AIR QUALITY ASSESSMENT REPORT
FORT WORTH CENTRAL CITY PROJECT
FORT WORTH, TEXAS

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1. EXECUTIVE SUMMARY

The U.S. Army Corps of Engineers and the Tarrant Regional Water District, in conjunction with the City of Fort Worth, Tarrant County, and other participants, is developing a plan for the Fort Worth Central City (FWCC) project. The FWCC project proposes to enhance the level of flood protection for the Central City (Trinity Uptown) area while providing quality of life enhancements and facilitating urban revitalization. The central concept for the FWCC project is the construction of a bypass channel that would carry floodwaters around the area immediately north of downtown Fort Worth.

In order to maintain existing thoroughfares and to provide more convenient public access to the Trinity Uptown, the proposed plan involves the extension of several existing roadways and the construction of several bridges over the bypass channel. The largest intersection that will be created as a result of the roadway extensions is the intersection of Henderson Street and White Settlement Road. Smaller modifications in the existing infrastructure of the Trinity Uptown are also planned.

The FWCC project requires an Environmental Impact Statement (EIS) in accordance with the requirements of the National Environmental Policy Act (NEPA). An air quality impacts analysis is required as part of the EIS. The primary objective of the air quality analysis is to demonstrate that emission changes resulting from the proposed project do not result in adverse cumulative impacts as evaluated in relation to the National Ambient Air Quality Standards (NAAQS) and regional air quality planning efforts.

The analysis presented in this report addresses the air quality impacts from the proposed changes to roadway systems and associated urban development, as well as the impacts from construction activities. Specifically, the impact of the change in mobile source emissions on ozone and carbon monoxide levels is addressed, as well as the impact of construction-related emissions.

1.1 SUMMARY OF OZONE IMPACTS FROM MOBILE SOURCES

Emissions of volatile organic compounds (VOCs) and nitrogen oxides (NO_x) from mobile sources can combine under the right conditions in a series of photochemical reactions to form ozone. Since these reactions take place over a period of several hours, maximum concentrations of ozone are often found at a significant distance downwind of the precursor sources. Therefore, ozone is a regional problem and not a localized condition. Accordingly, ozone impacts are accounted for through regional air modeling performed by the Texas Commission on Environmental Quality (TCEQ) in conjunction with regional urban planners.

It should be further noted that because of the proximity of the FWCC development to downtown Fort Worth, it is expected that a substantial portion of the populace will utilize alternate forms of transportation. This approach to urban development combats urban sprawl, which is a major contributor to regional vehicle emissions and ozone development.

1.2 SUMMARY OF CARBON MONOXIDE IMPACTS FROM MOBILE SOURCES

Concentrations of carbon monoxide (CO) occur in localized areas with heavy traffic congestion. Therefore, CO concentrations can be readily modeled for roadway construction projects. In this air quality assessment, a CO hotspot modeling analysis is conducted in order to demonstrate that CO impacts resulting from the increased traffic associated with the FWCC project do not result in an exceedance of the NAAQS.

In the hotspot analysis, CO emissions from the traffic volumes at the intersection of Henderson Street and White Settlement Road are modeled. This intersection is expected to have the largest traffic flow volumes following the completion of the project. Therefore, CO impacts from this intersection are expected to be most significant.

The Texas Department of Transportation (TxDOT) requires that reasonable alternative build scenarios be evaluated and compared in the CO air quality impact assessment. Accordingly, the CO air quality hotspot analysis presented in this report was conducted for a "build" case and a "no-build case." The "build case" accounts for the increased traffic associated with both the roadway expansion and the urban development planned as part of the FWCC project. The "no-build" case assumes the same roadway expansion, but excludes the increases in traffic expected as a result of the urban development associated with the FWCC project.

Maximum CO concentrations were estimated for each build scenario using United States Environmental Protection Agency (U.S. EPA) Guidance and the CAL3QHC model (Version 2.0). The results of this analysis are summarized in Table 1-1 below, in which the maximum CO concentrations predicted by CAL3QHC are compared with the NAAQS for CO for the one-hour and eight-hour averaging periods.

TABLE 1-1. SUMMARY OF CO MODELING RESULTS FOR HENDERSON ST. /WHITE SETTLEMENT RD. INTERSECTION

Modeling Scenario	Averaging Period	Background CO Concentration (ppm)	Modeled CO Concentration (ppm)	Total CO Concentration (ppm)	NAAQS (ppm)	Percent of NAAQS [a] (ppm)
2025 No-Build	1-hour	2.3	1.30	3.60	35	10.3
	8-hour	1.5	0.52	2.02	9	22.4
2025 Build	1-hour	2.3	1.50	3.80	35	10.9
	8-hour	1.5	0.60	2.10	9	23.3

[a] Total CO concentration expressed as a percentage of the NAAQS.

As shown in Table 1-1, the total one-hour and eight-hour CO concentrations are less than the corresponding NAAQS in both modeling scenarios. In addition, a comparison of the results for each of the modeled scenarios indicates that the proposed modifications associated with the FWCC project will not significantly worsen the air quality impacts that would already be expected if no construction associated with the project were to occur. Therefore, the results of this analysis indicate that the infrastructure modifications and urban development associated with the FWCC project will not result in an exceedance of the NAAQS for CO.

1.3 SUMMARY OF CONSTRUCTION-RELATED IMPACTS

During construction phase of the project, various activities will result in short-term elevated levels of airborne pollutants. Air quality impacts will mainly consist of airborne particular matter (PM) generated by earth moving activities and construction traffic on unpaved roads, as well as emissions from construction equipment.

It is expected that particulate emissions from earth-moving activities will be controlled through best practice control measures to maintain compliance with the TCEQ visible emission regulations. Emissions of particulate matter, NO_x, hydrocarbons, and CO from diesel fuel combustion are regulated by the U.S. EPA in Title 40 of the Code of Federal Regulations (40 CFR) Part 89.

Compliance with these regulations is expected to mitigate any short-term or cumulative impacts from construction-related activities.

2. PROJECT BACKGROUND

The U.S. Army Corps of Engineers and the Tarrant Regional Water District, in conjunction with the City of Fort Worth, Tarrant County, and other participants, is developing a plan for the Fort Worth Central City (FWCC) project. The FWCC project proposes to enhance the level of flood protection for the Central City (Trinity Uptown) area while providing quality of life enhancements and facilitating urban revitalization. The central concept for the FWCC project is the construction of a bypass channel that would carry floodwaters around the area immediately north of downtown Fort Worth.

In order to maintain existing thoroughfares and to provide more convenient public access to the Trinity Uptown, the proposed plan involves the extension of several existing roadways and the construction of several bridges over the bypass channel. The largest intersection that will be created as a result of the roadway extensions is the intersection of Henderson Street and White Settlement Road. Smaller modifications in the existing infrastructure of the Trinity Uptown are also planned. A map prepared by Bunt & Associates depicting the Trinity Uptown area and the proposed infrastructure modifications is included in Appendix A.

The FWCC project requires an Environmental Impact Statement (EIS) in accordance with the requirements of the National Environmental Policy Act (NEPA). An air quality impacts analysis is required as part of the EIS. The primary objective of the air quality analysis is to demonstrate that emission changes resulting from the proposed project do not result in adverse cumulative impacts as evaluated in relation to the National Ambient Air Quality Standards (NAAQS) and regional air quality planning efforts.

2.1 NATIONAL AMBIENT AIR QUALITY STANDARDS (NAAQS)

The NAAQS are air quality standards established by the United States Environmental Protection Agency (U.S. EPA) for six "criteria" pollutants. The standards for each criteria pollutant are summarized in Table 2-1. The primary standards are intended to protect public health, while the secondary standards provide protection of the public welfare, including wildlife, climate, recreation, transportation, and economic considerations.

2.2 EXISTING AIR QUALITY

The Texas Commission on Environmental Quality (TCEQ) is responsible for regulating the air quality throughout the state of Texas. The FWCC project is located within Tarrant County, which is designated as a serious nonattainment area for the one-hour ozone standard and moderate nonattainment area for the eight-hour ozone standard. Tarrant County is classified as an attainment area or unclassified for all other criteria pollutants.

TABLE 2-1. NATIONAL AMBIENT AIR QUALITY STANDARDS (NAAQS)

Criteria Pollutant	Primary	Secondary
Particulate Matter		
PM_{10}		
Annual Arithmetic Mean	50 $\mu g/m^3$	50 $\mu g/m^3$
24-Hour Average	150 $\mu g/m^3$	150 $\mu g/m^3$
$PM_{2.5}$		
Annual Arithmetic Mean	15 $\mu g/m^3$	15 $\mu g/m^3$
24-Hour Average	65 $\mu g/m^3$	65 $\mu g/m^3$
Sulfur Dioxide (SO_2)		
Annual Arithmetic Mean	0.03 ppm	No Standard
24-Hour Average	0.14 ppm	No Standard
3-Hour Average	No Standard	0.50 ppm
Carbon Monoxide (CO)		
8-Hour Average	9 ppm	No Standard
1-Hour Average	35 ppm	No Standard
Ozone (O_3)		
1-Hour Average*	0.12 ppm	0.12 ppm
8-Hour Average	0.08 ppm	0.08 ppm
Nitrogen Dioxide (NO_2)		
Annual Arithmetic Mean	0.053 ppm	0.053 ppm
Lead (Pb)		
Quarterly Average	1.5 $\mu g/m^3$	No Standard

* Standard for existing ozone non-attainment areas only.

2.3 AIR QUALITY IMPACTS ANALYSIS

The analysis presented in this report addresses the air quality impacts from the proposed changes to roadway systems and associated urban development, as well as the impacts from construction activities. Specifically, the impact of the change in mobile source emissions on ozone and carbon monoxide levels is addressed, as well as the impact of construction-related emissions.

2.3.1 IMPACT OF MOBILE SOURCE EMISSIONS ON OZONE

Emissions of volatile organic compounds (VOCs) and nitrogen oxides (NO_x) from mobile sources can combine under the right conditions in a series of photochemical reactions to form ozone. Since these reactions take place over a period of several hours, maximum concentrations of ozone are often found at a significant distance downwind of the precursor sources. Therefore, ozone is a regional problem and not a localized condition. Accordingly, impacts are modeled by the TCEQ for the entire ozone nonattainment area in order to demonstrate compliance with the NAAQS. Therefore, a modeling analysis to quantify the impact of emissions of VOC and NO_x from the proposed FWCC project on regional ozone levels is beyond the scope of this air quality impact assessment.

It should be further noted that because of the proximity of the FWCC development to downtown Fort Worth, it is expected that a substantial portion of the populace will utilize alternate forms of transportation. This approach to urban development combats urban sprawl, which is a major contributor to regional vehicle emissions and ozone development.

2.3.2 IMPACT OF MOBILE SOURCE EMISSIONS ON CO

Concentrations of carbon monoxide (CO) occur in localized areas with heavy traffic congestion. Therefore, CO concentrations can be readily modeled for roadway construction projects. In this air quality assessment, a CO hotspot modeling analysis is conducted in order to demonstrate that CO impacts resulting from the increased traffic associated with the FWCC project do not result in an exceedance of the NAAQS. The CO hotspot modeling analysis is described in detail in Section 3.

2.3.3 IMPACT OF CONSTRUCTION-RELATED ACTIVITIES

A qualitative discussion of the impact of construction activities on air quality is provided in Section 4.

3. CARBON MONOXIDE MODELING ANALYSIS

A CO hotspot modeling analysis was conducted in order to demonstrate that CO impacts resulting from the increased traffic associated with the FWCC project do not result in an exceedance of the NAAQS. In the hotspot analysis, CO emissions from the traffic volumes at the intersection of Henderson Street and White Settlement Road are modeled. This intersection is expected to have the largest traffic flow volumes following the completion of the project. Therefore, CO impacts from this intersection are expected to be most significant.

The Texas Department of Transportation (TxDOT) requires that reasonable alternative build scenarios be evaluated and compared in the CO air quality impact assessment. Accordingly, the CO air quality hotspot analysis presented in this air quality assessment report is conducted for a "build" case and a "no-build case." The "build case" accounts for the increased traffic associated with both the roadway expansion and the urban development planned as part of the FWCC project. The "no-build" case assumes the same roadway expansion, but excludes the increases in traffic expected as a result of the urban development associated with the FWCC project.

The following sections describe the modeling approach and results in detail.

3.1 MOBILE SOURCE EMISSION FACTORS

CO emission factors for use in this modeling analysis were obtained from the North Central Texas Council of Governments (NCTCOG). The data provided by NCTCOG is included for reference in Appendix B. Since posted speeds have not yet been established for the proposed road extensions, it is assumed that the speed limits on Henderson Street and White Settlement Road will not exceed 55 mph. Since this is most likely an upper estimate of the maximum vehicle travel speeds through this intersection, this assumption provides a worst-case estimates for CO concentrations.

The CO emission factors used in this modeling analysis for each of the modeled roadways are shown in Table 3-1.

TABLE 3-1. SPEED LIMITS AND ASSOCIATED EMISSION FACTORS

Speed Limit (mph)	Henderson St.	White Settlement Rd.
55.0	4.24 g/mi	4.24 g/mi
2.5 [a]	28.88 g/veh-hr	28.88 g/veh-hr

[a] Idling emission factors in g/veh-hr are calculated by multiplying the NCTCOG emission factors in g/mi by 2.5 mph, as recommended in U.S. EPA, *Technical Guidance on the Use of MOBILE6 for Emission Inventory Preparation*, 1/2002.

3.2 CAL3QHC MODELING ANALYSIS

The CO air quality modeling analysis for the FWCC project was conducted using CAL3QHC Version 2.0. The CAL3QHC model was developed by the U.S. EPA to estimate CO concentrations at roadway intersections. The CO emission factors obtained from the data provided by NCTCOG were used as input to the model.

The following sections provide a discussion of the input parameters required by the CAL3QHC model.

3.2.1 FREE FLOW LINKS

A free flow link is a straight segment of roadway with a constant width, height, traffic volume, travel speed, and vehicle emission factor. The link location is defined by its end point coordinates (X1, Y1, and X2, Y2). The road is represented by a new link when there is a change in width, traffic volume, travel speed, or CO emission factor. The link width is based on the proposed roadway design.

Henderson Street contains 6 lanes (3 lanes in each direction of travel). The proposed extension of White Settlement Road contains 4 lanes (2 lanes in each direction of travel). The lanes are assumed to be 10 feet wide on each of the roadways. Each free flow link in this analysis represents a single lane of a road. Therefore, flow links are 30 feet wide, which includes one lane of traveled roadway, plus a "mixing zone" with a width of 10 feet on each side to account for the dispersion of the plume generated by the wake of moving vehicles. In addition, this analysis assumes that the links are "at grade," resulting in a link height (i.e., mobile source height) of 0 feet.

3.2.2 QUEUE LINKS

A queue link is a straight segment of roadway on which vehicles are idling for a specified period of time. Each queue link has a constant width and emission source strength. Queue links are defined by two end points (X1, Y1, and X2, Y2). The coordinate pair, X1 and Y1, mark the location where the vehicles begin queuing at the intersection. The second coordinate pair, X2 and Y2, specifies the direction of the link. The model determines the length of the queue based upon the volume of vehicles in the queue and the capacity of the lanes near the intersection. The widths of the queue links included in this analysis are 10 feet. As in the case of free flow links, queue link height is set to 0 feet.

3.2.3 RECEPTOR LOCATIONS

In this analysis, receptors are located along the roadway at a distance of 10 feet from the edge of the mixing zone on each side of the road.[1] Additional receptors are placed along both sides of the road near the intersection since higher concentrations are expected in this area. All of the receptors have a height of 6 feet, which represents the approximate breathing height of the general public.[2]

3.2.4 AMBIENT CONDITIONS

Worst-case ambient meteorological conditions are used in the CAL3QHC modeling analysis. Wind speed, wind direction, atmospheric stability class, mixing height, and surface roughness are required as input in the CAL3QHC model. These parameters are quantified in Table 3-2.

TABLE 3-2. AMBIENT CONDITIONS

Parameter	Value
Wind Speed [a]	1 m/s
Atmospheric Stability Class [a]	F
Mixing Height [b]	1,000 m
Surface Roughness [c]	175 cm

[a] Wind speed of 1 m/s and atmospheric stability class F represent the most stable meteorological conditions, which results in minimal dispersion and therefore provides worst-case CO concentration estimates.

[b] U.S. EPA, User's Guide to CAL3QHC Version 2.0: A Modeling Methodology for Predicting Pollutant Concentrations Near Roadway Intersections, EPA-454/R-92-006 (Revised), Research Triangle Park, NC, September 1995.

[c] Ibid. This surface roughness is recommended for a city with the land use predominately dedicated to office buildings.

3.2.5 CHARACTERISTICS OF TRAFFIC FLOW

Queue length is determined from the traffic volume that occupies the particular queue of interest. Thus, the traffic volume in each of the individual links must be specified. Traffic volume assumptions are based on traffic flow diagrams provided by Bunt & Associates. These diagrams provided by Bunt & Associates are included for reference as Figures C-1 and C-3 for the "no-build" case and the "build" case, respectively. The assumed traffic volumes used in the modeling analysis are illustrated in Figures C-2 and C-4 for the "no-build" case and the "build" case, respectively.

The queue length is also a function of the capacity of the link. A saturation flow volume of 1,600 vehicles/lane/hr was used as a default estimate of the capacity of each lane.[3]

The traffic flow is also heavily influenced by the traffic light signals. Average signal cycle length, average red time length, clearance time lost, signal type, and arrival rate are required as input to CAL3QHC to account for the effect of the traffic signals. Both the "build" and "no-build" scenarios are modeled with traffic signals.

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[1] U.S. EPA, *Guideline for Modeling Carbon Monoxide from Roadway Intersections*, EPA-454/R-92-005 (revised), Research Triangle Park, NC, September 1995.

[2] U.S. EPA, *User's Guide to CAL3QHC Version 2.0: A Modeling Methodology for Predicting Pollutant Concentrations Near Roadway Intersections*, EPA-454/R-92-006 (Revised), Research Triangle Park, NC, September 1995.

[3] Ibid. This is a representative saturation flow volume for a typical urban intersection.

Table 3-3 summarizes the traffic signal parameters that best represent the Henderson Street/White Settlement Road intersection.

TABLE 3-3. TRAFFIC SIGNAL PARAMETERS

Parameter	Value
Average signal cycle length [1]	90 seconds
Average red time length[1]	40 seconds
Clearance time lost[1]	2 seconds
Signal type	Actuated
Arrival rate	Average progression

[1] Default CAL3QHC values were assumed.

3.3 AIR QUALITY MODELING ANALYSIS RESULTS

This section summarizes the results of the CO air quality modeling analysis conducted for the Henderson Street/White Settlement Road intersection. The CAL3QHC modeling input and output files are provided for reference in Appendix D. Figures E-1 and E-2 in Appendix E show the one-hour concentrations of CO in parts per million (ppm) at each receptor location for the no-build and build scenarios, respectively.

Table 3-4 below shows the maximum one-hour and eight-hour CO concentration for each modeled scenario.

TABLE 3-4. COMPARISON OF CO MODELING ANALYSIS RESULTS TO THE NAAQS

Modeling Scenario	Averaging Period	Background CO Concentration [a] (ppm)	Modeled CO Concentration (ppm)	Total CO Concentration (ppm)	NAAQS (ppm)	Percent of NAAQS [b] (ppm)
2025 No-Build	1-hour	2.3	1.30	3.60	35	10.3
	8-hour [c]	1.5	0.52	2.02	9	22.4
2025 Build	1-hour	2.3	1.50	3.80	35	10.9
	8-hour [c]	1.5	0.60	2.10	9	23.3

[a] Background concentrations were obtained from the U.S. EPA Air Quality Standards Database. Data was obtained from the TCEQ CAMS13 monitoring site (Site ID 1002) at 3317 Ross Ave., Fort Worth, TX.

[b] Total CO concentration expressed as a percentage of the NAAQS.

[c] 8-hour CO concentration is obtained by multiplying the modeled 1-hour concentration by a persistence factor of 0.4 per TxDOT Air Quality Guidelines, 1999.

As shown in Table 3-4, the total one-hour and eight-hour CO concentrations are less than the corresponding NAAQS in both modeling scenarios. In addition, a comparison of the results for the modeled scenarios indicates that the proposed modifications associated with the FWCC project will not significantly affect the air quality impacts that would already be expected if no construction associated with the project were to occur. Therefore, the results of this analysis indicate that the infrastructure modifications and urban development associated with the FWCC project will not result in an exceedance of the NAAQS for CO.

4. CONSTRUCTION IMPACTS

During construction phase of the project, various activities will result in short-term elevated levels of airborne pollutants. Air quality impacts will mainly consist of airborne particular matter (PM) generated by earth moving activities and construction traffic on unpaved roads, as well as emissions from construction equipment.

4.1 AIRBORNE PM EMISSIONS FROM CONSTRUCTION ACTIVITIES

During construction phase of the project, PM emissions from construction activities might be the most visible air quality impact. Texas Administrative Code (TAC) Title 30, Part 1, Chapter 111.111 provides for opacity limitations for emission sources in Texas. Specifically, Chapter 111.111(8) restricts opacity or visible emissions to 30%. Appropriate practices to control off-site migration of fugitive dust will be applied such that construction activity emissions result in impacts within the 30% visible emissions threshold. These practices may include the application of a water or chemical spray to roads, piles, and active excavation areas, as well as applying speed limits on construction equipment, especially on dry or windy days when the there is the greatest chance for fugitive dust generation and migration. With these and other appropriate mitigation measures in place, activities associated with earth moving are not expected to have significant short-term impacts, and should have no cumulative, long-term impacts on air quality.

4.2 POLLUTANTS FROM CONSTRUCTION RELATED COMBUSTION SOURCES

The project will utilize many non-road engines as well as motor vehicles on the construction site. Emissions from non-road engines and motor vehicles consist of volatile organic compounds (VOCs), carbon monoxide (CO), nitrogen oxides (NO_x), and particulate matter.

On November 15, 1990, the Clean Air Act Amendments of 1990 (CAAA) were enacted in order to broaden and strengthen the CAA. While the CAA had long specifically authorized EPA regulation of on-highway vehicle and engine emissions, the 1990 amendments extended EPA's authority to regulate nonroad vehicles and engines. Specifically, revised Section 213 directs EPA to: (1) conduct a study of emissions from nonroad engines and vehicles; (2) determine whether emissions of CO, NO_x, and volatile organic compounds (VOCs) from nonroad engines and vehicles are significant contributors to ozone or CO in more than one area which has failed to attain the NAAQS for ozone or CO; and (3) regulate those categories or classes of new nonroad engines and vehicles that contribute to such air pollution if nonroad emissions are determined to be significant. The Nonroad Engine and Vehicle Emission Study required by Section 213(a)(1) was completed in November 1991. Resulting regulations are published in Title 40 of the Code of Federal Regulations (40 CFR), Part 89.

40 CFR Part 89 establishes emission standards for NO_x, CO, hydrocarbons, and particulate matter from new and in-use nonroad diesel engines. The purpose of the standards is to address cumulative impacts upon urban areas, especially those that are nonattainment for criteria pollutants such as the Dallas / Fort Worth ozone nonattainment area, which includes Tarrant County. All construction equipment to be

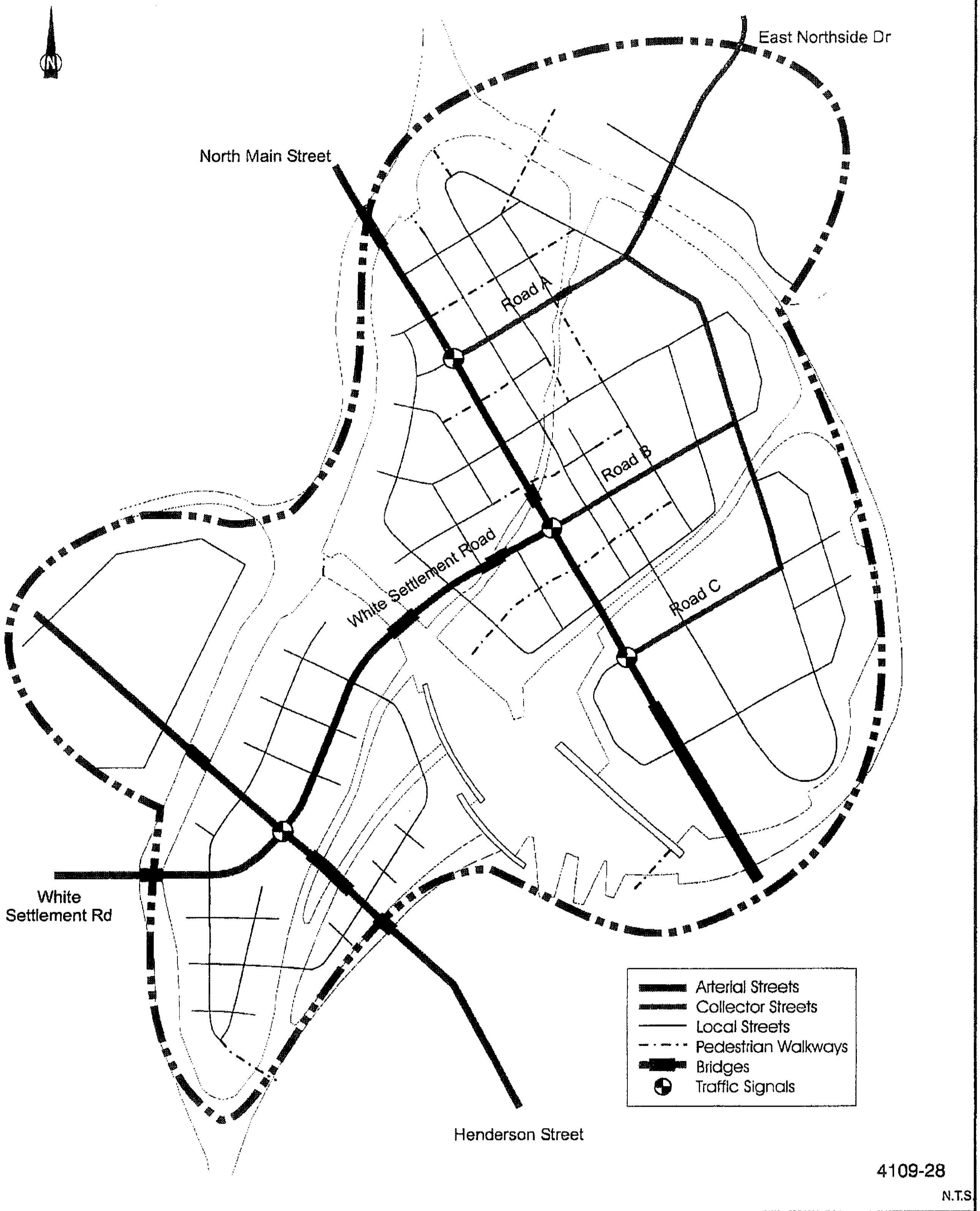
utilized for the FWCC project that meets the regulatory definition of a "nonroad engine" for the purposes of Part 89 will comply with applicable portions of the rule, including any applicable emission standards.

4.3 OTHER CONSTRUCTION-RELATED AIR QUALITY IMPACTS

Other construction related impacts might include disruptions in the flow of local traffic due to road closures and modifications to roadways. The disruptions in the flow of local traffic could result in greater emissions of carbon monoxide and other pollutants form vehicles; however, these impacts are expected to be small compared to the impacts already addressed earlier in this report for the project build case (Section 3).

