 .068 .066 2E-03 2E-03 1.277 13:55:54 2 0 1 2 3 4 5
.076 .073 .034 2E-03 2E-03 1.277 13:55:56 2 0 1 2 3 4 5
```