SPACE TRANSFER VEHICLE CONCEPTS AND REQUIREMENTS NAS8-37856 (NASA-CR-184490) SPACE TRANSFER VAS8-37856 VEHICLE CONCEPTS AND REQUIREMENTS. VOLUME 2, BOOK 2: APPENDIX (Martin Marietta Corp.) 119 p Unclas

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FOREWORD

This report, prepared by Martin Marietta Corporation, is submitted to George C. Marshall Space Flight Center, National Aeronautics and Space Administration (NASA), Marshall Space Flight Center (MSFC), Alabama, in response to the DR-5 requirements of contract NAS8-37856, Space Transfer Vehicle Concept and Requirements. It is the DR-5 identified in Data Procurement Document No. 709.

APPENDIX A

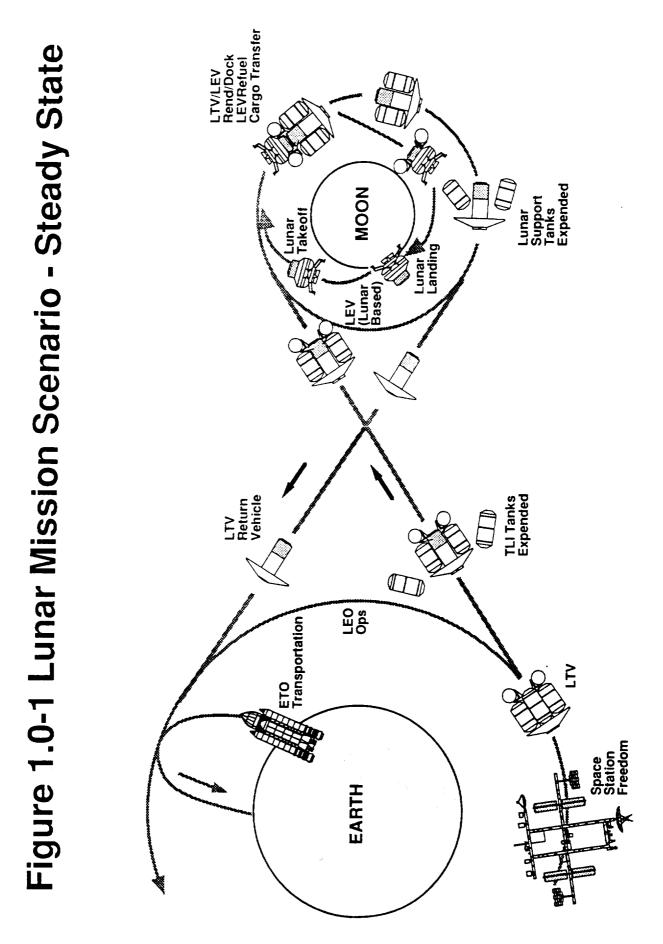
90-DAY STUDY CONCEPT DEFINITION

This appendix describes the work that was performed to define the Lunar transfer vehicle and Lunar excursion vehicle which were part of the "Report of the 90-Day Study on Human Exploration of the Moon and Mars." A detailed concept definition of both vehicles including overall dimensions, mass properties, subsystem definition, and operational flight sequences is contained herein. These data were presented at Interim Review #1 in December 1989.

1.0 MISSION SCENARIO

The steady-state Lunar mission scenario for the 90-day study is depicted in Figure 1.0-1. In this scenario, two separate vehicles, a Lunar transfer vehicle (LTV) and a Lunar excursion vehicle (LEV) are utilized to deliver cargo and crew to the Lunar surface. In the steady-state scenario shown, propellant is delivered to Space Station Freedom using the Earth to Orbit (ETO) Transportation System. After undergoing any required refurbishment and attachment of propellant tanks delivered from Earth, the LTV leaves Space Station Freedom with crew and/or cargo. The translunar injection (TLI) tanks are expended after the TLI burn. The LTV then performs a Lunar orbit insertion (LOI) burn. Once the LTV is in low Lunar orbit (LLO), the LEV acsends from the Lunar surface for rendezvous and docking with the LTV. After completing the docking maneuver, crew and/or cargo along with propellant is transferred to the LEV from the LTV. Once the LEV is fueled and has its crew and cargo, the vehicles separate and the LEV prepares for descent to the Lunar surface. The LTV propellant tanks for supplying fuel to the LEV are then expended and the LTV prepares for return to Space Station Freedom. The LTV engines are retracted, doors in the aerobrake are closed, and the LTV performs a transearth injection (TEI) burn. After the aeropass maneuver, the LTV performs a rendezvous maneuver with Space Station Freedom. The LEV remains on the Lunar surface until the LTV returns months later.

2.0 LTV/LEV CONCEPT DEFINITION



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The LTV/LEV stacked configuration as shown in Figure 2.0-1 is approximately 23 m in total length. The configuration consists of the LTV and the LEV along with their respective crew cabs and cargo. The LTV is a stage and a half concept with 4 expendable drop tanks. There are two separate crew cabs, one on the LTV and one on the LEV. Cargo along with propellant must be transferred from the LTV to the LEV.

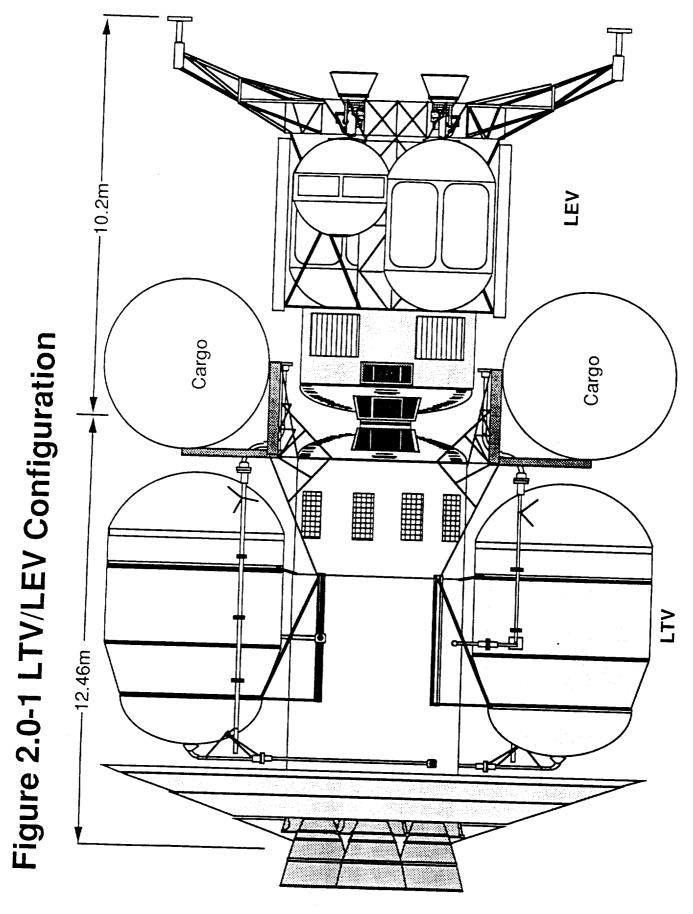
2.1 LTV CONFIGURATION

The basic LTV configuration shown in Figure 2.1-1 consists of a rigid 13.7 m aerobrake and a core vehicle that consists of a propulsion module and a lunar transit crew cab. Drop tank attach structure and feedlines are mounted to the core vehicle.

The aerobrake as shown in Figure 2.1-2 is a 13.7 m (45 ft) diameter rigid structure composed of composite materials and covered with advanced Shuttle-type thermal protection system tiles. A 7.6 m (25 ft) preassembled core with the engine nozzle doors, mechanisms, and tiles installed is delivered to orbit attached to the LTV. The outside periphery of the aerobrake (eight equal segments) is assembled at Space Station Freedom. The aerodynamic pressure environment, TPS (FRCI-12) thicknesses, and weight summary for the aerobrake are shown. The TPS for the aerobrake is tailored into four bands corresponding to the pressure and aeroheating regions. Total dry weight for the aerobrake is slightly over 2 t.

The core vehicle illustrated in Figure 2.1-3 is an integrated structure which includes the propulsion module, the transit crew cab, and the aerobrake attachment structure. The core is an integrated structure to reduce on orbit assembly times and structural weight. The basic core structure consists of a composite shell of graphite/epoxy with eight (8) longerons designed to transfer and distribute engine thrust loads and TLI and LLO tank loads. The longerons are equally spaced at 45° around the core. The engines are mounted on a set of crossbeams which intersect the shell (and longerons) at 0, 90, 180, and 270°. Auxiliary support/stabilizing beams run from each side of the engine mount beams to the other 45° spaced longerons. The aerobrake support is a trussed structure. The crew cab is built into the basic core unit but can be removed and replaced with a skirt of equal structural support. Ring frames are spaced at major interface locations to support drop tank and cargo attachment, with intermediate stiffening rings spaced as required to maintain structural rigidity along the core shell.

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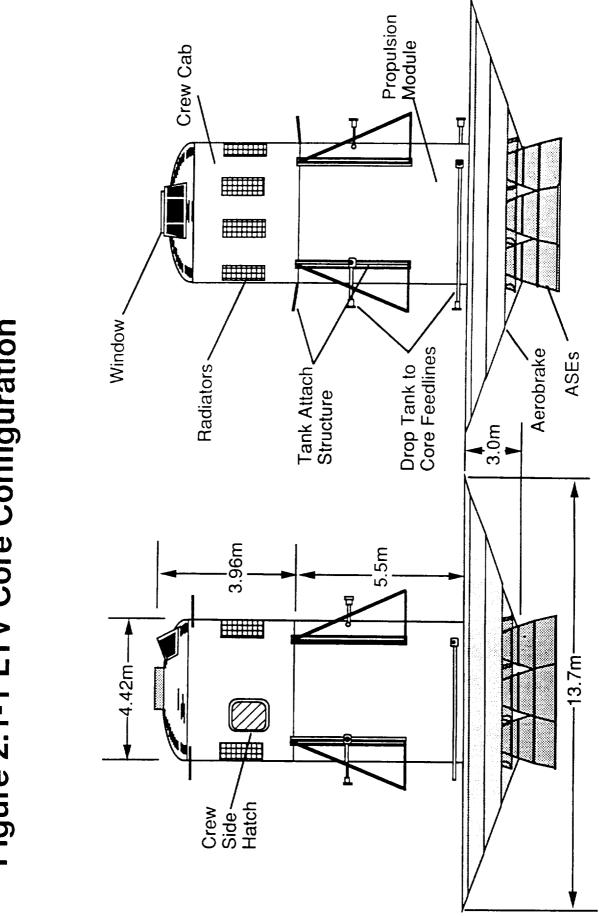
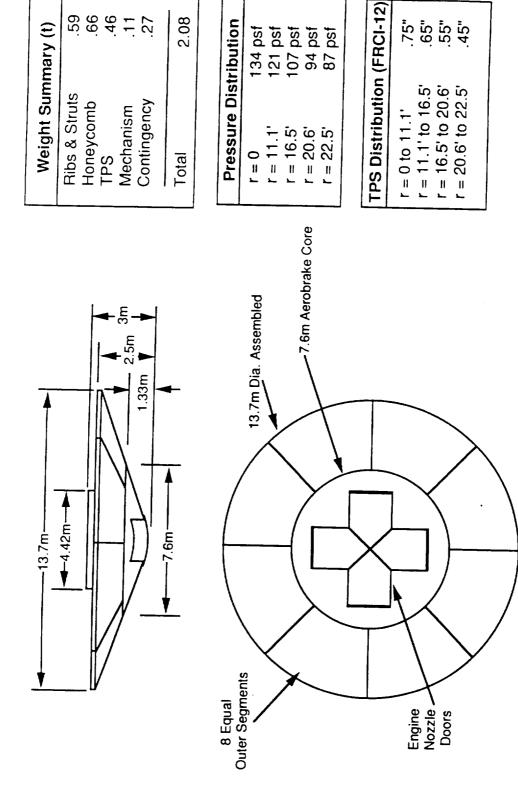


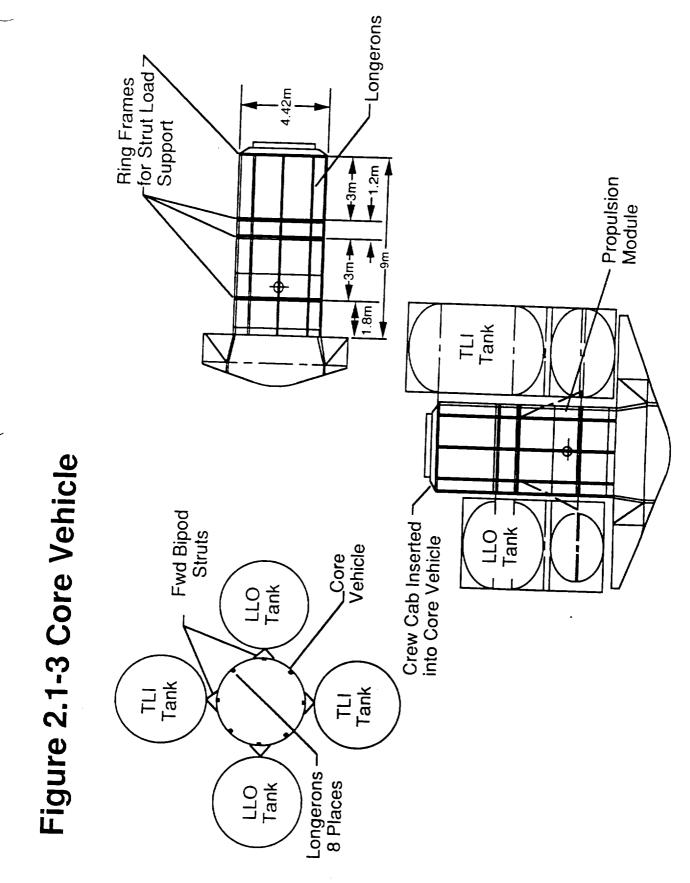
Figure 2.1-1 LTV Core Configuration

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Figure 2.1-2 Aerobrake Overview





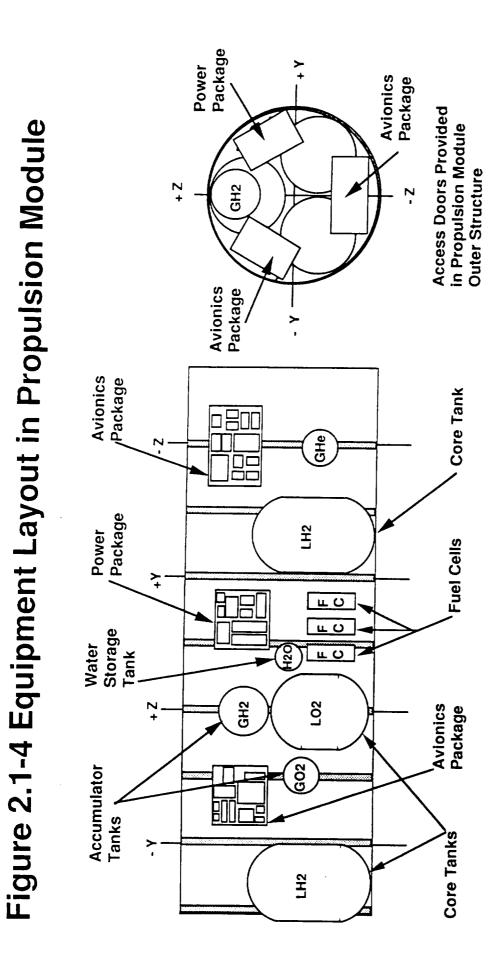
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The core propulsion module, approximatley 5.5 meters in length and 4.42 meters in diamter, includes core propellant tanks, plumbing, other subsystem equipment, and 4 advanced space engines (20,000 lbs thrust each). The three core propellant tanks (1 LO2 and 2 LH2) contain approximately 7 t of propellant. The 2 LO2 tanks are 1.9 m in diameter and 2.46 m in length. The LH2 tank is the same diameter but 3.15 m in length. The relative location for the various LTV subsystems are shown in Figure 2.1-4. The avionics is packaged in two avionics bays and electrical distribution is located above the fuel cells. The accumulator tanks for GH2 and GO2 are located near the LO2 tank. LN2 for crew ECLSS support is contained inside the crew cab. Access doors are provided in the core vehicle outer structure to allow for repairs and maintenance of equipment.

Figure 2.1-5 shows the TLI tanks with their LH2 and LO2 feedline connections mounted to the LTV core vehicle. The LLO tanks are mounted in a similar manner. This plan view indicates the position of the drop tanks around the core vehicle. Each TLI tank is 10.4 m long by 4.42 m in diamter and contains separate oxygen and hydrogen tanks connected by an intertank. Total propellant capacity of each TLI tank is 44.6 t. The two TLI tanks are expended after the TLI burn on the way to the moon. Each LLO tank is about 7 m in length and 4.42 m in diameter and contains separate oxygen and hydrogen tanks. Total propellant capacity of each LLO tank is 22.3 t. The LLO tanks are expended after rendezvous/docking with the LEV and transferring propellant in LLO. Both the TLI and LLO tanks are delivered to Space Station Freedom for each mission using expendable ETO transportation.