APPENDIX A

PROPOSED INFRASTRUCTURE MODIFICATIONS



BUNT & ASSOCIATES

Road Network Concept

Trinity Uptown Transportation Plan

Exhibit
2.1

APPENDIX B

CO EMISSION FACTORS PROVIDED BY NCTCOG

Carbon Monoxide(CO)
Composite Emission Factor For Freeways and Arterials

TARRANT COUNTY

	2007		2025	
	CO(g/mile)		CO(g/mile)	
Speeds	Freeway	Arterial	Freeway	Arterial
1	25.62	26.18	13.75	14.25
2	22.37	22.83	12.02	12.45
2.5	20.74	21.15	11.16	11.55
3	19.11	19.47	10.30	10.66
4	15.86	16.12	8.57	8.86
5	12.61	12.76	6.84	7.07
6	11.75	11.97	6.37	6.63
7	10.88	11.19	5.90	6.20
8	10.02	10.40	5.43	5.77
9	9.15	9.61	4.96	5.34
10	8.29	8.83	4.49	4.91
11	8.04	8.60	4.34	4.77
12	7.79	8.36	4.20	4.63
13	7.54	8.13	4.05	4.49
14	7.29	7.90	3.90	4.35
15	7.04	7.66	3.76	4.21
16	6.97	7.54	3.71	4.12
17	6.91	7.41	3.67	4.03
18	6.84	7.28	3.63	3.95
19	6.77	7.16	3.58	3.86
20	6.71	7.03	3.54	3.78
21	6.68	6.97	3.51	3.73
22	6.65	6.92	3.49	3.69
23	6.62	6.86	3.47	3.65
24	6.59	6.80	3.45	3.61
25	6.56	6.75	3.43	3.56
26	6.55	6.73	3.41	3.55
27	6.54	6.72	3.40	3.53
28	6.52	6.70	3.38	3.51
29	6.51	6.69	3.37	3.50
30	6.49	6.67	3.35	3.48
31	6.51	6.70	3.35	3.48
32	6.53	6.72	3.36	3.48
33	6.55	6.74	3.36	3.49
34	6.57	6.77	3.36	3.49
35	6.59	6.79	3.36	3.49
36	6.66	6.87	3.40	3.53
37	6.74	6.94	3.43	3.56
38	6.81	7.02	3.46	3.60
39	6.88	7.10	3.50	3.63
40	6.96	7.18	3.53	3.67
41	7.03	7.26	3.57	3.70
42	7.11	7.33	3.60	3.74
43	7.18	7.41	3.64	3.78
44	7.26	7.49	3.67	3.81
45	7.33	7.57	3.71	3.85
46	7.41	7.66	3.74	3.89
47	7.49	7.74	3.78	3.93
48	7.57	7.82	3.82	3.97
49	7.65	7.90	3.85	4.00
50	7.73	7.98	3.89	4.04
51	7.81	8.07	3.93	4.08
52	7.89	8.15	3.97	4.12
53	7.97	8.23	4.00	4.16
54	8.05	8.32	4.04	4.20
55	8.13	8.40	4.08	4.24

56	8.22	8.49	4.12	4.28
57	8.30	8.58	4.16	4.33
58	8.39	8.67	4.21	4.37
59	8.47	8.75	4.25	4.41
60	8.56	8.84	4.29	4.46
61	8.65	8.93	4.33	4.50
62	8.74	9.03	4.38	4.55
63	8.83	9.12	4.42	4.60
64	8.92	9.21	4.47	4.64
65	9.01	9.30	4.51	4.69

APPENDIX C

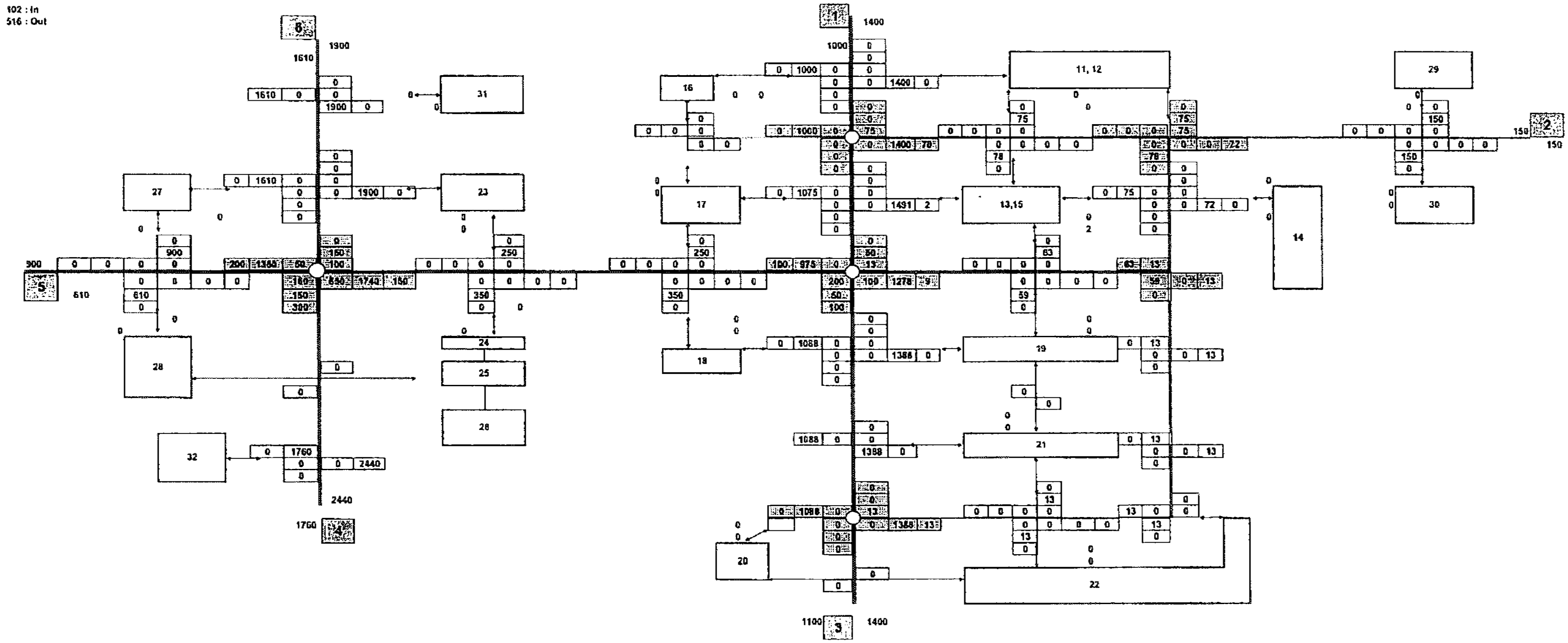
TRAFFIC FLOW VOLUME DIAGRAMS

2025 Background Traffic

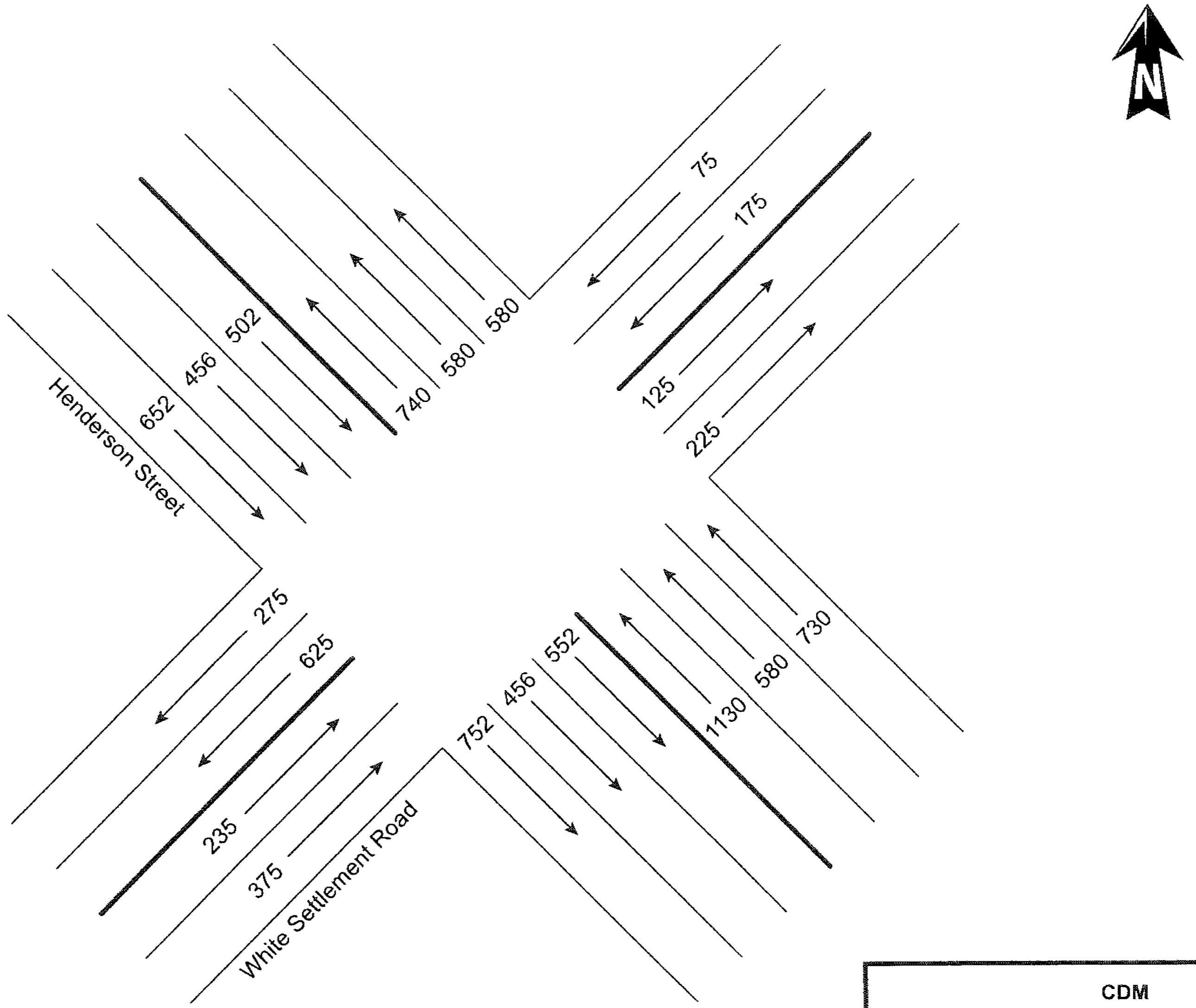
Time Period : PM

From: External

To: External



102 : In
516 : Out



CDM

Figure C-2.
Traffic Flows for "No-Build" Scenario

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054401.0035

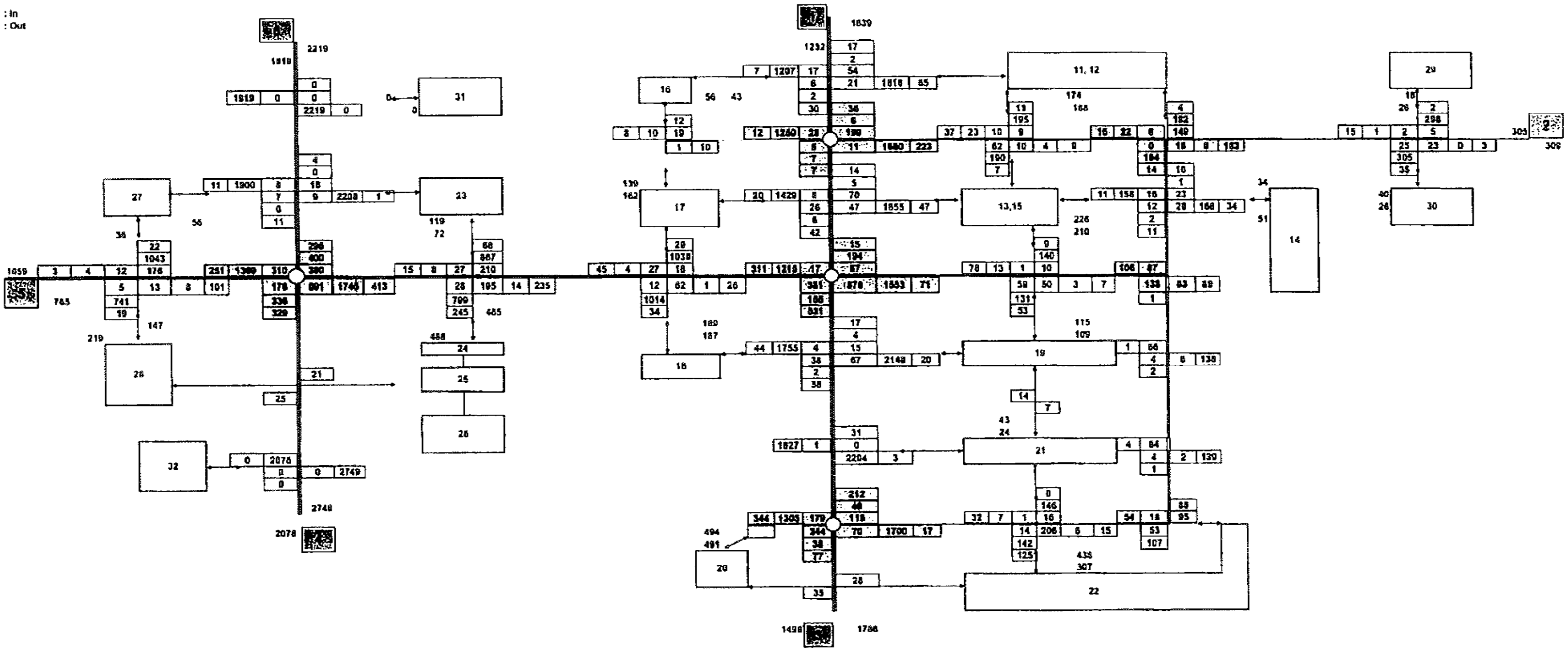
2025 Total Traffic

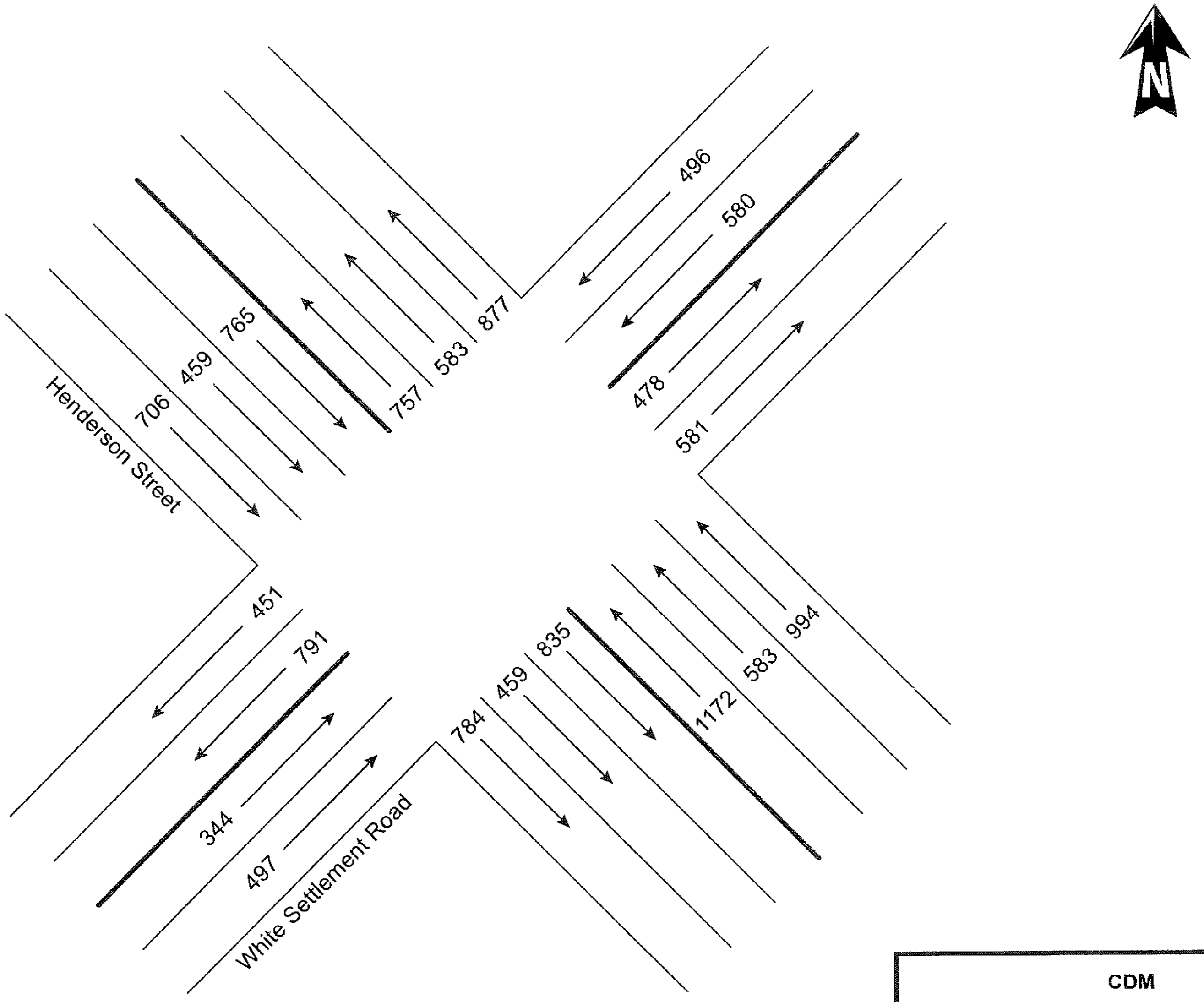
Time Period : PM

From: All Zones

To: All Zones

102 : In
516 : Out





CDM

Figure C-4.
Traffic Flows for "Build" Scenario

Trinity Consultants

February 2005
054401.0035

APPENDIX D

CAL3QHC INPUT AND OUTPUT FILES

NO-BUILD CASE INPUT FILE

```
''  60.0  175.0  0.0  0.0   183  1  0  0  'PPM'
''  -102.42  23.12  1.8
''  -111.2  27.89  1.8
''  -119.99  32.67  1.8
''  -127.13  8.98  1.8
''  -118.32  4.25  1.8
''  -123.59  34.57  1.8
''  -131.78  40.31  1.8
''  -145.07  20.0  1.8
''  -136.86  14.29  1.8
''  -138.86  45.24  1.8
''  -146.62  51.55  1.8
''  -154.38  57.86  1.8
''  -170.14  39.36  1.8
''  -162.37  33.07  1.8
''  -154.6  26.77  1.8
''  -154.71  58.12  1.8
''  -162.43  64.48  1.8
''  -182.41  49.49  1.8
''  -174.7  43.12  1.8
''  -166.33  67.66  1.8
''  -173.39  74.74  1.8
''  -193.63  60.63  1.8
''  -186.55  53.57  1.8
''  -176.07  77.4  1.8
''  -182.71  84.88  1.8
''  -189.34  92.36  1.8
''  -195.98  99.84  1.8
''  -202.62  107.32  1.8
''  -218.82  88.98  1.8
''  -212.18  81.5  1.8
''  -205.54  74.02  1.8
''  -198.9  66.54  1.8
''  -79.93  15.06  1.8
''  -89.33  18.47  1.8
''  -98.74  21.88  1.8
''  -111.61  0.75  1.8
''  -102.16  -2.52  1.8
''  -92.71  -5.79  1.8
''  -83.26  -9.05  1.8
''  88.1  15.61  1.8
''  78.49  12.82  1.8
''  79.08  -11.86  1.8
''  88.75  -9.29  1.8
''  107.72  18.96  1.8
''  97.86  17.3  1.8
''  93.92  -7.88  1.8
''  103.78  -6.25  1.8
''  128.19  23.96  1.8
''  118.47  21.59  1.8
''  112.29  -4.83  1.8
''  122.01  -2.48  1.8
''  131.73  -0.13  1.8
''  140.44  31.02  1.8
''  131.69  26.19  1.8
''  135.72  1.08  1.8
''  144.56  5.76  1.8
''  163.8  43.4  1.8
''  154.96  38.72  1.8
''  146.12  34.04  1.8
''  152.07  9.73  1.8
''  160.9  14.41  1.8
''  169.74  19.09  1.8
```

```
''  178.58  23.77  1.8
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''  -25.24  12.19  1.8
''  -35.24  12.19  1.8
''  -45.24  12.19  1.8
''  -55.24  12.19  1.8
''  -65.24  12.19  1.8
''  -15.24  -12.19  1.8
''  -25.24  -12.19  1.8
''  -35.24  -12.19  1.8
''  -45.24  -12.19  1.8
''  -55.24  -12.19  1.8
''  -65.24  -12.19  1.8
''  15.24  12.19  1.8
''  25.24  12.19  1.8
''  35.24  12.19  1.8
''  45.24  12.19  1.8
''  55.24  12.19  1.8
''  65.24  12.19  1.8
''  15.24  -12.19  1.8
''  25.24  -12.19  1.8
''  35.24  -12.19  1.8
''  45.24  -12.19  1.8
''  55.24  -12.19  1.8
''  65.24  -12.19  1.8
''  -15.24  22.19  1.8
''  -25.24  22.19  1.8
''  -35.24  22.19  1.8
''  -45.24  22.19  1.8
''  -55.24  22.19  1.8
''  -65.24  22.19  1.8
''  -15.24  -22.19  1.8
''  -25.24  -22.19  1.8
''  -35.24  -22.19  1.8
''  -45.24  -22.19  1.8
''  -55.24  -22.19  1.8
''  -65.24  -22.19  1.8
''  15.24  22.19  1.8
''  25.24  22.19  1.8
''  35.24  22.19  1.8
''  45.24  22.19  1.8
''  55.24  22.19  1.8
''  65.24  22.19  1.8
''  15.24  -22.19  1.8
''  25.24  -22.19  1.8
''  35.24  -22.19  1.8
''  45.24  -22.19  1.8
''  55.24  -22.19  1.8
''  65.24  -22.19  1.8
''  -15.24  32.19  1.8
''  -25.24  32.19  1.8
''  -35.24  32.19  1.8
''  -45.24  32.19  1.8
''  -55.24  32.19  1.8
''  -65.24  32.19  1.8
''  -15.24  -32.19  1.8
''  -25.24  -32.19  1.8
''  -35.24  -32.19  1.8
''  -45.24  -32.19  1.8
''  -55.24  -32.19  1.8
''  -65.24  -32.19  1.8
''  15.24  32.19  1.8
''  25.24  32.19  1.8
```

```
''  35.24  32.19  1.8
''  45.24  32.19  1.8
''  55.24  32.19  1.8
''  65.24  32.19  1.8
''  15.24  -32.19  1.8
''  25.24  -32.19  1.8
''  35.24  -32.19  1.8
''  45.24  -32.19  1.8
''  55.24  -32.19  1.8
''  65.24  -32.19  1.8
''  -15.24  42.19  1.8
''  -25.24  42.19  1.8
''  -35.24  42.19  1.8
''  -15.24  -42.19  1.8
''  -25.24  -42.19  1.8
''  -35.24  -42.19  1.8
''  15.24  42.19  1.8
''  25.24  42.19  1.8
''  35.24  42.19  1.8
''  15.24  -42.19  1.8
''  25.24  -42.19  1.8
''  35.24  -42.19  1.8
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''  15.24  72.19  1.8
''  15.24  82.19  1.8
''  15.24  92.19  1.8
''  15.24  102.19  1.8
''  15.24  112.19  1.8
''  15.24  122.19  1.8
''  15.24  132.19  1.8
''  -15.24  52.19  1.8
''  -15.24  62.19  1.8
''  -15.24  72.19  1.8
''  -15.24  82.19  1.8
''  -15.24  92.19  1.8
''  -15.24  102.19  1.8
''  -15.24  112.19  1.8
''  -15.24  122.19  1.8
''  -15.24  132.19  1.8
''  15.24  -52.19  1.8
''  15.24  -62.19  1.8
''  15.24  -72.19  1.8
''  15.24  -82.19  1.8
''  15.24  -92.19  1.8
''  15.24  -102.19  1.8
''  15.24  -112.19  1.8
''  15.24  -122.19  1.8
''  15.24  -132.19  1.8
''  -15.24  -52.19  1.8
''  -15.24  -62.19  1.8
''  -15.24  -72.19  1.8
''  -15.24  -82.19  1.8
''  -15.24  -92.19  1.8
''  -15.24  -102.19  1.8
''  -15.24  -112.19  1.8
''  -15.24  -122.19  1.8
''  -15.24  -132.19  1.8
''  88  1  0  'C'
1  1
''  'AG'  0.0  4.57  -73.15  4.57  275  4.24  0.0  9.14
1  1
''  'AG'  0.0  1.52  -73.15  1.52  625  4.24  0.0  9.14
```

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'' 'AG' 0.0 -1.52 -73.15 -1.52 235 4.24 0.0 9.14
1 1
'' 'AG' 0.0 -4.57 -73.15 -4.57 375 4.24 0.0 9.14
1 1
'' 'AG' -73.15 4.57 -106.07 16.5 275 4.24 0.0 9.14
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'' 'AG' -73.15 -1.52 -108.1 10.76 235 4.24 0.0 9.14
1 1
'' 'AG' -73.15 -4.57 -109.12 7.88 375 4.24 0.0 9.14
1 1
'' 'AG' -106.07 16.5 -127.98 28.41 275 4.24 0.0 9.14
1 1
'' 'AG' -107.09 13.63 -129.42 25.72 625 4.24 0.0 9.14
1 1
'' 'AG' -108.1 10.76 -130.87 23.04 235 4.24 0.0 9.14
1 1
'' 'AG' -109.12 7.88 -132.32 20.36 375 4.24 0.0 9.14
1 1
'' 'AG' -127.98 28.41 -143.69 39.41 275 4.24 0.0 9.14
1 1
'' 'AG' -129.42 25.72 -145.43 36.91 625 4.24 0.0 9.14
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'' 'AG' -130.87 23.04 -147.18 34.41 235 4.24 0.0 9.14
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'' 'AG' -132.32 20.36 -148.92 31.91 375 4.24 0.0 9.14
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'' 'AG' -143.69 39.41 -159.58 52.32 275 4.24 0.0 9.14
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'' 'AG' -145.43 36.91 -161.5 49.95 625 4.24 0.0 9.14
1 1
'' 'AG' -147.18 34.41 -163.42 47.58 235 4.24 0.0 9.14
1 1
'' 'AG' -148.92 31.91 -165.34 45.22 375 4.24 0.0 9.14
1 1
'' 'AG' -159.58 52.32 -171.74 62.35 275 4.24 0.0 9.14
1 1
'' 'AG' -161.5 49.95 -173.68 60.0 625 4.24 0.0 9.14
1 1
'' 'AG' -163.42 47.58 -175.62 57.65 235 4.24 0.0 9.14
1 1
'' 'AG' -165.34 45.22 -177.56 55.3 375 4.24 0.0 9.14
1 1
'' 'AG' -171.74 62.35 -181.78 72.42 275 4.24 0.0 9.14
1 1
'' 'AG' -173.68 60.0 -183.94 70.27 625 4.24 0.0 9.14
1 1
'' 'AG' -175.62 57.65 -186.09 68.11 235 4.24 0.0 9.14
1 1
'' 'AG' -177.56 55.3 -188.25 65.96 375 4.24 0.0 9.14
1 1
'' 'AG' -181.78 72.42 -325.76 234.68 275 4.24 0.0 9.14
1 1
'' 'AG' -183.94 70.27 -328.04 232.66 625 4.24 0.0 9.14
1 1
'' 'AG' -186.09 68.11 -330.32 230.64 235 4.24 0.0 9.14
1 1
'' 'AG' -188.25 65.96 -332.6 228.61 375 4.24 0.0 9.14
1 1
'' 'AG' 0.0 4.57 77.11 4.57 75 4.24 0.0 9.14
1 1
```

```
'' 'AG' 0.0 1.52 77.11 1.52 175 4.24 0.0 9.14
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'' 'AG' 0.0 -1.52 77.11 -1.52 125 4.24 0.0 9.14
1 1
'' 'AG' 0.0 -4.57 77.11 -4.57 225 4.24 0.0 9.14
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'' 'AG' 77.11 4.57 90.22 8.37 75 4.24 0.0 9.14
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'' 'AG' 77.11 -1.52 91.85 2.49 125 4.24 0.0 9.14
1 1
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1 1
'' 'AG' 90.22 8.37 108.98 11.52 75 4.24 0.0 9.14
1 1
'' 'AG' 91.03 5.43 109.48 8.51 175 4.24 0.0 9.14
1 1
'' 'AG' 91.85 2.49 109.98 5.51 125 4.24 0.0 9.14
1 1
'' 'AG' 92.66 -0.44 110.48 2.5 225 4.24 0.0 9.14
1 1
'' 'AG' 108.98 11.52 129.99 16.63 75 4.24 0.0 9.14
1 1
'' 'AG' 109.48 8.51 130.7 13.67 175 4.24 0.0 9.14
1 1
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1 1
'' 'AG' 110.48 2.5 132.14 7.75 225 4.24 0.0 9.14
1 1
'' 'AG' 129.99 16.63 144.13 24.44 75 4.24 0.0 9.14
1 1
'' 'AG' 130.7 13.67 145.58 21.76 175 4.24 0.0 9.14
1 1
'' 'AG' 131.42 10.71 147.03 19.08 125 4.24 0.0 9.14
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'' 'AG' 132.14 7.75 148.48 16.4 225 4.24 0.0 9.14
1 1
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1 1
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1 1
'' 'AG' 147.03 19.08 311.61 106.25 125 4.24 0.0 9.14
1 1
'' 'AG' 148.48 16.4 313.04 103.55 225 4.24 0.0 9.14
1 1
'' 'AG' 7.62 0.0 7.62 185.93 580 4.24 0.0 9.14
1 1
'' 'AG' 4.57 0.0 4.57 185.93 580 4.24 0.0 9.14
1 1
'' 'AG' 1.52 0.0 1.52 185.93 740 4.24 0.0 9.14
1 1
'' 'AG' -1.52 0.0 -1.52 185.93 502 4.24 0.0 9.14
1 1
'' 'AG' -4.57 0.0 -4.57 185.93 456 4.24 0.0 9.14
1 1
'' 'AG' -7.62 0.0 -7.62 185.93 652 4.24 0.0 9.14
1 1
'' 'AG' 7.62 185.93 7.62 -447.14 730 4.24 0.0 9.14
1 1
'' 'AG' 4.57 185.93 4.57 -447.14 580 4.24 0.0 9.14
1 1
'' 'AG' 1.52 185.93 1.52 -447.14 1130 4.24 0.0 9.14
```

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1, 1
'' 'AG'  -4.57  185.93  -4.57  -447.14  456  4.24  0.0  9.14
1, 1
'' 'AG'  -7.62  185.93  -7.62  -447.14  752  4.24  0.0  9.14
2, 1
'' 'AG'  -9.14  4.57  -73.15  4.57  0.0  3.05  1
90  40  2  275  28.88  1600  2  3
2, 1
'' 'AG'  -9.14  1.52  -73.15  1.52  0.0  3.05  1
90  40  2  625  28.88  1600  2  3
2, 1
'' 'AG'  -9.14  -1.52  -73.15  -1.52  0.0  3.05  1
90  40  2  235  28.88  1600  2  3
2, 1
'' 'AG'  -9.14  -4.57  -73.15  -4.57  0.0  3.05  1
90  40  2  375  28.88  1600  2  3
2, 1
'' 'AG'  9.14  4.57  77.11  4.57  0.0  3.05  1
90  40  2  75  28.88  1600  2  3
2, 1
'' 'AG'  9.14  1.52  77.11  1.52  0.0  3.05  1
90  40  2  175  28.88  1600  2  3
2, 1
'' 'AG'  9.14  -1.52  77.11  -1.52  0.0  3.05  1
90  40  2  125  28.88  1600  2  3
2, 1
'' 'AG'  9.14  -4.57  77.11  -4.57  0.0  3.05  1
90  40  2  225  28.88  1600  2  3
2, 1
'' 'AG'  7.62  6.1  7.62  185.93  0.0  3.05  1
90  40  2  580  28.88  1600  2  3
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2, 1
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2, 1
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90  40  2  456  28.88  1600  2  3
2, 1
'' 'AG'  -7.62  6.1  -7.62  185.93  0.0  3.05  1
90  40  2  652  28.88  1600  2  3
2, 1
'' 'AG'  7.62  -6.1  7.62  -447.14  0.0  3.05  1
90  40  2  730  28.88  1600  2  3
2, 1
'' 'AG'  4.57  -6.1  4.57  -447.14  0.0  3.05  1
90  40  2  580  28.88  1600  2  3
2, 1
'' 'AG'  1.52  -6.1  1.52  -447.14  0.0  3.05  1
90  40  2  1130  28.88  1600  2  3
2, 1
'' 'AG'  -1.52  -6.1  -1.52  -447.14  0.0  3.05  1
90  40  2  552  28.88  1600  2  3
2, 1
'' 'AG'  -4.57  -6.1  -4.57  -447.14  0.0  3.05  1
90  40  2  456  28.88  1600  2  3
```

```
2  1
''  'AG'  -7.62  -6.1  -7.62  -447.14  0.0  3.05  1
90  40  2  752  28.88  1600  2  3
1.0  0  4  1000.0  0.0  'Y'  10  0  35
** BREEZE
** PROJECTN  0 104 7 -177  0 0.9996 500000 0
** RAWFILE
```