The lunar transit crew cab, approximately 4 meters long and 4.42 meters in diameter, contains a side hatch for alternate crew egress/ingress as well as a standard Space Station Freedom berthing ring for attachment to Station. A window on the top of the crew cab allows viewing of the rendezvous/docking procedure while radiators provide thermal heat rejection.

Cargo is attached to the LTV as shown in Figure 2.1-6 utilizing the cargo support racks mounted above the LLO tanks. Also shown is the propellant transfer lines used for transferring propellant from the LTV to the LEV. Details of the cargo and propellant transfer will be discussed in a later section of this document. Preliminary mass properties of the LTV are shown. The total dry weight of the vehicle is slightly over 22 t with the crew module and drop tanks making up the majority of the weight.



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Interfaces to Crew Cab

- Power
- Avionics
 Water
 Oxygen Supply Line

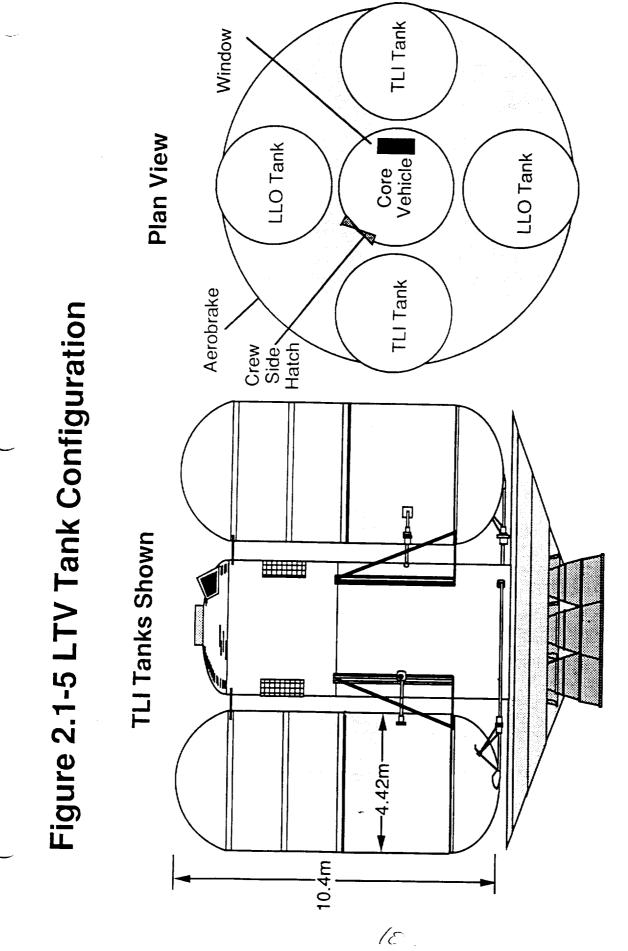
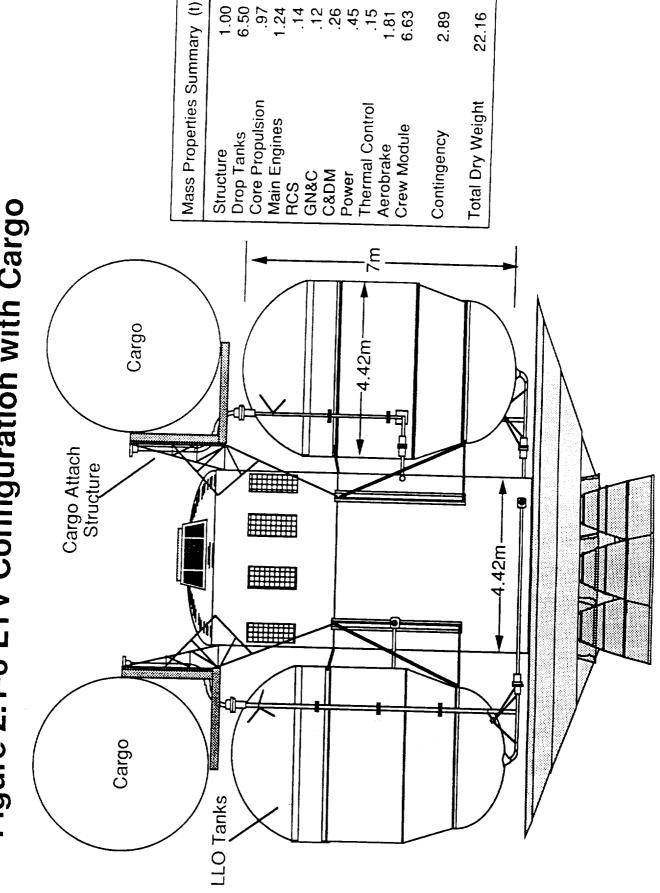


Figure 2.1-6 LTV Configuration with Cargo



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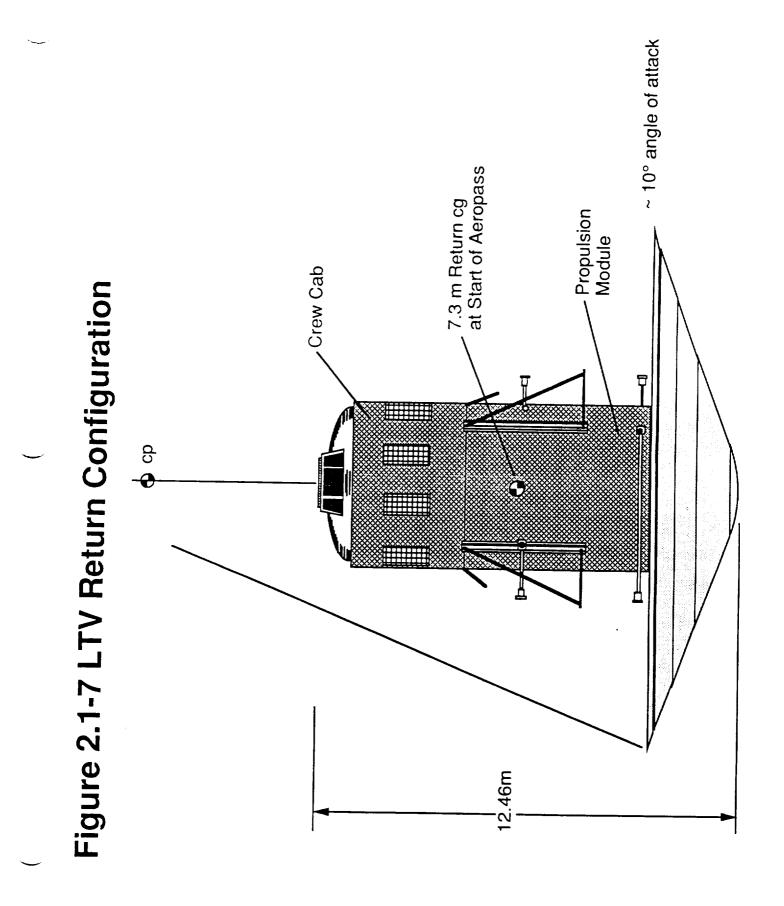
The LTV return configuration is depicted in Figure 2.1-7. The LTV is shown just before the aeropass maneuver begins. The 4 engine nozzles have been retracted and the aerobrake doors have been closed and sealed. The doors will remain closed until the vehicle has returned to Space Station Freedom. 15% of the propellant in the propulsion module core tanks remain for RCS maneuvers around Space Station Freedom. The aerobrake is sized for a 10° angle of attack and 20° wake angle. The cg of the vehicle during the aeropass maneuver is situated inside the propulsion module.

2.2 LEV CONFIGURATION

Side views of the LEV configuration are shown in Figure 2.2-1. The LEV consist of four advanced space engines, 4 landing legs, propellant tanks and support structure, subsystem equipment, the lunar crew cab, and the cargo transfer structure. The overall dimensions are 11.8 m from landing leg to landing leg and 10.2 m from the lunar surface to the top of the crew cab.

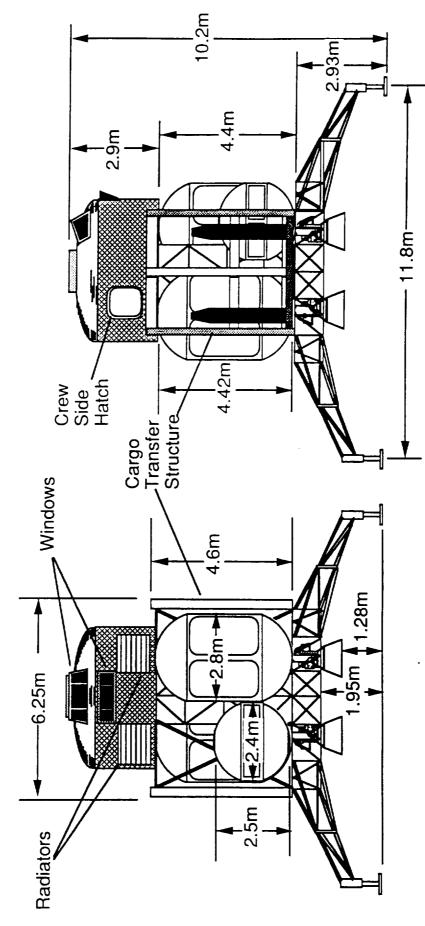
The lunar crew cab is 2.9 m high by 4.42 m in diameter. The lunar crew cab is smaller than the transit cab due to the limited stay in the lunar cab, only during the short descent/ascent to/from the lunar surface and for limited hours on the lunar surface. A window located in the top of the crew cab provides viewing for rendezvous/docking with the LTV and a side window provides viewing for landing operations on the lunar surface. Real time fiber optic imaging may be required to alleviate the problem of large cargo blocking the field of view of the landing legs. A crew side hatch provides egress/ingress on the lunar surface and radiators provide thermal heat rejection.

The core of the LEV contains subsystem equipment along with four propellant tanks (2 LO2 and 2 LH2) that hold 22.4 t of propellant. The LO2 tanks are almost spherical, 2.4 m by 2.5 m. The LH2 tanks are 2.8 m in diameter and 4.6 m long. Since propellant is transferred from the LTV, these four tanks are not structurally designed for wet launch but they do have multi-layer insulation for orbital boiloff reduction. The four ASEs (20,000 lbs thrust each) have no nozzle extensions and are approximately 1.3 m from the lunar surface after landing. The cargo transfer structure is located on either side of the core tanks and allows the cargo to be lowered directly to the lunar surface.









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Figure 2.2-2 shows a plan view of the LEV, the opposite side view of the LEV, and a preliminary mass properties summary of the vehicle. The position of the crew cab and windows, propellant tanks, and cargo mechanism is shown along with the 16.8 m diagonal spacing between the landing legs. Total dry weight of the LEV is about 9.2 t with the crew cab about one third of the total dry weight. The LEV configuration with cargo is illustrated in Figure 2.2-3. The chart illustrates how the cargo is attached to the cargo transfer mechanism and can be lowered directly to the lunar surface between the landing legs for cargo less than 6.1 m in total length.

2.3 SUBSYSTEM DEFINITION

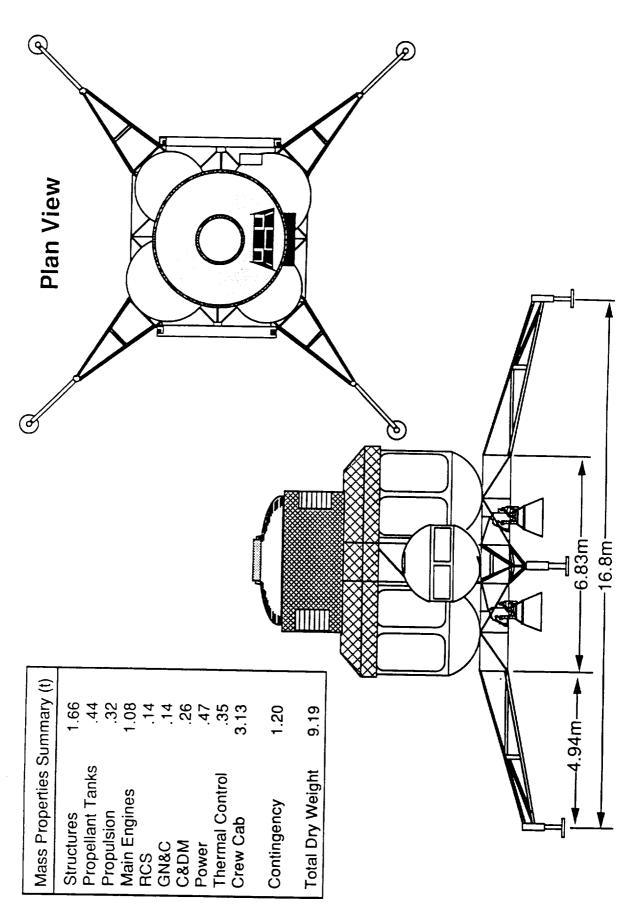
2.3.1 Aerobrake

A detailed view of the aerobrake is shown in Figure 2.3.1-1. The aerobrake is a rigid spherical sector-truncated cone composed of composite graphite/polyimide structure and honeycomb panels and covered with advanced Shuttle-type thermal protection system tiles (FRCI-12). The honeycomb outer panels are foam with aluminum facesheets (4 layers of .005 inch). The thin shell surface is supported by radial ribs that extend outward from a 7.6 m (25 ft) diameter central spherical core to a 13.7 m (45 ft) peripheral ring. Radial ribs are spaced at the panel interfaces and at the center of each outer panel. Circumferential stiffening rings are placed at the 7.6 m diameter and at the 13.7 m diameter locations. 16 support struts that extend from the core to the outer panels (2 per panel) also provide additional support. An isometric view of the aerobrake structure is shown in Figure 2.3.1-2. The 16 radial ribs, the 2 circumferential stiffening rings, and the 16 support struts are shown along with the core support structure and engine support structure.

Four, five-sided, pentagon-shaped doors as illustrated in Figure 2.3.1-3 provide openings for the 72" engine bells/nozzles plus clearance and misalignment tolerances. The doors open toward the outside of the aerobrake and remain open during all but the final aeropass operations. To open, the doors translate slighly outward (straight up motion) before being rotated about a hinged interface to preclude interference with the aerobrake TPS. Small motors designed to be failop, fail-op, fail-safe are used to drive the translation and hinge mechanisms. Operations are reversed for closure. The pentagon shape allows the doors to be supported by an aerobrake cap member running crosswise between the engines. Each door also contains a locking mechanism which fastens the door to the aerobrake cap member to preclude any tendancy of the door to open

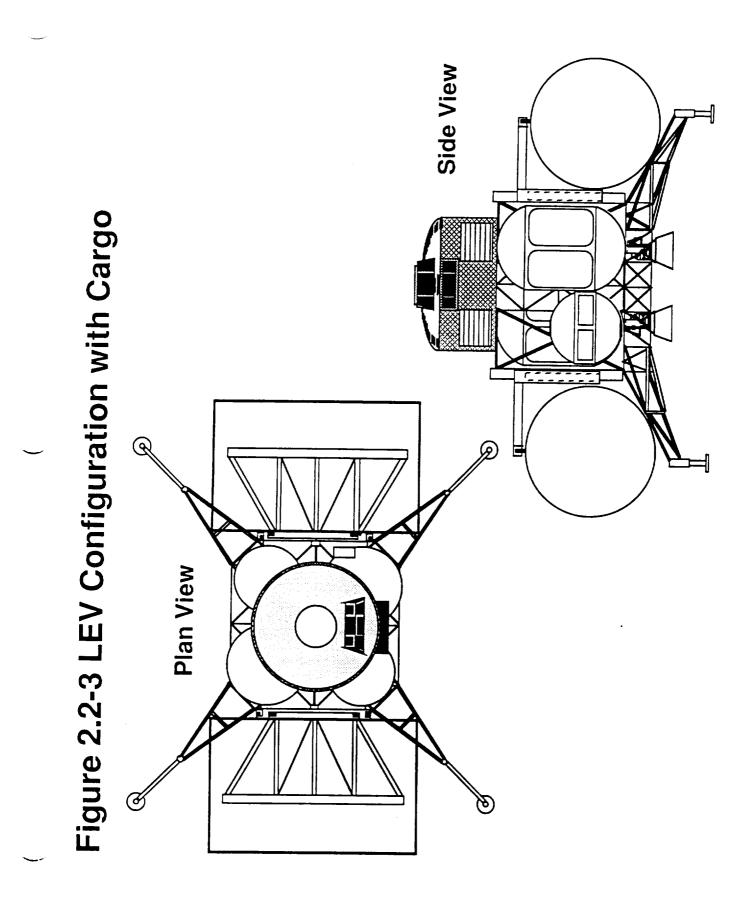
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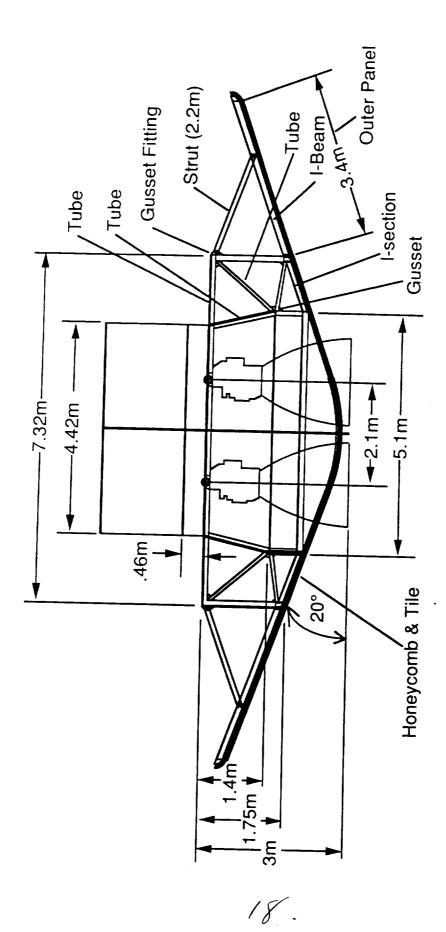
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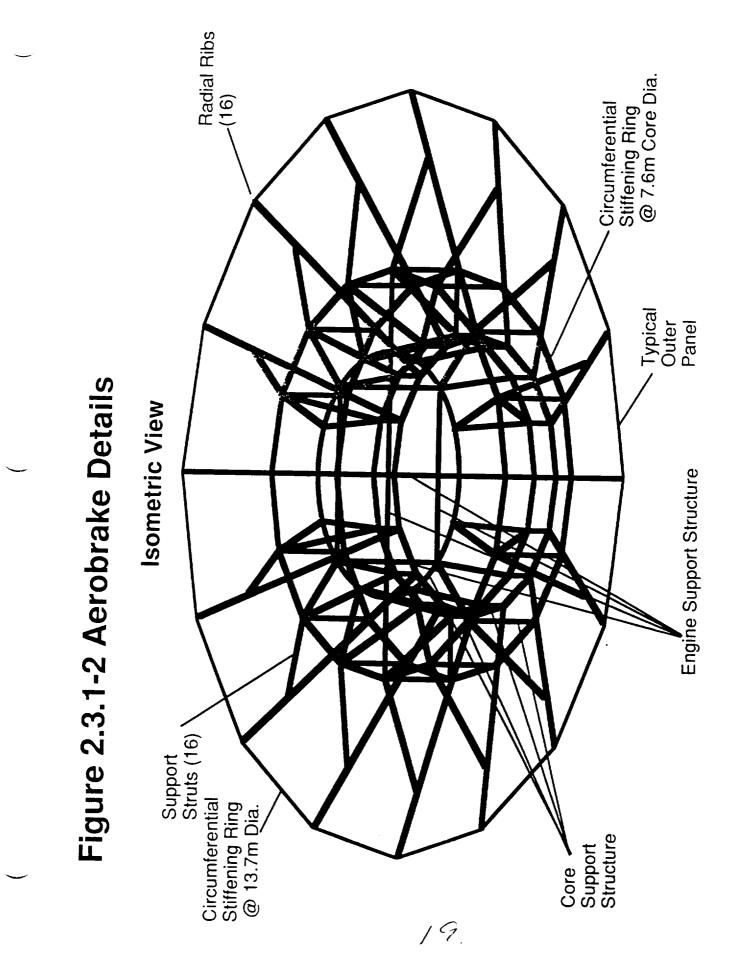
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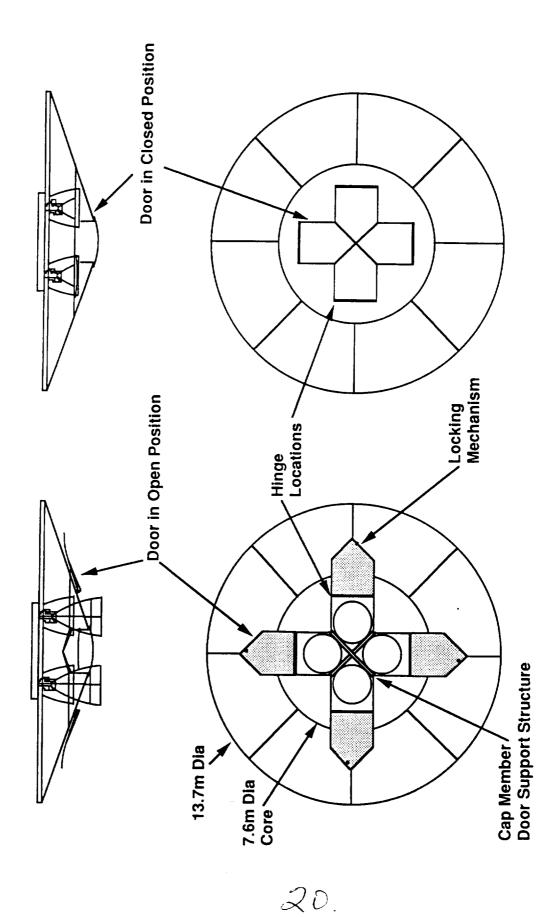
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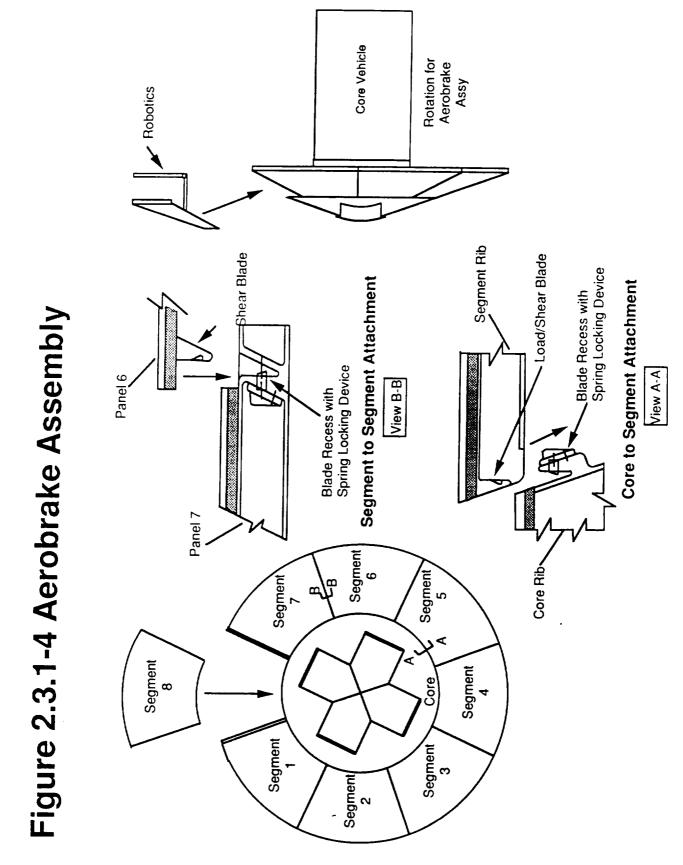


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during the aeropass operations. Provisions are included for emergency closure utilizing EVAsuited personnel if door mechanisms fail. As an option, the doors could be translated slightly outward (straight up motion), then slid back along the outside of the brake utilizing guide rails on the inside of the brake.

As illustrated in Figure 2.3.1-4, the eight outer aerobrake segments are attached to the aerobrake central core with the aid of Space Station Freedom robotics. The central core is attached to a daisy-wheel type structure and is rotated to allow attachment of each segment. The first of the eight panels has three radial ribs for support - one rib in the center of the panel and a rib on each side of the panel to provide support for the second and eighth segment. Panels two through seven are common and have two ribs each - one rib in the center of the panel and one rib on the side to provide support for the panel that attaches to it. The eighth and final panel to be attached has only one rib in the center since it is supported by the ribs on panels one and seven. Each outer segment will have been prefitted on the ground and clearly numbered to ensure a matched fit at station. The eight segments are snapped into place utilizing robotics. Each segment has shear pins/blades which fit into receiving lugs on the aerobrake central core and adjacent segments. These selflocking devices, spaced approximately one foot apart, minimize the need for EVA support to attach the segments. After each segment is attached to the central core with the shear pins, support struts must be attached on the backside of the aerobrake between the segment and the central core. The struts provide the necessary structural support for attaching the next panel as well as providing support during aeropass operations. The struts are attached to the individual segments and are pinned to the central core after initial segment attachment. EVA inspection of the assembled aerobrake may be required to ensure all panels are secured and locked in place.

An optional assembly technique for the aerobrake utilizes folded, deployable structure as shown in Figure 2.3.1-5. The structural ribs of each of the eight outer segments would be folded back against the central core of the aerobrake (toward the vehicle) in the ETO transportation mode using a hinged mechanism at the central core interface. The backside support struts would be prepinned to the central core and folded along with the ribs. The structural ribs of the segments would then be deployed (motor driven) and locked in place once the vehicle is at the station minimizing the EVA requirement. The backside support struts would then be pinned to the ribs using robotics. The segment panels would then be attached to the extended rib/strut configuration with self-locking devices using the station robotics. Inspection and verification of the assembled aerobrake could be performed by EVA suited crewmen. As an option to the above configuration,



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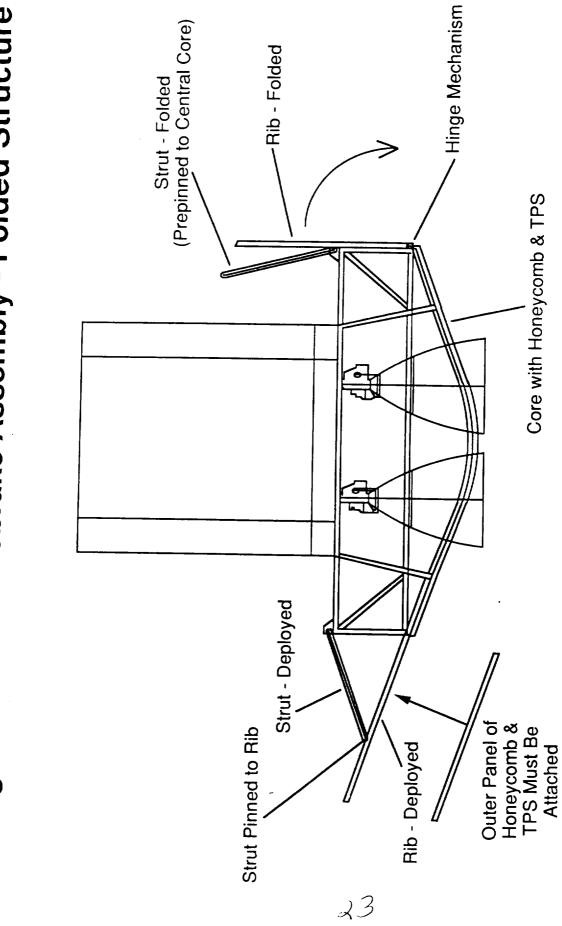
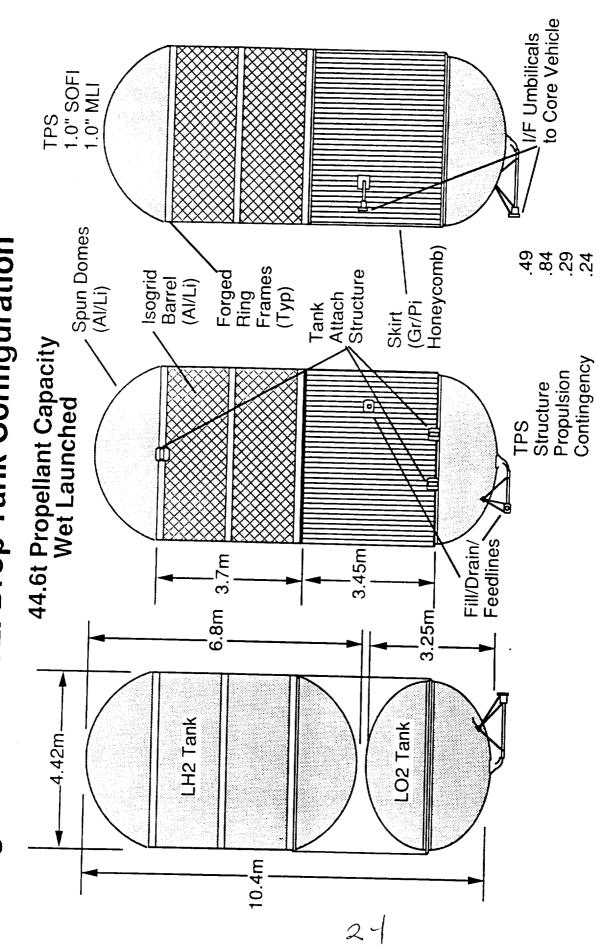


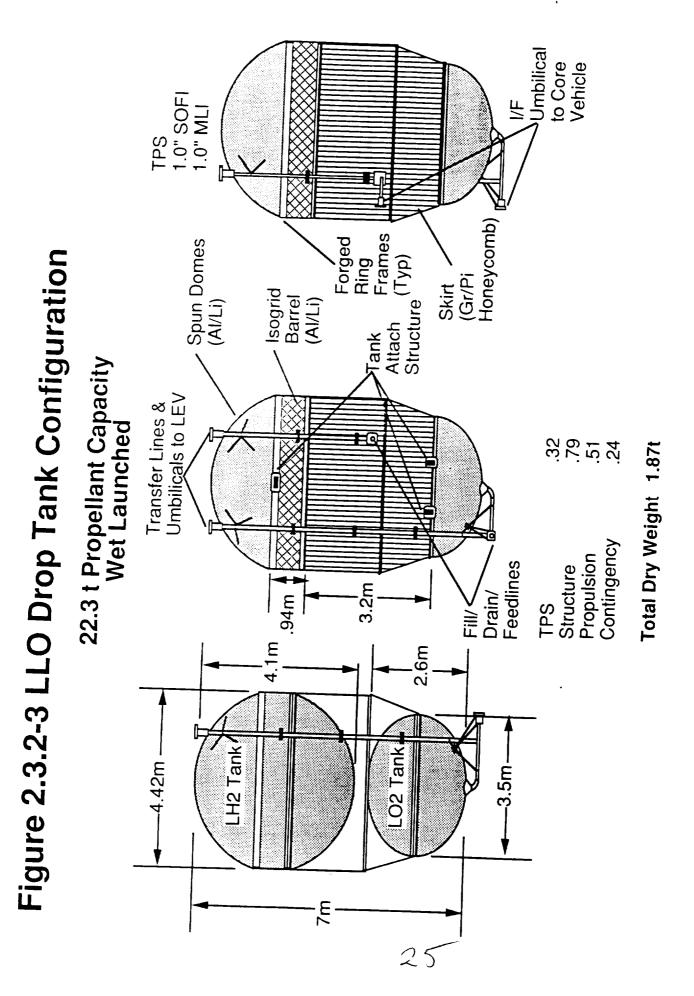
Figure 2.3.1-5 Aerobrake Assembly - Folded Structure

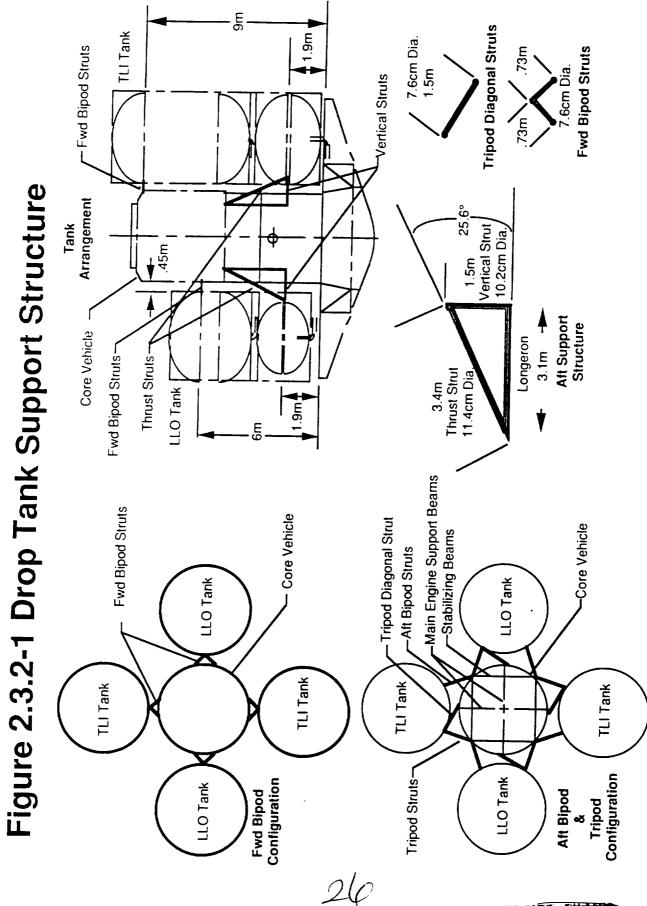
Figure 2.3.2-2 TLI Drop Tank Configuration



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Total Dry Weight 1.87t





the backside support struts could be jointed and prepinned to the panel ribs and central core. The struts could be automatically deployed and locked in place along with the structural ribs. This would require struts that are complex two-piece configurations, and they would be somewhat heavier than the one-piece versions described above. Segment panels could be attached in the same manner as described above.