NO-BUILD CASE OUTPUT FILE

```
1                           CAL3QHC - (DATED 95221)

                 CAL3QHC  PC  (32 BIT) VERSION 3.0.0
                (C) COPYRIGHT  1993-2000, TRINITY CONSULTANTS

 Run Began on  2/23/2005 at 18:53:17

     JOB:                                                       RUN:


     DATE : 02/23/   0
     TIME : 18:53:17

        The MODE flag has been set to C for calculating CO averages.

       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =   0.0 CM/S        VD =   0.0 CM/S      Z0 = 175. CM
        U =  1.0 M/S          CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =
1000. M    AMB =  0.0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION       *         LINK COORDINATES (M)          *    LENGTH
BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *  X1          Y1        X2          Y2      *     (M)
(DEG)            (G/MI)   (M) (M)       (VEH)

-------------------------*------------------------------------------*-------------------
------------------------------------------
      1.                      *     0.0         4.6      -73.2        4.6 *        73.
270. AG    275.    4.2    0.0  9.1
      2.                      *     0.0         1.5      -73.2        1.5 *        73.
270. AG    625.    4.2    0.0  9.1
      3.                      *     0.0        -1.5      -73.2       -1.5 *        73.
270. AG    235.    4.2    0.0  9.1
      4.                      *     0.0        -4.6      -73.2       -4.6 *        73.
270. AG    375.    4.2    0.0  9.1
      5.                      *   -73.2         4.6     -106.1       16.5 *        35.
290. AG    275.    4.2    0.0  9.1
      6.                      *   -73.2         1.5     -107.1       13.6 *        36.
290. AG    625.    4.2    0.0  9.1
      7.                      *   -73.2        -1.5     -108.1       10.8 *        37.
289. AG    235.    4.2    0.0  9.1
      8.                      *   -73.2        -4.6     -109.1        7.9 *        38.
289. AG    375.    4.2    0.0  9.1
      9.                      *  -106.1        16.5     -128.0       28.4 *        25.
299. AG    275.    4.2    0.0  9.1
     10.                      *  -107.1        13.6     -129.4       25.7 *        25.
298. AG    625.    4.2    0.0  9.1
     11.                      *  -108.1        10.8     -130.9       23.0 *        26.
298. AG    235.    4.2    0.0  9.1
     12.                      *  -109.1         7.9     -132.3       20.4 *        26.
298. AG    375.    4.2    0.0  9.1
     13.                      *  -128.0        28.4     -143.7       39.4 *        19.
305. AG    275.    4.2    0.0  9.1
     14.                      *  -129.4        25.7     -145.4       36.9 *        20.
305. AG    625.    4.2    0.0  9.1
     15.                      *  -130.9        23.0     -147.2       34.4 *        20.
305. AG    235.    4.2    0.0  9.1
     16.                      *  -132.3        20.4     -148.9       31.9 *        20.
305. AG    375.    4.2    0.0  9.1
     17.                      *  -143.7        39.4     -159.6       52.3 *        20.
```

```
309. AG    275.    4.2    0.0  9.1
   18.                          *   -145.4      36.9    -161.5       50.0 *       21.
309. AG    625.    4.2    0.0  9.1
   19.                          *   -147.2      34.4    -163.4       47.6 *       21.
309. AG    235.    4.2    0.0  9.1
   20.                          *   -148.9      31.9    -165.3       45.2 *       21.
309. AG    375.    4.2    0.0  9.1
   21.                          *   -159.6      52.3    -171.7       62.3 *       16.
310. AG    275.    4.2    0.0  9.1
   22.                          *   -161.5      50.0    -173.7       60.0 *       16.
310. AG    625.    4.2    0.0  9.1
   23.                          *   -163.4      47.6    -175.6       57.7 *       16.
310. AG    235.    4.2    0.0  9.1
   24.                          *   -165.3      45.2    -177.6       55.3 *       16.
310. AG    375.    4.2    0.0  9.1
   25.                          *   -171.7      62.3    -181.8       72.4 *       14.
315. AG    275.    4.2    0.0  9.1
   26.                          *   -173.7      60.0    -183.9       70.3 *       15.
315. AG    625.    4.2    0.0  9.1
   27.                          *   -175.6      57.7    -186.1       68.1 *       15.
315. AG    235.    4.2    0.0  9.1
   28.                          *   -177.6      55.3    -188.2       66.0 *       15.
315. AG    375.    4.2    0.0  9.1
   29.                          *   -181.8      72.4    -325.8      234.7 *     2 17.
318. AG    275.    4.2    0.0  9.1
   30.                          *   -183.9      70.3    -328.0      232.7 *     2 17.
318. AG    625.    4.2    0.0  9.1
   31.                          *   -186.1      68.1    -330.3      230.6 *     2 17.
318. AG    235.    4.2    0.0  9.1
   32.                          *   -188.2      66.0    -332.6      228.6 *     2 17.
318. AG    375.    4.2    0.0  9.1
   33.                          *      0.0       4.6      77.1        4.6 *       77.
90. AG      75.    4.2    0.0  9.1
   34.                          *      0.0       1.5      77.1        1.5 *       77.
90. AG     175.    4.2    0.0  9.1
   35.                          *      0.0      -1.5      77.1       -1.5 *       77.
90. AG     125.    4.2    0.0  9.1
   36.                          *      0.0      -4.6      77.1       -4.6 *       77.
90. AG     225.    4.2    0.0  9.1
   37.                          *     77.1       4.6      90.2        8.4 *       14.
74. AG      75.    4.2    0.0  9.1
   38.                          *     77.1       1.5      91.0        5.4 *       14.
74. AG     175.    4.2    0.0  9.1
   39.                          *     77.1      -1.5      91.8        2.5 *       15.
75. AG     125.    4.2    0.0  9.1
   40.                          *     77.1      -4.6      92.7       -0.4 *       16.
75. AG     225.    4.2    0.0  9.1
   41.                          *     90.2       8.4     109.0       11.5 *       19.
80. AG      75.    4.2    0.0  9.1
   42.                          *     91.0       5.4     109.5        8.5 *       19.
81. AG     175.    4.2    0.0  9.1
   43.                          *     91.8       2.5     110.0        5.5 *       18.
81. AG     125.    4.2    0.0  9.1
   44.                          *     92.7      -0.4     110.5        2.5 *       18.
81. AG     225.    4.2    0.0  9.1

                        PAGE  2
    JOB:                                                  RUN:


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```
      LINK VARIABLES
      --------------
        LINK DESCRIPTION          *        LINK COORDINATES (M)                   *    LENGTH
BRG TYPE   VPH    EF        H     W    V/C QUEUE
                                  *   X1            Y1          X2           Y2         *     (M)
(DEG)             (G/MI)   (M)  (M)       (VEH)

-----------------------*- ----------------- ----------------- -----*----------- ------
------------------------------- -------------------
         45.                      *   109.0        11.5       130.0         16.6 *       22.
76. AG     75.    4.2    0.0   9.1
         46.                      *   109.5         8.5       130.7         13.7 *       22.
76. AG    175.    4.2    0.0   9.1
         47.                      *   110.0         5.5       131.4         10.7 *       22.
76. AG    125.    4.2    0.0   9.1
         48.                      *   110.5         2.5       132.1          7.8 *       22.
76. AG    225.    4.2    0.0   9.1
         49.                      *   130.0        16.6       144.1         24.4 *       16.
61. AG     75.    4.2    0.0   9.1
         50.                      *   130.7        13.7       145.6         21.8 *       17.
61. AG    175.    4.2    0.0   9.1
         51.                      *   131.4        10.7       147.0         19.1 *       18.
62. AG    125.    4.2    0.0   9.1
         52.                      *   132.1         7.8       148.5         16.4 *       18.
62. AG    225.    4.2    0.0   9.1
         53.                      *   144.1        24.4       308.8        111.6 *      186.
62. AG     75.    4.2    0.0   9.1
         54.                      *   145.6        21.8       310.2        108.9 *      186.
62. AG    175.    4.2    0.0   9.1
         55.                      *   147.0        19.1       311.6        106.2 *      186.
62. AG    125.    4.2    0.0   9.1
         56.                      *   148.5        16.4       313.0        103.6 *      186.
62. AG    225.    4.2    0.0   9.1
          57.                      *     7.6         0.0         7.6        185.9 *      186.
360. AG     580.    4.2    0.0   9.1
          58.                      *     4.6         0.0         4.6        185.9 *      186.
360. AG     580.    4.2    0.0   9.1
          59.                      *     1.5         0.0         1.5        185.9 *      186.
360. AG     740.    4.2    0.0   9.1
          60.                      *    -1.5         0.0        -1.5        185.9 *      186.
360. AG     502.    4.2    0.0   9.1
          61.                      *    -4.6         0.0        -4.6        185.9 *      186.
360. AG     456.    4.2    0.0   9.1
          62.                      *    -7.6         0.0        -7.6        185.9 *      186.
360. AG     652.    4.2    0.0   9.1
          63.                      *     7.6       185.9         7.6       -447.1 *      633.
180. AG     730.    4.2    0.0   9.1
          64.                      *     4.6       185.9         4.6       -447.1 *      633.
180. AG     580.    4.2    0.0   9.1
          65.                      *     1.5       185.9         1.5       -447.1 *      633.
180. AG    1130.    4.2    0.0   9.1
          66.                      *    -1.5       185.9        -1.5       -447.1 *      633.
180. AG     552.    4.2    0.0   9.1
          67.                      *    -4.6       185.9        -4.6       -447.1 *      633.
180. AG     456.    4.2    0.0   9.1
          68.                      *    -7.6       185.9        -7.6       -447.1 *      633.
180. AG     752.    4.2    0.0   9.1
          69.                      *    -9.1         4.6       -27.5          4.6 *       18.
270. AG      34.  100.0    0.0   3.0 0.34   3.1
          70.                      *    -9.1         1.5       -50.8          1.5 *       42.
270. AG      34.  100.0    0.0   3.0 0.76   6.9
          71.                      *    -9.1        -1.5       -24.8         -1.5 *       16.
270. AG      34.  100.0    0.0   3.0 0.29   2.6
```

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      72.                                  *     -9.1     -4.6     -34.1      -4.6 *      25.
270. AG     34. 100.0   0.0  3.0 0.46   4.2
      73.                                  *      9.1      4.6      14.1       4.6 *       5.
90. AG     34. 100.0   0.0  3.0 0.09   0.8
      74.                                  *      9.1      1.5      20.8       1.5 *      12.
90. AG     34. 100.0   0.0  3.0 0.21   1.9
      75.                                  *      9.1     -1.5      17.5      -1.5 *       8.
90. AG     34. 100.0   0.0  3.0 0.15   1.4
      76.                                  *      9.1     -4.6      24.1      -4.6 *      15.
90. AG     34. 100.0   0.0  3.0 0.28   2.5
      77.                                  *      7.6      6.1       7.6      44.8 *      39.
360. AG     34. 100.0   0.0  3.0 0.71   6.4
      78.                                  *      4.6      6.1       4.6      44.8 *      39.
360. AG     34. 100.0   0.0  3.0 0.71   6.4
      79.                                  *      1.5      6.1       1.5      62.6 *      57.
360. AG     34. 100.0   0.0  3.0 0.91   9.4
      80.                                  *     -1.5      6.1      -1.5      39.6 *      33.
360. AG     34. 100.0   0.0  3.0 0.61   5.6
      81.                                  *     -4.6      6.1      -4.6      36.5 *      30.
360. AG     34. 100.0   0.0  3.0 0.56   5.1
      82.                                  *     -7.6      6.1      -7.6      49.6 *      43.
360. AG     34. 100.0   0.0  3.0 0.80   7.2
      83.                                  *      7.6     -6.1       7.6     -60.2 *      54.
180. AG     34. 100.0   0.0  3.0 0.89   9.0
      84.                                  *      4.6     -6.1       4.6     -44.8 *      39.
180. AG     34. 100.0   0.0  3.0 0.71   6.4
      85.                                  *      1.5     -6.1       1.5   -1064.8 *    1059.
180. AG     34. 100.0   0.0  3.0 1.38 176.4
      86.                                  *     -1.5     -6.1      -1.5     -42.9 *      37.
180. AG     34. 100.0   0.0  3.0 0.68   6.1
      87.                                  *     -4.6     -6.1      -4.6     -36.5 *      30.
180. AG     34. 100.0   0.0  3.0 0.56   5.1
      88.                                  *     -7.6     -6.1      -7.6     -65.8 *      60.
180. AG     34. 100.0   0.0  3.0 0.92  10.0

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     JOB:                                                                 RUN:


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      ADDITIONAL QUEUE LINK PARAMETERS
      --------------------------------
         LINK DESCRIPTION         *    CYCLE     RED     CLEARANCE   APPROACH   SATURATION
 IDLE   SIGNAL   ARRIVAL
                                  *    LENGTH    TIME    LOST TIME     VOL      FLOW RATE
EM FAC   TYPE      RATE
                                  *    (SEC)     (SEC)    (SEC)       (VPH)       (VPH)
(gm/hr)

-------------------------*------------------------------------------------------------------
-------------------------
      69.                         *     90        40       2.0         275        1600
28.88     2         3
      70.                         *     90        40       2.0         625        1600
28.88     2         3
      71.                         *     90        40       2.0         235        1600
28.88     2         3
      72.                         *     90        40       2.0         375        1600
28.88     2         3
      73.                         *     90        40       2.0          75        1600
28.88     2         3
```

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          74.                             *     90      40      2.0      175      160 0
28.88          2          3
          75.                             *     90      40      2.0      125      160 0
28.88          2          3
          76.                             *     90      40      2.0      225      160 0
28.88          2          3
          77.                             *     90      40      2.0      580      160 0
28.88          2          3
          78.                             *     90      40      2.0      580      160 0
28.88          2          3
          79.                             *     90      40      2.0      740      160 0
28.88          2          3
          80.                             *     90      40      2.0      502      160 0
28.88          2          3
          81.                             *     90      40      2.0      456      160 0
28.88          2          3
          82.                             *     90      40      2.0      652      160 0
28.88          2          3
          83.                             *     90      40      2.0      730      160 0
28.88          2          3
          84.                             *     90      40      2.0      580      160 0
28.88          2          3
          85.                             *     90      40      2.0     1130      160 0
28.88          2          3
          86.                             *     90      40      2.0      552      160 0
28.88          2          3
          87.                             *     90      40      2.0      456      160 0
28.88          2          3
          88.                             *     90      40      2.0      752      160 0
28.88          2          3

          RECEPTOR LOCATIONS
          ------------------
                                      *          COORDINATES (M)           *
           RECEPTOR                   *     X           Y          Z       *
       -------------------------  ----*----------- ------------- --------*
        1.                            *   -102.4       23.1        1.8     *
        2.                            *   -111.2       27.9        1.8     *
        3.                            *   -120.0       32.7        1.8     *
        4.                            *   -127.1        9.0        1.8     *
        5.                            *   -118.3        4.2        1.8     *
        6.                            *   -123.6       34.6        1.8     *
        7.                            *   -131.8       40.3        1.8     *
        8.                            *   -145.1       20.0        1.8     *
        9.                            *   -136.9       14.3        1.8     *
       10.                            *   -138.9       45.2        1.8     *
       11.                            *   -146.6       51.5        1.8     *
       12.                            *   -154.4       57.9        1.8     *
       13.                            *   -170.1       39.4        1.8     *
       14.                            *   -162.4       33.1        1.8     *
       15.                            *   -154.6       26.8        1.8     *
       16.                            *   -154.7       58.1        1.8     *
       17.                            *   -162.4       64.5        1.8     *
       18.                            *   -182.4       49.5        1.8     *
       19.                            *   -174.7       43.1        1.8     *
       20.                            *   -166.3       67.7        1.8     *
       21.                            *   -173.4       74.7        1.8     *
       22.                            *   -193.6       60.6        1.8     *
       23.                            *   -186.6       53.6        1.8     *
       24.                            *   -176.1       77.4        1.8     *
       25.                            *   -182.7       84.9        1.8     *
```

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JOB:                                                          RUN:

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  RECEPTOR LOCATIONS
  ------------------
                                  *          COORDINATES (M)            *
     RECEPTOR                     *       X          Y          Z       *
 ------------------------------   *----------------------------------------*
 26.                              *    -189.3      92.4        1.8     *
 27.                              *    -196.0      99.8        1.8     *
 28.                              *    -202.6     107.3        1.8     *
 29.                              *    -218.8      89.0        1.8     *
 30.                              *    -212.2      81.5        1.8     *
 31.                              *    -205.5      74.0        1.8     *
 32.                              *    -198.9      66.5        1.8     *
 33.                              *     -79.9      15.1        1.8     *
 34.                              *     -89.3      18.5        1.8     *
 35.                              *     -98.7      21.9        1.8     *
 36.                              *    -111.6       0.8        1.8     *
 37.                              *    -102.2      -2.5        1.8     *
 38.                              *     -92.7      -5.8        1.8     *
 39.                              *     -83.3      -9.1        1.8     *
 40.                              *      88.1      15.6        1.8     *
 41.                              *      78.5      12.8        1.8     *
 42.                              *      79.1     -11.9        1.8     *
 43.                              *      88.7      -9.3        1.8     *
 44.                              *     107.7      19.0        1.8     *
 45.                              *      97.9      17.3        1.8     *
 46.                              *      93.9      -7.9        1.8     *
 47.                              *     103.8      -6.2        1.8     *
 48.                              *     128.2      24.0        1.8     *
 49.                              *     118.5      21.6        1.8     *
 50.                              *     112.3      -4.8        1.8     *
 51.                              *     122.0      -2.5        1.8     *
 52.                              *     131.7      -0.1        1.8     *
 53.                              *     140.4      31.0        1.8     *
 54.                              *     131.7      26.2        1.8     *
 55.                              *     135.7       1.1        1.8     *
 56.                              *     144.6       5.8        1.8     *
 57.                              *     163.8      43.4        1.8     *
 58.                              *     155.0      38.7        1.8     *
 59.                              *     146.1      34.0        1.8     *
 60.                              *     152.1       9.7        1.8     *
 61.                              *     160.9      14.4        1.8     *
 62.                              *     169.7      19.1        1.8     *
 63.                              *     178.6      23.8        1.8     *
 64.                              *     -15.2      12.2        1.8     *
 65.                              *     -25.2      12.2        1.8     *
 66.                              *     -35.2      12.2        1.8     *
 67.                              *     -45.2      12.2        1.8     *
 68.                              *     -55.2      12.2        1.8     *
 69.                              *     -65.2      12.2        1.8     *
 70.                              *     -15.2     -12.2        1.8     *
 71.                              *     -25.2     -12.2        1.8     *
 72.                              *     -35.2     -12.2        1.8     *
 73.                              *     -45.2     -12.2        1.8     *
 74.                              *     -55.2     -12.2        1.8     *
 75.                              *     -65.2     -12.2        1.8     *
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                          PAGE  5
 JOB:                                                      RUN:


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  RECEPTOR LOCATIONS
  ------------------
                              *          COORDINATES (M)           *
    RECEPTOR                  *      X          Y          Z       *
 ------------------------- ----*----------- ---------------- --------*
 76.                          *      15.2       12.2        1.8    *
 77.                          *      25.2       12.2        1.8    *
 78.                          *      35.2       12.2        1.8    *
 79.                          *      45.2       12.2        1.8    *
 80.                          *      55.2       12.2        1.8    *
 81.                          *      65.2       12.2        1.8    *
 82.                          *      15.2      -12.2        1.8    *
 83.                          *      25.2      -12.2        1.8    *
 84.                          *      35.2      -12.2        1.8    *
 85.                          *      45.2      -12.2        1.8    *
 86.                          *      55.2      -12.2        1.8    *
 87.                          *      65.2      -12.2        1.8    *
 88.                          *     -15.2       22.2        1.8    *
 89.                          *     -25.2       22.2        1.8    *
 90.                          *     -35.2       22.2        1.8    *
 91.                          *     -45.2       22.2        1.8    *
 92.                          *     -55.2       22.2        1.8    *
 93.                          *     -65.2       22.2        1.8    *
 94.                          *     -15.2      -22.2        1.8    *
 95.                          *     -25.2      -22.2        1.8    *
 96.                          *     -35.2      -22.2        1.8    *
 97.                          *     -45.2      -22.2        1.8    *
 98.                          *     -55.2      -22.2        1.8    *
 99.                          *     -65.2      -22.2        1.8    *
100.                          *      15.2       22.2        1.8    *
101.                          *      25.2       22.2        1.8    *
102.                          *      35.2       22.2        1.8    *
103.                          *      45.2       22.2        1.8    *
104.                          *      55.2       22.2        1.8    *
105.                          *      65.2       22.2        1.8    *
106.                          *      15.2      -22.2        1.8    *
107.                          *      25.2      -22.2        1.8    *
108.                          *      35.2      -22.2        1.8    *
109.                          *      45.2      -22.2        1.8    *
110.                          *      55.2      -22.2        1.8    *
111.                          *      65.2      -22.2        1.8    *
112.                          *     -15.2       32.2        1.8    *
113.                          *     -25.2       32.2        1.8    *
114.                          *     -35.2       32.2        1.8    *
115.                          *     -45.2       32.2        1.8    *
116.                          *     -55.2       32.2        1.8    *
117.                          *     -65.2       32.2        1.8    *
118.                          *     -15.2      -32.2        1.8    *
119.                          *     -25.2      -32.2        1.8    *
120.                          *     -35.2      -32.2        1.8    *
121.                          *     -45.2      -32.2        1.8    *
122.                          *     -55.2      -32.2        1.8    *
123.                          *     -65.2      -32.2        1.8    *
124.                          *      15.2       32.2        1.8    *
125.                          *      25.2       32.2        1.8    *
```

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                          PAGE  6
  JOB:                                                  RUN:


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   RECEPTOR LOCATIONS
   ------------------
                                *          COORDINATES (M)          *
     RECEPTOR                   *      X          Y          Z      *
  ------------------------- ----*------- -------------------------- *
 126.                           *     35.2       32.2       1.8     *
 127.                           *     45.2       32.2       1.8     *
 128.                           *     55.2       32.2       1.8     *
 129.                           *     65.2       32.2       1.8     *
 130.                           *     15.2      -32.2       1.8     *
 131.                           *     25.2      -32.2       1.8     *
 132.                           *     35.2      -32.2       1.8     *
 133.                           *     45.2      -32.2       1.8     *
 134.                           *     55.2      -32.2       1.8     *
 135.                           *     65.2      -32.2       1.8     *
 136.                           *    -15.2       42.2       1.8     *
 137.                           *    -25.2       42.2       1.8     *
 138.                           *    -35.2       42.2       1.8     *
 139.                           *    -15.2      -42.2       1.8     *
 140.                           *    -25.2      -42.2       1.8     *
 141.                           *    -35.2      -42.2       1.8     *
 142.                           *     15.2       42.2       1.8     *
 143.                           *     25.2       42.2       1.8     *
 144.                           *     35.2       42.2       1.8     *
 145.                           *     15.2      -42.2       1.8     *
 146.                           *     25.2      -42.2       1.8     *
 147.                           *     35.2      -42.2       1.8     *
 148.                           *     15.2       52.2       1.8     *
 149.                           *     15.2       62.2       1.8     *
 150.                           *     15.2       72.2       1.8     *
 151.                           *     15.2       82.2       1.8     *
 152.                           *     15.2       92.2       1.8     *
 153.                           *     15.2      102.2       1.8     *
 154.                           *     15.2      112.2       1.8     *
 155.                           *     15.2      122.2       1.8     *
 156.                           *     15.2      132.2       1.8     *
 157.                           *    -15.2       52.2       1.8     *
 158.                           *    -15.2       62.2       1.8     *
 159.                           *    -15.2       72.2       1.8     *
 160.                           *    -15.2       82.2       1.8     *
 161.                           *    -15.2       92.2       1.8     *
 162.                           *    -15.2      102.2       1.8     *
 163.                           *    -15.2      112.2       1.8     *
 164.                           *    -15.2      122.2       1.8     *
 165.                           *    -15.2      132.2       1.8     *
 166.                           *     15.2      -52.2       1.8     *
 167.                           *     15.2      -62.2       1.8     *
 168.                           *     15.2      -72.2       1.8     *
 169.                           *     15.2      -82.2       1.8     *
 170.                           *     15.2      -92.2       1.8     *
 171.                           *     15.2     -102.2       1.8     *
 172.                           *     15.2     -112.2       1.8     *
 173.                           *     15.2     -122.2       1.8     *
 174.                           *     15.2     -132.2       1.8     *
```

```
   175.                          *      -15.2      -52.2         1.8   *
□
                              PAGE  7
     JOB:                                                    RUN:


     DATE : 02/23/   0
     TIME : 18:53:17


      RECEPTOR LOCATIONS
      ------------------
                                 *            COORDINATES (M)           *
        RECEPTOR                 *       X          Y            Z      *
   ------------------------------*-------------------------------------*
   176.                          *      -15.2      -62.2         1.8   *
   177.                          *      -15.2      -72.2         1.8   *
   178.                          *      -15.2      -82.2         1.8   *
   179.                          *      -15.2      -92.2         1.8   *
   180.                          *      -15.2     -102.2         1.8   *
   181.                          *      -15.2     -112.2         1.8   *
   182.                          *      -15.2     -122.2         1.8   *
   183.                          *      -15.2     -132.2         1.8   *
□
                              PAGE  8
     JOB:                                                    RUN:


      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

  WIND ANGLE RANGE:   0.-350.

  WIND  * CONCENTRATION
  ANGLE *       (PPM)
  (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12
REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

------*------------------------------------------------------------------------------
--------------------------------------------
   0.  *  0.0   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0
0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.0
  10.  *  0.0   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0
0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.0
  20.  *  0.0   0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  30.  *  0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
0.0   0.1   0.0   0.0   0.0   0.0   0.1   0.0
  40.  *  0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.0
  50.  *  0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.0
  60.  *  0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.1   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  70.  *  0.0   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0
0.1   0.0   0.1   0.0   0.0   0.0   0.0   0.0
  80.  *  0.0   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
```

```
  90.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .1  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 100.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 110.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 120.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 130.  *    0.1   0.1   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 140.  *    0.1   0.1   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 150.  *    0.1   0.0   0.1   0.0   0.0   0. 1  0.1   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 160.  *    0.1   0.0   0.1   0.0   0.0   0. 1  0.0   0.0   0 .0  0.1   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 170.  *    0.1   0.0   0.1   0.0   0.0   0. 1  0.0   0.0   0 .0  0.1   0.0   0 .1
0.0  0.0   0.0   0.1   0. 0   0.0   0.0   0 .0
 180.  *    0.1   0.1   0.1   0.0   0.0   0. 1  0.0   0.0   0 .0  0.1   0.0   0 .1
0.0  0.0   0.0   0.1   0. 0   0.0   0.0   0 .1
 190.  *    0.1   0.1   0.1   0.0   0.0   0. 1  0.1   0.0   0 .0  0.1   0.1   0 .1
0.0  0.0   0.0   0.1   0. 1   0.0   0.0   0 .1
 200.  *    0.0   0.1   0.1   0.0   0.0   0. 0  0.1   0.0   0 .0  0.1   0.1   0 .1
0.0  0.0   0.0   0.1   0. 1   0.0   0.0   0 .1
 210.  *    0.0   0.1   0.1   0.0   0.0   0. 0  0.1   0.0   0 .0  0.0   0.1   0 .0
0.0  0.0   0.0   0.0   0. 1   0.0   0.0   0 .0
 220.  *    0.0   0.1   0.1   0.0   0.0   0. 0  0.1   0.0   0 .0  0.0   0.1   0 .0
0.0  0.0   0.0   0.0   0. 1   0.0   0.0   0 .0
 230.  *    0.1   0.1   0.0   0.0   0.0   0. 1  0.1   0.0   0 .0  0.0   0.1   0 .0
0.0  0.0   0.0   0.0   0. 1   0.0   0.0   0 .0
 240.  *    0.1   0.1   0.0   0.0   0.0   0. 1  0.1   0.0   0 .0  0.1   0.1   0 .1
0.0  0.0   0.0   0.1   0. 0   0.0   0.0   0 .1
 250.  *    0.1   0.1   0.0   0.0   0.0   0. 1  0.0   0.0   0 .0  0.1   0.1   0 .1
0.0  0.0   0.0   0.1   0. 0   0.0   0.0   0 .1
 260.  *    0.1   0.0   0.1   0.0   0.0   0. 1  0.0   0.0   0 .0  0.1   0.0   0 .1
0.0  0.0   0.0   0.1   0. 0   0.0   0.0   0 .1
 270.  *    0.1   0.0   0.1   0.0   0.0   0. 1  0.0   0.0   0 .0  0.1   0.0   0 .1
0.0  0.0   0.0   0.1   0. 0   0.0   0.0   0 .1
 280.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 290.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .1
 300.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.1   0. 1   0.0   0.0   0 .1
 310.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .1
0.0  0.0   0.0   0.1   0. 1   0.0   0.0   0 .1
 320.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.1  0.0   0.0   0.0   0. 0   0.1   0.1   0 .0
 330.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.1  0.0   0.0   0.0   0. 0   0.2   0.1   0 .0
 340.  *    0.0   0.0   0.0   0.0   0.0   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.1   0.0   0 .0
 350.  *    0.0   0.0   0.0   0.0   0.1   0. 0  0.0   0.0   0 .0  0.0   0.0   0 .0
0.0  0.0   0.0   0.0   0. 0   0.0   0.0   0 .0

------*----------------- ----------------- ----------------- ----------------- ------
-------------------------------- -----------------
 MAX   *    0.1   0.1   0.1   0.1   0.1   0. 1  0.1   0.1   0 .1  0.1   0.1   0 .1
0.1  0.1   0.1   0.1   0. 1   0.2   0.1   0 .1
 DEGR. *  130   130   150    20     0   150   150    30     0   160   190   17 0
70    30     0   170   190   330    30   18 0

□
```

```
                                   PAGE  9
  JOB:                                                              RUN:


    MODEL RESULTS
    -------------

    REMARKS : In search of the angle corresponding to
              the maximum concentration, only the first
              angle, of the angles with same maximum
              concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32
REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
 ------*-----------------------------------------------------------------------------
---------------------------------------------------
   0.  *   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.0
  10.  *   0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.0
  20.  *   0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.1
0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.0
  30.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.1
0.0   0.0   0.0   0.0   0.1   0.1   0.0   0.0
  40.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.1
0.0   0.0   0.0   0.0   0.1   0.1   0.0   0.0
  50.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.1
0.0   0.0   0.0   0.1   0.1   0.1   0.0   0.0
  60.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.0
0.0   0.0   0.0   0.1   0.2   0.0   0.1   0.0
  70.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.0
0.0   0.0   0.0   0.2   0.2   0.0   0.1   0.0
  80.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.0
0.0   0.0   0.0   0.2   0.1   0.1   0.2   0.0
  90.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.0   0.0
0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
 100.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 110.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.1   0.0   0.0
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 120.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.0   0.0   0.0
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 130.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.1   0.0   0.1   0.0   0.0   0.0   0.0   0.0
 140.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.0
 150.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.1   0.1   0.0   0.0   0.0   0.0   0.0
 160.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.1   0.1   0.0   0.0   0.0   0.0   0.0
 170.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1   0.1   0.0   0.0   0.0   0.0   0.0
 180.  *   0.0   0.0   0.0   0.1   0.0   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1   0.1   0.0   0.0   0.0   0.0   0.0
 190.  *   0.0   0.0   0.0   0.1   0.0   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1   0.1   0.0   0.0   0.0   0.0   0.0
 200.  *   0.1   0.0   0.0   0.1   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1   0.1   0.0   0.0   0.0   0.0   0.0
```

```
 210.  *   0.1   0.0   0.0   0.1   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1   0.1   0.0   0.0   0.0   0.0   0.0
 220.  *   0.1   0.0   0.0   0.0   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0
 230.  *   0.1   0.0   0.0   0.0   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0
 240.  *   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0
 250.  *   0.0   0.0   0.0   0.1   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.0   0.1   0.0   0.0   0.0   0.0   0.0
 260.  *   0.0   0.0   0.0   0.1   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.0   0.1   0.0   0.0   0.0   0.0   0.0
 270.  *   0.1   0.0   0.0   0.1   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.0
 280.  *   0.1   0.0   0.0   0.1   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 290.  *   0.1   0.0   0.0   0.1   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 300.  *   0.1   0.0   0.0   0.2   0.2   0.2   0.2   0.2   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 310.  *   0.1   0.0   0.0   0.1   0.1   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 320.  *   0.1   0.1   0.2   0.1   0.1   0.1   0.1   0.0   0.1   0.1   0.1   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.0
 330.  *   0.0   0.2   0.2   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
0.0   0.0   0.0   0.1   0.0   0.1   0.2   0.0
 340.  *   0.0   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
0.0   0.0   0.0   0.1   0.0   0.1   0.2   0.0
 350.  *   0.0   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
0.0   0.0   0.0   0.1   0.0   0.1   0.1   0.0

------*-- ----------------- ----------------- ----------------- ----------------- ------
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 MAX   *   0.1   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2
0.1   0.1   0.1   0.2   0.2   0.1   0.2   0.0
 DEGR. *  200     0   320   300   300   300   300   300     0     0     0     0
110   150   130    70    60     0    80     0

□
                             PAGE 10
     JOB:                                                        RUN:


       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52
REC53 REC54 REC55 REC56 REC57 REC58 REC59 REC60

------*-- ----------------- ----------------- ----------------- ----------------- ------
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   0.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  10.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
```

```
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  20. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  30. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  40. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  50. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  60. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  70. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  80. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
  90. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 100. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 110. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 120. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 130. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 140. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 150. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 160. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 170. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 180. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 190. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 200. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 210. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 220. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 230. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 240. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 250. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 260. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 270. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 280. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 290. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 300. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 310. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 320. *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
```

```
 330.  *    0.0   0.0   0.0    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0    0.0   0.0   0.0    0.0   0.0   0.0
 340.  *    0.0   0.0   0.0    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0    0.0   0.0   0.0    0.0   0.0   0.0
 350.  *    0.0   0.0   0.0    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0    0.0   0.0   0.0    0.0   0.0   0.0

------*---------------------------------------------------------------------------------------
-----------------------------------------------------
 MAX   *    0.0   0.0   0.0    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0    0.0   0.0   0.0    0.0   0.0   0.0
 DEGR. *    0     0     0      0     0     0     0     0     0     0     0     0
0     0      0     0     0      0     0     0


                                 PAGE 11
      JOB:                                                               RUN:


        MODEL RESULTS
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        REMARKS : In search of the angle corresponding to
                  the maximum concentration, only the first
                  angle, of the angles with same maximum
                  concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* REC61 REC62 REC63 REC64 REC65 REC66 REC67 REC68 REC69 REC70 REC71 REC72
REC73 REC74 REC75 REC76 REC77 REC78 REC79 REC80

------*---------------------------------------------------------------------------------------
-----------------------------------------------------
   0.  *    0.0   0.0   0.0    0.3   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1
0.1   0.1    0.1   0.5   0.0    0.0   0.0   0.0
  10.  *    0.0   0.0   0.0    0.8   0.3   0.0   0.0   0.0   0.0   1.0   0.5   0.1
0.1   0.1    0.1   0.0   0.0    0.0   0.0   0.0
  20.  *    0.0   0.0   0.0    1.2   0.3   0.1   0.0   0.0   0.0   1.3   0.6   0.3
0.1   0.1    0.1   0.0   0.0    0.0   0.0   0.0
  30.  *    0.0   0.0   0.0    1.0   0.4   0.2   0.0   0.0   0.0   0.8   0.7   0.4
0.2   0.1    0.1   0.0   0.0    0.0   0.0   0.0
  40.  *    0.0   0.0   0.0    1.1   0.3   0.1   0.1   0.0   0.0   0.6   0.5   0.4
0.4   0.2    0.2   0.0   0.0    0.0   0.0   0.0
  50.  *    0.0   0.0   0.0    1.0   0.3   0.1   0.0   0.0   0.0   0.5   0.4   0.4
0.3   0.3    0.2   0.0   0.0    0.0   0.0   0.0
  60.  *    0.0   0.0   0.0    0.6   0.2   0.1   0.0   0.0   0.0   0.2   0.4   0.4
0.2   0.3    0.2   0.0   0.0    0.0   0.0   0.0
  70.  *    0.0   0.0   0.0    0.6   0.2   0.1   0.0   0.0   0.0   0.3   0.2   0.3
0.2   0.2    0.2   0.0   0.0    0.0   0.0   0.0
  80.  *    0.0   0.0   0.0    0.6   0.2   0.1   0.0   0.0   0.0   0.3   0.2   0.1
0.0   0.0    0.1   0.0   0.0    0.0   0.0   0.0
  90.  *    0.0   0.0   0.0    0.6   0.2   0.1   0.0   0.0   0.0   0.4   0.2   0.1
0.0   0.0    0.0   0.0   0.0    0.0   0.0   0.0
 100.  *    0.0   0.0   0.0    0.5   0.2   0.1   0.0   0.1   0.1   0.4   0.2   0.1
0.0   0.0    0.0   0.0   0.0    0.0   0.0   0.0
 110.  *    0.0   0.0   0.0    0.4   0.2   0.2   0.1   0.2   0.1   0.4   0.2   0.1
0.0   0.0    0.0   0.0   0.0    0.0   0.0   0.0
 120.  *    0.0   0.0   0.0    0.3   0.4   0.3   0.2   0.2   0.1   0.4   0.2   0.1
0.0   0.0    0.0   0.0   0.0    0.0   0.0   0.0
 130.  *    0.0   0.0   0.0    0.4   0.4   0.3   0.2   0.2   0.1   0.5   0.2   0.1
```

```
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 140.  *   0.0   0.0   0.0   0.7   0.5   0.3   0.3   0.1   0.1   0.7   0.2   0.1
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 150.  *   0.0   0.0   0.0   0.8   0.5   0.4   0.3   0.1   0.1   0.8   0.2   0.2
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 160.  *   0.0   0.0   0.0   0.9   0.5   0.4   0.3   0.1   0.1   0.8   0.2   0.2
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 170.  *   0.0   0.0   0.0   1.0   0.6   0.4   0.2   0.1   0.1   0.8   0.2   0.2
0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
 180.  *   0.0   0.0   0.0   0.7   0.5   0.2   0.2   0.1   0.1   0.3   0.1   0.0
0.0   0.0   0.0   0.4   0.2   0.0   0.0   0.0
 190.  *   0.0   0.0   0.0   0.4   0.2   0.2   0.1   0.1   0.1   0.1   0.0   0.0
0.0   0.0   0.0   0.7   0.4   0.2   0.1   0.0
 200.  *   0.0   0.0   0.0   0.3   0.2   0.2   0.1   0.1   0.1   0.0   0.0   0.0
0.0   0.0   0.0   0.6   0.4   0.2   0.1   0.1
 210.  *   0.0   0.0   0.0   0.3   0.2   0.2   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.5   0.2   0.2   0.1   0.1
 220.  *   0.0   0.0   0.0   0.3   0.2   0.2   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.5   0.2   0.1   0.1   0.0
 230.  *   0.0   0.0   0.0   0.3   0.2   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.5   0.2   0.1   0.1   0.0
 240.  *   0.0   0.0   0.0   0.2   0.1   0.1   0.1   0.0   0.1   0.0   0.0   0.0
0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
 250.  *   0.0   0.0   0.0   0.1   0.1   0.1   0.0   0.0   0.1   0.0   0.0   0.0
0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0
 260.  *   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.1   0.0   0.0   0.0
0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0
 270.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0
 280.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0
 290.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.1   0.1
0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0
 300.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.3   0.2   0.2
0.1   0.0   0.0   0.8   0.2   0.1   0.0   0.0
 310.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.4   0.2   0.2
0.2   0.0   0.1   1.0   0.2   0.1   0.0   0.0
 320.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.3   0.3   0.2
0.1   0.0   0.0   1.0   0.4   0.1   0.1   0.0
 330.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.1
0.1   0.1   0.0   1.2   0.4   0.1   0.1   0.0
 340.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.1
0.1   0.1   0.0   0.9   0.4   0.1   0.0   0.0
 350.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.3   0.2   0.1
0.1   0.1   0.0   0.6   0.2   0.0   0.0   0.0

------*-- ----------------- ----------------- ----------------- ----------------- ------
------------------------- -----------------
 MAX   *   0.0   0.0   0.0   1.2   0.6   0.4   0.3   0.2   0.1   1.3   0.7   0.4
0.4   0.3   0.2   1.2   0.4   0.2   0.1   0.1
 DEGR. *   0     0     0     20    170   150   140   110   100   20    30    30
40    50    40    330   190   190   190   200

□
                                PAGE 12
     JOB:                                                         RUN:


     MODEL RESULTS
     -------------

     REMARKS : In search of the angle corresponding to
               the maximum concentration, only the first
```

```
                    angle, of the angles with same maximum
                    concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  *  CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)*  REC81 REC82 REC83 REC84 REC85 REC86 REC87 REC88 REC89 REC90 REC91 REC92
REC93 REC94 REC95 REC96 REC97 REC98 REC99 RE100

------*-------------------------------------------------------------------------------
----------------------------------------------------
   0.  *   0.0   0.7   0.0   0.0   0.0   0.0   0.0   0.3   0.0   0.0   0.0   0.0
0.0   0.3   0.0   0.0   0.0   0.0   0.0   0.3
  10.  *   0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.8   0.3   0.0   0.0   0.0
0.0   0.6   0.3   0.0   0.0   0.0   0.0   0.0
  20.  *   0.0   0.1   0.0   0.0   0.0   0.0   0.0   1.0   0.3   0.1   0.0   0.0
0.0   0.8   0.4   0.2   0.0   0.0   0.0   0.0
  30.  *   0.0   0.1   0.0   0.0   0.0   0.0   0.0   1.0   0.4   0.2   0.0   0.0
0.0   0.6   0.2   0.2   0.1   0.0   0.0   0.0
  40.  *   0.0   0.1   0.0   0.0   0.0   0.0   0.0   1.0   0.3   0.1   0.1   0.0
0.0   0.6   0.2   0.1   0.1   0.0   0.0   0.0
  50.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9   0.3   0.1   0.0   0.0
0.0   0.7   0.2   0.1   0.0   0.0   0.0   0.0
  60.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0
  70.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0
  80.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0
  90.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0
 100.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0
 110.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0
 120.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0
 130.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   0.2   0.1   0.0   0.0
0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0
 140.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.7   0.2   0.1   0.1   0.0
0.0   0.6   0.2   0.1   0.1   0.0   0.0   0.0
 150.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8   0.2   0.2   0.1   0.0
0.0   0.8   0.2   0.2   0.1   0.0   0.0   0.0
 160.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.7   0.2   0.2   0.1   0.0
0.0   0.8   0.2   0.2   0.1   0.0   0.0   0.0
 170.  *   0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.7   0.2   0.2   0.0   0.0
0.0   0.8   0.2   0.2   0.0   0.0   0.0   0.1
 180.  *   0.0   0.4   0.1   0.0   0.0   0.0   0.0   0.4   0.2   0.0   0.0   0.0
0.0   0.3   0.1   0.0   0.0   0.0   0.0   0.4
 190.  *   0.0   0.7   0.4   0.2   0.1   0.0   0.0   0.1   0.0   0.0   0.0   0.0
0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.6
 200.  *   0.0   0.7   0.5   0.2   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6
 210.  *   0.0   0.8   0.2   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.7
 220.  *   0.0   0.7   0.2   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 230.  *   0.0   0.7   0.2   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9
 240.  *   0.0   0.5   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 250.  *   0.0   0.5   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
```

```
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 260.  *    0.0   0.5   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 270.  *    0.0   0.5   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 280.  *    0.0   0.4   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 290.  *    0.0   0.5   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 300.  *    0.0   0.3   0.3   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 310.  *    0.0   0.4   0.3   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
 320.  *    0.0   0.5   0.3   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
 330.  *    0.0   0.7   0.5   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
 340.  *    0.0   1.0   0.4   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 350.  *    0.0   0.7   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6

------*------------------------------------------------------------------------------
------------------------------------------
 MAX   *    0.0   1.0   0.5   0.2   0.1   0.1   0.0   1.0   0.4   0.2   0.1   0.0
0.0   0.8   0.4   0.2   0.1   0.0   0.0   1.0
 DEGR. *    0    340   330   190   190   200    0    40    30    30    40     0
0     20    20    20    30    0     0    330

□
                        PAGE 13
     JOB:                                                     RUN:


      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND   * CONCENTRATION
 ANGLE  *      (PPM)
 (DEGR)* RE101 RE102 RE103 RE104 RE105 RE106 RE107 RE108 RE109 RE110 RE111 RE112
RE113 RE114 RE115 RE116 RE117 RE118 RE119 RE120

------*------------------------------------------------------------------------------
------------------------------------------
   0.  *    0.0   0.0   0.0   0.0   0.0   0.4   0.0   0.0   0.0   0.0   0.0   0.3
0.0   0.0   0.0   0.0   0.0   0.3   0.0   0.0
  10.  *    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.7
0.2   0.0   0.0   0.0   0.0   0.6   0.2   0.0
  20.  *    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9
0.3   0.1   0.0   0.0   0.0   0.8   0.2   0.2
  30.  *    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
0.4   0.2   0.0   0.0   0.0   0.6   0.2   0.2
  40.  *    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
0.3   0.1   0.0   0.0   0.0   0.7   0.2   0.1
  50.  *    0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9
0.3   0.1   0.0   0.0   0.0   0.7   0.2   0.1
```

```
  60.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .5
0.2   0.1   0.0   0.0   0. 0   0.4   0.2   0 .1
  70.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .5
0.2   0.1   0.0   0.0   0. 0   0.4   0.2   0 .1
  80.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .5
0.2   0.1   0.0   0.0   0. 0   0.4   0.2   0 .1
  90.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .5
0.2   0.1   0.0   0.0   0. 0   0.3   0.2   0 .1
 100.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .6
0.2   0.1   0.0   0.0   0. 0   0.3   0.2   0 .1
 110.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .6
0.2   0.1   0.0   0.0   0. 0   0.3   0.2   0 .1
 120.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .6
0.2   0.1   0.0   0.0   0. 0   0.3   0.2   0 .1
 130.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .7
0.2   0.1   0.0   0.0   0. 0   0.4   0.2   0 .1
 140.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   1 .0
0.2   0.1   0.1   0.0   0. 0   0.6   0.2   0 .1
 150.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .8
0.2   0.2   0.1   0.0   0. 0   0.8   0.2   0 .2
 160.   *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .8
0.2   0.2   0.1   0.0   0. 0   0.8   0.2   0 .2
 170.   *    0.0   0.0   0.0   0.0   0.0   0. 1   0.0   0.0   0 .0   0.0   0.0   0 .8
0.2   0.2   0.0   0.0   0. 0   0.7   0.2   0 .2
 180.   *    0.2   0.0   0.0   0.0   0.0   0. 4   0.1   0.0   0 .0   0.0   0.0   0 .3
0.2   0.0   0.0   0.0   0. 0   0.3   0.1   0 .0
 190.   *    0.4   0.2   0.1   0.0   0.0   0. 7   0.4   0.2   0 .1   0.0   0.0   0 .1
0.0   0.0   0.0   0.0   0. 0   0.1   0.0   0 .0
 200.   *    0.4   0.2   0.1   0.1   0.0   0. 7   0.5   0.2   0 .1   0.1   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 210.   *    0.2   0.2   0.1   0.1   0.0   0. 7   0.2   0.2   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 220.   *    0.2   0.1   0.1   0.0   0.0   0. 7   0.2   0.1   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 230.   *    0.2   0.1   0.1   0.0   0.0   0. 7   0.2   0.1   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 240.   *    0.2   0.1   0.0   0.0   0.0   0. 5   0.2   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 250.   *    0.2   0.1   0.0   0.0   0.0   0. 5   0.2   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 260.   *    0.2   0.1   0.0   0.0   0.0   0. 5   0.2   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 270.   *    0.2   0.1   0.0   0.0   0.0   0. 5   0.2   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 280.   *    0.2   0.1   0.0   0.0   0.0   0. 5   0.2   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 290.   *    0.2   0.1   0.0   0.0   0.0   0. 5   0.2   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 300.   *    0.2   0.1   0.0   0.0   0.0   0. 5   0.2   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 310.   *    0.2   0.1   0.0   0.0   0.0   0. 6   0.2   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 320.   *    0.4   0.1   0.1   0.0   0.0   0. 5   0.2   0.1   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 330.   *    0.4   0.1   0.1   0.0   0.0   0. 6   0.2   0.1   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 340.   *    0.4   0.1   0.0   0.0   0.0   0. 6   0.3   0.1   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0
 350.   *    0.2   0.0   0.0   0.0   0.0   0. 6   0.2   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0

------*------------------------------------------------------------------------------------------------
--------------------------------------------------------------------
```

```
 MAX    *    0.4   0.2   0.1   0.1   0.0   0.7   0.5   0.2   0 .1   0.1   0.0   1 .0
0.4   0.2   0.1   0.0   0. 0   0.8   0.2   0 .2
 DEGR. *   190   190   190   200     0   230   200   190   19 0   200     0   14 0
30    30   140     0     0    20    10    2 0

□
                              PAGE 14
      JOB:                                                         RUN:


        MO DEL  RESULTS
        -------------

        RE MARKS :  In search  of the angle cor responding to
                    the maxim um concentration,  only the first
                    angle, of  the angles with  same maximum
                    concentra tions, is indicat ed as maximum.

 WIND ANG LE RANGE:    0.-35 0.

 WIND   *  CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* RE121 RE122 RE123  RE124 RE125 RE12 6 RE127 RE128 RE1 29 RE130 RE131 RE1 32
RE133 RE1 34 RE135 RE136 RE 137 RE138 RE139 R E140

------*----------------- ----------------- ----------------- ----------------- ------
------------------------ -----------------
   0.  *    0.0   0.0   0.0   0.3   0.0   0. 0   0.0   0.0   0 .0   0.3   0.0   0 .0
0.0   0.0   0.0   0.2   0. 0   0.0   0.2   0 .0
  10.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.7   0. 1   0.0   0.4   0 .2
  20.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0. 3   0.0   0.7   0 .2
  30.  *    0.1   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0. 4   0.1   0.7   0 .2
  40.  *    0.1   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0. 3   0.1   0.8   0 .2
  50.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.8   0. 3   0.1   0.6   0 .2
  60.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.5   0. 2   0.1   0.3   0 .2
  70.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.5   0. 2   0.1   0.3   0 .2
  80.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.5   0. 2   0.1   0.3   0 .2
  90.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.5   0. 2   0.1   0.3   0 .2
 100.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.5   0. 2   0.1   0.3   0 .2
 110.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.5   0. 2   0.1   0.3   0 .2
 120.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.5   0. 2   0.1   0.3   0 .2
 130.  *    0.0   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.6   0. 3   0.1   0.4   0 .2
 140.  *    0.1   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.1   0. 2   0.1   0.6   0 .2
 150.  *    0.1   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.1   0. 2   0.2   0.8   0 .2
 160.  *    0.1   0.0   0.0   0.0   0.0   0. 0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.8   0. 2   0.2   0.8   0 .2
 170.  *    0.0   0.0   0.0   0.1   0.0   0. 0   0.0   0.0   0 .0   0.1   0.0   0 .0
0.0   0.0   0.0   0.8   0. 2   0.2   0.7   0 .2
```

```
 180. *   0.0   0.0   0.0   0.4   0.2   0.0   0.0   0.0   0.0   0.4   0.1   0.0
0.0   0.0   0.0   0.3   0.2   0.0   0.3   0.1
 190. *   0.0   0.0   0.0   0.7   0.4   0.2   0.1   0.0   0.0   0.6   0.4   0.1
0.0   0.0   0.0   0.1   0.0   0.0   0.1   0.0
 200. *   0.0   0.0   0.0   0.7   0.4   0.2   0.1   0.1   0.0   0.7   0.4   0.2
0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0
 210. *   0.0   0.0   0.0   0.9   0.2   0.2   0.1   0.1   0.0   0.7   0.2   0.2
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 220. *   0.0   0.0   0.0   0.9   0.2   0.1   0.1   0.0   0.0   0.6   0.2   0.1
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 230. *   0.0   0.0   0.0   0.9   0.2   0.1   0.1   0.0   0.0   0.6   0.2   0.1
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 240. *   0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0   0.0   0.5   0.2   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 250. *   0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0   0.0   0.5   0.2   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 260. *   0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0   0.0   0.5   0.2   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 270. *   0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0   0.0   0.5   0.2   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 280. *   0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0   0.0   0.5   0.2   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 290. *   0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0   0.0   0.5   0.2   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 300. *   0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0   0.0   0.5   0.2   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 310. *   0.0   0.0   0.0   0.8   0.2   0.1   0.0   0.0   0.0   0.6   0.2   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 320. *   0.0   0.0   0.0   0.8   0.4   0.1   0.1   0.0   0.0   0.6   0.2   0.1
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 330. *   0.0   0.0   0.0   0.8   0.4   0.1   0.1   0.0   0.0   0.6   0.2   0.1
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 340. *   0.0   0.0   0.0   0.8   0.4   0.1   0.0   0.0   0.0   0.6   0.2   0.1
0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 350. *   0.0   0.0   0.0   0.6   0.2   0.0   0.0   0.0   0.0   0.5   0.2   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0

------*------------------------------------------------------------------------------
----------------------------------------------------
 MAX   *   0.1   0.0   0.0   0.9   0.4   0.2   0.1   0.1   0.0   0.7   0.4   0.2
0.1   0.1   0.0   1.1   0.4   0.2   0.8   0.2
 DEGR. *   30    0     0     210   190   190   190   200   0     210   190   200
200   200   0     140   30    150   40    10


                            PAGE 15
     JOB:                                                          RUN:


      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* RE141 RE142 RE143 RE144 RE145 RE146 RE147 RE148 RE149 RE150 RE151 RE152
RE153 RE154 RE155 RE156 RE157 RE158 RE159 RE160
```

```
------*-------------------------------------------------------------------------------------------
-----------------------------------------------------------------
   0.  *   0.0   0.3   0.0   0.0   0.3   0.0   0.0   0.3   0.3   0.3   0.3   0.2
0.2   0.2   0.1   0.1   0.2   0.2   0.2   0.2
  10.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.7   0.7   0.6   0.5
  20.  *   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.9   0.9   0.8   0.8
  30.  *   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.9   0.9   0.9   0.9
  40.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.9   0.9   0.9   0.9
  50.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.8
  60.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.4   0.4   0.4   0.4
  70.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.4   0.4   0.4   0.4
  80.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.4   0.4   0.4   0.4
  90.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.4   0.4   0.4   0.4
 100.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.4   0.4   0.4   0.4
 110.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.4   0.4   0.4   0.4
 120.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.4   0.4   0.4   0.4
 130.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.6   0.5   0.5   0.5
 140.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.9   0.8   0.9   0.9
 150.  *   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   1.0   1.0   1.0   1.0
 160.  *   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.8   1.0   0.9   0.9
 170.  *   0.2   0.1   0.0   0.0   0.1   0.0   0.0   0.1   0.1   0.1   0.1   0.1
0.1   0.1   0.1   0.1   0.8   0.8   0.7   0.7
 180.  *   0.0   0.4   0.2   0.0   0.4   0.1   0.0   0.3   0.3   0.4   0.4   0.4
0.4   0.4   0.4   0.4   0.3   0.4   0.4   0.4
 190.  *   0.0   0.7   0.3   0.2   0.6   0.4   0.1   0.7   0.7   0.8   0.8   0.8
0.8   0.8   0.8   0.8   0.1   0.1   0.1   0.1
 200.  *   0.0   0.9   0.4   0.2   0.6   0.4   0.2   1.0   0.8   0.8   0.8   0.8
0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0
 210.  *   0.0   1.0   0.2   0.2   0.7   0.2   0.2   1.1   0.9   0.9   0.8   0.8
0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0
 220.  *   0.0   1.0   0.2   0.1   0.6   0.2   0.1   0.9   0.8   0.7   0.7   0.7
0.7   0.7   0.7   0.7   0.0   0.0   0.0   0.0
 230.  *   0.0   1.0   0.2   0.1   0.6   0.2   0.1   0.8   0.8   0.7   0.7   0.7
0.7   0.7   0.7   0.7   0.0   0.0   0.0   0.0
 240.  *   0.0   0.8   0.2   0.1   0.4   0.2   0.1   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.6   0.6   0.0   0.0   0.0   0.0
 250.  *   0.0   0.8   0.2   0.1   0.4   0.2   0.1   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.6   0.6   0.0   0.0   0.0   0.0
 260.  *   0.0   0.7   0.2   0.1   0.4   0.2   0.1   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.6   0.6   0.0   0.0   0.0   0.0
 270.  *   0.0   0.7   0.2   0.1   0.4   0.2   0.1   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.6   0.6   0.0   0.0   0.0   0.0
 280.  *   0.0   0.6   0.2   0.1   0.4   0.2   0.1   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.6   0.6   0.0   0.0   0.0   0.0
 290.  *   0.0   0.6   0.2   0.1   0.5   0.2   0.1   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.6   0.6   0.0   0.0   0.0   0.0
```

```
 300.  *    0.0   0.6   0.2   0.1   0.5   0.2   0.1   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.6   0.6   0.0   0.0   0.0   0.0
 310.  *    0.0   0.7   0.2   0.1   0.7   0.2   0.1   0.7   0.7   0.7   0.7   0.7
0.7   0.7   0.7   0.7   0.0   0.0   0.0   0.0
 320.  *    0.0   0.7   0.4   0.1   0.7   0.2   0.1   0.7   0.7   0.7   0.7   0.7
0.7   0.7   0.7   0.6   0.0   0.0   0.0   0.0
 330.  *    0.0   0.8   0.4   0.1   0.7   0.2   0.2   0.8   0.8   0.8   0.8   0.8
0.7   0.6   0.6   0.6   0.0   0.0   0.0   0.0
 340.  *    0.0   0.8   0.4   0.1   0.6   0.3   0.2   0.8   0.8   0.7   0.6   0.6
0.6   0.6   0.6   0.6   0.0   0.0   0.0   0.0
 350.  *    0.0   0.6   0.2   0.0   0.6   0.2   0.0   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.5   0.3   0.0   0.0   0.0   0.0

------*-----------------------------------------------------------------------------
------------------------------------------
 MAX   *    0.2   1.0   0.4   0.2   0.7   0.4   0.2   1.1   0.9   0.9   0.8   0.8
0.8   0.8   0.8   0.8   1.0   1.0   1.0   1.0
 DEGR. *    20    230   200   190   330   190   200   210   210   210   190   190
190   190   190   190   150   160   150   150

▯
                          PAGE 16
      JOB:                                                        RUN:


       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* RE161 RE162 RE163 RE164 RE165 RE166 RE167 RE168 RE169 RE170 RE171 RE172
RE173 RE174 RE175 RE176 RE177 RE178 RE179 RE180

------*-----------------------------------------------------------------------------
------------------------------------------
   0.  *    0.2   0.2   0.2   0.2   0.1   0.3   0.3   0.3   0.3   0.3   0.3   0.3
0.3   0.3   0.2   0.2   0.2   0.2   0.2   0.2
  10.  *    0.3   0.3   0.3   0.2   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.1   0.1   0.6   0.6   0.6   0.6   0.5   0.5
  20.  *    0.8   0.8   0.7   0.6   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.7   0.7   0.6   0.6
  30.  *    0.9   0.9   0.8   0.8   0.7   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.7   0.6   0.7   0.7
  40.  *    0.9   0.9   0.9   0.8   0.7   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.6   0.6   0.6   0.5   0.5   0.5
  50.  *    0.8   0.7   0.7   0.7   0.7   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.6   0.6   0.5   0.5   0.5   0.5
  60.  *    0.4   0.4   0.4   0.4   0.4   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.3   0.3   0.2   0.2   0.2   0.2
  70.  *    0.4   0.4   0.4   0.4   0.4   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.3   0.3   0.2   0.2   0.2   0.2
  80.  *    0.4   0.4   0.4   0.4   0.4   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.3   0.3   0.2   0.2   0.2   0.2
  90.  *    0.4   0.4   0.4   0.4   0.4   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.3   0.3   0.2   0.2   0.2   0.2
 100.  *    0.4   0.4   0.4   0.4   0.4   0.0   0.0   0.0   0.0   0.0   0.0   0.0
```

```
0.0   0.0   0.3   0.3   0.2   0.2   0.2   0.2
 110.  *   0.4   0.4   0.4   0.4   0.4   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.3   0.2   0.2   0.2   0.2   0.2
 120.  *   0.4   0.4   0.4   0.4   0.4   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.3   0.2   0.2   0.2   0.2   0.2
 130.  *   0.5   0.5   0.5   0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.4   0.3   0.3   0.3   0.3   0.3
 140.  *   0.9   0.9   0.9   0.9   0.9   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.6   0.5   0.5   0.5   0.5   0.5
 150.  *   1.0   1.0   1.0   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.7   0.7   0.7   0.7
 160.  *   1.0   1.0   1.0   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.7   0.7   0.7   0.7
 170.  *   0.7   0.8   0.9   0.9   0.9   0.1   0.1   0.1   0.1   0.1   0.1   0.1
0.1   0.1   0.7   0.7   0.7   0.7   0.7   0.7
 180.  *   0.5   0.5   0.5   0.5   0.5   0.4   0.4   0.4   0.4   0.4   0.4   0.4
0.4   0.4   0.3   0.3   0.3   0.3   0.3   0.3
 190.  *   0.1   0.1   0.1   0.1   0.1   0.6   0.6   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.1   0.1   0.1   0.1   0.1   0.1
 200.  *   0.0   0.0   0.0   0.0   0.0   0.6   0.6   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.0   0.0   0.0   0.0   0.0   0.0
 210.  *   0.0   0.0   0.0   0.0   0.0   0.6   0.6   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.0   0.0   0.0   0.0   0.0   0.0
 220.  *   0.0   0.0   0.0   0.0   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 230.  *   0.0   0.0   0.0   0.0   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 240.  *   0.0   0.0   0.0   0.0   0.0   0.4   0.3   0.3   0.3   0.3   0.3   0.3
0.3   0.3   0.0   0.0   0.0   0.0   0.0   0.0
 250.  *   0.0   0.0   0.0   0.0   0.0   0.4   0.3   0.3   0.3   0.3   0.3   0.3
0.3   0.3   0.0   0.0   0.0   0.0   0.0   0.0
 260.  *   0.0   0.0   0.0   0.0   0.0   0.4   0.3   0.3   0.3   0.3   0.3   0.3
0.3   0.3   0.0   0.0   0.0   0.0   0.0   0.0
 270.  *   0.0   0.0   0.0   0.0   0.0   0.4   0.3   0.3   0.3   0.3   0.3   0.3
0.3   0.3   0.0   0.0   0.0   0.0   0.0   0.0
 280.  *   0.0   0.0   0.0   0.0   0.0   0.4   0.3   0.3   0.3   0.3   0.3   0.3
0.3   0.3   0.0   0.0   0.0   0.0   0.0   0.0
 290.  *   0.0   0.0   0.0   0.0   0.0   0.4   0.3   0.3   0.3   0.3   0.3   0.3
0.3   0.3   0.0   0.0   0.0   0.0   0.0   0.0
 300.  *   0.0   0.0   0.0   0.0   0.0   0.4   0.4   0.3   0.3   0.3   0.3   0.3
0.3   0.3   0.0   0.0   0.0   0.0   0.0   0.0
 310.  *   0.0   0.0   0.0   0.0   0.0   0.6   0.6   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 320.  *   0.0   0.0   0.0   0.0   0.0   0.7   0.6   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 330.  *   0.0   0.0   0.0   0.0   0.0   0.8   0.7   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.0   0.0   0.0   0.0   0.0   0.0
 340.  *   0.0   0.0   0.0   0.0   0.0   0.7   0.6   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.0   0.0   0.0   0.0   0.0   0.0
 350.  *   0.0   0.0   0.0   0.0   0.0   0.6   0.6   0.6   0.5   0.5   0.5   0.5
0.5   0.6   0.0   0.0   0.0   0.1   0.1   0.1

------*------------------------------------------------------------------------------------
------------------------------------------
 MAX   *   1.0   1.0   1.0   1.0   1.0   0.8   0.7   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.7   0.7   0.7   0.7   0.7   0.7
 DEGR. *  160   160   160   160   160   330   330   190   190   190   190   190
190   190   170   170   170   170   170   170

                                PAGE 17
       JOB:                                                       RUN:
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```
        MODEL RESULTS
        -------------

        REMARKS : In search of the angle corresponding to
                  the maximum concentration, only the first
                  angle, of the angles with same maximum
                  concentrations, is indicated as maximum.

   WIND ANGLE RANGE:   0.-350.

   WIND   * CONCENTRATION
   ANGLE  *      (PPM)
   (DEGR)* RE181 RE182 RE183
   ------*-----------------
     0.  *   0.2   0.2   0.2
    10.  *   0.5   0.5   0.5
    20.  *   0.6   0.7   0.7
    30.  *   0.7   0.7   0.7
    40.  *   0.5   0.5   0.5
    50.  *   0.5   0.5   0.5
    60.  *   0.2   0.2   0.2
    70.  *   0.2   0.2   0.2
    80.  *   0.2   0.2   0.2
    90.  *   0.2   0.2   0.2
   100.  *   0.2   0.2   0.2
   110.  *   0.2   0.2   0.2
   120.  *   0.2   0.2   0.2
   130.  *   0.3   0.3   0.3
   140.  *   0.5   0.5   0.5
   150.  *   0.7   0.7   0.7
   160.  *   0.7   0.7   0.7
   170.  *   0.7   0.6   0.6
   180.  *   0.3   0.3   0.3
   190.  *   0.1   0.1   0.1
   200.  *   0.0   0.0   0.0
   210.  *   0.0   0.0   0.0
   220.  *   0.0   0.0   0.0
   230.  *   0.0   0.0   0.0
   240.  *   0.0   0.0   0.0
   250.  *   0.0   0.0   0.0
   260.  *   0.0   0.0   0.0
   270.  *   0.0   0.0   0.0
   280.  *   0.0   0.0   0.0
   290.  *   0.0   0.0   0.0
   300.  *   0.0   0.0   0.0
   310.  *   0.0   0.0   0.0
   320.  *   0.0   0.0   0.0
   330.  *   0.0   0.0   0.0
   340.  *   0.0   0.0   0.0
   350.  *   0.1   0.1   0.1
   ------*-----------------
   MAX   *   0.7   0.7   0.7
   DEGR. *   170   160   160

   THE HIGHEST CONCENTRATION OF    1.30 PPM OCCURRED AT RECEPTOR REC70.
```