2.3.2 Drop Tanksets

As shown earlier in Figure 2.1-5, the LTV configuration consists of four drop tanksets (2 TLI tanksets and 2 LLO tanksets). These tanksets contain all the propellant required to perform the lunar mission (that needed by both the LTV and LEV). The tanksets are delivered wet to Space Station Freedom using ETO transportation. Once at Station, they are structurally attached to the LTV and fluid connections are made in preparation for the lunar mission. Propellant is routed from these tanksets through the LTV core tanks to the engines. Propellant for the LEV is contained in the LLO tanksets. The TLI tanksets are expended after the early TLI burn and the LLO tranksets are expended in LLO after the propellant has been transferred to the LEV.

The drop tanksets are mounted to the core vehicle in similar fashion as the ET/Orbiter attachment which is a three-point mount – two aft and one forward. Details of the tankset attachment is shown in Figure 2.3.2-1. One aft support is a tripod, making it fixed, while the other two mounts are bipods. The aft bipod permits lateral pivot motion and the forward bipod allows fore/aft motion. The aft bipod and tripod structure is attached to the LTV core vehicle and mated to the drop tanks at the LO2 tank ring frames. The forward bipod structure is attached to the LTV core vehicle and mated to the drop tanks at LH2 tank ring frames near the end of the tank. After structural mate is complete, fluid connections are made. The drop tankset/core vehicle propellant interfaces (two per tank) are located at two aft umbilical assemblies adjacent to, but separated from the two aft structural interfaces. The disconnects contain shutoff valves that are closed prior to retraction of the umbilical assembly.

The TLI drop tankset consists of an LH2 tank, an intertank, and a LO2 tank with corresponding feedlines and umbilicals. The tankset shown in Figure 2.3.2-2 is designed to be launched wet in the ETO transportation system. The LH2 tank has aluminum-lithium spun domes and an isogrid barrel section. The intertank is a graphite/polyimide honeycomb structure. The LO2 tank has aluminum-lithium spun domes with a forged ring center frame. The TPS consists of

1.0" of SOFI for prelaunch boiloff reduction and one inch of MLI for on orbit boiloff control on both tanks. The diameter of the TLI tankset is 4.42 m and the overall length is 10.4 m. Each TLI tankset contains a total of 44.6 t of propellant which is utilized during the TLI burn. Preliminary dry weight of the TLI tankset is shown as 1.87 t.

The LLO drop tankset as shown in Figure 2.3.2-3 is very similar to the TLI tankset with an LH2 tank, an intertank, and a LO2 tank. The LLO and TLI tanksets have similar TPS and are constructed with similar materials and manufacturing techniques. However, the LLO tankset not only has feedlines and umbilicals to the LTV core vehicle but also has transfer lines and umbilicals to fill the LEV. The diameter of the LLO tankset is 4.42 m at the LH2 tank diameter but tapers to 3.5 m at the LO2 tank location. Overall length is 7 m. Each LLO tankset contains 22.3 t of propellant which is utilized for the LLO burn and for supplying the LEV. The LLO tankset weights are similar to those of the TLI tankset because of the additional transfer lines to the LEV and the addition of a full communication device in each tank for propellant transfer.

2.3.3 Power

The LTV baseline power system utilizes current STS fuel cells which are significantly improved from the ones used for Apollo missions. These STS units are lighter (91kg) and produce 6 to 8 times more power (7 kW average) which results in fewer units and more efficient packaging. The fuel cells are packaged in the LTV skirt region and utilize propellant boiloff for fuel (450kg of H2 and O2 in 3 days). Water is produced as a byproduct (660 L in 3 days) and could be piped to the crew cab.

On long duration missions, solar arrays are required for power supply. The solar arrays as illustrated in Figure 2.3.3-1 must be extended out at least 12 feet from the core vehicle to clear the drop tanks and avoid shadowing from the tanks. Shadowing from overhead cargo may require further extension of the arrays. The arrays and masts are stored in a 6 foot long cannister recessed into the side of the core vehicle to prevent interference problems during ETO transportation. Batteries are also required for backup power supply when the arrays are not deployed. Fuel cells offer distinct advantages over solar arrays for short duration lunar missions in areas of weight, packaging, dependability, and eliminating the need for batteries. A weight comparison for the LTV power system with fuel cells and with solar arrays is provided.

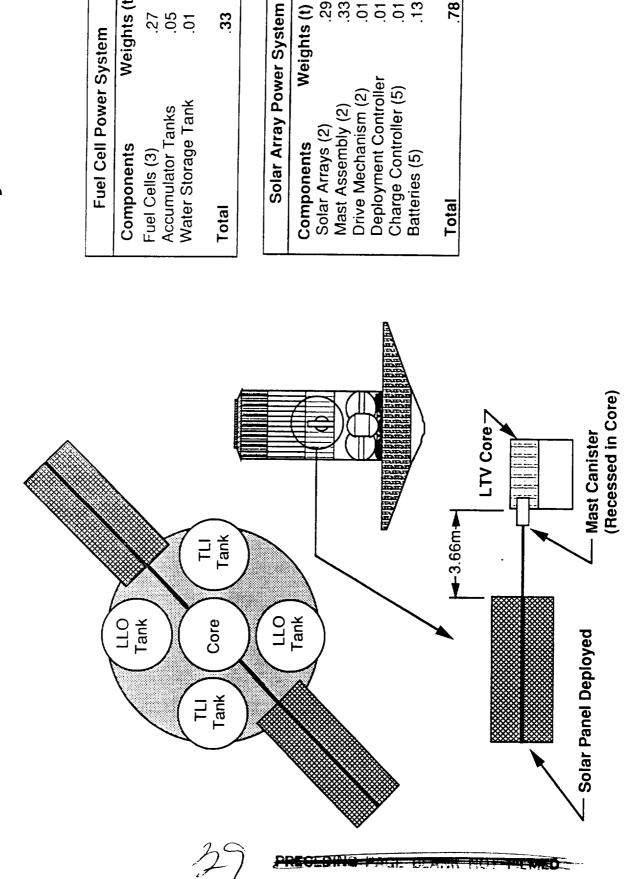
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Figure 2.3.3-1 Power System Solar Arrays vs Fuel Cells

Weights (t)

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Weights (t)

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2.3.4 Propulsion

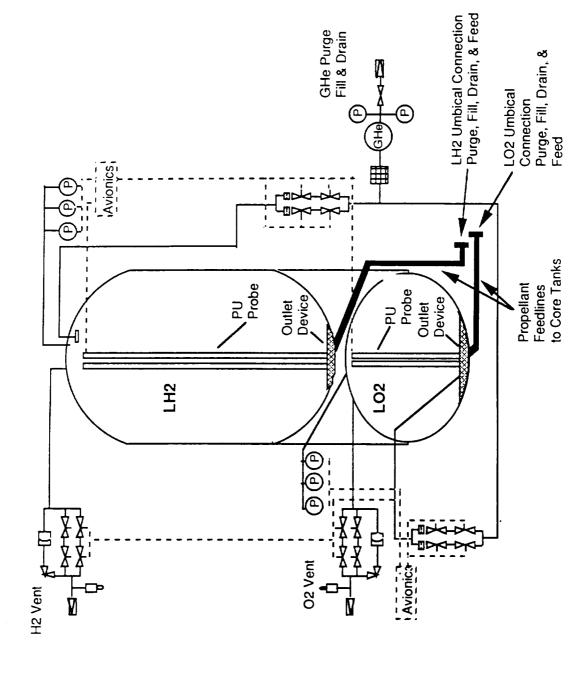
The TLI tankset propulsion schematic shown in Figure 2.3.4-1 indicates the various subsystems on the TLI tanksets. Gaseous helium was baselined as the tank pressurization systems. The LH2 and LO2 feedlines are also used for fill, drain, and purge as well as for feed for the engines. Each tank has a propellant outlet device and a propellant utilization probe. The LLO tankset propulsion schematic shown in Figure 2.3.4-2 indicates the various subsystems on the LLO tanksets. Each tank will have a full communication device for propellant transfer from the tanks to the LEV during lunar orbit. The transfer will be accomplished using cryo pumps. Gaseous helium was baselined as the tank pressurization systems. The LH2 and LO2 feedlines are capable of transferring propellant to the LTV and LEV and are also used for fill, drain, and purge.

As shown in the cross feed schematic in Figure 2.3.4-3, propellant is transferred from the drop tanksets to the core tanks before being routed to the engines. The cross feedline from the drop tanks to the core vehicle tanks is shown. The system is split into two zones taking propellant from one TLI and LLO tankset. The interfaces are set up so that there is no left or right tankset requirement. The zoning allows for equal propellant flow and reduces the required amount of linear feedline. Figure 2.3.4-4 shows the overall location of the subsystems for the LTV core tanks. The LO2 and LH2 cross feed system from the drop tanksets are connected to the core tanks to ensure that the LTV will always have propellant in case of mission abort. Gaseous helium is used for tank pressurization. GO2 and GH2 is used to fuel the reaction control system as well as providing fuel to the fuel cells.

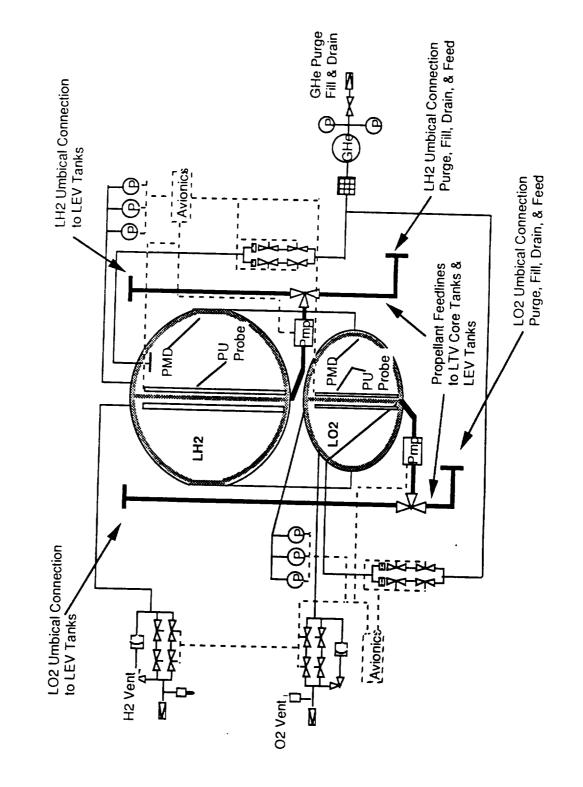
A trade study was conducted to determine the effect of different numbers and thrust levels of engines for the LTV. With only one or two engines, the thrust to weight ratio is very low and the vehicle incurs large gravity losses. As the number of engines increase, the gravity losses approach zero. For 20,000 lb thrust ASEs, the breakeven point is somewhere around 5 engines. However, another parameter that had to be considered if a common engine was to be used on the LTV and LEV was the throttling ratio of the engine. Based on an LEV throttling ratio constraint of 20:1, 4 engines (20,000 lb thrust ASEs) are required for the LEV. Therefore, based on gravity losses and throttling requirements, 4 ASE (20,000 lb thrust each) were baselined for both the LTV and LEV.

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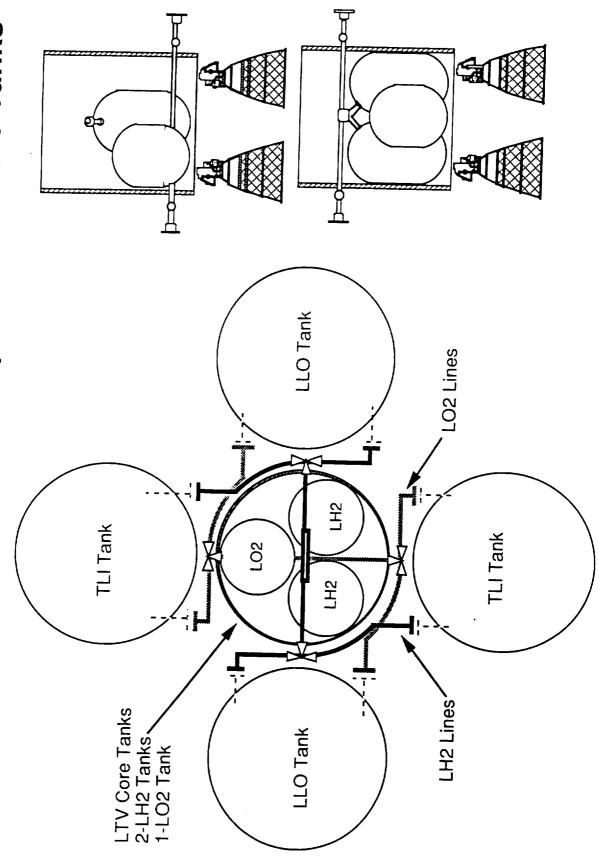


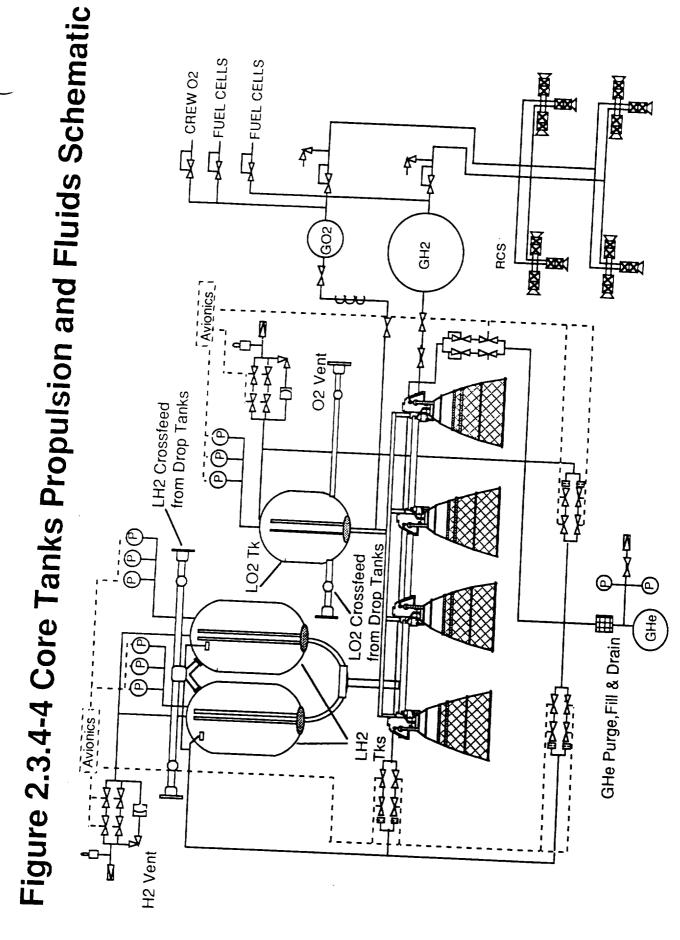




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A trade study was performed to evaluate preliminary insulation concepts for the LTV TLI and LLO drop tanksets. The analysis focused on the LH2 tanks since they represent the worst case for boiloff. Ground performance for various insulation configurations were determined simulating the conditions inside the ETO transportaion vehicle which was assumed to be continuously purged with gaseous nitrogen while on the launch pad. Various thicknessess of Spray-On-Foam-Insulation (SOFI) were analyzed. As expected, the boiloff rate was minimized as the SOFI thickness increased. However, since the insulating effect of the SOFI is marginal on orbit, minimizing the SOFI thickness is desirable. Based on External Tank experience and a review of Shuttle Centaur requirements, 2.54 cm of SOFI was baselined for both the TLI and LLO tanksets. The on orbit boiloff was estimated for three configurations of multi-layer insulation (MLI) varying from 1.3 cm to 5.0 cm in thickness. Since a combination of SOFI and MLI will be required on the tanks for ground and on orbit thermal control, the total weight penalty of insulation and boiloff was calculated for various SOFI/MLI combinations. Assuming a thirty day on orbit period before the mission begins, the combination of 2.54 cm of SOFI and 2.54 cm of MLI provided the lowest weight penalty and was baselined for the tanksets.

A trade study was also performed to evaluate the insulation concepts required for the LEV core tanks while on the lunar surface and on orbit. As stated earlier, the LH2 tanks were examined since they represent the worst boiloff. Various thicknesses of MLI, ranging from 1.3 cm to 10 cm were evaluated. The lunar surface conditions represented the worst case thermal environment for the LEV core tanks, particularly during the lunar cycle. Shading of the tanks during the lunar day is desirable to limit the boiloff. Only passive insulation concepts were considered, but further reductions in boiloff could be realized if active cooling such as mechanical refrigeration or a vapor-cooled shield were added. Based on the analyses, an insulation configuration of 5.0 cm of MLI was chosen as the baseline insulation concept for the LEV core tanks. This insulation concept will provide an LH2 boiloff of approximately 0.25% per day while on the lunar surface and 0.10% per day while on orbit.