BUILD CASE INPUT FILE

```
''  60.0  175.0  0.0  0.0  183  1  0  0  'PPM'
''  -102.42  23.12  1.8
''  -111.2  27.89  1.8
''  -119.99  32.67  1.8
''  -127.13  8.98  1.8
''  -118.32  4.25  1.8
''  -123.59  34.57  1.8
''  -131.78  40.31  1.8
''  -145.07  20.0  1.8
''  -136.86  14.29  1.8
''  -138.86  45.24  1.8
''  -146.62  51.55  1.8
''  -154.38  57.86  1.8
''  -170.14  39.36  1.8
''  -162.37  33.07  1.8
''  -154.6  26.77  1.8
''  -154.71  58.12  1.8
''  -162.43  64.48  1.8
''  -182.41  49.49  1.8
''  -174.7  43.12  1.8
''  -166.33  67.66  1.8
''  -173.39  74.74  1.8
''  -193.63  60.63  1.8
''  -186.55  53.57  1.8
''  -176.07  77.4  1.8
''  -182.71  84.88  1.8
''  -189.34  92.36  1.8
''  -195.98  99.84  1.8
''  -202.62  107.32  1.8
''  -218.82  88.98  1.8
''  -212.18  81.5  1.8
''  -205.54  74.02  1.8
''  -198.9  66.54  1.8
''  -79.93  15.06  1.8
''  -89.33  18.47  1.8
''  -98.74  21.88  1.8
''  -111.61  0.75  1.8
''  -102.16  -2.52  1.8
''  -92.71  -5.79  1.8
''  -83.26  -9.05  1.8
''  88.1  15.61  1.8
''  78.49  12.82  1.8
''  79.08  -11.86  1.8
''  88.75  -9.29  1.8
''  107.72  18.96  1.8
''  97.86  17.3  1.8
''  93.92  -7.88  1.8
''  103.78  -6.25  1.8
''  128.19  23.96  1.8
''  118.47  21.59  1.8
''  112.29  -4.83  1.8
''  122.01  -2.48  1.8
''  131.73  -0.13  1.8
''  140.44  31.02  1.8
''  131.69  26.19  1.8
''  135.72  1.08  1.8
''  144.56  5.76  1.8
''  163.8  43.4  1.8
''  154.96  38.72  1.8
''  146.12  34.04  1.8
''  152.07  9.73  1.8
''  160.9  14.41  1.8
''  169.74  19.09  1.8
```

```
''  178.58  23.77  1.8
''  -15.24  12.19  1.8
''  -25.24  12.19  1.8
''  -35.24  12.19  1.8
''  -45.24  12.19  1.8
''  -55.24  12.19  1.8
''  -65.24  12.19  1.8
''  -15.24  -12.19  1.8
''  -25.24  -12.19  1.8
''  -35.24  -12.19  1.8
''  -45.24  -12.19  1.8
''  -55.24  -12.19  1.8
''  -65.24  -12.19  1.8
''  15.24  12.19  1.8
''  25.24  12.19  1.8
''  35.24  12.19  1.8
''  45.24  12.19  1.8
''  55.24  12.19  1.8
''  65.24  12.19  1.8
''  15.24  -12.19  1.8
''  25.24  -12.19  1.8
''  35.24  -12.19  1.8
''  45.24  -12.19  1.8
''  55.24  -12.19  1.8
''  65.24  -12.19  1.8
''  -15.24  22.19  1.8
''  -25.24  22.19  1.8
''  -35.24  22.19  1.8
''  -45.24  22.19  1.8
''  -55.24  22.19  1.8
''  -65.24  22.19  1.8
''  -15.24  -22.19  1.8
''  -25.24  -22.19  1.8
''  -35.24  -22.19  1.8
''  -45.24  -22.19  1.8
''  -55.24  -22.19  1.8
''  -65.24  -22.19  1.8
''  15.24  22.19  1.8
''  25.24  22.19  1.8
''  35.24  22.19  1.8
''  45.24  22.19  1.8
''  55.24  22.19  1.8
''  65.24  22.19  1.8
''  15.24  -22.19  1.8
''  25.24  -22.19  1.8
''  35.24  -22.19  1.8
''  45.24  -22.19  1.8
''  55.24  -22.19  1.8
''  65.24  -22.19  1.8
''  -15.24  32.19  1.8
''  -25.24  32.19  1.8
''  -35.24  32.19  1.8
''  -45.24  32.19  1.8
''  -55.24  32.19  1.8
''  -65.24  32.19  1.8
''  -15.24  -32.19  1.8
''  -25.24  -32.19  1.8
''  -35.24  -32.19  1.8
''  -45.24  -32.19  1.8
''  -55.24  -32.19  1.8
''  -65.24  -32.19  1.8
''  15.24  32.19  1.8
''  25.24  32.19  1.8
```

```
''  35.24  32.19  1.8
''  45.24  32.19  1.8
''  55.24  32.19  1.8
''  65.24  32.19  1.8
''  15.24  -32.19  1.8
''  25.24  -32.19  1.8
''  35.24  -32.19  1.8
''  45.24  -32.19  1.8
''  55.24  -32.19  1.8
''  65.24  -32.19  1.8
''  -15.24  42.19  1.8
''  -25.24  42.19  1.8
''  -35.24  42.19  1.8
''  -15.24  -42.19  1.8
''  -25.24  -42.19  1.8
''  -35.24  -42.19  1.8
''  15.24  42.19  1.8
''  25.24  42.19  1.8
''  35.24  42.19  1.8
''  15.24  -42.19  1.8
''  25.24  -42.19  1.8
''  35.24  -42.19  1.8
''  15.24  52.19  1.8
''  15.24  62.19  1.8
''  15.24  72.19  1.8
''  15.24  82.19  1.8
''  15.24  92.19  1.8
''  15.24  102.19  1.8
''  15.24  112.19  1.8
''  15.24  122.19  1.8
''  15.24  132.19  1.8
''  -15.24  52.19  1.8
''  -15.24  62.19  1.8
''  -15.24  72.19  1.8
''  -15.24  82.19  1.8
''  -15.24  92.19  1.8
''  -15.24  102.19  1.8
''  -15.24  112.19  1.8
''  -15.24  122.19  1.8
''  -15.24  132.19  1.8
''  15.24  -52.19  1.8
''  15.24  -62.19  1.8
''  15.24  -72.19  1.8
''  15.24  -82.19  1.8
''  15.24  -92.19  1.8
''  15.24  -102.19  1.8
''  15.24  -112.19  1.8
''  15.24  -122.19  1.8
''  15.24  -132.19  1.8
''  -15.24  -52.19  1.8
''  -15.24  -62.19  1.8
''  -15.24  -72.19  1.8
''  -15.24  -82.19  1.8
''  -15.24  -92.19  1.8
''  -15.24  -102.19  1.8
''  -15.24  -112.19  1.8
''  -15.24  -122.19  1.8
''  -15.24  -132.19  1.8
''  88  1  0  'C'
1  1
''  'AG'  0.0  4.57  -73.15  4.57  451  4.24  0.0  9.14
1  1
''  'AG'  0.0  1.52  -73.15  1.52  791  4.24  0.0  9.14
```

```
1 1
'' 'AG'  0.0  -1.52  -73.15  -1.52  344  4.24  0.0  9.14
1 1
'' 'AG'  0.0  -4.57  -73.15  -4.57  497  4.24  0.0  9.14
1 1
'' 'AG'  -73.15  4.57  -106.07  16.5  451  4.24  0.0  9.14
1 1
'' 'AG'  -73.15  1.52  -107.09  13.63  791  4.24  0.0  9.14
1 1
'' 'AG'  -73.15  -1.52  -108.1  10.76  344  4.24  0.0  9.14
1 1
'' 'AG'  -73.15  -4.57  -109.12  7.88  497  4.24  0.0  9.14
1 1
'' 'AG'  -106.07  16.5  -127.98  28.41  451  4.24  0.0  9.14
1 1
'' 'AG'  -107.09  13.63  -129.42  25.72  791  4.24  0.0  9.14
1 1
'' 'AG'  -108.1  10.76  -130.87  23.04  344  4.24  0.0  9.14
1 1
'' 'AG'  -109.12  7.88  -132.32  20.36  497  4.24  0.0  9.14
1 1
'' 'AG'  -127.98  28.41  -143.69  39.41  451  4.24  0.0  9.14
1 1
'' 'AG'  -129.42  25.72  -145.43  36.91  791  4.24  0.0  9.14
1 1
'' 'AG'  -130.87  23.04  -147.18  34.41  344  4.24  0.0  9.14
1 1
'' 'AG'  -132.32  20.36  -148.92  31.91  497  4.24  0.0  9.14
1 1
'' 'AG'  -143.69  39.41  -159.58  52.32  451  4.24  0.0  9.14
1 1
'' 'AG'  -145.43  36.91  -161.5  49.95  791  4.24  0.0  9.14
1 1
'' 'AG'  -147.18  34.41  -163.42  47.58  344  4.24  0.0  9.14
1 1
'' 'AG'  -148.92  31.91  -165.34  45.22  497  4.24  0.0  9.14
1 1
'' 'AG'  -159.58  52.32  -171.74  62.35  451  4.24  0.0  9.14
1 1
'' 'AG'  -161.5  49.95  -173.68  60.0  791  4.24  0.0  9.14
1 1
'' 'AG'  -163.42  47.58  -175.62  57.65  344  4.24  0.0  9.14
1 1
'' 'AG'  -165.34  45.22  -177.56  55.3  497  4.24  0.0  9.14
1 1
'' 'AG'  -171.74  62.35  -181.78  72.42  451  4.24  0.0  9.14
1 1
'' 'AG'  -173.68  60.0  -183.94  70.27  791  4.24  0.0  9.14
1 1
'' 'AG'  -175.62  57.65  -186.09  68.11  344  4.24  0.0  9.14
1 1
'' 'AG'  -177.56  55.3  -188.25  65.96  497  4.24  0.0  9.14
1 1
'' 'AG'  -181.78  72.42  -325.76  234.68  451  4.24  0.0  9.14
1 1
'' 'AG'  -183.94  70.27  -328.04  232.66  791  4.24  0.0  9.14
1 1
'' 'AG'  -186.09  68.11  -330.32  230.64  344  4.24  0.0  9.14
1 1
'' 'AG'  -188.25  65.96  -332.6  228.61  497  4.24  0.0  9.14
1 1
'' 'AG'  0.0  4.57  77.11  4.57  496  4.24  0.0  9.14
1 1
```

```
''  'AG'  0.0  1.52  77.11  1.52  580  4.24  0.0  9.14
1, 1
''  'AG'  0.0  -1.52  77.11  -1.52  478  4.24  0.0  9.14
1, 1
''  'AG'  0.0  -4.57  77.11  -4.57  581  4.24  0.0  9.14
1, 1
''  'AG'  77.11  4.57  90.22  8.37  496  4.24  0.0  9.14
1, 1
''  'AG'  77.11  1.52  91.03  5.43  580  4.24  0.0  9.14
1, 1
''  'AG'  77.11  -1.52  91.85  2.49  478  4.24  0.0  9.14
1, 1
''  'AG'  77.11  -4.57  92.66  -0.44  581  4.24  0.0  9.14
1, 1
''  'AG'  90.22  8.37  108.98  11.52  496  4.24  0.0  9.14
1, 1
''  'AG'  91.03  5.43  109.48  8.51  580  4.24  0.0  9.14
1, 1
''  'AG'  91.85  2.49  109.98  5.51  478  4.24  0.0  9.14
1, 1
''  'AG'  92.66  -0.44  110.48  2.5  581  4.24  0.0  9.14
1, 1
''  'AG'  108.98  11.52  129.99  16.63  496  4.24  0.0  9.14
1, 1
''  'AG'  109.48  8.51  130.7  13.67  580  4.24  0.0  9.14
1, 1
''  'AG'  109.98  5.51  131.42  10.71  478  4.24  0.0  9.14
1, 1
''  'AG'  110.48  2.5  132.14  7.75  581  4.24  0.0  9.14
1, 1
''  'AG'  129.99  16.63  144.13  24.44  496  4.24  0.0  9.14
1, 1
''  'AG'  130.7  13.67  145.58  21.76  580  4.24  0.0  9.14
1, 1
''  'AG'  131.42  10.71  147.03  19.08  478  4.24  0.0  9.14
1, 1
''  'AG'  132.14  7.75  148.48  16.4  581  4.24  0.0  9.14
1, 1
''  'AG'  144.13  24.44  308.76  111.63  496  4.24  0.0  9.14
1, 1
''  'AG'  145.58  21.76  310.18  108.94  580  4.24  0.0  9.14
1, 1
''  'AG'  147.03  19.08  311.61  106.25  478  4.24  0.0  9.14
1, 1
''  'AG'  148.48  16.4  313.04  103.55  581  4.24  0.0  9.14
1, 1
''  'AG'  7.62  0.0  7.62  185.93  877  4.24  0.0  9.14
1, 1
''  'AG'  4.57  0.0  4.57  185.93  583  4.24  0.0  9.14
1, 1
''  'AG'  1.52  0.0  1.52  185.93  757  4.24  0.0  9.14
1, 1
''  'AG'  -1.52  0.0  -1.52  185.93  765  4.24  0.0  9.14
1, 1
''  'AG'  -4.57  0.0  -4.57  185.93  459  4.24  0.0  9.14
1, 1
''  'AG'  -7.62  0.0  -7.62  185.93  706  4.24  0.0  9.14
1, 1
''  'AG'  7.62  185.93  7.62  -447.14  994  4.24  0.0  9.14
1, 1
''  'AG'  4.57  185.93  4.57  -447.14  583  4.24  0.0  9.14
1, 1
''  'AG'  1.52  185.93  1.52  -447.14  1172  4.24  0.0  9.14
```

```
1  1
''  'AG'  -1.52  185.93  -1.52  -447.14  835  4.24  0.0  9.14
1  1
''  'AG'  -4.57  185.93  -4.57  -447.14  459  4.24  0.0  9.14
1  1
''  'AG'  -7.62  185.93  -7.62  -447.14  784  4.24  0.0  9.14
2  1
''  'AG'  -9.14  4.57  -73.15  4.57  0.0  3.05  1
90  40  2  451  28.88  1600  2  3
2  1
''  'AG'  -9.14  1.52  -73.15  1.52  0.0  3.05  1
90  40  2  791  28.88  1600  2  3
2  1
''  'AG'  -9.14  -1.52  -73.15  -1.52  0.0  3.05  1
90  40  2  344  28.88  1600  2  3
2  1
''  'AG'  -9.14  -4.57  -73.15  -4.57  0.0  3.05  1
90  40  2  497  28.88  1600  2  3
2  1
''  'AG'  9.14  4.57  77.11  4.57  0.0  3.05  1
90  40  2  496  28.88  1600  2  3
2  1
''  'AG'  9.14  1.52  77.11  1.52  0.0  3.05  1
90  40  2  580  28.88  1600  2  3
2  1
''  'AG'  9.14  -1.52  77.11  -1.52  0.0  3.05  1
90  40  2  478  28.88  1600  2  3
2  1
''  'AG'  9.14  -4.57  77.11  -4.57  0.0  3.05  1
90  40  2  581  28.88  1600  2  3
2  1
''  'AG'  7.62  6.1  7.62  185.93  0.0  3.05  1
90  40  2  877  28.88  1600  2  3
2  1
''  'AG'  4.57  6.1  4.57  185.93  0.0  3.05  1
90  40  2  583  28.88  1600  2  3
2  1
''  'AG'  1.52  6.1  1.52  185.93  0.0  3.05  1
90  40  2  757  28.88  1600  2  3
2  1
''  'AG'  -1.52  6.1  -1.52  185.93  0.0  3.05  1
90  40  2  765  28.88  1600  2  3
2  1
''  'AG'  -4.57  6.1  -4.57  185.93  0.0  3.05  1
90  40  2  459  28.88  1600  2  3
2  1
''  'AG'  -7.62  6.1  -7.62  185.93  0.0  3.05  1
90  40  2  706  28.88  1600  2  3
2  1
''  'AG'  7.62  -6.1  7.62  -447.14  0.0  3.05  1
90  40  2  994  28.88  1600  2  3
2  1
''  'AG'  4.57  -6.1  4.57  -447.14  0.0  3.05  1
90  40  2  583  28.88  1600  2  3
2  1
''  'AG'  1.52  -6.1  1.52  -447.14  0.0  3.05  1
90  40  2  1172  28.88  1600  2  3
2  1
''  'AG'  -1.52  -6.1  -1.52  -447.14  0.0  3.05  1
90  40  2  835  28.88  1600  2  3
2  1
''  'AG'  -4.57  -6.1  -4.57  -447.14  0.0  3.05  1
90  40  2  459  28.88  1600  2  3
```

```
2  1
''  'AG'  -7.62  -6.1  -7.62  -447.14  0.0  3.05  1
90  40  2  784  28.88  1600  2  3
1.0  0  4  1000.0  0.0  'Y'  10  0  35
** BREEZE
** PROJECTN  0 104 7 -177  0 0.9996 500000 0
** OUTFILE  "G:\EC\054401\0035\Modeling\Build Case (022305).lst"
** RAWFILE
```