2.3.5 Other Subsystems

The various subsystems for both the LEV and LTV are shown in Figure 2.3.5-1. Except for the automated landing system on the LEV, commonality exists between vehicles for all subsystem components. All subsystems are man-rated, redundant, fault tolerant (configured to be

Figure 2.3.5-1 LTV/LEV Subsystem Description

LTV/LEV SUBSYSTEM COMMONALITY

REACTION CONTROL SYSTEM Accumulator Tanks Thrusters Valves & Lines Conditioning Units

GUIDANCE, NAVIGATION & CONTROL

Flight Controller IMU Processor Thrust Controller GPS/Deep Space Receiver Rendezvous & Docking Radar System Collision Advoidance System

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LEV UNIQUE SUBSYSTEM

Automatic Landing System

ELECTRICAL POWER

Fuel Cells Radiators Residual H2O System Reactant Tanks (LH2 & LO2) Power Distribution & Management Valves & Lines

COMMUNICATION & DATA HANDLING

GPS/Deep Space Antenna System STDN/TDRS Transponder 20W RF Power Amp S-Band RF System VHF System Ku Band System Video & Imaging Processor System Data Processing and Storage System TDRSS Health & Instrumentation Monitoring System Central Computers 12:21 PM 2/15/91

fail op, fail op, fail safe) to ensure crew safety. A more detailed listing of these subsystem components were generated to determine mass properties.

3.0 ON ORBIT OPERATIONS

3.1 CARGO TRANSFER

During steady state operations, cargo is delivered via the ETO transportation system and attached to the LTV at Space Station Freedom. The LEV is waiting on the lunar surface for the LTV to arrive in LLO. The LEV will then ascend from the surface and rendezvous and dock with the LTV in LLO. The cargo on the LTV must be autonomously transferred from the LTV to the LEV for delivery to the lunar surface.

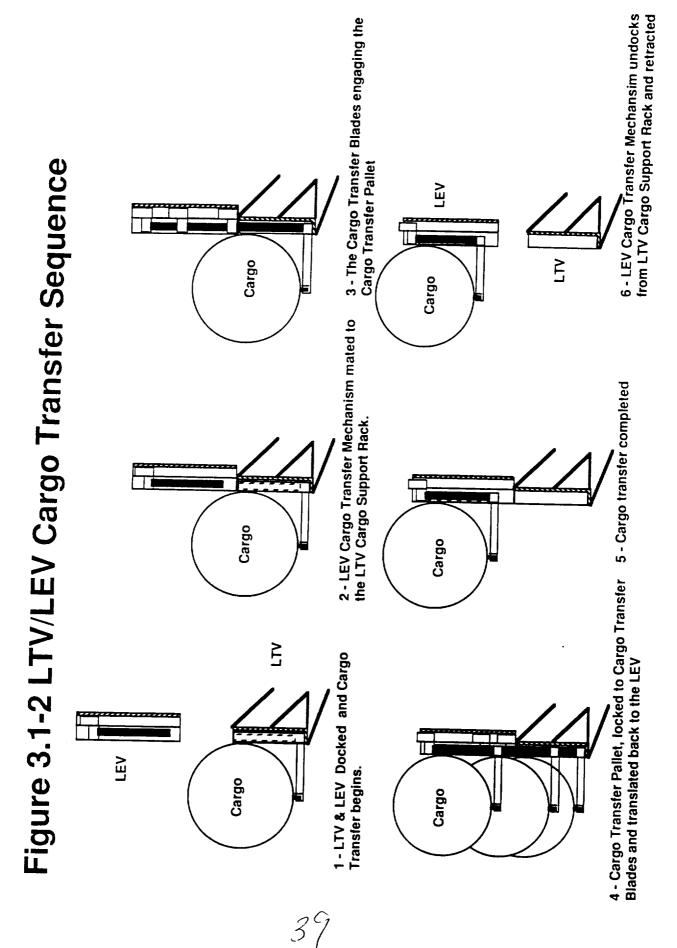
Cargo is mounted to the LTV as shown in Figure 3.1-1 via a cargo transfer pallet which consist of a "L" shaped structure housing the cargo pick up points. A payload support structure on the LTV has guide rails built into it to seat the cargo transfer pallet (CTP) and automatically lock the CTP into place. Cargo transfer between the LTV and LEV is achieved by using a mechanism similar to a forklift mounted on the LEV. The forklift type blades engage the payload support structure which releases the mounting pins holding the cargo to the LTV and locks the cargo to the blades.

Figure 3.1-2 illustrates the cargo transfer sequence between the two vehicles in LLO. Cargo is mounted to the cargo transfer pallet. The CTP with cargo is then mounted into the payload support structure on the LTV. The cargo transfer pallet is held in place with latching pins that automatically activate via a tripping mechanism when the CTP is seated. Sensors will indicate that the pins are seated. After the docking maneuvers between the LTV and LEV are completed at LLO, the cargo transfer operation is instituted when the cargo alignment docking interface (CADI) unit, is raised from the LEV and mates with the payload support structure. The alignment device consist of two tapered pins that mate into the respective receptacles on the payload support structure. Once the alignment is made, the two forklift type blades are raised from the LEV on guide rails and engage the CTP. This action releases the mounting pins holding the CTP to the payload support structure and locks the CTP to the blades. The blades then retract down the guide rails to the LEV. The CADI unit is then undocked and lowered back to the LEV completing the transfer sequence.

		Front View	Unit consist of the Cargo Alignment Docking Interface Unit, Guide Rails and Transfer Blades	
argo Transfer Components	tructure Cargo Transfer Pallet (CTP) (Transfers from LTV to LEV)	Side View Plan View Fr Fr	Top View	Side View
Figure 3.1-1 Car	LTV Payload Support Struc	Front View		

38

LTV/LEV Docked Prior to Cargo Transfer



IR#1/CD28

3.2 PROPELLANT TRANSFER

During steady state operations, propellant is delivered in the TLI and LLO tanksets via the ETO transporation system and attached to the LTV at Space Station Freedom. The steady state mission scenario is the same as that described in the cargo transfer operation. The LEV core tanks are essentially empty of propellant once the LEV and LTV have docked. Propellant in the LLO tanksets on the LTV must be autonomously transferred from the LTV to the LEV core tanks to provide propellant for the LEV to continue its mission.

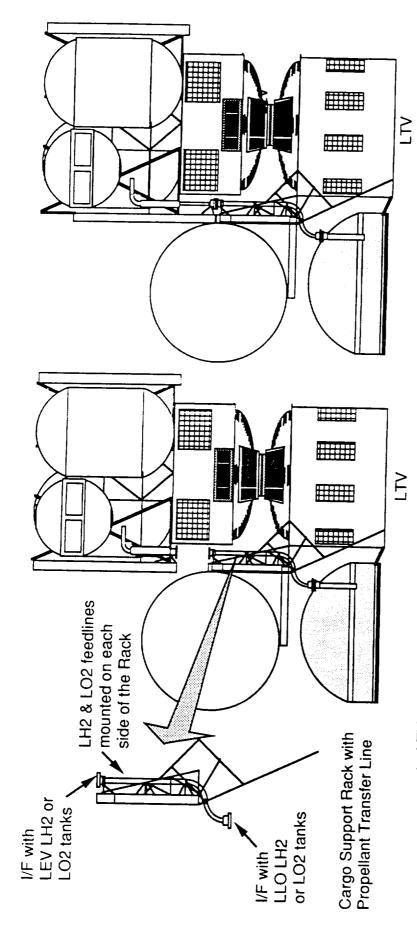
Figure 3.2-1 illustrates the propellant transfer operation that is taking place in conjunction with the cargo transfer operation. In order to transfer propellant from the LLO tanksets to the LEV, interface feedlines (LO2 and LH2) are mounted in the cargo support rack. After the vehicles are docked, the cargo transfer mechanism extends from the LEV and mates with the cargo support rack. This allows the LEV crossfeed to extend using a series of internal bellows and connect with the LO2 and LH2 interfaces on the cargo support rack. Propellant is then transferred using the cryo pumps located in the LLO tanksets. The connecting sequence is reversed once the propellant has been transferred.

3.3 CARGO UNLOADING ON LUNAR SURFACE

Cargo unloading on the lunar surface will be similar to that of on orbit transfer of the cargo from the LTV to the LEV. The forklift -like mechanism mounted on the LEV will be used for transfer. The various positions of the cargo once attached to the LEV are shown in Figure 3.3-1. The cargo is lowered to just below the crew cab for better viewing during landing on the lunar surface. The cargo can then be lowered along the transfer mechanism to heights which allow for unloading to transporters or others means for lunar deployment. Figure 3.3-2 illustrates an option for unloading cargo directly onto a lunar transporter. After the LEV lands on the lunar surface, the transporter will be positioned under the cargo. Guide rails will guide the cargo directly to the transporter using the forklift mechanism on the LEV. Once the cargo is on the transporter, the forklift blades will unlink and retract back to the LEV. The LEV configuration lowers the cargo to within .9 m of the lunar surface if the cargo fits between the landing legs (< 6.1 m).

4.0 MANIFEST DATA

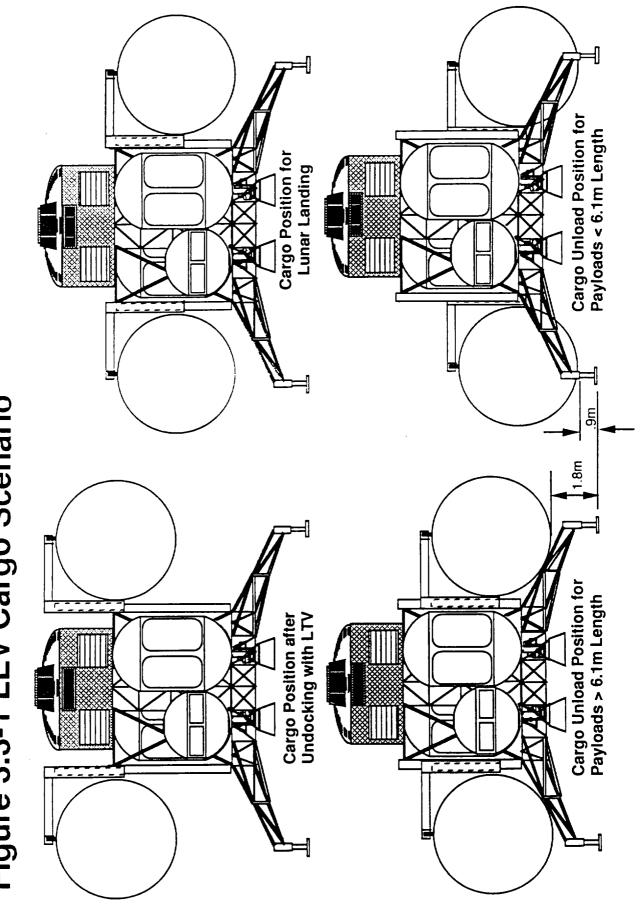
Figure 3.2-1 Propellant Transfer from LTV to LEV



41

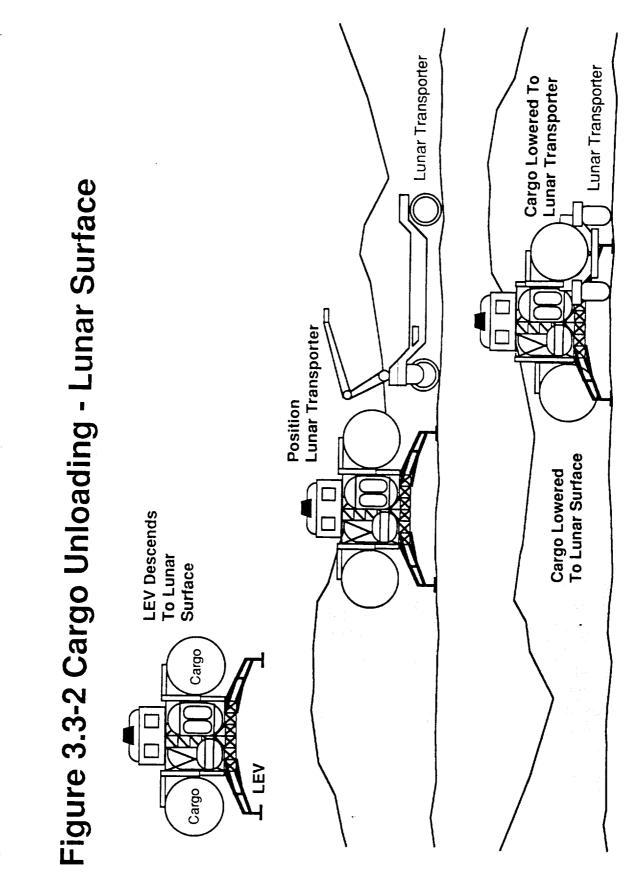
1 - LTV/LEV docked and ready to begin Cargo and Propellant transfer. The Cargo Transfer Mechanism will extend from the LEV, and align with the Cargo Support Rack. This will bring the propellant Interface into contact and allow for the refueling of the LEV before the cargo is transferred.

2 - The Cargo Transfer Mechanism has mated with the Cargo Support Rack. When the CTM is extended the LEV Propellant Interfaces (LH2 & LO2) mounted on each side of the CTM are also extended through use of a series of internal bellows. This allows for the linear motion the I/Fs need to complete the hookup and the propellant is then transferred.



42

Figure 3.3-1 LEV Cargo Scenario



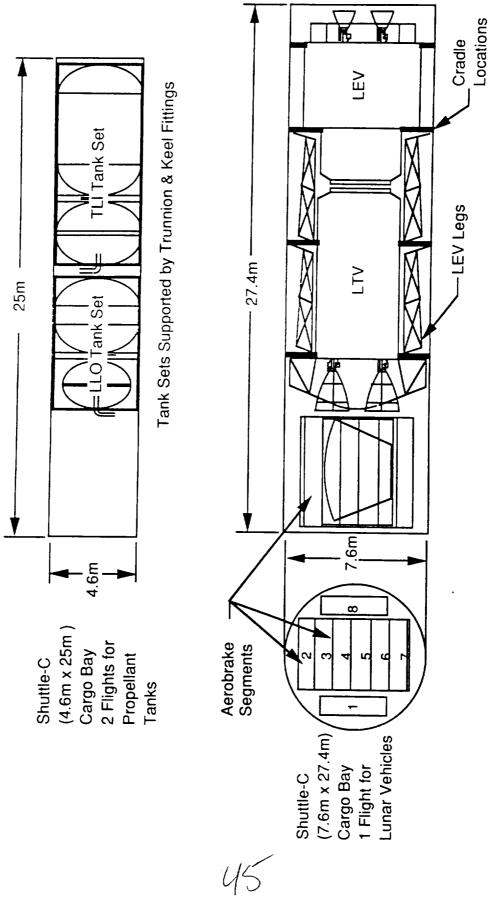
JRH011890-16

The LTV and LEV described in the preceding pages were manifested in the ETO transporation system to determine the number of flights required to Space Station Freedom. The ETO transportation system utilized in the manifest was the Shuttle-C (4.6 m x 25 m cargo bay and 7.6 m by 25 m cargo bay).

The LTV core vehicle and aerobrake outer segments, along with the basic LEV and its detached landing legs require a full Shuttle-C (7.6m x 27.4m) cargo bay for manifesting as shown in Figure 4.0-1. Both the LTV core and LEV will each require two mounting cradles utilizing standard trunnion and keel fittings to secure the payloads in the cargo bay. Special packaging and mounting provisions will be required for the aerobrake outer segments and the LEV landing legs.

The propellant-loaded drop tanksets are packaged in the Shuttle-C (4.6m x 25m) cargo bay. One TLI tankset and one LLO tankset are packaged together in the cargo bay. Two Shuttle-C flights are required to bring all four tanksets to station. Each tankset is supported in the cargo bay using trunnion and keel fittings. Although not volume limited in the Shuttle-C, the weight of the two tanksets pushes the performance limits of the vehicle. Each tankset and the lunar vehicles will also be equipped with handling/grappling fixtures to accommodate transfer from the cargo bay to the station by a cargo transfer or similar vehicle.





STV CONCEPT SELECTION SS FREEDOM ON-ORBIT OPERATIONS EVALUATION

PRELIMINARY DATA

DON BRYANT MDSSC-KSC 6/2/90

44

41

6/2/90

Don Bryant MDSSC-KSC

DESCRIPTION: Multilstage TV & Separate LV - Single Cr	parate		LV - Single Cr			ew Cab	Cab	2		ar 'afaic ion =		_ ۲	= rv, 3A = AUB, 0A	ר ני י	I Cargo, & a II Cr	Cryo lanker/xier system DATE 5/30/90
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48

4E-3A

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METHODOLOGY

- Researched past KSC study reports to establish individual element task timelines and input same into spreadsheets (One for each concept initial flight and if appropriate, steady state/reflight). (See Methodology Illustration, Ref "C") <u>ີ</u>
- Produced timelines for 8 concepts (5 with reflights) based on spreadsheet output data. 6.
- Produced concept comparison charts utilizing spreadsheet data. ۲.
- (TBS) All of the above data is to be evaluated to produce summary charts. æ.