BUILD CASE OUTPUT FILE

```
1                          CAL3QHC - (DATED 95221)

             CAL3QHC  PC  (32 BIT) VERSION  3.0.0
            (C) COPYRIGHT  1993-2000, TRINITY CONSULTANTS

 Run Began on  2/23/2005 at 16:59:34

     JOB:                                                         RUN:


     DATE : 02/23/   0
     TIME : 16:59:34

        The MODE flag has  been set to C for calculating CO  averages.

       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =   0.0 CM/S        VD =   0.0 CM/S       Z0 = 175.  CM
        U =  1.0 M/S          CLAS =   4   (D)     ATIM =  60.  MINUTES      MIXH  =
1000. M    AMB =  0.0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION      *        LINK COORDINATES (M)           *    LENGTH
BRG TYPE   VPH    EF       H   W    V/C QUEUE
                                *   X1          Y1         X2          Y2      *     (M)
(DEG)             (G/MI)    (M)  (M)       (VEH)

--------------------------*------------------------------------------*-----------
------------------------------------------------
       1.                       *      0.0        4.6      -73.2         4.6 *       73.
270. AG     451.    4.2    0.0  9.1
       2.                       *      0.0        1.5      -73.2         1.5 *       73.
270. AG     791.    4.2    0.0  9.1
       3.                       *      0.0       -1.5      -73.2        -1.5 *       73.
270. AG     344.    4.2    0.0  9.1
       4.                       *      0.0       -4.6      -73.2        -4.6 *       73.
270. AG     497.    4.2    0.0  9.1
       5.                       *    -73.2        4.6     -106.1        16.5 *       35.
290. AG     451.    4.2    0.0  9.1
       6.                       *    -73.2        1.5     -107.1        13.6 *       36.
290. AG     791.    4.2    0.0  9.1
       7.                       *    -73.2       -1.5     -108.1        10.8 *       37.
289. AG     344.    4.2    0.0  9.1
       8.                       *    -73.2       -4.6     -109.1         7.9 *       38.
289. AG     497.    4.2    0.0  9.1
       9.                       *   -106.1       16.5     -128.0        28.4 *       25.
299. AG     451.    4.2    0.0  9.1
      10.                       *   -107.1       13.6     -129.4        25.7 *       25.
298. AG     791.    4.2    0.0  9.1
      11.                       *   -108.1       10.8     -130.9        23.0 *       26.
298. AG     344.    4.2    0.0  9.1
      12.                       *   -109.1        7.9     -132.3        20.4 *       26.
298. AG     497.    4.2    0.0  9.1
      13.                       *   -128.0       28.4     -143.7        39.4 *       19.
305. AG     451.    4.2    0.0  9.1
      14.                       *   -129.4       25.7     -145.4        36.9 *       20.
305. AG     791.    4.2    0.0  9.1
      15.                       *   -130.9       23.0     -147.2        34.4 *       20.
305. AG     344.    4.2    0.0  9.1
      16.                       *   -132.3       20.4     -148.9        31.9 *       20.
305. AG     497.    4.2    0.0  9.1
      17.                       *   -143.7       39.4     -159.6        52.3 *       20.
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309. AG    451.   4.2    0.0  9.1
            18.                 *   -145.4       36.9    -161.5       50.0 *      21.
309. AG    791.   4.2    0.0  9.1
            19.                 *   -147.2       34.4    -163.4       47.6 *      21.
309. AG    344.   4.2    0.0  9.1
            20.                 *   -148.9       31.9    -165.3       45.2 *      21.
309. AG    497.   4.2    0.0  9.1
            21.                 *   -159.6       52.3    -171.7       62.3 *      16.
310. AG    451.   4.2    0.0  9.1
            22.                 *   -161.5       50.0    -173.7       60.0 *      16.
310. AG    791.   4.2    0.0  9.1
            23.                 *   -163.4       47.6    -175.6       57.7 *      16.
310. AG    344.   4.2    0.0  9.1
            24.                 *   -165.3       45.2    -177.6       55.3 *      16.
310. AG    497.   4.2    0.0  9.1
            25.                 *   -171.7       62.3    -181.8       72.4 *      14.
315. AG    451.   4.2    0.0  9.1
            26.                 *   -173.7       60.0    -183.9       70.3 *      15.
315. AG    791.   4.2    0.0  9.1
            27.                 *   -175.6       57.7    -186.1       68.1 *      15.
315. AG    344.   4.2    0.0  9.1
            28.                 *   -177.6       55.3    -188.2       66.0 *      15.
315. AG    497.   4.2    0.0  9.1
            29.                 *   -181.8       72.4    -325.8      234.7 *    2 17.
318. AG    451.   4.2    0.0  9.1
            30.                 *   -183.9       70.3    -328.0      232.7 *    2 17.
318. AG    791.   4.2    0.0  9.1
            31.                 *   -186.1       68.1    -330.3      230.6 *    2 17.
318. AG    344.   4.2    0.0  9.1
            32.                 *   -188.2       66.0    -332.6      228.6 *    2 17.
318. AG    497.   4.2    0.0  9.1
            33.                 *      0.0        4.6      77.1        4.6 *      77.
90. AG    496.   4.2   0.0   9.1
            34.                 *      0.0        1.5      77.1        1.5 *      77.
90. AG    580.   4.2   0.0   9.1
            35.                 *      0.0       -1.5      77.1       -1.5 *      77.
90. AG    478.   4.2   0.0   9.1
            36.                 *      0.0       -4.6      77.1       -4.6 *      77.
90. AG    581.   4.2   0.0   9.1
            37.                 *     77.1        4.6      90.2        8.4 *      14.
74. AG    496.   4.2   0.0   9.1
            38.                 *     77.1        1.5      91.0        5.4 *      14.
74. AG    580.   4.2   0.0   9.1
            39.                 *     77.1       -1.5      91.8        2.5 *      15.
75. AG    478.   4.2   0.0   9.1
            40.                 *     77.1       -4.6      92.7       -0.4 *      16.
75. AG    581.   4.2   0.0   9.1
            41.                 *     90.2        8.4     109.0       11.5 *      19.
80. AG    496.   4.2   0.0   9.1
            42.                 *     91.0        5.4     109.5        8.5 *      19.
81. AG    580.   4.2   0.0   9.1
            43.                 *     91.8        2.5     110.0        5.5 *      18.
81. AG    478.   4.2   0.0   9.1
            44.                 *     92.7       -0.4     110.5        2.5 *      18.
81. AG    581.   4.2   0.0   9.1

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       JOB:                                               RUN:


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      LINK VARIABLES
      --------------
        LINK DESCRIPTION        *        LINK COORDINATES (M)          *    LENGTH
BRG TYPE  VPH    EF       H     W    V/C QUEUE
                                *  X1          Y1         X2          Y2     *     (M)
(DEG)           (G/MI)   (M)   (M)       (VEH)
------------------------------------*- --------------------------------------------- -----*------------------ ------
------------------------------------------------------
       45.                      *  109.0       11.5      130.0       16.6 *       22.
76. AG    496.    4.2     0.0   9.1
       46.                      *  109.5        8.5      130.7       13.7 *       22.
76. AG    580.    4.2     0.0   9.1
       47.                      *  110.0        5.5      131.4       10.7 *       22.
76. AG    478.    4.2     0.0   9.1
       48.                      *  110.5        2.5      132.1        7.8 *       22.
76. AG    581.    4.2     0.0   9.1
       49.                      *  130.0       16.6      144.1       24.4 *       16.
61. AG    496.    4.2     0.0   9.1
       50.                      *  130.7       13.7      145.6       21.8 *       17.
61. AG    580.    4.2     0.0   9.1
       51.                      *  131.4       10.7      147.0       19.1 *       18.
62. AG    478.    4.2     0.0   9.1
       52.                      *  132.1        7.8      148.5       16.4 *       18.
62. AG    581.    4.2     0.0   9.1
       53.                      *  144.1       24.4      308.8      111.6 *      186.
62. AG    496.    4.2     0.0   9.1
       54.                      *  145.6       21.8      310.2      108.9 *      186.
62. AG    580.    4.2     0.0   9.1
       55.                      *  147.0       19.1      311.6      106.2 *      186.
62. AG    478.    4.2     0.0   9.1
       56.                      *  148.5       16.4      313.0      103.6 *      186.
62. AG    581.    4.2     0.0   9.1
       57.                      *    7.6        0.0        7.6      185.9 *      186.
360. AG    877.    4.2    0.0   9.1
       58.                      *    4.6        0.0        4.6      185.9 *      186.
360. AG    583.    4.2    0.0   9.1
       59.                      *    1.5        0.0        1.5      185.9 *      186.
360. AG    757.    4.2    0.0   9.1
       60.                      *   -1.5        0.0       -1.5      185.9 *      186.
360. AG    765.    4.2    0.0   9.1
       61.                      *   -4.6        0.0       -4.6      185.9 *      186.
360. AG    459.    4.2    0.0   9.1
       62.                      *   -7.6        0.0       -7.6      185.9 *      186.
360. AG    706.    4.2    0.0   9.1
       63.                      *    7.6      185.9        7.6     -447.1 *      633.
180. AG    994.    4.2    0.0   9.1
       64.                      *    4.6      185.9        4.6     -447.1 *      633.
180. AG    583.    4.2    0.0   9.1
       65.                      *    1.5      185.9        1.5     -447.1 *      633.
180. AG   1172.    4.2    0.0   9.1
       66.                      *   -1.5      185.9       -1.5     -447.1 *      633.
180. AG    835.    4.2    0.0   9.1
       67.                      *   -4.6      185.9       -4.6     -447.1 *      633.
180. AG    459.    4.2    0.0   9.1
       68.                      *   -7.6      185.9       -7.6     -447.1 *      633.
180. AG    784.    4.2    0.0   9.1
       69.                      *   -9.1        4.6      -39.2        4.6 *       30.
270. AG     34.  100.0    0.0   3.0 0.55    5.0
       70.                      *   -9.1        1.5      -82.7        1.5 *       74.
270. AG     34.  100.0    0.0   3.0 0.97   12.3
       71.                      *   -9.1       -1.5      -32.1       -1.5 *       23.
270. AG     34.  100.0    0.0   3.0 0.42    3.8
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      72.                          *     -9.1       -4.6      -42.3       -4.6 *       33.
270. AG      34. 100.0   0.0  3.0 0.61   5.5
      73.                          *      9.1        4.6       42.2        4.6 *       33.
90. AG      34. 100.0   0.0   3.0 0.61   5.5
      74.                          *      9.1        1.5       47.8        1.5 *       39.
90. AG      34. 100.0   0.0   3.0 0.71   6.4
      75.                          *      9.1       -1.5       41.0       -1.5 *       32.
90. AG      34. 100.0   0.0   3.0 0.59   5.3
      76.                          *      9.1       -4.6       47.9       -4.6 *       39.
90. AG      34. 100.0   0.0   3.0 0.71   6.5
      77.                          *      7.6        6.1        7.6      279.0 *      2 73.
360. AG      34. 100.0   0.0  3.0 1.07  45.5
      78.                          *      4.6        6.1        4.6       45.0 *       39.
360. AG      34. 100.0   0.0  3.0 0.71   6.5
      79.                          *      1.5        6.1        1.5       67.3 *       61.
360. AG      34. 100.0   0.0  3.0 0.93  10.2
      80.                          *     -1.5        6.1       -1.5       69.8 *       64.
360. AG      34. 100.0   0.0  3.0 0.94  10.6
      81.                          *     -4.6        6.1       -4.6       36.7 *       31.
360. AG      34. 100.0   0.0  3.0 0.56   5.1
      82.                          *     -7.6        6.1       -7.6       55.3 *       49.
360. AG      34. 100.0   0.0  3.0 0.86   8.2
      83.                          *      7.6       -6.1        7.6     -642.4 *      6 36.
180. AG      34. 100.0   0.0  3.0 1.22 106.0
      84.                          *      4.6       -6.1        4.6      -45.0 *       39.
180. AG      34. 100.0   0.0  3.0 0.71   6.5
      85.                          *      1.5       -6.1        1.5    -1195.2 *     11 89.
180. AG      34. 100.0   0.0  3.0 1.43 198.2
      86.                          *     -1.5       -6.1       -1.5     -148.5 *      1 42.
180. AG      34. 100.0   0.0  3.0 1.02  23.7
      87.                          *     -4.6       -6.1       -4.6      -36.7 *       31.
180. AG      34. 100.0   0.0  3.0 0.56   5.1
      88.                          *     -7.6       -6.1       -7.6      -76.7 *       71.
180. AG      34. 100.0   0.0  3.0 0.96  11.8
▯
                          PAGE  3
      JOB:                                                          RUN:


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       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION          *    CYCLE      RED      CLEARANCE   APPROACH   SATURATION
 IDLE    SIGNAL    ARRIVAL
                                   *    LENGTH     TIME     LOST TIME     VOL      FLOW RATE
EM FAC    TYPE      RATE
                                   *     (SEC)     (SEC)      (SEC)      (VPH)      (VPH)
(gm/hr)

--------------------------*----------------------------------------------------------------
-----------------------
      69.                          *      90        40        2.0        451        1600
28.88       2         3
      70.                          *      90        40        2.0        791        1600
28.88       2         3
      71.                          *      90        40        2.0        344        1600
28.88       2         3
      72.                          *      90        40        2.0        497        1600
28.88       2         3
      73.                          *      90        40        2.0        496        1600
28.88       2         3
```

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        74.                        *      90       40       2.0        580       160 0
28.88          2          3
        75.                        *      90       40       2.0        478       160 0
28.88          2          3
        76.                        *      90       40       2.0        581       160 0
28.88          2          3
        77.                        *      90       40       2.0        877       160 0
28.88          2          3
        78.                        *      90       40       2.0        583       160 0
28.88          2          3
        79.                        *      90       40       2.0        757       160 0
28.88          2          3
        80.                        *      90       40       2.0        765       160 0
28.88          2          3
        81.                        *      90       40       2.0        459       160 0
28.88          2          3
        82.                        *      90       40       2.0        706       160 0
28.88          2          3
        83.                        *      90       40       2.0        994       160 0
28.88          2          3
        84.                        *      90       40       2.0        583       160 0
28.88          2          3
        85.                        *      90       40       2.0       1172       160 0
28.88          2          3
        86.                        *      90       40       2.0        835       160 0
28.88          2          3
        87.                        *      90       40       2.0        459       160 0
28.88          2          3
        88.                        *      90       40       2.0        784       160 0
28.88          2          3

        RECEPTOR LOCATIONS
        ------------------
                                   *        COORDINATES (M)         *
          RECEPTOR                 *      X           Y         Z   *
       ----------------------------*------------------------------- *
       1.                          *    -102.4       23.1       1.8 *
       2.                          *    -111.2       27.9       1.8 *
       3.                          *    -120.0       32.7       1.8 *
       4.                          *    -127.1        9.0       1.8 *
       5.                          *    -118.3        4.2       1.8 *
       6.                          *    -123.6       34.6       1.8 *
       7.                          *    -131.8       40.3       1.8 *
       8.                          *    -145.1       20.0       1.8 *
       9.                          *    -136.9       14.3       1.8 *
      10.                          *    -138.9       45.2       1.8 *
      11.                          *    -146.6       51.5       1.8 *
      12.                          *    -154.4       57.9       1.8 *
      13.                          *    -170.1       39.4       1.8 *
      14.                          *    -162.4       33.1       1.8 *
      15.                          *    -154.6       26.8       1.8 *
      16.                          *    -154.7       58.1       1.8 *
      17.                          *    -162.4       64.5       1.8 *
      18.                          *    -182.4       49.5       1.8 *
      19.                          *    -174.7       43.1       1.8 *
      20.                          *    -166.3       67.7       1.8 *
      21.                          *    -173.4       74.7       1.8 *
      22.                          *    -193.6       60.6       1.8 *
      23.                          *    -186.6       53.6       1.8 *
      24.                          *    -176.1       77.4       1.8 *
      25.                          *    -182.7       84.9       1.8 *
```

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JOB:                                                        RUN:


DATE : 02/23/   0
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 RECEPTOR LOCATIONS
 ------------------
                               *             COORDINATES (M)              *
    RECEPTOR                   *       X            Y             Z       *
-------------------------------*------------------------------------------*
26.                            *     -189.3        92.4          1.8      *
27.                            *     -196.0        99.8          1.8      *
28.                            *     -202.6       107.3          1.8      *
29.                            *     -218.8        89.0          1.8      *
30.                            *     -212.2        81.5          1.8      *
31.                            *     -205.5        74.0          1.8      *
32.                            *     -198.9        66.5          1.8      *
33.                            *      -79.9        15.1          1.8      *
34.                            *      -89.3        18.5          1.8      *
35.                            *      -98.7        21.9          1.8      *
36.                            *     -111.6         0.8          1.8      *
37.                            *     -102.2        -2.5          1.8      *
38.                            *      -92.7        -5.8          1.8      *
39.                            *      -83.3        -9.1          1.8      *
40.                            *       88.1        15.6          1.8      *
41.                            *       78.5        12.8          1.8      *
42.                            *       79.1       -11.9          1.8      *
43.                            *       88.7        -9.3          1.8      *
44.                            *      107.7        19.0          1.8      *
45.                            *       97.9        17.3          1.8      *
46.                            *       93.9        -7.9          1.8      *
47.                            *      103.8        -6.2          1.8      *
48.                            *      128.2        24.0          1.8      *
49.                            *      118.5        21.6          1.8      *
50.                            *      112.3        -4.8          1.8      *
51.                            *      122.0        -2.5          1.8      *
52.                            *      131.7        -0.1          1.8      *
53.                            *      140.4        31.0          1.8      *
54.                            *      131.7        26.2          1.8      *
55.                            *      135.7         1.1          1.8      *
56.                            *      144.6         5.8          1.8      *
57.                            *      163.8        43.4          1.8      *
58.                            *      155.0        38.7          1.8      *
59.                            *      146.1        34.0          1.8      *
60.                            *      152.1         9.7          1.8      *
61.                            *      160.9        14.4          1.8      *
62.                            *      169.7        19.1          1.8      *
63.                            *      178.6        23.8          1.8      *
64.                            *      -15.2        12.2          1.8      *
65.                            *      -25.2        12.2          1.8      *
66.                            *      -35.2        12.2          1.8      *
67.                            *      -45.2        12.2          1.8      *
68.                            *      -55.2        12.2          1.8      *
69.                            *      -65.2        12.2          1.8      *
70.                            *      -15.2       -12.2          1.8      *
71.                            *      -25.2       -12.2          1.8      *
72.                            *      -35.2       -12.2          1.8      *
73.                            *      -45.2       -12.2          1.8      *
74.                            *      -55.2       -12.2          1.8      *
75.                            *      -65.2       -12.2          1.8      *
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                              PAGE  5
 JOB:                                                      RUN:

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  RECEPTOR LOCATIONS
  ------------------
                               *          COORDINATES (M)          *
    RECEPTOR                   *      X          Y           Z      *
 ------------------------------*-------------------------------------*
 76.                           *      15.2       12.2        1.8   *
 77.                           *      25.2       12.2        1.8   *
 78.                           *      35.2       12.2        1.8   *
 79.                           *      45.2       12.2        1.8   *
 80.                           *      55.2       12.2        1.8   *
 81.                           *      65.2       12.2        1.8   *
 82.                           *      15.2      -12.2        1.8   *
 83.                           *      25.2      -12.2        1.8   *
 84.                           *      35.2      -12.2        1.8   *
 85.                           *      45.2      -12.2        1.8   *
 86.                           *      55.2      -12.2        1.8   *
 87.                           *      65.2      -12.2        1.8   *
 88.                           *     -15.2       22.2        1.8   *
 89.                           *     -25.2       22.2        1.8   *
 90.                           *     -35.2       22.2        1.8   *
 91.                           *     -45.2       22.2        1.8   *
 92.                           *     -55.2       22.2        1.8   *
 93.                           *     -65.2       22.2        1.8   *
 94.                           *     -15.2      -22.2        1.8   *
 95.                           *     -25.2      -22.2        1.8   *
 96.                           *     -35.2      -22.2        1.8   *
 97.                           *     -45.2      -22.2        1.8   *
 98.                           *     -55.2      -22.2        1.8   *
 99.                           *     -65.2      -22.2        1.8   *
100.                           *      15.2       22.2        1.8   *
101.                           *      25.2       22.2        1.8   *
102.                           *      35.2       22.2        1.8   *
103.                           *      45.2       22.2        1.8   *
104.                           *      55.2       22.2        1.8   *
105.                           *      65.2       22.2        1.8   *
106.                           *      15.2      -22.2        1.8   *
107.                           *      25.2      -22.2        1.8   *
108.                           *      35.2      -22.2        1.8   *
109.                           *      45.2      -22.2        1.8   *
110.                           *      55.2      -22.2        1.8   *
111.                           *      65.2      -22.2        1.8   *
112.                           *     -15.2       32.2        1.8   *
113.                           *     -25.2       32.2        1.8   *
114.                           *     -35.2       32.2        1.8   *
115.                           *     -45.2       32.2        1.8   *
116.                           *     -55.2       32.2        1.8   *
117.                           *     -65.2       32.2        1.8   *
118.                           *     -15.2      -32.2        1.8   *
119.                           *     -25.2      -32.2        1.8   *
120.                           *     -35.2      -32.2        1.8   *
121.                           *     -45.2      -32.2        1.8   *
122.                           *     -55.2      -32.2        1.8   *
123.                           *     -65.2      -32.2        1.8   *
124.                           *      15.2       32.2        1.8   *
125.                           *      25.2       32.2        1.8   *
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                           PAGE  6
 JOB:                                                  RUN:


 DATE : 02/23/   0
 TIME : 16:59:34

  RECEPTOR LOCATIONS
  ------------------
                                  *           COORDINATES (M)           *
    RECEPTOR                      *       X          Y          Z       *
 ---------------------------- ----*----------- ---------------- --------*
126.                              *     35.2       32.2        1.8     *
127.                              *     45.2       32.2        1.8     *
128.                              *     55.2       32.2        1.8     *
129.                              *     65.2       32.2        1.8     *
130.                              *     15.2      -32.2        1.8     *
131.                              *     25.2      -32.2        1.8     *
132.                              *     35.2      -32.2        1.8     *
133.                              *     45.2      -32.2        1.8     *
134.                              *     55.2      -32.2        1.8     *
135.                              *     65.2      -32.2        1.8     *
136.                              *    -15.2       42.2        1.8     *
137.                              *    -25.2       42.2        1.8     *
138.                              *    -35.2       42.2        1.8     *
139.                              *    -15.2      -42.2        1.8     *
140.                              *    -25.2      -42.2        1.8     *
141.                              *    -35.2      -42.2        1.8     *
142.                              *     15.2       42.2        1.8     *
143.                              *     25.2       42.2        1.8     *
144.                              *     35.2       42.2        1.8     *
145.                              *     15.2      -42.2        1.8     *
146.                              *     25.2      -42.2        1.8     *
147.                              *     35.2      -42.2        1.8     *
148.                              *     15.2       52.2        1.8     *
149.                              *     15.2       62.2        1.8     *
150.                              *     15.2       72.2        1.8     *
151.                              *     15.2       82.2        1.8     *
152.                              *     15.2       92.2        1.8     *
153.                              *     15.2      102.2        1.8     *
154.                              *     15.2      112.2        1.8     *
155.                              *     15.2      122.2        1.8     *
156.                              *     15.2      132.2        1.8     *
157.                              *    -15.2       52.2        1.8     *
158.                              *    -15.2       62.2        1.8     *
159.                              *    -15.2       72.2        1.8     *
160.                              *    -15.2       82.2        1.8     *
161.                              *    -15.2       92.2        1.8     *
162.                              *    -15.2      102.2        1.8     *
163.                              *    -15.2      112.2        1.8     *
164.                              *    -15.2      122.2        1.8     *
165.                              *    -15.2      132.2        1.8     *
166.                              *     15.2      -52.2        1.8     *
167.                              *     15.2      -62.2        1.8     *
168.                              *     15.2      -72.2        1.8     *
169.                              *     15.2      -82.2        1.8     *
170.                              *     15.2      -92.2        1.8     *
171.                              *     15.2     -102.2        1.8     *
172.                              *     15.2     -112.2        1.8     *
173.                              *     15.2     -122.2        1.8     *
174.                              *     15.2     -132.2        1.8     *
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   175.                               *        -15.2       -52.2        1.8    *

                               PAGE  7
     JOB:                                                          RUN:


     DATE : 02/23/   0
     TIME : 16:59:34


      RECEPTOR LOCATIONS
      ------------------
                                      *           COORDINATES (M)            *
         RECEPTOR                     *      X           Y          Z        *
   -------------------------------*-----------------------------------------*
   176.                               *      -15.2       -62.2        1.8    *
   177.                               *      -15.2       -72.2        1.8    *
   178.                               *      -15.2       -82.2        1.8    *
   179.                               *      -15.2       -92.2        1.8    *
   180.                               *      -15.2      -102.2        1.8    *
   181.                               *      -15.2      -112.2        1.8    *
   182.                               *      -15.2      -122.2        1.8    *
   183.                               *      -15.2      -132.2        1.8    *

                               PAGE  8
     JOB:                                                          RUN:


      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND   * CONCENTRATION
 ANGLE  *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12
REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

------*-------------------------------------------------------------------------
-------------------------------------------
   0.  *   0.0   0.0   0.0   0.1   0.2   0.0   0.0   0.1   0.2   0.0   0.0   0.0
0.2   0.1   0.2   0.0   0.0   0.1   0.1   0.0
  10.  *   0.0   0.0   0.0   0.2   0.2   0.0   0.0   0.2   0.2   0.0   0.0   0.0
0.2   0.1   0.2   0.0   0.0   0.2   0.1   0.0
  20.  *   0.0   0.0   0.0   0.2   0.2   0.0   0.0   0.2   0.1   0.0   0.0   0.0
0.1   0.2   0.2   0.0   0.0   0.2   0.2   0.0
  30.  *   0.0   0.0   0.0   0.2   0.2   0.0   0.0   0.2   0.0   0.0   0.0   0.0
0.0   0.2   0.1   0.0   0.0   0.0   0.2   0.0
  40.  *   0.0   0.0   0.0   0.2   0.2   0.0   0.0   0.2   0.0   0.0   0.0   0.0
0.0   0.2   0.0   0.0   0.0   0.0   0.2   0.0
  50.  *   0.0   0.0   0.0   0.2   0.1   0.0   0.0   0.2   0.1   0.0   0.0   0.0
0.1   0.2   0.0   0.0   0.0   0.0   0.2   0.0
  60.  *   0.0   0.0   0.0   0.2   0.1   0.0   0.0   0.2   0.2   0.0   0.0   0.0
0.2   0.2   0.1   0.0   0.0   0.1   0.1   0.0
  70.  *   0.0   0.0   0.0   0.2   0.1   0.0   0.0   0.1   0.2   0.0   0.0   0.0
0.2   0.1   0.2   0.0   0.0   0.2   0.0   0.0
  80.  *   0.0   0.0   0.0   0.1   0.2   0.0   0.0   0.2   0.2   0.0   0.0   0.0
0.2   0.1   0.2   0.0   0.0   0.2   0.1   0.0
```

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  90.  *    0.0    0.0    0.0    0.2    0.2    0. 0    0.0    0.1    0 .1    0.0    0.0    0 .0
0.2   0.0    0.1    0.0    0. 0    0.1    0.1    0 .0
 100.  *    0.0    0.0    0.0    0.0    0.1    0. 0    0.0    0.0    0 .1    0.0    0.0    0 .0
0.1   0.0    0.1    0.0    0. 0    0.1    0.1    0 .0
 110.  *    0.0    0.0    0.0    0.0    0.0    0. 0    0.0    0.0    0 .0    0.0    0.0    0 .0
0.1   0.0    0.0    0.0    0. 0    0.0    0.0    0 .0
 120.  *    0.0    0.0    0.0    0.0    0.0    0. 0    0.0    0.0    0 .0    0.0    0.0    0 .0
0.0   0.0    0.0    0.0    0. 0    0.0    0.0    0 .0
 130.  *    0.2    0.1    0.0    0.0    0.0    0. 0    0.0    0.0    0 .0    0.0    0.0    0 .0
0.0   0.0    0.0    0.0    0. 0    0.0    0.0    0 .0
 140.  *    0.2    0.1    0.0    0.0    0.0    0. 2    0.1    0.0    0 .0    0.0    0.0    0 .0
0.0   0.0    0.0    0.0    0. 0    0.0    0.0    0 .0
 150.  *    0.2    0.1    0.2    0.0    0.0    0. 2    0.1    0.0    0 .0    0.0    0.1    0 .0
0.0   0.0    0.0    0.0    0. 1    0.0    0.0    0 .0
 160.  *    0.2    0.0    0.2    0.0    0.0    0. 2    0.1    0.0    0 .0    0.2    0.1    0 .2
0.0   0.0    0.0    0.2    0. 1    0.0    0.0    0 .0
 170.  *    0.2    0.1    0.2    0.0    0.0    0. 2    0.0    0.0    0 .0    0.2    0.0    0 .2
0.0   0.0    0.0    0.2    0. 0    0.0    0.0    0 .2
 180.  *    0.2    0.2    0.2    0.0    0.0    0. 2    0.1    0.0    0 .0    0.2    0.1    0 .2
0.0   0.0    0.0    0.2    0. 1    0.0    0.0    0 .2
 190.  *    0.1    0.2    0.2    0.0    0.0    0. 1    0.2    0.0    0 .0    0.2    0.2    0 .2
0.0   0.0    0.0    0.2    0. 2    0.0    0.0    0 .2
 200.  *    0.1    0.2    0.2    0.0    0.0    0. 1    0.2    0.0    0 .0    0.1    0.2    0 .1
0.0   0.0    0.0    0.1    0. 2    0.0    0.0    0 .1
 210.  *    0.0    0.2    0.2    0.0    0.0    0. 0    0.2    0.0    0 .0    0.1    0.2    0 .1
0.0   0.0    0.0    0.1    0. 2    0.0    0.0    0 .1
 220.  *    0.1    0.2    0.1    0.0    0.0    0. 1    0.2    0.0    0 .0    0.0    0.2    0 .0
0.0   0.0    0.0    0.0    0. 2    0.0    0.0    0 .0
 230.  *    0.1    0.2    0.0    0.0    0.0    0. 1    0.2    0.0    0 .0    0.1    0.2    0 .1
0.0   0.0    0.0    0.1    0. 2    0.0    0.0    0 .1
 240.  *    0.2    0.2    0.1    0.0    0.0    0. 1    0.2    0.0    0 .0    0.1    0.2    0 .1
0.0   0.0    0.0    0.1    0. 1    0.0    0.0    0 .1
 250.  *    0.2    0.2    0.1    0.0    0.0    0. 2    0.1    0.0    0 .0    0.2    0.2    0 .2
0.0   0.0    0.0    0.2    0. 0    0.0    0.0    0 .1
 260.  *    0.2    0.2    0.1    0.0    0.0    0. 2    0.0    0.0    0 .0    0.2    0.1    0 .2
0.0   0.0    0.0    0.2    0. 1    0.0    0.0    0 .2
 270.  *    0.2    0.0    0.1    0.0    0.0    0. 2    0.1    0.0    0 .0    0.2    0.0    0 .2
0.0   0.0    0.0    0.2    0. 1    0.0    0.0    0 .2
 280.  *    0.1    0.0    0.1    0.0    0.0    0. 0    0.1    0.0    0 .0    0.2    0.0    0 .0
0.0   0.0    0.0    0.0    0. 1    0.0    0.0    0 .0
 290.  *    0.0    0.0    0.0    0.0    0.0    0. 0    0.0    0.0    0 .0    0.0    0.0    0 .0
0.0   0.0    0.0    0.0    0. 1    0.0    0.0    0 .1
 300.  *    0.0    0.0    0.0    0.0    0.0    0. 0    0.0    0.0    0 .0    0.0    0.1    0 .1
0.0   0.0    0.0    0.1    0. 1    0.0    0.0    0 .2
 310.  *    0.0    0.0    0.0    0.0    0.0    0. 0    0.0    0.0    0 .0    0.1    0.1    0 .1
0.0   0.0    0.0    0.1    0. 2    0.0    0.0    0 .2
 320.  *    0.0    0.0    0.0    0.0    0.1    0. 0    0.0    0.0    0 .0    0.0    0.0    0 .0
0.1   0.1    0.1    0.0    0. 1    0.2    0.2    0 .1
 330.  *    0.0    0.0    0.0    0.0    0.1    0. 0    0.0    0.0    0 .1    0.0    0.0    0 .0
0.1   0.1    0.1    0.0    0. 0    0.2    0.1    0 .0
 340.  *    0.0    0.0    0.0    0.0    0.2    0. 0    0.0    0.1    0 .1    0.0    0.0    0 .0
0.1   0.0    0.1    0.0    0. 0    0.1    0.1    0 .0
 350.  *    0.0    0.0    0.0    0.1    0.2    0. 0    0.0    0.0    0 .2    0.0    0.0    0 .0
0.1   0.0    0.2    0.0    0. 0    0.2    0.0    0 .0

------*----------------- ----------------- ----------------- ----------------- ------
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 MAX   *    0.2    0.2    0.2    0.2    0.2    0. 2    0.2    0.2    0 .2    0.2    0.2    0 .2
0.2   0.2    0.2    0.2    0. 2    0.2    0.2    0 .2
 DEGR. *   130    180    150     10      0    140    190     10       0    160    190    16 0
0     20      0    160    190     10     20    170

▯
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                              PAGE  9
      JOB:                                                          RUN:


        MODEL RESULTS
        -------------

        REMARKS : In search of the angle corresponding to
                  the maximum concentration, only the first
                  angle, of the angles with same maximum
                  concentrations, is indicated as maximum.

    WIND ANGLE RANGE:   0.-350.

    WIND   *  CONCENTRATION
    ANGLE *       (PPM)
    (DEGR)*  REC21 REC22 REC23  REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32
   REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
   ------*------------------------------------------------------------------------------
   ------------------------------------------------
     0.  *   0.0   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
   0.0   0.0   0.0   0.2   0.2   0.2   0.2   0.0
    10.  *   0.0   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.0
    20.  *   0.0   0.2   0.2   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.0
    30.  *   0.0   0.1   0.2   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
   0.0   0.0   0.0   0.1   0.2   0.2   0.3   0.0
    40.  *   0.0   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
   0.0   0.0   0.0   0.2   0.2   0.2   0.2   0.0
    50.  *   0.0   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
   0.0   0.0   0.0   0.2   0.2   0.2   0.3   0.0
    60.  *   0.0   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.2
   0.0   0.0   0.0   0.2   0.2   0.3   0.2   0.0
    70.  *   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.1
   0.0   0.0   0.0   0.2   0.2   0.3   0.3   0.0
    80.  *   0.0   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.0
   0.0   0.0   0.0   0.2   0.4   0.3   0.3   0.0
    90.  *   0.0   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.0
   0.0   0.0   0.0   0.1   0.3   0.2   0.1   0.0
   100.  *   0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.1   0.0
   0.1   0.0   0.0   0.1   0.0   0.0   0.0   0.0
   110.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.1   0.1   0.0
   0.3   0.1   0.0   0.0   0.0   0.0   0.0   0.1
   120.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.0   0.0
   0.3   0.1   0.0   0.0   0.0   0.0   0.0   0.2
   130.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
   0.2   0.0   0.2   0.0   0.0   0.0   0.0   0.2
   140.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
   0.2   0.2   0.2   0.0   0.0   0.0   0.0   0.2
   150.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.0
   0.0   0.2   0.2   0.0   0.0   0.0   0.0   0.0
   160.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.0   0.0   0.0   0.0
   0.1   0.2   0.2   0.0   0.0   0.0   0.0   0.0
   170.  *   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.2   0.0   0.0   0.0   0.0
   0.2   0.2   0.2   0.0   0.0   0.0   0.0   0.0
   180.  *   0.0   0.0   0.0   0.2   0.0   0.2   0.2   0.2   0.0   0.0   0.0   0.0
   0.2   0.2   0.2   0.0   0.0   0.0   0.0   0.0
   190.  *   0.1   0.0   0.0   0.2   0.1   0.2   0.2   0.2   0.0   0.0   0.0   0.0
   0.2   0.2   0.2   0.0   0.0   0.0   0.0   0.2
   200.  *   0.2   0.0   0.0   0.2   0.2   0.2   0.2   0.2   0.0   0.0   0.0   0.0
   0.2   0.2   0.2   0.0   0.0   0.0   0.0   0.2
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 210.  *   0.2   0.0   0.0   0.1   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.2   0.2   0.2   0.0   0.0   0.0   0.0   0 .1
 220.  *   0.2   0.0   0.0   0.1   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.2   0.2   0.1   0.0   0.0   0.0   0.0   0 .1
 230.  *   0.2   0.0   0.0   0.0   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.2   0.2   0.0   0.0   0.0   0.0   0.0   0 .0
 240.  *   0.1   0.0   0.0   0.1   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.2   0.2   0.1   0.0   0.0   0.0   0.0   0 .1
 250.  *   0.0   0.0   0.0   0.1   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.2   0.2   0.1   0.0   0.0   0.0   0.0   0 .2
 260.  *   0.1   0.0   0.0   0.2   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.2   0.0   0.1   0.0   0.0   0.0   0.0   0 .0
 270.  *   0.1   0.0   0.0   0.2   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.2   0.1   0.2   0.0   0.0   0.0   0.0   0 .0
 280.  *   0.2   0.0   0.0   0.2   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 290.  *   0.2   0.0   0.0   0.2   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 300.  *   0.3   0.0   0.0   0.3   0.3   0.3   0.2   0.2   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 310.  *   0.2   0.0   0.0   0.2   0.2   0.2   0.2   0.2   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0.0   0.1   0.1   0 .0
 320.  *   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0 .2   0.2   0.2   0 .2
0.0   0.0   0.0   0.1   0.1   0.1   0.2   0 .0
 330.  *   0.0   0.2   0.2   0.0   0.0   0.0   0.0   0.0   0 .2   0.2   0.2   0 .2
0.0   0.0   0.0   0.2   0.1   0.2   0.2   0 .0
 340.  *   0.0   0.2   0.2   0.0   0.0   0.0   0.0   0.0   0 .2   0.2   0.2   0 .2
0.0   0.0   0.0   0.2   0.1   0.2   0.2   0 .0
 350.  *   0.0   0.2   0.1   0.0   0.0   0.0   0.0   0.0   0 .2   0.2   0.2   0 .2
0.0   0.0   0.0   0.2   0.1   0.2   0.2   0 .0

------*-------------------------------------------------------------------------------------
-------------------------------------------------
 MAX   *   0.3   0.2   0.2   0.3   0.3   0.3   0.2   0.2   0 .2   0.2   0.2   0 .2
0.3   0.2   0.2   0.2   0.4   0.3   0.3   0 .2
 DEGR. *  300    0     20   300   300   300   160   150     0     0     0     0
110   140   130    0     80    60    30   120

                                PAGE 10
     JOB:                                                         RUN:


      MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52
REC53 REC54 REC55 REC56 REC57 REC58 REC59 REC60

------*-------------------------------------------------------------------------------------
-------------------------------------------------
   0.  *   0.0   0.1   0.1   0.0   0.0   0.0   0.1   0.0   0 .0   0.1   0.1   0 .0
0.0   0.0   0.1   0.1   0.0   0.0   0.0   0 .1
  10.  *   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.0   0 .0   0.1   0.1   0 .0
```

```
 0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.3
  20.   *   0.0   0.1   0.0   0.0   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.1
 0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.3
  30.   *   0.0   0.1   0.0   0.0   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.1
 0.0   0.0   0.1   0.2   0.0   0.0   0.0   0.3
  40.   *   0.0   0.1   0.1   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.1   0.1
 0.0   0.0   0.2   0.3   0.0   0.0   0.0   0.3
  50.   *   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.0   0.0   0.1   0.0   0.4
 0.0   0.0   0.3   0.3   0.0   0.0   0.0   0.3
  60.   *   0.0   0.0   0.0   0.0   0.0   0.1   0.1   0.1   0.0   0.1   0.1   0.1
 0.1   0.1   0.1   0.1   0.1   0.1   0.1   0.1
  70.   *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2   0.0   0.0   0.0
 0.2   0.2   0.0   0.0   0.2   0.2   0.2   0.0
  80.   *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.4   0.1   0.0   0.0   0.0
 0.4   0.4   0.0   0.0   0.4   0.4   0.4   0.0
  90.   *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.3   0.0   0.0   0.0   0.0
 0.4   0.3   0.0   0.0   0.4   0.4   0.4   0.0
 100.   *   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
 0.3   0.0   0.0   0.0   0.3   0.3   0.3   0.0
 110.   *   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.0
 0.2   0.1   0.0   0.0   0.2   0.2   0.2   0.0
 120.   *   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.0
 0.2   0.1   0.0   0.0   0.2   0.2   0.2   0.0
 130.   *   0.1   0.0   0.0   0.2   0.1   0.0   0.0   0.2   0.1   0.0   0.0   0.0
 0.2   0.2   0.0   0.0   0.2   0.2   0.2   0.0
 140.   *   0.2   0.0   0.0   0.2   0.1   0.0   0.0   0.2   0.2   0.0   0.0   0.0
 0.0   0.2   0.0   0.0   0.2   0.2   0.2   0.0
 150.   *   0.2   0.0   0.0   0.1   0.2   0.0   0.0   0.0   0.2   0.0   0.0   0.0
 0.0   0.2   0.0   0.0   0.2   0.2   0.2   0.0
 160.   *   0.2   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.2   0.0   0.0   0.0
 0.0   0.2   0.0   0.0   0.2   0.2   0.2   0.0
 170.   *   0.1   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.2   0.0   0.0   0.0
 0.1   0.1   0.0   0.0   0.2   0.2   0.1   0.0
 180.   *   0.0   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.2   0.0   0.0   0.0
 0.2   0.0   0.0   0.0   0.2   0.2   0.0   0.0
 190.   *   0.0   0.0   0.0   0.1   0.2   0.0   0.0   0.2   0.2   0.0   0.0   0.0
 0.2   0.0   0.0   0.0   0.2   0.2   0.0   0.0
 200.   *   0.0   0.0   0.0   0.2   0.1   0.0   0.0   0.2   0.2   0.0   0.0   0.0
 0.2   0.0   0.0   0.0   0.2   0.2   0.0   0.0
 210.   *   0.2   0.0   0.0   0.2   0.0   0.0   0.0   0.2   0.1   0.0   0.0   0.0
 0.1   0.0   0.0   0.0   0.2   0.1   0.0   0.0
 220.   *   0.2   0.0   0.0   0.2   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.0
 0.0   0.1   0.0   0.0   0.1   0.0   0.0   0.0
 230.   *   0.2   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
 0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 240.   *   0.3   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 250.   *   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 260.   *   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.1
 270.   *   0.0   0.1   0.1   0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.0
 0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.1
 280.   *   0.0   0.1   0.3   0.0   0.0   0.4   0.0   0.0   0.0   0.1   0.0   0.1
 0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.1
 290.   *   0.0   0.3   0.3   0.0   0.0   0.2   0.0   0.0   0.0   0.1   0.0   0.1
 0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.1
 300.   *   0.0   0.3   0.2   0.0   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.1
 0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.1
 310.   *   0.0   0.3   0.1   0.0   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.2
 0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.1
 320.   *   0.0   0.2   0.1   0.0   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.2
 0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.0
```

```
 330.  *   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.0   0.0   0.1   0.1   0.1
0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
 340.  *   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.1
0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
 350.  *   0.0   0.0   0.1   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.2   0.1
0.0   0.0   0.1   0.1   0.0   0.0   0.0   0.1

------*-----------------------------------------------------------------------------
--------------------------------------------
 MAX   *   0.3   0.3   0.3   0.2   0.2   0.4   0.1   0.4   0.2   0.1   0.2   0.4
0.4   0.4   0.3   0.3   0.4   0.4   0.4   0.3
 DEGR. *   240   290   280   110   150   280     0    80    70     0   350    50
80    80    50    40    80    80    80    10


                          PAGE 11
    JOB:                                                          RUN:


      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* REC61 REC62 REC63 REC64 REC65 REC66 REC67 REC68 REC69 REC70 REC71 REC72
REC73 REC74 REC75 REC76 REC77 REC78 REC79 REC80

------*-----------------------------------------------------------------------------
--------------------------------------------
   0.  *   0.3   0.3   0.3   0.4   0.0   0.0   0.0   0.0   0.0   0.9   0.4   0.3
0.2   0.2   0.2   0.6   0.0   0.0   0.0   0.0
  10.  *   0.3   0.3   0.3   1.1   0.3   0.0   0.0   0.0   0.0   1.3   0.8   0.3
0.2   0.2   0.2   0.2   0.0   0.0   0.0   0.0
  20.  *   0.3   0.3   0.3   1.3   0.7   0.2   0.0   0.0   0.0   1.5   1.2   0.5
0.2   0.2   0.2   0.0   0.0   0.0   0.0   0.0
  30.  *   0.3   0.3   0.3   1.2   0.8   0.2   0.1   0.0   0.0   1.2   1.2   0.5
0.3   0.2   0.2   0.0   0.0   0.0   0.0   0.0
  40.  *   0.3   0.3   0.3   1.3   0.7   0.2   0.1   0.0   0.0   1.0   0.9   0.6
0.5   0.3   0.3   0.0   0.0   0.0   0.0   0.0
  50.  *   0.3   0.3   0.3   1.3   0.6   0.1   0.1   0.0   0.0   0.6   0.7   0.5
0.5   0.3   0.3   0.0   0.0   0.0   0.0   0.0
  60.  *   0.1   0.1   0.1   1.0   0.5   0.1   0.0   0.0   0.0   0.5   0.6   0.4
0.3   0.3   0.3   0.0   0.0   0.0   0.0   0.0
  70.  *   0.0   0.0   0.0   1.0   0.5   0.1   0.0   0.0   0.0   0.7   0.5   0.3
0.3   0.3   0.2   0.0   0.0   0.0   0.0   0.0
  80.  *   0.0   0.0   0.0   1.0   0.4   0.1   0.0   0.0   0.0   0.6   0.3   0.2
0.1   0.1   0.1   0.0   0.0   0.0   0.0   0.0
  90.  *   0.0   0.0   0.0   1.0   0.4   0.1   0.0   0.0   0.0   0.6   0.3   0.1
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
 100.  *   0.0   0.0   0.0   1.0   0.3   0.1   0.2   0.2   0.2   0.6   0.3   0.1
0.0   0.0   0.0   0.2   0.1   0.1   0.0   0.0
 110.  *   0.0   0.0   0.0   0.9   0.4   0.4   0.3   0.3   0.3   0.6   0.2   0.1
0.0   0.0   0.0   0.3   0.2   0.2   0.1   0.1
 120.  *   0.0   0.0   0.0   0.6   0.7   0.4   0.4   0.3   0.3   0.6   0.4   0.1
0.0   0.0   0.0   0.4   0.3   0.2   0.2   0.1
 130.  *   0.0   0.0   0.0   0.8   0.7   0.5   0.4   0.3   0.3   0.8   0.4   0.1
```

```
0.0   0.0   0.0   0.5   0. 4   0.2   0.2   0 .2
 140.  *    0.0   0.0   0.0   0.8   0.8   0.6   0.4   0.3   0 .3   0.8   0.4   0 .2
0.1   0.0   0.0   0.4   0. 4   0.2   0.2   0 .2
 150.  *    0.0   0.0   0.0   0.9   0.8   0.8   0.4   0.3   0 .3   0.9   0.4   0 .4
0.1   0.0   0.0   0.4   0. 4   0.4   0.2   0 .2
 160.  *    0.0   0.0   0.0   1.2   0.8   0.8   0.4   0.4   0 .3   1.0   0.4   0 .4
0.1   0.1   0.0   0.4   0. 4   0.4   0.2   0 .2
 170.  *    0.0   0.0   0.0   1.4   0.9   0.6   0.4   0.3   0 .3   1.1   0.5   0 .2
0.0   0.0   0.0   0.5   0. 4   0.4   0.2   0 .2
 180.  *    0.0   0.0   0.0   1.0   0.6   0. 4   0.3   0.3   0 .3   0.6   0.2   0 .0
0.0   0.0   0.0   1.0   0. 6   0.4   0.2   0 .2
 190.  *    0.0   0.0   0.0   0.5   0.4   0. 4   0.3   0.3   0 .3   0.1   0.0   0 .0
0.0   0.0   0.0   1.1   1. 0   0.6   0.4   0 .2
 200.  *    0.0   0.0   0.0   0.4   0.4   0. 3   0.3   0.3   0 .3   0.0   0.0   0 .0
0.0   0.0   0.0   1.3   1. 0   0.7   0.5   0 .4
 210.  *    0.0   0.0   0.0   0.4   0.4   0. 3   0.3   0.3   0 .2   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0. 7   0.6   0.5   0 .3
 220.  *    0.0   0.0   0.0   0.4   0.4   0. 3   0.3   0.3   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   0.8   0. 7   0.6   0.6   0 .2
 230.  *    0.0   0.0   0.0   0.4   0.4   0. 3   0.3   0.3   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   0.7   0. 6   0.6   0.5   0 .3
 240.  *    0.0   0.0   0.0   0.4   0.3   0. 3   0.3   0.2   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   1.0   0. 5   0.5   0.4   0 .3
 250.  *    0.0   0.0   0.0   0.4   0.3   0. 3   0.2   0.0   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   1.0   0. 5   0.5   0.3   0 .4
 260.  *    0.0   0.1   0.1   0.2   0.2   0. 0   0.0   0.1   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   1.0   0. 4   0.3   0.1   0 .1
 270.  *    0.0   0.1   0.1   0.0   0.0   0. 0   0.0   0.0   0 .1   0.0   0.0   0 .0
0.0   0.0   0.0   1.0   0. 3   0.2   0.0   0 .0
 280.  *    0.1   0.1   0.2   0.0   0.0   0. 0   0.0   0.0   0 .0   0.1   0.1   0 .1
0.0   0.0   0.0   1.0   0. 3   0.2   0.0   0 .0
 290.  *    0.1   0.1   0.3   0.0   0.0   0. 0   0.0   0.0   0 .0   0.4   0.2   0 .1
0.1   0.0   0.1   1.0   0. 3   0.2   0.0   0 .0
 300.  *    0.1   0.3   0.3   0.0   0.0   0. 0   0.0   0.0   0 .0   0.4   0.4   0 .3
0.2   0.2   0.2   1.1   0. 3   0.3   0.0   0 .0
 310.  *    0.1   0.2   0.2   0.0   0.0   0. 0   0.0   0.0   0 .0   0.4   0.4   0 .3
0.3   0.1   0.2   1.2   0. 5   0.3   0.1   0 .0
 320.  *    0.1   0.2   0.2   0.0   0.0   0. 0   0.0   0.0   0 .0   0.5   0.4   0 .3
0.3   0.2   0.1   1.3   0. 6   0.3   0.2   0 .0
 330.  *    0.1   0.2   0.2   0.0   0.0   0. 0   0.0   0.0   0 .0   0.4   0.3   0 .3
0.2   0.2   0.1   1.4   0. 7   0.3   0.2   0 .0
 340.  *    0.2   0.2   0.2   0.0   0.0   0. 0   0.0   0.0   0 .0   0.4   0.3   0 .3
0.2   0.2   0.2   1.3   0. 7   0.3   0.0   0 .0
 350.  *    0.2   0.2   0.2   0.0   0.0   0. 0   0.0   0.0   0 .0   0.4   0.3   0 .3
0.2   0.2   0.2   1.1   0. 4   0.0   0.0   0 .0

------*-----------------------------------------------------------------------------------------
-----------------------------------------------------------
 MAX   *    0.3   0.3   0.3   1.4   0.9   0. 8   0.4   0.4   0 .3   1.5   1.2   0 .6
0.5   0.3   0.3   1.4   1. 0   0.7   0.6   0 .4
 DEGR. *    0     0     0     170   170   150    120   160   110    20    20    4 0
50    40    40    330   200   200   220   20 0

□
                          PAGE 12
    JOB:                                                       RUN:

     MODEL RESULTS
     -------------

     REMARKS : In search of the angle corresponding to
               the maximum concentration, only the first
```

```
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* REC81 REC82 REC83 REC84 REC85 REC86 REC87 REC88 REC89 REC90 REC91 REC92
REC93 REC94 REC95 REC96 REC97 REC98 REC99 RE100

------*----------------------------------------------------------------------------
-------------------------------------------
   0.  *  0.0   1.1   0.4   0.4   0.3   0.2   0.2   0.4   0.0   0.0   0.0   0.0
0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.4
  10.  *  0.0   0.6   0.4   0.3   0.2   0.2   0.1   1.0   0.3   0.0   0.0   0.0
0.0   0.9   0.4   0.0   0.0   0.0   0.0   0.2
  20.  *  0.0   0.4   0.4   0.3   0.2   0.2   0.1   1.3   0.6   0.2   0.0   0.0
0.0   1.0   0.8   0.2   0.0   0.0   0.0   0.0
  30.  *  0.0   0.5   0.5   0.4   0.3   0.3   0.1   1.2   0.8   0.2   0.1   0.0
0.0   0.8   0.6   0.2   0.1   0.0   0.1   0.0
  40.  *  0.0   0.5   0.5   0.4   0.3   0.2   0.1   1.2   0.6   0.2   0.1   0.0
0.0   0.6   0.4   0.2   0.2   0.1   0.1   0.0
  50.  *  0.0   0.5   0.4   0.4   0.3   0.1   0.1   1.2   0.6   0.1   0.1   0.0
0.0   0.7   0.4   0.1   0.1   0.1   0.1   0.0
  60.  *  0.0   0.4   0.4   0.3   0.1   0.1   0.0   1.0   0.5   0.1   0.0   0.0
0.0   0.6   0.4   0.1   0.0   0.0   0.0   0.0
  70.  *  0.0   0.4   0.2   0.1   0.1   0.1   0.0   1.0   0.5   0.1   0.0   0.0
0.0   0.6   0.4   0.1   0.0   0.0   0.0   0.0
  80.  *  0.0   0.1   0.1   0.1   0.1   0.0   0.0   1.0   0.4   0.1   0.0   0.0
0.0   0.6   0.3   0.1   0.0   0.0   0.0   0.0
  90.  *  0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0   0.4   0.1   0.0   0.0
0.0   0.6   0.3   0.1   0.0   0.0   0.0   0.0
 100.  *  0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0   0.4   0.1   0.0   0.0
0.0   0.6   0.3   0.1   0.0   0.0   0.0   0.0
 110.  *  0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0   0.3   0.1   0.0   0.0
0.0   0.6   0.2   0.1   0.0   0.0   0.0   0.0
 120.  *  0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9   0.5   0.1   0.0   0.1
0.1   0.6   0.4   0.1   0.0   0.0   0.0   0.0
 130.  *  0.1   0.0   0.0   0.0   0.0   0.0   0.0   1.0   0.4   0.1   0.1   0.1
0.1   0.7   0.4   0.1   0.0   0.0   0.0   0.0
 140.  *  0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.8   0.4   0.3   0.2   0.1
0.1   0.7   0.4   0.2   0.1   0.0   0.0   0.0
 150.  *  0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.8   0.4   0.5   0.2   0.1
0.1   0.9   0.4   0.4   0.1   0.0   0.0   0.0
 160.  *  0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.7   0.5   0.5   0.2   0.2
0.1   1.0   0.4   0.4   0.1   0.1   0.0   0.0
 170.  *  0.2   0.1   0.0   0.0   0.0   0.0   0.0   1.0   0.6   0.3   0.2   0.1
0.1   1.1   0.5   0.2   0.0   0.0   0.0   0.1
 180.  *  0.2   0.6   0.2   0.0   0.0   0.0   0.0   0.7   0.3   0.1   0.1   0.1
0.0   0.5   0.2   0.0   0.0   0.0   0.0   0.6
 190.  *  0.2   0.8   0.6   0.2   0.2   0.0   0.0   0.2   0.1   0.1   0.1   0.1
0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.9
 200.  *  0.2   0.9   0.7   0.3   0.2   0.2   0.0   0.1   0.1   0.1   0.1   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.7
 210.  *  0.2   1.0   0.4   0.2   0.2   0.1   0.0   0.1   0.1   0.1   0.1   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8
 220.  *  0.2   0.8   0.3   0.2   0.2   0.0   0.0   0.1   0.1   0.1   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9
 230.  *  0.3   0.8   0.3   0.2   0.1   0.0   0.0   0.1   0.1   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1
 240.  *  0.2   0.7   0.2   0.2   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0
0.1   0.0   0.0   0.0   0.0   0.0   0.0   1.2
 250.  *  0.2   0.6   0.2   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
```

```
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1
 260.  *   0.2   0.6   0.2   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
 270.  *   0.0   0.6   0.2   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
 280.  *   0.0   0.7   0.3   0.3   0.1   0.2   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
 290.  *   0.0   0.6   0.4   0.4   0.2   0.3   0.3   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0
 300.  *   0.0   0.7   0.4   0.5   0.5   0.4   0.3   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1
 310.  *   0.0   0.6   0.5   0.7   0.7   0.3   0.3   0.0   0.0   0.0   0.0   0.0
0.0   0.1   0.0   0.0   0.0   0.0   0.0   1.2
 320.  *   0.0   0.8   0.8   0.8   0.7   0.3   0.3   0.0   0.0   0.0   0.0   0.0
0.0   0.1   0.1   0.0   0.0   0.0   0.0   1.3
 330.  *   0.0   1.2   1.1   0.8   0.6   0.3   0.3   0.0   0.0   0.0   0.0   0.0
0.0   0.1   0.0   0.0   0.0   0.0   0.0   1.2
 340.  *   0.0   1.4   1.1   0.7   0.3   0.2   0.2   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.3
 350.  *   0.0   1.4   0.8   0.5   0.3   0.2   0.2   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1

------*------------------------------------------------------------------------------
-----------------------------------------------
 MAX   *   0.3   1.4   1.1   0.8   0.7   0.4   0.3   1.3   0.8   0.5   0.2   0.2
0.1   1.1   0.8   0.4   0.2   0.1   0.1   1.3
 DEGR. *  230   350   330   320   320   300   290    20    30   160   140   160
120   170    20   150    40    40    30   320


                              PAGE 13
     JOB:                                                        RUN:


      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *       (PPM)
 (DEGR)* RE101 RE102 RE103 RE104 RE105 RE106 RE107 RE108 RE109 RE110 RE111 RE112
RE113 RE114 RE115 RE116 RE117 RE118 RE119 RE120

------*------------------------------------------------------------------------------
-----------------------------------------------
   0.  *   0.0   0.0   0.0   0.0   0.0   0.6   0.1   0.0   0.0   0.0   0.0   0.4
0.0   0.0   0.0   0.0   0.0   0.4   0.0   0.0
  10.  *   0.0   0.0   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.0   0.9
0.3   0.0   0.0   0.0   0.0   0.9   0.4   0.0
  20.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1
0.6   0.1   0.0   0.0   0.0   1.0   0.6   0.2
  30.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1
0.8   0.2   0.0   0.0   0.0   0.7   0.4   0.2
  40.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.2
0.6   0.2   0.1   0.0   0.0   0.7   0.4   0.2
  50.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.2
0.6   0.1   0.1   0.0   0.0   0.7   0.4   0.1
```

```
  60.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .9
 0.5  0.1   0.0   0.0   0.0   0.6   0.4   0 .1
  70.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .9
 0.5  0.1   0.0   0.0   0.0   0.6   0.4   0 .1
  80.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .9
 0.4  0.1   0.0   0.0   0.0   0.6   0.3   0 .1
  90.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .9
 0.4  0.1   0.0   0.0   0.0   0.5   0.3   0 .1
 100.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   1 .0
 0.4  0.1   0.0   0.0   0.0   0.5   0.3   0 .1
 110.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   1 .0
 0.3  0.1   0.0   0.0   0.0   0.5   0.2   0 .1
 120.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   1 .0
 0.5  0.1   0.0   0.0   0.0   0.5   0.4   0 .1
 130.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   1 .1
 0.5  0.1   0.0   0.0   0.0   0.7   0.4   0 .1
 140.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   1 .1
 0.4  0.2   0.1   0.0   0.0   0.7   0.4   0 .2
 150.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .9
 0.4  0.4   0.1   0.1   0.0   0.9   0.4   0 .4
 160.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .8
 0.4  0.4   0.1   0.1   0.0   1.0   0.4   0 .4
 170.  *   0.0   0.0   0.0   0.0   0.0   0.1   0.0   0.0   0 .0   0.0   0.0   0 .9
 0.4  0.2   0.1   0.0   0.0   1.0   0.5   0 .2
 180.  *   0.2   0.0   0.0   0.0   0.0   0.6   0.2   0.0   0 .0   0.0   0.0   0 .6
 0.2  0.0   0.0   0.0   0.0   0.5   0.2   0 .0
 190.  *   0.6   0.2   0.2   0.0   0.0   0.8   0.6   0.2   0 .2   0.0   0.0   0 .1
 0.0  0.0   0.0   0.0   0.0   0.1   0.0   0 .0
 200.  *   0.5   0.3   0.2   0.2   0.0   0.9   0.7   0.3   0 .2   0.1   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 210.  *   0.3   0.2   0.2   0.1   0.0   0.9   0.4   0.2   0 .2   0.1   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 220.  *   0.3   0.2   0.2   0.0   0.0   0.8   0.3   0.2   0 .2   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 230.  *   0.4   0.2   0.1   0.0   0.0   0.8   0.3   0.2   0 .1   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 240.  *   0.3   0.2   0.0   0.0   0.0   0.7   0.2   0.2   0 .0   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 250.  *   0.3   0.2   0.0   0.0   0.0   0.6   0.2   0.2   0 .0   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 260.  *   0.3   0.2   0.0   0.0   0.0   0.6   0.2   0.2   0 .0   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 270.  *   0.3   0.2   0.0   0.0   0.0   0.6   0.2   0.2   0 .0   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 280.  *   0.3   0.2   0.0   0.0   0.0   0.6   0.2   0.2   0 .0   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 290.  *   0.3   0.2   0.0   0.0   0.0   0.6   0.2   0.2   0 .0   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 300.  *   0.3   0.3   0.0   0.0   0.0   0.8   0.2   0.2   0 .0   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 310.  *   0.5   0.3   0.1   0.0   0.0   0.7   0.3   0.2   0 .1   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 320.  *   0.6   0.3   0.2   0.0   0.0   0.6   0.3   0.2   0 .2   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 330.  *   0.7   0.3   0.2   0.0   0.0   0.7   0.4   0.3   0 .2   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 340.  *   0.7   0.3   0.0   0.0   0.0   1.0   0.6   0.3   0 .2   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0
 350.  *   0.4   0.0   0.0   0.0   0.0   1.1   0.4   0.1   0 .0   0.0   0.0   0 .0
 0.0  0.0   0.0   0.0   0.0   0.0   0.0   0 .0