49

Don Bryant MDSSC-KSC

GROUNDRULES AN ASSUMPTIONS

NOTES & OBSERVATIONS:

- Timeline data were derived from the MDSSC-KSC On-Orbit Assembly/Servicing processing times are "KSC Ground equivalent" times and do not have EVA and Task Definition Study GFY 1989 Summary Report of November 1989. All automation enhancements yet incorporated.
- When fully assembled for initial mission , Configurations 3A-3, and 4E-3A&B exceed the presently planned ASF length. •
- When fully assembled, Configurations 4E-2A, 4E-2B, 4E-3A, and 4E-3B have widths that are marginal or greater than planned ASF width.
- TLV refurbishment times could be impacted by lunar dust cleanup. •

GROUNDRULES AN ASSUMPTIONS

GENERAL

- õ SSF resources required to support the timeline are: IVA (2); EVA including cabin atmosphere loss associated with Airlock use; MSC; ASF; DMS; TCS; Power.
 - SSF assembly/refurbishment crew of 4 is baseline.
- The only on-orbit cryo servicing will be for concepts 4E-3A & B steady state missions These missions will be supplied from a tanker that includes an integral propellant transfer system (including displacement gas supply). •
- All other Propellant Tanks are assumed to be delivered full and no top-off capability is required from SSF resources. •
- All cargo is passive and is pre-assembled into single or dual containers when received.
- Advanced OMV will be available to support deployment and retrieval operations. •
- All LVs require on-orbit erection of the cargo platform and installation of (2) filled cryo Propellant Tanks and (4) Landing Legs
- * TLVs require no on-orbit assembly.

GROUNDRULES AL ASSUMPTIONS

SPECIFIC GROUNDRULES (per flight)

3A-2

- LV & TV are mated when delivered to SSF.
- TLV Core/LV will be delivered first, Cargo will be last

3A-3

- LV & LOI Stages are mated when delivered to SSF.
- TLI Stage will be delivered first, Cargo will be last.

3A-5

- TLI Tanks are pre-plumbed to a dual tank type interface when delivered.
- TLV Core requires no on-orbit assembly and will be delivered first , Cargo will be last. •

GROUNDRULES AN ASSUMPTIONS

SPECIFIC GROUNDRULES (per flight) (Cont)

4E-2A,B

 TV Core/Aerobrake/Cargo delivered first - TLI/LOI Tanks Last 4E-3A,B

TLI Stage will be delivered first, - Re-supply Tanker Last (reflights only)

4E-5B

TLV Stage/Aerobrake will be delivered First.

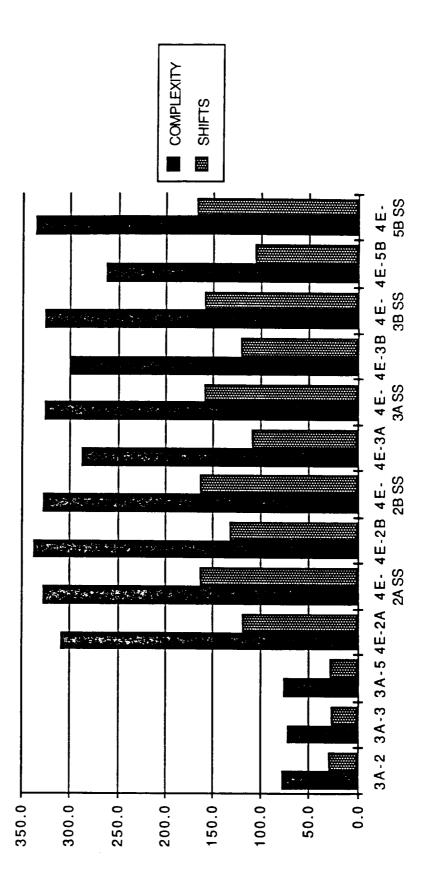
Don Bryant MDSSC-KSC

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COMPARISCIA TABLE

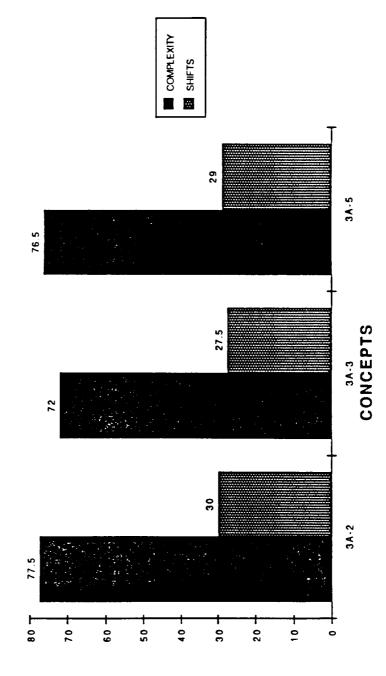
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STV CONCEPT ON-ORBIT OPERATIONS AT SS FREEDOM COMPARISON - OVERVIEW

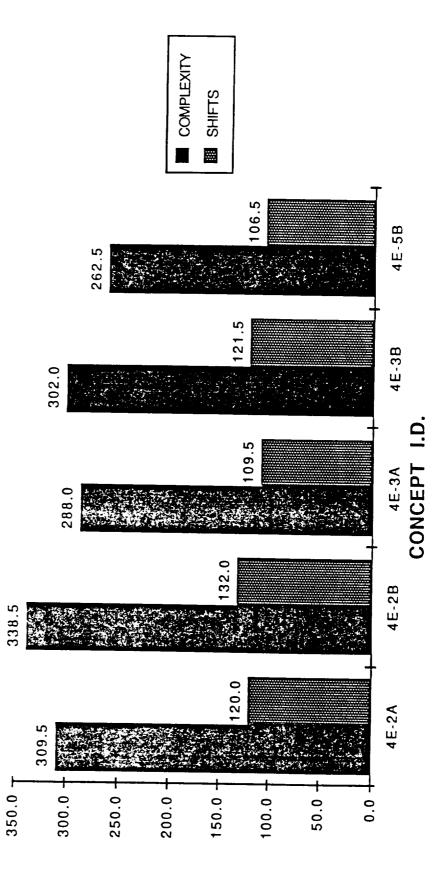




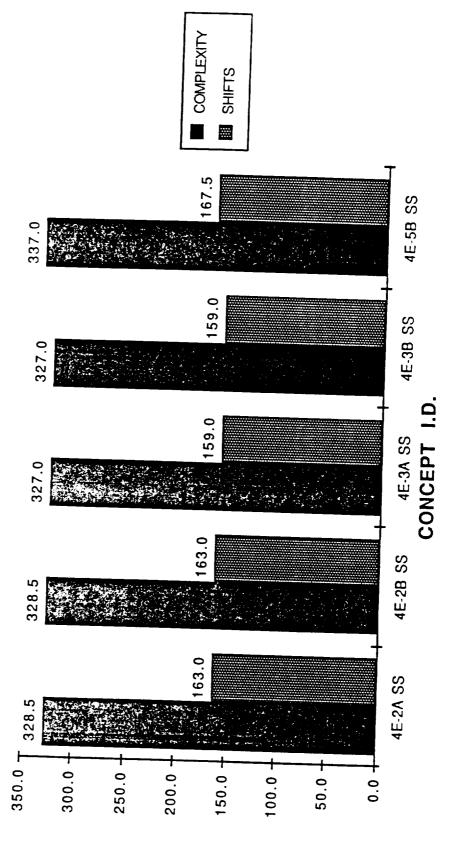
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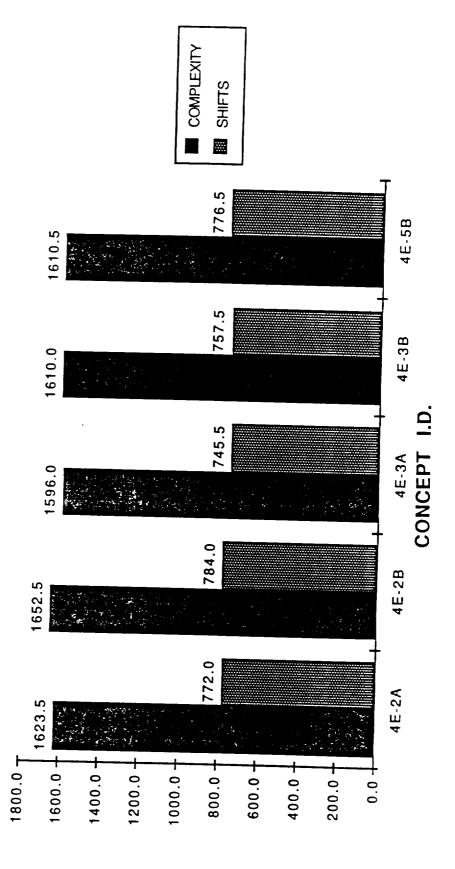
MANNED CONFIGURATIONS -INITIAL LAUNCH COMPARISONS



MANNED CONFIGURATIONS -STEADY STATE COMPARISON



MANNED CONFIGURATIONS -LIFETIME (5 FLIGHT) COMPARISON



BACKUP DATA

CONCEPT #3A-2		ELEA	ELEMENTS	-			CORE,	2 = 1		= TLI TANKS,	3 = L	LV, 7 = CARGO	00				
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3A

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CONCEPT #3A-5		ELEMENTS	AENI		2 = 1	0 8		TANK	= TOI & LOI TANKS, 4A = TI V 7			1 1	CARGO			
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3A_

CONCEPT #4E-2A		ELEI	ELEMENTS	Ts	8	1×.		1 2 1	0 1	ANK	=TV, 2 =TLI & LOI TANKS, 3B	= LV, 5A	5A = A/B, 6A	= CC, 7 =	CARGO		
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4E-2

CONCEPT #4E-2A SS		ELE)	ELEMENTS		18 ⊨]	۲, 2 ۲	יד	- -	1 10	ANKS	3B = L	=TV, 2 =TLI & LOI TANKS, 3B = LV. 5A = A/B. 5A	∕B. 5A =	- N UU			
DESCRIPTION: SINGLE STAGE SEPARATE TV	SEP	ARA	Τ	5e 1	۲ ۲	V/DR	OP T	W/DROP TANKS	ະອັ ເກ	SING	E CRE	SINGLE CREW CABIN			000	DATE 5/30/90	
COMPLEXITY FACTORS				11		11	ESO	RESOURCES	1.	SHIFTS	S		Ú	COMPLEVIEN	191		
CANDIDATE TASK (Select Only As Appropriate)	2 2 2	EVAHMS 18	8	7	N	~	2 5 A	A 6 A	<u> </u>	-		HS	TOTAL	FACTOR	CON	COMMENTS	
Refurbishment Phase Crew Module Refurb					·	 	ļ'	45.0									
Electrical Checkout Fright Servicing	• >		2.0	•	•		1.5		· ·			 	5.0	0,0	45.0		
Aerobrake TPS Repair	< ×			• •	• •	_	<u>`</u> ~			• •			0.0	3.0	24.0		
Subsystem Leak And Functionals ICS Returbishment	× >	•	60	•		· ·			•				0.0	0 0	7.5 18.0		_
Avionics System Verification	< •	• •	6.0	• •			· ·	· ·	• •				6.0	3 0 1.0	18.0 6.0		
Hardware Delivery Phase Delivery Vehicle Ottoading Receiving Inspection	•••	××		0.0		1.0 1.0		<u> </u>	0.5	0.5	 		5.0	20	10.0		
Assessment of the post of the	×	_	1.5			· ·		•	, 				1.5	2.0	7.5		
Assembly Element Assembly STV Assembly	**	**		, u	, u		<u> </u>	·	· ;			0	2 0	5.0	0.0		
Verification Phase	-	,	-+	_			_	·	2	o. -			8.0	5.0	40.0		
Interface Vertication Integrated Vehicle Test			1.0	1.0 1.	1.0 1.0	0 1.0 5 0.5		2.0	•••	• •		44	4 C 0 C	0.0	4.0		
Maie & Berthing Test				· ·	<u>.</u>	•	_	•						2.0	0.0		
Cryo Servicing	-			<u>-</u> -	<u>.</u>	•	•	,		•		o	0	2.0	0.0		
Correction Disease	-+	\neg	-+		•	_		,	•	•		000		2.0	0.0		
Fluids Top Off Vehicle Closeout				<u> </u>						4		4	0	1.0	4.0		
0	×		· ·	· ·	• •				• •	0.5		4.0	<u> </u>	0.0	40		
aunch Bhasa		-+	-		-		·			c	_	06	<u>~</u>	0	0.5		
Countdown Operations												2.5	5	2.0	5.0		
De-Integration Phase Post Flicht Insuestion	+	+		+		_				+		~					
		₩ -	4.0		• •	• •	2.0	2.0				33.0		0.0	0 60		
Crew Module/Return Cargo Destow		-	• •	·			•	0.6	•	,		9.0		0. •	0.6		
									GRA	L ON	GRAND TOTALS	163.0	0	B/U	328.5		

4E-2A

CONCEPT #4E-2B		ELEMENTS	MEN	TS	18 =	2	= T	=TV, 2 =TLI & LOI TANKS, 3B	ō	LANK	C 'S	8 = [= LV, 5A	A = A/B, 6B	= TVCC. 6C	= LVCC. 7 = CAI	CABGO
DESCRIPTION SINGLE STAGE SEPARATE TV	ESE	PARA	TET	•8 ≥	2	W/DF	PP	W/DHOP TANKS	S S	'na	AL C	REW	DUAL CREW CABIN	Z		I I	DATE 5/30/90
COMPLEXITY FACTORS							JESC	1 m	ES .	SHI	FTS				COMPLEXITY		COMMENTS
CANDIDATE TASK (Sicked Only As Apyrepriate)	EVA	EVARMS 18	18	2	5	~ ~	2 3	38 5	A 16	5A 6B 6C	2 2	<u>-</u>		TOTAL	FACTOR	СОМ	
Refurbishment Phase Crew Modulo Refurb Leschical Checkout Engine Survicing Aurdarako EPS Repair Sutasydom Lasak And Lunctionala						· · · · · · · · · · · · · · · · · · ·			<u> </u>			·		00000	00000	00000	
ICS Retrativition										<u></u>			k	000		00	
Hardware Delivery Phase Delivery Vehicle Offloading Receiving Inspection Installation at Temporary Location	· · ×	×××	10 15	100	1.0	101	0 2	00	0.5	· · · ·	00	505		855 855 195	2 0 2 0 2 0	17.0 17.0 12.5	To ASF Assy Fixt. for 113 & ITA for 5A
Assembly Phase Element Assembly STV Assembly	××	××		1.5	1.5	- 1.5	- 4	0 11.0	0		· •	1.0		15.0 10.0 25.0	5.0	75.0 50.0	
Verilication Phase Interface Verification Integrated Vehicle Test Mate & Berthing Test			10.1	1.0	1.0 1	101	0.0	2.0	217	0.0	1	1.0		6.0 8.0 7.0 21.0	1.0 2.0 2.0	6.0 8.0 14.0	
Propellant Servicing Phase Cryo Top Oli Cryo Top Oli									· ·		ļ · ·	, ,		0.0	2.0	0.0	
closeout Phase Fluids Top-Oil Vehicle Closeout Crew Ingress Pre Deployment C/O	×								4400	0 4.0 0 4.0 5 0.5	0.019.9			8.0 8.0 1.0 1.0 1.0	0 0 0 0 0 0 0 0	80 90 10 10 10 10 10	
Launch Phase Counidown Operations										<u> </u>	<u> </u>			2.5	2.0	5.0	Requires OMV
De-Integration Phase Post Flight Inspection Propellant Residual Drain Crew Module/Return Cargo Destow	×	×	29 4.0	• • •										33.0 4.0 46.0	3.0 2.0 1.0	0.0 0.0 0.6	
									U U	GRAND		TOTALS		132.0	N/A	338.5	

4E-\

CONCEPT #4E-2B SS		ELEMENTS	(EN)		18 =T	۲, 2 ۲	IL I	 *	0 1	TV, 2 =TLI & LOI TANKS, 3B	, 38 = L	= LV, 5A = A/B, 5A		CC, 6B = TVCC, 6C = LVCC, 7 = CARGO	. 7 = CARGO
DESCRIPTION: SINGLE STAGE SEPARATE TV	SEPAF	ATE		۲ ۲	& LV W/DROP TANKS &	ROP	TAN	KS 8	DO	AL CI	DUAL CREW CABIN	BIN			DATE 5/31/90
COMPLEXITY FACTORS					11	1 1	S	JACE		· SHIFTS	S		COMPLEXITY	TASK	COMMENTS
CANDIDATE TASK (Select Only As Appropriate)	EVA	EVARMS	8 -	7	2	5	2 5 A	A 6B	2 1	4		TOTAL SHIFTS	FACTOR	COMPLEXITY	
Refurblshment Phase Crew Module Refurb	•	•						45		,		45.0	-		
Electrical Checkout Envine Servicing	• >	•	2.0	•			-		•	•		3.5	0.0	3.5	
Langue Servicing Aerobrake TPS Repair	< ×		D. ,		•		<u>_</u>	•••	• •	, ,		250	0.0	24.0	
Subsystem Leak And Functionals	×:	•	6.0	,				'	•	1		6.0	3.0	18.0	
Avionics System Verification	K •		6.0		• •	• •	· ·	• •		• •		6 0 9	3.0	18.0 6.0	
Hardware Delivery Dhees		Ť	╋	+	+	+	+	\downarrow	_			77.0			
Delivery Vehicle Offloading	1	×	,	_	1.0	1.0 1.0			0.5	0.5		5.0	2.0	10.0	
Receiving Inspection Installation at Terrowary I creation	• >	× >		1.0	_		0	•				0,14	0.0	10.0	
	<u>،</u>	¢	2						•	•		11.5	0.0	¢. /	
Assembly Phase Flement Assembly			•	,					<u> </u>				2	0	
STV Assembly	×	×		1.5 1	1.5 1.	1.5 1.5	5	•	1.0	1.0		8.0	2.0	40.0	
			┥	╉	+	+	-		\downarrow			8.0			
Verrication Prase Interface Verification					_	-						4	0	4	
Integrated Vehicle Test			1.0	0.5 0	0.5 0	0.5 0.	, 10	2.0	•	•		2.0	0	0.5	
Mate & Berthing Test			•	•	•	•		•	•	•		0.0	2.0	0.0	
Propellant Servicing Phase			† .	1.	$\frac{1}{1}$	╋	+	┿	ŀ	ŀ	T) n			
Cryo Servicing			•	•		•	<u>'</u>	1	•	•		0.0	50	0.0	
												0.0		0.0	
Closeout Phase			-						<u> </u>						
						••• •••		4 4	• •	• •	_	0.0	0.1	4 4	
Crew Ingress	×	_					•		_	•		0.5	10	0.5	
Pre Deployment C/O					•	•				•		0.5 9.0	1.0	0.5	
Launch Phase Countdown Operations							<u> </u>					25	0.0	4	
				\dashv	-	-	-					2.5		2	
De-Integration Phase Post Flight Inspection	×	×	29		· ·	•	2.0	2.0		•		33.0	3.0	0.66	
Propellant Residual Drain	•		4.0		· ·		•		'	•		40	2.0	0.0	
			•	,	,		•	ר. ה		,		46.0	<u>-</u>	ה. מ	
						SRA	GRAND TOTALS	OTAL	Ś			163.0	N/A	328.5	

4E-2B

CONCEPT #4E-3A		ELEN	ELEMENTS: 1c	5: tc		= TLI Stage, 1E	ge, 1		= LOI Stage, 3B	tage,	38	ר, בי	5A = A/B, 6A	= CC, 7 =	Cargo		
DESCRIPTION: Multistage TV & Separate LV	arate		- Sh	Single Crew Cab	rew	Cab								 • •	6 D	DATE 5/30/90	
COMPLEXITY FACTORS				1 1			RESOURCES	JRCE	$ \cdot $	SHIFTS	S			COMPLEXITY	N ASK	<u>ronuente</u>	
CANDIDATE TASK (Select Only As Appropriate)	Ε<	EVAHMS	2	ш Н	38	5A 6	6 A 7.0 7.0	0 2.					TOTAL SHIFTS	FACTOR	CON		
Refurbishment Phase Crew Modula Raturb								ļ		1							
Electrical Checkout	• •						• •	•					0	-	0		
Engine Servicing	,	•	,	•	,			, ,	_				00		00		
Aeroorake LPS Hepair Subsystem Leak And Functionals			•		,		<u>.</u>			<u> </u>			0) m	00		
1CS Returbishment	•		• •					• •					0 0	e) (0		
Avionics System Verification	•	•	,	,	,		•	•				<u>.</u>			00		
Hardware Delivery Phase Delivery Vehicle Ottheration	T	1	<u> </u>	+		+	<u> </u>	+		+	+	+	>				
Receiving Inspection		××	<u>, 0</u>	1.5 2		, , 10, 10,	0.5	0.0			<u>.</u>		6.5	~ ~	13		
Installation at Temporary Location	×			2.0			j						0 0 0	N IS	55		
Assembly Phase	╎	T	\dagger	+	╀	+	+	\downarrow	Ţ	╉	╉	-	-+ 				
Element Assembly STV Assembly	* >	* >		, c 4 c	0,0	11.0		_	<u> </u>				15	4	60		
	<	<			2	•	-	D.					9	ŝ	30		
Verification Phase Interface Verification							Ļ			\vdash	╞	<u> </u>					
Integrated Volucie Test			0	10.1	0	- ~	, , , ,	• •	_				4 10		4 v		
Maie & Berlinng lesi				•		0	0 1.0	1.0					5	6	<u>, 6</u>		
Propellant Servicing Phase	1-		\vdash		-	┼	╂—			+	+-	\downarrow	2				
Cryo Tap Olf			, ,		· ·	· ·					_		0 0	~ ~	00		
Closeout Phase	+	\uparrow	+	╉	+	+	_			+	+	\square	0	•	>		
I huids Top OII						4							4				
Vehicle Closuoti	,					4						_	4	. –	শ		
nt c/o	<	_		· ·	· ·	0.5	• •	• •					0.5		0.5		
			+	\dashv		-				_			6		n D		
Countdown Operations													2 6				
		-		-		_					_		5.5	N	n		
Post Flight Inspection	×	×	, 20	29.0	0 0				-				;				
				4.0	<u>;</u>	_		• •					ۍ ۲	- 	66 a		
Crew Module/Return Cargo Destow				•	' 	0.6	•	•					6) o n		
	\mathbf{I}	1	$\left \right $	$\left \right $]	GRAND TOTALS	6	DTAT	5	40	a/u	206		
											-	, ,			007		

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CONCEPT # 4E-3A SS		ELEN	ELEMENTS:	-		LI SI	= TLI Stage, 1E		ē	= LOI Stage, 3B		= LV. 5A	= A/B	9 = CC 2 = 9		Tanker/Vier autom
DESCRIPTION: Multistage TV & Set	parate	Separate LV -	Sing	Single C	crew Cab	Cab				1		•		 - - - - -		DATE 5/30/90
COMPLEXITY FACTORS							SOU	ACE	S - S	RESOURCES - SHIFTS				COMPLEXITY		In AURENTE
CANDIDATE TASK (Scienti Only As Appropriate)	E < P	EVARMS 1C 1E	10		38 5	5A 6/	6A 7.0 7.0 8.0	0.70	0.0				TOTAL SHIFTS	FACTOR	00	
Refurblshment Phase Crow Modulo Refurb Li loctrical Checkour Engine Survicing Aerobrake TPS Repair Subsystem Loak And Functionals	***			20 80	~ N	- 45.0 1.5 2.5	0						م 2 5 5 5 5		45 35 24 18 18	
rest returnsamment Avionics System Vertification	×					, , , ,	• •	• •					6 6 7		18 6	
Installation of the second of	×	×××	15	2.0			0.5	0.5	1.0 1.0 1.5				3.5 3 12	20 20 20	7 6 27.5	Roturning LOf stage at ASF for returb then move to LTA during TLI stage arivat
Assembly Prase Lloment Assembly STV Assembly	××	××		0,1	· ·	• •	1.0	1.0	2.0				o vo o	4 10	0 25	Tanker VF connection
Verification Phase Interface Verification Integrated Vehicle Test Male & Berthing Test			· · · ·	00	· · · ·	5.0							- 4 O W		-40	
Propellant Servicing Phase Cryo Top Ott Cryo Top Ott			- S 	2.0		• •		• •			<u> </u>		~ ~ ~ ~	20	₹0	
Lioseout Phase Fluids Top-Off Vehicle Closeout Crew Ingress Pre Deployment C/O	×					4.0	• • • •		0.5				4 4 0 0 0 2 2 2 2 2		4 4 0 0 10 10 0	Tanker disconnect
Launch Phase Countdown Operations De Internation Phase			╏───┤	┠──┤	┨───┨				╏──┤	┼──┤			2.5 2.5	2	S	
Post Flight Inspection Propellant Resident Drain Crew Module/Return Cargo Destow	×	×		# 4 # 0, 1	2.0	9.0	• • •	• • •					4 0 4 33 46	60 F	6 6 8 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8	
									GRAN	0 1	GRAND TOTALS		159	8/U	327	

4E-3Å

CONCEPT #4E-3B		ELEM	ELEMENTS: 1c	3: 1c	п	TLI Stage, 1E	ige,		[0]	= LOI Stage, 3B	38 =	LV, 5A	A = A/B, 6B	= cc, 6c =	CC, 7 = Cargo		
DESCRIPTION: Multistage TV & Separate LV - Dual Crew	Irate	י -	Dual	I Cre		Cabs										DATE 5/30/90	
COMPLEXITY FACTORS CANDIDATE TASK (Select Only As Appropriate)	EVA	EVARMS 1 C		15	38	5A 6	RESOURCES	URCI C 7.	0URCES - 5	· SHIFTS	s		TOTAL SHIFTS	COMPLEXITY FACTOR	COMPLEXITY	COMMENTS	
Refurbishment Phase Crew Module Refurb Flectrical Checkouf Engino Servicing Aurodarako 11'S Repatr Subsystem Leak And Functionals ICS Refurbishment Avionics System Verification													0000000				
Hardware Dellvery Phase Delivery Vehicle Offoading Receiving Inspection Installation at Temporary Location	· · ×	×××	1.5	2002	100	0.5	1 1 1		5 0.5				5 5 5 0	~~~~	52 I I I		
Assembly Phase Element Assembly STV Assembly	××	**		5.0	2.0 1	11.0		<u> </u>	· •			ļ	15 8 21	- 4 10	30 60		
Verification Phase Interface Verification Integrated Vehicle Test Mate & Berthing Test	<u> </u>		, 0, ,	0.0	2.0	0.10	0 2 0		· · · ·				6 r r r		6 / 4		T
Propellant Servicing Phase Cryo Servicing Cryo Top Ott							<u> </u>	· ·	· ·	ļ	<u> </u>			~~~	00		
Closeout Phase I hinds Top Off Vehicle Closeout Crew Ingress Pre Deployment C/O	×					4400	4 0 0 5 0 4 4 0 0 5 0 0 5 0 4 0						∞ ∞ -		œ œ - -		
Launch Phase Countdown Operations													2.5 2.5	2	م.		
De-Integration Phase Post Flight Inspection Propellant Residual Drain Crow Module/Roturn Cargo Destow	×	×		29.0 4.0	• • •	2.0 2.	2.0	• • •					33 4 46	- 53	δ δ α α		
	1	1	1	1	1		$\left\{ \right.$		GF F	GRAND TOTALS	NOTAL N	L s	121.5	8/U	302]

4E-3

CONCEPT # 4E-3A SS ELEMENTS: 1C : DESCRIPTION: Multistage TV & Separate LV - Dual Crew	r ate	ELEMENTS: 1C LV - Dual Crew	ENTS Dual	1. 1C		TLI Stage, 1E Cabs	ge, 1		= LOi Stage, 5A = A	A/B, 6B = CC, 7	r = Cargo, & B		Cryo Tanker/Transfer System	
COMPLEXITY FACTORS CANDIDATE TASK (Select Only As Appropriate)	EVA		1 C	RESOURCES - SHIFTS C 1 E 5 A 6 B 7.0 7.0	A 6	68 - SH	411F 7 5 0 7. C	SHIFTS 7.0 7.0 8.0		TOTAL	COMPLEXITY FACTOR	TASK COMPLEXITY	COMMENTS	
Refurbishment Phase Crew Module Relurb Electional Charterat		•	· ·		45					45		45		
Engine Servicing Aerobrake TPS Repair	××	•••		_				· · · ·	<u>.</u>	2 8 2 2 8 5	- e e	2.5 7.5		
Subsystem Leak And Functionals LCS Refurbishment Avionics System Verification	***	• • •		6.0		• • •	• • •			992	n n -	6 18 6 18		
Hardware Dollvery Phase Delivery Vehicle Ottloading Receiving Inspection Installation at Temporary Location	×	×××	2.05	5.0		0.5	5 0.5	100		3.5 3.5 1.7	2 5 5	7 6 27.5		
Assembly Phase Element Assembly STV Assembly	××	××		. 0.		-	, 1 .0	2.0		0 0 0	4 10	0 25	Cryo Tanker I/F connect	
Verification Phase Interface Verification Integrated Vehicle Test Mate & Berthing Test			• • •	100	2.0					- 4 0 4	0	- 40		
Propellant Servicing Phase Cryo Servicing Cryo Top Ott				2.0	•••		· ·			~ ~ ~ ~	5 5	40		
Closeout Phase Fluids Top Off Vehicle Closeout Crow Ingress Pre Deployment C/O	×				4400	0055 00				4 4 0 0 0 4 N N N N		4 4 0 5 0 5 0 5	Tanker Disconnect	
Launch Phase Countdown Operations				1						25 25	2	S		
De-Integration Phase Post Flight Inspection Propollunt Residual Drain Crew Module/Neturn Cargo Destow	×	×	· · ·	29.0 2	2 0 2.0		• • •			9 4 0 4 6 9 4 6	e v -	66 8 6		
								GR	GRAND TOTALS		N/A	327		

4E-36

Page 1

CONCEPT # 4E-5B		ELEJ	ELEMENTS	+	2 = TLM	LMC	J Tar	LOI Tanks, 2B	1 11	A/B	Tank	3, 4E	A/B Tanks, 4B = TLV, 5B	۲۷. ۵	18 = A/8, 6D	= C.C 7 =	Cargo		
DESCRIPTION: Single Propulsion Stage		Combined Vehicle w/	blned	l Vel	hcle		l qo'	Drop Tanks								-	b	DATE 5/30/90	
COMPLEXITY FACTORS									sout	RESOURCES		· SHIFTS	s			ICOMPLEXITY	TASK	COMMENTS	T
CANDIDATE TASK (Select Only As Appropriate)	EVA	EVARMS	N	5	5	2 2	2 A 2 A		4B 5B 6D	6 D	~	~	 		TOTAL	FACTOR	CON		
Refurbishment Phase Grew Modulo Refurb Liscringut Checkout Engine Servicing Aerchrake LPS Reputir			<u> </u>												0000		0000		1
Hardware Delivery Phase Delivery Vuhicle Offloading Receiving Inspection Installation at Temporary Location	×	×××	00.	00,	1 1 1	1.0 0.5 1.0 0.5	505	1.0	0.5 0.5	,	0.5 0.5 -	0.5			7.5 7.5 1.5 16.5	~~~~~	15 15 7.5		
Assembly Phase Licmont Assembly STV Assembly	××	××	. 2	1.5	15	15 10	0 1.0		6.5 1.0	• •	. 1.0	1.0			8.5 9 17.5		34 45		1
Verification Phase Interface Verification Integrated Vehicle Test Mate & Berthing Test			1.0 1	1.0 1 0.5 0	1.0 1.	1.0 1.0 0.5 -	0, , ,	3.0	1.0	2.0					3 6 7	0	66 7	Demate/mate to A/B	
Propellant Servicing Phase Cryo Top Ott Cryo Top Ott			· · ·				<u> </u>		1 1	• •	• •		<u>├</u>		000	0 N	00		
croseout Prase Fluids Top-Off Crewing Clossout Crew Ingress Pre Deployment C/O			• • • •		• • • •	· · · · ·	· · · ·	• • • •		4.0					9 2 4 4 0 5 5 5		4 4 0.5 5.5		
Launch Phase Countdown Operations			╞──┨			├							┟──┤	├──-┨	2.5 2.5	5	5		1
Verintegration Frase Post Flight Inspection Propellant Residual Drain Crew Module/Return Cargo Destow	×	×			· · · ·	·• ·	•••	29.0	10	2.0					32 9 45	ю о -	9 & O		
							ļ	ļ]	Ĭ	GRA		GRAND TOTALS	S	106.5	N/A	262.5		7

4E-5

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Page 1

CONCEPT #4E-5B SS ELEMENTS: 2 = TLI/LOI Ta DFSCRIPTION Single Propulsion Stage Combined Vehicle w/Drop	ш ў	ELEMENTS: 2 Combined Veh	ENTS: Jed V	: 2 = Vehic	= TLI/LOI icle w/Dr	Drop	Tanks, 2A p Tanks		= A/B		A/B Tanks, 4B		= TLV, 5B	B = A/B, 6D	6D = CC,	., 7 = Cargo		DATE 5/30/90
								RESOURCES	URC	ES -	SHIFTS	FTS			C	COMPLEXITY		COMMENTS
FACTURS	EVAR	EVARMS2.02.02.02.02	2.02	.0 2	02	0 2 4	2 A	4 B	58 6D			0		SH SH	TOTAL SHIFTS	FACTOR	COMPLEXITY	
Select Unit As Aparopriate			+	┼-	_	<u> </u>												
Refurbishment Phase	,		•		•					45.0					45		45	 Simolilied Aerobrake
Crew module regula	,	•	•	•		•	•	2.0	1.0	•	,					- 6	24	
Engine Servicing	* *	•			· ·	• •		0.8	1.5						5.1) m	4 5	Simplified Aerobrake
Aerobrake TPS Nepair Subsystem Leak And Functionals TCS floturbishment Avtenucs System Vertificution	(××·	•••			· · · ·			6.0 6.0							6 6 5.5	n n -	م 29 م	
Hardware Delivery Phase Delivery Vehicle Offbading Receiving Inspection Installation at Temporary Location	· · ×	×××	0.0	1.0	1.0 1.0	0 0 2	0.5	· . 1.5			0.5.0	0.5			6 6 1.5 1.5	200	12 12 7.5	
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Crew Module/Return Cargo Destow												GRA	GRAND TOTAL	Ш	45 167.5	N/A	337	