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```

```
 MAX   *   0.7   0.3   0.2   0.2   0.0   1.1   0.7   0.3   0 .2   0.1   0.0   1 .2
0.8   0.4   0.1   0.1   0.0   1.0   0.6   0 .4
 DEGR. *  340   200   190   200     0   350   200   200   190   200     0    40
30   150    40   150     0   170    20   150

▯
                         PAGE 14
      JOB:                                                    RUN:


        MODEL RESULTS
        -------------

        REMARKS : In search of the angle corresponding to
                  the maximum concentration, only the first
                  angle, of the angles with same maximum
                  concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* RE121 RE122 RE123 RE124 RE125 RE126 RE127 RE128 RE129 RE130 RE131 RE132
RE133 RE134 RE135 RE136 RE137 RE138 RE139 RE140

------*------------------------------------------------------------------------------
------------------------------------------------
   0.  *   0.0   0.0   0.0   0.4   0.0   0.0   0.0   0.0   0 .0   0.4   0.1   0 .0
0.0   0.0   0.0   0.3   0.0   0.0   0.3   0 .0
  10.  *   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.0   0 .0   0.1   0.0   0 .0
0.0   0.0   0.0   0.9   0.3   0.0   0.8   0 .3
  20.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.0   0.5   0.1   0.8   0 .4
  30.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.0   0.8   0.2   0.8   0 .4
  40.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.1   0.6   0.2   0.8   0 .4
  50.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.1   0.6   0.1   0.7   0 .4
  60.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0.5   0.1   0.5   0 .4
  70.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0.5   0.1   0.5   0 .4
  80.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0.4   0.1   0.5   0 .3
  90.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0.4   0.1   0.5   0 .3
 100.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0.4   0.1   0.5   0 .3
 110.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0.3   0.1   0.5   0 .2
 120.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0.5   0.1   0.5   0 .4
 130.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.1   0.5   0.1   0.7   0 .4
 140.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.3   0.5   0.2   0.7   0 .4
 150.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   1.2   0.4   0.4   0.9   0 .4
 160.  *   0.1   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.9   0.4   0.4   1.0   0 .4
 170.  *   0.0   0.0   0.0   0.1   0.0   0.0   0.0   0.0   0 .0   0.1   0.0   0 .0
0.0   0.0   0.0   0.9   0.4   0.3   0.9   0 .5
```

```
 180.  *   0.0   0.0   0.0   0.6   0.2   0. 0  0.0   0.0   0 .0   0.6   0.2   0 .0
0.0  0.0   0.0   0.5   0. 2  0.0   0.5   0 .1
 190.  *   0.0   0.0   0.0   0.9   0.6   0. 2  0.2   0.0   0 .0   0.8   0.6   0 .2
0.2  0.0   0.0   0.1   0.0   0.0   0.1   0 .0
 200.  *   0.0   0.0   0.0   0.8   0.5   0. 3  0.2   0.2   0 .0   0.9   0.7   0 .3
0.2  0.1   0.0   0.0   0. 0  0.0   0.0   0 .0
 210.  *   0.0   0.0   0.0   1.0   0.3   0. 2  0.2   0.1   0 .0   0.9   0.4   0 .2
0.2  0.1   0.0   0.0   0. 0  0.0   0.0   0 .0
 220.  *   0.0   0.0   0.0   1.1   0.4   0. 2  0.2   0.0   0 .0   0.7   0.3   0 .2
0.2  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 230.  *   0.0   0.0   0.0   1.1   0.4   0. 2  0.1   0.0   0 .0   0.7   0.3   0 .2
0.1  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 240.  *   0.0   0.0   0.0   1.1   0.3   0. 2  0.0   0.0   0 .0   0.7   0.2   0 .2
0.0  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 250.  *   0.0   0.0   0.0   1.0   0.3   0. 2  0.0   0.0   0 .0   0.6   0.2   0 .2
0.0  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 260.  *   0.0   0.0   0.0   1.0   0.3   0. 2  0.0   0.0   0 .0   0.6   0.2   0 .2
0.0  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 270.  *   0.0   0.0   0.0   1.0   0.3   0. 2  0.0   0.0   0 .0   0.6   0.2   0 .2
0.0  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 280.  *   0.0   0.0   0.0   1.0   0.3   0. 2  0.0   0.0   0 .0   0.6   0.2   0 .2
0.0  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 290.  *   0.0   0.0   0.0   1.0   0.3   0. 2  0.0   0.0   0 .0   0.6   0.2   0 .2
0.0  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 300.  *   0.0   0.0   0.0   1.1   0.3   0. 3  0.0   0.0   0 .0   0.7   0.2   0 .2
0.0  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 310.  *   0.0   0.0   0.0   1.1   0.5   0. 3  0.1   0.0   0 .0   0.7   0.3   0 .2
0.1  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 320.  *   0.0   0.0   0.0   1.1   0.6   0. 3  0.2   0.0   0 .0   0.7   0.3   0 .2
0.2  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 330.  *   0.0   0.0   0.0   1.2   0.7   0. 3  0.2   0.0   0 .0   0.7   0.3   0 .2
0.2  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 340.  *   0.0   0.0   0.0   1.3   0.6   0. 3  0.0   0.0   0 .0   0.8   0.5   0 .3
0.2  0.0   0.0   0.0   0. 0  0.0   0.0   0 .0
 350.  *   0.0   0.0   0.0   1.1   0.4   0.0   0.0   0.0   0 .0   0.9   0.3   0 .1
0.0  0.0   0.0   0.0   0. 0  0.0   0.1   0 .0

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 MAX   *   0.1   0.1   0.0   1.3   0.7   0. 3  0.2   0.2   0 .0   0.9   0.7   0 .3
0.2  0.1   0.0   1.3   0. 8  0.4   1.0   0 .5
 DEGR. *   30   160     0   340   330   200   190   200     0   200   200   20 0
190  200     0   140    3 0   150   160   1 70

□
                              PAGE 15
     JOB:                                                                RUN:


      MODEL RESULTS
      -------------

      REMARKS : In search of the angle cor responding to
                the maxim um concentration, only the first
                angle, of the angles with same maximum
                concentra tions, is indicat ed as maximum.

 WIND ANGLE RANGE:   0.-35 0.

 WIND  *  CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* RE141 RE142 RE143 RE144 RE145 RE14 6 RE147 RE148 RE1 49 RE150 RE151 RE1 52
RE153 RE154 RE155 RE156 RE 157 RE158 RE159 R E160
```

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-------*------------------ ----------------- ----------------- ----------------- ------
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   0.   *    0.0   0.4   0.0   0.0   0.4   0.1    0.0   0.4   0 .4   0.4   0.4   0 .4
0.3   0.3   0.3   0.3   0. 2   0.2   0.2   0 .2
  10.   *    0.0   0.1   0.0   0.0   0.1   0. 0    0.0   0.1   0 .1   0.1   0.0   0 .0
0.0   0.0   0.0   0.0   0. 9   0.8   0.8   0 .7
  20.   *    0.2   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   1. 0   1.0   1.0   1 .0
  30.   *    0.2   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   1. 0   1.0   1.0   1 .0
  40.   *    0.2   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   1. 0   1.0   1.0   1 .0
  50.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   1. 0   1.0   1.0   1 .0
  60.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 8   0.8   0.8   0 .8
  70.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 8   0.8   0.8   0 .8
  80.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 8   0.8   0.8   0 .8
  90.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 9   0.8   0.8   0 .8
 100.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 9   0.8   0.8   0 .8
 110.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 9   0.8   0.8   0 .8
 120.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 9   0.8   0.8   0 .8
 130.   *    0.1   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   1. 1   1.1   1.1   1 .0
 140.   *    0.2   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   1. 2   1.2   1.1   1 .0
 150.   *    0.4   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   1. 2   1.3   1.2   1 .1
 160.   *    0.4   0.0   0.0   0.0   0.0   0. 0    0.0   0.0   0 .0   0.0   0.0   0 .0
0.0   0.0   0.0   0.0   0. 9   1.1   1.1   1 .1
 170.   *    0.2   0.1   0.0   0.0   0.1   0. 0    0.0   0.1   0 .1   0.1   0.1   0 .1
0.1   0.1   0.1   0.1   0. 9   0.9   1.0   0 .9
 180.   *    0.0   0.7   0.2   0.0   0.6   0. 2    0.0   0.5   0 .5   0.6   0.6   0 .6
0.7   0.7   0.7   0.7   0. 6   0.6   0.6   0 .6
 190.   *    0.0   0.8   0.4   0.2   0.8   0. 6    0.2   0.8   0 .9   1.0   1.0   1 .0
1.0   1.1   1.1   1.1   0. 1   0.1   0.1   0 .1
 200.   *    0.0   1.0   0.5   0.3   0.8   0. 7    0.3   1.1   1 .1   1.1   1.2   1 .2
1.2   1.2   1.2   1.3   0. 0   0.0   0.0   0 .0
 210.   *    0.0   1.2   0.4   0.2   0.9   0. 4    0.2   1.3   1 .2   1.2   1.1   1 .2
1.2   1.2   1.2   1.2   0. 0   0.0   0.0   0 .0
 220.   *    0.0   1.2   0.4   0.2   0.7   0. 3    0.2   1.2   1 .1   1.1   1.0   1 .1
1.1   1.1   1.1   1.1   0. 0   0.0   0.0   0 .0
 230.   *    0.0   1.2   0.4   0.2   0.7   0. 3    0.2   1.1   1 .1   1.0   1.0   1 .0
1.0   1.0   1.0   1.0   0. 0   0.0   0.0   0 .0
 240.   *    0.0   1.1   0.3   0.2   0.6   0. 2    0.2   1.0   1 .0   1.0   1.0   1 .0
1.0   1.0   1.0   1.0   0. 0   0.0   0.0   0 .0
 250.   *    0.0   1.0   0.3   0.2   0.5   0. 2    0.2   0.9   0 .9   0.9   0.9   0 .9
0.9   0.9   0.9   0.9   0. 0   0.0   0.0   0 .0
 260.   *    0.0   0.9   0.3   0.2   0.5   0. 2    0.2   0.9   0 .9   0.9   0.9   0 .9
0.9   0.9   0.9   0.9   0. 0   0.0   0.0   0 .0
 270.   *    0.0   0.9   0.3   0.2   0.5   0. 2    0.2   0.9   0 .9   0.9   0.9   0 .9
0.9   0.9   0.9   0.9   0. 0   0.0   0.0   0 .0
 280.   *    0.0   0.9   0.3   0.2   0.5   0. 2    0.2   0.9   0 .9   0.9   0.9   0 .9
0.9   0.9   0.9   0.9   0. 0   0.0   0.0   0 .0
 290.   *    0.0   0.9   0.3   0.2   0.6   0. 2    0.2   0.9   0 .9   0.9   0.9   0 .9
0.9   0.9   0.9   0.9   0. 0   0.0   0.0   0 .0
```

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 300.  *   0.0   1.0   0.3   0.3   0.7   0.2   0.2   1.0   1.0   1.0   1.0   1.0
1.0   1.0   1.0   1.0   0.0   0.0   0.0   0.0
 310.  *   0.0   1.0   0.5   0.3   0.8   0.3   0.2   1.0   1.0   1.0   1.0   1.0
1.0   1.0   1.0   1.0   0.0   0.0   0.0   0.0
 320.  *   0.0   1.1   0.5   0.3   0.8   0.3   0.2   1.1   1.1   1.1   1.1   1.1
1.1   1.0   1.0   1.0   0.0   0.0   0.0   0.0
 330.  *   0.0   1.2   0.7   0.3   0.8   0.3   0.2   1.2   1.2   1.2   1.2   1.2
1.1   1.1   1.0   1.0   0.0   0.0   0.0   0.0
 340.  *   0.0   1.3   0.6   0.3   0.7   0.4   0.2   1.3   1.2   1.2   1.2   1.1
1.0   1.0   1.0   0.9   0.0   0.0   0.0   0.0
 350.  *   0.0   1.0   0.4   0.0   0.9   0.3   0.2   1.0   1.0   1.0   1.0   0.9
0.7   0.7   0.6   0.4   0.0   0.0   0.0   0.0

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 MAX   *   0.4   1.3   0.7   0.3   0.9   0.7   0.3   1.3   1.2   1.2   1.2   1.2
1.2   1.2   1.2   1.3   1.2   1.3   1.2   1.1
 DEGR. *  150   340   330   200   210   200   200   210   210   210   200   200
200   200   200   200   140   150   150   150

□
                             PAGE 16
      JOB:                                                          RUN:


       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-350.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* RE161 RE162 RE163 RE164 RE165 RE166 RE167 RE168 RE169 RE170 RE171 RE172
RE173 RE174 RE175 RE176 RE177 RE178 RE179 RE180

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   0.  *   0.2   0.2   0.2   0.2   0.2   0.4   0.3   0.4   0.4   0.4   0.5   0.5
0.5   0.5   0.3   0.3   0.3   0.3   0.3   0.3
  10.  *   0.5   0.5   0.5   0.4   0.2   0.1   0.1   0.1   0.1   0.1   0.1   0.1
0.1   0.1   0.6   0.6   0.6   0.6   0.6   0.5
  20.  *   1.0   0.9   0.9   0.8   0.7   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.7   0.8   0.8   0.7
  30.  *   1.0   1.0   1.0   1.0   0.9   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.8   0.8   0.8   0.8   0.8   0.8
  40.  *   1.0   1.0   1.0   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.7   0.7   0.6   0.6
  50.  *   1.0   1.0   1.0   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.7   0.6   0.6   0.6
  60.  *   0.8   0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.5   0.5   0.5   0.4   0.4   0.4
  70.  *   0.8   0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.5   0.5   0.5   0.4   0.4   0.4
  80.  *   0.8   0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.5   0.5   0.5   0.4   0.4   0.4
  90.  *   0.8   0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.5   0.5   0.5   0.4   0.4   0.4
 100.  *   0.8   0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0   0.0
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0.0   0.0   0.5   0.5   0.5   0.4   0.4   0.4
 110.  *   0.8   0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.5   0.5   0.4   0.4   0.4   0.4
 120.  *   0.8   0.8   0.8   0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.5   0.5   0.4   0.4   0.4   0.4
 130.  *   1.0   1.0   1.0   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.6   0.6   0.6   0.6
 140.  *   1.0   1.0   1.0   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.7   0.7   0.6   0.6   0.6   0.6
 150.  *   1.1   1.1   1.1   1.1   1.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   0.9   0.8   0.8   0.8   0.8   0.8
 160.  *   1.1   1.1   1.1   1.1   1.1   0.0   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0   1.0   0.9   0.9   0.8   0.8   0.8
 170.  *   0.9   1.0   1.1   1.1   1.1   0.1   0.1   0.1   0.1   0.1   0.1   0.1
0.1   0.1   0.9   0.8   0.8   0.8   0.8   0.8
 180.  *   0.6   0.6   0.6   0.6   0.6   0.6   0.6   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.4   0.4   0.4   0.4   0.4   0.4
 190.  *   0.1   0.1   0.1   0.1   0.1   0.8   0.8   0.8   0.8   0.8   0.8   0.8
0.8   0.8   0.1   0.1   0.1   0.1   0.1   0.1
 200.  *   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.8   0.8   0.8   0.8
0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0
 210.  *   0.0   0.0   0.0   0.0   0.0   0.9   0.9   0.8   0.8   0.8   0.8   0.8
0.8   0.8   0.0   0.0   0.0   0.0   0.0   0.0
 220.  *   0.0   0.0   0.0   0.0   0.0   0.7   0.7   0.7   0.7   0.7   0.7   0.7
0.7   0.7   0.0   0.0   0.0   0.0   0.0   0.0
 230.  *   0.0   0.0   0.0   0.0   0.0   0.7   0.7   0.7   0.7   0.7   0.7   0.7
0.7   0.7   0.0   0.0   0.0   0.0   0.0   0.0
 240.  *   0.0   0.0   0.0   0.0   0.0   0.6   0.6   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.0   0.0   0.0   0.0   0.0   0.0
 250.  *   0.0   0.0   0.0   0.0   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 260.  *   0.0   0.0   0.0   0.0   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 270.  *   0.0   0.0   0.0   0.0   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 280.  *   0.0   0.0   0.0   0.0   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 290.  *   0.0   0.0   0.0   0.0   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5
0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0
 300.  *   0.0   0.0   0.0   0.0   0.0   0.6   0.6   0.6   0.6   0.6   0.6   0.6
0.6   0.6   0.0   0.0   0.0   0.0   0.0   0.0
 310.  *   0.0   0.0   0.0   0.0   0.0   0.7   0.7   0.7   0.7   0.7   0.7   0.7
0.7   0.7   0.0   0.0   0.0   0.0   0.0   0.0
 320.  *   0.0   0.0   0.0   0.0   0.0   0.8   0.7   0.7   0.7   0.7   0.7   0.7
0.7   0.7   0.0   0.0   0.0   0.0   0.0   0.0
 330.  *   0.0   0.0   0.0   0.0   0.0   0.9   0.8   0.8   0.8   0.9   0.9   0.9
0.9   0.9   0.0   0.0   0.0   0.0   0.0   0.0
 340.  *   0.0   0.0   0.0   0.0   0.0   0.8   0.7   0.7   0.8   0.8   0.8   0.8
0.9   0.9   0.0   0.0   0.0   0.0   0.0   0.0
 350.  *   0.0   0.0   0.0   0.0   0.0   0.7   0.7   0.7   0.7   0.7   0.7   0.7
0.7   0.8   0.1   0.1   0.1   0.1   0.1   0.1

------*------------------ ----------------- ----------------- ------------------ ------
--------------------------------------- -----------------
 MAX   *   1.1   1.1   1.1   1.1   1.1   0.9   0.9   0.8   0.8   0.9   0.9   0.9
0.9   0.9   1.0   0.9   0.9   0.8   0.8   0.8
 DEGR. *  150   150   150   150   150   210   210   190   190   330   330   330
330   330   160   160   160    20    20    30

▯
                         PAGE 17
    JOB:                                                      RUN:
```

```
        MODEL RESULTS
        -------------

        REMARKS : In search of the angle corresponding to
                  the maximum concentration, only the first
                  angle, of the angles with same maximum
                  concentrations, is indicated as maximum.

    WIND ANGLE RANGE:   0.-350.

    WIND   * CONCENTRATION
    ANGLE  *      (PPM)
    (DEGR)* RE181 RE182 RE183
    ------*------------------
      0.  *   0.3   0.3   0.3
     10.  *   0.5   0.5   0.6
     20.  *   0.7   0.8   0.8
     30.  *   0.8   0.8   0.8
     40.  *   0.6   0.6   0.6
     50.  *   0.6   0.6   0.6
     60.  *   0.4   0.4   0.4
     70.  *   0.4   0.4   0.4
     80.  *   0.4   0.4   0.4
     90.  *   0.4   0.4   0.4
    100.  *   0.4   0.4   0.4
    110.  *   0.4   0.4   0.4
    120.  *   0.4   0.4   0.4
    130.  *   0.6   0.5   0.5
    140.  *   0.6   0.5   0.5
    150.  *   0.7   0.7   0.7
    160.  *   0.8   0.8   0.8
    170.  *   0.8   0.8   0.7
    180.  *   0.4   0.4   0.4
    190.  *   0.1   0.1   0.1
    200.  *   0.0   0.0   0.0
    210.  *   0.0   0.0   0.0
    220.  *   0.0   0.0   0.0
    230.  *   0.0   0.0   0.0
    240.  *   0.0   0.0   0.0
    250.  *   0.0   0.0   0.0
    260.  *   0.0   0.0   0.0
    270.  *   0.0   0.0   0.0
    280.  *   0.0   0.0   0.0
    290.  *   0.0   0.0   0.0
    300.  *   0.0   0.0   0.0
    310.  *   0.0   0.0   0.0
    320.  *   0.0   0.0   0.0
    330.  *   0.0   0.0   0.0
    340.  *   0.0   0.0   0.0
    350.  *   0.1   0.1   0.1
    ------*------------------
    MAX   *   0.8   0.8   0.8
    DEGR. *   30    20    20

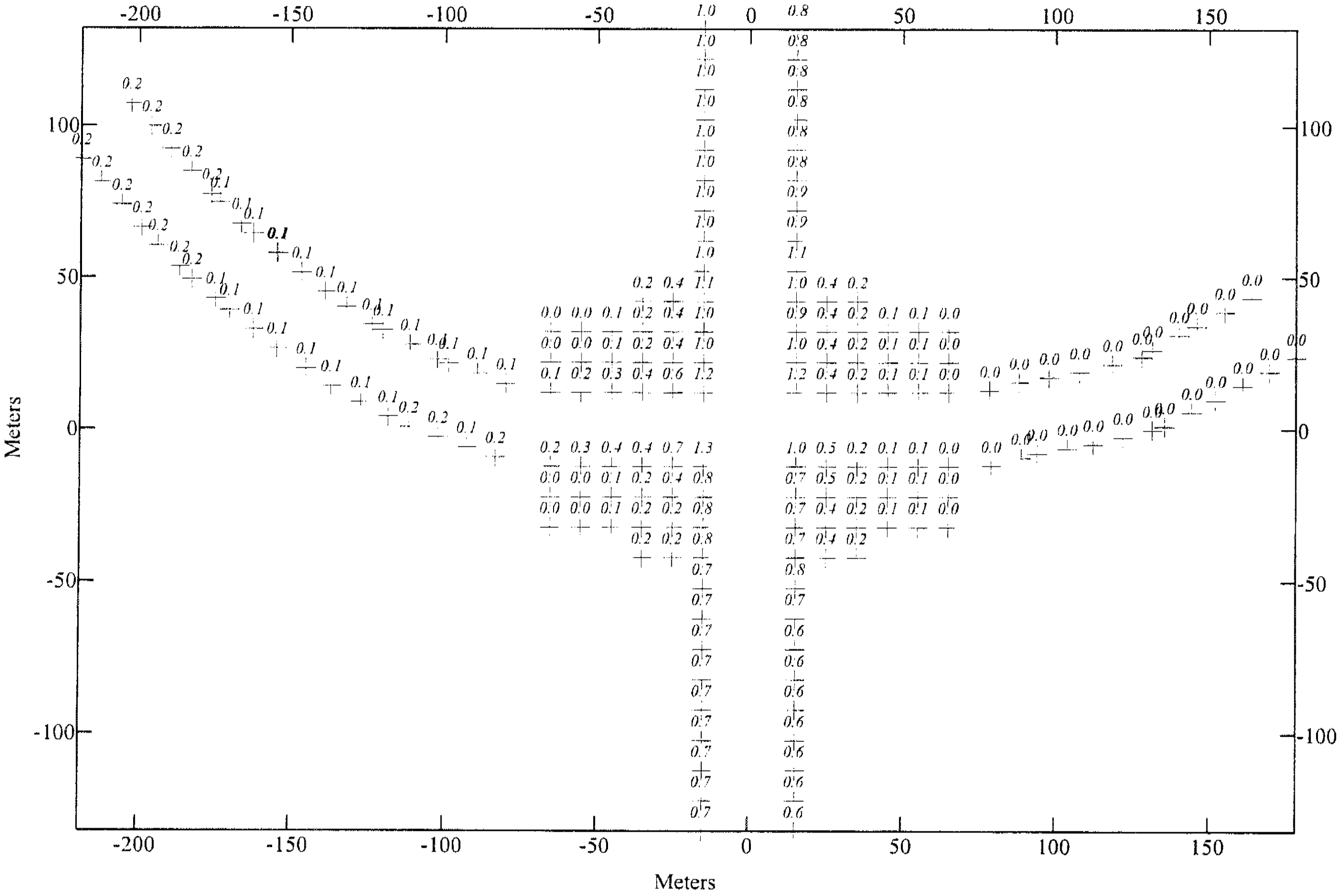
    THE HIGHEST CONCENTRATION OF    1.50 PPM OCCURRED AT RECEPTOR REC70.
```

APPENDIX E

CAL3QHC CONCENTRATION PLOTS

Figure E-1. Hourly CO Concentrations for 2025 - No-Build Case

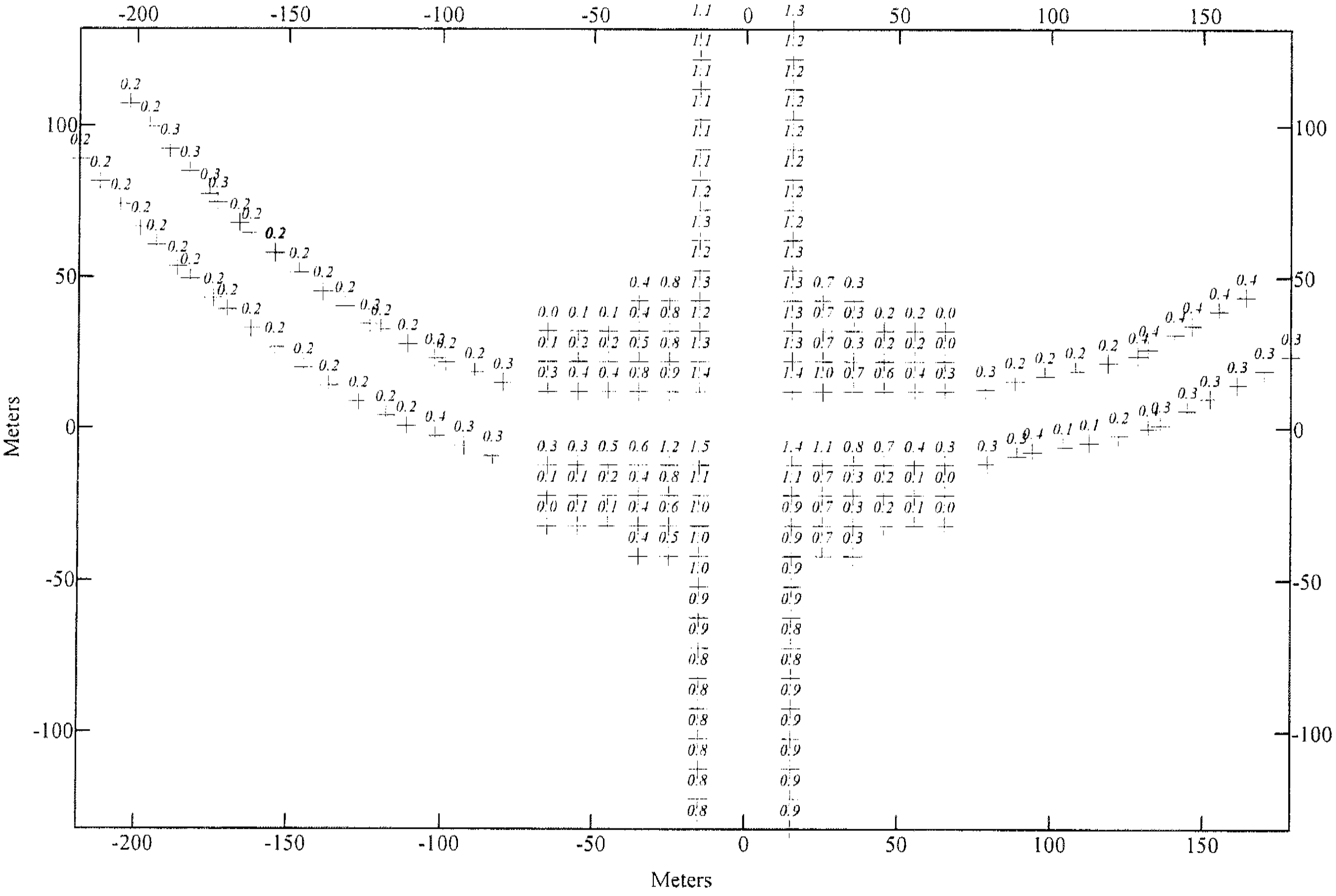
NAAQS = 35 ppm



(Concentrations shown in parts per million.)

Figure E-2. Hourly CO Concentrations for 2025 - Build Case

NAAQS = 35 ppm



(Concentrations shown in parts per million.)