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Page 1

STV/LTS Phase II On-Orbit Operation Evaluations

Overall Assumptions - All Configurations

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		Overall Assumptions - All Configurations (Cont)
	J	 Control and monitoring of the A/B functions is through a single ASF to A/B umbilical The umbilical is designed to permit a minimum A/B rotation of 315 degrees while connected
-		It is highly desirable to maintain ASF Doors and Segments closed during assembly operations to protect the aerobrake from micrometeorite/debris damage and a constantly changing thermal environment.
		ASF Doors and Segments must remain open during all periods when the SSRMS supports A/B assembly
		Wher (PDG
		 ASF may be closed during SPDM only assembly Special end effectors as required to support assembly will be stored on the SPDM body pre-task
2		Special adapter OSE structures are provided as required to attach A/B elements to the MSC for transportation.
7		All A/B configurations have a special passive female adapter at their forward (TPS) center to interface with the Assembly and Servicing Facility (ASF) Aerobrake Assembly and attach Fixture (AAF) active probe
		Closeout of this AB/AAF adapter TPS discontinuity is not timelined
Ĺ	C	 Indicates that this assumption is also a recomendation

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A grapple fixture is located on the aft (structure) side of every aerobrake segment 7

The launch carrier vehicle is docked at the SSF ITA with cargo doors open prior to timeline start

GRIGINAL PACE IS OF POOR QUALITY

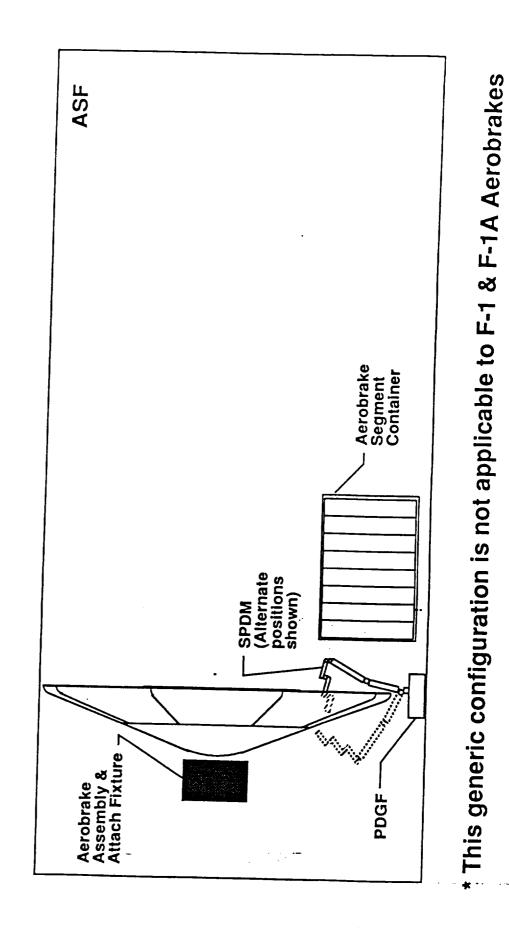


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Overall Assumptions - All Configurations (Cont) In order to make direct one to one comparisons between all configuration scenarios, the following MSFC Rigid A/B Groundrules and Assumptions have been adopted for all scenarios	Turntable will hold the aerobrake to facilitate robotic assembly with only one RMS. Assembly operations are limited to available SSF robotic capabilities. RMS maneuvers not limited by hanger.	Note: "Hanger" is assumed to be the Assembly and Servicing Facility (ASF) without Mobile Manipulators. The "Turntable" is assumed to be the ASF Aerobrake Assembly And Attach Fixture without any robotic capabilities.	Crew. robotic arm , lights, cameras, etc. are in place on SSF and ready for assembly operations.	 Aerobrake segments are stored where the robotic arm can grapple each one and assemble it without translation. 	EVA required for backup of all robotic tasks, but will be used for contingency only	Segment design should consider tolerance buildup and loading for space environment		
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Recommendations - All Configurations

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Recommendations - All Configurations	orporate all checked (sign AAAF as a specia Provide AAAF with g multiple TV cameras in a single rotation/p Provide at least one assembly and to free	Develop AAAF to A/B interface to minimize TPS closeout after disconnect	-KSC 11/30/90
	Design Design Design Design a	Develo	NDSSC-KSC
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MMC R-2 Aerobrake Assembly Timeline

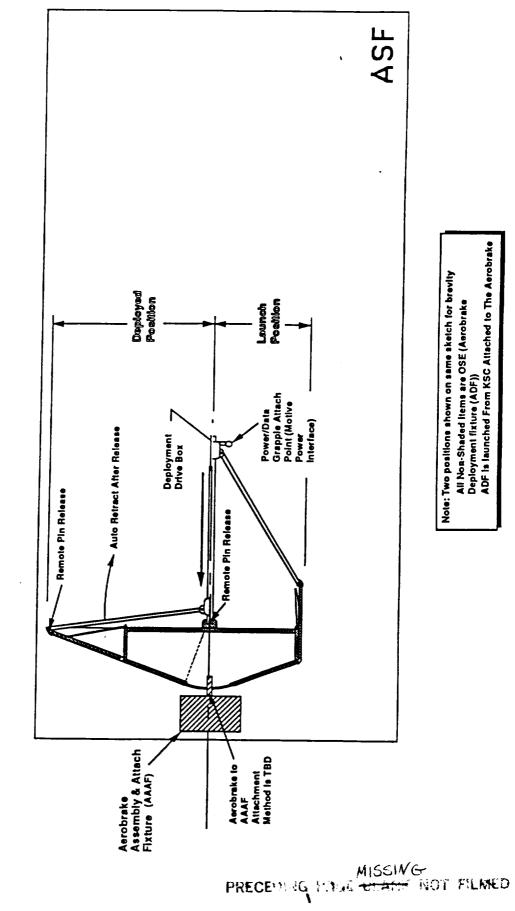
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110 Aerobrake Side Section #2 TPS Closeout Installation (12.9 Hrs.) Aerobrake Side Section #1 TPS Closeout Installation (13.0Hrs.) (58.5 Total Hrs.) Aerobrake Side Section #2 Installation (2.2Hrs.) 🔉 Aerobrake Side Section #1 Installation (2.1 Hrs.) HOURS Final Securing (1.5 Hrs.) 📓 Final TPS Inspection (18.5 Hrs.) Aerobrake Unprotected By ASF (23.7 Hrs. Total) (19.2 Hrs.) Receive Aerobrake in ASF (4.8 Hrs.) MSC Preparations (3.5 Hrs.) ASF Closure (0.5 Hrs.) (4.5 Hrs.) 0

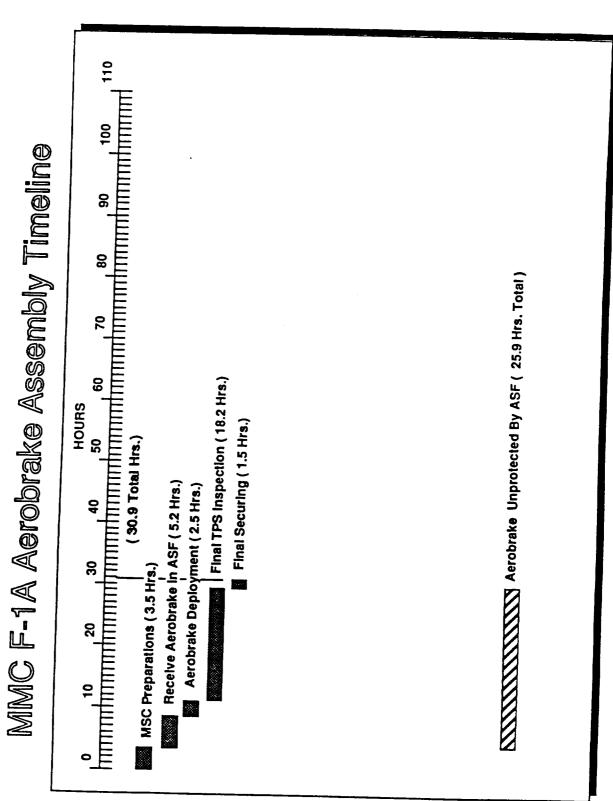
MMC R-3 Aerobrake Assembly Timeline

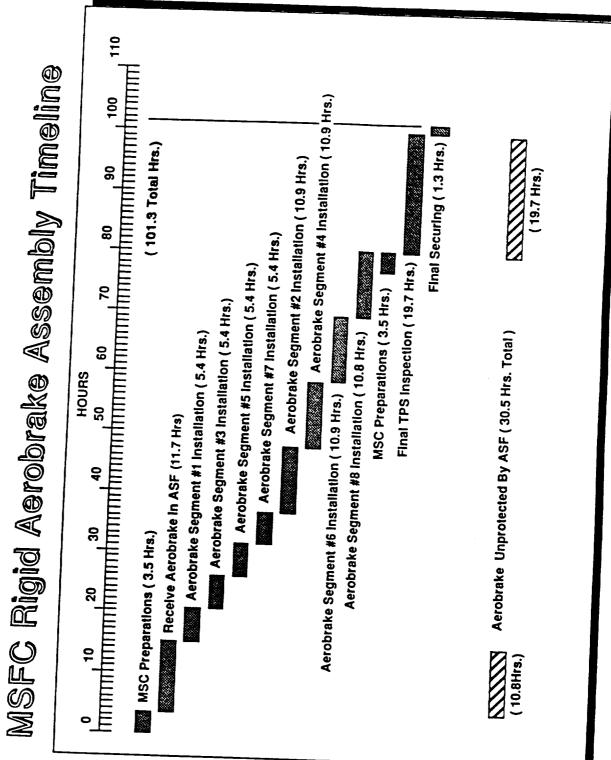
110 MMC F-1 Aerobrake Assembly Timeline Aerobrake Unprotected By ASF (30.8 Hrs. Total) Final TPS Inspection (18.2 Hrs.) Final Securing (1.5 Hrs.) (35.9 Total Hrs.) Aerobrake Deployment (7.3 Hrs.) Receive Aerobrake in ASF (5.4 Hrs.) MSC Preparations (3.5 Hrs.)

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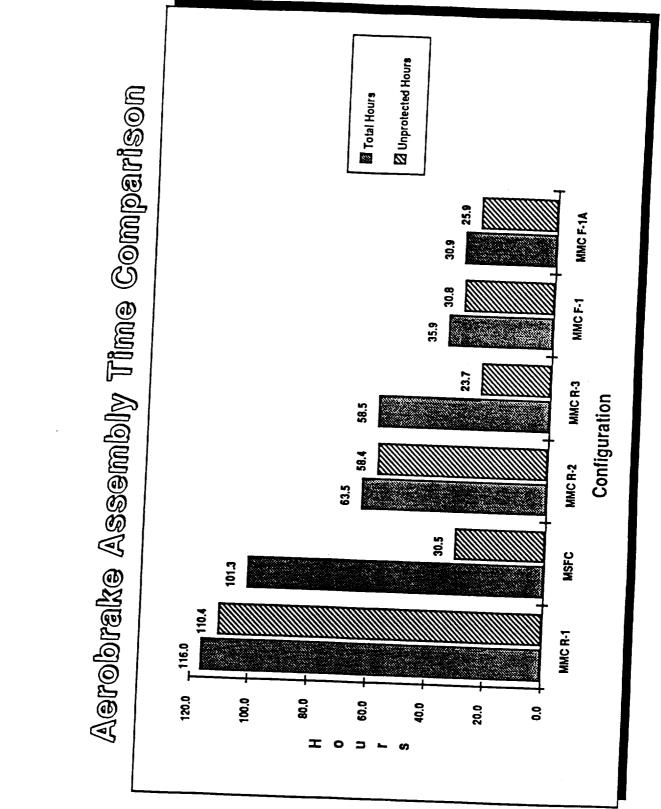
Configuration F-1A OSE





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MMC R-1 AGrobraka Assembly Timelline Immutium Immut	Final Securing (1.9 Hrs.)
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Conclusions	The preceding Assembly Timeline Comparison chart reiterates:	The MMC R-1 configuration requires the most on-orbit assembly time	 The MSFC Rigid option takes_Athe greatest amount of on-orbit assembly time, but: The long duration tasks are good automation candidates This is possibly the lowest risk option 	Addition of robotics capabilities to the ASF could reduce already low A/B exposure time	The MMC R-2 configuration represents a considerable improvement from an assembly timeline standpoint but exposure time is still high due to the need to support sections with the SSRMS while making actual attachment connections with the SPDM	The MMC R-3 configuration assembly time is only reduced by 8 percent compared to R-2 but the exposure time is reduced by 96 percent.	This option appears to have the greatest potential for minimizing operations complexity and risk due to its overall simplicity and minimum number of parts to be manipulated on-orbit
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43

 Conclusions (Cont) On-orbit assembly time for the MMC F-1 option is next to the lowest of all options but: This option presents the greatest risk due to: This option presents the greatest risk due to: Deployment mechanism complexity Supporting OSE complexity Operational complexity associated with OSE to flight hardware interface mate on-orbit Suggested Improvements would not appreciably reduce the risk associated with flight mechanism complexity On-orbit assembly time for the MMC E-1 doption is the lowest of all options but: 	flight hardware interfaces.
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STV/LTS Network Logic Derived Schedules

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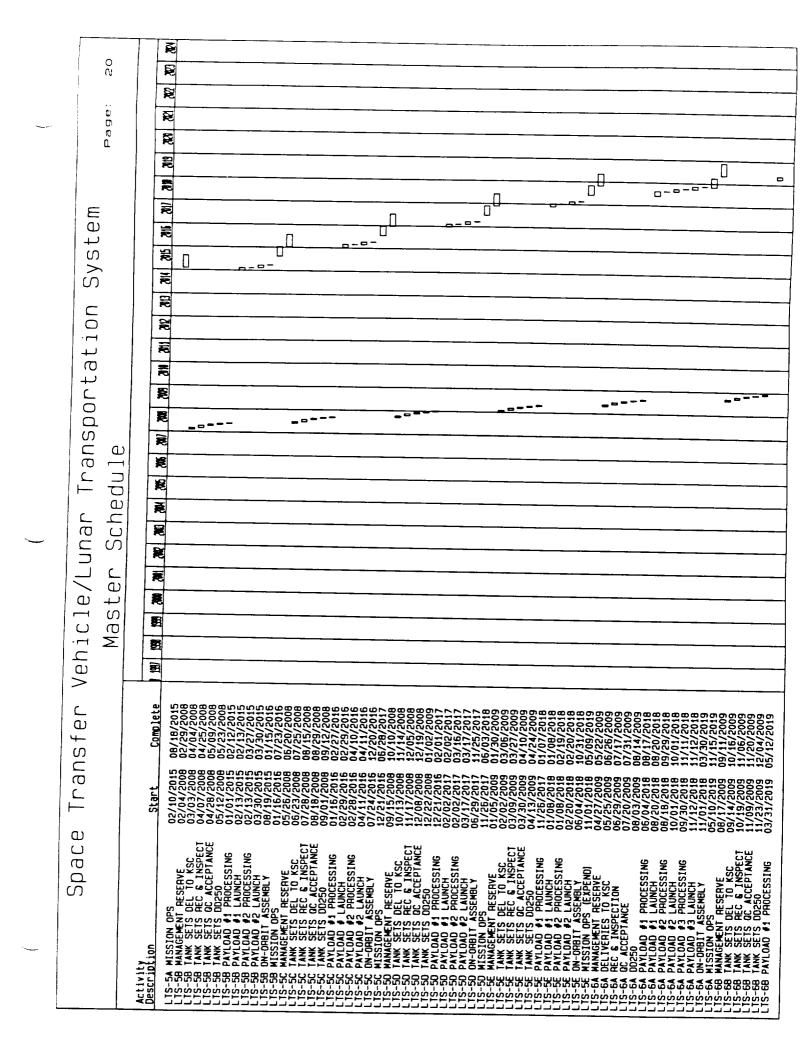
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Space	Transfer	Vehicle/Lunar Transportation System Master Schedule	0 0 :
Activity Description	Start Complete		
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HUMAN FACTORS HUMAN FACTORS PROGRAM	10/02/1997 06/30/2023		
VALUE ENGINEERING Value Engineering Program	10/02/1997 06/30/2023		
ENGINEERING ECONOMIC ANALYSIS Engineering Economic Analysis	10/02/1997 06/30/2023		
<i>Safety</i> Safety program	10/02/1997 06/30/2023		
<i>RELIABILITY</i> RELIABILITY PROGRAM	10/02/1997 05/30/2023		
MAINTAINABILITY MAINTAINABILITY PROGRAM	10/02/1997 05/30/2023		
<i>guality assuranc</i> e Quality assurance program	10/02/1997 05/30/2023		
PROGRAM ADWINISTRATION PROGRAM ADMINISTRATION	10/02/1997 05/30/2023		
PROCATAM PLANNING & CONTROL PROGRAM PLANNING & CONTROL	10/02/1997 06/30/2023		
CONTRACTS ADMINISTRATION CONTRACTS ADMINISTRATION	E202/06/30 /06/2023		
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Space	Transfer	Vehicle/Lunar Transportation System	Page: 2	n N
		Master Schedule		
Activity Description	Start Complete		222 222 223	R.
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MANUFACTURING ENGINEERING	10/02/199/ 05/30/2023			
support management support management	10/02/1997 06/30/2023			
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<i>Configuration Management</i> Data Management Configuration Management	10/02/1997 06/30/2023 10/02/1997 06/30/2023			
DATA MAMAGEMENT FINANCE MANAGEMENT	10/02/1997 06/30/2023			
SUBCONTPACT MANAGEMENT SUBCONTRACT MANAGEMENT	10/02/1997 06/30/2023			